

1444

FIELD BOOK

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CHICAGO, ILL.

2+31 = Date 2+39L & Walk 7'

2+63 = Hole

2+65-23

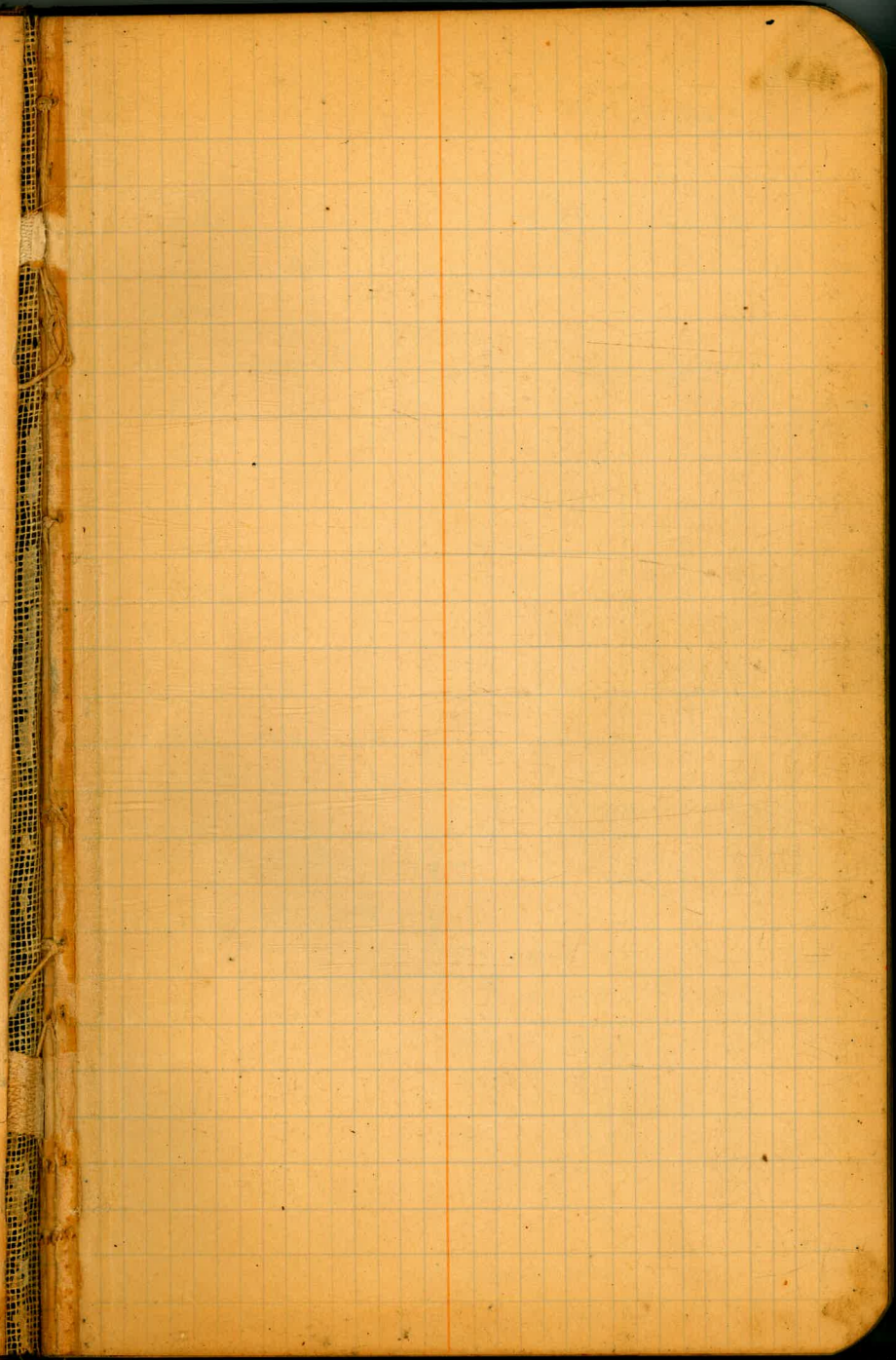
THE FREDERICK POST CO.
 ENGINEERS and SURVEYORS
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 GEORGETOWN, Md.

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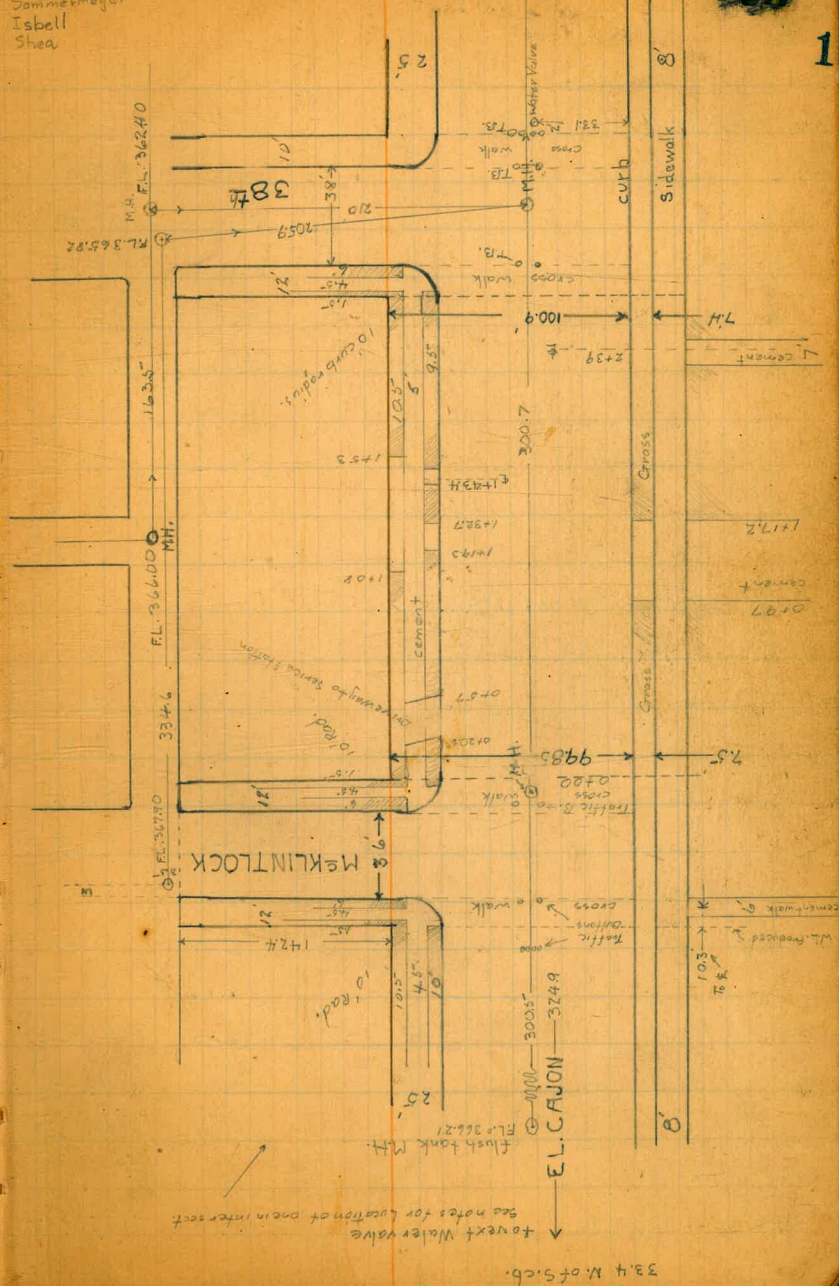
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X Sections for traffic tunnels
on El. Cajon between W.L. McKlintock
and W.L. 38th H.I.

EL Cajon 125' st. 25' cbs	18.75' $\frac{1}{4}$ ' ^s	373.50
BM = B.P. + 4.55	378.05	SW. Cor. El. Cajon 37 th
W.L. McKlintock	60' st. 12' cbs 36' roadway.	
N.L. El. Cajon on dirt	4.6	373.5 ✓
+1.05 = Nedge of sidewalk	4.69	373.36 ✓
+1.8 = S "	4.78	373.27 ✓
N. cb. El. Cajon top cb.	5.03	373.02 ✓
cut,	5.48	372.57 ✓
$\frac{1}{4}$	5.29	372.76 ✓
$\frac{1}{2}$	5.08	372.97 ✓
$\frac{3}{4}$	5.38	372.67 ✓
S. cb. El. Cajon in gutter	5.55	372.50 ✓
top cb.	4.99	373.06 ✓
+7.4 = N. edge sidewalk	4.74	373.31 ✓
+15.4 = S " "	4.61	373.44 ✓
W. cb. line McKlintock		
S. edge walk	4.58	373.47 ✓
N. " "	4.81	373.24 ✓
S. cb. top cb.	4.85	373.20 ✓
cut,	5.56	372.49 ✓
$\frac{1}{4}$	5.43	372.62 ✓
$\frac{1}{2}$	5.18	372.87 ✓
$\frac{3}{4}$	5.38	372.67 ✓
N. cb.	5.58	372.47 ✓
N.L. cut,	5.37	372.68 ✓

3/7/32
Osborne
Sommermeier
Isbell
Shea



H.I.
378.05

2

N.L.	top cb.	4.93	373.12 ✓
E. M ^c Klintock			
N.L.	on paving	5.06	72.99 ✓
N. cb.		5.73	72.32 ✓
$\frac{1}{4}$		5.41	72.64 ✓
E		5.27	72.78 ✓
$\frac{1}{4}$		5.46	72.59 ✓
s. cb.	gut.	5.63	72.42 ✓
	top cb.	4.92	73.13 ✓
N. edge walk		4.79	73.26 ✓
S. " "		4.55	73.50 ✓
E + 8 on N.L. = 6" water Valve			
E. cb. line M ^c Klintock			
s. edge walk		4.78	73.27 ✓
N. " "		4.95	73.10 ✓
s. cb.	top cb.	5.04	73.01 ✓
	gut.	5.73	72.32 ✓
$\frac{1}{4}$		5.51	72.54 ✓
E		5.20	72.85 ✓
$\frac{1}{4}$		5.46	72.59 ✓
N. cb.		5.80	72.25 ✓
N.L.	in gut.	5.63	72.42 ✓
	top cb.	5.17	72.88 ✓
cb. + 7.7'			
2.2' N. of E = M.H.	on rim	5.21	72.84 ✓
	flow line	11.91	66.14 ✓

378.05

3

0+00 = E.L. McKlintock

N. h.	on dirt.	5.0	373.1 ✓
+10.5	- edge of walk	4.88	73.17 ✓
+15.5	" " "	5.01	73.04 ✓
N. cb.	top cb.	5.12	72.93 ✓
	cut	5.26	72.19 ✓
$\frac{1}{4}$		5.46	72.59 ✓
$\frac{1}{2}$		5.23	72.82 ✓
$\frac{3}{4}$		5.60	72.45 ✓
S. cb.	cut.	5.20	72.25 ✓
	top cb.	5.16	72.89 ✓
N. edge walk	- Note - for pluses see sketch.	5.04	73.01 ✓
S. " "		4.89	73.16 ✓

0+02

1.7' N. of N. cb. = Fire Hydrant.

4.2' S. of $\frac{1}{2}$ = Water Valve

0+13.5 = 1.7' S. of s. cb. = Pole

0+20.5 = W. end of driveway on N. side.

S. edge walk.		4.97	73.08 ✓
N. " "		5.12	72.87 ✓
3.5' S. of s. cb.	= 8" tree		
s. cb.	top cb.	5.32	72.67 ✓
	cut.	5.99	72.06 ✓
$\frac{1}{4}$		5.70	72.35 ✓
$\frac{1}{2}$		5.46	72.59 ✓

37805 ✓

4

1/4		5.69	372.36 ✓
N. cb.	gut. in driveway	6.11	71.94 ✓
	top cb.	5.48	72.57 ✓
+9.5 =	Sedge walk	5.34	72.71 ✓
+14.5 =	N. " "	5.22	72.83 ✓
N.L.		5.2	72.9 ✓
0+45.1 = 6" Drainage outlet in srb.			
0+57 = E. end of driveway on N. side			
N.L.		5.7	72.4 ✓
N.	edge walk	5.80	72.25 ✓
S.	" "	5.85	72.20 ✓
N. cb.	top cb.	6.02	72.03 ✓
	gut. in driveway	6.55	71.50 ✓
1/4		6.09	71.96 ✓
E		5.76	72.29 ✓
1/4		5.96	72.09 ✓
S. cb.	top cb. gut.	6.14	71.91 ✓
	top cb.	5.44	72.61 ✓
N.	edge walk	5.36	72.69 ✓
S.	" "	5.08	72.97 ✓
0+71.5 = 3.5' S. of S. cb. = 9" tree			
0+73 = Water Meter on North			
0+75			
S.	edge walk	5.27	72.78 ✓
N.	" "	5.55	72.50 ✓
S. cb.	top cb.	5.72	72.33 ✓
	gut.	6.26	71.79 ✓

$\frac{1}{4}$		6.08	371.97 ✓
$\frac{1}{2}$		6.03	72.02 ✓
$\frac{3}{4}$		6.24	71.81 ✓
N. cb.	gut	6.72	71.33 ✓
	top cb.	6.25	71.80 ✓
S. edge walk		6.11	71.94 ✓
N. " "		6.06	71.99 ✓
N.L.	on dirt.	6.0	72.1 ✓
0+83 = $\frac{1}{2}$ cement walk on north. from N edge of walk to N.L.			
0+97 = W. end of front walk to school			
N.L.		6.2	71.9 ✓
N. edge walk		6.24	71.81 ✓
S. " "		6.33	71.72 ✓
N. cb.	top	6.56	71.49 ✓
	gut	6.88	71.17 ✓
$\frac{1}{4}$		6.49	71.56 ✓
$\frac{1}{2}$		6.15	71.90 ✓
$\frac{3}{4}$		6.22	71.83 ✓
S. cb.	gut	6.29	71.76 ✓
	top	5.67	72.38 ✓
N. edge walk		5.50	72.55 ✓
S. " "		5.22	72.83 ✓
†+08 = W. end of Concrete apron in front of Bldg. on North. N.L. to N. edge walk.			
S. edge walk on south		5.20	72.85 ✓
N. " "		5.37	72.48 ✓

S. cb	top	5.73	372.32 ✓
	gut.	6.32	71.73 ✓
$\frac{1}{4}$		6.29	71.76 ✓
$\frac{1}{2}$		6.24	71.81 ✓
$\frac{3}{4}$		6.63	71.42 ✓
N. cb	gut.	7.15	70.90 ✓
	top	6.64	71.41 ✓
S. edge walk		6.40	71.65 ✓
N. " "		6.26	71.77 ✓
N. h. on cement		6.21	71.84 ✓
1+17.2 = E. end of front walk to school - cement			
N. h. on cement		6.17	71.88 ✓
V. edge walk		6.45	71.60 ✓
S. " "		6.56	71.49 ✓
N. cb.	top	6.73	71.32 ✓
	gut.	7.28	70.77 ✓
$\frac{1}{4}$		6.67	71.38 ✓
$\frac{1}{2}$		6.23	71.82 ✓
$\frac{3}{4}$		6.38	71.67 ✓
S. cb	gut.	6.42	71.63 ✓
	top	5.94	72.11 ✓
N. edge walk		5.83	72.22 ✓
S. " "		5.42	72.63 ✓

1+19.3 W. end of concrete walk from cb. to s. edge walk on North

1.5' S. of S. cb. = Pole

1+32.7 = E. end of concrete walk from N. cb. to s. edge of walk on North.			
s. edge walk	5.67	372.38	✓
N. " "	5.97	72.08	✓
S. cb. top	6.02	72.03	✓
gut.	6.60	71.45	✓
$\frac{1}{4}$	6.58	71.47	✓
$\frac{1}{2}$	6.53	71.52	✓
$\frac{3}{4}$	6.89	71.16	✓
N. cb. gut	7.42	70.63	✓
top	6.80	71.25	✓
s. edge walk	6.74	71.31	✓
N. " "	6.50	71.55	✓
N. li. on cement	6.15	71.90	✓
1+43.4 = E. 4 walk from N. cb. to s. edge walk on North			
1+53 = E. end of concrete apron in front of Bldg. on North N. li. to N. edge walk.			
N. li. on cement	6.21	71.84	✓
N. edge of walk	6.88	71.17	✓
S. " " "	6.98	71.07	✓
1.5' N. of cb. = water meter			
N. cb. top	7.10	70.95	✓
gut.	7.65	70.40	✓
$\frac{1}{4}$	7.15	70.90	✓
$\frac{1}{2}$	6.70	71.35	✓
$\frac{3}{4}$	6.73	71.32	✓
S. cb. gut.	6.74	71.31	✓

37805

s. cb.	top	6.08	371.97 ✓
N. edgewalk		6.10	71.95 ✓
s. " "		5.86	72.19 ✓
1+66.7 = 6" drainage outlet in s. cb.			
1+75			
s. edgewalk		5.95	72.10 ✓
N. " "		6.24	71.81 ✓
s. cb.	top	6.24	71.81 ✓
	gut.	6.90	71.15 ✓
$\frac{1}{4}$		6.88	71.17 ✓
E		6.94	71.11 ✓
$\frac{1}{4}$		7.27	70.78 ✓
N. cb.	to gut.	8.00	70.05 ✓
	top	7.37	70.68 ✓
s. edgewalk		7.24	70.81 ✓
N. " "		7.16	70.89 ✓
N.L. on dirt.		6.8	71.3 ✓
2+00			
N.L. on dirt		6.8	71.3 ✓
N. edgewalk		7.42	70.63 ✓
s. " "		7.58	70.49 ✓
N. cb.	top	7.71	70.34 ✓
	gut.	8.31	69.74 ✓
$\frac{1}{4}$		7.53	70.52 ✓
E		7.12	70.93 ✓
$\frac{1}{4}$		7.10	70.95 ✓

8

372.05

9

s. cb.	gut.	7.00	371.05 ✓
	top	6.26	71.79 ✓
N. edge walk		6.43	71.62 ✓
s. " "		6.27	71.78 ✓
2+25			
s. edge walk		6.46	71.59 ✓
N. " "		6.63	71.42 ✓
s. cb.	top	6.59	71.46 ✓
	gut.	7.21	70.84 ✓
4		7.30	70.75 ✓
8		7.28	70.77 ✓
4		7.83	70.22 ✓
N. cb.	gut	8.64	69.41 ✓
	top	8.06	69.99 ✓
s. edgewalk		7.83	70.22 ✓
N. " "		7.75	70.30 ✓
N. L.		7.2	70.9 ✓
2+31	1.5' s. of s.cb. = Pole		
2+39	of cement walk 7' wide. from s. edge walk to school on South.		
2+50			
N. L.	on dirt	7.6	70.5 ✓
N. edge walk		8.11	69.94 ✓
s. " "		8.18	69.87 ✓
N. cb.	top	8.34	69.71 ✓
	gut.	8.93	69.12 ✓
4		8.04	70.01 ✓

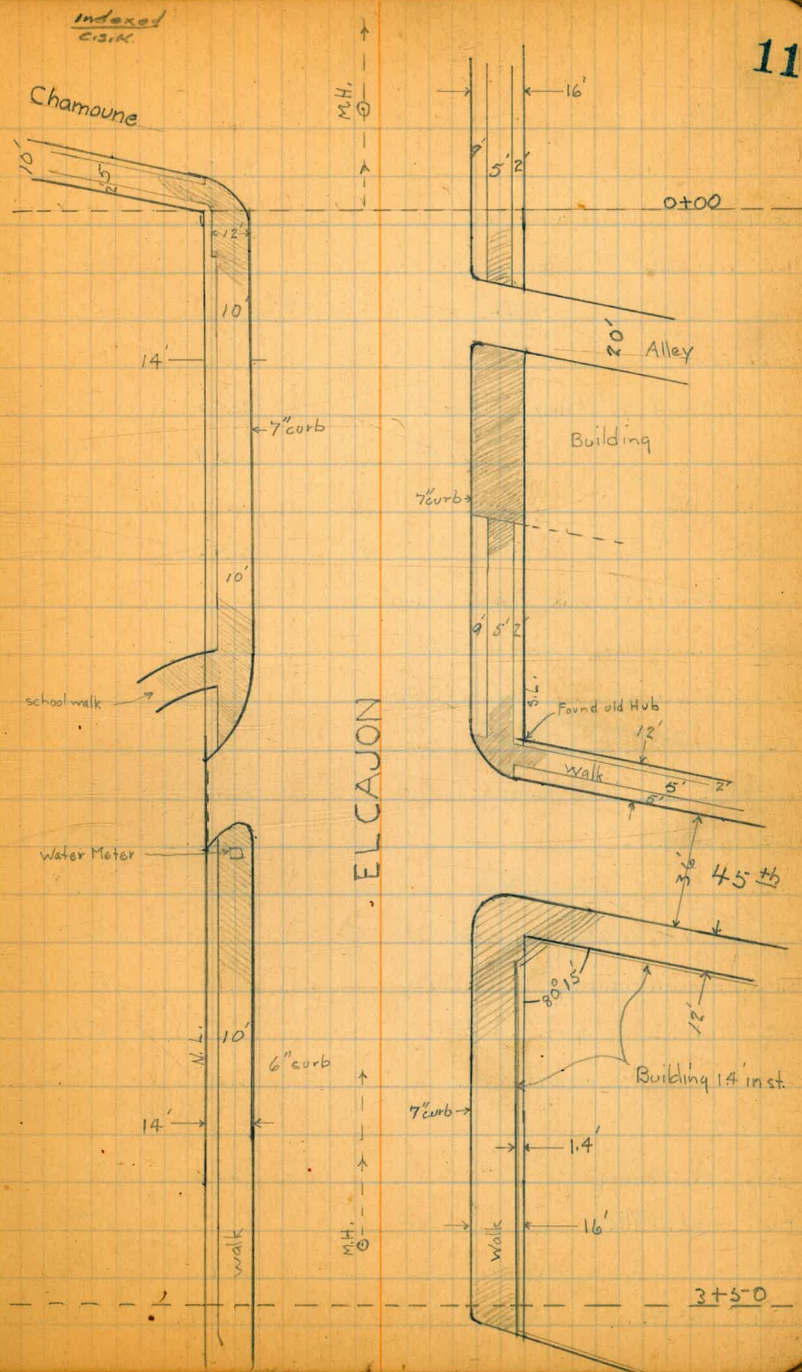
♀		7.57	370.48
♂		7.47	70.58
s.cb.	cut.	7.43	70.62
	top	6.93	71.12
N. edge walk		6.82	71.23
S. edge walk		6.66	71.39
2+53 = 6" Drainage outlet in s.cb.			
2+65.23 = W.L. of 38 th st.			
S. edge walk		6.79	71.26
N. " "		6.95	71.10
s.cb.	top	6.90	71.15
	cut	7.52	70.53
♂		7.59	70.46
♀		7.66	70.39
♂		8.27	69.78
N.cb.	cut.	8.09	68.96
	top	8.50	69.55
S. edge walk		8.34	69.71
N. " "		8.26	69.79
N.L. on dirt		8.00	70.05
31.3' E. of W.L. 38 th - 39.8' N. of S.cb. EL. Cajon = Drop M.H.			
	Rim	8.13	69.92
Flow line of 8" line from W.M.H. at Alley + 38 th			
		15.76	362. ²⁹ ₃₂
F.L. of E+W. Line on EL. Cajon + E.M.H. " " "			
		16.67	361. ³⁸ ₄₁

X Sections for traffic tunnel on El Cajon

Between W.L. Chamoune + E.L. Highland N. of EL Cajon

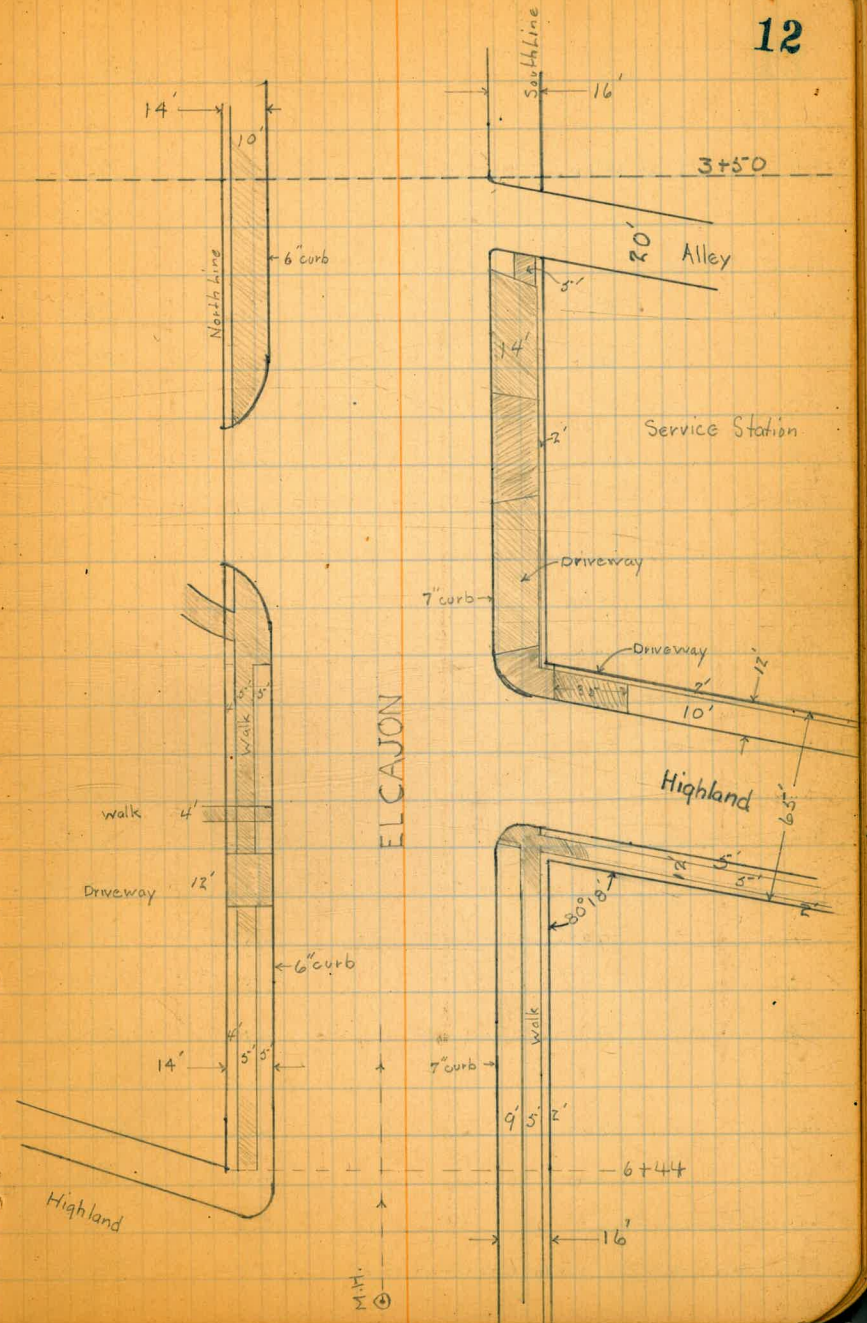
14' cb on N.

EL Cajon = 100' st. 70' Roadway	17.5'	1/4 S. 16' cb	
0+00 = line at right angle to N.L. EL Cajon at N.W. prop. cor.			
EL Cajon + Chamoune	H. I.	sw. BR EL Cajon + Chamoune	
B.M. +743	364.01		356.58
16.8' E. of 0+00			
33.8' N. of S. cb EL Cajon = M.H. Rim	6.16	359.85	✓
flowline	22.73	41.28	✓
0+00			
N.L. EL Cajon on dirt	5.2	58.8	✓
+2' = edge of walk	4.97	59.04	✓
N. cb.	top	5.14	58.87
	cut.	5.22	58.19
1/4		5.93	58.08
1/4		6.08	57.93
1/4		6.50	57.51
s.cb.	cut	7.16	56.85
	top	6.44	57.57
+9 = N. edge walk		6.38	57.63
+14 = S. " "		6.26	57.75
S.L. on dirt		6.1	57.9
0+15.7 = PC. 2' Rad. Alley return			
S.h.		5.9	58.1
+2'		6.06	57.95
+7		6.15	57.86
s.cb.	top	6.29	57.92



36401

gut.	7.00	357.01	✓
0+17.0 = P.C. 2' Rad. Alley Ret.			
14.2' N. of S.L. top cb.	6.24	57.74	✓
gut.	6.92	57.09	✓
0+19.5			
± S.L. at E.L. of 20' Alley top cb.	6.06	57.95	✓
gut.	6.19	57.82	✓
14.2' N. of S.L.	6.90	57.11	✓
S. cb.	6.98	57.03	✓
0+21.3 = end of 12' walk start of 10' walk			
2' S. of N.L. = edge of walk	5.07	58.94	✓
0+24.5 = 1.6' N. of S.L. = Water Valve			
0+29.5			
N.L. on E. side of Alley paving	6.43	57.58	✓
14.2' N. of S.L.	6.78	57.23	✓
S. cb.	6.85	57.16	✓
0+37.1 = P.C. at 2' Rad. Alley ret.			
S.L. on paving	6.10	57.91	✓
14.2' N. of S.L. gut. - at P.C.	6.63	57.38	✓
top cb.	6.00	58.01	✓
0+38.7			
S.L. on paving	6.06	57.95	✓
+6 = W.L. Alley in gut.	6.66	57.35	✓
top cb.	5.95	58.06	✓
S. cb. at P.C. top cb.	6.09	57.92	✓



	gut.	36401 ✓	6.76	357.25 ✓
0+39.6				
S.L. at W.L. of Alley	top cb.		5.92	58.09 ✓
	gut.		5.92	58.09 ✓
+13.5 = Pole				
S.cb.	top		6.08	57.93 ✓
	gut.		6.77	57.24 ✓
$\frac{1}{4}$			6.44	57.57 ✓
$\frac{1}{4}$			6.01	58.00 ✓
$\frac{1}{4}$			5.91	58.10 ✓
N. cb.	gut.		6.01	58.00 ✓
	top		5.74	58.67 ✓
+10 = N. edge of walk			5.02	58.99 ✓
N.L. on dirt			5.1	58.9 ✓
1+00				
N.L.			5.5	58.5 ✓
+4 = N. edge of walk			5.52	58.49 ✓
N. cb.	top		5.72	58.29 ✓
	gut.		6.33	57.68 ✓
$\frac{1}{4}$			6.06	57.95 ✓
$\frac{1}{4}$			6.02	57.99 ✓
$\frac{1}{4}$			6.43	57.58 ✓
S.cb.	gut.		6.22	57.19 ✓
	top		6.85 ?	57.16 ✓
+14 = S. edge of walk			6.20	57.81 ✓
S.L. on concrete apron in front of store			5.94	58.07 ✓

364.01 ✓

14

1+00.3

S. cb. line at W. end of Walk in front of store

1+03.2

S.L.	at W. " " " " " " " "	5.93	358.08 ✓
+2 =	S. edge of walk	6.21	57.80 ✓
+7 =	M. " " "	6.23	57.78 ✓
S. cb.	top	6.27	57.74 ✓
	gut	6.24	57.17 ✓

1+37

1.5' N. of N. cb. = Fire Hydrant

1+39.8

S.L.		6.4	57.6 ✓	
+2 =	walk	6.24	57.77 ✓	
+7 =	"	6.26	57.75 ✓	
S. cb.	top	6.43	57.58 ✓	
	gut.	6.98	57.03 ✓	
$\frac{1}{4}$		6.38	57.63 ✓	
$\frac{1}{2}$		6.10	57.91 ✓	
$\frac{3}{4}$		6.13	57.88 ✓	
N. cb. =	P.C. at Ret. to school driveway	gut.	6.48	57.53 ✓
		top	5.90	58.11 ✓
+10 =	N. edge walk + E. edge of 12' walk to school	5.80	58.21 ✓	
N.L.		5.9	58.1 ✓	
1+41.3				
N.L. =	E. edge of school walk	5.76	58.25 ✓	

364.01 ✓

15

1+50

N.L.	on walk	5.79	358.22 ✓
+4	= Edge of walk on El Cajon	5.82	58.19 ✓
+13.1	= cb.	5.90	58.11 ✓
	top	6.54	57.47 ✓
	cut.	6.56	57.45 ✓
N. cb.		6.18	57.83 ✓
$\frac{1}{4}$		6.11	57.90 ✓
$\frac{1}{4}$		6.44	57.57 ✓
S. cb.	cut.	7.01	57.00 ✓
	top	6.50	57.51 ✓
+9	= edge walk	6.32	57.69 ✓
+14	= " "	6.23	57.78 ✓
S.L.		6.2	57.8 ✓

+5-2.2

4' S. of N.L. = W. edge school walk

1+54.3

N.L.	= " " " "	5.81	58.20 ✓
+4	= edge walk	5.83	58.18 ✓
+11.8	= cb.	5.88	58.13 ✓
	top	6.49	57.52 ✓
	cut	6.62	57.39 ✓

1+56.1

45.5 N. of S.L. = Water Valve

1+58.8

18.5 S. of N.L. = Water Valve

1+65-

1.5 s. of S. cb. = Pole

1+65.6

4' s. of N.L. N. edge of walk meets curb on return ^{top} 5.86 57.15 ✓

gut. 6.37 57.64 ✓

1+65.8

S.L. 6.4 57.6 ✓

+2 6.23 57.78 ✓

+7 6.35 57.66 ✓

S. cb. at P.C. of return top 6.54 57.47 ✓

gut. 7.00 57.01 ✓

1/4 6.42 57.59 ✓

1/2 6.12 57.83 ✓

3/4 6.30 57.71 ✓

N. cb. 5.56 58.45 ✓

+ 10.1 = cb. on ret. gut. 6.38 57.63 ✓

top 5.87 58.14 ✓

N.L. 5.9 58.1 ✓

1+66.4R

S.L. = 1 Prop. Hub on E.L. 45th = S.E. Prop. Cor. El. Cajon + 45th

1+68.5-

S.L. = E. edge of walk on E. side of 45th 6.26 57.75 ✓

1+71.7

N.L. = cb. on ret. top 5.83 58.18 ✓

gut 6.43 57.58 ✓

364.01 ✓

17

1+73.6

S.L. = W. edge walk on E. side 45th 6.38 357.63 ✓

+2 = edge of walk in return 6.40 57.61 ✓

+13.6 = cb on ret. top 6.58 57.43 ✓

gut 7.04 56.97 ✓

S. cb. line 7.05 56.96 ✓

1+77.2

7.8' N. of S.L. = P.C. of return. 10' rad. topcb. 6.54 57.47 ✓

gut 7.09 56.92 ✓

1+78.8

N.L. on paving in school drive 6.39 57.62 ✓

N. cb. 6.66 57.35 ✓

7 6.33 57.68 ✓

8 6.28 57.73 ✓

6 6.40 57.61 ✓

S. cb. 6.93 57.08 ✓

S.L. = E. cb. of 45th gut. 7.20 56.81 ✓

top 6.56 57.45 ✓

1+94

N.L. on paving 6.39 57.62 ✓

+9' S. = Easterly Point of W. ret. of drive gut 6.52 57.49 ✓

topcb. 6.04 57.97 ✓

N. cb. 6.73 57.28 ✓

1+97

S.L. = 8 45th 6.71 57.30 ✓

S. cb. 6.61 57.40 ✓

$\frac{1}{4}$		6.44	357.57 ✓
$\frac{1}{4}$		6.31	57.70 ✓
$\frac{1}{4}$		6.44	57.57 ✓
N. cb. = P.C. of return to drive	gut.	6.74	57.27 ✓
	top	6.14	57.87 ✓
+10 = edge walk		5.94	58.07 ✓
+13 = top cb. on return		5.86	58.15 ✓
	gut.	6.32	57.69 ✓
W.L.		6.33	57.68 ✓
2+00			
2' S. of N.L. = $\frac{1}{4}$ 1'x1' concrete box holding a Water Valve.			
11' S. of N.L. = $\frac{1}{4}$ of 6'x5' concrete meter box - 6' ^{wide} along El Cajon			
6" pipe + 2 meters	top of pipe	9.34	54.67 ✓
	Bottom of box	10.33	53.68 ✓
12.8 S. of N.L. = Water Valve			
2+14.6			
4.7' N. of S.L. = P.C. of return 10' rad. top cb.		6.74	57.27 ✓
	gut	7.32	56.69 ✓
2+15.2			
S.L. = W. cb. of 45' \pm	top cb.	6.77	57.24 ✓
	gut.	7.42	56.59 ✓
+12.6 = cb. on ret.	top.	6.72	57.29 ✓
	gut	7.26	56.75 ✓
s. cb.		7.22	56.79 ✓
$\frac{1}{4}$		6.54	57.42 ✓

364.01 ✓

19

E		6.46	357.55 ✓
$\frac{1}{4}$		6.51	57.50 ✓
N.cb.	gut.	6.77	57.24 ✓
	top	6.14	57.87 ✓
+10 = edge of walk		5.97	58.04 ✓
N.L.		5.9	58.1 ✓
2+24			
N.L.		6.0	58.0 ✓
+4 = edge of walk		6.01	58.00 ✓
N.cb.	top	6.17	57.84 ✓
	gut.	6.83	57.18 ✓
$\frac{1}{4}$		6.58	57.43 ✓
E		6.43	57.58 ✓
$\frac{1}{4}$		6.70	57.31 ✓
S.cb.	gut.	7.22	56.79 ✓
	top	6.73	57.28 ✓
S.L.		6.52	57.49 ✓
2+25.3			
1.5' S. of S.cb. = Pole			
2+31.3			
S.L. on doorway of Bldg.			
2+32.1			
1.4' N. of S.L. = edge of Building - on walk		6.52	57.49 ✓
S.cb.	top	6.82	57.19 ✓
	gut.	7.26	56.75 ✓

364.01 ✓

T.P.		6.74	357.27 ✓
	+ 5.14		362.41 ✓
2:50			
1.4' N. of S.L. = edge of Bldg. - on walk		4.94	357.47 ✓
S. cb.	top	5.23	57.18 ✓
	gut	5.70	56.71 ✓
$\frac{1}{4}$		5.23	57.18 ✓
E		4.94	57.47 ✓
$\frac{1}{4}$		5.07	57.34 ✓
N. cb	gut.	5.38	57.03 ✓
	top	4.71	57.70 ✓
+ 10 = edge of walk		4.60	57.81 ✓
N.L.		4.6	57.8 ✓
3:00			
N.L.		4.8	57.6 ✓
+ 4 = edge walk		4.74	57.67 ✓
N. cb.	top cb.	4.95	57.46 ✓
	gut.	5.60	56.81 ✓
$\frac{1}{4}$		5.22	57.19 ✓
E		5.15	57.26 ✓
$\frac{1}{4}$		5.34	57.07 ✓
S. cb	gut	5.84	56.57 ✓
	top	5.42	56.99 ✓
+ 14.6 = edge of bldg.		5.10	57.31 ✓

$$\begin{array}{r} 364.01 \\ - 6.74 \\ \hline 357.27 \\ + 5.14 \\ \hline 362.41 \end{array}$$

20

36.241 ✓

3+33.4

50' S. of N.L. = M.H. Rim	5.21	357.20 ✓
Flow Line	22.38	40.03 ✓

³
2+50

1.4' N. of S.L.	5.38	57.03 ✓
S. cb. - P.C. Alley ret. ^{2' Rad.} top	5.53	56.88 ✓
cut	5.90	56.51 ✓

$\frac{1}{4}$	5.56	56.85 ✓
---------------	------	---------

E	5.16	57.25 ✓
---	------	---------

$\frac{1}{4}$	5.38	57.03 ✓
---------------	------	---------

N. cb	cut	5.83	56.58 ✓
-------	-----	------	---------

top	5.10	57.31 ✓
-----	------	---------

+10 = edge of walk	4.85	57.56 ✓
--------------------	------	---------

N.L.	4.9	57.5 ✓
------	-----	--------

3+51.8

14.6' N. of S.L. = P.C. of 2' Rad. Alley ret. top cb.	5.52	56.89 ✓
---	------	---------

cut.	5.84	56.57 ✓
------	------	---------

3+54.

S.L. = E.L. 20' Alley = Wedge of Bldg. top cb. + cut.	5.50	56.91 ✓
---	------	---------

14.6' N. of S.L.	5.85	56.56 ✓
------------------	------	---------

S. cb.	5.89	56.52 ✓
--------	------	---------

3+65.4

S.L. = E. of Alley paving	5.72	56.69 ✓
---------------------------	------	---------

S. cb.	5.90	56.51 ✓
--------	------	---------

21

362.41 ✓

22

3+72

15.9' N. of S.L. = P.C. 2' Rad. Alley ret.	top cb.	5.60	356.81 ✓
	gut.	5.88	56.53 ✓

3+73.5

S.L.		5.49	56.92 ✓
------	--	------	---------

+ 8.6' N. = cb line of Alley	gut.	5.75	56.66 ✓
	top cb.	5.52	56.89 ✓

S. cb. = P.C. of Alley ret.	top	5.60	56.81 ✓
	gut.	5.94	56.47 ✓

3+74

2.5' S. of S. cb. = Pole

3+75.5

N.L.		5.2	57.2 ✓
------	--	-----	--------

+ 4 = edge of walk		4.99	57.42 ✓
--------------------	--	------	---------

N. cb	top	5.21	57.20 ✓
-------	-----	------	---------

	gut	5.88	56.53 ✓
--	-----	------	---------

$\frac{1}{4}$		5.47	56.94 ✓
---------------	--	------	---------

$\frac{1}{2}$		5.27	57.14 ✓
---------------	--	------	---------

$\frac{1}{4}$		5.55	56.86 ✓
---------------	--	------	---------

S. cb.	gut	5.95	56.46 ✓
--------	-----	------	---------

	top	5.60	56.81 ✓
--	-----	------	---------

+ 9 = edge of walk		5.41	57.00 ✓
--------------------	--	------	---------

+ 14 = " " "		5.30	57.11 ✓
--------------	--	------	---------

S.L. = W.L. Alley	top cb.	5.39	57.02 ✓
-------------------	---------	------	---------

	gut.	5.49	56.92 ✓
--	------	------	---------

356.14

T.P. on bench Sw. BR. EL. Cajon + Highland		6.28	356.13 ✓
--	--	------	----------

+ 5.43 361.57 ✓

3+78.3

S.L. 4.2 357.4 ✓

+2 = edge of walk 4.49 359.08 ✓

+2 = " " 4.59 361.98 ✓

S.cb. = E. end of driveway to Gas Station top 4.72 366.85 ✓

gut 5.12 366.45 ✓

3+83.7

7 N. of S.L. E. edge of driveway + edge of walk 4.64 366.93 ✓

S.cb. on paving 5.13 366.44 ✓

3+86.8

2' N. of S.L. = E. edge. drive + edge of walk 4.56 367.01 ✓

S.cb. 5.13 366.44 ✓

4+07.5

S.L. 4.6 369.0 ✓

+2 = S. edge of driveway 4.67 366.90 ✓

S.cb. 5.27 366.30 ✓

1/4 4.78 366.79 ✓

1/4 4.57 369.00 ✓

1/4 4.75 366.82 ✓

N.cb. = P.C. of curved ret. to school drive gut 5.22 366.35 ✓

top 4.56 367.01 ✓

+10 = edge walk 4.36 367.21 ✓

N.L. 4.4 367.2 ✓

4+15.2

N.L.		4.4	357.2	✓
4' S. of N.L. = edge walk		4.36	57.21	✓
12.6' S. " " = cb. on ret.	top	4.55	57.02	✓
	gut.	5.17	56.40	✓
N. cb.		5.22	57.35	✓
2' N. of S.L. = edge of driveway		4.68	56.89	✓
S. cb. = W. et end of driveway	top cb.	4.93	56.64	✓
	gut.	5.26	56.31	✓
4+21.4				
S.L.		4.6	57.0	✓
+ 2' N. of S.L. = Back edge of walk	driveway W. end of	4.71	56.86	✓
S. cb.	top	4.93	56.64	✓
	gut.	5.29	56.28	✓
4+25.2				
4' S. of N.L. = edge of walk meets curb on ret.	top cb.	4.48	57.09	✓
	gut.	4.97	56.60	✓
N. cb.		5.21	56.36	✓
4+27.				
N.L. = cb. on return	top cb.	4.50	57.07	✓
	gut.	4.94	56.63	✓
N. cb.		5.23	56.34	✓
4+34				
5.2' S. of S. cb. = Inlet pipe for Gas tanks for Service Station				
4+42.6				
3.9' S. of S. cb. = Inlet pipe	" " " " "			

361.57 ✓

25

4+50

N.L. on paving - school drive 5.19 356.38 ✓

N. cb. 5.34 56.23 ✓

+ 4 4.86 56.71 ✓

9 4.68 56.89 ✓

+ 4 4.91 56.66 ✓

S. cb. gut. 5.40 56.17 ✓

top 5.05 56.52 ✓

+4 = Inlet pipe for Gas tank.

+14 = edge of walk 4.86 56.71 ✓

S.L. 4.9 56.7 ✓

4+60.2

S.L. 4.8 56.8 ✓

+2' N. of S.L. edge of walk + E. end of driveway 4.92 56.65 ✓

S. cb. top 5.09 56.48 ✓

gut. 5.43 56.14 ✓

4+65.5

S.L. 4.9 56.7 ✓

+2 edge of driveway 4.91 56.64 ✓

S. cb. top 5.09 56.48 ✓

gut. in driveway 5.42 56.15 ✓

4+69.6

N.L. = cb. on ret. to school drive top cb. 4.81 56.76 ✓

N. cb. gut. 5.28 56.29 ✓

N. cb. 5.43 56.14 ✓

361.57 ✓

26

4+73			
N.L.	4.7	356.9 ✓	
+4' - edge of walk meets cb. on ret.	4.84	56.73 ✓	
	gut.	5.30	56.27 ✓
N. cb.	5.43	56.14 ✓	
4+86.7			
N.L. = E. edge of 12' Curved walk to school	4.64	56.93 ✓	
+4' S. = edge of walk	4.76	56.81 ✓	
T.P. on bench SW cor. Highland			
4+88.5 + 5.00	361.14 ✓	356.14	
S.L.	4.4	356.7 ✓	
+2 = 1 edge of drive way	4.49	56.65 ✓	
S.cb. = in drive way	5.07	56.07 ✓	
‡	4.58	56.56 ✓	
‡	4.39	56.75 ✓	
‡	4.58	56.56 ✓	
N. cb. = P.C. of curved ret. to school drive - gut.	5.12	56.02 ✓	
Fire Hydrant	top	4.47	56.67 ✓
+1.4	Fire Hydrant		
+10 = edge of walk + E. edge of curved walk	4.31	56.83 ✓	
N.L. on walk	4.20	56.94 ✓	
4+91.3			
45.8' N. of S.L. = Water Valve			
4+95.57			
2' N. of S.L. edge of walk + W. end of driveway	4.50	56.64 ✓	
S. cb.	5.08	56.06 ✓	

4+99.5

N.L. = W. edge of curved walk.		4.18	356.96 ✓
N. cb.	top	4.48	56.66 ✓
	gut	5.17	55.97 ✓

5+00.5

N.L.		4.3	56.8 ✓
+2.4 = W. edge of red walk		4.23	56.91 ✓
N. cb.	top	4.51	56.63 ✓
	gut.	5.16	55.98 ✓

 $\frac{1}{7}$

4.64 56.50 ✓

 $\frac{1}{4}$

4.46 56.64 ✓

 $\frac{1}{7}$

4.59 56.55 ✓

S. cb. = P.C. of return	gut	5.09	56.05 ✓
	top	4.71	56.43 ✓

+14 = edge of walk 4.49 56.65 ✓

S.L. 4.8 56.6 ✓

5+01.1

N.L. 4.3 56.8 ✓

+4 S. = edge of walk + W. edge of sch. walk 4.28 58.66 ✓

N. cb. top 4.51 56.63 ✓

gut. 5.17 55.97 ✓

5+02.9

E. side of Highland

2' N. of S.L. = edge of walk + E. edge of walk on 4.48 56.66 ✓

5+09.4

N.L. 3.4 57.7 ✓

+4 = edge of walk.		4.29	356.85 ✓
+9 = edge of 5' walk from here West.		4.39	56.75 ✓
N. cb.	top	4.53	56.61 ✓
	gut.	5.16	55.98 ✓
S.L.		4.58	56.56 ✓
13.2' N. of S.L. = cb. on ret.	top	4.71	56.43 ✓
	gut.	5.15	55.99 ✓
S. cb.		5.12	56.02 ✓
5+12			
1.8' N. of N. cb. = Pole			
5713			
3.2' N. of S.L. = PC. of ret.	this ret. apparently has no regular Radius		
	top cb.	4.70	56.44 ✓
	gut.	5.20	55.94 ✓
5+13.7			
# S.L. = E. cb. line of Highland	top	4.69	56.45 ✓
	gut.	5.26	55.84 ✓
S. cb.		5.01	56.13 ✓
$\frac{1}{4}$		4.61	56.53 ✓
$\frac{1}{2}$		4.47	56.67 ✓
$\frac{3}{4}$		4.66	56.48 ✓
N. cb.	gut.	5.19	55.95 ✓
	top	4.54	56.60 ✓
+5' = edge of walk		4.40	56.74 ✓
+10 = " " "		4.28	56.86 ✓

N.L.		3.6	359.5 ✓
5+14			
2.5' N. of N.cb. = water Meter.			
5+12.3			
2.6.3' S. of N.L. = Water Valve			
5+34.5			
N.L.		3.6	52.5 ✓
+4 = edge of walk		4.37	56.77 ✓
+9 " " "		4.51	56.63 ✓
N.cb.	top	4.68	56.46 ✓
	gut.	5.29	55.85 ✓
$\frac{1}{4}$		4.67	56.47 ✓
E		4.62	56.52 ✓
$\frac{1}{4}$		4.69	56.45 ✓
S.cb.		4.75	56.39 ✓
S.L. = E of roadway of Highland		4.79	56.35 ✓
5+54			
7.9' N. of S.L. = PC. of return	top cb.	4.94	56.20 ✓
	gut.	5.52	55.62 ✓
5+55.5			
S.L. = W. cb. line of Highland	top	5.04	56.10 ✓
	gut	5.64	55.50 ✓
+13.7 = cb. on ret.	top	4.93	56.21 ✓
	gut.	5.44	55.70 ✓
S.cb.		5.47	55.67 ✓

Note: Highland has 41' roadway

No regular Rad.

361.14 ✓

30

1/4		4.84	356.30 ✓
1/2		4.80	56.34 ✓
1/4		4.82	56.32 ✓
N. cb. = E 4' walk to house	gut.	5.38	55.76 ✓
	top	4.76	56.38 ✓
+10 = edge of req. walk		4.54	56.60 ✓
N.L. on walk		3.96	57.18 ✓
Shots on cb. lines of Highland to show drainage			
50' s. of S.L. on E. cb.	top	5.00	56.14 ✓
	gut.	5.76	55.38 ✓
50' s. of S.L. on W. cb.	top	5.18	55.96 ✓
	gut.	5.83	55.31 ✓
T.P. on bench		5.00	356.14 ✓
+ 5.18			361.32 ✓
5+60.3			
S.L. = edge of walk on Highland.			
5+62.6			
N.L.		4.2	57.1 ✓
+4 = edge of walk		4.77	56.55 ✓
+9 = " " "		4.90	56.42 ✓
N. cb.	top	4.95	56.37 ✓
	gut.	5.56	55.76 ✓
1/4		5.06	56.26 ✓
1/2		4.88	56.44 ✓
1/4		5.10	56.22 ✓

361.32 ✓

S.cb. PC. of return	gut.	5.66	355.66 ✓
	top	5.18	56.14 ✓
S.L.		5.08	56.24 ✓
5+65.6			
S.L. = edge of walk on Highland.		5.06	56.26 ✓
+2 = edge of walk on EL Cajon		5.03	56.29 ✓
+7 = " " " " " "		5.09	56.23 ✓
S.cb.	top	5.18	56.14 ✓
	gut	5.66	55.66 ✓
5+67			
N.cb. = E. end of driveway			
5+67.5			
1.7' S. of S.cb. = Pole			
5+78.3			
N.cb. = W. end of driveway			
6+00			
S.L.		4.6	56.7 ✓
+2 = edge walk		5.16	56.16 ✓
+7 " "		5.27	56.05 ✓
S.cb.	top	5.34	55.98 ✓
	gut	5.80	55.52 ✓
$\frac{1}{4}$		5.30	56.02 ✓
$\frac{1}{2}$		5.10	56.22 ✓
$\frac{3}{4}$		5.23	56.09 ✓
N.cb.	gut	5.72	55.60 ✓

31

361.32 ✓

	top	5.14	356.18 ✓
+5 = edge of walk		4.99	356.33 ✓
+10 = " " "		4.81	356.41 ✓
N.L.		3.6	359.7 ✓
6+38			
3' S. of S.cb. = 3" tree			
6+41			
N.L.		4.7	356.6 ✓
+4 = edge walk		5.04	356.28 ✓
+9 = " "		5.12	356.20 ✓
N.cb.	top	5.26	356.06 ✓
	gut.	5.90	355.42 ✓
$\frac{1}{4}$		5.41	355.91 ✓
$\frac{1}{2}$		5.13	356.19 ✓
$\frac{3}{4}$		5.31	356.01 ✓
S.cb.	gut	5.84	355.48 ✓
	top	5.52	355.80 ✓
+9 = edge of walk		5.27	356.05 ✓
+14 = " " "		5.24	356.08 ✓
S.L.		4.5	356.8 ✓
6+44			
N.L. = E. Line of Highland			
6+82.6			
50' N. of S.L. = M.H.	flow line	18.50	42.82

32

Shots to show drainage on 45th st. S. of EL. Cajon

50' S. of S.L. EL. Cajon on E. cb. 45 th	top cb.	EL.	357.07
	gut.		356.39
50' S. of S.L. EL. Cajon on W. cb. 45 th	top cb.		356.88
	gut.		356.20

Herbert Hoover
"TUNNEL CONST."

33

North side Int. Tunnel And Stairway = 0 + 00	362.76	Flow Line Grade	Cuts	
+40	16.01	346.75	346.20	+0.55
top step stairway on north.	17.47	345.29	345.80	-0.51
	4.55	358.21	358.23	-0.02

B.M. C.T. in Walk 357.77
 4.97
 362.76 = X
 2.31 -
 = 360.45
 360.46 = B.M.
 0.01 = Error.

Additional Grades

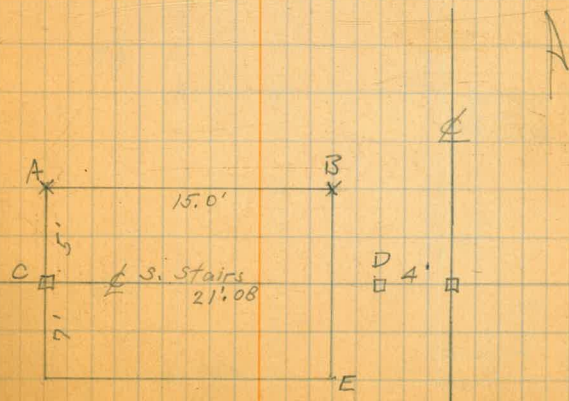
North Stairs top step	363.35	5.12	358.23	358.23	
" " S.T. "	17.03	346.32	346.23		
" " L. Tunnel			346.20		
South Stairs	11.15	352.20	346.20		+6.00

360.46 = B.M.
 2.89 +
 363.35 = X

raised to fit tunnel

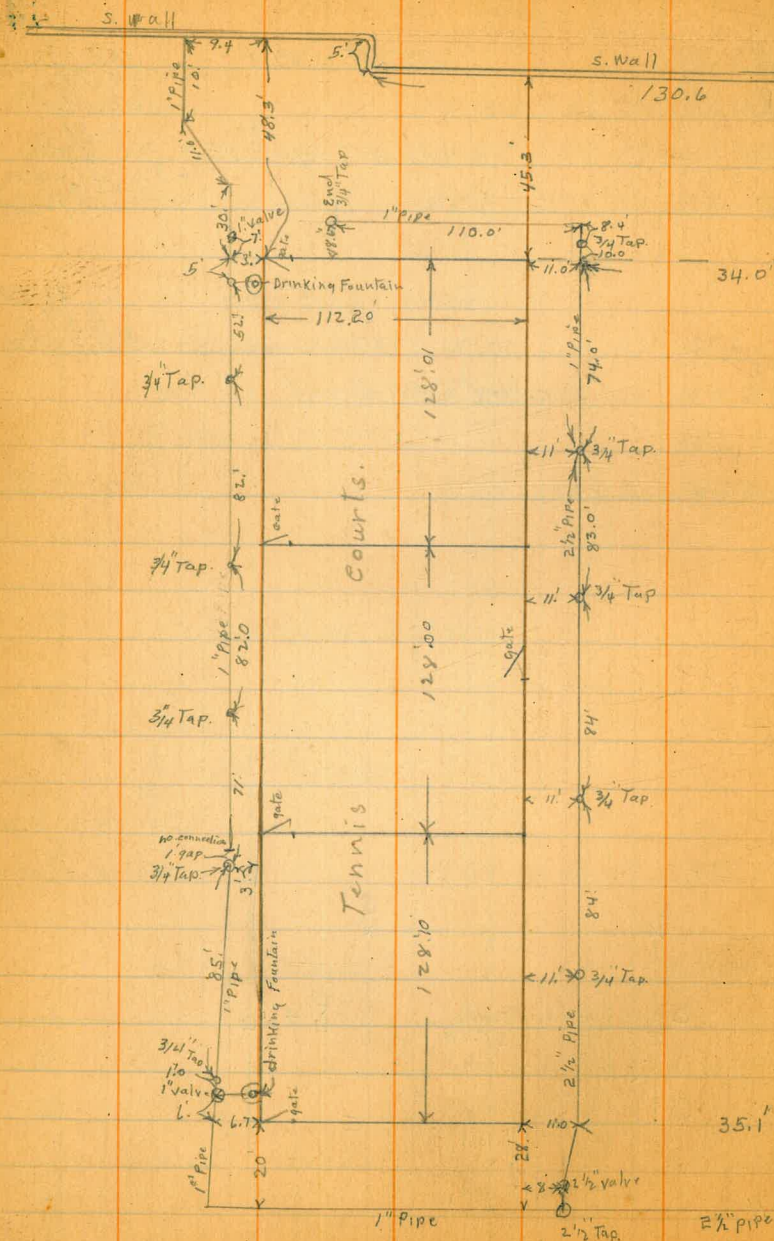
Additional Grades

B.M. C. Tin walk			357.77		
+ 1.03	358.80				
South side int. & Tunnel & S. Stairs	12.63	346.17	346.17		
1.35	359.12		B.M. 357.77		
D	12.92	346.20	Gr = 346.20		
B	1.46	357.66	Gr = 357.70	F. 0.04'	
E	1.39	357.72	Gr = 357.70	C. 0.02'	
4.55	362.32		B.M. 357.77		
A	4.73	357.59	Gr = 357.70	F. 0.11'	
C	4.66	357.66	Gr = 357.70	F. 0.04'	



Indian

Village



Location of Tennis
Courts & water system.
S. of Indian Village
W. of Park Blvd.

Walker
2.15.32

WOODROW WILSON SEWER AND
"TUNNEL CONST"

	6.23	379.73		373.50	BM. B.P. 51/67 37th and El Cajon Top Fire Hyd. McClintock & El Cajon.
T.P.	2.61	377.72	4.62	375.11	
Rim M.H. at McClintock St.	4.91	372.81			
Flow line 2 M.H.	"	"	11.69	366.03	
Rim M.H. 38th St.	7.80	369.92			
Flow line MH 38th St.	16.31	361.41			

Construction notes for Sewer

	+	x	-	Elev. of siders	Flow Line Grades	Cuts	offsets	McClintock & El Cajon. B.M. Fire Hyd.	375.11 3.62+ 378.13=x
Existing MH. McClintock St. = 0+00		378.13			366.03				
+16.8 Break.			5.45	372.68	365.87	+6.81			
+26.8 Break.			5.55	372.58	362.48	+10.07			
+30.8 = 1/2 Tunnel (out)					362.46				
+50.2			5.76	372.37	362.38	+9.99			
+75.2			5.99	372.14	362.28	+9.86			
+100.2			6.21	371.92	362.18	+9.74			
+125.2			6.39	371.74	362.08	+9.66			
+150.2			6.72	371.41	361.98	+9.43			
+175.2			6.90	371.23	361.88	+9.35			
+200.2			7.12	371.01	361.78	+9.23			
+225.2			7.29	370.84	361.68	+9.16			
+250.2			7.53	370.60	361.58	+9.02			
+275.2			7.81	370.32	361.50	+8.82			
+300.2 = MH 38th					361.41				
					361.38 - plus				

Walker
4-15-32

TUNNEL GRADES
Woodrow Wilson Jr. Hgh

3.14 378.25 375.11 8M

Grades Tunnel
Flow Line

A = 10' West Wood stairs Elev. for top step	5.18	373.07	372.96	+0.17
B = Elev. for top step	5.41	372.84	372.96	-0.12
C = Elev. Tunnel Elev.	5.86	372.39	363.91	+8.48
D = Elev. for Flow Tunnel	5.46	372.79	363.71	+9.08
E = Elev. for Flow Tunnel	5.21	373.04	363.71	+9.33
F = Elev. for top step	5.55	372.70	372.75	-0.05
G = Elev. for top step	5.67	372.58	372.75	-0.17
H = Elev. Roadway (not 2.0')			363.22	
I = cut to flow line tunnel	5.97	372.28	363.91	+8.37

3.18 378.29 375.11

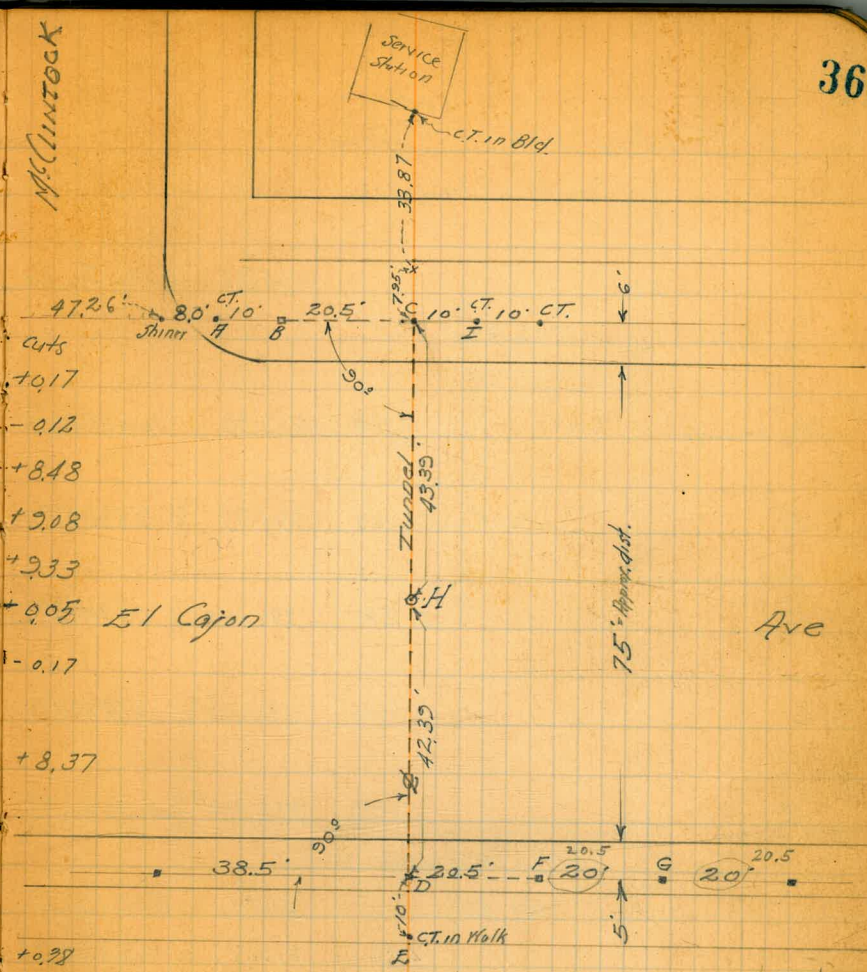
D	14.58	363.71	363.71	
H	14.69	363.60	363.22	+0.28

Pierce 6-9-32

2.48 377.59 B.M. 375.11

3'S. of C	13.73	363.86		
H	6.15	371.44	363.40	C. 8.04
	14.19	363.40	Fl. at eas built	

McClintock



12.57 126.4
- 3.86
12.69

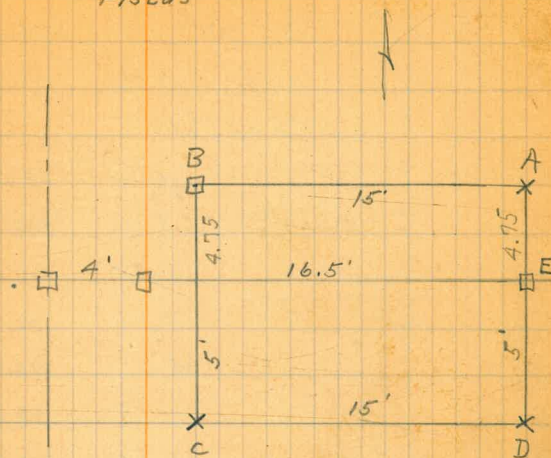
Woodrow Wilson Tunnel
South Stairway

June 4, 1932

Pierce
Hatch
Fiscus

37

	3.31		375.11	B.M. Top F.H.	
		378.42			
A on curb	5.70	372.92	Top wall/373.39	F 0.67 = 8"	
B	6.69	371.73	373.39	F 1.66 = 1-7 $\frac{7}{8}$ "	
C	5.58	372.84	373.39	F 0.55 = 6 $\frac{5}{8}$ "	
D	5.60	372.82	373.39	F 0.57 = 6 $\frac{7}{8}$ "	
E.	5.72	372.70	Top step 372.75	F 0.05 = $\frac{5}{8}$ "	

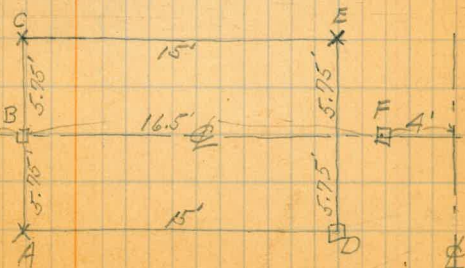


North Stairway

June 28, 1932

Pierce
McCarty

	2.42	377.53	375.11	B.M. Top F.H.	
A	4.07	372.96	Top Wall 373.43	F 0.67 = 8" ✓	
B	4.48	373.05	Top step 372.96	C 0.09 = 1 $\frac{1}{8}$ " ✓	
C	4.64	372.89	373.43	F 0.54 = 6 $\frac{1}{2}$ " ✓	
D	5.78	371.95	373.43	F 1.68 = 1-8 $\frac{1}{2}$ " ✓	
E	4.81	372.72	373.43	F 0.71 = 8 $\frac{1}{2}$ " ✓	
F	14.40	363.13	363.96	F 0.83 = 10" ✓	



Cross Section Alley Block 19 Normal Heights
 From Collier to Copley
 Between Mansfield + 35th St.

9-7-32
 Moore
 6380
 Halpin
 38

BM	5.60	396.97	391.37	528.84 Collier + M. Van
TP	4.63	398.01	354	393.43

H.Cb of Collier

H.E. Cor. Mansfield Paving	4.64	393.42	
Top Cb	4.14	393.92	
H.L. Alley	4.59	393.47	
H.L. Ground	5.2	92.9	
E.L.	5.1	93.0	
E.L. Top Cb	4.52	393.54	
H.X. Cor. 35th St. Paving	5.50	392.56	
Top Cb	5.03	393.03	

Plotted #18 9-12-32

15' S of H.L. Collier - N. Edge Cor. Mansfield + E. Cb

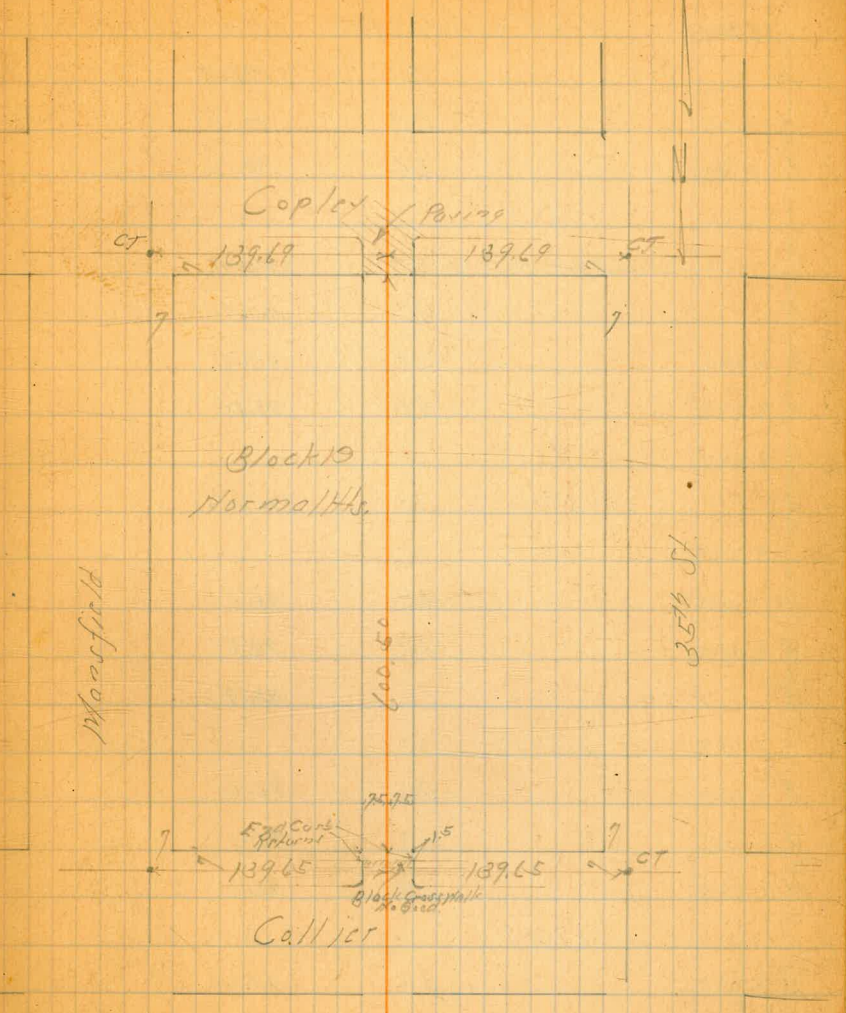
E	Top Cb + Ground	4.20	393.86
L		4.4	93.7
H	Top Cb	4.34	393.72

H.L. Collier

H		4.0	94.1
L		4.1	94.0
E		3.9	94.2

25' N of H.L. Collier

-1.5	2 1/2 Brick Chimney	2.9	95.2
E		2.9	95.2
L		2.8	95.3
H		2.8	95.3



Mansfield

35th St

398.06

50 ft of H.L. Collier

N	3.0	95.1
S	2.4	95.7
E	2.4	95.7

80 ft

3.5 W of Car. H. post to Garage	3.00	395.06
E	3.0	95.1
S	3.1	95.0
N	3.1	95.0

90 ft

2.5 E of E.L. = St. & Ribbon Dr.	3.00	395.06
----------------------------------	------	--------

100 ft

N	3.0	95.1
S	3.3	94.8
E - Fence	3.2	94.9

150 ft

E	3.1	95.0
S	3.0	95.1
N	2.9	95.2

175 ft

N	2.7	95.4
S	2.7	95.4
E	3.0	95.1

200 ft

E	3.2	94.9
S	2.8	95.3

398.06

H

2.7

395.4

250 ft

H

2.8

95.3

S

3.3

94.8

E

3.1

95.0

TP

5.02 400.81

2.27

395.79

300 ft

E

5.6

395.2

S

5.9

394.9

H

5.9

394.9

325 ft

H

6.0

394.8

S

5.9

394.9

E

5.9

394.9

350 ft

+1.5 - Fence

5.5

395.3

E

5.5

395.3

S

5.5

395.3

H

5.6

395.2

383 ft

H

5.7

395.1

S

5.6

395.2

+1.5 - St. Board Shed

5.4

395.4

403 ft

E

5.5

395.3

H - H.L. Board Shed

5.5

395.3

39

400.81

B	5.6	395.2
H	5.2	395.6
	425 H	
H	5.7	395.1
B	5.6	395.2
F - Fence	5.7	395.1
	457 H	
-1.5 = Garage Wood Floor	5.70	395.1
F	5.8	395.0
B	5.5	395.3
H	5.7	395.1
	500 H	
H	5.8	395.0
B	5.5	395.3
F - Fence	5.5	395.3
	526 H	
F	5.4	395.4
B	5.5	395.3
H	5.7	395.1
	557 H	
H	5.0	395.7
B	5.0	395.7
F - Edge Conc Apron	5.20	395.6
+4 = Garage Conc Floor	4.84	396.03

400.81

40

	575 H	
F	5.0	395.8
B	4.9	95.9
H	5.4	95.4
	595 H	
H	5.5	95.3
B	5.6	95.2
F	5.2	95.6
	600.50 H - JL Cap/ry	
F Top Ch	5.94	94.87
F on Pav/ry	6.13	94.68
B " "	6.30	94.51
H " "	6.06	94.75
H Top Ch	5.95	94.86
	S. Ch of Cap/ry	
H Top Ch	6.85	94.53
H on Pav/ry	6.56	94.25
B " "	6.59	94.27
F " "	6.63	94.18
F Top Ch	6.21	94.55
BM	5.95	394.86
	394.86	394.86

BP 52
Cap/ry +
Misc/ry
394.86

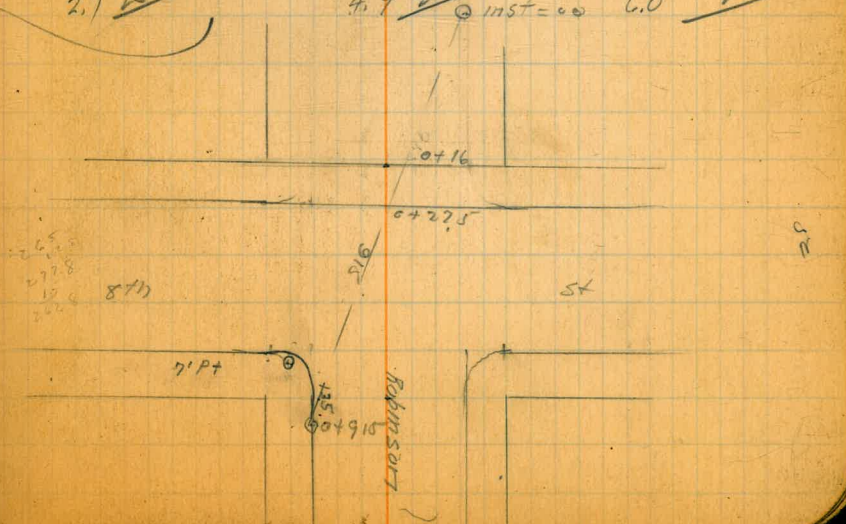
Levels 8th and Robinson
to

1/14/33
Brens
Harris
Phelps

41

Sta	+	HT	-	Elev	BM NW cor Robinson and 8th Plum curb
8-915	2.80				
0-27.5				4.46	273.29
0-16.0				4.32	273.43
0+00				1.20	276.55
S 12'				5.00	272.8
N 12'				0.72	277.1
0+25				4.8	273.0
0+50	0.67				-12.00
0+75	0.69				-11.55
1+00					
1+25					
1+34.9	Top Curb				
1+75					
1+85					
1+89					
2+00	+ 2.0	N 12' 257.6	1.3	254.3	S 12' 244.4
2+20	2.1	12.5 11.86	4.6	262.9	4.2 241.4
2+50	5.2	8.5 11.17	8.6	269.2	8.9 258.2
2+67	1.7	7th. l.	2.5	275.3	11.8 266.0
2+86			0.8	277.0	7.9 269.9
3+26	0.24	277.6	0.15	277.6	1.2 276.6
3+50	2.4	on walk to Gar.	1.7	276.1	5.6 272.2
3+75	4.8	279.0	5.4	272.4	9.1 268.7
4+00	6.2	271.6	7.5	270.3	12.8 265.0
4+20	4.8	273.0	10.9	266.9	15.0 252.8
			10.0	267.8	14.2 263.6
			14.8	263.0	

Sta	+	HT	-	Elev	BM NW cor Robinson and 8th Plum curb
1.8				276.0	
7.7				270.0	
7.2				FS. 12.00	
4.9				FS. 11.55	
14.0				250.7	
14.0				241.6	
14.9				240.7	
13.9				241.7	
				back of curb	
2.7				252.9	
4.8				273.0	
12.6				265.2	
9.2				7.7	
5.4				250.2	
14.2				241.4	
14.6				241.0	
14.5				241.1	
13.5				242.1	
4.9				250.7	
				inst = 00	
7.7				26.84	
16.4				26.1.4	
11.4				255.0	
6.9				248.7	
14.3				241.3	
14.7				240.9	
15.3				back of curb	
				240.3	
				on part	
6.0				249.6	



32

	N 1/2	E	S 1/2
4+40	$\frac{276.8}{+1.0 \text{ (B.S. 8.95)}}$	$\frac{275.4}{2.4 \text{ (F.S. 2.45)}}$	$\frac{269.4}{9.4}$
4+70	$\frac{279.1}{5.2}$	$\frac{277.8}{6.5}$	$\frac{277.8}{6.5}$
5+18	$\frac{279.9}{4.4}$	$\frac{279.8}{4.5}$	$\frac{279.9}{4.4}$
5+47.7	$\frac{280.9}{3.4}$ C6 27.7 Not d.	$\frac{280.64}{2.67}$ on Pav	$\frac{280.92}{3.39}$ on top of 10.3' 5.0' E

230 on B.M. SE Cor 10th + Robinson

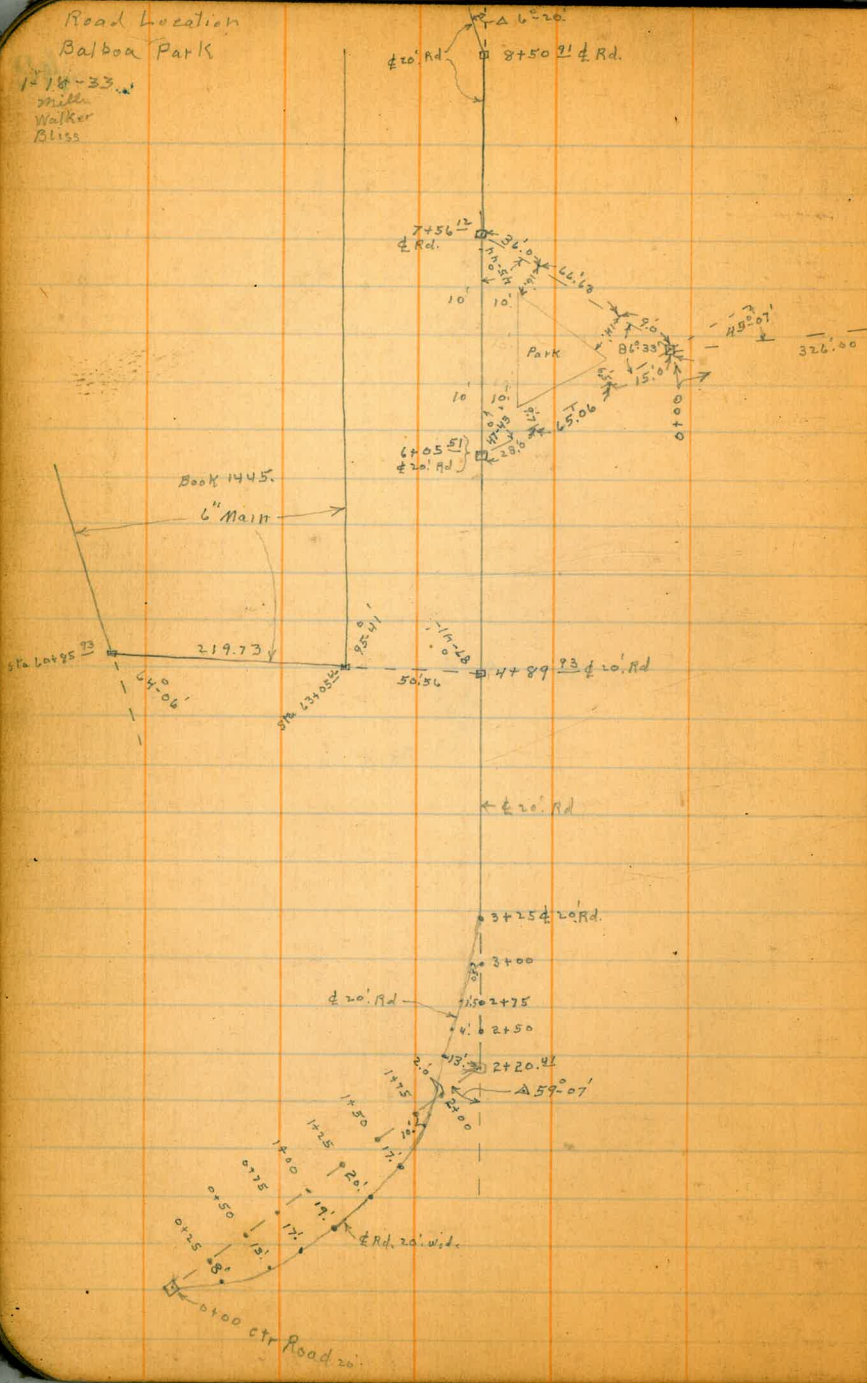
(287.01)

Garage $\frac{285}{-5}$ — Sta 4150

Garage
House
Cone
Porch
Sta 2486

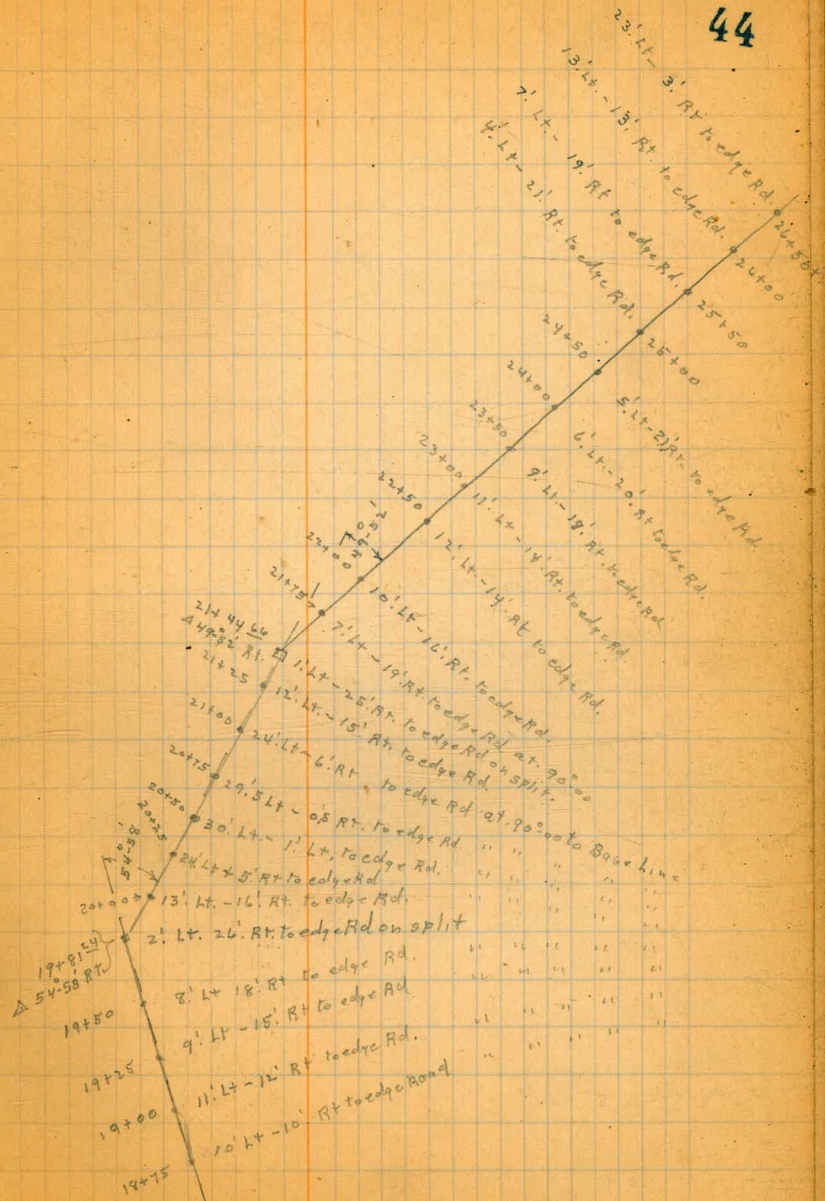
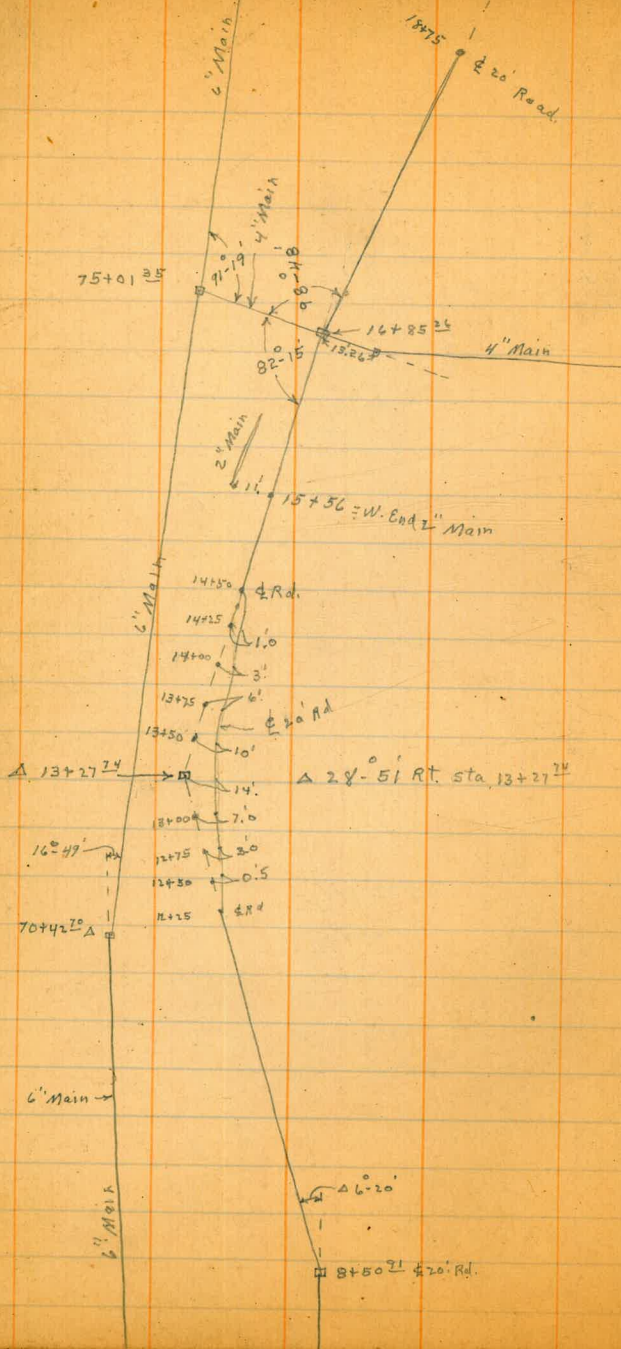
Road Location
Balboa Park

18-33
Miller
Walker
Bliss



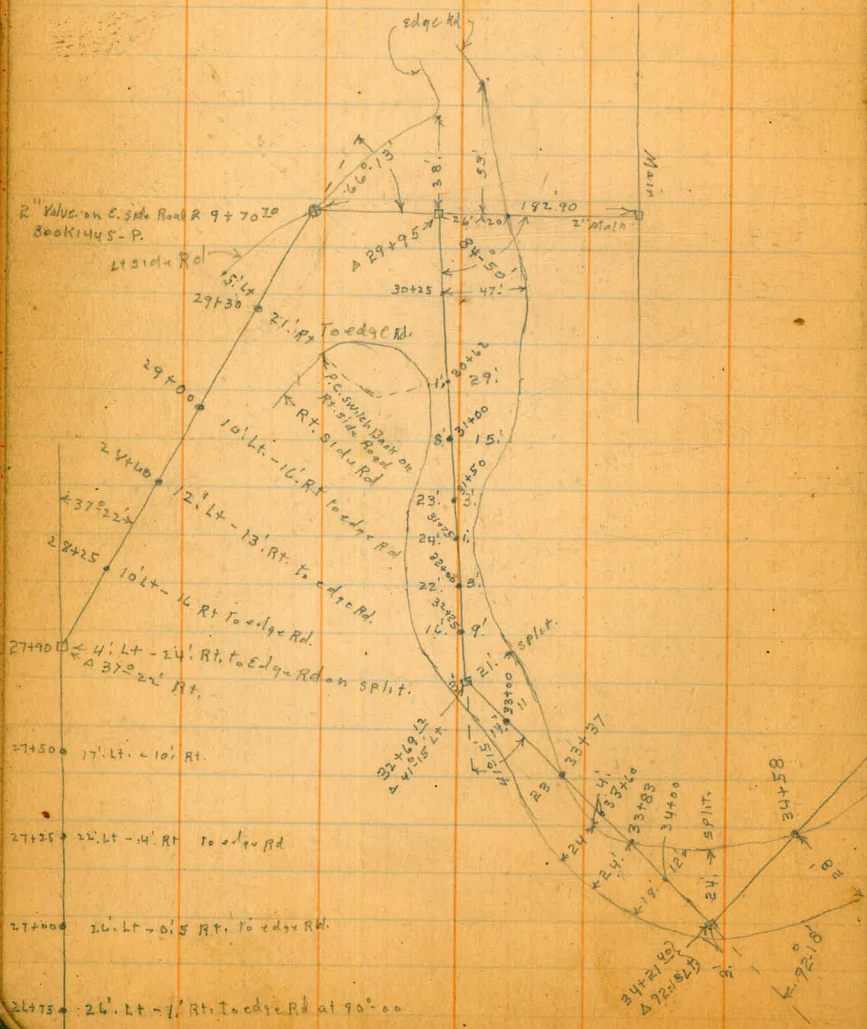
Road to 26th St.
Page 46

Creosote on Central Basin E. 2. 2. 2. 2. 2.

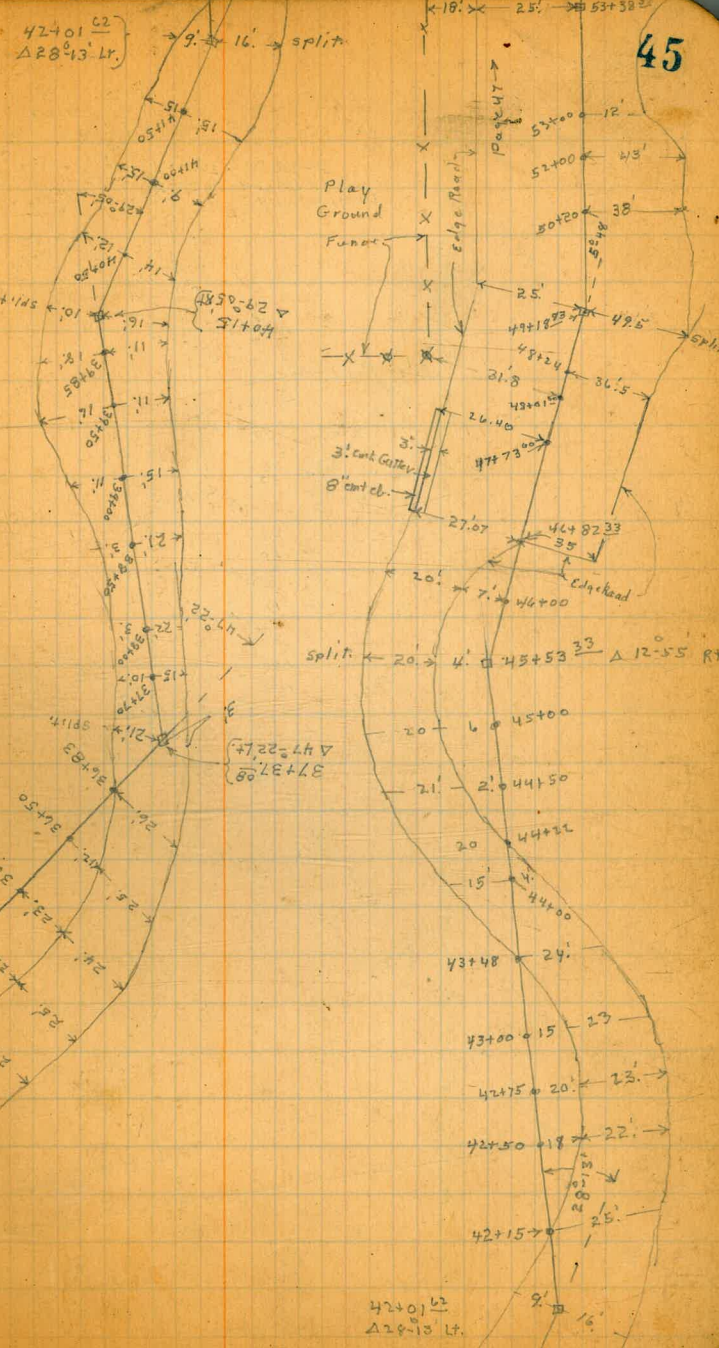


4553.33
129
4682.33
90.67
4773.00

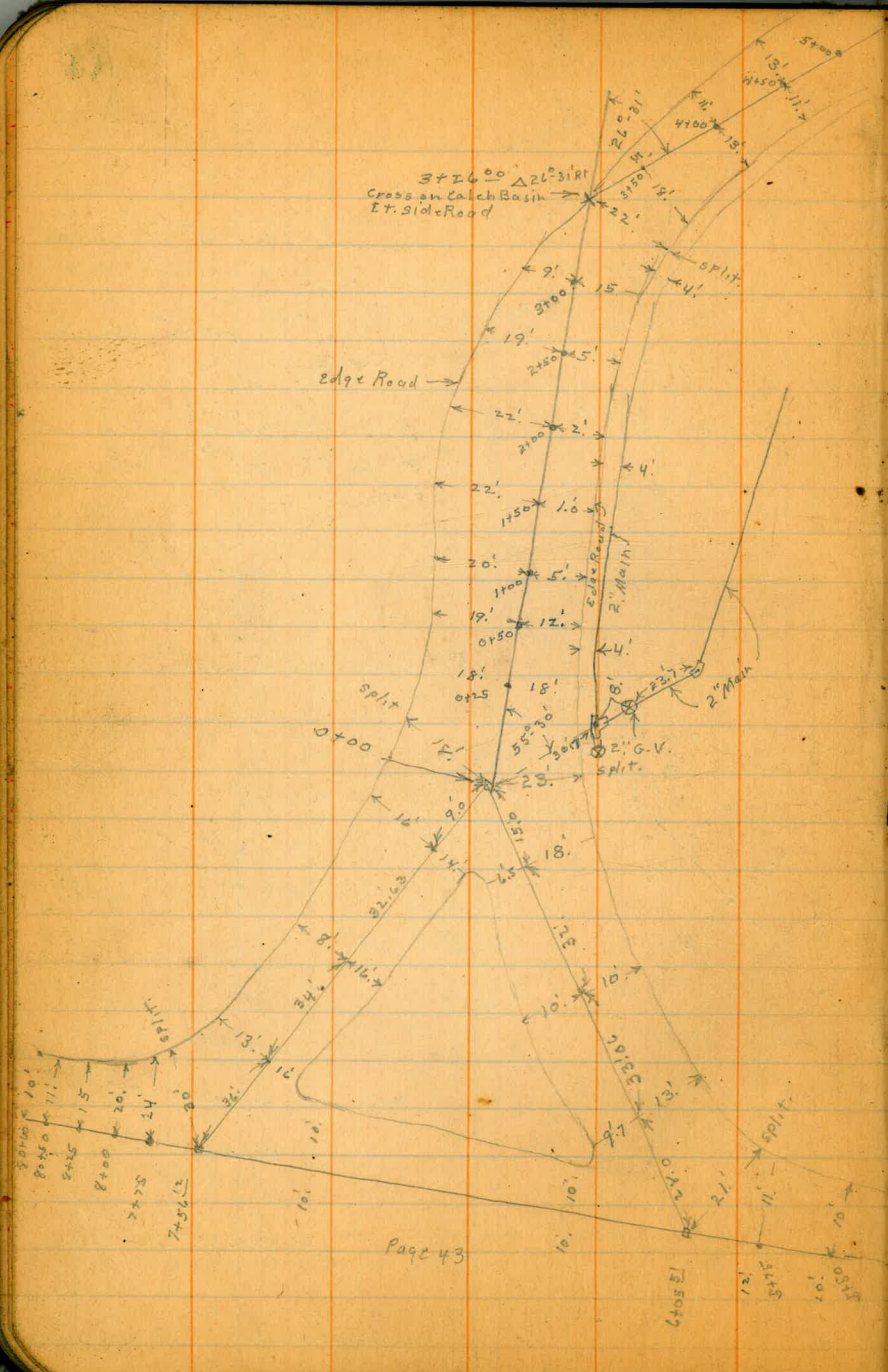
From Sta 29+70.20 to Sta 15+56
R" Main 1" to Lt. of Lt. Side of Road.



45

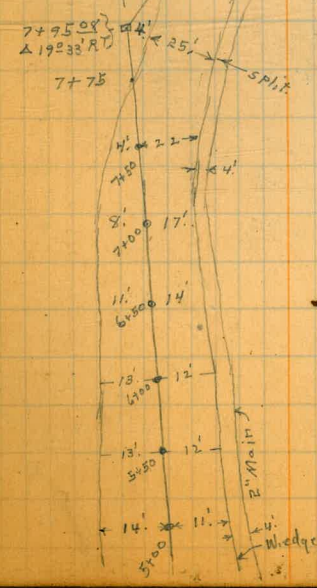


3+26⁰⁰ Δ26°31'RT
 Cross on Catch Basin
 Et. Side Road



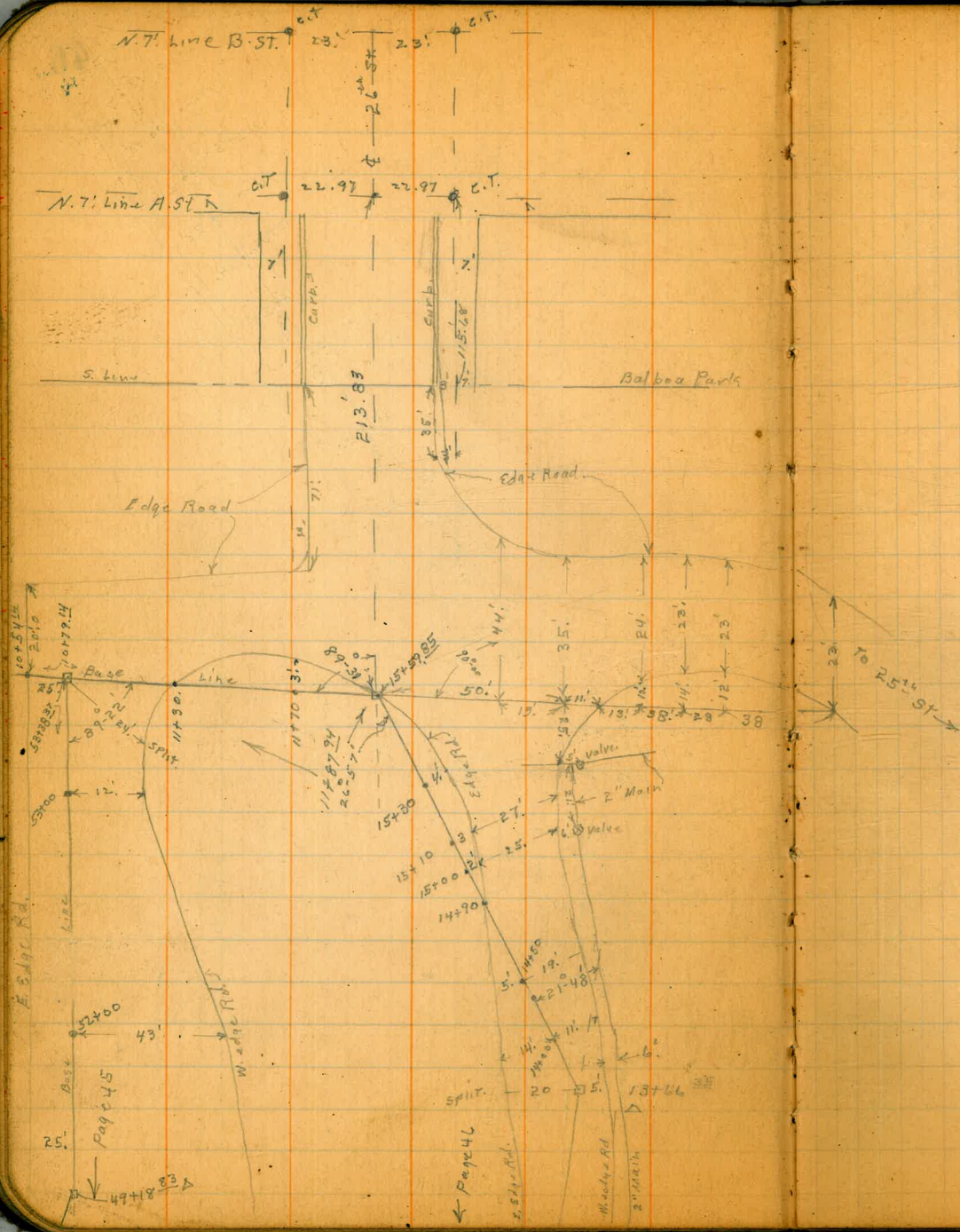
Page 43

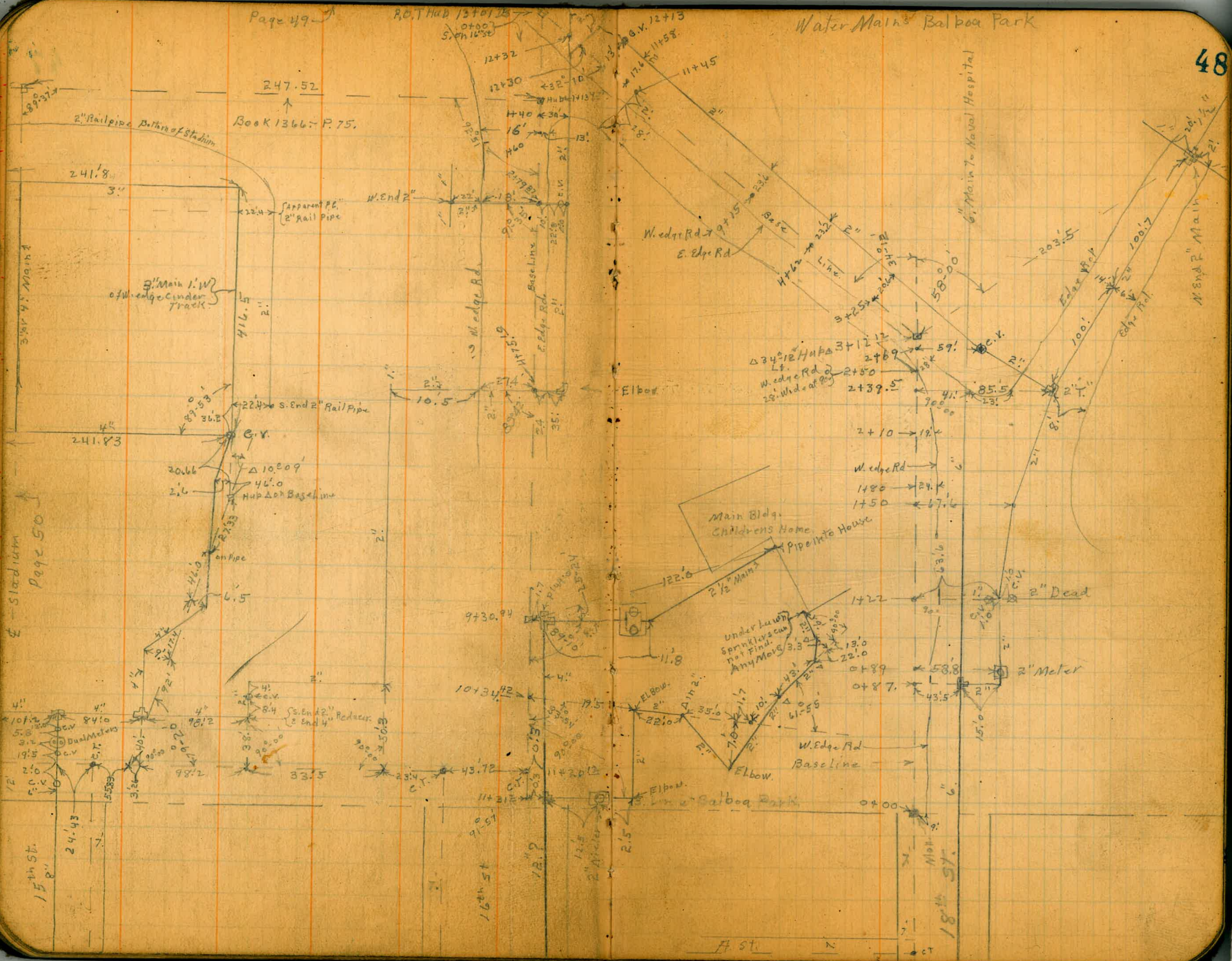
13766²⁵ Δ
 13450
 13000
 12+50
 11700
 11450
 20' 15"
 18' 7"
 15'
 14' 21"
 14' 23"
 14' 24"
 14' 25"
 14' 26"
 14' 27"
 14' 28"
 14' 29"
 14' 30"



47-22
44-41

120.03





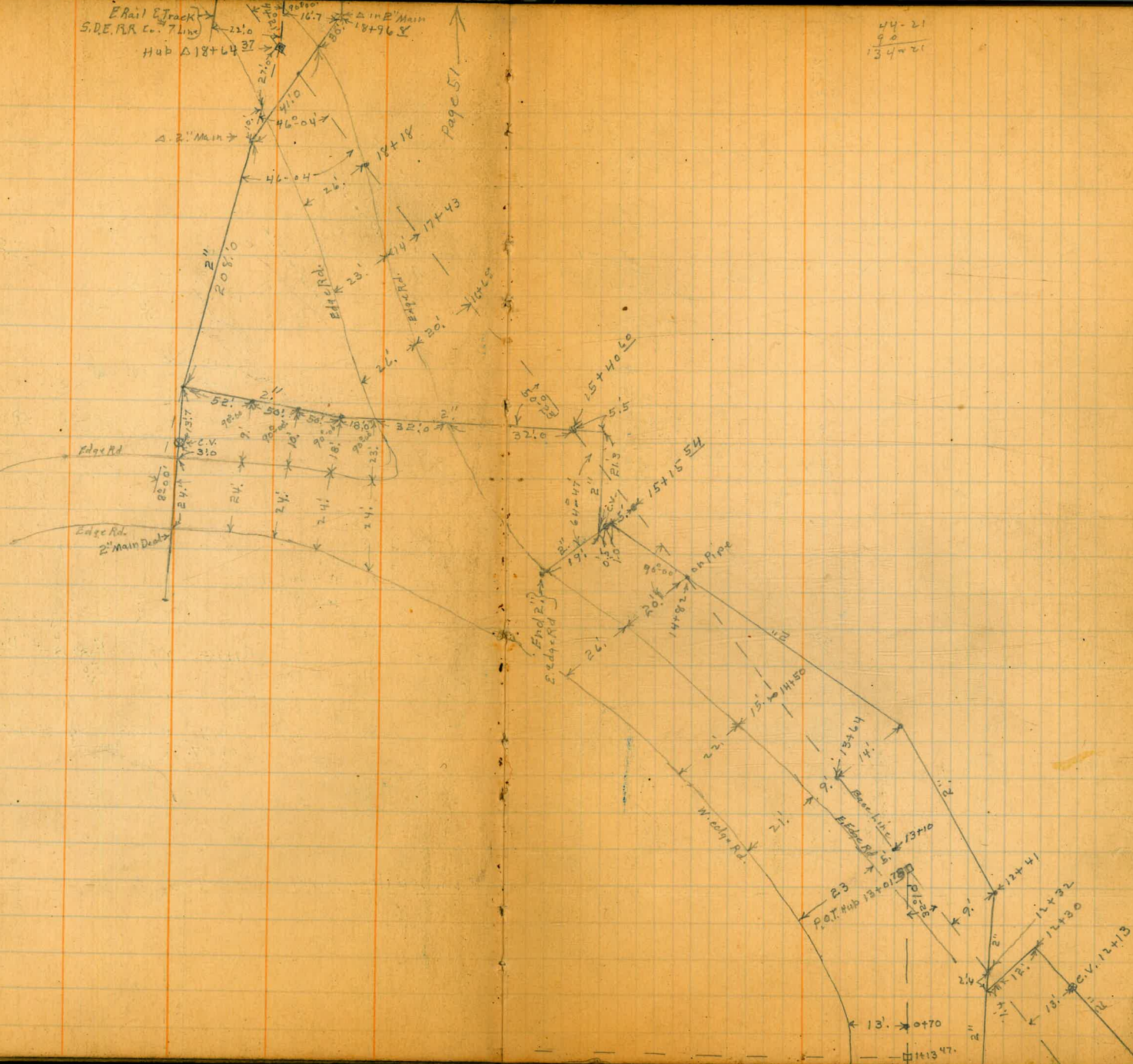
E Stadium Page 50

A ST

18th St

E Rail & Track
S.D.E. RR Co. 7 line
Hub Δ 18+64 37

44-21
90
134+21



To Lawn Sprinkler System

Meter Box Dual Meters

GGV

13th St

14th St

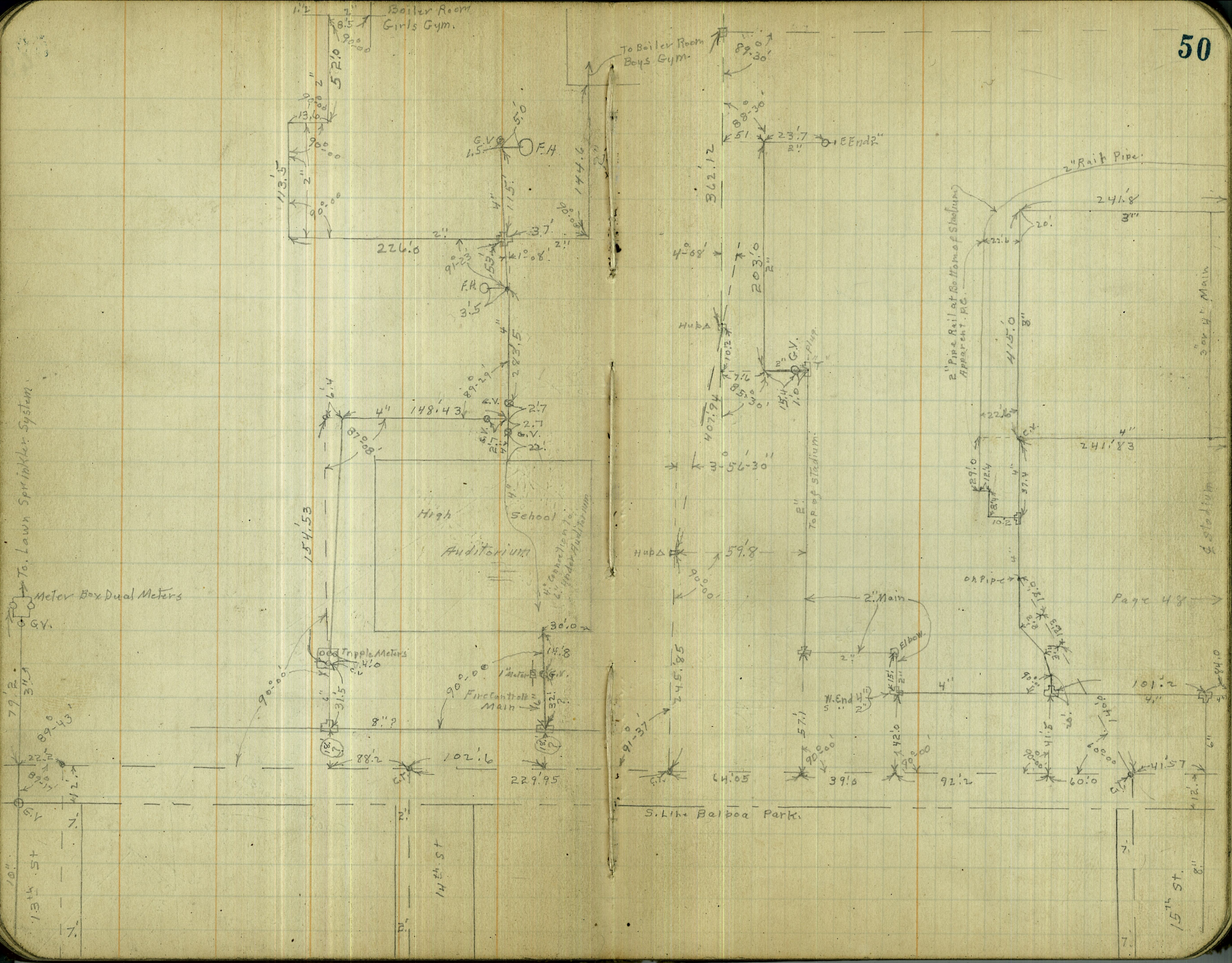
15th St

Boiler Room
Girls Gym.

To Boiler Room
Boys Gym.

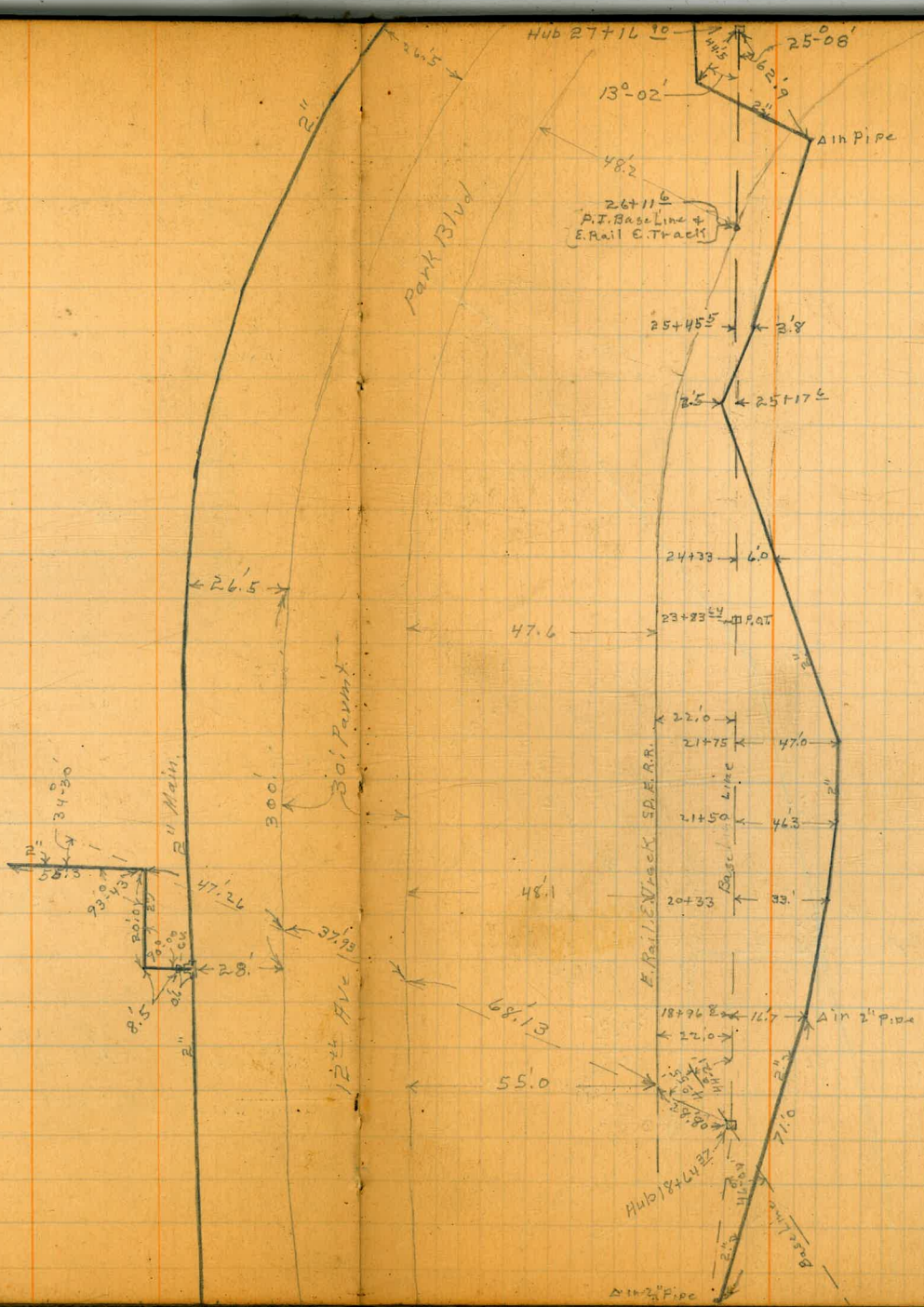
High School
Auditorium

S. L. the Balboa Park.



Page 48

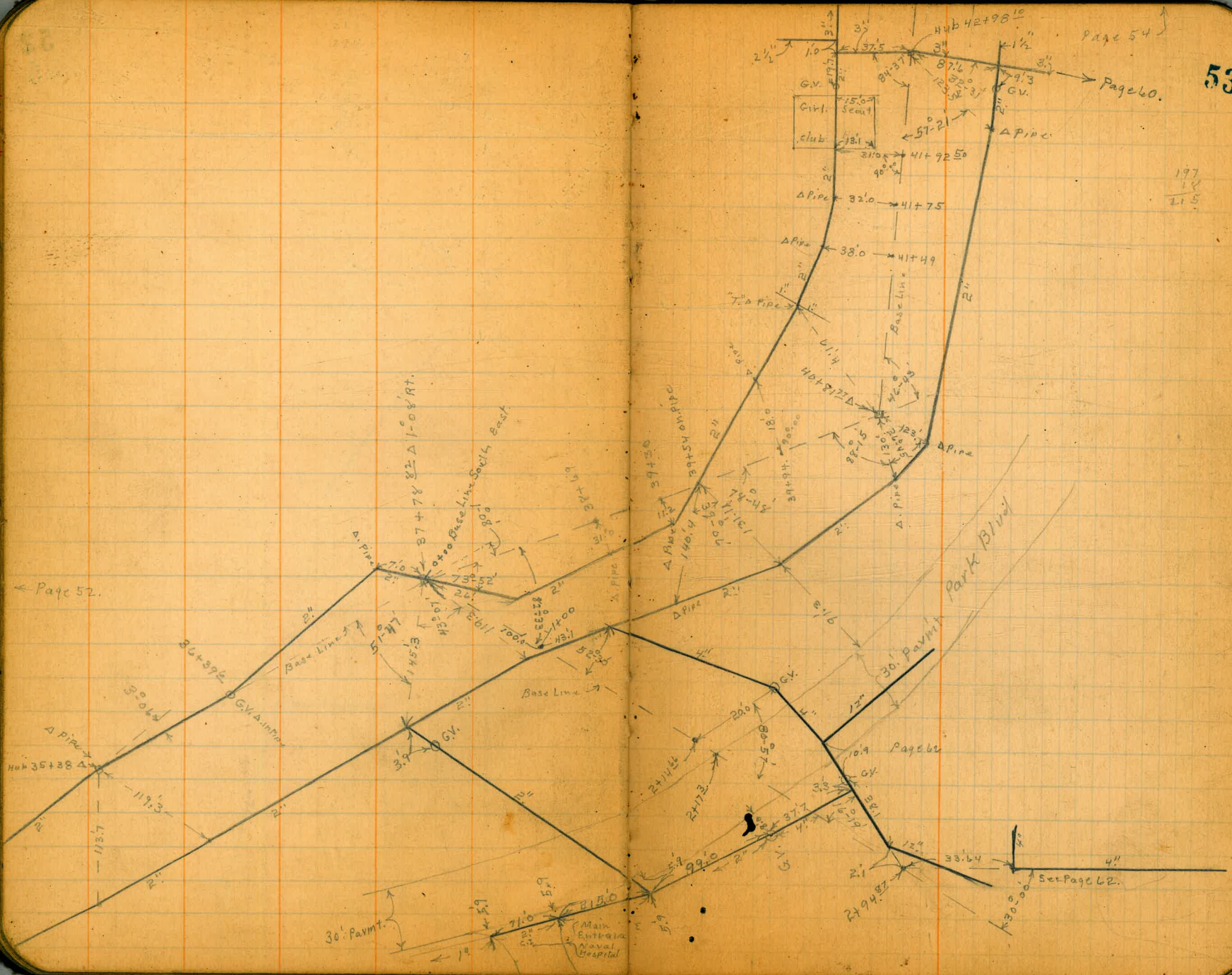
15th St



← Page 49

Page 54
Page 60

197
1.5
21.5



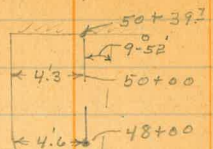
Book 1308-979

Laurel St.

c.T. in Pavmt.
51+89.7

51+37.7²² Δ Laurel
c.T. in Pavmt.

Pavmt.



Hub. 47+58.45 Δ 9.52 Lt.
on e. Edge Pavmt.

46+77.8²⁰
Edge Pavmt.

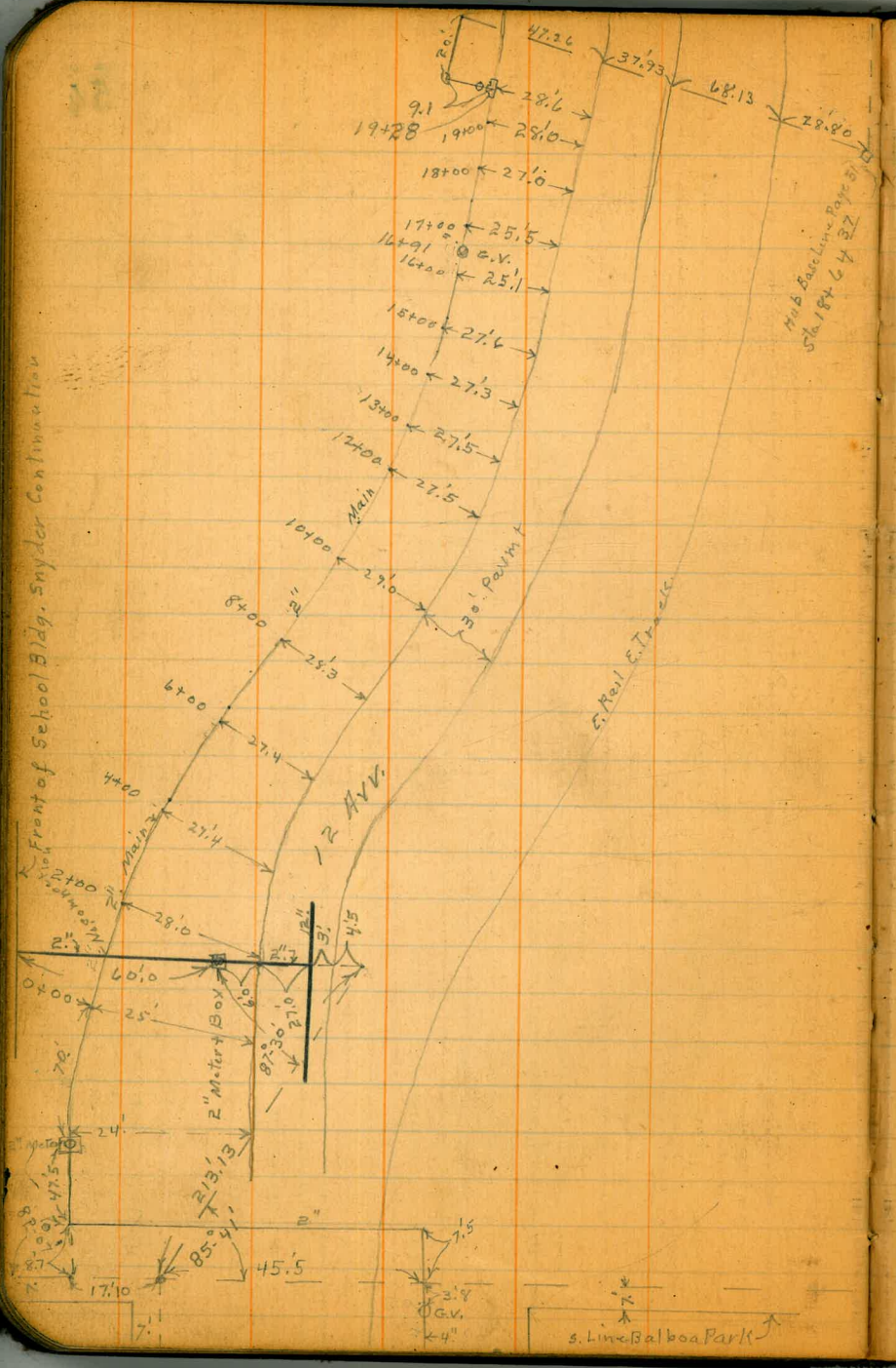


P.O.T. Hub 45+16.59

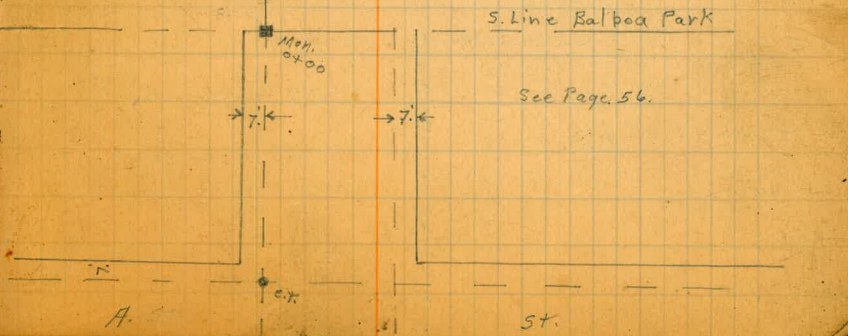
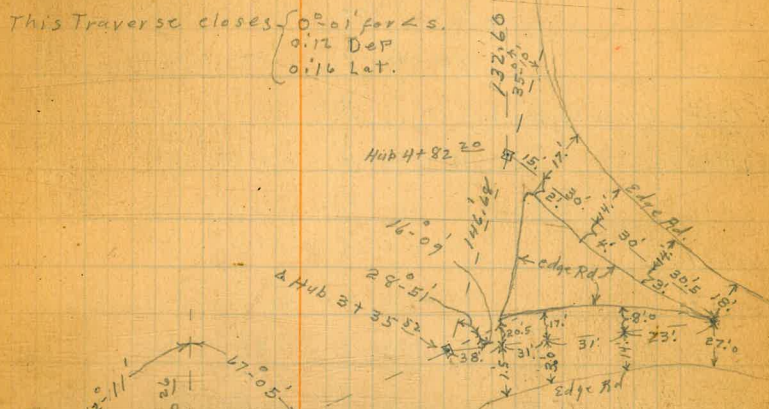
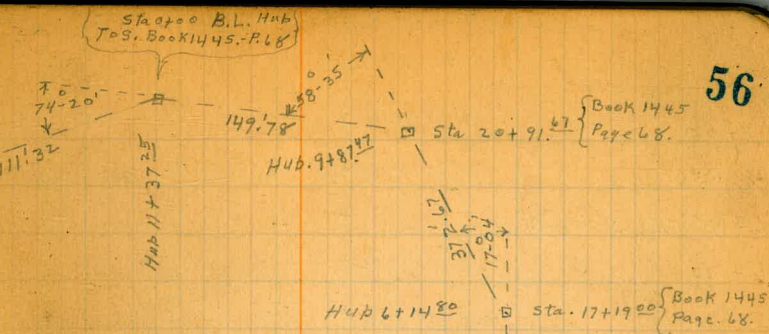
Base Line

Hub 42+98.10

Front of School Bldg. Snyder Continuation



4/6/33. Road Location Golden Hill Park.



Golden Hill Part A Road location

Base Line

7+00 5' Lt = W. edge • 16' Rt = E. edge
 6+50 12' Lt = W. edge • 9' Rt = E. edge
 6+14⁸⁰ Hub Δ 17-04' Lt. □
 6+10 16' Lt. W. edge • 3' Rt. E. edge
 5+70 11' Lt. W. edge • 8' Rt. E. edge
 5+30 11' Lt. W. edge • 12' Rt. = E. Edge
 4+90 13' Lt = W. edge • 17' Rt = E. edge
 4+82²⁰ Hub Δ 35-10' Lt. □
 4+70 12' Lt = W. edge • 8' Rt = E. edge
 4+40 7' Lt = W. edge 12' Rt. = E. edge.
 4+11 6' Lt = N.W. edge • 13' Rt = S.E. edge
 3+77 8' Lt N.W. edge • 12' Rt = S.E. Edge
 3+35⁵² Hub Δ 28-51' Lt. □
 3+30 15' Lt = N. edge • 8' Rt = S. edge
 2+90 7' Lt = N. edge • 12' Rt = S. edge
 2+35 B.L. = N. edge • 20' Rt = S. edge
 1+85 3' Rt = N. edge Rd.
 29' " = S. " "
 3' Rt = N. Edge Rd.
 35' " = S. "
 1+60
 1+41 Base line = N. edge
 1+15 12' B Lt = N. Edge •
 0+90
 0+85 Hub Δ 17-05' Rt. □
 0+68 13' Rt = W. Edge Road
 72' " = E " "
 13' Rt = W. side Road
 71' Rt = E " "
 18' Rt = W. cont. of N. End.
 73' Rt = E. cont. of N. End.

57

15+10 8' Lt = S. edge • 12' Rt. = N. edge
 14+79¹⁷ Δ 52-32' Rt. 1' Lt = S. edge • 19' Rt = N. edge < split.
 14+50 13' Lt = S.E. edge • 8' Rt = N.W. edge
 14+20 18' Lt = E. edge • 2' Rt = W. edge
 13+70 17' Lt = E. edge • 3' Rt = W. edge
 12+80 4' Lt = E. edge • 14' Rt = W. edge.
 12+48⁵⁷ Δ 16-20' Lt. □
 12+40 B.L. = E. edge • 20' Rt = W. edge Rd.
 12+10 • 2' Rt = S. E. edge 22' Rt = N.W. edge
 11+87 B.L. = S.E. edge • 18' Rt = N.W. Edge
 11+60 11' Lt = S. E. • 9' Rt = N. Edge
 3' Lt = N. Edge
 11+37²⁵ Hub Δ 74-20' Lt 22' Lt = S. edge □ on split of L.
 11+15 11' Lt = S. edge • 10' Rt = N. edge
 10+90 B.L. = S. edge • 19' Rt = N. Edge
 10+70 • 5' Rt = S. edge 25' Rt = N. Edge
 10+45 • 6' Rt = S. edge 24' Rt = N. edge
 10+20 B.L. = S. W. edge • 19' Rt = N.E. edge
 10+00 12' Lt = W. Edge • 10' Rt = E. edge
 9+87⁴⁷ Hub Δ 58-35' Lt. □
 9+80 15' Lt = W. edge • 3' Rt = E. Edge
 9+60 16' Lt = W. edge • 8' Rt = E. edge
 9+30 3' Lt W. edge • 15' Rt = E. edge Rd.
 9+00 1' Lt = W. edge • 17' Rt = E. edge
 8+50 1' Lt = W. edge • 17' Rt = E. edge
 8+00 2' Lt = W. edge • 18' Rt. E. edge
 7+50 2' Lt = W. Edge • 18' Rt = E. edge

Golden Hill Park Road location

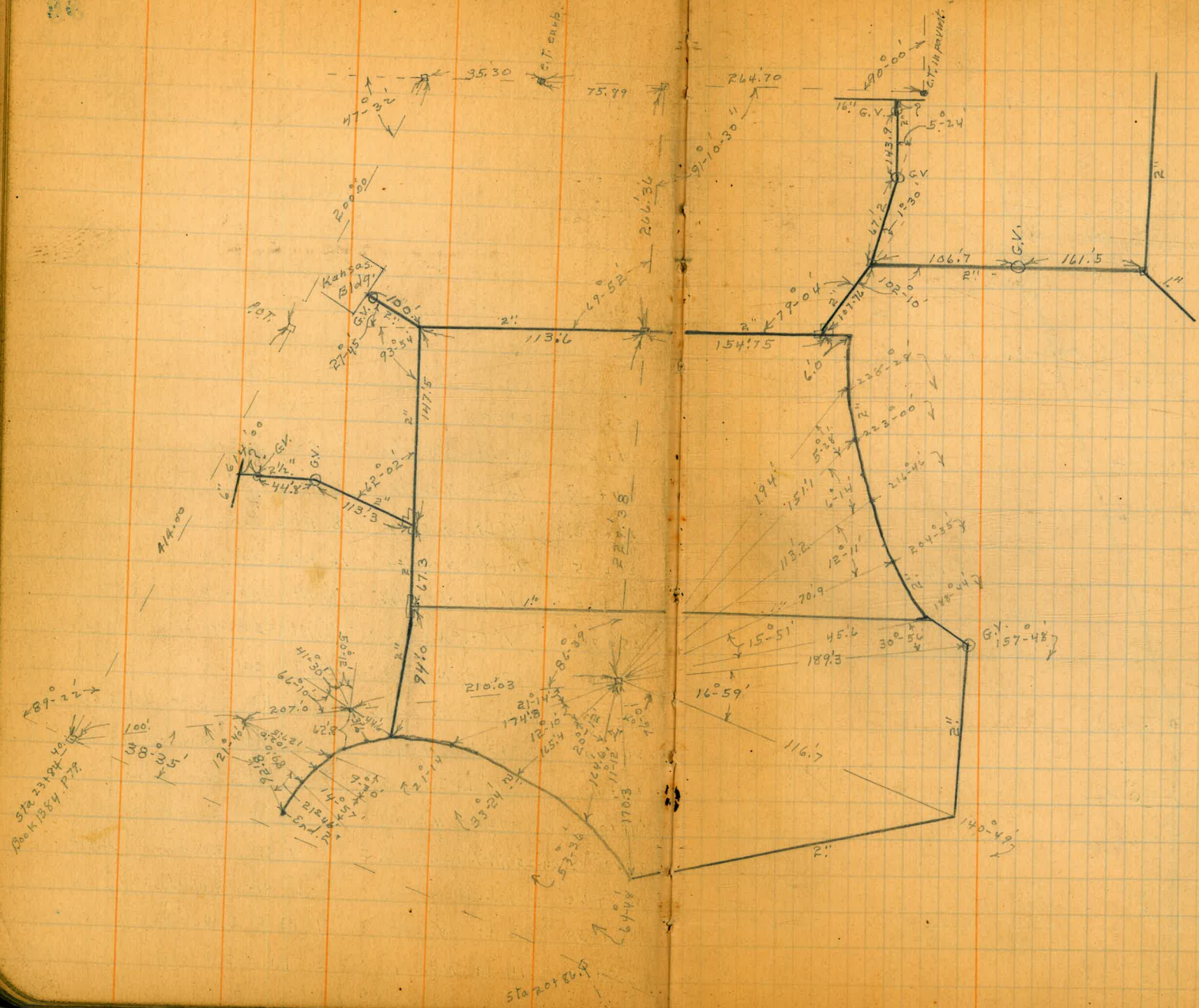
Baseline →

22+50	9' Lt = N.E. edge	8' Rt = S.W. edge
22+20	9' Lt = N.E. edge	9' Rt = S.W. edge
21+89 ⁴¹ Δ 32° 11' Lt	15' Lt = N.E. edge	2' Rt = S.W. edge
21+70	10' Lt = N.E. edge	9' Rt = S.W. edge
21+50	4' Lt = E. edge	15' Rt = W. edge
21+20	7' Lt = E. edge	18' Rt = W. edge
20+90	7' Lt = E. edge	13' Rt = W. edge
20+62 ⁴⁰ Δ 68° 17' Lt	19' Lt = E. edge	1' Rt = W. edge Rel. L split
20+50	12' Lt = E. edge	11' Rt = W. edge
20+30	5' Lt = E. edge	16' Rt = W. edge
20+10	B.L. = E. edge	20' Rt = W. edge
19+90	1' Lt = S.E. edge	20' Rt = N.W. edge
19+70	7' Lt = S. edge	15' Rt = N. edge
19+75 ⁴² Δ 98° 38' Lt	24' Lt = S. edge Rd	
	4' Lt = N. " " "	L split
19+10	2' Lt = S.W. edge	15' Rt = N.E. edge
18+90	B.L. = S.W. edge	17' Rt = N.E. edge
18+60	3' Lt = S.W. edge	14' Rt = N.E. edge
18+20	9' Lt = S.W. edge	8' Rt = N.E. edge
17+80	14' Lt = S.W. edge	2' Rt = N.E. edge
17+50	16' Lt = S.W. edge	B.L. = N.E. edge
17+20	13' Lt = S.W. edge	4' Rt = N.E. edge
16+88 ⁶³ Δ 63° 12' Rt	1' Lt = S. edge	17' Rt = N. edge Rel split
16+60	11' Lt = S. edge	7' Rt = N. edge
16+30	15' " = S. " "	2' Rt = N. edge
16+00	15' Lt = S. edge	1' Rt = N. edge Rd
15+60	12' Lt = S. edge	4' Rt = N. edge

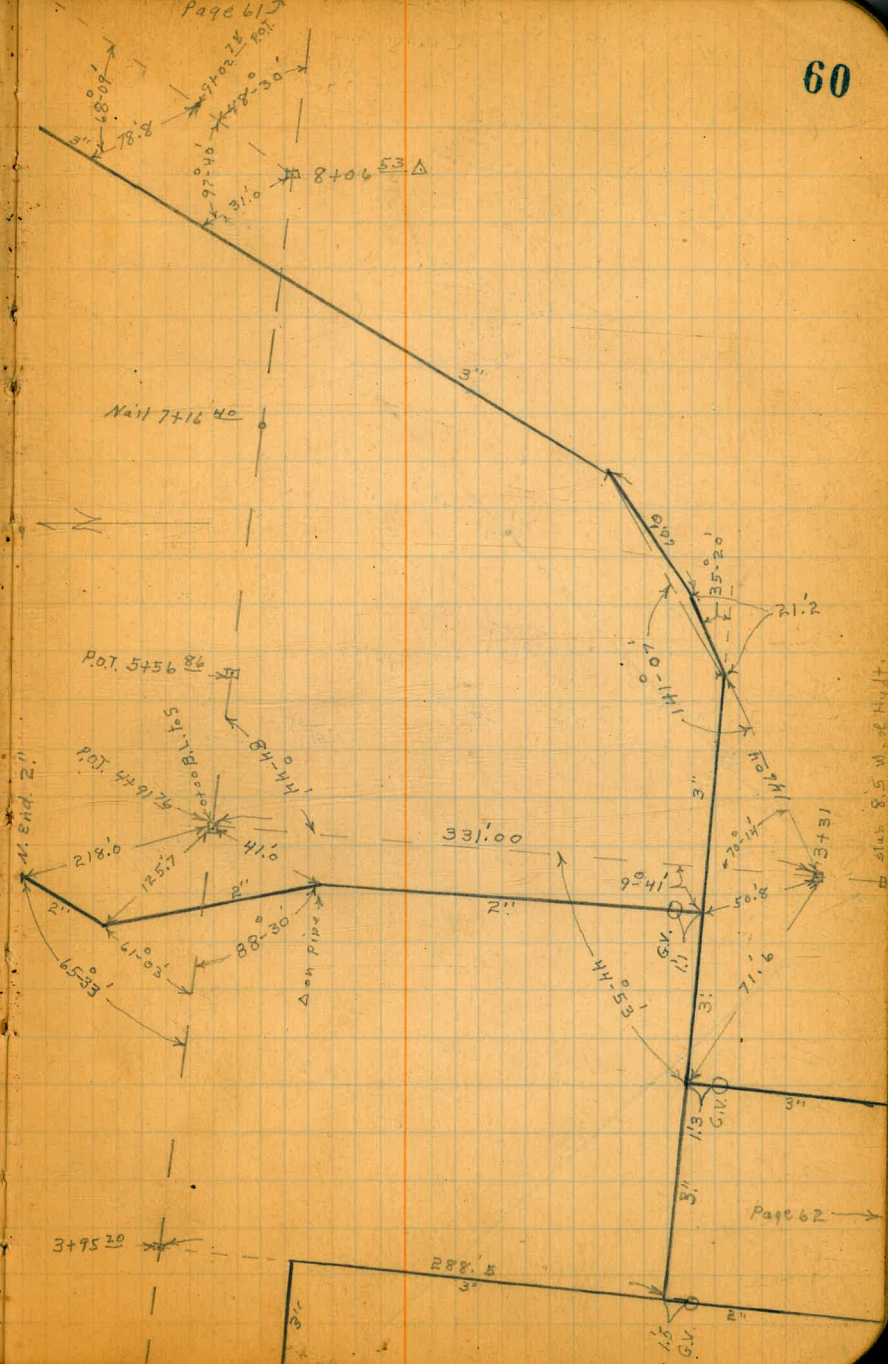
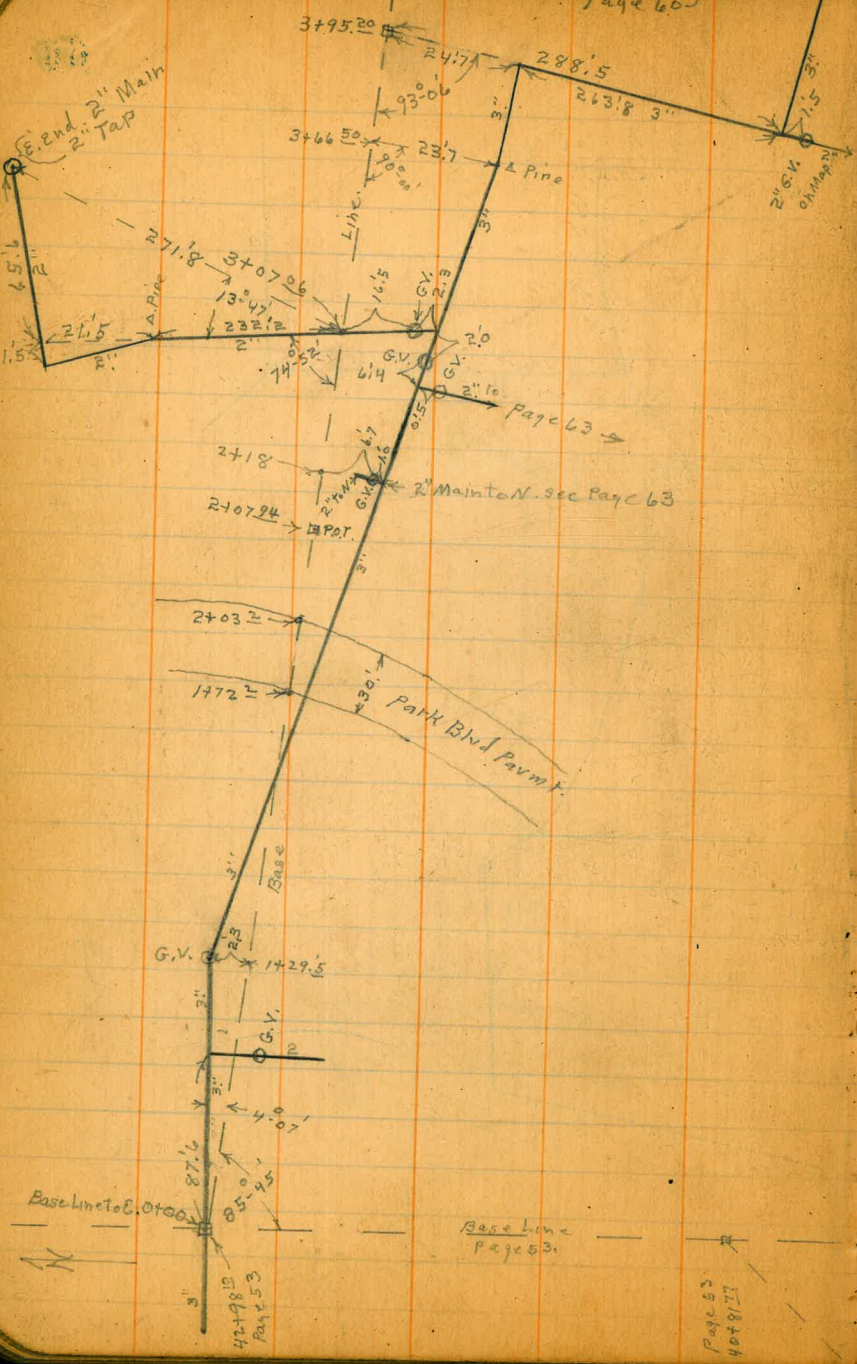
58

27+30 ²⁶ = 0+00		
27+20	25' Lt = N.E. edge	3' Rt = S.W. edge
27+00	14' Lt = N.E. edge	6' Rt = S.W. " "
26+70	6' Lt = N.E. edge	12' Rt = S.W. " "
26+35	1' Lt = N.E. edge	16' Rt = S.W. " "
26+00	1' Lt = N.E. edge	16' Rt = S.W. " "
25+70	1' Lt = N.E. edge	16' Rt = S.W. edge
25+40	2' Lt = N.E. edge	15' Rt = S.W. " "
25+00	10' Lt = N.E. edge	9' Rt = S.W. edge
24+70	13' Lt = N.E. edge	5' Rt = S.W. edge
24+40	14' Lt = N.E. edge	3' Rt = S.W. edge
24+10	12' Lt = N.E. edge	3' Rt = S.W. edge
23+80 ²⁰ Δ 24° 25' Rt	9' Lt = N.E. edge	9' Rt = S.W. edge split
23+60	12' Lt = N.E. edge	6' Rt = S.W. edge
23+30	16' Lt = N.E. edge	1' Rt = S.W. edge
23+00	14' Lt = N.E. edge	3' Rt = S.W. edge

Water Lines South of Organ Pavilion
Base Line Book K. 1384 - P. 79.



33-24
21-14
12-10
53-36
33-24
20-12
64.48
53-36
11-12
140-49
64-48
76-01
157.44
140.49
12.59
188-44
157-48
30-56
204
6

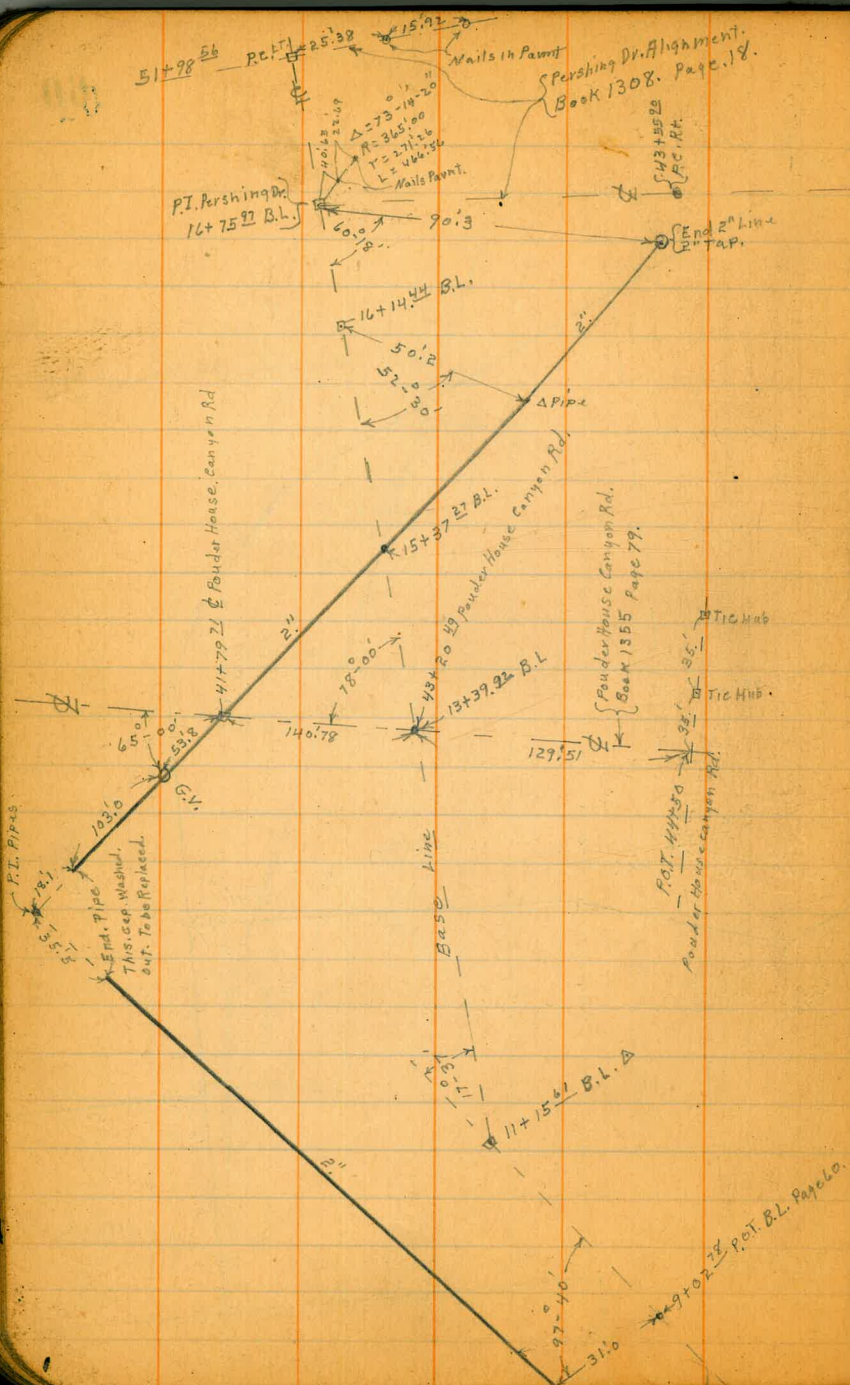


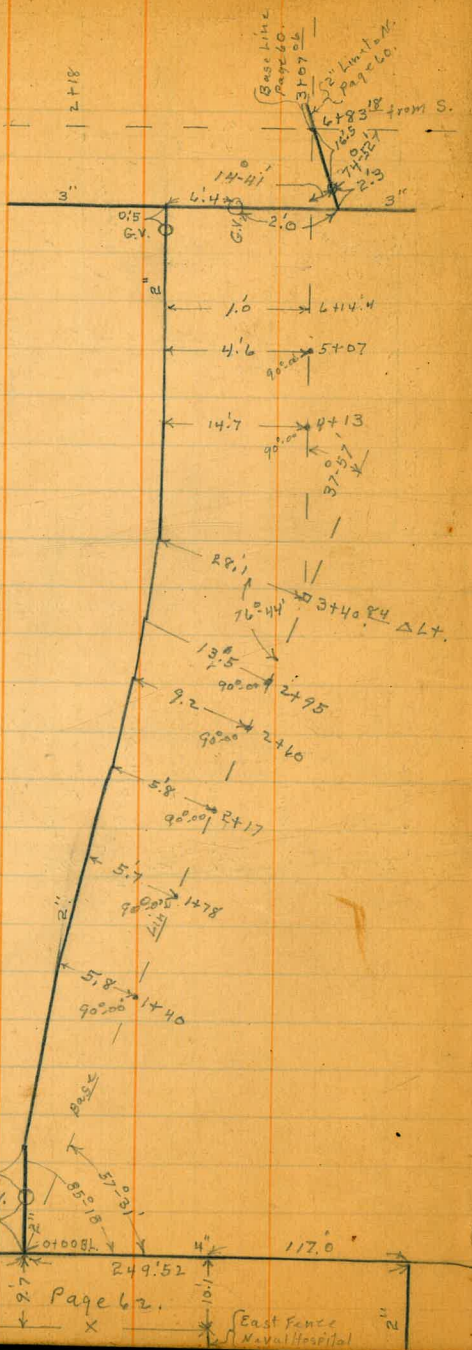
8.5 w. of H.H.H.

Page 55
40+81.11

Base Line
Page 63

Page 62





N. Fence
Naval Hospital

Page 62.

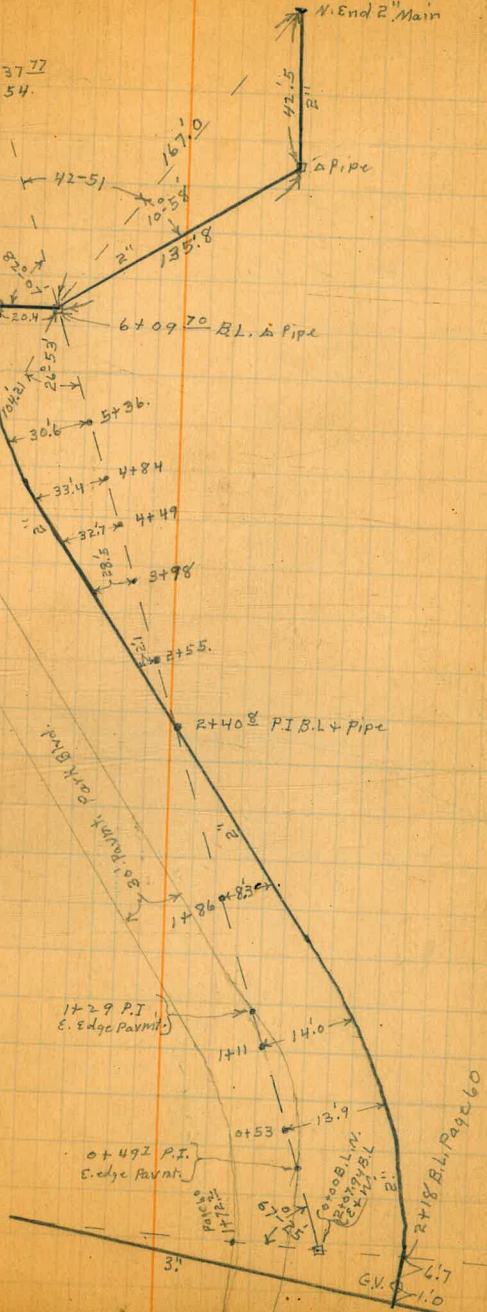
East Fence
Naval Hospital

Claret St

51+37.77
C.T. Page 54.

47+58.45
Page 54.

B.L. Page 54.



112-35

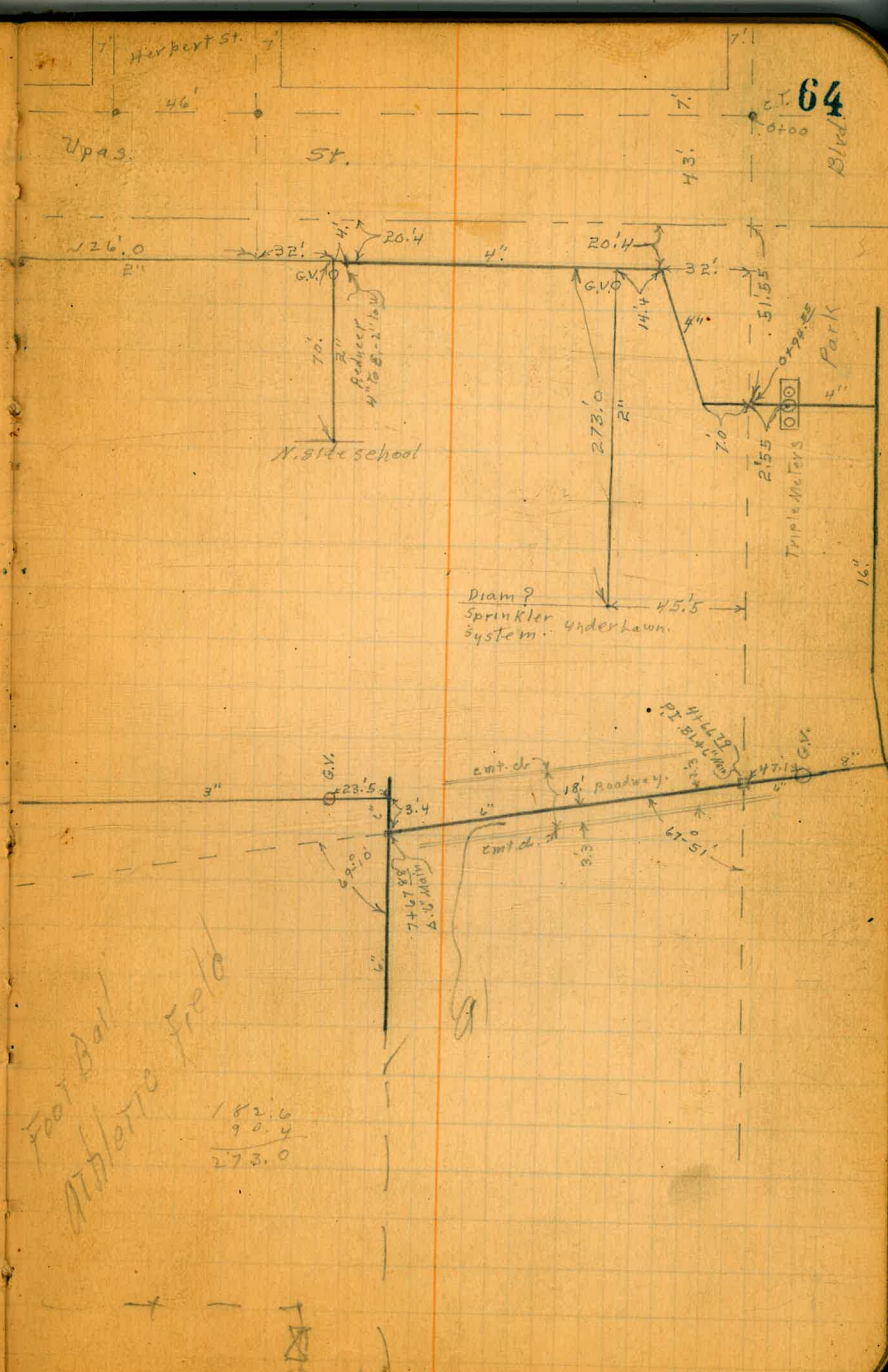
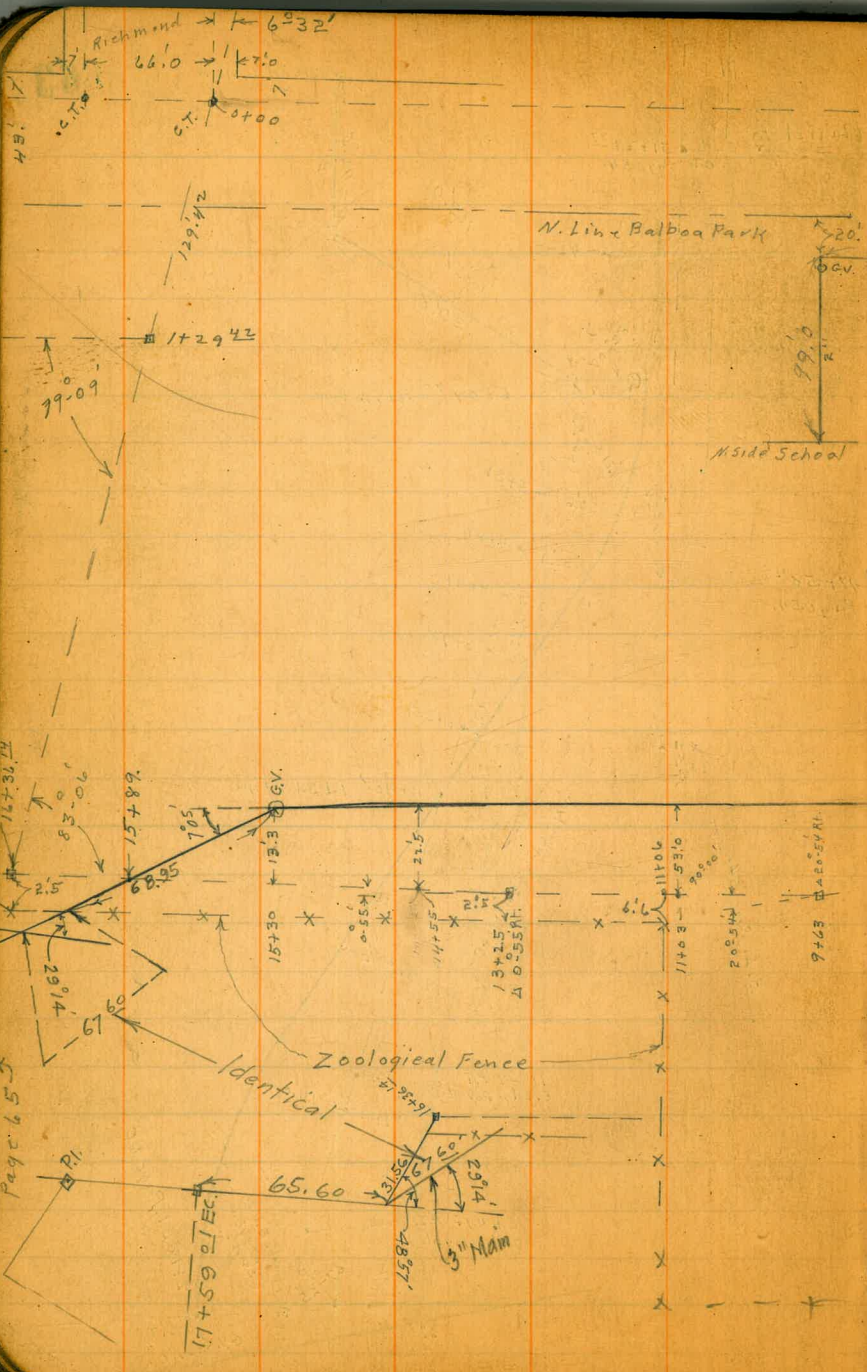
1+29 P.I.
E. Edge Pavmt.

0+492 P.I.
E. edge Pavmt.

2+18 B.L. Page 60

3"

G.V.

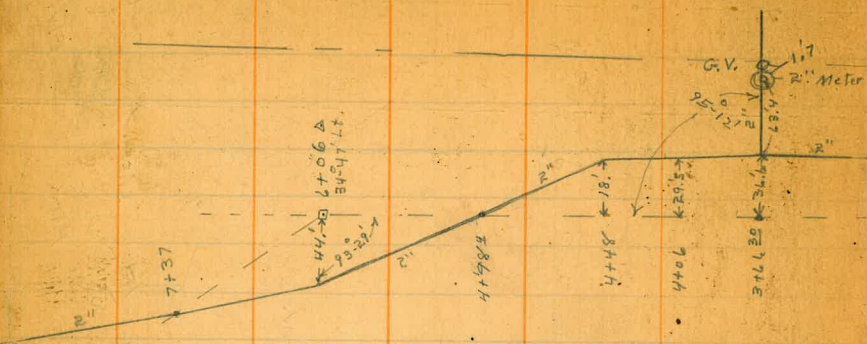


64
Blvd

Foot Ball
Athletic Field

182.6
90.4
273.0

Page 66

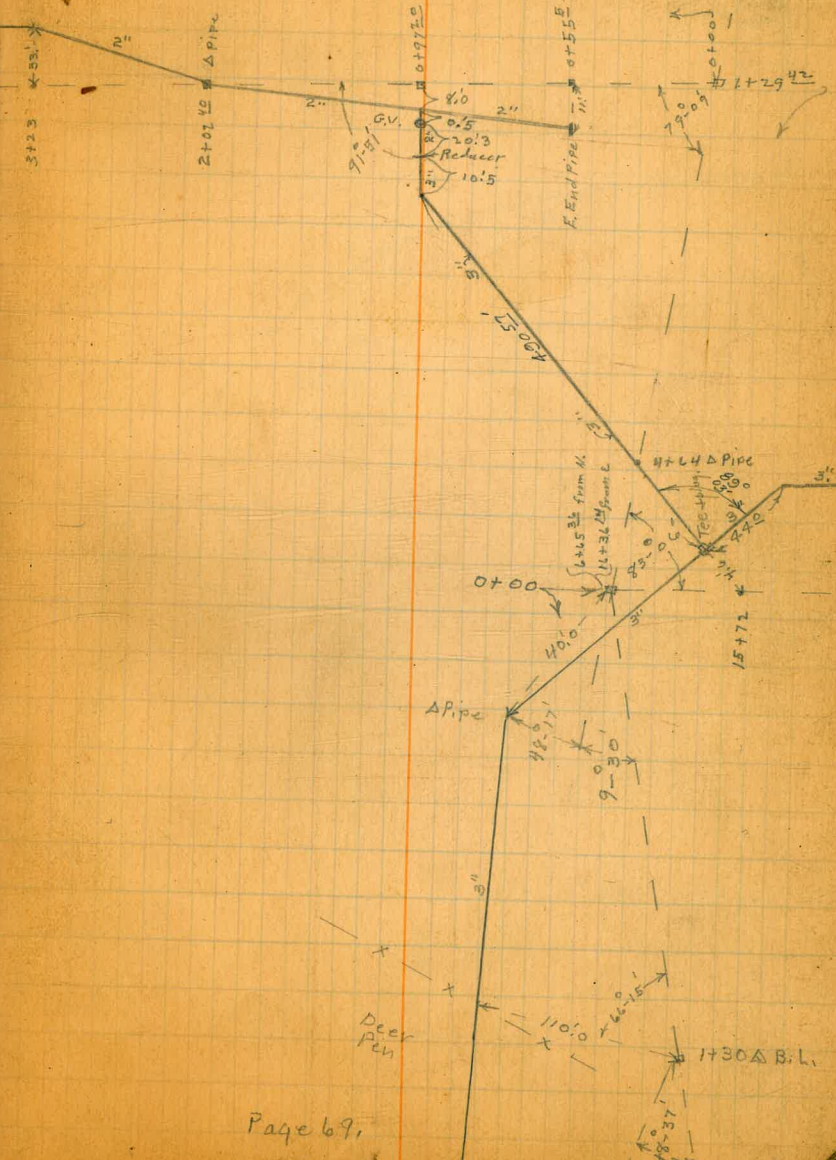


N Line Balboa park

UPAS

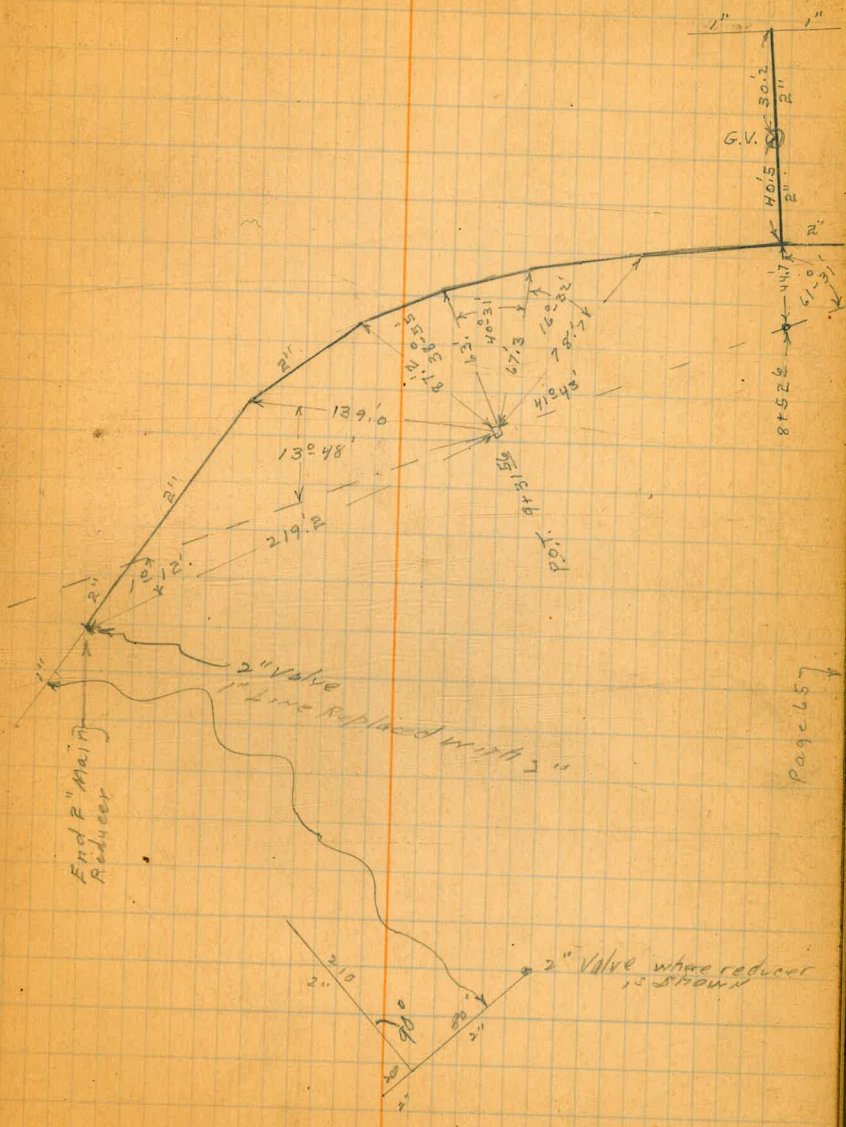
Richmond st
66
ST

65
0+00



Page 69,

Page 67



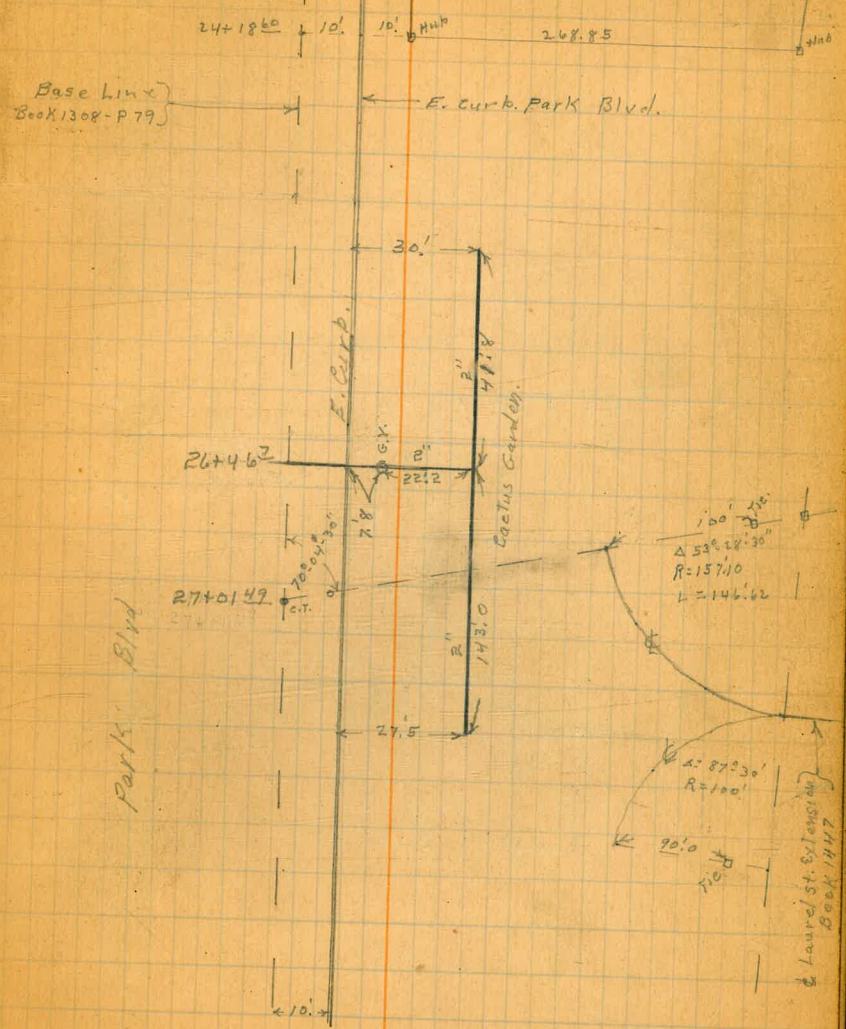
Page 65

29 02 66
35.86
28.51.00

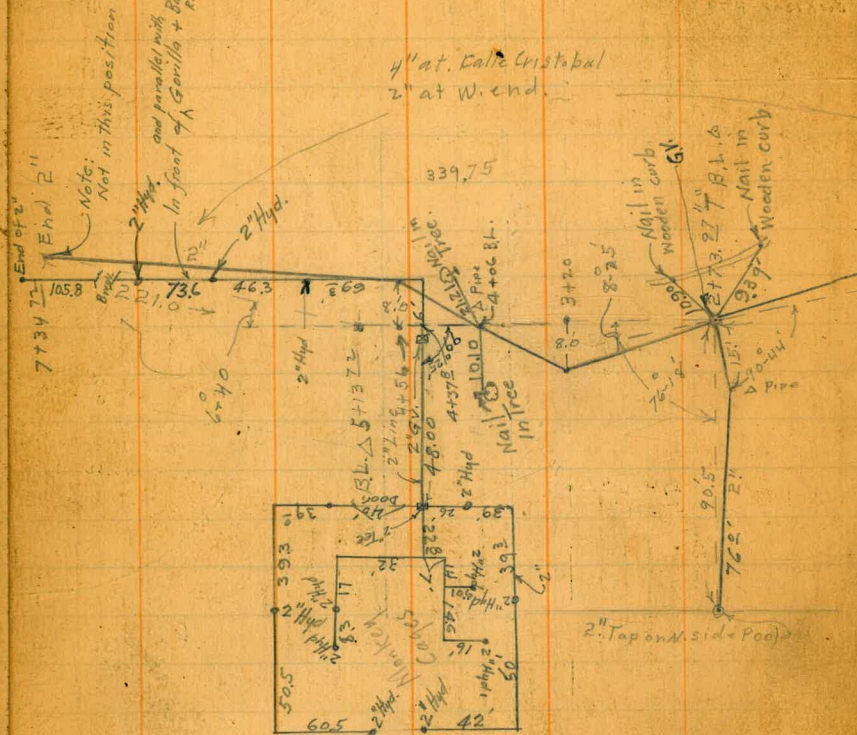
30

Proposed site
Little Theatre.

67



1196
31800
1145710

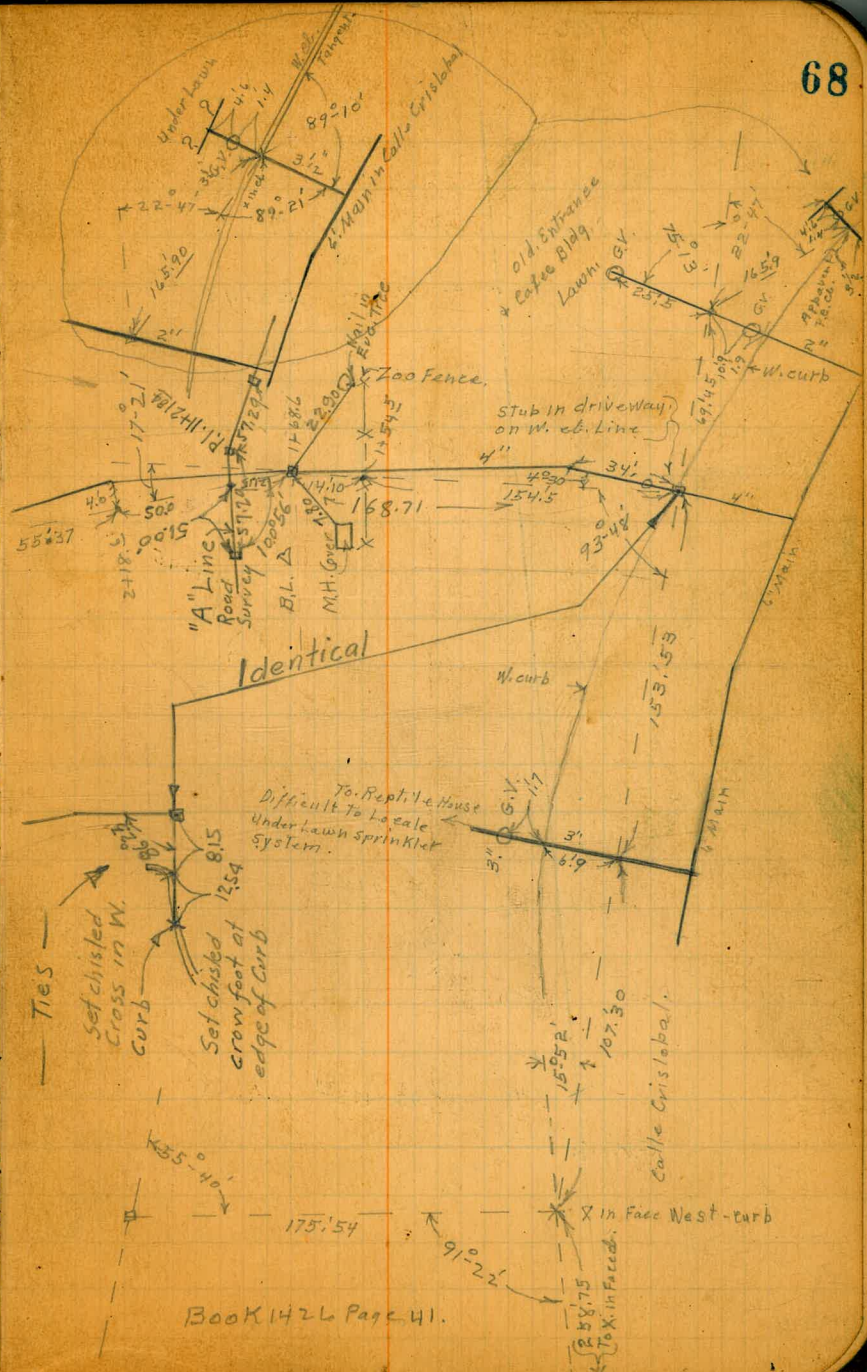


4" at Calle Cristobal
2" at W. end.

93-18
4-30
98-18

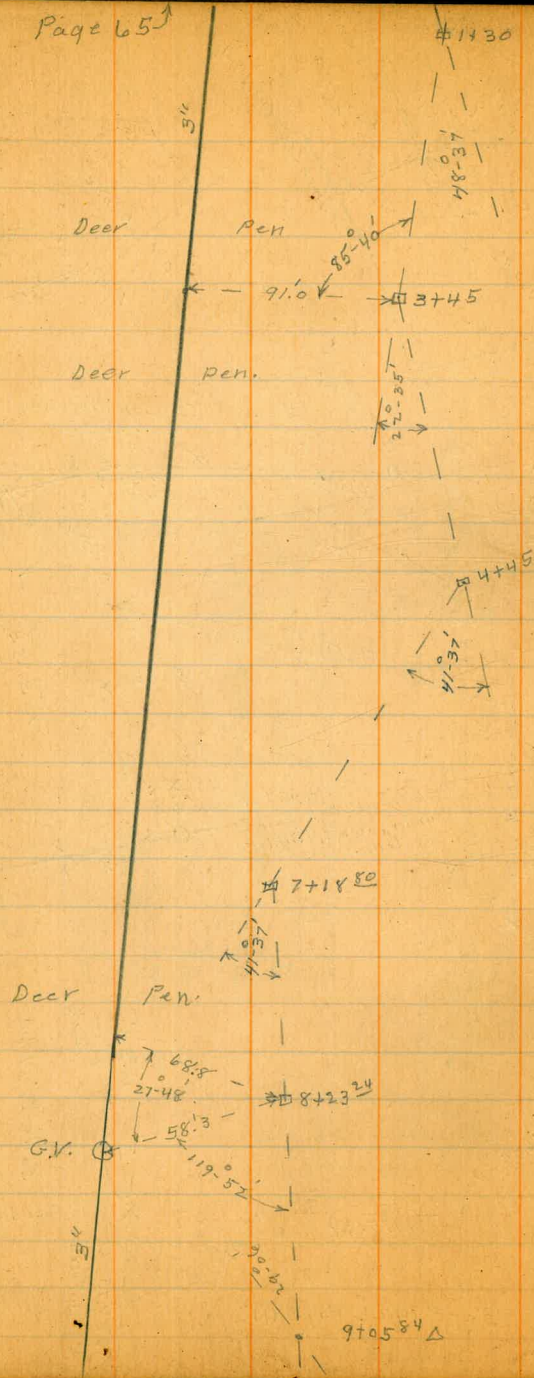
14900
11680
10500

4400
3+20
2+72
44



BOOK 1426 Page 41.

Page 65



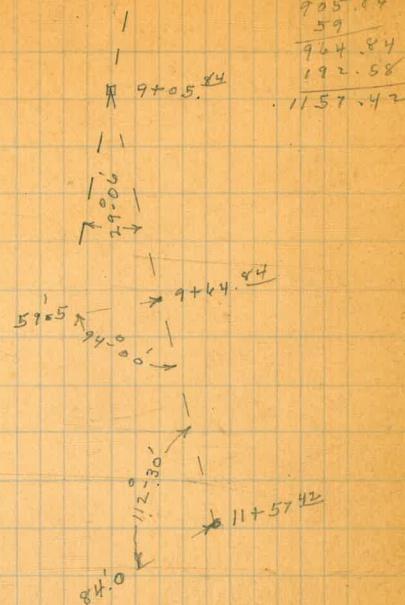
plotted to here.
c.s.k.

87
End. 3"

69

Deer Pens

Deer Pens
S. End 3" Main.



705.84
59
764.84
192.58
1157.42

89

90

Water Connections
 Park Blvd Book 1308-P.79.
 Base Line

Upas

St.

1'

Park Blvd.

0+97.47 Δ

20°-07'-30"

Fire Hydr.
on East

G.V. 1916

4.1

57-19-20

57

G.V.

Fire Hydr.
on West

42.2

9000

6+6.93

5.4

6+99.20

G.V.

7+08.19

22.30

2000

G.V.

8+67.25 c.T. in curb.

8+68.95 Hub

19°-59'-20"

9705.20

1.2

G.V.

Base line is on E.
Curb of Park Blvd.

9758.40

R.1

Fire Hydr.

Park Blvd.

9458⁴⁰ F.H.

11+04³⁰ G.V.

G.V. 60.2 → 11+54

11+67²⁰ G.V.

W. curb →

59.0

Baseline is on E
Curb of Park Blvd

Riser of Fire Hydt.
Bent over. No.

36.5 → 12+08

G.V. 12+38²⁰ G.V.

13+11³⁰ G.V.

G.V. 60.4 → 14+01²⁰

14+20 could not find G.V.

G.V. 17.0 → Fire Hydt 14+58⁵
Riser no Hydt.

G.V. 60.0 → 15+21

could not find G.V.

G.V. 60.7 → 16+54

16+51³ Plug in Dead End 2" Pipe no Valve

Hydt. Riser
no Fire Hydt.

36.5 → 14+99

72

17+65⁴⁰ G.V.

60.4

17+75

90°

18+14 G.V.

61.7 → 18+72

60.2 → 19+14 G.V.

59.0

Baseline = E. cl.

Hydrant
Riser no
Fire Hydt.

20+16²⁰ G.V.

20+88²⁰ G.V.

G.V. 61.0 → 21+18²

21+79 G.V.

G.V. to Fire Hydt on
W. Hydt not in

25.0 → 21+07

63.3 → 21+25

23+08 G.V.

23+75⁵ G.V.

G.V. ⊗
G.V. ⊗

60.7 → 23+89
60.2 → 25+48
25+68 5 → ⊗ G.V. 1.2 ✓

W. Curb ⊗ 59.0 ← East Curb
Base Line

26+46 7 ← 17.8 ⊗ G.V.
Line in Eacus Cards
Page 67 ✓

✓ G.V. ⊗
Fire Hydt Riser
No. Hydt. ⊗
✓ G.V. ⊗

60.3 → 26+61
26+86 ← ⊗ G.V. 1.2 ✓
60.5 → 27+06
95.00 → ⊗ G.V. 1.2 27+40 ✓
60.5 → 28+58 5
90.00

Blvd.

29+54 7 ← 1.3 ⊗ G.V. ✓
2.0
29+58 5 ← 16.4 → Fire Hydt.
G.V. 29+63 2 ← curb.

30+05 8 ← 12.7 →
10.0' →
Canadian Legion Bldg

Park

30+53 4 → 30+53 3 ← curb.
0.5 → 9.5 →

30+84 5 ← 4.7 ⊗ G.V. ✓

31+99 3 ← 4.2 ⊗ G.V. ✓

32+51 ⊗ 9.0 → 8.5 → Fire Hydt.
G.V.

0.5 → 4.8
34+95 2 ← Fire Hydt.
curb

52.0 → C.T. 35+44 2 3
C.T.

⊕ Lavret St

Hawthorn St. 7 Sec
33rd. to Felton

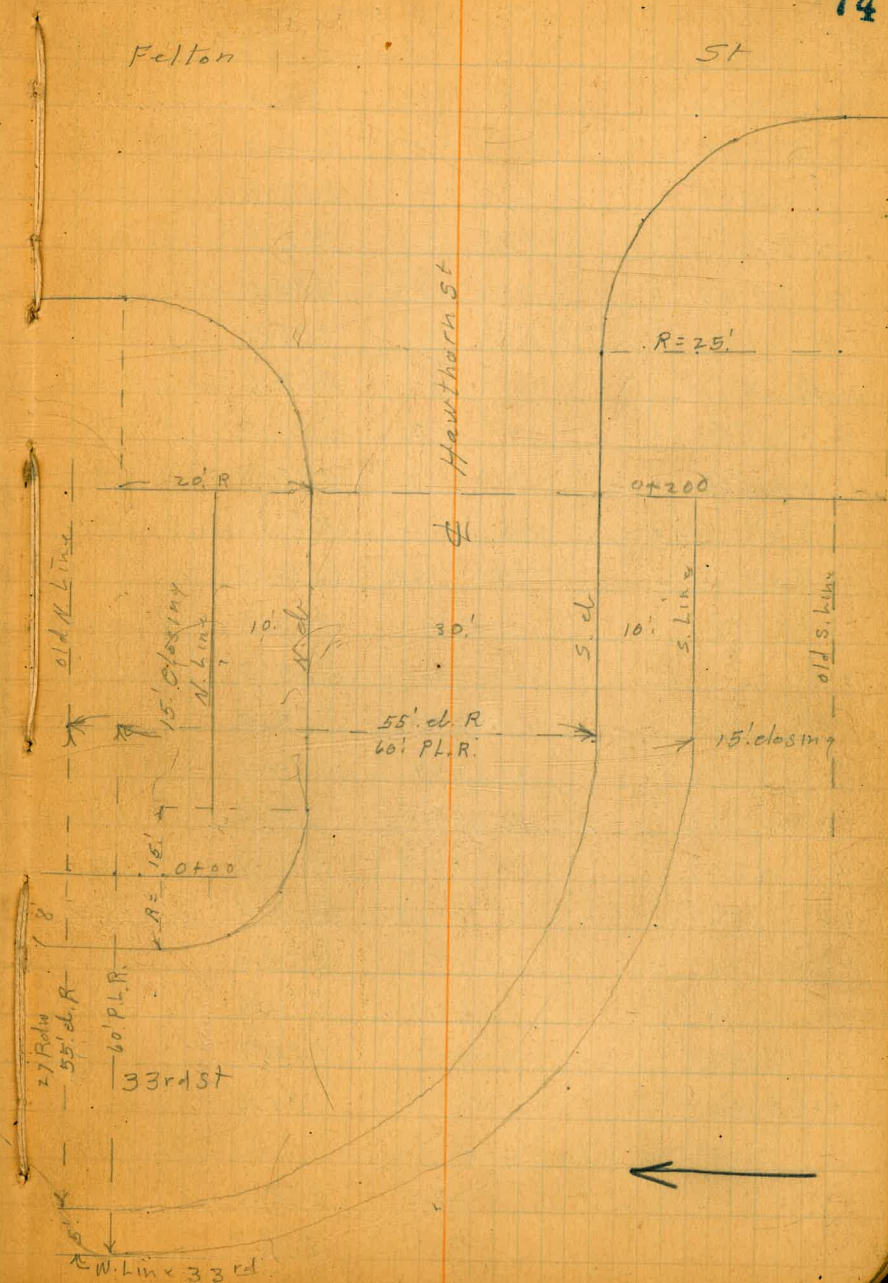
6-27-34
Miller
Walker
Baker
S.W. 33rd
& Juniper

Indexed
C.S.K.

B.M. B.P. Top Wall	3.07	281.21		278.12
TP	0.37	268.67	12.91	268.30
Set B.M. B.P. S.W. of Highview Dr. & 33rd St.			0.29	268.38
T.P.	1.88	259.82	10.73	257.94

65' W. of E. line 33rd = 25' W. of W. line 33rd.

old N. line	17.1	242.7		
15' S = N.	23.3	236.5		
70' W. of above	24.6	235.2		
25' S = N. cl	29.0	230.8	✓	
10' W. of above	28.0	231.8		
40' S = ♀	36.0	223.8	✓	
10' W. of above	35.5	224.3		
46' S.	44.2	215.6		
10' W. of above	37.8	222.0		
49' S	36.3	223.5		
2' W. of above	45.2	214.6		
8' W. " "	46.5	213.3		
10' W. " "	38.3	221.5		
55' S = S. cl. line	36.4	223.4	✓	
5' W. of 55' S.	39.1	220.7		
7' W. " "	45.6	214.2		
15' W. " "	47.4	212.4		
21' W. " "	42.0	217.8		
T.P.	1.31	259.25	1.88	257.94
65' S = New. S. line	36.8	222.5		
80' S = old S. "	39.0	220.3		



259.25

50' W. of E. line 33rd = 10' W. of W. Line

80.5 = old s. line	30.7	228.6
65.9 = New s. "	28.2	231.1
S. cl.	28.0	231.3
+ 9.	26.1	233.2
+ 11	33.0	226.3
±	34.2	225.1
+ 14	33.7	225.6
N. cl.	20.7	238.6
N. Line	14.3	245.0
15' N = old N line	6.3	253.0

40' W. of E. line = W. line 33rd st.

-15 = old N. line { S. End. } { W. side } ent. wall	1.08	258.17
N.	9.6	249.7
+ 3	10.8	248.5
+ 5	29.9	229.4
cl.	29.9	229.4
+ 3	27.0	232.3
±	27.0	232.3
+ 4	25.5	233.8
+ 5	19.9	239.4
cl.	20.7	238.6
S.	22.6	236.7
+ 15 = old s. line	27.4	231.9
5' E. of W. line = W. cl. line		
- 15 = old s. line	27.0	232.3
S	21.6	237.7

259.25

Hawthorn. St.

75

cl.	18.0	241.3
±	17.6	241.7
+ 10	17.6	241.7
cl.	11.1	248.2
N	15.3	244.0
+ 1.5' S. End. Outlet. 18" ^{Cor.} _{Iron} Culvert	12.1	247.2
+ 5 { N. End. 8" W. cl. at End of Pavmt. } { S. End. ent. cl. }	6.2	253.1
+ 15	1.09	258.16
+ 16. S. End grating cl. inlet.	1.86	257.39
+ 16 N. End. 12" Inlet Pipe	7.5	251.8
+ 19.5 = N. End. grating	1.85	257.40
+ 26. gutter at N. End cl. inlet	1.15	258.10
+ 26. ent. cl.	0.72	259.13
6.75' E. of W. cl. = W. 1/4		
- 25. on pav	0.83	258.42
- 15.6 S. End "	1.75	257.50
- 15.0 E. & W. cl.	1.07	258.18
N. Line	6.4	252.9
cl.	10.1	249.2
+ 7	13.3	246.0
±	12.0	247.3
S. cl.	14.5	244.8
S. Line	18.0	241.3
+ 15 = old s. line	24.8	234.5

259.25

6.75' e. of W. 1/4 = Φ 33rd st

-15 = old S. line	22.3	237.0
S. line	15.4	243.9
cl	12.1	247.2
Φ	9.6	249.7
cl	6.5	252.8
N	3.5	255.8
+5	2.0	257.3
+15 eq W. cl	1.13	258.12
+15.3 S. End Pav	1.72	257.53
+25 on "	0.72	258.53
6.75' e. of Φ = E. 1/4		
-25 on Pav.	0.64	258.61
-15 S. End "	1.54	257.67
-15 E+W. cl.	1.03	258.22
N	2.4	256.9
cl.	3.9	255.4
+7	4.5	254.8
Φ	6.8	252.5
cl	10.8	248.5
S	13.5	245.8
+15	19.0	240.3
6.75' e. of E. 1/4 = E. cl. 33 rd .		
-15 old S. line	17.1	242.2
S.	11.9	247.4
cl	9.8	249.5
Φ	6.2	253.1

Hawthorn

259.25

76

cl.	4.1	255.2
N	2.7	256.6
+15 = { S. End. N+S. cl. E. End. E+W. cl.	0.95	258.30
+15. S. End. pavmt.	1.31	257.94
+25 gutter	0.66	258.59
+25 cont. cl.	0.14	259.09
8' e. of cl = E. Line 33 rd = 0+00		
-15	1.0	258.3
N	3.2	256.1
cl	4.7	254.6
Φ	7.1	252.2
cl.	9.3	250.0
S	11.0	248.3
+15	12.5	246.8
0+25		
-10.7' = N. side shed.	12.6	246.7
S.	10.6	248.7
cl.	9.4	249.9
Φ	8.2	251.1
cl.	7.0	252.3
N	6.6	252.7
+15	2.6	256.7
0+50		
-15	3.8	255.5
-5	6.9	252.4
N	7.4	251.9

259.25

0+50 (cow)

N. d.	old s. line	8.2	251.1
♀		9.8	249.5
d.		11.5	247.8
s		12.1	247.2
+15		14.3	245.0

0+75

-15		16.3	243.0
s		14.4	244.9
d.		13.4	245.9
♀		11.7	247.6
d.		10.3	249.0
N		9.1.	250.2
+6		7.8	251.5
+10		5.6	253.7
+15	old N. line	5.0	254.3

0+90

-15		6.9	252.4
N		10.7	248.6
d.		11.9	247.4
♀		12.9	246.4
T.P.	3.82 251.13	11.94	247.31
d.		6.7	244.4
s		8.2	242.9
+15		10.5	240.6

1+12

-43		27.0	224.1
-----	--	------	-------

251.13

Hawthorn St.

77

-15	old s. line	21.6	229.5
s		20.8	230.3
d.		20.4	230.7
♀		17.6	233.5
d.		13.2	237.9
N		10.5	240.6
+15		6.6	244.5
+25		2.7	248.4

1+20

-20		2.8	248.3
-15		4.2	246.9
N.		10.7	240.4
d.		15.0	236.1
♀		18.9	232.2
d.		23.7	227.4
s.		25.5	225.6
+15		26.9	224.2
+30		29.9	221.2
+50		29.9	221.2

1+35

-55		39.7	211.4
-30		33.7	217.4
-15		27.8	223.3
s		21.3	229.8
d.		15.9	235.2
♀		11.4	239.7

251.13

1+35 (con)

el.	6.7	244.4
N	3.7	247.4
+7	1.7	249.4
+15	0.7	250.4

1+47

-15	+0.5	251.6
N	1.5	249.6
el.	3.1	248.0
⊕	6.7	244.4
dr	9.4	241.3
S.	14.3	236.8
+15	21.0	230.1
+33	25.7	225.4
+40	28.7	222.4

1+75

-30	16.1	235.0
-15	13.1	238.0
S	10.0	241.1
dr	7.3	243.8
⊕	3.7	247.4
el	1.3	249.8
TP	6.83	256.40
N.	5.1	251.3
+15	2.8	253.6

256.40

1+97

78

-15	1.2	255.2
N	3.4	253.0
el.	5.1	251.3
⊕	5.9	250.5
el	8.9	247.5
S	10.7	245.7
+15	13.0	243.4

2+00 = W. Line Felton

-15	12.7	243.7
S	10.1	246.3
el	8.4	248.0
⊕	5.2	251.2
+5.15 = W. end. Ex. cont. el.	5.20	251.20
+5.15 = gutter W. edge pav	5.80	250.60
el. " " "	5.44	250.96
N. " " "	5.25	251.15
+10.15 N. gutter " "	5.24	251.16
+10.15 N. cont. dr W. end	4.61	251.79
+10. = old. N. Line	4.3	252.1
	10' E.	
-15. old N. Line	4.7	251.7
- 2.6 Ex. cont. d.	4.73	251.67
- 2.6 gutter	5.29	251.11
N	5.33	251.07
el	5.54	250.86
+11.2 gutter	5.90	250.50

256.40

10' E. of W. Line Felton (con)

N db + 11.3 = s. amt. db.	5.36	251.04
¢	5.4	251.0
cb	7.2	249.2
S	8.9	247.5
+15 old s. line	11.4	245.0
20' E. of W. Line		
-15	10.5	245.9
S	8.1	248.3
cl	6.7	249.7
¢ = ex. amt. cl	5.53	250.87
¢ gutter pav.	6.16	250.24
cl	5.73	250.67
N	5.52	250.88
+15	5.36	251.04

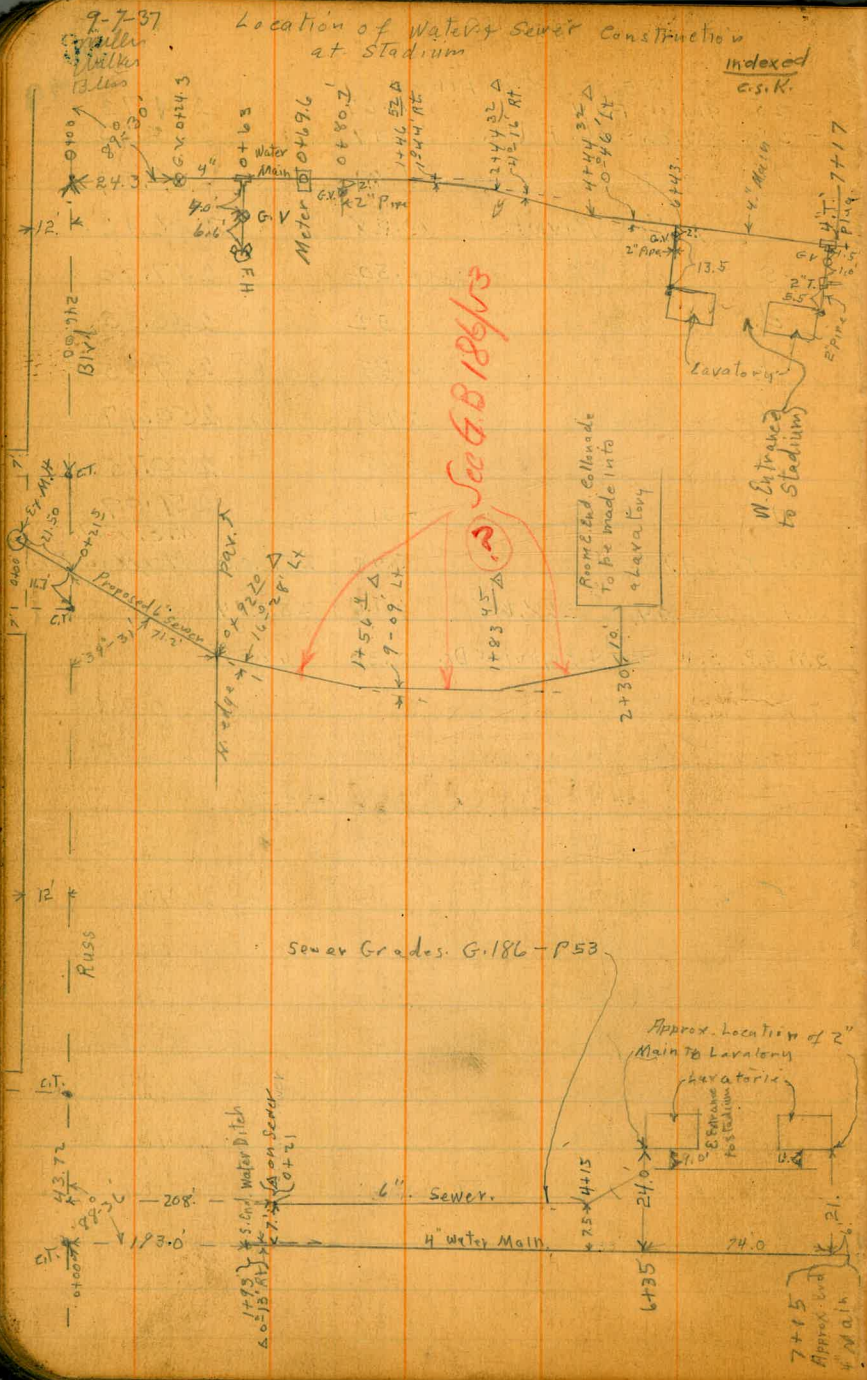
35' E. of W. Line

-15	Pav.	5.20	251.20
N	"	5.54	250.86
cl	"	5.88	250.52
¢	"	6.58	249.82
+12.8 gutter	"	7.27	249.13
+12.8 ex. amt. cl.		6.61	249.79
cb.		6.6	249.8
S		7.4	249.0
+15		9.1	247.3

256.40

45' E. of W. Line

-25 gutter pav	11.67	244.73	79
-25 = W. amt. db. Felton	11.77	245.23	
-15 " " " "	9.81	246.59	
-15 gutter paymt.	10.28	246.12	
S	8.50	247.90	
cl	7.52	248.88	
¢	6.55	249.85	
cl	5.93	250.47	
N	5.65	250.75	
+15	5.31	251.09	
B.M. T. C. T. N.	5.40	251.00	N. E. Felton F. Hawthorn
T.P. 12.94	268.68	0.66	255.74
R.M. B.P. S.W. 33 rd + Highview Dr.	0.30	268.38	



71.2	444.32	97.8	10.6	4	63
21.5	198.6	44.3	67.6	24.3	24.3
63.7	643.0		63.3	38.7	38.7
156.4	324		88-36	643	643
27.0	193	394	6	71.2	71.2
185		469			
46					
230.00					

443
74
717

TABLE No. 1

Distance of slope stake from top or shoulder
stake for roadway width roadway 12 to 1.
If ground is nearly level the cut fill at side
stake is located by the double entry method in
left column and top row. The number in body
of table is same row and column number.

from side stake to slope stake. If ground is not
level the slope stake is located by the double
entry method in the table. Add this amount
to cut or fill and find in table. Set up
rod at this point and line of sight should cut
larger.

IMPROVED TABLES
AND
INFORMATION

TABLE No. 2

To find Tangent and External for curve of
any other degree divide by degree of curve and
add connection found in column of connections.

Degree of curve with a given I may be found
by dividing tangent (or external), opposite I by
given tangent (or external).

The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

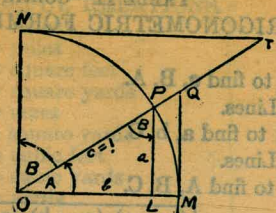


TABLE II

TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = \frac{1}{\tan B}$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = \frac{1}{\cot B}$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = \frac{1}{\sec B}$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = \frac{1}{\csc B}$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

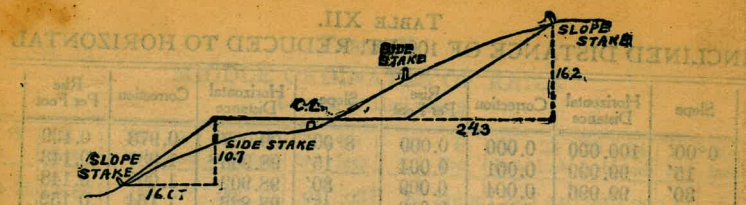
$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

648
220
c

15730
11703
4427

23.5
530
302.00
050.50

1	2	3	4	5	6	7	8	9	10
0	1	2	3	4	5	6	7	8	9



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

Balboa Park Books

- 1444 -
- 1445 -
- 1355
- 1384
- 1397
- 1426 -
- 1308 -

88° 02'

1782

156
25
131

60
72.2
39
64
255.2
9.2
246.0

3742.60

$$\begin{array}{r} 1201 \\ 502 \\ \hline 1703 \end{array}$$

$$\begin{array}{r} 36335 \\ 1709 \\ \hline 34632 \\ 30623 \\ \hline .09 \end{array}$$

346.26

$$\begin{array}{r} 1207 \\ 502 \\ \hline 1709 \end{array}$$

$$\begin{array}{r} 36335 \\ 1709 \\ \hline 34626 \\ .06 \\ \hline 34632 \end{array}$$

$$\begin{array}{r} 1278 \\ 502 \\ \hline 1780 \end{array}$$

$$\begin{array}{r} 1713 \\ 34632 \end{array}$$

$$\begin{array}{r} 21205 \\ 20055 \\ \hline 1150 \end{array}$$

39.48	74.48	14.80	89.20	35.52
1448.57	75.12	85.20	177.10	41.48
1479.17		100.00		77.00
30.83				75.48
1510.00	1187.94	2189.41	129.42	417.00
	108.80	36.59	70.58	69.34
	1079.14	2220.00	200.00	387.47
				17
1137.25	80.70	323		62
	29.30	83		37
22.75	10.00	4.06		38
1160.00		42		69
49.75	197.20	4.48		
1187.00	5.20		98.46	63.
	206.40	137.41	58.15	8.526
37.25		98.46	40.31	
72.75	58.15	38.55		8.7
110.00	41.43	8.33		20.5
	16.32			29.2
				36.6
1137.25	427	28		
111.32	675	20.5		
1248.57		11.4		
		5		
		20.5		
		36.9		
1348.57				
71.5				
1420.0				
1688.63				
31.37				
1720.00				
1945.47	8578			
24.53	93			
1970.00	42.39			
1945.47				
116.93				
2062.40				
27.60				
2090.00				