

1450  
ATLANTIC ST.  
MARASTHY TO BROADWAY

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LEVEL BOOK

373 A

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# KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

## Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

5470-L  
2147 B  
2198 B

ENGINEERING DEPARTMENT,  
CITY OF SAN DIEGO,  
CALIFORNIA.

Atlantic St	Juniper to Harasthyt-	
Proposed Culvert	Atlantic at Bean	33
Rosecrans	P.H. Way to Gaines	34
Jefferson & Rosecrans		<del>41-93</del> <sup>46-99</sup>
Survey of Knoxville St.	Northward from Merens.	<del>42-95</del> <sup>50-59</sup>
	Along Tecolote Creek.	

Cross Section Atlantic St  
Suniper to Harastby

BM	135	11.35	10.00	NEBR Suniper Atlantic
43 + 56.68 = NCB of Suniper				
66 ft - New C&B C Topls	1.08	10.27		
66 ft Paving	1.66	9.69		
46 ft "	2.01	9.34		
46 ft Top C6	1.35	10.00		
43 + 70.68 = NCB Suniper				
34 ft - Existing C6 Top	1.42	9.93		
34 ft 07 Pav	1.98	9.37		
30 ft " "	2.03	9.32		
20 ft " "	2.11	9.24		
10 ft " "	2.18	9.17		
1/2 " "	2.34	9.11		
16 ft " "	2.44	8.91		
20 ft " "	2.69	8.66		
27 ft " "	2.87	8.48		
30 ft " "	2.82	8.53		
46 ft " "	2.51	8.84		
46 ft Top C6 ✓	2.47	8.88		

	11.35		11.35
44+0			
46 ft - Top C6 ✓	2.55	8.80	
46 ft Gutter	3.3	8.1	
30 ft	3.1	8.3	
20 ft	2.8	8.6	
10 ft - Edge Pav	2.36	8.99	
1/2 " " "	2.22	9.13	
10 ft Edge " "	2.15	9.20	
20 ft	2.6	8.8	
30 ft	2.7	8.7	
46 ft Gutter	2.5	8.9	
44+50			
46 ft Gutter	3.1	8.5	
30 ft	3.0	8.4	
20 ft	2.7	8.7	
10 ft - Edge Pav	2.20	9.15	
1/2 " " "	2.26	9.09	
10 ft - Edge " "	2.42	8.93	
20 ft	3.1	8.5	
30 ft	3.4	8.0	

2

1135

46 Lt	3.5	7.9
46 Lt Top cb ✓	3.78	8.57
4570		
46 Lt Top cb ✓	3.00	8.35
46 Lt	4.0	7.4
30 Lt	3.1	7.8
20 Lt	3.2	8.2
10 Lt = Edge Pav	2.55	8.80
✓ 7 07 "	2.49	8.86
10 Rt = Edge "	2.38	8.97
30 Rt	3.0	8.4
30 Rt	3.2	8.2
46 Rt = Gutter	2.7	8.7
45+50		
46 Rt = Gut	3.4	8.0
30 Rt	3.3	8.1
30 Rt	3.2	8.2
10 Rt = Edge Pav	2.59	8.76
✓ 7 09 "	2.69	8.66
10 Lt " "	2.84	8.51

1135

3

20 Lt	3.7	7.7
30 Lt	3.9	7.5
46 Lt	4.2	7.2
46 Lt Top cb ✓	3.20	8.15
46 Lt 0		
46 Lt - Top cb ✓	3.37	7.98
16 Lt	4.4	7.0
30 Lt	3.9	7.5
20 Lt	3.9	7.5
10 Lt = Edge Pav	3.05	8.30
✓ 7 07 "	2.91	8.44
10 Rt = Edge "	2.81	8.54
20 Rt	3.4	8.0
30 Rt	3.8	7.6
46 Rt = Gut	3.7	7.7
46 Lt 50		
46 Rt = Gut	3.8	7.6
30 Rt	3.8	7.6
20 Rt	3.5	7.9
10 Rt = Edge Pav	3.01	8.34

11.35

✓ $\frac{1}{2}$ 07 Pav	3.10	8.25
10 Lt = Edge Pav.	3.21	8.09
20 Lt	4.2	7.2
30 Lt	1.5	6.9
46 Lt	4.7	6.7
46 Lt = TopCb ✓	3.62	7.73
47+0		
46 Lt = TopCb ✓	3.84	7.51
46 Lt	4.9	6.5
30 Lt	4.7	6.7
20 Lt	4.3	7.1
10 Lt = Edge Pav	3.50	7.85
✓ $\frac{1}{2}$ 07 "	3.33	8.02
10 Rt = Edge "	3.24	8.11
20 Rt	3.9	7.5
30 Rt	4.1	7.3
46 Rt = Gut	3.9	7.5
47+50 = S End Cb on Rt. ✓		
46 Rt = TopCb End. ✓	3.18	8.17
46 Rt	4.0	7.4

11.35

1/4

30 Rt	4.4	7.0
20 Rt	3.9	7.5
10 Rt = Edge Pav	3.51	7.84
✓ $\frac{1}{2}$ 07 "	3.58	7.77
10 Lt = Edge	3.70	7.65
20 Lt	1.5	6.9
30 Lt	4.7	6.7
46 Lt	4.9	6.5
46 Lt TopCb ✓	4.04	7.37
48+0 = N End Cb on Rt ✓		
46 Lt = TopCb ✓	4.23	7.12
46 Lt	5.1	6.3
30 Lt	5.0	6.4
20 Lt	4.5	6.9
10 Lt = Edge Pav	3.99	7.36
✓ $\frac{1}{2}$ 07 "	3.86	7.49
10 Rt = Edge	3.83	7.52
20 Rt	4.3	7.1
30 Rt	4.7	6.7
46 Rt	4.4	7.0
46 Rt TopCb ✓	3.57	7.78

11.35

48+50

46 Pt = Gutter	4.8	6.6
30 Pt	4.9	6.5
20 Pt	4.4	7.0
20 Pt - Edge Par	4.08	7.27
✓ 1/2 on "	4.13	7.22
10 Lt = Edge	4.26	7.09
20 Lt	4.9	6.5
30 Lt	5.2	6.2
46 Lt	5.5	5.9
46 Lt TopCb ✓	4.4	6.89

48+55

46 Lt = Grating 5.51 5.84

49+0

46 Lt TopCb ✓	4.65	6.70
30 Lt = Top Rail	4.58	6.77
20 Lt	4.7	6.7
10 Lt - Edge Par	4.36	6.99
✓ 1/2 on "	4.30	7.05
10 Pt - Edge	4.26	7.09

11.35

5

20 Pt	4.8	6.6
30 Pt	5.0	6.4
46 Pt	5.1	6.3

49+23 - 1/2 Lt on Pt

46 Pt TopCb ✓	3.94	7.41
46 Pt Grating	4.97	6.38

49+3246 - 1/2 RR Spar

46 Pt - TopCb ✓	3.90	7.45
46 Pt	4.8	6.6
30 Pt	4.6	6.8
20 Pt	4.3	7.1

10 Pt = Edge Par 4.12 7.23

✓ 1/2 on " 1/2 Spar 4.23 7.12

10 Lt - Edge 4.26 7.09

20 Lt 4.8 6.6

30 Lt 5.1 6.3

46 Lt 5.6 5.8

46 Lt - TopCb ✓ 4.61 6.74

49+36 1/2 Lt on Lt

46 Lt - TopCb ✓ 4.60 6.75

46 Lt Grating 5.66 5.75

1135

49+50

46 Lt TopCb ✓ 4.55 6.80

46 Lt 5.3 6.1

30 Lt 5.2 6.2

20 Lt 4.9 6.5

10 Lt Edge Pair 4.14 7.21

✓ 1/2 02 4.07 7.28

10 Rt Edge 4.03 7.32

20 Rt TopRail 4.02 7.33

30 Rt 3.9 7.5

46 Rt 3.9 7.5

46 Rt TopCb ✓ 3.74 7.61

TP 643 140 3.77 7.58

49+81 = Grating 3.4 x 2.4

37.5 Rt 02 Grating 6.43 ~~7.42~~ <sup>7.58</sup>

50+0

46 Rt TopCb ✓ 6.14 7.87

46 Rt 6.9 7.1

30 Rt 6.8 7.2

20 Rt 6.7 7.3

1401

10 Rt Edge Pair 6.50 7.51

✓ 1/2 02 6.52 7.49

10 Lt Edge 6.53 7.48

30 Lt 7.3 6.7

30 Lt 7.6 6.4

46 Lt 7.6 6.4

46 Lt TopCb ✓ 6.94 7.07

50 + 51.83 = 52 Laurel

46 Lt TopCb ✓ 6.67 7.34

46 Lt 7.4 6.6

30 Lt 7.4 6.6

20 Lt 7.1 6.9

10 Lt Edge Pair 6.48 7.59

✓ 1/2 02 6.31 7.70

10 Rt Edge 6.30 7.71

20 Rt 6.6 7.4

30 Rt 6.7 7.3

37 Rt Grating 3.4 x 2.4 6.66 7.35

46 Rt 6.9 7.1

46 Rt TopCb ✓

6



14.01

## S.E. Curb Lot at Center Rd.

54 Rt Top Cb ✓ 6.03 7.98

54 Rt 7.02 6.99

## 50+91.83 = S Laurel

46 Rt 5.3 8.7

30 Rt 6.8 7.7

20 Rt 6.8 7.2

10 Rt. Edge Pav 6.04 7.97

✓ 1/2 07 " 6.02 7.99

10 Lt. Edge 6.12 7.89

20 Lt 7.1 6.9

30 Lt 7.3 6.7

46 Lt 7.1 6.9

## 51+31.83 = N.L.

46 Lt Top Cb ✓ 6.15 7.86

46 Lt 7.1 6.9

30 Lt 7.1 6.9

20 Lt 6.6 7.4

10 Lt = Edge Pav 5.80 8.21

✓ 1/2 07 " 5.70 8.31

14.01

10 Rt = Edge Pav 5.63 8.38

20 Rt 6.5 7.5

30 Rt 6.5 7.5

46 Rt 6.1 7.9

46 Rt Top Cb ✓ 5.25 8.76

51+50

46 Rt. Top Cb ✓ 5.14 8.87

20 Rt 6.1 7.9

30 Rt 6.2 7.8

20 Rt 6.2 7.8

15 Rt 6.0 8.0

10 Rt. Edge Pav 5.45 8.54

✓ 1/2 07 " 5.54 8.47

10 Lt. Edge 5.65 8.36

20 Lt 6.6 7.4

30 Lt 7.0 7.0

46 Lt 7.0 7.0

46 Lt Top Cb ✓ 5.97 8.04

52+0

46 Lt Top Cb ✓ 5.45 8.56

46 Lt 6.5 7.5

7

	14.01		
30 Lt	6.4	7.6	
20 Lt	5.9	8.1	
10 Lt - Edge Par	5.15	8.86	
✓ 1/2 oz "	4.98	9.03	
10 Rt - Edge	4.92	9.09	
20 Rt	5.7	8.3	
30 Rt	5.2	8.2	
46 Rt	5.3	8.7	
46 Rt - TopCb ✓	4.63 ✓	9.38	
	52+50		
46 Rt - TopCb ✓	4.08	9.93	
46 Rt	5.1	8.9	
30 Rt	5.4	8.6	
20 Rt	5.1	8.9	
10 Rt - Edge Par	4.33	9.68	
✓ 1/2 oz "	4.45	9.56	
10 Lt - Edge "	4.63	9.38	
20 Lt	5.5	8.5	
30 Lt	6.0	8.0	
46 Lt	5.9	8.1	
46 Lt - TopCb ✓	4.87 ✓	9.14	

	14.01		88
	53+50		
46 Lt - TopCb ✓	1.41	9.57	
46 Lt	5.5	8.5	
30 Lt	5.4	8.6	
20 Lt	4.9	9.1	
10 Lt - Edge Par	4.06	9.95	
✓ 1/2 oz "	3.95	10.06	
10 Rt - Edge "	3.88	10.13	
20 Rt	4.1	9.6	
30 Rt	4.9	9.1	
46 Rt	4.3	9.7	
46 Rt - TopCb ✓	3.50	10.51	
	53+50		
46 Rt - TopCb ✓	2.92	11.09	
46 Rt	3.8	10.2	
30 Rt	4.4	9.6	
20 Rt	3.9	10.1	
10 Rt - Edge Par	3.36	10.65	
✓ 1/2 oz "	3.45	10.56	
10 Lt - Edge "	3.58	10.43	

14.01

20 Lt	45	9.5
30 Lt	50	9.0
46 Lt	50	9.0
46 Lt = TopCb	✓ 393	10.08

54+0

46 Lt - TopCb	✓ 341	10.60
46 Lt	46	9.4
30 Lt	45	9.5
30 Lt	38	10.2

10 Lt - Edge Par	3.04	10.97	54+22
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✓ 1/2 07 "	2.92	11.09	38 Pt. Open Out Grating 2.82
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10 Pt - Edge "	2.86	11.15
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20 Pt	3.8	10.2
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30 Pt	3.9	10.1
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46 Pt	3.2	10.8
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46 Pt - TopCb	✓ 246	11.55
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54+50

46 Pt - TopCb	✓ 1.89	12.12
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46 Pt	2.7	11.3
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30 Pt	3.3	10.7
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14.01

9

30 Pt	3.1	10.9
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10 Pt - Edge Par	2.34	11.67
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✓ 1/2 07 "	2.38	11.63
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10 Lt - Edge	2.50	11.51
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20 Lt	3.5	10.5
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30 Lt	4.1	9.9
-------	-----	-----

46 Lt	4.3	9.7
-------	-----	-----

46 Lt - TopCb	✓ 293	11.08
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55+0

46 Lt - TopCb	✓ 243	11.58
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46 Lt	3.7	10.3
-------	-----	------

30 Lt	3.3	10.7
-------	-----	------

20 Lt	2.8	11.2
-------	-----	------

10 Lt - Edge Par	1.97	12.04
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✓ 1/2 07 "	1.88	12.13
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10 Pt - Edge	1.82	12.19
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20 Pt	2.5	11.5
-------	-----	------

30 Pt	2.8	11.2
-------	-----	------

46 Pt	2.3	11.7
-------	-----	------

46 Pt - TopCb	✓ 1.38	12.63
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14.01

55+50

46 Pt-TopCb	✓	0.90	13.11
46 Pt		2.0	12.0
30 Pt		2.3	11.7
20 Pt		2.0	12.0
10 Pt-Edge Pav		1.33	12.68
✓ 1/2 .07 "		1.38	12.63
10 Pt-Edge "		1.52	12.49
20 Lt		2.6	11.4
30 Lt		3.0	11.0
46 Lt		3.0	11.0
46 Lt-TopCb	✓	1.93	12.08

56+0

46 Lt-TopCb	✓	1.45	12.56
46 Lt		2.4	11.6
30 Lt		2.4	11.6
20 Lt		1.9	12.1
10 Lt-Edge Pav		0.97	13.04
✓ 1/2 .07 "		0.86	13.15
10 Pt-Edge "		0.82	13.19

14.01

10

20 Pt		1.6	12.4
30 Pt		1.8	12.2
46 Pt		1.1	12.9
46 Pt-TopCb	✓	0.42	13.59
TP	7.47	19.98	1.50
			12.51

56+50

46 Pt-TopCb	✓	5.90	14.08
46 Pt		6.9	13.1
30 Pt		6.6	13.4
20 Pt		6.6	13.4
10 Pt-Edge Pav		6.30	13.68
✓ 1/2 .07 "		6.40	13.58
10 Lt-Edge "		6.55	13.43
20 Lt		7.2	12.8
30 Lt		7.6	12.4
46 Lt		7.9	12.1
46 Lt-TopCb	✓	6.94	13.04

56+68 = So End Fall Widths Pav ing

46 Lt-TopCb	✓	6.74	13.24
46 Lt on Pav		7.42	12.56

19-98

40 Lt on Paving	712	12.81
30 Lt " "	675	13.23
20 Lt " "	657	13.41
10 Lt " "	636	13.62
1/2 " " "	620	13.78
10 Pt " "	609	13.89
20 Pt " "	612	13.86
30 Pt " "	615	13.83
40 Pt " "	630	13.68
46 Pt " "	640	13.58
46 Pt Topcb ✓	573	14.25

57+87.53 B.C. Lt

46 Pt. Topcb ✓	469	15.29
46 Pt on Paving	534	14.64
40 Pt " "	534	14.74
30 Pt " "	509	14.89
20 Pt " "	502	14.96
10 Pt " "	501	14.97
1/2 " " "	506	14.92
10 Lt " "	520	14.78

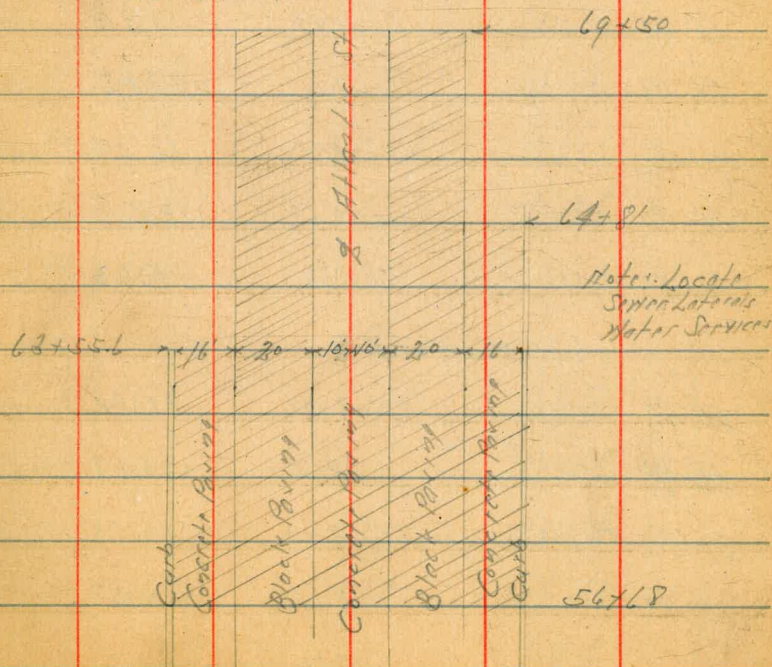
19-98

11

20 Lt on Paving	538	14.60	
30 Lt " "	570	14.28	
40 Lt " "	606	13.92	
46 Lt " "	624	13.74	
46 Lt Topcb ✓	565	14.33	
TP 374	18.27	545	14.53
BM	607	12.20	

BPE in the Co  
Front Adm Bldg  
Lindbergh Field  
12.235

Sketch of Paving At Lindbergh Field  
From Sta. 56+68 to 69+50



Atlantic St.

B.M.	3.59	15.82	12.23
	63+55.6 = 11' End Full Width Pav		
46' Lt TopCb	✓	195	13.87
46' Lt on Pav		216	13.16
30' Lt		215	13.67
20' Lt		205	13.77
10' Lt		191	13.88
1/2		194	13.88
10' Rt		192	13.90
20' Rt		196	13.86
30' Rt		208	13.74
46' Rt		238	13.44
46' Rt TopCb	✓	180	14.02

63+79.05 = E.C.

46' Rt TopCb	✓	202	13.80
46' Rt on Pav		215	13.17
30' Rt Edge Pav		232	13.50
10' Rt		213	13.69
1/2		21	13.4

15.82

Dec 30-32  
12

10' Lt Edge Pav		232	13.50
30' Lt		248	13.34
46' Lt		212	12.6
46' Lt TopCb	✓	228	13.54
		64+0	
46' Lt TopCb	✓	248	13.34
46' Lt		213	12.5
30' Lt Edge Pav		273	13.09
10' Lt		257	13.25
1/2		26	13.2
10' Rt Edge Pav		241	13.41
30' Rt		253	13.29
46' Rt on Pav		287	12.95
46' Rt TopCb	✓	225	13.57

64+50

46' Rt TopCb	✓	215	13.17
46' Rt Pav		337	12.45
30' Rt		303	12.79
10' Rt Edge Pav		291	12.91
1/2		32	12.6

15.82

10' Lt Edge Pav	3.09	12.73
30' Lt " "	3.24	12.58
46' Lt	3.9	11.9
46' Lt Top Cb	✓ 3.05	12.77

64+81

46' Lt Top Cb	✓ 3.38	12.44
46' Lt	4.3	11.5
30' Lt Edge Pav	3.59	12.25
10' Lt Edge Pav	3.42	12.40
✓ 1/2	3.6	12.2
10' Rt Edge Pav	3.23	12.59
30' Rt " "	3.33	12.49
46' Rt Top Pav	3.66	12.16
46' Rt Top Cb	✓ 3.98	12.84

65+0

46' Rt Top Cb	✓ 3.17	12.65
46' Rt	3.9	11.9
30' Rt Edge Pav	3.52	12.30
10' Rt Edge Pav	3.45	12.37
✓ 1/2	3.9	11.9

15.82

10' Lt Edge Pav	3.66	12.16
30' Lt " "	3.82	12.00
46' Lt	4.5	11.3
46' Lt Top Cb	✓ 3.59	12.23

65+50

46' Lt Top Cb	✓ 4.08	11.74
46' Lt	5.1	10.7
30' Lt Edge Pav	4.32	11.50
10' Lt " "	4.16	11.66
✓ 1/2	4.8	11.0
10' Rt Edge Pav	3.96	11.86
30' Rt " "	4.06	11.76
46' Rt	4.5	11.3
46' Rt Top Cb	✓ 3.62	12.20

66+0

46' Rt Top Cb	✓ 4.06	11.76
46' Rt	5.0	10.8
30' Rt Edge Pav	4.50	11.32
10' Rt " "	4.42	11.40
✓ 1/2	5.1	10.7

B3

15.82

10 Lt Edge Pav	4.69	11.13
30 Lt	4.82	11.00
46 Lt	5.8	10.0
46 Lt TopCb	4.69	11.13

66+50

46 Lt TopCb	5.80	10.62
46 Lt	6.3	9.6
30 Lt Edge Pav	5.42	10.40
10 Lt	5.23	10.59
5	5.7	10.1
10 Rt Edge Pav	4.94	10.88
30 Rt	5.00	10.82
46 Rt	5.9	10.1
46 Rt TopCb	4.54	11.28

67+0

46 Rt TopCb	4.82	11.00
46 Rt	5.8	10.0
30 Rt Edge Pav	5.31	10.51
10 Rt	5.18	10.64
5	5.9	9.9

15.82

14

10 Lt Edge Pav	5.47	10.35
30 Lt	5.69	10.13
46 Lt	6.5	9.3
46 Lt TopCb	5.46	10.36

67+50

46 Lt TopCb	5.70	10.72
46 Lt	6.8	9.0
30 Lt Edge Pav	5.94	9.88
10 Lt	5.73	10.09
5	6.0	9.8
10 Rt Edge Pav	5.48	10.34
30 Rt	5.51	10.31
46 Rt	5.9	9.9
46 Rt TopCb	5.09	10.73

68+0

46 Rt TopCb	5.34	10.48
46 Rt	6.3	9.5
30 Rt Edge Pav	5.79	10.03
10 Rt	5.69	10.13
5	6.2	9.5



15.82

10 Lt	Edge Pwr	5.93	9.89
30 Lt	" "	6.16	9.68
46 Lt	" "	6.9	8.9
46 Lt	Top Cb ✓	5.92	9.90

68+50

46 Lt	Top Cb ✓	6.16	9.66
46 Lt	" "	7.1	8.7
30 Lt	Edge Pwr	6.40	9.42
10 Lt	" "	6.17	9.65
✓ 1/2	" "	6.5	9.3
10 Rt	Edge Pwr	5.94	9.88
30 Rt	" "	6.03	9.79
46 Rt	" "	6.5	9.3
46 Rt	Top Cb ✓	5.61	10.21

69+0

46 Rt	Top Cb ✓	5.80	10.02
46 Rt	" "	6.8	9.0
30 Rt	Edge Pwr	6.24	9.58
10 Rt	" "	6.16	9.66
1/2	" "	6.7	9.1

15.82

15

10 Lt	Edge Pwr	6.38	9.44
30 Lt	" "	6.54	9.28
46 Lt	" "	7.3	8.5
46 Lt	Top Cb ✓	6.42	9.39

69+50 = N End 2 Strip Black Paint

46 Lt	Top Cb ✓	6.66	9.16
46 Lt	" "	7.3	8.5
30 Lt	02 Edge Pwr	6.85	8.97
20 Lt	02 " "	6.71	9.11
10 Lt	02 Edge " "	6.60	9.22
✓ 1/2	" "	7.0	8.8
10 Rt	" " "	6.42	9.40
20 Rt	02 " "	6.45	9.37
30 Rt	" " "	6.55	9.27
46 Rt	" "	6.9	8.9
46 Rt	Top Cb ✓	6.08	9.74
TP	2.22 12.00	6.04	9.78
	70+0		
46 Rt	Top Cb ✓	7.53	9.47
46 Rt	" "	3.3	8.7

12.00

30 Pt		3.5	8.5
30 Pt		3.6	8.4
✓ 1/2		3.6	8.4
30 Lt		3.8	8.2
30 Lt		3.9	8.1
46 Lt		3.9	8.1
46 Lt - Top Ch	✓	3.01	8.99

70+50

46 Lt - Top Ch	✓	3.18	8.82
46 Lt		4.0	8.0
30 Lt		4.3	7.7
20 Lt		4.1	7.9
✓ 1/2		3.8	8.2
30 Pt		3.9	8.1
30 Pt		3.9	8.1
46 Pt		3.8	8.2
46 Pt - Top Ch	✓	3.75	9.25

71+0

46 Pt - Top Ch	✓	3.90	9.10
46 Pt		3.6	8.4

12.00

16

30 Pt		4.0	8.0
30 Pt		4.2	7.8
✓ 1/2		4.0	8.0
30 Lt		4.3	7.7
30 Lt		4.3	7.7
46 Lt		4.3	7.7
46 Lt - Top Ch	✓	3.27	8.73

71+50

46 Lt		3.45	8.55
46 Lt - Top Ch	✓	4.4	7.6
30 Lt		4.5	7.5
30 Lt		4.4	7.6
✓ 1/2		4.1	7.9
30 Pt		4.2	7.8
30 Pt		4.2	7.8
46 Pt		4.0	8.0
46 Pt - Top Ch	✓	3.05	8.95

72+0

46 Pt - Top Ch	✓	3.23	7.77
46 Pt		4.2	7.8

12.00

30 Pt	44	7.6
30 Pt	44	7.6
✓ 2	43	7.7
30 Lt	46	7.4
30 Lt	47	7.3
46 Lt	46	7.4
46 Lt - TopCb	✓ 3.65	8.85

72+50

46 Lt - TopCb	✓ 3.25	8.25
46 Lt	48	7.2
30 Lt	46	7.4
30 Lt	47	7.3
2	43	7.8
30 Pt	45	7.5
30 Pt	47	7.3
46 Pt	43	7.7
46 Pt - TopCb	✓ 3.42	8.58

73+0

46 Pt - TopCb	✓ 3.47	8.53
46 Pt	44	7.6

12.00

30 Pt	48	7.2	17
30 Pt	49	7.3	
✓ 2	47	7.3	
30 Lt	48	7.2	73+31=
30 Lt	50	7.0	M.H. 11/15/54
46 Lt	48	7.2	2.81
46 Lt - TopCb	✓ 3.88	8.12	

73+50

46 Lt - TopCb	✓ 4.00	8.0
46 Lt	49	7.1
30 Lt	49	7.1
30 Lt	49	7.1
✓ 2	46	7.4
30 Pt	47	7.3
30 Pt	48	7.2
46 Pt	45	7.5
46 Pt - TopCb	✓ 3.62	8.38

74+0

46 Pt - TopCb	✓ 3.78	8.22
46 Pt	46	7.4

1200

30 Rt		49	7.1
20 Rt		50	7.0
✓ 1/2		50	7.0
20 Lt		51	6.9
30 Lt		49	7.1
46 Lt		51	6.9
46 Lt-TopCb	✓	419	7.83

74+50

46 Lt-TopCb	✓	422	7.78
46 Lt		51	6.9
30 Lt		52	6.8
20 Lt		51	6.9
✓ 1/2		50	7.0
20 Rt		48	7.2
30 Rt		48	7.2
46 Rt		47	7.3
46 Rt-TopCb	✓	384	6.16

75+096 = opp Cb in hole Rt + Lt

46 Rt-TopCb	✓	380	8.20
46 Rt on Grating		482	7.18

1200

18

30 Rt		49	7.1
20 Rt		49	7.1
✓ 1/2		48	7.2
30 Lt		51	6.9
30 Lt		52	6.8
46 Lt on Grating		522	6.78
46 Lt-TopCb	✓	421	7.79

75+50

46 Lt-TopCb	✓	400	8.00
46 Lt		52	6.8
30 Lt		51	6.9
20 Lt		49	7.1
✓ 1/2		48	7.2
20 Rt		46	7.4
30 Rt		50	7.0
46 Rt		46	7.4
46 Rt-TopCb	✓	372	8.28

96+0

46 Rt-TopCb	✓	256	8.44
46 Rt		45	7.5

120°

30 Pt		46	7.4
20 Pt		48	7.2
✓ 2		46	7.4
20 Lt		42	7.3
30 Lt		50	7.0
46 Lt		49	7.1
46 Lt TopCb	✓	381	8.16
	76+50		
46 Lt TopCb	✓	374	8.26
46 Lt		49	7.1
30 Lt		47	7.3
20 Lt		46	7.4
✓ 2		44	7.6
20 Pt		46	7.4
30 Pt		45	7.5
46 Pt		43	7.7
46 Pt TopCb	✓	337	8.63
	77+0		
46 Pt TopCb	✓	325	8.15
46 Pt		42	7.8

120°

19

30 Pt		45	7.5
20 Pt		44	7.6
✓ 2		44	7.6
20 Lt		45	7.5
30 Lt		46	7.4
46 Lt		48	7.2
46 Lt TopCb	✓	357	8.43
TP	3.21	11.66	3.55
	77+50		8.25
46 Lt TopCb	✓	314	8.52
46 Lt		43	7.4
30 Lt		42	7.5
20 Lt		40	7.7
✓ 2		39	7.8
20 Pt		39	7.8
30 Pt		39	7.8
46 Pt		34	8.3
46 Pt TopCb	✓	274	8.92
	77+99-400 Sh. Sassafras		
46 Pt TopCb	✓	252	9.14

11.66

46 Pt	3.6	8.1
30 Pt	3.6	8.1
20 Pt	3.7	8.0
✓ 1/2	3.8	7.9
30 Lt	3.9	7.8
30 Lt	4.2	7.5
46 Lt	4.1	7.6
46 Lt - TopCb ✓	3.00	8.66
78 + 39 = 2 Sarrafra		
46 Lt - TopCb ✓	3.02	8.64
46 Lt	4.2	7.5
30 Lt	4.2	7.5
20 Lt	4.2	7.5
✓ 1/2	3.7	8.0
20 Pt	3.8	7.9
30 Pt	3.6	8.1
46 Pt	3.2	8.5
78 + 79 = 4 Sarrafra		
46 Pt - TopCb ✓	2.55	9.11
46 Pt	3.3	8.4

11.66

2R

30 Pt	3.9	7.8
20 Pt	4.1	7.6
✓ 1/2	4.1	7.6
30 Lt	4.2	7.5
30 Lt	4.2	7.5
46 Lt	4.3	7.4
46 Lt - TopCb ✓	3.02	8.64
79 + 0		
46 Lt - TopCb ✓	3.09	8.57
46 Lt	4.4	7.3
30 Lt	4.3	7.4
20 Lt	4.2	7.5
✓ 1/2	4.3	7.4
20 Pt	4.1	7.6
30 Pt	3.9	7.8
46 Pt	3.9	8.8
46 Pt - TopCb ✓	2.66	9.00
79 + 50		
46 Pt - TopCb ✓	2.81	8.82
46 Pt	3.3	8.4

11.66

30 Pt	40	7.7
30 Pt	40	7.7
✓ $\frac{1}{2}$	41	7.6
20 Lt	40	7.7
30 Lt	42	7.4
40 Lt	45	7.2
46 Lt - Top Cb ✓	324	8.42
80+0		
46 Lt - Top Cb ✓	337	8.27
46 Lt	45	7.2
30 Lt	45	7.2
20 Lt	41	7.3
✓ $\frac{1}{2}$	42	7.5
20 Pt	41	7.6
30 Pt	41	7.6
46 Pt	35	8.2
46 Pt - Top Cb ✓	303	8.63
80+50		
46 Pt - Top Cb ✓	310	8.56
46 Pt	39	7.8

11.66

30 Pt	43	7.4	21
20 Pt	41	7.3	
✓ $\frac{1}{2}$	43	7.4	
20 Lt	46	7.1	
30 Lt	44	7.3	
46 Lt	48	6.9	
46 Lt - Top Cb ✓	354	8.12	
81+0			
46 Lt - Top Cb ✓	370	7.96	
46 Lt	48	6.9	81+05 =
30 Lt	47	7.0	41 Lt - 100
20 Lt	47	7.0	150
✓ $\frac{1}{2}$	45	7.2	7.1
20 Pt	45	7.2	
30 Pt	46	7.1	
46 Pt	38	7.9	
46 Pt - Top Cb ✓	326	8.40	
81+50			
46 Pt - Top Cb ✓	330	8.28	
46 Pt	39	7.8	

1166

30 Pt	4.3	7.4
20 Pt	4.4	7.3
✓ 1/2	4.6	7.1
20 Lt	4.8	6.9
30 Lt	4.9	6.8
46 Lt	4.9	6.8
46 Lt - TopCb ✓	3.81	7.85

8270

46 Lt - TopCb ✓	3.87	7.79
46 Lt	4.9	6.8
30 Lt	4.9	6.8
20 Lt	4.9	6.8
✓ 1/2	4.6	7.1
20 Pt	4.5	7.2
30 Pt	4.4	7.3
46 Pt	4.2	7.5
46 Pt - TopCb ✓	3.51	8.15

82750

46 Pt TopCb ✓	3.50	8.16
46 Pt	4.3	7.4

1166

22

30 Pt	4.4	7.3
20 Pt	4.5	7.2
✓ 1/2	4.5	7.2
20 Lt	4.8	6.9
30 Lt	5.0	6.7
46 Lt	4.8	6.9
46 Lt - TopCb ✓	3.87	7.79

82772 = Opp Cb / 46 Lt Pt Lt

46 Lt - TopCb ✓	3.86	7.80
46 Lt Grat top	4.89	6.77
38 Lt MH on Rim	4.16	7.50
30 Lt	5.0	6.7
20 Lt	4.8	6.9
✓ 1/2	4.4	7.3
20 Pt	4.5	7.2
30 Pt	4.5	7.2
46 Pt on Grat top	4.49	7.17
46 = TopCb ✓	3.47	8.19

82708.95 = Cb Pt Lt

46 Pt	3.34	8.32
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11.66

11' Pt		4.3	7.4
30' Pt		4.3	7.4
30' Pt		4.4	7.3
✓ 8		4.3	7.4
30' Lt		4.1	7.1
30' Lt		4.8	6.9
46' Lt		4.7	7.0
46' Lt TopCb	✓	3.66	8.00
TP	592	13.91	3.67
		7.99	

83+17.61 = 100.61

46' Lt. TopCb	✓	5.87	8.04
46' Lt		7.0	6.9
30' Lt		7.0	6.9
30' Lt		6.8	7.1
✓ 8		6.5	7.4
30' Pt		6.6	7.3
30' Pt		6.6	7.3
46' Pt		6.5	7.4
46' Pt - TopCb	✓	5.53	8.38

1291

83+50

46' Pt. TopCb	✓	5.47	8.44
46' Pt		6.3	7.6
30' Pt		6.5	7.4
30' Pt		6.7	7.2
✓ 8		6.5	7.4
30' Lt		6.7	7.2
30' Lt		7.1	6.8
46' Lt		7.1	6.8
46' Lt. TopCb	✓	5.76	8.15
		8.41	0
46' Lt. TopCb	✓	5.67	8.24
46' Lt		7.0	6.9
30' Lt		7.0	6.9
✓ 8		6.8	7.1
✓ 8		6.3	7.6
30' Pt		6.4	7.5
30' Pt		6.3	7.6
46' Pt		6.3	7.7
46' Pt - TopCb	✓	5.31	8.57

12-21-32  
23

13.91

84+50

46 R <sup>1</sup> TopCb	✓	519	8.72
46 R <sup>1</sup>		63	7.6
30 R <sup>1</sup>		62	7.7
30 R <sup>1</sup>		64	7.5
✓ 2		64	7.5
20 Lt		66	7.3
30 Lt		68	7.1
46 Lt		68	7.1
46 Lt TopCb	✓	548	8.43

85+0

46 Lt TopCb	✓	527	8.64
46 Lt		64	7.5
30 Lt		66	7.3
20 Lt		64	7.5
✓ 2		61	7.8
20 R <sup>1</sup>		62	7.7
30 R <sup>1</sup>		62	7.7
46 R <sup>1</sup>		60	7.9
46 R <sup>1</sup> TopCb	✓	502	8.89

13.91

85+50

224

46 R <sup>1</sup> TopCb	✓	486	9.05
46 R <sup>1</sup>		59	8.0
30 R <sup>1</sup>		60	7.9
30 R <sup>1</sup>		60	7.9
✓ 2		58	8.1
20 Lt		62	7.7
30 Lt		64	7.5
46 Lt		64	7.5
46 Lt TopCb	✓	513	8.78

86+00

46 Lt TopCb	✓	504	8.87
46 Lt		61	7.8
30 Lt		62	7.6
20 Lt		61	7.8
✓ 2		58	8.1
20 R <sup>1</sup>		59	8.0
30 R <sup>1</sup>		58	8.1
46 R <sup>1</sup>		57	8.2
46 R <sup>1</sup> TopCb	✓	472	9.18

1391

86+50

46' Pt TopCb ✓	466	9.25
46' Pt	56	8.5
30' Pt	58	8.1
20' Pt	59	8.0
✓ 2	56	8.5
20' Lt	59	8.0
20' Lt	22	7.7
46' Lt	61	7.8
46' Lt TopCb ✓	486	9.05

87+00

46' Lt TopCb ✓	471	9.20
46' Lt	60	7.9
30' Lt	60	7.9
20' Lt	59	8.0
✓ 2	56	8.5
20' Pt	57	8.2
30' Pt	56	8.5
46' Pt	56	8.3
46' Pt TopCb ✓	446	9.45

1391

87+50

46' Pt TopCb ✓	430	9.61
46' Pt	54	8.5
30' Pt	54	8.5
20' Pt	55	8.4
✓ 2	55	8.4
20' Lt	57	8.2
30' Lt	60	7.9
46' Lt	58	8.1
46' Lt TopCb ✓	458	9.33

88+00

46' Lt TopCb ✓	446	9.45
46' Lt	57	8.2
30' Lt	57	8.2
20' Lt	55	8.4
✓ 2	52	8.6
20' Pt	52	8.7
30' Pt	52	8.7
46' Pt	51	8.8
46' Pt TopCb ✓	413	9.78

25

13.91

88+50

46' Pt. Top C3 ✓	397	9.94
46' Pt	52	8.7
30' Pt	53	8.6
20' Pt	53	8.6
✓ 2	52	8.7
20' Lt	54	8.5
30' Lt	57	8.2
46' Lt	55	8.4
46' Lt = Top C6 ✓	121	9.69

88+63 = At End of Lt. C6 Pt. of Pt.

46' Lt = Top C6 ✓	123	9.68
46' Pt. " "	398	9.93

89+0

46' Pt	51	8.8
30' Pt	50	8.9
30' Pt	50	8.9
✓ 2	49	9.0
30' Lt	53	8.6
30' Lt	55	8.4

13.91

226

26' Lt

55

8.4

89+50

46' Lt	53	8.6
30' Lt	51	8.8
30' Lt	49	9.0
✓ 2	47	9.2
20' Pt	48	9.1
30' Pt	49	9.0
46' Pt	51	8.8

90+0

46' Pt	51	8.8
30' Pt	49	9.0
30' Pt	49	9.0
✓ 2	48	9.1
20' Lt	49	9.0
30' Lt	52	8.7
46' Lt	55	8.4

90+50

46' Lt	56	8.3
30' Lt	55	8.4

1422 p 39  
44  
47  
60

1450 p 40  
871

2229 p 58

1791 p 1  
p 27  
p 70  
p 99

1049 p 48

871 p 50

1050 p 44

64.58	44.07
<u>15</u>	<u>7</u>
49.58	37.07

3832, 3613

1391

20 Lt	54	8.5
✓ 20 Lt	49	9.0
30 Pt	52	8.6
30 Pt	53	8.6
46 Pt	53	8.6
91+0		
46 Pt	52	8.6
30 Pt	51	8.8
30 Pt	50	8.9
✓ 20 Lt	50	8.9
20 Lt	54	8.5
30 Lt	54	8.5
46 Lt	58	8.1
91+50		
46 Lt	57	8.2
30 Lt	55	8.4
30 Lt	54	8.5
✓ 20 Lt	51	8.8
20 Pt	52	8.6
30 Pt	52	8.6

1391

277

46 Lt	55	8.4
92+0		
46 Pt	54	8.5
30 Pt	52	8.7
30 Pt	52	8.7
✓ 20 Lt	51	8.8
20 Lt	54	8.5
30 Lt	56	8.3
46 Lt	58	8.1
92+50		
46 Lt	59	8.0
30 Lt	57	8.2
30 Lt	55	8.4
✓ 20 Lt	54	8.5
20 Pt	55	8.4
30 Pt	56	8.3
46 Pt	59	8.0
93+0		
46 Pt	59	8.0
30 Pt	57	8.2

1391

20 Pt	5.8	8.1
✓ 2	5.6	8.3
20 Lt	5.9	8.0
30 Lt	6.0	7.9
40 Lt	6.2	7.7
93+50		
40 Lt	6.2	7.7
30 Lt	6.0	7.9
20 Lt	5.9	8.0
✓ 2	5.6	8.3
20 Pt	5.8	8.1
30 Pt	5.9	8.0
40 Pt	6.0	7.9
94+0		
40 Pt	6.2	7.6
30 Pt	6.1	7.8
20 Pt	6.0	7.9
✓ 2	5.9	8.2
30 Lt	6.0	7.9
30 Lt	6.2	7.7

1391

289

40 Lt	6.2	7.6	
TP 3.02	1197	496	895
94+50			
<u>11.97</u>			
40 Lt	4.7	7.3	
30 Lt	4.4	7.6	
30 Lt	4.2	7.8	
✓ 2	3.8	8.4	
30 Pt	4.2	7.8	
30 Pt	4.3	7.7	
40 Pt	4.4	7.6	
95+0			
40 Pt	4.5	7.5	
30 Pt	4.5	7.5	
30 Pt	4.5	7.5	
✓ 2	4.1	7.9	
30 Lt	4.5	7.5	
30 Lt	4.6	7.4	
40 Lt	5.0	7.0	
95+50			
40 Lt	5.1	6.9	



1197

30 Lt	49	7.1
20 Lt	47	7.3
✓ 5	44	7.6
30 Pt	45	7.5
30 Pt	44	7.6
46 Pt	43	6.7

96+0 = Prop Cutvert

46 Pt	44	7.6
30 Pt	44	7.6
20 Pt	45	7.5
✓ 5	49	7.7
30 Lt	46	7.4
30 Lt	47	7.3
46 Lt	51	6.9

96+50

46 Lt	49	7.1
30 Lt	48	7.2
20 Lt	46	7.4
✓ 5	43	7.8
30 Pt	42	7.8

1197

229

30 Pt	41	7.9
46 Pt	40	8.0

97+0

46 Pt	40	8.0
30 Pt	39	8.1
20 Pt	41	7.9
✓ 5	39	8.1
20 Lt	46	7.4
30 Lt	47	7.3
46 Lt	49	7.1

97+50

30 Lt	40	8.0
20 Lt	38	8.2
✓ 5	35	8.5
30 Pt	35	8.5
30 Pt	36	8.4

98+0

30 Pt	32	8.8
20 Pt	33	8.7
5	32	8.8

11.97

20 Lt 37 8.3

30 Lt 38 8.2

98+50

20 Lt 39 8.6

20 Lt 34 8.6

✓ 2 30 9.0

20 Pt 31 8.9

30 Pt 30 9.0

98+64.05 - C6 FC

30 Pt 29 9.1

20 Pt 31 8.9

✓ 2 29 9.1

20 Lt 32 8.8

30 Lt 33 8.7

98+73.59 - P21 FC

30 Lt 32 8.8

20 Lt 32 8.8

✓ 2 28 9.2

20 Pt 30 9.0

30 Pt 29 9.1

11.97

TP 5.30 1513 214 9.83

99+0

30 Pt 6.0 9.1

20 Pt 6.0 9.1

✓ 2 59 9.2

20 Lt 6.3 9.8

30 Lt 6.3 9.8

99+50

30 Lt 6.0 9.1

20 Lt 6.0 9.1

✓ 2 58 9.3

20 Pt 6.0 9.1

30 Pt 6.0 9.1

100+0

30 Pt 5.8 9.3

30 Pt 5.9 9.2

✓ 2 5.5 9.6

20 Lt 5.7 9.4

30 Lt 5.7 9.4

30

15.13

100+50

30 Lt	51	9.5
20 Lt	51	9.5
✓ 2	53	9.8
20 Pt	57	9.4
30 Pt	57	9.4

101+0

30 Pt	54	9.7
30 Pt	55	9.6
✓ 2	53	9.8
20 Lt	55	9.6
30 Lt	55	9.6

101+50

30 Lt	55	9.6
20 Lt	53	9.8
✓ 2	53	9.8
20 Pt	52	9.9
30 Pt	49	10.2

101+67.4 - 5 Ind 60 Pt

30.5 Pt - Top 65	159	10.54
------------------	-----	-------

15.13

102+0

30.5 Pt - Gutter in Driveway	497	10.16
20 Pt	51	10.0
✓ 2	51	10.0
20 Lt	54	9.7
30 Lt	54	9.7

102+50

30 Lt	51	9.5
20 Lt	51	9.5
✓ 2	52	9.9
20 Pt	51	10.0
30.5 Pt	49	10.2
30.5 Pt Top 65	128	10.85

103+0

30.5 Pt Top 65	412	11.01
30.5 Pt - Gut	50	10.1
20 Pt	51	10.0
✓ 2	52	9.9
20 Lt	55	9.6
30 Lt	55	9.6

31

15.13

10341743 - St. Haroldby

30.41 07 Pav 582 9.31

30.41 " " 540 9.73

30.41 " " 506 10.07

30.41 " " 463 10.50

30.591 " " 457 10.56

BM 509 10.01

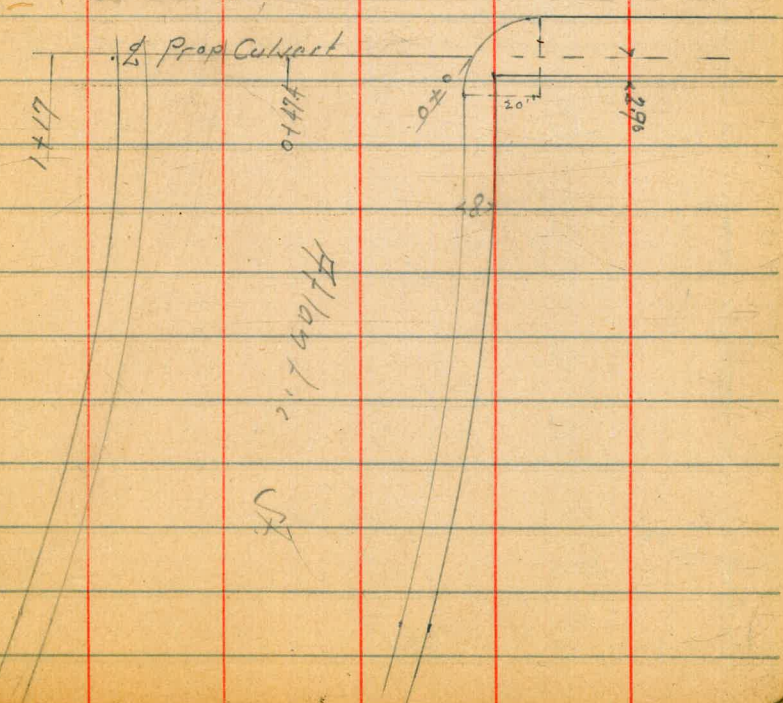
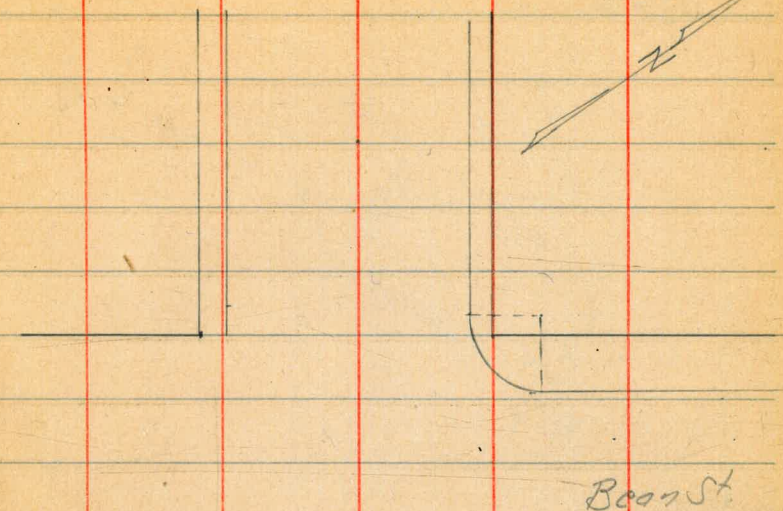
NE B.P.  
Haroldby  
Atlantic  
10.00

32

Proposed Culvert  
Atlantic & Bean St.

1-7-88 33  
Moore  
Sills  
Northboro

B.M.	224	1207	12.1	9.83	JP Pagoda
070			4.3	7.8	✓
+47.40	g Atlantic		4.7	7.4	✓
+90			5.3	6.8	✓
+93.4	W.C. Atlantic		4.7	7.1	✓
1+01.4	W.C. "		3.9	8.4	✓
+12			5.5	6.6	✓
+17			14.3	-2.2	✓



Cross Section N/4 28 of Rosecrans St. & S/4  
Cart Line of Pacific Hwy. Jefferson St to Gainant St.

Levels Next Page

INDEXED

C.S.R.

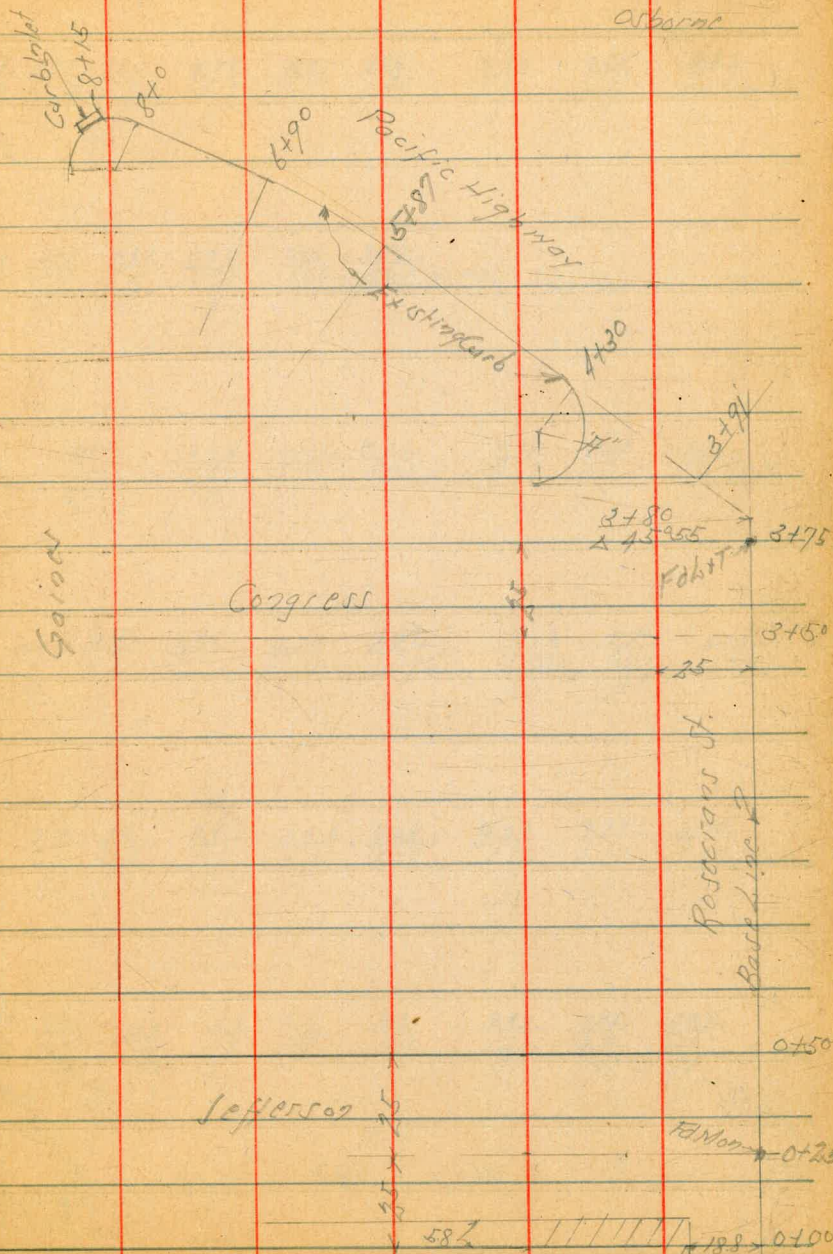
April 28-44

Sisson

Bliss

Arbore

34



Lt. W

R

Rt. E

1+0

409	392	380	388	405	416	420	425	5.03
497	509	526	518	501	490	488	481	4.03
25	21	16	11	5		4	15	25

0+93

16 Lt. Fly Tail Pojo

409	391	380	384	406	414			
497	515	516	522	500	492			
25	19	16	12	5				

0+75

405	366	401	411	419	425	5.06
501	540	505	495	487	481	4.00
25	15	5		4	15	25

0+50

11 L. Jefferson

40	37	345	322	399	412	470	5.05
51	54	561	534	507	494	436	4.01
25	18	13	5		5	15	25

0+25

39	38	35	366	404	426	429	5.06
57	53	56	540	502	480	427	4.00
25	20	7	5		5	15	25

0+0 = Sly Jefferson

438	431	41	33	37	42	443	485	509
468	475	50	58	54	49	465	421	397
25	18	15	8	5		5	15	25

25 = W. Reservoir

25 = L. Reservoir

9.06

TP

2.64

9.06

4.85

5.42

BM

5.65

10.27

4.62

S. E. P. & Curve  
San Diego  
Reservoir

L+

2

R1

36 36

2+50

<u>434</u>	<u>4.05</u>	<u>462</u>	<u>473</u>	<u>522</u>
472	5.01	489	483	579
25	19	5		15

742 16 W - Ely Power Tel Pol

2+25

<u>429</u>	<u>4.10</u>	<u>452</u>	<u>425</u>	<u>489</u>	<u>521</u>
477	4.96	454	431	477	585
25	19	5		5	15

2+10

<u>428</u>	<u>4.10</u>	<u>437</u>	<u>446</u>	<u>469</u>	<u>5.15</u>	<u>533</u>
478	4.96	469	460	437	3.91	573
25	18	5		5	15	25

1+80

<u>4.12</u>	<u>4.03</u>	<u>4.10</u>	<u>4.35</u>	<u>4.46</u>	<u>4.57</u>	<u>5.08</u>	<u>5.30</u>
4.84	5.03	4.96	4.71	4.60	4.49	3.98	3.76
25	18	13	5		5	15	25

1+50

<u>4.13</u>	<u>3.97</u>	<u>4.28</u>	<u>4.39</u>	<u>4.45</u>	<u>4.91</u>	<u>5.15</u>
4.93	5.09	4.78	4.67	4.61	4.15	3.91
25	17	5		4	15	25

1+25

<u>4.05</u>	<u>3.92</u>	<u>4.18</u>	<u>4.32</u>	<u>4.32</u>	<u>4.82</u>	<u>5.08</u>
5.01	5.14	4.88	4.74	4.74	4.64	3.98
25	15	5		5	15	25

9.06

9.06



275 = Congress

275 Lt P Rt  
 $\frac{391}{5.15}$   $\frac{394}{5.17}$   $\frac{388}{5.18}$   $\frac{389}{5.20}$   $\frac{425}{4.81}$   $\frac{429}{4.87}$   
75 50 25 21 5

264 = Gutter Line to West

$\frac{361}{5.15}$   $\frac{328}{5.31}$   $\frac{385}{5.21}$   $\frac{380}{5.24}$   $\frac{426}{4.80}$   $\frac{441}{4.65}$   
75 65 28 20 5

159 25 Lt = Fly Paper Pole

250 = SL Congress

$\frac{392}{5.09}$   $\frac{380}{5.26}$   $\frac{434}{4.72}$   $\frac{444}{4.62}$   $\frac{462}{4.39}$   
25 19 5 15

225

$\frac{405}{5.01}$   $\frac{381}{5.23}$   $\frac{423}{4.83}$   $\frac{448}{4.88}$   $\frac{450}{4.56}$   $\frac{488}{4.18}$   
25 20 12 5 15

270

$\frac{419}{4.87}$   $\frac{391}{5.15}$   $\frac{461}{4.46}$   $\frac{469}{4.37}$   $\frac{511}{3.95}$   
25 20 5 15

275

$\frac{426}{4.80}$   $\frac{401}{5.05}$   $\frac{477}{4.77}$   $\frac{480}{4.76}$   $\frac{524}{3.82}$   
25 20 5 15

8.34

LT

Δ

570

4.29 ~~5.45~~ ~~5.37~~ 3.59  
7.05  
2.08

4225

3.84 ~~4.56~~ ~~4.46~~ 3.79  
4.50  
10.100

4750

3.95 ~~4.67~~ ~~4.60~~ 3.88  
4.39  
10.100  
0.72  
8.34

IP 3.79 8.34 4.51 4.55

4730 C6 EC

~~4.62~~ ~~4.88~~ 3.89  
4.44  
4.06  
5.07  
5.91

17 7 Rcl

~~4.54~~ ~~4.84~~ 3.96  
4.52  
0.86  
5.10  
5.91

3791 Taken on line of Congress 5.43 5.11  
89 84

484.385 387 387 408 419  
177 521 519 519 498 487  
10.00 18 17 5

7750

2.92

2.28

5.12

6.06

6

gutter

6490 App C6 EC

3.27

2.62

5.07

5.92

6450

3.48

2.88

4.86

5.46

640

3.85

3.09

4.49

5.25

487 Approx C6 BC

3.91

3.17

4.43

5.17

5750

3.51

3.40

4.83-1.00

4.94 gutter

8.34

8.34

39  
37

831

8715 = Cobble lot at Gairnest

870

834

2.57

577

50

1.69

675

675 = Gairnest  
of 10/10/23

2.68

575

=cb

2.04

630

=4000

834

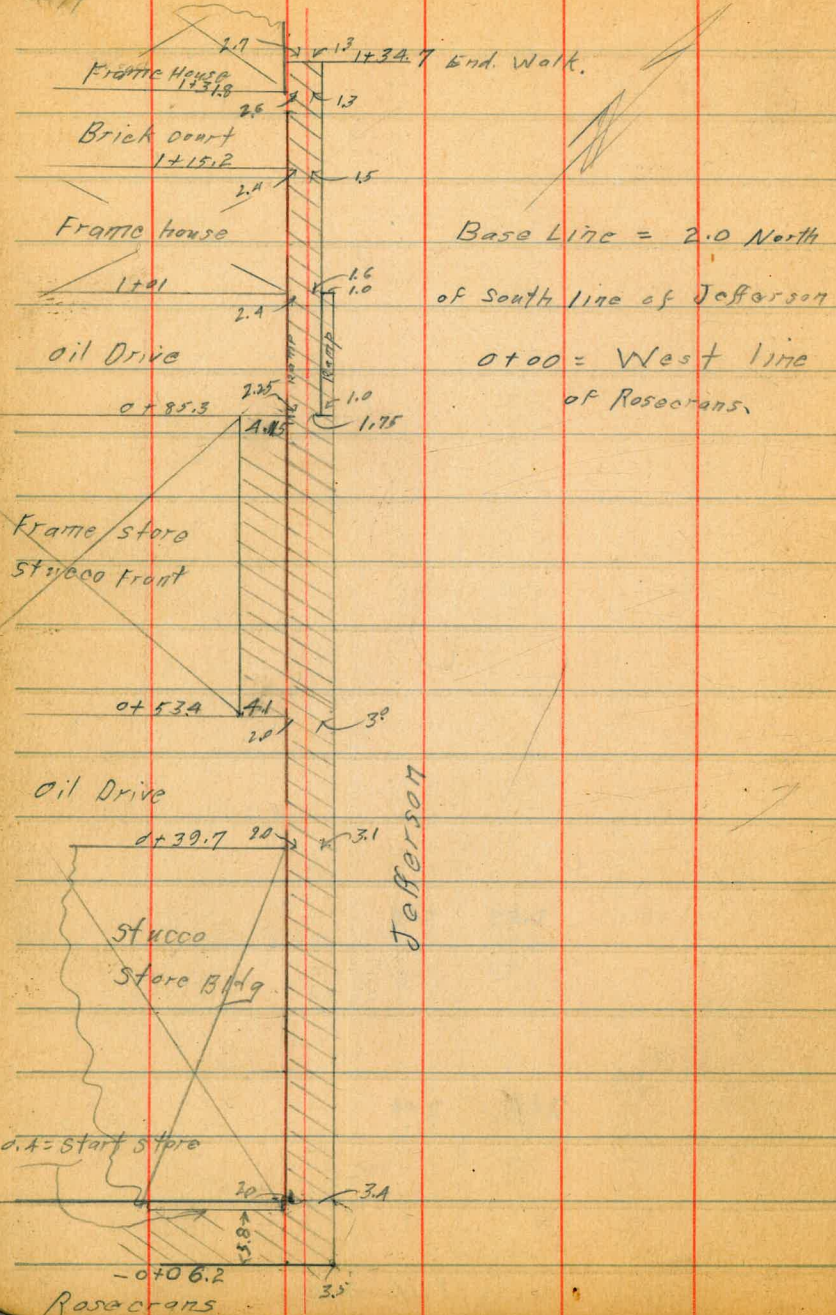
Sammermajor  
W. Moore  
B299

S.W. Cor. Jefferson & Rose crans - To West

indexed  
e.s.k

8-1-44

41



B.M. = B.P.  
90° 15' 14" from  
Rose crans.  
W. Side Road:

5.37	9.68	—	4.31
T.P.	4.92	10.52	4.08 5.60
	3.60		
T.P.	4.72	8.92	5.20 5.32
	4.72	8.98	4.66
			4.26 ✓ (Cor. walk)
	-0+06.3		
	3.5 RT		4.9 4.1
	2.0 LT		4.8 4.2
	-0+06.2 Edge Walk		
	3.5 RT		4.72 4.26
	3.6 RT Ground		4.9 4.1
	0+00		
	3.4 RT Walk		4.66 4.32
	3.5 RT		4.8 4.2
	2.1 T		4.67 4.31
	0+20		
	3.2 RT		4.61 4.37
	3.3 RT		5.0 4.0
	2.1 T		4.63 4.35

X-Sec. S.W. Cor. Jefferson & Rose crans,  
to West

42

0+39.7

8.98

1+00

8.98

3.1 RT Walk

4.62 4.36

1.6 LT

4.91 4.07

3.2 RT

4.9 4.1

2.4 LT

5.05 3.93

2.0 LT

4.64 4.34

1+01

0+53.4

1.6 RT <sup>top</sup> Ramp

4.94 4.04

3 RT Walk

4.68 4.36

2.6 RT <sup>Bottom</sup> Ramp

5.16 3.82

3.1 RT

4.8 4.2

2.7 RT

5.3 3.7

2 LT

4.42 4.56

1.6 LT

4.90 4.08

6.1 LT

4.18 4.70

2.4 LT

4.37 4.61

0+85.3

1+15<sup>2</sup>

2.75 RT Walk

4.83 4.15

1.5 RT <sup>Edge</sup> Walk

4.82 4.16

2.8 RT

5.1 3.9

1.6 RT

5.2 3.8

2.25 LT

4.53 4.45

2.4 LT

4.80 4.18

6.4 LT

4.26 4.72

1+31.8

0+86.3

1.3 RT

4.80 4.18

1.75 RT <sup>Top Ramp</sup>

4.98 4.20

1.4 RT

5.1 3.9

2.75 RT <sup>Bottom "</sup>

4.99 3.99

2.6 RT

4.73 4.25

1.6 LT <sup>Top Ramp</sup>

4.62 4.36

1+34.7

2.25 LT <sup>Bottom Ramp</sup>

4.71 4.27

over

S.W. Jefferson in. Reservoirs  
x-sec. to Wash

43  
43

1+34.7      x  
8.98

1.30+ End Walk      5.09      3.89

1.4 RT Ground      5.1      3.9

2.74+ End. walk      4.95      4.03

1+50

1.4 RT. Ground      4.9      4.1

2.74+ ✓      4.8      4.2

T.P.      5.97      10.72      4.23      4.75

T.P.      4.20      9.87      5.05      5.67

Starting B.M.

S.B. 431      5.54      4.33

4.31

ERROR      0.02

indexed  
c.s.s.

Survey of Knoxville ST.

(old Empire St.)

C Moore Marana Blvd. to Litchfield St.

Sommer Meyer  
W. Moore  
10-10-44.

Levels p 50

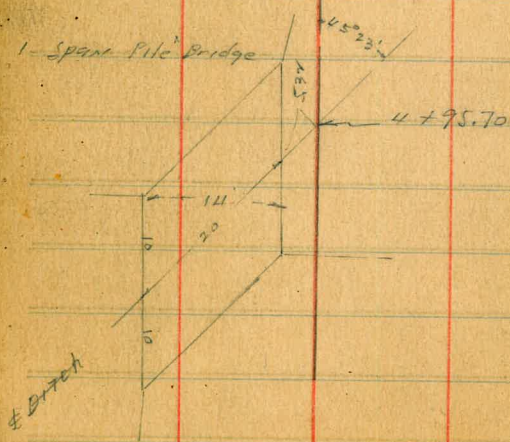
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FB. 871-31-50.

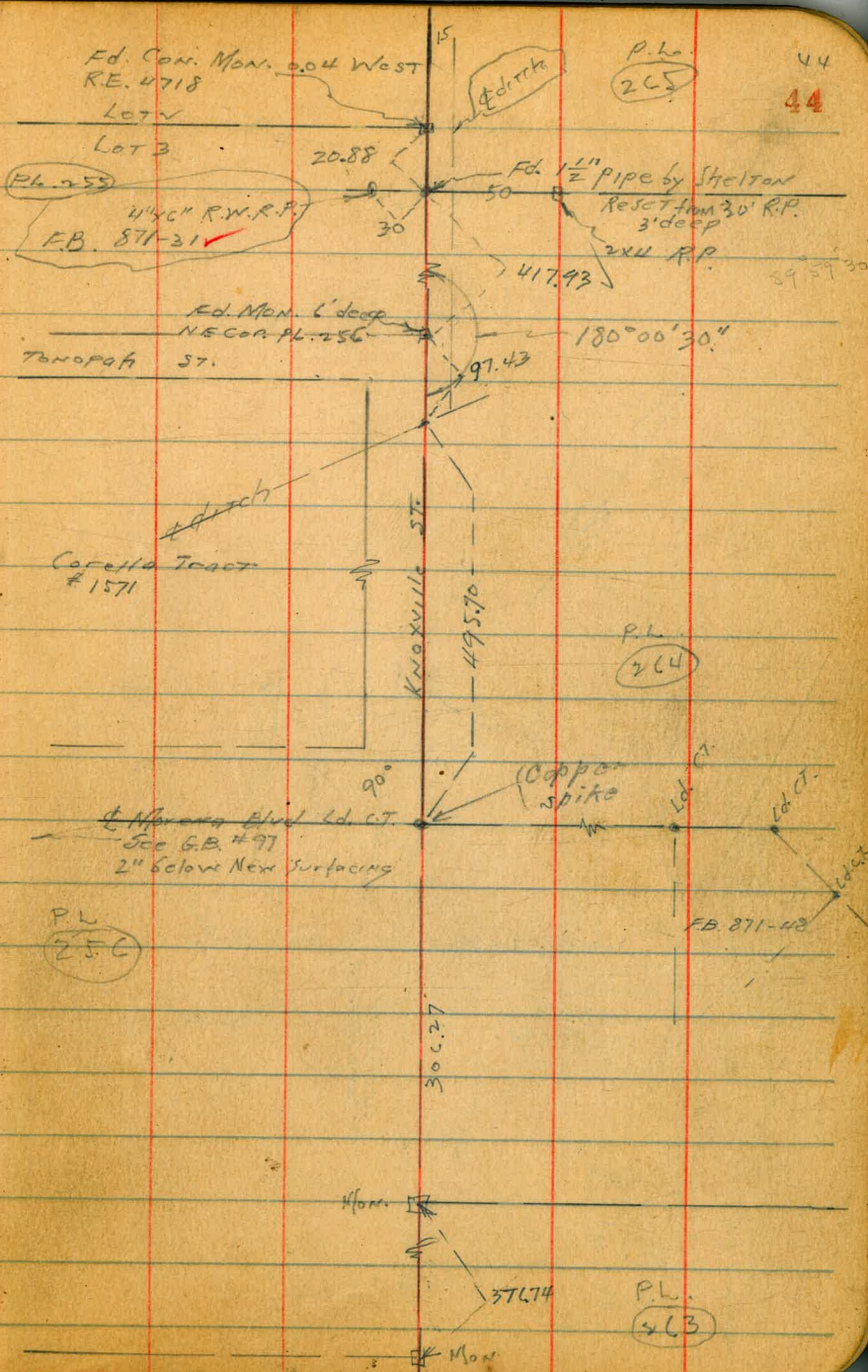
Puebla  
Line

Puebla  
Line

1-Span Pile Bridge



# Ditch



P.L.  
265

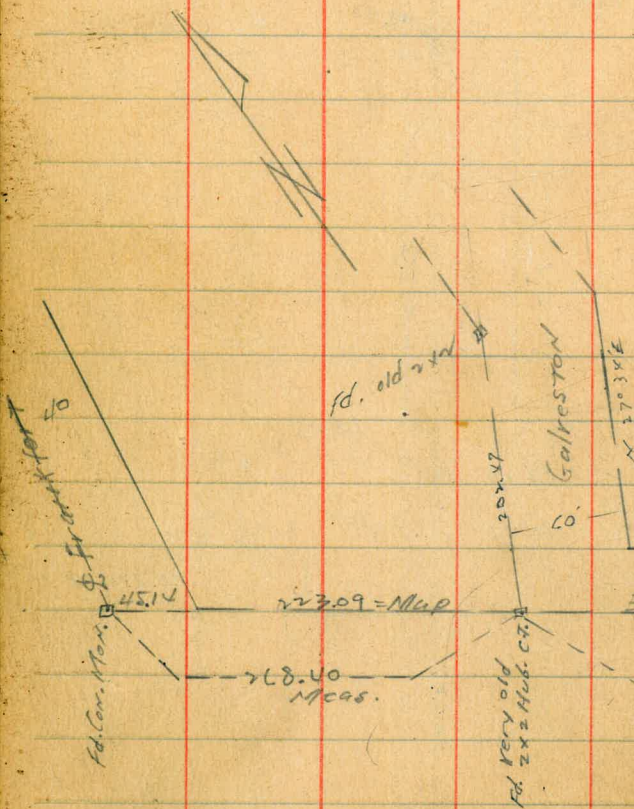
44  
44

P.L.  
264

P.L.  
25-C

P.L.  
263





22359  
 4514  
 768.73

EMPIRE ST.

- 574.90 Meas -  
 574.46 = Map

Berry St

Gardena St.

Knoxville St. 627.51

90° 06'

N 52° 50' W

Pd. broken off & under  
 Mail box post 2/18/48  
 Reset in correct  
 position 2/16/49  
 C.H.S.

see above  
 PL. 265

Set 2 in Hub 1' deep  
 on NE Cor. Cox. Mon.  
 Rd. Mon. RE. 4718 to be  
 0.77 WEST AND  
 0.31 South

439.05

Lot 2 Cox. Mon.  
 Lot 3 RE. 4718

> 20.88  
 50'

1 1/2" pipe

3 1/2" RP  
 1" mark

PL. 264



0+00 x wt, Rose crans

0-11 = Present Line of Valley gut.

0-20 cb line

0-35

0-50 2 Rose crans

Reduced 11-2-44

T.P. p. 41 4.01 8.30  
This Book

42C

Baseline =  
N14 Jefferson

R7

47

3.87	<del>4.03</del>	<del>4.02</del>	<del>4.14</del>
4.43	$\frac{4.25}{30}$	$\frac{4.28}{65}$	$\frac{4.16}{100}$
3.42	<del>3.70</del>	<del>3.81</del>	<del>3.92</del>
4.88	$\frac{4.60}{30}$	$\frac{4.49}{65}$	$\frac{4.38}{100}$
3.70	<del>3.95</del>	<del>4.08</del>	<del>4.21</del>
4.50	$\frac{4.35}{30}$	$\frac{4.22}{65}$	$\frac{4.09}{100}$
4.94	<del>4.19</del>	<del>4.53</del>	<del>4.66</del>
4.86	$\frac{3.81}{30}$	$\frac{3.77}{65}$	$\frac{3.66}{100}$
5.01	<del>5.00</del>	<del>5.02</del>	<del>5.11</del>
4.79	$\frac{3.30}{30}$	$\frac{3.08}{65}$	$\frac{3.19}{100}$

8.30 ✓

0 + 60 = Gr. Brk.

0 + 40 = Gr. Brk.

0 + 27.6 Front of Bldg.

0 + 25

0 + 20

0 + 10

Baseline

R7.

401	3.96	3.91		
429	$\frac{4.34}{3.5}$	$\frac{4.35}{7.7}$		
401	7.11	7.22		
429	$\frac{4.19}{3.5}$	$\frac{4.08}{7.7}$		
405	7.27	7.87	7.43	7.53
425	$\frac{4.03}{7.7}$	$\frac{3.93}{3.0}$	$\frac{3.87}{6.5}$	$\frac{3.77}{1.00}$
407	7.22	7.32	7.33	7.41
423	$\frac{4.08}{7.7}$	$\frac{3.98}{3.0}$	$\frac{3.97}{6.5}$	$\frac{3.89}{1.00}$
405	7.27	7.26	7.36	7.36
425	$\frac{4.06}{3.0}$	$\frac{4.04}{6.5}$	$\frac{3.96}{1.00}$	
404	7.17	7.15	7.25	
426	$\frac{4.13}{3.0}$	$\frac{4.15}{6.5}$	$\frac{4.05}{1.00}$	

8.30

8.30 ✓

← BASELINE

Rt.

1+28

4.03	3.79	3.80
4.27	$\frac{4.51}{3.3}$	$\frac{4.50}{7.7}$

1+00

4.01	3.86	3.90
4.29	$\frac{4.44}{3.5}$	$\frac{4.40}{7.7}$

0+80

4.06	3.91	4.06
4.24	$\frac{4.39}{3.5}$	$\frac{4.24}{7.7}$

0+61.5

3.97	3.91	3.91
4.33	$\frac{4.39}{3.5}$	$\frac{4.39}{7.7}$

8.30

8.30 ✓

Sketch P. 44.

Levels on Knoxville ST

C.S.M.  
1-19-45

✓ 100

1 + 50

1 + 00

0 + 50

0 + 00 & 20' Strip Pav. on Marana Blvd.

TP 4.67 14.07 4.35 9.40

B.M. B.P. Top  
in Let Hand  
Teeoffers  
Culv. 3.71 13.75 10.04

on Marana Blvd.

Reduced & Plotted 1/24-45  
C.P.H.

LT

Pueblo  
L.M.S.

RT

50

8.5	8.1	9.0	8.0	7.9
$\frac{5.6}{60}$	$\frac{5.4}{30}$	5.1	$\frac{6.1}{8}$	$\frac{6.7}{30}$

8.2	8.5	8.9	8.3	7.9
$\frac{5.9}{60}$	$\frac{5.6}{30}$	5.2	$\frac{5.8}{4}$	$\frac{6.2}{30}$

8.4	8.4	8.4	8.0	8.0
$\frac{5.7}{60}$	$\frac{5.7}{30}$	5.7	$\frac{6.1}{7}$	$\frac{6.1}{30}$

8.0	8.3	8.4	8.1
$\frac{6.1}{60}$	$\frac{5.8}{30}$	5.7	$\frac{6.0}{30}$

9.32	9.2	9.1	9.0
$\frac{4.75}{60}$	$\frac{4.9}{30}$	5.0	$\frac{5.1}{30}$

~~14.07~~

	9.7	5.7	5.6	10.6	10.9	12.8	13.0	10.6	9.8
4+50	<u>8.7</u>	<u>12.7</u>	<u>12.8</u>	<u>7.8</u>	<u>3.5</u>	<u>5.6</u>	<u>5.6</u>	<u>7.8</u>	<u>8.6</u>
	73	67	37	35	30 23	18		6	30

T.P. 7.11 18.41 2.77 11.30

	5.8	10.1	10.6	13.9	9.6	9.8	10.6	9.7	9.7
4+20	<u>8.3</u>	<u>4.0</u>	<u>3.5</u>	<u>0.4</u>	<u>4.5</u>	<u>4.3</u>	<u>3.5</u>	<u>4.4</u>	<u>4.4</u>
	65	60	55	47	38	30		8	30

	5.6	9.9	14.1	9.1	9.4	9.9	9.4	9.3
4+00	<u>8.5</u>	<u>4.2</u>	<u>0.0</u>	<u>5.0</u>	<u>4.7</u>	<u>4.2</u>	<u>4.7</u>	<u>4.8</u>
	79	72	60	52	30		8	30

dash

TOP  
dyke

	8.9	9.0	9.6	8.7	8.6
3+50	<u>5.2</u>	<u>5.1</u>	<u>4.5</u>	<u>5.4</u>	<u>5.5</u>
	60	30		7	30

	8.9	8.9	9.3	8.4	8.4
3+00	<u>5.2</u>	<u>5.2</u>	<u>4.8</u>	<u>5.7</u>	<u>5.7</u>
	60	30		8	30

	8.6	8.6	9.1	8.1	8.1
2+50	<u>5.6</u>	<u>5.5</u>	<u>5.0</u>	<u>6.0</u>	<u>6.0</u>
	60	30		10	30

Stoo

9.8	9.8	12.1	<del>14.1</del>	14.8	5.9	5.8	12.9	15.1	12.4	10.8
8.6	8.6	4.0		3.6	12.5	12.6	5.5	3.3	6.0	8.1
60	34	30	20	4		20	25	30	37	50

10.2  
8.2  
60

10.7  
7.7  
24

13.9  
4.5  
40

13.2  
13.6

14.4  
14.4

6.1  
6.1

14.8  
14.8

5.8  
5.8

14.6  
14.6

deck  
bridge

4489

10.2

8.2  
60

10.8	14.0	13.5	12.1	6.1	5.8	5.8	14.2	14.2	11.8	10.4
7.6	4.4	4.9		12.3	12.6	12.6	4.2	4.2	6.6	8.0
47	40	32	30	21		14	22	27	30	36

4488

4487

5.6  
12.8

5.6  
12

14.4  
17

13.1  
22

11.1  
30

4481

10.2

8.2  
60

14.4	13.5	9.9	5.6	14.4	14.1	11.2
4.0	4.9		12.8	4.0	4.3	7.2
45	36	30	23		19	30

4465

9.7

8.7  
60

9.7	5.6	5.9	6.0	14.4	14.3	11.1	9.9
8.7	12.8		12.4	4.0	4.1	7.3	8.5
57	49	30	22	18		8	30

1841

1841



7+00

C+50

7.10 18.00 7.51 10.90

5+93/3 Pueblo Line to West

5+50

5+20

5+10

18.41

L7

PL

PT

52

11.3	12.2	11.9	10.7	13.0	10.2	6.6	6.7	10.0	10.6	14.3	11.9
6.7	5.8	7.3	5.0	7.8	11.4	11.3	8.0	7.4	3.7	6.6	
60	35	30	13	8	5	21	23	30	35	40	

11.0	11.8	11.2	11.4	11.6	11.3	6.3	6.4	11.6	15.3	11.0
7.0	6.2	5.8	6.4	6.7	11.7	11.6	6.4	2.7	7.0	
60	41	40	30		5	21	29	30	42	

30 18.41

10.9	11.3	11.6	11.6	10.8	11.3	10.8	10.6	6.6	6.7	11.4	11.3
8.1	7.1	6.8	7.5	7.1	7.6	7.8	11.8	11.7	4.0	7.1	
60	4	30	27	4	5	7	23	30	35	42	

10.1	10.9	11.1	11.8	11.8	6.5	6.2	11.1	15.9	10.9
8.3	7.3	6.6	11.7	12.2	2.5	7.5			
60	30	22	2	8	23	30	38	47	

9.5	10.5	10.6	12.9	13.4	6.1	6.1	10.1	14.0	11.4
8.9	7.8	5.5	5.0	12.3	12.3	4.4	7.0		
60	30	28	22	8	25	30	35	45	

9.4	10.2	10.2	14.0	14.1	13.6	1.0	5.8	5.9	12.7	14.3	10.6
9.0	8.2	4.4	4.3	4.8	11.4	12.6	12.5	4.7	4.1	7.0	
60	30	27	22	3	5	9	23	30	36	50	

18.41

12.8  
 5.2  
 70  
 11.0  
 70  
 11.0  
 7.0  
 48

9x100

13.0  
 5.0  
 60

7x80

7x50

7x25

8

7x50

1800

L7

PL

R7

53

13.4 10.7 9.1 10.3 13.6 13.0 12.6 8.2 8.4 16.0 12.5  
 4.0 8.3 7.7 4.4 5.0 5.4 9.8 9.0 2.0 5.5  
 38 30 27 13 5 5 7 23 32 39

11.5 10.1 9.1 10.0 13.1 14.0 13.0 7.7 8.6 15.8 12.2  
 6.5 8.3 8.0 4.3 4.0 5.0 10.3 9.4 2.2 5.8  
 37 30 28 15 3 3 22 28 36

12.3 12.1 9.6 9.9 12.0 11.9 7.7 8.0 16.0 12.3  
 5.7 5.3 8.4 5.1 5.0 6.1 10.3 10.0 2.0 5.7  
 60 30 24 14 11 1 22 30 36

12.1 12.3 9.6 12.4 12.0 12.0 7.4 7.4 15.6 11.9  
 5.9 5.7 8.4 5.0 6.0 6.0 10.0 10.0 2.4 6.1  
 60 30 23 15 10 5 6 22 30 37

11.6 11.9 12.0 10.6 12.9 11.6 ~~8.5~~ 7.6 15.4 11.9  
 6.4 6.0 7.4 5.1 6.4 10.5 10.4 2.4 6.1  
 60 30 20 14 10 4 22 28 35

11.9 11.8 11.7 12.0 9.6 9.4 7.3 7.2 11.9 15.2 11.6  
 6.1 6.3 5.0 8.4 8.0 10.7 10.8 6.1 2.8 6.4  
 60 30 18 10 4 7 20 21 28 35

1800

L.P. PL. P.T.

54

150

14.2	15.2	15.4	12.8	13.6	14.1	12.0	9.7	9.7	14.7
7.6	6.6	6.4	9.0	8.4	7.7	9.8	12.1	12.1	7.1
6.4	6.1	30 26	13		15	22	26	41	45

11+00

13.3	14.6	14.7	14.8	12.3	12.7	14.0	15.8	15.1	12.1	9.6	9.8	15.6	13.4
8.5	7.2	7.0	9.5	9.1	7.8	6.0	6.7	9.7	12.3	12.0	6.2	8.4	
7.0	8.7	6.0	5.0	4.3	3.0	2.3		5	9	15	7	10	4.5

10+80

13.1	14.2	14.6	13.7	12.2	12.1	13.3	14.1	16.6	17.3	12.5	9.7	9.7	15.8	13.8
8.7	7.6	7.3	7.5	7.7	8.5	7.7	5.3	4.5	9.3	12.1	12.1	6.0	8.0	
9.3	9.1	6.4	6.0	5.4	3.6	2.3	1.0	4	4.5	5	12	28	37	4.2

10+50

12.8	14.0	14.1	11.8	11.8	11.8	12.5	12.8	13.7	14.6	13.2	9.6	9.6	15.7	13.7
9.0	7.8	7.7	10.0	10.0	9.3	8.1	4.4	8.6	12.2	12.2	6.1	8.1		
10.4	10.0	8.0	9.6	6.0	4.8	3.4	3.0	1.7	8	8.6	6	2.4	3.2	3.8

T.P.

5.01. 21.75 12.6 15.74

21.75

10

14.1	13.6	11.6	11.0	11.0	12.3	12.5	12.7	12.9	13.0	11.9	12.0	14.0	14.0	13.0	9.4	9.4	13.3	12.5
3.9	4.4	6.4	7.0	7.0	5.7	5.5	5.3	5.0	6.1	6.0	4.0	4.0	5.0	8.6	8.6	4.7	5.5	
11.7	10.9	10.1	9.1	8.5	7.5	6.0	4.0	3.0	2.4	1.5	1.0	3	4.0	3	6	2.3	2.5	1.0

9+50

The ditch on Rt. 15 Present Channel.

13.3	13.3	10.9	11.0	10.9	14.3	14.5	14.5	11.4	10.0	13.0	12.0	9.6	9.6	15.0	12.7
4.7	4.7	7.1	7.0	7.1	3.5	6.6	8.0	5.0	6.0	8.5	8.4	3.0	5.3		
11.7	10.4	8.5	6.0	4.0	3.5	3.0	2.9	2.3	4	6	8	2.5	3.2	3.8	

E.L. of Present Rd.

18.00

18.00

+20

L+	P.	R
16.7 7.1 60	16.6 6.7 30 25	16.1 7.2 22
16.5 6.8 3	17.3 6.0	16.5 6.8 13
		16.7 6.6 30

T.P. 5.58 2326 4.07 17.68

14

L+	P.	R
16.1 5.7 60	16.4 5.3 30 25	16.5 6.0 22
15.8 6.0 3	16.7 5.6 3	17.4 4.4
		16.6 5.7 5
		16.6 5.7 30

+50

15.7 6.1 60	16.0 5.8 30 25	15.3 5.5 22
16.0 5.8 3	17.1 4.7	16.5 5.3 7
		16.4 5.4 30

13

15.4 6.4 60	15.1 6.1 35	15.0 6.8 30
15.4 6.4 3	16.7 5.1	15.9 5.9 30

+50

15.6 6.4 60	15.5 6.3 50	14.7 7.1 47	14.8 7.0 30 20	15.1 6.1 18	16.3 5.5 10	14.8 7.0 3	16.0 5.8	14.4 7.4 30
-------------------	-------------------	-------------------	----------------------	-------------------	-------------------	------------------	-------------	-------------------

12+00

14.5 7.3 66	14.0 7.4 60	14.6 7.4 38	15.4 6.4 35	15.4 6.4 30	15.8 6.4 8	13.4 8.4	13.3 8.5 15	13.2 8.6 37
W.L.Rd.				E.L.Rd.		W. edge Channel		

2175

2175

Lr

Pl.

Rr

+50

17.8	17.8	16.9	17.1	17.6	17.6
5.5	5.5	6.4	6.2	5.7	5.7
30	25	22	3		30

+10

17.8	17.1	16.9	16.9	17.3	17.3
5.5	5.6	6.4	6.4	6.0	6.0
30	24	22	30		30

15

16.9	16.9	17.5	17.4
6.4	6.4	5.8	5.9
30	3		30

14 + 70.99 S.L. EMPIRE ST

16.8	16.9	16.9	17.1
6.5	6.4	6.4	6.2
60	30		30

*change to 60 ft.*

+55

16.6	16.9	16.9	16.9	17.1	17.1
6.7	6.4	7.0	6.2	6.2	6.2
60	30	20	27		30

14 + 30

16.7	16.8	16.8	16.8
6.6		6.5	6.5
60	30		30

23.26

23.26

167  $\frac{1}{2}$  3' <sup>con</sup> walk

150

126  $\frac{1}{2}$  2.8' <sup>con</sup> walk

17

150

16400

2326

Lr

P.L.

Pr

57

1871 L

$\frac{4.55}{23.8}$

186

$\frac{4.7}{30}$

187

5.1

183

$\frac{5.0}{30}$

1816 V

$\frac{5.0}{30}$

187

$\frac{5.1}{30}$

181

5.2

182

$\frac{5.1}{30}$

183

50

30

180

53

24

177

5.6

22

176

5.7

3

181

5.2

183

5.2

30

179

54

30

181

5.2

24

173

6.0

22

175

5.8

3

178

5.5

181

5.2

30

2326

L+

P.L.

R+

+50

19.6	19.6	18.9	19.1	19.2	19.0
<u>3.7</u>	<u>3.7</u>	<u>4.4</u>	<u>4.2</u>	<u>4.1</u>	<u>4.3</u>
30	28	26	8		30

19

19.2	19.2	18.7	18.8	19.0	19.1
<u>4.1</u>	<u>4.1</u>	<u>4.0</u>	<u>4.5</u>	<u>4.3</u>	<u>4.2</u>
30	26	24	6		30

+50

18.9	19.0	18.5	18.6	19.0	19.2
<u>4.4</u>	<u>4.3</u>	<u>4.8</u>	<u>4.7</u>	<u>4.3</u>	<u>4.1</u>
30	25	23	6		30

+21

E 3' <sup>Comp</sup> walk

18.66 ✓
<u>4.60</u>
24.5

9.21

18+09

E 10' <sup>Comp</sup> drive

18.66 ✓
<u>4.60</u>
28.5

17+92

E 9' <sup>Comp</sup> drive

18.52 ✓	18.7	18.6	18.5
<u>4.74</u>	<u>4.6</u>	<u>4.7</u>	<u>4.8</u>
30.2	30	20	

23.26

23.26

check to orig. BM.      4.26    10.01    10.04    1  
 T.P.      4.35    14.27    7.07    11.92  
 T.R.      1.31    18.99    5.58    17.68

✓✓

40.198.5 SL Garden St on diag.

$\frac{21.3}{2.0}$	$\frac{21.1}{2.2}$	$\frac{20.1}{3.2}$	$\frac{20.5}{7.8}$	$\frac{20.2}{3.1}$
30	15	5		30

+ 50

$\frac{20.2}{3.1}$	$\frac{19.8}{3.5}$	$\frac{19.4}{3.9}$	$\frac{19.5}{3.5}$	$\frac{19.7}{3.6}$
30	28	11		30

40 to 0

$\frac{19.7}{3.6}$	$\frac{19.0}{4.3}$	$\frac{19.3}{4.0}$	$\frac{19.8}{3.5}$	$\frac{19.7}{3.6}$
30	28	10		30

23.26

23.26



Indexed  
C.S.K.

# Survey for Prop. Connections to 18" Trunk Sewer on Gardena Ave.

#957

4-4-47

- Osborne  
Hardin  
Smith  
Worrell

W.O. 279

30  
Center  
Way

Ext. 18" V.P. Sewer

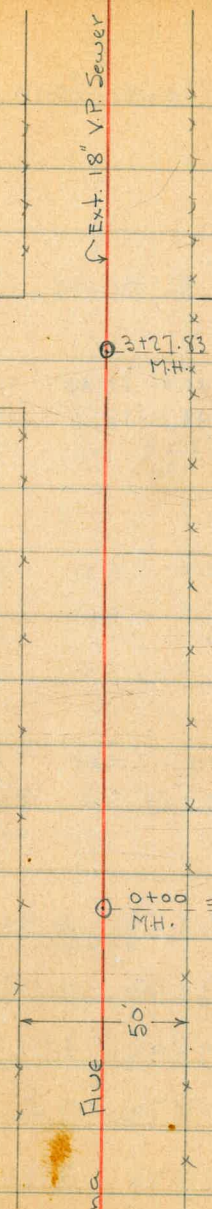
3+27.93 = 57+28.60  
M.H.

0+00 = 60+56.18 - Draw. # RS 339-3  
M.H.

50'

Gardena Ave

59



Levels on Prop. Sewer Conn. - Gardena Ave.

Lt. = N.

ϕ = ϕ 18" Sewer

Rt. = S. 19 1-

0+43 - 56.7 Rt. = ϕ House

22.87  
5.72  
56.7  
floor

0+00 = ϕ Ext. Sewer

23.6	22.7	23.08	15.72	22.6	22.8
5.0	5.9	5.51	12.87	6.0	5.8
25	10	Rim	FL. 18" U.P.	10	25

0+50

23.3	22.1	22.3	22.3	22.3
8.3	6.5	6.3	6.3	6.3
25	10		10	25

0-100 - for profile of st.

22.5	21.7	21.9	21.9	22.0
6.1	6.9	6.7	6.7	6.6
25	10		10	25

6.67 28.59 6.40 21.92

28.59

4.50 28.32 0.10 23.82

6.96 23.92 1.76 16.96

6.44 18.72 3.46 12.28

6.91 15.74 3.31 8.75

R.P. in Roadwall  
Tealote Creek  
+ Morena Blvd.

B.M. 2.02 12.06 10.04

2+01 - 17.2 Rt. = P. pole

2+00

Lt.		Rt.	
24.5	23.8	24.0	23.5
4.1	4.8	4.6	5.1
25	10	10	25

1+81 - Prop. Lat. to Rt.

23.9	23.5	24.0	22.8
4.7	5.1	4.6	5.8
	10	25	75

1+63 - Prop. Lat. to Lt.

24.5	24.6	23.6	23.7
4.1	4.3	5.0	4.9
75	25	10	

1+50

24.6	23.4	23.6	23.3	23.7
4.2	5.2	5.0	5.3	4.9
25	10		10	25

0+97 = Lat. to Lt.

24.3	24.2	23.2	23.3	23.0	23.3
4.3	4.4	5.4	5.3	5.6	5.3
50	25	10		10	25

0+97

0+79 = Line of prop. Lat. to Rt.

23.2	23.0	23.2	22.5
5.4	5.6	5.4	6.1
	10	25	75

0+50

24.2	22.9	23.1	22.7	23.0
4.4	5.7	5.8	5.9	5.6
25	10	-	10	25

28.59

2+01- 17.2 Rt. #P4681

Set B.M. = Spike in Pole 4.00 24.59

4+00 = end.

3+77- 73.5 Lt. = Conc. found. for Prop. House

3+59- 51' Rt. = House

3+50

3+27.83 = Ext. Sewer M.H. = Center Way

2+83 = Prop lat. on Lt.

2+50 = 63' Rt. = House

2+26 = Prop. lat. on Lt.

2+25- 153 Lt. = House

Lt.

R

Rt.

26.0	25.0	25.2	25.0	25.0
2.6	3.6	3.4	3.6	3.6
25	10		10	25

27.18

141

73.5

Top  
found.

25.5	24.7	25.1	24.6	24.9
3.1	3.9	3.5	4.0	3.7
25	10		10	25

26.18

241

51'

floor

27.2	26.3	25.5	24.8	25.31	17.94	24.6
1.4	2.3	3.1	3.8	3.28	10.65	4.0
125	75	25	10	Rim	FL. 18" V.P.	10

24.9	25.5	24.5	24.6	24.2	24.6
3.7	3.1	4.1	4.0	4.4	4.0
75	25	10		10	25

25.1	24.1	24.4	23.9	24.3	24.67
3.5	4.5	4.2	4.7	4.3	3.92
25	10		10	25	63 floor House

24.5	25.0	24.0	24.2
4.1	3.6	4.6	4.4

28.0  
0.60

153

floor.

28.59

Continuic Levels along Prop. Sewer - Tecolote  
Canyon - from Book 2133 - P. 79

39+00

38+50

38+00

37+50

37+00

36+50

36+00

35+50

35+00

Lt.

±

Rt.

64

9.2  
20  
25.0

9.2  
25.0

1.7  
15  
32.5

8.2  
26.0

9.0  
20  
25.2

8.9  
25.3

2.8  
15  
31.4

5.0  
25  
29.2

4.4  
40  
29.8

old Dirt Reservoir

6.3  
27.9

8.3  
30  
25.9

6.4  
27.8

0.0  
30  
34.2

7.6  
26.6

9.7  
30  
24.5

8.8  
25.4

8.5  
20  
25.7

0.4  
45  
33.8

9.1  
25.1

24.2

10.0

34.21 ✓

9.4  
25  
24.8  
TOP

0.5  
40  
33.7

43+00

42+50

42+00

41+53 - 7.5' Lt. =  $\Phi$  Tel. pole # J.P.C. 4791

41+52 - 9.7' Lt. =  $\Phi$  Pole # C-4797

41+50

41+46.5 = Cross wire fence - Beg. planted field

41+00

40+60

40+30

T.R. 10.37 36.26 8.32 25.89

40+00

39+70 = Beg. Trash Dump

39+50

Lt  $\Phi$  Rt

65

<sup>28.0</sup>  
8.3 7.8 6.1 <sup>28.2</sup>  
15 15

7.8 <sup>28.5</sup>

<sup>27.6</sup>  
8.7 7.2 4.6 <sup>31.7</sup>  
30 30  
edge field

<sup>24.2</sup> 12.1 <sup>27.8</sup> 8.5 6.8 <sup>24.5</sup> 4.0 <sup>30.3</sup>  
40 35 = Bank of Ditch 40

10.4 <sup>25.9</sup> 13.1 <sup>23.2</sup> 13.2 <sup>23.1</sup> 10.3 <sup>26.0</sup> 10.1 <sup>26.4</sup>  
40 15 25 50

13.9 <sup>22.4</sup>

<sup>22.5</sup> 13.8 <sup>22.5</sup> 13.8 10.5 <sup>25.8</sup> 10.7 <sup>25.6</sup>  
25 10 40  
36.26 ✓

<sup>23.0</sup> 11.2 <sup>22.6</sup> 11.6 <sup>25.7</sup> 8.5 8.2 <sup>26.0</sup>  
35 10 30 = Tbc

8.9 <sup>25.3</sup>  
34.21 ✓

Lt.

T

Rt.

66

check Hub elev.

5.26

31.00

3596 =

22133: P. 31

46+69.76 = end = Hub. = 48+79.83 on P Line

46+00

45+50

45+00

44+50

44+00

43+50

5.26  
on Hub.  
31.005.7  
30.66.0  
29.36.3  
30.06.5  
29.87.2  
29.17.6  
28.7

36.26 ✓

BB

Notes Reduced. 2-28-51

Levels along E of "B" Line - New line  
 Beg. at 77+61.05 on "P" Line - end at 96+00  
 on "P" line = Eq. - Sketch - B.2133 - P. 7  
 W.O. 20790 3-20-51 - 70.

81+00 - 115 Lt. - ± Creek

80+93 - 21' Lt. - ± 24" Cottonwood.

80+50

80+00

79+78 - 6 Lt. - ± 12" Oak

79+50 - 35' Lt. - ± Creek

79+04 - Cross wire fence

79+00

78+50

78+00

B.M. 7.62 62.57 ✓

5495 Hub. 77+ 61.05

Lt.

±

±

67

47.7  
 14.9  
 115  
 ± Creek

7.5<sup>55.1</sup>

8.1<sup>54.5</sup>

7.2<sup>55.4</sup>

46.8  
 15.8  
 35  
 ± Creek

4.8<sup>57.8</sup>

5.9<sup>56.7</sup>

6.5<sup>56.0</sup>

7.0<sup>55.6</sup>

62.57 ✓



85+80 = ± Wash - To E.

85+70

85+60

84+50

84+00

83+50

T.P. 6.33 68.06 0.84 61.73

83+00 - 155' H. = ± Creek

82+50

82+00

81+50

Lt.

82<sup>59.9</sup>

Rt.

68

8.5<sup>62.5</sup>

4.6<sup>63.5</sup>

4.6<sup>63.5</sup>

4.3<sup>63.8</sup>

5.1<sup>63.0</sup>

68.06 ✓

48.3  
14.3  
155  
± Creek

4.6<sup>60.0</sup>  
95

0.4<sup>60.7</sup>

1.9<sup>60.7</sup>

2.9<sup>59.7</sup>

5.0<sup>57.6</sup>

62.57 ✓

88+98 - 11 Lt. -  $\phi$  18" Euc.

88+93 - 23.5' Lt. =  $\pm$  72" - A trunk Euc. Tree

88+50

88+00

87+50

87+17 = Bank

87+08 =  $\pm$  Wash

87+00

86+60

86+27.10 = 86+38.83 on P Line = Ang. Pt.

86+00

Lt.

$\phi$

Rt.

69

2.2 <sup>6.9</sup>

6.0 <sup>6.1</sup>

6.9 <sup>6.2</sup>

7.6 <sup>6.5</sup>

9.8 <sup>6.3</sup>

7.9 <sup>6.2</sup>

7.0 <sup>6.1</sup>

5.22 <sup>6.84</sup>  
on Hub.

5.3 <sup>6.8</sup>

68.06 ✓

93+00 - 150 Lt. = ± Creek

92+50

92+00

91+90 - 8' Rt. = ± 10" Pepper

91+84 - 6' Rt. = ± 8" Pepper

91+50

91+00

90+50

T.P. 6.84 73.36 1.54 66.52

90+00 - 110 Lt. = ± Creek

89+50

89+05 - 14.5 Rt. = ± 36" Euc.

89+00

	Lt.	±	Rt.
	57.6	9.3	4.3
	15.8	110	69'
± Creek			

57.8

7.0

7.0

6.9

6.9

73.36

	Lt.	±	Rt.
	54.6	6.2	1.8
	13.5	90	66.3
± Creek	110		

1.7

1.4  
68.06

Lt.

±

Rt.

11

By 95+00  
check T.P. - B.2133 - R40 1.03 72.33 72.31 = P.40

95+15.25 = 96+00 on "P" Line = end.

94+50

3.69  
on Hub. <sup>69.57</sup>

94+00

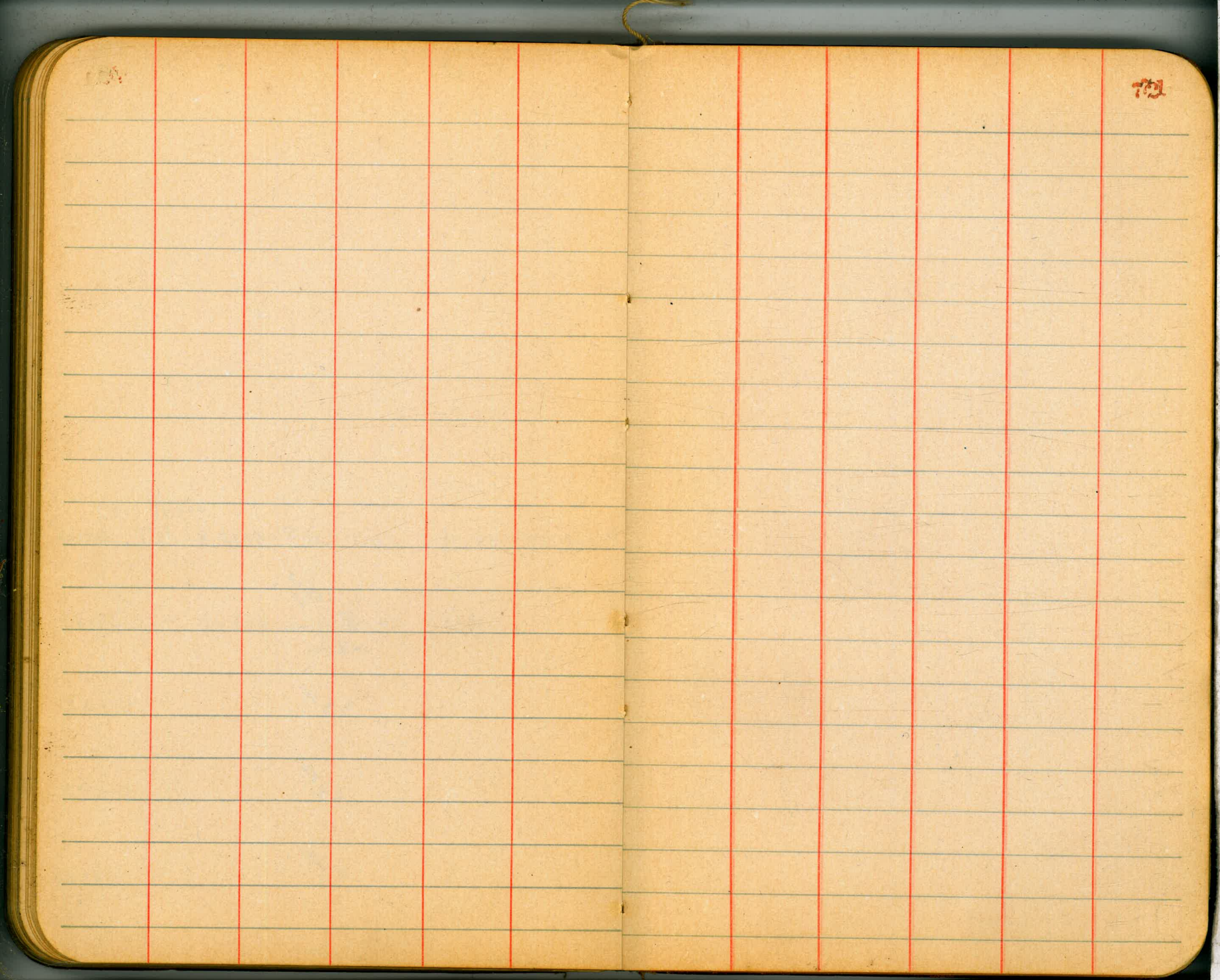
3.3700

93+50

3.4700

4.1693

73.36 ✓



70

71

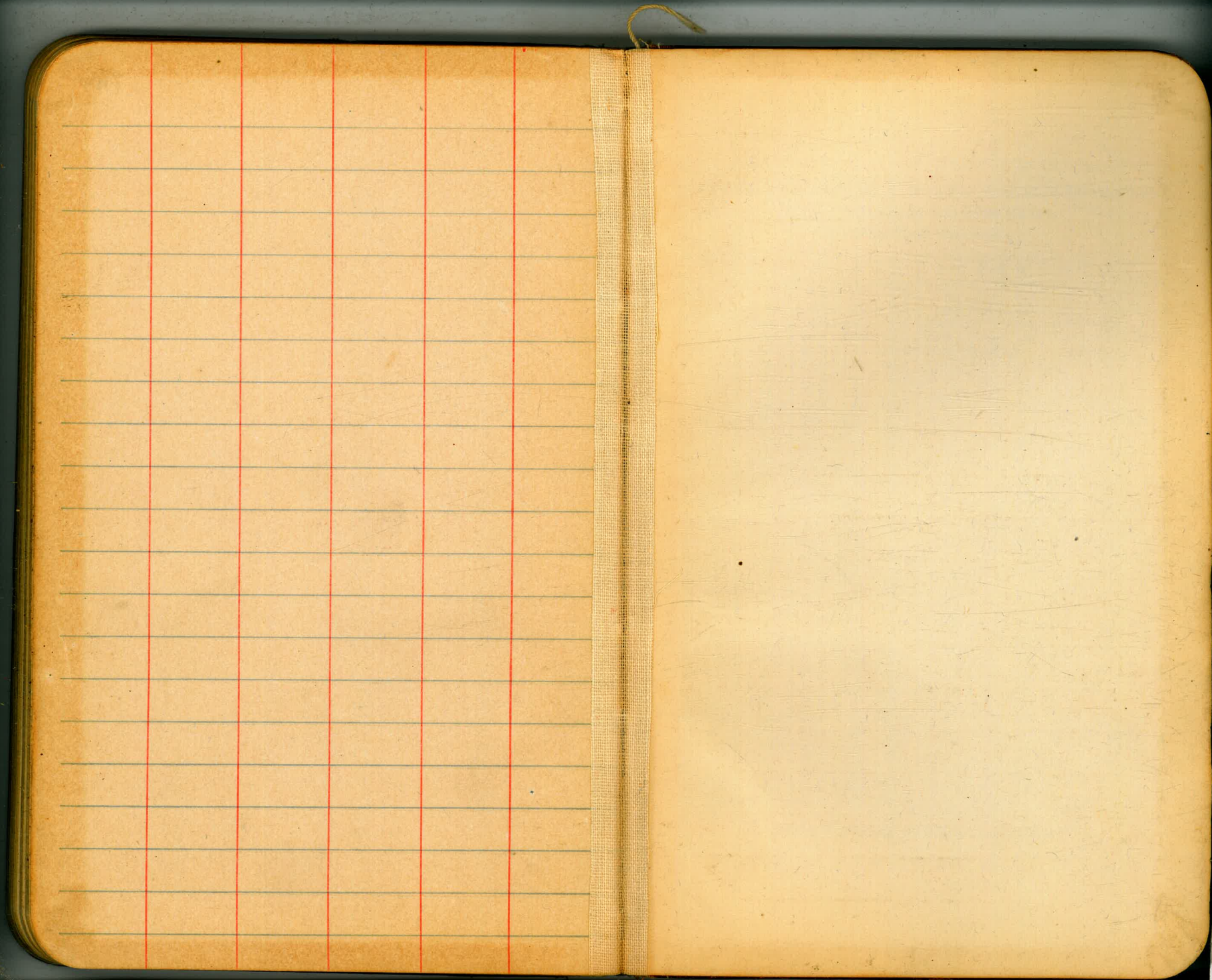












593.13  
 417.93  
 -----  
 10.11.06

77+61.05 - 54.95  
 79+58.64 - 63.98  
 86+38.85 - 63.83  
 92+57.30 - 74.36

22 E 20+15.35  
 55  
 20+70



DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

528.3  
 71.2  
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 626.5