

1451

LEVEL BOOK

373 A

# KEUFFEL & ESSER CO.

## DRAWING MATERIALS

AND

## SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

### Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

" Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

*Capt. Deland  
Marine Rifle Range*

ENGINEERING DEPARTMENT  
CITY OF SAN DIEGO,  
CALIFORNIA.

INDEXED  
M.R.  
JAN 23 1950  
*Completely*

ENGINEERING DEPARTMENT,  
CITY OF SAN DIEGO,  
CALIFORNIA.

Survey Lease PL 1311 79-80  
Miramor Rd  
101 Highway Junction

Cross Section Sassafras  
1615 From South to Horton

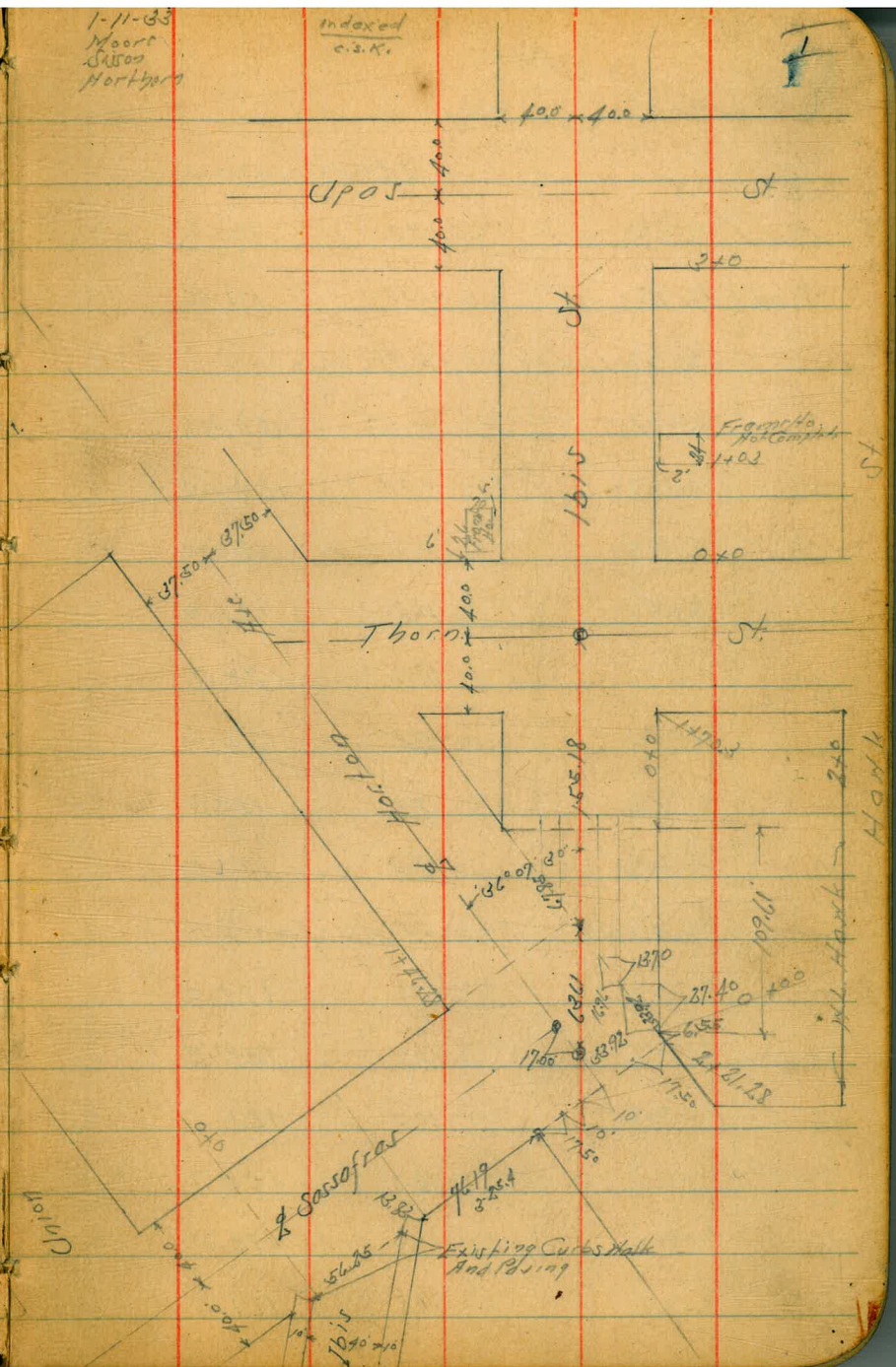
80' Hdr  
20' Cb  
10' Qls

1-11-63  
Moore  
Sassafras  
Horton

Indexed  
c.s.K.

F

BM	12.95	98.95	86.00	SE 8 P Spruce
TP	11.515	110.37	0.095	98.855
TP	11.23	120.13	1.47	108.90
BM		0.39	119.74	SW CT Sassafras
TP	12.91	132.98	0.06	120.07
210' approach of 1615 From South				
S Topch		12.93		120.05
S Gutter cap		13.60		119.38
Cb		12.4		120.6
H		11.8		121.2
g		11.1		121.9
H		10.5		122.5
Cb		8.6		124.4
H		1.5		131.5
0+28.13 = appz 1615 From South				
H		9.9		123.1
Cb		12.0		120.0
H		12.7		120.3
H		13.4		120.4



Sarrofras

132.98

132.98

2

			S	10.5	122.5
1/4	124	120.6		0+95.48	
Cb	124	120.6	S	9.8	123.2
S on Edge Parrot	1133	121.66	Cb	10.3	122.7
	0+56.25 = opp FC 1615		1/4	10.8	122.2
S on Parrot	10.02	122.96	S	11.8	121.2
S Top Cb	994	124.04	1/4	12.2	120.8
Cb	110	122.0	Cb	12.1	120.9
1/4	11.2	121.8	H	12.1	120.9
1/2	12.3	120.7		1+20.88	
1/4	124	120.6	H	11.6	121.4
Cb	123	120.7	Cb	11.1	121.9
H	125	120.5	1/4	8.6	124.4
	0+70.08 = opp FL 1615 From South		1/2	6.6	126.4
H	120	121.0	1/4	7.2	125.8
Cb	122	120.8	Cb	7.2	125.8
1/4	125	121.5	S	3.0	130.0
1/2	12.3	120.7		1+16.28 = H.L. Horton	
1/4	12.3	120.7	S	+5.1	138.1
Cb	11.8	121.2	Cb	+3.1	136.1

128.98

152.32

3

					1/4	11.4	144.9
1/4		+15	134.5		1/2	14.0	142.3
1/2		0.4	132.6		1/4	17.3	139.0
1/4		4.0	129.0		cb	20.4	135.9
cb		37	129.3		N	25.1	131.2
N		9.3	123.7				
	1+12.78 = N cb Horton						
					N	24.1	132.2
N		2.4	130.6		cb	16.7	139.6
cb		1.4	131.6		1/4	13.4	142.9
TP	12.65	144.74	0.89	132.09	1/2	11.2	145.1
1/4		8.2	136.5		1/4	8.0	148.3
1/2		5.0	139.7		cb	5.4	150.9
1/4		2.8	141.9		S	1.8	154.5
cb		1.6	143.1		TP	12.90	168.90
S		0.4	144.3				
						1+93.78 = 1/4	
TP	12.14	156.32	0.56	144.80	S	9.8	158.9
BM		11.8	145.14	on N Non Sassafras + Horton	cb	13.3	155.5
	1+73.78 = 1/4				1/4	15.9	152.8
S		5.9	151.4		1/2	19.0	149.7
cb		10.3	146.0		1/4	22.2	146.5

Sassafras

16870

cb	26.6	142.1
H	31.6	137.1
2+0378-Cb		
H	26.9	141.8
Cb	23.1	145.6
1/4	19.1	149.6
g	16.0	152.7
1/4	13.0	155.7
Cb	10.2	158.5
S	16	162.1
2+2128-FL Horton		
S	2.1	166.6
1655-FL 16N		
Cb	2.1	166.3
cb	4.7	164.0
1/4	6.6	162.1
g	10.0	158.7
1/4	13.1	155.6
Cb	15.9	152.8
H	19.5	149.2

Cross Section 16N  
Horton to S.L. Upas

16870.

0+0-FL Horton + FL 16N

F	24	166.3
0+27.4		
F	1.6	167.1
Cb	9.9	158.8
TP	12.53	168.33
1290		
155.80		
0+41.10		
1/4	14.9	153.4
Cb	9.7	158.6
F	0.9	167.4
0+54.8		
F	7.04	168.7
Cb	8.9	158.4
1/4	13.7	154.6
g	18.8	149.5
0+68.5		
1/4	21.5	146.8
g	16.2	152.1
1/4	12.4	155.9

4

1615

168.33

168.33

Cb 8.1 160.2

1+50

F 71.0 169.3

F +38 172.1

0+82.2

Cb 3.2 165.1

F 71.5 169.5

1/4 7.0 161.3

Cb 7.5 160.8

1/2 10.9 157.4

1/4 11.7 156.6

1/4 18.6 154.7

1/2 16.1 152.2

Cb 19.2 149.1

1/4 19.9 148.4

+8 21.8 146.5

Cb 25.2 143.1

+10 29.3 139.0

1409.6 Sec 80 W. side

1/4 29.0 139.3

1/4 31.3 137.0

1+70.3 = 54. Thorn

+9 31.3 137.0

1/4 29.6 141.1

+11 28.2 140.1

+10 27.1 141.2

Cb 34.1 144.2

+13 19.2 149.1

1/4 19.2 149.1

Cb 16.2 152.1

1/2 14.5 153.8

1/4 11.8 156.5

1/4 11.0 157.3

1/2 8.2 160.1

Cb 6.6 161.7

1/4 4.5 163.8

F 40.5 168.8

Cb 1.6 166.7

F +42 172.5



1610

168.33

S 6 Tborn

201025  
10/14

168.33

S Tborn

6

F	+5.5	173.8
Cb	+0.4	168.7
1/4	1.5	166.8
1/2	5.1	163.2
3/4	9.7	158.6
Cb	14.1	154.2
+13	20.3	148.0
+15	26.3	142.0
H	26.0	142.3
H	24.2	144.1
+5	24.5	143.8
+7	19.1	149.2
Cb	13.2	155.1
1/4	8.6	159.7
1/2	4.2	164.1
3/4	0.0	168.3
Cb	+2.7	171.0
F	+6.8	175.1

S 1/4

F	+7.5	175.8
Cb	+3.0	171.3
1/4	+1.0	169.3
1/2	4.03	164.30
3/4	8.0	160.3
Cb	12.0	156.3
+14	18.2	150.1
+16	23.0	145.3
H	23.0	145.3
H	21.6	146.7
+6	21.6	146.7
+8	16.5	151.8
Cb	11.6	156.7
1/4	7.2	161.0
1/2	2.8	165.5
3/4	13.24	177.54
TR	13.24	177.54
1/4	4.03	164.30
1/2	9.0	168.5
Cb	5.7	171.8

H 1/4

on 1400

F	0.5	177.0
	NC6	
F	0.7	176.8
BM	0.23	176.81
C6	5.4	172.1
1/4	8.5	167.0
1/2	10.9	166.6
1/4	15.8	161.7
C6	19.9	157.6
+10	23.1	154.4
+12	28.5	149.0
N	28.6	148.9
	H.L. Thorn = 0+0	
N	36.3	141.2
+5	26.3	151.2
+15	26.5	151.0
+18	22.2	155.3
C6	22.0	155.5
1/4	17.7	159.8
1/2	14.0	163.5

on Peg  
N.E. Thorn  
+ 1611

1/4		10.4	167.1
C6		7.8	169.7
F		1.9	175.6
	0+25		
F		8.5	169.0
C6		13.6	163.9
TP	1.39	166.26	164.87
1/4		5.0	161.3
1/2		6.2	160.1
1/4		11.8	154.5
C6		14.9	151.4
+5		14.5	151.8
+12		18.3	148.0
+15		24.1	142.2
N		24.1	142.2
+5 - Fly House		24.1	142.2
	0+50		
-20		27.0	139.3
N		25.1	141.2
C6		22.6	143.7

1615

16626

1/4		16.4	149.9
1/2		17.6	148.7
+5		17.6	148.7
1/4		13.8	152.5
cb		9.4	156.9
F		6.2	160.1
TP	7.60	16118 ✓ 126.8	153.58 ✓
		0+75	
I		7.1	154.1
cb		12.7	148.5
1/4		13.1	148.1
1/2		14.8	146.4
1/4		16.2	145.0
cb		19.4	141.8
1/2		19.6	141.6
+20		20.6	140.6
		140	
-10	= Sky Dirt Disc 10" Wide	20.3	140.9
1/2		19.6	141.6
cb		18.8	142.4

16118

8

1/4		17.1	144.1
1/2		16.2	145.0
1/4		15.2	146.0
cb		12.0	149.2
F		10.2	151.0
		1+25	
I		10.1	151.1
cb		10.2	151.0
1/4		11.3	149.9
1/2		11.0	150.2
1/4		11.3	149.9
cb		15.2	146.0
+15		15.7	145.5
1/2		18.3	142.9
+10	= Fly From Ho.	18.3	142.9
		1430	
-10		17.8	143.4
1/2		17.8	143.4
+5		15.3	145.9
cb		14.8	146.4

1/4	11.3	149.9
1/8	11.1	150.1
1/4	11.1	150.1
cb	8.6	152.6
F	4.3	156.9
1+50		
F	2.5	158.7
cb	5.5	155.7
1/4	9.3	151.9
1/8	11.0	150.2
1/4	11.2	150.0
cb	12.2	149.0
+15	13.3	147.9
H	17.6	143.6
+10 = 1/4 Ho.	17.6	143.6
+20	19.5	141.7
1+75		
-20	19.8	141.4
-10	17.2	144.0
H	17.0	144.2

+5	14.0	147.2
cb	11.8	149.4
1/4	11.7	149.5
1/8	11.0	150.2
1/4	8.5	152.7
cb	6.2	155.0
F	3.9	157.3
2+0		
F	4.6	156.6
cb	9.5	151.7
1/4	10.4	150.8
1/8	11.9	149.3
1/4	12.3	148.9
cb	14.7	146.5
H	17.6	143.6
+20	18.7	142.5
2+25		
-20	18.3	142.9
H	16.8	144.4
cb	14.1	147.1

1/4	12.6	148.6
1/2	12.5	148.7
3/4	11.7	149.5
cb	9.7	151.5
F	7.0	154.2

2+50

F	8.9	152.3
cb	11.2	150.0
1/4	12.1	149.1
1/2	11.9	149.3
3/4	11.4	149.8
cb	13.8	147.4
H	15.2	146.0
+20	16.1	145.1

2+75

-20	11.9	149.3
H	11.5	149.7
cb	9.1	152.1
1/4	10.4	150.8
1/2	11.2	150.0

1/4	11.2	150.0
cb	10.5	150.7
F	8.7	152.5

2+0 = S.L. Upel

F	7.2	154.0
cb	7.7	153.5
1/4	7.2	154.0
1/2	6.4	154.8
3/4	5.9	155.3
cb	5.4	155.8
H	5.1	156.1
+10	4.8	156.4

Crown Section Thorns  
1615 to Hawk

80' wide  
20' Cbr  
10' 1/4

18912

11

BN	12.31	189.12	176.81	07 Pm NE Thorn Hill			
					cb	2.5	186.6
		0+0 FL 1615			1/4	2.2	186.9
					1/2	1.7	187.4
N		13.3	175.8		1/4	1.7	187.4
cb		11.9	177.2		cb	2.5	186.6
1/4		12.3	176.8		S	4.2	184.9
1/2		13.1	176.0		TP	12.00	201.60
1/4		14.0	175.1			0.52	188.60
cb		15.0	174.1			0.795	
S		16.4	172.7		S	12.5	189.1
		0.125			cb	11.7	189.9
S		8.4	180.7		1/4	11.4	190.2
cb		6.8	182.3		1/2	10.9	190.7
1/4		6.2	182.9		1/4	10.4	191.2
1/2		6.4	182.7		cb	10.7	190.9
1/4		5.6	183.5		H	12.3	189.3
cb		5.6	183.5			14.0	
H		8.3	180.8		H	8.1	193.5
		0.150			cb	7.1	194.5
H		8.1	186.0		1/4	7.0	194.6
					1/2	7.2	194.4

201.60

1/4	75	194.1
cb	81	193.5
S	85	193.1
	1+25	
S	5.3	196.3
cb	4.4	197.2
1/4	4.2	197.4
1/2	3.9	197.7
1/4	3.9	197.7
cb	4.0	197.6
N	4.9	196.7
	1+50	
N	0.5	201.1
cb	0.4	201.2
1/4	0.4	201.2
1/2	0.6	201.0
1/4	0.9	200.7
cb	1.0	200.6
S	2.0	199.6

201.60

12

TP	12.20	212.55	1.25	200.35
		1+75		
S		9.6		203.0
cb		8.1		204.5
1/4		7.6		205.0
1/2		7.6		205.0
1/4		6.9		205.7
cb		7.2		205.4
N		7.0		205.6
		210 = r.H. Markt		
N		4.1		208.5
cb Top		4.20		208.25 208.0 = profile
Gutter on Pav		4.91		207.64
1/4		4.78		207.77
1/2		4.94		207.61
1/4		5.30		207.25
Gutter " "		5.93		206.63
cb Top		5.32		207.23 207.0 "
S		5.8		206.8

Cross Section from  
1615 to Horton

80. Wide  
20. Cbs  
10. Qts.

147.77

13

BM 2.63 147.77 ✓

145.14

Mo. of  
Sassafras  
Horton

cb

6.4

141.4

S

7.2

140.6

W.L. 1615

28 Mo. of W.L. 1615

S

6.7

141.1

S

13.0

134.8

cb

5.0

142.8

cb

10.1

137.7

1/4

3.8

144.0

1/4

8.9

138.9

1/2

2.2

145.6

1/2

8.0

139.8

1/4

1.0

146.8

1/4

7.4

140.4

cb

7.05

148.3

cb

7.2

140.6

1/10

7.20

149.8

1/10

6.7

141.1

1/16

6.2

141.6

45.5 ft. = Ed Horton on S

1/1

6.2

141.6

1/1

14.4

133.4

5 ft. of W.L. 1615

cb

14.4

133.4

6 ft. of W.L. - Conc. Porch

5.51

142.26

1/4

12.8

135.0

15 ft. of W.L. 1615

1/2

13.3

134.5

1/1

6.7

141.1

1/4

14.2

133.6

cb

5.8

142.0

18 ft. of W.L.  
1615 on W.L.  
by Peppertown

cb

15.5

132.3

1/4

5.8

142.0

S

18.4

129.4

1/2

6.8

141.0

1/2

15.4

136.78

12.53

135.24

1/4

8.0

139.8

54 ft. of W.L. 1615

1/1 Garage 2nd floor

5.4

142.4



T 6077

136.78

14

E.L. Horton on Diog

S	77	129.4
cb	89	127.9
1/4	84	128.4
1/2	83	128.5
1/4	77	129.4
cb	1.5	130.3
N	6.0	130.8

Sassafras St. 4 1/2 W  
Additional Outs on North

140.07

2-10-33 15

				SWCT Sassafras 1615	60' N of N.L. Sassafras	15.7	124.4
BM	900	128.74	119.74		75' N " " " "	15.8	124.3
		0+95.48				1+83.78 = 2 Hortos	
		15' N of N.L. Sassafras	7.7	126.04	85' N of N.L. Sassafras	14.5	125.6
					55' N " " " "	12.5	127.6
		1+20.88			42' N " " " "	13.5	126.6
		40' N of N.L. Sassafras	7.3	126.4	30' N " " " "	7.7	132.4
					5' N " " " "	8.8	131.3
		20' N " " " "	7.6	121.1			
		1+46.88 = N.L. Hortos				1+93.78 = E 1/4	
		20' N of N.L. Sassafras	6.3	122.4	15' N of N.L. Sassafras	7.7	132.4
					40' N " " " "	6.8	133.3
		40' N " " " "	7.0	121.7	52' N " " " "	11.9	128.2
		60' N " " " "	6.7	122.0	67' N " " " "	10.9	129.2
		1+63.78 = WCB Hortos			90' N " " " "	13.3	126.8
		70' N of N.L. Sassafras	6.0	122.7		2+03.78 = E 1/2	
		45' N " " " "	5.5	123.2	95' N of N.L. Sassafras	11.4	128.7
		35' N " " " "	4.5	124.2	75' N " " " "	8.9	131.2
		20' N " " " "	0.5	128.2	62' N " " " "	9.9	130.2
		1+73.78 = N 1/4			52' N " " " "	5.3	134.7
TP	11.75	140.07	0.42	128.33	27' N " " " "	6.3	133.8
					15' N " " " "	1.1	139.0
		20' N of N.L. Sassafras	8.7	131.4			
		35' N " " " "	14.9	125.2			

16th St.

Addition of outer on West

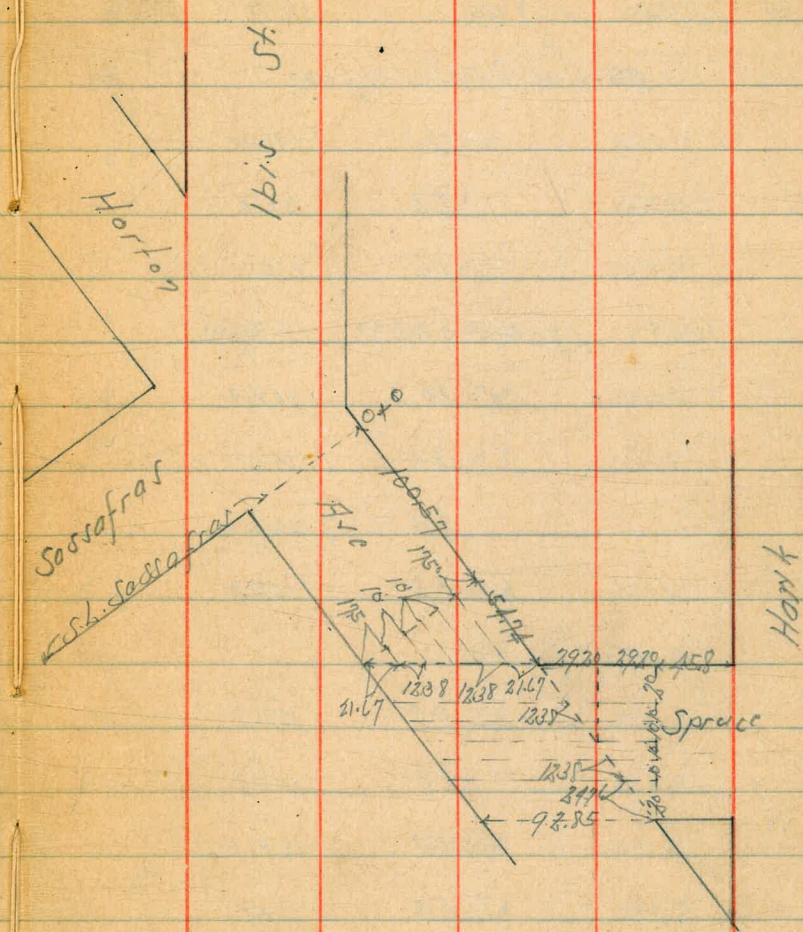
140.07

1709.6

5' W of W.L. 16th	4.3	135.8
11' W	8.2	131.9
25' W	10.5	129.6
40' W	14.2	125.9

1750

30' W of W.L. 16th	9.0	131.1
15' W	8.1	137.0



Cross Section Horton And Spruce  
 Sassafras to Hawk  
 See Sketch Page 16

75' H. de  
 175' Cb  
 20' Qz

170.57

75'S

8-25-33  
 Wagon  
 Station  
 Northway  
 17

BM 12.94 158.08 145.14

25'S of S.L. Sassafras

H 12.1 146.0

Cb 5.3 152.8

1/4 1.6 156.5

TP 13.12 190.57 0.63 157.45

1/2 10.8 159.8

1/4 8.3 162.3

Cb 6.4 164.2

E 2.5 168.1

50'S

E 0.7 169.9

Cb 3.4 167.2

1/4 5.2 165.4

1/2 6.5 164.2

1/4 8.3 162.3

Cb 11.0 159.6

H 14.6 154.0

H

Cb

1/4

1/2

1/4

TP

Cb

E

E

Cb

1/4

1/2

1/4

Cb

H

1/2

1/4

12.29 182.72 0.14 170.43

11.0

157.6

6.1

164.5

3.5

167.1

2.2

168.4

0.9

169.7

0.14

170.43

11.5

171.2

9.3

173.4

160.57'S

5.3

172.4

6.5

176.2

7.6

175.1

9.7

173.0

11.4

171.3

12.4

170.3

16.3

166.4

127.91'S

6.7

176.0

5.8

176.9

18272

cb		17	178.0
F		25	180.2
	100.57 South 155.31 South = H.C.	Spruce or Diog.	
TP	720	18961	0.31 182.41
F		62	183.4
cb		94	180.2
1/4		115	178.1
2		137	175.9
1/4		143	175.3
cb		167	172.9
H		232	166.4
	H.C. or Diog.		
H		179	171.8
cb		147	174.9
1/4		128	176.8
2		111	178.5
1/4		86	181.0
cb		64	183.2
F		30	186.6

18961

18

	2 Spruce or Diog.		
F		10	188.6
cb		33	186.3
1/4		52	184.4
2	or Mon	721	182.40
1/4		92	180.4
cb		118	177.8
H		164	173.2
	S Cb or Diog.		
H		130	176.6
cb		90	180.6
1/4		67	182.9
2		47	184.9
1/4		30	186.6
cb		20	187.6
F		20	187.6
	S L Spruce or Diog.		
F		88	186.8
cb		39	185.7
1/4		50	184.6

189.61

2	5.3	184.3
1/4	6.4	183.2
Cb	8.6	181.0
H	14.3	175.3

## Cross Section Spruce

39.2' E of E.L. Horton on N  
= E.L. Horton on Spruce

2	1.1	188.5
1/4	1.0	188.6
Cb	0.9	188.7
H.L.	0.5	188.1

58.1' E of E.L. Horton on N  
= E.L. Horton on S

H	1.0	188.6
Cb	2.3	187.3
1/4	2.1	182.5
2	2.3	187.3
1/4	2.7	186.9
Cb	2.6	182.0
S	2.8	186.8

20 ft. dr  
20 Cbs  
16 Gls

189.61

19

102' E of E.L. Horton. 2' N of H.L. Hank

S	+0.5	190.1
+10	+0.7	190.3
+14	2.5	187.1
Cb	3.0	186.6
1/4	3.0	186.6

2	3.1	186.5
1/4	3.1	186.5
Cb	3.2	186.4
1/6	3.0	186.6
+15	1.9	187.7
H	0.1	189.5

104.2' E = H.L. Hank

H	2.4	187.2
+14 = Top Existing Cb	2.93	186.68
Gutter on Pavement	3.64	185.97
Cb " "	3.39	186.22
1/4 " "	3.19	186.42
2 " "	3.02	186.54
1/4 " "	2.95	186.66

189.61

20

Cb 07 Pav 129 300 186.61

+ 6 - Top Existing Cb 2.41 187.20

+ 6 Gutter 3.02 186.59

S 2.7 186.91

4-7-33  
Miller  
Walker  
Bliss

16<sup>th</sup> ST X Sec  
Commercial South  
For RePavement & Removal of Public Seates.

Indexed  
costs.

BM.B.P.	1.47	13.99	12.52
30' N. of S. Line Commercial = S. Rail S.D. & H. RR Spur			
W. Line 16 <sup>th</sup>		<u>13.99</u> 3.58	10.41
+14' = W. cl		3.37	10.62
cl + 18' = W. Rail S.D.E.R.R.		3.00	10.99
20' N. of S. Line Commercial			
cl + 18' W. Rail S.D.E.R.R.		3.09	10.90
" + 10		3.50	10.69
cl.		4.17	9.82
W. Line 14		4.52	9.43
14' N. of S. Line Commercial = S. cl			
W. Line 10 gutter		5.03	8.96
" " " Top cl.		5.70	8.29
+4 = P.C. Top cl		4.99	9.00
" " gutter		5.63	8.36
cl.		4.79	9.20
+10		3.70	10.29
+18 = W. Rail		3.13	10.86

13.99  
00 = S. Line Commercial  
13.99  
3.27 10.74

cl + 18			
+10			3.80 10.19
+5.			4.70 9.29
gutter			5.69 8.30
cl.			5.00 8.99
W.			4.85 9.14
31' S.			
W.			5.1 8.89
+4 = W. edge cur. walls			5.12 8.87
+9.33 = 8 " " "			5.25 8.74
cl.			5.29 8.70
gutter			5.98 8.01
+5			5.02 8.97
+10			4.17 9.84
+15			3.73 10.46
+27.9 W. Rail S.D. E.R.R.			3.54 10.45
Bet 31' S. & 37' S. Curb Cockeyed 0.25 E. of Line			
" 39' S & 48' S Curb Badly Broken.			



13.99

48' S. 13.99

cl + 40 = N. Rail S. D. E. R.R.	3.59	10.40
cl + 23	3.79	10.75
+ 15	4.13	9.86
+ 10	4.56	9.43
+ 5	5.23	8.76
gutter	6.07	7.92
cl	5.44	8.55
+ 4.67 = E. edge cmt walk	5.37	8.62
+ 10. W " " "	5.27	8.72
W.	5.3	8.69
65.55.		
W.	5.3	8.69
+ 4 = W. edge walk	5.42	8.57
+ 9.33 E " "	5.52	8.47
cl	5.56	8.43
gutter at N. End 2. 4" pipe Drain	6.18	7.81
+ 5	5.30	8.69
+ 10	4.74	9.25
+ 15	4.39	9.60
+ 20	4.24	9.75
+ 40	4.03	9.96

13.99

66.0 S. 13.99

16" ST

22

cl + 40	4.03	9.96
+ 20	4.29	9.70
+ 15	4.41	9.58
+ 10	4.67	9.32
+ 5	5.21	8.78
cl. line on asphalt Runway	5.46	8.53
+ 4.67 " " "	5.48	8.51
+ 10. " " "	5.38	8.61
W. " " "	5.40	8.59
Bet 66.0 S. + 79.5. Asphalt Runway Laid over Curb		
+ Walk to W. Line		
78.6 S.		
W. on asphalt Runway	5.43	8.56
+ 4	5.43	8.56
+ 9.33	5.51	8.48
cl. line	5.49	8.50
+ 4	5.32	8.67
+ 5.2 pavmt.	4.89	9.10
+ 5.2 N.W. Cor. Seales platform	4.79	9.20
+ 74.9 N.E. " " "	4.84	9.15
+ 149 Pavmt.	4.80	9.19

13.99

78.6 5. (204)  
13.99  
4.72

9.27

13.99 13.99

90.75 6.07

7.92

8.32

8.18

8.34

23  
Pavmt.  
Top ent. wall  
Pavmt.  
Top ent. wall

+ 20

2.4 E. of E. cb = S.W. cor scales Base

5.47

5.81

+ 40.

4.35

9.64

5.2 E " " " = S.E. " " "

5.67

80.5.

95. N.

el + 40

4.35

9.64

W.

5.6

8.39

" + 20

4.72

9.27

+ 4 = W. side walk

5.61

8.38

+ 15

Pav.

4.80

9.19

+ 9.33 = E " "

5.72

8.77

+ 14.9

scales platform.

4.84

9.15

el

5.75

8.21

+ 5.2

"

4.79

9.20

gutter at N. End. 6" Pipe

6.36

7.63

+ 5

Pavmt.

5.56

8.63

+ 5

5.91

8.08

+ 3

5.78

8.21

gutter S. End. 2, 4' pipes

6.23

7.76

+ 5.2 scales platform.

4.77

9.24

el

5.66

8.33

+ 14.9 " "

4.81

9.18

+ 4.67 = E. edge ent walk

5.64

8.35

+ 15 pavmt.

4.82

9.17

+ 10. = W " " "

5.54

8.25

+ 20

5.09

8.90

W.

5.4

8.59

+ 40

4.80

9.19

83.8 S.

98. S.

scales Base

5.83

8.16

pavmt.

2.4 E. of E. cb = N.W. Cor

5.67

8.32

Top ent. wall

+ 40

4.80

9.19

" "

5.59

8.40

Pavmt.

+ 20

5.09

8.90

5.2 " " " " = N.E. "

5.67

8.32

Top ent. wall

+ 15

4.82

9.17

85.0 S.

El. dirt Under  
scales platform  
Base

7.3

6.69

+ 14.9

scales platform

4.81

9.18

+ 5.2

" "

4.77

9.24

13.99			13.99			16 <sup>th</sup> St. 24		
+5.0	pavmt.	5.96	8.03	+10	5.57	8.62		
ch		5.75	8.71	+5	5.82	8.17		
+4.67	= E. edge walk	5.73	8.76	ch. line on asphalt Runway	5.77	8.22		
+10	= W " "	5.61	8.38	+4.67 W " " "	5.70	8.79		
W		5.5	8.49	+10 " " "	5.54	8.45		
	98.2 S.			W.	5.6	8.39		
W.		5.5	8.49		112.0 S.			
+4	on asphalt Runway	5.51	8.48	W	5.6	8.39		
+9.33	" " "	5.61	8.38	+4	5.70	8.29		
ch	" " "	5.60	8.39	+9.33	5.81	8.18		
+5.2	pavmt.	4.86	9.13	ch	5.91	8.08		
+5.2	S.W. cor scales platform	4.81	9.18	gutter at S. End 6" Pipe	6.52	7.47		
+14.9	S.E. " " "	4.91	9.08	+5	6.07	7.92		
+15		4.84	9.15	+10	5.83	8.16		
+20		5.15	8.84	+15	5.68	8.31		
+40		4.76	9.23	+20	5.49	8.56		
	110.0 S			+40	5.12	8.87		
ch +40.0		5.04	8.98					
+20		5.39	8.60					
+15		5.49	8.50					

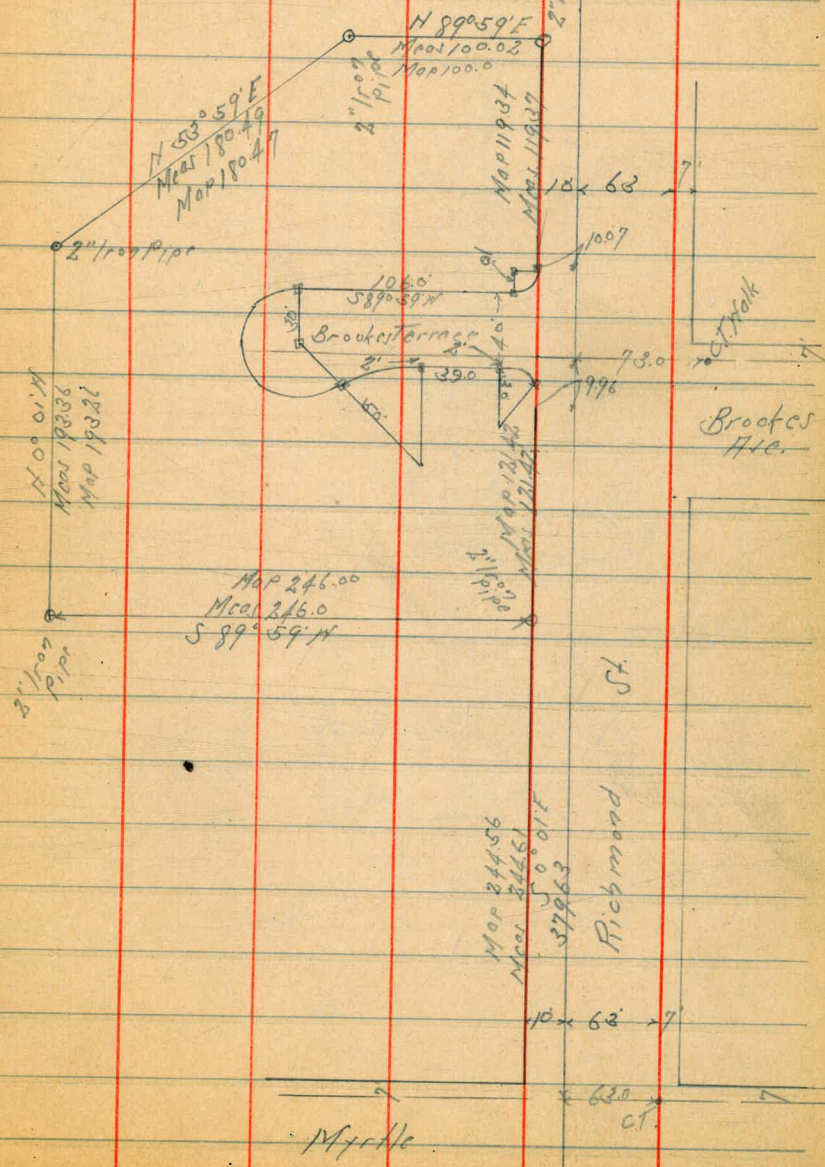
117.5  
13.99  
5.15

eb + 40 E.		8.84
+ 20	5.60	8.39
+ 10	5.96	8.03
+ 2.5 = N.E. cor. catch basin	6.33	7.66
gutter = N.W. " " "	6.58	7.41
eb.	5.95	8.04
+ 4.67 E. edge walk	5.88	8.11
+ 10. W " " "	5.76	8.23
W.	5.6	8.39
121.5		
W.	5.7	8.29
+ 4 N. edge walk	5.86	8.13
+ 9.33 E " "	5.96	8.03
eb	6.00	7.99
gutter, S.W. cor. catch basin	6.36	7.63
+ 2.5 = S.E. " " "	6.31	7.68
+ 10	5.99	8.00
+ 20	5.61	8.38
+ 40	5.17	8.82

Survey Brookies Terrace

indexed  
c.s.N.

5-16-33  
Moore 26  
Sisson  
Northey



Alignment Miramar Road  
From Nly. End of Grading to Rose Canyon High Way

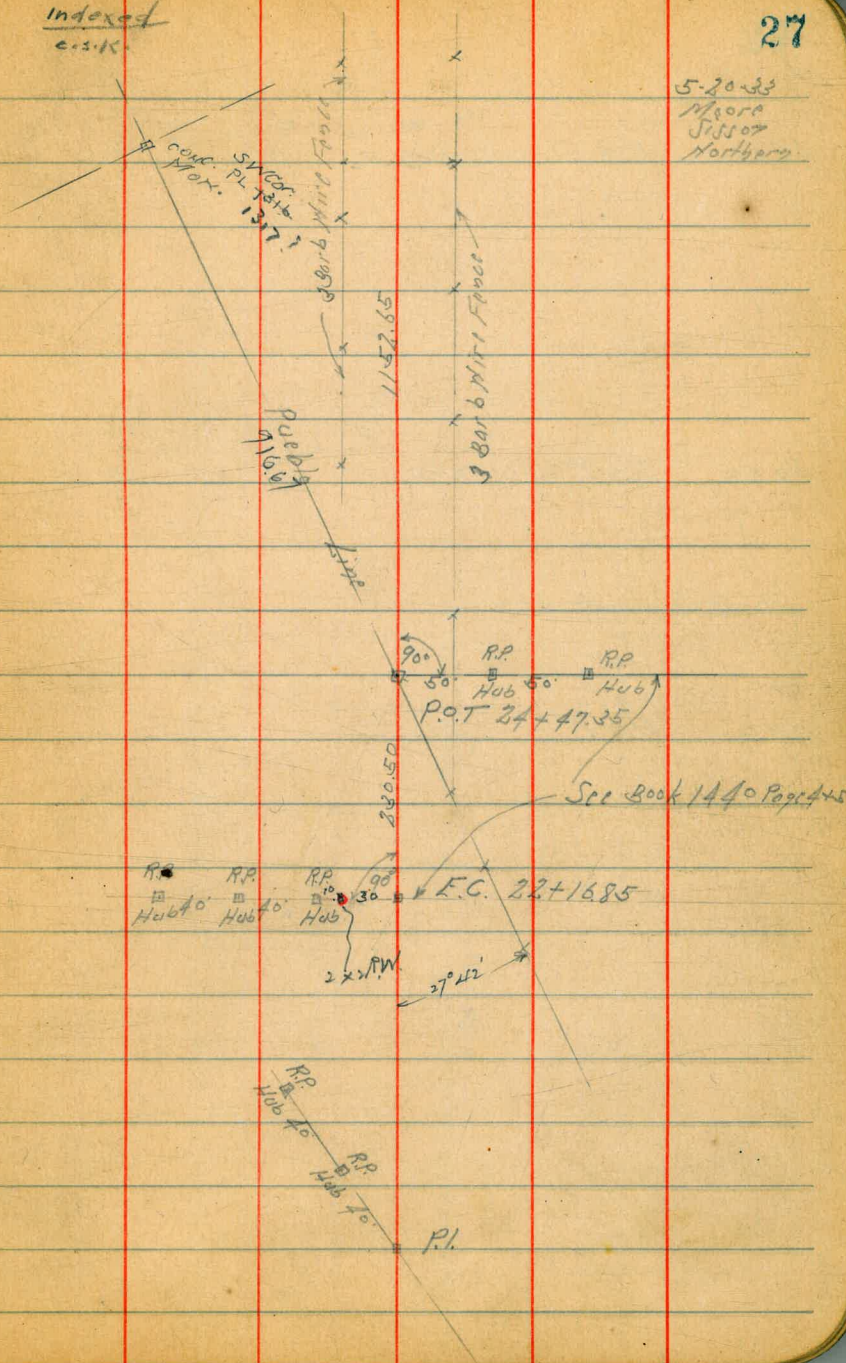
Indexed  
e.s.k.

5-20-33  
Moore  
Jessor  
Northway

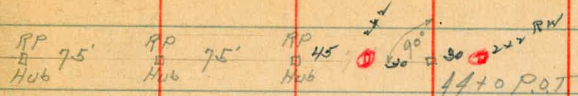
Note: For Cross Sections See Page 27 to

24+47.35 P.O.T.

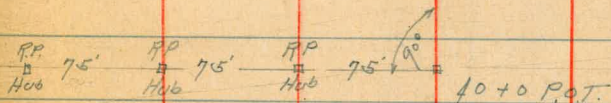
22+16.85 F.C.



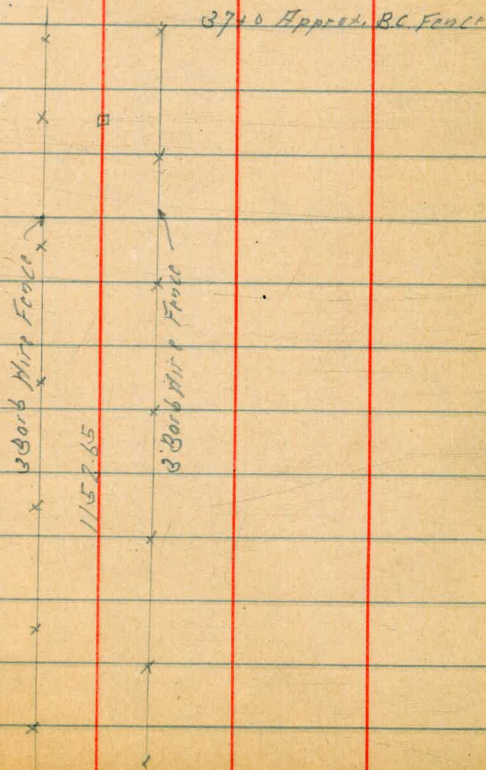
44+0 P.O.T.



40+0 P.O.T.



36+0 P.O.T.



56+0 P.O.T.

49+50 P.O.T.

55.00

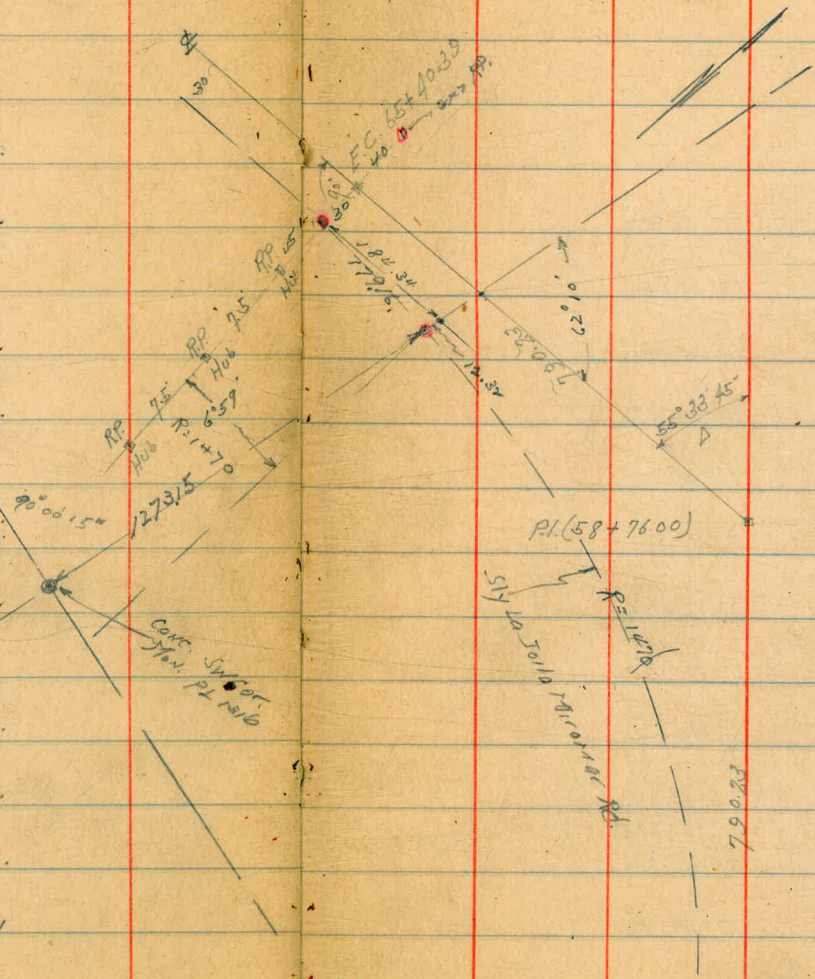


5-22-33

⊙ = 2x4 Hubs replaced

+50	14° 35.731'
58	13° 38.436'
+50	12° 41.141'
57	$\Delta = 55^\circ 33' 45''$ 11° 43.846'
+93 Culvert	11° 35.825'
+50	R=1500.0 10° 46.551'
56	T=790.23 9° 49.256'
+50	L=1454.62 8° 51.961'
55	7° 54.666'
+50	6° 57.371'
54	6° 00.076'
+50	5° 02.781'
53	4° 05.486'
+50	3° 08.191'
52	2° 10.896'
+50	1° 13.601'
51	0° 16.306'

50+8577 B.C.



RP 75 Hub      RP 78 Hub      BC 50+8577      30      20

Lt.

65+4039 F.C.	27° 46.866'
65	27° 09.566'
+50	26° 03.271'
64	25° 05.976'
+50	24° 08.681'
63	23° 11.386'
+50	22° 14.091'
62	21° 16.796'
+50	20° 19.501'
61	19° 22.206'
+68 Culvert	18° 43.245'
+50	18° 24.911'
60	17° 27.616'
+50	16° 30.321'
59 P.O.C.	15° 33.026'

72+1266 P.O.T.

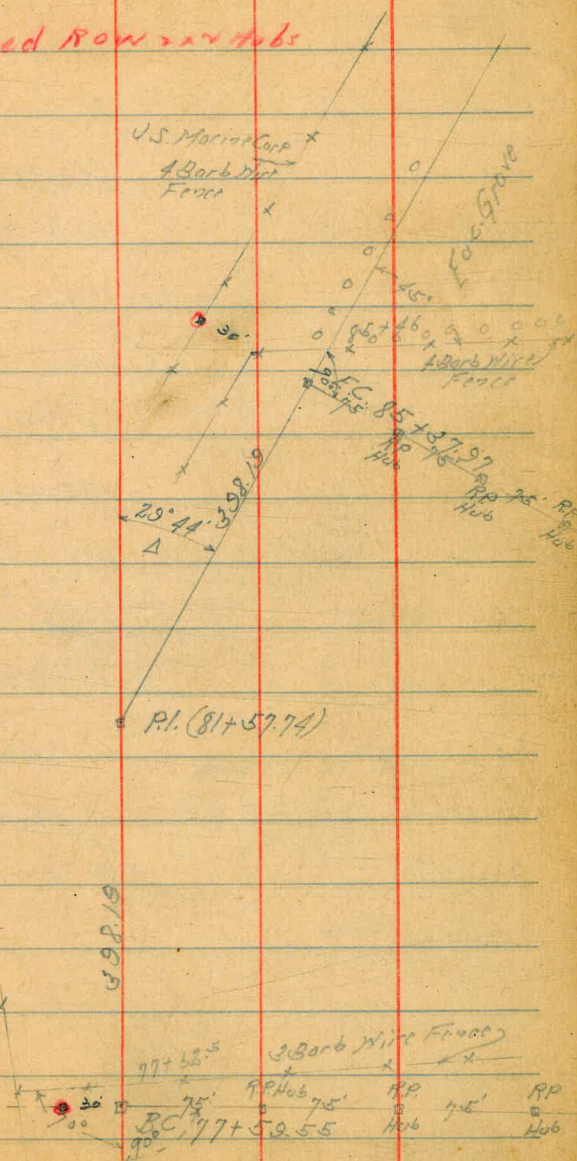
73+140  $\frac{90y}{P.O.T.} \frac{4-34}{10}$   $\frac{P.O.T.}{10}$

RP 75' RP 75' RP 75'  $\frac{90y}{P.O.T.}$   
 Hub Hub Hub P.O.T. 72+1266

Rt.

85+37.97	E.C.		14° 52'
85			14° 08.482'
+50			13° 11.187'
84			12° 13.892'
+50			11° 16.597'
83		$\Delta = 29^{\circ} 44'$	10° 19.302'
+50		$R = 1500.0$	9° 22.007'
		$T = 398.19$	
82		$L = 778.42$	8° 24.712'
+50			7° 27.417'
81			6° 30.122'
+50			5° 32.827'
80			4° 35.532'
+50	P.P.C.		3° 38.237'
79			2° 40.942'
+50			1° 43.647'
78			0° 46.352'
77+59.55	B.C.		

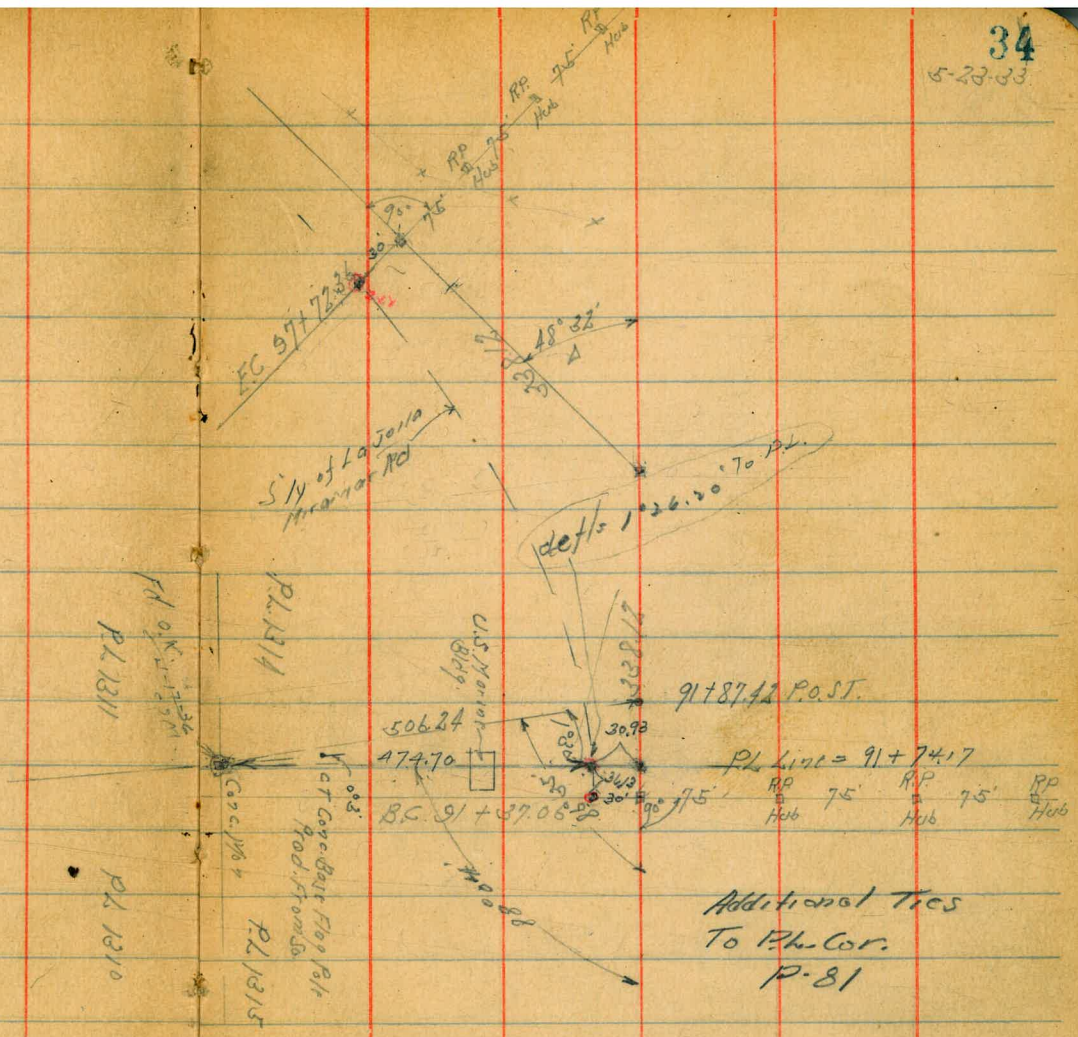
o - replaced Row 2 &amp; 4 hubs

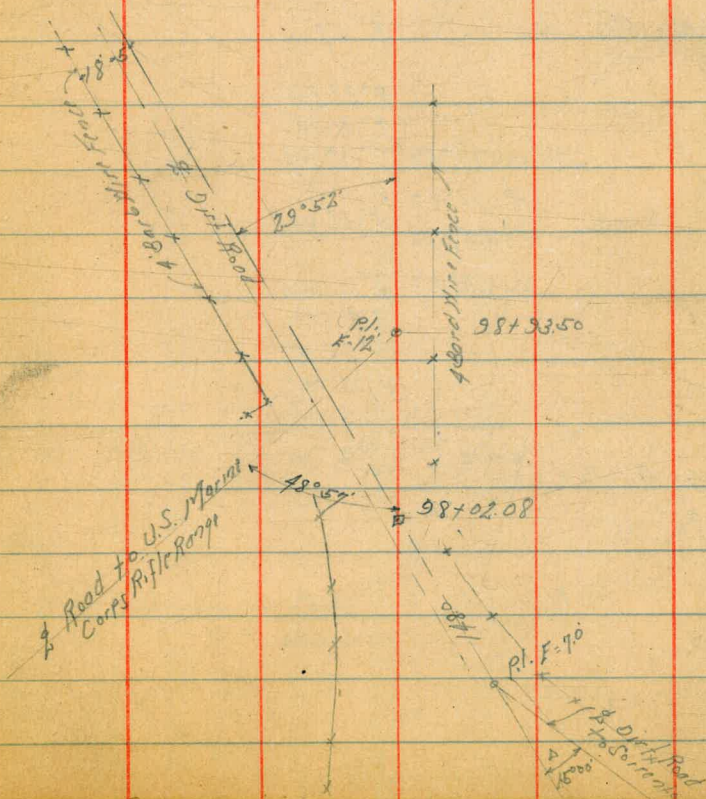


97+72.36	EC.	21° 16'
+50		23° 24.746'
97		21° 30.156'
+50	A = 48° 32'	19° 35.566'
96	P = 7500'	17° 40.976'
+50	T = 33812'	
	L = 635.30	15° 46.386'
95	P.O.C.	13° 51.796'
+50		11° 57.206'
94		10° 02.616'
+50		8° 08.026'
93		6° 13.436'
+50		4° 18.846'
92		2° 24.256'

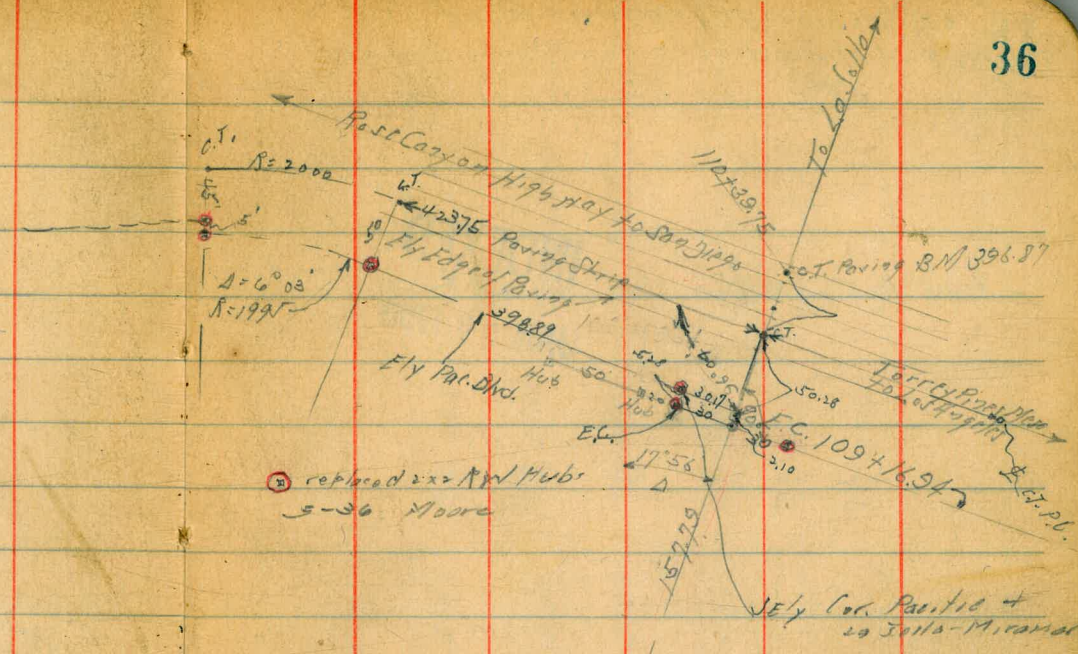
91+37.06 B.C.

85+70.50 P.O.T.



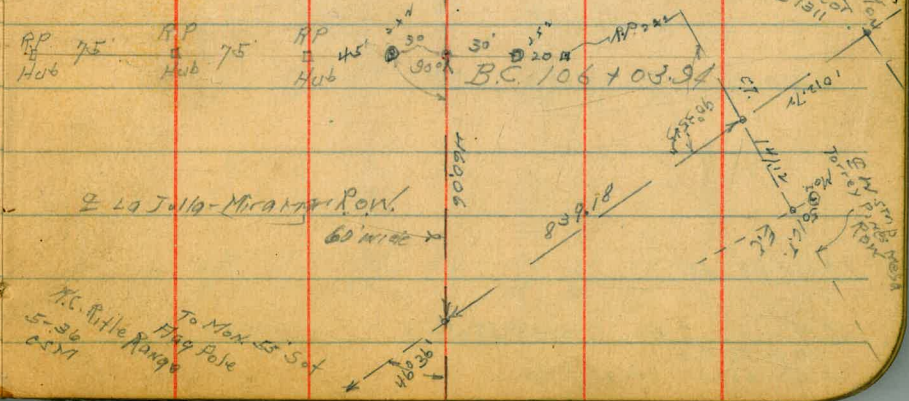


Rt.



109+16.94	E.C.	8° 58'
109		8° 28.884'
+66.94		7° 31.25'
+50		7° 02.941'
+16.94		6° 06.01'
108	P.O.C.	5° 36.998'
		L=313.00'
+50		4° 11.055'
+03.94		3° 51.83'
107		2° 45.112'
+53.94		1° 25.94'
+50		1° 13.168'

106+03.94 B.C.



Cross Section Miramar Road  
 Nly End of Grading to Post Canyon Highway  
 For Alignment See Page 27 to 36

37  
 5-24-33 ✓  
 Moore  
 JENSEN  
 Northern

+ 47.35 P.O.T on Pl. List

INDEXED  
 MK  
 JAN 23 1950

24

+ 50

23

+ 50

22+16.85 EC.

BM 2.90 25848  
 07 40 TIC 406  
 Lt 22+16.85 EC 1440 Page 15

Station	Left	Right	PI
24	5.6 40	5.4 23	5.2 23
+ 50	5.5 40	4.9 23	4.3 23
23	4.4 40	4.2 23	3.5 27
+ 50	5.6 40	5.0 23	4.6 27
22+16.85 EC.	2.8 40	2.9 23	2.6 27

25848



H.I.  
352.6

+50

4  
352.6  
24  
40  
353.8  
22  
28  
352.5  
25  
10  
353.5  
22  
10  
352.9  
22  
10  
R1  
353.0  
20  
40

TP 2.20 355.04 5.64 352.84

27

352.8  
5.7  
40  
353.2  
5.3  
28  
353.0  
5.5  
10  
353.2  
5.3  
10  
353.4  
5.1  
28  
353.4  
5.1  
10

+50

H.I. = 358.45

353.2  
5.3  
40  
353.4  
5.1  
28  
353.3  
5.2  
10  
353.6  
4.9  
10  
353.9  
4.6  
28  
353.7  
4.8  
40

26

353.0  
5.5  
40  
353.2  
5.3  
28  
353.4  
5.1  
14  
354.2  
4.3  
14  
354.1  
4.4  
28  
354.1  
4.4  
40

+50 = Prop. Culvert

352.4  
6.1  
40  
352.8  
5.7  
28  
353.0  
5.5  
15  
354.1  
4.4  
15  
354.1  
4.4  
28  
354.0  
4.5  
40

25

352.4  
6.1  
40  
352.9  
5.6  
28  
352.9  
5.6  
15  
353.3  
5.2  
15  
353.6  
4.9  
28  
353.7  
4.8  
40

352.48

358.48

750

30

750

29

750

28

355.04

H. C. BURTON

1.5 40	352.5	8.7 40	351.3	1.5 40	350.8	1.5 40	350.6	1.5 40	350.5	1.5 40	350.5	1.5 40	350.5	1.5 40	350.5	1.5 40	350.5
2.6 23	352.4	8.6 23	351.4	2.6 23	350.5	2.6 23	350.2	2.6 23	350.5	2.6 23	350.2	2.6 23	349.6	2.6 23	350.1	2.6 23	350.1
2.8 10	352.2	4.0	351.0	4.8	352.2	4.8	349.6	4.8	352.2	4.8	349.6	4.8	349.6	4.8	349.6	4.8	349.6
2.5 10	352.5	8.6 23	351.4	4.6 23	350.4	4.6 23	349.6	4.6 23	350.4	4.6 23	349.6	4.6 23	349.6	4.6 23	349.2	4.6 23	349.2
2.8 40	352.2	8.6 40	351.4	4.8 40	350.2	4.8 40	350.0	4.8 40	350.2	4.8 40	350.0	4.8 40	350.0	4.8 40	349.2	4.8 40	349.2
2.5 40	352.5	8.6 40	351.4	4.8 40	350.2	4.8 40	350.0	4.8 40	350.2	4.8 40	350.0	4.8 40	350.0	4.8 40	349.2	4.8 40	349.2

355.04

TP 0.72 Hail 7.41 356.29 6.16 348.88  
33+50

+50

33

+50 = Prop Culvert

32

+50

31

355.04

H. 1. 30700

4	3490	348.9	348.8	348.2	348.1
6.0 10.	6.1 23.	6.2 23.	6.8 23.	6.9 10.	
348.4	348.5	348.6	348.0	347.3	
6.6 10.	6.5 23.	6.4	7.0 23.	7.7 10.	
348.5	348.3	348.6	347.2	346.4	
6.5 10.	6.7 23.	6.4	7.8 23.	8.6 10.	
349.0	348.7	348.7	348.6	348.3	
6.6 10.	6.3 23.	6.3	6.4 23.	6.7 10.	
348.5	349.4	349.1	347.7	348.2	
6.5 10.	5.6 23.	5.9	6.3 23.	6.8 10.	
350.0	349.8	349.5	349.1	348.7	
5.0 10.	5.2 23.	5.5	5.9 23.	6.3 10.	

355.04

		Lt		Rt.
750		352.8	352.0	351.9
		$\frac{5.5}{40}$	$\frac{4.3}{23}$	$\frac{4.1}{23}$
		351.7	351.6	351.5
36		$\frac{4.6}{40}$	$\frac{4.7}{23}$	$\frac{4.8}{23}$
		351.1	350.9	351.0
750		$\frac{5.2}{40}$	$\frac{5.4}{23}$	$\frac{5.3}{23}$
		350.5	350.1	350.1
35		$\frac{5.8}{40}$	$\frac{6.2}{23}$	$\frac{6.2}{23}$
		349.6	349.7	349.7
750		$\frac{6.7}{40}$	$\frac{6.6}{23}$	$\frac{6.6}{23}$
		349.0	349.1	349.8
34		$\frac{7.2}{40}$	$\frac{7.2}{23}$	$\frac{7.5}{23}$
		356.29		356.29

H 312 7 9

150

39

150

38

= Prep Cultured

150

37

35629

17

352.4

39  
40

352.1

42  
40

351.1

52  
40

350.7

56  
40

351.9

44  
40

353.2

31  
40

18

352.4

39  
40

351.9

44  
40

351.3

50  
40

350.9

54  
40

352.1

42  
40

352.4

39  
40

35629

19

352.7

36  
40

352.1

42  
40

351.9

44  
40

351.8

45  
40

351.9

44  
40

351.9

44  
40

42

✓

352.2

41  
40

351.9

44  
40

351.6

49  
40

351.7

46  
40

352.5

38  
40

352.8

35  
40

TP on Pot 46 9.45 362.57 3.17 353.12

356.29

H: 307 29

H: 1. 367 17



40

+50

2.9	353.4	353.2	353.1	353.4	353.0
40	23	23	23	23	23

356.29

41

+50

2.2	354.1	353.9	353.8	353.7	354.1
40	23	23	23	23	23

42

+50

2.8	354.8	355.1	354.7	354.3	354.4
40	23	23	23	23	23

2.4	356.4	356.3	356.4	356.6	355.8
40	23	23	23	23	23

2.1	357.2	357.1	357.5	357.3	357.3
40	23	23	23	23	23

2.7	358.8	358.8	358.6	357.8	357.4
40	23	23	23	23	23

317  
353.45  
353.17

+50

44	356.9	356.7	355.8	355.2	R1
40	5.7	5.9	6.8	7.4	7.7
	23	23		23	40

45

	358.2	358.1	356.4	356.0	355.5
40	4.4	4.5	6.2	6.6	7.1
	23	23		23	40

+50

	358.6	358.1	356.9	356.3	356.0
40	4.0	4.5	5.7	6.2	6.6
	23	23		23	40

44

	358.5	358.1	357.30	356.4	355.7
40	4.1	3.8	5.27	6.2	6.9
	23	23	09/200	23	40

+50

	358.6	358.2	357.6	356.9	356.0
40	4.0	4.4	5.0	5.7	6.6
	23	23		23	40

43

	359.5	358.1	357.4	356.5	356.1
40	3.1	4.5	5.2	6.1	6.5
	23	23		23	40

362.57

362.57

✓

750

48

750

47

750

TP 1.74 357.60 6.71 355.86

46

362.57

357.60

\*

77 40	351.7	79 28	349.7	70	350.6	82 28	349.4	84 40	349.2
59 40	352.5	64 28	352.4	65	353.0	70 28	351.6	71 40	351.6
62 40	354.4	67 28	353.9	69	353.7	47 28	352.9	50 40	352.3
70 40	355.6	73 28	355.3	78	354.8	40 28	353.6	45 40	353.1
59 40	356.7	65 28	356.1	75	355.1	82 28	354.4	87 40	353.9

362.57



49

357.60

7.50 P.O.T.

50

TP 0.70 347.17 11.13 346.47

7.50

50 + 85.77 B.C.H.

51

357.60

↑

347.17

8.8

348.8

9.7

347.9

11.6

346.1

5.0

344.2

5.0

341.9

5.0

341.4

41

8.9

348.7

10.2

347.4

11.5

346.1

8.1

344.1

5.0

342.2

5.0

341.9

8.9

348.7

10.38

347.9

11.9

345.7

347.17

17.8

343.39

5.0

341.9

4

9.1

348.5

10.2

347.4

12.0

345.6

8.1

344.1

5.0

341.9

5.0

341.5

9.5

348.1

10.1

347.5

12.1

345.5

5.0

344.0

5.0

342.2

5.0

342.0

41

TP 0.45 335.75 11.87 335.30

54

+ 50

53

+ 50

52

51450

34717



41	528.5	330.4	332.2	334.2	335.8
50.2	331.1	332.5	332.7	335.9	338.0
16.1	332.3	334.0	334.9	336.1	338.9
50.9	335.3	336.9	338.2	338.2	338.9
11.9	337.6	339.0	340.1	341.1	341.6
9.6	339.1	340.1	341.1	342.4	
6.1	341.1	342.4			

34717

34717

+93 Prop Culvert 18"

+50  
IP 0.18 324.04 11.89 323.86

56

+50

55

54150  
325.75

324.04

335.75

4	5	6	7	8	9
55.0	55.0	55.0	55.0	55.0	55.0
316.3	317.5	318.2	319.2	319.9	320.5
57.7	60.5	65.8	48.3	41.5	38.5
319.5	321.1	323.0	324.7	326.0	326.6
58.6	61.7	62.8	61.1	59.8	58.8
320.5	321.5	324.4	326.6	328.5	328.5
55.3	54.0	54.4	52.2	50.5	49.5
323.6	324.5	326.4	328.6	329.6	329.6
62.2	61.5	61.4	62.2	62.2	62.2
327.0	327.6	329.4	331.3	332.7	332.7
60.8	60.2	61.1	61.5	61.5	61.5



325.75

750

59

750

TP 4.06 325.33 2.77 321.27

58

750

57+10

324.04

321.33

324.04

41 4 191

3/3.7 3/14.0 3/15.0 3/16.3 3/17.0

11.6 11.3 10.3 10.0 8.2  
50. 23. 23. 28. 50.0

3/17.1 3/19.2 3/20.3 3/20.4 3/21.1

7.2 6.1 5.0 4.9 4.2  
50. 23. 23. 23. 50.0

3/19.6 3/21.5 3/22.9 3/23.9 3/24.5

5.7 5.8 4.4 4.4 5.8  
50. 23. 23. 23. 50.0

9.0 6.1 6.8 1.1 5.0  
50. 23. 23. 23. 50.0

3/11.2 3/14.5 3/16.4 3/19.1 3/21.1

12.8 9.5 7.6 4.9 2.9  
50. 23. 23. 23. 50.0

3/10.5 3/11.9 3/13.3 3/15.1 3/16.5

13.6 12.1 10.7 8.9 7.5  
50. 23. 23. 23. 50.0

324.04

62

TP 12.84 331.43 0.90 318.59

~~331.43~~

~~X~~

+50

50.8	50.8	50.8	50.8	50.8
12.6	11.5	10.6	10.1	10.8
312.3	319.9	320.8	321.3	320.6
312.3	315.2	331.43	316.5	316.0
50.8	50.8	50.8	50.8	50.8

61

+70 Prop Cukert

~~319.49~~

~~325.33~~

+50

TP 5.56 319.49 11.40 313.93

50.8	50.8	50.8	50.8	50.8
15.2	10.5	8.9	7.8	8.1
304.3	309.0	310.6	311.7	310.9
304.3	305.5	305.4	306.4	307.4
50.8	50.8	50.8	50.8	50.8
15.3	14.1	13.0	10.6	8.5
304.2	305.4	306.5	308.9	311.0
304.2	305.5	306.5	308.9	311.0
50.8	50.8	50.8	50.8	50.8

60

325.33

319.5  
319.5  
319.5

325.33

62+50

9.6  
50

8.1  
23

7.5

7.1  
23

4.9  
50

321.8  
50

323.3  
23

323.9

324.3  
23

326.5  
50

63

325.4  
50

325.2  
23

325.7

326.0  
23

327.6  
50

+50

5.5  
50

5.0  
23

2.7

2.1  
23

2.4  
50

64

325.9  
50

316.4  
23

328.7

329.3  
23

329.0  
50

+50

326.7  
50

328.8  
23

328.5

327.5  
23

328.6  
50

65

326.3  
50

328.6  
23

328.1

328.6  
23

329.8  
50

327.2  
50

328.1  
23

328.4

329.0  
23

329.3  
50

44

48

41

11 ✓

331.43

331.43

68

+50

67

+50

66

TP 07 Nov 10.26 339.04 2.65 328.78  
65+40.39 FC

65+40.39 F.C.

331.43

41

332.2  
6.8  
40

331.3  
7.7  
40

330.4

8.6  
40

329.7  
9.3  
40

329.1

10.0  
40

327.9

3.5  
50

332.9  
6.1  
23

332.2  
6.8  
23

331.0

8.0  
23

330.6  
8.4  
23

329.1

9.9  
23

328.4

3.0  
23

21

333.9  
5.1  
40

332.5  
4.5  
23

331.9

7.1  
23

331.2  
7.8  
23

329.9

9.1  
23

329.0

3.85  
07 Nov 23  
331.43

17

334.5  
4.5  
23

333.8  
5.2  
23

332.6

6.4  
23

331.5  
7.5  
23

330.8

8.2  
23

329.0

2.1  
50

71  
TP 786 3.4427 2.63 336.41

+50

70

+50

69

68+50

339.04

FreeBentor 58	4.0 40	4.2 23	3.0 30	2.4 23	1.6 40
	335.0	334.8	336.0	336.6	337.7
	8.5 40	7.0 23	7.0 40	6.0 23	6.5 40
	336.8	337.3	337.3	338.3	339.2
	5.8 40	4.2 23	3.9 30	3.0 23	2.2 40
	332.9	334.7	335.1	336.0	336.8
	6.1 40	4.5 23	4.5 30	4.4 23	4.1 40
	331.9	334.5	334.5	334.6	334.9
	7.1 40	6.0 23	5.5 30	4.7 23	3.8 40
	331.7	333.0	333.5	334.3	335.2
	7.0 40	6.9 23	4.7 30	4.6 23	4.4 40
	331.7	332.1	334.3	334.4	334.6
	339.04				



BM 4.75 34478 4.24 340.03

Spt 15 Power  
Pole 100' Pt  
70+50

74

+50

73

+50

72

71+50

34427

339.5	339.4	340.3	340.3	339.5
48 10	49 23	40	40 23	48 10
339.7	339.6	339.4	341.4	339.7
46 10	47 23	49	49 23	46 10
338.8	340.2	339.7 ✓	339.7	341.2
45 10	41 23	46	46 23	45 10
339.2	339.3	339.6	339.6	339.2
45 10	45 23	47 23	47 23	45 10
336.9	337.5	339.3	339.5	339.3
74 10	65 23	50	48 23	50 10
336.8	336.8	338.6	339.3	339.1
75 10	75 23	57	50 23	51 10

34127

77

+50

TP 2.55 334.53 12.80 337.98

76

+60 Power Pole 18 1/2

+50

75

74150

34478

5-26-33

41

4

R1

333.2	329.0	325.2	321.8	315.8
12 50 NY Edge Pro.	5.5 23	9.3	12.6 23	18.7 50
334.2	331.3	329.1	326.7	322.5
50 23	5.0 23	5.4	7.8 23	12.0 50
335.4	334.3	332.8	331.2	328.9
9.4 50	10.5 23	12.0	13.6 23	15.9 50
336.9	336.7	335.7	334.7	332.6
7.9 50	8.1 23	9.1	10.1 23	12.2 50
338.0	338.4	338.3	337.4	336.3
6.8 10	6.4 23	6.5	7.4 23	8.5 50
339.2	338.8	339.0	339.7	340.0
5.6 20	6.0 23	5.8	5.1 23	4.8 20

34478

+50

79

+50

TP 11.77  
1101 Parker Palm  
394277+94 346.10 0.20 334.83

78

+84 Parker Palm 394277

+59.55 BC. Pt.

77+10 - Prop. Culture 18"  
334.53

11	65 40	339.6	338.0	335.8	10.3 40	334.0	333.0	331.0	15 20
21	65 20	340.0	338.2	336.1	10.0 20	333.5	332.5	328.7	15 20
31	60	340.1	339.5	336.8	9.3	332.5	332.1	329.07	15.16 20
41	65 20	340.3	338.2	335.9	10.2 20	332.1	332.1	328.0	15 20
51	65 40	340.4	338.2	335.5	10.6 40	332.3	332.3	328.0	15 20
61	65 20	340.0	338.2	336.1	10.0 20	333.5	332.5	328.0	15 20
71	65 20	340.0	338.2	336.1	10.0 20	333.5	332.5	328.0	15 20
81	65 20	340.0	338.2	336.1	10.0 20	333.5	332.5	328.0	15 20
91	65 20	340.0	338.2	336.1	10.0 20	333.5	332.5	328.0	15 20

334.53

TP 6.13 34990 2.33 343.77

+83 Power Pole 17' W of A

+50

82

+50

81

+50

+35 Power Pole 13' W of A

80

34610

34610

41

42

41

344.0

344.4

342.9

341.9

342.3

21/20

21/30

17/23

32

42/23

32/40

343.3

343.3

344.7

342.9

341.8

341.9

28/20

28/28

14/23

32

43/23

42/40

342.6

342.5

341.6

342.2

342.3

32/40

32/23

45

39/23

38/40

341.9

341.5

340.9

341.3

342.9

42/28

46/23

52

48/23

32/40

341.4

340.9

340.6

341.1

340.5

47/40

52/23

55

50/23

56/40

340.6

340.2

339.9

340.3

339.9

55/40

59/23

62

58/23

62/40

34610

+77 Power Pole 2.5' H of A

+3797 FC

85

+50

84

+50

83

34990

Mount Force  
+5'

41

345.4

4.5  
40'

346.2

3.7  
40'

346.4

3.5  
40'

346.0

3.9  
40'

345.5

4.1  
40'

344.4

5.5  
40'

346.1

3.8  
23'

346.0

3.9  
23'

345.9

4.0  
23'

345.9

4.0  
23'

344.6

5.2  
23'

345.4

4.5  
23'

345.29

4.4  
23' H of A

344.9

5.0

345.5

4.4

345.2

4.7

344.8

5.1

344.5

4.5

344.6

5.3  
23'

344.5

5.4  
23'

343.9

6.0  
23'

344.7

5.2  
23'

344.7

5.9  
23'

344.5

5.4  
23'

344.5

5.1  
40'

344.8

5.1  
40'

342.6

7.3  
40'

343.5

6.6  
40'

342.4

7.5  
40'

344.1

5.8  
40'

34990

+75 Pop. or Pop. 10. R/ of 8

+50

IP 9.67 35756 201 34789

88

+50

87

+50

86

34990

41 81 R1 ✓

3484 3490 3489 3483 3483

92 86 87 92 92  
40 23 23 40 40

3460 3474 3474 3472 3469 3473

29 25 25 27 28 26  
40 23 23 40 40

3454 3466 3464 3469 3476

45 23 25 28 23  
40 23 40

3453 3461 3464 3468 3459

46 28 25 28 40  
40 23 40

3452 3461 3455 3466 3464

47 28 44 28 25  
40 23 40

3453 3459 3457 3460 3452

Marine 46 40 42 29 47  
41 40 23 23 40

34990

+75 Power Pole 4' Pt of 4

+3706 BC Lt

TP 10.82 36818 0.20 25736

91

+50

90

+50

89

257.56

41

358.0

10.2  
40  
Morning  
Pole  
36

356.9

0.7  
40

355.9

17  
40

353.5

4.1  
40

351.2

6.4  
40

350.3

7.2  
40

42

358.0

10.2  
23  
9.92  
674.4.6  
368.18

356.7

0.9  
23

355.2

2.4  
23

353.4

4.2  
23

352.1

5.6  
23

350.4

7.2  
23

257.56

41

358.2

10.9  
23  
10.9

357.4

0.2  
23

355.3

2.3  
23

353.0

4.6  
23

351.6

6.0  
23

350.4

7.2  
23

357.3

10.9  
40

356.3

1.3  
40

354.1

2.6  
40

352.6

5.0  
40

350.9

6.9  
40

350.1

7.5  
40

2

		41		42		41
+50		361.7		362.9		362.5
+18	Power Pole 36 ft of 2	65 40	65 23	4.4	67 23	49 40
+06	Water Meter + Pump 33 ft of 2	362.7	363.5	362.6	363.9	361.8
94		55 40	49 23	56 16	43	61 23
		363.0	363.2	362.2	363.6	363.2
+50		52 40	Fence 27	50 23	60 16	46
		363.3	362.8	361.4	362.7	363.1
93		49 40	64 23	68 16	55	51 23
		360.1	360.9	361.0	363.3	362.2
+50		81 40	73 23	72	49 16	60 23
		358.9	359.5	359.7	358.8	358.5
92		93 40	87 23	85	94 23	97 40
	368.18			368.18		



+58 Temp. Pale on 2

+50

+17 Water Meter 10.19 of 2

97

TP 9.56 377.61 0.13 368.05

+50

96

Marine  
Feet  
38

+50

95

368.18

368.18

367.7	368.5	368.5	370.1	370.6
99 40	91 23	91	75 23	70 40
366.2	367.1	367.4	368.1	368.0
114 40	105 23	102	95 23	96 40
364.5	365.7	377.61	366.2	367.2
37 40	25 35	26 23	24 23	20 40
363.0	364.9	365.6	364.8	364.9
52 40	33 30	32 23	2.1 23	2.4 40
362.3	364.1	364.5	363.7	364.4
59 40	41 30	37 23	2.8 5	4.5 23
362.5	363.5	364.2	363.2	363.6
57 40	Marine Feet 32	47 23	40 5	50 23
				46 40

TP 12.39 388.35 1.65 375.96

99

+93.5 - 2 Road to Marine Rifle Range Taken on 2 Road

+93.5 Telp. Pole 32' Ht of 2

+75 Telp. Pole 10' Ht of 2 35' H. Mission Bell

+50

+20 - Fence Cor 12' Ht. of 2

98+02.08 Taken on 2 Sorrento Road

98+02.08 = 2 Sorrento Road

97+72.36 F.C.

377.61

	Lt			RT
	3741	3740	3740	3755 ✓
	35/40	32/23	32/23	21/23
	366.5	3712	373.7	3753
	111/200	6.4/100	6.9/100	2.3
	3724	372.7	372.2	373.6
	52/40	4.9/23	5.4/34	4.0/23
	3732	372.7	3714	370.2
	14/200	4.9/100	6.2	7.4/100
	3702	3711	3714	3724
	7.4/40	6.5/23	6.2	5.2/23
	3690	3696	37067	3708
	8.5/40	8.0/23	6.94/23	6.8/23
			072406	6.1/40
			377.61	



105

+50

104

TP 12.41 400.20 0.56 387.79

+62 = Telp Pole 1 A. P. 1/4

+50

103

102+50

388.35

H R

3920 3936 3941 3953 3968

82 66 61 49 24  
40 28 20 20 40

3893 3911 3912 3922 3937

10.9 91 90 80 65  
40 23 23 23 40

386.5 3891 3891 3888 389.5

13.7 111 111 114 10.7  
40 23 23 23 40

3859 3876 400.20 386.7 3874

2.5 0.8 0.8 1.7 1.0  
40 23 23 23 40

3845 3859 3860 3849 3861

8.9 25 24 25 22  
40 23 23 23 40

3817 3839 3845 3830 3845

6.7 4.5 3.9 5.1 3.6  
40 23 23 23 40

388.35

+27 = Telp Pole 22' Pt of d

108

+50

+25 = Telp Pole 13' Pt Power Pole 50' Lt of d

107

+50

106 x 03.91 BC Pt

TP 8.79 108.88 0.11 100.09

105 x 50

100.20

Lt

Rt

Pt

402.2

403.1

402.5 ✓

402.0

403.8

403.8

405.0

6.7  
26'

6.8  
28'

6.6  
28'

6.8  
8'

5.1  
12'

5.1  
28'

3.9  
40'

402.0

402.3

401.9

401.9

403.8

404.4

405.0

6.9  
40'

6.6  
28'

7.0

7.0  
3'

5.1  
6.0

4.5  
28'

Power 3.9  
25'

4.0

401.5

401.4

401.3

402.4

403.5

404.7

7.1  
40'

7.5  
28'

7.6

6.5  
4'

Angle  
Force  
19'

5.4  
28'

4.2  
40'

398.9

399.6

399.3

400.7

403.1

405.1

100  
40'

9.3  
28'

9.6  
3'

8.2

5.8  
28'

3.8  
40'

396.6

397.9

397.8

398.8 ✓

400.7

402.9

12.3  
40'

11.0  
28'

11.1  
5'

10.1

Force 8.2  
17'

2.8  
28'

6.0  
40'

394.1

395.5

402.88

398.1

400.2

6.1  
40'

4.7  
28'

3.9

Telp  
Power  
15'

2.1  
28'

2.0  
40'

400.20

B.M. <sup>Mag</sup> 10371 288151 Torrey Mesa Lab. 2.20' 410.88 409.66 ✓ 409.60 should be 409.69

TP 6.13 413.08 7.53 406.95

TP 11.51 408.48 11.91 396.97

C.T.S. Bound  
Rose Canyon

109+59.34 Fly Edge Point Rose Canyon

+42 = Top Pole 25 ft of L

+22 = Power Pole 25 ft of L

+16.94 FC

109

108+50

408.88

4	4	4	4	4	4
396.10	396.36	396.73	397.08	397.31	
12.78 10'	12.52 23'	12.15	11.80 23'	11.57 10'	
397.6	398.8	399.2	399.0	400.2	
11.3 10'	10.1 23'	9.7	9.9 12'	8.7 23'	Fence Cap. 38'
398.5	399.6	399.8	399.6	401.2	
10.4 10'	9.3 23'	9.0	9.3 10'	7.7 18'	7.7 23'
400.9	401.7	401.6	401.2	403.7	402.8
8.0 10'	7.2 23'	7.3	7.7 12'	6.2 17'	6.1 23'
		408.88			5.8 10'

Miramar Road  
Check Levels

63  
5-26-33

TP 2.375 326.03 6.685 323.655

TP 12.543 360.523 2.21 347.98

TP 0.283 330.34 12.66 330.057

0.7 E.C. Hub  
85+87.97 4.96 345.23 (345.29)

TP 0.405 342.717 10.30 342.312 342.39  
on % Hub 50+85.7780

TP 4.62 350.19 1.707 345.57

TP 0.817 352.612 8.495 351.795

TP 8.457 347.277 0.63 338.82

TP 3.033 360.29 5.31 357.257

TP 1.685 339.45 6.49 337.765

TP 9.52 362.567 3.26 353.047 353.12  
on % Hub 50+10

BM 4.335 344.255 1.45 339.92 (340.03)  
S.P.A. Point Polt  
100' W 71+50

TP 5.22 356.307 2.385 351.087

TP 8.195 341.37 0.765 333.175

TP 4.047 353.472 7.01 349.425

on % Hub 65+40.39 EC 5.26 328.68 (328.72)

TP 3.470 356.435 5.852 352.965

TP 8.74 333.94 0.83 352.20

BM 3.237 358.817 355.58  
on % Hub 40+710 Hub  
H. 22+15.85 EC

326.03

BM Moz  
103 W 388 + 51  
Torrey Mts. Feb

1.10' W. W. E. V.

2.00

410.79

(410.88)

(409.69)

TP 8.84 412.79 4.155 403.95

TP 11.235 408.105 8.067 396.87

on C.T. S. Board  
Rose Canyon

TP 12.495 404.537 0.173 399.442

TP 12.85 392.615 0.196 379.765

TP 11.993 379.961 0.427 367.968

TP 8.135 368.395 0.263 360.26

075 H. 44  
911-3706 B.C. H.

2.243

358.28

358.28

260.522



Levels on paving & culverts  
STATE & Fish

SWBP 11.74 42.16 30.45 Col. & Fish

100' Soft Fish

W cb 42.16 / 5.32 36.84 ✓

W gut 5.82 36.34 ✓

1/4 4.83 37.33 ✓

C 4.25 37.81 ✓

1/4 4.19 37.97 ✓

E gut 4.41 37.75 ✓

E cb 5.67 38.49 ✓

85' S

E cb 5.85 38.31 ✓

E gut 4.52 37.64 ✓

W gut 5.85 36.31 ✓

W cb 5.27 36.89 ✓

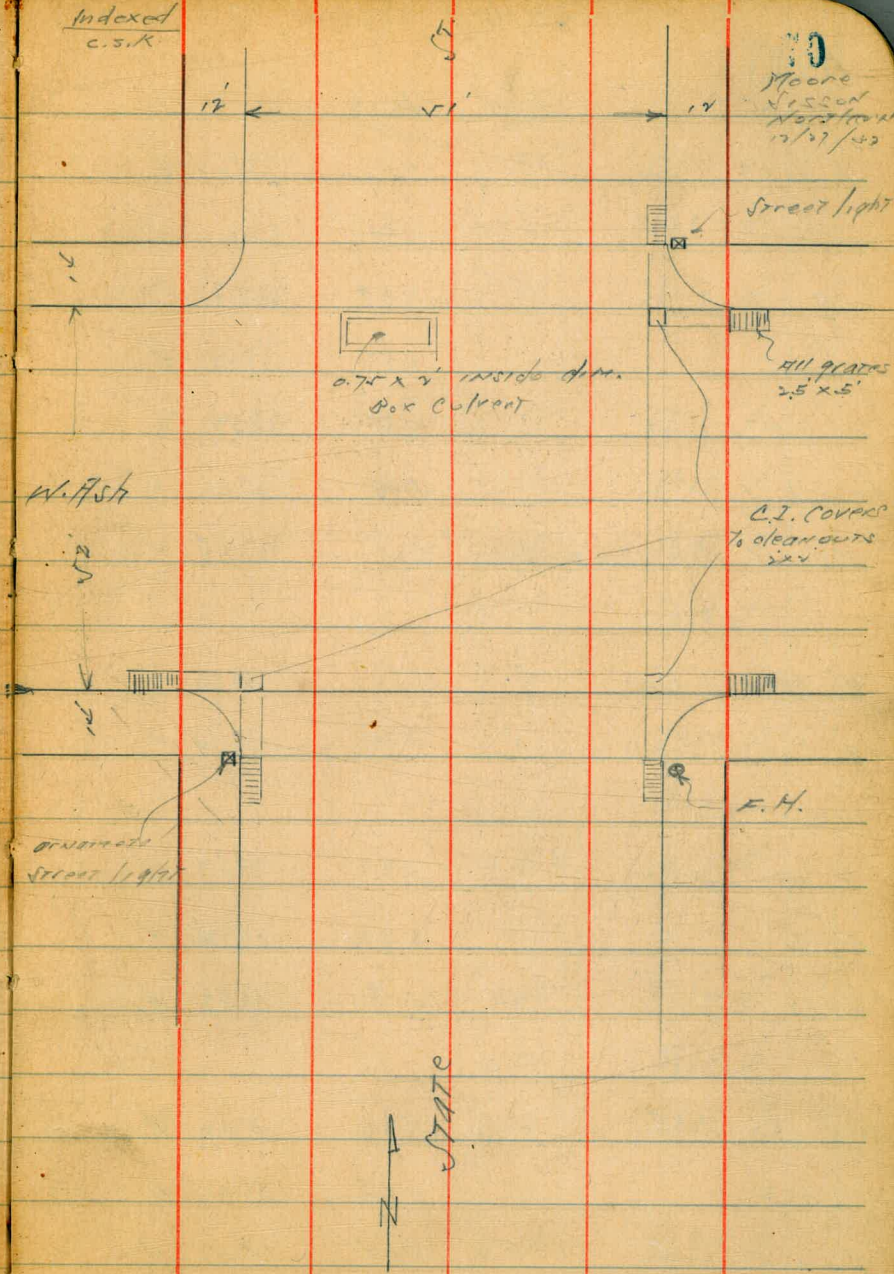
83' S

W gut in drive 5.80 36.36 ✓

E gut 4.59 37.57 ✓

E cb 3.88 38.28 ✓

Indexed  
C.S.K.



10  
Moore  
Paved  
Water Main  
12/27/43

0.75 x 4' inside diam.  
Box Culvert

Street Light

Hill grade  
2.5 x 5'

C.I. Covers  
7/8 cleanouts  
2x2

W. Fish

Grass  
Street Light

F.H.

N  
STATE

42.16

N'S	42.16		
E gut in drive	4.66	3750	✓
1/2	4.85	3771	✓
C	4.69	3747	✓
1/2	4.94	3744	✓
W gut in drive	5.84	3634	✓
cb + 4	5.15	3701	✓
W.L. & exact stop entrance	5.01	3715	✓
67'S			
W gut in drive	5.86	3630	✓
E " " "	5.74	3744	✓
66'S			
E gut in drive	4.73	3743	✓
W "	5.94	3624	✓
" cb top	5.17	3699	✓
57'S			
W cb	5.16	3700	✓
W gut	6.05	3611	✓
E " drive	5.13	3703	✓

42.16

71.71

W'S	42.16		
E cb top	4.55	3761	✓
" gut	5.20	3696	✓
W gut drive	5.99	3617	✓
W'S			
W.L. & entrance to <sup>lower</sup> point <sup>top</sup>	4.89	3727	✓
+ 8	5.11	3705	✓
W gut drive	6.07	3609	✓
1/2	5.49	3667	✓
C	5.40	3676	✓
1/2	5.04	3714	✓
E gut	5.27	3689	✓
E cb	4.63	3753	✓
16'S			
E cb	4.66	3750	✓
gut	5.31	3685	✓
W gut drive	6.10	3606	✓
14'S			
W cb	5.11	3695	✓
gut	6.22	3594	✓

42.16

E gut	42.16 5.39	36.77	✓
ob	4.68	37.48	✓
S/S - Sedge grate			
E ob	4.76	37.40	✓
gut top grate inlet	5.54	36.61	✓
+2.5 " "	5.51	36.65	✓
1/4	4.99	37.17	✓
c	5.26	36.90	✓
1/4	5.54	36.61	✓
+10.25 grate inlet	6.19	35.97	✓
w gut on grate	6.21	35.95	✓
ob	5.14	37.02	✓
S/L 1004			
w/l cor return	4.86	37.30	✓
w ob	5.11	37.05	✓
" gut grate	5.79	36.37	✓
" FL. Culvert inlet	6.75	35.41	✓
1/4	5.23	36.73	✓
c	5.16	37.00	✓
1/4	4.95	37.21	✓

42.16

E top grate	42.16 4.55	37.61	✓
E FL. Culvert inlet	5.75	36.38	✓
E top ob	4.77	37.39	✓
E.L.	4.49	37.67	✓
S ob 1756			
E ob STATE top clearout cover	4.79	37.37	✓
" " FL. " Junction	6.15	36.01	✓
E 1/4	4.72	37.44	✓
c	4.80	37.36	✓
1/4	5.11	37.05	✓
w ob. line ASB top clearout cover	5.62	36.54	✓
" " FL. Culvert Junction	6.91	35.15	✓
S 1/4 ASB			
w ob STATE	5.72	37.04	✓
1/4	4.82	37.33	✓
c	4.59	37.57	✓
1/4	4.39	37.77	✓
E ob	4.04	37.82	✓
S ASB			
E ct STATE	4.85	38.31	✓

73

4216

2 1/4	4.08	3808	✓
C	4.27	3789	✓
1/4	4.39	3777	✓
W of stage	4.52	3761	✓
N 1/4 ash			
W of	4.23	3793	✓
1/4	4.10	38.06	✓
C	4.29	38.27	✓
1/4	4.74	38.44	✓
E of	3.24	38.72	✓
N of ash			
E of Top clear out Corer	3.09	39.07	✓
" " F.L. " Junction	4.45	3771	✓
1/4	4.36	3880	✓
C	3.51	3865	✓
1/4	4.78	38.38	✓
W of	4.14	38.02	✓
N of ash			
W of top	3.64	3852	✓
gut	4.15	3801	✓

4216

1/4	3.22	3874	✓ 70
C	3.21	38.95	✓
1/4	2.97	39.19	✓
E of Top grate	2.74	38.42	✓
" FL Culvert inlet	3.94	38.22	✓
" Top of	2.74	39.22	✓
5' N of N of ash			
E of	2.69	39.27	✓
E gut Top grate	3.46	38.90	✓
1/4	2.91	39.25	✓
C	3.07	39.09	✓
1/4	3.00	38.86	✓
W. gut	4.08	38.08	✓
W of	3.60	38.56	✓
25' N of N			
W of	3.25	38.91	✓
gut	3.74	38.24	✓
1/4	2.90	39.26	✓ 2.74
C	2.75	39.21	✓
1/4	2.70	39.21	✓

42.16

E gut	42.16 2.12	3904	✓
E ob	2.42	3974	✓
40' N of HL gate			
E ob	2.19	3997	✓
gut	2.87	3929	✓
1/4	2.46	3970	✓
C	2.57	3959	✓
1/4	2.68	3948	✓
W gut	2.50	3866	✓
W ob	2.02	3914	✓
FL STATE			
N ob top grate	2.75	3941	✓
" " FL Culvert inlet	2.97	3819	✓
1/4	3.22	3894	✓
C	3.70	3846	✓
1/4	4.27	3789	✓
S ob FL Cul. inlet	6.0	3616	✓
" top ob & grate	4.85	3731	✓
S'E of FL STATE			
S ob	4.75	3741	✓

42.16

gut & grate	42.16 5.40	3676	✓
S 1/4	4.18	3798	✓
C	2.57	3859	✓
1/4	2.24	3892	✓
N gut & grate	3.62	3852	✓
N ob	2.73	3923	✓
S'E of FL STATE			
N ob	2.58	3958	✓
gut	3.41	3875	✓
1/4	2.11	3905	✓
C	2.22	3894	✓
1/4	2.84	3834	✓
S gut	4.75	3741	✓
S ob	4.26	3790	✓
S'E			
S gut & drive	4.66	3750	✓
N "	2.38	3878	✓
" ob	2.56	3960	✓
S'E of FL STATE			
N ob	2.50	3966	✓

42.16

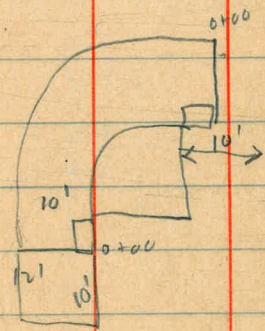
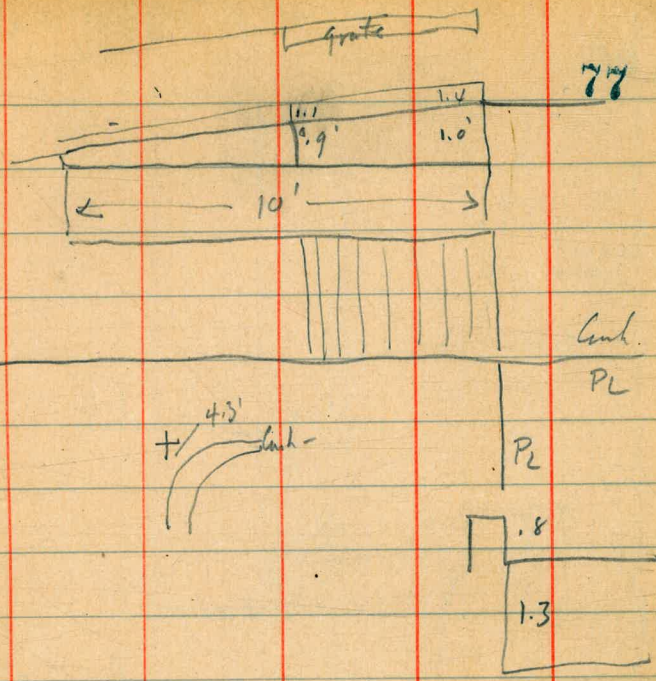
	42.16		
N. gut	5.31	38.85	✓
1/2	2.92	39.22	✓
c	3.05	39.11	✓
1/2	4.53	38.63	✓
S gut & drive	4.38	37.78	✓
10' W of W.L. State			
S cb	5.00	37.16	✓
S gut & grate	5.66	36.50	✓
S FL outlet to Col.	7.01	35.15	✓
1/2	5.29	36.87	✓
c	4.70	37.46	✓
1/2	4.46	37.70	✓
N gut	4.29	37.77	✓
N cb	3.55	38.61	✓
25' W of W.L. State			
N cb	3.72	38.42	✓
gut	4.47	37.69	✓
1/2	4.51	37.65	✓
c	4.71	37.45	✓
1/2	5.29	36.87	✓

42.16

	42.16		
S 1/2 + 11.5' top of wing wall	6.10	36.06	✓
S gut FL culvert	7.12	35.02	✓
S Top grate	6.19	35.97	✓
S top cb	5.12	37.04	✓
10' W of W.L. State			
S top cb	5.33	36.83	✓
S gut	7.17	34.99	✓
N cb + 2.5' end Culv. Apron	7.14	35.02	✓
1/2	5.22	36.62	✓
c	4.93	37.43	✓
1/2	4.66	37.50	✓
gut	4.69	37.47	✓
N cb	4.92	38.22	✓
25' W of W.L. State			
N cb	4.32	37.82	✓
gut	5.02	37.12	✓
1/2	5.03	37.13	✓
c	5.29	36.87	✓
1/2	6.01	36.15	✓
S gut	7.17	34.99	✓

4216

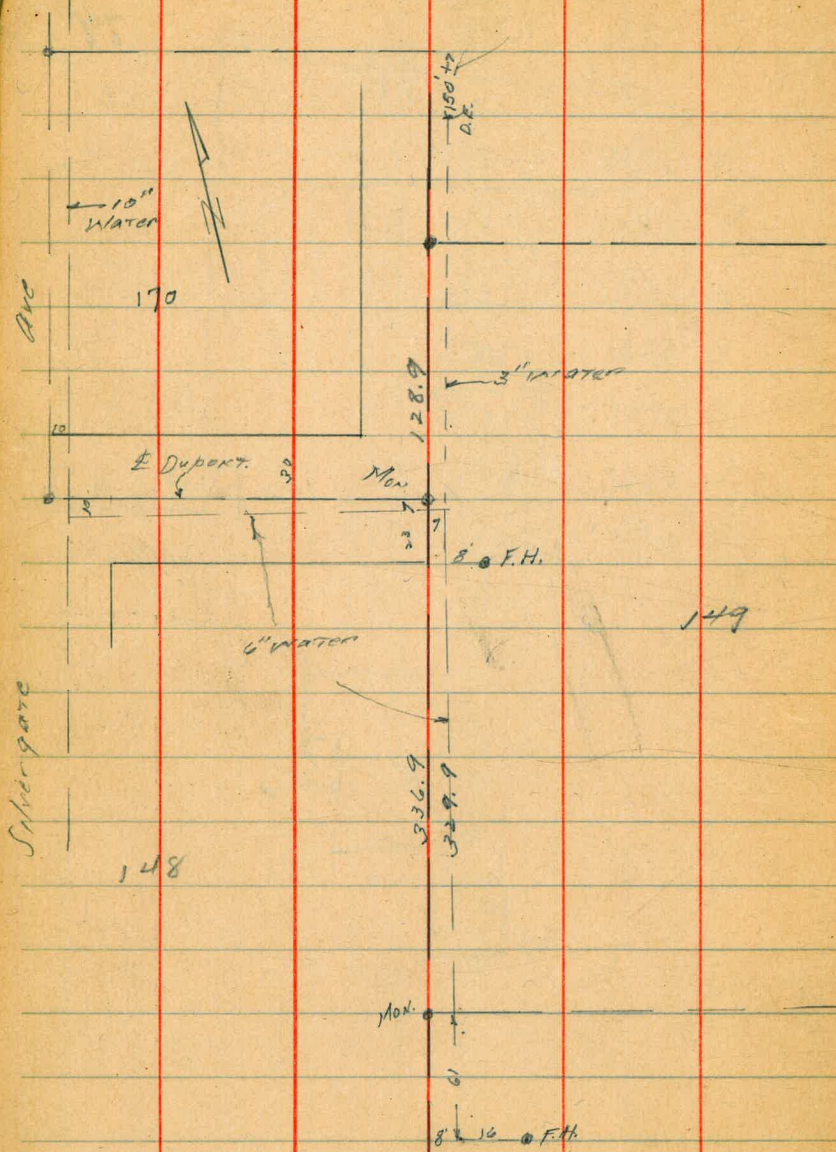
S ct	42.16	3631	✓
	5.85		
40' W of W/L STATE			
S Top ct	6.30	3586	✓
907	7.02	3484	✓
1/2	6.20	3574	✓
c	5.68	3648	✓
1/4	5.38	3678	✓
907	5.49	3667	✓
✓ ct	4.75	3741	✓



Location of 6" water line

Moore  
1-5-38

Indexed  
C.S.K.



Ave

Silvergore

170

149

178

141



P.L. 1311

1-14-50 Survey Proposed Lease

Moore

Begg Torrey Pines Drive LN

Sherridan

Crawford Torrey Pines Road, 101 Highway

and Miramar Rd. Junction

INDEXED

WK

JAN 23 1950

= Ed. Ld. CT.

○ = Set City disk

□ = " " Cor. Men. Standard Brass Tablet

□ = " " 2"x2" RW Hub & disk

Ref Bks, 1424-24

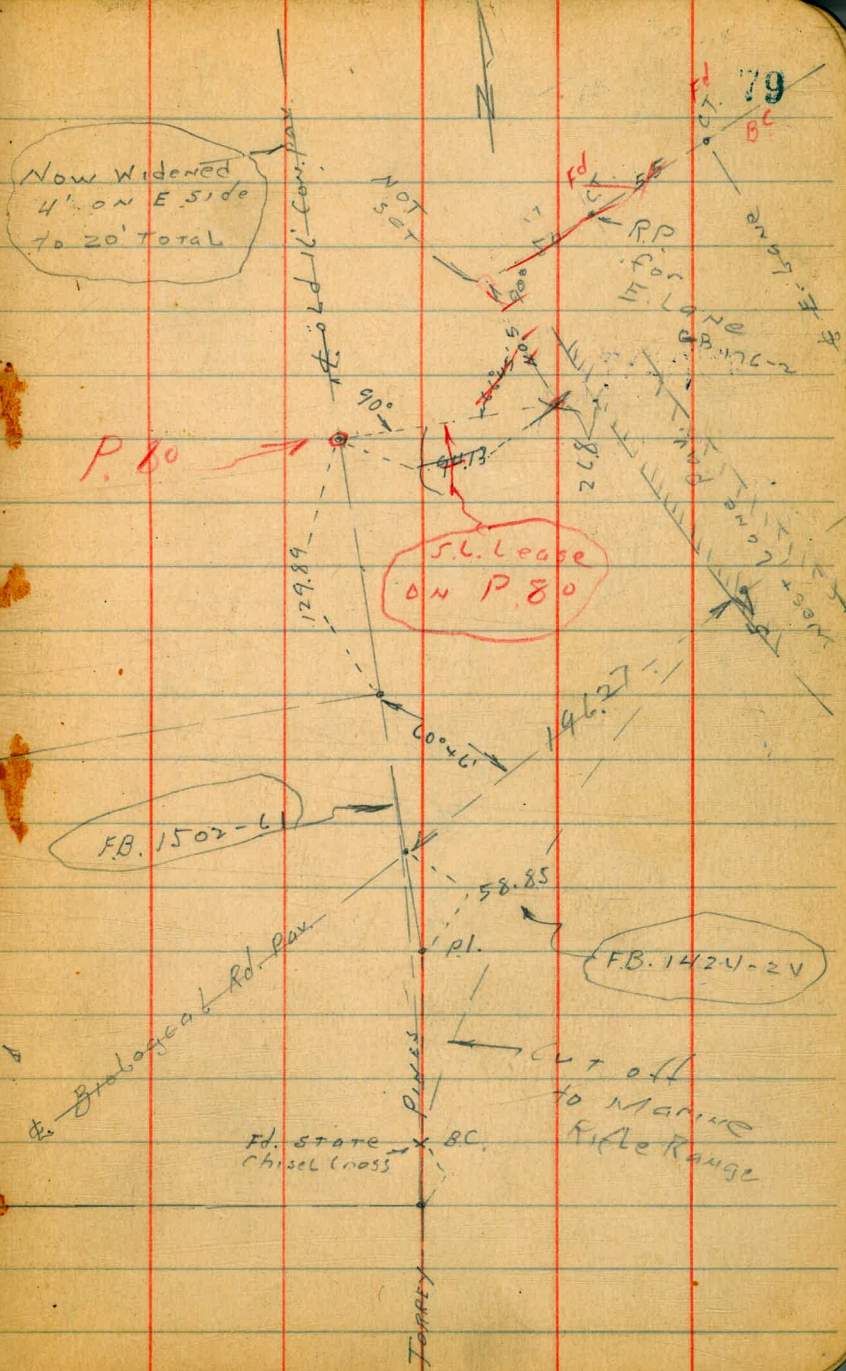
1675-26

1149-74

1502-61

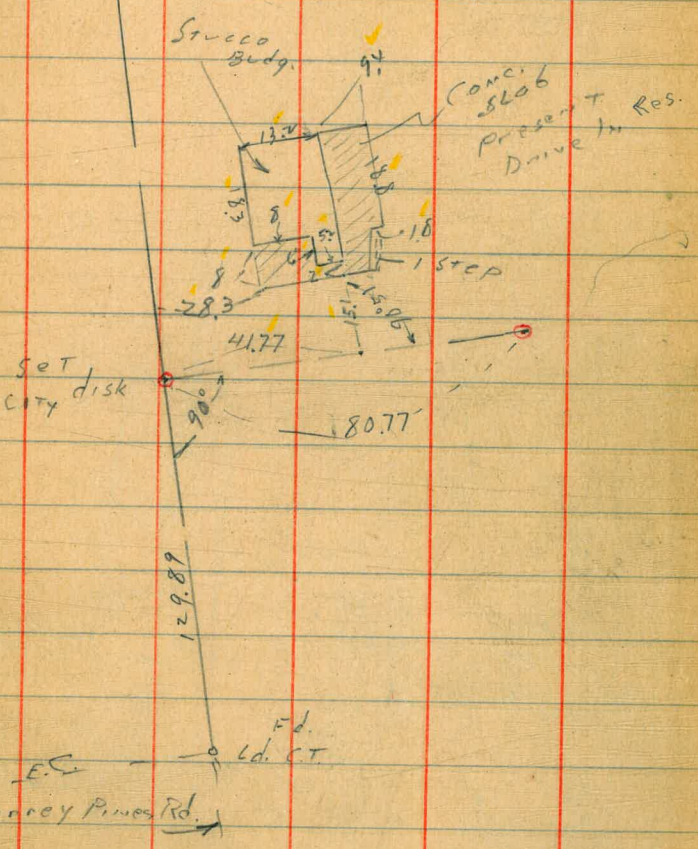
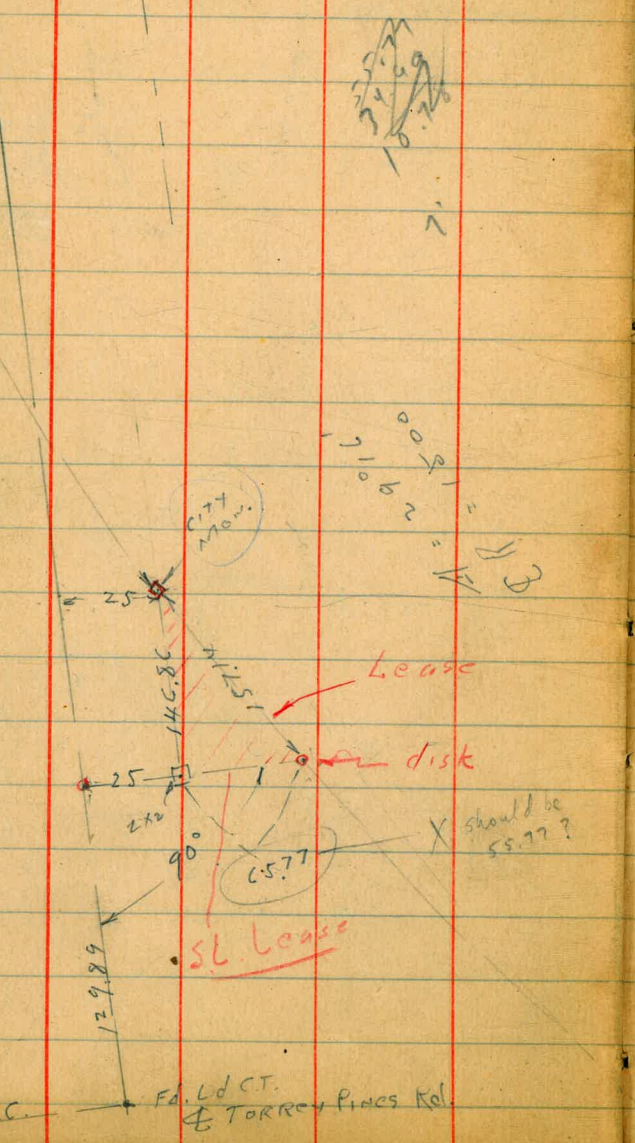
Gr. Bk 17C-2

W/O, 20006



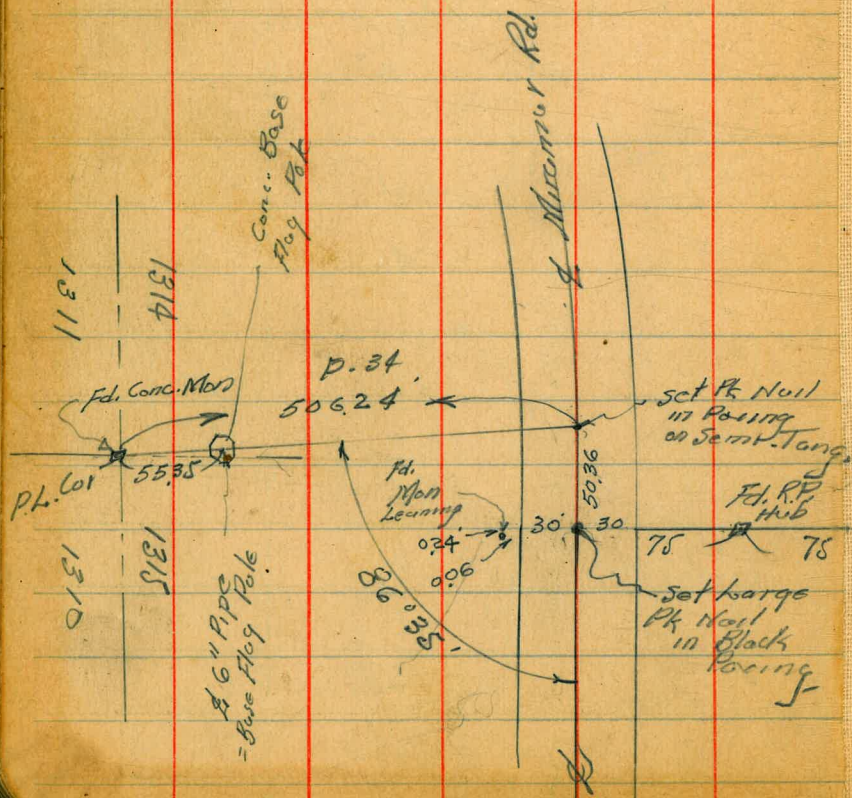
50  
53  
v.c. 61  
Fd. State Ld C.T.  
E.C. ON  
East Lane

T.B. J. 1033-10  
R 1550  
48.84



81 Ties To Pts. Cor. 1310, 1311, 1314, 1315

Walker  
Pope  
H-Hinson  
6-17-52



good Conditions  
F.d. R.P. Hub.  
91437.06

64153  
 48439  
 15714

8077  
 25  
 65.77

23.1  
 129.89  
 126.78  
 279.17  
 12  
 267.17  
 279.17  
 58.85  
 220.32  
 12  
 208.32

25  
 7  
 32  
 14  
 18

10  
 5.33  
 4.67

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.