1443

See Book # 1441/1 for Location of Sections "B", "D" & "F"

## Contents



ED



Indexed
C.S.K.

SERA WEEKLY COST SEGREGATION SHEET

NAME OF PROJECT Recreational Area NO 38-B11-4A WEEK ENDING ~~THURS~~ WED Nov 28-34

| Kind of Work | Charge | ~~Fri.~~ Thu | ~~Sat.~~ Fri | ~~Mon.~~ Sat | ~~Tues.~~ Mon | ~~Wed.~~ Tue | ~~Thurs.~~ Wed | Total |
|---|---|---|---|---|---|---|---|---|
| DRILLING HOLES | SERA Payroll | 12.75 | | | | | | |
| | Supervision | .44 | | | | | | |
| | Spons.Labor | 4.28 | | | | | | |
| | Equip.Rental | 24.00 | | | | | | |
| | Mat'l Spons. | | | | | | | |
| | " CWA SERA | | | | | | | |
| RAKING ROCK | SERA Payroll | 10.35 | | | | | | |
| | Supervision | .30 | | | | | | |
| | Spons.Labor | | | | | | | |
| | Equip.Rental | | | | | | | |
| | Mat'l Spons. | | | | | | | |
| | " CWA SERA | | | | | | | |
| SURFACE ROQUE COURT | SERA Payroll | 19.95 | | | | | | |
| | Supervision | .90 | | | | | | |
| | Spons.Labor | | | | | | | |
| | Equip.Rental | | | | | | | |
| | Mat'l Spons. | | | | | | | |
| | " CWA SERA | | | | | | | |
| RE-CYR | SERA Payroll | 12.55 | | | | | | |
| | Supervision | .40 | | | | | | |
| | Spons.Labor | | | | | | | |
| | Equip.Rental | | | | | | | |
| | Mat'l Spons. | | | | | | | |
| | " CWA SERA | | | | | | | |
| EXTEM | SERA Payroll | 18.75 | | | | | | |
| | Supervision | .90 | | | | | | |
| | Spons.Labor | | | | | | | |
| | Equip.Rental | 1.50 | | | | | | |
| | Mat'l Spons. | | | | | | | |
| | " CWA SERA | | | | | | | |
| PLANTING TREES | SERA Payroll | 13.95 | | | | | | |
| | Supervision | .50 | | | | | | |
| | Spons.Labor | | | | | | | |
| | Equip.Rental | | | | | | | |
| | Mat'l Spons. | 17.00 | | | | | | |
| | " CWA SERA | | | | | | | |
| CULTIVATING & WATERING | SERA Payroll | 5.33 | | | | | | |
| | Supervision | .20 | | | | | | |
| | Spons.Labor | | | | | | | |
| | Equip.Rental | | | | | | | |
| | Mat'l Spons. | | | | | | | |
| | " CWA SERA | | | | | | | |
| POURING CONCRETE | SERA Payroll | 19.95 | | | | | | |
| | Supervision | .90 | | | | | | |
| | Spons.Labor | | | | | | | |
| | Equip.Rental | 1.50 | | | | | | |
| | Mat'l Spons. | 29.13 | | | | | | |
| | " CWA SERA | 14.25 | | | | | | |
| Spreading Dirt | SERA Payroll | 6.90 | | | | | | |
| | Supervision | .50 | | | | | | |
| | Spons.Labor | | | | | | | |
| | Equip.Rental | | | | | | | |
| | Mat'l Spons. | | | | | | | |
| | " CWA SERA | | | | | | | |
| PICK EX. | SERA Payroll | 11.35 | | | | | | |
| | Supervision | .40 | | | | | | |
| | Spons.Labor | | | | | | | |
| | Equip.Rental | | | | | | | |
| | Mat'l Spons. | | | | | | | |
| | " CWA SERA | | | | | | | |
| Total This Sheet | | | | | | | | |
| Brought Forward | | | | | | | | |
| Total | | | | | | | | |

Fill out this form completely and send in a copy with the WEEKLY REPORT

SIGN _____ Clerk

1

5.69 — 5.90 − 5.48 = .42

5.48 + .21 + .49 + .31 = 5.79

5.40 + .21 = 5.69

5.69

0+00 H.I. 279.02 − 4.62 = 274.40

0+35, 5.07

279.02 − 273.20 = 5.82

279.02 − 273.95 = 5.07

279.02 − 273.55 = 5.47

0+00 H.I. 279.02 − 4.12 = 274.90

279.02 − 273.20 = 5.82

Cent. Rd. 5.32 Rod

279.02 − 273.95 = 5.07

0+284.57 Rod.

279.02 − 273.55 = 5.47

49.7 Rod

+53

indexed
G.S.K.

# CROSS SECTION

of

# RECREATION AREA

N.E. Section

# BALBOA PARK

3-3-'32

| | |
|---|---|
| Drebert | Chief |
| Walton | Inst. 3-3 to 3-8 |
| Bailey | Hd. Ch. 3-3 to 3-8 |
| Kanagy | Rr. Ch. 3-3 to 4-5 |
| Elder | Inst. 3-8 to 3-10 |
| Bell | Hd. Ch. 3-8 to 4-5 |
| Clavert | 3-12 |
| Keyser | 3-14 to 4-5 |
| Mosier | 4-5 |
| Olmsted | 4-5 |
| De Perini | 4-5 |

For Map and instruction and description see pages 1 and 2 of book # 1441.
Further reference, page 33, book # 1426

This book contains only sections east of Texas St. base line. ℄

Survey of Sewer line from field house and swiming pool to Main in Florida St. Canyon See page 34

3-10-32

Drebert
Elder
Kanagy
Bell

1

CROSS SECTION of Section "B". (700' East of Texas St. base line & 600' So. of 0+00).

| | + | H.I. | − | |
|---|---|---|---|---|
| E.T. Line Texas. N. Prop. Upas | 3.44 | 284.36 | | 280.92 |
| B.L. +25 | | | | |
| 0+00 | | | 3.85 | 280.6 |
| 0+25 | | | 4.3 | 280.1 |
| 0+50 | | | 4.9 | 279.5 |
| 0+75 | | | 5.0 | 279.4 |
| 1+00 | | | 5.4 | 279.0 |
| +25 | | | 5.7 | 278.7 |
| +50 | | | 6.0 | 278.4 |
| +75 | | | 6.0 | 278.4 |
| 2+00 | | | 6.2 | 278.2 |
| +25 | | | 6.3 | 278.1 |
| +50 | | | 6.1 | 278.3 |
| +75 | | | 5.9 | 278.5 |
| 3+00 | | | 5.3 | 279.1 |
| +25 | | | 4.9 | 279.5 |
| +50 | | | 4.7 | 279.7 |
| +75 | | | 3.9 | 280.5 |
| 4+00 | | | 4.0 | 280.4 |
| +25 | | | 4.1 | 280.3 |
| +50 | | | 3.9 | 280.5 |
| +75 | | | 3.9 | 280.5 |
| 5+00 | | | 3.8 | 280.6 |

3-12-32

| | + | H.I. | − | |
|---|---|---|---|---|
| | | 284.36 | | |
| B.L. +25 | | | | |
| 5+25 | | | 3.5 | 280.9 |
| +50 | | | 3.8 | 280.6 |
| +75 | | | 4.5 | 279.9 |
| 6+00 | | | 5.1 | 279.3 |
| A | | | | |
| 6+00 | | | 4.0 | 280.4 |
| 5+75 | | | 3.6 | 280.8 |
| +50 | | | 3.3 | 281.1 |
| +25 | | | 3.3 | 281.1 |
| +00 | | | 3.3 | 281.1 |
| 4+75 | | | 3.1 | 281.3 |
| +50 | | | 3.2 | 281.2 |
| +25 | | | 3.1 | 281.3 |
| +00 | | | 3.3 | 281.1 |
| 3+75 | | | 3.4 | 281.0 |
| +50 | | | 4.2 | 280.2 |
| +25 | | | 4.6 | 279.8 |
| +00 | | | 5.0 | 279.4 |
| 2+75 | | | 5.5 | 278.9 |
| +50 | | | 6.1 | 278.3 |
| +25 | | | 6.6 | 277.8 |
| +00 | | | 6.6 | 277.8 |
| 1+75 | | | 6.3 | 278.1 |

| | + | H.I. | − | |
|---|---|---|---|---|
| | | 284.36 | | |
| A | | | | |
| 1+50 | | | 6.0 | 278.4 |
| +25 | | | 6.0 | 278.4 |
| +00 | | | 5.5 | 278.9 |
| 0+75 | | | 5.4 | 279.0 |
| +50 | | | 5.1 | 279.3 |
| +25 | | | 4.3 | 280.1 |
| +00 | | | 3.78 | 280.6 |
| A+25 | | | | |
| 0+00 | | | 4.00 | 280.4 |
| +25 | | | 4.3 | 280.1 |
| +50 | | | 4.8 | 279.6 |
| +75 | | | 5.4 | 279.0 |
| 1+00 | | | 5.9 | 278.5 |
| +25 | | | 6.3 | 278.1 |
| +50 | | | 6.7 | 277.7 |
| +75 | | | 6.8 | 277.6 |
| 2+00 | | | 7.1 | 277.3 |
| +25 | | | 7.1 | 277.3 |
| +50 | | | 6.4 | 278.0 |
| +75 | | | 5.5 | 278.9 |
| 3+00 | | | 4.7 | 279.7 |
| +25 | | | 4.3 | 280.1 |
| +50 | | | 3.3 | 281.1 |

| | + | H.I. 284.36 | − | |
|---|---|---|---|---|
| A+25 | | | | |
| 3+75 | | | 2.9 | 281.5 |
| 4+00 | | | 2.4 | 282.0 |
| +25 | | | 2.0 | 282.4 |
| +50 | | | 2.2 | 282.2 |
| +75 | | | 2.2 | 282.2 |
| 5+00 | | | 2.3 | 282.1 |
| +25 | | | 2.5 | 281.9 |
| +50 | | | 2.6 | 281.8 |
| +75 | | | 3.1 | 281.3 |
| 6+00 | | | 3.4 | 281.0 |
| B | | | | |
| 6+00 | | | 2.9 | 281.5 |
| 5+75 | | | 2.5 | 281.9 |
| +50 | | | 2.1 | 282.3 |
| +25 | | | 1.5 | 282.9 |
| +00 | | | 1.3 | 283.1 |
| 4+75 | | | 1.7 | 282.7 |
| +50 | | | 1.8 | 282.6 |
| +25 | | | 1.9 | 282.5 |
| +00 | | | 2.2 | 282.2 |
| 3+75 | | | 2.6 | 281.8 |
| +50 | | | 3.1 | 281.3 |
| +25 | | | 4.1 | 280.3 |

| | + | H.I. 284.36 | − | |
|---|---|---|---|---|
| B | | | | |
| 3+00 | | | 5.0 | 279.4 |
| 2+75 | | | 5.9 | 278.5 |
| +50 | | | 6.6 | 277.8 |
| +25 | | | 7.6 | 276.8 |
| +00 | | | 7.9 | 276.5 |
| 1+75 | | | 7.8 | 276.6 |
| +50 | | | 7.2 | 277.2 |
| +25 | | | 6.5 | 277.9 |
| +00 | | | 5.9 | 278.5 |
| 0+75 | | | 5.4 | 279.0 |
| +50 | | | 4.8 | 279.6 |
| +25 | | | 4.6 | 279.8 |
| +00 | | | 4.56 | 279.8 |
| B+25 | | | | |
| 0+00 | | | 5.56 | 278.8 |
| +25 | | | 5.3 | 279.1 |
| +50 | | | 5.5 | 278.9 |
| +75 | | | 5.7 | 278.7 |
| 1+00 | | | 6.3 | 278.1 |
| +25 | | | 6.7 | 277.7 |
| +50 | | | 7.5 | 276.9 |
| +75 | | | 8.3 | 276.1 |
| 2+00 | | | 8.9 | 275.5 |

| | + | H.I. 284.36 | − | |
|---|---|---|---|---|
| B+25 | | | | |
| 2+25 | | | 8.7 | 275.7 |
| +50 | | | 7.8 | 276.6 |
| +75 | | | 6.4 | 278.0 |
| 3+00 | | | 5.7 | 278.7 |
| +25 | | | 4.9 | 279.5 |
| +50 | | | 3.6 | 280.8 |
| +75 | | | 2.9 | 281.5 |
| 4+00 | | | 2.5 | 281.9 |
| +25 | | | 1.9 | 282.5 |
| +50 | | | 1.8 | 282.6 |
| +75 | | | 1.6 | 282.8 |
| 5+00 | | | 1.5 | 282.9 |
| +25 | | | 1.6 | 282.8 |
| +50 | | | 1.7 | 282.7 |
| +75 | | | 2.2 | 282.2 |
| 6+00 | | | 2.7 | 281.7 |
| C | | | | |
| 6+00 | | | 3.0 | 281.4 |
| 5+75 | | | 2.6 | 281.8 |
| +50 | | | 2.4 | 282.0 |
| +25 | | | 2.4 | 282.0 |
| +00 | | | 2.3 | 282.1 |
| 4+75 | | | 2.3 | 282.1 |

| | + | H.I. 284.36 | − | |
|---|---|---|---|---|
| C | | | | |
| 4+50 | | | 2.2 | 282.2 |
| +25 | | | 2.9 | 281.5 |
| +00 | | | 3.4 | 281.0 |
| 3+75 | | | 3.9 | 280.5 |
| +50 | | | 4.6 | 279.8 |
| +25 | | | 5.4 | 279.0 |
| +00 | | | 6.8 | 277.6 |
| 2+75 | | | 7.8 | 276.6 |
| +50 | | | 9.2 | 275.2 |
| +25 | | | 10.1 | 274.3 |
| +00 | | | 9.9 | 274.5 |
| 1+75 | | | 9.0 | 275.4 |
| +50 | | | 8.1 | 276.3 |
| +25 | | | 7.6 | 276.8 |
| +00 | | | 7.2 | 277.2 |
| 0+75 | | | 6.7 | 277.7 |
| +50 | | | 6.6 | 277.8 |
| +25 | | | 6.6 | 277.8 |
| +00 | | | 6.76 | 277.6 |
| C+25 | | | | |
| 0+00 | | | 7.96 | 276.4 |
| +25 | | | 7.8 | 276.6 |
| +50 | | | 7.7 | 276.7 |

| | + | H.I. 284.36 | − | |
|---|---|---|---|---|
| C+25 | | | | |
| 0+75 | | | 7.6 | 276.8 |
| 1+00 | | | 8.1 | 276.3 |
| +25 | | | 8.3 | 276.1 |
| +50 | | | 8.8 | 275.6 |
| +75 | | | 9.7 | 274.7 |
| +90 | | | 11.1 | 273.3 |
| 2+00 | | | 11.1 | 273.3 |
| +25 | | | 10.4 | 274.0 |
| +50 | | | 9.9 | 274.5 |
| +75 | | | 9.2 | 275.2 |
| 3+00 | | | 8.4 | 276.0 |
| +25 | | | 7.2 | 277.2 |
| +50 | | | 6.4 | 278.0 |
| +75 | | | 5.7 | 278.7 |
| 4+00 | | | 5.1 | 279.3 |
| +25 | | | 4.5 | 279.9 |
| +50 | | | 4.4 | 280.0 |
| +75 | | | 4.4 | 280.0 |
| 5+00 | | | 4.1 | 280.3 |
| +25 | | | 4.0 | 280.4 |
| +50 | | | 3.6 | 280.8 |
| +75 | | | 3.6 | 280.8 |
| 6+00 | | | 4.0 | 280.4 |

| | + | H.I. 284.36 | − | |
|---|---|---|---|---|
| II | | | | |
| 6+00 | | | 5.8 | 278.6 |
| 5+75 | | | 5.6 | 278.8 |
| +50 | | | 5.7 | 278.7 |
| +25 | | | 6.3 | 278.1 |
| +00 | | | 6.1 | 278.3 |
| 4+75 | | | 6.0 | 278.4 |
| +50 | | | 6.1 | 278.3 |
| +25 | | | 6.6 | 277.8 |
| +00 | | | 7.4 | 277.0 |
| 3+75 | | | 8.0 | 276.4 |
| +50 | | | 9.2 | 275.2 |
| +25 | | | 10.3 | 274.1 |
| +00 | | | 10.4 | 274.0 |
| 2+75 | | | 10.4 | 274.0 |
| +50 | | | 10.3 | 274.1 |
| II+09, 2+50 | | | 10.4 | 274.0 |
| II+15, 2+50 | | | 12.9 | 271.5 |
| II, 2+25 | | | 10.5 | 273.9 |
| II+11, 2+25 | | | 11.0 | 273.4 |
| II+19, 2+25 | | | 12.3 | 272.1 |
| II, 2+00 | | | 10.9 | 273.5 |
| 1+75 | | | 11.7 | 272.7 |
| +50 | | | 11.5 | 272.9 |

| Sta | 18' Rt Grade | ℄ Grade | 18' Lt Grade | Sta Deft. | |
|---|---|---|---|---|---|
| 46+00 | 253.50 | 254.00 | 254.50 | | |
| 45+50 | 253.21 | 253.68 | 254.01 | | |
| 45+00 | 252.93 | 253.36 | 253.52 | | |
| 44+50 | 252.63 | 253.04 | 253.03 | | |
| 44+00 | 252.50 | 252.88 | 252.72 | | |
| 43+50 | 252.67 | 253.03 | 252.77 | | |
| 43+00 | 253.06 | 253.41 | 253.08 | | |
| 42+50 | 253.75 | 254.10 | 253.75 | | |
| 42+00 | 254.70 | 255.05 | 254.70 | | |
| 41+50 | 255.65 | 256.00 | 255.65 | | |
| 41+00 | 256.60 | 256.95 | 256.60 | | |
| 40+50 | 257.64 | 257.99 | 257.69 | | |
| 40+00 | 258.35 | 258.60 | 258.47 | | |
| 39+50 07 | 258.90 | 259.10 | 259.30 | E.C. 10°47.5' | R=200 |
| 39+25 | 259.02 | 259.35 | 259.69 | 7°12' | Δ=21°-35 Rt |
| 39+12 90 | 259.08 | 259.48 | 259.88 | | L=75.34 |
| 39+00 | 259.27 | 259.60 | 259.94 | 3°37' | S.T=38.12 |
| 38+74 73 | 259.65 | 259.85 | 260.05 | B.C | Def per ft=8.594 |
| 38+32 60 | 260.35 | 260.30 | 260.25 | | |
| 37+90 55 | 261.05 | 260.75 | 260.45 | E.C. 57°30' | R=150 |
| 37+75 | 261.52 | 260.98 | 260.56 | 54°32' | Δ=115° Lt |
| 37+50 | 261.95 | 261.36 | 260.75 | 49°45' | L=301.07 |
| 37+25 | 262.32 | 261.73 | 261.12 | 44°59 | L Ch 253.02 |
| | | | | | Df=11.459' |

70 80
69 85
.85

| Sta | 18' Rt Grade | ℄ Grade | 18' Lt Grade | Sta Df | Curve Data |
|---|---|---|---|---|---|
| 37+00 | 262.70 | 262.11 | 261.50 | 40°12' | |
| 36+75 | 263.07 | 262.48 | 261.87 | 35°26' | |
| 36+50 | 263.45 | 262.85 | 262.25 | 30°39' | |
| 36+25 | 263.82 | 263.23 | 262.62 | 25°53 | |
| 36+00 | 264.20 | 263.60 | 263.00 | 21°06' | |
| 35+75 | 264.57 | 263.98 | 263.38 | 16°20 | |
| 35+50 | 264.95 | 264.35 | 263.75 | 11°34' | |
| 35+25 | 265.20 | 264.73 | 264.24 | 6°47 | |
| 35+00 | 265.45 | 265.12 | 264.74 | 2°01' | |
| 34+89 48 | 265.55 | 265.28 | 264.95 | P.C. | |
| ~~34+50~~ | ~~265.80~~ | ~~265.87~~ | 265.60 | | |
| 33+99 48 | 266.30 | 266.63 | 266.90 | P.T. 45°00' | |
| 33+75 | 266.52 | 266.99 | 267.42 | 40°08' | |
| 33+50 | 266.75 | 267.37 | 267.95 | 35°09' | R=144 |
| 33+25 | 267.12 | 267.74 | 268.32 | 30°11' | Δ=90° Rt. |
| 33+00 | 267.50 | 268.12 | 268.70 | 25°13' | L=226.19 |
| 32+75 | 267.85 | 268.50 | 269.07 | 20°14' | L Ch=203.65 |
| 32+50 | 268.25 | 268.87 | 269.45 | 15°16' | Df=11.937' |
| 32+25 | 268.72 | 269.24 | 269.73 | 10°17' | |
| 32+00 | 269.19 | 269.62 | 270.00 | 5°19' | |
| 31+73 29 | 269.70 | 270.00 | 270.30 | P.C. | |
| 31+32 | 270.60 | 270.56 | 270.70 | | |
| 30+91 29 | 271.18 | 270.98 | 270.78 | P.T. | |

| | + | H.I. 284.36 | − | |
|---|---|---|---|---|
| C+40, I+50 | | | 9.4 | 275.0 |
| II, I+37 | | | 9.5 | 274.9 |
| I+25 | | | 9.0 | 275.4 |
| +00 | | | 8.9 | 275.5 |
| 0+75 | | | 8.6 | 275.8 |
| +50 | | | 8.6 | 275.8 |
| +25 | | | 8.7 | 275.7 |
| +00 | | | 8.14 | 276.3 |
| II+25 | | | | |
| 0+00 | | | 10.40 | 274.0 |
| +25 | | | 9.7 | 274.7 |
| +50 | | | 9.8 | 274.6 |
| +75 | | | 9.5 | 274.9 |
| 1+00 | | | 9.6 | 274.8 |
| +15 | | | 9.8 | 274.6 |
| +25 | | | 11.7 | 272.7 |
| +50 | | | 12.0 | 272.4 |
| +75 | | | 11.3 | 273.1 |
| 2+00 | | | 11.5 | 272.9 |
| +25 | | | 12.2 | 272.2 |
| +50 | | | 13.6 | 270.8 |
| +63 | | | 13.4 | 271.0 |
| +66 | | | 11.5 | 272.9 |

| | + | H.I. 284.36 | − | |
|---|---|---|---|---|
| II+25 | | | | |
| 2+75 | | | 12.1 | 272.3 |
| 3+00 | | | 12.4 | 272.0 |
| +25 | | | 11.5 | 272.9 |
| +50 | | | 11.3 | 273.1 |
| +75 | | | 10.8 | 273.6 |
| 4+00 | | | 10.4 | 274.0 |
| +25 | | | 9.8 | 274.6 |
| +50 | | | 9.4 | 275.0 |
| +75 | | | 9.0 | 275.4 |
| 5+00 | | | 8.5 | 275.9 |
| +25 | | | 8.4 | 276.0 |
| +50 | | | 8.5 | 275.9 |
| +75 | | | 8.6 | 275.8 |
| 6+00 | | | 8.9 | 275.5 |
| PR Rock II+25, 2+75 | 2.74 | 275.24 ✓ | 11.86 | 272.50 ✓ |
| E | | | | |
| 6+00 | | | 3.0 | 272.2 |
| 5+75 | | | 2.7 | 272.5 |
| +50 | | | 2.4 | 272.8 |
| +25 | | | 2.1 | 273.1 |
| +00 | | | 2.6 | 272.6 |
| 4+75 | | | 2.9 | 272.3 |
| +50 | | | 2.7 | 272.5 |

| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| E | | | | |
| 4+25 | | | 3.0 | 272.2 |
| +00 | | | 3.2 | 272.0 |
| 3+75 | | | 3.6 | 271.6 |
| +50 | | | 4.2 | 271.0 |
| +25 | | | 4.5 | 270.7 |
| +00 | | | 4.6 | 270.6 |
| 2+90 | | | 4.4 | 270.8 |
| +75 | | | 4.4 | 270.8 |
| +60 | | | 4.4 | 270.8 |
| +50 | | | 4.9 | 270.3 |
| +25 | | | 3.7 | 271.5 |
| +00 | | | 2.6 | 272.6 |
| 1+75 | | | 2.0 | 273.2 |
| +70 | | | 2.7 | 272.5 |
| +50 | | | 2.6 | 272.2 |
| +25 | | | 3.3 | 271.9 |
| +05 | | | 2.8 | 272.4 |
| +00 | | | 1.3 | 273.9 |
| 0+75 | | | 1.0 | 274.2 |
| +50 | | | 1.1 | 274.1 |
| +25 | | | 1.2 | 274.0 |
| +00 | | | 2.51 | 272.7 |



| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| E+25 | | | | |
| 0+00 | | | 3.75 | 271.5 |
| +25 | | | 2.4 | 272.8 |
| +30 | | | 1.3 | 273.9 |
| +50 | | | 1.5 | 273.7 |
| +75 | | | 1.5 | 273.7 |
| +90 | | | 1.7 | 273.5 |
| +95 | | | 2.9 | 272.3 |
| 1+00 | | | 3.1 | 272.1 |
| +25 | | | 3.0 | 272.2 |
| +50 | | | 2.8 | 272.4 |
| +75 | | | 2.2 | 273.0 |
| 2+00 | | | 3.1 | 272.1 |
| +25 | | | 4.3 | 270.9 |
| +50 | | | 5.3 | 269.9 |
| +75 | | | 5.4 | 269.8 |
| 3+00 | | | 5.5 | 269.7 |
| +25 | | | 5.7 | 269.5 |
| +50 | | | 5.4 | 269.8 |
| +75 | | | 5.3 | 269.9 |
| 4+00 | | | 5.1 | 270.1 |
| +25 | | | 5.0 | 270.2 |
| +50 | | | 5.0 | 270.2 |
| +75 | | | 5.3 | 269.9 |

| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| E+25 | | | | |
| 5+00 | | | 5.4 | 269.8 |
| +25 | | | 5.4 | 269.8 |
| +50 | | | 5.1 | 270.1 |
| +75 | | | 5.2 | 270.0 |
| 6+00 | | | 5.4 | 269.8 |
| F | | | | |
| 6+00 | | | 7.4 | 267.8 |
| 5+75 | | | 7.1 | 268.1 |
| +50 | | | 7.2 | 268.0 |
| +25 | | | 7.1 | 268.1 |
| +00 | | | 7.0 | 268.2 |
| 4+75 | | | 7.0 | 268.2 |
| +50 | | | 6.7 | 268.5 |
| +25 | | | 6.6 | 268.6 |
| +00 | | | 6.5 | 268.7 |
| 3+75 | | | 6.5 | 268.7 |
| +50 | | | 6.0 | 269.2 |
| +25 | | | 6.0 | 269.2 |
| +00 | | | 6.2 | 269.0 |
| 2+75 | | | 6.3 | 268.9 |
| +50 | | | 6.5 | 268.7 |
| +46 | | | 5.5 | 269.7 |
| +25 | | | 4.6 | 270.6 |

| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| F | | | | |
| 2+00 | | | 3.9 | 271.3 |
| 1+75 | | | 3.3 | 271.9 |
| +50 | | | 3.0 | 272.2 |
| +40 | | | 2.9 | 272.3 |
| +35 | | | 3.6 | 271.6 |
| +25 | | | 3.5 | 271.7 |
| +00 | | | 3.9 | 271.3 |
| 0+75 | | | 3.5 | 271.7 |
| +50 | | | 3.4 | 271.8 |
| E+47.0+50 | | | 2.4 | 272.8 |
| +25 | | | 4.0 | 271.2 |
| +00 | | | 4.99 | 270.2 |
| F+25 | | | | |
| 0+00 | | | 5.54 | 269.7 |
| +25 | | | 4.5 | 270.5 |
| +50 | | | 3.9 | 271.3 |
| +75 | | | 3.9 | 271.3 |
| 1+00 | | | 3.9 | 271.3 |
| +25 | | | 3.7 | 271.5 |
| +50 | | | 3.8 | 271.4 |
| +75 | | | 4.3 | 270.9 |
| 2+00 | | | 4.9 | 270.3 |
| +25 | | | 5.6 | 269.6 |
| +46 | | | 6.5 | 268.7 |

| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| F+25 | | | | |
| 2+50 | | | 7.6 | 267.6 |
| +75 | | | 7.0 | 268.2 |
| 3+00 | | | 6.7 | 268.5 |
| +25 | | | 6.4 | 268.8 |
| +50 | | | 6.4 | 268.8 |
| +75 | | | 6.2 | 269.0 |
| 4+00 | | | 6.8 | 268.4 |
| +25 | | | 7.4 | 267.8 |
| +50 | | | 7.6 | 267.6 |
| +75 | | | 7.6 | 267.6 |
| 5+00 | | | 8.2 | 267.0 |
| +25 | | | 8.1 | 267.1 |
| +50 | | | 7.8 | 267.4 |
| +75 | | | 7.9 | 267.3 |
| 6+00 | | | 7.8 | 267.4 |
| G | | | | |
| 6+00 | | | 8.2 | 267.0 |
| 5+75 | | | 8.6 | 266.6 |
| +50 | | | 8.8 | 266.4 |
| +25 | | | 9.2 | 266.0 |
| +00 | | | 8.8 | 266.4 |
| 4+75 | | | 8.2 | 267.0 |
| +50 | | | 7.6 | 267.6 |



| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| G | | | | |
| 4+25 | | | 7.2 | 268.0 |
| +00 | | | 7.0 | 268.2 |
| 3+75 | | | 6.6 | 268.6 |
| +50 | | | 6.9 | 268.3 |
| +25 | | | 7.4 | 267.8 |
| +00 | | | 7.7 | 267.5 |
| 2+75 | | | 8.6 | 266.6 |
| +50 | | | 8.5 | 266.7 |
| +43 | | | 8.9 | 266.3 |
| +40 | | | 8.2 | 267.0 |
| +25 | | | 7.4 | 267.8 |
| +00 | | | 6.5 | 268.7 |
| 1+75 | | | 5.1 | 270.1 |
| +50 | | | 4.7 | 270.5 |
| +25 | | | 4.7 | 270.5 |
| +23 | | | 5.3 | 270.9 |
| +00 | | | 4.7 | 270.5 |
| 0+75 | | | 4.6 | 270.6 |
| +50 | | | 4.6 | 270.6 |
| G+07, 0+75 | | | 5.0 | 270.2 |
| +11, 0+75 | | | 4.3 | 270.9 |
| +10, 0+50 | | | 4.0 | 271.2 |
| G, 0+25 | | | 5.0 | 270.2 |

| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| G | | | | |
| 0+00 | | | 5.90 | 269.3 |
| G+25 | | | | |
| 0+00 | | | 6.70 | 268.5 |
| +25 | | | 6.0 | 269.2 |
| +36 | | | 4.0 | 271.2 |
| +50 | | | 4.2 | 271.0 |
| +75 | | | 4.3 | 270.9 |
| +83 | | | 4.5 | 270.7 |
| +87 | | | 5.4 | 269.8 |
| 1+00 | | | 5.4 | 269.8 |
| +25 | | | 5.5 | 269.7 |
| +28 | | | 6.3 | 268.9 |
| +30 | | | 5.4 | 269.8 |
| +50 | | | 5.6 | 269.6 |
| +75 | | | 5.9 | 269.3 |
| 2+00 | | | 6.8 | 268.4 |
| +25 | | | 8.5 | 266.7 |
| +40 | | | 8.8 | 266.4 |
| +45 | | | 9.8 | 265.4 |
| +50 | | | 9.6 | 265.6 |
| +75 | | | 9.5 | 265.7 |
| 3+00 | | | 8.6 | 266.6 |
| +25 | | | | |

| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| G+25 | | | | |
| 3+50 | | | 8.6 | 266.6 |
| +75 | | | 7.7 | 267.5 |
| 4+00 | | | 7.0 | 268.2 |
| +25 | | | 6.9 | 268.3 |
| +50 | | | 7.5 | 267.7 |
| +75 | | | 7.7 | 267.5 |
| 5+00 | | | 8.3 | 266.9 |
| +25 | | | 9.5 | 266.7 |
| +50 | | | 10.0 | 265.2 |
| +75 | | | 9.1 | 266.1 |
| 6+00 | | | 8.1 | 267.1 |
| H | | | | |
| 6+00 | | | 8.0 | 267.2 |
| 5+75 | | | 8.5 | 266.7 |
| +50 | | | 9.7 | 265.5 |
| +25 | | | 11.5 | 263.7 |
| +00 | | | 10.5 | 264.7 |
| 4+75 | | | 9.2 | 266.0 |
| +50 | | | 8.5 | 266.7 |
| +25 | | | 8.3 | 266.9 |
| +00 | | | 7.8 | 267.4 |
| 3+75 | | | 7.9 | 267.3 |
| +50 | | | 8.6 | 266.6 |

| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| H | | | | |
| 3+25 | | | 9.3 | 265.9 |
| +00 | | | 9.6 | 265.6 |
| 2+75 | | | 11.0 | 264.2 |
| +50 | | | 10.3 | 264.9 |
| +40 | | | 10.5 | 264.7 |
| +35 | | | 9.5 | 265.7 |
| +25 | | | 8.7 | 266.5 |
| +00 | | | 7.6 | 267.6 |
| 1+75 | | | 6.9 | 268.3 |
| +50 | | | 6.4 | 268.8 |
| +42 | | | 6.4 | 268.8 |
| +39 | | | 7.6 | 267.6 |
| +36 | | | 6.9 | 268.3 |
| +25 | | | 6.4 | 268.8 |
| +09 | | | 7.3 | 267.9 |
| +04 | | | 5.9 | 269.3 |
| +00 | | | 5.8 | 269.4 |
| 0+90 | | | 5.5 | 269.7 |
| +87 | | | 6.4 | 268.8 |
| +75 | | | 6.3 | 268.9 |
| +50 | | | 7.3 | 267.9 |
| +25 | | | 6.4 | 268.8 |
| +00 | | | 7.97 | 267.2 |

| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| H+25 | | | | |
| 0+00 | | | 8.82 | 266.4 |
| +25 | | | 8.3 | 266.9 |
| +30 | | | 9.0 | 266.2 |
| +50 | | | 8.9 | 266.3 |
| +75 | | | 8.0 | 267.2 |
| +94 | | | 7.9 | 267.3 |
| 1+00 | | | 6.9 | 268.3 |
| +13 | | | 7.0 | 268.2 |
| +18 | | | 8.1 | 267.1 |
| +25 | | | 7.4 | 267.8 |
| +48 | | | 8.6 | 266.6 |
| +50 | | | 9.0 | 266.2 |
| +53 | | | 7.6 | 267.6 |
| +75 | | | 7.9 | 267.3 |
| 2+00 | | | 8.5 | 266.7 |
| +25 | | | 9.3 | 265.9 |
| +36 | | | 9.9 | 265.3 |
| +41 | | | 11.6 | 263.6 |
| +50 | | | 11.3 | 263.9 |
| +75 | | | 11.6 | 263.6 |
| 3+00 | | | 10.5 | 264.7 |
| +25 | | | 9.8 | 265.4 |
| +50 | | | 9.3 | 265.9 |

| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| H+25 | | | | |
| 3+75 | | | 8.7 | 266.5 |
| 4+00 | | | 8.8 | 266.4 |
| +25 | | | 9.2 | 266.0 |
| +50 | | | 9.5 | 265.7 |
| +75 | | | 10.4 | 264.8 |
| 5+00 | | | 11.1 | 264.1 |
| +25 | | | 12.3 | 262.9 |
| +50 | | | 10.8 | 264.4 |
| +75 | | | 9.2 | 266.0 |
| 6+00 | | | 8.5 | 266.7 |
| I | | | | |
| 6+00 | | | 9.0 | 266.2 |
| 5+75 | | | 9.7 | 265.5 |
| +50 | | | 10.8 | 264.4 |
| +25 | | | 13.4 | 261.8 |
| +00 | | | 13.9 | 261.3 |
| 4+75 | | | 11.9 | 263.3 |
| +50 | | | 10.2 | 265.0 |
| +25 | | | 9.8 | 265.4 |
| +00 | | | 9.6 | 265.6 |
| 3+75 | | | 9.7 | 265.5 |
| +50 | | | 9.9 | 265.3 |
| +25 | | | 10.2 | 265.0 |

| | + | H.I. 275.24 | − | |
|---|---|---|---|---|
| I | | | | |
| 3+00 | | | 11.1 | 264.1 |
| 2+75 | | | 12.8 | 262.4 |
| +50 | | | 13.0 | 262.2 |
| +36 | | | 12.7 | 262.5 |
| +30 | | | 11.3 | 263.9 |
| +25 | | | 11.0 | 264.2 |
| +00 | | | 10.0 | 265.2 |
| 1+75 | | | 9.1 | 266.1 |
| +72 | | | 11.0 | 264.2 |
| +50 | | | 9.2 | 266.0 |
| +34 | | | 9.4 | 265.8 |
| +30 | | | 8.5 | 266.7 |
| +25 | | | 8.3 | 266.9 |
| +13 | | | 8.1 | 267.1 |
| +08 | | | 9.1 | 266.1 |
| +00 | | | 9.5 | 265.7 |
| 0+75 | | | 10.0 | 265.2 |
| +50 | | | 10.8 | 264.4 |
| +25 | | | 10.5 | 264.7 |
| +20 | | | 9.0 | 266.2 |
| +00 | | | 10.10 | 265.1 |
| TP. Rock I, 2+50 | | 4.45 | 267.09 | 12.60 | 262.64 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| I+25 | | | | |
| 0+00 | | | 2.42 | 264.7 |
| +15 | | | 1.6 | 265.5 |
| +25 | | | 3.6 | 263.5 |
| +35 | | | 4.4 | 262.7 |
| +50 | | | 4.0 | 263.1 |
| +75 | | | 3.6 | 263.5 |
| 1+00 | | | 2.7 | 264.4 |
| +25 | | | 2.4 | 264.7 |
| +33 | | | 1.2 | 265.9 |
| +50 | | | 1.7 | 265.4 |
| +54 | | | 2.9 | 264.2 |
| +75 | | | 2.8 | 264.3 |
| 2+00 | | | 4.2 | 262.9 |
| I+14, 2+00 | | | 2.4 | 264.7 |
| I+19, 2+00 | | | 4.6 | 262.5 |
| I+25, 2+50 | | | 5.0 | 262.1 |
| 2+75 | | | 5.8 | 261.3 |
| 3+00 | | | 5.5 | 261.6 |
| +25 | | | 4.7 | 262.4 |
| +50 | | | 3.5 | 263.6 |
| +75 | | | 2.8 | 264.3 |
| 4+00 | | | 2.9 | 264.2 |
| +25 | | | 3.4 | 263.7 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| I+25 | | | | |
| 4+50 | | | 4.2 | 262.9 |
| +75 | | | 6.0 | 261.1 |
| 5+00 | | | 7.6 | 259.5 |
| +25 | | | 5.4 | 261.7 |
| +50 | | | 2.2 | 264.9 |
| +75 | | | 1.4 | 265.7 |
| 6+00 | | | 1.1 | 266.0 |
| J | | | | |
| 6+00 | | | 2.6 | 264.5 |
| 5+75 | | | 2.6 | 264.5 |
| +50 | | | 3.6 | 263.5 |
| +25 | | | 6.6 | 260.5 |
| +00 | | | 9.0 | 258.1 |
| 4+75 | | | 9.1 | 258.0 |
| +50 | | | 7.7 | 259.4 |
| +25 | | | 6.5 | 260.6 |
| +00 | | | 5.9 | 261.2 |
| 3+75 | | | 5.3 | 261.8 |
| +50 | | | 5.0 | 262.1 |
| +25 | | | 5.0 | 262.1 |
| +10 | | | 5.2 | 261.9 |
| +05 | | | 6.5 | 260.6 |
| +00 | | | 6.6 | 260.5 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| J | | | | |
| 2+75 | | | 6.7 | 260.4 |
| +50 | | | 6.9 | 260.2 |
| +25 | | | 5.7 | 261.4 |
| +00 | | | 5.5 | 261.6 |
| 1+96 | | | 6.0 | 261.1 |
| +90 | | | 4.3 | 262.8 |
| +75 | | | 3.6 | 263.5 |
| +60 | | | 3.2 | 263.9 |
| +50 | | | 4.0 | 263.1 |
| +25 | | | 3.8 | 263.3 |
| +00 | | | 4.3 | 262.8 |
| 0+75 | | | 5.0 | 262.1 |
| +50 | | | 5.5 | 261.6 |
| +25 | | | 6.4 | 260.7 |
| +20 | | | 2.1 | 265.0 |
| +00 | | | 2.90 | 264.2 |
| J+25 | | | | |
| 0+00 | | | 3.33 | 263.8 |
| +15 | | | 2.5 | 264.6 |
| +25 | | | 7.8 | 259.3 |
| +50 | | | 7.7 | 259.4 |
| +75 | | | 6.4 | 260.7 |
| 1+00 | | | 5.3 | 261.8 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| J+25 | | | | |
| 1+25 | | | 4.9 | 262.2 |
| +50 | | | 5.4 | 261.7 |
| +75 | | | 5.7 | 261.4 |
| +87 | | | 6.1 | 261.0 |
| +92 | | | 4.9 | 262.2 |
| 2+00 | | | 5.7 | 261.4 |
| +13 | | | 6.0 | 261.1 |
| +14 | | | 7.4 | 259.7 |
| +25 | | | 7.7 | 259.4 |
| +35 | | | 6.9 | 260.2 |
| +50 | | | 7.4 | 259.7 |
| +51 | | | 8.3 | 258.8 |
| +53 | | | 7.7 | 259.4 |
| +75 | | | 7.6 | 259.5 |
| 3+00 | | | 7.7 | 259.4 |
| +05 | | | 7.4 | 259.7 |
| +08 | | | 6.3 | 260.8 |
| +25 | | | 6.1 | 261.0 |
| +50 | | | 6.5 | 260.6 |
| +75 | | | 6.8 | 260.3 |
| 4+00 | | | 7.6 | 259.5 |
| +25 | | | 8.4 | 258.7 |
| +50 | | | 9.7 | 257.4 |
| +75 | | | 10.7 | 256.4 |
| 5+00 | | | 10.5 | 256.6 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| J+25 | | | | |
| 5+25 | | | 8.5 | 258.6 |
| +50 | | | 6.0 | 261.1 |
| +75 | | | 5.0 | 262.1 |
| 6+00 | | | 5.2 | 261.9 |
| K | | | | |
| 6+00 | | | 8.2 | 258.9 |
| 5+75 | | | 8.2 | 258.9 |
| +50 | | | 9.1 | 258.0 |
| +25 | | | 10.8 | 256.3 |
| +00 | | | 12.0 | 255.1 |
| 4+75 | | | 13.0 | 254.1 |
| +50 | | | 12.0 | 255.1 |
| +25 | | | 10.5 | 256.6 |
| +00 | | | 9.3 | 257.8 |
| 3+75 | | | 8.9 | 258.2 |
| +50 | | | 8.0 | 259.1 |
| +25 | | | 7.6 | 259.5 |
| +00 | | | 8.8 | 258.3 |
| 2+75 | | | 9.5 | 257.6 |
| +68 | | | 10.1 | 257.0 |
| +65 | | | 9.0 | 258.1 |
| +50 | | | 8.7 | 258.4 |
| +34 | | | 8.9 | 258.2 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| K | | | | |
| 2+32 | | | 8.3 | 258.8 |
| +25 | | | 8.6 | 258.5 |
| +00 | | | 8.3 | 258.8 |
| 1+75 | | | 7.1 | 260.1 |
| +50 | | | 6.5 | 260.6 |
| +25 | | | 6.6 | 260.5 |
| +00 | | | 7.8 | 259.3 |
| 0+75 | | | 10.2 | 256.9 |
| +50 | | | 9.8 | 257.3 |
| +25 | | | 10.5 | 256.6 |
| +12 | | | 2.8 | 264.3 |
| +00 | | | 3.65 | 263.5 |
| K+25 | | | | |
| 0+00 | | | 3.92 | 263.2 |
| +13 | | | 3.4 | 263.7 |
| +25 | | | 8.2 | 258.9 |
| +50 | | | 11.7 | 255.4 |
| +75 | | | 11.7 | 255.4 |
| 1+00 | | | 11.2 | 255.9 |
| +15 | | | 9.0 | 258.1 |
| +25 | | | 7.6 | 259.5 |
| +50 | | | 8.0 | 259.1 |
| +75 | | | 8.3 | 258.8 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| K+25 | | | | |
| 2+00 | | | 9.4 | 257.7 |
| +25 | | | 10.0 | 257.1 |
| +35 | | | 10.2 | 256.9 |
| +38 | | | 11.0 | 256.1 |
| +50 | | | 10.0 | 257.1 |
| +75 | | | 10.6 | 256.5 |
| +78 | | | 11.5 | 255.6 |
| +90 | | | 11.0 | 256.1 |
| 3+00 | | | 9.1 | 258.0 |
| +15 | | | 8.7 | 258.4 |
| +20 | | | 7.8 | 259.3 |
| +25 | | | 7.8 | 259.3 |
| +50 | | | 8.6 | 258.5 |
| +75 | | | 9.2 | 257.9 |
| 4+00 | | | 11.0 | 256.1 |
| +25 | | | 12.4 | 254.7 |
| +50 | | | 12.5 | 254.6 |
| +75 | | | 14.5 | 252.6 |
| 5+00 | | | 14.2 | 252.9 |
| +25 | | | 12.4 | 254.7 |
| +50 | | | 11.4 | 255.7 |
| +75 | | | 11.1 | 256.0 |
| 6+00 | | | 10.9 | 256.2 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| L | | | | |
| 6+00 | | | 14.0 | 253.1 |
| 5+75 | | | 13.6 | 253.5 |
| +50 | | | 14.0 | 253.1 |
| +25 | | | 15.3 | 251.8 |
| +00 | | | 16.6 | 250.5 |
| 4+75 | | | 15.3 | 251.8 |
| +50 | | | 14.1 | 253.0 |
| +25 | | | 12.5 | 254.6 |
| +00 | | | 11.1 | 256.0 |
| 3+75 | | | 9.9 | 257.2 |
| +50 | | | 9.5 | 257.6 |
| +25 | | | 9.1 | 258.0 |
| +12 | | | 10.6 | 256.5 |
| +00 | | | 11.7 | 255.4 |
| 2+97 | | | 12.5 | 254.6 |
| +85 | | | 12.0 | 255.1 |
| +84 | | | 12.5 | 254.6 |
| +82 | | | 11.9 | 255.2 |
| +75 | | | 11.8 | 255.3 |
| +50 | | | 11.3 | 255.8 |
| +40 | | | 11.9 | 255.2 |
| +38 | | | 10.6 | 256.5 |
| +25 | | | 10.6 | 256.5 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| L | | | | |
| 2+00 | | | 10.8 | 256.3 |
| 1+75 | | | 10.1 | 257.0 |
| +50 | | | 9.8 | 257.3 |
| +25 | | | 10.5 | 256.6 |
| +00 | | | 13.2 | 253.9 |
| 0+75 | | | 10.6 | 256.5 |
| +50 | | | 9.4 | 257.7 |
| +25 | | | 8.0 | 259.1 |
| +12 | | | 4.0 | 263.1 |
| +00 | | | 4.23 | 262.9 |
| L+25 | | | | |
| 0+00 | | | 4.55 | 262.6 |
| +12 | | | 4.2 | 262.9 |
| +25 | | | 7.5 | 259.6 |
| +50 | | | 9.5 | 257.6 |
| +75 | | | 11.0 | 256.1 |
| 1+00 | | | 13.5 | 253.6 |
| +08 | | | 13.7 | 253.4 |
| +12 | | | 12.4 | 254.7 |
| +25 | | | 11.5 | 255.6 |
| +50 | | | 11.2 | 255.9 |
| +75 | | | 11.4 | 255.7 |
| 2+00 | | | 12.2 | 254.9 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| L+25 | | | | |
| 2+25 | | | 12.1 | 255.0 |
| +35 | | | 11.6 | 255.5 |
| +40 | | | 13.0 | 254.1 |
| +42 | | | 12.4 | 254.7 |
| +50 | | | 12.4 | 254.7 |
| +75 | | | 12.5 | 254.6 |
| 3+00 | | | 12.5 | 254.6 |
| +25 | | | 11.5 | 255.6 |
| +50 | | | 10.6 | 256.5 |
| +75 | | | 10.7 | 256.4 |
| 4+00 | | | 12.3 | 254.8 |
| +25 | | | 13.4 | 253.7 |
| +50 | | | 14.6 | 252.5 |
| +75 | | | 16.6 | 250.5 |
| 5+00 | | | 19.0 | 248.1 |
| +05 | | | 21.0 | 246.1 |
| +10 | | | 18.6 | 248.5 |
| +25 | | | 17.7 | 249.4 |
| +50 | | | 17.0 | 250.1 |
| +75 | | | 17.2 | 249.9 |
| 6+00 | | | 17.0 | 250.1 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| M | | | | |
| 6+00 | | | 19.9 | 247.2 |
| 5+75 | | | 19.4 | 247.7 |
| +50 | | | 19.2 | 247.9 |
| +25 | | | 20.2 | 246.9 |
| +12 | | | 20.8 | 246.3 |
| +08 | | | 22.0 | 245.1 |
| +00 | | | 19.9 | 247.2 |
| 4+75 | | | 18.0 | 249.1 |
| +50 | | | 17.1 | 250.0 |
| +25 | | | 16.6 | 250.5 |
| +00 | | | 15.6 | 251.5 |
| 3+75 | | | 14.3 | 252.8 |
| +50 | | | 13.4 | 253.7 |
| +25 | | | 13.1 | 254.0 |
| +00 | | | 13.5 | 253.6 |
| 2+75 | | | 13.5 | 253.6 |
| +50 | | | 13.3 | 253.8 |
| +25 | | | 13.8 | 253.3 |
| +00 | | | 13.8 | 253.3 |
| 1+75 | | | 12.9 | 254.2 |
| +50 | | | 12.8 | 254.3 |
| +25 | | | 13.4 | 253.7 |
| +00 | | | 13.4 | 253.7 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| M | | | | |
| 0+75 | | | 10.5 | 256.6 |
| +50 | | | 9.3 | 257.8 |
| +25 | | | 7.8 | 259.3 |
| +00 | Gutter | | 5.02 | 262.07 |
| +00 | Top of Curb | | 3.87 | 263.22 |
| M+25 | | | | |
| 0+00 | Gutter | | 5.78 | 261.31 |
| +00 | Top of Curb | | 4.52 | 262.57 |
| +05 | | | 5.0 | 262.1 |
| +10 | | | 7.5 | 259.6 |
| +25 | | | 8.3 | 258.8 |
| +50 | | | 9.9 | 257.2 |
| +75 | | | 11.1 | 256.0 |
| 1+00 | | | 12.7 | 254.4 |
| +25 | | | 14.0 | 253.1 |
| +50 | | | 13.9 | 253.2 |
| +75 | | | 14.1 | 253.0 |
| 2+00 | | | 15.8 | 251.3 |
| +25 | | | 14.6 | 252.5 |
| +50 | | | 13.7 | 253.4 |
| +75 | | | 14.3 | 252.8 |
| 3+00 | | | 14.6 | 252.5 |
| +25 | | | 15.0 | 252.1 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| M+25 | | | | |
| 3+50 | | | 16.1 | 251.0 |
| +75 | | | 17.1 | 250.0 |
| 4+00 | | | 18.3 | 248.8 |
| +25 | | | 18.9 | 248.2 |
| +50 | | | 19.6 | 247.5 |
| +75 | | | 20.4 | 246.7 |
| 5+00 | | | 21.6 | 245.5 |
| +13 | | | 25.2 | 241.9 |
| +25 | | | 23.0 | 244.1 |
| +50 | | | 22.8 | 244.3 |
| +75 | | | 23.0 | 244.1 |
| 6+00 | | | 23.6 | 243.5 |
| N | | | | |
| 6+00 | | | 30.4 | 236.7 |
| 5+75 | | | 28.2 | 238.9 |
| +50 | | | 28.0 | 239.1 |
| M+40, 5+50 | | | 24.9 | 242.2 |
| N, 5+25 | | | 27.9 | 239.2 |
| 5+00 | | | 26.8 | 240.3 |
| M+38, 5+00 | | | 22.8 | 244.3 |
| N, 4+75 | | | 25.2 | 241.9 |
| M+43, 4+75 | | | 22.8 | 244.3 |
| N, 4+50 | | | 22.7 | 244.4 |

| | + | H.I. 267.09 | − | |
|---|---|---|---|---|
| N | | | | |
| 4+25 | | | 22.0 | 245.1 |
| +00 | | | 21.5 | 245.6 |
| 3+75 | | | 20.7 | 246.4 |
| +50 | | | 19.5 | 247.6 |
| +28 | | | 18.3 | 248.8 |
| +25 | | | 16.8 | 250 3 |
| +20 | | | 14.6 | 252.5 |
| +00 | | | 14.9 | 252.2 |
| 2+75 | | | 14.6 | 252.5 |
| +68 | | | 14.6 | 252.5 |
| +60 | | | 20.1 | 247.0 |
| +50 | | | 17.1 | 250.0 |
| M+35, 2+50 | | | 20.0 | 247.1 |
| M+30, 2+50 | | | 15.3 | 251.8 |
| N, 2+25 | | | 18.0 | 249.1 |
| 2+13 | | | 19.0 | 248.1 |
| +00 | | | 17.3 | 249.8 |
| 1+75 | | | 16.0 | 251.1 |
| +50 | | | 14.5 | 252.6 |
| +25 | | | 13.8 | 253.3 |
| +00 | | | 13.4 | 253.7 |
| 0+75 | | | 12.6 | 254.5 |
| +50 | | | 11.4 | 255.7 |

| | | + | H.I. | − | |
|---|---|---|---|---|---|
| | | | 267.09 | | |
| N | | | | | |
| 0+25 | | | | 10.9 | 256.2 |
| +19 | Toe Concrete spillway | | | 9.31 | 257.78 |
| +00 | Lip of Spillway | | | 6.09 | 261.0 |

Details of Spillway

East Side N+4.3. West Side M.+34.3

Lip = 0+00 Toe = 0+19

West End of Curb along 0+00 = L+29.3

| L+29.3 | | | 267.09 | | |
|---|---|---|---|---|---|
| 0+00 | Gutter | | | 4.62 | 262.47 |
| +00 | Top of Curb | | | 3.48 | 263.61 |

East End of Curb along 0+00 = M+34.3

| M+34.3 | | | 267.09 | | |
|---|---|---|---|---|---|
| 0+00 | Gutter | | | 5.99 | 261.10 |
| +00 | Top of Curb | | | 4.73 | 262.36 |
| R. Stone | | 8.85 | 275.72 | 0.22 | 266.87 |
| N.W. B.P. Arizona & Hpas | | | | 5.75 | 269.97 269.95 |



Trees

#1 N.W. Cor. B.L., 1+00, south to B.L., 2+40, East to A+15, 2+55, East to C, 2+45, North to C+38, 1+50, North to D+30, 1+10, West to C+25, 0+65 West to B.L., 1+00.

#2 Group of four trees centered at B+15, 2+75 10' Radius.

#3 N.W. Cor. D+40, 1+88, South to D+22, 2+30, East to F, 2+40, East to G+35, 2+30, East to I+08, 2+00, North to I, 1+85, West to H+10, 1+60, West to D+40, 1+88.

#4 Scrub oaks centered at F+35, 1+50. 20' Radius.

#5 " " " " G+30, 0+60. 15' "

#6 N.W. Cor. I+40, 0+50, South to I+20, 0+95, South to I+25, 1+25, East to K+35, 2+25, North to M, 1+60, North to M, 1+40, West to K+12, 1+15, North to J+25, 0+60, West to I+40, 0+50.

#7 N.W. Cor. L+12, 0+60, East to M+25, 0+85, North to M+25, 0+65, West to L+12, 0+60.

#8 Lone Euca. 2' dia. M+40, 2+00.

#9 Two trees M+20, 3+23 & M+30, 3+26

## Trenches

#1 2.5' trench 0.7' deep. B.L., 4+80 to B.L +10, 4+70 to B.L + 27, 4+87 to A, 4+75 to A+15, 4+80 to A+35, 4+70 to A+25, 4+35 to B.L + 35, 4+35 to B.L. + 13, 4+50 to B.L, 4+40

#2 A+25, 4+35 to A+25, 4+25 to A+10, 3+75 to B, 3+70 to B + 35, 3+95 to B+10, 4+25 to B, 4+10 to A+25, 4+25.

#3 B+35, 3+95 to B+45, 4+55 to B+10, 4+25

#4 B+45, 4+55 to C+05, 5+20 to B+35, 5+30 to B+25, 5+20 to B+05, 5+30 to B+30, 5+60.

#5 B+05, 5+30 to B, 5+40 to A+30, 5+25 to A+42, 5+05 to A+35, 4+70

#6 C+05, 5+20 to C+20, 5+55 to C+25, 5+85 to C+38, 5+97.

#7 4' Trench, 2' deep. G+15, 5+05 to G+25, 5+40.

#8 2.5' " 1' deep. J+35, 5+00 to J+40, 4+65 to K+40, 4+20 to L+37, 3+37.

3-17-32 Shoemaker Updegraf Woods 8-18-34 Urebert Kanagy Bell Keyser

21

## Cross Section of Section "D" (Texas St. Base Line to 700' East & 600' to 1200' South of 0+00)

See P.73 for H.I. of 8-18-34

| | + | H.I. 279.43 8-18-34 | − | | |
|---|---|---|---|---|---|
| 1" offset hub B.L.5+92 | 4.20 | 282.44 | | 278.24 | 3/19/32 |
| B.L. +25 | | | | | 8-18-34 |
| 6+25 | | | 3.5 | 278.9 | |
| +50 | | | 3.8 | 278.6 | |
| +75 | | | 3.9 | 278.5 | |
| 7+00 | | | 4.4 | 278.0 | |
| +25 | | | 4.6 | 277.8 | |
| +50 | | | 4.7 | 277.7 | |
| +75 ✓ | | 8-18-34 | 2.4 4.7 | 277.7 | 277.0 |
| 8+00 | Sta. | 8-18-34 ELEV. | 2.5 4.8 | 277.6 | 276.9 |
| +25 | 8+66 | 275.8 | 2.5 5.2 | 277.2 | 276.9 |
| +50 | 8+54 | 277.7 | 1.5 5.9 | 276.5 | 277.9 |
| +75 | 8+50 | 277.9 | 4.1 6.3 | 276.1 | 275.3 |
| | 8+40 | 277.9 | | | |
| | 8+37 | 276.8 | | | |
| 9+00 | | | 3.8 6.8 | 275.6 | 275.6 |
| +25 | | | 4.3 6.7 | 275.7 | 275.1 |
| +50 | | | 4.6 7.5 | 274.9 | 274.8 |
| +75 | | | 5.2 7.7 | 274.7 | 274.2 |
| 10+00 | | | 5.9 7.9 | 274.5 | 273.5 |
| +25 | | | 6.0 8.1 | 274.3 | 273.4 |
| +50 | | | 6.2 8.9 | 273.5 | 273.2 |
| +75 | | | 6.6 9.5 | 272.9 | 272.8 |

| | + | H.I. 279.43 / 282.44 → 8-18-'34 | − | | 8-18-'34 |
|---|---|---|---|---|---|
| B.L. +25 | | | | | |
| | | 8-18-'34 → 7.4 | | | |
| 11+00 | | | 10.0 | 272.4 | 272.0 |
| | | | 8.0 10.5 | 271.9 | 271.4 |
| +50 | | | 8.5 11.2 | 271.2 | 270.9 |
| +75 | | | 8.7 11.6 | 270.8 | 270.7 |
| 12+00 | | | 8.7 11.7 | 270.7 | 270.7 |
| A | | | | | |
| | | | 10.0 | | |
| 12+00 | | | 13.0 | 269.4 | 269.4 |
| 11+75 | | | 10.1 13.0 | 269.4 | 269.3 |
| +50 | | | 9.7 12.6 | 269.8 | 269.7 |
| +25 | | | 9.2 12.2 | 270.2 | 270.2 |
| 11+00 | | | 8.7 11.8 | 270.6 | 270.7 |
| 10+75 | | | 8.8 11.4 | 271.0 | 270.6 |
| +50 | | | 9.3 10.8 | 271.6 | 270.1 |
| +25 | | | 7.9 10.3 | 272.1 | 271.5 |
| +00 | | | 8.1 9.9 | 272.5 | 271.3 |
| 9+75 | | | 6.7 9.1 | 273.3 | 272.7 |
| +50 | | | 5.8 8.5 | 273.9 | 273.6 |
| +25 | | | 5.8 8.0 | 274.4 | 273.6 |
| +00 | | | 4.8 7.3 | 275.1 | 274.6 |
| 8+75 | 8-18-'34 STA. 8+37 8+40 8+60 | ELEV. 276.8 277.8 276.5 | 4.0 6.5 | 275.9 | 275.4 |
| +50 | | | 1.8 5.4 | 277.0 | 277.6 |
| +25 | | | 2.6 4.7 | 277.7 | 276.8 |
| 8+00 | | | 2.4 4.1 | 278.3 | 277.0 |

Shoemaker 8-18-'34
Updegraf
Woods

22

| | + | H.I. 279.43 / 282.44 | − | | 8-18-'34 |
|---|---|---|---|---|---|
| A | | | | | |
| | | | 2.2 | | |
| 7+75 | | | 3.8 | 278.6 | 277.2 |
| +50 | | | 3.8 | 278.6 | |
| +25 | | | 3.5 | 278.9 | |
| +00 | | | 3.1 | 279.3 | |
| 6+75 | | | 3.0 | 279.4 | |
| +50 | | | 2.9 | 279.5 | |
| +25 | | | 2.5 | 279.9 | |
| A+25 | | | | | |
| 6+25 | | | 1.7 | 280.7 | |
| +50 | | | 2.1 | 280.3 | |
| +75 | | | 2.5 | 279.9 | |
| 7+00 | | | 2.6 | 279.8 | |
| +25 | | | 3.0 | 279.4 | |
| +50 | | | 3.3 | 279.1 | |
| +75 | | | 1.9 3.5 | 278.9 | 277.5 |
| 8+00 | 8-18-'34 STA. 8+36 8+38 8+66 | ELEV. 277.0 277.7 275.6 | 2.1 4.1 | 278.3 | 277.3 |
| +25 | | | 2.6 4.7 | 277.7 | 276.8 |
| +50 | 48' East of A 7+75 = 278.4 | | 1.6 5.4 | 277.0 | 277.8 |
| +75 | | | 3.9 6.3 | 276.1 | 275.5 |
| 9+00 | | | 4.9 7.2 | 275.2 | 274.5 |
| +25 | | | 5.7 8.4 | 274.0 | 273.7 |
| +50 | | | 6.8 9.4 | 273.0 | 272.9 |
| +75 | | | 7.5 10.5 | 271.9 | 271.9 |

| | + | H.I. 279.43 → 282.44 | − | | 8-18-34 |
|---|---|---|---|---|---|
| A+25 | | | | | |
| 10+00 | | | 8.4 11.2 | 271.2 | 271.0 |
| +25 | | | 9.5 12.0 | 270.4 | 269.9 |
| +50 | | | 9.7 12.3 | 270.1 | 269.7 |
| +75 | | | 9.9 12.7 | 269.7 | 269.5 |
| 11+00 | | | 10.1 12.9 | 269.5 | 269.3 |
| +25 | | | 10.3 13.0 | 269.4 | 269.1 |
| +50 | | | 10.3 13.3 | 269.1 | 269.1 |
| +75 | | | 10.8 13.7 | 268.7 | 268.6 |
| 12+00 | | | 10.9 13.7 | 268.7 | 268.5 |
| B | | | | | |
| 12+00 | | | 11.2 14.2 | 268.2 | 268.2 |
| 11+75 | | | 11.4 14.5 | 267.9 | 268.0 |
| +50 | | | 11.3 14.2 | 268.2 | 268.1 |
| +25 | | | 11.0 14.0 | 268.4 | 268.4 |
| +00 | | | 10.9 13.9 | 268.5 | 268.5 |
| 10+75 | | | 10.3 13.4 | 269.0 | 269.1 |
| +50 | | | 10.1 13.1 | 269.3 | 269.3 |
| +25 | | | 9.6 12.5 | 269.9 | 269.8 |
| +00 | | | 9.3 12.0 | 270.4 | 270.1 |
| 9+75 | | | 8.4 11.1 | 271.3 | 271.0 |
| +50 | | | 7.6 9.9 | 272.5 | 271.8 |
| +25 | | | 6.7 9.0 | 273.4 | 272.7 |
| 9+00 | | | 5.7 8.2 | 274.2 | 273.7 |

Shoemaker 8-18-34
Updegraf
Woods



| | + | H.I. 279.43 282.44 | − | | 8-18-34 |
|---|---|---|---|---|---|
| B | | | | | |
| 8+75 | | | 5.2 7.2 | 275.2 | 274.2 |
| +50 | | | 6.2 | 276.2 | |
| +25 | | | 5.2 | 277.2 | |
| 7+75 | | | 0.6 4.4 | 278.0 | 278.8 |
| +50 | | | 3.7 | 278.7 | |
| +25 | | | 3.4 | 279.0 | |
| +00 | | | 3.1 | 279.3 | |
| 6+75 | | | 2.6 | 279.8 | |
| +50 | | | 2.0 | 280.4 | |
| +25 | | | 1.6 | 280.8 | |
| B+25 | | | | | |
| 6+25 | | | 1.2 | 281.2 | |
| +50 | | | 2.0 | 280.4 | |
| +75 | | | 2.8 | 279.6 | |
| 7+00 | | | 3.6 | 278.8 | |
| +25 | | | 4.4 | 278.0 | |
| +50 | | | 4.8 | 277.6 | |
| +75 | | | 5.0 | 277.4 | |
| 8+00 | | | 5.5 | 276.9 | |
| +25 | | | 6.2 | 276.2 | |
| +50 | | | 7.2 | 275.2 | |
| +75 | | | 5.9 8.0 | 274.4 | 273.5 |
| 9+00 | | | 6.6 9.1 | 273.3 | 272.8 |

274.15
.78
274.93

| | + | H.I. 279.43 - 282.44 | − 8-18-34 | | 8-18-34 |
|---|---|---|---|---|---|
| B+25 | | | | | |
| 9+25 | | | 7.7 10.0 | 272.4 | 271.7 |
| +50 | | | 8.6 10.9 | 271.5 | 270.8 |
| +75 | | | 9.1 11.7 | 270.7 | 270.3 |
| 10+00 | | | 9.4 12.2 | 270.2 | 270.0 |
| +25 | | | 9.9 12.8 | 269.6 | 269.5 |
| +50 | | | 10.5 13.2 | 269.2 | 268.9 |
| +75 | | | 10.6 13.7 | 268.7 | 268.8 |
| 11+00 | | | 11.1 14.1 | 268.3 | 268.3 |
| +25 | | | 11.5 14.6 | 267.8 | 267.9 |
| +50 | | | 11.7 14.5 | 267.9 | 267.7 |
| +75 | | | 11.8 14.8 | 267.6 | 267.6 |
| 12+00 | | | 11.5 14.5 | 267.9 | 267.9 |
| C | | | | | |
| 12+00 | | | 11.4 14.3 | 268.1 | 268.0 |
| 11+75 | | | 12.2 15.1 | 267.3 | 267.2 |
| +50 | | | 12.2 15.3 | 267.1 | 267.2 |
| +25 | | | 11.4 14.2 | 268.2 | 268.0 |
| +00 | | | 11.1 13.8 | 268.6 | 268.3 |
| 10+75 | | | 10.8 13.3 | 269.1 | 268.6 |
| +50 | | | 10.0 12.9 | 269.5 | 269.4 |
| +25 | | | 9.4 12.4 | 270.0 | 270.0 |
| +00 | | | 9.0 12.0 | 270.4 | 270.4 |
| 9+75 | | | 8.7 11.8 | 270.6 | 270.7 |

Shoemaker 8-18-'34
Updegraf 8-20-'34
Woods



| | + | H.I. 279.43 - 282.44 | − 8-18-'34 | | 8-18-'34 |
|---|---|---|---|---|---|
| C | | | | | |
| 9+50 | | | 8.3 11.3 | 271.1 | 271.1 |
| +25 | | | 8.0 10.8 | 271.6 | 271.4 |
| 9+00 | | | 7.2 9.9 | 272.5 | 272.2 |
| 8+75 | | | 6.2 9.1 | 273.3 | 273.2 |
| +50 | | | 8.1 | 274.3 | |
| +25 | | | 7.3 | 275.1 | |
| +00 | | | 6.7 | 275.7 | |
| 7+75 | | | 6.8 | 275.6 | |
| +50 | | | 6.4 | 276.0 | |
| +25 | | | 5.5 | 276.9 | |
| +00 | | | 4.0 | 278.4 | |
| 6+75 | | | 2.9 | 279.5 | |
| +50 | | | 2.2 | 280.2 | |
| +25 | | | 1.6 | 280.8 | |
| C+25 | | | | | |
| 6+25 | | | 2.6 | 279.8 | |
| +50 | | | 3.4 | 279.0 | |
| +75 | | | 4.5 | 277.9 | |
| 7+00 | | | 5.5 | 276.9 | |
| +25 | | | 6.8 | 275.6 | |
| +50 | | | 7.8 | 274.6 | |
| +75 | | | 8.2 | 274.2 | |
| 8+00 | | | 8.1 | 274.3 | |

See page 73 for H.I.

| | + | H.I. 274.93 → 8-20-34 282.44 | − | | 8-20-34 |
|---|---|---|---|---|---|
| C+25 | | | | | |
| 8+25 | | | 8.1 | 274.3 | |
| +50 | | | 8.4 | 274.0 | |
| +75 | | | 9.1 (2.0) | 273.3 | 272.9 |
| 9+00 | | | 9.8 (2.9) | 272.6 | 272.0 |
| +25 | | | 10.5 (3.2) | 271.9 | 271.7 |
| +50 | | | 11.0 (3.9) | 271.4 | 271.0 |
| +75 | | | 11.6 (4.5) | 270.8 | 270.4 |
| 10+00 | | | 11.9 (5.2) | 270.5 | 269.7 |
| +25 | | | 12.5 (5.5) | 269.9 | 269.4 |
| +50 | | | 12.9 (6.5) | 269.5 | 268.4 |
| +75 | | | 13.6 (6.7) | 268.8 | 268.2 |
| 11+00 | | | 14.3 (8.0) | 268.1 | 266.9 |
| +25 | | | 14.8 (8.5) | 267.6 | 266.4 |
| +50 | | | 15.7 (9.0) | 266.7 | 265.9 |
| +75 | | | 15.6 (8.3) | 266.8 | 266.6 |
| 12+00 | | | 15.0 (7.5) | 267.4 | 267.4 |
| II | | | | | |
| 12+00 | | | 16.8 (9.9) | 265.6 | 265.0 |
| 11+75 | | | 16.8 (10.1) | 265.6 | 264.8 |
| +50 | | | 16.5 (9.2) | 265.9 | 265.7 |
| +25 | | | 16.1 (8.6) | 266.3 | 266.3 |
| +00 | | | 15.0 (7.6) | 267.4 | 267.3 |
| 10+75 | | | 14.3 (7.0) | 268.1 | 267.9 |

Shoemaker 8-20-34
Updegraf
Woods,

25

OS lower on AV than original TBM

| | + | H.I. 274.93 → 8-20-34 282.44 | − | | 8-20-34 |
|---|---|---|---|---|---|
| II | | | | | |
| 10+50 | | | 13.4 (6.6) | 269.0 | 268.3 |
| +25 | | | 13.0 (6.2) | 269.4 | 268.7 |
| +00 | | | 12.4 (5.6) | 270.0 | 269.3 |
| 9+75 | | | 12.0 (5.0) | 270.4 | 269.9 |
| +50 | | | 11.0 (3.8) | 271.4 | 271.1 |
| +25 | | | 10.4 (3.3) | 272.0 | 271.6 |
| +00 | | | 9.8 (2.9) | 272.6 | 272.0 |
| 8+75 | | | 9.5 (2.6) | 272.9 | 272.3 |
| +50 | | | 9.1 | 273.3 | |
| +25 | | | 9.2 | 273.2 | |
| +00 | | | 9.3 | 273.1 | |
| 7+75 | | | 9.8 | 272.6 | |
| +50 | | | 9.3 | 273.1 | |
| +25 | | | 8.9 | 273.5 | |
| +00 | | | 8.0 | 274.4 | |
| 6+75 | | | 6.7 | 275.7 | |
| +50 | | | 5.6 | 276.8 | |
| +25 | | | 4.4 | 278.0 | |
| II+25 | | | | | |
| 6+25 | | | 7.4 | 275.0 | |
| +50 | | | 8.5 | 273.9 | |
| +75 | | | 9.2 | 273.2 | |
| 7+00 | | | 10.1 | 272.3 | |

| | + | H.I. 282.44 | − | |
|---|---|---|---|---|
| II+25 | | | | |
| 7+25 | | | 10.8 | 271.6 |
| +50 | | | 10.7 | 271.7 |
| +75 | | | 10.6 | 271.8 |
| 8+00 | | | 10.2 | 272.2 |
| +25 | | | 9.5 | 272.9 |
| +50 | | | 9.5 | 272.9 |
| +75 | | | 9.7 | 272.7 |
| 9+00 | | | 10.1 | 272.3 |
| +25 | | | 10.4 | 272.0 |
| +50 | | | 10.9 | 271.5 |
| +75 | | | 11.8 | 270.6 |
| 10+00 | | | 12.5 | 269.9 |
| +25 | | | 13.1 | 269.3 |
| +50 | | | 13.5 | 268.9 |
| +75 | | | 13.7 | 268.7 |
| 11+00 | | | 13.7 | 268.7 |
| +25 | | | 14.8 | 267.6 |
| +50 | | | 15.3 | 267.1 |
| +75 | | | 16.2 | 266.2 |
| 12+00 | | | 17.5 | 264.9 |
| E | | | | |
| 12+00 | | | 16.1 | 266.3 |
| 11+75 | | | 14.7 | 267.7 |

| | + | H.I. 282.44 | − | |
|---|---|---|---|---|
| E | | | | |
| 11+50 | | | 13.7 | 268.7 |
| +25 | | | 13.1 | 269.3 |
| +00 | | | 12.8 | 269.6 |
| 10+75 | | | 12.3 | 270.1 |
| +50 | | | 12.2 | 270.2 |
| +25 | | | 12.1 | 270.3 |
| +00 | | | 11.9 | 270.5 |
| 9+75 | | | 11.2 | 271.2 |
| +50 | | | 10.6 | 271.8 |
| +25 | | | 10.2 | 272.2 |
| +00 | | | 9.8 | 272.6 |
| 8+75 | | | 9.5 | 272.9 |
| +50 | | | 9.5 | 272.9 |
| +25 | | | 10.2 | 272.2 |
| +00 | | | 10.8 | 271.6 |
| 7+75 | | | 10.9 | 271.5 |
| +50 | | | 11.6 | 270.8 |
| +25 | | | 12.0 | 270.4 |
| +00 | | | 11.9 | 270.5 |
| 6+75 | | | 11.4 | 271.0 |
| +50 | | | 11.1 | 271.3 |
| +25 | | | 10.7 | 271.7 |

| | + | H.I. 282.44 | − | |
|---|---|---|---|---|
| E | | | | |
| 6+25 | | | 12.6 | 269.8 |
| +50 | | | 12.7 | 269.7 |
| +75 | | | 12.9 | 269.5 |
| 7+00 | | | 13.2 | 269.2 |
| +25 | | | 13.0 | 269.4 |
| +50 | | | 12.5 | 269.9 |
| +75 | | | 11.8 | 270.6 |
| 8+00 | | | 10.9 | 271.5 |
| +25 | | | 10.2 | 272.2 |
| +50 | | | 9.9 | 272.5 |
| +75 | | | 9.8 | 272.6 |
| 9+00 | | | 9.8 | 272.6 |
| +25 | | | 10.0 | 272.4 |
| +50 | | | 10.2 | 272.2 |
| +75 | | | 10.4 | 272.0 |
| 10+00 | | | 10.5 | 271.9 |
| +25 | | | 10.9 | 271.5 |
| +50 | | | 11.1 | 271.3 |
| +75 | | | 11.3 | 271.1 |
| 11+00 | | | 11.9 | 270.5 |
| +25 | | | 12.4 | 270.0 |
| +50 | | | 12.8 | 269.6 |
| +75 | | | 13.7 | 268.7 |
| 12+00 | | | 15.0 | 267.4 |

| | + | H.I. 282.44 | − | |
|---|---|---|---|---|
| PP Rock Ft+15, 10+90 | 2.07 | 274.10 | 10.41 | 272.03 |
| F | | | | |
| 12+00 | | | 5.3 | 268.8 |
| 11+75 | | | 4.2 | 269.9 |
| +50 | | | 3.4 | 270.7 |
| +25 | | | 3.0 | 271.1 |
| +00 | | | 2.5 | 271.6 |
| 10+75 | | | 2.3 | 271.8 |
| +50 | | | 2.0 | 272.1 |
| +25 | | | 1.8 | 272.3 |
| +00 | | | 1.7 | 272.4 |
| 9+75 | | | 1.7 | 272.4 |
| +50 | | | 1.8 | 272.3 |
| +25 | | | 1.9 | 272.2 |
| +00 | | | 2.0 | 272.1 |
| 8+75 | | | 2.1 | 272.0 |
| +50 | | | 2.0 | 272.1 |
| +25 | | | 2.4 | 271.7 |
| +00 | | | 2.9 | 271.2 |
| 7+75 | | | 4.1 | 270.0 |
| +50 | | | 4.6 | 269.5 |
| +25 | | | 5.3 | 268.8 |
| +00 | | | 5.9 | 268.5 |
| 6+75 | | | 5.9 | 268.5 |

| | + | H.I. 274.10 | − | |
|---|---|---|---|---|
| F | | | | |
| 6+50 | | | 5.8 | 268.3 |
| +25 | | | 6.1 | 268.0 |
| F+25 | | | | |
| 6+25 | | | 6.2 | 267.9 |
| +50 | | | 6.3 | 267.8 |
| +75 | | | 6.6 | 267.5 |
| 7+00 | | | 5.9 | 268.2 |
| +25 | | | 5.8 | 268.3 |
| +50 | | | 5.8 | 268.3 |
| +75 | | | 5.6 | 268.5 |
| 8+00 | | | 4.7 | 269.4 |
| +25 | | | 4.2 | 269.9 |
| +50 | | | 3.0 | 271.1 |
| +75 | | | 2.8 | 271.3 |
| 9+00 | | | 3.0 | 271.1 |
| +25 | | | 3.2 | 270.9 |
| +50 | | | 3.2 | 270.9 |
| +75 | | | 2.6 | 271.5 |
| 10+00 | | | 2.2 | 271.9 |
| +25 | | | 1.8 | 272.3 |
| +50 | | | 1.6 | 272.5 |
| +75 | | | 1.5 | 272.6 |

| | + | H.I. 274.10 | − | |
|---|---|---|---|---|
| 11+00 | | | 1.7 | 272.4 |
| +25 | | | 2.0 | 272.1 |
| +50 | | | 2.3 | 271.8 |
| +75 | | | 3.1 | 271.0 |
| 12+00 | | | 4.3 | 269.8 |
| G | | | | |
| 12+00 | | | 4.0 | 270.1 |
| 11+75 | | | 2.7 | 271.4 |
| +50 | | | 2.4 | 271.7 |
| +25 | | | 2.0 | 272.1 |
| +00 | | | 1.6 | 272.5 |
| 10+75 | | | 1.5 | 272.6 |
| +50 | | | 1.4 | 272.7 |
| +25 | | | 2.0 | 272.1 |
| +00 | | | 2.4 | 271.7 |
| 9+75 | | | 3.2 | 270.9 |
| +50 | | | 3.6 | 270.5 |
| +25 | | | 4.2 | 269.9 |
| +00 | | | 4.6 | 269.5 |
| 8+75 | | | 4.5 | 269.6 |
| +50 | | | 5.3 | 268.8 |
| +25 | | | 5.4 | 268.7 |
| +00 | | | 4.7 | 269.4 |

| | + | H.I. 274.10 | − | |
|---|---|---|---|---|
| G | | | | |
| 7+75 | | | 5.7 | 268.4 |
| +50 | | | 6.2 | 267.9 |
| +25 | | | 6.4 | 267.7 |
| +00 | | | 6.4 | 267.7 |
| 6+75 | | | 6.6 | 267.5 |
| +50 | | | 7.0 | 267.1 |
| +25 | | | 7.1 | 267.0 |
| G+25 | | | | |
| 6+25 | | | 7.0 | 267.1 |
| +50 | | | 6.9 | 267.2 |
| +75 | | | 6.7 | 267.4 |
| 7+00 | | | 6.4 | 267.7 |
| +25 | | | 6.2 | 267.9 |
| +50 | | | 5.9 | 268.2 |
| +75 | | | 5.6 | 268.5 |
| 8+00 | | | 5.7 | 268.4 |
| +25 | | | 6.2 | 267.9 |
| +50 | | | 6.8 | 267.3 |
| +75 | | | 7.5 | 266.6 |
| 9+00 | | | 6.8 | 267.3 |
| +25 | | | 6.3 | 267.8 |
| +50 | | | 5.3 | 268.8 |
| +75 | | | 4.3 | 269.8 |

| | + | H.I. 274.10 | − | |
|---|---|---|---|---|
| G+25 | | | | |
| 10+00 | | | 3.0 | 271.1 |
| +25 | | | 1.9 | 272.2 |
| +50 | | | 1.5 | 272.6 |
| +75 | | | 1.4 | 272.7 |
| 11+00 | | | 1.3 | 272.8 |
| +25 | | | 1.8 | 272.3 |
| +50 | | | 2.3 | 271.8 |
| +75 | | | 3.4 | 270.7 |
| 12+00 | | | 4.3 | 269.8 |
| H | | | | |
| 12+00 | | | 3.7 | 270.4 |
| 11+75 | | | 2.8 | 271.3 |
| +50 | | | 2.2 | 271.9 |
| +25 | | | 1.6 | 272.5 |
| +00 | | | 1.5 | 272.6 |
| 10+75 | | | 1.2 | 272.9 |
| +50 | | | 1.9 | 272.2 |
| +25 | | | 2.8 | 271.3 |
| +00 | | | 3.6 | 270.5 |
| 9+75 | | | 5.2 | 268.9 |
| +50 | | | 6.6 | 267.5 |
| +25 | | | 8.1 | 266.0 |
| +00 | | | 8.8 | 265.3 |

| | + | H.I. 274.10 | − | |
|---|---|---|---|---|
| H | | | | |
| 8+75 | | | 8.8 | 265.3 |
| +50 | | | 8.0 | 266.1 |
| +25 | | | 7.3 | 266.8 |
| +00 | | | 6.9 | 267.2 |
| 7+75 | | | 6.5 | 267.6 |
| +50 | | | 6.4 | 267.7 |
| +25 | | | 6.0 | 268.1 |
| +00 | | | 6.1 | 268.0 |
| 6+75 | | | 6.6 | 267.5 |
| +50 | | | 6.4 | 267.7 |
| +25 | | | 6.2 | 267.9 |
| H+25 | | | | |
| 6+25 | | | 7.0 | 267.1 |
| +50 | | | 6.7 | 267.4 |
| +75 | | | 6.5 | 267.6 |
| 7+00 | | | 6.5 | 267.6 |
| +25 | | | 6.2 | 267.9 |
| +50 | | | 7.0 | 267.1 |
| +75 | | | 7.3 | 266.8 |
| 8+00 | | | 8.1 | 266.0 |
| +25 | | | 8.4 | 265.7 |
| +50 | | | 8.9 | 265.2 |
| +75 | | | 10.3 | 263.8 |

| | + | H.I. 274.10 | − | |
|---|---|---|---|---|
| H+25 | | | | |
| 9+00 | | | 10.9 | 263.2 |
| +25 | | | 9.6 | 263.5 |
| +50 | | | 8.2 | 265.9 |
| +75 | | | 6.3 | 267.8 |
| 10+00 | | | 5.3 | 268.8 |
| +25 | | | 4.2 | 269.9 |
| +50 | | | 3.4 | 270.7 |
| +75 | | | 2.4 | 271.7 |
| 11+00 | | | 2.0 | 272.1 |
| +25 | | | 2.2 | 271.9 |
| +50 | | | 2.6 | 271.5 |
| +75 | | | 3.0 | 271.1 |
| 12+00 | | | 3.9 | 270.2 |
| I | | | | |
| 12+00 | | | 4.4 | 269.7 |
| 11+75 | | | 3.4 | 270.7 |
| +50 | | | 3.4 | 270.7 |
| +25 | | | 3.4 | 270.7 |
| +00 | | | 3.9 | 270.2 |
| 10+75 | | | 4.5 | 269.6 |
| +50 | | | 4.8 | 269.3 |
| +25 | | | 5.8 | 268.3 |
| +00 | | | 6.7 | 267.4 |

| | + | H.I. 274.10 | − | |
|---|---|---|---|---|
| I | | | | |
| 9+75 | | | 9.6 | 264.5 |
| +50 | | | 10.6 | 263.5 |
| +25 | | | 12.1 | 262.0 |
| +00 | | | 12.5 | 261.6 |
| 8+75 | | | 11.9 | 262.2 |
| +50 | | | 10.7 | 263.4 |
| +25 | | | 10.0 | 264.1 |
| +00 | | | 8.9 | 265.2 |
| 7+75 | | | 8.3 | 265.8 |
| +50 | | | 8.2 | 265.9 |
| +25 | | | 7.6 | 266.5 |
| +00 | | | 7.6 | 266.5 |
| 6+75 | | | 7.9 | 266.2 |
| +50 | | | 8.2 | 265.9 |
| +25 | | | 8.0 | 266.1 |
| I+25 | | | | |
| 6+25 | | | 8.6 | 265.5 |
| +50 | | | 8.7 | 265.4 |
| +75 | | | 8.9 | 265.2 |
| 7+00 | | | 8.7 | 265.4 |
| +25 | | | 8.8 | 265.3 |
| +50 | | | 9.2 | 264.9 |
| +75 | | | 9.2 | 264.9 |



| | + | H.I. 274.10 | − | |
|---|---|---|---|---|
| I+25 | | | | |
| 8+00 | | | 10.1 | 264.0 |
| +25 | | | 10.7 | 263.4 |
| +50 | | | 12.0 | 262.1 |
| +75 | | | 13.3 | 260.8 |
| 9+00 | | | 14.3 | 259.8 |
| +25 | | | 13.4 | 260.7 |
| +50 | | | 12.2 | 261.9 |
| +75 | | | 10.4 | 263.7 |
| 10+00 | | | 9.2 | 264.9 |
| +25 | | | 7.8 | 266.3 |
| +50 | | | 7.1 | 267.0 |
| +75 | | | 6.1 | 268.0 |
| 11+00 | | | 5.8 | 268.3 |
| +25 | | | 5.1 | 269.0 |
| +50 | | | 4.9 | 269.2 |
| +75 | | | 5.1 | 269.0 |
| J | | | | |
| 11+50 | | | 7.3 | 266.8 |
| +25 | | | 7.5 | 266.6 |
| +00 | | | 8.0 | 266.1 |
| 10+75 | | | 9.0 | 265.1 |
| +50 | | | 9.7 | 264.4 |
| +25 | | | 10.5 | 263.6 |

| | + | H.I. 274.10 | − | |
|---|---|---|---|---|
| J | | | | |
| 10+00 | | | 11.5 | 262.6 |
| 9+75 | | | 13.2 | 260.9 |
| +50 | | | 15.1 | 259.0 |
| +25 | | | 16.1 | 258.0 |
| +00 | | | 15.8 | 258.3 |
| 8+75 | | | 14.5 | 259.6 |
| +50 | | | 12.9 | 261.2 |
| +25 | | | 11.5 | 262.6 |
| +00 | | | 10.9 | 263.2 |
| 7+75 | | | 10.3 | 263.8 |
| +50 | | | 10.1 | 264.0 |
| +25 | | | 10.1 | 264.0 |
| +00 | | | 10.3 | 263.8 |
| 6+75 | | | 10.2 | 263.9 |
| +50 | | | 10.2 | 263.9 |
| +25 | | | 10.0 | 264.1 |
| J+25 | | | | |
| 6+25 | | | 13.0 | 261.1 |
| +50 | | | 12.9 | 261.2 |
| +75 | | | 12.3 | 261.8 |
| 7+00 | | | 12.3 | 261.8 |
| +25 | | | 12.2 | 261.9 |
| +50 | | | 12.2 | 261.9 |

| | + | H.I. 274.10 | − | |
|---|---|---|---|---|
| J+25 | | | | |
| 7+75 | | | 12.0 | 262.1 |
| 8+00 | | | 11.9 | 262.2 |
| +25 | | | 12.6 | 261.5 |
| P. Rock J, 8+42 | 2.48 | 264.07 ✓ | 12.51 | 261.59 ✓ |
| J+25 | | | | |
| 8+50 | | | 4.4 | 259.7 |
| +75 | | | 6.0 | 258.1 |
| 9+00 | | | 7.3 | 256.8 |
| +25 | | | 7.5 | 256.6 |
| +50 | | | 6.5 | 257.6 |
| +75 | | | 3.9 | 260.2 |
| 10+00 | | | 3.0 | 261.1 |
| +25 | | | 1.8 | 262.3 |
| +50 | | | 1.6 | 262.5 |
| +75 | | | 1.1 | 263.0 |
| K | | | | |
| 10+50 | | | 3.2 | 260.9 |
| +25 | | | 3.6 | 260.5 |
| +00 | | | 3.9 | 260.2 |
| 9+75 | | | 5.9 | 258.2 |
| +50 | | | 8.5 | 255.6 |
| +25 | | | 9.6 | 254.5 |
| +00 | | | 9.6 | 254.5 |

| | + | H.I. 264.07 | − | |
|---|---|---|---|---|
| K | | | | |
| 8+75 | | | 8.6 | 255.5 |
| +50 | | | 7.5 | 256.6 |
| +25 | | | 5.8 | 258.3 |
| +00 | | | 5.0 | 259.1 |
| 7+75 | | | 5.1 | 259.0 |
| +50 | | | 5.0 | 259.1 |
| +25 | | | 5.3 | 258.8 |
| +00 | | | 5.2 | 258.9 |
| 6+75 | | | 5.7 | 258.4 |
| +50 | | | 6.2 | 257.9 |
| +25 | | | 5.8 | 258.3 |
| K+25 | | | | |
| 6+25 | | | 8.8 | 255.3 |
| +50 | | | 8.7 | 255.4 |
| +75 | | | 8.0 | 256.1 |
| 7+00 | | | 8.5 | 255.6 |
| +25 | | | 8.4 | 255.7 |
| +50 | | | 8.3 | 255.8 |
| +75 | | | 8.0 | 256.1 |
| 8+00 | | | 8.7 | 255.4 |
| +25 | | | 8.9 | 255.2 |
| +50 | | | 10.2 | 253.9 |
| +75 | | | 10.9 | 253.2 |

| | + | H.I. 264.07 | − | |
|---|---|---|---|---|
| K+25 | | | | |
| 9+00 | | | 11.8 | 252.3 |
| +25 | | | 10.9 | 253.2 |
| +50 | | | 9.7 | 254.4 |
| +75 | | | 8.8 | 255.3 |
| 10+00 | | | 6.5 | 257.6 |
| L | | | | |
| 10+00 | | | 9.0 | 255.1 |
| 9+75 | | | 11.6 | 252.5 |
| +50 | | | 13.1 | 251.0 |
| +25 | | | 13.5 | 250.6 |
| +00 | | | 14.3 | 249.8 |
| 8+75 | | | 13.6 | 250.5 |
| +50 | | | 12.6 | 251.5 |
| +25 | | | 11.6 | 252.5 |
| +00 | | | 11.1 | 253.0 |
| 7+75 | | | 11.1 | 253.0 |
| +50 | | | 11.2 | 252.9 |
| +25 | | | 11.7 | 252.4 |
| +00 | | | 11.8 | 252.3 |
| 6+75 | | | 12.4 | 251.7 |
| +50 | | | 12.6 | 251.5 |
| +25 | | | 11.8 | 252.3 |
| +00 | | | 11.0 | 253.1 |


253.1

Trenches.

#1 4' Trench, 1' deep. G+08, 8+55
to G+20, 9+45.

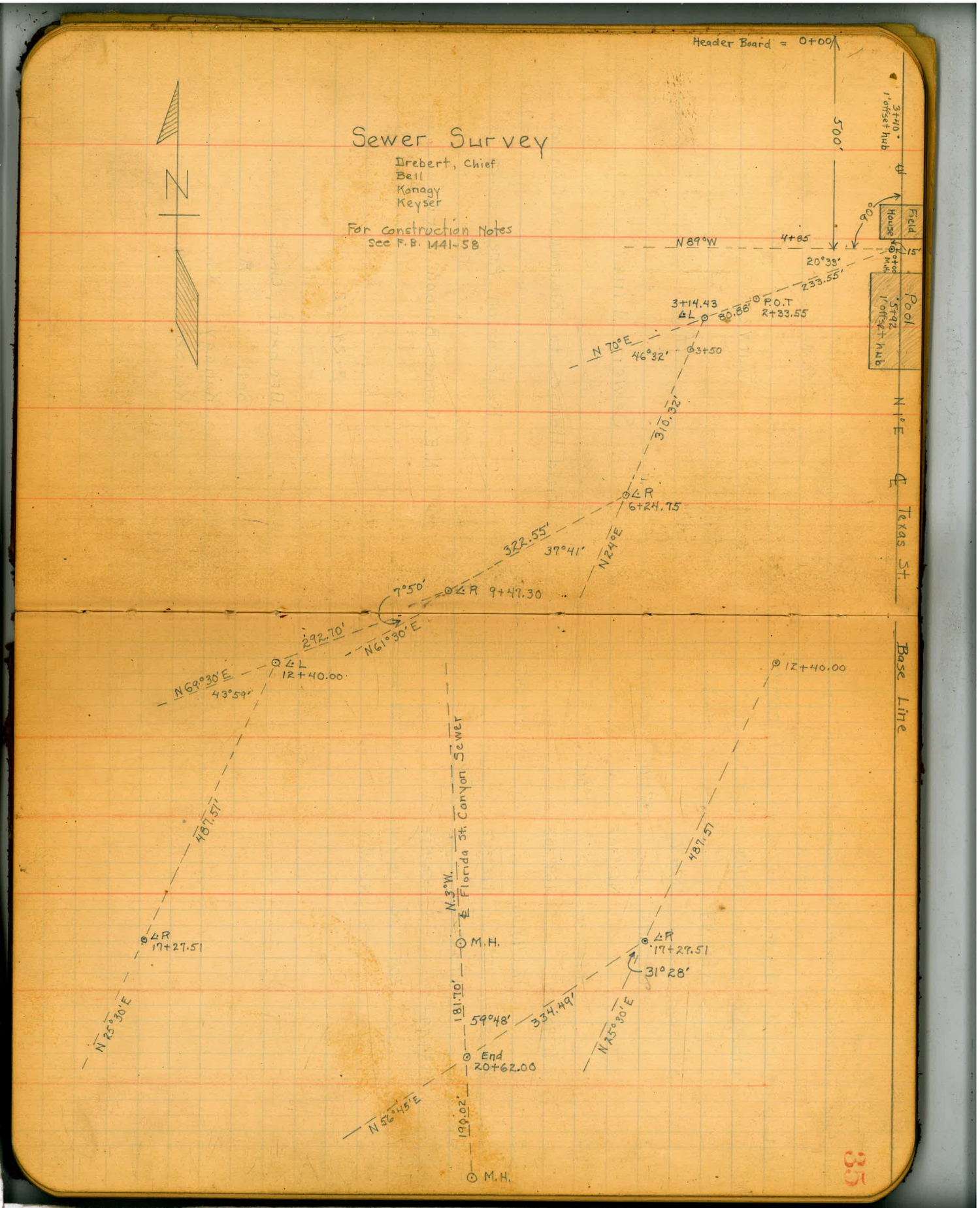
indexed
C.S.K.



# Survey
# of
# Sewer Line
## Field House to Florida St. Canyon
## Recreation Area
## N.E. Corner Balboa Park

3-24-32

Drebert, Chief
Bell
Kanagy Ch.
Keyser Ch.




# Sewer Survey

Drebert, Chief
Bell
Konagy
Keyser

For Construction Notes
See F.B. 1441-58

3-24-32

Irebert
Bell
Kanagy
Keyser



| Angle Point | Hor. Distance | Station | Mag. Bearing | Angle Right | Angle Left | Description |
|---|---|---|---|---|---|---|
| | | | N 89°W | | | |
| 1 | | 0 + 00 | | | 20°33' | 15' South of Field House and 500' South of 0+00 (header board 40' South of North Line of Hpas); and 15' West of Texas St. Base Line. |
| | 314.43 | | N 70°E | | | |
| 2 | | 3+14.43 | | | 46°32' | |
| | 310.32 | | N 24°E | | | |
| 3 | | 6+24.75 | | 37°41' | | Bottom of Canyon |
| | 322.55 | | N 61°30'E | | | |
| 4 | | 9+47.30 | | 7°50' | | " " " |
| | 292.70 | | N 69°30'E | | | |
| 5 | | 12+40.00 | | | 43°59' | " " " |
| | 487.51 | | N 25°30'E | | | |
| 6 | | 17+27.51 | | 31°28' | | " " " |
| | 334.49 | | N 56°45'E | | | |
| 7 | | 20+62.00 | | | 59°48' | On ℄ of Florida St. Canyon Main |
| | | | N 3°W | | | |

3-25-32

Drebert
Bell
Kanagy
Keyser

# ℄ Profile of Sewer Line from Field House to Florida St. Canyon Main.

| | | + | H.I. | − | | |
|---|---|---|---|---|---|---|
| | | | | | | 267.29 |
| 1' offset hub B.L. 5+92 | | 1.49 | 279.73 ✓ | | | 278.24 |
| 0+00 | Hub | | | 1.34 | 278.4 | |
| +25 | | | | 1.7 | 278.0 | |
| +50 | | | | 3.8 | 275.9 | |
| +75 | | | | 5.0 | 274.7 | |
| 1+00 | | | | 6.0 | 273.7 | |
| +25 | | | | 6.2 | 273.5 | |
| +50 | | | | 7.4 | 272.3 | |
| +75 | | | | 8.8 | 270.9 | |
| 2+00 | | | | 10.0 | 269.7 | |
| +25 | | | | 10.7 | 269.0 | |
| +33.55 | P.O.T. hub. | | | 11.19 | 268.5 | |
| +40 | | | | 12.1 | 267.6 | |
| T.P. #1 | Rock opp. 3+90 | 0.35 | 267.29 ✓ | 12.79 | 266.94 ✓ | |
| 2+48 | | | | 2.6 | 264.7 | |
| +50 | | | | 2.7 | 264.6 | |
| +75 | | | | 5.0 | 262.3 | |
| +80 | | | | 6.3 | 261.0 | |
| +85 | | | | 8.8 | 258.5 | |
| +97 | | | | 9.5 | 257.8 | |
| +98 | | | | 12.0 | 255.3 | |
| 3+00 | | | | 12.0 | 255.3 | |
| +06 | | | | 11.6 | 255.7 | |
| +08 | | | | 9.7 | 257.6 | |
| 3+14.43 | Hub | | | 8.53 | 258.8 | |
| +19 | | | | 9.2 | 258.1 | |
| T.P. #2 | Rock in Gully opp. 3+14.43 | 0.51 | 254.86 ✓ | 12.94 | 254.35 ✓ | |
| 3+25 | | | | 1.3 | 253.6 | |
| +50 | | | | 3.5 | 251.4 | |
| +71 | | | | 5.2 | 249.7 | |
| +72 | | | | 3.9 | 251.0 | |
| +75 | | | | 3.8 | 251.1 | |
| 4+00 | | | | 6.4 | 248.5 | |
| +20 | | | | 7.8 | 247.1 | |
| +25 | | | | 8.9 | 246.0 | |
| +29 | | | | 10.0 | 244.9 | |
| +40 | | | | 11.7 | 243.2 | |
| +50 | | | | 11.5 | 243.4 | |
| +53 | | | | 11.1 | 243.8 | |
| +75 | | | | 12.2 | 242.7 | |
| T.P. #3 | Lath on ℄ at 4+83 | 0.00 | 242.10 ✓ | 12.76 | 242.10 ✓ | |
| 5+00 | | | | 2.4 | 239.7 | |
| +05 | | | | 3.3 | 238.8 | |
| +06 | | | | 4.5 | 237.6 | |
| +25 | | | | 5.5 | 236.6 | |

| | + | H.I. | − | |
|---|---|---|---|---|
| | | 242.10 | | |
| 5+40 | | | 6.4 | 235.7 |
| +43 | | | 5.7 | 236.4 |
| +50 | | | 5.5 | 236.6 |
| +75 | | | 6.4 | 235.7 |
| 6+00 | | | 8.6 | 233.5 |
| +09 | | | 10.2 | 231.9 |
| +13 | | | 12.1 | 230.0 |
| +15 | | | 11.9 | 230.2 |
| T.P.#4 Hub at 6+24.75 | 1.10 | 235.54 ✓ | 7.66 | 234.44 ✓ |
| 6+50 | | | 3.8 | 231.7 |
| +63 | | | 5.3 | 230.2 |
| +75 | | | 6.7 | 228.8 |
| +83 | | | 8.8 | 226.7 |
| 7+00 | | | 9.8 | 225.7 |
| +09 | | | 10.5 | 225.0 |
| +10 | | | 8.9 | 226.6 |
| +16 | | | 7.6 | 227.9 |
| +25 | | | 6.8 | 228.7 |
| +35 | | | 6.7 | 228.8 |
| +50 | | | 8.3 | 227.2 |
| +75 | | | 11.4 | 224.1 |
| 8+00 | | | 13.4 | 222.1 |
| 03 | | | 12.9 | 222.6 |
| 05 | | | 11.2 | 224.3 |

| | + | H.I. | − | |
|---|---|---|---|---|
| | | 235.54 | | |
| 8+25 | | | 12.3 | 223.2 |
| T.P.#5 Lath on ℄ at 8+30 | 0.89 | 223.41 ✓ | 13.00 | 222.54 ✓ |
| 8+50 | | | 3.1 | 220.3 |
| +67 | | | 5.5 | 217.9 |
| +70 | | | 7.0 | 216.4 |
| +75 | | | 6.8 | 216.6 |
| 9+00 | | | 8.4 | 215.0 |
| +01 | | | 7.9 | 215.5 |
| +02 | | | 6.9 | 216.5 |
| +08 | | | 5.9 | 217.5 |
| +25 | | | 5.9 | 217.5 |
| +41 | | | 9.0 | 214.4 |
| +47.30 Hub | | | 10.09 | 213.3 |
| +50 | | | 10.5 | 212.9 |
| +67 | | | 12.8 | 210.6 |
| +75 | | | 12.3 | 211.1 |
| T.P.#6 Lath on ℄ at 9+89 | 1.54 | 212.48 ✓ | 12.47 | 210.94 ✓ |
| 10+00 | | | 2.8 | 209.7 |
| +07 | | | 3.6 | 208.9 |
| +10 | | | 4.4 | 208.1 |
| +15 | | | 4.8 | 207.7 |
| +20 | | | 4.0 | 208.5 |
| +25 | | | 4.1 | 208.4 |
| +50 | | | 5.0 | 207.5 |

| | + | H.I. 212.48 | − | |
|---|---|---|---|---|
| 10+75 | | | 6.1 | 206.4 |
| +83 | | | 7.4 | 205.1 |
| +95 | | | 7.9 | 204.6 |
| 11+00 | | | 6.9 | 205.6 |
| +25 | | | 7.6 | 204.9 |
| +35 | | | 8.8 | 203.7 |
| +38 | | | 10.0 | 202.5 |
| +40 | | | 10.6 | 201.9 |
| +46 | | | 9.4 | 203.1 |
| +50 | | | 9.1 | 203.4 |
| +56 | | | 7.8 | 204.7 |
| +75 | | | 7.4 | 205.1 |
| 12+00 | | | 8.9 | 203.6 |
| +25 | | | 11.4 | 201.1 |
| T.P.#7 Hub at 12+40.00 | 0.82 | 201.02 | 12.28 | 200.20 |
| 12+48 | | | 2.9 | 198.1 |
| +50 | | | 4.5 | 196.5 |
| +55 | | | 4.6 | 196.4 |
| +56 | | | 2.9 | 198.1 |
| +67 | | | 3.6 | 197.4 |
| +68 | | | 5.3 | 195.7 |
| +75 | | | 5.4 | 195.6 |
| +77 | | | 4.1 | 196.9 |
| 13+00 | | | 3.0 | 198.0 |

| | + | H.I. 201.02 | − | |
|---|---|---|---|---|
| 13+25 | | | 5.1 | 195.9 |
| +48 | | | 7.5 | 193.5 |
| +50 | | | 9.2 | 191.8 |
| +55 | | | 9.6 | 191.4 |
| +56 | | | 7.8 | 193.2 |
| +75 | | | 8.0 | 193.0 |
| 14+00 | | | 9.3 | 191.7 |
| +25 | | | 10.9 | 190.1 |
| +32 | | | 11.5 | 189.5 |
| +33 | | | 12.7 | 188.3 |
| +39 | | | 12.7 | 188.3 |
| +40 | | | 11.5 | 189.5 |
| +50 | | | 10.6 | 190.4 |
| +75 | | | 11.1 | 189.9 |
| 15+00 | | | 12.3 | 188.7 |
| T.P.#8 Lath on E at 15+15 | 2.78 | 190.95 | 12.85 | 188.17 |
| 15+25 | | | 4.0 | 187.0 |
| +45 | | | 7.0 | 184.0 |
| +47 | | | 8.1 | 182.9 |
| +49 | | | 8.0 | 183.0 |
| +50 | | | 7.0 | 184.0 |
| +75 | | | 7.4 | 183.6 |
| +95 | | | 9.0 | 182.0 |
| +97 | | | 10.1 | 180.9 |

| | + | H.I. 190.95 | − | |
|---|---|---|---|---|
| 16+00 | | | 9.3 | 181.7 |
| +07 | | | 6.6 | 184.4 |
| +25 | | | 7.3 | 183.7 |
| +50 | | | 10.0 | 181.0 |
| +67 | | | 12.6 | 178.4 |
| T.P.#9 {Lath on ℄ at 16+65 | 2.54 | 181.22 | 12.27 | 178.68 |
| 16+68 | | | 4.2 | 177.0 |
| +73 | | | 4.5 | 176.7 |
| +75 | | | 3.5 | 177.7 |
| +82 | | | 3.0 | 178.2 |
| +98 | | | 4.8 | 176.4 |
| 17+00 | | | 5.9 | 175.3 |
| +01 | | | 6.4 | 174.8 |
| +06 | | | 6.4 | 174.8 |
| +10 | | | 5.0 | 176.2 |
| +20 | | | 4.5 | 176.7 |
| +25 | | | 5.0 | 176.2 |
| +29.51 | Hub | | 5.17 | 176.0 |
| +40 | | | 7.2 | 174.0 |
| +43 | | | 8.4 | 172.8 |
| +46 | | | 8.6 | 172.6 |
| +47 | | | 7.1 | 174.1 |
| +50 | | | 6.8 | 174.4 |
| +59 | | | 5.2 | 176.0 |

| | + | H.I. 181.22 | − | |
|---|---|---|---|---|
| 17+75 | | | 6.4 | 174.8 |
| 18+00 | | | 10.0 | 171.2 |
| +04 | | | 10.3 | 170.9 |
| +10 | | | 11.6 | 169.6 |
| +22 | | | 12.3 | 168.9 |
| +25 | | | 11.3 | 169.9 |
| +29 | | | 11.5 | 169.7 |
| +30 | | | 13.2 | 168.0 |
| +50 | | | 13.6 | 167.6 |
| +60 | | | 14.1 | 167.1 |
| +61 | | | 12.6 | 168.6 |
| +75 | | | 11.3 | 169.9 |
| 19+00 | | | 12.0 | 169.2 |
| +25 | | | 13.8 | 167.4 |
| T.P.#10 {Lath 6' No. of 19+10 | 0.18 | 168.52 | 12.88 | 168.34 |
| 19+37 | | | 1.7 | 166.8 |
| +42 | | | 2.6 | 165.9 |
| +50 | | | 2.5 | 166.0 |
| +67 | | | 3.4 | 165.1 |
| +70 | | | 4.4 | 164.1 |
| +75 | | | 4.7 | 163.8 |
| +95 | | | 6.2 | 162.3 |
| +96 | 3' $H_2O$ Pipe | | 5.63 | 162.89 |
| 20+00 | | | 5.7 | 162.8 |

| | | + | H.I. | − | | |
|---|---|---|---|---|---|---|
| | | | 168.52 | | | |
| 20+17 | | | | 6.5 | 162.0 | |
| +25 | | | | 7.3 | 161.2 | |
| +36 | | | | 7.6 | 160.9 | |
| +40 | | | | 8.0 | 160.5 | |
| +45 | | | | 8.6 | 159.9 | |
| +50 | | | | 8.3 | 160.2 | |
| +51 | | | | 7.1 | 161.4 | |
| TP#11 | +62.00 | Hub (End of Line) | | 7.99 | 160.53 ✓ | Approximately opposite 17+50 on "A" Line. Book# 1355 |
| TP#12 | Lath 65' N. of 20+00 | 3.00 | 167.28 ✓ | 4.24 | 164.28 ✓ | |
| | Flow Line of M.H. 181.70' N. of 20+62 | | | 9.45 | 157.83 ✓ | |
| TP#11 | | 1.67 | 162.20 ✓ | 6.75 | 160.53 ✓ | |
| | Flow Line of M.H. 190.02' So. of 20+62 | | | 10.80 | 157.40 ✓ | |
| TP#13 | Rock in road | 2.49 | 163.97 ✓ | 0.72 | 161.48 ✓ | |
| TP#14 | " | 0.23 | 155.41 ✓ | 8.79 | 155.18 ✓ | |
| TP#15 | Rock | 2.89 | 150.05 ✓ | 8.25 | 147.16 ✓ | |
| TP#16 | Rock in Bridal Path | 6.82 | 146.72 ✓ | 10.15 | 139.90 ✓ | |
| TP#17 | Lath 10' E. of 16+12 | 9.62 | 148.68 ✓ | 7.66 | 139.06 ✓ | Laurel St. Extension 16+12 |
| B.M. 15+56 Hub | | | | 0.33 | 148.35 ✓ | 148.51 (.16) P.C. on Laurel St. Extension. Book# 1397 Page 79 (Walker) |
| B.M. 39+50 Hub | | | | 16.70 | 131.98 ✓ | 131.92 (.06) & Hub on "A" Line. Book# 1355 Page 64 (Sisson) |

Note:- Total distance between M.H.'s = 190.02 + 181.72 = 371.72'

Difference in Elev. of Flow Lines = 157.83 − 151.40 ✓ = 6.43'

Rate of Grade = 0.0173' per foot

Elev. of flow line at 20+62 = 151.40 + (190.02 × 0.0173) = 151.40 + 3.29 = 154.69

See 820/17

3-30-32

Drebert
Kanagy
Bell
Keyser

# Cross Section of Section F (1200' to 2150' So. of 0+00 & Texas St. Base Line to 400' East.)

| | + | H.I. | − | |
|---|---|---|---|---|
| B.M. Hub | | | | 1441/21 |
| B.L. 11+15 | 6.00 | 280.15 ✓ | | 274.15 |
| B.L. + 25 | | | | |
| 12+25 | | | 8.8 | 271.4 |
| +50 | | | 7.5 | 272.7 |
| +75 | | | 6.6 | 273.6 |
| 13+00 | | | 6.1 | 274.1 |
| +25 | | | 6.0 | 274.2 |
| +50 | | | 6.5 | 273.7 |
| +75 | | | 7.0 | 273.2 |
| 14+00 | | | 7.4 | 272.8 |
| +25 | | | 7.8 | 272.4 |
| +50 | | | 8.0 | 272.2 |
| +75 | | | 7.9 | 272.3 |
| 15+00 | | | 8.0 | 272.2 |
| +25 | | | 8.2 | 272.0 |
| +50 | | | 8.2 | 272.0 |
| +75 | | | 8.3 | 271.9 |
| 16+00 | | | 8.3 | 271.9 |
| +25 | | | 8.8 | 271.4 |
| +50 | | | 9.4 | 270.8 |
| +75 | | | 9.7 | 270.5 |
| 17+00 | | | 10.0 | 270.2 |



| | + | H.I. | − | |
|---|---|---|---|---|
| | | 280.15 | | |
| B.L. + 25 | | | | |
| 17+25 | | | 10.2 | 270.0 |
| +50 | | | 10.6 | 269.6 |
| +75 | | | 10.2 | 270.0 |
| 18+00 | | | 9.5 | 270.7 |
| +25 | | | 8.9 | 271.3 |
| +50 | | | 9.1 | 271.1 |
| +75 | | | 9.6 | 270.6 |
| 19+00 | | | 10.2 | 270.0 |
| +25 | | | 11.2 | 269.0 |
| +50 | | | 11.9 | 268.3 |
| +75 | | | 12.5 | 267.7 |
| 20+00 | | | 12.9 | 267.3 |
| +25 | | | 13.8 | 266.4 |
| +50 | | | 14.7 | 265.5 |
| +75 | | | 15.2 | 265.0 |
| 21+00 | | | 16.0 | 264.2 |
| +25 | | | 17.1 | 263.1 |
| +50 | | | 17.4 | 262.8 |
| B.L.+45, 21+50 | | | 19.7 | 260.5 |
| A, 21+50 | | | 23.2 | 257.0 |
| A+03, 21+50 | | | 24.8 | 255.4 |
| A+08, 21+50 | | | 20.7 | 259.5 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| B.L. 45, 21+25 | | | 19.7 | 260.5 |
| A, 21+25 | | | 20.6 | 259.6 |
| A+05, 21+25 | | | 19.0 | 261.2 |
| A, 21+00 | | | 17.0 | 263.2 |
| 20+75 | | | 15.8 | 264.4 |
| +50 | | | 14.6 | 265.6 |
| +25 | | | 13.7 | 266.5 |
| +00 | | | 12.8 | 267.4 |
| 19+75 | | | 11.6 | 268.6 |
| +50 | | | 11.0 | 269.2 |
| +25 | | | 10.2 | 270.0 |
| +00 | | | 9.6 | 270.6 |
| 18+75 | | | 9.1 | 271.1 |
| +50 | | | 8.4 | 271.8 |
| +25 | | | 8.1 | 272.1 |
| +00 | | | 8.5 | 271.7 |
| 17+75 | | | 8.8 | 271.4 |
| +50 | | | 8.9 | 271.3 |
| +25 | | | 8.8 | 271.4 |
| +00 | | | 8.5 | 271.7 |
| 16+75 | | | 8.6 | 271.6 |
| +50 | | | 8.3 | 271.9 |
| +25 | | | 8.0 | 272.2 |
| +00 | | | 7.7 | 272.5 |



| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| A | | | | |
| 15+75 | | | 7.6 | 272.6 |
| +50 | | | 7.5 | 272.7 |
| +25 | | | 7.5 | 272.7 |
| +00 | | | 7.4 | 272.8 |
| 14+75 | | | 7.4 | 272.8 |
| +50 | | | 7.0 | 273.2 |
| +25 | | | 6.6 | 273.6 |
| +00 | | | 6.2 | 274.0 |
| 13+75 | | | 5.9 | 274.3 |
| +50 | | | 6.0 | 274.2 |
| +25 | | | 6.0 | 274.2 |
| +00 | | | 6.5 | 273.7 |
| 12+75 | | | 7.5 | 272.7 |
| +50 | | | 8.9 | 271.3 |
| +25 | | | 10.0 | 270.2 |
| A+25 | | | | |
| 12+25 | | | 11.2 | 269.0 |
| +50 | | | 10.5 | 269.7 |
| +75 | | | 9.3 | 270.9 |
| 13+00 | | | 8.5 | 271.7 |
| +25 | | | 7.5 | 272.7 |
| +50 | | | 6.8 | 273.4 |
| +75 | | | 6.2 | 274.0 |

| | | | | | | |
|---|---|---|---|---|---|---|
| | | | 280.15 | | | |
| A+25 | | | | | | |
| 14+00 | | | 5.5 | 274.7 | | |
| +25 | | | 6.0 | 274.2 | | |
| +50 | | | 6.2 | 274.0 | | |
| +75 | | | 6.3 | 273.9 | | |
| 15+00 | | | 6.4 | 273.8 | | |
| +25 | | | 6.6 | 273.6 | | |
| +50 | | | 6.6 | 273.6 | | |
| +75 | | | 6.6 | 273.6 | | |
| 16+00 | | | 6.6 | 273.6 | | |
| +25 | | | 6.6 | 273.6 | | |
| +50 | | | 6.9 | 273.3 | | |
| +75 | | | 7.3 | 272.9 | | |
| 17+00 | | | 6.9 | 273.3 | | |
| +25 | | | 7.1 | 273.1 | | |
| +50 | | | 7.0 | 273.2 | | |
| +75 | | | 7.4 | 272.8 | | |
| 18+00 | | | 7.3 | 272.9 | | |
| +25 | | | 7.0 | 273.2 | | |
| +50 | | | 7.2 | 273.0 | | |
| +75 | | | 7.9 | 272.3 | | |
| 19+00 | | | 8.2 | 272.0 | | |
| +25 | | | 8.9 | 271.3 | | |
| +50 | | | 9.5 | 270.7 | | |

| | | | | | | |
|---|---|---|---|---|---|---|
| | | + | H.I. | − | | |
| | | | 280.15 | | | |
| A+25 | | | | | | |
| 19+75 | | | | 10.5 | 269.7 | |
| 20+00 | | | | 11.5 | 268.7 | |
| +25 | | | | 12.5 | 267.7 | |
| +50 | | | | 13.5 | 266.7 | |
| +75 | | | | 14.7 | 265.5 | |
| 21+00 | | | | 15.6 | 264.6 | |
| +25 | | | | 16.9 | 263.3 | |
| +50 | | | | 18.6 | 261.6 | |
| B | | | | | | |
| 21+50 | | | | 16.1 | 264.1 | |
| +25 | | | | 15.1 | 265.1 | |
| +00 | | | | 13.8 | 266.4 | |
| 20+75 | | | | 12.7 | 267.5 | |
| +50 | | | | 11.8 | 268.4 | |
| +25 | | | | 10.8 | 269.4 | |
| +00 | | | | 9.8 | 270.4 | |
| 19+75 | | | | 8.9 | 271.3 | |
| +50 | | | | 7.7 | 272.5 | |
| +25 | | | | 6.9 | 273.3 | |
| +00 | | | | 6.3 | 273.9 | |
| 18+75 | | | | 6.0 | 274.2 | |
| +50 | | | | 5.3 | 274.9 | |
| +25 | | | | 4.9 | 275.3 | |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| B | | | | |
| 18+00 | | | 5.4 | 274.8 |
| 17+75 | | | 5.4 | 274.8 |
| +50 | | | 4.8 | 275.4 |
| +25 | | | 4.3 | 275.9 |
| +00 | | | 4.4 | 275.8 |
| 16+75 | | | 4.5 | 275.7 |
| +50 | | | 4.4 | 275.8 |
| +25 | | | 4.4 | 275.8 |
| +00 | | | 4.4 | 275.8 |
| 15+75 | | | 4.4 | 275.8 |
| +50 | | | 4.9 | 275.3 |
| +25 | | | 5.0 | 275.2 |
| +00 | | | 5.2 | 275.0 |
| 14+75 | | | 5.4 | 274.8 |
| +50 | | | 5.6 | 274.6 |
| +25 | | | 5.9 | 274.3 |
| +00 | | | 6.3 | 273.9 |
| 13+75 | | | 7.0 | 273.2 |
| +50 | | | 8.0 | 272.0 |
| +25 | | | 9.2 | 271.0 |
| +00 | | | 9.9 | 270.3 |
| 12+75 | | | 10.6 | 269.6 |
| +50 | | | 11.5 | 268.7 |
| +25 | | | 12.0 | 268.2 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| B+25 | | | | |
| 12+25 | | | 12.4 | 267.8 |
| +50 | | | 12.1 | 268.1 |
| +75 | | | 11.6 | 268.6 |
| 13+00 | | | 11.0 | 269.2 |
| +25 | | | 10.3 | 269.9 |
| +50 | | | 9.1 | 271.1 |
| +75 | | | 7.7 | 272.5 |
| 14+00 | | | 7.0 | 273.2 |
| +25 | | | 6.3 | 273.9 |
| +50 | | | 5.6 | 274.6 |
| +75 | | | 5.1 | 275.1 |
| 15+00 | | | 4.8 | 275.4 |
| +25 | | | 4.5 | 275.7 |
| +50 | | | 4.2 | 276.0 |
| +75 | | | 4.2 | 276.0 |
| 16+00 | | | 3.9 | 276.3 |
| +25 | | | 3.5 | 276.7 |
| +50 | | | 3.3 | 276.9 |
| +75 | | | 3.1 | 277.1 |
| 17+00 | | | 3.1 | 277.1 |
| +25 | | | 3.4 | 276.8 |
| +50 | | | 3.6 | 276.6 |
| +75 | | | 3.9 | 276.3 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| B+25 | | | | |
| 18+00 | | | 4.2 | 276.0 |
| +25 | | | 4.4 | 275.8 |
| +50 | | | 4.7 | 275.5 |
| +75 | | | 5.3 | 274.9 |
| 19+00 | | | 5.7 | 274.5 |
| +25 | | | 6.3 | 273.9 |
| +50 | | | 7.0 | 273.2 |
| +75 | | | 7.7 | 272.5 |
| 20+00 | | | 8.6 | 271.6 |
| +25 | | | 9.5 | 270.7 |
| +50 | | | 10.5 | 269.7 |
| +75 | | | 11.3 | 268.9 |
| 21+00 | | | 12.2 | 268.0 |
| +25 | | | 13.4 | 266.8 |
| +50 | | | 14.3 | 265.9 |
| C | | | | |
| 21+50 | | | 13.4 | 266.8 |
| +25 | | | 12.0 | 268.2 |
| +00 | | | 10.9 | 269.3 |
| 20+75 | | | 9.9 | 270.3 |
| +50 | | | 9.2 | 271.0 |
| +25 | | | 8.3 | 271.9 |
| +00 | | | 7.3 | 272.9 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| C | | | | |
| 19+75 | | | 6.7 | 273.5 |
| +50 | | | 6.2 | 274.0 |
| +25 | | | 5.7 | 274.5 |
| +00 | | | 5.3 | 274.9 |
| 18+75 | | | 4.8 | 275.4 |
| +50 | | | 4.6 | 275.6 |
| +25 | | | 4.4 | 275.8 |
| +00 | | | 4.2 | 276.0 |
| 17+75 | | | 3.9 | 276.3 |
| +50 | | | 4.0 | 276.2 |
| +25 | | | 3.8 | 276.4 |
| +00 | | | 3.6 | 276.6 |
| 16+75 | | | 3.6 | 276.6 |
| +50 | | | 3.6 | 276.6 |
| +25 | | | 3.7 | 276.5 |
| +00 | | | 4.1 | 276.1 |
| 15+75 | | | 4.4 | 275.8 |
| +50 | | | 4.8 | 275.4 |
| +25 | | | 5.0 | 275.2 |
| +00 | | | 5.2 | 275.0 |
| 14+75 | | | 5.6 | 274.6 |
| +50 | | | 6.2 | 274.0 |
| +25 | | | 7.0 | 273.2 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| C | | | | |
| 14+00 | | | 8.1 | 272.1 |
| 13+75 | | | 9.2 | 271.0 |
| +50 | | | 10.1 | 270.1 |
| +25 | | | 11.1 | 269.1 |
| +00 | | | 11.7 | 268.5 |
| 12+75 | | | 12.2 | 268.0 |
| +50 | | | 12.4 | 267.8 |
| +25 | | | 12.8 | 267.4 |
| C+25 | | | | |
| 12+25 | | | 13.2 | 267.0 |
| +50 | | | 12.9 | 267.3 |
| +75 | | | 12.2 | 268.0 |
| 13+00 | | | 12.1 | 268.1 |
| +25 | | | 11.5 | 268.7 |
| +50 | | | 10.9 | 269.3 |
| +75 | | | 9.8 | 270.4 |
| 14+00 | | | 8.5 | 271.7 |
| +25 | | | 7.4 | 272.8 |
| +50 | | | 6.8 | 273.4 |
| +75 | | | 6.3 | 273.9 |
| 15+00 | | | 6.0 | 274.2 |
| +25 | | | 5.7 | 274.5 |
| +50 | | | 5.5 | 274.7 |



| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| C+25 | | | | |
| 15+75 | | | 4.8 | 275.4 |
| 16+00 | | | 4.4 | 275.8 |
| +25 | | | 4.3 | 275.9 |
| +50 | | | 3.9 | 276.3 |
| +75 | | | 4.1 | 276.1 |
| 17+00 | | | 4.3 | 275.9 |
| +25 | | | 4.8 | 275.4 |
| +50 | | | 5.0 | 275.2 |
| +75 | | | 5.3 | 274.9 |
| 18+00 | | | 5.4 | 274.8 |
| +25 | | | 5.7 | 274.5 |
| +50 | | | 5.4 | 274.8 |
| +75 | | | 5.5 | 274.7 |
| 19+00 | | | 5.8 | 274.4 |
| +25 | | | 6.3 | 273.9 |
| +50 | | | 6.5 | 273.7 |
| +75 | | | 7.2 | 273.0 |
| 20+00 | | | 7.5 | 272.7 |
| +25 | | | 7.9 | 272.3 |
| +50 | | | 8.8 | 271.4 |
| +75 | | | 10.2 | 270.0 |
| 21+00 | | | 11.2 | 269.0 |
| +25 | | | 12.1 | 268.1 |
| +50 | | | 13.4 | 266.8 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| II | | | | |
| 21+50 | | | 15.5 | 264.7 |
| +25 | | | 14.3 | 265.9 |
| +00 | | | 13.2 | 267.0 |
| 20+75 | | | 12.2 | 268.0 |
| +50 | | | 11.5 | 268.7 |
| +25 | | | 10.3 | 269.9 |
| +00 | | | 9.6 | 270.6 |
| 19+75 | | | 9.0 | 271.2 |
| +50 | | | 8.3 | 271.9 |
| +25 | | | 7.8 | 272.4 |
| +00 | | | 7.5 | 272.7 |
| 18+75 | | | 7.3 | 272.9 |
| +50 | | | 6.9 | 273.3 |
| +25 | | | 6.6 | 273.6 |
| +00 | | | 6.5 | 273.7 |
| 17+75 | | | 6.0 | 274.2 |
| +50 | | | 5.7 | 274.5 |
| +25 | | | 5.4 | 274.8 |
| +00 | | | 5.0 | 275.2 |
| 16+75 | | | 4.7 | 275.5 |
| +50 | | | 4.6 | 275.6 |
| +25 | | | 4.5 | 275.7 |
| +00 | | | 4.8 | 275.4 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| II | | | | |
| 15+75 | | | 5.4 | 274.8 |
| +50 | | | 5.6 | 274.6 |
| +25 | | | 6.0 | 274.2 |
| +00 | | | 6.7 | 273.5 |
| 14+75 | | | 6.7 | 273.5 |
| +50 | | | 7.6 | 272.6 |
| +25 | | | 8.6 | 271.6 |
| +00 | | | 9.4 | 270.8 |
| 13+75 | | | 10.4 | 269.8 |
| +50 | | | 11.1 | 269.1 |
| +25 | | | 11.6 | 268.6 |
| +00 | | | 12.1 | 268.1 |
| 12+75 | | | 12.9 | 267.3 |
| +50 | | | 14.0 | 266.2 |
| +25 | | | 15.0 | 265.2 |
| II+25 | | | | |
| 12+25 | | | 16.1 | 264.1 |
| +50 | | | 16.2 | 264.0 |
| +75 | | | 14.4 | 265.8 |
| 13+00 | | | 12.9 | 267.3 |
| +25 | | | 12.0 | 268.2 |
| +50 | | | 11.6 | 268.6 |
| +75 | | | 10.8 | 269.4 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| II +25 | | | | |
| 14+00 | | | 10.0 | 270.2 |
| +25 | | | 9.3 | 270.9 |
| +50 | | | 8.0 | 272.2 |
| +75 | | | 7.4 | 272.8 |
| 15+00 | | | 7.5 | 272.7 |
| +25 | | | 7.1 | 273.1 |
| +50 | | | 6.7 | 273.5 |
| +75 | | | 6.0 | 274.2 |
| 16+00 | | | 5.5 | 274.7 |
| +25 | | | 5.2 | 275.0 |
| +50 | | | 5.0 | 275.2 |
| +75 | | | 5.2 | 275.0 |
| 17+00 | | | 5.5 | 274.7 |
| +25 | | | 6.0 | 274.2 |
| +50 | | | 6.3 | 273.9 |
| +75 | | | 6.7 | 273.5 |
| 18+00 | | | 7.1 | 273.1 |
| +25 | | | 7.6 | 272.6 |
| +50 | | | 8.3 | 271.9 |
| +75 | | | 8.6 | 271.6 |
| 19+00 | | | 9.1 | 271.1 |
| +25 | | | 9.4 | 270.8 |
| +50 | | | 10.8 | 269.4 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| II +25 | | | | |
| 19+75 | | | 11.3 | 268.9 |
| 20+00 | | | 12.3 | 267.9 |
| +25 | | | 13.2 | 267.0 |
| +50 | | | 14.5 | 265.7 |
| +75 | | | 15.5 | 264.7 |
| E | | | | |
| 20+75 | | | 19.3 | 260.9 |
| +50 | | | 18.5 | 261.7 |
| +25 | | | 17.2 | 263.0 |
| +00 | | | 15.9 | 264.3 |
| 19+75 | | | 14.2 | 266.0 |
| +50 | | | 13.2 | 267.0 |
| +25 | | | 12.0 | 268.2 |
| +00 | | | 11.1 | 269.1 |
| 18+75 | | | 10.6 | 269.6 |
| +50 | | | 9.7 | 270.5 |
| +25 | | | 9.0 | 271.2 |
| +00 | | | 8.3 | 271.9 |
| 17+75 | | | 7.6 | 272.6 |
| +50 | | | 7.4 | 272.8 |
| +25 | | | 7.0 | 273.2 |
| +00 | | | 6.6 | 273.6 |
| 16+75 | | | 6.5 | 273.7 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| E | | | | |
| 16+50 | | | 6.3 | 273.9 |
| +25 | | | 6.4 | 273.8 |
| +00 | | | 6.3 | 273.9 |
| 15+75 | | | 6.8 | 273.4 |
| +50 | | | 7.3 | 272.9 |
| +25 | | | 7.9 | 272.3 |
| +00 | | | 8.0 | 272.2 |
| 14+75 | | | 8.2 | 272.0 |
| +50 | | | 8.5 | 271.7 |
| +25 | | | 9.0 | 271.2 |
| +00 | | | 10.0 | 270.2 |
| 13+75 | | | 10.9 | 269.3 |
| +50 | | | 12.0 | 268.2 |
| +25 | | | 13.1 | 267.1 |
| +00 | | | 15.3 | 264.9 |
| 12+75 | | | 17.6 | 262.6 |
| +50 | | | 17.7 | 262.5 |
| +25 | | | 16.6 | 263.6 |
| E+25 | | | | |
| 12+25 | | | 14.6 | 265.6 |
| +50 | | | 18.2 | 262.0 |
| +75 | | | 18.8 | 261.4 |
| 13+00 | | | 17.1 | 263.1 |

| | + | H.I. 280.15 | − | |
|---|---|---|---|---|
| E+25 | | | | |
| 13+25 | | | 13.9 | 266.3 |
| +50 | | | 12.5 | 267.7 |
| +75 | | | 11.5 | 268.7 |
| 14+00 | | | 10.2 | 270.0 |
| +25 | | | 9.4 | 270.8 |
| +50 | | | 9.4 | 270.8 |
| +75 | | | 9.0 | 271.2 |
| 15+00 | | | 9.5 | 270.7 |
| +25 | | | 9.2 | 271.0 |
| +50 | | | 8.6 | 271.6 |
| +75 | | | 8.2 | 272.0 |
| 16+00 | | | 7.8 | 272.4 |
| +25 | | | 7.3 | 272.9 |
| +50 | | | 8.3 | 271.9 |
| +75 | | | 7.8 | 272.4 |
| 17+00 | | | 8.5 | 271.7 |
| +25 | | | 8.9 | 271.3 |
| +50 | | | 9.6 | 270.6 |
| +75 | | | 10.2 | 270.0 |
| 18+00 | | | 10.5 | 269.7 |
| +25 | | | 10.9 | 269.3 |
| +50 | | | 12.2 | 268.0 |
| P. Rock F, 16+00 | | 3.38 | 274.03 | 9.50 | 270.65 ✓ |

| | + | H.I. 274.03 | − | |
|---|---|---|---|---|
| E+25 | | | | |
| 18+75 | | | 7.5 | 266.5 |
| 19+00 | | | 8.5 | 265.5 |
| +25 | | | 8.8 | 265.2 |
| +50 | | | 10.7 | 263.3 |
| +75 | | | 12.6 | 261.4 |
| 20+00 | | | 14.2 | 259.8 |
| +25 | | | 15.5 | 258.5 |
| F | | | | |
| 20+00 | | | 18.6 | 255.4 |
| 19+75 | | | 16.8 | 257.2 |
| +50 | | | 15.0 | 269.0 |
| +25 | | | 13.2 | 270.8 |
| 19+00 | | | 13.1 | 270.9 |
| 18+75 | | | 12.1 | 271.9 |
| +50 | | | 9.6 | 274.4 |
| +25 | | | 8.3 | 275.7 |
| +00 | | | 7.2 | 276.8 |
| 17+75 | | | 6.7 | 277.3 |
| +50 | | | 5.7 | 278.3 |
| +25 | | | 4.9 | 279.1 |
| +00 | | | 4.2 | 279.8 |
| 16+75 | | | 3.6 | 280.4 |
| +50 | | | 3.3 | 280.7 |

| | + | H.I. 274.03 | − | |
|---|---|---|---|---|
| F | | | | |
| 16+25 | | | 3.4 | 270.6 |
| +00 | | | 3.4 | 270.6 |
| 15+75 | | | 3.3 | 270.7 |
| +50 | | | 3.3 | 270.7 |
| +25 | | | 3.9 | 270.1 |
| +00 | | | 4.1 | 269.9 |
| 14+75 | | | 4.0 | 270.0 |
| +50 | | | 4.1 | 269.9 |
| +25 | | | 4.3 | 269.7 |
| +00 | | | 4.5 | 269.5 |
| 13+75 | | | 5.7 | 268.3 |
| +50 | | | 6.5 | 267.5 |
| +25 | | | 8.3 | 265.7 |
| +00 | | | 12.2 | 261.8 |
| 12+75 | | | 15.4 | 258.6 |
| +50 | | | 11.0 | 263.0 |
| +25 | | | 7.2 | 266.8 |
| F+25 | | | | |
| 12+25 | | | 6.2 | 267.8 |
| +50 | | | 10.1 | 263.9 |
| +75 | | | 15.0 | 259.0 |
| +82 | | | 18.2 | 255.8 |
| 13+00 | | | 13.8 | 260.2 |

274.03

| | | |
|---|---|---|
| F +25 | | |
| 13+25 | 9.7 | 264.3 |
| +50 | 7.0 | 267.0 |
| +75 | 6.1 | 267.9 |
| 14+00 | 5.1 | 268.9 |
| +25 | 5.0 | 269.0 |
| +50 | 5.2 | 268.8 |
| +75 | 5.2 | 268.8 |
| 15+00 | 5.1 | 268.9 |
| +25 | 4.6 | 269.4 |
| +50 | 4.1 | 269.9 |
| +75 | 4.1 | 269.9 |
| 16+00 | 4.7 | 269.3 |
| +25 | 4.8 | 269.2 |
| +50 | 4.9 | 269.1 |
| +75 | 5.1 | 268.9 |
| 17+00 | 5.8 | 268.2 |
| +25 | 6.6 | 267.4 |
| +50 | 7.9 | 266.1 |
| +75 | 9.0 | 265.0 |
| 18+00 | 10.4 | 263.6 |
| +25 | 11.2 | 262.8 |
| +50 | 13.0 | 261.0 |
| +75 | 15.9 | 258.1 |

274.03

| | | |
|---|---|---|
| F +25 | | |
| 19+00 | 18.3 | 255.7 |
| +25 | 18.6 | 255.4 |
| +50 | 19.9 | 254.1 |
| +75 | 21.1 | 252.9 |
| G | | |
| 19+25 | 25.5 | 248 5 |
| +00 | 26.0 | 248.0 |
| 18+75 | 22.1 | 251.9 |
| +50 | 16.8 | 257.2 |
| +25 | 14.3 | 259.7 |
| +00 | 13.0 | 261.0 |
| 17+75 | 11.2 | 262.8 |
| +50 | 10.1 | 263.9 |
| +25 | 8.5 | 265.5 |
| +00 | 7.7 | 266.3 |
| 16+75 | 6.9 | 267.1 |
| +50 | 6.2 | 267.8 |
| +25 | 5.9 | 268.1 |
| +00 | 5.7 | 268.3 |
| 15+75 | 5.0 | 269.0 |
| +50 | 5.2 | 268.8 |
| +25 | 5.4 | 268.6 |
| +00 | 5.9 | 268.1 |

| | + | H.I. 274.03 | | |
|---|---|---|---|---|
| G | | | | |
| 14+75 | | | 6.0 | 268.0 |
| +50 | | | 6.0 | 268.0 |
| +25 | | | 5.9 | 268.1 |
| +00 | | | 6.2 | 267.8 |
| 13+75 | | | 7.0 | 267.0 |
| +50 | | | 8.9 | 265.1 |
| +25 | | | 13.1 | 260.9 |
| +00 | | | 18.5 | 255.5 |
| 12+88 | | | 22.3 | 251.7 |
| +75 | | | 17.6 | 256.4 |
| +50 | | | 9.3 | 264.7 |
| 12+25 | | | 6.1 | 267.9 |
| G+25 | | | | |
| 12+25 | | | 5.7 | 268.3 |
| +50 | | | 8.2 | 265.8 |
| +75 | | | 13.1 | 260.9 |
| 15+50 | | | 5.7 | 268.3 |
| +75 | | | 5.8 | 268.2 |
| 16+00 | | | 6.0 | 268.0 |
| +25 | | | 6.8 | 267.2 |
| +50 | | | 7.7 | 266.3 |
| +75 | | | 8.4 | 265.6 |

| | + | H.I. 274.03 | − | | |
|---|---|---|---|---|---|
| G+25 | | | | | |
| 17+00 | | | 9.2 | 264.8 | |
| +25 | | | 10.6 | 263.4 | |
| +50 | | | 12.3 | 261.7 | |
| +75 | | | 14.4 | 259.6 | |
| 18+00 | | | 16.2 | 257.8 | |
| H | | | | | |
| 17+25 | | | 13.0 | 261.0 | |
| +00 | | | 10.6 | 263.4 | |
| 16+75 | | | 9.4 | 264.6 | |
| +50 | | | 9.0 | 265.0 | |
| +25 | | | 7.5 | 266.5 | |
| +00 | | | 6.8 | 267.2 | |
| 15+75 | | | 6.0 | 268.0 | |
| 12+50 | | | 6.3 | 267.7 | |
| +25 | | | 5.0 | 269.0 | |
| H+25 | | | | | |
| 12+25 | | | 5.0 | 269.0 | 1443/29 |
| F, 12+00 | | | 5.1 | 268.9 | 268.8 |

3-5-'32

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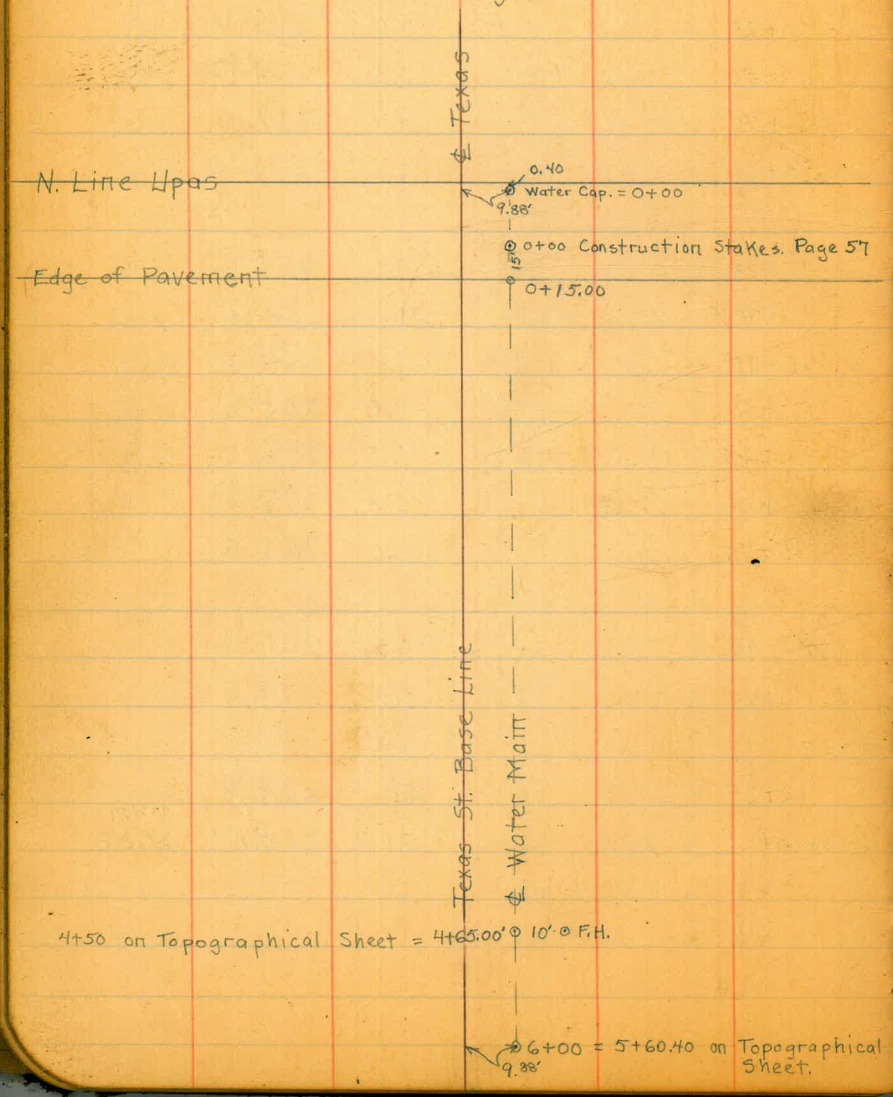
Mosien
Olmstead
De Perini

℄ Location and Profile of Water Line from N. Line of Upas, 9.88' East of ℄ of Texas St., to Field House and Swiming Pool.






## Profile of Water Line

| | + | H.I. | − | | |
|---|---|---|---|---|---|
| C.T. on N. Prop. Line of Upas & E. 7' " of Texas. | 2.85 | 283.77 | | 280.92 | |
| Top of 0+00 Water Cap on Pavement | | | 3.41 | 280.36 | |
| +20 N. Gutter of Upas | | | 3.72 | 280.05 | |
| +39.60 Header Board | | | 3.45 | 280.32 | |
| +50 | | | 3.2 | 280.6 | |
| +75 | | | 3.4 | 280.4 | |
| 1+00 | | | 4.1 | 279.7 | |
| +25 | | | 4.4 | 279.4 | |
| +50 | | | 4.8 | 279.0 | |
| +75 | | | 5.1 | 278.7 | |
| 2+00 | | | 5.5 | 278.3 | |
| +25 | | | 5.5 | 278.3 | |
| +50 | | | 5.5 | 278.3 | |
| +75 | | | 5.6 | 278.2 | |
| 3+00 | | | 5.5 | 278.3 | |
| +25 | | | 5.0 | 278.8 | |
| +50 | | | 4.6 | 279.2 | |
| +75 | | | 4.4 | 279.4 | |
| 1' offset Hub 3+40 P. Texas St. B.L. | 6.18 | 285.40 | 4.55 | 279.22 | 1441/3 279.21 |
| 4+00 | | | 5.8 | 279.6 | |
| +25 | | | 5.3 | 280.1 | |
| +50 | | | 5.4 | 280.0 | |
| +75 | | | 5.3 | 280.1 | |

| | + | H.I. | − | |
|---|---|---|---|---|
| | | 285.40 | | |
| 5+00 | | | 5.2 | 280.2 |
| +25 | | | 5.7 | 279.7 |
| +50 | | | 5.2 | 280.2 |
| +75 | | | 5.1 | 280.3 |
| 6+00 | | | 5.5 | 279.9 |
| 1' offset Hub 5+92 Texas St. B.L. | | | 7.13 | 278.27 (1443/21) 278.24 |

4-8-'32

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Olmsted
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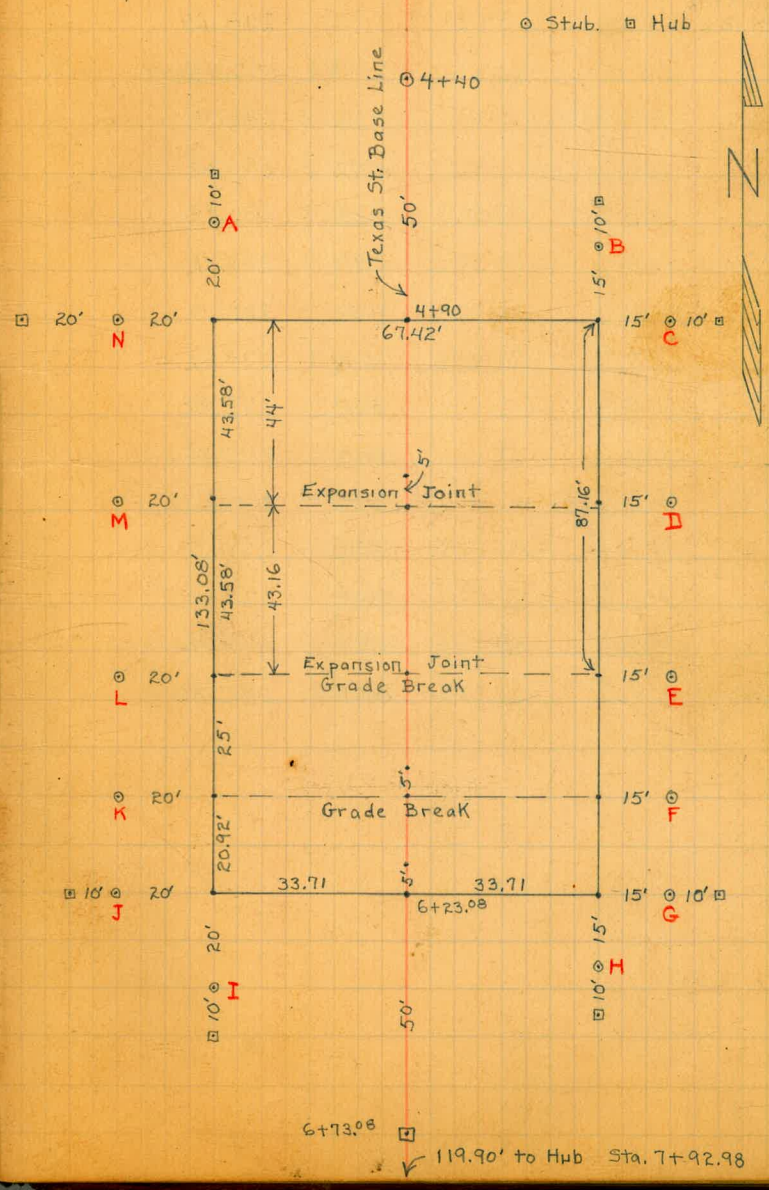
55

# Outlay of Swiming Pool - Balboa Park Recreation Area



4-8-'32

## Cuts and Fills on Swiming Pool

| Station | + | H.I. | − | Elev. |
|---|---|---|---|---|
| 1' offset Hub 5+92 Texas St. B.L. | 6.07 | 284.31 | | 278.24 |
| A | | | 6.78 | 277.53 |
| B | | | 3.96 | 280.35 |
| C | | | 3.42 | 280.89 |
| D | | | 3.38 | 280.93 |
| E | | | 3.79 | 280.52 |
| F | | | 4.21 | 280.10 |
| G | | | 4.49 | 279.82 |
| H | | | 5.43 | 278.88 |
| I | | | 8.53 | 275.78 |
| J | | | 8.84 | 275.47 |
| K | | | 8.46 | 275.85 |
| L | | | 8.82 | 275.49 |
| M | | | 7.93 | 276.38 |
| N | | | 8.01 | 276.30 |



| Sidewalk Subgrade | | Slab Subgrade | | Top of Curb 279.62 |
|---|---|---|---|---|
| 278.66 | F 1.13 | 275.62 | C 1.91 | F 2.09 |
| " | C 1.69 | " | C 4.73 | C 0.73 |
| " | C 2.23 | " | C 5.27 | C 1.27 |
| " | C 2.27 | 273.87 | C 7.06 | C 1.31 |
| " | C 1.86 | 272.12 | C 8.40 | C 0.90 |
| " | C 1.44 | 269.12 | C 10.98 | C 0.48 |
| " | C 1.16 | 270.12 | C 9.70 | C 0.20 |
| " | C 0.22 | " | C 8.76 | F 0.74 |
| " | F 2.88 | " | C 5.66 | F 3.84 |
| " | F 3.19 | " | C 5.35 | F 4.15 |
| " | F 2.81 | 269.12 | C 6.73 | F 3.77 |
| " | F 3.17 | 272.12 | C 3.37 | F 4.13 |
| " | F 2.28 | 273.87 | C 2.51 | F 3.24 |
| " | F 2.36 | 275.62 | C 0.68 | F 3.32 |

4-9-'32

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Olmsted
De Perini

# Construction Stakes on Water Line to Swiming Pool and Field House.

| Station | + | H.I. | − | Elev. 1943/1 | Flow Line Grade | Cut |
|---|---|---|---|---|---|---|
| C.T. on N. Prop. Line of Hpas and E. T'Line of Texas St. | 2.48 | 283.40 | | 280.92 | | |
| 0+00 {25' So. of N. Line of Hpas & 5'E. of Texas St. B.L. | | | 3.35 | 280.05 | 277.50 | |
| +50 | | | 3.12 | 280.28 | 277.25 | 3.0 |
| 1+00 | | | 3.99 | 279.41 | 277.00 | 2.4 |
| +50 | | | 4.91 | 278.49 | 276.75 | 1.7 |
| 2+00 | | | 5.24 | 278.16 | 276.50 | 1.7 |
| +50 | | | 5.15 | 278.25 | 276.25 | 2.0 |
| 3+00 | | | 4.76 | 278.64 | 276.00 | 2.6 |
| +50 | | | 4.05 | 279.35 | 276.17 | 3.2 |
| 4+00 | | | 3.47 | 279.93 | 276.25 | 3.7 |
| +50 | | | 3.17 | 280.23 | 276.37 | 3.9 |
| 5+00 {5' N. of N. Line of Pool | | | 3.95 | 279.45 | 276.50 | 3.0 |
| 1+41 {Special Shot on top of 4" E.X.W. Water Pipe | | | 5.16 | 278.24 | | |
| C.T. B.M. | 3.67 | 284.59 | | 280.92 | | |
| Flow Line Grade at 0+00 | | | 7.34 | 277.25 | | |

Flow Line grade checked at 277.25 4-15-'32.

4-15-'32

57

4-14-32

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Olmsted
De Perini

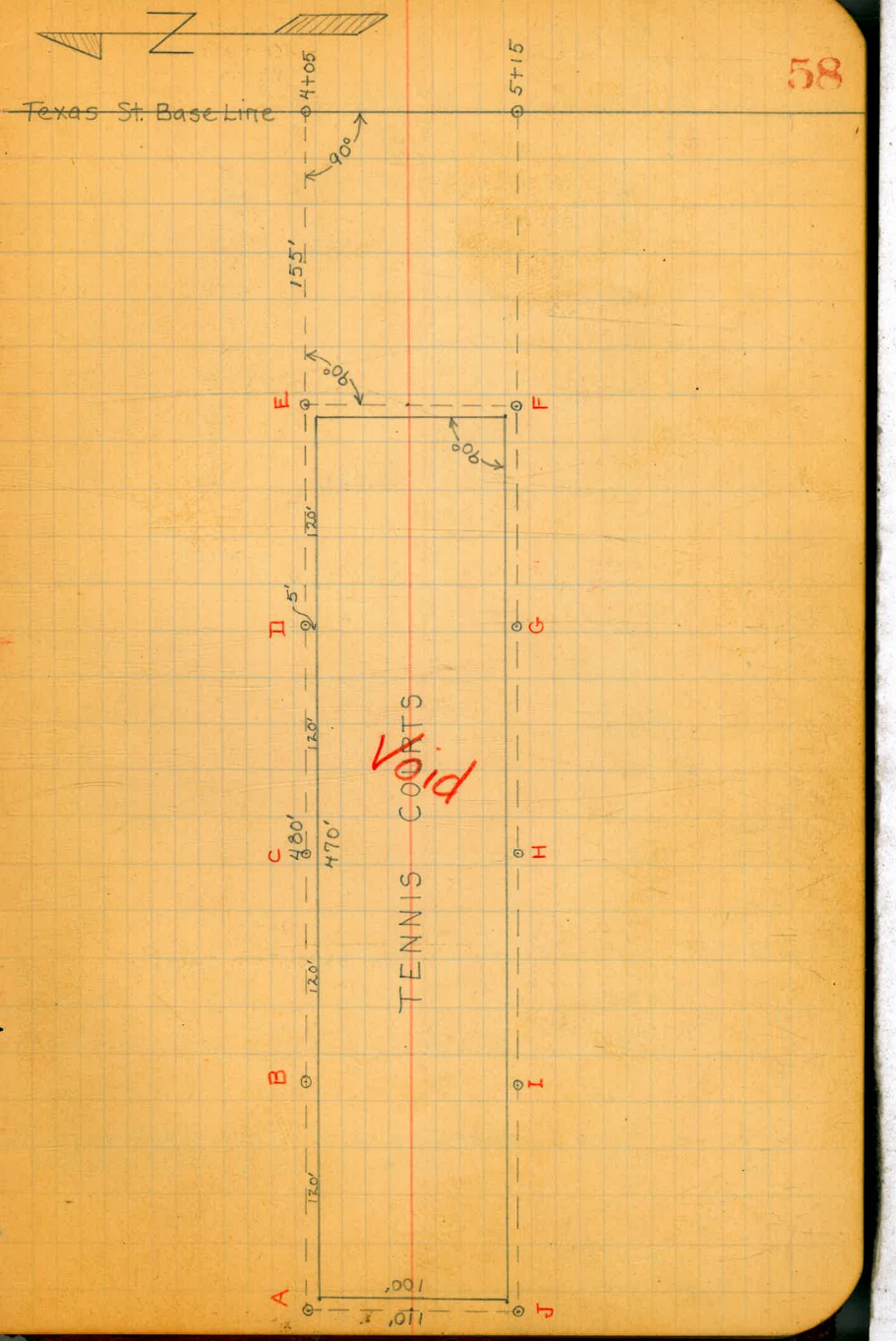
58

Grade Stakes on Tennis Courts (410' to 510' So. of 0+00 and 160' to 630' West of Texas St. B.L.)

Subgrade Elev. 271.50'

| Station | + | H.I | − | Elev. 1441/3 | |
|---|---|---|---|---|---|
| B.M. 1' offset Hub B.L. 3+40 | 0.01 | 279.22 | | 279.21 | |
| A | | | 6.74 | 272.48 | C 0.98 |
| B | | | 4.81 | 274.41 | C 2.91 |
| C | | | 6.39 | 272.83 | C 1.33 |
| D | | | 7.06 | 272.16 | C 0.66 |
| E | | | 5.52 | 273.70 | C 2.20 |
| F | | | 6.63 | 272.59 | C 1.09 |
| G | | | 8.69 | 270.53 | F 0.97 |
| H | | | 9.14 | 270.08 | F 1.42 |
| I | | | 6.69 | 272.53 | C 1.03 |
| J | | | 9.20 | 270.02 | F 1.48 |

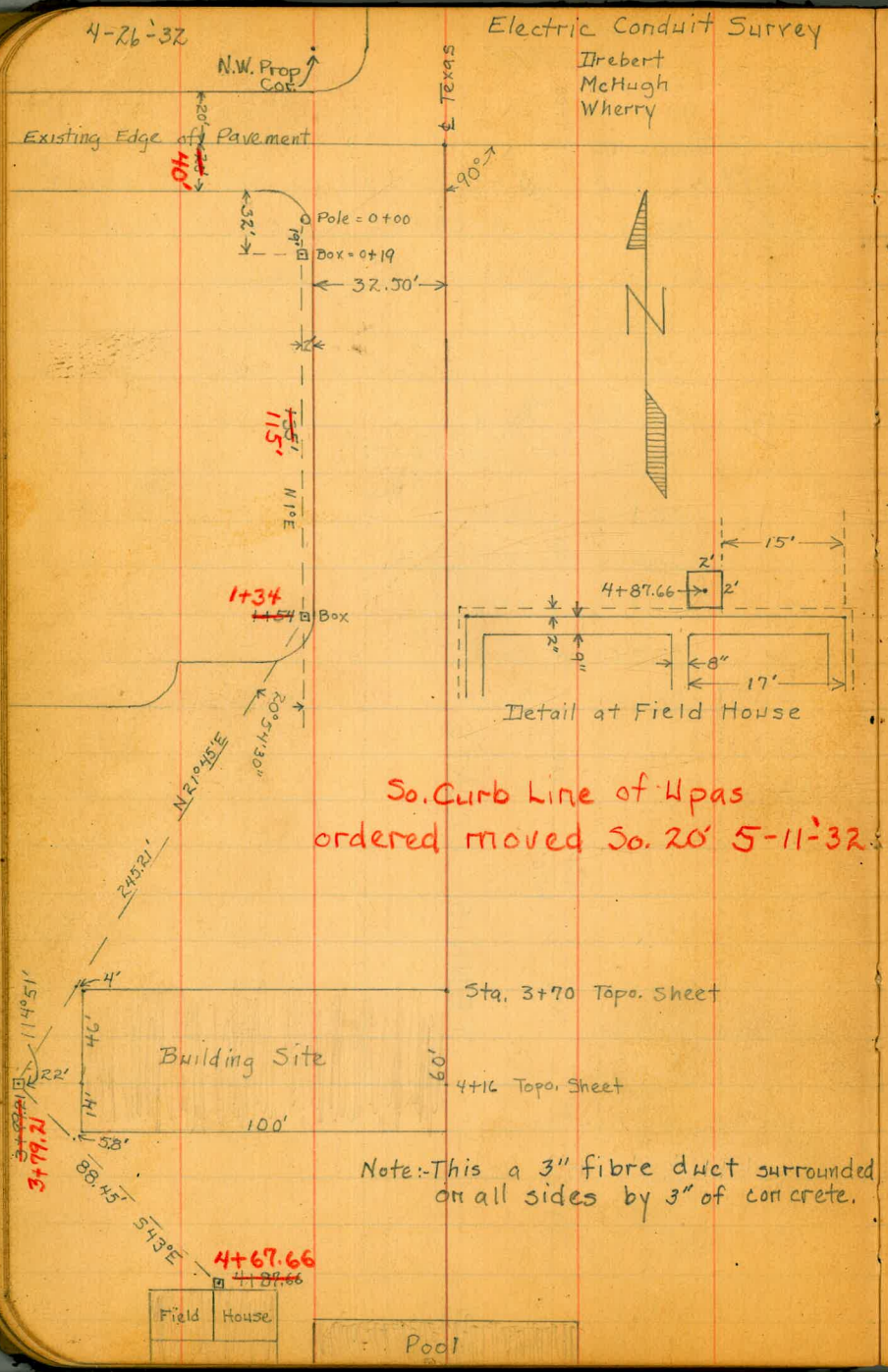
Void
See Page 61



4-26-32

# Electric Conduit Survey

Irebert
McHugh
Wherry




So. Curb Line of Upas ordered moved So. 20' 5-11-32

Note:-This a 3" fibre duct surrounded on all sides by 3" of concrete.

59

## Profile of ℄ of Conduit

| Station | + | H.I. | − | | |
|---|---|---|---|---|---|
| C.T. on N. Prop. line of Upas & E. "I" Line of Texas. | 3.48 | 284.40 | | 280.92 | |
| 0+00 | | | 4.3 | 280.1 | |
| +19 | | | 4.8 | 279.5 | |
| +50 | | | 5.2 | 279.2 | |
| 1+00 | | | 6.4 | 278.0 | |
| TP +~~54~~ 34 ℄ | 4.83 | 282.26 | 6.97 | 277.43 | Removed |
| 2+00 | | | 5.0 | 277.3 | |
| +50 | | | 5.4 | 276.9 | |
| 3+00 | | | 5.8 | 276.5 | |
| +50 | | | 6.2 | 276.1 | |
| +~~99.21~~ 79.21 ℄ | | | 7.7 | 274.6 | |
| 4+50 | | | 6.9 | 275.4 | |
| +~~87.66~~ 67.66 | | | 6.3 | 276.0 | |
| 1' offset Hub B.L. 3+40 | | | 3.05 | 279.21 | 144-1/3 279.21 |

4-27-32

| | | | | | |
|---|---|---|---|---|---|
| B.M. See Above. | 1.90 | 282.82 | | 280.92 | |
| 0+~~93.5~~ 73.5 (Conduit Sta) | | Bottom of Pipe | 6.18 | 276.64 | |

Note:- 0+93.50 on Conduit Line = 1+41.50 on Water Line

4-27-32

Irebert
McHugh
Wherry

# Construction Stakes on Electric Conduit Line

| Station | + | H.I. | − | Elev (1443/1) | Grade Flow Line | Cut | | Station | − | Elev |
|---|---|---|---|---|---|---|---|---|---|---|
| C.T. on N. Prop. Line of Upas & E. 9' Line of Texas | 1.90 | 282.82 | | 280.92 | | | | | | |
| 93 ~~72~~ So. of N. Line of Upas & 34.5' W. of Texas St. B.L. | | | 2.7 | 280.1 | | | 5' W | 0+03 | 4.6 | 278.7 |
| +19 First Pull Box. | | | 3.2 | 279.6 | 278.0 | 1.6 | " | +19 | 4.7 | 278.6 |
| +50 | | | 3.6 | 279.2 | 277.5 | 1.7 | " | +50 | 5.6 | 277.7 |
| 1+00 | | | 4.8 | 278.0 | 276.8 | 1.2 | " | 1+00 | 6.6 | 276.7 |
| +34 ~~+54~~ Second Pull Box | | | 5.5 | 277.3 | 276.0 | 1.3 | " | +34 | 6.6 | 276.7 |
| 2+00 | | | 5.6 | 277.2 | 275.6 Brk. | 1.6 | " | +50 | 7.0 | 276.3 |
| +50 | | | 6.0 | 276.8 | 275.3 | 1.5 | " | 2+00 | 7.2 | 276.1 |
| 3+00 | | | 6.4 | 276.4 | 274.9 Brk. | 1.5 | " | +50 | 7.0 | 276.3 |
| +50 | | | 6.8 | 276.0 | 274.2 | 1.8 | " | +70 | 7.5 | 275.8 |
| 79.71 ~~+99.21~~ Third Pull Box | | | 8.2 | 274.6 | 273.5 Brk. | 1.1 | " | 3+00 | 7.3 | 276.0 |
| 4+50 | | | 7.6 | 275.2 | 274.2 | 1.0 | 5' So. | +50 | 8.0 | 275.3 |
| 67.66 ~~+87.66~~ End Pull Box | | | 7.0 | 275.8 | 275.0 | 0.8 | " | +79.21 | 8.7 | 274.6 |
| 1' offset Hub | | | | 1441/3 | | | | 4+00 | 9.0 | 274.3 |
| 3+40 | | | 3.61 | 279.21 | | | | +50 | 7.5 | 275.8 |
| | | | | 279.21 | | | | +65 | 7.5 | 275.8 |

Note :- So. Line of Parking Area is Sta. 2+~~90~~ 70 ±
Grade there is 275.0'

Elevations of Top of Concrete Covering Conduit 60

H.I.
277.53 B.M.
+5.75
283.28

5-4-'32

Drebert
McHugh
Wherry

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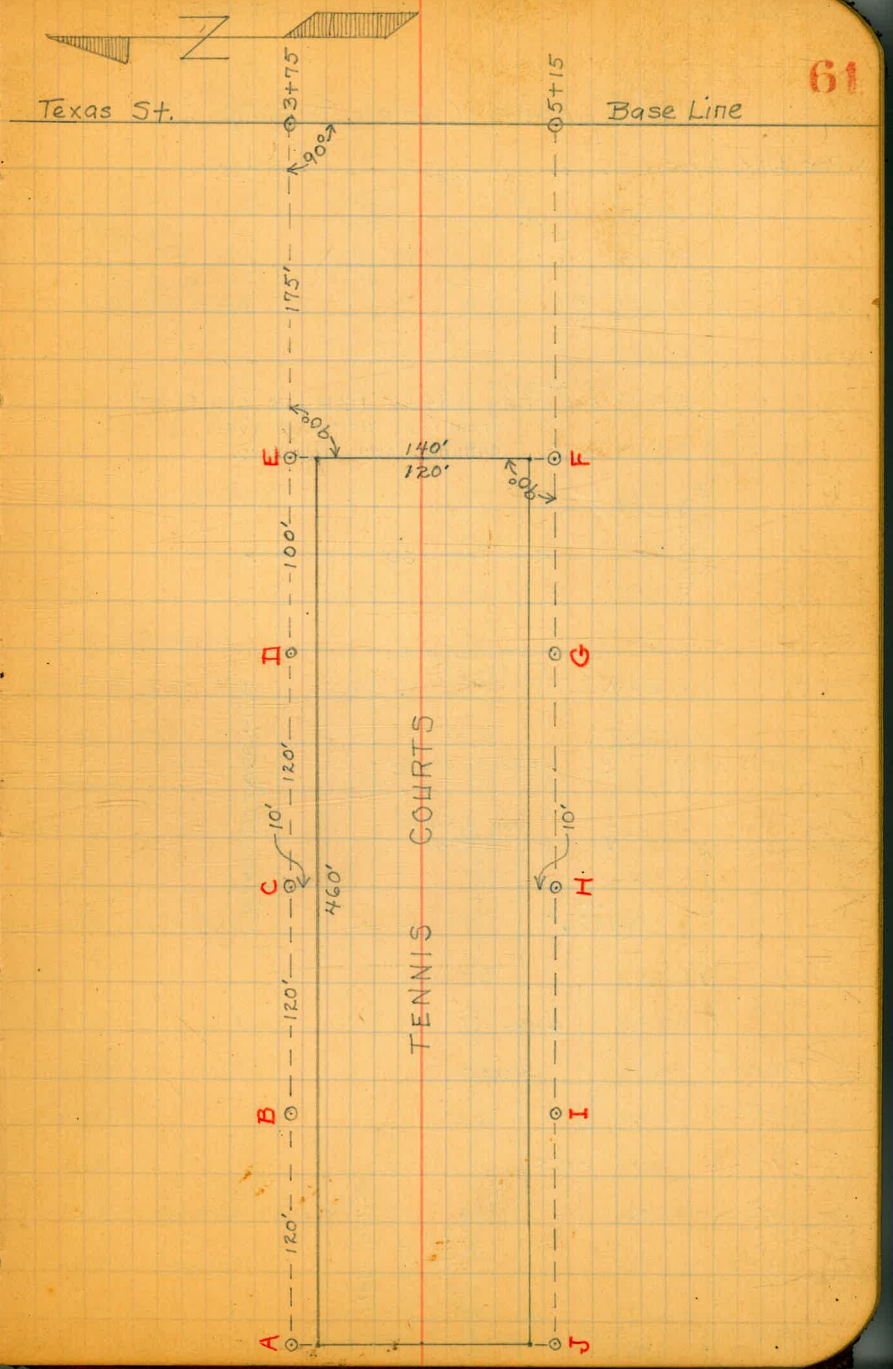
## Grade Stakes on Tennis Courts (385' to 505' So. of 0+00 and 175' to 635' West of Texas St. B.L.)

1' Fall in 120' from N. to S.

| | Station | + | H.I. | − | Elev 1443/58 | |
|---|---|---|---|---|---|---|
| | Grade Stake "H" | 6.11 | 276.19 | | 270.08 | |
| 272.50' | A | | | 3.70 | 272.49 | F 0.01 |
| | B | | | 1.35 | 274.84 | C 2.34 |
| | C | | | 2.51 | 273.68 | C 1.18 |
| | D | | | 3.78 | 272.41 | F 0.09 |
| | E | | | 2.64 | 273.55 | C 1.05 |
| 271.50' | F | | | 4.79 | 271.40 | F 0.10 |
| | G | | | 5.66 | 270.53 | F 0.97 |
| | H | | | 6.11 | 270.08 | F 1.42 |
| | I | | | 3.66 | 272.53 | C 1.03 |
| | J | | | 6.17 | 270.02 | F 1.48 |

Courts extended 8' south (128' overall instead of 120') as per instructions of Mr. Phelps Oct. 1932
1' Fall in 128' from N. to S.

Drebert



6-20-32 Direbert

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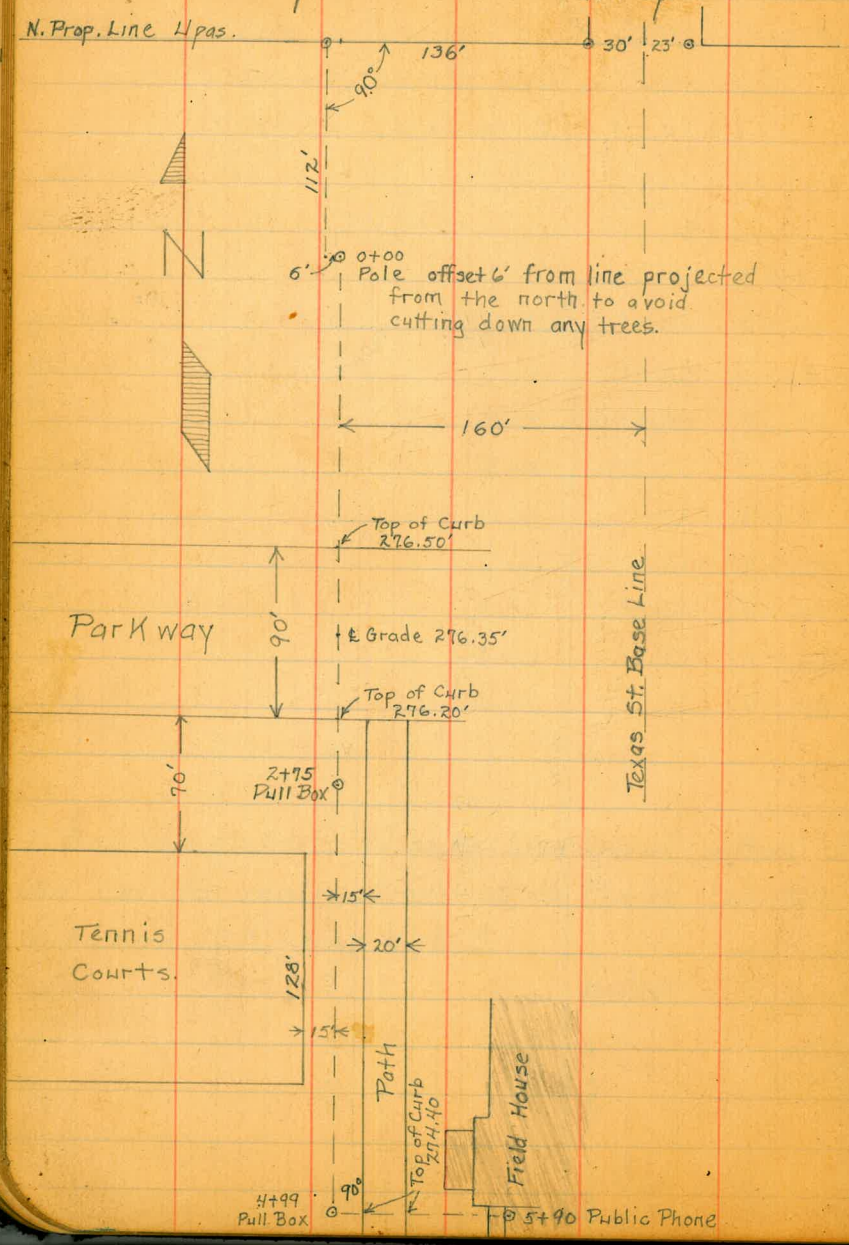
# Telephone Cable Survey




# Telephone Cable & Profile

| Station | + | H.I. | − | Elev. |
|---|---|---|---|---|
| C.T. on N. Prop. Line of Hpas & E. 7' Line of Texas | 0.53 | 281.45 | | Page 1 280.92 |
| 0+00 72' So. of Pavement Edge. | | | 4.0 | 277.4 |
| +50 | | | 5.0 | 276.4 |
| 1+00 | | | 6.1 | 275.3 |
| +50 | | | 6.9 | 274.5 |
| +53 Edge of Road | | | 5.3 | 276.1 |
| 2+00 | | | 5.4 | 276.0 |
| +50 | | | 5.7 | 275.7 |
| +75 Pull Box | | | 5.9 | 275.5 |
| PI +90 ℄ Brk. 4.94 | | 280.25 | 6.14 | 275.30 |
| 3+00 | | | 6.4 | 273.8 |
| +50 | | | 7.2 | 273.0 |
| 4+00 | | | 8.1 | 272.1 |
| +50 | | | 7.9 | 272.3 |
| +99 Pull Box | | | 7.6 | 272.6 |
| 5+11 | | | 7.5 | 272.7 |
| +14 Edge of Path | | | 5.8 | 274.4 |
| +34 " " " | | | 5.6 | 274.6 |
| +37 | | | 6.6 | 273.6 |
| +50 | | | 6.1 | 274.1 |
| +82.5 Outside Foundation | | | 3.9 | 276.3 |
| +83.5 Inside " | | | 3.2 | 277.0 |
| +90 | | | 2.2 | 278.0 |
| Pool Stake | | | 2.69 | 277.54 Page 56 277.53 |

6-22-'32 Drebert

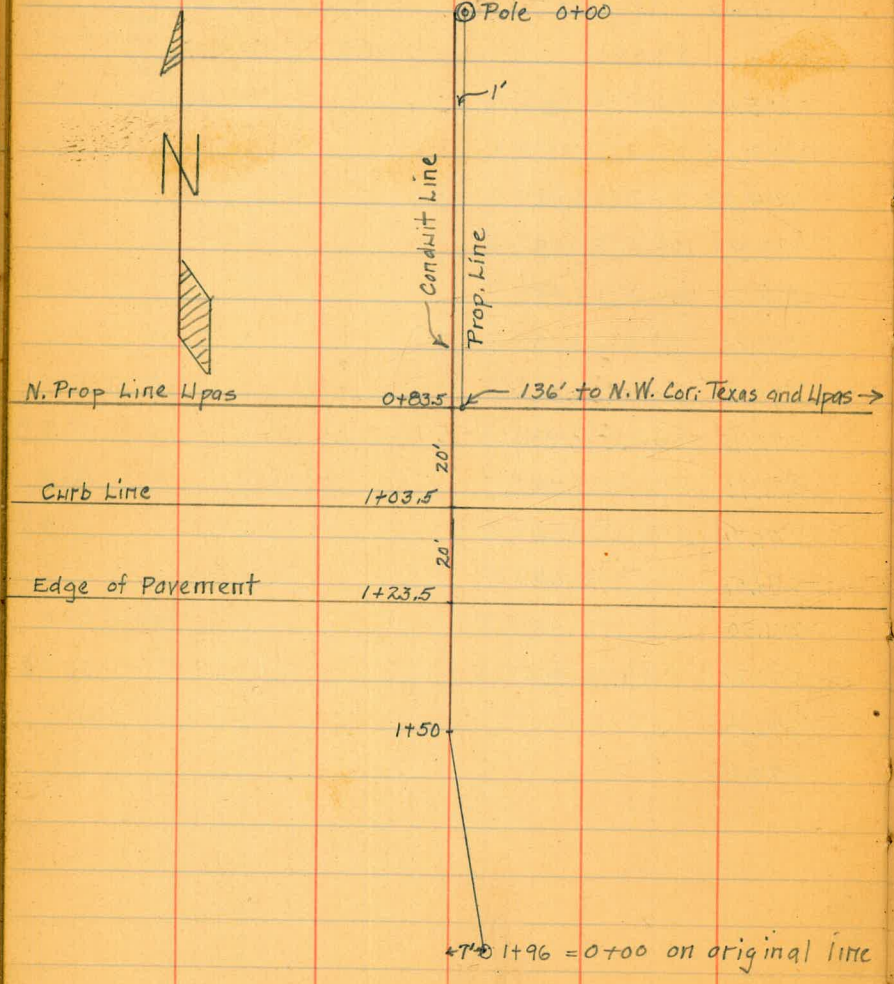


# Construction Stakes on Telephone Conduit.

| Station | + | H.I. | − | Elev. 1443/1 | Flow Line Grade | Cut. |
|---|---|---|---|---|---|---|
| C.T. N. Prop. Hpas E. 7' Line Texas | 0.10 | 281.02 | | 280.92 | | |
| 0+00 {112' So. of N. Prop. Hpas. | | | 3.36 | 277.66 | 275.90 | 1.76 |
| +50 | | | 4.48 | 276.54 | 275.23 | 1.31 |
| 1+00 | | | 5.53 | 275.49 | 274.58 | 0.91 |
| +50 | | | 6.16 | 274.86 | 273.93 | 0.93 |
| 2+00 | | | 4.89 | 276.13 | 273.28 | 2.85 |
| +50 | | | 5.09 | 275.93 | 272.63 | 3.30 |
| +75 Pull Box | | | 5.36 | 275.66 | 272.30 | 3.36 |
| 3+00 | | | 6.01 | 275.01 | 272.18 | 2.83 |
| +50 | | | 7.33 | 273.69 | 271.96 | 1.73 |
| 4+00 | | | 8.22 | 272.80 | 271.74 | 1.06 |
| +50 | | | 8.02 | 273.00 | 271.52 | 1.48 |
| +99 Pull Box | | | 8.24 | 272.78 | 271.30 | 1.48 |
| 5+50 | | | 6.77 | 274.25 | 272.30 | 1.95 |
| +82 | | | | | 272.94 | |
| +90 | | | | | 273.10 | |

7-20-37 Urebert

# Telephone Conduit Extension

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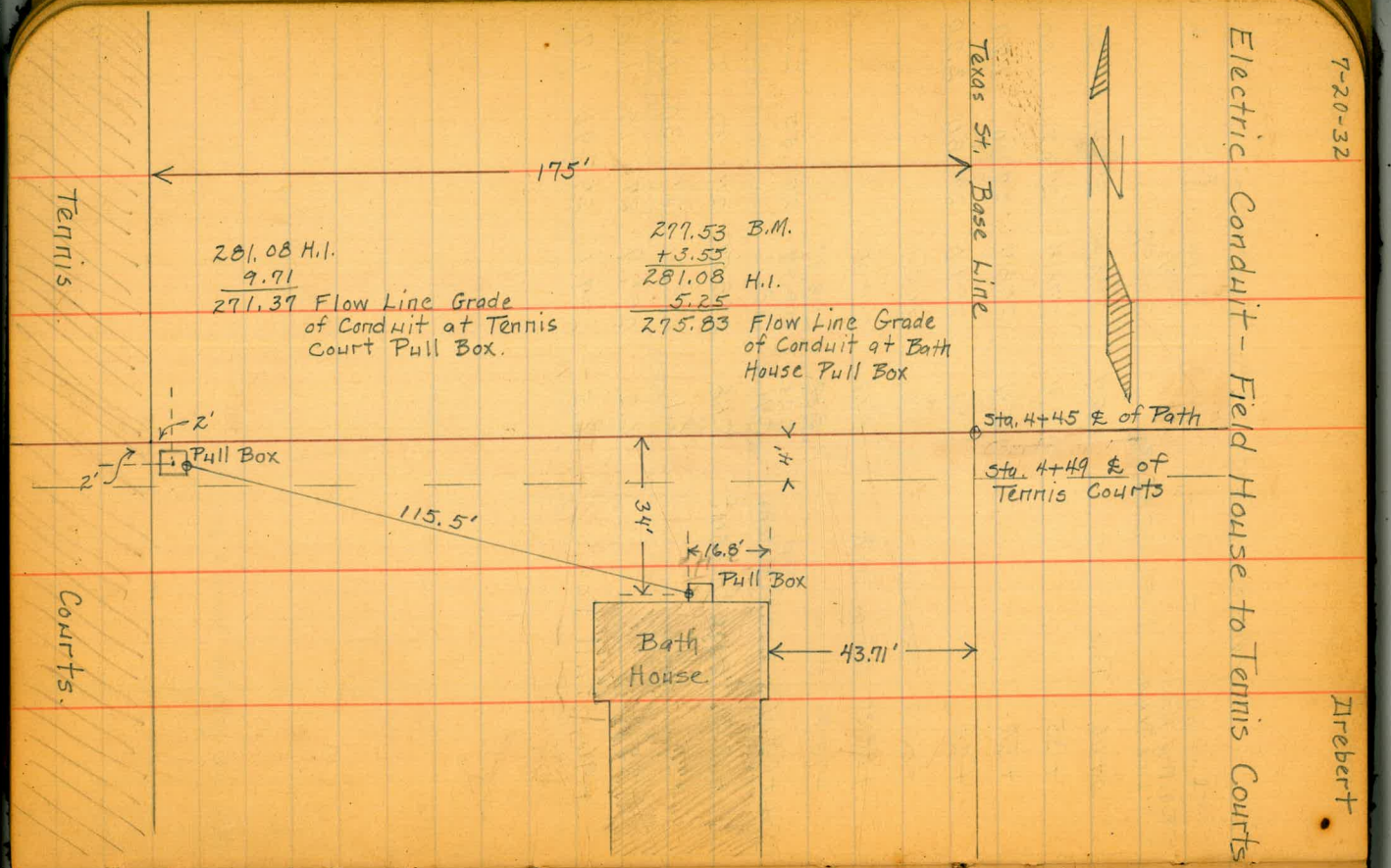
## Extension Construction Stakes

| Station | | + | H.I. | − | Elev. | Flow Line | Cut |
|---|---|---|---|---|---|---|---|
| C.T.N. Prop. Hpas E.T' Line Texas | | 3.15 | 284.07 | | 1443/1 280.92 | | |
| 0+00 | Pole | | | 5.7 | 278.4 | 277.4 | 1.00 |
| +25 | | | | 5.7 | 278.4 | 277.2 | 1.20 |
| +50 | | | | 5.4 | 278.7 | 277.0 | 1.70 |
| +75 | | | | 5.1 | 279.0 | 276.80 | 2.20 |
| +83.50 | Prop. Line | | | 5.0 | 279.1 | | |
| +88.30 | N. Edge Walk | | | 5.02 | 279.05 | | |
| +93.30 | S. " " | | | 5.08 | 278.99 | | |
| 1+03.50 | Curb | | | 5.20 Top<br>5.91 Bottom | 278.87<br>278.16 | 276.55 | 2.30 |
| +23.50 | Edge Pavement | | | 5.48 | 278.59 | 276.50 | 2.10 |
| +50 | L' | | | 6.1 | 278.0 | 276.30 | 1.70 |
| +75 | | | | 6.2 | 277.9 | 276.10 | 1.80 |
| +96 | Pull Box | | | 6.5 | 277.6 | 275.90 | 1.70 |

7-20-32

# Electric Conduit - Field House to Tennis Courts

Arebert

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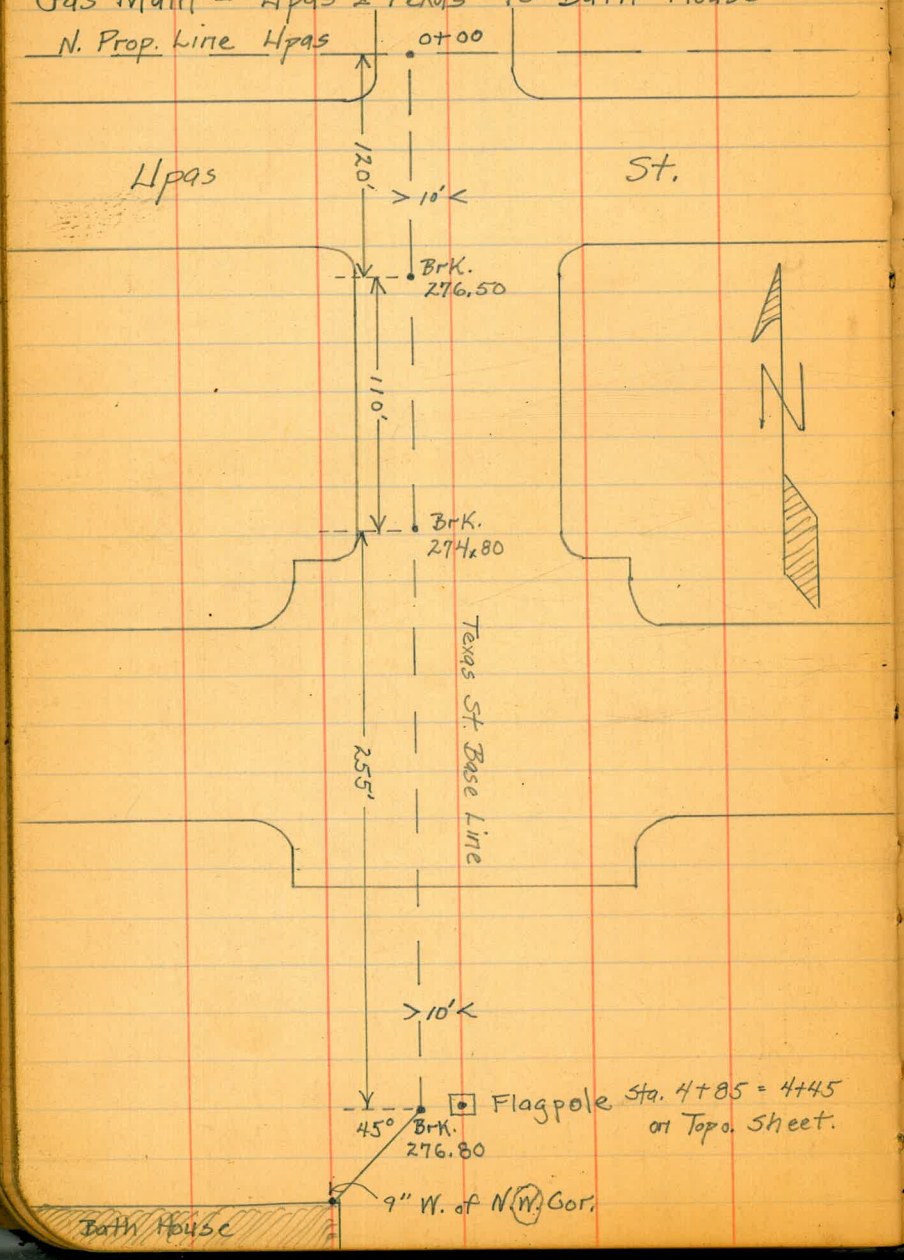
10-15-32 Hrebert



# Gas Main – Hpas & Texas to Bath House



Chalmers St. Cross Section
E.L. India to E.L. Columbia

80' wide
Qts 10.5
42' Bet Edge of Gutter

| | | | |
|---|---|---|---|
| BM 11.55 | 77.63 | 66.08 | SW BP Chalmers & India |
| E.L. India | | | |
| S Cb Top | 9.62 | 68.01 | |
| ↓ +.5 = Edge Gutter | 9.51 | 68.12 | |
| ↓ 1/4 " Paving | 9.58 | 68.05 | |
| ↓ ℄ " " | 9.65 | 67.98 | ℄ |
| ↓ 1/4 " " | 9.66 | 67.97 | |
| ↓ +10.5 = Edge Gutter | 9.58 | 68.05 | |
| N Cb Top + Paving | 9.57 | 68.06 | |
| 12' E of E.L. India | | | |
| N Cb in Drive | 8.77 | 68.86 | |
| ↓ +.5 = Edge Gutter | 8.49 | 69.14 | |
| ↓ 1/4 " | 8.3 | 69.3 | |
| ↓ ℄ " | 8.2 | 69.4 | ℄ |
| ↓ 1/4 " | 8.7 | 68.91 | |
| ↓ +10.5 Edge Gutter | 8.53 | 69.10 | |
| S Cb Gutter | 8.89 | 68.74 | |
| Top Cb | 8.08 | 69.55 | |
| 25' E of E.L. India | | | |
| S Cb Top | 6.41 | 71.22 | |
| Gutter | 7.84 | 70.39 | |
| ↓ +.5 = Edge Gutter | 6.92 | 70.71 | |
| ↓ 1/4 " | 7.2 | 70.4 | |
| ↓ ℄ " | 6.9 | 70.7 | |
| ↓ 1/4 " | 6.9 | 70.7 | |

Indexed
C.S.K.

3-1-33
Moore
Sisson

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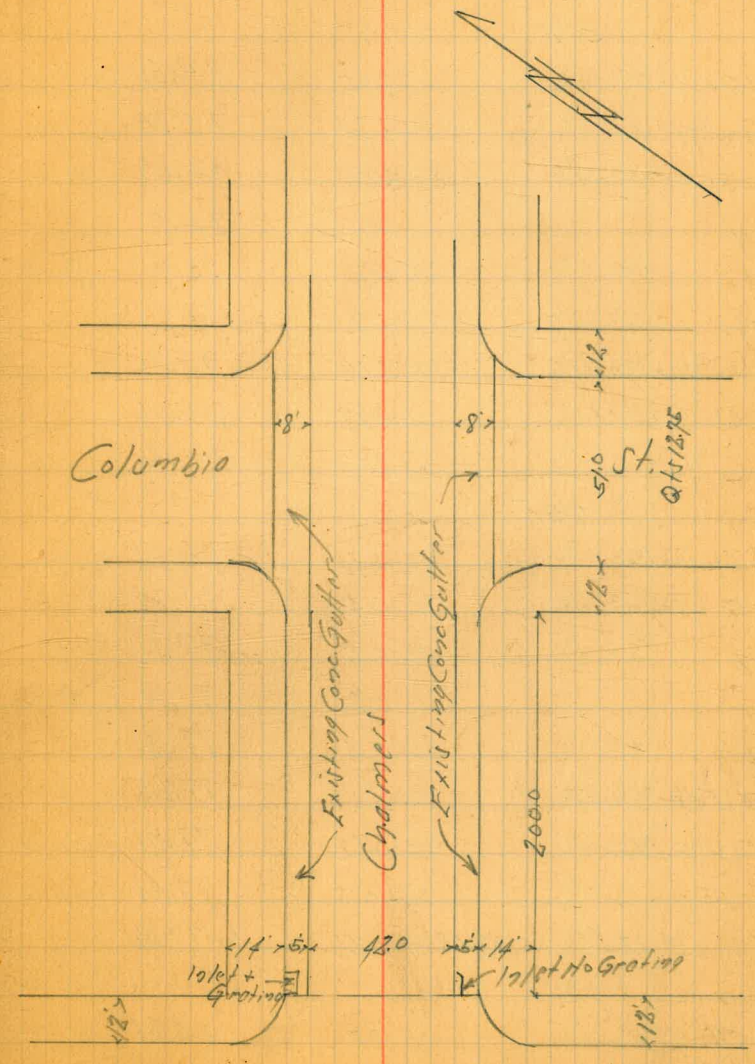


Chalmers

77.63

| | | |
|---|---|---|
| +10.5 Edge Gutter | 6.78 | 70.85 |
| NCb Drive | 7.04 | 70.59 |
| 50 E | | |
| NCb Top | 3.05 | 74.58 |
| Gutter | 3.84 | 73.79 |
| +5 = Edge Gutter | 3.56 | 74.07 |
| " | 3.7 | 73.9 |
| ℄ | 3.7 | 73.9 |
| " | 3.9 | 73.9 |
| +10.5 Edge Gutter | 3.69 | 73.94 |
| S Cb Gutter | 3.97 | 73.66 |
| Top | 3.17 | 74.46 |
| 75 E | | |
| S Cb Gutter | 0.74 | 76.89 |
| +5 = Edge Gutter | 0.44 | 77.19 |
| " | 0.5 | 77.1 |
| ℄ | 0.2 | 77.4 |
| " | 0.3 | 77.3 |
| +10.5 Edge Gutter | 0.38 | 77.25 |
| N Cb Gutter | 0.62 | 77.01 |
| Top | +0.18 | 77.81 |
| TP 12.46 89.48 | 0.61 | 77.02 |
| 100 E | | |
| N Cb Top | 8.5 | 80.87 |
| Gutter | 9.28 | 80.20 |
| +5 = Edge Gutter | 9.05 | 80.43 |

89.48

| | | |
|---|---|---|
| " | 9.0 | 80.5 |
| ℄ on N.H. Cover | 8.51 | 80.97 |
| " | 8.9 | 80.6 |
| +10.5 Edge Gutter | 9.13 | 80.35 |
| S Cb Gutter | 9.42 | 80.06 |
| S Cb Top | 8.57 | 80.91 |
| 125 E | | |
| S Cb Top | 5.27 | 84.21 |
| Gutter | 6.11 | 83.37 |
| +5 = Edge Gutter | 5.88 | 83.60 |
| " | 5.7 | 83.8 |
| ℄ | 5.1 | 84.0 |
| " | 5.7 | 83.8 |
| +10.5 Edge Gutter | 5.79 | 83.69 |
| N Cb Gutter | 6.02 | 83.46 |
| N Cb Top | 5.20 | 84.28 |
| 150 E | | |
| N Cb Top | 3.04 | 87.44 |
| Gutter | 2.83 | 86.65 |
| +5 = Edge Gutter | 2.58 | 86.90 |
| " | 2.4 | 87.1 |
| ℄ | 3.5 | 87.0 |
| " | 2.7 | 86.7 |
| +10.5 Edge Gutter | 2.60 | 86.88 |
| S Cb Gutter | 2.89 | 86.59 |
| S Cb Top | 2.07 | 87.41 |

Cholmers

89.48

| | | | | |
|---|---|---|---|---|
| TP | 11.42 | 100.13 | 0.77 | 88.71 |
| | | 175 E | | |
| S Cb Top | | | 9.59 | 90.54 |
| Gutter | | | 10.35 | 89.78 |
| ↓ +5 = Edge Gutter | | | 10.06 | 90.07 |
| ¼ | | | 10.4 | 89.7 |
| ↓ ℄ | | | 10.0 | 90.1 |
| ¼ | | | 10.1 | 90.0 |
| ↓ +10.5 = Edge Gutter | | | 9.95 | 90.18 |
| N Cb Gutter | | | 10.23 | 89.90 |
| N Cb Top | | | 9.39 | 90.74 |
| | | 188 E | | |
| N Cb Top | | | 7.70 | 92.43 |
| Gutter | | | 8.52 | 91.61 |
| ↓ +5 = Edge Gutter | | | 8.30 | 91.83 |
| ¼ | | | 8.5 | 91.6 |
| ↓ ℄ | | | 8.6 | 91.5 |
| ¼ | | | 8.9 | 91.2 |
| ↓ +10.5 Edge Gutter | | | 8.47 | 91.66 |
| S Cb Gutter | | | 8.69 | 91.44 |
| S Cb Top | | | 7.88 | 92.25 |
| | | 300 E = N.L Columbia | | |
| S Cb Top | | | 6.35 | 93.78 |
| Gutter | | | 7.29 | 92.84 |
| ↓ +5 = Edge Gutter | | | 7.00 | 93.13 |
| ¼ | | | 7.9 | 92.2 |

100.13

| | | | |
|---|---|---|---|
| ↓ ℄ | 7.5 | 92.6 | ✓ |
| ¼ | 7.3 | 92.8 | |
| ↓ +10.5 = Edge Gutter | 6.62 | 93.41 | |
| N Cb Gutter | 6.81 | 93.32 | |
| N Cb Top | 6.11 | 94.02 | |
| | N Cb | | |
| N L Top Cb | 6.12 | 94.01 | |
| ↓ N Edge Gutter | 6.61 | 93.52 | |
| Cb in " | 6.77 | 93.36 | |
| ↓ +5 = S Edge " | 6.52 | 93.61 | |
| ¼ | 6.3 | 93.8 | |
| ↓ ℄ | 6.5 | 93.6 | ✓ |
| ¼ | 6.9 | 93.2 | |
| +10.5 = Edge Gutter | 6.65 | 93.48 | |
| Cb on " | 6.93 | 93.20 | |
| S Edge " | 6.73 | 93.40 | |
| S L Top Cb | 6.82 | 93.81 | |
| | W ¼ | | |
| S | 5.8 | 94.3 | |
| S Edge Gutter | 5.89 | 94.24 | |
| Cb on " | 6.22 | 93.91 | |
| ↓ +5 = Edge " | 5.91 | 94.17 | |
| ¼ | 6.0 | 94.1 | ✓ |
| ↓ ℄ | 5.7 | 94.4 | |
| ¼ | 5.5 | 94.6 | |
| ↓ +10.5 = Edge Gutter | 5.83 | 94.30 | |

Chalmers

100.13

| | | |
|---|---|---|
| Cb on Gutter | 6.17 | 93.96 |
| N Edge " | 5.88 | 94.25 |
| N L | 5.8 | 94.3 |
| ℄ | | |
| N L | 4.7 | 95.4 |
| N Edge Gutter | 5.17 | 94.96 |
| Cb on " | 5.16 | 94.67 |
| ↓ +5 : S Edge " | 5.28 | 94.85 |
| ¼ " | 5.0 | 95.1 |
| ↓ ℄ " | 5.1 | 95.0 ✓ |
| ¼ " | 5.4 | 94.7 |
| ↓ +10.5 : N Edge Gutter | 5.23 | 94.90 |
| Cb on " | 5.55 | 94.58 |
| S Edge " | 5.24 | 94.89 |
| S L | 4.7 | 95.4 |
| E ℄ | | |
| S L | 4.3 | 95.8 |
| S Edge Gutter | 4.57 | 95.56 |
| Cb on " | 4.87 | 95.26 |
| ↓ N Edge " | 4.55 | 95.58 |
| ¼ " | 4.7 | 95.4 |
| ↓ ℄ " | 4.3 | 95.8 ✓ |
| ¼ " | 4.6 | 95.5 |
| ↓ +10.5 : Edge Gutter | 4.51 | 95.62 |
| Cb on " | 4.78 | 95.35 |
| N Edge " | 4.19 | 95.64 |

100.13

| | | |
|---|---|---|
| N L | 4.0 | 96.1 |
| E Cb | | |
| N L Top Cb | 3.11 | 97.02 |
| Gutter Dirt | 3.4 | 96.7 |
| N Edge Gutter | 3.78 | 96.35 |
| Cb on " | 4.03 | 96.10 |
| ↓ +5 : Edge " | 3.76 | 96.37 |
| ¼ " | 4.0 | 96.1 |
| ↓ ℄ " | 3.6 | 96.5 ✓ |
| ↓ ℄ : N of Lot on M K R.R. " | 3.75 | 96.38 |
| ¼ " | 4.1 | 96.0 |
| ↓ +10.5 : Edge Gutter " | 3.91 | 96.22 |
| Cb on " | 4.22 | 95.91 |
| S Edge " | 3.92 | 96.21 |
| S L Top Cb | 3.18 | 96.95 |
| Dirt " | 3.7 | 96.4 |
| E L Columbia | | |
| S Cb Top | 3.16 | 96.97 |
| Gutter " | 3.96 | 96.17 |
| ↓ +5 : Edge Gutter " | 3.68 | 96.45 |
| ¼ " | 3.5 | 96.6 |
| ↓ ℄ " | 3.2 | 96.9 ✓ |
| ¼ " | 3.6 | 96.5 |
| ↓ +10.5 : Edge Gutter " | 3.62 | 96.51 |
| N Cb Gutter " | 3.90 | 96.23 |
| N Cb Top " | 3.11 | 97.02 |
| B M | 3.02 | 97.11 |

SEBP Chalmers & Columbia 97.11

Mc Kee St Cross Section
California to Kellogg

40' Roadway
10' Q's

| | | | | |
|---|---|---|---|---|
| BM | 7.96 | 60.47 | 52.51 | NEBP Hodgens & California |
| | 0+0 - 12 = E Gutter of California | | | |
| SCb | on Paving | | 4.03 | 56.44 |
| ¼ | " " | | 3.86 | 56.61 |
| ✓ E | " " | | 3.82 | 56.65 |
| ¼ | " " | | 3.62 | 56.85 |
| NCb | " " | | 3.50 | 56.97 |
| | E.L. California | | | |
| NCb Top | | | 2.55 | 57.92 |
| Gutter | on Paving | | 2.82 | 57.25 |
| ¼ | " " | | 2.75 | 57.72 |
| ✓ E | " " | | 2.78 | 57.69 |
| ¼ | " " | | 2.12 | 57.34 |
| S Gutter | " " | | 3.91 | 56.56 |
| S Cb | Top | | 3.31 | 57.16 |
| | 12½ E of E.L. Calif | | | |
| SCb | Top | | 1.77 | 58.70 |
| Gutter | | | 2.5 | 58.0 |
| ¼ | | | 2.0 | 58.5 |
| ✓ E | | | 1.7 | 58.8 |
| ¼ | | | 1.8 | 58.7 |
| N Gutter | | | 2.0 | 58.5 |
| NCb | Top | | 0.93 | 59.54 |
| TP | 12+60 | 72.86 | 0.31 | 60.86 |

Indexed
C.S.K.I

Sec 2015
12/27/49
31

8-13-23
Moore
Northam
Sisson

71

72.86

25' E of E.L. California

| | | |
|---|---|---|
| NCb Top | 11.91 | 60.95 |
| Gutter | 12.7 | 60.2 |
| ¼ | 12.5 | 60.4 |
| ✓ E | 12.5 | 60.4 |
| ¼ | 12.9 | 60.0 |
| Gutter | 13.3 | 59.6 |
| SCb Top | 12.57 | 60.29 |
| | 50' E of E.L. Calif | |
| SCb Top | 9.25 | 63.51 |
| Gutter | 9.9 | 63.0 |
| ¼ | 9.3 | 63.6 |
| ✓ E | 9.2 | 63.7 |
| ¼ | 9.4 | 63.5 |
| Gutter | 9.4 | 63.5 |
| NCb Top | 8.89 | 63.97 |
| | 75' E of E.L. Calif | |
| NCb Top | 5.05 | 67.81 |
| Gutter | 5.6 | 67.3 |
| ✓ ¼ | 5.5 | 67.4 |
| E | 5.5 | 67.4 |
| ¼ | 5.8 | 67.1 |
| Gutter | 5.9 | 67.0 |
| SCb Top | 5.60 | 67.3 |

McKee St.

72.86

100' E of EL California

| | | | |
|---|---|---|---|
| S Gutter in Driveway | | 2.31 | 70.55 |
| ¼ | | 1.8 | 71.1 |
| ½ | | 1.7 | 71.2 |
| ¼ | | 1.6 | 71.3 |
| Gutter | | 1.6 | 71.3 |
| N Cb Top | | 1.03 | 71.83 |
| TP | 12.64 84.99 | 0.51 | 72.35 |

125' E of EL Calif

| | | | |
|---|---|---|---|
| N Cb Top | | 9.20 | 75.79 |
| Gutter | | 9.7 | 75.3 |
| ¼ | | 9.8 | 75.2 |
| ½ | | 10.0 | 75.0 |
| ¼ | | 10.1 | 74.9 |
| Gutter | | 10.4 | 74.6 |
| S Cb Top | | 9.98 | 75.01 |

150' E of EL Calif

| | | | |
|---|---|---|---|
| S Gutter in Drive | | 6.65 | 78.34 |
| ¼ | | 6.3 | 78.6 |
| ½ | | 6.1 | 78.8 |
| ¼ | | 6.1 | 78.8 |
| Gutter | | 6.0 | 78.9 |
| N Cb Top | | 5.35 | 79.64 |

84.99

175' E of EL Calif.

| | | | |
|---|---|---|---|
| N Cb Top | | 1.40 | 83.59 |
| Gutter | | 2.0 | 83.0 |
| ¼ | | 2.1 | 82.9 |
| ½ | | 2.2 | 82.8 |
| ¼ | | 2.3 | 82.7 |
| Gutter | | 2.6 | 82.4 |
| S Cb Top | | 2.28 | 82.71 |
| TP | 9.43 93.90 | 0.52 | 81.47 |

199.6' E of EL Calif.

| | | | |
|---|---|---|---|
| S Cb Top | | 7.44 | 86.46 |
| Gutter | | 7.7 | 86.2 |
| ¼ | | 7.3 | 86.6 |
| ½ | | 7.3 | 86.6 |
| ¼ | | 6.9 | 87.0 |
| Gutter | | 7.0 | 86.9 |
| N Cb Top | | 6.47 | 87.43 |

209.6' E of McKee Ave

| | | | |
|---|---|---|---|
| N Cb Top | | 4.98 | 88.92 |
| Gutter on Paving | | 5.66 | 88.24 |
| ¼ " " | | 5.51 | 88.39 |
| ½ " " | | 5.57 | 88.33 |
| ¼ " " | | 5.92 | 87.98 |
| Gutter " " | | 6.40 | 87.50 |
| S Cb Top | | 5.93 | 87.97 |

McKee St.

93.90

W Gutter of Kelhaven Blvd

| | | | | |
|---|---|---|---|---|
| S Eb of Paving | | | 6.29 | 87.66 |
| W | " | " | 6.04 | 87.86 |
| E | " | " | 5.75 | 87.15 |
| W | " | " | 5.62 | 87.28 |
| W Cb | " | " | 5.52 | 87.38 |
| TP | 0.17 | 81.18 | 12.89 | 81.01 |
| TP | 0.04 | 68.51 | 12.71 | 68.47 |
| TP | 3.47 | 60.81 | 11.17 | 57.34 |
| BM | | | 8.28 | 52.53 |

NE BP Hydrant Elev 52.51

8-18-34 Shoemaker-Updegraf, Woods.

B.M. 11+15 P.I. 31c 1441

| | | | | |
|---|---|---|---|---|
| Hub on B.L. | 5.28 | 279.43 | | 274.15 |
| BL+25E 8+66 | | | 3.6 | 275.8 |
| 8+54 | | | 1.7 | 277.7 |
| 8+40 | | | 1.5 | 277.9 |
| 8+37 | | | 2.6 | 276.8 |
| A East 8+37 | | | 2.6 | 276.8 |
| 8+40 | | | 1.6 | 277.8 |
| 8+60 | | | 2.9 | 276.5 |
| A+25E 8+66 | | | 3.8 | 275.6 |
| 8+38 | | | 1.7 | 277.7 |
| 8+36 | | | 2.4 | 277.0 |

Balbo Park - Swimming Pool Area -
Line Change - Road Around Ball Grounds

12/1/33

(Same)
13+01.49 P.T. (North line of Road South of Pool)

13+55.83 P.C. Rt.

Δ = 39°30R
T = 59.96
L = 115.13
R = 167.0

See Page 2 Book 1479

14+70.96 P.T.

18+47.33 PC. Lt

Δ = 207°30'L

L =
R = 343.49

30+91.31 = PT Eqv.
30+61.06

Levels taken Top of Stakes Blued

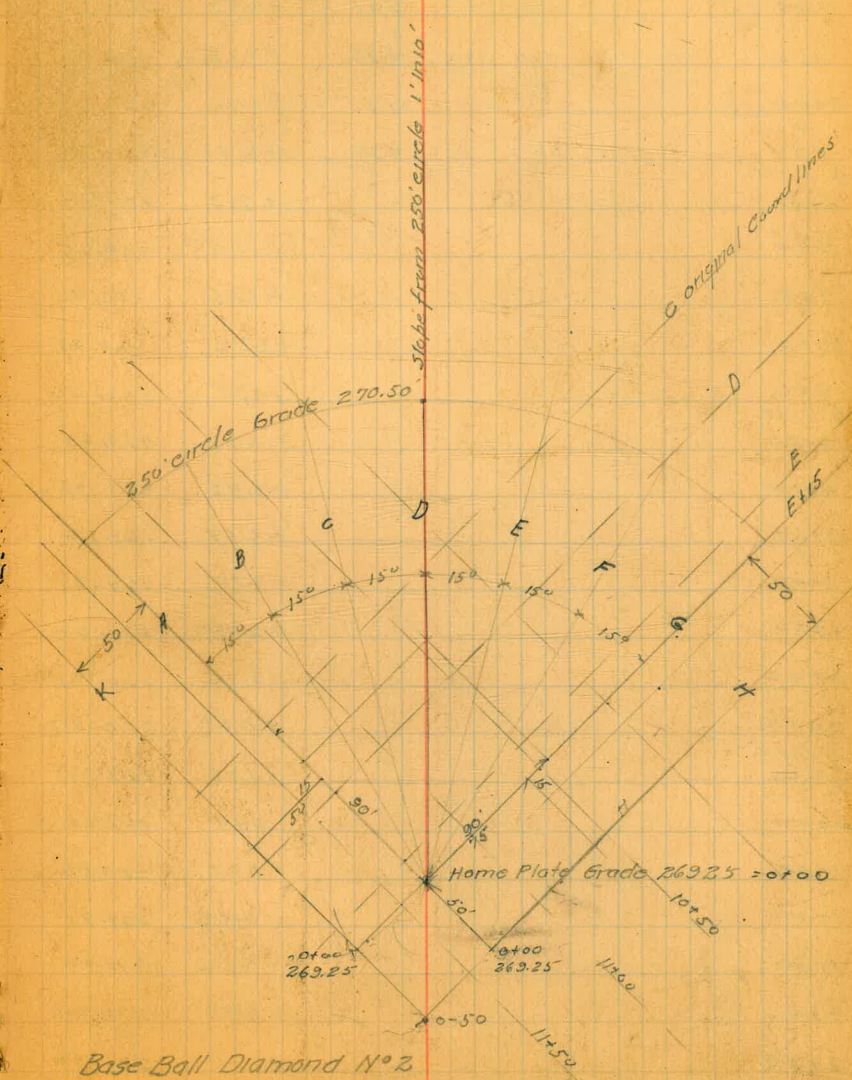
| Sta | + | HI | Rod | Cut +or- Fill | Grade |
|---|---|---|---|---|---|
| A Line | | | | | |
| 0+00 | 0.615 | 274.76 | 5.51 | +0.63 | 269.25 |
| +50 | | | 5.26 | -1.60 | 269.50 |
| 1+00 | | | 5.01 | -2.16 | 269.75 |
| +50 | | | 4.76 | -0.94 | 270.00 |
| 2+00 | | | 4.51 | +0.17 | 270.25 |
| +50 | | | 4.26 | +2.20 | 270.50 |
| B Line | | | | | |
| 0+50 | | | | | 269.50 |
| 1+00 | | | | -1.38 | 269.75 |
| +50 | | | | -0.71 | 270.00 |
| 2+00 | | | | +0.44 | 270.25 |
| +50 | | | | +3.3 | 270.50 |
| C Line | | | | | |
| 0+50 | | | | -0.73 | 269.50 |
| 1+00 | | | | -1.47 | 269.75 |
| +50 | | | | -0.05 | 270.00 |
| 2+00 | | | | +0.28 | 270.25 |
| +50 | | | | +1.72 | 270.50 |
| D Line | | | | | |
| 0+50 | | | | | 269.50 |
| 1+00 | | | | -0.31 | 269.75 |
| +50 | | | | +0.52 | 270.00 |
| 2+00 | | | | +0.57 | 270.25 |
| +50 | | | | +2.29 | 270.50 |
| E Line | | | | | |
| 0+50 | | | | +0.18 | 269.50 |
| 1+00 | | | | -0.33 | 269.75 |
| +50 | | | | +0.28 | 270.00 |
| 2+00 | | | | +1.20 | 270.25 |
| +50 | | | | +2.15 | 270.50 |

Fill cut from top of stakes which are about .9' above ground



B M Elev 274.15 Sta 11+15 Base Line Back 1441.21

Elev. Top of Culvert Headwall 267.54




Base Ball Diamond N° 2

Recreational Area Balboa Park

Scale 1" = 100'

| Stg | + | H.I | Rod | cut + | Fill − | Grade |
|---|---|---|---|---|---|---|
| F Line | | | | | | |
| 0+50 | | | 5.26 | | | 269.50 |
| 1+00 | | | 5.01 | +0.67 | | 269.25 |
| +50 | | | 4.76 | +0.28 | | 270.00 |
| 2+00 | | | 4.51 | +1.46 | | 270.25 |
| +50 | | | 4.26 | +2.41 | | 270.50 |
| G Line | | | | | | |
| 0+50 | | | | +1.63 | | 269.50 |
| 1+00 | | | | +1.80 | | 269.25 |
| +50 | | | | +2.33 | | 270.00 |
| 2+00 | | | | +2.92 | | 270.25 |
| +50 | | | | +2.95 | | 270.50 |
| H Line | | | | | | |
| 0-50 | | | | +1.73 | | 269.25 |
| 0+00 | | | | +2.46 | | 269.25 |
| 0+50 | | | | +3.54 | | 269.50 |
| 1+00 | | | | +3.70 | | 269.25 |
| 1+50 | | | | +2.89 | | 270.00 |
| 2+00 | | | | +2.30 | | 270.25 |
| 2+50 | | | | +1.55 | | 270.50 |
| K Line | | | | | | |
| 0-50 | | | | +1.73 | | 269.25 |
| 0+00 | | | | -1.44 | | 269.25 |
| 0+50 | | | | -3.75 | | 269.50 |
| 1+00 | | | | -1.42 | | 269.25 |
| 1+50 | | | | -1.22 | | 270.00 |
| 2+00 | | | | -0.45 | | 270.25 |
| 2+50 | | | | +1.75 | | 270.50 |

451 305 146 595 449 | 451 371 570 426 94 | 451 384 457 543 426 87 | 451 457 426 424 33 | 451 426 448 534 501 | 426 443 33 532 501 | 426 177 284 448 501 147 | 426 639 501 213 501 212 | 274.13 61 274.76 269.21 5.51 274.96 270.10 426

501 134 370 501 321 | 501 434 69 | 534 501 | 532 501 | 448 501 147 | 639 501 | 213 501 212

906 526 3.75 | 695 526 1 | 599 526 73 | 526 508 18 | 526 363 163 | 526 172 354 | 526

551 305 246 | 551 488 63 | 695 551 144 | 551 328 173

# Ground Levels

| Sta | + | HI | − | Elev | BM |
|---|---|---|---|---|---|
| X | | | | | |
| 0-50 | | 274.76 | 4.44 | 270.32 | |
| 0+00 | | | 6.98 | 67.78 | |
| 0+50 | | | 9.04 | 65.72 | |
| 1+00 | | | 7.30 | 67.46 | |
| 1+50 | | | 6.95 | 67.81 | |
| 2+00 | | | 5.88 | 68.88 | |
| 2+50 | | | 3.60 | 71.16 | |
| A Line | | | | | |
| 0+00 | | | 5.53 | 69.23 | |
| 0+50 | | | 7.91 | 66.85 | |
| 1+00 | | | 7.90 | 66.86 | |
| 1+50 | | | 6.63 | 68.13 | |
| 2+00 | | | 5.31 | 69.45 | |
| 2+50 | | | 2.96 | 71.80 | |
| B Line | | | | | |
| 0+50 | | | | | |
| 1+00 | | | 7.39 | 67.37 | |
| 1+50 | | | 6.36 | 68.40 | |
| 2+00 | | | 4.95 | 69.81 | |
| 2+50 | | | 1.61 | 73.15 | |
| C. Line | | | | | |
| 0+50 | | | 6.74 | 68.02 | |
| 1+00 | | | 7.23 | 67.53 | |
| 1+50 | | | 5.87 | 68.89 | |
| 2+00 | | | 5.15 | 69.61 | |
| 2+50 | | | 3.43 | 71.33 | |

| Sta | + | HI | - | Elev |
|---|---|---|---|---|
| D Line | | | | |
| 0+50 | | 74.76 | | |
| 1+00 | | | 6.23 | 68.53 |
| +50 | | | 4.93 | 69.83 |
| 2+00 | | | 4.87 | 69.89 |
| +50 | | | 2.83 | 71.93 |
| E Line | | | | |
| 0+50 | | | 5.82 | 68.94 |
| 1+00 | | | 6.16 | 68.60 |
| +50 | | | 5.31 | 69.45 |
| 2+00 | | | 4.07 | 70.69 |
| 2+50 | | | 3.01 | 71.75 |
| F Line | | | | |
| 0+50 | | | | |
| 1+00 | | | 5.32 | 69.42 |
| +50 | | | 5.31 | 69.43 |
| 2+00 | | | 3.79 | 70.97 |
| 2+50 | | | 2.63 | 72.13 |
| G Line | | | | |
| 0+50 | | | 4.46 | 70.30 |
| 1+00 | | | 3.80 | 70.96 |
| +50 | | | 3.22 | 71.54 |
| 2+00 | | | 2.36 | 72.40 |
| +50 | | | 2.35 | 72.41 |
| H Line | | | | |
| 0-50 | | | | |
| 0+00 | | | 3.62 | 71.14 |
| +50 | | | 2.70 | 72.06 |
| 1+00 | | | 2.08 | 72.68 |
| +50 | | | 246 | 72.30 |
| 2+00 | | | 3.04 | 71.72 |
| +50 | | | 3.55 | 71.21 |

# DIRECTIONS FOR USE OF TABLES

## TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

## TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

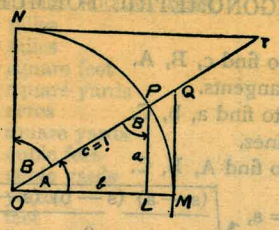



TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

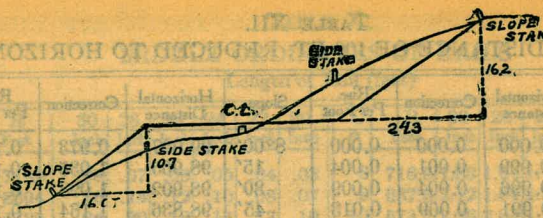
$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \text{Cos } A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \text{Cos } A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \tfrac{1}{2}(A+B)}{\tan \tfrac{1}{2}(A-B)}$$




## DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 0 00 | 0 15 | 0.30 | 0.45 | 0.60 | 0.75 | 0.90 | 1.05 | 1.20 | 1.35 | 0 |
| 1 | 1.50 | 1 65 | 1 80 | 1.95 | 2.10 | 2.25 | 2.40 | 2.55 | 2.70 | 2.85 | 1 |
| 2 | 3.00 | 3.15 | 3.30 | 3 45 | 3.60 | 3 75 | 3.90 | 4.05 | 4.20 | 4 35 | 2 |
| 3 | 4.50 | 4 65 | 4.80 | 4.95 | 5 10 | 5 25 | 5 40 | 5.55 | 5.70 | 5.85 | 3 |
| 4 | 6.00 | 6 15 | 6.30 | 6.45 | 6.60 | 6.75 | 6.90 | 7.05 | 7.20 | 7.35 | 4 |
| 5 | 7 50 | 7.65 | 7.80 | 7.95 | 8.10 | 8.25 | 8.40 | 8.55 | 8.70 | 8.85 | 5 |
| 6 | 9 00 | 9 15 | 9.30 | 9.45 | 9.60 | 9.75 | 9.90 | 10.05 | 10.20 | 10.35 | 6 |
| 7 | 10.50 | 10 65 | 10.80 | 10.95 | 11.10 | 11.25 | 11.40 | 11.55 | 11 70 | 11.85 | 7 |
| 8 | 12.00 | 12 15 | 12.30 | 12.45 | 12.60 | 12.75 | 12.90 | 13.05 | 13.20 | 13.35 | 8 |
| 9 | 13 50 | 13 65 | 13 80 | 13 95 | 14.10 | 14.25 | 14.40 | 14 55 | 14.70 | 14.85 | 9 |
| 10 | 15.00 | 15 15 | 15 30 | 15 45 | 15.60 | 15.75 | 15.90 | 16.05 | 16.20 | 16 35 | 10 |
| 11 | 16 50 | 16 65 | 16 80 | 16.95 | 17 10 | 17.25 | 17.40 | 17.55 | 17.70 | 17.85 | 11 |
| 12 | 18 00 | 18.15 | 18.30 | 18 45 | 18.60 | 18 75 | 18.90 | 19.05 | 19.20 | 19 35 | 12 |
| 13 | 19 50 | 19 65 | 19.80 | 19.95 | 20.10 | 20.25 | 20 40 | 20.55 | 20.70 | 20.85 | 13 |
| 14 | 21.00 | 21 15 | 21.30 | 21.45 | 21 60 | 21.75 | 21.90 | 22 05 | 22 20 | 22 35 | 14 |
| 15 | 22 50 | 22 65 | 22 80 | 22 95 | 23.10 | 23.25 | 23.40 | 23.55 | 23.70 | 23.85 | 15 |
| 16 | 24.00 | 24 15 | 24 30 | 24 45 | 24 60 | 24.75 | 24 90 | 25 05 | 25.20 | 25.35 | 16 |
| 17 | 25.50 | 25 65 | 25.80 | 25 95 | 26.10 | 26 25 | 26 40 | 26.55 | 26.70 | 26.85 | 17 |
| 18 | 27.00 | 27 15 | 27.30 | 27 45 | 27.60 | 27.75 | 27.90 | 28.05 | 28 20 | 28.35 | 18 |
| 19 | 28 50 | 28 65 | 28 80 | 28.95 | 29.10 | 29.25 | 29.40 | 29.55 | 29.70 | 29.85 | 19 |
| 20 | 30 00 | 30 15 | 30.30 | 30.45 | 30.60 | 30.75 | 30.90 | 31.05 | 31.20 | 31.35 | 20 |
| 21 | 31 50 | 31 65 | 31.80 | 31.95 | 32 10 | 32 25 | 32.40 | 32.55 | 32 70 | 32 85 | 21 |
| 22 | 33 00 | 33 15 | 33 30 | 33 45 | 33.60 | 33 75 | 33.90 | 34.05 | 34.20 | 34.35 | 22 |
| 23 | 34 50 | 34 65 | 34.80 | 34.95 | 35.10 | 35 25 | 35 40 | 35.55 | 35.70 | 35 85 | 23 |
| 24 | 36.00 | 36 15 | 36.30 | 36 45 | 36.60 | 36.75 | 36.90 | 37.05 | 37 20 | 37.35 | 24 |
| 25 | 37.50 | 37.65 | 37 80 | 37.95 | 38.10 | 38.25 | 38.40 | 38.55 | 38.70 | 38.85 | 25 |
| 26 | 39 00 | 39 15 | 39 30 | 39 45 | 39 60 | 39.75 | 39.90 | 40.05 | 40.20 | 40.35 | 26 |
| 27 | 40 50 | 40 65 | 40 80 | 40.95 | 41.10 | 41.25 | 41 40 | 41.55 | 41.70 | 41.85 | 27 |
| 28 | 42 00 | 42 15 | 42.30 | 42.45 | 42.60 | 42 75 | 42.90 | 43.05 | 43.20 | 43.35 | 28 |
| 29 | 43 50 | 43 65 | 43.80 | 43 95 | 44.10 | 44 25 | 44 40 | 44.55 | 44.70 | 44 85 | 29 |
| 30 | 45 00 | 45 15 | 45.30 | 45 45 | 45.60 | 45.75 | 45 90 | 46.05 | 46 20 | 46.35 | 30 |
| 31 | 46.50 | 46.65 | 46.80 | 46 95 | 47.10 | 47 25 | 47.40 | 47.55 | 47.70 | 47.85 | 31 |
| 32 | 48 00 | 48.15 | 48.30 | 48 45 | 48.60 | 48 75 | 48.90 | 49.05 | 49 20 | 49.35 | 32 |
| 33 | 49.50 | 49 65 | 49.80 | 49.95 | 50.10 | 50.25 | 50.40 | 50.55 | 50 70 | 50.85 | 33 |
| 34 | 51 00 | 51.15 | 51.30 | 51.45 | 51.60 | 51.75 | 51 90 | 52.05 | 52.20 | 52.35 | 34 |
| 35 | 52 50 | 52.65 | 52.80 | 52.95 | 53.10 | 53.25 | 53.40 | 53.55 | 53.70 | 53.85 | 35 |
| 36 | 54 00 | 54 15 | 54.30 | 54 45 | 54.60 | 54.75 | 54.90 | 55.05 | 55.20 | 55.35 | 36 |
| 37 | 55 50 | 55 65 | 55.80 | 55 95 | 56.10 | 56.25 | 56.40 | 56.55 | 56.70 | 56.85 | 37 |
| 38 | 57.00 | 57.15 | 57 30 | 57 45 | 57.60 | 57 75 | 57.90 | 58.05 | 58.20 | 58 35 | 38 |
| 39 | 58 50 | 58.65 | 58 80 | 58 95 | 59.10 | 59 25 | 59.40 | 59 55 | 59.70 | 59.85 | 39 |
| 40 | 60 00 | 60 15 | 60 30 | 60 45 | 60 60 | 60.75 | 60 90 | 61.05 | 61 20 | 61.35 | 40 |
| 41 | 61.50 | 61 65 | 61 80 | 61 95 | 62 10 | 62 25 | 62.40 | 62 55 | 62 70 | 62.85 | 41 |
| 42 | 63 00 | 63.15 | 63 30 | 63 45 | 63 60 | 63 75 | 63 90 | 64 05 | 64 20 | 64.35 | 42 |
| 43 | 64.50 | 64 65 | 64 80 | 64.95 | 65.10 | 65 25 | 65 40 | 65.55 | 65.70 | 65.85 | 43 |
| 44 | 66 00 | 66 15 | 66 30 | 66.45 | 66.60 | 66 75 | 66.90 | 67.05 | 67.20 | 67.35 | 44 |
| 45 | 67 50 | 67 65 | 67 80 | 67.95 | 68.10 | 68.25 | 68.40 | 68.55 | 68.70 | 68.85 | 45 |
| 46 | 69 00 | 69 15 | 69 30 | 69.45 | 69.60 | 69.75 | 69.90 | 70.05 | 70.20 | 70.35 | 46 |
| 47 | 70 50 | 70 65 | 70 80 | 70 95 | 71.10 | 71.25 | 71 40 | 71.55 | 71.70 | 71.85 | 47 |
| 48 | 72.00 | 72 15 | 72.30 | 72.45 | 72.60 | 72.75 | 72.90 | 73 05 | 73.20 | 73 35 | 48 |
| 49 | 73 50 | 73 65 | 73.80 | 73.95 | 74.10 | 74.25 | 74.40 | 74.55 | 74.70 | 74.85 | 49 |
| 50 | 75.00 | 75 15 | 75.30 | 75.45 | 75.60 | 75.75 | 75.90 | 76.05 | 76.20 | 76.35 | 50 |

Computed by L. Leland Locke.

Bundle's of Laths 1111 Stakes 11 Hubs 18

Elev. of Laurel St. Ext. -

15+56 - 148.51 #1397 P.77

POT 38+00 35'L & Hub #1355 79 "C"

39+50 & " #1355 64 "A" 131.92

Ernst Mosiem - F2766

2°55'

8" Bet X St. Pipe line