

1402

Perry Dr. et al.

BASIS

FIELD BOOK

No. 385F

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

16-1-23
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Perry Dr.	54 th to Fairmont	1-5
UNION St.	N. of Walnut	6-8
Perry Dr.		9-16
Santa Barbara	Cape May to Valtair	17-18
Pentucket St	Juniper to Ravenna Park	19-35
Nashington	5 to 8	36-50
Commonwealth Ave	Ivy to Juniper	51
Hendricks Ave	Richmond to Normal	52
Duncan Add.		53
62 ND	Imperial Ave. to Bridge	54-60
64 TH	Akins	61-63
J.M.'s	Imperial Ave @ Encanto	64
54 TH Extension	Mission Valley Rd.	65-71
62 ND	Akins to Brooklyn	72-78
Udal	N. of Rosecrans	79-

7/2/30
London

Location Perry Drive From 54th St Ext. to Farmort.

0+00

1+00

1+46⁰² B.C.

$\Delta = 8^{\circ}23'45'' L$

$R = 1000$

$T = 73.40$

$L = 146.53$

2+00

1^o-32-06 53.98

2+50

2^o-58-02 50.00

2+92⁵⁵ E.C.

4-11-52 42.55

3+00

4+00

5+00

5+07¹⁷ B.C.

$\Delta = 29^{\circ}12' L$

$R = 1000$

$T = 260.48$

$L = 509.64$

5+50

1-12-12 42.01

6+00

2-38-02 50.00

6+50

4-04-05 "

7+00

5-30-01 "

7+50

6-55-58 "

8+00

8-21-54 "

8+50

9-47-51 "

9+00

11-13-47 "

9+50

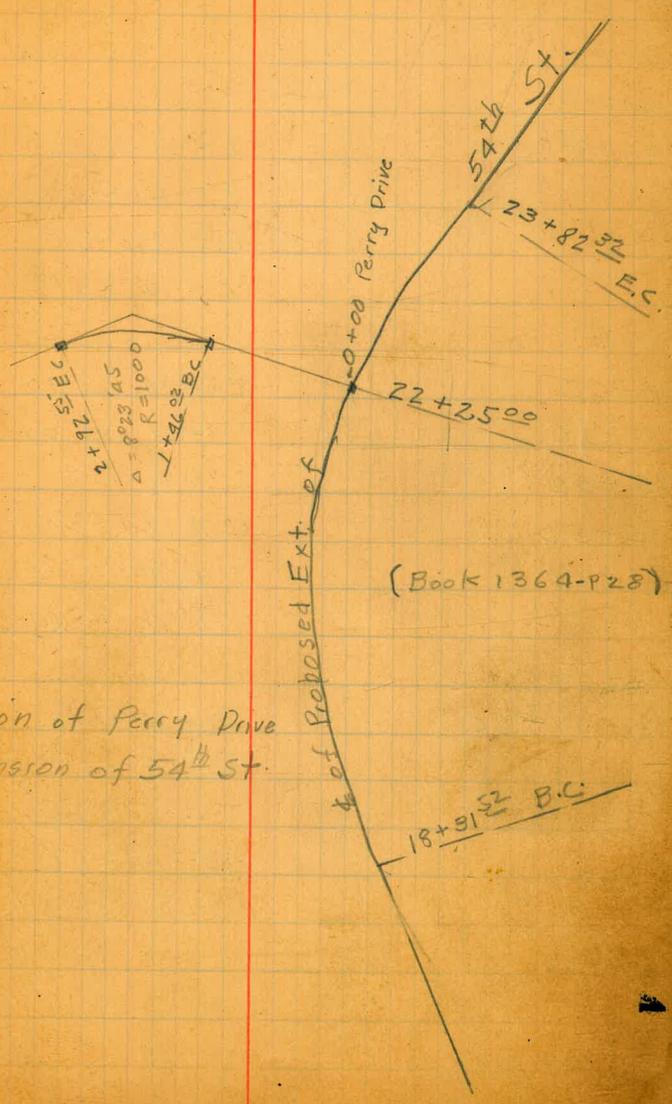
12-39-44 "

10+00

14-05-41 "

Duerm,
Osborne
Driebert.

0 1



Junction of Perry Drive
to Extension of 54th St.

Ext. of Proposed Ext. of

10+17⁶³ E.C.

14-36-00 17.63

11+00

12+00

13+00

13+73⁰ B.C. $\Delta = 31^{\circ}48' R \checkmark$ $R = 500$ $T = 142.43 \checkmark$ $L = 277.51 \checkmark$

14+00

14+00

1-32-28⁰ 26.90

14+50

4-24-21 50.00

15+00

7-16-14 "

15+50

10-08-07 "

16+00

13-00-00 "

16+50⁶¹ E.C.

15-54-00 50.61

17+00

17+68⁰² B.C. $\Delta = 27^{\circ}20' L$ $R = 1000$ $T = 243.16 \checkmark$ $L = 477.06 \checkmark$

18+00

0-54-58" 31.98

18+50

2-20-55 50.00

19+00

3-46-52 "

19+50

5-12-49 "

20+00

6-38-46 "

20+50	8+04-43	50.00
21+00	9-30-40	"
21+50	10-56-37	"
22+00	12-22-34	"
22+45 ⁰⁸ E.C.	13-40-00	45.08
23+00		
23+11 ²⁹ B.C.	$\Delta = 30^{\circ}20' R$	
	$R = 800$	
	$T = 216.86 \checkmark$	
	$L = 423.53 \checkmark$	
23+50	1 ^o 23'-36	38.91
24+00	3-11'-02	50.00
24+50	4-58-28	"
25+00	6-45-54	"
25+50	8-33-20	"
26+00	10-20-46	"
26+50	12-08-12	"
27+00	13-55-38	"
27+34 ⁶² E.C.	15-10-00	34.62
28+00		
29+03 ³⁰ B.C.	$\Delta = 22^{\circ}19' R$	
= 28+93 ³⁰	$R = 1000$	
	$T = 197.25 \checkmark$	
	$L = 389.50 \checkmark$	

29+00	0-11-31	6.70
29+50	1-37-28	50.00
30+00	3-03-25	"
30+50	4-29-22	"
31+00	5-55-19	"
31+50	7-21-16	"
32+00	8-47-13	"
32+50	10-13-10	"
32+82 ⁸⁰ E.C.	11-09-30	32.80
33+00		
34+00		
35+00		
36+00		
37+00		
37+38 ⁴ B.C.	$\Delta = 26^{\circ}44' L$	
	$R = 1000$	
	$T = 237.62$ ✓	
	$L = 466.58$ ✓	
37+50	0-20-23	11.86
38+00	1-46-20	50.00
38+50	3-12-17	"
39+00	4-38-14	"
39+50	6-04-11	"
40+00	7-30-08	"
40+50	8-56-05	"

Def'l chord

41+00		10-22-02	50.00
41+50		11-47-59	"
42+00		13-13-56	"
42+04 ⁷²	E.C.	13-22-00	4.72
43+00			
44+00			
45+00			
46+00			
47+00			
48+00	Hub East of Fairmont.		

0+15		
W.L. Pav		9.14
+19 ✓		6.47
+35 ✓		4.46
+50 ✓		2.90
+60 ^E ✓		2.00
+60 ^S Pc. NE ret		1.13
+74 ^Z Pav at cross cb		1.37
0+28 ⁴⁰ = $\frac{1}{2}$ Pav on W.L.		
+74 ^Z top cross cb		1.20
+74 ^Z Pav		2.08
+60 ✓		2.97
+45 ✓		4.25
+30 ✓		5.70
+15 ✓		7.44
W.L. ✓		9.34
0+36 ^Z = N curb		
W.L. Pav		9.28
+10		8.08
+19 ^Z E in N cb Pav		7.17
+19 ^Z top cb		6.28
+37 ^S Pav		5.45
+37 ^S top N cb		4.83
+58 gut		3.98
+58 top N cb		3.28
+74 ^S cross cb Pav		2.51
+74 ^S top cross cb		1.69

7

0+47 ³ = Nob on W.L. = beg walk on E	
+83	0.4
+68 ^Z w edgewalk	2.74
+50	4.3
+25	6.3
W.L. top Nob	8.44
W.L. gut.	9.30
0+75	
W.L.	8.4
+6	8.3
+8	7.5
+25	6.2
+40	4.9
+54 ^Z W. walk	3.78
+59 ^L E ✓	3.63
+60	2.9
1+00	
+54 ^S = E.L. on Drive	3.48
+48 E wall	3.75
+43 ^Z W. Wall	3.84
+25	5.3
+7	6.9
W.L.	8.2
1+10	
step house 2' west	7.50

	1+25	144.59		
W.L.			6.6	
+5			5.6	
+20			4.6	
+31 ²	W. walk		3.45	
+36	E walk		3.34	
+38 ²	E.L.		3.0	
	1+50			
+25	E. walk		2.40	
+23	E.L. on walk		2.39	
+20	W. walk		2.41	
+10			2.0	
W.L.			2.6	
Brass Plug				
B.M.			8.15	136.44
T.P.	11.14	154.98	0.75	143.84
	1+70			
W.L.			7.7	
+6			7.5	
+8			8.8	
+8 ²	E.L.		8.8	
+12 ²	bottom steps		7.39	
+15			8.4	
+25			8.2	
+37	garage		7.3	
-	1+59 top steps		9.04	145.94
-	1+82 ✓ ✓		1.97	
	1+85 ⁶⁰			
1+7			2.1	

Set Walnut
W.L. Union

B.M.	0.35	136.79		136.44
T.P.			12.90	123.89
Neb Walnut 18 ² N of W.L.			2.66	134.13
T.P. 0 0 44		124.33		123.89
T.P. 0 77		112.33	12.77	111.56
T.P. 0 39		100.00	12.72	99.61
T.P. 0 20		87.31	12.89	87.11
B.M. BP NE Indiac Glaston			11.07	86.24
				(86.18)
				Miller

Book 1364
P 17

Levels on Perry Drive

B.M.#3	3.35	341.01	337.66	
0+00			2.06	338.75 on hub
1+00			10.2	330.8
1+46 ⁰² BC	0.55	328.74	12.82	328.19
2+00			4.6	324.1
+50			9.5	319.2
T.P.	0.04	315.80	12.98	315.76
2+92 ⁵⁵ EC			0.88	314.92 on hub
3+50			8.1	307.7
T.P.	0.80	303.74	12.86	302.94
4+00			7.0	296.7
5+07 ²⁹ EC			9.33	294.41 on hub
5+50			10.5	293.2
6+00			11.5	292.2
6+50			12.0	291.7
T.P.	3.02	293.69	13.07	290.67
7+00			8.7	285.0
T.P.	0.90	281.61	12.98	280.71
7+50			5.1	276.5
8+00			9.3	272.3
T.P.	1.20	269.93	12.88	268.73
8+50			6.6	263.3
T.P.	0.32	257.11	13.14	256.79
9+00			5.8	251.3
9+50			10.8	246.3

1/29/30 Landon
Permit
1364

Perry Dr.

9

				257.11
10+17 ⁶³ EC			11.30	245.81 on hub
T.P. 2.03	246.80	12.34		244.77
11+00		12.7		234.1
T.P. 3.53	237.70	12.63		234.17
12+00		12.9		224.8
13+00		11.4		226.3
13+73 ¹⁰ BC		11.82		225.88 on hub
14+00		11.8		225.9
14+50		10.6		227.1
15+00		5.7		232.0
T.P. 0.31	225.33	12.68		225.02
15+50		2.8		222.5
16+00		11.5		213.8
T.P. 2.77	214.3	13.17		212.12
16+50 ⁶⁴ EC		3.11		211.82 on hub
17+00		7.8		207.1
17+68 ⁰² BC		11.2		203.7
18+00		9.3		205.6
18+50		8.9		206.0
19+00		14.6		200.3
19+50		16.9		198.0
20+00		18.7		196.2
20+50		18.1		196.8
21+00		6.9		208.0

	214.93			
21+50		38	211.1	
22+00		7.5	207.4	
T.P. 0.56	204.22	11.27	203.66	
22+45 ⁰⁸ EC		1.2	203.0	
23+11 ⁰⁹ BC		8.8	195.4	
23+50		9.3	194.9	
24+00		5.1	199.1	
24+50		9.5	194.7	
T.P. 0.34	191.54	13.02	191.20	
25+00		6.3	185.2	
25+50		5.0	186.5	
26+00		6.9	184.6	
26+50		8.9	182.6	
27+00		12.4	179.1	
T.P. 2.89	181.33	13.10	178.44	
27+34 ⁶³ EC		3.47	177.86	on Hub
28+00		4.4	176.9	
29+03 ³⁹		4.5	176.8	
29+60		11.8	169.5	
30+10		11.4	169.9	
30+60		7.5	173.8	
31+10		6.7	174.6	
31+60		8.0	173.3	
T.P. 1.38	170.27	12.44	168.89	

170-27

32+10			3.1	167.2
32+60			6.0	164.3
32+92 ⁸⁰ E.C.			5.90	164.37 on hub
34+10			10.3	160.0
35+10			12.4	157.9
T.P.	3.74	161.17	12.84	157.43
36+10			5.7	155.5
37+48 ⁴⁰ B.C.			11.8	149.4
38+10			9.5	151.7
38+60			8.8	152.4
39+10			6.6	154.6
39+60			3.4	157.8
40+10			3.8	157.4
40+60			6.4	154.8
41+10			9.1	152.1
T.P.	5.97	154.01	13.13	148.04
41+60			1.7	152.3
42+14 ²⁰ E.C.			4.18	149.83
43+10			12.8	141.2
T.P.	2.65	143.76	12.90	141.11
44+10			8.4	135.4
45+10			9.3	134.5
46+10			8.8	135.0
47+10			6.0	137.8
47+60			8.73	135.03 on hub

X sec Perry Drive (Stationing corrected for Equation on P3)

L F R 11

338.6			0+00			338.6
$\frac{100}{-0.3}$						$\frac{100}{-0.3}$
343.2			1+00			329.4
$\frac{100}{+12.4}$						$\frac{82}{-1.4}$
344.1			1+46 ⁰²			322.8
$\frac{67}{+3.3}$						$\frac{145}{-8.0}$
344.9			2+00			310.8
$\frac{100}{+23.7}$						$\frac{68}{-13.3}$
341.2			3+50			297.5
$\frac{62}{+13.0}$						$\frac{95}{-26.6}$
344.0			4+00			281.3
$\frac{100}{+27.9}$						$\frac{75}{+26.2}$
337.1						$\frac{42}{+13.0}$
333.90						$\frac{43}{-13.0}$
320.7						$\frac{90}{-26.4}$
$\frac{75}{+26.2}$						$\frac{111}{-33.2}$
320.7						$\frac{127}{-43.2}$
323.2						
$\frac{72}{+26.5}$						
296.7						
$\frac{40}{-13.0}$						
283.7						
$\frac{100}{-28.0}$						
268.7						

L

E

R

320.4
62
+26.0

307.9
30
+13.5

5707.99
294.4
281.4
35
-13.0

257.8
110
-34.6

531.0
85
+38.8

305.20
25
+13.0

6+00
292.2
266.2
61
-26.0

253.7
100
-38.3

311.10
75
+26.1

7+00
285.0

258.8
70
-26.2

251.8
100
-39.2

301.0
68
+24.5

7+50
287.50
276.5
263.5
40
-13.0

249.4
76
-27.1

246.0
120
-30.5

301.3
80
+27.0

8+00
272.3
262.7
33
-9.6

246.2
65
-26.1

243.90
100
-28.4

275.9
80
+12.6

8+50 ✓
271.7
263.3
34
+8.6

242.10
70
-21.7

240.50
100
-22.8

L

E

R

12

281.60
90
+30.3

9+00 ✓
251.3

273.5
50
+26.2

263.7
25
+16.4

9+30 ✓
247.3

235.1
52
-11.7

235.1
75
-12.2

240.6
100
-6.7

285.80
95
+40.0

259.6
30
+13.8

10+17.63 ✓
245.8
240.
231.0

234.6
85
-11.2

237.5
100
-8.3

260.1
70
+26.0

11+00 ✓
234.1
226.8
25
-8.0

228.3
74
-5.8

234.1
93
-0.0

262.1
100
+37.3

250.5
70
+25.7

226.1
83
+1.3

12+00
228.0
224.8
221.6
24
+0.8

232.8
58
+8.0

237.4
83
+12.6

242.5
100
+17.7

235.4
100
+9.1

249.6
70
-6.7

221.3
24
-5.0

13+00
226.3

248.9
100
+22.6

L	C	R
$\begin{array}{r} 15.3 \\ \hline 105 \\ -10.6 \\ \hline \end{array}$	$\begin{array}{r} 14+00 \\ 216.2 \\ 225.9 \\ 239.6 \\ \hline 44 \\ -9.7 \\ \hline 40 \\ +13.7 \\ \hline \end{array}$	$\begin{array}{r} 256.2 \\ 263.2 \\ \hline 100 \\ +30.3 \\ \hline 120 \\ +37.3 \\ \hline \end{array}$
$\begin{array}{r} 211.1 \\ \hline 100 \\ -20.9 \\ \hline \end{array}$	$\begin{array}{r} 15+00 \\ 212.2 \\ 232.0 \\ 245.0 \\ \hline 55 \\ -198 \\ \hline 47 \\ +13.0 \\ \hline \end{array}$	$\begin{array}{r} 263.7 \\ \hline 120 \\ +31.7 \\ \hline \end{array}$
$\begin{array}{r} 207.1 \\ \hline 100 \\ -6.7 \\ \hline \end{array}$	$\begin{array}{r} 16+00 \\ 207.1 \\ 213.8 \\ 226.9 \\ \hline 47 \\ -6.7 \\ \hline \end{array}$	$\begin{array}{r} 219.4 \\ \hline 120 \\ +45.6 \\ \hline \end{array}$
$\begin{array}{r} 202.9 \\ 200.4 \\ 202.4 \\ \hline 110 \\ -0.8 \\ \hline 90 \\ -33 \\ \hline 60 \\ -1.2 \\ \hline \end{array}$	$\begin{array}{r} 17+68 \\ 201.2 \\ 203.7 \\ 224.9 \\ \hline 5 \\ -1.5 \\ \hline 34 \\ +21.2 \\ \hline \end{array}$	$\begin{array}{r} 229.0 \\ 244.7 \\ \hline 78 \\ +35.3 \\ \hline 95 \\ +41.0 \\ \hline \end{array}$
$\begin{array}{r} 18+50 \\ 206.0 \\ 214.0 \\ 230.5 \\ \hline 30 \\ +8.0 \\ \hline 100 \\ +24.5 \\ \hline \end{array}$	$\begin{array}{r} 18+70 \\ 202.4 \\ 232.8 \\ 246.0 \\ \hline 55 \\ +30.4 \\ \hline \end{array}$	$\begin{array}{r} 230.5 \\ 244.7 \\ \hline 100 \\ +24.5 \\ \hline \end{array}$

L	C	R
$\begin{array}{r} 197.3 \\ 196.4 \\ 197.7 \\ \hline 125 \\ -0.7 \\ \hline 100 \\ -1.6 \\ \hline 85 \\ -0.3 \\ \hline \end{array}$	$\begin{array}{r} 19+50 \\ 198.0 \\ 199.6 \\ \hline 10 \\ +1.6 \\ \hline 50 \\ +25.9 \\ \hline \end{array}$	$\begin{array}{r} 223.9 \\ \hline 50 \\ +25.9 \\ \hline \end{array}$
$\begin{array}{r} 193.7 \\ 193.7 \\ 192.7 \\ 193.2 \\ \hline 90 \\ -14.5 \\ \hline 100 \\ -14.3 \\ \hline 55 \\ -13.3 \\ \hline 25 \\ -14.8 \\ \hline \end{array}$	$\begin{array}{r} 21+00 \\ 208.0 \\ 218.0 \\ 219.0 \\ \hline 10 \\ +5.0 \\ \hline 27 \\ +11.0 \\ \hline 60 \\ +24.4 \\ \hline \end{array}$	$\begin{array}{r} 232.4 \\ \hline 60 \\ +24.4 \\ \hline \end{array}$
$\begin{array}{r} 191.1 \\ 191.7 \\ 195.7 \\ \hline 100 \\ -20.0 \\ \hline 65 \\ -18.4 \\ \hline 25 \\ -15.2 \\ \hline \end{array}$	$\begin{array}{r} 21+50 \\ 211.1 \\ 215.1 \\ 216.1 \\ 218.5 \\ 230.4 \\ \hline 10 \\ +2.0 \\ \hline 20 \\ 0.0 \\ \hline 60 \\ +7.4 \\ \hline 75 \\ +19.3 \\ \hline \end{array}$	$\begin{array}{r} 230.4 \\ \hline 75 \\ +19.3 \\ \hline \end{array}$
$\begin{array}{r} 194.1 \\ 189.4 \\ 190.1 \\ 195.1 \\ \hline 140 \\ -13.3 \\ \hline 100 \\ -14.0 \\ \hline 70 \\ -17.3 \\ \hline 26 \\ -12.3 \\ \hline \end{array}$	$\begin{array}{r} 21+75 \\ 205.0 \\ 214.8 \\ 233.7 \\ 238.7 \\ \hline 30 \\ +7.4 \\ \hline 65 \\ +26.3 \\ \hline 75 \\ +31.3 \\ \hline \end{array}$	$\begin{array}{r} 238.7 \\ \hline 75 \\ +31.3 \\ \hline \end{array}$
$\begin{array}{r} 186.1 \\ 184.8 \\ 187.8 \\ 190.1 \\ \hline 100 \\ -13.0 \\ \hline 65 \\ -14.3 \\ \hline 45 \\ -11.3 \\ \hline 20 \\ -9.0 \\ \hline \end{array}$	$\begin{array}{r} 22+00 \\ 207.4 \\ 214.8 \\ 233.7 \\ 238.7 \\ \hline 30 \\ +7.4 \\ \hline 65 \\ +26.3 \\ \hline 75 \\ +31.3 \\ \hline \end{array}$	$\begin{array}{r} 238.7 \\ \hline 75 \\ +31.3 \\ \hline \end{array}$
$\begin{array}{r} 186.1 \\ 184.8 \\ 187.8 \\ 190.1 \\ \hline 100 \\ -13.0 \\ \hline 65 \\ -14.3 \\ \hline 45 \\ -11.3 \\ \hline 20 \\ -9.0 \\ \hline \end{array}$	$\begin{array}{r} 24+00 \\ 189.1 \\ 218.1 \\ 223.6 \\ \hline 60 \\ +19.0 \\ \hline 75 \\ +24.5 \\ \hline \end{array}$	$\begin{array}{r} 223.6 \\ \hline 75 \\ +24.5 \\ \hline \end{array}$

L

E

R

183.4
 $\frac{15}{-11.3}$
 190.5
 $\frac{13}{-4.2}$
 194.7

24+80

194.8

25+00 ✓

183.2
 $\frac{2}{-2.0}$
 185.2
 195.2
 $\frac{7}{+10.0}$

26+50

180.2
 182.6
 191.6
 $\frac{14}{-2.4}$
 $\frac{28}{+13.0}$

221.4
 $\frac{86}{+38.8}$

29+03³⁰

173.5
 $\frac{100}{-3.3}$
 171.0
 $\frac{87}{-5.8}$
 172.2
 $\frac{48}{-4.6}$
 170.1
 $\frac{14}{-6.7}$
 176.8
 191.5
 $\frac{35}{+14.7}$
 202.8
 $\frac{70}{+26.0}$

30+10

173.0
 $\frac{100}{-1.6}$
 174.6
 176.6
 $\frac{5}{+2.0}$
 183.4
 $\frac{12}{+8.8}$
 198.5
 $\frac{60}{+23.9}$
 204.1
 $\frac{80}{+29.5}$

L

E

R 14

167.8
 $\frac{35}{-6.0}$
 169.5
 $\frac{25}{-4.3}$
 172.4
 $\frac{18}{-1.4}$
 173.8
 $\frac{25}{+4.5}$
 178.3

30+60 ✓

100
 $\frac{100}{+13.5}$

168.1
 $\frac{110}{-6.5}$
 165.2
 $\frac{65}{-9.4}$
 170.6
 $\frac{40}{-4.0}$

31+10 ✓

174.6
 $\frac{40}{+3.2}$
 177.8
 $\frac{60}{+13.0}$
 187.6
 $\frac{100}{+24.0}$
 198.6

31+60 ✓

173.3
 $\frac{22}{+9.2}$
 182.5
 $\frac{35}{+13.0}$
 186.3
 $\frac{75}{+23.9}$
 197.2

32+60 ✓

163.3
 $\frac{100}{-1.0}$
 163.3
 $\frac{85}{-1.0}$
 164.3
 $\frac{17}{+3.0}$
 167.3
 $\frac{53}{+25.8}$
 190.1
 $\frac{72}{+39.0}$
 203.3

34+10

159.2
 $\frac{100}{-0.8}$
 157.9
 $\frac{55}{-2.1}$
 158.6
 $\frac{10}{-1.4}$
 160.0
 $\frac{22}{+4.5}$
 164.5
 $\frac{77}{+39.0}$
 199.0

36+10

153.3
 $\frac{100}{-2.2}$
 154.5
 $\frac{84}{-1.0}$
 153.1
 $\frac{37}{-2.4}$
 155.2
 $\frac{32}{-0.3}$
 155.5
 $\frac{25}{+1.6}$
 157.1
 $\frac{65}{+25.1}$
 182.1
 $\frac{70}{+26.6}$

L

E

R

36+4

155.5

36+55

151.6

36+70

151.7

 $\frac{5}{-0.1}$

151.6

 $\frac{15}{+7.2}$

158.9

 $\frac{67}{+16.3}$

168.0

 $\frac{90}{+26.0}$

177.70

37+00

150.2

 $\frac{5}{+0.5}$

150.7

 $\frac{19}{+7.5}$

157.7

 $\frac{23}{+9.2}$

159.4

 $\frac{40}{+20.2}$

170.4

 $\frac{70}{+28.0}$

178.2

37+48¹⁴

149.4

 $\frac{6}{+0.1}$

149.5

 $\frac{7}{+4.7}$

154.1

 $\frac{85}{+37.2}$

186.60

37+52

175.1

7

37+55

152.5

L

E

R 15

 $\frac{100}{-9.0}$

145.6

 $\frac{78}{-7.6}$

145.0

 $\frac{75}{-6.5}$

148.1

 $\frac{21}{-3.4}$

151.1

39+10

154.6

 $\frac{27}{+4.1}$

158.7

 $\frac{70}{+27.0}$

181.6

39+60

157.8

 $\frac{44}{+6.9}$

164.7

 $\frac{70}{+11.7}$

169.5

40+60

154.8

 $\frac{60}{+6.1}$

160.9

 $\frac{79}{+12.8}$

165.6

41+60

152.3

 $\frac{84}{+13.1}$

165.4

42+48

147.3

 $\frac{25}{+1.8}$

149.1

 $\frac{100}{+23.2}$

170.5

44+10

135.4

 $\frac{18}{-0.6}$

134.8

 $\frac{23}{+4.7}$

140.1

 $\frac{85}{+24.1}$

159.6

L

±

R

$$\begin{array}{r}
 132.3 \\
 100 \\
 -22 \\
 \hline
 131.1 \\
 75 \\
 -34 \\
 \hline
 121.3 \\
 50 \\
 -32 \\
 \hline
 133.5 \\
 45 \\
 -10 \\
 \hline
 134.5 \\
 45+10 \\
 134.5
 \end{array}$$

$$\begin{array}{r}
 157.6 \\
 90 \\
 +13.1 \\
 \hline
 157.6
 \end{array}$$

$$\begin{array}{r}
 130.8 \\
 100 \\
 -4.2 \\
 \hline
 129.9 \\
 40 \\
 -5.1 \\
 \hline
 128.4 \\
 15 \\
 -6.6 \\
 \hline
 133.5 \\
 10 \\
 -1.5 \\
 \hline
 135.0 \\
 46+10 \\
 135.0 \\
 22 \\
 +11.0 \\
 \hline
 146.0
 \end{array}$$

$$\begin{array}{r}
 156.0 \\
 90 \\
 +21.0 \\
 \hline
 156.0
 \end{array}$$

$$\begin{array}{r}
 147.8 \\
 100 \\
 -10.0 \\
 \hline
 137.1 \\
 30 \\
 -10.7 \\
 \hline
 134.2 \\
 25 \\
 -3.6 \\
 \hline
 137.8 \\
 47+10 \\
 137.8 \\
 45 \\
 +6.8 \\
 \hline
 144.6
 \end{array}$$

$$\begin{array}{r}
 151.1 \\
 75 \\
 +13.3 \\
 \hline
 151.1
 \end{array}$$

$$\begin{array}{r}
 125.5 \\
 100 \\
 -7.5 \\
 \hline
 126.0 \\
 42 \\
 -9.0 \\
 \hline
 127.8 \\
 32 \\
 -3.2 \\
 \hline
 135.0 \\
 47+60 \\
 135.0 \\
 50 \\
 +6.9 \\
 \hline
 141.9
 \end{array}$$

$$\begin{array}{r}
 146.0 \\
 65 \\
 +11.0 \\
 \hline
 146.0
 \end{array}$$

$$\begin{array}{r}
 129.6 \\
 48+06 \\
 129.6 \\
 40 \\
 +9.2 \\
 \hline
 128.0
 \end{array}$$

$$\begin{array}{r}
 128.0 \\
 40 \\
 +9.2 \\
 \hline
 128.0
 \end{array}$$

48+59 = Approx 4 of Fairmount.

$$\begin{array}{r}
 128.0 \\
 128.0
 \end{array}$$

0+00 B.C.

$$\Delta = 62^{\circ}10' R$$

$$R = 400$$

$$T = 241.14$$

$$L = 434.00$$

0+86[±]

6-13' 86.63

1+73[±]

12-26'

2+60[±]

18-39

3+47[±]

24-52

4+34[±] E.C.

31-05

4+52⁸⁴ B.C.

$$\Delta = 62^{\circ}10' L$$

$$R = 350$$

$$T = 210.99$$

$$L = 379.75$$

5+28⁷¹

6-13' 75.80

6+04⁷⁴

12-26'

6+80⁶⁹

18-39

7+56⁶⁴

24-52

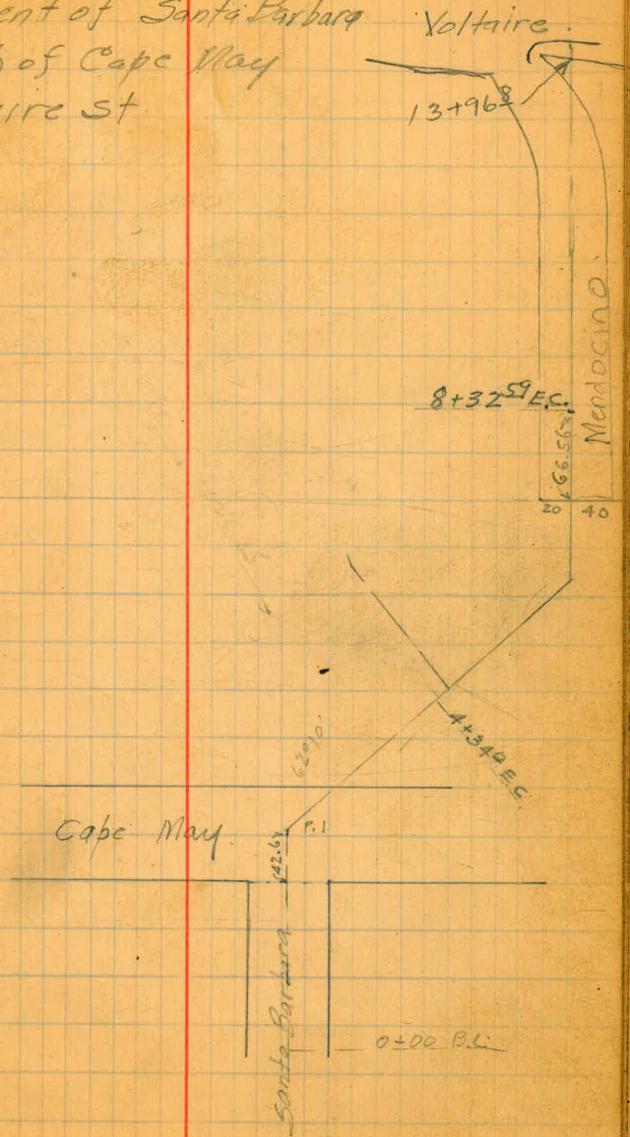
8+32⁵¹ E.C.

31-05

3/9/31 Loudon

17

Alignment of Santa Barbara
from South of Cape May
into Voltaire St



Profile of 100 on P 17

B.M	12 91	170.18	157.27	✓	SE BP
0+00			0.4		Santa Clara Paper Mill
0+86 ^B			6.0		
1+28 ^B	top cb		8.39		
1+73 ^E			9.2		
B.M	5 36	162.63	157.27		
2+24 ^E	top N. cb		5.65		
2+60 ^E	ban		6.50		
2+94 ^E	pan Nor swiret		7.82		
3+47 ^E			8.1		
3+60 ^E	top cb		8.15		
4+34	E.C.		6.8		
4+52 ^B	B.C.		7.7		
5+28 ^E			13.2		
T.P.	0.82	150.97	12.48		
T.P.	0.09	138.05	13.01		
6+04 ^E			1.8		
6+80 ^B			14.1		
T.P.	0.82	125.75	13.12		
T.P.	0.90	113.49	13.16		
7+56 ^B			11.8		
T.P.	1.20	101.76	12.93		
8+32 ^E	E.C.		4.1		
9+00			6.4		

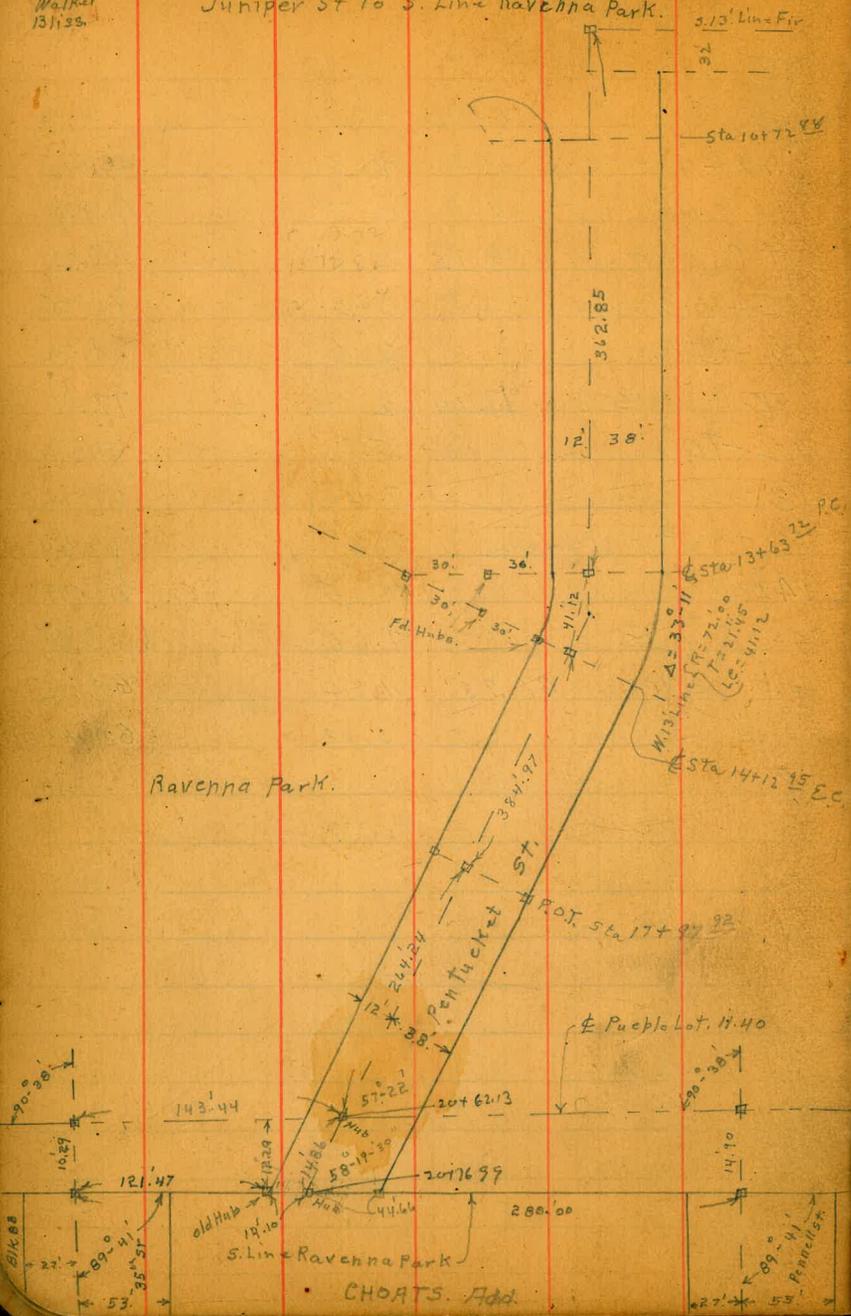
10+00		9.3	92.46
11+00		10.7	91.06
T.P. 0.67	89.95	12.48	89.28
12+00		6.2	83.75
12+56		7.6	82.35
T.P. 0.13	77.14	12.94	77.01
12+70		5.9	71.24
13+00		7.4	69.74
13+96 ^B	= sl. Voltaire	7.2	69.94
14+08	= ob. line. top cb	7.15	69.99
14+08	guf	7.66	69.48
T.P. 2.41	67.73	11.82	65.32
Calabria & Voltaire			
B.P. SE		5.28	62.45 B.M.

(62.37)

107.8
77
70

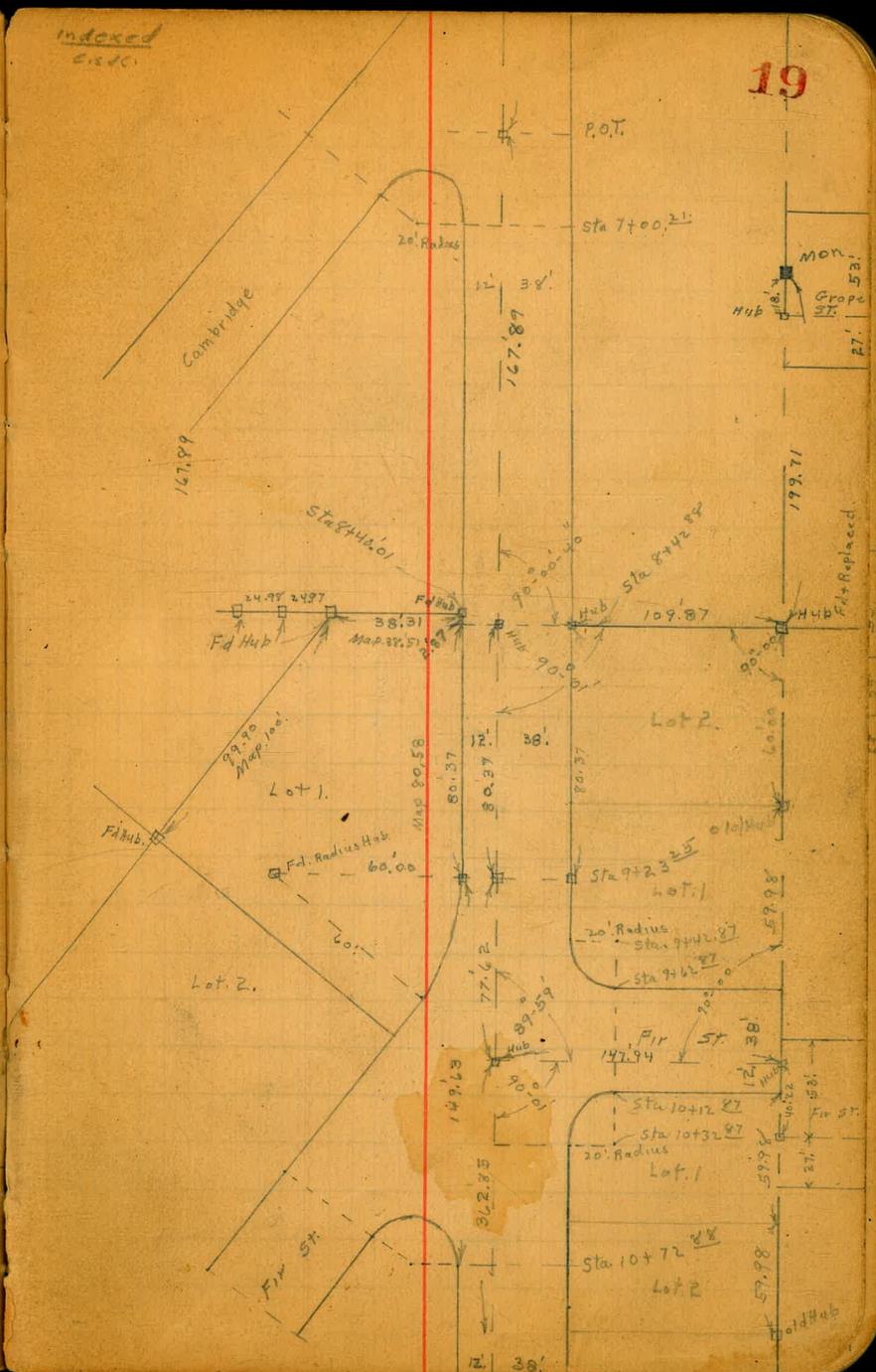
11-25-37
Miller
Walker
Bliss

Pentucket St. 7 Sec.
Juniper St to S. Line Ravenna Park.



indexed
C.S.D.C.

19



10. wide
10. ch
10. 14s.

Pentucket St. X Sec

B.M. B.P.	4.82	271.25	266.43
		S. line Juniper (on diagonal)	
W. on s. edge emt. walk	7.73	261.52	
+ 7.8. s. End ch. Return	10.16	261.09	
+ 7.9. gutter s. edge Parmit.	10.65	260.60	
+ 10.06 = W. ch. ^{line} " " "	10.64	260.61	
1/4 " " "	10.74	260.51	
1/4 " " "	11.11	260.14	
1/4 " " "	11.80	259.45	
+ 1.5. e. gutter on ch. inlet.	11.89	259.36	
+ 1.5. s. End. emt. ch.	11.11	260.14	
+ 6	11.5	259.8	
ch	16.2	255.1	
E.	22.2	249.1	
+ 2.5	28.0	243.3	
$\left. \begin{array}{l} \text{Pentucket on S. line Juniper} \\ 3.33 \text{ S. of S. line Juniper on W.} \end{array} \right\} \text{at } 90^\circ \text{ to Pent.}$			
1/4 on s. edge parmit.	11.11	260.14	
W. 1/4	10.8	260.5	
W. ch	10.4	260.9	
+ 6	7.3	264.0	
W.	6.6	264.7	
$0+00 = \left\{ \begin{array}{l} \text{S. line Juniper on E.} \\ 6.65 \text{ S. of S. line Juniper on W.} \end{array} \right\} \text{at } 90^\circ \text{ to } 00$			
E. = 25	28.0	243.3	
E.	22.2	249.1	
ch.	16.2	255.1	
+ 8	10.8	260.5	

S. W. Corner
+ Juniper

271.25

21

1/4	10.6	260.7
1/4	10.8	260.5
1/4	10.7	260.6
+ 8	10.5	260.7
ch.	9.3	262.0
+ 7	6.4	264.9
W.	6.1	265.2
0+25 S		
W.	6.0	265.3
ch.	4.5	264.5
+ 4	8.1	263.2
1/4	8.8	262.5
1/4	8.4	262.5
+ 6	8.4	262.9
1/4	10.6	260.7
T.P.	10.97	273.74
ch.	20.7	253.0
E.	23.5	250.2
+ 13	25.7	248.0
+ 25	29.0	244.7
0+50 S		
E. = 20	25.6	248.1
E.	20.7	253.0
ch.	17.8	255.9
1/4	14.4	259.3
+ 7	9.6	264.1

273.74

♀	9.4	264.3
ly	9.3	264.4
cb.	8.5	265.2
w.	7.0	266.7
0+75 S		
w	5.9	267.8
cb	7.3	266.4
ly	8.2	265.5
♀	8.5	265.2
ly	12.2	261.5
cb.	15.6	258.1
E.	17.9	255.8
+ 20	23.1	
1+00 S		
-10	17.4	256.3
E	14.4	259.3
cb.	12.2	261.5
ly	10.2	263.5
+ 5	8.9	264.8
♀	8.1	265.6
ly	7.2	266.5
cb.	6.5	267.2
w.	5.5	268.2

273.74

Pentucket

22

1+25 S		
w	4.5	269.2
cb	5.7	268.0
ly	6.3	267.4
♀	6.9	266.8
ly	8.3	265.4
cb.	10.2	263.5
E.	11.7	262.0
+10	13.3	260.4
1+50 S		
-10	11.2	262.5
E	7.6	264.1
cb	8.0	265.2
ly	7.0	266.7
♀	6.0	267.7
ly	5.6	268.1
cb	5.2	268.5
w	4.1	269.6
1+75 S.		
w.	3.9	269.8
cb.	4.3	269.4
ly	4.8	268.9
♀	4.8	268.9
ly	5.0	268.7
cb	6.3	267.4
E.	7.4	266.3

273.74

2+00 S

E	6.0	267.7
cb	5.5	268.2
" ₁₄	4.6	269.1
♀	4.2	269.5
" ₁₄	4.1	269.6
cb	3.9	269.8
W	3.6	270.1

2+41 S

on W. ch. line Eucalyptus Tree 5" Diam

2+47

W. ch. line Eucalyptus Tree 6" Diam

2+56

W. ch. line Eucalyptus Tree 6" Diam

2+66

W. ch. line Eucalyptus Tree 14" Diam

2+73

W. ch. line Eucalyptus Tree 6" Diam

2+89

W. ch. line Eucalyptus Tree 8" Diam

2+50 S

W	3.9	269.8
cb	3.6	270.1
" ₁₄	3.6	270.1
♀	3.6	270.1
" ₁₄	3.6	270.1

273.74

Pentucket 23

cb	3.8	269.9
E	3.8	269.9

3+00 S

E	3.1	270.6
cb	3.5	270.2
" ₁₄	3.7	270.0
♀	4.1	269.6
" ₁₄	4.6	269.1
cb	5.0	268.7
W	5.4	268.3

3+50 S

W	7.1	266.6
cb	6.5	267.2
" ₁₄	6.0	267.7
♀	5.4	268.3
" ₁₄	5.3	268.4
cb	4.8	268.9
E	4.3	269.4

4+00 S

E	6.7	262.0
cb	7.3	266.4
" ₁₄	7.9	265.8
♀	8.3	265.4
" ₁₄	8.9	264.8
cb	9.4	264.3
W	9.6	264.1

257.95

N. Line Ivy St.

E. = 40. on Diagonal 60.37 wide

E. = N.E. Cor Ivy + Pentucket. +6.3 264.3

+2.0 260.0

cb +0.4 258.4

1/4 0.4 257.6

E 1.1 256.9

1/4 2.8 255.2

cb. 4.4 253.6

W. = N.W. Cor Ivy + Pentucket. 8.2 249.8

+10 14.0 244.0

+20 23.5 234.5

+35 29.0 229.0

+40. 26.2 231.8

-25' S. of W. = E Ivy St.

W-43 28.3 229.7

W-15 14.6 243.4

W. 8.9 249.1

+10 5.2 252.8

+19 2.4 255.6

+28 = E 1.8 256.2

+37 1.8 256.2

+46 1.7 256.3

+56 = E 1.0 257.0

From S. Line Ivy, Pentucket 50' wide 10' chs - 7.5' dia. {51.85 Wide}

50' S. of N. Line = S. Line Ivy St. {on diagonal}

26.23 E. of E. Line = E.C. 20' Radius Curve +2.6 260.6

E. at P.I. 20' Radius Curve 2.8 255.2

cb. 2.8 255.2

1/4 2.7 255.3

257.95

Pentucket

N.B. This is Sec. for Establishment of Grade
Do not use For Yardage.

25

E 2.8 255.2

1/4 2.8 255.2

cb. 3.0 255.0

3' E. of W. Line 3.5 254.5

W. = P.I. 20' Radius Curve 5.4 252.6

W+6 5.8 252.2

W+15.25 = E.C. 20' Radius Curve 12.3 245.7

W+34' 18.8 239.2

0+00 =	{	PI 20' Radius Curve on E.	}	at 90°-60' to Pentucket
		13.72 S. of P.I. 20' Radius Curve on W.		

W-20 10.8 247.2

W-5 6.5 251.5

W. 4.1 253.9

cb. 3.2 254.8

1/4 3.1 254.9

E 3.1 254.9

1/4 2.9 255.1

cb. 2.8 255.2

E. at P.I. 20' Rad. Curve 2.8 255.2

0+01.53 P.C. 20' Radius Curve on W

W. line at P.C. 15.25 S. of P.I. 4.0 254.0

0+26.23 P.L. 20' Radius Curve on E.

E. at P.C. 20' Rad. Curve on E. 3.8 254.2

cb 4.0 254.0

1/4 4.0 254.0

E 4.2 253.8

1/4 4.2 253.8

257.95

0+26²³ (con)

cb	4.2	253.8
W.	5.2	252.8
W+10	6.8	251.2

0+39

W-20	12.6	245.4
W-10	9.2	248.8
W.	6.4	251.6
cb	4.8	253.2
1/4	4.9	253.1
4	4.8	253.2
1/4	4.5	253.5
cb	4.5	253.5
E	4.4	253.6

0+50

E	4.8	253.2
cb	4.9	253.1
1/4	5.0	253.0
4	5.2	252.8
1/4	5.3	252.7
cb	5.2	252.8
W.	10.3	247.2
+10	13.5	244.8
+25	18.3	239.7

0+75

W-30	27.0	231.0
W-15	22.4	233.6

257.95

Pentucket

26

W.	14.3	243.7
cb	6.7	251.3
1/4	4.2	251.8
4	4.2	251.8
1/4	6.0	252.0
cb	6.0	252.0
E	6.2	251.8

1+00

E	7.1	250.9
cb	7.0	251.0
1/4	7.1	250.9
4	7.2	250.8
1/4	7.0	251.0
cb	7.1	250.9
+2	7.2	250.8
W	12.2	248.8
+15	17.8	240.2
+30	23.0	235.0
+40	23.0	235.0

1+17

W-15	12.9	245.1
W	9.3	248.2
cb	7.9	250.1
1/4	7.7	250.3
4	7.8	250.2
1/4	7.9	250.1

257.95

1+17 (Con)

cl	7.7	250.3
----	-----	-------

E	7.7	250.3
---	-----	-------

1+50

c	9.2	248.8
---	-----	-------

d	9.2	248.8
---	-----	-------

1/4	9.2	248.8
-----	-----	-------

1/4	9.2	248.8
-----	-----	-------

1/4	9.0	249.0
-----	-----	-------

cl	8.9	249.1
----	-----	-------

W.	9.3	248.7
----	-----	-------

1+89¹⁶

P.C.

Rt.

 $\Delta = 14^{\circ} 46'$
 $EA = 5^{\circ} 00'$

W.	10.9	247.1
----	------	-------

cl	10.6	247.4
----	------	-------

1/4	11.0	248.0
-----	------	-------

1/4	10.8	247.2
-----	------	-------

1/4	10.8	247.2
-----	------	-------

cl	10.7	247.3
----	------	-------

E	10.8	247.2
---	------	-------

2+53⁵⁹

Ctr Curve

E	12.8	245.2
---	------	-------

d	12.8	245.2
---	------	-------

1/4	12.8	245.2
-----	------	-------

1/4	12.8	245.2
-----	------	-------

1/4	12.8	245.2
-----	------	-------

cl	12.8	245.2
----	------	-------

W	12.8	245.2
---	------	-------

257.95

Pentucket

27

T.P. 1.42

246.31

13.06

244.89

W. 13. Line
P.I. Hub.3+18⁰² E.C.

W.

2.5 243.8

cl

2.5 243.8

1/4

2.4 243.9

1/4

2.4 243.9

1/4

2.4 243.9

cl

2.5 243.8

E.

2.5 243.8

4+02

41

P.C. 60'

Rad Curve on W. W. Side of Conden.

E.

3.3 243.0

cl

3.4 242.7

1/4

3.5 242.8

1/4

3.3 243.0

1/4

3.4 242.9

cl

3.3 243.0

W.

2.9 243.1

4+65

44

W

3.4 242.9

cl

3.7 242.6

+1

4.1 242.2

1/4

3.8 242.5

1/4

3.7 242.6

1/4

3.9 242.4

cl

4.2 242.1

E

3.8 242.5

246.31 ✓
 5+28 47 P.C. 20' Radius Curve S.W. Cor Camden + Pentucket

E	4.2	242.1
+9	4.9	241.4
cb	5.4	240.9
1/4	4.7	241.6
1/2	4.7	241.6
3/4	4.8	241.5
+5	5.2	241.1
cb	4.7	241.6
W.	4.6	241.2

5+50 58 P.C. 60' Radius N.W. Pentucket + Cambridge

W.	4.7	241.6
cb	5.2	241.1
+2	5.7	240.6
1/4	5.1	241.2
1/2	5.0	241.3
3/4	5.1	241.2
+6	5.3	241.0
cb	5.8	240.5
+2	5.2	241.1
E.	4.6	241.7

6+25 40

E	6.4	239.9
+9	6.6	239.7
cb	7.5	238.8
1/4	6.5	239.8
1/2	6.5	239.8

246.31 ✓ Pentucket

28

+5	7.6	238.7
cb	6.5	239.8
W.	6.2	240.1

6+50

W.	6.7	239.6
cb	7.1	239.2
+1	8.1	238.2
1/4	7.3	239.0
1/2	7.3	239.0
3/4	7.3	239.0
+6	7.9	238.4
cb	7.4	238.9
E.	7.3	239.0

6+75

E	8.3	238.0
cb	8.5	237.8
+1	9.6	236.7
1/4	8.4	237.9
1/2	8.3	238.0
3/4	8.2	238.1
+7	8.7	237.6
cb	8.2	238.1
W.	8.0	238.3

246.31 ✓

7+00²¹ P. e. 20' Radius Curve S.W. Pentucket + Cambridge

W.	9.8	236.5
cb	9.5	236.8
+1	10.1	236.2
1/4	9.6	236.7
⊕	9.6	236.7
1/4	9.7	236.6
cb	10.0	236.3
E.	10.0	236.3
7+25		
E.	12.0	234.3
cb	12.1	234.2
+1	12.8	233.5
1/4	12.8	233.5
⊕	11.7	234.6
1/4	11.7	234.6
+7	12.0	234.3
cb	11.7	234.6
W.	11.8	234.5
T.P.	0.53	234.47 ✓
7+50.		
W.	1.9	232.6
cb	2.3	232.2
1/4	2.3	232.2
⊕	2.2	232.3
1/4	2.5	232.0
+7	3.5	231.0

234.47

Pentucket

29

cb	2.6	231.9
E.	2.8	231.7
7+75		
E.	5.6	228.9
cb	5.6	228.9
1/4	5.4	229.1
⊕	5.3	229.2
1/4	5.3	229.2
cb	5.2	229.3
W.	4.9	229.6
8+00		
W	8.0	226.5
cb	8.2	226.3
+1	8.8	225.7
1/4	8.7	225.8
⊕	8.4	226.1
1/4	8.5	226.0
cb	8.5	226.0
E.	8.6	225.9
T.P.	0.13	221.37
8+40 ²¹ on W.	13.23	221.24
8+42 ²² on E.	} N. Line Ravenna Park Unit 1 on diagonal	
E	1.0	220.4
cb in washout.	2.0	219.4
1/4	0.7	220.7
⊕	0.7	220.7
1/4	0.7	221.0

221.37

cb		0.4	221.0
W		0.0	221.4
	8+83 ⁰⁷		
W		5.2	216.2
cb		5.5	215.9
1/4		5.5	215.9
⊕		5.7	215.7
1/4		6.1	215.3
cb		6.1	215.3
E		5.7	215.7
	9+23 ²⁵ P.C. 60' Radius N.W. Cor. Pentucket + Fir Stk		
E		9.1	212.3
cb		10.2	211.2
1/4		10.1	211.3
⊕		9.9	211.5
1/4		9.8	211.6
cb		9.9	211.5
W		9.8	211.6
T.P.	4.30 212.76	12.91	208.46
	9+42 ⁸⁷ P.C. 20' Radius N.E. Cor Fir + Pentucket		
W		2.5	210.3
cb		2.6	210.2
1/4		2.6	210.2
⊕		2.7	210.1
1/4		2.4	210.4
cb		2.1	210.7
E		1.5	211.3

212.76

Pentucket

30

9+62⁸⁷ N. Line Fir on E.

E		3.1	209.7
cb		3.2	209.6
1/4		3.3	209.5
⊕		3.5	209.3
1/4		3.8	209.0
cb		3.8	209.0
W		4.1	208.7

9+87⁸⁷ ⊕ Fir on E.

W		5.0	207.8
cb		5.0	207.8
1/4		4.6	208.2
⊕		4.4	208.4
1/4		4.5	208.3
cb		4.5	208.3
E		4.4	208.4
+50'E		0.6	212.2

10+12⁸⁷ S. Line Fir on E.

E		5.0	207.8
cb		5.5	207.3
1/4		5.7	207.1
⊕		5.5	207.3
1/4		5.6	207.2
cb		5.6	207.2
W		5.9	206.9

212.76

10+32⁸⁷ - P.C. 20' Radius S.E. Cor. Pentucket + Fir.

W.	6.3	206.5
cb	6.5	206.3
1/4	6.3	206.5
±	6.2	206.6
1/4	6.5	206.3
cb	6.2	206.6
E.	5.8	202.0

10+72⁸⁸ P.C. 20' Radius S.W. Cor. Pentucket + 1/4

E	7.1	205.7
cb	7.4	205.4
1/4	7.6	205.2
±	7.7	205.1
1/4	7.8	205.0
cb	8.0	204.8
W.	7.4	204.4

11+00

W.	8.0	204.8
cb	8.4	204.4
1/4	8.5	204.3
±	8.4	204.4
1/4	8.3	204.5
cb	8.2	204.6
E	8.1	204.7

212.74

Pentucket

31

11+50

E	9.4	203.4
cb	9.7	203.1
1/4	9.7	203.1
±	9.7	203.1
1/4	9.9	202.9
cb	10.0	202.8
W	9.2	203.6

12+00

W.	10.8	202.0
cb	11.1	201.7
1/4	10.8	202.0
±	10.8	202.0
1/4	11.0	201.8
cb	11.0	201.8
E	10.8	202.0

12+50

E	12.0	200.8
cb	12.0	200.8
1/4	11.9	200.9
±	11.9	200.9
1/4	11.8	201.0
cb	11.8	201.0
W	11.8	201.0

Set. BM

1.41	211.35
T.P. 2.60	203.29
12.07	200.69

W. 13' Line Hub.
Sta. 9+23.25

203.29

13+00

W	3.0	200.3
cb	3.0	200.3
+1	3.5	199.8
1/4	3.4	199.9
⊕	3.4	199.9
1/4	3.5	199.8
cb	3.7	199.6
E	3.6	199.2
	$\Delta 33-11$	
	$\frac{1}{2}A = 85.00$	
	$\frac{1}{2}L = 49.23$	
E	4.9	198.4
cb	4.9	198.4
1/4	4.5	198.8
⊕	4.4	198.9
1/4	4.5	198.8
+7	4.3	199.0
cb	4.1	199.2
W	4.1	199.2
	$14+12.25$	
	E.C.	
W	4.4	198.9
cb	4.6	198.9
+1	4.9	198.4
1/4	5.0	198.3
⊕	5.0	198.3
1/4	5.1	198.2
cb	5.1	198.2
E	5.3	198.0

203.29

Pentucket

14+50

32

E	5.3	198.0
cb	5.1	198.2
+1	5.6	197.7
1/4	5.2	198.1
⊕	5.0	198.3
1/4	5.2	198.1
+7	5.0	198.3
cb	5.0	198.3
W	4.7	198.6
	$15+00$	
W	5.2	198.1
cb	5.3	198.0
+1	5.7	197.6
1/4	5.4	197.9
⊕	5.1	198.2
1/4	5.2	198.1
cb	5.4	197.9
+1	5.0	198.3
E	5.0	198.3
	$15+50$	
E	4.9	198.4
cb	5.0	198.3
1/4	5.0	198.3
⊕	4.9	198.4
1/4	5.1	198.2
cb	5.3	198.0
W	5.1	198.2

203.29

16+00

W	5.1	198.2
cl	5.0	198.3
1/4	5.0	198.3
♀	4.8	198.5
1/4	4.8	198.5
cl	5.0	198.3
E	4.9	198.4

16+50

E	4.8	198.5
cl	4.8	198.5
1/4	4.7	198.6
♀	4.6	198.7
1/4	4.8	198.5
cl	4.6	198.7
W	4.8	198.5

17+00

W	4.3	199.0
cl	4.4	198.9
1/4	4.6	198.7
♀	4.3	199.0
1/4	4.3	199.0
cl	4.5	198.8
E	4.3	199.0

203.29

17+50

E	4.3	199.0
cl	4.6	198.7
1/4	4.4	198.9
♀	4.3	199.0
1/4	4.5	198.8
cl	4.4	198.9
W	4.3	199.0

18+00

W	4.8	198.5
cl	4.7	198.6
1/4	5.1	198.2
♀	5.0	198.3
1/4	5.2	198.1
cl	5.4	197.9
E	4.8	198.5

T.P.-ROT.Hub.

1.62

199.67

5.24

198.05

W-13' Line
Sta. 17+97.22

18+40

E-♀ cmt. Drive to E	1.71	197.96
+5.5♀ " " "	1.83	197.84
+8.5♀ W. end. cmt. Drive	2.83	197.34
cl	2.4	197.3
1/4	2.4	197.3
♀	2.3	197.4
1/4	2.5	197.2
+7	2.6	197.1
cl	2.0	197.7
W	2.0	197.7

Pentucket

33

199.67

18+82

w.	3.5	196.2
cb	3.7	196.0
+7	4.2	195.5
1/4	3.8	195.9
+	3.7	196.0
1/4	3.8	195.9
cb	4.1	195.6
+3	3.5	196.2
+5.5 w. end cobbble walk	3.19	196.48
C. on " "	3.03	196.64

19+00

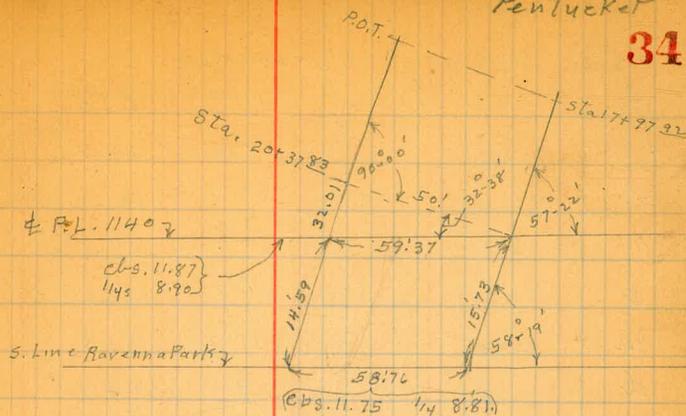
E	4.1	196.6
+	4.3	195.4
cb	4.8	194.9
1/4	4.4	195.3
+	4.5	195.2
1/4	4.6	195.1
+7	4.8	194.9
cb	4.5	195.2
w.	4.1	195.6

19+25

w.	5.4	194.3
cb	5.4	194.3
+1	6.0	193.7
1/4	6.0	193.7
+	5.8	193.9

Pentucket

34



T 199.67

19+25 (con)

1/4	5.8	193.9
cb	6.0	193.8
+2	5.6	194.1
E	5.3	194.4
19+59		
E. on + cmt. Drive	6.99	192.68
+5.5 " " "	7.11	192.56
+8.5 w. end cmt. drive	7.59	192.08
cb	7.8	191.9
1/4	7.4	192.1
+	7.4	192.3
1/4	8.0	191.7
+7	7.7	192.0
cb	7.4	192.3
w.	7.2	192.5

199.67

20+00

W.	9.9	189.8
+8	10.0	189.7
cb	10.6	189.1
1/4	10.2	189.5
±	9.8	189.9
1/4	10.2	189.5
cb	9.8	189.9
E	9.4	190.1

Sta 20+37⁸³

see plat Page 34.

E.	12.1	187.6
+7	12.6	187.1
cb	13.1	186.6
1/4	12.8	186.9
±	12.7	187.0
1/4	12.8	186.9
+6	13.2	186.5
cb	12.3	187.4
W.	12.4	187.3

20+62.13 E = 20+37.83 E
20+69.84 W

± P.L. 1140, on diagonal

59.37 wide
11.47 chs.
2.90 1/4s.

W.	14.8	184.9
cb	14.6	185.1
1/4	14.5	185.2
±	14.0	185.7
1/4	13.7	186.0
cb	13.6	186.1
E	12.1	187.6

20+76.99 E = 20+53.56 E
20+84.43 W 199.67

Pentucket

35

S. line Ravenna Park as staked on ground,
on Diagonal58.76 wide
11.75 chs.
8.81 1/4s.

E.	13.4	186.1
cb	14.3	185.4
1/4	14.7	185.0
±	14.8	184.9
1/4	15.5	184.2
cb	15.5	184.2
+8	15.6	184.1
W.	16.7	183.0

Set. B.M. B.P. Top cont. Wall }
4' E. of E. Line Pentucket }
6' N. of S. line Ravenna Park }

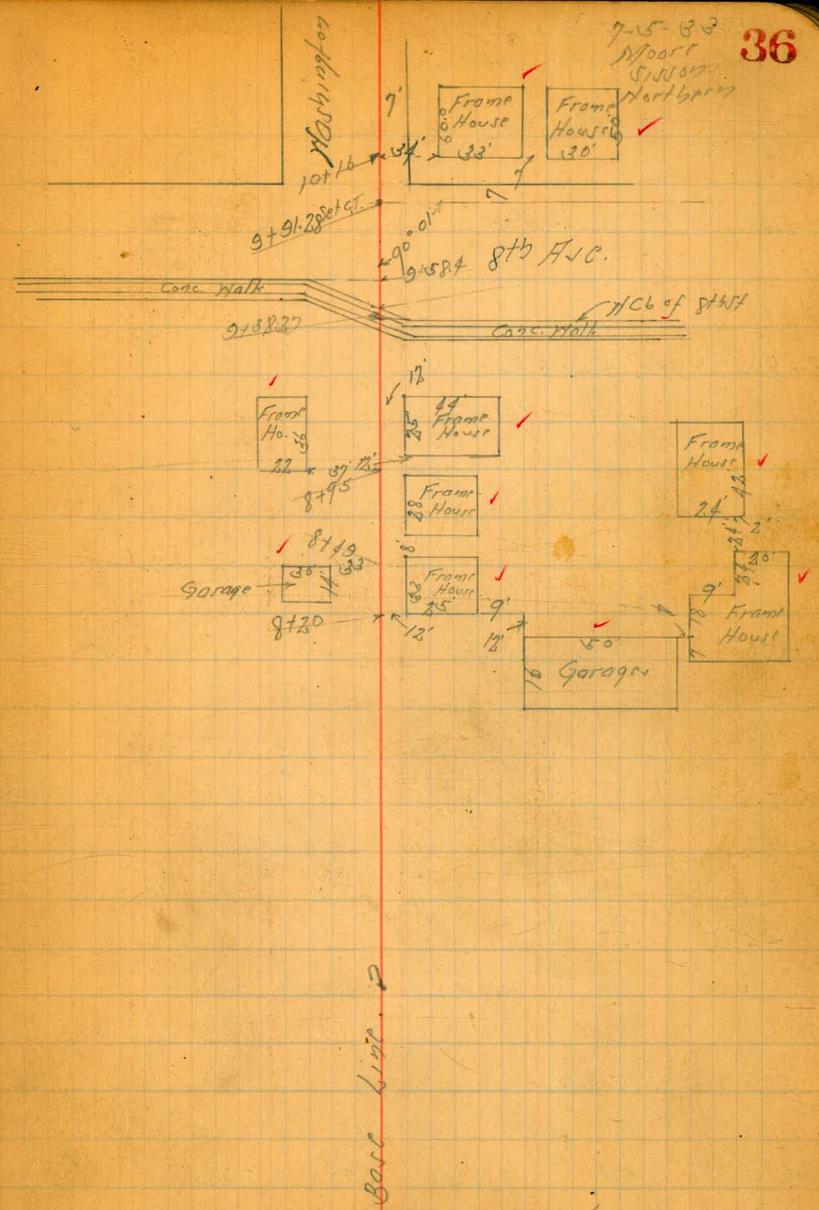
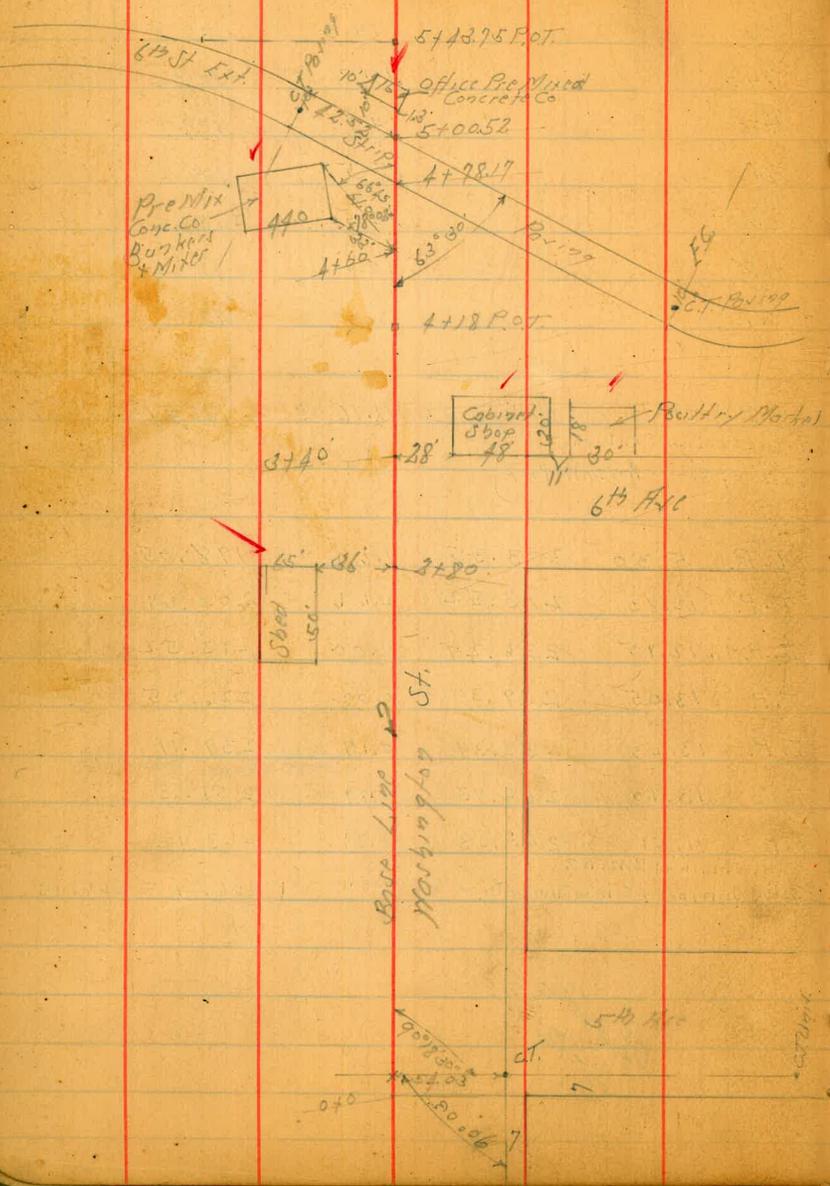
11.16 188.51

T.P.	5.30	203.35	1.62	198.05
T.P.	12.83	213.52	2.66	200.69
T.P.	12.75	226.27	0.00	213.52
T.P.	13.05	239.30	0.02	226.25
T.P.	13.23	252.34	0.19	239.11
T.P.	13.10	264.73	0.71	251.63
T.P.	11.61	275.03	1.31	263.42
chk. original B.M. B.P.				
S.W. Jumper + Commonwealth.			8.64	266.39 = 266.43

Plotted
12-12-32

Washington St. Cross Section
5th Flc to 8th Flc

Indexed
C.S.K.



Washington St Cross Section
5th Ave to 8th Ave.

See Sketch Page 36

3+10 = E.L. Sixth Ave

2+80 = W.L. Sixth Ave

2+0

1+50

0+80

0+485

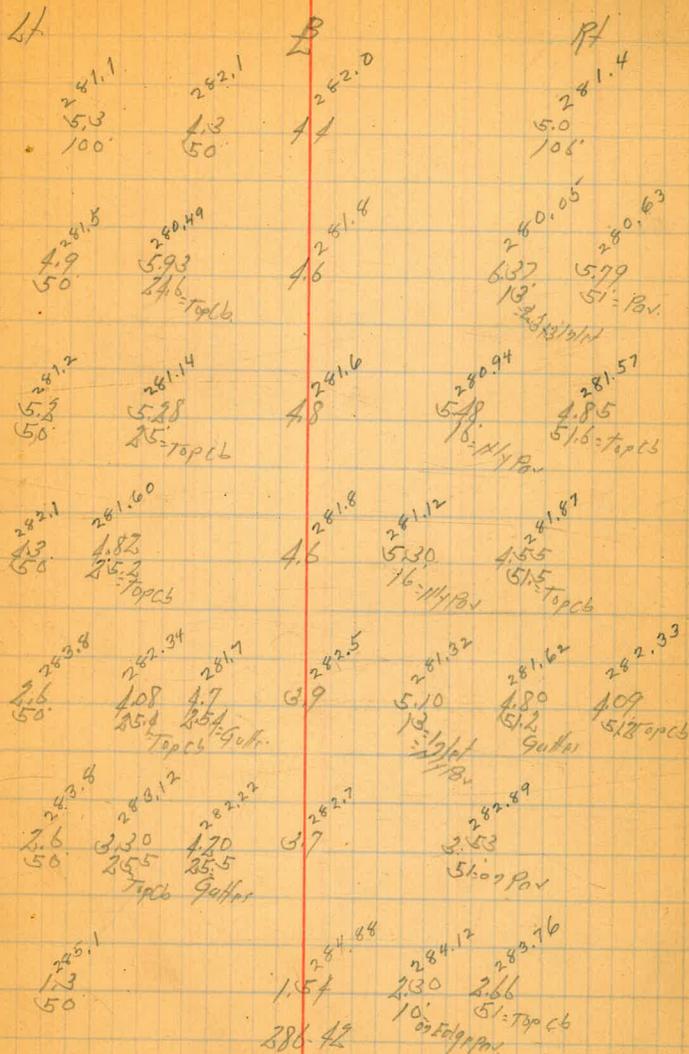
0+0 = W.L. 5th Ave

TP 1.54 286.42 8.06 284.88

BM 3.93 292.44
9 289.01

NYBP
Washington
+ 215 St.

7-6-33 37



TP 1.31 244.77 11.87 243.46

5+13.75

5+18

5+13

5+00.52 Taken on Fly Edge 6th St. Parking

5+00.52 - Fly 6th St. Parking

TP 7.52 255.33 40.82 247.81

TP 6.28 288.63 4.52 282.35

4+78.17

286.87

Nail Pro Mix Plant.

Lt. B. Pt.
 237.9 242.1 244.1 225.6 222.1 220.1 225.9 243.8
 17.4 13.2 11.8 29.7 33.2 35.2 39.4 11.5
 100' 50' 80' 60' 80' 100' 150'
 241.5 241.4 245.0 245.6 232.1 226.6 222.6 223.6 222.4 221.4 219.4
 13.8 13.9 10.3 9.7 8.4 8.7 8.7 8.5 8.4 8.4 8.4
 100' 50' 80' 60' 60' 90' 110' 125'
 261.5 240.5 241.8 245.0
 7.6 14.8 16.5 10.3
 110' 90' 50' 80'
 238.66 241.83 245.11 248.41 251.65 254.97
 15.67 13.50 10.32 6.22 3.68 0.36
 106' 50' 80' 50' 100' 150'
 265.5 262.6 241.7 242.5 245.1 246.8 245.3 26.8 223.9 251.2
 710.2 77.3 13.6 12.8 10.22 8.5 10.0 28.5 31.2 31.2
 100' 85' 67' 25' 24.9 30' 36' 100' 100' 125'
 274.4 271.5 266.5 243.1 245.9
 17.5 15.4 20.4 4.38 41.0
 100' 80' 62' 60' 100'
 250.7 239.5 228.1
 36.2 47.4 58.8
 65' 100' 140'
 286.87

7+10

TP 9.68 266.90 0.25 257.22

6+85

TP 12.71 257.47 0.01 244.76

6+60

6+35

6+10

5+95

5+60

244.77

Lt.	B	Pt
241.4 25.5 100	238.3 28.8 50	235.7 31.2 25
246.5 30.4	255.3 11.6 30	263.5 3.4 45
		263.9 30 100
230.4 26.7 100	229.6 27.9 50	224.8 23.7 38
		242.0 15.5
		252.8 4.7 25
		249.2 8.3 78
		250.2 7.2 100
220.5 24.3 100	225.1 19.7 75	215.6 27.2 45
		228.7 16.1 25
		237.1 5.7
		240.6 4.2 8
		236.8 8.0 18
		237.8 7.0 50
		242.0 2.8 75
		239.9 4.9 100
208.1 36.7 100	210.6 34.2 70	217.1 27.8 50
		223.0 21.8 15
		228.6 18.2
		231.8 13.0 15
		232.2 12.6 25
		234.1 10.7 100
		237.9 6.9 125
205.7 39.1 100	212.8 32.0 43	214.2 30.6 10
		217.7 27.1
		225.5 19.3 50
		231.4 13.4 75
		233.3 11.5 110
		239.9 4.9 135
218.2 36.6 100	220.1 34.7 75	220.2 34.6 50
		222.1 32.7 19
		216.8 28.0
		218.7 26.1 20
		225.0 12.8 50
		231.9 12.9 100
		243.1 1.7 130
238.3 6.5 110	234.2 10.6 95	241.1 3.7 75
		242.3 3.5 50
		248.7 1.1 13
		237.6 7.2
		220.6 24.2 30
		218.5 26.3 55
		220.2 24.6 88
		229.2 15.6 100
		241.0 3.8 135

8753

8714

TP 9.91 288.21 0.15 278.30

7495

7487

7480

TP 12.11 278.45 0.58 266.34

7465

7485

266.90

$\frac{251.1}{6.5/100}$ $\frac{253.2}{5.0/75}$ $\frac{253.8}{4.1/50}$ $\frac{253.6}{5.1/35}$ $\frac{252.8}{5.1/18}$ $\frac{253.2}{5.0/50}$ $\frac{253.7}{4.5/50}$ $\frac{253.6}{4.6/100}$
 $\frac{283.2}{5.0/100}$ $\frac{273.5}{4.7/50}$ $\frac{283.2}{5.0/37}$ $\frac{281.5}{6.7/20}$ $\frac{281.2}{7.0/70}$ $\frac{282.6}{5.8/50}$ $\frac{283.0}{5.2/100}$

$\frac{283.3}{4.8/100}$ $\frac{276.5}{5.0/50}$ $\frac{288.21}{271.4/77}$ $\frac{274.4}{4.1/65}$ $\frac{280.5}{4.2/50}$ $\frac{283.3}{4.8/100}$

$\frac{265.9}{13.0/25}$ $\frac{269.5}{9.0/25}$ $\frac{279.6}{7.0/55}$ $\frac{282.3}{7.8/100}$

$\frac{276.6}{1.9/100}$ $\frac{269.7}{9.8/50}$ $\frac{264.1}{14.4/100}$ $\frac{266.0}{12.5/30}$ $\frac{267.5}{11.0/50}$ $\frac{269.3}{9.2/100}$

$\frac{269.9}{7.0/100}$ $\frac{266.0}{0.9/75}$ $\frac{260.2}{6.7/50}$ $\frac{278.45}{256.9/100}$ $\frac{260.9}{6.0/20}$ $\frac{262.3}{4.6/50}$ $\frac{264.0}{8.9/100}$

$\frac{254.6}{12.3/100}$ $\frac{254.1}{13.8/80}$ $\frac{249.1}{17.8/50}$ $\frac{243.7}{23.2/15}$ $\frac{250.1}{14.8/100}$ $\frac{261.3}{5.6/25}$ $\frac{262.5}{4.5/50}$ $\frac{263.5}{3.1/100}$
 266.90

9+48.3 - N 28° 16' From N

9+91

9+38.27 - N 66° of 816 From South

9+29

9+28

BM 5.87 290.31 284.44 SE Top Hyd Washington St

BM 3.85 284.44 NW B.P. University St 28438

TP 3.85 288.29 3.77 284.44 SE Top Hyd Washington + 816 St

5+0

288.21

Lt. 282.1 8.3/100
 283.8 6.5/100
 284.2 6.1/50
 284.0 6.3/33
 281.7 8.6/22

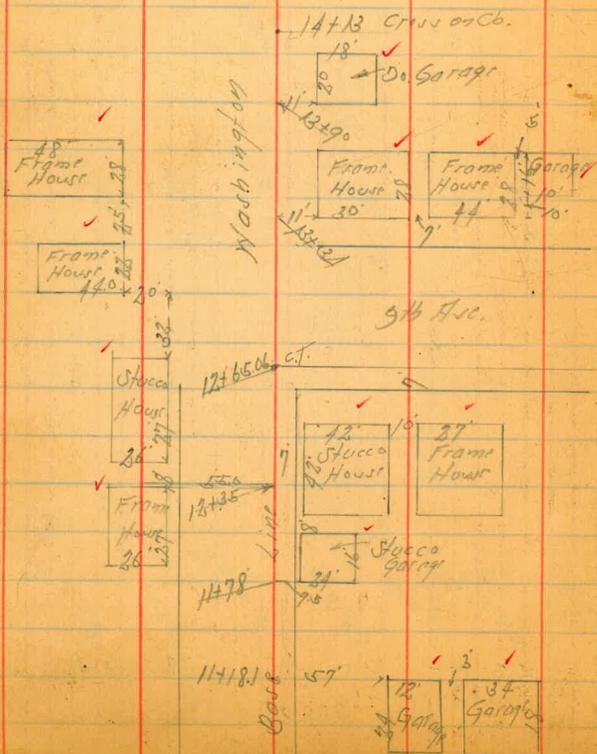
281.8 8.5/50
 280.75 9.48/9
 280.54 9.73/29
 281.6 8.7
 281.9 8.4
 282.8 7.5
 285.0 5.8/10
 284.8 5.5/50
 284.7 5.6/100

281.50 8.8/Top of Arch
 281.72 8.59/50 Top of
 282.00 8.31/100 Top of

284.1 6.2/100
 284.6 5.7/50
 284.7 5.6/25
 282.7 7.6/19
 285.0 5.8/10
 284.8 5.5/50
 284.7 5.6/100

290.31
 288.21

283.2 5.0/100
 284.2 4.0/30
 284.5 3.7/26
 283.7 4.5/20
 284.1 4.1
 285.4 3.8/6
 284.8 3.1/50
 284.7 3.5/100



TP 3.44 282.84 4.65 284.40

12+0

11+281 = 8' Alley From So.

TP 5.11 289.05 6.37 283.94

10+50

9+99

9+98 = E.L. 8^{1/2} from So.

9+8827 = E.C. 8^{1/2} from N

9+584 = W.C. 8^{1/2} from N
290.31

S.W. 7^{1/2} CT
No. 16, 100, 100
+ 9^{1/2} ft

Lt	\$	Pt
6.7 100	282.24	284.6
5.1 50	284.0	285.0
4.9 100	284.2	284.21
4.7 50	284.4	285.26
4.8 100	284.4	285.90
5.2 100	285.0	289.05
4.6 45	285.7	283.2
6.7 43	283.6	283.5
7.1	283.2	286.1
6.8 7	283.5	286.5
4.2 10	286.1	286.6
5.8 50	286.5	
5.7 100	286.6	
4.9 100	285.4	282.05
4.9 45	285.4	282.11
7.6 43	282.7	282.6
8.2 33	282.05	285.5
8.2 33	282.05	286.0
8.2 33	282.05	285.3
7.8 100	282.5	282.4
8.2 33	282.03	282.6
8.2	282.1	
8.0 100	282.31	282.4
8.2 50	282.04	282.6
8.3 43	282.00	
8.9 100	281.36	
8.3 7	282.00	
8.1 50	282.18	
8.1 100	282.36	
8.1 100	281.96	281.67
8.7 50	281.57	281.99
8.8 33	281.45	
9.3 100	281.10	
8.6 50	281.67	
8.3 100	281.99	
8.3 100	290.31	

7-26-33 45
 Moore
 S. West
 Herbert
 Kazary
 Rt

TP 0.87 278.58 13.06 272.71

14+75

14+45

14+13 P.O.T. Cross to Curb

13+60

13+28.06 - E.L. 9th Ave

BM 1.37 285.77

13+18.06 - FCB 9th Ave

12+68.06 - WCB 9th Ave
 282.84

Six 7' of
 water depth
 4.9' 100'

H B

170 76	268.8	263.3	261.5	251.2	240.8	241.4	238.2	240.5
6.5 70	279.3	260.4	25.4	205.4	150 13	144 50	176 66	453 100
4.7 76	281.1	280.9	281.1	281.59	276.0	271.4	262.8	257.7
3.4 60	282.4	282.15	3.9 34-1142	4.8 Topch	9.8 12	14.4 30	25.6 50	32.6 77
3.2 60	282.6	282.67	3.6 28-Topch	3.7 on Pav	3.2 2.0 Topch	3.2 50	282.6	274.5
3.2 60	282.6	282.27	3.5 28-Topch	3.7 on Pav	3.8 17-Topch	3.0 50	283.8	272.5
7.6 100	280.6	282.7	3.0 282-9th	5.0 on Pav	282.46	282.97	283.8	284.3
6.8 100	281.0	283.3	285.77	5.3 on Pav	282.63	283.05	283.8	284.05
4.5 50	283.3	283.63	285.77	5.3 on Pav	283.63	284.37	284.56	284.75
4.3 50	283.3	283.63	285.77	7.0 Topch	283.63	284.37	284.56	284.75

16723

1670

15775

15750

TP

15725

1570

010

261.01

1267

260.91

273.58

Lt.

210.7

50.3
100

215.5

45.5
60

220.0

41.0
30

233.7

27.6

Conc. Garage

12.6

18

22.1

Frame House ✓
3.7
26
15.0

Frame House ✓
17.0

25.2

2.8

17.5

53.5

11.0

272.0

214.5

46.5
100

216.0

45.0
80

219.7

41.3
25

232.8

39.0

242.4

18.6
25

251.3

9.7
50

259.8

1.2
75

274.0

13.0
100

228.5

32.5
85

224.7

32.3
50

222.4

32.6
20

223.6

37.4

233.8

27.2
50

242.3

18.7
40

249.4

11.6
60

261.0

0.0
80

274.0

13.0
100

242.6

18.4
90

238.2

32.2
65

231.5

39.5
60

224.6

36.4

238.0

28.0
25

242.1

18.9
46

250.4

10.2
70

260.3

0.7
85

270.5

19.5
100

255.2

18.4
85

242.2

31.4
45

261.01

34.6
30

232.1

41.5

235.1

38.5
70

241.6

32.0
60

264.4

9.7
100

263.9

9.7
85

250.2

23.4
50

244.6

29.0
25

241.0

32.6

235.4

38.2
10

234.4

39.7
30

236.6

37.0
55

240.3

33.0
60

241.1

32.5
75

248.8

29.8
100

273.58

17+64.6

17+54.40 P.O.T.

17+50

TP 11.87 283.75 0.10 271.88

17+43

17+06

17+06

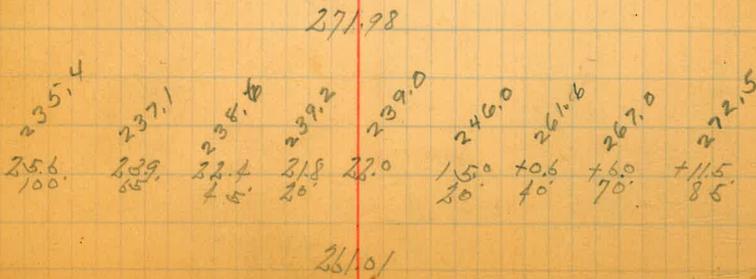
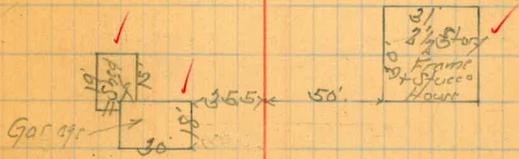
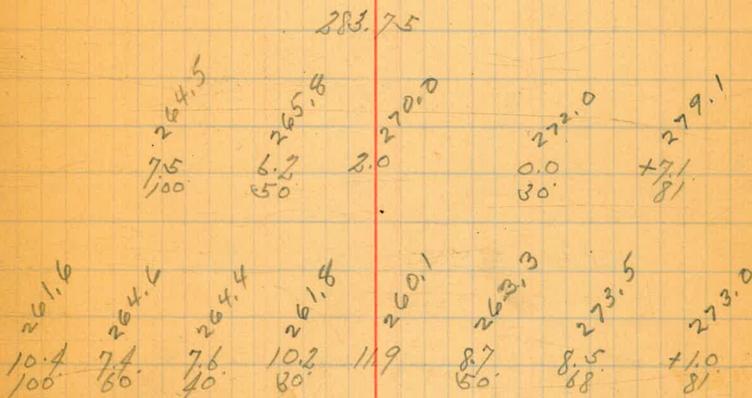
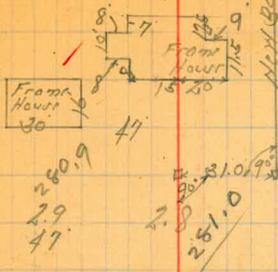
TP 12.09 271.98 1.12 259.89

16+69

261.01

Lt.

Rt.



261.01

19+52

H.
 227.2
 42.4
 140
 235.2
 34.4
 90
 232.7
 36.9
 40.8 Bot Conns
 238.0
 81.6 Bot Conns
 241.8
 27.8
 25 Bot Conns
 247.3
 22.5
 7.5 Bot Conns

19+23

222.4
 17.2
 140
 228.7
 40.9
 90
 239.0
 30.6
 40
 249.0
 30.0
 141
 32
 255.5
 263.5
 66
 80

18+93

235.9
 33.7
 140
 209.5
 30.1
 90
 250.0
 19.6
 27
 8.6
 261.0
 30.0
 38
 269.6
 274.1
 4.5
 50

TP 0.75 269.62 11.54 268.87

269.62

18+51 P.O.T

246.9
 33.5
 140
 252.9
 27.5
 75
 269.1
 11.9
 38
 18+51
 273.0
 7.4
 11
 278.0
 274.2
 4.8
 50

26' French H.

TP 2.05 280.41 5.89 278.36

280.41

18+07.5

271.0
 12.8
 140
 278.3
 5.5
 100
 281.8
 3.0
 50
 280.41
 282.4
 1
 283.2
 50.6
 50

18+07.5 283.25

3.1
 16
 15
 250
 27
 31.0
 27
 27

20+72

20+72

20+51

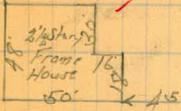
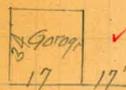
TP 12.87 292.32 210 279.45

TP 11.93 281.55 0.00 269.62

20+21

19+75

269.62



8.0 254.3
140

7.5 254.4
100

8.5 253.4
70

12.7 279.6
50

15.2 277.1
38

10.0 282.3

30.3 272.0
40

15.1 277.2
60

267.0
-2.6
140

269.0
-0.6
115

272.6
+3.0
77

261.9
7.7
36

262.4
7.7
16

267.8
1.8

267.4
2.2
14

260.1
9.5
39

268.1
1.5
60

241.8
27.8
140

245.7
23.9
106

245.3
24.3
50

240.1
29.5
30

244.5
25.1

240.8
23.8
30

251.0
18.6
60

LT

8.4 283.9
140

9.5 286.5
95

7.4 284.9
46

7.2 285.1
72

7-27-33 49

RT

8.1 284.2
32

5.3 287.0
60

292.32

269.62

Next Day

BM			2.98	298.44
TP	7.20	301.42	1.56	294.22

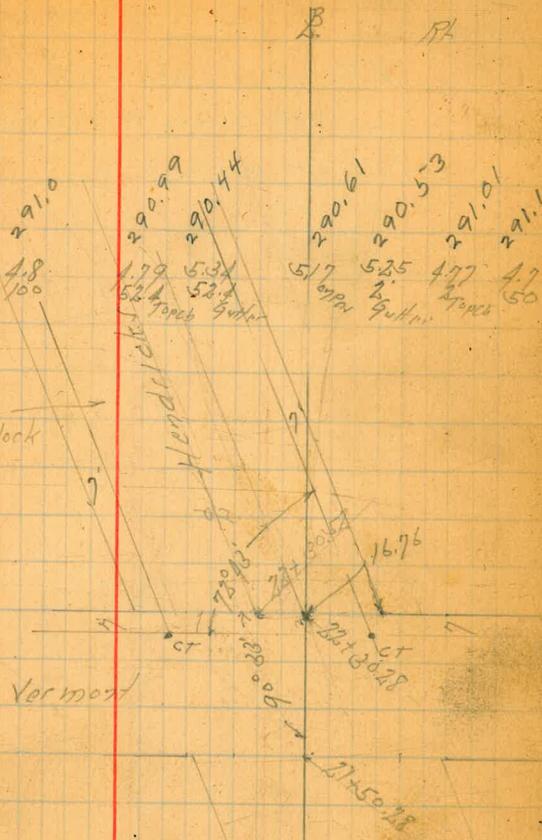
22730.28

Six BP
Hendricks
Richmond
298.48

LT

B RT

Note: See Profile
For this Block



21450.28 = N. Vermont

288.14	288.8	289.01	288.93	288.83	288.31	288.97	288.4
7.7	7.0	6.77	7.15	6.95	7.17	6.81	7.0
100	50	109	109	107	100	100	100
		Topch	Gutter	Topch	Gutter	Topch	Topch

29578

TP	7.15	295.78	2.69	288.63
----	------	--------	------	--------

292.32

292.32

9/27/39 Ties on Commonwealth Ave.

Miller
Walker
Bliss

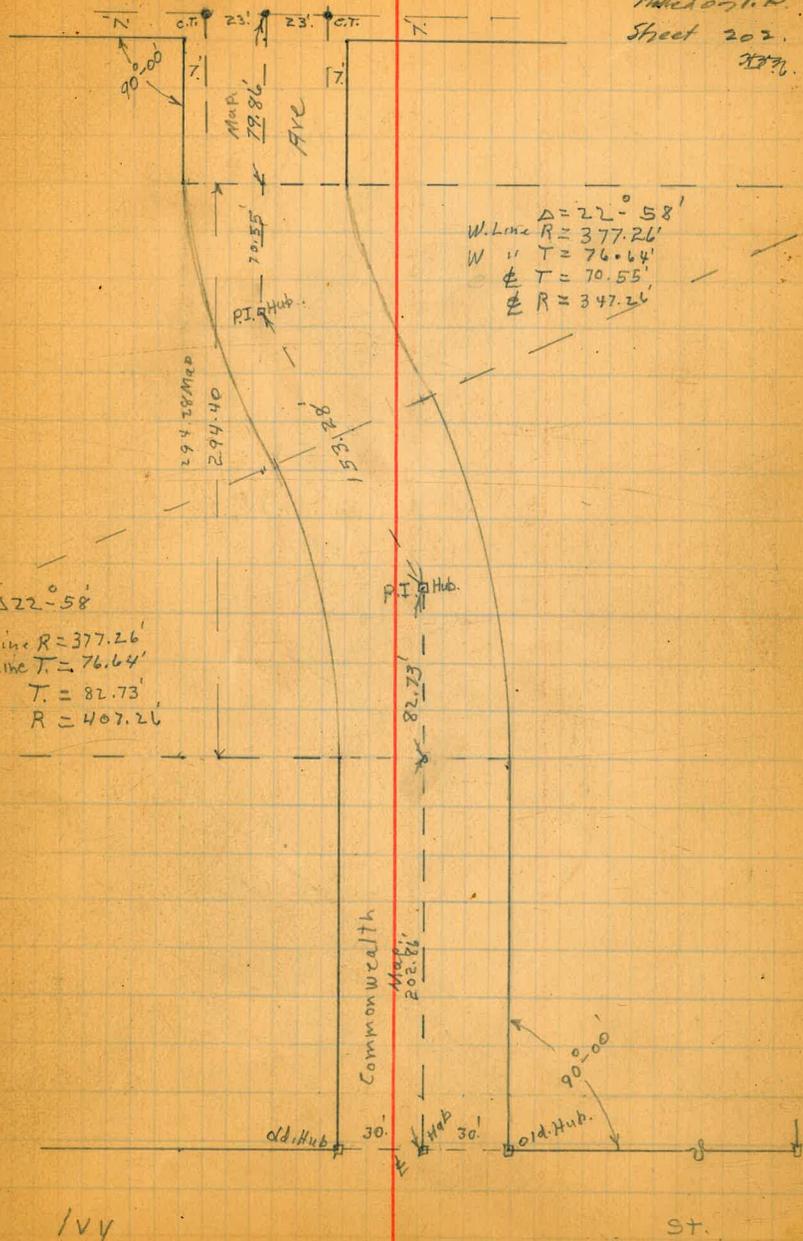
Ivy To Juniper

Indexed
C.S.K.

Note. Map gives $\Delta 23-12'$ W. Line Rad. 375.8
for both Curves. This would not chk. for
Length of Block.

Juniper

St 14th 51
Pentucket T.P.
Sheet 202
1879



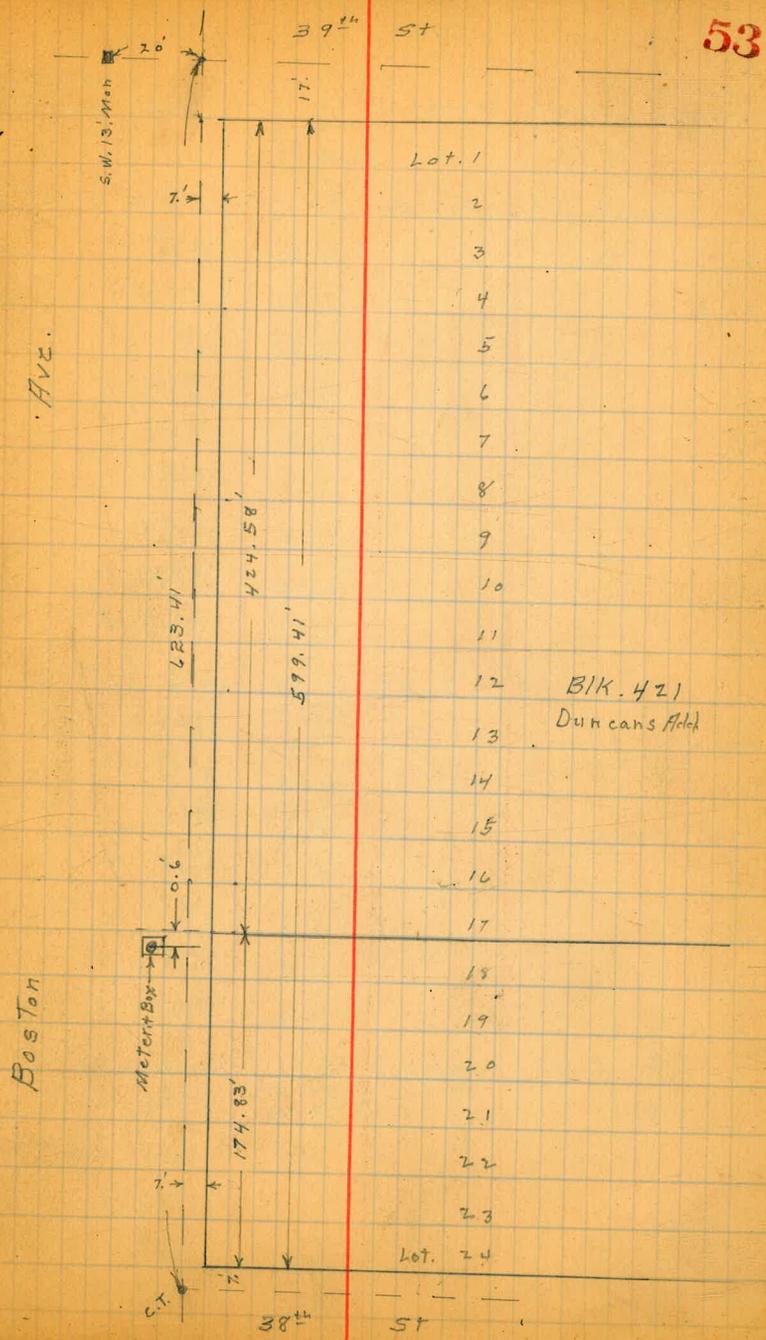
Pentucket. See Page 20. for ties.

Ivy

St.

1-8-35
Meier
Walker
Bliss

Survey BIK. 421 Duncans Adbl
for location of Water Meter



200.08

200.08

0+23

(con)
200.1
6.6

1935 ✓

20.2 Lt

30.3 "

8.4 1917 ✓

0+65⁸⁸

S. Rail S.D.A. RR

8.49 19159 ✓

30.3 Lt Rail

20.2 " "

8.22 19186 ✓

10.1 " "

7.93 19215 ✓

Φ "

7.63 19245 ✓

10.1 Rt "

7.38 19270 ✓

20.2 " "

7.13 19295 ✓

30.3 " "

6.93 19315 ✓

0+70⁴⁴

N. Rail S.D.A. RR.

6.87 19371 ✓

30.3 Rt Rail

20.2 " "

7.10 19298 ✓

10.1 " "

7.35 19275 ✓

Φ "

7.60 19248 ✓

10.1 Lt "

7.90 19218 ✓

20.2 " "

8.21 19187 ✓

30.3 " "

8.50 19158 ✓

0+75 L 81-46 to Φ 62⁴⁴ st.

9.2 190.9 ✓

30.3 Lt

20.2 "

8.8 191.3 ✓

10.1 "

8.6 191.5 ✓

Φ

7.8 192.3 ✓

10.1 Rt

8.0 192.1 ✓

20.2 "

7.8 192.3 ✓

30.3 "

7.7 192.4 ✓

200.08

200.1

0+83 L 81-46

to Φ 62nd

30.3 Rt

8.3 1918 ✓

20.2 "

8.9 1912 ✓

10.1 "

9.2 190.9 ✓

Φ

8.0 1921 ✓

10.1 Lt

9.9 190.2 ✓

20.2 "

11.7 188.4 ✓

30.3 "

13.6 186.5 ✓

1+00 L 81-46 to Φ 62nd

30.3 Lt

14.5 185.6 ✓

20.2 "

13.2 186.9 ✓

10.1 "

11.4 188.7 ✓

Φ

11.4 188.7 ✓

10.1 Rt

11.1 189.0 ✓

20.2 "

10.9 189.2 ✓

30.3 "

9.5 190.6 ✓

1+18⁵⁵ = S. Line Akin St. L 81-46 to Φ 62nd

30.3 Rt

11.0 189.1 ✓

20.2 "

12.1 188.0 ✓

10.1 "

12.4 187.7 ✓

Φ

13.2 186.9 ✓

T.P.

4.12 191.32

12.88 187.20

10.1 Lt

191.3
5.3

20.2 "

5.6 185.9 ✓

30.3 "

6.0 185.3 ✓

55

191.32

1+43⁸⁰ ϕ AK in St. $\angle 81-46$ to ϕ 62nd

30.3 Lt	191.32	6.0	185.3	✓
20.2 "		5.8	185.5	✓
10.1 "		5.4	185.9	✓
ϕ		5.2	186.1	✓
ϕ Granite Mon		5.4	185.68	
10.1 Rt	191.3	4.9	186.5	✓
20.2 "		4.4	186.9	✓
30.3 "		4.0	187.3	✓

1+69⁸⁵ N. Line AK in $\angle 81-46$ to ϕ 62nd

30.3 Rt	N.E. cor 62 nd + AK in	4.2	187.5	✓	cty Date Palm
20.2 "		4.6	186.7	✓	
10.1 "		4.7	186.6	✓	
ϕ		4.8	186.5	✓	
10.1 Lt		5.2	186.1	✓	
20.2 "		5.3	186.0	✓	
30.3 "		5.3	186.0	✓	

1+73³³ at 90°-00 to ϕ 62nd

30. Lt		5.4	185.9	✓
20. "		5.1	186.2	✓
10. "		5.0	186.3	✓
ϕ		4.2	187.1	✓
10. Rt		4.8	186.5	✓
20. "		4.6	186.7	✓
30. "	N.E. cor 62 nd + AK in	4.2	187.1	✓

191.32

62nd St.

56

2+0⁰

30. Rt	191.3	4.2	187.1	✓
20. "		4.3	187.0	✓
10. "		4.3	187.0	✓
ϕ		4.2	187.1	✓
10. Lt		4.5	186.8	✓
20. "		5.0	186.3	✓
30. "		4.6	186.7	✓

2+25

30. Lt		4.2	187.1	✓
20. "		4.2	187.1	✓
10. "		4.0	187.3	✓
ϕ		3.8	187.5	✓
10. Rt		4.3	187.0	✓
20. "		4.2	187.1	✓
29.5 "		3.01	188.31	✓

S. Side Garage
Cmt. floor

2+38

29.5 Rt		3.01	188.31	✓
20. "		4.6	186.7	✓
10. "		5.8	185.5	✓
4. "		5.6	185.7	✓
ϕ		3.8	187.5	✓
10. Lt		3.9	187.4	✓
20. "		3.7	187.6	✓
30. "		4.1	187.2	✓

N. Side Garage
Cmt. floor

191.32

2+56 191.5

30' Lt	4.2	187.1 ✓
20' "	4.2	187.1 ✓
10' "	4.0	187.3 ✓
☐	4.5	186.8 ✓
4' Rt	7.6	183.7 ✓
10' "	7.8	183.5 ✓
16' "	7.7	183.6 ✓
20' "	4.9	186.4 ✓
30' "	3.8	187.5 ✓

2+66

30' Rt	9.4	181.9 ✓
20' "	8.0	183.3 ✓
10' "	8.5	182.8 ✓
3' "	8.4	182.9 ✓
☐	6.2	185.1 ✓
5' Lt	5.4	185.9 ✓
10' "	3.8	187.5 ✓
20' "	4.0	187.3 ✓
30' "	4.2	187.1 ✓

2+75

30' Lt	5.2	186.1 ✓
20' "	6.7	184.6 ✓
10' "	7.3	184.0 ✓
☐	9.5	181.8 ✓
10' Rt	9.7	181.6 ✓
20' "	9.3	182.0 ✓
30' "	9.0	182.3 ✓

S. Side Wash

S. side wash

191.32

62nd St.

57

2+80 191.32

30' Rt	8.9	182.4 ✓
20' "	9.2	182.1 ✓
10' "	9.6	181.7 ✓
☐	9.8	181.5 ✓
10' Lt	9.8	181.5 ✓
20' "	8.2	183.1 ✓
27' "	7.2	184.1 ✓
28' "	4.9	186.4 ✓
30' "	4.9	186.4 ✓

2+85

30' Lt	10.3	181.0 ✓
20' "	10.1	181.2 ✓
10' "	10.0	181.3 ✓
☐	9.8	181.5 ✓
10' Rt	9.5	181.8 ✓
20' "	9.1	182.2 ✓
30' "	8.9	182.4 ✓

2+97

34' Rt. Top. emb. Wall	5.11	186.21 ✓
33' "	8.7	182.6 ✓
30' "	9.0	182.3 ✓
20' "	8.9	182.2 ✓
10' "	9.0	182.3 ✓
☐	9.5	181.8 ✓
10' Lt	10.0	181.3 ✓
20' "	10.4	180.9 ✓
30' "	10.6	180.7 ✓

S. Side Wash

S. Side Wash

N. Side Wash

191.32

3+10 191.32

30' Lt	10.0	181.5 ✓
20' "	9.6	181.7 ✓
10' "	9.4	181.9 ✓
⊕	9.2	182.1 ✓
10' Rt	8.6	182.7 ✓
20' "	8.5	182.8 ✓
22' "	7.6	183.7 ✓
30' "	7.2	184.1 ✓

3+20

30' Rt	7.1	184.2 ✓
22' "	7.2	184.1 ✓
20' "	8.0	183.3 ✓
10' "	8.1	183.2 ✓
6' "	7.7	183.6 ✓
3' "	6.2	185.1 ✓
⊕	5.7	185.6 ✓
16' Lt	7.9	185.6 ✓
20' "	9.3	182.0 ✓
30' "	9.7	181.6 ✓

3+25

30' Lt	7.8	183.5 ✓
20' " Top dyke	4.0	187.3 ✓
10' " " "	4.3	187.0 ✓
5' "	5.8	185.5 ✓
	5.5	185.8 ✓
5' Rt	6.0	185.3 ✓

N. edge wash

N. side wash

N " "

191.32

62nd St

6' Rt	7.8	183.5 ✓
10' "	7.9	183.4 ✓
20' "	7.9	183.4 ✓
22' "	6.2	184.1 ✓
30' "	5.1	186.2 ✓

T.P. 11.26 197.47

3+30

30' Rt	5.1	186.21
	197.5	
	197.47	
	11.4	1861 ✓
	12.1	1854 ✓
22' "		
20' "	13.9	1836 ✓
10' "	13.6	1839 ✓
7' "	13.3	1842 ✓
5' "	12.3	1852 ✓
⊕	11.8	1857 ✓
10' Lt	12.3	1852 ✓
20' "	12.3	1852 ✓
30' Lt. Top dyke	10.8	1867 ✓

3+35

30' Lt	13.0	1845 ✓
20' "	12.4	1847 ✓
10' "	12.2	1853 ✓
⊕	12.2	1853 ✓
6' Rt	12.7	1848 ✓
10' "	13.4	1841 ✓
20' "	13.3	1842 ✓
22' "	12.1	1854 ✓
30' "	11.4	186.1 ✓

58

197.47

3+50

~~197.5~~

11.8

185.7 ✓

30' RT

12.0

185.5 ✓

20' "

11.8

185.7 ✓

10' "

⊕

11.5

186.0 ✓

10' Lt

11.6

185.9 ✓

20' "

12.0

185.5 ✓

30' "

12.0

185.5 ✓

4+00

10.7

186.8 ✓

30' Lt

10.4

187.1 ✓

20' "

10.4

187.1 ✓

10' "

⊕

10.2

187.3 ✓

10' RT

10.4

187.1 ✓

20' "

10.3

187.2 ✓

30' "

9.9

187.6 ✓

4+50

7.0

190.5 ✓

30' RT

7.5

190.0 ✓

20' "

7.9

189.6 ✓

10' "

⊕

7.2

190.3 ✓

10' Lt

7.3

190.2 ✓

20' "

7.5

190.0 ✓

30' "

7.4

190.1 ✓

5+00

0.9

196.6 ✓

30' Lt

0.9

196.6 ✓

20' "

197.47

6 2nd ST

59

~~197.5~~

1.2

196.3 ✓

10' Lt

1.1

196.4 ✓

⊕

1.7

195.8 ✓

10' RT

1.3

196.2 ✓

20' "

1.6

195.9 ✓

30' "

T.P.

11.29 208.65

0.11

197.36

5+25

~~208.7~~

9.0

199.7 ✓

30' RT

9.2

199.5 ✓

20' "

9.3

199.4 ✓

10' "

⊕

9.0

199.7 ✓

10' Lt

9.0

199.7 ✓

20' "

8.6

✓00.1 ✓

30' "

8.2

✓00.5 ✓

5+50

5.4

✓03.3 ✓

30' Lt

5.8

✓02.9 ✓

20' "

6.3

✓02.4 ✓

10' "

⊕

6.3

✓02.4 ✓

5' RT

7.5

✓01.2 ✓

10' "

7.2

✓01.5 ✓

20' "

7.1

✓01.6 ✓

30' "

6.6

✓02.1 ✓

208.65

6+00

708.7

2.8

7059 ✓

30' Rt

3.0

7057 ✓

20' "

2.8

7059 ✓

10' "

3.0

7057 ✓

6' "

2.3

7064 ✓

d

2.1

7066 ✓

10' Lt

1.5

7074 ✓

20' "

1.1

7076 ✓

30' "

T.P.

465

212.70

0.60

208.05

T.P.

2.94

208.65

6.99

205.71

continued on page 72.

62nd St.

60

208.65
 208.7
 208.65
 0+42

15' Lt	4.6	✓04.1 ✓
6' "	4.7	✓04.0 ✓
4' "	6.7	✓07.0 ✓
⊕	6.7	✓07.0 ✓
8' Rt	6.6	✓07.1 ✓
9' "	4.4	✓04.3 ✓
15' "	4.7	✓04.0 ✓

0+44

15' Rt.	8.7	✓00.0 ✓	s. side wash.
8' "	7.4	✓01.3 ✓	
⊕	7.2	✓01.5 ✓	
6' Lt	7.0	✓01.7 ✓	
8' "	4.7	✓04.0 ✓	
15' "	4.8	✓03.9 ✓	

0+60

15' Lt	5.7	✓03.0 ✓	
19' "	5.9	✓02.8 ✓	
8' "	8.4	✓00.3 ✓	s. side wash
⊕	8.8	199.9 ✓	
10' Rt	10.0	198.7 ✓	
15' "	10.0	198.7 ✓	

0+63

15' Rt	10.0	198.7 ✓	
10' "	10.0	198.7 ✓	
⊕	9.0	199.7 ✓	
15' Lt	9.1	199.6 ✓	s. edge Wash

208.65
 208.65
 208.7
 0+80

64th St 62

15' Lt	9.7	199.0 ✓	
10' "	10.4	198.3 ✓	
⊕	10.5	198.2 ✓	
15' Rt.	9.4	199.3 ✓	

0+95

15' Rt	9.2	199.5 ✓	N. side Wash
⊕	9.5	199.4 ✓	
4' Lt	9.7	199.0 ✓	
5' "	10.5	198.2 ✓	
15' "	10.8	197.9 ✓	

1+05

15' Lt	10.6	198.1 ✓	
7' "	10.0	198.7 ✓	
6' "	9.1	199.6 ✓	
⊕	9.0	199.7 ✓	
6' Rt.	9.1	199.6 ✓	N. side Wash
11' Rt.	6.0	✓07.7 ✓	
15' "	5.3	✓03.4 ✓	

1+15

15' Rt	4.9	✓03.8 ✓	
10' "	5.3	✓03.4 ✓	
5' "	8.5	✓00.2 ✓	
⊕	8.6	✓00.1 ✓	
6' Lt	8.4	✓00.3 ✓	
8' "	9.9	198.8 ✓	N. side Wash
15' "	10.3	198.4 ✓	" " "

208.65

1+20 $\frac{208.65}{208.7}$
4.4

15' LT		4.4	✓04.5 ✓
10' "		4.8	✓03.9 ✓
7' "		7.5	✓01.2 ✓
⊕		8.0	✓00.7 ✓
5' RT		7.7	✓01.0 ✓
8' "		5.2	✓03.5 ✓
15' "		4.7	✓04.0 ✓

1+30

22' RT	⊕ dirt Floor Garage	4.7	✓04.0 ✓
15' "		5.2	✓03.5 ✓
5' "		6.9	✓01.8 ✓
⊕		7.1	✓01.6 ✓
7' LT		6.8	✓01.9 ✓
10' "		4.9	✓03.8 ✓
15' "		4.3	✓04.4 ✓

1+60

15' LT		4.6	✓04.1 ✓
⊕		4.6	✓04.1 ✓
15' RT		5.0	✓03.7 ✓

1+86

22.5' RT	⊕ dirt Floor garage	4.5	✓04.2 ✓
----------	---------------------	-----	---------

2+00

15' RT		4.3	✓04.4 ✓
⊕		4.2	✓04.5 ✓
15' LT		4.2	✓04.5 ✓

208.65

208.7

2+26

16.5' LT	⊕ dirt Floor garage	3.5	✓05.2 ✓
15' "		3.5	✓05.2 ✓
⊕		3.2	✓05.5 ✓
15' RT		3.5	✓05.2 ✓

2+50

15' RT		2.2	✓06.5 ✓
⊕		2.1	✓06.6 ✓
15' LT		1.9	✓06.8 ✓

T.P.	72.83	218.10	3.38	205.27	
T.P.	8.32	225.16	1.26	216.84	S.W. Akin
R.M. Spk.			4.59	220.57	⊕ 66 th St.
				=220.56	

continued on Page 75

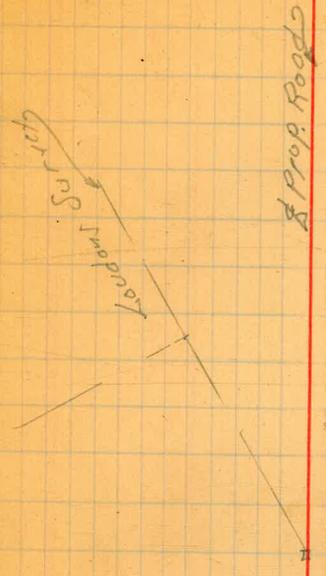
Alignment
8+88.70 North
1402/65

Proposed Ext. of 54th St.
Collector to Mission Valley Road Through
Marcellino Tract.
Alignment

10+19.17 P.O.T.

8+88.70 P.O.T.

Indexed
c.s.K.



10+19.17

8+88.70

From Collector to
Sta 8+88.70 Same
as 1364 Page 28

Rt.

+6911	F.C.	17° 02'
+50		15° 56.30'
17+0	A 34° 04'	13° 04.41'
+50	P.O.C. R 500.0	10° 12.53'
16+0	T 152.18	7° 20.64'
+50	A 227.29	4° 28.76'
15+0	D 3.7377	1° 36.87'
14+71.82	B.C.	

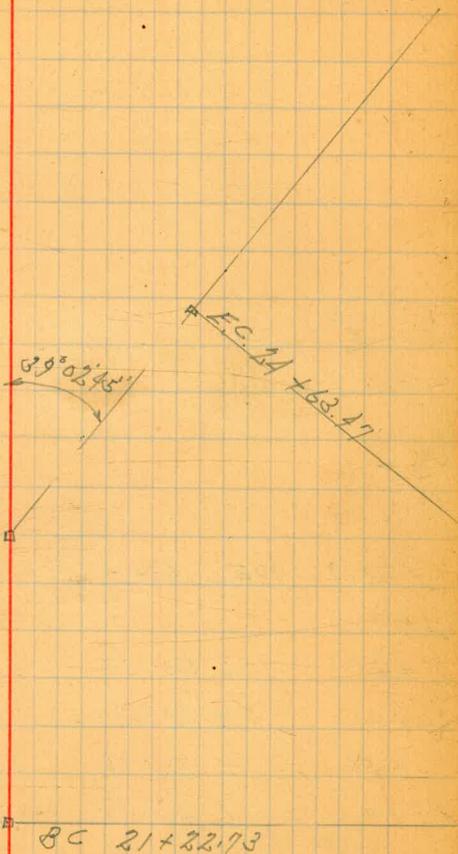
34° 04'

F.C. 17+69.11

B.C. 14+71.82

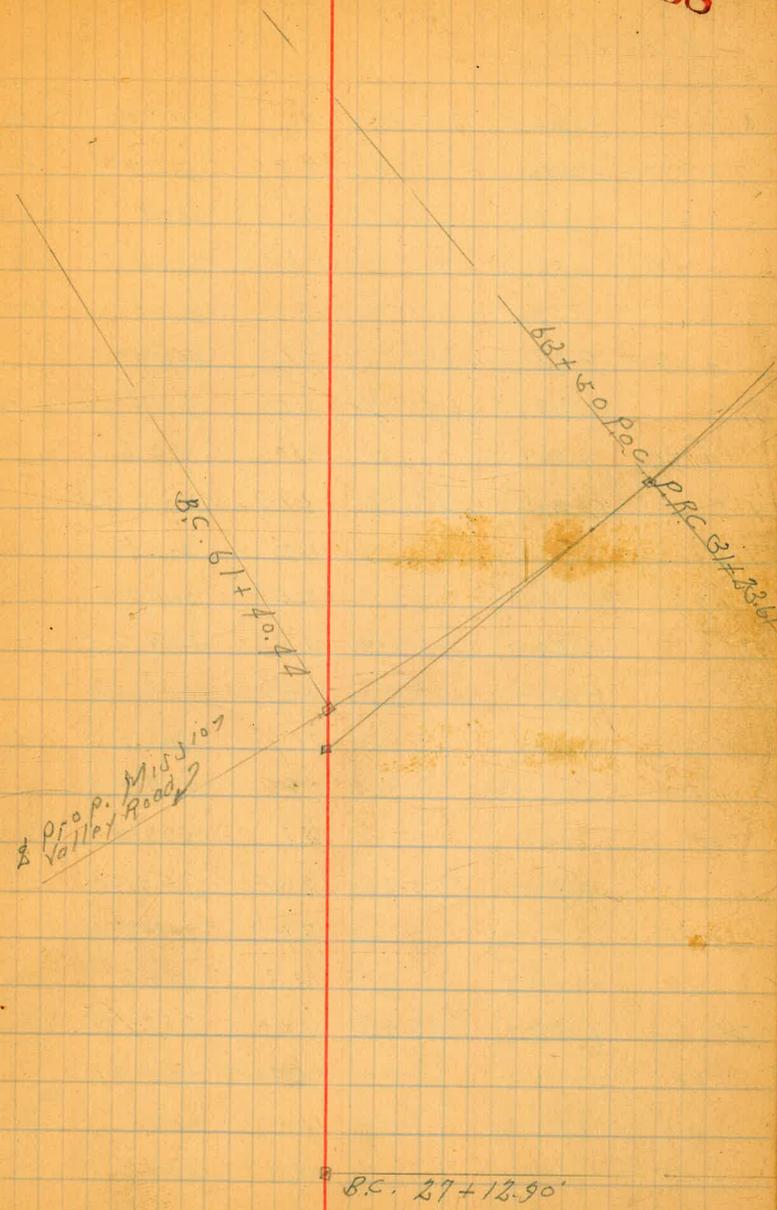
Rt.

+63.47	EC		19° 31.36'
+50			18° 45.06'
24+0	A	39° 02' 45"	15° 53.17'
+50	R	500'	13° 01.29'
28+0	T	177.27	10° 09.40'
+50	L	340.74	7° 17.52'
22+0	D	3.4377	4° 25.63'
+50			1° 33.75'
21+22.73	BC		



PL

+ 22.61	P.R.C. = 63+50	26° 48.50
31+0		25° 15.88
+ 50	A 53' 37	22° 00.08
30+0	R 438.89	18° 44.28
+ 50	T 231.78	15° 38.48
29+0	L 410.71	12° 12.68
+ 50	D 3.916	8° 56.88
28+0		5° 41.08
+ 50		2° 25.28
27+12.90	BC	



Proposed Ext. of 54th St.
 Collier to Mission Valley Road
 & Levels

B.M	2.84	358.94	356.10	07 Hub 8+88.70 B.C. 1864-P39
8+88.70 P.O.T.		2.8	356.1	
9+70		3.1	355.8	
+50		5.6	353.3	
10+0		11.1	342.8	
+19.17 P.O.T. = Old P.L.		14.12	344.82	
TP	0.89	345.71	344.82	10+19.17 07 Hub
+50		9.1	336.6	
TP	0.05	332.58	332.53	
11+0		11.5	321.1	
+28		18.3	314.4	
TP	0.54	319.99	319.45	
TP	0.31	307.23	306.92	
+50		3.6	303.6	
+65		8.8	298.4	
12+0		14.2	293.0	
TP	0.87	295.28	294.41	
+25		7.0	288.3	
+50		13.3	282.0	
TP	1.39	283.61	282.22	
+75		15.4	268.2	
13+0		16.5	267.1	
+45		18.3	265.3	
+50 - Sly Wash		20.1	263.5	
+75 = 11/4 "		20.3	263.3	

283.61

Aug 28-35 69
 S. J. J. 07
 Northey
 Walker

13+80		19.0	264.6	
14+0		19.5	264.1	
+35		21.5	262.1	
+40		20.0	263.6	
+50		19.8	263.8	
+71.82 B.C. P.L.		16.6	262.0	
15+0		8.0	275.6	
+34		5.6	278.0	
+40 = Sly Wash		9.8	273.8	
+50 = 11/4 "		9.6	274.0	
TP	12.72	296.01	0.32	283.29
16+0		0.9	295.1	
TP	12.16	307.96	0.21	305.80
+20		4.0	304.0	Top of Station 16+0
TP	12.61	320.27	0.30	307.66
+50		9.9	310.4	
17+0		3.0	317.3	
TP	12.72	332.70	0.29	319.98
+50		8.2	324.52	
+69.11 F.C.		4.75	327.95	07 Hub
TP	13.09	345.41	0.38	332.32
18+0		12.5	332.9	
+50		3.8	341.6	
TP	13.16	358.34	0.23	345.18
19+0		8.7	349.6	

358.34

19+50			1.5	356.8	
TP	13.12	370.85	0.61	357.73	
20+0			8.0	362.9	
+50			0.4	370.5	
TP	12.18	382.81	0.22	370.63	
21+0			5.9	376.9	
+22.73 B.C. Pt			2.00	380.8	07 Hub
TP	12.99	394.85	0.95	381.86	
+50			9.3	385.6	
22+0			1.3	393.6	
TP	13.38	406.70	0.53	394.32	
+50			3.5	403.2	
TP	11.41	417.72	0.39	406.131	
+75			10.2	407.5	
23+0			8.1	409.6	
+25			5.0	412.7	
+50			4.2	413.5	
+75			3.6	414.1	
24+0			5.2	412.5	
+50			7.5	410.2	
+63.47 F.C.			8.55	409.17	07 Hub
TP	0.81	405.26	13.27	404.45	
25+0			2.4	402.9	
+50			8.1	397.2	

70

405.26

TP	039	393.18	12.37	392.89	
26+0			2.1	391.1	
+40			4.8	388.4	
+50			5.8	387.4	
27+0			9.6	383.6	
+12.90 B.C. Pt.			10.03	383.15	07 Hub
+50			9.7	383.5	
+65			6.8	386.4	
28+0			3.3	389.7	
TP	13.13	406.15	0.16	393.02	
+50			9.3	396.9	
+65			6.0	400.2	
TP	12.77	418.56	0.36	405.79	
+85			14.7	403.9	
29+0			13.3	405.3	
TP	13.02	431.18	0.40	418.16	
+25			17.3	413.8	
+35			12.8	418.4	
+50			9.7	421.5	
+75			4.1	427.1	
B.M.			9.58	421.60	07 Hub 61+40.44 17.08107 Pt. 421.78
TP	12.47	443.37	0.28	430.90	
30+0			11.0	432.4	
+10			8.8	434.6	

443.37

30 + 50

4.3

439.1

TP

5.86

448.29

0.94

442.43

31 + 0

5.6

442.7

+ 23.61 = 63 + 50 PRC.
Missioo Valley Pa.

5.3

443.0

1-29-36 62nd St. X Sec. AKins to Brooklyn.

Miller
Walker
Bliss

Continued from Page 54.

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Indexed
C.S.K.

223.66

72

BM. & Mon.	12.80	198.48		185.68	62 nd AKins.
T.P.	12.97	<u>211.02</u>	0.43	198.05	
		6+50			
30' Lt			+0.7	211.7	
20' Lt			+0.4	211.4	
10' "			-0.8	210.2	
∅			1.0	210.0	
7' Rt			2.3	208.7	
10' "			2.1	208.9	
20' "			1.9	209.1	
30' "			1.9	209.1	
T.P.	12.81	223.66	0.17	210.85	
		7+00			
30' Rt			10.8	212.9	
20' "			10.4	212.9	
14' "			10.3	213.4	
10' "			10.7	213.0	
7' "			10.8	212.9	
∅			9.8	213.9	
10' Lt			8.9	214.8	
20' "			8.6	215.1	
30' "			8.2	215.5	
		7+50			
30' Lt.			5.0	218.7	
20' "			5.1	218.6	

10' Lt.					
∅					
5' Rt					
10' Rt.					
15' "					
20' "					
30' "					
		8+00			
30' Rt			2.6	221.1	
20' "			2.6	221.1	
14' "			2.2	221.5	
10' "			2.5	221.2	
5' "			2.8	220.9	
∅			1.6	222.1	
10' Lt			1.7	222.0	
20' "			1.2	222.5	
30' "			1.3	222.4	
T.P.	12.85	236.29	0.22	223.44	
		8+50			
30' Lt			9.0	227.3	
20' "			9.2	227.1	
10' "			9.3	227.0	
∅			9.2	227.1	
4' Rt			10.2	226.1	
10' "			9.9	226.4	
20' "			10.2	226.1	
23' "			10.5	225.8	

236.29

8+50 (con)

24' RT	9.8	226.5
30' "	10.2	226.1

9+00

30' RT	4.6	231.7
25' "	4.3	232.0
22' "	5.5	230.8
20' "	5.5	230.8
10' "	5.1	231.2
Φ	5.5	230.8
10' Lt	5.7	230.6
20' "	6.0	230.3
30' "	6.5	229.8

9+50

30' Lt.	6.2	230.1
20' "	5.2	231.1
10' "	4.4	231.9
Φ	3.7	232.6
10' RT	3.3	233.0
20' "	2.8	233.5
23' "	2.7	233.6
24' "	1.5	234.8
30' "	1.1	235.2

10+00

30' RT	0.6	235.7
23' "	2.1	234.2
20' "	2.4	233.9

236.29

62nd St.

73

10' RT	3.1	233.2
8' "	2.6	233.7
Φ	4.4	231.9
10' Lt	5.5	230.8
20' "	7.2	229.1
30' "	8.1	228.2
40' "	9.0	227.3

10+50

40' Lt	6.0	230.3
30' "	6.6	229.7
20' "	6.1	230.2
10' "	5.6	230.7
Φ	5.0	231.3
10' RT	3.4	232.9
20' "	3.2	233.1
27' "	3.2	233.1
30' "	1.9	234.4

T.P. 12.05 245.27 3.07 233.22

11+00

40' RT	9.3	236.0
30' "	11.2	234.1
27' "	12.1	233.2
20' "	11.9	233.4
10' "	12.0	233.3
Φ	12.5	232.8
5' Lt	12.2	233.1

245.27

11+00 (con)

10' Lt.	10.7	234.6
20 "	9.3	236.0
30 "	8.2	237.1

11+50

30' Lt	4.5	240.8
20' "	5.5	239.8
10' "	6.7	238.6
±	8.4	236.9
3 RT	9.5	235.8
10' "	9.5	235.8
20' "	10.0	235.3
30' "	10.1	235.2
35' "	10.0	235.3
50' "	6.4	238.9

11+94 = S. Line Brooklyn.

43' RT	6.0	239.3	
30' "	6.6	238.7	
20' "	6.5	238.8	
10' "	6.2	239.1	
±	5.4	239.9	
2' Lt	5.4	239.9	
3' "	4.5	240.8	
10' "	3.8	241.5	
20' "	2.3	243.0	
20' "	1.3	244.0	
Nail in T.P. Pale 12.94	257.60	0.61	244.66

S.W. 62nd
+ Brooklyn.

257.60

62nd St.

74

11+94 (con)

30' Lt.	13.4	244.2
---------	------	-------

12+24 = ± Brooklyn.

300' Lt	7.0	250.6
250' "	5.6	252.0
200' "	5.1	252.5
150' "	5.7	251.9
100' "	7.2	250.4
50' "	10.4	247.2
30' "	12.3	245.3
±	14.2	243.4
30' RT = East	14.8	242.8
50' " "	13.7	243.9
100' " "	8.6	249.0
150' " "	4.6	253.0
200' " "	0.8	256.8

T.P. 13.12 270.16 0.56 257.04

250 East 9.2 261.0

300 " 4.4 265.8

T.P. 7.20 277.11 0.25 269.91

350' East 6.1 271.0

405.6 = W. Line 63rd St. 1.7 275.4BM Top Fire Hdt. 5.82 271.29 S.E. 63rd
+ Brooklyn.

BM 0.10 271.39 271.29

4+65th = E. Line 63rd St. + 1.8

5+00 + 0.8

± Brooklyn

228.54

3+50

15' RT	4.0	224.5
11' "	4.2	224.3
10' "	5.0	223.5
Φ	4.7	223.8
10' LT	5.0	223.5
15' "	4.1	224.4
T.P.	12.44	240.79
	0.19	228.35

3+75

15' LT	12.4	228.4
Φ	12.0	228.8
10' RT	12.3	228.5
11' "	11.6	229.2
15' "	11.6	229.2

4+00

15' RT	7.5	233.3
11' "	8.3	232.5
10' "	9.0	231.8
Φ	8.2	232.6
15' LT	8.8	232.0

4+25

15' LT	5.5	235.3
Φ	5.3	235.5
10' RT	5.8	235.0
11' "	4.9	235.9
15' "	4.3	236.5

64th St.

76

240.79

4+50

15' RT	1.2	239.6
11' "	2.0	238.8
10' "	3.0	232.8
Φ	2.6	238.2
15' LT	3.2	232.6
T.P.	7.64	247.17
	1.26	239.53

4+75

15' LT	7.7	239.5
Φ	7.3	239.9
10' RT	7.2	240.0
15' RT	6.4	240.8

→ 4+72 out of position

28' RT Garage floor dirt	5.2	241.97
--------------------------	-----	--------

5+00

15' RT	4.4	242.8
11' "	4.7	242.5
10' "	6.9	241.2
Φ	6.2	241.0
15' LT	7.6	239.6
20' "	7.9	239.3

5+50

20' LT	8.0	239.2
15' "	6.8	240.4
Φ	4.8	242.4
13' RT	4.3	242.9
15' "	2.6	244.6
20' "	2.4	244.8

247.17

6+00

20' RT	3.2	244.6
15' "	3.9	243.3
♀	4.7	242.5
15' Lt	7.3	239.9
20' "	8.2	239.0

6+50

20' Lt	10.0	237.2
15' "	9.1	238.1
♀	5.5	241.7
2' RT	4.0	243.2
15' "	4.5	242.7
20' "	4.0	243.2

6+75

20' RT	4.6	242.6
15' "	5.2	242.0
7' "	8.1	239.1
♀	8.8	238.4
15' Lt	10.9	236.3
20' "	11.6	235.6

7+00

20' Lt	14.3	232.9
15' "	14.0	233.2
♀	12.5	234.7
15' RT	10.3	236.9
20' "	9.5	237.7
T.P.	3.75	238.94
	11.98	235.19

238.94

7+27

25' RT	5.3	233.6
15' "	8.0	230.9
♀	13.0	225.9
15' Lt in wash	16.8	222.1
40' " " "	18.5	220.4

7+40

40' Lt	15.7	223.2
15' "	16.3	222.6
♀ in wash	17.2	221.7
10' RT	15.0	223.9
15' "	12.8	226.1
30' "	7.0	231.9

7+57

40' RT	7.7	231.2
26' "	13.0	225.9
15' " in wash	17.0	221.9
12' "	15.4	223.5
♀	14.4	224.5
15' Lt	13.0	225.9
40' "	11.5	227.4

7+75

40' Lt	8.5	230.4
15' "	9.9	229.0
♀	11.0	227.9
15' Lt Rk	13.8	225.1
25' Lt in wash Rk	16.2	222.7
40' " Rk	11.3	227.6

64th St.

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238.94

8400

40' RT		13.0	225.9
33' "	17' Wash.	15.0	223.9
15' "		10.5	228.4
♀		7.6	231.3
15' LT		6.8	232.1
25' "		6.2	232.7

8+32⁸⁵ = S. Line Brooklyn Ave

20' LT		2.1	236.8
15' "		2.2	236.7
♀		4.0	234.9
15' RT		6.6	232.3
37' "	w. side wash	12.2	226.7
50' "	E " "	11.8	227.1

8+62⁸⁵ = ♀ Brooklyn

15' RT		3.3	235.6
♀		1.0	237.9
15' LT		+3.4	242.3

8+92⁸⁵ = N. Line Brooklyn

15' LT		+4.5	243.4
♀		+1.0	239.9
15' RT		1.0	237.9

64th St

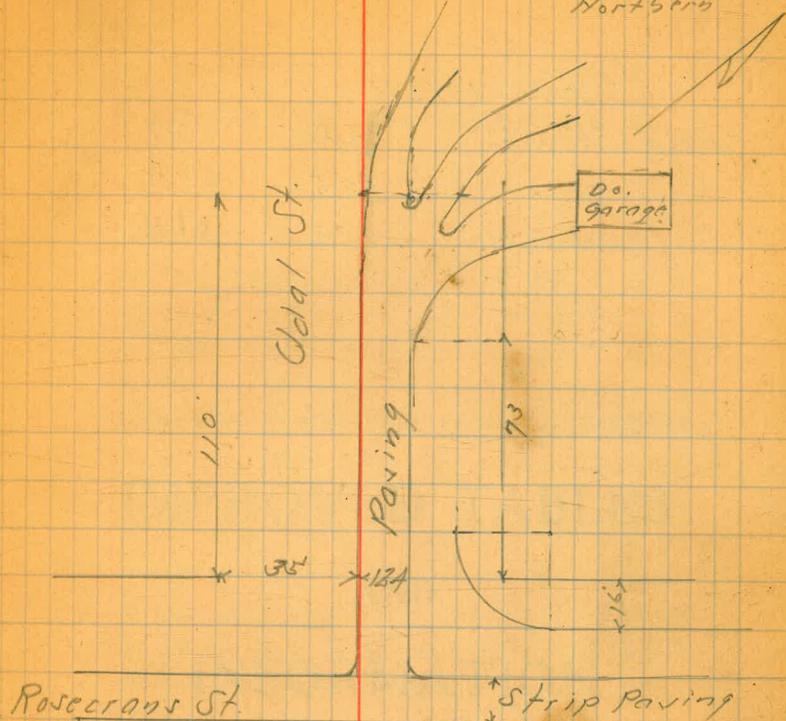
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Udal St. Levels on Strip Paving
West of Rosecrans

BM	8.27	22.19	13.92	N.W.B.P. Rosecrans Udal
16' E of N.L. Rosecrans = C&G line				
S Edge Strip Pav		11.18	11.01	
15' N = N Edge Pav		10.82	11.37	
N.L. Rosecrans				
S Edge Strip Pav		9.36	12.83	
12.4' N = N Edge		9.29	12.90	
25' W of N.L. Rosecrans				
S Edge Strip Pav		6.12	16.17	
12.2' N = N Edge "		6.21	15.98	
50' W of N.L. Rosecrans				
S Edge Strip Pav		2.92	19.27	
12' N = N Edge "		2.77	19.42	
TP	8.48	20.35	0.32	21.87
73' W of N.L. Rosecrans				
S Edge Paving		8.01	22.34	
12' N = N Edge Pav		7.97	22.38	
92' W of N.L. Rosecrans = Opp. of De Garage				
1' N of 2 = S Edge Pav.		5.48	24.87	
15' N of 2		5.10	25.25	
21' N of 2		5.48	24.87	
49' N of 2 = De Garage C&G Floor 16' SW side		4.21	26.14	

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C.S.K.

Nov. 15 1928
Siron 79
Northboro



3035

110' N of W L. Puccran

2.5' N of $\frac{1}{2}$ = S Edge Pav	298	27.37
13' N of $\frac{1}{2}$ = 0.7 Pav	265	27.70
131' N of $\frac{1}{2}$ = N Edge	125	29.10

DIRECTIONS FOR USE OF TABLES

TABLE No. 1

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in both

IMPROVED TABLES

AND

INFORMATION

TABLE No. 2
To find Tangent and External for curve of any other degree, divide by degree of curve and add connection found in column of connections. Degree of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external).
The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

363.97
5
781.985

40°
64-28-3

3738 211.
328V 8.8
450 202.2
237
693 4.6
2064

269.91
6.54
276.45
5.16
271.29
277.11
5.82

2.8 3.8
1.2 19
+

204.2
123
2165

21.45
62.85
84.30

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