

1447

PASTE

LEVEL BOOK

No. 1380

8" = .67 11" = 0.833
 10" = .83
 4" = .33
 2" = .17



ENGINEERING DEPARTMENT,
 CITY OF SAN DIEGO,
 CALIFORNIA.

MICROFILMED

U. S. G. 1364

13 - 196 = 4 - 72° to curve. 418° = 3141
 25158

4120
 38
 77

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.
 ENGINEERING and DRAFTING SUPPLIES
 IRVING PARK STATION
 CHICAGO, ILL.

70 14

Walker
Brooks
Clovert
Nelson
3-29-32

LEVELS on Existing Paving & Curb
ON PARK BLVD. AND
AND CROSS SECTION EAST AND WEST ROAD
FROM PARK BLVD. TO PERSHING DRIVE
See Sketch Page 2 and 3
Alignment East and West Road in Book 1397
" Copied in this Book
See P-69

2.57 295.99

29342

B.M. top High
Book 1319-75

0-50'

E top cb.	3.90	292.09
" Gut. on Paving	4.55	291.44
L " " "	3.90	292.09
W " " "	4.50	291.49
W top cb.	3.90	292.09

0+00-3.15 South of South Line ^{Proposed Throat} LITTLE

W top cb.	3.83	292.16
" Gut. on Paving	4.40	291.59
L " " "	3.84	292.15
E " " "	4.45	291.54
E top cb.	3.85	292.14

0+52.85

E top cb.	3.90	292.09
" Gut. on Paving	4.49	291.50
L " " "	3.85	292.14
W " " "	4.45	291.54
" top cb.	3.85	292.14

1+13.35

W " " "	3.93	292.06
" Gut. on Paving	4.50	291.49
L " " "	3.86	292.13

295.99

1

E Gut. on Paving	4.47	291.52
" top cb.	3.92	292.07

1+52.85

E top cb.	3.90	292.09
" Gut. on Paving	4.50	291.49
L " " "	3.89	292.10
W " " "	4.43	291.56
" top cb.	3.89	292.10

2+00

W " " "	4.00	291.99
W Gut. on Paving	4.55	291.44
L " " "	3.92	292.07
E " " "	4.50	291.49
E top cb.	3.97	292.02

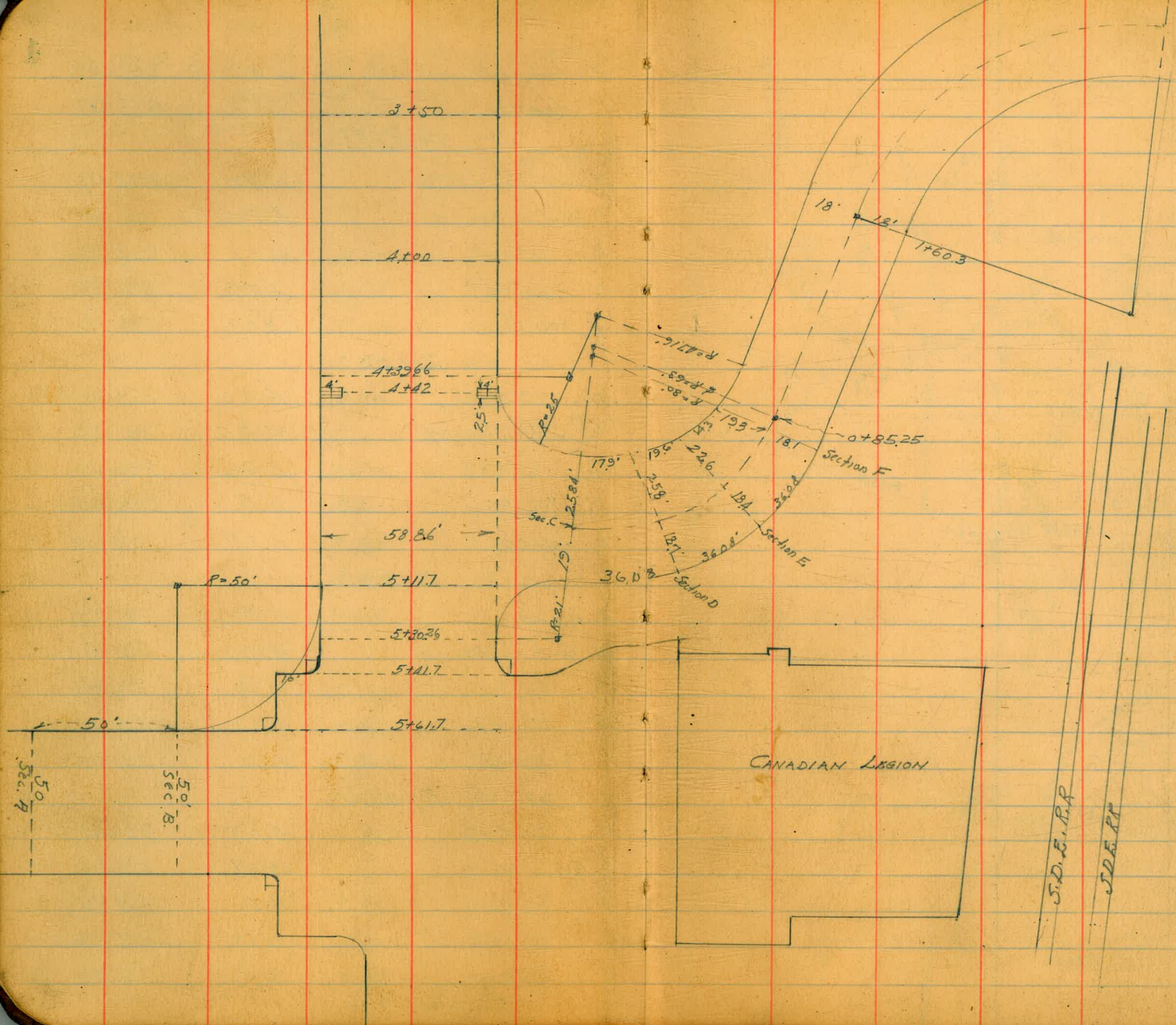
2+50

E top cb.	4.20	291.79
E Gut. on Paving	4.80	291.19
L " " "	4.14	291.85
W " " "	4.73	291.26
" on top cb.	4.12	291.80

3+00

W " " "	4.50	291.49
" Gut. on Paving	5.07	290.92
L " " "	4.50	291.49
E " " "	5.13	290.86
E	4.51	291.48

Cont. on P. 4



3+50

E top cb.	4.83	291.16
E Gut. on Paving.	5.47	290.52
L " "	4.87	291.12
M " " "	5.40	290.59
" top cb.	4.83	291.16

4+00

M top cb.	5.10	290.89
" Gut. on Paving.	5.66	290.33
L " "	5.16	290.83
E " " "	5.78	290.21
E top cb.	5.13	290.86

4+39.66

E top cb.	5.26	290.73
E Gut. on Paving.	5.88	290.11
L " "	5.42	290.57
M " " "	5.86	290.13
" top cb.	5.25	290.74

4+42 = 2 Existing Drains

M top cb.	5.55	290.44
" Gut. on Grating.	5.90	290.09
" " " Flow line 8" pipe		
Mcb + 4 " " " "	7.85	288.14
" " + 4 " top Grating.	5.73	290.26
L on Paving.	5.44	290.55
E Gut. - 4' on Grating.	5.74	290.25

E Gut. - 4' on Flow line 8" pipe	7.80	288.19
E Gut. on Grating.	5.91	290.08
E top cb.	5.26	290.73

5+11.7

E top cb.	5.36	290.63
E Gut. on Paving.	5.89	290.10
L " "	5.79	290.20
M " " "	5.80	290.19
M top cb.	5.27	290.72

5+30.26

M top cb.	5.30	290.69
M Gut. on Paving.	5.85	290.14
L " "	5.84	290.15
E " " "	5.86	290.13
E top cb.	5.35	290.64

T.P. 0.83 294.25 2.57 293.42

5+41.7 = 632.92' North of S Laurel St.

-15' on cb.	3.62	290.63
-15' " Gut. on Paving.	4.09	290.16
-5' " " " "	4.13	290.12
-5' " top cb. at P.C. of S' Radius.	3.61	291.64
E Gut. on Paving. Int. cb. lines	4.14	290.11
L on Rim M.H.	4.20	290.05
M Gut. on Paving. Int. cb. lines	4.09	290.16
+5' on Paving. at Pl. S' Rad.	4.12	290.13
+5' " (b) " " " "	3.61	290.64

+15' on cb	3.68	290.57
+15' " Paving	4.29	289.96
5+61.7=N cb line - 9 st.		
-20' on cb RC. 5' Radius.	3.79	290.46
-20' " Gut " " "	4.35	289.90
M cb. on paving.	4.00	290.25
E " "	4.09	290.16
E cb. Int. on Paving.	4.13	290.12
E. cb. Intersection + 25.5 on Paving	4.04	290.21 at Bottom dep

SECTION A

South top cb	5.81	288.44
" Gut. on Paving.	6.43	287.82
E " "	5.86	288.39
N Gut. " "	6.42	287.83
N top cb.	5.84	288.41

Section B

N " "	4.54	289.71
N Gut. on Paving	5.14	289.11
E	4.58	289.67
South Gut. on "	5.13	289.12
" top cb.	4.53	289.72

South Branch
EAST AND WEST ROAD
See sketch p. 2
Stations are \angle

294.14

6

0.72 294.14

293.42

BM on top of

Section C

\angle
18' Lt
45' Lt

7.1 287.0
7.2 286.9
7.0 287.1

1+60.3 = B.C. Rt $81^{\circ}30'$ $\angle R=100'$

19' Rt

3.7 290.4

\angle

4.2 289.9

60' Lt

6.6 287.5

25.84 Lt

4.9 289.2

18' Lt

7.9 286.2

Section D

\angle on hub.

7.53 286.6

25.8' Lt

6.0 288.1

18' Rt

7.7 286.4

\angle

5.2 288.9

63' Rt

5.0 289.1

18.7

5.2 288.9

1+80

25' Rt

5.0 288.1

63' Rt

5.2 288.9

Section E

18' Rt

7.4 286.7

35' Rt

5.8 288.3

\angle

8.0 286.1

18.4 Rt

6.4 287.7

18' Lt

8.4 285.7

\angle

6.4 287.7

60' Lt

7.5 286.6

22.6 Lt

6.6 287.5

2+00

35' Lt

6.5 287.6

66' Lt

8.0 286.1

Section F

42' Lt

9.0 285.1

35' Lt

6.7 287.4

18' Lt

9.0 285.1

19.3 Lt

6.8 287.3

\angle

9.0 285.1

\angle

7.0 287.1

18' Rt

8.0 286.1

18.1 Rt

6.4 287.7

55' Rt

5.6 288.5

40' Rt

5.5 288.6

70' Rt

4.9 289.2

1+10

2+20

45' Rt

7.0 287.1

70' Rt

5.0 289.1

18' Rt

6.9 287.2

48' Rt

8.0 286.1

18' Rt.			8.8	285.3
£			9.6	284.5
18' Lt.			10.0	284.1
43' Lt.			10.3	283.8
68' Lt.			9.3	284.8
T.P.	3.78	286.52	11.40	282.74
	2+42.76			
18' Lt.			5.1	281.4
17' Lt.			5.1	281.4
8' Lt.			8.6	277.9
£			4.7	281.8
3' Rt.			3.6	282.9
18' Rt.			1.7	284.8
55' Rt.			+2.0	288.5
	2+50			
55' Rt.			+2.0	288.5
28' Rt.			1.0	285.5
18' Rt.			4.3	282.2
£			8.7	277.8
6' Lt.			11.3	275.2
18' Lt.			5.6	280.9
233' Lt. = 8" line			8.1	278.4
	2+60			
329' Lt. = 8" line			9.8	276.7
18' Lt.			14.1	272.4
6' Lt.			15.4	271.1

O.P. RI Hub
South Branch
A-8130 & R100

£			14.1	272.4
3' Rt.			12.1	274.4
18' Rt.			11.7	274.8
30' Rt.			12.5	274.0
35' Rt.			1.2	285.3
55' Rt.			+1.9	288.4
T.P.	3.41	276.10	12.83	273.69
	2+80			
60' Rt.			+13.0	289.1
56' Rt. = N edge Main Abutment			+11.3	287.4
40' Rt.			+4.3	280.4
30' Rt.			1.9	274.2
18' Rt.			11.2	264.9
£			18.0	258.1
10' Lt.			23.0	253.1
18' Lt.			20.0	256.1
35' Lt.			19.5	256.6
43' Lt.			17.3	258.8
63' Lt. = 8" line			4.1	272.0
	2+90			
87.8' Lt.			0.6	275.5
75' Lt.			3.8	272.3
43' Lt.			20.0	256.1
32' Lt.			27.0	249.1
18' Lt.			27.4	248.7
£			26.0	250.1

abutment
5' East of
this point

276.10

7' Rt.		19.1	257.0
18' Rt.	North edge of conc.	10.0	266.1
29' Rt. = Piers		5.1	271.0
3 + 0.254 = E.C. Approx. 2 West Piers			
28.6' Rt.	Top on Bottom Main Span = North edge Con. Piers	+ 6.50	282.60
28.6' Rt.	on top Con. Pier	7.93	268.17
28.4' "	" Ground at Abace pier	8.2	267.9
18' Rt.		14.0	262.1
T.P.	0.31	263.92	12.49 263.61
9' Rt.		7.5	256.4
2		17.3	246.6
4' Lt.		19.0	244.9
14.4' Lt.	on top of open Con Drain	3.3.4	240.5 South edge
18' Lt.		23.4	240.5
22' Lt.	" " " " " "	24.0	239.9 North edge
28.4' Lt.	at Con. Pier on Ground	21.8	242.1
28.4' "	on " "	18.82	245.10
32' Lt.		21.4	242.5
55' Lt.		7.2	256.7
T.P.	7.40	271.01	0.31 263.61

Cont. on Page 11

CROSS SECTION

North Branch to East + West Road. 8
Sketch Page 3on Iron Bolt
Bolt 1319-75

1.69	293.83	292.14
0 - 45.29		
28' Lt.	2.5	291.3
18' Lt.	2.6	291.2
2	2.3	291.5
34.9' Rt.	2.1	291.7
0 - 25		
35' Rt.	2.0	291.8
28.5' Rt.	2.4	291.4
2	3.1	290.7
18' Lt.	3.7	290.1
28' Lt.	4.0	289.8
0 + 00		
28' Lt.	5.7	288.1
18' Lt.	5.2	288.6
2	4.4	289.4
23.1' Rt.	3.3	290.5
33' Rt.	3.0	290.8
0 + 25		
50' Rt.	4.0	289.8
19.4' Rt.	4.2	289.6
2	5.1	288.7
18' Lt.	5.8	288.0
30' Lt.	5.7	288.1

0 + 51.28 = E.C.

293.83

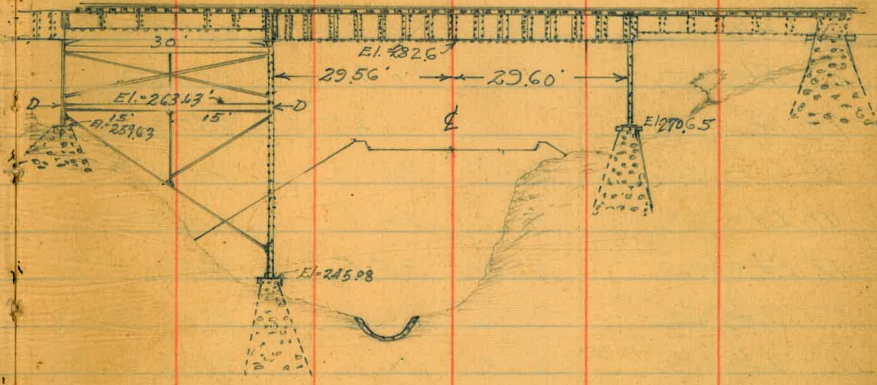
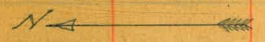
35' Lt.	6.2	287.6
18' Lt.	6.0	287.8
2	5.6	288.2
18' Rt.	4.9	288.9
40' Rt.	4.0	289.8
0+75		
45' Rt.	4.7	289.1
18' Rt.	5.2	288.6
2	5.8	288.0
18' Lt.	5.8	288.0
45' Lt.	6.5	287.3
1+00		
55' Lt.	6.6	287.2
18' Lt.	6.6	287.2
2	7.1	286.7
18' Rt.	6.5	287.3
57' Rt.	4.9	288.9
1+25		
60' Rt.	5.0	288.8
18' Rt.	7.6	287.2
2	7.4	286.4
18' Lt.	7.9	285.9
60' Lt.	6.7	287.1
1+76.77 = 80' Lt.		
70' Lt.	6.8	287.0
30' Lt.	9.2	284.6

293.83

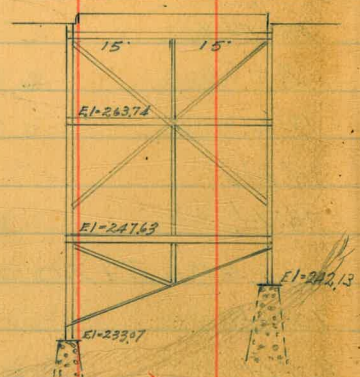
18' Lt.	9.3	284.5	9
2	9.4	284.4	
18' Rt.	9.0	284.8	
34' Rt.	8.3	285.5	
70' Rt.	6.9	286.9	
TR	4.64	287.38	11.09
2+00			282.74
70' Rt.		1.4	286.0
18' Rt.		3.2	284.2
2		4.1	283.3
18' Lt.		4.2	283.2
30' Lt.		3.8	283.6
70' Lt.		1.0	286.4
2+20			
70' Lt.		5.6	281.8
25' Lt.		10.0	277.4
18' Lt.		6.4	281.0
2		5.8	281.6
18' Rt.		4.8	282.6
70' Rt.		2.2	285.2
2+42.3 = "B" Line			
18' Rt.		5.9	281.5
11' Rt.		6.6	280.8
8' Rt.		9.0	278.4
2		7.0	280.4
7.7' Rt.		10.8	276.6

on p. 2, hub
page 7

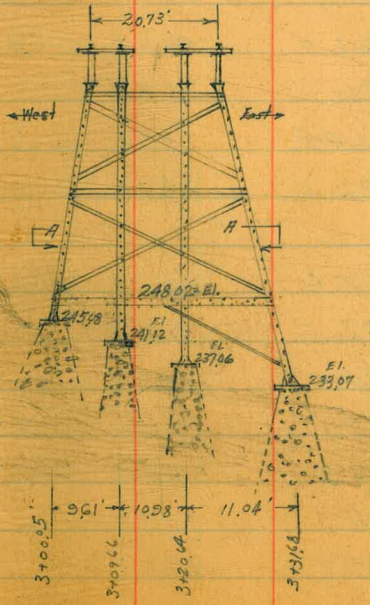
18' Lt.	14.0	272.8
28' Lt.	18.8	268.6
50' Lt.	15.2	272.2
63' Lt.	11.2	276.2
73' Lt.	10.4	277.0
81.2' Lt.	11.6	275.8



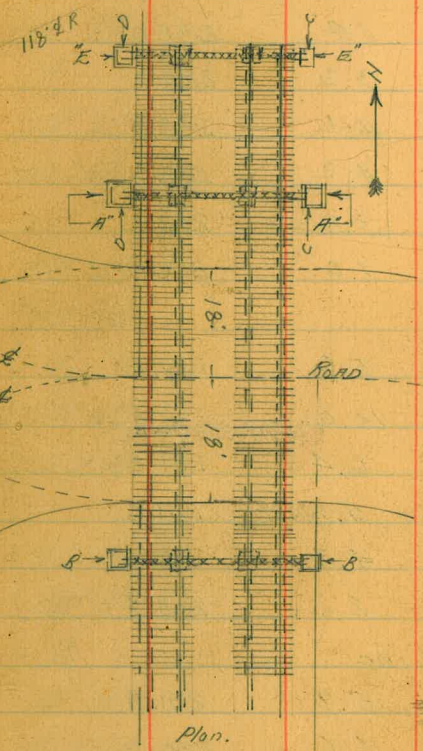
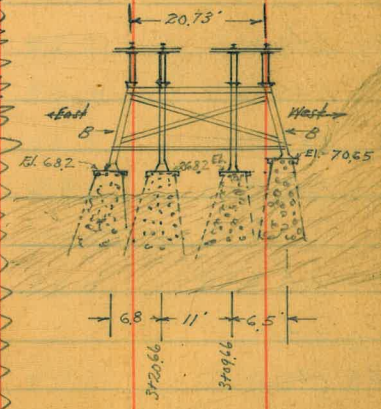
Section C-C



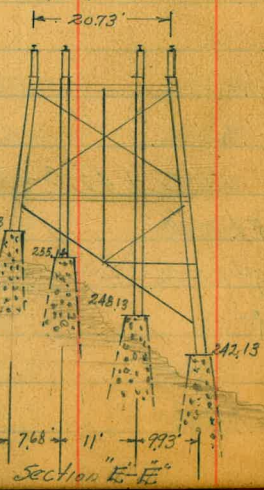
Section A-A



Section B-B



Plan.



Section E-E

100' ER

200' P 45° 30'

Cont. from Page 8

259.47

11

	↑ 271.01		20' Lt	28.2	231.3
116	259.47	12.70	18' Lt	24.7	234.8
	3+35.57	86. 58'30"	6	13.3	246.2
30' Rt.	+6.0	265.5	18' Rt.	1.2	258.3
23' Rt.	+0.9	260.4	30' Rt.	+5.3	264.8
18' Rt.	1.8	257.7			
2	14.0	245.5	3+75		
11' Lt.	18.8	240.7	30' Rt.	+6.4	265.9
18' Lt.	24.5	235.0	18' Rt.	1.8	257.7
21' Lt.	26.4	233.1	2	12.0	247.5
25' Lt.	31.0	228.5	10' Lt.	17.7	241.8
27' Lt.	28.1	231.4	18' Lt.	21.0	238.5
30' Lt.	27.8	231.7	30' Lt.	29.9	229.6
36' Lt.	27.0	232.5	41' Lt.	37.3	221.2
42' Lt.	26.6	232.9	49' Lt.	45.3	214.2
50' Lt.	24.4	235.1	53' Lt.	50.3	209.2
60' Lt.	22.0	237.5	60' Lt.	50.3	209.2
	3+50		61' Lt.	43.8	215.7
70' Lt.	28.6	230.9	72' Lt.	40.4	219.1
60' Lt.	32.5	227.0	86' Lt.	35.4	224.1
46' Lt.	34.0	225.5			
43' Lt.	37.1	222.4	4+00		
37' Lt.	37.3	222.2	106' Lt.	49.5	210.0
35' Lt.	34.5	225.0	91' Lt.	50.3	209.2
30' Lt.	33.9	225.6	86' Lt.	56.6	202.9
28' Lt.	32.2	227.3	74' Lt.	55.4	204.1
			68' Lt.	48.1	211.4
			30' Lt.	29.7	230.3

259.47

259.53

18' Lt.		22.8	236.7
L		13.5	246.0
18' Rt.		+0.4	259.9
30' Rt.		+3.8	268.3
T.P.	5.57	259.53	5.51 253.96
	4+25		
40' Rt.		+17.4	276.9
30' Rt.		+12.8	272.3
18' Rt.		+3.6	263.1
L		11.7	247.8
18' Lt.		20.4	239.1
30' Lt.		26.7	232.8
48' Lt.		37.0	222.5
78' Lt.		52.4	207.1
91' Lt.		56.0	203.5
98' Lt.		60.2	199.3
117' Lt.		61.8	197.7
123' Lt.		57.3	202.2
	4+50		
130' Lt.		63.7	195.8
132' Lt.		67.0	192.5
117' Lt.		67.0	192.5
109' Lt.		62.0	197.5
98' Lt.		57.2	202.3
63' Lt.		40.6	218.9
39' Lt.		28.6	230.9
15' Lt.		18.6	240.9

on 20th
12' Rt L
4+00

L		9.4	250.1
9' Rt.		4.0	255.5
18' Rt.		+4.3	263.8
20' Rt.		+5.8	265.3
30' Rt.		+9.5	269.0
35' Rt.		+11.5	271.0
	4+65		
35' Rt.		+9.3	268.8
18' Rt.		+2.5	262.0
12' Rt.		0.2	259.3
2' Rt.		3.6	255.9
L		5.0	254.5
12' Lt.		13.9	245.6
18' Lt.		18.0	241.5
31' Lt.		24.0	235.5
37' Lt.		27.6	231.9
44' Lt.		30.7	228.8
59' Lt.		38.4	221.1
72' Lt.		46.2	213.3
85' Lt.		51.3	208.2
103' Lt.		62.4	197.1
112' Lt.		71.0	188.5
122' Lt.		64.3	195.2
	4+80		
130' Lt.		63.0	196.5
116' Lt.		67.7	191.8

112' Lt.	70.2	189.3
104' Lt.	70.4	189.1
94' Lt.	58.1	201.4
84' Lt.	54.5	205.0
66' Lt.	45.4	214.1
53' Lt.	38.4	221.1
40' Lt.	32.9	226.6
18' Lt.	19.1	240.4
6' Lt.	9.3	250.2
L	7.0	252.5
12' Rt.	1.8	257.7
18' Rt.	+0.7	260.2
30' Rt.	+4.8	264.3
35' Rt.	+6.1	265.6
35' Rt.	+4.9	264.4
27' Rt.	+3.2	262.7
18' Rt.	0.6	258.9
6' Rt.	5.6	253.9
L	8.9	250.6
10' Lt.	12.3	247.2
18' Lt.	15.3	244.2
30' Lt.	25.2	234.3
43' Lt.	35.0	224.5
50' Lt.	38.2	221.3
66' Lt.	41.2	218.3

4+90

70' Lt.	45.4	214.1
81' Lt.	53.0	206.5
95' Lt.	60.6	198.9
107' Lt.	68.0	191.5
115' Lt.	75.2	184.3
130' Lt.	68.5	191.0
138' Lt.	64.4	195.1
105' Lt.	63.8	195.7
94' Lt.	58.4	201.1
81' Lt.	54.4	205.1
78' Lt.	51.0	208.5
70' Lt.	46.3	213.2
53' Lt.	40.6	218.9
33' Lt.	28.1	231.4
24' Lt.	19.8	240.7
18' Lt.	16.3	243.2
16' Lt.	15.1	144.4
6' Lt.	12.2	147.3
L	10.4	149.1
8' Rt.	6.7	252.8
18' Rt.	1.8	257.7
35' Rt.	+3.9	263.4
35' Rt.	+2.3	261.8
18' Rt.	4.8	256.7

5+00

5+15

259.53

259.53

252.1 14

8' Rt.	8.2	251.3
6	11.9	247.6
6' Lt.	15.4	244.1
18' Lt.	18.1	241.4
23' Lt.	19.3	240.2
30' Lt.	25.7	233.8
50' Lt.	39.1	220.4
65' Lt.	48.1	211.4
84' Lt.	55.1	204.4
105' Lt.	60.8	198.7
5+25		
96' Lt.	58.7	200.8
84' Lt.	56.0	203.5
75' Lt.	52.9	206.6
62' Lt.	45.8	213.7
49' Lt.	37.1	222.4
39' Lt.	30.6	228.9
33' Lt.	25.3	234.2
25' Lt.	20.7	238.8
18' Lt.	19.0	240.5
5' Lt.	15.8	243.7
6	13.1	246.4
18' Rt.	6.3	253.2
35' Rt.	11.0	260.5
5+39.77 = E.C.		
35' Rt.	0.0	259.5

18' Rt.	7.4	
chk. on B.M. ^{8.41}	259.52	8.41
T.P. 1.07	248.51	12.08
247.44		
2	3.7	244.8
10' Lt.	8.1	240.4
18' Lt.	9.9	238.6
30' Lt.	13.0	235.5
40' Lt.	17.5	231.0
53' Lt.	23.9	224.6
58' Lt.	27.4	221.1
70' Lt.	32.0	216.5
85' Lt.	39.6	208.9
5+50		
67' Lt.	28.1	220.4
59' Lt.	24.1	224.4
48' Lt.	21.7	226.8
35' Lt.	15.8	232.7
25' Lt.	12.8	235.7
18' Lt.	10.7	237.8
13' Lt.	9.3	239.2
2	3.1	245.4
8' Rt.	0.5	248.0
18' Rt.	+1.7	250.2
30' Rt.	+8.5	257.0
5+75		
30' Rt.	+5.8	254.3

251.11 on 466 15'
251.12 Pt. No. 5-137

18' Rt.	+ 0.6	249.1
Σ	6.5	242.0
10' Lt.	10.3	238.2
18' Lt.	11.9	236.6
30' Lt.	14.0	234.5
45' Lt.	19.7	228.8
60' Lt.	25.2	223.3
6+00		
45' Lt.	21.5	227.0
25' Lt.	14.2	234.3
18' Lt.	12.7	235.8
Σ	8.8	239.7
18' Rt.	2.1	246.4
30' Rt.	+ 3.0	251.5
6+25		
30' Rt.	0.1	248.4
18' Rt.	4.1	244.4
Σ	11.1	237.4
18' Lt.	16.9	231.6
30' Lt.	20.2	228.3
45' Lt.	24.1	224.4
6+50		
45' Lt.	27.1	221.4
30' Lt.	22.8	225.7
18' Lt.	19.1	229.4
12' Lt.	16.5	232.0

Σ	13.1	235.4
14' Rt.	7.0	241.5
18' Rt.	5.5	243.0
30' Rt.	2.4	246.1
7+00		
30' Rt.	3.9	244.6
18' Rt.	9.1	239.4
7' Rt.	11.7	236.8
Σ	14.8	233.7
8' Lt.	18.5	230.0
18' Lt.	20.1	228.4
26' Lt.	22.2	226.3
45' Lt.	29.8	218.7
7+27		
45' Lt.	32.0	216.5
24' Lt.	23.8	224.7
18' Lt.	22.2	226.3
8' Lt.	19.3	229.2
Σ	16.5	232.0
10' Rt.	12.9	235.6
18' Rt.	10.5	238.0
34' Rt.	3.0	245.5
7+50		
35' Rt.	4.7	243.8
18' Rt.	12.4	236.1
T.P.	11.3	237.43
12.21	236.30	

6' Rt.	4.9	232.5
£	6.7	230.7
5' Lt.	8.4	229.0
18' Lt.	13.2	224.2
30' Lt.	16.6	220.8
45' Lt.	22.3	215.1
7+69.77 = 80.		
45' Lt.	23.0	214.4
30' Lt.	17.9	219.5
18' Lt.	13.7	223.7
12' Lt.	11.8	225.6
£	8.4	229.0
18' Rt.	1.3	236.1
30' Rt.	+4.7	242.1
35' Rt.	+7.1	244.5
40' Rt.	+8.6	246.0
8+00		
40' Rt.	+8.8	246.6
23' Rt.	+1.7	239.1
18' Rt.	1.0	236.4
£	9.3	228.1
7' Lt.	11.4	226.0
18' Lt.	14.2	223.2
30' Lt.	18.5	218.9
44' Lt.	23.1	214.3

8+25

42' Lt.	24.4	213.0
24' Lt.	17.1	220.3
18' Lt.	15.2	222.2
5' Lt.	12.4	225.0
£	10.8	226.6
18' Rt.	2.1	235.3
30' Rt.	+3.7	241.1
45' Rt.	+10.0	247.4
8+50		
45' Rt.	+8.6	246.0
30' Rt.	+1.8	239.2
18' Rt.	1.8	235.6
£	10.9	226.5
7' Lt.	13.6	223.8
18' Lt.	15.9	221.5
30' Lt.	21.1	216.3
TP	1.13	227.69
8+75		
45' Lt.	18.3	209.4
30' Lt.	11.8	215.9
18' Lt.	8.1	219.6
£	2.4	225.3
12' Rt.	+3.2	230.9
18' Rt.	+5.0	232.7
36' Rt.	+4.4	242.1
46' Rt.	+18.0	245.7

00254106£

8+35.22

9+00

50' Rt.	+16.8	244.5
40' Rt.	+13.0	240.7
28' Rt.	+6.0	233.7
18' Rt.	+1.9	229.6
2	3.1	224.6
18' Lt.	9.0	218.7
30' Lt.	13.4	214.3

18' Lt.	15.8	211.9
6' Lt.	13.1	214.6
2	11.4	216.3
10' Rt.	8.4	219.3
18' Rt.	5.3	222.4
25' Rt.	2.9	224.8
30' Rt.	1.9	225.8
40' Rt.	+0.5	228.2

9+50

10+17.60 = B.C.

30' Lt.	14.5	213.2
18' Lt.	10.4	217.3
2	6.6	221.1
18' Rt.	1.1	226.6
30' Rt.	+3.1	230.8
40' Rt.	+6.9	234.6

40' Rt.	1.6	226.1
25' Rt.	4.3	223.4
18' Rt.	6.1	221.6
6' Rt.	11.3	216.4
2	13.5	214.2
18' Lt.	17.9	209.8
30' Lt.	20.9	206.8

9+75

10+35

45' Rt.	+5.2	232.9
30' Rt.	+1.2	228.9
18' Rt.	3.6	224.1
9' Rt.	6.2	221.5
2	8.5	219.2
18' Lt.	11.7	216.0
25' Lt.	13.5	214.2
30' Lt.	15.5	212.2

30' Lt.	22.1	205.6
18' Lt.	18.3	209.4
7' Lt.	17.0	210.7
2	15.4	212.3
12' Rt.	10.7	217.0
18' Rt.	9.7	218.0
30' Rt.	6.0	221.7
40' Rt.	2.9	224.8

10+00

10+69.96 = E.C.

30' Lt.	18.2	209.5
---------	------	-------

20' Rt. 5.6 221.1
 30' Rt. 9.2 218.5
 18' Rt. 12.3 215.4
 7' Rt. 14.2 213.5
 L 16.9 210.8
 18' Lt. 23.5 204.2
 30' Lt. 26.5 201.2

11+00

30' Lt. 29.2 198.5
 22' Lt. 26.5 201.2
 18' Lt. 25.2 202.5
 L 19.9 207.8
 10' Rt. 16.6 211.1
 18' Rt. 15.5 212.2
 30' Rt. 13.2 214.5
 40' Rt. 10.3 216.4

T.P. 2.12 217.96 11.85 215.84

11+25

42' Rt. 2.7 215.2
 18' Rt. 9.3 208.6
 L 13.8 204.1
 18' Lt. 17.2 200.7
 30' Lt. 20.2 197.7

11+50

30' Lt. 22.2 195.7
 18' Lt. 20.9 197.0

217.96

10' Lt. 19.7 198.2
 L 17.2 200.7
 18' Rt. 13.4 204.5
 30' Rt. 10.7 207.2
 35' Rt. 9.8 208.1
 T.P. 1.43 206.73 12.66 205.30

11+75

36' Rt. 1.8 204.9
 30' Rt. 3.0 203.7
 18' Rt. 5.1 201.6
 L 10.1 196.6
 18' Lt. 13.4 193.3
 30' Lt. 15.0 191.7

12+00

30' Lt. 20.0 186.7
 18' Lt. 17.1 189.6
 L 13.7 193.0
 18' Rt. 8.2 199.5
 30' Rt. 5.9 200.8

12+25

30' Rt. 9.7 197.0
 18' Rt. 12.9 193.8
 L 17.7 189.0
 18' Lt. 22.1 184.6
 30' Lt. 24.3 182.4
 36' Lt. 35.5 181.2

12+50		
45' Lt.	33.8	172.9
40' Lt.	32.0	174.7
18' Lt.	27.0	179.7
11' Lt.	25.2	181.5
Σ	21.8	184.9
18' Rt.	16.3	190.4
30' Rt.	12.8	193.9
T.P.	0.36	194.27
	12.82	193.91

12+75		
30' Rt.	1.8	192.5
18' Rt.	5.1	189.2
Σ	11.3	183.0
18' Lt.	16.5	177.8
30' Lt.	20.3	174.0
40' Lt.	24.0	170.3
50' Lt.	28.6	165.7
60' Lt.	33.1	161.2
70' Lt.	37.3	157.0

13+00		
50' Lt.	26.8	167.5
30' Lt.	18.5	175.8
18' Lt.	15.6	178.7
Σ	9.8	184.5
18' Rt.	3.9	190.4
30' Rt.	10.2	194.5

36' Rt.	+2.3	196.6
13+32		
36' Rt.	+5.1	199.4
30' Rt.	+3.4	197.7
18' Rt.	0.3	194.0
5' Rt.	2.9	191.4
Σ	4.4	189.9
18' Lt.	10.7	183.6
30' Lt.	15.1	179.2
42' Lt.	17.2	177.1

13+50		
40' Lt.	16.4	177.9
30' Lt.	13.7	180.6
18' Lt.	9.7	184.6
Σ	3.6	190.7
18' Rt.	+1.0	195.3
30' Rt.	+4.6	198.9
40' Rt.	+7.0	201.3

13+75		
40' Rt.	+6.8	201.1
18' Rt.	+0.9	195.2
Σ	5.5	188.8
10' Lt.	8.5	185.8
18' Lt.	10.6	183.7
30' Lt.	13.9	180.4

13+82

30' Lt.	13.8	180.5
18' Lt.	9.8	184.5
6' Lt.	8.9	186.3
Σ	5.9	188.4
18' Rt.	0.0	194.3
38' Rt.	+5.7	200.0
45' Rt.	+7.5	202.8
14+00		
40' Rt.	+3.3	197.6
30' Rt.	+0.8	195.1
18' Rt.	2.4	191.9
Σ	7.3	187.0
12' Lt.	10.8	183.5
18' Lt.	11.9	182.4
30' Lt.	15.0	179.3
14+2.5		
30' Lt.	18.7	175.6
18' Lt.	15.7	178.6
Σ	10.5	183.8
18' Rt.	6.9	187.4
30' Rt.	5.9	188.4
35' Rt.	5.6	188.7
14+50		
30' Rt.	11.1	183.2
18' Rt.	11.5	182.8
Σ	15.3	179.0

18' Lt.	19.2	175.1
30' Lt.	22.3	172.0
14+75		
30' Lt.	26.9	167.4
18' Lt.	22.9	171.4
8' Lt.	19.8	174.5
Σ	18.5	175.8
18' Rt.	16.3	178.0
30' Rt.	16.7	178.1
T.P.	0.29	182.33
15+00		
30' Rt.	8.7	173.6
18' Rt.	8.0	174.3
Σ	8.8	173.5
12' Lt.	10.5	171.8
18' Lt.	13.1	169.2
30' Lt.	20.0	162.3
15+12		
42' Lt.	30.3	152.0
30' Lt.	25.6	156.7
18' Lt.	18.1	164.2
Σ	11.1	171.2
14' Rt.	10.8	171.5
18' Rt.	11.5	170.8
30' Rt.	14.2	168.1
T.P.	0.41	169.82
12.92	169.41	

on Rt. 20' Rt.
14+60

15+35

45' Rt.	16.3	153.5
30' Rt.	12.9	156.9
18' Rt.	11.0	158.8
Σ	10.1	159.7
18' Lt.	16.3	159.5
30' Lt.	21.1	148.7
44' Lt.	26.0	143.8
56' Lt.	30.0	139.8
67' Lt.	32.7	137.1
68' Lt. = W. edge bridle path	34.6	135.2
80' Lt.	34.1	135.7

15+56 = B.C. Lt.

67' Lt.	34.7	135.1
56' Lt. = W. edge bridle path	34.9	134.9
55' Lt.	33.6	136.2
35' Lt.	30.5	139.3
18' Lt.	24.9	144.9
Σ	21.6	148.2
18' Rt.	21.6	148.2
35' Rt.	22.4	147.4
47' Rt.	21.6	148.2

T.P.	2.05	160.00	11.87	157.95	on 2466
T.P.	1.15	149.62	11.53	148.47	15+56 = B.C. Lt.

15+75

70' Rt.	2.0	147.6
---------	-----	-------

64' Rt.	2.5	147.1
55' Rt. bottom ditch	10.2	139.4
43' Rt.	3.4	146.2
18' Rt.	5.5	144.1
Σ	6.3	143.3
18' Lt.	9.1	140.5
30' Lt.	11.3	138.3
45' Lt.	13.2	136.4
46' Lt. = W. edge bridle path	14.3	135.3
60' Lt. = E " " "	14.0	135.6
66' Lt.	15.5	134.1
75' Lt.	16.5	133.1

16+00

75' Lt.	17.1	132.5
55' Lt.	15.2	134.4
47' Lt. = E. edge bridle path	13.8	135.8
31' Lt. = W " " "	13.9	135.7
30' Lt.	11.9	137.7
18' Lt.	10.2	139.4
Σ	8.7	140.9
18' Rt.	6.8	142.8
27' Rt.	6.6	143.0

35' Rt.	12.3	137.3
46' Rt.	5.9	143.7
58' Rt.	5.0	144.6

16+25

16+25

62' Rt.	4.7	144.9
45' Rt. - top Bank	8.3	141.3
41' Rt. - bottom ditch	13.0	136.6
33' Rt. = " "	13.0	136.6
27' Rt. = top Bank.	8.5	141.1
18' Rt.	9.0	140.6
2	10.4	139.2
10' Lt.	11.3	138.3
11' Lt. - W. edge bridle path	13.6	136.0
18' Lt. in " "	13.8	135.8
30' Lt. E " " "	13.7	135.9
37' Lt.	15.3	134.3
75' Lt.	18.9	130.7

16+50

75' Lt.	19.8	129.8
54' Lt.	19.0	130.6
38' Lt.	17.8	131.8
18' Lt.	14.4	135.2
6' Lt.	12.7	136.9
3' Lt.	13.6	136.0
2	13.8	135.8
14' Rt.	14.0	135.6
15' Rt.	12.0	137.6
18' Rt.	11.7	137.9
31' Rt.	11.4	138.2
32' Rt.	13.9	135.7

42' Rt.	14.5	135.1
48' Rt.	11.1	138.5
58' Rt.	9.6	140.0
T.P.	1.90	138.75
	12.77	136.85

N.Y. Co. High Wk
24" Con. Culvert
on highest top

16+75

70' Rt.	2.5	136.2
48' Rt.	3.1	135.6
44' Rt. - W. edge bridle path	4.1	134.6
30' Rt. - E " "	3.7	135.0
24' Rt.	3.8	135.0
18' Rt.	5.0	133.7
2	5.7	133.0
18' Lt.	7.6	131.1
30' Lt.	8.9	129.8
60' Lt.	9.4	129.3
72' Lt. - top Bank of channel	10.0	128.7
76' Lt. - Bottom " "	13.5	125.2
86' Lt. = " "	13.1	125.6
88' Lt. - top Bank of "	10.4	128.3

17+00

85' Lt.	10.6	128.1
75' Lt. top of Bank.	10.9	127.8
73' Lt. Bottom channel	12.7	126.0
60' " " "	13.1	125.6
59' " top Bank "	10.1	128.6
36' Lt.	9.7	129.0

17+00 cont.

18' Lt.	8.8	129.9
2	8.0	130.7
18' Rt.	7.1	131.6
30' Rt.	7.2	131.5
54' Rt.	6.1	132.6
62' Rt.	4.0	134.7
79' Rt.	3.7	135.0
17+25		
71' Rt.	6.4	132.3
64' Rt.	7.5	131.2
34' Rt.	8.3	130.4
18' Rt.	9.0	129.7
2	9.2	129.5
18' Lt.	9.5	129.2
51' Lt. at channel	10.2	128.5
52' Bot. "	13.0	125.7
65' " "	12.8	125.9
72' top "	11.0	127.7
17+50		
70' Lt. top channel	11.5	127.2
67' " Bot. "	13.2	125.5
46' " " "	13.2	125.5
45' " top "	10.7	128.0
18' Lt.	10.6	128.1
2	10.7	128.0
18' Rt.	10.8	128.0

35' Rt.	10.6	128.1
51' Rt.	10.1	128.7
63' Rt.	9.5	129.2
74' Rt.	8.5	130.2
17+80		
70' Rt.	13.8	125.0
65' Rt.	13.2	125.6
41' Rt.	13.3	125.5
18' Rt.	12.5	126.2
2	12.3	126.4
18' Lt.	12.2	126.5
38' Lt. - top channel	11.5	127.2
40' Lt. = Bot. "	13.8	125.0
63' Lt. = " "	13.3	125.4
72' Lt.	11.7	127.0
17+85		
70' Lt. - top channel	11.7	127.0
64' Lt. - Bot. "	13.7	125.0
18' Lt. = " "	14.7	124.0
2 - " "	14.6	124.1
18' Rt. = " "	16.2	122.5
60' Rt. = " "	16.3	122.4
70' Rt. = " "	16.4	122.3
17+95 = East edge channel		
70' Rt.	16.3	122.4
18' Rt.	16.2	122.5

2		14.6	124.1
18' Lt.		14.5	124.2
64' Lt.		13.5	125.2
70' Lt.		11.7	127.0
T.P.	6.74 133.13	12.36	126.39
	18+00		18+36.89
75' Lt.		6.1	127.0
55' Lt.		8.1	125.0
18' Lt.		9.1	124.0
2		10.2	122.9
3' Rt.		8.2	124.9
18' Rt.		7.6	125.5
30' Rt.		7.3	125.8
54' Rt.		8.3	124.8
66' Rt.		8.0	125.1
	18+15		
73' Rt.		6.4	126.7
51' Rt.		8.9	124.2
18' Rt.		7.4	125.7
2		6.5	126.6
18' Lt.		6.3	126.8
57' Lt.		6.1	127.0
	18+50		
63' Lt.		6.2	126.9
30' Lt.		6.5	126.6
18' Lt.		6.8	126.3

2		7.2	125.9
18' Rt.		7.5	125.6
60' Rt.		7.8	125.3
	18+62		
60' Rt.		8.0	125.1
18' Rt.		8.1	125.0
2		8.2	124.9
18' Lt.		7.6	125.5
38' Lt.		6.5	126.6
60' Lt.		4.6	128.5
	18+85		
50' Lt.		2.9	130.2
30' Lt.		5.3	127.8
18' Lt.		5.9	127.2
2		6.5	126.6
18' Rt.		7.3	125.8
60' Rt.		8.2	124.9
	19+00		
60' Rt.		7.8	125.3
18' Rt.		6.4	126.7
2		5.6	127.5
18' Lt.		4.1	129.0
30' Lt.		2.2	130.9
50' Lt.		0.7	132.4
T.P.	6.53 138.71	0.95	132.18
	19+25		

138.11
19+25
chk. on "A" line 39+50
6.60 138.52
6.60 132.11
- corrected
131.92 = B.M.

Powder Canyon

50' Lt. 5.1 133.4
18' Lt. 6.4 132.1
Σ 7.2 131.3
18' Rt. 7.6 130.9
50' Rt. 8.3 130.2
19+65
50' Rt. 8.1 130.4
40' Rt. 6.9 131.6
18' Rt. 5.7 132.8
Σ 5.1 133.4
18' Lt. 4.4 134.1
30' Lt. 4.1 134.4
50' Lt. 3.9 134.6

19+82

50' Lt. 4.8 133.7
30' Lt. 6.0 132.5
18' Lt. 6.3 132.2
Σ 5.9 132.6
18' Rt. 5.7 132.8
33' Rt. 6.7 131.8
45' Rt. 7.8 130.7

19+92

50' Rt. 10.2 128.3

138.52
18' Rt. 9.7 128.8
Σ 9.6 128.9
18' Lt. 9.2 129.3
30' Lt. 9.0 129.5
50' Lt. 8.9 129.6

20+00

50' Lt. 9.5 129.0
30' Lt. 9.8 128.7
18' Lt. 9.4 129.1
Σ 10.0 128.5
18' Rt. 11.1 127.4
50' Rt. 12.4 126.1

20+24.71 = B.C. Lt. 38° Σ R = 300'

50' Rt. 10.7 127.8
18' Rt. 10.2 128.3
Σ on Hub 9.55 129.0
5' Lt. 11.8 126.7
30' Lt. 11.3 127.2
50' Lt. 11.1 127.4

20+30

50' Lt. 8.4 130.1
18' Lt. 9.0 129.5
Σ 9.4 129.1
18' Rt. 10.0 128.5
50' Rt. 10.4 128.1

20+50

50' Rt.	6.7	131.8
30' Rt.	7.2	131.3
18' Rt.	8.0	130.5
↳	8.3	130.2
18' Lt.	8.0	130.5
50' Lt.	7.7	130.8

20+75

57' Lt.	7.0	131.5
30' Lt.	6.7	131.8
18' Lt.	6.4	132.1
↳	5.2	133.3
18' Rt.	3.8	134.7
50' Rt.	1.8	136.7
T.P.	12.67	150.05
	114	137.38

21+00

50' Rt.	5.5	144.5
30' Rt.	8.3	141.7
18' Rt.	10.4	139.6
↳	12.2	137.8
18' Lt.	14.3	135.7
30' Lt.	15.3	134.7
50' Lt.	15.5	134.5

21+25

54' Lt.	13.0	137.0
42' Lt.	11.0	139.0

30' Lt.	2.5	140.5
18' Lt.	7.7	142.3
↳	5.3	144.7
18' Rt.	1.7	148.3
30' Rt.	+1.0	151.0

21+50

47' Rt.	+19.6	169.6
38' Rt.	+18.3	168.3
30' Rt.	+15.8	165.8
18' Rt.	+10.8	160.8
↳	+4.3	154.3
18' Lt.	1.5	148.5
30' Lt.	5.0	145.0
T.P.	12.72	162.26
	0.51	149.54

21+75

42' Lt.	17.5	144.8
30' Lt.	12.7	149.6
18' Lt.	7.2	155.1
↳	+1.1	163.4
18' Rt.	+9.3	171.6
30' Rt.	+13.7	176.0
39' Rt.	+17.8	180.1
48' Rt.	+21.8	184.1
53' Rt.	+24.0	186.3
61' Rt.	+27.0	189.3
65' Rt.	+27.5	189.8

T.P. 12.05 173.88 0.43 161.83 ^{on Spindel} 3'4" 21+75

22+00

70' Rt.	+30.9	204.2
	+28.3	202.2
58' Rt.	+23.8	197.7
45' Rt.	+16.9	190.8
30' Rt.	+9.9	183.8
18' Rt.	+5.3	179.2
2	5.3	168.6
18' Lt.	14.8	159.1
30' Lt.	20.9	153.0
40' Lt.	25.6	148.3

22+23.68 = Ec.

41' Lt.	26.3	147.6
30' Lt.	21.7	152.8
18' Lt.	15.4	158.5
2	5.3	168.6
18' Rt.	+5.4	179.3
27' Rt.	+10.4	184.3
42' Rt.	+19.4	193.3
53' Rt.	+25.7	199.6
62' Rt.	+30.0	203.9
74' Rt.	+35.7	209.6
80' Rt.	+38.1	212.0

22+50

82' Rt.	+36.4	210.3
64' Rt.	+29.2	203.1

46' Rt.	+21.8	195.7
35' Rt.	+16.7	190.6
18' Rt.	+7.5	181.4
2	3.8	170.1
8' Lt.	7.5	166.4
18' Lt.	15.0	158.9
30' Lt.	20.7	153.2
40' Lt.	26.3	147.6

22+75

40' Lt.	24.6	149.3
25' Lt.	16.2	157.7
18' Lt.	12.6	161.3
2	1.9	172.0
10' Rt.	+2.6	176.5
18' Rt.	+8.3	182.2
30' Rt.	+13.4	187.3
47' Rt.	+20.0	193.9
67' Rt.	+27.0	200.9
84' Rt.	+33.6	207.5

23+00

60' Rt.	+16.1	190.0
39' Rt.	+11.1	185.0
30' Rt.	+7.2	181.1
18' Rt.	+4.4	178.3
8' Rt.	+1.2	175.1
2	2.3	170.6

115.88

18' Lt.	11.5	162.4
35' Lt.	21.4	152.5
23+17		
36' Lt.	23.8	150.1
22' Lt.	17.7	156.2
18' Lt.	13.2	160.7
9' Lt.	8.5	165.4
2	6.7	167.2
18' Rt.	3.2	170.7
36' Rt.	0.3	173.6
T.P.	12.21	180.84
23+34.54 = B.C.		
30' Rt.	16.0	164.8
18' Rt.	18.0	162.8
2	21.2	159.6
7' Lt.	22.7	158.1
18' Lt.	27.3	153.5
30' Lt.	31.4	149.4
40' Lt.	33.5	147.3
23+50		
50' Lt.	37.5	143.3
30' Lt.	33.0	147.8
18' Lt.	30.8	150.0
2	26.9	153.9
18' Rt.	23.8	157.0
40' Rt.	20.4	160.4

180.84

28

23+64

40' Rt.	22.9	157.9
18' Rt.	26.7	154.1
2	30.6	150.2
18' Lt.	32.8	148.0
40' Lt.	35.6	145.2
50' Lt.	37.0	143.8
23+75		
50' Lt.	34.0	146.8
30' Lt.	29.4	151.4
18' Lt.	28.0	151.8
2	26.5	154.3
18' Rt.	24.0	156.8
30' Rt.	20.6	160.2
40' Rt.	18.6	162.2
24+00		
30' Rt.	8.4	172.4
18' Rt.	10.8	170.0
13' Rt.	10.9	169.9
2	16.2	164.6
18' Lt.	20.1	160.7
30' Lt.	23.5	157.3
42' Lt.	27.1	153.7
24+13		
40' Lt.	24.9	155.9
30' Lt.	21.8	159.0

18' Lt.	17.3	163.5
6' Lt.	12.8	168.0
6	9.3	171.5
18' Rt.	4.7	176.1
35' Rt.	3.5	177.3
40' Rt.	2.8	178.0

24+30

55' Rt.	+7.0	187.8
30' Rt.	+3.5	184.3
18' Rt.	0.0	180.8
6	6.9	173.9
10' Lt.	10.7	170.1
18' Lt.	14.9	165.9
30' Lt.	21.0	159.8
42' Lt.	25.6	155.2

24+35

47' Lt.	26.3	154.5
30' Lt.	20.1	160.7
18' Lt.	14.2	166.6
6	6.2	174.6
18' Rt.	+2.3	183.1
37' Rt.	+10.0	190.8
50' Rt.	+15.1	195.9

24+75

52' Rt.	+18.8	199.6
39' Rt.	+13.9	294.7

18' Rt.	+3.8	184.6
6	3.7	177.1
18' Lt.	12.8	168.0
30' Lt.	17.7	163.1
50' Lt.	24.8	156.0

2.5+00

50' Lt.	24.4	156.4
30' Lt.	15.7	165.1
18' Lt.	10.1	170.7
6	1.8	179.0
10' Rt.	+3.4	184.2
18' Rt.	+7.1	187.9
22' Rt.	+8.6	189.4
33' Rt.	+14.9	195.7
50' Rt.	+21.5	202.3
55' Rt.	+22.0	202.8

2.5+25

56' Rt.	+25.0	205.8
46' Rt.	+21.4	202.2
27' Rt.	+13.8	194.6
18' Rt.	+8.8	189.6
12' Rt.	+6.3	187.1
6	1.2	179.6
18' Lt.	10.0	170.8
30' Lt.	14.3	166.5
41' Lt.	21.3	159.5

25+50

45 Lt.	21.8	159.0
31 Lt.	17.2	163.6
18 Lt.	9.1	171.7
T.P.	12.40	189.50
Σ	3.74	177.10
18 Rt.	8.8	180.7
30 Rt.	1.1	188.4
48 Rt.	+5.0	194.5
58 Rt.	+14.8	204.3
	+18.1	207.6

25+75

56 Rt.	+17.7	207.2
44 Rt.	+12.6	202.1
30 Rt.	+5.7	195.2
18 Rt.	0.7	188.8
Σ	9.1	180.4
18 Lt.	17.4	172.1
30 Lt.	23.7	165.8
50 Lt.	34.1	155.4

26+00

78 Lt.	45.1	144.4
68 Lt.	48.4	141.1
56 Lt.	38.5	151.0
34 Lt.	26.9	162.6
18 Lt.	18.0	171.5
Σ	9.1	180.4

18 Rt.	0.4	189.1
30 Rt.	+4.2	193.7
55 Rt.	+17.4	206.9

26+25

54 Rt.	+18.6	208.1
46 Rt.	+15.5	205.0
30 Rt.	+7.0	196.5
18 Rt.	+1.9	191.4
10 Rt.	3.3	186.2
Σ	7.1	182.4
18 Lt.	16.1	173.4
30 Lt.	22.1	167.4
53 Lt.	34.9	154.6
64 Lt.	38.8	150.7

26+50

66 Lt.	36.5	153.0
48 Lt.	30.4	159.1
30 Lt.	21.7	167.8
18 Lt.	15.0	174.5
Σ	5.5	184.0

T.P.	11.76	198.67	2.59	186.91
chk. on	BM. TP - P-41	^{Book 1397} 9.45	189.22	
		^{corrected} 9.45	198.72	temp. BM. TP
18 Rt.		6.5	192.2	
30 Rt.		1.5	197.2	
40 Rt.		+4.8	203.5	

50' Rt.	+ 8.5	207.2
26+75		
45' Rt.	+ 2.5	201.2
30' Rt.	5.7	193.0
18' Rt.	9.7	189.0
10' Rt.	14.0	184.7
Σ	17.6	181.1
18' Lt.	26.0	172.7
30' Lt.	33.6	165.1
50' Lt.	40.0	158.7
56' Lt.	41.2	157.5
27+00		
63' Lt.	41.8	156.9
51' Lt.	40.6	158.1
45' Lt.	39.4	159.3
38' Lt.	35.7	163.0
18' Lt.	27.5	171.2
8' Lt.	26.0	172.7
Σ	23.1	175.6
18' Rt.	17.8	180.9
30' Rt.	12.6	186.1
27+18		
30' Rt.	19.6	179.1
18' Rt.	24.9	173.8
Σ	28.8	169.9
18' Lt.	25.6	173.1

30' Lt.	30.5	168.2
40' Lt.	31.0	167.7
50' Lt.	32.7	166.0
27+25		
50' Lt.	30.7	168.0
30' Lt.	26.8	171.9
18' Lt.	25.0	173.7
Σ	24.1	174.6
18' Rt.	23.2	175.5
30' Rt.	22.0	176.7
39' Rt.	18.2	180.5
27+35.97 = EG.		
43' Rt.	19.3	179.4
30' Rt.	19.8	178.9
18' Rt.	18.2	180.5
Σ	18.6	180.1
18' Lt.	19.8	178.9
30' Lt.	22.4	176.3
48' Lt.	27.4	171.3
27+50		
50' Lt.	27.2	171.5
30' Lt.	19.0	179.7
18' Lt.	15.2	183.5
Σ	12.0	186.7
18' Rt.	13.0	185.7
30' Rt.	14.5	184.2

27+75

38' Rt.	+1.3	200.0
18' Rt.	+1.1	199.8
2	3.4	195.3
18' Lt.	3.8	188.9
30' Lt.	15.5	183.2

28+00

40' Lt.	21.6	177.1
30' Lt.	17.5	181.2
18' Lt.	12.2	186.5
2	2.4	196.3
18' Rt.	+7.0	205.7
26' Rt.	+11.0	209.7
45' Rt.	+16.9	215.6
50' Rt.	+18.4	217.1

28+25

55' Rt.	+26.8	215.5
25' Rt.	+14.6	213.3
18' Rt.	+11.5	210.2
9' Rt.	+5.3	204.0
2	+1.7	200.4
11' Lt.	3.3	195.4
18' Lt.	7.7	191.0
30' Lt.	14.5	184.2
46' Lt.	22.0	176.7

45' Lt.	21.3	177.4
18' Lt.	6.3	192.4
2	+3.9	202.6
18' Rt.	+13.6	212.3
46' Rt.	+27.0	225.7
56' Rt.	+31.0	229.7

28+75

60' Rt.	+34.3	233.0
50' Rt.	+30.1	228.8
30' Rt.	+20.0	218.7
18' Rt.	+13.9	212.6
2	+4.6	203.3
18' Lt.	4.8	193.9
30' Lt.	11.2	187.5
40' Lt.	16.5	182.2

29+00

45' Lt.	18.1	180.6
30' Lt.	10.6	188.1
18' Lt.	3.9	194.8
2	+4.9	203.6
18' Rt.	+14.0	212.7
38' Rt.	+23.8	222.5
55' Rt.	+33.0	231.7

29+25

56' Rt.	+32.8	231.5
46' Rt.	+27.7	226.4

30' RT		+19.6	218.3
18' RT		+13.4	212.1
2		+5.7	204.4
18' LT		2.6	196.1
30' LT		9.2	189.5
40' LT		13.4	185.3
29+50			
40' LT		10.4	188.3
30' LT		7.0	191.7
18' LT		0.5	198.2
T.P.	12.71	210.30	1.13 197.59
2		4.1	206.2
18' RT		+4.2	214.5
28' RT		+9.0	219.3
45' RT		+17.0	227.3
57' RT		+23.3	233.6
T.P.	10.71	217.22	3.79 206.51
29+75			
60' RT		+18.2	235.4
46' RT		+13.4	230.6
30' RT		+5.6	222.8
18' RT		+0.6	217.8
2		8.0	209.2
6' LT		10.3	206.9
18' LT		15.8	201.4
30' LT		21.0	196.2

on Lot 18' LT
30' RT
29+45

on Lot 18' LT
30' RT
29+50

45' LT		28.2	189.0
30+00			
45' LT		25.6	191.6
30' LT		19.7	197.5
18' LT		13.9	203.3
2		6.2	211.0
18' RT		+2.5	219.7
30' RT		+7.6	224.8
50' RT		+16.0	233.2
60' RT		+19.1	236.3
30+25			
55' RT		+17.0	234.2
40' RT		+12.0	229.2
18' RT		+2.4	219.6
8' RT		1.1	216.1
2		5.1	212.1
18' LT		12.3	204.9
30' LT		16.7	200.5
44' LT		23.3	193.9
30+50			
45' LT		23.7	193.5
34' LT		18.8	198.4
18' LT		11.5	205.7
2		4.2	213.0
18' RT		+3.7	220.9
30' RT		+8.4	225.6

52' Rt.	+15.7	232.9
30' Rt.		
52' Rt.	+14.5	231.7
30' Rt.	+8.0	225.2
18' Rt.	+3.5	220.7
12' Rt.	+1.1	218.3
8' Rt.	2.0	215.2
ℓ	5.1	212.1
18' Lt.	12.2	205.0
30' Lt.	17.5	199.7
40' Lt.	22.4	194.8
40' Lt.	25.3	191.9
18' Lt.	14.4	202.8
ℓ	6.4	210.8
18' Rt.	+1.1	218.3
30' Rt.	+5.2	222.4
54' Rt.	+12.8	230.0
45' Rt.	+7.1	224.3
30' Rt.	+3.2	220.4
18' Rt.	0.5	216.7
8' Rt.	5.5	211.7
ℓ	9.0	208.2
18' Lt.	17.0	200.2
30' Lt.	22.5	194.7

31+00

31+25

42' Lt.	27.9	189.3
50' Lt.	31.6	175.6
62' Lt.	36.9	180.3
72' Lt.	39.6	177.6
73' Lt.	39.9	177.3
38' Lt.	27.3	189.9
30' Lt.	23.9	193.3
18' Lt.	19.5	197.7
ℓ	12.4	204.8
18' Rt.	7.1	210.1
30' Rt.	2.0	215.2
30' Rt.	1.3	215.9
18' Rt.	10.1	207.1
ℓ	17.8	199.4
18' Lt.	24.6	192.6
30' Lt.	27.0	190.2
56' Lt.	33.5	183.7
66' Lt.	36.3	180.9
60' Lt.	31.3	185.9
37' Lt.	26.3	190.9
30' Lt.	23.3	193.9
18' Lt.	18.9	198.3
ℓ	11.8	205.4

31+35

31+45

31+60

18' Rt.		3.7	213.5
30' Rt.		+0.9	218.1
T.P	12.90	222.90	7.22 210.00
	31+86		
35' Rt.		+5.0	227.9
30' Rt.		+4.3	227.2
18' Rt.		0.6	222.3
♀		7.9	215.0
12' Lt.		12.9	210.0
18' Lt.		17.0	205.9
30' Lt.		22.3	200.6
50' Lt.		30.4	192.5
65' Lt.		36.8	186.1
	32+00		
65' Lt.		35.5	187.4
41' Lt.		25.7	197.2
30' Lt.		20.9	202.0
18' Lt.		15.3	207.6
♀		7.4	215.5
5' Rt.		4.8	218.1
18' Rt.		+0.8	223.7
35' Rt.		+7.1	230.0
	32+50		
40' Rt.		+9.7	232.6
18' Rt.		+2.3	225.2
8' Rt.		1.8	221.1
♀		5.6	217.3

on g. Pr. 4th
31+71.85

18' Lt.		14.0	208.9
30' Lt.		19.3	203.6
37' Lt.		22.1	200.8
51' Lt.		27.9	195.0
68' Lt.		34.5	188.4
	33+00		
70' Lt.		31.5	191.4
64' Lt.		29.8	193.1
30' Lt.		15.7	207.2
18' Lt.		11.0	211.9
7' Lt.		6.8	216.1
♀		2.8	220.1
18' Rt.		+4.4	227.3
30' Rt.		+8.9	231.8
40' Rt.		+12.0	234.9
	33+27.96=86. Rt.		
40' Rt.		+13.9	236.8
30' Rt.		+11.1	234.0
18' Rt.		+7.4	230.3
♀		0.5	222.4
18' Lt.		7.9	215.0
30' Lt.		12.9	210.0
47' Lt.		19.2	203.7
51' Lt.		20.6	202.3
	33+50		
45' Lt.		14.2	208.7
40' Lt.		12.3	210.6

30 Lt.		11.0	211.9
18 Lt.		3.7	219.2
T.P.	11.47	233.88	0.49 222.41
£		7.9	226.0
18 Rt.		2.3	231.6
30 Rt.		+1.1	235.0
45 Rt.		+4.0	237.9
	33+75		
45 Rt.		+4.0	237.9
30 Rt.		+2.2	236.1
18 Rt.		+0.4	234.3
£		3.7	230.2
18 Lt.		9.0	224.9
30 Lt.		11.7	222.2
	34+00		
30 Lt.		4.7	229.2
18 Lt.		2.6	231.3
£		0.5	233.4
T.P.	8.55	241.34	1.09 232.79
18 Rt.		6.1	235.2
40 Rt.		3.8	237.5
	34+25		
40 Rt.		4.1	237.2
18 Rt.		5.0	236.3
£		6.2	235.1
18 Lt.		7.5	233.8

30 Lt.		8.3	233.0
	34+50		
30 Lt.		6.0	235.3
18 Lt.		5.4	235.9
£		5.5	235.8
18 Rt.		4.9	236.4
30 Rt.		4.6	236.7
40 Rt.		4.3	237.0
	34+75		
40 Rt.		4.7	236.6
18 Rt.		5.0	236.3
£		5.2	236.1
18 Lt.		5.5	235.8
30 Lt.		5.7	235.8
40 Lt.		6.1	235.2
	35+00		
40 Lt.		5.9	235.4
18 Lt.		4.9	236.4
£		4.9	236.4
18 Rt.		4.9	236.4
50 Rt.		4.6	236.7
	35+11.65 = E.C.		
80 Rt.		4.0	237.3
30 Rt.		5.0	236.3
18 Rt.		5.1	236.2
£ on Herb.		5.35	236.0

18' Lt.	5.0	2363
30' Lt.	5.2	2361
60' Lt.	6.0	2353
80' Lt.	6.6	2347

75' Rt. on Paving	5.80	235.54
100' Rt. " "	5.18	236.16
135' Rt. " "	4.31	237.03
150' Rt. " "	3.98	237.96

35+25

35+43.⁰⁸ = 10' South of North edge of Paving

80' Lt.	5.1	2362
40' Lt.	5.6	235.7
L	5.9	235.4
40' Rt.	5.3	236.0
80' Rt.	4.6	236.7

150' Rt. on Paving	3.39	
125' Rt. " "	4.34	
100' Rt. " "	5.11	
75' Rt. " "	5.73	
50' Rt. " "	6.05	235.29

35+27

80' Rt.	5.7	235.6
40' Rt.	6.3	235.0
L	6.7	234.6
40' Lt.	5.8	235.5
80' Lt.	5.2	236.1

25' Rt. " "	6.29	235.05
L	6.29	235.05
25' Lt. " "	5.90	235.44
50' Lt. " "	5.45	235.89
75' Lt. " "	4.93	
100' Lt. " "	4.41	

35+33.⁰⁸ = North edge East Paving Richburg Drive

125' Lt. " "	3.91	
150' Lt. " "	3.23	

150' Lt. on Paving	3.27	238.07
135' Lt. " "	3.96	237.38
100' Lt. " "	4.52	236.82
75' Lt. " "	5.15	236.19
50' Lt. " "	5.54	235.80
25' Lt. " "	6.08	235.26
L	6.32	235.02
25' Rt. " "	6.36	234.98
50' Rt. " "	6.10	235.24

35+53.⁰⁸ = 20' South of North edge of Paving.

150' Lt. on Paving	3.12	
125' Lt. " "	3.81	
100' Lt. " "	4.30	
75' Lt. " "	4.84	
50' Lt. " "	5.34	236.00
25' Lt. " "	5.79	235.25
L	6.15	235.19

25' Rt. on Paving.	6.23	235.11
50' Rt. " " "	5.99	235.35
75' " " "	5.61	
100' " " "	5.05	
125' " " "	4.25	
150' " " "	3.35	

35 + 63.⁰⁸ = South edge Paving.

150' Rt. on Paving.	3.46	
125' Rt. " " "	4.35	
100' " " "	5.06	
75' " " "	5.72	
50' " " "	6.10	235.24
25' " " "	6.30	235.04
1/2 " " "	6.24	235.10
25' Lt. " " "	5.89	235.45
50' Lt. " " "	5.48	235.86
75' " " "	4.88	
100' " " "	4.38	
125' " " "	3.89	
150' " " "	3.21	

"Additional"
 ROSS SECTIONS
 on Right from 3+50 to T+00
 259.47-T Page 11

259.53

3+50

39' Rt.	+11.3	270.8
43' Rt.	+16.7	276.2
53' Rt.	+26.3	285.8
63' Rt.	+28.8	288.3
70' Rt.	+29.5	289.0

3+75

70' Rt.	+28.5	288.0
56' Rt.	+28.0	287.5
48' Rt.	+24.5	284.0
38' Rt.	+12.3	271.8
43' Rt.	+22.6	282.1
53' Rt.	+27.7	287.2
63' Rt.	+28.3	287.8

259.53T P-12
 4+25

66' Rt.	+28.0	287.5
58' Rt.	+24.4	283.9
44' Rt.	+19.0	278.5

4+50

45' Rt.	+14.6	274.1
55' Rt.	+17.2	276.7
65' Rt.	+21.6	281.1
80' Rt.	+27.8	287.3

4+65

75' Rt.	+24.0	283.5
65' Rt.	+19.5	279.0
50' Rt.	+13.5	273.0

4+80

45' Rt.	+10.0	269.5
60' Rt.	+15.8	275.3

4+90

38' Rt.	+5.5	265.0
50' Rt.	+10.2	269.7
60' Rt.	+14.4	274.9

5+00

60' Rt.	+13.5	273.0
54' Rt.	+11.3	270.8
41' Rt.	+5.6	265.1

5+15

45' Rt.	+6.5	266.0
49' Rt.	+7.7	267.2
60' Rt.	+12.6	272.1

5+25

42' Rt.	+4.0	263.5
51' Rt.	+7.4	266.9
60' Rt.	+11.7	270.7

5+39.7T=EC

45' Rt.	+4.2	263.7
51' Rt.	+6.0	266.5

5+50

42' RT	+14.1	262.6
52' RT	+16.6	265.1

5+75

41' RT	+11.2	259.7
50' RT	+14.8	263.3

6+00

44' RT	+9.0	257.5
50' RT	+11.7	260.2

6+25

42' RT	+4.9	
50' RT	+8.9	

6+50

33' RT	1.5	
45' RT	+4.2	
50' RT	+6.6	

Notes
A-2A-32

CONSTRUCTION GRADES
EAST AND WEST ROAD South Ent.

Stations + - Elev. $\pm 283.01 - 283.01$

A.	E	Rt.
+58 99.5	+40 11.5 283.01 ✓	+50 34.5

0+78	282.38	283.62 283.59 ✓	284.00 = K.C. on Rt.
------	--------	--------------------	----------------------

0+55.72		285.47 ✓ 284.24	286.42 +1.8 24.7
---------	--	--------------------	---------------------

See Page 70 for Construction El. S. Entrance

Station	Distance	Construction El. N. Entrance	Elevation	Notes
0+42		291.50	291.50	
	10'	291.50 Paving -	291.50	
	10'	291.15	291.45	
0+25 = V.C.	10.77	290.90	291.35	25'
	63	290.60	291.20	
		290.35	291.00	
	22	290.93	290.98	
0+20	88	290.25	290.80	
		289.75	290.20	
	888	289.05	289.75	
0+15	898	288.30	289.15	
	7.5	287.50	288.55	
	8'	286.70	287.85	
0+10	14'	285.60	286.60	
	15'	284.60	285.29	
		S	N	

+25 35.6	+15 5.1 6.6 287.25 ✓	+10.5 22.1
-------------	-------------------------------	---------------

out
6.1
288.34

+10
4.8
3.8
288.69

out
5.5
287.00

0+00 See sketch → Page 69 for alignment
1.07 294.49 293.42 B.M. top Hy. dt. P-1

0.0
29.0

+0.5
4.5
5.0
287.28
294.49

31 +1.9
5.0 2.4
287.50

Stations	+	x	North	±	South
				Elev.	
2+75			266.40	267.42	266.60
2+50			270.64	269.47	268.25
2+25			272.82	271.52	270.22
2+00			274.87	273.57	272.27
1+75			276.80	275.62	274.90
1+50.74 - B.C. R. L. R. 100'			278.40	277.64	276.80
1+30			279.70	279.34	278.85
1+20					
1+10			280.98	280.98	280.98
1+00			281.55	281.80	282.00
0+99.90					

4	2	Rt.
Lt. 3+20 Grpt. = 263.34		Rt. 42
Rt. 2+85 = Grpt. 265.79		3+00 265.05
	267.42	
	+7.1	
	17.9	+17.2
	25.0	73.1
	269.47	
	+13.0	
	14.0	+15.8
	23.0	22.4
	271.52	
	+11.0	
	9.2	+17.7
	58.5	85.3
	20.9	
	273.57	
	+9.6	
	52.9	+15.3
		75.7
	10.7	
	8.2	
	18.9	
	275.62	
	+9.0	
	7.81	+13.5
	16.8	68.5
	277.65	
	0.4	
	14.3	
	280.16	280.16
	0.0	
	13.5	
	280.98	281.05
	+5.8	
	37.7	+6.2
	281.30	39.3
	+5.2	
	7.5	
	12.7	
	281.80	282.00
	294.49	

SUP. 1.30

Station	+	x	North	±	South
5+00			250.18	249.37	248.50
TP			252.28	251.37	250.46
4+75			252.28	251.37	250.46
TP	1.03	262.31	12.69	261.28	
4+50			254.28	253.37	252.46
4+25			256.28	255.37	254.46
4+00			258.28	257.37	256.46
+75			260.28	259.37	258.46
3+50			262.05	261.37	260.60
3+24.61-BG.R.			263.30	263.41	263.11
	+23	263.36		263.54	
	3+13	264.80		264.84	
TP			264.80	265.10	264.80
3+0346-BC	10.39	273.97	0.14	263.58	
TP	12.61	263.72		251.11	

Station	±	RT
5+00	-116 ✓ 34.4	+119 ✓ 11.8 12.9 249.37
4+75	-86 ✓ 29.9	+52 ✓ 5.7 10.9 251.37 262.31
4+50	-170 ✓ 42.5	+72 ✓ 13.4 20.6 253.37
4+25	-356 ✓ 70.4	+65 ✓ 12.1 18.6 255.37
4+00	-58.7 ✓ 10.5	+2.2 ✓ 74.4 16.6 257.37
+75	-491 ✓ 70.7	-2.1 ✓ 16.7 12.6 259.37
3+50	-214 ✓ 79.1	+180 ✓ 15.7 229.1 ✓ 43.0
3+24.61-BG.R.		+126 ✓ 13.5 +26.1 ✓ 40.6
		11.2 ✓ 11.3 ✓ 11.5 ✓
	Lt 263.34	3+20-263.50 ft 3+14-264.30 ft
		-92 ✓ 10.6 263.41
		-10.7 ✓ 18.9 265.09 273.97

8% Grade
1.91 sup

Book 1397
P-79

Station	T	N.	Elev.	S	Exp.	Lt.	E	Rt.	
7 + 17.17-BC.		231.50	232.00	232.11	-137 37.6	-0.7 5.0 5.7	232.00	+55 20.0	
7 + 00		232.95	233.37	233.25	-136 37.4	0.0 11.4 11.4	233.37	+7.4 37.6	
6 + 75		235.07	235.37	235.07	-145 38.8	-0.4 2.8 2.4	235.37 237.74	+6.2 20.3	
T.P. 0.23	237.74	12.70	237.51	237.07	-165 41.8	2.2 15.0 13.84	237.37	+4.0 18.1	
6 + 50		237.07	237.37	237.07					
6 + 25		239.07	239.37	239.07	-165 41.8	-1.9 12.7 10.84	239.37 250.21	+5.0 19.5	
T.P. 0.06	250.21	12.16	250.15	241.07	-149 39.4	-1.7 2.6 2.09	241.37	+5.4 19.9	
6 + 00		241.12	241.37	241.07					
		6.03	256.88						
Set temp BM. on R.P. hub 556. At 4 7+17.17-BC									
5 + 75		243.37	243.37	242.90	-116 34.4	-1.6 24.5 18.94	243.37	+7.4 18.9	
	24.01								
5 + 18.55-EG		245.80	245.49	244.95	-132 35.3	-0.8 17.6 16.8	245.49	+10.5 25.2	
S. Top cb El. 246.21									
5 + 44.6 End of Culvert. Low end grating El. 245.32									
N. Top cb El. 246.93									
5 + 25		247.95	247.37	246.65	-140 38.0	10.8 14.1 14.9	247.37 262.31	+12.5 27.2	
	262.31								

8% Grade
 11% slope

Station	L	T	N	+ Elev	S
9 + 50			213.45	213.37	212.90
+25			215.15	215.37	215.00
9 + 00			217.07	217.37	217.07
TP	0.66	226.43	11.97	225.77	217.07 end slab 8+28.83 E.E.
+75			219.05	219.37	219.15
8 + 50			220.90	221.37	221.37
8 + 42.83			221.45	221.95	221.05
5.7 top ab			222.82		223.42
8 + 38.83			223.52	221.08	222.68
Low end of Grating					224.32
N. Top ab					
8 + 25			222.80	223.37	223.70
8 + 00			224.72	225.37	225.95
7 + 75			226.72	227.37	228.02
7 + 50			228.75	229.37	229.85
7 + 25			230.80	231.37	231.55

237.74

Super Elev = .05 per ft.
800 grade.

L	T	R
		213.37
		+53 ✓ 90 299
+17 ✓ 192		217.37
		226.93
-35 ✓ 208	+51 ✓ 70 219.37-2675	+4.2 ✓ 122 164
		221.37
		+20.2 ✓ 34.7
		+39 ✓ 119 158
-37 ✓ 22.6		221.95
		+177 ✓ 32.2
		+36 ✓ 10.8 14.4
-65 ✓ 26.8		223.37
		+15.2 ✓ 29.7
		+15 ✓ 10.9 17.4
-64 ✓ 26.6		225.37
		+141 ✓ 28.6
-95 ✓ 31.2		+11 ✓ 93 104
		227.37
		+122 ✓ 26.7
-112 ✓ 33.8		-06 ✓ 50 84
		229.37
		+93 ✓ 23.8
		+06 ✓ 60 64
		231.37
		237.74

Station	+	T	N	E	S
11 + 50			198.95	199.18	198.70
11 + 25			206.75	206.18	206.75
TP	0.83	207.97	1273	207.14	
11 + 06.64 = EC. 10 + 84.07 = Equation.			202.95	202.65	202.10
			203.65	203.37	202.85
10 + 50			205.87	205.37	204.77
TP	0.85	219.87	7.41	219.02	48.95 RT + L
10 + 25			208.00	207.37	206.72
10 + 00				209.90	209.37 208.77
9 + 75			211.67	211.37	210.80
9 + 58.41 = BC. H.		226.43	212.85	212.70	212.20

Super Elev. 2.5 per ft. 8%

Lt.	E	Rt.
+1.8 ✓ 8.3 199.18	+59 ✓ 204	202.64 202.00 11.2
-3.5 ✓ 22.2	+30 ✓ 3.8 6.8 201.18 207.97 +2.5 ✓ 17.7 17.2 202.65	+86 ✓ 231 213.2 1.27 214.47 12.47 22.00
-16 ✓ 19.4	-27 ✓ 21.1	+112 ✓ 25.7
-38 ✓ 22.7	+51 ✓ 11.4 16.5 203.37	+110 ✓ 25.5
-38 ✓ 22.7	+60 ✓ 8.5 14.5 205.37 219.87	+126 ✓ 27.1
-20 ✓ 20.0	+45 ✓ 12.5 19.0 207.37	+146 ✓ 29.1
-19 ✓ 19.9	+4.5 ✓ 12.5 17.0 209.37	+129 ✓ 29.4
-11 ✓ 18.7	+51 ✓ 9.9 13.0 211.37	+151 ✓ 29.6
+21 ✓ 16.6	+57 ✓ 20 13.7 212.70 226.43	+157 ✓ 30.2

	N	E	S
Station 107	-	-	-
13 + 82.57 Break		51.0x	
24.8 57.8			
13 + 57.57 "			
24.8 32.5			
13 + 32.57 "			
24.8 7.5			
+25		185.10	
24.80			
13 + 07.57 "			
12.9			
12 + 82.57 P.V.C		188.58	
12 + 75		189.18	
12 + 50		191.18	
T.P	70.02	195.63	12.36
12 + 25		193.18	
12 + 00		195.18	
11 + 80 low end of Grat.		196.49	
11 + 75	207.97	196.88	197.18
		196.88	

	W	E	Rt.
	+41 18.6	+82 74 13.6 180.08	+189 33.4
	+21 16.6	+78 35 13.3 182.30	+127 32.2
	-24 20.6	+55 37 11.3 184.46	+124 26.9
	-132 34.8	-0.9 76.0 3.1 186.55 1.40	+52 19.7
	-310 63.5	-51 122 7.1 188.58	-05 17.7
	-122 45.6	-50 106 4.4 191.18	-15 14.2
	-129 30.3	-39 63 3.4 193.18	-05 17.7
	-23 31.0	-19 2.3 0.4 195.18 196.3	+34 17.9
		-06 16.8 197.18 207.97	

200.00

8 7/8 Grade

Station	+	-	N	E	S			
16+00			158.05	158.84	159.50	-242 53.3	-18.0 81 +9.9 158.84	168.84
15+75			160.65	162.34	161.84	-26.0 56.0	-18.1 5.7 +17.4 161.34 148.95	168.84
15+56 = 86.14	0.48	148.95	162.70	163.74	163.55	-283 57.5	-14.7 16.2 13.5 163.24 159.76	168.84
TP	0.27	159.76	11.23 12.94 +25 165.95	148.47 = correct 148.53 157.58	159.43 166.34			
15+12			167.64	167.64	168.93	-159 40.9	+3.7 7.1 4.8 167.64 172.43	168.84
TP	0.36	172.43	12.26 168.50	172.07 168.84	168.65		+4.7 13.8 13.5 168.84	168.84
14+82.57 = 5.10				170.58		+12 15.7	+4.8 8.9 13.7 170.58	168.84
14+57.57				173.05		+12 15.7	+4.8 8.3 11.3 173.05 184.93	168.84
TP	1.12	184.33	12.42	183.21				168.84
14+32.57						+23 16.3	+4.6 7.6 13.2 175.46	168.84
14+07.57						+32 17.7	+9.3 15.6 17.8 177.80 195.63	168.84

Super = 0.6 per ft
 0.78
 10% Grade
 500' V.S.

168.84
2.70
168.84

195.63

Station	+	x	N	E	S	Elev.
18+00			139.95	140.95	140.85	
17+75			141.45	142.16	142.75	
17+67 ⁵ low end of Grt. El. 142.07						
17+50			143.35	144.15	144.90	
17+25			145.60	146.38	147.16	
	+12.57 = P.V.C		146.80	147.58	148.36	
T.P.	7.54	137.10	8.68	129.56	17+25	on 2 stub
17+00			148.06	148.84	149.62	
16+75			150.56	151.34	152.12	
16+50			153.06	153.84	154.62	
T.P.	7.32	138.24	12.63	136.32		
16+25			155.56	156.34	157.12	
		148.95				

100 V.C.

10.0%

Lt. E 148.01 Rt.

-163 ✓ 11.4	-17.4 ✓ 14.6 + 3.35 140.45	-165 ✓ 11.7
-174 ✓ 11.1	-15.6 ✓ 13.37 + 3.06 142.16	-181 ✓ 11.1
-163 ✓ 11.5	-16.1 ✓ 3.04 + 7.04 144.14	-181 ✓ 11.1
-181 ✓ 11.1	-16.8 ✓ 7.5 + 5.3 146.38	-176 ✓ 11.4
	147.58	
	137.10	
-201 ✓ 11.1	-18.1 ✓ 1.5 + 10.6 148.84	-186 ✓ 11.1
-226 ✓ 11.1	-18.3 ✓ 5.2 + 13.1 151.34	-182 ✓ 11.1
-233 ✓ 11.1	(11.1) + 15.6 153.84	-18.7 ✓ 11.1
-244 ✓ 11.1	-17.1 ✓ 3.7 + 7.4 156.34 148.25	-18.4 ✓ 11.1

Station	+	x	N	E.	S	Lt	∅	Rt
20 + 00			135.90	136.38	136.25	-81 79.1	-7.4 3.42 1.03 136.05	-101 37.1
19 + 75			135.40	135.82	135.60	-31 27.6	-2.3 3.62 1.33 135.79	-38 37.7
19 + 50			135.35	135.64	135.40	-31 27.6	-3.1 3.5 1.4 135.65	-44 33.6
19 + 25			135.50	135.80	135.50	-42 33.3	-4.3 3.6 1.3 135.80	-69 36.6
19 + 00			135.91	136.21	135.95	-67 37.1	-8.7 3.6 0.3 136.21	-107 37.4
18 + 75			136.55	136.87	136.70	-104 32.6	-10.5 10.7 0.2 136.87	-125 35.7
18 + 50			137.50	137.80	137.70	-123 35.5	-11.8 11.1 0.7 137.80	-133 37.0
18 + 30.89 = E.C. + 19.1			138.40	138.68	138.90	-118 39.7	-13.3 11.7 1.6 138.68	-164 41.6
18 + 25			138.65	139.00	139.20		139.00 137.10	

400' V.C.

Station	+	x	N	Elev.	S
22+00			147.35	147.99	148.50
TP	4.17	172.51	0.13	168.34	
21+75			145.57	146.30	147.03
TP	12.33	168.47	1.20	156.14	
21+50			143.83	144.61	145.39
TP	12.44	157.34	0.30	144.90	
21+25			142.14	142.92	143.70
21+12.57 = E.V.C			141.30	142.08	142.86
TP	11.79	145.20	3.49	133.41	
21+00			140.45	141.23	142.01
	4.98	136.90		131.92	
Chk. 8M. Powder House Canyon			4.98	132.12	
20+75			139.00	139.60	140.35
20+50			137.70	138.25	138.65
20+24.71 = B.C.			136.65	137.12	137.25

137.40

R 300' = .75 = 1/2 Roadway
6.75%

400 V.C.

Lt	Rt	51
+101 34.6	+211 38 146.99 172.51	+29.6 29.3 71.0
+85 23.0	+17.9 5.3 23.2 145.90 168.47	26.0 27.5 419 56.4
+53 7.8	+10.7 1.0 13.7 143.61 157.34	+18.8 23.9 423.5 38+00
+19 7.6	+3.0 0.3 3.3 141.92	+6.8 21.3 17.0
	141.08	
-46 23.9	-2.4 7.23 4.93 140.27 145.20	-2.2 22.3
-21 27.6	-5.3 3.50 +1.75 138.85	-3.6 25.4
-16 28.4	-6.4 5.8 28.6 137.69	-8.2 27.3
-35 31.3	-7.6 3.3 3.3 136.77 137.10	-10.3 32.5

Station	+	T	N	4	S
			Elev.		
24+25			163.83	162.18	162.53
T.P.	13.62	184.19	0.24	171.57	
24+00			162.14	161.49	160.84
23+75			160.45	159.80	159.15
23+65	Low end Grating Rt. El. 158.19'				
23+50			158.70	158.11	157.45
1046					
old 23+34.54 BC Rt.			157.40	157.06	157.72
23+25			156.90	156.42	155.80
23+00			155.00	154.73	154.40
22+94.93 BC Rt			154.65	154.40	154.10
22+75			153.10	153.05	152.90
22+50			151.75	151.36	151.46
22+23.68 RC			149.20	149.58	149.90
268		172.51			

Slope 0.5 per ft

Station	+	T	N	4	S
					+11.2
					10.8
					22.0
					162.18
					184.19
					+19.0
					24.0
					+21.7
					36.2
					+4.3
					7.7
					12.0
					160.49
					+10.3
					19.6
					+12.0
					26.5
					-4.4
					7.7
					13.7
					158.80
					-1.8
					19.7
					-3.1
					18.5
					13.90
					157.11
					+0.7
					15.2
					+3.7
					7.75
					16.45
					156.06
					+7.9
					18.5
					+8.9
					22.8
					+16.3
					19.0
					18.78
					153.73
					27.8
					28.4
					+33.8
					18.3
					+7.6
					22.1
					+18.3
					0.55
					19.46
					152.95
					26.9
					28.0
					+48.1
					62.6
					12.7
					24.5
					22.15
					150.96
					+29.1
					29.0
					+58.5
					69.0
					+21.0
					3.9
					23.3
					148.58
					172.51
					+18.9
					27.8
					+30.8
					29.9
					+52.7
					74.2

		N	E	S				
+70		180.35	179.70	179.05		+6.7	+16.6	1271
26+50		179.01	178.36	177.71	-17.0 42.5	6.7 7.45 177.36	22.8	416
T.P.	8.89	184.81	0.89	175.92		+6.7	+18.8	+29.0
26+25	8.89	184.81	177.33	176.68	-13.2 36.8	2.4 9.1 175.68 184.81	29.9	43.5
T.P.	3.99	176.81	11.37	172.82		+6.5	+18.2	+28.5
26+00		175.65	175.00	174.35	-14.7 37.0	3.7 19.2 174.00	28.6	48.0
25+75		173.96	173.31	172.66	+0.6 15.1	+8.1 38.0 178.8 172.31	+18.0 23.5	+30.7 45.2
25+50		172.27	171.62	170.97	+1.3 15.8	+10.1 34.0 13.57 170.62	+18.0 23.5	+33.4 47.9
25+25		170.58	169.93	169.28	+1.9 16.4	+10.5 47.3 15.26 168.99	+19.8 24.4	+34.7 49.6
25+00		168.89	168.24	167.79	+3.3 17.8	+11.9 48.3 15.37 167.24	+21.0 25.0	+34.5 49.0
24+75		167.20	166.55	165.90	+2.2 16.7	+11.6 7.0 18.64 165.55	+20.6 24.8	48.0 48.5
24+50		165.51	164.86	164.21	+2.4 16.9	+10.7 36.0 28.35 163.86 184.19	+20.0 24.5	48.8 45.9
		184.19						

Station	N	Elev.	S
28+40	190.60	191.19	191.75
28+2.5	189.65	190.18	190.65
28+00	188.30	188.49	188.65
T.P. 12.67 208.22	159	195.55	
27+93.11 = 86 Lt.	187.85	187.92	188.05
27+75.28 27+75	186.90	186.80	186.70
27+74.52 EC			
T.P. 12.99 197.14	0.66	184.15	
27+50	185.37	185.11	184.90
27+35.97 = EC 57.1A	184.37	184.17	183.80
27+25	183.83	183.43	183.00
27+20 Grd. Pt. 182.69			
27+14.5 Grd. Lt. 182.85			
27+00	182.30	181.74	181.20
+90	181.71	181.06	180.41
26+75	180.70	180.05	179.40

Slope = 0.5 per ft
6.75%

on slope stake
145' Lt. 27+50
6.75%
18.10

Slope = 0.5 per ft
6.75%

Lt.	Rt.	St.
+27 172	+11.4 38 15.2 183.18	+32.9 47.4
(out)	+9.0 11.7 20.7 187.49 208.22	(out)
+23 168	+9.6 06 186.92	+22.4 36.9
(out)	+9.5 18 113.4 183.80	(out)
26+90 67.5 18.10	+26 13.49 13.03 184.11 197.14	+23 16.8
-8.7 30.1	-3.1 2.7 1.6 183.17	-4.1 23.1
13 16	(out) 182.43	
-24.5 53.8	-4.8 8.9 2.1 180.74	0.0 14.5
-20.9 16.4	+2.3 3.5 5.8 179.05 184.81	-10.2 19.6 +14.3 28.8

Station	+	x	N	Elev.	S	Lt.	E	H.
30 + 50			204.34	204.99	205.64	+26 17.1	+8.7 6.1 14.8 204.96	+332 37.7
30 + 25			202.75	203.40	204.05	+31 17.6	+9.5 6.97 14.17 202.68	+256 40.1
30 + 00			201.15	201.80	202.45	+29 17.4	+7.9 8.21 18.15 201.00	+188 43.2
29 + 75			199.55	200.20	200.85	+29 17.4	+10.0 9.9 13.25 199.30 212.15	+298 44.3
T.P.	12.66	219.15	173.	206.49				
29 + 50		X	197.90	198.55	199.20	+17 16.2	+8.5 7.1 18.6 197.61	+280 40.5
29 + 25			196.28	196.93	197.58	+13 15.8	+8.7 8.6 14.3 197.93	+271 41.6
29 + 00			194.59	195.24	195.89	+20 16.5	+9.5 8.5 14.0 194.24	+330 47.5
28 + 75			192.90	193.55	194.20	+24 16.9	+10.7 5.0 15.7 192.55	+352 49.9
28 + 60			191.88	192.53	193.18		+11.9 5.9 17.3 190.86 208.22	+358 50.3
28 + 50				191.86		+17 17.2		
			208.22					

Station	+	x	-	to/er	
32 + 75			219.25	219.55	219.25
TP	13.91	232.89	0.17	218.98	219.25 of 40L 31+90 10' 41.2
32 + 50			217.56	217.86	217.56
32 + 25			215.88	216.18	215.98
32 + 00			214.28	214.58	214.35
31 + 71.85 = E.C.			212.35	212.78	212.65
31 + 50			210.95	211.38	211.50
App + 43	Low end	210.92 ft	210.48	210.92	211.12
	Grating	210.36 ft			
31 + 25		x	209.22	209.78	210.15
31 + 00			207.60	208.19	208.70
30 + 75			205.95	206.59	207.25

219.15

Lt.	L	Rt.
out	out	out
	219.55	
-248 ✓ 54.2	-0.6 ✓ 7.9 1.3 217.86	+95 ✓ 34.0
out	out	out
	216.18	
-209 ✓ 48.3	+09 ✓ 3.7 4.6 214.49	+128 ✓ 57.3
-244 ✓ 53.6	-2.6 ✓ 9.18 6.57 212.58	+69 ✓ 31.4
out	-10.5 ✓ 18.5 80.4 211.11	out
-289 ✓ 60.4	-1.0 ✓ 10.76 9.72 209.43	+81 ✓ 22.6
-165 ✓ 21.7	+2.8 ✓ 8.6 11.4 207.74	+137 ✓ 58.2
+08 ✓ 15.3	+6.1 ✓ 7.0 13.1 206.05 219.15	+19.7 ✓ 34.2

Station	Pov. 236.50	234.30	Pov. 235.30	235.20
	10.38	236.05	12.38	234.70
	2.10	235.80	12.8	234.60
	10.1	235.55	4	234.50
34+85.08 = P.C.C. on Rt.		235.30	6	234.25
		234.95	10	233.75
		5.47	10	233.20
		234.70	11.2	233.20
		5.2	11.2	11.14
		234.45	8	232.25
		8	12	11.9
34+73.08 = P.V.C.		234.10	12	231.10
		9.5	12	9.1
		233.55	15	230.35
		232.70	15	13.6
		232.92	15	230.54
34+50	13.61	231.60	15	230.36
+375		231.05	15	229.22
+35		230.76	16.34	228.60
34+25	16.34	230.35	16.34	228.41
+225		229.55	16.34	227.40
+075		229.05	11.98	226.95
34+00	11.98	228.90		226.76
+965		227.10		225.35
33+75		226.40		224.45
Appr. +60	Low and Grating	239.11	6.87	226.02
T.P.	13.09	225.15		223.85
33+50		223.88		222.50
		223.13		222.50
33+27.96 = C.C. on Rt.		221.30		220.80
		221.24		220.80
33+00		222.85		220.80

Lt.	Rt.	Rt.
+18	+2.7	28 + 31
16.3	2.6	3.7
31	5.3	5.7
4.9	233.80	233.20
234.20		
	+3.3	2.7 + 4.0
+2.3	3.9	6.7
16.3	6.2	18.5
33	232.92	232.38
5.6		
233.50		
	+4.5	2.6 + 6.1
+3.5	3.2	8.7
18.0	7.7	20.6
3.2	231.40	230.4
6.7		237.11
232.44		
232.1		
	+5.4	+8.0
	4.0	7.5
+3.2	9.4	
17.7	227.68	
	+5.4	+8.9
	5.7	23.4
+2.3	11.1	
16.8	228.00	
	+3.9	+9.7
	12.8	24.2
-4.2	226.30	
23.3	239.11	
	+1.5	+9.8
	6.3	24.3
-15.7	224.61	
41.5		
	-0.8	+9.6
	10.5	24.1
-22.8	9.76	
51.2	223.13	
	-1.1	+7.9
	12.78	27.4
-24.6	11.55	
53.9	221.24	
	232.89	

Station	+	-	Elev.
117	235.55		235.55
118	235.55		235.55
119	235.55		235.55
120	235.55		235.55
121	235.55		235.55
122	235.55		235.55
123	235.55		235.55
124	235.55		235.55
125	235.55		235.55
126	235.55		235.55
127	235.55		235.55
128	235.55		235.55
129	235.55		235.55
130	235.55		235.55
131	235.55		235.55
132	235.55		235.55
133	235.55		235.55
134	235.55		235.55
135	235.55		235.55
136	235.55		235.55
137	235.55		235.55
138	235.55		235.55
139	235.55		235.55
140	235.55		235.55
141	235.55		235.55
142	235.55		235.55
143	235.55		235.55
144	235.55		235.55
145	235.55		235.55
146	235.55		235.55
147	235.55		235.55
148	235.55		235.55
149	235.55		235.55
150	235.55		235.55
151	235.55		235.55
152	235.55		235.55
153	235.55		235.55
154	235.55		235.55
155	235.55		235.55
156	235.55		235.55
157	235.55		235.55
158	235.55		235.55
159	235.55		235.55
160	235.55		235.55
161	235.55		235.55
162	235.55		235.55
163	235.55		235.55
164	235.55		235.55
165	235.55		235.55
166	235.55		235.55
167	235.55		235.55
168	235.55		235.55
169	235.55		235.55
170	235.55		235.55
171	235.55		235.55
172	235.55		235.55
173	235.55		235.55
174	235.55		235.55
175	235.55		235.55
176	235.55		235.55
177	235.55		235.55
178	235.55		235.55
179	235.55		235.55
180	235.55		235.55
181	235.55		235.55
182	235.55		235.55
183	235.55		235.55
184	235.55		235.55
185	235.55		235.55
186	235.55		235.55
187	235.55		235.55
188	235.55		235.55
189	235.55		235.55
190	235.55		235.55
191	235.55		235.55
192	235.55		235.55
193	235.55		235.55
194	235.55		235.55
195	235.55		235.55
196	235.55		235.55
197	235.55		235.55
198	235.55		235.55
199	235.55		235.55
200	235.55		235.55

T.P. 01.30' Radius hub on Lt. 3.83 235.38 Temp. 8.M.

E.C. 30' Radius Rt. Axel Lt.

10.06' Ahead PRC on Lt.
21.02 " PRC on Rt.

34+96.31 = PRC on Lt.
239.11

St.	±	Elev.
117		235.55
118		235.55
119		235.55
120		235.55
121		235.55
122		235.55
123		235.55
124		235.55
125		235.55
126		235.55
127		235.55
128		235.55
129		235.55
130		235.55
131		235.55
132		235.55
133		235.55
134		235.55
135		235.55
136		235.55
137		235.55
138		235.55
139		235.55
140		235.55
141		235.55
142		235.55
143		235.55
144		235.55
145		235.55
146		235.55
147		235.55
148		235.55
149		235.55
150		235.55
151		235.55
152		235.55
153		235.55
154		235.55
155		235.55
156		235.55
157		235.55
158		235.55
159		235.55
160		235.55
161		235.55
162		235.55
163		235.55
164		235.55
165		235.55
166		235.55
167		235.55
168		235.55
169		235.55
170		235.55
171		235.55
172		235.55
173		235.55
174		235.55
175		235.55
176		235.55
177		235.55
178		235.55
179		235.55
180		235.55
181		235.55
182		235.55
183		235.55
184		235.55
185		235.55
186		235.55
187		235.55
188		235.55
189		235.55
190		235.55
191		235.55
192		235.55
193		235.55
194		235.55
195		235.55
196		235.55
197		235.55
198		235.55
199		235.55
200		235.55

+0.4
0.2 slope 1
3.5
235.60

3.2 +1.0
4.0 1.0 too close
235.10

+1.5
1.5 slope 3.6
4.1
235.00

2.9 +1.2
4.1 1.2 too slope
235.00

+1.9
1.9 slope 2.7
4.6
234.50

+2.1
2.7
4.8
234.50
239.11

2.06' Ahead PRC on Lt.

2.8 +2.1
4.9 2.1 too slope
234.20

2.06' Ahead PRC on Rt.

El. on Conduit put in

Station.	HI	El.
T.P. 098	29315	292.17
	$\frac{6.50}{29315}$	on Tile
T.P. Rt of 1+25 Slope =	286.65	
	$\frac{1.70}{286.65}$	278.00
	288.35	9.57
	$\frac{11.25}{288.35}$	268.43
17' Rt. top. 2+25 =	277.13	
	$\frac{0.87}{277.13}$	
	278.00	

2+41 Elec. = Tele. end of pipe = 7.8 285.4

2+32 Wiped joint 8.25 285.0

1+55
77
86

1+37.5 Bend in pipe. 6.9 286.3

1+17 Cable Box 12.8 280.4

1+15 Bend in pipe. $\frac{50}{280.0}$ 280.0

1+00 = 0+53 = 70°30' to Right 284.33 Grade

0+84 = Bend in pipe. $\frac{36}{12.9}$ 280.3

0+59 Bend in pipe 5.20 288.0

0+55 = Wiped joint. 4.60 288.6

0+00 = East curb of Park Blvd.

El. on top of Electric Conduit as in ground.

NORTH ENTRANCE
EAST AND WEST ROAD
Cont. from P-59

Lt

R

Rt

Station 0+50	284.65	284.62	284.10
0+41.06 = E.C. of 100' R. Radius. 33.94	285.60	285.29	284.60
0+21.06			
0-2.65 = End V.C.			
0-11.30			
0-15.65			
0-28.65			
0-41.65 = Center V.C.			
0-55.65			
0-80.65 = East abutment Pt. Blvd. 1.07	294.49	293.42	8M top Hyd. P-1

+27 253	285.29	Radial	+30 6.2 9.2	285.29	Radial 100'R	285.20	+4.6 32.9
+08 19.7	287.16	Radial	+20 5.8 7.8	286.76	Radial 100'R	287.00	+2.8 27.6
	289.40	Radial	+23 5.5 5.8	288.70	Radial 100'R	288.20	
-25 257	290.00	Radial	+20 5.2 5.2	289.10	Radial 100'R	289.00	+2.0 29.6
	291.0 = Fill Sec						
			+01 4.9 5.0	289.40			
-22 253	290.50	Radial	-0.2 4.4 4.2	290.10			
	291.5 = Fill Sec						
-16 29.4	290.90	Radial	-0.1 3.8 3	290.60	Not Radial	290.10	+1.3 35.0
	291.90 = Fill Sec						
0.0 19.5	291.20	Radial	+0.2 3.1 3.3	291.00		290.50	+1.0 38.0
			0.1 3.0	291.50			
				294.49			

North Entrance

[Page 71 for 5. Entrance]

Station	26680 26480	26500	26509	26480
3+03.46 = 3+03.46	26480	26500	26509	26480
3+00	3.08	3.14	3.779	
2+90	26° 07'	9.077	26505	
2+75	24° 17.6'	13.617	26570	26620-26530
2+67	21° 33.5'	7.13	26665	26700-26848
2+50	17° 00'	15.43	26705	26809-26913
2+47	16° 26'	2.723	26870	26973
2+30 = Great	13° 20.2'	4.492	27008	27112
+25	12° 26'	14.18	27047	271.5
+02.27	22.295		272.35	273.38
2+00	8° 17.07'	18.00	272.35	273.38
1+75	3° 18.56'	22.694	274.35	275.25
1+56.85 = 80.27.8R	157.10'	16.482	275.90	276.61
1+25			278.70	279.00
1+00			280.57	280.87
0+75			282.45	282.74
0+60			283.60	283.87

M4 = 10.94 per foot

14.5 cut = 0.9078
17.0 cut = 0.89181
14.5 cut = 1.09232

75% ~~8.20%~~ sup 10.4

+18
20.0

+95
52.5

+126
49

+102
55.3

+71
42.9

+45
32.5

265.09

267.44

269.49

+83
15.1
23.4
271.12

+86
12.5
27.1
273.38

+88
13.5
12.3
275.25

+7.7
9.7
17.4
277.06 + 1.50

+72
3.3
15.5
278.99

+42
6.8
11.7
282.74
284.49

10.94
2.3
32.92
21.58
25.16
90.52
8.17

10.9
2.3
32.7
21.3
2.8

+108
57.7

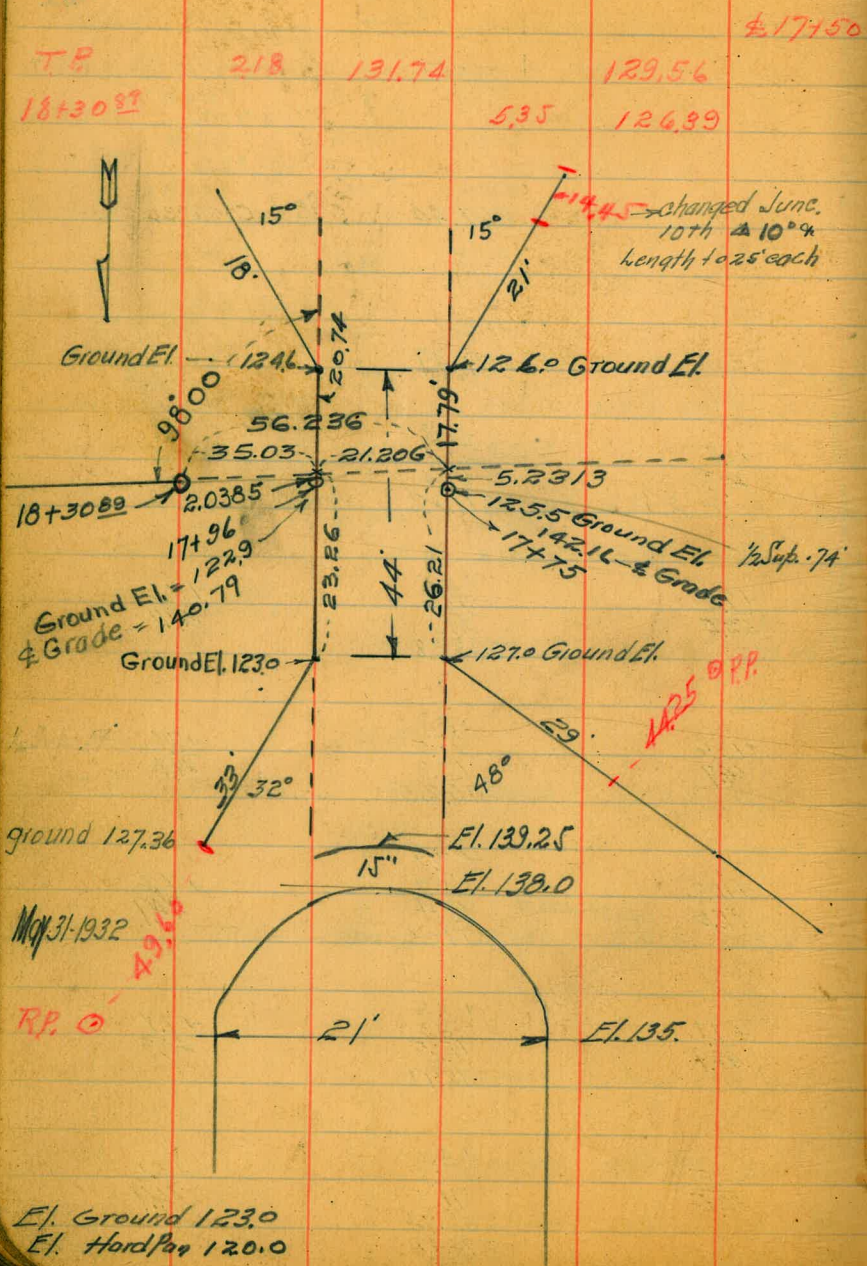
+87
49.3

+7.6
44.9

+77
45.3

+7.1
43.7

+5.6
56.9



Type D-2 Curb Inlet 1284B

£

Station	Description	RT	LT	RT	LT	RT	LT
2+78	Rt. Top C.B. 15.0'	267.21	267.18	17+72'		142.38	
+86	4" Pipe Low end Grating - E126579			17+70 1/2	Low end Grating	142.07	
2+90	Rt. Top C.B. 15.0'	266.38	266.20	17+62		143.18	123.5
3+23	Top B. Lt. Top C.B. - 15.5'	264.80	264.30				
3+21 1/4	4" Pipe Low end Grating	263.34					
3+13	Lt. Top C.B. 16.0'	265.60	265.10				
							257.91
							248.02
							242.50
							233.00
							228.40
5+46 1/2	Rt. Top C.B. 15.0'	246.21	245.66				241.09
5+44 1/2	4" Pipe Low end Grating						234.76
5+36	Rt. Top C.B. 15.0'	246.93	246.47	23+61 1/4		157.88	155.31
						158.54	153.00
						157.88	152.66
							144.15
8+40 1/2		223.42	222.82	23+63 1/2	4" Pipe Low end Grating	158.19	
8+38 1/2	4" Pipe Low end Grating	221.88	222.62	23+71 1/2		157.20	158.55
8+30 1/2		224.32	223.52	27+11.9		182.80	181.50
				27+13 1/2	4" Pipe Low end Grating	182.85	
11+85 1/2		196.79	195.79	27+21 1/2		183.37	182.17
11+84 1/2	4" Pipe Low end Grating						175.88
11+75 1/2		198.17	197.12	27+16 1/2		182.64	181.84
				27+18 1/2	4" Pipe Low end Grating	182.69	
15+17 1/2		168.06	167.06	27+26 1/2		183.31	182.51
15+16 1/2	4" Pipe Low end Grating						
15+10 1/2		169.06	168.06	31+41		211.27	210.52
15+25 1/2		167.38	166.33	31+43 1/2	4" Pipe Low end Grating	210.92	208.44
15+24 1/2	4" Pipe Low end Grating						206.93
15+15 1/2		168.33	167.33	31+51		211.25	203.59
							192.86
							192.56
							180.16

Note change in Grade line to 1.00' higher

33+58²

33+60² Pipe

33+68⁰

RT

225.67

225.17

Lowland Grotting 224.261

RT

226.20

225.84

220.64

215.15

Ch. Etc. from Bridle path to Pershing Dr.
Aug 18-1925

24" Con. Culvert. Bridle Path				Sta. 16+75
B.M. N.W. Cor. Wing Wall	2.13	138.98		136.85
B.M.	12.52	150.29	1.21	Sta. 21 By. 137.77 Pipe
	11.96	161.73	0.52	142.77
	12.36	173.58	0.51	161.22
B.M. Marked 165.68			7.78	Sta 23+ 165.80
	12.15	183.45	2.28	171.30
B.M. Marked 180.87			2.50	27+00 Low slope stake. 180.95
	12.26	195.04	0.67	182.78
	12.18	206.57	0.65	194.39
B.M. Marked 202.94			3.53	Sta 27+ 203.04
	11.91	216.82	1.65	204.91
B.M. Marked 219.35			3.38	Sta 31+ 213.44
	12.55	229.17	0.20	216.62
	11.08	238.96	1.29	227.88
B.M. Marked 235.38 - 30' R. Hub. Left			3.48	235.48
B.M. Peg about 22' W. of Sta. 13+40				El. 179.38
B.M. Peg. about 25' Left of Sta. 11+50				El. 196.77 - ch - 196.74
B.M. Peg about 28' Left of Sta. 13+85				El. 182.52
B.M. on Con. joint 15' N of 100' R. N. entrance				292.12 out.
B.M. First Pier plate 19' S. Sta 3+03 ⁴⁶				268.26
B.M. Fire Plug. cor Yorick Theatre				293.42
Top cb = 15+07 ²⁵ El. 169.07	9-Pipe			Top cb = 15+15 ²⁵ El. 168.27
Low end +14 ²⁷ Grating	12 ✓			Low end Grad. +22 ²⁵ 166.62
End Box +16				End Box +24 166.44
Top cb +17 ²⁵ 168.07				Top cb +25 ²⁵ 167.27
F.L. Pipe 160.00				F.L. Pipe 163.12
H. Wall. 16.5+31.5				El. F.L. 148.05

B.M. Park Blvd. Top F. Hyd.	293.42
B.M. " " old New cb =	292.08
B.M. Top catch Basin W. of Sta. 27+20	El. 184.27
B.M. Peg 25 Right of Sta 31+65	213.44
B.M. Top Catch Basin W. of Sta. 5+40	246.85
B.M. " " " " " " 8+40	223.69
" " " " " " 11+75	198.20
" " " " " " 15+20	168.87
" " N.W. Wing Wall	17+70 142.13
" " Catch Basin " " " "	23+72 159.82
" " " " " " " "	33+70 225.78

Hough
Sept. 7-32
Station

Powder House, Canyon Road
Construction Grades

141.60

+50

+25

34+00

3M.

6.87

147.29

1.18

140.42

West
Peg

+75

+50

+25

33+00

+75

+50

+25

32+00

+75

3.19 144.30 to Hub

+50



66

-2.3
23.5

-1.9
22.8

-1.9
22.8

-2.2
23.3

-2.4
23.6

-2.3
23.5

-1.6
22.4

-0.8
21.6

0.0
20.0

1.8
3.7
+1.8
18.3

1.0
3.2
+2.2
18.7

6.6
1.8
-4.8
139.80

5.1
1.4
-3.7
140.20

4.7
3.0
-3.7
140.60

10.7
6.3
-4.6
141.00
147.29

10.1
5.2
-4.3
141.50

9.6
5.3
-4.3
142.00

8.7
3.2
-3.7
142.50

7.5
4.3
-3.2
143.00

7.3
3.8
-3.5
29.6

6.5
3.3
-3.2
144.00

5.3
2.8
-2.5
144.50

3.2
2.5
-0.7
145.00

-7.7 Set Hub in Road
31.6 guard 4' out.

-7.6
31.4 guard 5' out

-7.4
31.1 r 7' out.

-7.3
31.0 r 3' in

-6.6
29.9

-7.1
30.7 r 3' in

-7.3
31.0 r 3' in

6.3
29.5 10.0
37

-6.4
29.6 7.6
32

-5.8
28.7 8.5
2.7

-5.1
27.7 7.3
2.2

-4.5
26.8 6.2
1.7

Station

141.72

+75

6.1
5.2
-0.9
136.57
141.72

-4.0
26.0

+50

5.8
4.9
-0.9
136.75

-3.1
24.7

+25

5.1
4.2
-0.3
136.92

-3.2
24.8

37+00

5.7
4.6
-0.8
137.07

-3.9
25.9

+75

5.6
4.7
-0.7
137.27

-2.4
25.1

+50

6.2
4.8
-1.2
137.45

-6.2
27.3

+25

6.82

141.60

6.94

134.78

E Hub

3.2
3.8
-0.4
20.6

6.9
4.0
-2.9
137.70

-7.5
31.3

36+00

3.8
3.0
-0.8
21.2

8.0
3.6
-4.4
137.95
141.60

-7.9
31.9

+75

5.0

3.0
-2.0
23.6

8.9
5.4
-3.5
138.20

-7.4
31.1

10.4
3.0

+50

6.2

2.6
-3.6
25.4

9.3
5.7
-6.1
138.40

-7.6
31.4

10.2
2.6

+25

6.0

2.3
-3.7
25.6

8.7
2.9
-5.8
138.70

-7.4
31.1

9.7
2.3

35+00

5.3

2.0
-3.3
25.0

8.2
2.6
-5.6
139.00

-7.4
31.1

9.4
2.0

+75

4.4

1.8
-2.6
23.9

7.4
2.2
-5.2
139.40

-7.3
31.0

9.1
1.8

HS 141.60

+75
Station

+50

+25

A1+00

+75

+50

+25

40+00

+82³⁵

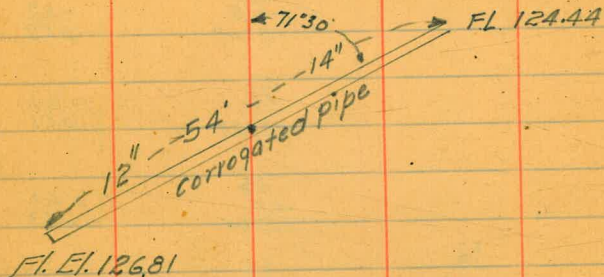
39+50⁰¹

+90²²
DM line

+58⁶³

+25

TP
38+00



4.20 141.97

TP 1.83 141.72 2.08 139.89

Page 65
137.77

-0.4
131.56

-3.2
24.8

E. 131.68
0.0
16.5

-2.0
132.03

-5.0
27.5

-1.4
22.1

-4.3
132.50

-9.6
34.4

-4.1
26.2

-5.1
132.97

-10.2
35.3

-4.8
27.2

-4.6
133.44

-9.1
33.7

-5.1
27.7

-3.9
133.91

-10.3
35.5

-5.6
28.4

-3.0
134.38

-11.1
36.6

HI 132.56

-6.8
30.2

-4.5
134.80

-6.1
29.2

BM 137.77
1.74

Rad = -90
33.5

135.40

-6.4
29.6

HI 132.57
9.03
TP 130.48
2.08
132.56

-1.4
22.1

2.9
5.9
-2.0
136.00

-4.0
26.0

5.7
-0.0
136.23

-3.5
25.2

6.8
5.6
-1.2
136.40

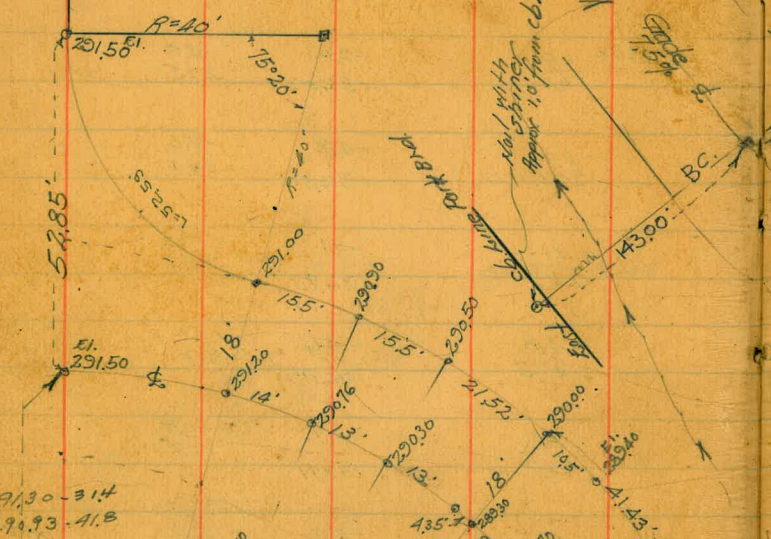
-3.3
25.0

HI = 141.97

"ALIGNMENT"

EAST AND WEST ROAD IN BAMBOO PARK
BETWEEN PARK BLDG. and PARKING DRIVE

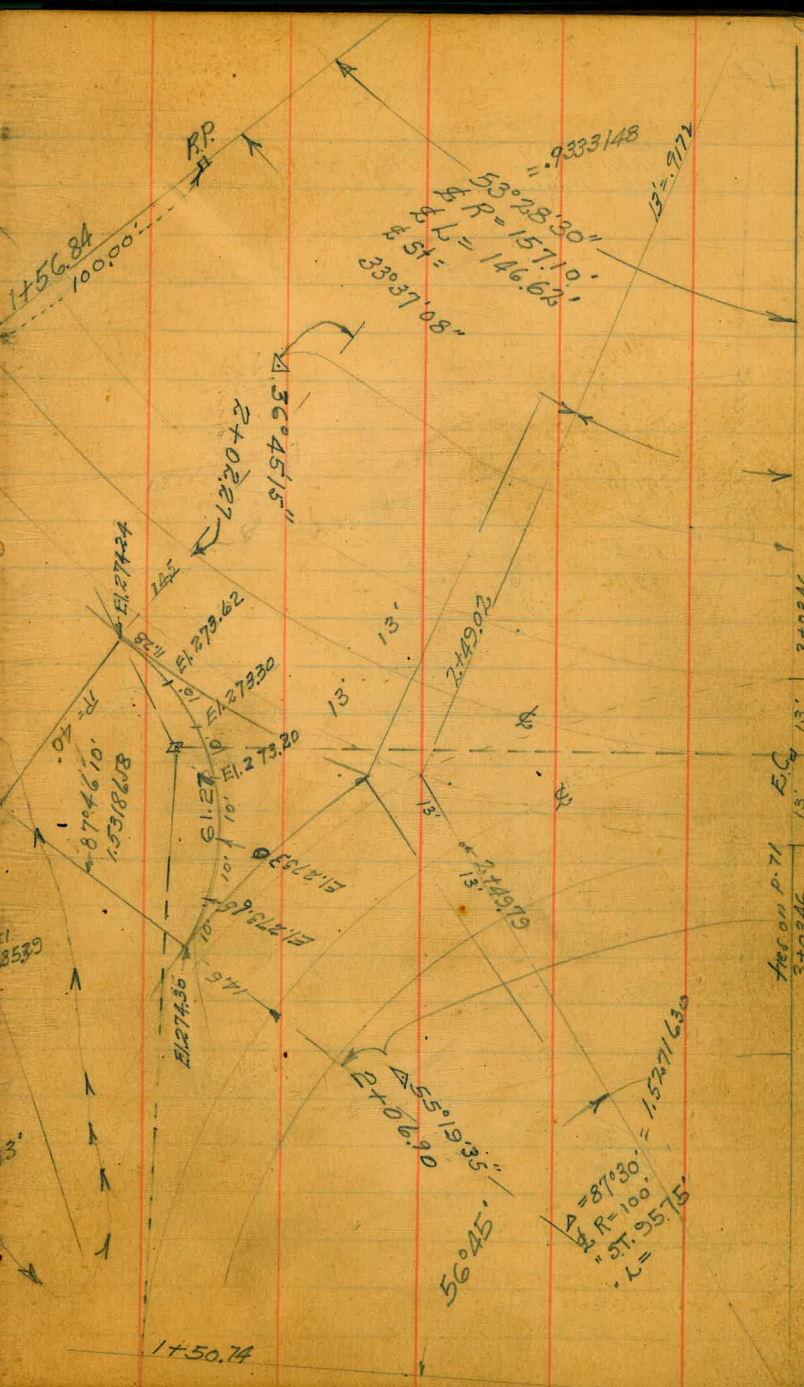
El. Topog 291.45-51.8



El. Topog = 291.30 - 314
= 279.93 - 41.8



See Page 41 for El. of construction grades



$\Delta = 53^{\circ}28'30''$
 $R = 1571.0'$
 $L = 146.62'$
 $\Delta = 33^{\circ}37'08''$
 $L = 933.148'$
 $B = 977'$

$\Delta = 87^{\circ}30'$
 $R = 100'$
 $L = 51.9575'$

Area on p. 71 = 370346
 Area on p. 72 = 370346

1+50.74

B.V.D.

Measures
116.23'

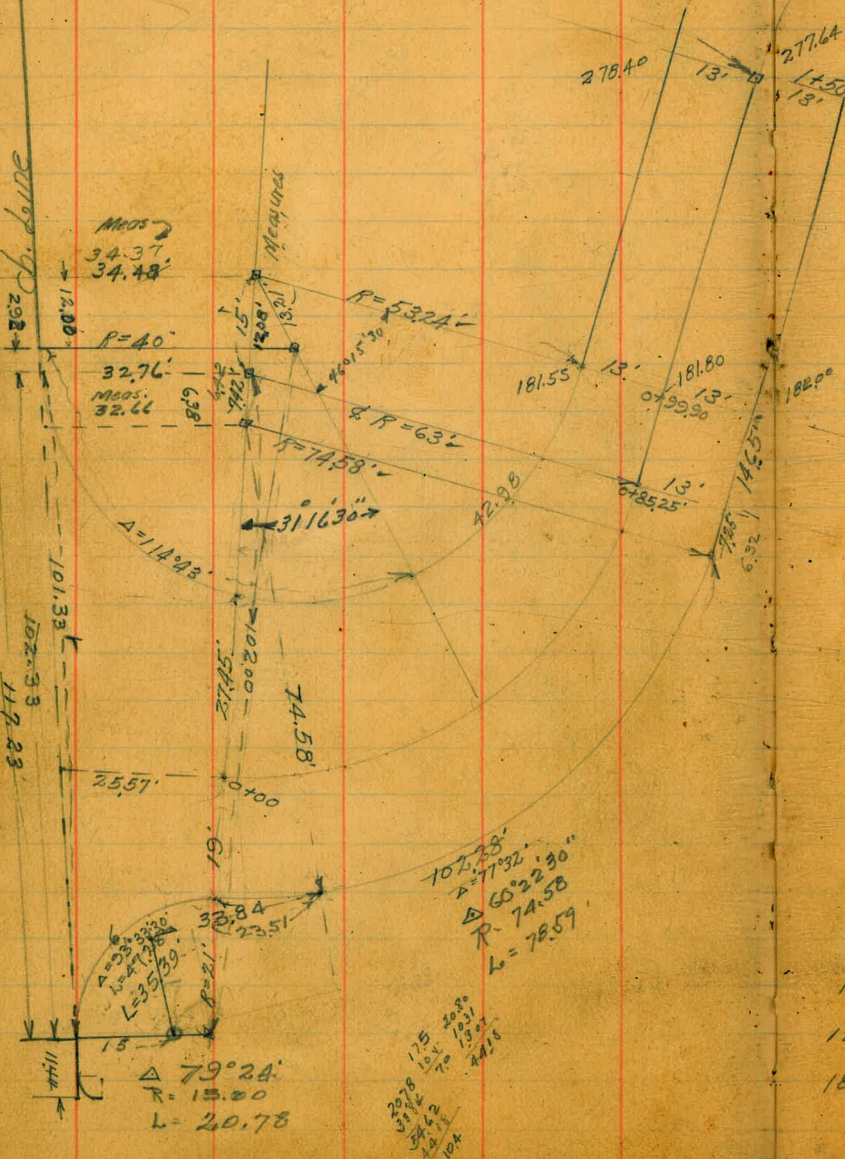
PARK

2 Nail in paving
With string
approx. 1' from cb.
121.00'

$\Delta = 87^{\circ}30'$
 $R = 100'$

See Page 69

CONSTRUCTION E.I. South Entrance



8'	281.55		
7'	282.25	282.00	14.65' ✓
10'	282.85	283.55	6.3' ✓
8.0'	283.80	284.05	13.5
12.0	284.60	285.15	13.0'
10	285.90	285.95	24.0
8.5	287.10	287.10	21.00
8'	288.00	288.10	17.5
9.5'	cb = 289.42	288.85	
	288.75 Ex. cb	288.85	
12'	cb = 290.02	290.12 cb	13.07'
	289.35	289.45	
12'	cb = 290.52	290.42 cb	10.31'
	289.85	289.75	
12'	cb = 290.67	289.62 cb	10.4'
	Grade 290.00	289.35 Grade	10.4'
18'	cb = 290.67	290.67 cb	
	Pav. = 290.00	290.00 Pav.	

North

South

Stations	Align	Defl. Δ	Curve Data
5 + 18.55 = E.C.	25°30'		24.30-22.19
+25	22° 48.07'	2° 49.85'	
5 + 100	19° 57.27'	5° 31.55'	
+75	17° 06.47'	8° 22.35'	
4 + 50	14° 16.67'	11° 13.05'	
+25	11° 25.87'	14° 03.85'	
4 + 00	8° 35.07'	16° 54.55'	
+75	5° 44.27'	19° 45.95'	
+50	2° 53.47'	22° 36.05'	
3 + 24.61 = B.C.			
	21.15'		
3 + 03.46 = E.C.	43°45'		
3 + 00	42° 45.53'		
+75	35° 35.78'		
+50	28° 26.08'		
+25	21° 16.38'		
2 + 00	14° 06.68'		
+75	6° 56.98'		
1 + 50.74 = B.C.			
+25			
1 + 00			
+85.25 = E.C.	38°46'		
+75	34° 06.33'	4° 40.1'	
+50	22° 44.22'	16° 02.1'	
+25	11° 22.11'	21° 43'	
0 + 00		33° 05.1'	
		58° 56'	

8901179
 $\Delta = 51200$
 $R = 251.58'$
 $L = 223.94'$
 $ST = 120$

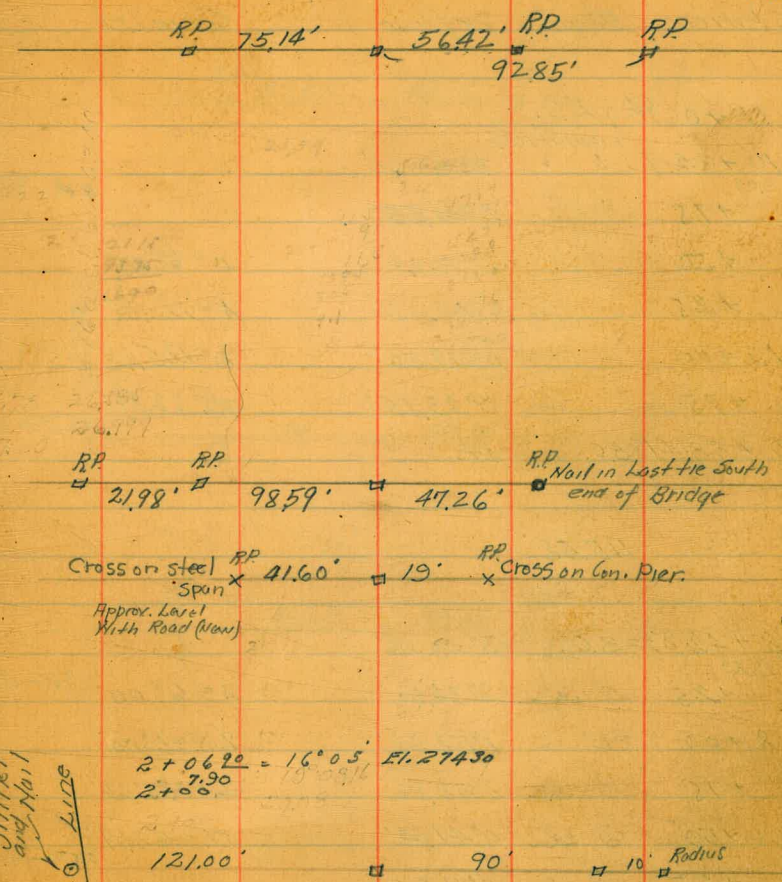
26.44-23.56
 26.84-23.92

1.5271630
 $\Delta = 87.30'$
 $R = 100'$
 $L = 152.72'$
 $ST = 95.75$

888121 = 414
 $L = 114.49$

28.62-
 27.77-

$\Delta = 77.93$
 $R = 63'$
 $L = 85.25$
 $ST =$



Stations Align. Defln. Curve Data

11 + 06.64 } E.C.
 10 + 84.07 } equation
 9.07
 + 75 2° 06.75'
 + 50 2° 11.00' Δ = 6° 00'
 + 25 1° 35.25' R = 1200'
 10 + 00 0° 59.50' L = 125.66'
 + 75 0° 13.75' ST = 62.89'
 9 + 58.41 - B.C. Lt. 16.79 → 16.49

9.18 - 8.97

16.79 → 16.49

115.58'

500
2.89
7.2

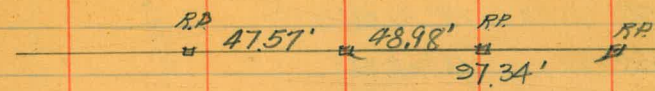
8 + 42.83 = E.C. 3° 00.00'
 17.83
 + 25 0° 25 2° 34.50' Δ = 6° 00' 17.61 - 18.05
 8 + 00 1° 2 1° 58.68' L.R = 1200'
 + 75 1° 38 1° 22.86' L = 125.66'
 + 50 2° 14 0° 47.04' ST = 62.89'
 + 25 2° 50 0° 11.22' 24.70 - 25.30
 783 + 17.17 - B.C. Lt. 7.73 - 7.93

110.47198

1.01211

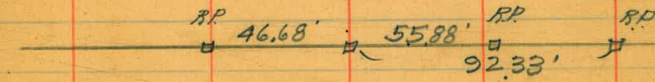
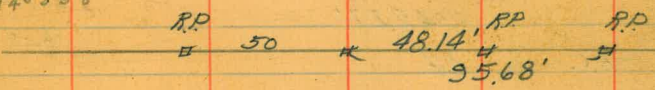
7 + 00
 + 50
 6 + 00
 5 + 75 168.62'

913 ST
 53.62 - 24°
 182710
 54813.0
 274065
 456775
 125982



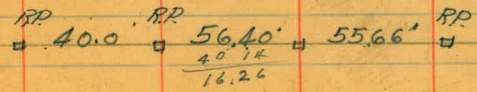
302
 .86603
 646
 519218
 941414
 579618
 55945588

2630
 .89493
 56.48
 715944
 357972
 536958
 447465
 505416414
 4814
 24



21°
 93358
 75
 280074
 573432
 7014394

27°30
 62.87
 887
 44009
 50296
 50296
 5576569



91355
 647
 24°
 639486
 365420
 448130
 59106685
 5742
 269

Station	Align.	Defln. A	True Bearing	Curve Data
+50	7 43	18° 31.56'		
+25	10 27	16° 08.32'		
17+00	12 30	13° 45.08'		$\Delta = 52^{\circ} 30'$
+75	14 53	11° 21.84'		$R = 300'$
+50	17 16	8° 58.60'		$L = 274.89'$
+25	19 40	6° 35.35'		$ST = 147.94'$
16+00	22 03	4° 12.11'		
+75	24 26	1° 48.87'		
+56	= B.C. 24 13	Lt.		

5.73 M per foot

145' { 95/13
10483

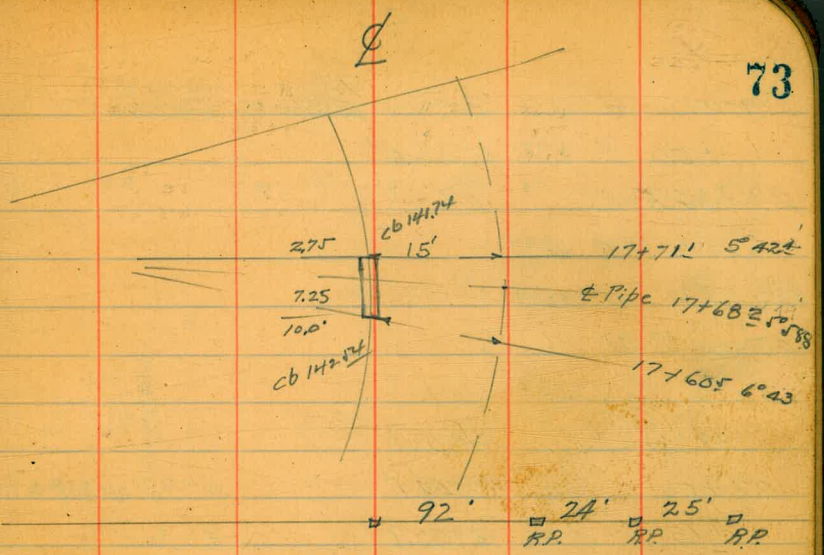
2379-2621
18.08-19.92

15+00

14+00

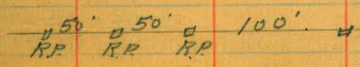
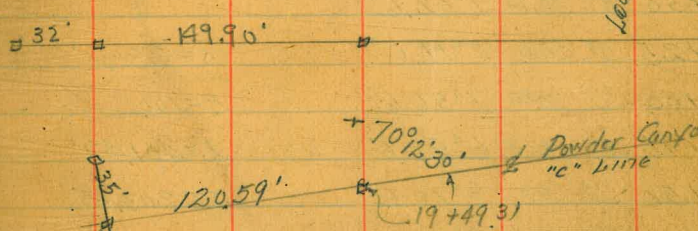
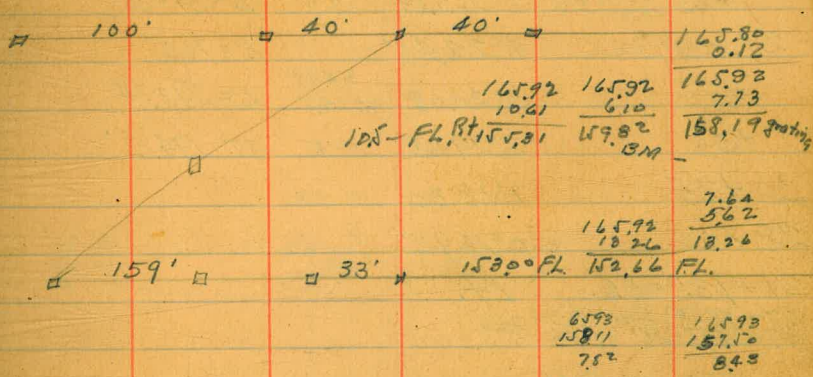
13+00

12+00



Station	Align.	Defln.	TRUE BEARING	CURVE DATA
23+50	1° 19.22'	0° 26.6'		
old 23+34.54 = B.C.		RT.		
+25	0° 43.25'			
23+00	0° 07.93'			
New 22+94.93 = B.C.				
+23.68 = E.C.	19° 00'			
22+00	2° 16'	16° 44.1'	$\Delta = 38° 00'$	248.276
+75	4° 39'	14° 20.9'	$R = 300'$	
+50	7° 02'	11° 57.7'	$L = 198.97'$	
+25	9 25	9° 34.5'	$JT = 103.30$	
21+00	11 49	7° 11.3'	23.79 14.5	25'
+75		4° 48.1'		262.29.1
+50		2° 24.9'		265.29.5
+24.71 = B.C.		Lt.		
20+00				
+75				
+49.31				
+25				
19+00				
+50				
+30.89 = E.C.		26° 15'		
5.89'			5.60	5.71 - 6.07
+25		25° 41.25'	0° 33.7'	23.75
18+00		23° 18.04'	2° 57'	
17+75		20° 54.80'	5° 20'	

23+65 grading El. 168.19



Louis DePrenon

Station	Align.	Defln. A	TRUE BEARING	CURVE DATA
+25		5° 23.84'	10° 06'	$\Delta = 31^{\circ} 00'$
29+00		4° 22.46'	11 8	$R = 700'$
+75		3° 21.08'	$\frac{2.448}{12914.5}$	$L = 378.74$
+50		2° 19.68'	13 20	ST. 194.12'
+25		1° 18.30'	14 12	
28+00		0° 16.92'	15 13	
27+93.11 = 86.	LT.			
27+75.58	Equation			
27+74.52	FC	11° 30'		
+50		10° 54.61'		
old.				
+35.97 = E.C.		11° 30'	10 36	
+25		10° 18.65'	11° 11.6'	1° 12'
27+00		9° 42.68'	10° 28.6'	1 48
+75		9° 06.72'	9° 45.6'	
+50		8° 30.76'	9° 02.6'	
+25		7° 54.8'	8° 19.6'	
26+00		7° 18.84'	7° 36.6'	
+75		6° 42.876'	6° 53.6'	
+50		6° 07'	6° 10.6'	
+25		5° 31'	5° 27.6'	
25+00		4° 55'	4° 44.6'	
+75		4° 19.03'	4° 01.6'	
+50		3° 43.06'	3° 18.6'	
+25		3° 07.10'	2° 35.6'	
24+00		2° 31.14'	1° 52.6'	
23+75		1° 55.18'	1° 09.6'	

10 90
10 54
36

4014257

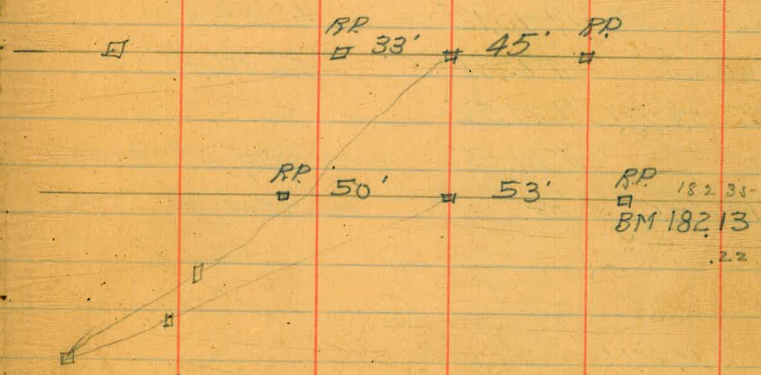
$\Delta = 23^{\circ} 00'$
 $R = 1000'$
 $L = 401.43'$
ST. 203.45

$L\pi = 1194.73'$
 $Lh = 479.59'$
 $Lst. 243.07'$
Min = 1.439
.98786 = 24.6965
14.5. 1.01214 = 25.9035

£

28+20
27+93.11
82

28+20
731
319

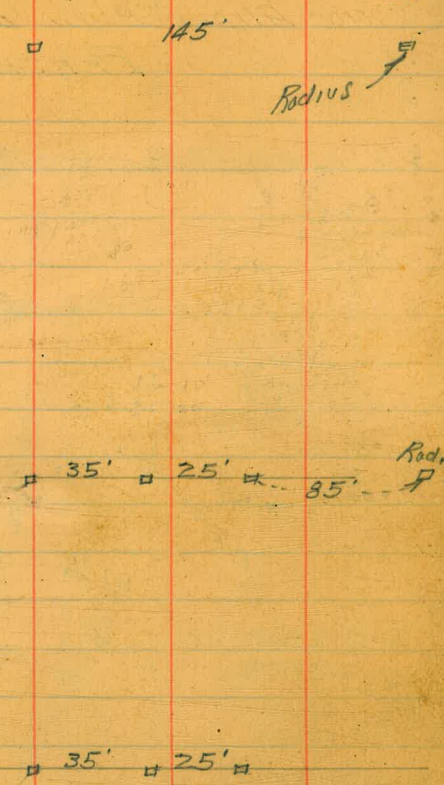


144
230
288
860
12

Station	Align.	Defln.	True Bearing	Curve Data
35+33.08	=Northedge	Pinny	Pershing	DIVE
+11.65	=E.C.		36°17.50'	
35+00	0°	19	33°59.17'	$\Delta 121.8152$
+75	7°	16	29°02.82'	$\Delta 73°35'$
+50	12°	19	24°06.47'	$R=145'$
+25	17°	08	19°10.12'	$L=183.69'$
34+00	22°	05	14°13.87'	$J.T. 106.48'$
+75	27°	00	9°17.52'	
+50			4°21.17'	
34+30			32°15'48"	$R=159.5$
			10 80	
33+27.96	=B.C.		Rt	Angle. 21°45'48"

156.11

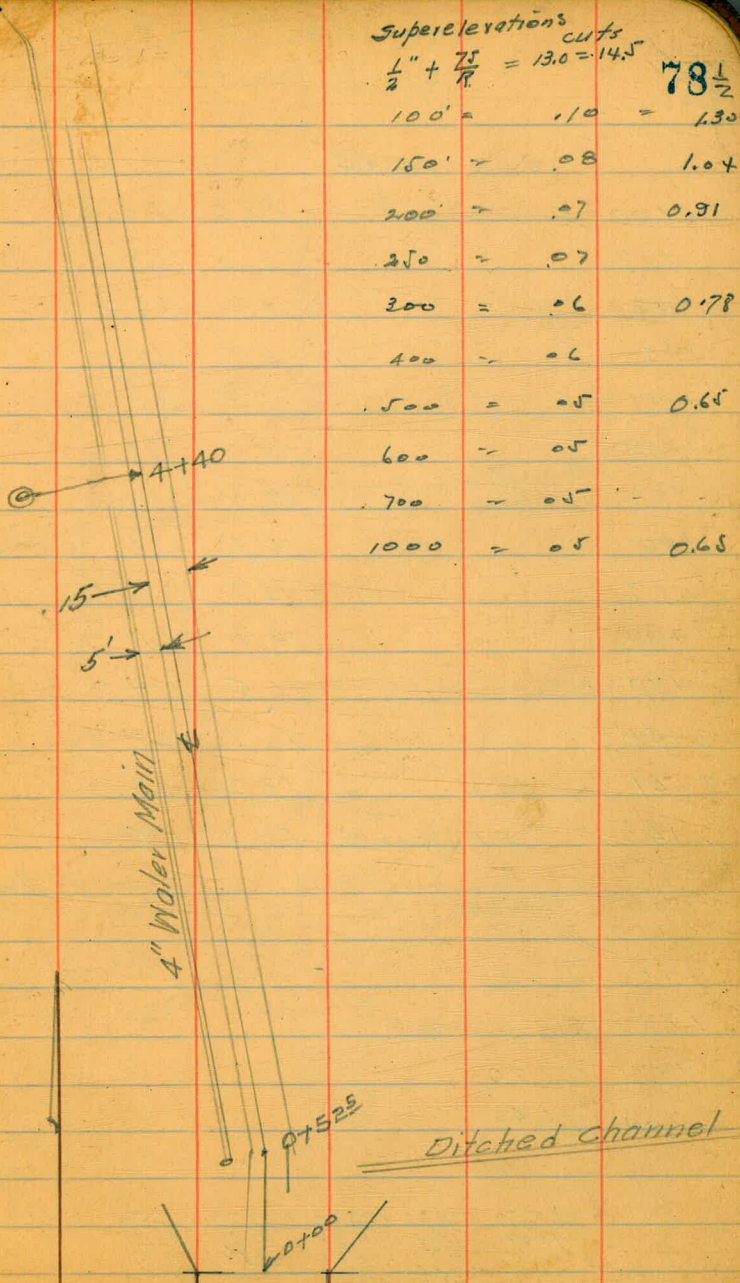
31	+71.85	=E.C.	15°30'	
	+50.		14°36.3'	0° 54
	+25		13°34.8'	1° 55'
31+00			12°39.5'	2 56
	+75		11°32.1'	3 58
	+50		10°30.8'	4 50
	+25		9°29.4'	6 04
30+00			8°28'	7 02
	+75		7°26.6'	8 03
29+50			6°25.2'	9 05



Sept - 20 - 1932

Sta.	+	HI	-	El.	2% Grade + or -
					1347.00
6+00					
+75					1344.00
+50					
+25					133.00
5+00					
+75					132.00
+50					
+25					131.00
4+00					
+75					130.00
+50					
+25					129.00
3+00					
+75					128.00
+50					
+25					127.00
2+00					
+75					126.00
+50					
+25					125.00
1+00					
+75					124.00
+50					123.00
0+00					

M.H.



B.M. Top N.W.
Wing Wall Wheeler Bridge

14213

Location and Levels
Proposed channel

Station	8.03	141.44	133.41	2 Stub 20+75-P-51
0+00 = Bottom channel	12.8	128.6		
+03	13.0	128.4		
+10	5.0	136.4		
+25	4.5	136.9		
+50	5.7	135.7		
1+00	8.2	133.2		
+22	11.2	130.2		
+50	14.4	127.0		
+57	13.8	128.6		
1+82	14.7	126.7		

+90 = Bottom channel	16.5	124.9
2+40 = " "	16.2	125.2
2+41 = top Bank	13.2	128.2
2+48 = " " Int slope on Lt.	13.2	128.2

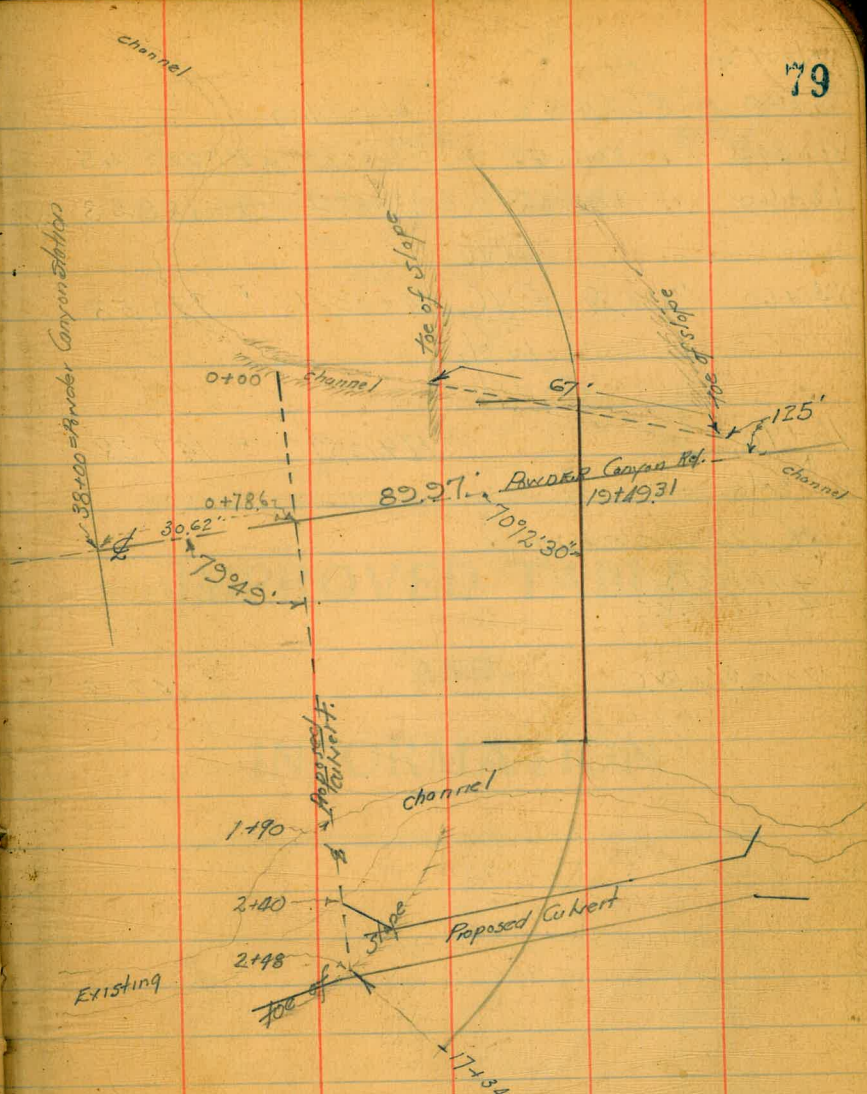
CONSTRUCTION GRADES ABOVE CHANNEL

Station	GRADES
0+00	128.50
+50	128.25
1+00	128.00 = Break
+50	127.20
2+00	126.40

128.50	128.25	128.00	127.20	126.40
11.39	11.64	11.87	12.69	13.49
9.18	4.20	6.31	12.47	12.39
+2.21	+7.44	+5.58	+0.27	+0.50

B.M. P-25

131.92
7.97
139.89-x



New Sta.

3+00 = El. 265.37 old station

10+84.2 ^{8.7%} r 202.65 = ^{Equation} 011+06.64 = El. 202.65

12+60 = 188.55 = P.V.C. 12+82.57 r 188.58 P.V.C.

200' VC

14+60 r 170.58 E.V.C. 14+82.57 r 170.58

10.0%

16+90 17+12.57 r 147.58

30%

Handwritten signature

12+82.57 = P.V.C.
14+82.57 = E.V.C.

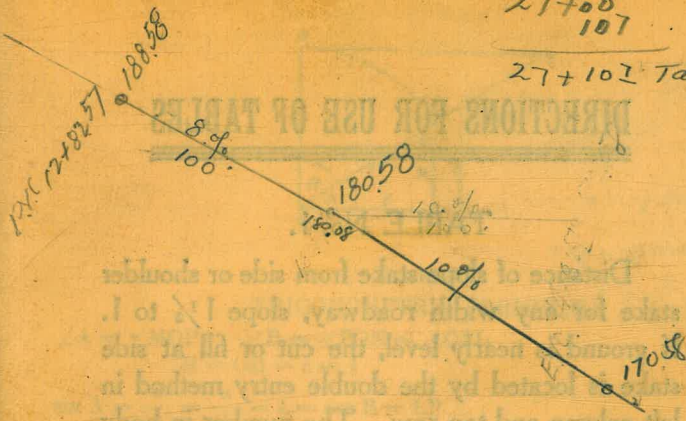
17+12.57 = P.V.C.

El. 188.58
170.58

147.58

27+00
107

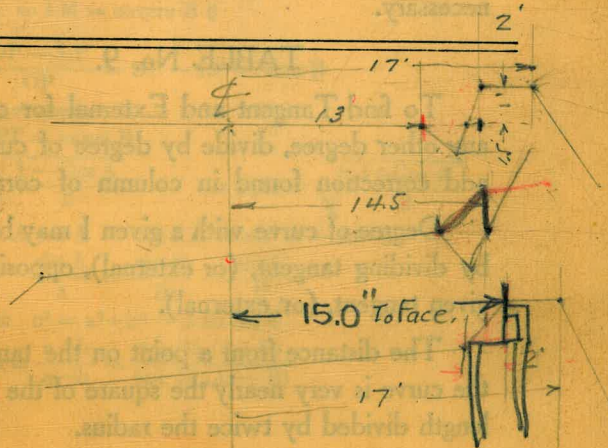
27+102 Tang.



IMPROVED TABLES

AND

INFORMATION



DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

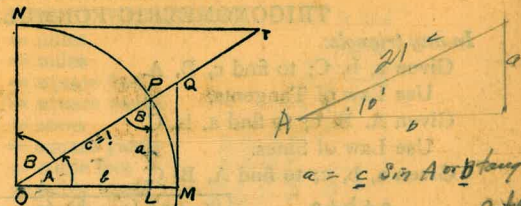


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Sines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$

$\begin{array}{r} 26 \ 7 \\ 23 \ 18 \\ \hline 2 \ 57 \\ \\ 2 \ 2 \ 7 \ 8 \\ 2 \ 0 \ 5 \ 6 \\ \hline 2 \ 2 \ 7 \\ 2 \ 1 \ 7 \\ \hline 4 \ 8 \ 1 \end{array}$

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Tangents.

Given A, B, c; to find a, b, C.

Use Law of Sines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\text{or } \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (E + b + 4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	$\frac{1}{16}$
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	$\frac{1}{8}$
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	$\frac{3}{16}$
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	$\frac{1}{4}$
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	$\frac{5}{16}$
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	$\frac{3}{8}$
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	$\frac{7}{16}$
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	$\frac{1}{2}$
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	$\frac{9}{16}$
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	$\frac{5}{8}$
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	$\frac{11}{16}$
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	$\frac{3}{4}$
$\frac{13}{16}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	$\frac{13}{16}$
$\frac{7}{8}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	$\frac{7}{8}$
$\frac{15}{16}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	$\frac{15}{16}$
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.0000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links
360° = 21600' = 1296000"		
Radius = arc of 57.2957790°		
Arc of 1° (radius = 1) = .017453292		
Arc of 1' (radius = 1) = .000290888		
Arc of 1" (radius = 1) = .000004848		

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{\pi}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11½ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{Mv^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

Horizontal Distance = R - R sin² a + C cos a

Vertical Distance = R ½ sin 2 a + C sin a

R = Reading × $\frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

3245
1786
19470
9735
22715
8245
1633520

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4374	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9348	5.6713	9353	5.7694	9358	5.8708	9363	5.9758	9368	6.0844	9372	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.4300	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	9995	31.242	9996	34.368	997	38.189	997	42.964	998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
90	60'	cos	50'	cos	40'	cos	30'	cos	20'	cos	10'	cos	0'

TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20

8988 48140 53.56
42940
32000
26964
50360
49940
54200

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=70°	I	T	E	I=80°	I	T	E	I=90°
61°	3375.0	920.2		71°	4086.9	1308.2		81°	4893.6	1805.3	
10'	3386.3	925.9	+	10'	4099.5	1315.6	+	10'	4908.0	1814.7	+
20'	3397.5	931.6	5° C.	20'	4112.1	1322.9	5° C.	20'	4922.5	1824.1	5° C.
30'	3408.8	937.3	T	30'	4124.8	1330.3	T	30'	4937.0	1833.6	T
40'	3420.1	943.1	.25	40'	4137.4	1337.7	.30	40'	4951.5	1843.1	.36
50'	3431.4	948.9	E	50'	4150.1	1345.1	E	50'	4966.1	1852.6	E
62°	3442.7	954.8	.080	72°	4162.8	1352.6	.110	82°	4980.7	1862.2	.149
10'	3454.1	960.6		10'	4175.6	1360.1		10'	4995.4	1871.8	
20'	3465.4	966.5		20'	4188.5	1367.6		20'	5010.0	1881.5	
30'	3476.8	972.4		30'	4201.2	1375.2		30'	5024.8	1891.2	
40'	3488.3	978.3		40'	4214.0	1382.8		40'	5039.5	1900.9	
50'	3499.7	984.3		50'	4226.8	1390.4		50'	5054.3	1910.7	
63°	3511.1	990.2	10° C.	73°	4239.7	1398.0	10° C.	83°	5069.2	1920.5	10° C.
10'	3522.6	996.2	T	10'	4252.6	1405.7	T	10'	5084.0	1930.4	T
20'	3534.1	1002.3		20'	4265.6	1413.5		20'	5099.0	1940.3	
30'	3545.6	1008.3	.51	30'	4278.5	1421.2	.61	30'	5113.9	1950.3	.72
40'	3557.2	1014.4	E	40'	4291.5	1429.0	E	40'	5128.9	1960.2	E
50'	3568.7	1020.5	.159	50'	4304.6	1436.8	.220	50'	5143.9	1970.3	.299
64°	3580.3	1026.6		74°	4317.6	1444.6		84°	5159.0	1980.4	
10'	3591.9	1032.8		10'	4330.7	1452.5		10'	5174.1	1990.5	
20'	3603.5	1039.0		20'	4343.8	1460.4		20'	5189.3	2000.6	
30'	3615.1	1045.2		30'	4356.9	1468.4		30'	5204.4	2010.8	
40'	3626.8	1051.4		40'	4370.1	1476.4		40'	5219.7	2021.1	
50'	3638.5	1057.7		50'	4383.3	1484.4		50'	5234.9	2031.4	
65°	3650.2	1063.9	T	75°	4396.5	1492.4	T	85°	5250.3	2041.7	T
10'	3661.9	1070.2	.76	10'	4409.8	1500.5	.91	10'	5265.6	2052.1	1.09
20'	3673.7	1076.6	E	20'	4423.1	1508.6	E	20'	5281.0	2062.5	E
30'	3685.4	1082.9		30'	4436.4	1516.7		30'	5296.4	2073.0	
40'	3697.2	1089.3	.240	40'	4449.7	1524.9	.332	40'	5311.9	2083.5	.450
50'	3709.0	1095.7		50'	4463.1	1533.1		50'	5327.4	2094.1	
66°	3720.9	1102.2		76°	4476.5	1541.4		86°	5343.0	2104.7	
10'	3732.7	1108.6		10'	4489.9	1549.7		10'	5358.6	2115.3	
20'	3744.6	1115.1		20'	4503.4	1558.0		20'	5374.2	2126.0	
30'	3756.5	1121.7		30'	4516.9	1566.3		30'	5389.9	2136.7	
40'	3768.5	1128.2	20° C.	40'	4530.4	1574.7	20° C.	40'	5405.6	2147.5	20° C.
50'	3780.4	1134.8	T	50'	4544.0	1583.1	T	50'	5421.4	2158.4	T
67°	3792.4	1141.4	1.02	77°	4557.6	1591.6	1.22	87°	5437.2	2169.2	1.45
10'	3804.4	1148.0	E	10'	4571.2	1600.1	E	10'	5453.1	2180.2	E
20'	3816.4	1154.7	.321	20'	4584.8	1608.6	.445	20'	5469.0	2191.1	.603
30'	3828.4	1161.3		30'	4598.5	1617.1		30'	5484.9	2202.2	
40'	3840.5	1168.1		40'	4612.2	1625.7		40'	5500.9	2213.2	
50'	3852.6	1174.8		50'	4626.0	1634.4		50'	5517.0	2224.3	
68°	3864.7	1181.6		78°	4639.8	1643.0		88°	5533.1	2235.5	
10'	3876.8	1188.4	25° C.	10'	4653.6	1651.7	25° C.	10'	5549.2	2246.7	25° C.
20'	3889.0	1195.2	T	20'	4667.4	1660.5	T	20'	5565.4	2258.0	T
30'	3901.2	1202.0		30'	4681.3	1669.2		30'	5581.6	2269.3	
40'	3913.4	1208.9	1.28	40'	4695.2	1678.1	1.53	40'	5597.8	2280.6	1.83
50'	3925.6	1215.8	E	50'	4709.2	1686.9	E	50'	5614.2	2292.0	E
69°	3937.9	1222.7	.403	79°	4723.2	1695.8	.558	89°	5630.5	2303.5	.756
10'	3950.2	1229.7		10'	4737.2	1704.7		10'	5646.9	2315.0	
20'	3962.5	1236.7		20'	4751.2	1713.7		20'	5663.4	2326.6	
30'	3974.8	1243.7		30'	4765.3	1722.7		30'	5679.9	2338.2	
40'	3987.2	1250.8		40'	4779.4	1731.7		40'	5696.4	2349.8	
50'	3999.5	1257.9		50'	4793.6	1740.8		50'	5713.0	2361.5	
70°	4011.9	1265.0	30° C.	80°	4807.7	1749.9	30° C.	90°	5729.7	2373.3	30° C.
10'	4024.4	1272.1	T	10'	4822.0	1759.0	T	10'	5746.3	2385.1	T
20'	4036.8	1279.3	1.54	20'	4836.2	1768.2	1.84	20'	5763.1	2397.0	2.20
30'	4049.3	1286.5		30'	4850.5	1777.4		30'	5779.9	2408.9	
40'	4061.8	1293.6		40'	4864.8	1786.7		40'	5796.7	2420.9	
50'	4074.4	1300.9	.485	50'	4879.2	1796.0	.671	50'	5813.6	2432.9	.910

T = R tan ½ I E = R exsec ½ I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=100°	I	T	E	I=110°	I	T	E	I=120°
91°	5830.5	2444.9	+	101°	6950.6	3278.1	+	111°	8336.7	4386.1	+
10'	5847.5	2457.1	5° C.	10'	6971.3	3294.1	5° C.	10'	8362.7	4407.6	5° C.
20'	5864.6	2469.3	T	20'	6992.0	3310.1	T	20'	8388.9	4429.2	T
30'	5881.7	2481.5	.43	30'	7012.7	3326.1	.51	30'	8415.1	4450.9	.62
40'	5898.8	2493.8	E	40'	7033.6	3342.3	E	40'	8441.5	4472.7	E
50'	5916.0	2506.1	.200	50'	7054.5	3358.5	.268	50'	8468.0	4494.6	.360
89°	5933.2	2518.5	10° C.	109°	7075.5	3374.9	10° C.	119°	8494.6	4518.6	10° C.
10'	5950.5	2531.0	T	10'	7096.6	3391.2	T	10'	8521.3	4538.8	T
20'	5967.9	2543.5		20'	7117.8	3407.7		20'	8548.1	4561.1	
30'	5985.3	2556.0		30'	7139.0	3424.3		30'	8575.0	4583.4	
40'	6002.7	2568.6		40'	7160.3	3440.9		40'	8602.1	4606.0	
50'	6020.2	2581.3		50'	7181.7	3457.6		50'	8629.3	4628.6	
93°	6037.8	2594.0	10° C.	103°	7203.2	3474.4	10° C.	113°	8656.6	4651.3	10° C.
10'	6055.4	2606.8	T	10'	7224.7	3491.3	T	10'	8684.0	4674.2	T
20'	6073.1	2619.7	.86	20'	7246.3	3508.2	.103	20'	8711.5	4697.2	.125
30'	6090.8	2632.6	E	30'	7268.0	3525.2	E	30'	8739.2	4720.3	E
40'	6108.6	2645.5	.401	40'	7289.8	3542.4	.536	40'	8767.0	4743.6	.721
50'	6126.4	2658.5		50'	7311.7	3559.6		50'	8794.9	4766.9	
94°	6144.3	2671.6		104°	7333.6	3576.8		114°	8822.9	4790.4	
10'	6162.2	2684.7		10'	7355.6	3594.2		10'	8851.0	4814.1	
20'	6180.2	2697.9		20'	7377.8	3611.7		20'	8879.3	4837.8	
30'	6198.3	2711.2		30'	7399.9	3629.2		30'	8907.7	4861.7	
40'	6216.4	2724.5		40'	7422.2	3646.8		40'	8936.3	4885.7	
50'	6234.6	2737.9	15° C.	50'	7444.6	3664.5	15° C.	50'	8965.0	4909.9	15° C.
95°	6252.8	2751.3	T	105°	7467.0	3682.3	T	115°	8993.8	4934.1	T
10'	6271.1	2764.8	1.30	10'	7489.6	3700.2	1.56	10'	9022.7	4958.6	1.93
20'	6289.4	2778.3	E	20'	7512.2	3718.2	E	20'	9051.7	4983.1	E
30'	6307.9	2792.0	.604	30'	7534.9	3736.2	.806	30'	9080.9	5007.8	1.09
40'	6326.3	2805.6		40'	7557.7	3754.4		40'	9110.3	5032.6	
50'	6344.8	2819.4		50'	7580.5	3772.6		50'	9139.8	5057.6	
96°	6363.4	2833.2		106°	7603.5	3791.0		116°	9169.4	5082.7	
10'	6382.1	2847.0		10'	7626.6	3809.4		10'	9199.1	5107.9	
20'	6400.8	2861.0		20'	7649.7	3827.9		20'	9229.0	5133.3	
30'	6419.5	2875.0	20° C.	30'	7672.9	3846.5	20° C.	30'	9259.0	5158.8	20° C.
40'	6438.4	2889.0	T	40'	7696.3	3865.2	T	40'	9289.2	5184.5	T
50'	6457.3	2903.1	1.74	50'	7719.7	3884.0	2.08	50'	9319.5	5210.3	2.52
97°	6476.2	2917.3	E	107°	7743.2	3902.9	E	117°	9349.9	5236.2	E
10'	6495.2	2931.6	.809	10'	7766.8	3921.9	1.08	10'	9380.5	5262.3	1.46
20'	6514.3	2945.9		20'	7790.5	3940.9		20'	9411.3	5288.6	
30'	6533.4	2960.3		30'	7814.3	3960.1		30'	9442.2	5315.0	
40'	6552.6	2974.7		40'	7838.1	3979.4		40'	9473.2	5341.5	
50'	6571.9	2989.2		50'	7862.1	3998.7		50'	9504.4	5368.2	
98°	6591.2	3003.8		108°	7886.2	4018.2		118°	9535.7	5395.1	
10'	6610.6	3018.4	25° C.	10'	7910.4	4037.8	25° C.	10'	9567.2	5422.1	25° C.
20'	6630.1	3033.1	T	20'	7934.6	4057.4	T	20'	9598.9	5449.2	T
30'	6649.6	3047.9		30'	7959.0	4077.2		30'	9630.7	5476.5	
40'	6669.2	3062.8	2.18	40'	7983.5	4097.1	2.61	40'	96		

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord and multiply by length of chord.

TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

Allyn E. Chain from Ref. Mail 2284 from Butts Plan.

Official Crops by 1000s
 Station 16700
 18+00
 150
 19+00
 150
 20+00
 150
 21+00
 150
 22+00
 150

Grades
 162
 146
 144
 141.9
 141.9
 141.9
 142
 145.9
 148.9
 151.9
 155.9
 167.9

11+80
 11+97

1456.85
 41.06
 1158

398
 353
 75.1

158.84
 24.2
 183.4

78
 07
 99
 84
 14

22.6
 14
 8.6
 285.25
 18
 290.43

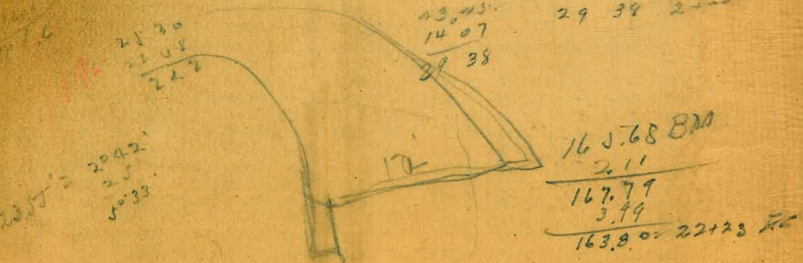
25.00
 38.56
 14.4
 26
 26.44

Grade 65%
 33.79
 31.78
 1.56
 68
 17.7
 67.7

Frank Wherry
 183.87

11 100 8°-9' = 275
 15 44 15° 19' 2150
 29 39 2100

43.45
 14.07
 29.38



446 410 374
 187 18V 161
 25.9 726 193 740

C-2004 Spat. Pole
 in Fill
 c. 2395 Pole and Guy.

331.61
 1.5
 333.18
 120.59
 89.97
 36.62

205.7
 77
 198

TP on Rock L 22+00 → 168.34 D-51
 18.30

181.64
 0.43
 181.21 = TP
 12.064
 193.27 = X
 0.50
 192.77 = TP
 12.97
 205.74 = X
 5.71
 199.93 = TP
 7.70
 207.63 = X
 12.91
 194.72 = TP
 2.58
 197.60 = TP
 0.19
 197.11 = TP
 23.89
 210.00 = X
 19.30
 199.60 = TP
 7.32
 206.94 = X
 12.40
 198.04 = TP
 3.07
 197.11 = TP
 12.59
 184.12 = 03 Error
 154.15 = TP
 12.99
 177.14 = X

chk. on TP D-50