

1453

MICROFILMED

JAN 25 1965

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

33.5
16.5
0.8
0.1
7.0
0.6
5.92
5.66

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
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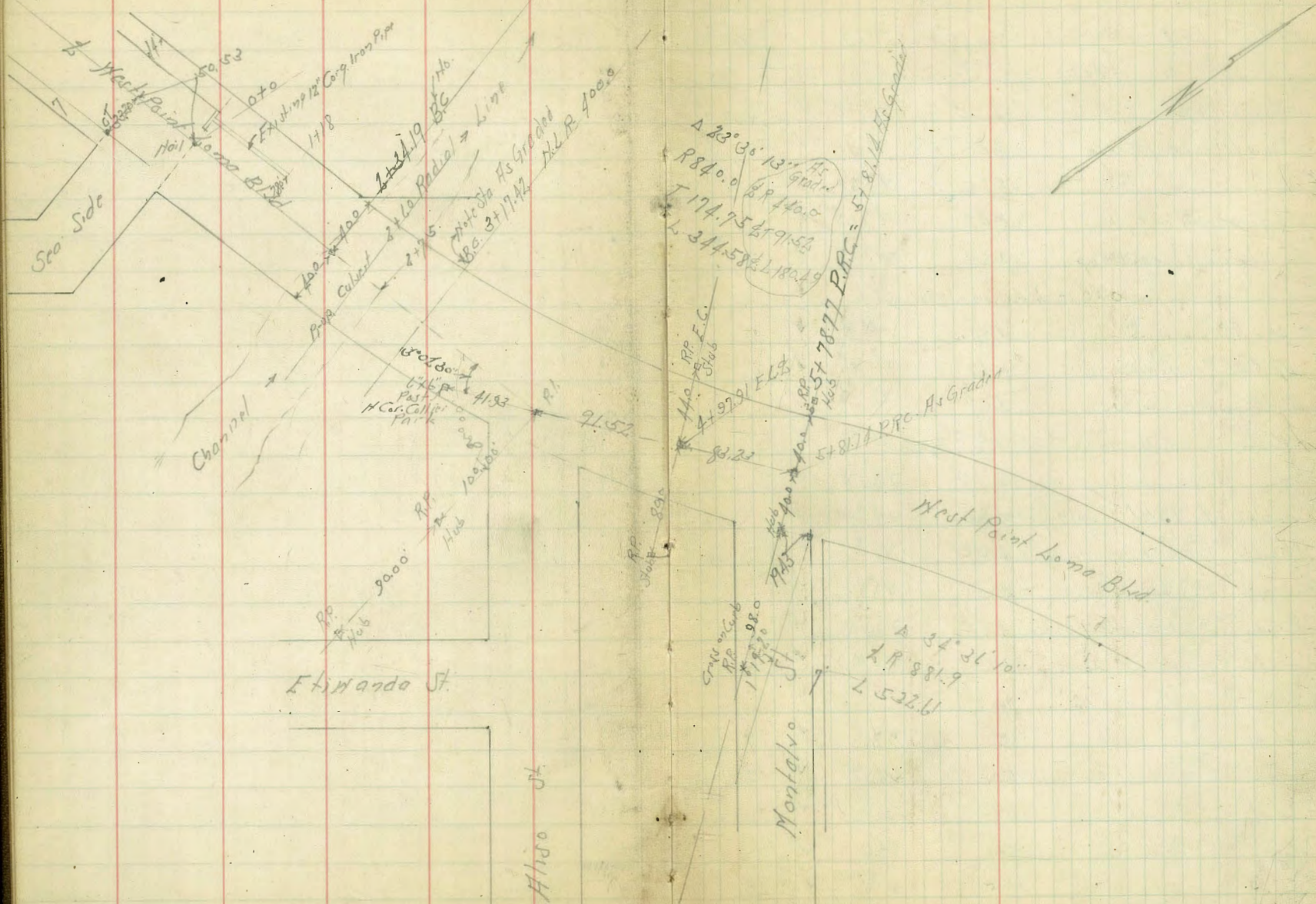
West Point Loma Blvd.		1-14
Alley 21 Kimball Add.	²⁵⁻²⁶ IYJ	15-20
Robinson Ave Bridge		21-26
Buchanan Ave.		27-39
Kettner Blvd.		40-46
Kalmia		47.
Russ Blvd.		48-66
Adams Ave		67-72
Marilou Park		73-74
Police Target Range		75-79
		80-

West Point Loma Blvd.
Sea Side to Montalvo

Intact
C.S.K.

3-20-33
Moore
Jesse
Holburn

2



West Point Loma Blvd.
Cross Sections
Seaside to Menlo Park

80 ft

29.55 ~~29.6~~

2-21-33

3

BM. 193 29.55 29.55 27.62
0 - 50.53 = W.L. Seaside

H Cb Top	2.15	✓ 17.40	✓
Gutter on paving	2.81	✓ 16.74	✓
" " "	2.25	✓ 17.30	✓
S Cb Gutter	2.40	✓ 17.15	✓
+24 = Existing Cb Top	1.69	✓ 17.86	✓
0+0 = E.L. Seaside			
40' Pt	2.8	✓ 16.8	✓
284' Pt Existing Cb	3.49	✓ 16.06	✓
284' Pt Gutter on paving	4.07	✓ 15.18	✓
26' Pt	4.05	✓ 15.50	✓
" " "	3.77	✓ 15.78	✓
23' Lt = 1/2 Inlet C' Opening	4.65	✓ 14.90	✓
26' Lt Gutter on paving	4.72	✓ 14.83	✓
26' Lt Top Cb	4.02	✓ 15.53	✓
39' Lt = 1/2 Foot Bridge on Deck	3.85	✓ 15.70	✓
40' Lt	3.6	✓ 16.0	✓
0+10			
40' Lt	5.0	✓ 14.6	✓
33' Lt = 1/2 Foot Bridge on Deck	5.02	✓ 14.53	✓
23' Lt	5.4	✓ 14.2	✓
" " "	4.6	✓ 15.0	✓
23' Pt	4.5	✓ 15.1	✓
26' Pt = End Ex 4' 10" 20' Foot Cb	4.51	✓ 15.04	✓

Spk. N.Y.
W. Point Loma
Seaside
1237-Prop

40' Pt			
45' Pt			
0+25			
45' Pt			
40' Pt			
23' Pt			
" " "			
23' Lt			
31' Lt = 1/2 Foot Bridge on Deck			
35' Lt			
40' Lt			
50' Lt			
TP	1.70	18.335	12.915
0+50			
50' Lt			
40' Lt			
35' Lt			
29' Lt = 1/2 Foot Br. on Deck			
23' Lt			
" " "			
23' Pt			
30' Pt			
33' Pt			
40' Pt			
50' Pt			

29.55	29.6	✓ 15.3	✓
	6.3	✓ 14.6	✓
	7.0		
	8.2	✓ 14	✓
	8.2	✓ 14	✓
	7.5	✓ 11	✓
	7.4	✓ 12	✓
	9.2	✓ 10.4	✓
	6.96	✓ 15.9	✓
	10.0	19.6	✓
	12.0	17.6	✓
	18.5	11	✓
	18.335	16.635	
	18.33		
	17.9	0.6	✓
	8.6	9.7	✓
	5.7	12.6	✓
	2.55	15.78	✓
	4.6	13.7	✓
	4.8	13.5	✓
	3.7	14.6	✓
	4.8	13.5	✓
	8.0	10.3	✓
	7.3	9.1	✓
	12.0	6.3	✓

225' Pt. Paper Park

18.335

0775

18.33

60 ft		21.3	-3.0	✓
43 ft		17.9	0.2	✓
40 ft		15.0	3.3	✓
30 ft		9.2	9.1	✓
23 ft		8.7	9.6	✓
2		8.4	9.93	✓
23 ft		9.7	8.63	✓
28 ft: 1/2 Foot Br. Ground Height = 1/2 Bridge		10.6	7.7	✓
30 ft		11.5	6.8	✓
40 ft		15.1	3.2	✓
50 ft		20.6	-2.3	✓
60 ft		20.6	-2.3	✓
	1+0			
65 ft		21.8	-3.5	✓
40 ft		19.7	-1.4	✓
38 ft: 1/2 Foot Br. on Deck		17.6	0.7	✓
23 ft		11.7	6.6	✓
2		10.0	8.3	✓
23 ft		14.2	4.1	✓
TP	0.46	6.04	12.755	5.58
			6.04	
40 ft		8.0	-2.0	✓
60 ft		10.5	-4.5	✓
75 ft		11.1	-5.1	✓

6.04

6.04

4

17.25 = Beg. of North Grass

80 ft		11.0	-5.0	✓
40 ft		10.8	-4.8	✓
23 ft		9.5	-3.5	✓
2		8.6	-2.6	✓
23 ft		10.1	-4.1	✓
28 ft		10.1	-4.1	✓
7 ft of Lad top 2" Pipe on top		9.6	-3.6	✓
40 ft		10.5	-4.5	✓
43 ft: 1/2 Foot Br. on Deck		6.9	-0.9	✓
80 ft		10.5	-4.5	✓
	1+50			
80 ft		10.5	-4.5	✓
43 ft: 1/2 Foot Br. on Deck		6.8	-0.8	✓
40 ft		10.5	-4.5	✓
23 ft		10.6	-4.6	✓
2		10.8	-4.8	✓
23 ft		11.1	-5.1	✓
40 ft		10.9	-4.9	✓
80 ft		10.8	-4.8	✓
	2+0			
80 ft		11.5	-5.5	✓
40 ft		11.6	-5.6	✓
23 ft		11.0	-5.0	✓
2		10.6	-4.6	✓
23 ft		10.7	-4.7	✓

6.04

6.04

40 Lt	10.8	-4.8	✓
44 Lt = 1/2 Foot Bridge on Deck	6.9	-0.9	✓
80 Lt	10.5	-4.5	✓

2+34.19 = B.F. Lt.

80 Lt	11.4	-5.4	✓
46 Lt = 1/2 Foot Bridge on Deck	7.1	-1.1	✓
40 Lt	11.1	-5.1	✓
23 Lt	11.0	-5.0	✓
1/2	11.8	-5.8	✓
23 Pt	11.3	-5.3	✓
40 Pt	11.4	-5.4	✓
80 Pt	11.1	-5.1	✓

2+60 = Prop. Channel on Radial Line

80 Pt	12.0	-6.0	✓	Main Channel
40 Pt	12.3	-6.3	✓	Has About 1 foot of very soft mud
23 Pt = Bot Channel	12.8	-6.8	✓	Note: 2+52
1/2	13.0	-7.0	✓	2+68
23 Lt	13.0	-7.0	✓	Approx. Same Elev. as 2+10
40 Lt	13.0	-7.0	✓	
46 Lt = 1/2 Foot Br. on Deck	7.0	-1.0	✓	
80 Lt	13.0	-7.0	✓	

2+75

80 Lt	10.3	-4.3	✓
47 Lt = 1/2 Foot Br. on Deck	7.1	-1.1	✓
40 Lt	10.3	-4.3	✓
23 Lt	10.3	-4.3	✓

6.04

5

1/2	10.7	-4.3	✓
23 Pt	11.6	-5.6	✓
40 Pt	11.6	-5.6	✓
80 Pt	11.4	-5.4	✓

3+0

80 Pt	11.2	-5.2	✓
40 Pt	11.2	-5.2	✓
23 Pt	11.1	-5.1	✓
1/2	10.4	-4.4	✓
23 Lt	10.5	-4.5	✓
40 Lt	10.3	-4.3	✓
46 Lt = 1/2 Foot Bridge on Deck	6.8	-0.8	✓
80 Lt	10.5	-4.5	✓

3+50

80 Lt	10.4	-4.4	✓
43 Lt = 1/2 Foot Br. on Deck	6.35	-0.3	✓
40 Lt	10.4	-4.4	✓
23 Lt	10.5	-4.5	✓
1/2	10.6	-4.6	✓
23 Pt	10.7	-4.7	✓
40 Pt	10.8	-4.8	✓
80 Pt	10.5	-4.5	✓

3+75

80 Pt	8.6	-4.6	✓
46 Pt	9.6	-3.6	✓
23 Pt	10.6	-4.6	✓

6.04

6.0

8			10.6	-1.6	✓
33 Lt			10.5	-4.5	✓
40 Lt = 1/2 Foot Br. on Deck			6.8	-0.2	✓
40 Lt Ground			10.5	-4.5	✓
80 Lt			10.5	-4.5	✓
	4+0				
80 Lt			10.4	-4.4	✓
40 Lt			9.7	-3.7	✓
39 Lt = 1/2 Foot Br. on Deck			5.3	0.7	✓
23 Lt			9.0	-3.0	✓
8			8.9	-2.9	✓
23 Pt			5.5	0.5	✓
38.5 Pt. Power Pole					
40 Pt			0.8	5.2	✓
TP	12.79	18.53	0.30	5.74	
			18.5		
60 Pt			10.9	7.6	✓
	4+25		18.5		
60 Pt			8.8	15.7	✓
40 Pt			8.8	14.7	
23 Pt			5.0	13.5	✓
8			7.2	11.2	✓
23 Lt			10.5	8.0	✓
32 Lt = 1/2 Foot Br. on Steps			9.9	8.6	✓
40 Lt			9.8	8.7	✓
60 Lt			12.0	6.5	✓
TP	12.30	30.45	0.38	18.15	

30.45

30.4

6

	4+50				
60 Lt. 1/2 Line House at Food			10.8	19.6	✓
40 Lt			8.9	11.5	✓
23 Lt			10.7	19.7	✓
21 Lt = 1/2 Foot Br. on Step			8.7	11.7	✓
8			7.1	13.3	✓
23 Pt			6.4	11.0	✓
40 Pt			4.1	16.3	✓
50 Pt			2.4	18.0	✓
TP	7.54	36.79	1.20	29.25	
	4+75				
40 Pt			4.1	34.7	✓
23 Pt			5.0	31.8	✓
8			6.2	30.6	✓
23 Lt			8.5	18.3	✓
30 Lt = Twin Equ. Trees					
40 Lt			8.8	18.0	✓
47 Lt = 1/2 Line House Ground			10.2	16.6	✓
47 Lt on Floor			8.38	18.4	✓
	5+0				
40 Lt			8.6	18.4	✓
23 Lt			7.3	19.5	✓
8			5.8	31.0	✓
23 Pt			4.5	31.3	✓
35 Pt. Power Pole					
40 Pt			3.1	33.7	✓

3679

5125

36.8

40 Pt	3.3	32.5	/
23 Pt	4.5	34.9	/
4	6.0	30.8	/
23 Lt	7.4	29.4	/
35 Lt - Fac Tr			
40 Lt	8.8	28.0	/

5150

43 Lt 1/2 Do Garage	8.8	28.0	/
40 Lt	8.7	28.1	/
23 Lt	8.0	28.8	/
4	6.2	30.6	/
23 Pt	4.8	32.0	/
40 Pt - 1/4 End Cl. Top	2.63	34.16	/

For Check 34.19 * 237-5

5178.77 - PRC

40 Pt	4.0	32.8	/
23 Pt	5.0	31.8	/
4 on Hub	6.96	29.83	/
23 Lt	8.5	28.3	/
40 Lt	9.2	27.6	/

West Point Lemoa Blvd Cross Sections
 Wly Pt. 319 to Causeway

70' Rod

BM	467	5.29	0.62	5.3	
		40+0			
35' Pt		4.7	0.6	✓	
23' Pt		4.5	0.8	✓	
+		4.5	0.8	✓	
23' Lt		6.0	-0.7	✓	
35' Lt		5.6	-0.3	✓	
40' Lt		8.5	-3.2	✓	
55' Lt		9.0	-3.7	✓	
65' Lt		16	3.7	✓	
76' Lt	↳ S.D. E. Co. PP. Top Row	0.80	4.49		
		40+50			
50' Lt		8.8	-3.5	✓	
40' Lt		8.4	-3.1	✓	
35' Lt		5.4	-0.1	✓	
23' Lt		6.1	-0.8	✓	
+		4.5	0.8	✓	
23' Pt		5.0	0.3	✓	
35' Pt		5.0	0.3	✓	
		41+0			
35' Pt		4.9	0.4	✓	
23' Pt		4.9	0.4	✓	
+		5.1	0.2	✓	
23' Lt		4.8	0.5	✓	
35' Lt		5.4	-0.1	✓	

1107.00 Pk
 Line Pk
 1237-10

	5.29	5.3	
42' Lt	8.7	-3.4	✓
50' Lt	8.7	-3.4	✓
	41+50		
50' Lt	8.9	-3.6	✓
44' Lt	9.0	-3.7	✓
35' Lt	4.5	0.8	✓
23' Lt	4.5	0.8	✓
+	4.9	0.4	✓
23' Pt	5.0	0.3	✓
35' Pt	4.9	0.4	✓
	42+0		
35' Pt	5.0	0.3	✓
23' Pt	5.1	0.2	✓
+	4.7	0.6	✓
23' Lt	4.7	0.6	✓
35' Lt	4.8	0.5	✓
44' Lt	8.8	-3.5	✓
52' Lt	8.6	-3.3	✓
	42+50		
54' Lt	8.6	-3.3	✓
42' Lt	8.8	-3.5	✓
35' Lt	4.7	0.6	✓
23' Lt	4.8	0.5	✓
+	4.9	0.4	✓
23' Pt	4.9	0.4	✓
35' Pt	5.1	0.2	✓

3-28-33
 No. 1
 9

B

5.29

5.3

13+0

35 Pt	4.9	0.4	✓
23 Pt	4.9	0.4	✓
L	4.8	0.5	✓
23 Lt	4.6	0.7	✓
35 Lt	4.7	0.6	✓
42 Lt	8.7	-3.4	✓
53 Lt	8.5	-3.2	✓

13+50

55 Lt	8.6	-3.3	✓
42 Lt	8.7	-3.4	✓
35 Lt	4.5	0.8	✓
23 Lt	4.7	0.6	✓
L	4.6	0.7	✓
23 Pt	4.8	0.5	✓
35 Pt	4.9	0.4	✓

14+0

35 Pt	4.7	0.6	✓
23 Pt	4.5	0.8	✓
L	4.6	0.7	✓
23 Lt	4.5	0.8	✓
35 Lt	4.5	0.8	✓
23 Lt	8.5	-3.2	✓
55 Lt	8.5	-3.2	✓

14+50

55 Lt	9.0	-3.7	✓
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5.29

5.3

10

25 Lt	9.0	-3.7	✓
30 Lt	9.0	-3.7	✓
23 Lt	4.6	0.7	✓
L	4.4	0.9	✓
23 Pt	4.5	0.8	✓
35 Pt	4.5	0.8	✓

15+0

35 Pt	4.4	0.9	✓
23 Pt	4.4	0.9	✓
L	4.3	1.0	✓
11 Lt	4.4	0.9	✓
13 Lt	8.6	-3.3	✓
23 Lt	9.6	-4.3	✓
35 Lt	9.6	-4.3	✓
55 Lt	8.7	-3.4	✓

15+50

55 Lt	8.4	-3.1	✓
35 Lt	9.6	-4.3	✓
23 Lt	9.6	-4.3	✓
5 Lt	8.4	-3.1	✓
L	4.3	1.0	✓
23 Pt	4.3	1.0	✓
35 Pt	4.4	0.9	✓

TP	4.85	6.41	3.73	1.56
----	------	------	------	------

6.41

4610

6.4

35 Pt	5.1	1.0	✓
23 Pt	5.2	1.2	✓
10 Pt	5.8	0.6	✓
1/2	7.7	-1.3	✓
6 Lt	9.1	-3.2	✓
23 Lt	10.5	-6.1	✓
35 Lt	10.5	-4.1	✓
55 Lt	9.3	-2.9	✓

46+50

55 Lt	9.7	-3.3	✓
35 Lt	10.5	-4.1	✓
23 Lt	10.5	-4.1	✓
5 Lt	10.5	-4.1	✓
1/2	7.4	-1.0	✓
5 Pt	5.5	0.9	✓
23 Pt	5.4	1.0	✓
35 Pt	5.4	1.0	✓

4710

35 Pt	5.2	1.2	✓
23 Pt	5.3	1.1	✓
1/2	5.6	0.8	✓
7 Lt	9.9	-3.5	✓
23 Lt	10.3	-3.9	✓
35 Lt	9.7	-3.3	✓
55 Lt	9.7	-3.3	✓

6.41

47+3270 BC

6.41

11

745 Lt = 2 Elec RR Top Rail	1.96	4.45	✓
64 Lt	3.2	3.2	✓
54 Lt	9.8	-3.4	✓
35 Lt	10.0	-3.6	✓
23 Lt	9.6	-3.2	✓
5 Lt	9.8	-3.4	✓
1/2 02 Hub	6.97	-0.56	✓
2 Pt	5.2	1.2	✓
23 Pt	5.0	1.4	✓
35 Pt	5.4	1.0	✓

47+50

35 Pt	5.0	1.4	✓
23 Pt	5.0	1.4	✓
3 Pt	5.5	0.9	✓
1/2	6.9	-0.5	✓
7 Lt	9.8	-3.4	✓
23 Lt	9.6	-3.2	✓
35 Lt	9.8	-3.4	✓
50 Lt	9.8	-3.4	✓

48+0

50 Lt	9.7	-3.3	✓
35 Lt	9.8	-3.4	✓
23 Lt	9.2	-2.8	✓
4 Lt	9.3	-2.9	✓
1/2	6.1	0.3	✓

	6.41			
23 Pt	54	1.0	✓	
35 Pt	57	0.7	✓	
	48+50			
35 Pt	50	1.4	✓	
23 Pt	49	1.5	✓	
2 Pt	52	1.2	✓	
2	64	0	✓	
5 Lt	90	-2.6	✓	
23 Lt	98	-3.4	✓	
35 Lt	98	-3.4	✓	
48 Lt	92	-2.8	✓	
	49+0			
48 Lt	94	-3.0	✓	
35 Lt	97	-3.3	✓	
23 Lt	97	-3.3	✓	
15 Lt	96	-3.2	✓	
8 Lt	65	-0.1	✓	
2	47	1.7	✓	
23 Pt	46	1.8	✓	
35 Pt	42	2.2	✓	
	49+50			
35 Pt	36	2.8	✓	
23 Pt	40	2.4	✓	
2	46	1.8	✓	
13 Lt	55	0.9	✓	
20 Lt	96	-3.2	✓	

	6.41	6.4		
23 Lt	98	-3.4	✓	
35 Lt	98	-3.4	✓	
45 Lt	95	-3.1	✓	
	50+0			
45 Lt	92	-2.8	✓	
35 Lt	97	-3.3	✓	
23 Lt	78	-1.2	✓	
15 Lt	39	2.5	✓	
2	41	2.3	✓	
23 Pt	39	2.5	✓	
35 Pt	32	3.2	✓	
	50+50			
35 Pt	25	3.9	✓	
23 Pt	27	3.7	✓	
2	34	3.0	✓	
23 Lt	36	2.8	✓	
25 Lt	43	2.1	✓	
35 Lt	88	2.2	✓	
46 Lt	92	2.9	✓	
	51+0			
45 Lt	80	-1.6	✓	
35 Lt	34	3.0	✓	
20 Lt	31	3.3	✓	
2	29	3.5	✓	
23 Pt	18	4.6	✓	
35 Pt	17	4.7	✓	

	11.40	11.4	
23' Pt on Paving	5.87	5.53	✓
29' Pt Gutter on Paving	6.21	5.19	✓
29' Pt Existing Ob Top	5.55	5.85	✓
35' Pt	5.5	5.90	✓
54150			
29' Pt Existing Ob Top	5.60	5.8	✓
Gutter on Paving	6.21	5.19	✓
23' Pt " "	5.85	5.55	✓
± " "	4.90	6.50	✓
23' Lt " "	4.39	7.01	✓
35' Lt " "	4.39	7.01	✓
5510			
35' Lt on Paving	4.36	7.04	✓
23' Lt " "	4.38	7.02	✓
± " "	4.94	6.46	✓
23' Pt " "	5.96	5.44	✓
29' Pt " " Gutter	6.27	5.03	✓
29' Pt Existing Ob Top	5.74	5.66	✓

BM

843

297

BR HW G/L
100 N.W. Pl. Wm
8-11-11
300

11.4
5.75

5-17-33

See Alley BIK. 21. Kimballs Add.

Miller
Walker
Bliss
B.M.B.R.

0.26 130.93 130.67

N.E. I +
25th St.

T.P. 0.54 118.82 12.65 118.28

17' N. of S. line I. St. = N. edge cmt. gutter

W. 3.46 15.20

ϕ 4.99 13.83

E 14' N. of S. line I. St. = 5. ch. line 6.25 12.57

E. cmt. ch 5.85 12.97

E. 9" gutter 6.41 12.41

ϕ " " 5.14 12.68

W. " " 3.80 15.02

W. " ch. 3.07 15.75

12' N. of S. line I. St. = S. edge cmt. gutter

W. cmt. ch 3.07 15.75

W. " gutter 3.61 15.21

ϕ " " 4.86 13.96

E. " " 6.16 12.66

E. " ch. 5.72 13.10

0 ± 00 = S. line I. St.

E. - 5. ground 7.1 11.7

E. - 0.7 " " 6.4 12.4

(N. End. 8" cmt. Wall)

E. (S. End. Return 5.60 13.22

+ 0.1 5.9 12.9

ϕ 5.8 13.0

+ 6 5.6 13.20

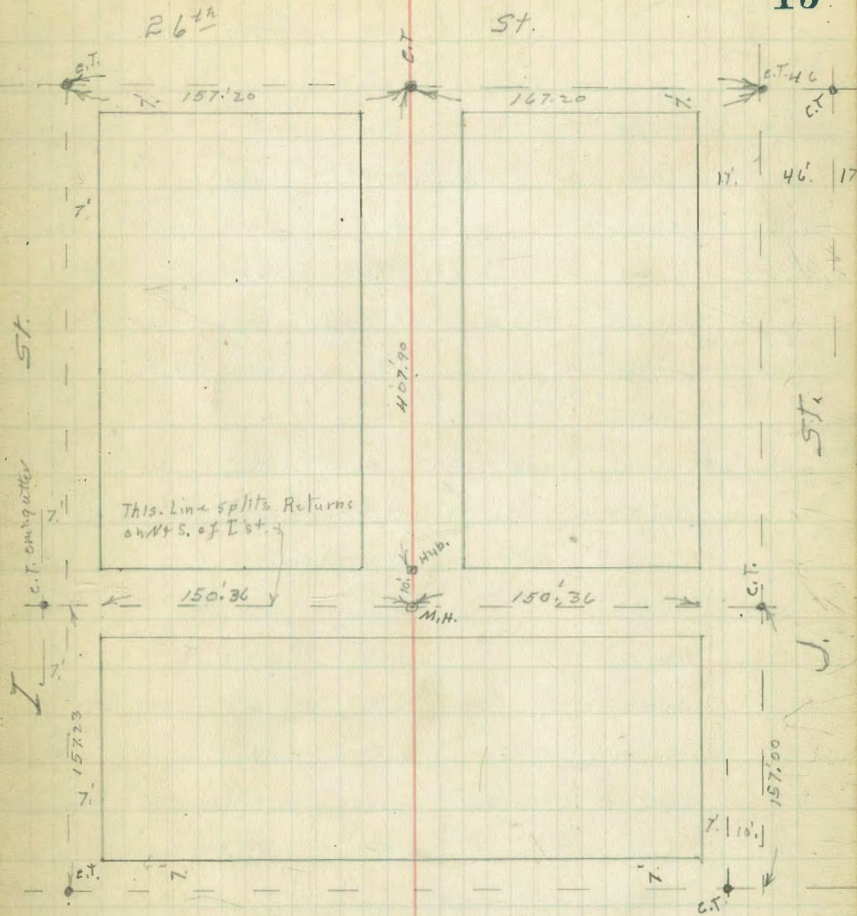
W. ground 3.5 15.3

W. cmt. ch. 2.80 16.0

Plotted
M.F.B.

Indexed
c.s.K.

15



	118.82			
	0+21' S.			
W.		7.0	111.8	
☼		7.9	110.9	
+9.4 ground		8.4	110.4	
+9.4 Top. cmt. wall. wedge		8.09	110.73	
E. Base "		9.4	109.4	
+5		9.8	109.0	

Black Acacia 4" Diam on E. line, at Base of wall

	0+32	Wall on 2.6" Wide from Here Southly		
	0+44			
Black Acacia 5" Diam	0.3	in Alley at Base wall		
T.P.	0.78	110.10	9.50	109.32

	0+46			
E-5'		2.6	107.5	
E	Base wall	2.0	107.9	
+1.0	Top " w. edge	0.57	109.53	
+1.0	ground in alley	1.01	109.09	
☼		0.4	109.7	
W.		+0.9	111.0	

	0+55			
W.		+2.2	112.3	
+5		0.5	109.6	
☼		0.8	109.3	
+8.9		1.5	108.6	
+8.9	Top wall wedge	1.04	109.06	
E. = Black Acacia 7" Diam	at Base wall	2.6	107.5	
+5'		3.2	106.9	

	110.10			
	0+63			
Black Acacia 3" Diam	0.3	in Alley		
	0+70	Garage on W. dirt floor		Back
E-5		3.4	106.7	
E		3.0	107.1	
E+0.5	{ Base wall Acacia 7" Diam.	3.0	109.1	
E+1.2	Top wall. w. edge	1.71	108.39	
+1.3		2.0	108.1	
☼		1.6	108.5	
+5		1.2	108.9	
W.		0.0	110.1	
+16.5	floor	+2.8	112.9	

	1+00			
W		1.1	109.0	
+3		2.4	107.7	
☼		2.9	107.2	
+8.9		3.1	107.0	
+8.8	Top wall	2.82	107.28	
E	Base "	4.2	105.9	
+5'		4.6	105.5	
	1+10 = { S. End. 6" wall. N. " cmt steps			
-5		4.8	105.3	
2		4.3	105.8	
+1.2	Top wall	3.08	107.02	
+1.2	Top step	3.6	106.5	
☼		3.2	106.9	
W.		2.4	107.7	

110.10

1+40³⁶ = N. line E+W. Alley

W.	2.9	107.2
♀	4.0	106.1
E	4.3	105.8

1+50³⁸ = ♀ E+W. Alley

E. on Hub	5.33	104.77
E. " ground.	5.0	105.1
♀ " Top. M.H.	4.22	105.88
W.	2.9	107.2

1+60³⁶ = S. line E+W. Alley

W. - 1 garage floor	3.1	107.0
♀	4.8	105.3
+ 9.5 = W. side garage	5.7	104.4

1+63 dirt garage on E. dirt floor 0.5 in Alley

0.5 W. of E. line = floor. 5.8 104.3

1+73 dirt garage on E. dirt floor 0.6 in Alley

0.5 W. of E. line = floor. 6.4 103.7

♀ 5.6 104.0

W. 4.3 105.8

1+89.5 End. garage on E. dirt floor. 0.8 in Alley

6.9 W. of E. line = floor. 6.6 103.5

1+ 2+00

W	5.2	104.9
♀	6.6	103.5
E.	7.0	103.1

110.10

2+02

E-1,2 = W. side house	8.6	101.5
E	8.3	101.8
+3	7.3	102.8
♀	7.0	103.1
W.	5.5	104.6

2+30

W	6.7	103.4
+5	7.8	102.3
♀	8.3	101.8
E	9.2	100.9

T.P. 0.81 102.20 8.77 101.39

2+39

0.3 W. of E. line = W. end. 3' Walk. 1.90 100.30

2+50

Pepper Tree 14" Diam. ♀ on E. Line

2+70

E	3.1	99.1
♀	3.1	99.1
+5	2.8	99.4
W.	1.5	100.7

3+00⁷² = N. Line J. S+

W	4.3	97.9
+5	5.5	96.7
♀	5.7	96.5
E	5.8	96.4

Alley BJK 21 Kimballs.

17

102.20
3+10⁸ = N. End. emt. cross wall.

E. Top ch. Alley paymt.	6.49	95.71
⊥ " "	6.83	95.32
W. " " " "	5.76	96.44

3+20⁸ N. of line

W emt. ch	5.93	96.27
W emt. gutter	6.73	95.47
⊥ " "	7.23	94.97
E " "	7.63	94.57
E. emt. ch.	6.83	95.37

3+23⁸ = S. side emt. gutter

E.	7.43	94.77
⊥	7.03	95.17
W.	6.59	95.61
T.P.	10.36	106.34
B.M.B.P.	6.46	99.88 = 99.87 + J.

S.P. 25¹¹

Hub 3.72 108.49 104.77 E. Line N+S. Alley

0+00 = E. line N+S. Alley		
N.	2.7	105.8
⊥	3.4	105.1
+ 8.1 = N. side garage	3.8	104.7
0+17.6		

0.4 N. of S. line N. side garage to E.	6.1	102.4
2.0 " " " " " " " " W.	6.1	102.4
⊥	6.0	102.5
N	5.1	103.4

0+22 ch garage on S. dirt floor 0.5 in Alley		
8.5 N. of S. line = floor	6.9	101.6
0+30 ch garage on S. dirt floor 0.6 in Alley		
0.6 N. of S. line = floor	8.0	100.5
0+43 garage on S. dirt floor 0.6 in Alley		

N	9.1	99.4
⊥	9.5	99.0
+ 9.4 = floor	9.9	98.6
0+52 garage on S. dirt floor 0.6 in Alley		
3+06 = floor	10.4	98.1
⊥	10.2	98.3
N	10.0	98.5

W. entrance

108.49

0+55 = W. End. garage on N. cmt. floor 1.3 Back
 1.3 N. of N. line = floor 10.40 98.1
 0+61 garage on S. dirt floor 0.9 in Alley
 0.9 N. of S. Line = floor 10.7 97.8
 0+73 = W. End. Tile Garage 2.7 in Alley
 S. Entrance

0+77 E. end. cmt. floored garage on N

N-1.3 = floor 10.73 97.76
 N 10.8 97.7
 ♀ 11.1 97.4
 S 11.0 97.5
 0+983 = { E. End Tile garage on S.
 W. " Fence " " 2.7 in Alley

1+00

S. 11.4 97.1
 ♀ 11.3 97.2
 N. 11.2 97.3

1+43 = Garage on N. dirt floor 0.3 Back
 W. " " " " 1.5 "

N 10.3 98.2
 ♀ 10.0 98.5
 S. 9.7 98.8
 +1.5 8.9 99.6

1+50

S 8.7 99.8
 ♀ on Top M.H. 8.54 99.95
 N. 9.7 98.8

108.49

Alley BIK 21 Kimball's

19

1+60

N 7.0 101.5
 ♀ 7.3 101.2
 +5 6.8 101.7
 S 4.9 103.6

1+75

S 2.5 106.0
 +5 3.9 104.6
 ♀ 4.7 103.8
 N 5.2 103.3

T.P. 12.48 119.73 1.24 107.25

2+00

N 11.6 108.1
 ♀ 11.7 108.0
 +6 11.0 108.7
 S. 10.0 109.7

2+25

S 4.9 114.8
 ♀ 6.2 113.8
 N 6.6 113.1

2+50

N. 1.2 118.5
 ♀ 0.7 119.0
 +8.4 = N. End. cmt. Wall 0.4 119.3
 S. 0.4 119.3
 T.P. 12.26 131.70 0.29 119.44

131.70

2775

S.		9.0	122.7
♀		9.3	122.4
N.		9.2	122.5
<hr/>			
		300	
		4100	
N.		4.9	126.8
♀		4.5	127.2
S.		4.6	127.1
T.P.	12.68	143.86	0.52 - 131.18
<hr/>			
		325	
		4125	
S.		11.6	132.3
♀		11.7	132.2
N.		12.3	131.6

³/₄ 35 garage on N. dirt floor 3' Back

N-3. = floor

		11.0	132.9
<hr/>			
		3142	
		4140	
N.		10.2	133.7
♀		9.5	134.4
S.		10.1	133.8
<hr/>			
		3478	
		4175	
S.		5.2	138.9
♀		5.4	138.8
N.		5.0	138.9

Added 5-9-30
20

143.86

Alley Bk 21. Kimball's

20

4400.2 = W. Line 26th St.
W. edge paymt.

N. amt. ch.	2.38	141.48
N. gutter paymt.	2.52	141.34
♀	3.01	140.85
S.	2.74	141.12
S. amt. ch.	2.68	141.18
<hr/>		
10' E = W. ch. Line		
S. amt. ch.	2.89	140.97
S. paymt.	3.32	140.54
♀	3.24	140.62
N.	3.04	140.82
N. amt. ch.	2.65	141.31
ch K. original B.M.	13.17	130.67 = 130.67

Cross Section Proposed Bridge
Robinson St. 8th to 10th St

See Sketch Page 21

0+94.54

Lt			8		Rt
275.3	275.9	276.2	273.6	257.85	265.1
5.3 100	4.7 55	4.4 116	7.0	227.3 FL 55.5 End Cut.	15.5 100

0+83

276.0	276.4	276.2	264.2	261.2	267.8
4.6 100	4.2 65	4.4	16.4 35	19.4 52	12.8 75

0+53

277.6	277.1	276.7	273.8
3.0 100	3.5 50	3.9	6.8 10

0+47.27

277.7	277.4	277.1	274.0
2.9 100	3.2 50	3.5 12	6.6

0+0

278.0
2.6
100

F Cb of Robinson Top Cb

276.87	273.93	273.37	272.85	265.86
2.71 95	6.5 30	7.21	7.73 30	14.72 115 - End Cb

F Cb of 8th St Gutter

276.41	273.53	272.93	272.28	265.54	270.26
4.7 95	7.05 30	7.65	8.30 30 C.B. 076 grain	15.04 115	10.30 Floor Lint Catch Basin

BM

5.63

280.58

274.95

NW CP
Robinson St
343

280.58

2+19.65 - Canyonway Takeover 2 of Imp.

1+99.65 - N. Cb Canyonway

1+90

1+75

1+50

TP 3.57 258.55 1298 254.98

TP 0.27 267.96 12.89 267.69

1+30

1+10

280.58

244.11 14.44 150° Pav	242.81 15.74 100° Pav	241.45 17.16 50° Pav	240.25 18.30 = Pav	239.28 19.27 50° Pav	239.43 19.12 66-54 Block Pav	242.8 15.8 100-111 Road
243.6 15.00 130° Pav	242.09 16.46 65° Pav	240.54 17.01 Gutter	241.01 17.54 100-30	240.2 18.1 65	237.18 21.37 67-FL Drain	240.2 10.9 97-44R
244.38 14.17 150° Pav	244.04 16.51 120 Topc	242.9 15.7 60	241.4 17.2	240.5 18.1 35	240.5 18.1 70	247.2 9.4 105-111R
246.1 12.5 150	249.0 9.6 100	249.6 9.0 60	247.0 11.6	241.5 17.1 35	242.4 16.2 80	251.3 7.3 100-111R
252.8 5.8 150	256.4 2.2 100	258.6 0.0 40	254.3 4.2	242.3 16.2 47	243.3 15.3 85	248.4 10.2 100
			258.55 -			255.0 8.6 113
						261.4 10.2 120-44R
						261.4 12.5 125
						261.6 6.5 130
						261.6 12.8 138
						261.6 12.6 136-54R
						258.5 11.3 128-51R
261.7 18.9 150	266.2 15.4 100	266.2 14.4 70	266.6 14.0 30	261.3 17.3	244.8 35.8 55	244.2 36.4 85
					248.4 32.2 100	258.5 22.1 116-111R
271.2 9.4 100	274.9 5.7 50	275.9 4.7 24	268.1 12.5	250.4 30.2 57	255.6 25.0 100	263.6 17.0 120
			280.58			

3+56.6

LT	Z	RT
277.9 +7.7 100.	278.1 +7.9 65.	276.6 +6.4 10-2/16
276.6 +6.4 95.	260.3 9.9 95.	243.8 26.4 70.
236.9 33.3 100.	234.4 30.8 115.	237.0 34.2 150.

3+45

278.0 +7.8 100.	278.2 +8.0 55.	276.9 +6.7 25.	275.7 +5.5	260.5 9.7 95.	241.5 28.7 75.	237.7 32.5 100.	234.8 35.4 115.	233.5 36.7 150.
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3+25

277.8 +7.6 125.	277.5 +7.3 100.	277.3 +7.1 66.	275.2 +5.0 15.	268.9 1.8	255.0 15.2 95.	240.1 30.1 70.	237.6 32.6 100.	235.3 34.9 118.	231.8 37.4 126.	230.5 37.7 160.
-----------------------	-----------------------	----------------------	----------------------	--------------	----------------------	----------------------	-----------------------	-----------------------	-----------------------	-----------------------

3+0

272.8 +2.6 150.	271.8 +1.6 100.	273.7 +2.5 70.	272.4 +2.2 30.	263.4 6.8	253.0 17.2 25.	240.1 30.1 60.	237.1 33.1 80-1/4 Drain	233.6 36.6 95-1/2 Drain	237.0 33.2 100-1/4 Drain	239.3 30.9 115.	237.1 32.1 150.
-----------------------	-----------------------	----------------------	----------------------	--------------	----------------------	----------------------	-------------------------------	-------------------------------	--------------------------------	-----------------------	-----------------------

TP

11.73

270.18

0.10

258.45

270.18

2+75

251.1 +7.5 150.	256.2 +2.4 115.	254.1 +4.5 75.	253.1 +5.5 35.	256.4 2.2	244.1 14.5 40.	239.6 19.0 60-1/4 Drain	235.59 22.96 70-1/2 Column 1	239.0 19.6 95-1/2 Drain	239.3 19.3 100	238.7 19.9 150.
-----------------------	-----------------------	----------------------	----------------------	--------------	----------------------	-------------------------------	------------------------------------	-------------------------------	----------------------	-----------------------

2+55

257.1 1.5 150.	251.8 6.8 100.	254.4 4.2 135.	250.3 8.3	242.0 16.6 15.	238.55 20.0 50-1/2 Col. Valley South	239.8 18.8 100.	240.0 18.6 150.
----------------------	----------------------	----------------------	--------------	----------------------	--	-----------------------	-----------------------

2+49

242.6 16.0 150.	239.7 18.9 125.	250.9 7.7 70.	252.4 6.2 25.	242.9 15.7 15.	241.8 16.8	239.13 19.42 68-1/2 Block 1A	239.8 18.8 100.	240.3 18.3 120.	252.3 6.3 150.
-----------------------	-----------------------	---------------------	---------------------	----------------------	---------------	------------------------------------	-----------------------	-----------------------	----------------------

2+39.82 = FC6 Caryota Way

258.55

253.4 5.2 150.	246.1 12.5 120.	242.9 15.7 65.	240.51 18.34 90-1/2	240.98 17.57 70.	239.26 19.39 67-1/2 Block 2A	240.4 18.2 100.	241.3 17.3 120.	248.6 10.0 140.	254.8 28 155.
----------------------	-----------------------	----------------------	---------------------------	------------------------	------------------------------------	-----------------------	-----------------------	-----------------------	---------------------

5+33.44

TP 7.07 285.38 310 278.31

5+11.42 Δ on Lt. Taken on Split of Δ

4+89.4 Δ on Lt.

4+58

4+40

4+10

3+80

TP 11.40 281.41 019 270.01
270.18

Lt.

Δ

Rt.

280.0 276.3 278.2 278.8 279.8
5.4 9.1 7.2 6.6 5.6
50 15 45 100

279.85 278.1 270.6 273.9 273.6 277.9 277.9 277.9
1.56 3.3 10.9 7.6 7.8 3.5 3.5 3.5
56.3 30 25 8 30 50 100

280.3 279.1 268.0 262.5 267.3 276.8
1.1 2.3 13.1 20.9 14.1 4.6
100 45 25 20 50 100

279.9 279.0 278.3 262.2 261.4 267.8 253.9 260.6 269.3 274.4
1.5 2.4 3.1 19.2 20.0 2.3 3.0 20.8 12.1 7.0
100 75 45 15 30 7 30 55 95 100

280.0 279.1 277.7 267.2 259.6 258.0 250.2 249.4 258.7 264.1
1.4 2.3 3.7 14.2 21.8 2.4 3.2 3.0 2.7 17.3
100 70 45 15 18 17 50 75 100

279.6 279.4 277.2 266.7 260.7 261.3 250.0 244.4 253.2 266.4
1.2 2.0 4.2 14.7 20.7 20.1 20.0 27.0 23.2 25.0
100 80 35 17 30 30 50 90 100 125

278.7 278.4 277.7 276.7 272.5 260.8 256.6 254.7 240.5 241.0 246.2
2.7 3.0 3.7 4.4 8.9 20.6 25.8 26.7 40.9 10.4 35.0
100 65 35 10 30 30 60 75 85 100 125

281.41

Lt

S

Rt

BM

3.37

282.01

JF 87
 Feb 16 10 1/2 10 1/2
 282.01

6 + 11 1/2 = 17.7 10 1/2 ft

57 60.8

285.38

281.2

1.2
 30

280.96

4.12
 20
 2 top 6

280.32

5.04
 30
 5 1/2 ft
 27 ft

280.71

4.67
 30 ft

280.22

5.16
 20
 5 1/2 ft
 30 ft

280.91

4.17
 20
 7 top 6

281.2

4.2
 30

284.0

4.1
 100

280.0

5.4
 50

279.4

6.0
 36

279.2

6.2

279.7

5.7
 32

285.38

Buchanan Ave. Cross Section
6th St. Ext to Maryland St.

8-15-33
Moore
Singer
Hartford
Kansas

Massachusetts
8+60.31
ΔP. 38°59'

6+11.25
ΔP. 28°09'

4+81.72
ΔP. 26°31'

0+95.90

0+0

See C-13-154-3

for ties on 6th St. Ext.

6th St. Ext. Oct. Ct.

Buchanan Ave

FC
38-3072
Paving

8-15-33
Moore
Singer
Hartford
Kansas

12+72.71
ΔP. 19°3'

12+76.59

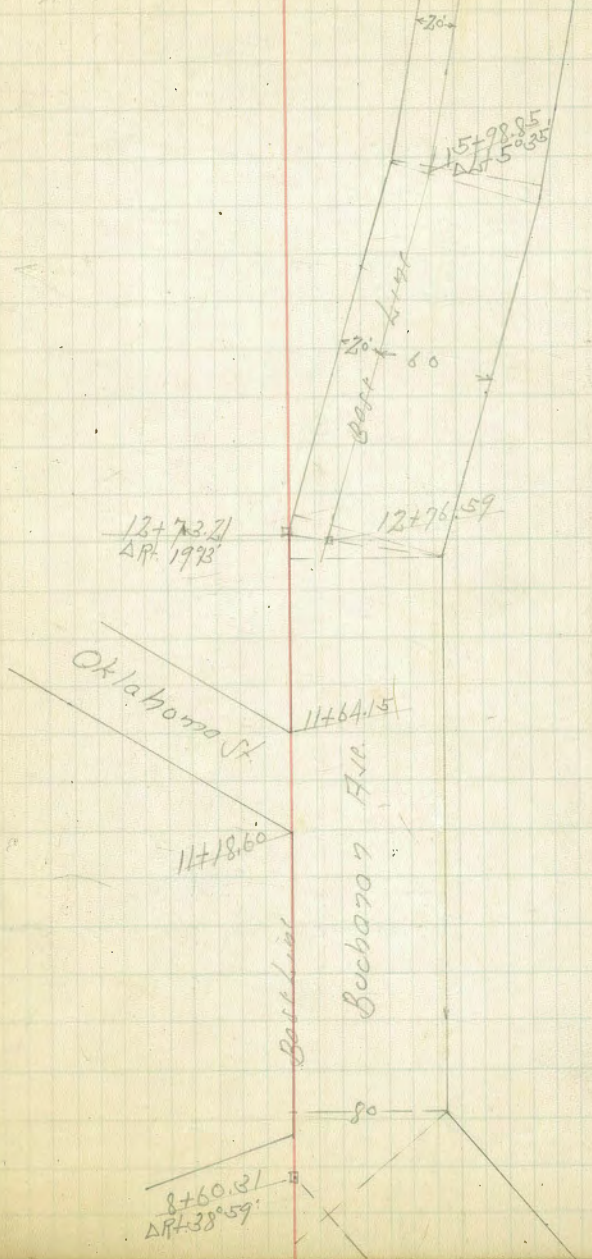
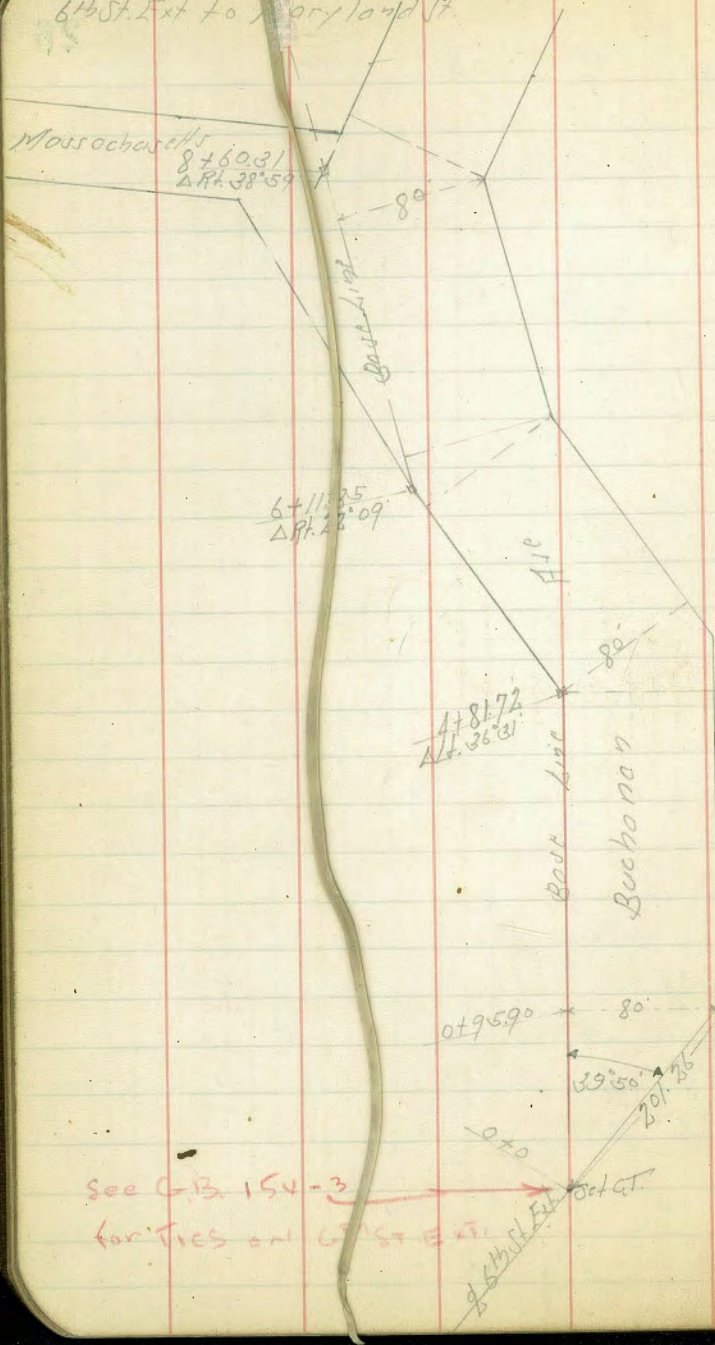
Oklahoma St.

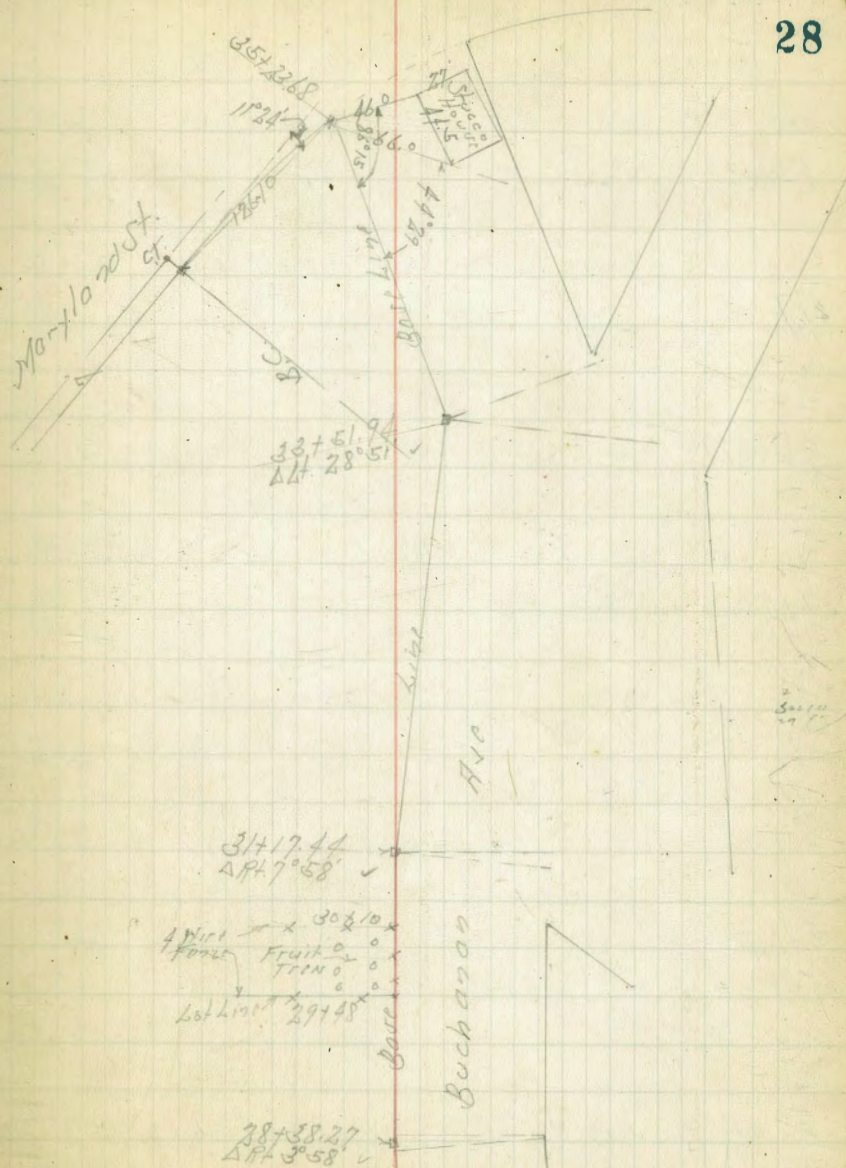
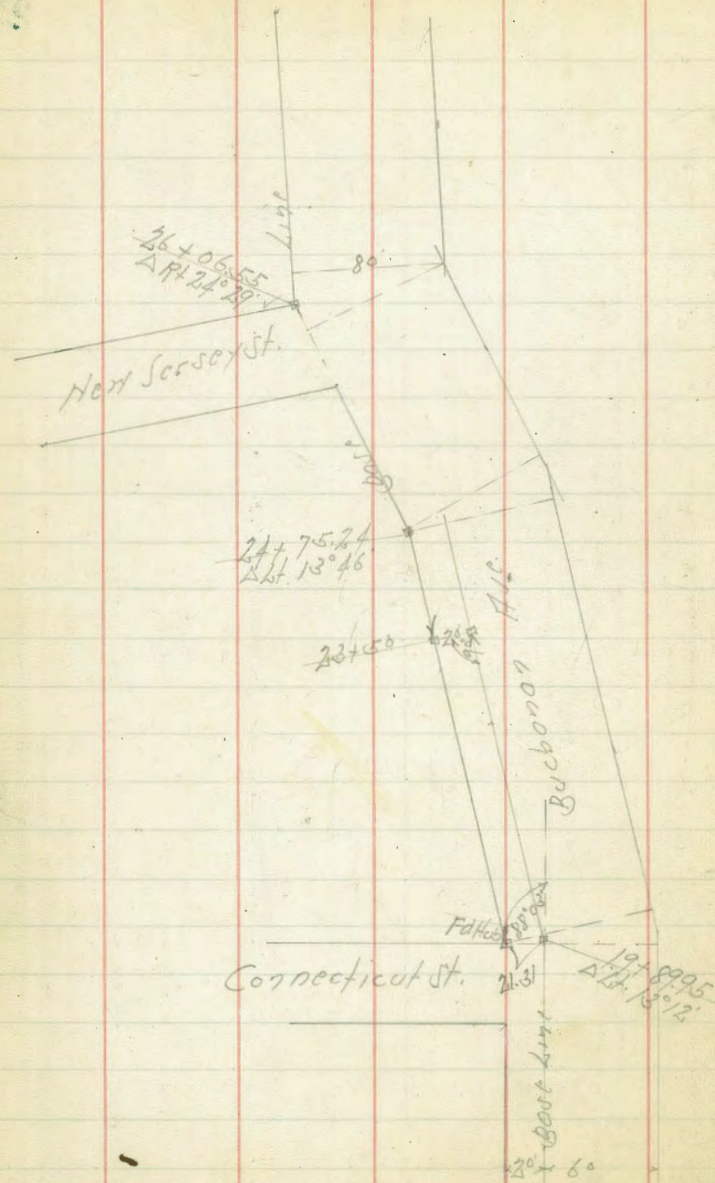
11+64.15

11+18.60

Buchanan Ave

8+60.31
ΔP. 38°59'





Buchanan Ave. Cross Section
Sixth St. Ext. to Maryland St.

8-17-33
Moore
Sisson
Northrup
Koroff

29

2+0

Lt	Clearance	Rt.
80.5	78.7	76.4 79.6 75.8 76.4 70.9
93 40	111	13.4 15 10.2 30 14.0 45 14.4 80 18.9 115

1+50

72.1	72.4	79.1 74.7 70.2 77.0
17.7 50	77.4	10.7 35 15.1 50 17.6 80 12.8 100

1+36.07

72.0	71.4	69.0 70.2
12.8 50	18.4	19.8 50 19.6 80

1+20

70.4 71.0 67.3	68.5 78.7 77.3 87.5
19.4 50 18.8 85 22.5	21.3 30 11.4 35 12.5 85 2.3 80

0+95.90

66.7	71.7	75.7 82.5 85.4
23.1 50	18.1	14.1 30 7.3 50 14.0 80 = 2 paving

0+47.95

66.0	81.5	82.35
23.8 50	8.3	7.46 40 = 2 paving

0+0 = 1/2 Sixth St Ext

79.38

10.43

BM 0.19 89.81'

89.62

CT to Penn. 74
Sixth St Ext
33730.72 T.C

89.81

6+11.35 Δ Pt 22° 09 Taken as Split

5+50

4+81.72 Δ Lt 36° 31 Taken as Split of Angle

4+50

4+0

TP 12.48 100.13 216 8765

3+50

3+0

2+50

89.81

Lt	B	Pt					
133.1	117.1	103.1	97.6	91.6	96.1	98.7	
+33.0 30	+17.0	+3.0 40	2.5 50	8.5 70	1.0 100	1.4 140	
124.2	112.0	100.1	95.1	95.2	91.4	97.9	
+24.1 30	+11.9	0.0 45	5.0 55	4.9 70	8.7 100	2.2 140	
114.1	105.3	96.5	90.6	88.2	87.7	94.6	
+14.0 30	+5.2	6.6 40	9.5 55	11.9 100	12.4 120	5.5 135	
116.1	105.0	94.1	87.9	86.0	85.8	86.0	
+16.0 30	+4.9	6.0 50	13.2 60	14.1 80	14.2 100	14.1 140	
116.6	104.1	91.3	86.4	84.6	80.2	84.4	85.4
+16.5 30	+4.0	8.8 45	13.7 55	15.5 80	19.9 90	15.7 100	14.7 140
							100.13
107.8	99.5		84.1	84.1	76.6	84.2	86.3
+18.0 15	+7.8		5.7 50	5.7 70	13.2 80	5.6 90	3.5 140
99.4	94.5	88.8	82.1	81.8	74.3	81.7	82.5
+9.6 30	+4.7	1.3 30	7.7 40	8.0 70	15.5 85	8.1 100	7.3 140
92.8	88.0		80.1	76.2	72.6	76.9	72.2
+3.0 35	1.8		9.7 40	12.1 90	17.2 100	13.9 115	17.6 140
	89.81						

9+25 = Bottom of Gulch From Lt

9+0

8+60.31 Δ Pt 38°49' Taken on Split

8+0

TP 11.70 128.03 0.12 116.33

TP 11.56 116.45 7.98 104.89

7+50

7+0

TP 12.80 112.87 0.06 100.07

100.13

Lt B Pt

118.7 114.8 110.9

9.3 132 17.1
60' 30'

121.5 116.9 112.5 106.9 104.8 102.3 102.3

6.5 111 15.5 21.1 23.2 25.7 25.7
60' 30' 30' 60' 80' 100'

138.5 121.4 107.8 103.9 100.5 100.5 111.6

+10.5 6.62 20.2 24.1 27.5 27.5 16.4
40' 24.46 45' 80' 100' 110' 135'

144.5 126.9 119.7 105.4 102.8 98.8 102.7 115.5

+16.5 11 8.3 22.6 25.2 29.2 25.3 12.5
48' 30' 45' 80' 100' 110' 120'

128.03

131.0 119.0 102.6 102.4 98.8 99.9 104.4

+18.1 76.1 19.3 19.5 14.1 13.0 8.5
30' 45' 60' 80' 100' 125'

131.0 117.8 102.5 100.8 96.6 99.0 102.6

+18.1 74.9 10.4 12.1 16.3 13.9 10.3
30' 45' 60' 80' 100' 130'

112.87

100.13

13+50

TP 13.31 150.62^v 0.30 138.31^v

12+73.21 Takasas Split of A

13+50

TP 13.74 138.61 2.16 125.87^v

7 11+64.15 = E.L. Oklo 3070 St

7 11+0

7 10+0

7A

9+50

138.03

H

B

PT

143.3 130.6 126.0 129.6 129.6 146.6 158.1 171.0
 7.3 29.0 24.6 21.0 21.0 4.0 +7.5 +20.4
 80 40 20 10 10 35 60 80

150.62
 135.3 125.0 124.6 124.9 125.9 142.1 143.6 149.1
 3.3 13.6 14.0 12.7 12.7 3.5 +5.0 +10.5
 100 50 20 = 1/2 16 70 60 = 1/2 80

127.0 123.9 122.7 124.6

11.6 14.7 15.9 14.0
 80 40 1/2 60

138.61

128.0 119.5 119.2 119.0 127.6 137.0 147.5
 0.0 8.5 8.83 9.0 0.4 +9.0 +19.5
 60 30 27 1/2 35 60 80 = 1/2 100

125.2 117.2 115.6 115.1 132.0 140.5

2.8 10.8 12.4 13.9 +4.0 +13.5
 60 30 40 80 100

125.2 110.0 110.5 110.0 110.5 116.8

2.8 18.0 17.5 18.0 17.5 11.2
 50 20 60 60 100

125.2 118.6 110.4 107.2 106.0 107.3 108.0

2.8 12.4 17.6 20.8 22.0 20.7 20.0
 60 30 20 50 80 110

138.03

17+50

LT	B	Rt
159.2	144.1	149.1 152.6 154.6 161.8 176.6 186.9
26 70	17.7 20	127 9.2 7.2 0.0 +14.8 +25.1

17+0

155.4	148.9	143.3 150.3 154.1 170.0 181.1
6.4 75	12.9 50	18.5 11.5 7.7 +8.2 +19.3

16+50

158.1	144.0	138.7 146.7 148.0 159.3 172.3 184.3
3.7 70	17.8 55	22.1 15.1 12.8 2.5 +10.5 +22.5

15+98.85 4/15/03 5 Taken of Splat

154.2	146.5	137.1 145.1 146.1 162.8 171.3 186.3
7.6 75	15.3 55	24.7 16.7 15.7 +15.0 +9.5 +24.5

15+50

145.3	142.2	136.3 138.4 142.8 142.5 179.4 182.3
16.5 70	19.5 55	25.5 23.4 19.4 19.3 +7.5 +20.5

TP 11.64 161.78 0.48 150.14

146.1	135.0	139.8 139.9 150.2 170.1 182.1
5.5 70	15.6 50	10.8 10.7 0.1 +19.5 +31.5

15+0

144.3	131.0	136.3 137.4 150.6 166.4 182.1
-------	-------	-------------------------------

14+50

6.3 70	19.6 35	14.8 13.2 0.0 +15.8 +31.5
-----------	------------	---------------------------

14+0

147.8	139.2	132.8 127.6 133.6 133.7 153.6 169.6 181.6
2.8 80	11.4 70	17.8 23.0 17.0 16.9 +3.0 +19.0 +31.0

150.62

150.62

24+0

TP

12.43

210.98

0.00

198.55

Pay 30° Pt
24+0

23+50

From Here
Base Line = Start of Line

23+0

22+40

TP

10.24

198.55

0.45

188.31

21+60

21+0

20+60

188.76

Lt.

B

Pt.

202.2 192.7 185.0 189.0 189.2 201.2 208.0 218.0 229.0

8.8
70 18.3
50 26.0
22 22.0
74 21.8
20 98
45 30.0
60 +70
80 80.5
100 +181
100

210.98

191.7 184.7 180.3 183.3 185.3 186.2 198.0 111.5 224.8

6.8
70 12.9
55 18.2
40 15.2
70 13.2
74 12.3
20 0.6
45 +13.0
80 80.5
100 26.3
100 ?

194.5 185.0 175.0 181.7 181.8 184.0 195.7 208.5 221.0

4.0
80 15.5
55 23.5
20 16.8
70 16.7
74 14.5
10 2.8
30 +10.0
60 60.5
80 +23.5
80

191.1 183.8 177.7 172.4 179.7 180.8 197.5 207.7 220.5

7.4
70 14.7
50 20.8
30 26.1
20 18.8
74 17.7
10 1.0
40 +9.2
60 60.5
80 +23.0
80

198.55

188.2 178.8 173.5 168.6 172.5 175.4 176.2 190.8 201.8 214.0

0.6
70 10.0
55 15.3
30 20.2
20 76.3
15 13.4
18 12.6
40 +2.0
60 +13.0
80 +25.2
80

188.3 174.5 170.0 159.8 164.3 171.3 172.7 184.4 187.8 200.8

0.5
80 14.0
80 18.8
35 19.0
27 22.5
15 21.5
74 17.5
18 16.1
45 4.4
60 1.0
80 +12.0
80

183.2 172.5 164.8 162.8 170.9 170.9

5.6
70 16.3
80 24.0
25 26.0
15 17.9
17.9

188.76

					Lt.	B	Pl.	
28+0					227.9	210.1 210.0	220.8 240.7	257.9
					$\frac{3.8}{55}$	$\frac{21.6}{15}$ 21.7	$\frac{10.9}{36}$ + $\frac{9.0}{80}$	+ $\frac{20.2}{100}$
27+50					224.2	244.1 206.9 216.7 206.5	220.0 233.7	243.9
					$\frac{7.5}{40}$	$\frac{17.6}{25}$ $\frac{24.8}{15}$ 25.0 $\frac{25.2}{10}$	$\frac{11.7}{50}$ + $\frac{2.0}{80}$	+ $\frac{13.2}{100}$
TP	12.99	231.66	0.66	218.67		231.66		
27+0					219.8	211.8 203.7 203.5 203.6 215.5	234.4	245.5
					$\frac{10.5}{45}$	$\frac{7.5}{25}$ $\frac{15.6}{10}$ 15.9 $\frac{15.7}{10}$ $\frac{3.8}{40}$	+ $\frac{15.1}{80}$	+ $\frac{26.2}{100}$
TP	12.39	219.33	4.04	206.24		219.33		
26+30					205.6	199.6 200.5		
					$\frac{5.4}{100}$	$\frac{11.4}{35}$ 10.5		
26+06.55	Δ Rt 24° 29'	Taken on Split of Δ			207.9	203.3 198.9 197.9 198.8	220.5 238.6	
					$\frac{3.1}{70}$	$\frac{7.7}{40}$ $\frac{12.1}{20}$ 13.1 $\frac{12.2}{70}$	+ $\frac{9.5}{60}$ + $\frac{17.6}{80}$	
25+40					210.8	199.1 190.9	206.6 225.1 235.0	
					$\frac{0.2}{60}$	$\frac{11.9}{30}$ 20.1	$\frac{4.4}{40}$ + $\frac{16.1}{80}$ + $\frac{24.0}{100}$	
24+75.24	Δ Lt 13° 46'	Taken on Split of Δ			207.6	199.5 193.8 190.3 188.3 190.5 207.0 220.0 232.2		
	210.98				$\frac{3.4}{70}$	$\frac{11.5}{50}$ $\frac{17.2}{20}$ 20.7 $\frac{22.7}{10}$ 20.5 $\frac{4.0}{50}$ $\frac{19.0}{80}$ + $\frac{21.2}{100}$		
						210.98		

31+50

269.4	247.3	234.4	233.8	239.2		256.9	291.9
+18.5 100'	36 80'	16.5 30'	17.1 10'	11.7		+6.0 40'	+4.0 100'

31+17.44 A.P.H. 7'58" Taken on Split of A

248.8	231.9	230.4	234.5	254.9	279.1	291.9
21 80'	19.0 30'	20.5 25'	16.4	+4.0 40'	+28.2 80'	+41.0 100' 5/16"

TP 12.00 250.85 1.77 238.85

250.85

30+50

242.6	234.5	227.5	229.6	246.6	267.1	273.1
+2.0 80'	61 45'	12.1 20'	11.0	+6.0 40'	+21.5 80'	+22.5 75'

30+10

236.8	226.3	225.5	231.7	239.6	257.1	265.6	275.6
3.8 55'	14.3 38'	15.1	8.9 10'	10 30'	+16.5 55'	+25.0 80'	+35.0 75'

TP 12.05 240.62 3.09 228.57

Top of Iron
Fence Post
29148

240.62

29+50

225.4	220.7	223.7	221.6	240.7	258.7
6.3 80'	11.0 30'	8.0	10.1 8'	+9.0 40'	+27.0 80'

29+0

227.8	217.8	218.3	220.4	239.7	261.7
29 80'	129 30'	13.3	11.2 10'	+8.0 40'	+30.0 80'

28+38.27 A.P.H. 3'58"

231.66

230.1	213.5	214.5	228.1	242.7	253.8 209.6
1.5 60'	18.7 25'	17.2	3.1 40'	+11.0 80'	22.1 + ? 100'

231.66 ✓

34+85

TP 12.06 285.04 1.18 272.98

34+80

34+0

33+51.94 Δ Lt 28° 51' Takt on Split of A

33+0

TP 12.05 274.16 0.63 262.11

TP 12.13 262.74 0.24 250.61

32+50

32+0

250.85

LI								RI
291.5	279.0	269.5	282.7	286.0				
+6.5 90	6.0 45	15.5	2.3 35	+1.0 45				
		285.04						
290.7	280.2	261.6	258.7	268.8	282.2	291.2		
+16.5 125	+6.0 100	12.6 50	15.5 15	10.4	+8.0 40	+1.0 45		
281.2	260.6	254.0	252.7	255.6	270.7	281.2	289.2	
+7.0 100	12.6 50	20.2 50	21.5 15	18.6	3.5 40	+7.0 60	+15.0 80	
287.8	277.2	265.5	249.7	251.5	273.5	292.7		
+13.6 125	+3.0 100	8.7 70	21.5 35	22.7	0.7 45	+12.5 45		
280.2	246.2	244.1	250.2	270.6	292.2			
+5.0 100	28.0 35	30.1 15	24.0	3.6 40	+18.0 80			
				274.16				
273.9	250.6	242.7	241.6	247.5	265.4	291.9		
+23.0 100	0.3 50	8.2 35	9.3 20	3.4	+14.5 40	+4.0 90		
274.1	248.5	238.8	238.3	241.1	261.0	291.9		
+23.2 100	2.4 50	12.1 35	12.6 5	9.8	+10.1 40	+4.0 45		
			250.85					

BM

282

312.02

S.F.B.P.
Tillery
Cleveland
312.02

TP

5.85

314.84

0.10

308.99

TP

12.74

309.09

0.21

296.35

35723.68 = H.L. Maryland Taken on H.L. Maryland

TP

12.04

296.56

0.52

284.52

285.04

293.2

292.0

292.2

292.8

293.3

3.9
1504.6
1004.4
50

3.8

5.3
50

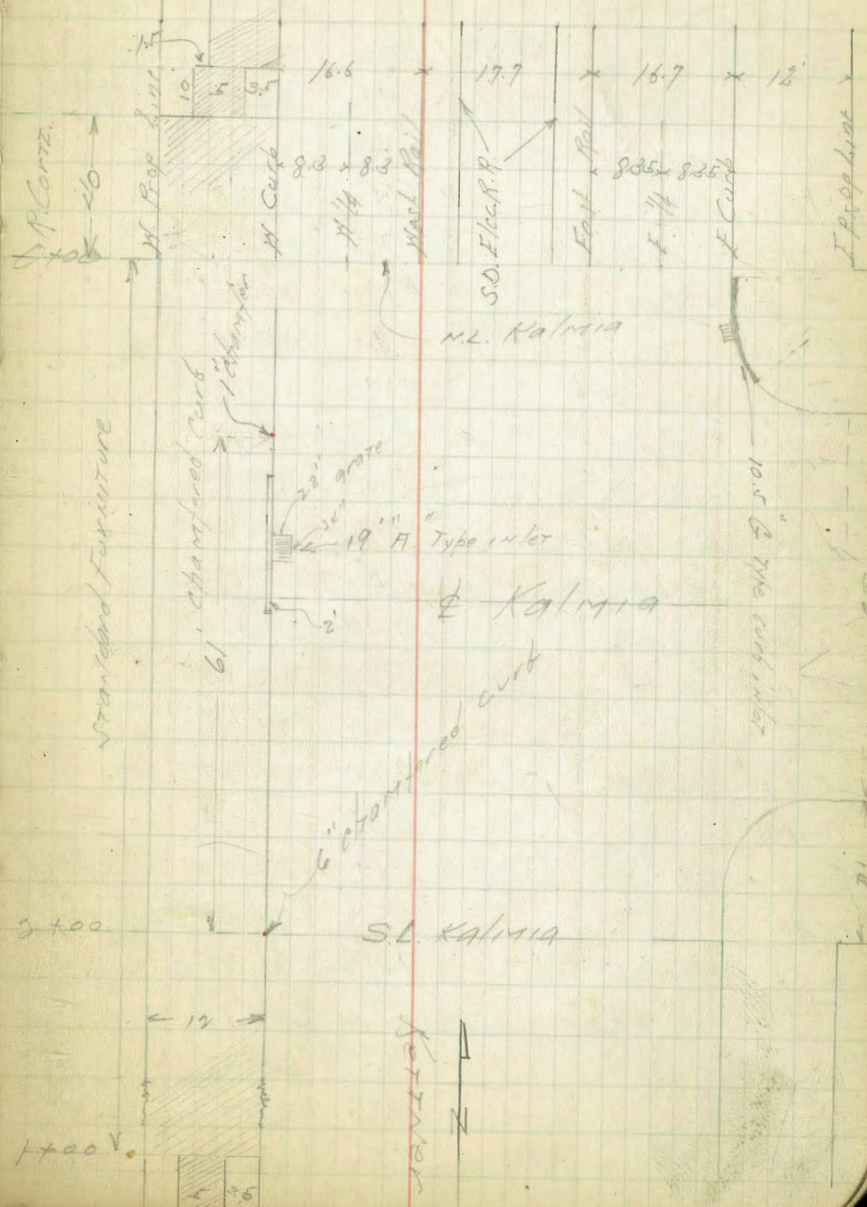
296.56

Cross Section Kettner Blvd.
200' S of S.L. Kalmia to 200' N of N.L. Kalmia
150

Nov. 3. 23
Mason
Supt
Kettner Blvd
40

BM	10.87	29.38	29.02	N.W.S.P. Jupiter + Kettner Blvd
200' S of S.L. Kalmia = 0400				
W Top cb		10.18	29.21	
W gut		10.61	28.78	
W 1/4		9.73	29.66	
W rail		9.26	30.13	
E "		9.07	30.32	
E 1/4		8.85	30.54	
E gut		8.99	30.40	
E cb		8.20	31.19	
0425				
E cb		8.10	31.29	
E gut		8.92	30.47	
E 1/4		8.88	30.51	
E rail		9.01	30.38	
W "		9.20	30.19	
W 1/4		9.65	29.74	
W gut		10.55	28.84	
W cb		10.07	29.32	
0450				
W cb		9.97	29.42	
W gut		10.45	28.94	
W 1/4		9.57	29.82	
W rail		9.13	30.26	
E "		8.97	30.42	

NOTE:
W 1/4 = Midway between
W of W rail of W track
W of E rail of E track
E 1/4 = Midway between
E of W rail of W track
E of E rail of E track



39.39

E 1/2	8.87	30.52
E quit	8.86	30.53
E cb	7.99	31.40
E cb	7.95	31.44
E quit	8.78	30.61
E 1/2	8.73	30.66
E rail	8.93	30.46
W "	9.09	30.30
W 1/2	9.53	29.86
W quit	10.45	28.94
W cb	9.98	29.41
W cb	9.99	29.40
W quit	10.44	28.97
W 1/2	9.52	29.87
W rail	9.05	30.34
E rail	8.88	30.51
E 1/2	8.65	30.74
E quit	8.72	30.65
E cb	7.86	31.53
W quit	10.40	28.99
W cb	9.91	29.43
W L	9.61	29.78

0775

1700 = full in' width Cen. Side walk or

1706 = S edge drive in

also SE of Standard Furniture Co. Plant

West

39.39

41

W quit	10.41	28.98
W W	9.94	29.45
W W = W.L.	9.61	29.78
W quit	10.37	29.02
W W	9.90	29.49
W.L.	9.57	29.82
W quit = cb drive	10.37	29.02 on paving
W 1/2	9.47	29.92
W rail	9.02	30.37
E rail	8.82	30.57
E 1/2	8.61	30.78
E quit	8.65	30.74
E cb	7.79	31.60
W quit	10.31	29.08
3 W	9.94	29.47
W L	9.62	29.77
W quit	10.32	29.07
3 W	9.81	29.58
W L	9.52	29.87

1705

1719 = E 10.5 wide entrance to house

7725

1735 = 10.5 wide entrance to house

145

W cb	993	29.46
W gut	10.33	29.06
W 1/4	9.4v	29.97
W rail	89v	30.47
E rail	8.77	30.62
E 1/4	8.6v	30.77
E gut	8.61	30.78
E cb	7.73	31.66

1455

E gut	8.60	30.79
E cb	7.7x	31.65
3.5 E wedge walk	7.73	31.66

1766 = S edge of drive in

W gut	10.30	29.09
" cb	9.86	29.53
W.L.	9.66	29.73

1768

W gut	10.2v	29.16
2 W	9.78	29.61
W.L.	9.63	29.76

1771 = 2 5' wide driveway to plant

W gut	10.20	29.19
+3	9.79	29.60
W.L. entrance	9.61	29.78

1776 = S.L. of drive in to plant

-10 W.L. slopes down to plant	11.16	28.23
	10.0v	29.35
+3	9.69	29.70
+9	9.79	29.60
W gut	10.17	29.22
W 1/4	9.53	29.86
W rail	8.83	30.56
E rail	8.7v	30.67
E 1/4	8.63	30.76
E gut	8.61	30.78
E cb	8.33	31.06
+3.5 wedge walk	7.9v	31.47

1788

E gut	8.58	30.81
E cb	8.3v	31.04
+3.5 wedge walk	7.96	31.43

1795 W.L. of drive in to plant

W gut	10.3v	29.07
+3	9.89	29.50
+9	9.69	29.70
W.L.	9.93	29.46

10 W of W.L. in drive 11.13 28.26 slopes down

1798 Wedge of curb drive in

W gut	10.37	29.02
W cb	10.03	29.36
+3	9.58	29.81

WL	9.16	30.23	
2+00 = SL Kalmia St			80' wide
W Top of 6" chartered curb	9.08	30.31	14' cts
W gut	10.37	29.02	13' 1/2 cts
W 1/4	9.67	29.72	
W rail	8.80	30.59	
E rail	8.58	30.81	
E 1/4	8.53	30.86	
E gut	8.57	30.82	
E cb	7.94	31.45	
3' N of SL of Kalmia = 1/2" wide doorway ^{to plant}			
W gut	10.41	28.98	
W cb	9.14	30.27	
W L entrance	8.95	30.44	
Set Kalmia			
W cb	9.20	30.19	
W gut	10.44	28.95	
W 1/4	9.63	29.76	
W rail	8.78	30.61	
E rail	8.61	30.78	
E 1/4	8.45	30.94	
E cb line NOT gutter	8.47	30.92	
4' SE of last rod = gut	8.51	30.88	
" " = top of return	7.88	31.51	= 1/2" return
1/4" on Kalmia			
E cb line paving	8.48	30.91	

E 1/4	8.50	30.89	
E rail	8.65	30.74	
W rail	8.77	30.62	
W 1/4	9.71	29.68	
W gut	10.50	28.89	
W cb	9.30	30.09	
1/4 + 11 = S end of inlet opening			
W gut	10.55	28.84	
Top of opening	10.05	29.34	
W cb	9.38	30.01	
1/2" Kalmia			
W cb	9.27	30.12	
W gut	10.57	28.82	
W 1/4	9.78	29.61	
W rail	8.78	30.61	
E "	8.69	30.70	
E 1/4	8.53	30.86	
E cb line paving	8.51	30.88	
1/2" = 1/2" inlet grating 24" x 28" sq.			
W. flowline bot. of box	13.04	26.37	and 18" Cor. 1 P.P.
on grating	10.66	28.73	
Top opening	10.05	29.34	
W " cb	9.31	30.08	
1/4" Kalmia			
W cb	9.37	30.02	
W gut	10.49	28.90	

39.39

w 1/4	9.71	29.68
w rail	8.77	30.62
E rail	8.70	30.69
E 1/4	8.59	30.88
E. cb line opening	8.75	30.64
1/4 + 4 = N edge inter opening		
w gut	10.40	29.99
Top opening	9.85	29.54
" w/cb	9.40	29.99
1/4 + 8 = N edge chamfered curb		
w gut	10.36	29.05
" Top curb	9.39	30.00
N. cb of Kalmia		
w cb	9.41	29.98
w gut	10.27	29.12
w 1/4	9.46	29.93
w rail	8.72	30.67
E rail	8.62	30.77
E 1/4	8.65	30.74
E. cb line	9.00	30.39
1/4 N.E. of last rod = gut of return	9.31	30.08
Top + 1/2 of return	8.38	31.01
N. cb + 6		
w gut	10.27	29.12
" cb	9.41	29.98

39.39

N. cb + 10.5		
w gut	10.25	29.14
" cb	9.88	29.51
N.L. Kalmia = 0+00 = N.L. Standard Furn. Co.		
w Top cem curb wall	9.05	30.34
" " sidewalk	9.32	30.07
w cb	9.81	29.58
" gut	10.22	29.17
w 1/4	9.31	30.08
w rail	8.73	30.66
E rail	8.61	30.78
E 1/4	8.66	30.73
E gut	8.90	30.49
E. cb Top return	7.95	31.44
0+03		
w gut	10.17	29.22
" cb	9.73	29.66
N.L. on sidewalk	9.50	30.09
" " Top cem wall	8.60	30.79
0+15 = 1/2 of entrance to R. Court Co.		
N.L. - 7.5	8.25	31.04
w/L Top wall	8.61	30.78
" on sidewalk	9.24	30.15
w cb	9.65	29.74
w/gut	10.17	29.22
w 1/4	9.15	30.24

44

and 1/2 of
R. Court Co.
2009

3939

0+15

W rail	8.70	30.69
E rail	8.55	30.84
E 1/4	8.59	30.80
E gut	8.93	30.46
" cb	8.27	31.12
+ 2.5 wedge walk	8.03	31.36
0+25		
- 2.5	8.08	31.31
E cb	8.34	31.05
" gut	8.94	30.45
" 1/4	8.57	30.82
" rail	8.46	30.93
W rail	8.62	30.77
" 1/4	9.06	30.33
" gut	10.01	29.38
" cb	9.55	29.84
0+28 = N end wall of H.L.		
W L Top wall	8.45	30.94
" on sidewalk	9.11	30.28
W cb	9.53	29.86
" gut	9.97	29.42
0+33 = 1/2 of 8.6 wide curb drive in W		
W gut	9.85	29.51
" cb	9.50	29.89
W L on sidewalk	9.12	30.27
+ 08 " drive in	10.11	29.28

to Cord's hardware house

3939

45

0+40 = N end full in width walk		
W L on sidewalk	9.08	30.31
W cb	9.21	29.98
" gut	9.87	29.52
" 1/4	8.91	30.48
" rail	8.52	30.87
E rail	8.41	30.98
E 1/4	8.43	30.96
" gut	8.81	30.58
" cb	8.18	31.21
+ 3.5 W. edge walk	7.82	31.57
0+50		
- 3.5	7.74	31.65
E cb	7.96	31.43
" gut	8.60	30.79
" 1/4	8.38	31.01
E rail	8.34	31.05
W "	8.47	30.92
W 1/4	8.81	30.58
W gut	9.84	29.55
W cb	9.38	30.01
+ 3.5 edge walk	9.25	30.14
77 " "	9.15	30.24
78.5 " "	9.13	30.26

see sketch

39.39

0+64 broken curb east			
E cb - 3.5	7.57	31.82	
E ct	7.47	31.92	
E gut	8.24	31.15	
0+75			
- 3.5 edge walk	7.44	31.95	
E cb	7.37	32.02	
" gut	8.18	31.21	
" 1/4	8.07	31.32	
" rail	8.25	31.14	
W rail	8.34	31.05	
W 1/4	8.67	30.72	
" gut	9.62	29.77	
" cb	9.13	30.26	
1+00			
W cb	8.98	30.41	
" gut	9.47	29.92	
" 1/4	8.57	30.82	
" rail	8.21	31.17	
E "	8.14	31.25	
" 1/4	7.95	31.44	
" gut	8.03	31.36	
" cb	7.77	32.12	
+ 3.5	7.17	32.22	

39.39

46

1+25			
E cb	7.20	32.19	
" gut	8.00	31.39	
" 1/4	7.88	31.51	
" rail	8.02	31.37	
W "	8.09	31.30	
" 1/4	8.45	30.94	
" gut	9.30	30.09	
" cb	8.80	30.59	
1+50			
W cb	8.67	30.78	
" gut	9.12	30.27	
" 1/4	8.48	31.11	
" rail	8.04	31.35	
E "	7.82	31.57	
" 1/4	7.71	31.68	
" gut	7.85	31.54	
" cb	7.08	32.31	
T.P. 5+03	38.86	576	33.63

Cross section of Kalmia
Kettner east

30' wide
14' cb
13' 1/4"

38.86

47

	38.86		
N.E. Return Kalmia & Ket.			
N.L. Kalmia & Ecb Ket = 0700			
gut	8.36	30.50	
cb	7.44	31.44	
0+01 = N end opening			
gut	8.40	30.46	
top opening	7.88	30.98	
" cb	7.46	31.40	
0+05 & grate			
flowline bot. box	13.61	25.25	24" pipe
grating	8.58	30.28	
top opening	8.05	30.81	
" cb	7.63	31.23	
0+11.5 S end opening under			
gut	8.79	30.07	
top opening	8.28	30.58	
" cb	7.86	31.00	
0+16.5			
gut	8.61	30.25	
curb	7.95	30.91	
0+22 = EL Kettner & Ncb Kalmia 100			
gut	8.50	30.36	
top return curb	8.02	30.84	
" curb to east	7.56	31.30	

N 1/4	8.01	30.85	
C	7.51	31.35	
S 1/4	7.60	31.26	
S gut	7.93	30.93	
S cb	7.46	31.40	
25' E			
S cb	6.29	32.57	
S gut	6.88	31.98	
S 1/4	6.56	32.30	
C	6.43	32.43	
N 1/4	6.63	32.23	
N gut	7.01	31.85	
N cb	6.28	32.58	
T.P. 531	38.94	5.23	33.63
check to BM.	992	29.02	29.02

X Sec. Russ Blvd.
 from 24th to 26th Sts.
 60' Wide - 10' cbs - 10' 1/4s.
 S. Line = S. line Balboa Park.

12-21-33
 Miller
 Walker
 Bliss

Indexed
 c.s.k.

209.04

709.04
 6.2

48

Only Trees 6" in Diameter and larger Located.

"A" = Acacia Tree
 "E" = Eucalyptus Tree
 Pine = Pine Tree
 Pep. = Pepper Tree
 "P" = Palm Tree

B.M. B.P.	8.57	205.49		196.92	
Set B.M. B.P.	4.00	209.04	0.45	205.04	
26 th St. Walk Curb + Pavmt. to S. line Park					
" " 60' Wide - 10' Cbs - 10' 1/4s.					
E. cb. line 26 th St.					
S. on	emt. cb.	5 line Park.	$\frac{209.04}{5.95}$	203.09	X
S	gutter	pavmt.	6.70	202.34	X
+10	cb.		6.6	202.4	X
+20	1/4.		6.7	202.3	X
+30	cb.		7.0	202.0	X
+40	1/4		7.0	202.0	X
+50	cb.		7.1	201.9	X
+60	N.		7.0	202.0	X
		E. 1/4			
N			7.0	202.0	✓
cb			6.9	202.1	✓
1/4			6.8	202.2	✓
cb			6.6	202.4	✓
1/4			6.4	202.6	✓

cb					
S. on pav.					
					6.15
					202.89
					✓
					5.85
S. on pav.					203.19
cb					✓
1/4					6.1
					202.9
					✓
1/4					6.3
					202.7
					✓
cb					6.5
					202.5
					✓
1/4					6.7
					202.3
					✓
cb					7.0
					202.0
					✓
N.					7.3
					201.7
					✓
					7.4
N					201.6
					✓
cb					7.2
					201.8
					✓
1/4					7.0
					202.0
					✓
cb					6.9
					202.1
					✓
1/4					6.7
					202.3
					✓
cb					6.3
					202.7
					✓
S. on Pav.					6.12
					202.97
					✓
					5.94
S. on N. End emt. cb.					203.10
					✓
S. on pav. gutter					6.58
					202.46
					✓
cb					6.8
					202.24
					✓
1/4					7.2
					201.9
					✓
cb					7.7
					201.3
					✓
1/4					8.2
					200.8
					✓
cb					8.8
					200.2
					✓
N.					8.8
					200.2
					✓

209.04

0+00 = W. line 26th St.

N	209.04 8.5	100.5	✓
el. = s.w. edge present Rd.	8.9	100.1	✓
1/4	7.7	101.3	✓
ϕ	7.0	101.0	✓
1/4	6.7	101.3	✓
el	6.4	101.6	✓
S.	5.8	103.4	✓

0+06

33' N. of S. "A" 12" Diam.

0+25

S	6.1	101.9	✓
+2	7.1	101.9	✓
el	6.9	101.1	✓
1/4	7.1	101.9	✓
ϕ	7.3	101.7	✓
1/4	8.2	100.8	✓
el	8.2	100.8	✓
N	8.6	100.4	✓
+2 = s. edge Present Rd.	8.8	100.4	✓

0+36

26' N. of S. line "C" 14" Diam.

0+39

S. on s.e. Cor. cmt. walk	6.85	101.9	✓
2.5' N. = N. 2. Cr " "	6.90	101.1	✓

This walk extends to 0+50

209.04

Russ Blvd

49

0+41.5 209.04 over catch	7.4	101.6	✓	Top.
3.3 N. of S. ctr 1.5x1.5 Grating Basin	8.2	100.8	✓	F.L. 6" Pipe outlet
over catch	7.5	101.5	✓	Top.
19.2 N. of S. ctr 1.5x1.5 Grating Basin	9.05	199.99	✓	F.L. 8" Pipe outlet To North
0+50				
N-2 = s. edge Present Rd.	8.0	101.0	✓	
N	8.0	101.0	✓	
el	7.7	101.3	✓	
1/4	7.7	101.3	✓	
ϕ	7.3	101.7	✓	
1/4	7.0	101.0	✓	
el	6.9	101.1	✓	
+6.3	6.46	101.58	✓	on cmt. el.
+7.5	6.30	101.7	✓	on " "
	6.80	101.2	✓	on walk to E
	6.72	101.3	✓	" " " E
S.	5.41	103.63	✓	on cmt. el.

0+69.

0+67.6

0+62 ϕ Drive

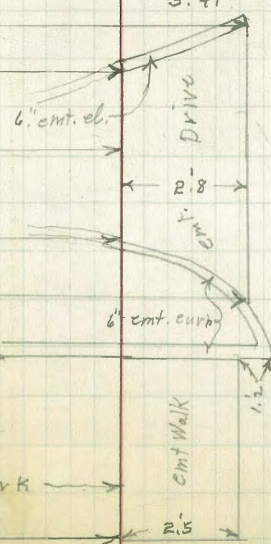
0+56.4

0+55

0+50

0+39

S. line Park



210.23

1718 210.23

5-12.8 = Garage 4.90 205.33 ✓ on ent. floor

S. on & ent. drive 5.75 204.48 ✓

+3' N = N. End. ent. Drive 4.05 204.18 ✓

1725

S. 5.5 204.7 ✓

cl 6.0 204.2 ✓

1/4 5.7 204.5 ✓

+7' "E" Tree 24" Diam 5.5 204.7 ✓

♀ 5.8 204.4 ✓

1/4 5.9 204.3 ✓

cl 5.9 204.3 ✓

N 5.7 204.5 ✓

+7 = S. edge present Rd 5.7 204.5 ✓

1733

33' N of S. 8" E. Tree 5.5 204.7 ✓

1735

24' N of S. 24" E. Tree 5.8 204.4 ✓

1737

25' N of S. 10" E. Tree 5.9 204.3 ✓

1742

25' N of S. 6" E. Tree 5.9 204.3 ✓

43' N of S. 8" E. Tree 5.7 204.5 ✓

1749

36' N of S. 8" E. Tree 5.7 204.5 ✓

210.23

Russ Blvd

51

1750 210.23

N. 3.8 206.4 ✓

cl 3.6 206.6 ✓

1/4 3.6 206.6 ✓

♀ 3.7 206.5 ✓

1/4 3.8 206.4 ✓

cl 4.2 206.0 ✓

S. 3.4 206.8 ✓

1752

46' N of S. 8" E. Tree

1756

33' N of S. 6" E. Tree

1762

49' N of S. 12" E. Tree

1771

24' N of S. 6" E. Tree

→ out of place 1776

30' N of S. 6" E. Tree

38' N of S. 6" E. Tree

1775

210.23

S. 1.1 209.1 ✓

cl 1.7 208.5 ✓

1/4 1.8 208.4 ✓

+2 0.9 209.3 ✓

♀ 0.7 209.5 ✓

1/4 0.8 209.4 ✓

cl 0.7 209.5 ✓

N 0.5 209.7 ✓

210.20

26' N of S. 15" E. Tree
1781

1783

58' N of S. 18" E. Tree

T.P. 9.20 218.93 0.50 209.73

1786 = Garage on S.

~~218.93~~

N. 8.1 210.8 ✓

cb 8.1 210.8 ✓

1/4 8.1 210.8 ✓

4 8.2 210.7 ✓

+9 8.4 210.5 ✓

1/4 9.2 209.7 ✓

cb 9.2 209.7 ✓

+9.5 = 0.5 in st. emt. floor. 8.86 210.07 ✓

1790

55' N of S. 8" E. Tree

25' N of S. 6" E. "

1794

30' N of S 6" E. Tree

1795

57' N of S. 8" E. Tree

1796

52' N of S. 6" E. Tree

1799

25' N of S. 6" E. Tree

218.93

~~218.93~~

Pruss Bnd.

52

2+00

S+0.3 = 0.3 in st. N side shed. 6.0 212.9 ✓

S+6 6.3 212.6 ✓

cb 7.5 211.4 ✓

1/4 7.6 211.3 ✓

+1 6.7 211.7 ✓

4 6.7 211.7 ✓

1/4 6.8 211.1 ✓

cb 6.8 211.1 ✓

N 6.9 211.0 ✓

2+05

27' N of S. = 6" E. Tree

2+10

32' N of S. = 12" E. Tree

~~218.93~~

2+18 4 garage on S. Line emt. floor

S. on emt. floor 4.27 214.66 ✓

2+21

38' N of S. 8" E. Tree

2+25

N 4.3 214.6 ✓

cb 4.1 214.8 ✓

1/4 3.7 215.7 ✓

4 3.8 215.1 ✓

+9 3.9 215.0 ✓

1/4 4.5 214.4 ✓

cb 4.1 214.8 ✓

S. 3.3 215.6 ✓

218.93 218.93

2+27 = 1/2 Garage on S. line cmt. floor
S. on floor. 3.31 ~15.62 ✓

2+34

49' N. of S. 18" Pine Tree

2+50

59.5' N. of S. 20" Pine Tree

2+50

S 2.8 ~16.1 ✓

+8 on P.O.T. Hub. 3.01 ~15.92 ✓

el 3.0 ~15.9 ✓

1/4 2.9 ~16.0 ✓

+4 2.4 ~16.5 ✓

1/2 2.4 ~16.5 ✓

1/4 2.4 ~16.5 ✓

el 2.4 ~16.5 ✓

N 2.3 ~16.6 ✓

2+6B

39' N. of S. line = 18" Pine Tree.

S. line at E. End. 4. garages
2+72 = 1/2 Garage on South cmt. floor
2+75 ~15.7 ✓ dirt floors
215.37 This is the only
one of the 4 garages
on line above, with cmt. floor.

S. 3.5 ~15.4 ✓

el 3.9 ~15.0 ✓

1/4 4.0 ~14.9 ✓

+4 3.2 ~15.7 ✓

1/2 3.1 ~15.8 ✓

1/4 3.0 ~15.9 ✓

el 2.8 ~16.1 ✓

N. 2.7 ~16.2 ✓

218.93

218.93

Russ. Blvd

2+98 = W. End. of 4 Garages on W.

S. floor 4.5 ~14.4 ✓
2+99.5 = 1/2 con. Walk on South 214.58
This Walk is Not Very good 3+00
apparently slabs of conc. layed on ground

N. 3.8 ~15.1 ✓

el 3.8 ~15.1 ✓

1/4 4.0 ~14.9 ✓

1/2 4.1 ~14.8 ✓

+5 4.3 ~14.6 ✓

1/4 4.8 ~14.1 ✓

el 4.8 ~14.1 ✓

S. 4.9 ~14.0 ✓

3+05

55' N. of S. = 20" Pine Tree

3+25

S 5.5 ~13.4 ✓

el 5.6 ~13.3 ✓

1/4 5.8 ~13.1 ✓

+5 4.9 ~14.0 ✓

1/2 4.8 ~14.1 ✓

1/4 4.9 ~14.0 ✓

el 4.2 ~14.7 ✓

N. 4.2 ~14.7 ✓

3+43

35' N. of S. = 18" Pine Tree

218.93

3+50

218.93

N	5.2	✓13.7	✓
cl	5.2	✓13.7	✓
1/4	5.3	✓13.6	✓
♀	5.6	✓13.3	✓
+5	5.9	✓13.0	✓
1/4	6.6	✓12.3	✓
cl	6.3	✓12.6	✓
S.	6.2	✓12.7	✓

from 3+59 to 3+69 Garage on S. 2'0 in Alley emt floor
2'0 N. of S. emt. floor.

6.60 ✓12.33 ✓

3+70

37' N of S. = 20" Pine Tree

from 3+69 to 4+11 Lattice Fence 2'0 in St.

3+75

S.	6.9	✓12.0	✓
cl	7.3	✓11.6	✓
1/4	7.2	✓11.7	✓
+5	6.5	✓12.4	✓
♀	6.3	✓12.6	✓
1/4	6.2	✓12.7	✓
cl	6.3	✓12.6	✓
N	6.0	✓12.9	✓

3+94

32' N of S. 18" Pine Tree

218.93

Russ. Blvd

4+00 218.93

54

N	6.5	✓12.4	✓
cl	6.5	✓12.4	✓
1/4	6.8	✓12.1	✓
♀	6.8	✓12.1	✓
+6	7.3	✓11.6	✓
1/4	8.0	✓10.9	✓
cl	8.1	✓10.8	✓
S	7.6	✓11.3	✓

4+06

55' N of S. line = 20" Pine Tree

4+25

S.	8.4	✓10.5	✓
cl	8.8	✓10.1	✓
1/4	8.8	✓10.1	✓
+5	7.8	✓11.1	✓
♀	7.8	✓11.1	✓
1/4	7.6	✓11.3	✓
cl	7.6	✓11.3	✓
N.	7.5	✓11.4	✓

T.P. 3.04 212.52 9.45 209.48

4+34

41' N. of S. = 8" Pine Tree

212.52

	4+50	212.52	
N		2.0	✓10.5 ✓
cb		2.2	✓10.3 ✓
"4		2.5	✓10.0 ✓
±		2.7	✓9.8 ✓
+6		2.7	✓9.8 ✓
"4		3.5	✓9.0 ✓
cb.		3.4	✓9.1 ✓
S.		3.2	✓9.3 ✓

4+60

31' N of S. = 8" Pine Tree

4+63

0.5 N. of N. Line = 18" Pine Tree.

4+72 garage on S. end floor 2' Back.

		212.52	
S. - 2'0 floor		4.09	✓08.43 ✓
S. on end apron		4.25	✓08.27 ✓
S+0.8" N. end end Apron		4.31	✓08.21 ✓

4+75

S.		4.6	✓07.9 ✓
cb		4.6	✓07.9 ✓
"4		4.5	✓08.0 ✓
+5		3.9	✓08.6 ✓
±		3.8	✓08.7 ✓
"4		3.5	✓09.0 ✓
cb		3.1	✓09.4 ✓
N.		3.0	✓09.5 ✓

212.52

Russ. Blvd.

4+90

38' N of S. line = 10" Pine Tree

5+00

		212.52	
N		3.7	✓08.8 ✓
cb		3.9	✓08.6 ✓
"4		4.3	✓08.2 ✓
±		4.7	✓07.8 ✓
+7		5.0	✓07.5 ✓
"4		5.4	✓07.1 ✓
cb		5.4	✓07.1 ✓
+4 = N. End end Walk 6' wide		5.13	✓07.39 ✓
S. on 7' " "		5.14	✓07.38 ✓

5+25

S.		5.2	✓07.3 ✓
cb		5.9	✓06.6 ✓
"4		6.0	✓06.5 ✓
+2		5.3	✓07.4 ✓
±		5.4	✓07.1 ✓
"4		5.0	✓07.5 ✓
cb		4.8	✓07.7 ✓
N		4.4	✓08.1 ✓

5+27

40' N. of S. 30" Pine Tree.

5+46

36' N. of S. 10" Pine Tree

55

212.52

5+50 212.52

N	5.7	206.8	✓
cl	5.3	207.2	✓
1/4	5.3	207.2	✓
⊕	5.7	206.8	✓
+8	6.2	206.3	✓
1/4	7.0	205.5	✓
cl	6.7	205.8	✓
S.	5.7	206.8	✓

5+60 = E. Line 25th

S	7.7	204.8	✓
cl	8.0	204.5	✓
1/4	7.6	204.9	✓
+2	6.8	205.7	✓
⊕	6.8	205.7	✓
1/4	6.6	205.9	✓
cl	6.4	206.1	✓
N	6.2	206.3	✓

25th St 100' Wide - 20' cbs - 15' 1/4 s.

5' W. of E. Line

N.	6.6	205.9	✓
cl	6.7	205.8	✓
1/4	7.4	205.1	✓
C	7.7	204.8	✓
1/4	8.0	204.5	✓
cl	8.5	204.0	✓
S.	9.3	203.2	✓

212.52

Russ Blvd.

E. curb line

212.52

S. end of N. End.	7.48	203.04	✓	56
S. gutter pav "	10.01	202.51	✓	
cl	9.1	203.4	✓	
1/4	8.5	204.0	✓	
cl	8.3	204.2	✓	
1/4	8.1	204.4	✓	
cl	7.8	204.7	✓	
N	7.5	205.0	✓	

E. 1/4

N	7.1	205.4	✓	
cl	7.5	205.0	✓	
1/4	7.9	204.6	✓	
⊕	8.3	204.2	✓	
1/4	8.6	203.9	✓	
cl	9.0	203.5	✓	
S. on Mend pav	9.64	202.86	✓	
⊕				
S. on end pav	9.40	203.12	✓	
cl	8.8	203.7	✓	
1/4	8.3	204.2	✓	
⊕	7.9	204.6	✓	
1/4	7.6	204.9	✓	
cl	7.2	205.3	✓	
N	6.9	205.6	✓	

212.52

W. 1/4

212.52

N	8.0	2025	✓
cl	8.2	2043	✓
1/4	8.5	2040	✓
cl	8.6	2039	✓
1/4	8.9	2036	✓
cl	9.1	2034	✓
S. on end pav	9.51	20301	✓

W. cl.

S. gutter	9.98	20254	✓
S. emt. cl	9.49	20303	✓
cl	9.5	20310	✓
1/4	9.3	20311	✓
cl	9.1	20314	✓
1/4	9.0	20315	✓
cl	8.7	2038	✓
N	8.5	20410	✓

0+00 = W. line 25th St.

N	9.0	20315	✓
cl	9.0	20315	✓
1/4	9.2	20313	✓
cl	9.4	2031	✓
1/4	9.3	20311	✓
cl	9.9	2026	✓
S.	9.5	20310	✓
S + 0.5 on curb. Extending to Sta 0+51.8	9.25	20327	✓
T.P.	5.15	207.83	9.83 202.68 ✓

207.83

Russ. Blvd.

207.83

chk BM		5.85	201.98	N.W. 25 th St. 57
T.P.	1.68	204.36	5.15	201.95

0+09

57' N = 30" Pine Tree

0+15

36' N of Sabine = 20" Pine Tree

19.5' " " " = 20" Pepper Tree

0+13.4

204.4

0.7 S. of S. = Top emt. cl Brk 1.05 203.4 ✓

0+25

S - 0.7 on Top emt. cl. 1.83 204.6 ✓

-0.6 2.3 204.1 ✓

S. 2.4 204.0 ✓

cl 3.1 204.3 ✓

1/4 2.2 204.4 ✓

cl 2.2 204.4 ✓

1/4 2.4 204.0 ✓

cl 2.9 204.5 ✓

N. 2.9 204.5 ✓

0+37

31' N. of S. = Pepper Tree

0+49

56' N of S. = 30" Pine Tree

204.36

R+50

204.36

3.0

Y01.3 ✓

N

cl

3.3

Y01.0 ✓

1/4

3.4

Y00.9 ✓

Φ

3.4

Y00.9 ✓

1/4

3.7

Y00.6 ✓

cl

4.3

Y00.0 ✓

S

4.0

Y00.3 ✓

S+0.7 Top emt. cl

3.42

Y00.91 ✓

0+51.8

S-0.7 = { W. end curb
E. edge walk to S.

3.56

Y00.80 ✓

0+55.8

S-0.7 = W. edge walk to S

3.70

Y00.66 ✓

0+73.5

30' N. of S. Line = 36" Pine Tree

0+75

S

5.0

199.3 ✓

cl

5.0

199.3 ✓

1/4

4.8

199.5 ✓

Φ

4.4

199.9 ✓

1/4

4.8

199.5 ✓

cl

4.6

199.7 ✓

N.

4.2

Y00.1 ✓

0+94

S-0.7 = { W. End. W entrance garage
E. side Paved Drive

5.21

199.15 ✓

S-24 on con.

199.20

S-34 " dirt

199.7

S-70 " "

200.7

204.36

Russ. Blvd

1+00

204.36

5.6

198.7 ✓

58

N.

cl

5.8

198.5 ✓

1/4

5.6

198.7 ✓

Φ

5.9

198.4 ✓

1/4

5.9

198.4 ✓

cl

5.5

198.8 ✓

S.

5.6

198.7 ✓

+0.7 on emt. Dr

5.47

198.89 ✓

1+12

43' N. of S. = 24" Pine Tree

1+20

S-0.5 emt. Dr

5.91

198.45 ✓

0.3 N. of S. = curb
12" x 18" catch basin
grating outlet
4" Pipe to N.

6.05

198.31 ✓ Grating

6.53

197.83 ✓ F.L.

1+22

25' N = 36" Palm Tree

1+24

22' N. of S. = outlet 4" Pipe

6.83

197.53 ✓

F.L.

1+25

S-0.5 on emt. dr.

5.83

198.53 ✓

S

5.8

198.56 ✓

cl

5.6

198.7 ✓

1/4

6.2

198.1 ✓

Φ

6.5

197.8 ✓

1/4

6.6

197.7 ✓

cl

6.5

197.8 ✓

N.

6.5

197.8 ✓

204.36

0.4 S. of S. line = { W. edge emt. Dr. 1+30.3
E. side of E. entrance Garage 204.36
5.61 198.75 on emt. Dr
1+31

34' N. of S. = 36" Palm Tree

1+34

57' N. of S. = 24" Pine Tree

T.P. 5.82 204.55 204.55
5.63 198.73

1+43

28' N. of S. line 6" Palm Tree.

1+50

N	8.2	196.3	✓
cl	8.1	196.4	✓
1/4	7.9	196.6	✓
ϕ	7.1	197.4	✓
1/4	6.6	197.9	✓
cl	6.1	198.4	✓
S.	5.7	198.8	✓

1+66

35' N. of S. Line 30" Pine Tree.

1+75

S	5.5	199.0	✓
cl	6.1	198.4	✓
1/4	7.0	197.5	✓
ϕ	7.7	196.8	✓
1/4	8.3	196.2	✓
cl	8.4	196.1	✓
N	7.9	196.6	✓

204.55

Russ Blvd

1+81.3

204.55

2.3 S. of S. Line N. End emt. Walk 5.32 199.73 ✓ 59

1+93 garage on S. emt. floor 1.6 Back

S-1.6 floor 4.87 199.68 ✓

S. on emt. Apron 5.18 199.37 ✓

0.6 N. of S. = N. end Apron 5.27 199.78 ✓

2+00

N. 9.5 195.0 ✓

cl 7.7 196.8 ✓

1/4 8.1 196.7 ✓

7.7 5.6 198.9 ✓

ϕ 6.3 198.0 ✓

1/4 6.1 198.4 ✓

cl 5.4 198.7 ✓

S. 5.4 199.1 ✓

2+05

34' N. of S. = 30" Pine Tree

2+08 Garage on S. emt. floor 1.6 Back

S-1.6 floor 4.90 199.68 ✓

S. on emt. apron 5.06 199.49 ✓

0.8 N. of S. = N. end apron 5.12 199.43 ✓

2+15 5.26 3' Walk

0.8 N. of S. = N. End Walks 5.26 199.29 ✓

2+19.5

16' N. of S. Line 30" Pine Tree.

204.55

2+25

204.55

S	4.9	1996	✓
cl	5.4	199.1	✓
h4	5.6	198.9	✓
±	5.7	198.8	✓
+7	5.9	198.6	✓
h4	7.5	197.0	✓
cl	8.3	196.2	✓
N	8.7	195.8	✓

2+435

19' N of S 16" Pine Tree

2+50

N	7.3	197.2	✓
cl	6.8	197.7	✓
h4	6.1	198.4	✓
±	5.3	199.2	✓
h4	5.0	199.5	✓
cl	5.0	199.5	✓
S	4.5	200.0	✓

2+69

17' N. of S. line 16" Pine Tree

2+75

57' N. of S. line 18" Pine Tree

2+75

S	4.7	199.8	✓
cl	4.8	199.7	✓
h4	4.6	199.9	✓

204.55

Russ Blvd.

204.55

60

±	4.5	200.0	✓
h4	4.6	199.9	✓
cl	5.0	199.5	✓
N	5.6	198.9	✓
2+855 ± 30" Walk on S. 0.5 Back			
S-0.5 = N end walk	5.93	198.62	✓
2+92 ± garage on S. cmt. floor 2.9 Back			
S-2.9 floor	5.76	198.79	✓
S-0.4 N end cmt. apron	6.01	198.54	✓
S	6.0	198.5	✓

3+00

N	5.5	199.0	✓
cl	5.2	199.3	✓
h4	5.3	199.2	✓
±	5.4	199.1	✓
h4	5.6	198.9	✓
cl	6.0	198.5	✓
S	6.1	198.4	✓

3+07 garage on S. Dirt floor 0.3 Back

S-0.3 floor	6.3	198.2	✓
-------------	-----	-------	---

3+10

52' N. of S. line 16" Pine Tree

204.55

3+25

~~204.55~~
7.0

S		197.5	✓
cl	7.0	197.5	✓
14	6.5	198.0	✓
Φ	6.2	198.3	✓
14	6.5	198.0	✓
cl	6.5	198.0	✓
N	6.3	198.7	✓

3+37

62' N of S. line 36" Pine Tree.

35' " " " " 24' " "

3+50

N	7.8	196.7	✓
Φ	7.9	196.6	✓
14	7.9	196.6	✓
Φ	7.8	196.7	✓
14	7.6	196.9	✓
cl	8.0	196.5	✓
S.	8.2	196.3	✓

3+60 Φ Double garage on s. cmt. floor 0.2 Back

S-0.2 floor 8.71 195.84 ✓

3+69

45' N of S. line 24" Pine Tree.

3+70⁵ Φ cmt walk on S.

S-0.2 N. End Walk 9.22 195.33 ✓

204.55

Riiss. Blvd

3+75

~~204.55~~
9.5

S.		195.0	✓	61
cl	9.5	195.0	✓	
14	9.5	195.0	✓	
Φ	9.2	195.3	✓	
14	9.1	195.4	✓	
cl	9.0	195.5	✓	
N.	8.9	195.6	✓	

3+80

24' N of S. line 24" Pine Tree

3+92

58' N of S. line 24" Pine Tree

T.P. 0.17 193.09 11.63 192.92

4+00

~~193.09~~

N	+1.7	194.8	✓
cl	+1.5	194.6	✓
14	+1.1	194.1	✓
Φ	+0.9	193.9	✓
14	+0.9	193.9	✓
cl	+0.9	193.9	✓
S.	+0.6	193.6	✓

4+05 garage on s. cmt. floor 0.1 Back

S-0.1 floor +0.50 193.59 ✓

4+12

28' N of S. line small Palm Tree

193.09

4+25

193.09
0.8

1910

✓

S

el

0.8

1922

✓

1/4

0.8

1922

✓

E

0.6

1924

✓

1/4

0.5

1925

✓

el

0.4

1926

✓

N

0.4

1926

✓

4+50

N

2.0

1910

✓

el

1.9

1911

✓

1/4

1.9

1911

✓

E

2.3

1907

✓

1/4

2.6

1904

✓

el

2.7

1903

✓

S

2.6

1904

✓

4+65

39' N of S. Line 6" Oak Tree

From 4+68⁵ to 4+96⁵ double garage with

apartment above. Built with overhang

Second floor apartment 15.4'3" in st.

emt apron 0.5' in st.

garage front 3.4' back

4+78⁵ garage door

S-3.4 floor

4.15

188.94

✓

0.5' N of S. = N end apron

4.41

188.68

✓

193.09

193.09

Russ Blvd

4+90⁵ garage Door

S-3.4 = floor

4.52

188.57

✓ 62

0.5' N of S. = N end apron

4.73

188.36

✓

5+00

45' N of S. Line 14' Oak Tree

4+75

193.1

S

4.5

188.6

✓

el

4.1

1890

✓

1/4

3.9

1892

✓

E

4.0

1891

✓

1/4

3.3

1898

✓

el

3.4

1897

✓

N

3.4

1897

✓

5+00

N

4.8

1883

✓

el

4.8

1883

✓

1/4

5.4

1877

✓

E

5.4

1877

✓

1/4

5.5

1876

✓

el

5.6

1875

✓

S

5.5

1876

✓

5+08 Garage on S. emt. floor 4.2' back

S- floor

5.42

18767

✓

S. on emt apron

5.85

18724

✓

0.9' N of S. Line N end apron

5.94

18715

✓

5+15 To 5+52. Fence on S. 0.6' in st.

193.09

5+18

32' N of s. line

14" Oak Tree

5+25 193.11

s	7.2	185.9	✓
d	7.0	186.1	✓
h4	6.8	186.3	✓
Φ	7.1	186.0	✓
h4	7.2	185.9	✓
el	7.5	185.6	✓
N	6.6	186.5	✓

5+26

60' N of s. line 12" Oak Tree

5+33

2' N of s. line 5" Logquat. Tree

5+35

40' N of s. line 5" Acacia Tree

5+40

23' N of s. line 6" Fruit Tree

5+50

N	9.0	184.1	✓
el	8.8	184.3	✓
h4	8.9	184.2	✓
Φ	9.1	184.0	✓
h4	9.3	183.8	✓
el	9.6	183.5	✓
s	9.6	183.5	✓

193.09

5+53.6

193.09

Russ Blvd

63

s. on 4. emt. walk

9.75 1853.4 ✓

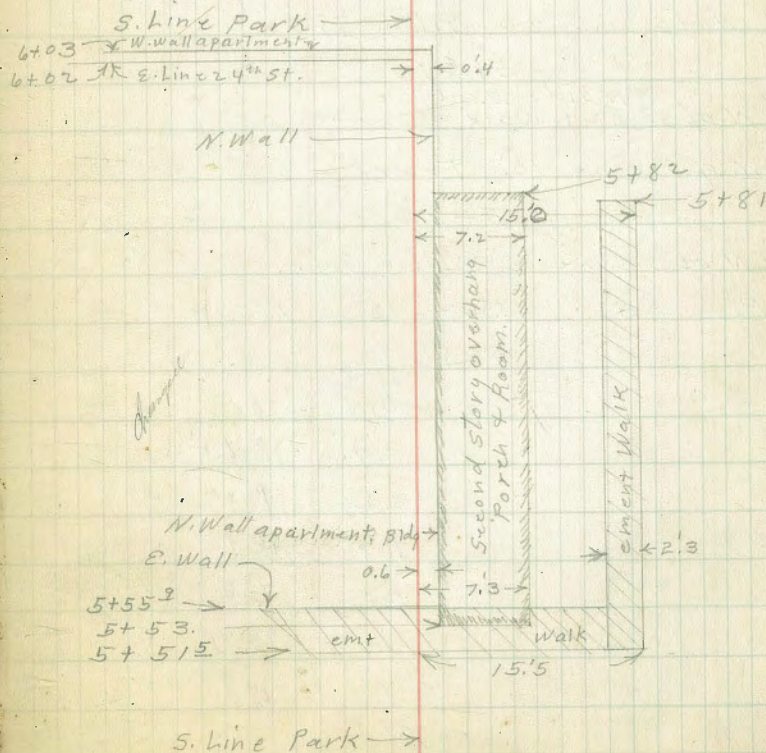
15.5' N. on emt. walk.

10.08 18301 ✓

2.4' N = 12" Apple Tree

5+58

51' N. of s. 14" Oak Tree



193.09

5+75

~~193.1~~

S.	11.8	1813	✓
cl	12.2	1809	✓
+5 N edge emt walk	12.25	18084	✓
1/4	12.2	1809	✓
⊕	11.7	181.4	✓
1/4	11.4	181.7	✓
cl	11.1	182.0	✓
N.	11.3.	1818	✓

5+79

24' N of S. line 20" Willow Tree

5+81

15' N of S. line ^{S. side w. end} emt. walk

40' N. of S. line 10" Tree

5+86

27' N of S. line 16" Willow Tree

T.P. 0.71 181.50 12.30 180.79

5+86 ~~181.5~~

N	0.4	181.1	✓
cl	0.9	1806	✓
1/4	1.2	1803	✓
⊕	1.7	1798	✓
1/4	1.7	1798	✓
cl	1.6	1799	✓
S.	1.6	1799	✓

181.50

Russ Blvd

5+99 ~~181.5~~

64

S.	3.1	1784	✓
cl	3.1	1784	✓
1/4	3.1	1784	✓
⊕	2.3	1794	✓
1/4	1.7	1798	✓
cl	1.2	1803	✓
N	1.0	180.5	✓

5+99

5 8' N. of S. Line Italian Cypress Tree

6.000

55' N of S. line 16" Pepper Tree

6+02 - E. Line 24" ^{60' wide} ^{10' dia} ^{10' dia} ^{10' dia}

N.	2.5	1790	✓
cl	2.8	178.7	✓
1/4	3.3	178.7	✓
⊕	3.7	1778	✓
1/4	4.0	177.5	✓
cl	4.3	177.7	✓
S. emt. walk	4.31	177.7	✓
E. cl			
S. on end emt. cl	4.83	176.7	✓
S. gutter Pav	5.56	176.0	✓
cl	4.8	176.7	✓
1/4	4.8	176.7	✓
⊕	4.6	176.9	✓
1/4	4.1	177.4	✓

18150

8. el (con)

181.5

3.9

1776

✓

el

4.0

177.5

✓

N

8' W. of E. el

20' N. of S. Line 48" Palm Tree

3' W. of E. el.

48' N. of S. line 4" Tree

E. 1/4

N

4.1

1774

✓

el

4.9

1766

✓

1/4

5.1

1764

✓

E

5.3

1762

✓

1/4

5.5

1760

✓

el

5.6

1759

✓

S.

pavmt.

5.58

1760

✓

E 24th St.

S. pav.

6.03

175.5

✓

el

6.0

175.5

✓

1/4

5.8

175.7

✓

E

5.6

175.9

✓

1/4

5.3

1762

✓

el

5.1

176.4

✓

N

4.6

1769

✓

6' W of E

46' N. of S. Line 24" Pepper Tree.

18150

W. 1/4

181.5

7.3

1742

✓

65

N

7.8

1737

✓

el

1/4

7.3

1742

✓

E

6.3

1752

✓

1/4

6.3

1752

✓

el

6.2

175.3

✓

S. pav.

6.65

1749

✓

7' W. of W. 1/4

14' N. of S. Line 14" Oak Tree.

W. el

S. on cont. el. vend.

7.00

1745

✓

S. gutter pav

7.42

1741

✓

el

8.4

173.1

✓

1/4

8.3

173.2

✓

E

9.9

1716

✓

1/4

10.5

1710

✓

el

10.1

1714

✓

N

9.6

1719

✓

W. Line 24th St

N

10.1

1714

✓

el

10.4

1711

✓

1/4

11.0

1705

✓

E

11.2

1703

✓

1/4

10.5

1710

✓

el

10.0

1715

✓

S.

7.6

1739

✓

181.50

T.P. 8.70 183.10 7.10 174.40

PM. N.W. 24th + B 3.23 177.87 = 179.88

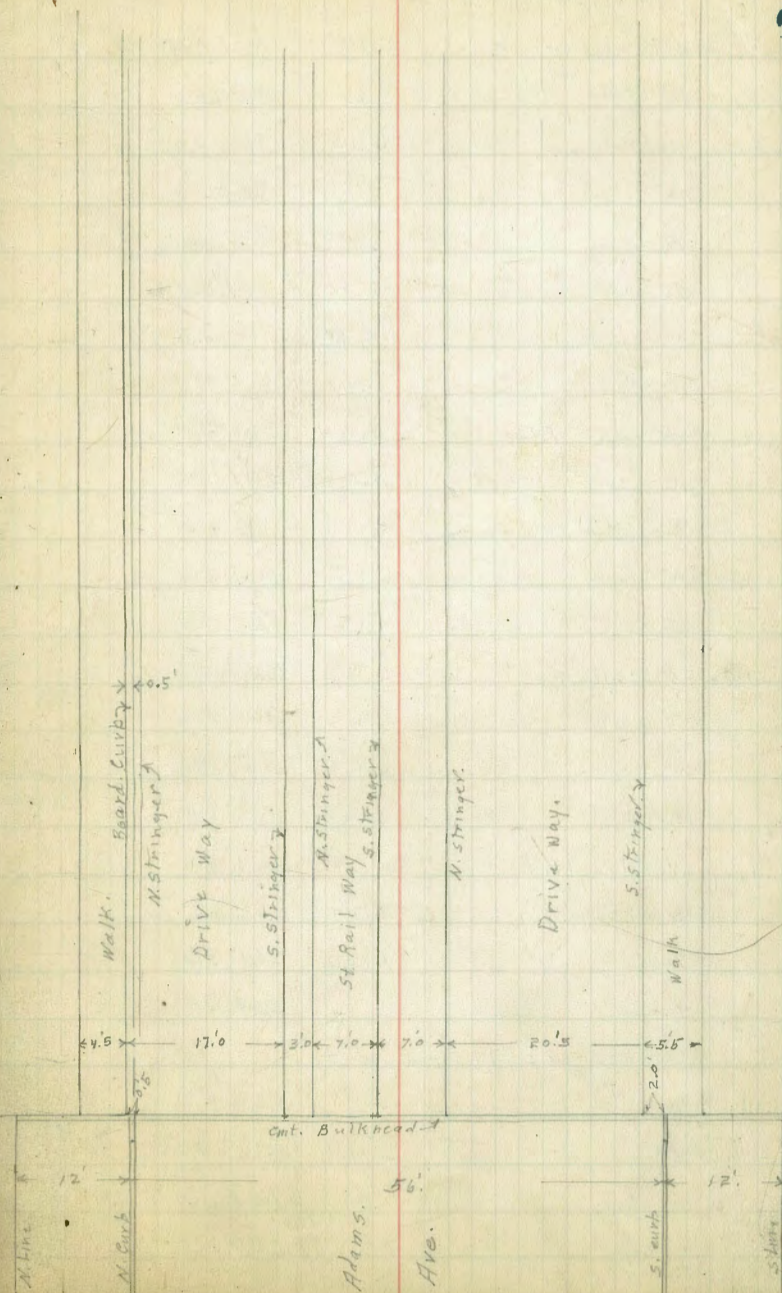
X. Sec. Adams Ave Bridge E. of 39th St.

3-16-34
Miller
Walker
Bliss.

Indexed
cis.K.

57

BM. B.P.	0.18 -	371.05	370.87
T.P.	6.40	367.38	10.07 360.98
		Paymt. at W. End. Bridge	
N. line on cont. Bulkhead.		5.05	362.33
N. cont. el.		5.08	362.30
N. gutter		5.50	361.88
+ 8.5 ft Roadway		5.25	362.13
+ 16.5		5.07	362.31
+ 19.5		5.07	362.31
+ 26.5		5.12	362.26
+ 33.5		4.88	362.50
+ 43.25 ft Roadway		4.88	362.50
+ 54.		4.92	362.46
+ 56 gutter Paymt		5.03	362.35
+ 56 s. el. cont Bulkhead.		5.07	362.31
S. line	" "	5.08	362.30
	0+00 =	{ E. Edge cont. Bulk head. W. end. stringers	
N. Line Boardwalks } N. Walk		5.24	362.14
S. " " " " }		5.24	362.14
N. stringer Rdw.		5.90	361.48
S. " " "		5.90	361.48
N. " " R.R.		5.88	361.52
S. " " " "		5.85	361.53
N. Edge Roadway Board Deck		5.08	362.30
S. " " " " "		5.05	362.33
N. edge walk } S. Walk		5.09	362.30
S. " " " " }		5.12	362.26



367.38

0 + 12.20 Cap #1

N. Walk	{ N. edge Floor	5.84	361.54
	{ S. edge "	5.84	361.54
N. Roadway	{ N. stringer	6.13	361.25
	{ S. "	6.12	361.26
R.R.	{ N. "	6.09	361.29
	{ S. "	6.10	361.28
S. Roadway	{ N. on deck	5.35	362.03
	{ S. " "	5.40	361.98
S. walk	{ N. edge Floor	5.64	361.74
	{ S. " "	5.60	361.78

0 + 22 Cap #2

N. walk	N.	6.15	361.23
	S.	6.16	361.22
N. Roadway	N. stringer	6.43	360.95
	S. "	6.45	360.93
R.R.	N. "	6.43	360.95
	S. "	6.40	360.98
S. Roadway	N. edge deck	5.79	361.59
	S. " "	5.85	361.53
S. walk	N.	6.02	361.36
	S.	6.14	361.24

0 + 44 = Cap #3

N. walk	N.	6.41	360.97
	S.	6.41	360.97
N. Roadway	N. stringer	6.71	360.67
	S. "	7.73	359.65

367.38

68

R.R.	N. stringer	7.84	359.54
	S. "	7.85	359.53
S. Roadway	N. deck	6.15	361.23
	S. "	6.25	361.13
S. walk	N.	6.42	360.96
	S.	6.54	360.84

0 + 60.25 = Cap #4

N. walk	N.	6.75	360.63
	S.	6.72	360.66
N. Rdw.	N. stringer	7.03	360.35
	S. "	7.02	360.36

R.R.	N. "	7.18	360.20
	S. "	7.17	360.21
S. Rdw.	N. deck	6.66	360.72
	S. "	6.65	360.73
S. walk	N. edge	6.80	360.58
	S. "	6.92	360.46

0 + 76.20 = Cap #5

N. walk	N. edge	7.05	360.33
	S. "	7.06	360.32
N. Rdw.	N. stringer	7.34	360.04
	S. "	7.40	359.98
R.R.	N. "	7.49	359.89
	S. "	7.47	359.91
S. Rdw.	N. on Deck	6.91	360.47
	S. " "	6.93	360.45

367.38

0+76.20 = Cap #5 (con)

S. walk	N. edge	7.09	360.29
	S. "	7.27	360.11
		0+92.10 = Cap #6	
N. walk	N. edge	7.42	359.96
	S. "	7.40	359.98
N. Rdw.	N. stringer	7.69	339.69
	S. "	7.65	359.73
R.R.	N. "	7.78	359.60
	S. "	7.78	359.60
S. Rdw.	N. on deck	7.24	360.14
	S. " "	7.25	360.13
S. walk	N. edge	7.43	359.95
	S. "	7.61	359.77
		1+08.10 = Cap #7	
N. walk	N.	7.71	359.67
	S.	7.70	359.68
N. Rdw.	N. stringer	8.02	359.36
	S. "	8.00	359.38
R.R.	N. "	8.04	359.30
	S. "	8.11	359.29
S. Rdw.	N. deck	7.56	359.82
	S. "	7.71	359.67
S. walk	N.	7.90	359.48
	S.	8.08	359.30

367.38

69

1+24.10 = Cap #8

N. walk	N.	8.12	359.26
	S.	8.12	359.26
N. Rdw.	N. stringer	8.41	358.97
	S. "	8.37	359.01
R.R.	N. "	8.39	358.99
	S. "	8.35	359.03
S. Rdw.	N. deck	7.86	359.52
	S. "	8.07	359.31
S. walk	N.	8.21	359.17
	S.	8.37	359.01
		1+40.10 = Cap #9	
N. walk	N.	8.45	358.93
	S.	8.45	358.93
N. Rdw.	N. stringer	8.74	358.64
	S. "	8.71	358.67
R.R.	N. "	8.73	358.65
	S. "	8.67	358.71
S. Rdw.	N. deck	8.09	359.31
	S. "	8.23	359.15
S. walk	N.	8.37	359.01
	S.	8.58	358.80

367.38

1 + 56 = Cap. 10

N. walk	N.	8.74	358.64
	S.	8.74	358.64
N. Rdw	N stringer	9.02	358.36
	S. "	9.01	358.37
RR.	N. "	9.03	358.35
	S. "	9.02	358.36
S. Rdw	N. deck	8.48	358.90
	S. "	8.56	358.82
S. walk	N	8.74	358.64
	S.	8.96	358.42

1 + 76 = Cap. 11

N. walk	N.	9.00	358.38
	S.	9.03	358.35
N. Rdw	N. stringer	9.33	358.65
	S. "	9.32	358.66
RR.	N.	9.34	358.64
	S.	9.33	358.65
S. Rdw	N deck	8.85	358.53
	S. "	8.93	358.45
S. walk	N.	9.14	358.24
	S.	9.27	358.11

367.38

1 + 97 = Cap. 12

N. walk	N.	9.51	357.87
	S.	9.51	357.87
N. Rdw	N stringer	9.81	357.57
	S. "	9.78	357.60
RR.	N "	9.84	357.54
	S. "	9.87	357.51
S. Rdw	N deck	9.31	358.07
	S. "	9.39	357.99
S. walk	N	9.70	357.68
	S	9.87	357.51

2 + 12 = Cap. 13

N. walk	N.	9.80	357.58
	S.	9.81	357.57
N. Rdw	N stringer	10.07	357.31
	S. "	10.06	357.32
RR.	N "	10.18	357.20
	S. "	10.20	357.18
S. Rdw.	N on deck	9.68	357.70
	S. on "	9.73	357.65
S. walk	N	9.88	357.50
	S.	10.07	357.31

70

367.38

2+29^{lb} Cap. # 14

N. walk	N	10.11	357.27
	S.	10.10	357.28
N. Rdw	N. stringer	10.38	357.00
	S. "	10.38	357.00
R.R.	N "	10.49	356.89
	S. "	10.48	356.90
S. Rdw	N. deck	9.89	357.79
	S. "	9.91	357.47
S. walk	N.	10.07	357.31
	S.	10.18	357.20

2+45^{lb} Cap. 15

N. walk	N	10.39	356.99
	S.	10.42	356.96
N. Rdw	N. stringer	10.70	356.68
	S. "	10.80	356.58
R.R.	N "	10.85	356.53
	S. "	10.80	356.58
S. Rdw	N deck	10.09	357.29
	S. "	10.15	357.23
S. walk	N.	10.27	357.11
	S.	10.37	357.01

367.38

2+60^{lb} = Cap. # 16

71

N. walk	N	10.70	356.68
	S	10.70	356.68
N. Rdw	N stringer	10.98	356.40
	S. "	11.00	356.38
R.R.	N "	11.14	356.24
	S. "	11.11	356.27
S. Rdw	N deck	10.41	356.97
	S. "	10.50	356.88
S. walk	N.	10.65	356.73
	S.	10.73	356.65

2+77 = Cap. 17

N. walk	N	11.05	356.33
	S	11.01	356.37
N. Rdw	N. stringer	11.28	356.10
	S. "	11.34	356.04
R.R.	N "	11.47	355.91
	S. "	11.47	355.91
S. Rdw	N deck	10.74	356.64
	S. "	10.74	356.64
S. walk	N	10.86	356.52
	S.	10.85	356.53

367.38

	2+86 ⁴³ W. edge E. Cmt. Bulkhead. on Bridge		
N. Walk	N. Floor	11.15	356.23
	S. "	11.17	356.21
N. Rdw	N stringer	11.48	355.90
	S. "	11.58	355.88
R. R.	N "	11.63	355.75
	S "	11.60	355.78
S. Rdw.	N deck	10.90	356.48
	S. "	10.84	356.54
S. Walk	N. Floor	10.96	356.42
	S. "	10.92	356.46

2+86⁴³ Cmt. Bulk Head

N. on cmt. Bulk head		10.85	356.53
N. edge N. Boardwalk on Bulkhead		10.85	356.53
S. edge N. Rdw	" "	10.81	356.57
N. " RR	" "	10.83	356.55
N. " S. Rdw	Top. Parvt.	10.77	356.61
S. " S. "	on Bulkhead	10.83	356.55
S. line	" "	10.84	356.54

367.38

72

3.30 W. of W. Bulk Head. = End. Existing Rails			
S. Rail		4.95	362.43
N. Rail		4.96	362.42
T.P.	7.78	373.13	2.03
original B.M.			2.25
			370.88 = 370.87

$$\begin{array}{r} 361.52 \\ 356.55 \\ \hline 718.07 \\ 359.03 \end{array}$$

Con. from Book 1448 - P. 80.

Topog. Bk 35 Marilou Park.
for Police Target Range.

indexed
c.s.K.

73

Instrument at B. Ely. Cor. Bk. 35. El 85.65
Azimuth Parallel To E. High St.

station	Azimuth	stadia	Vert. L.	Dist	Diff Elev	
44	206°34'	300.	+0°07'	300.0	+0.60	86.25
45	203°15'	302.	+0°10'	302.0	+0.85	86.51
46	215°41'	246.	-0°46'	246.0	-3.29	82.36
47	216°48'	244.	-1°10'	244.0	-4.95	80.65
48	217°53'	239.	-1°12'	239.0	-5.02	80.63
49	220°02'	230.	-0°37'	230.0	-2.48	83.17
50	207°34'	172.	-0°29'	172.0	-1.45	84.20
51	205°34'	176.	-1°02'	176.0	-3.18	82.47
52	202°49'	184.	-1°05'	184.0	-3.48	82.17
53	201°32'	186.	-0°43'	186.0	-2.33	83.32
54	177°42'	150.	-0°34'	150.0	-1.48	84.17
55	178°40'	144.	-0°55'	144.0	-2.31	83.34
56	179°00'	133.	-1°09'	133.0	-2.67	82.98
57	178°54'	126.	-0°22'	126.0	-0.80	84.85
58	164°17'	139.	-0°34'	139.0	-1.37	84.28
59	164°17'	134.	-1°05'	134.0	-2.53	83.12
60	164°17'	125.	-1°06'	125.0	-2.40	83.25
61	164°17'	117.	+0°13'	117.0	+0.41	84.24
62	164°17'	107.	-0°13'	107.0	-0.40	85.25
63	164°17'	101.	-0°34'	101.0	-0.99	84.66
64	187°30'	111.	-0°56'	111.0	-1.82	83.83
65	187°10'	121.	-0°21'	121.0	-0.71	84.94
66	210°08'	154.	-0°44'	154.0	-1.98	83.67
67	217°04'	171.	-1°10'	171.0	-3.48	82.17

Station	Azimuth	Stadia	Vert L.	Dist		
68	217°-30'	179'	-0°-47'	179.0	-2.44	83.21
69	224°-55'	185'	-0°-54'	185.0	-2.81	82.74
70	238°-17'	171'	-1°-05'	171.0	-3.24	82.41
71	244°-42'	183'	-1°-00'	183.0	-3.20	82.45
72	229°-32'	235'	-0°-51'	235.0	-3.48	82.17
73	250°-36'	184'	-1°-20'	184.0	-4.29	81.36
74	255°-41'	183'	-1°-01'	183.0	-3.25	82.46
75	242°-33'	141'	-1°-02'	141.0	-2.55	83.16
76	241°-35'	154'	-1°-27'	154.0	-3.90	81.75
77	231°-01'	161'	-1°-19'	161.0	-3.70	81.95
78	230°-46'	151'	-1°-09'	151.0	-3.04	82.61
79	223°-04'	173'	-1°-13'	173.0	-3.65	81.97
80	223°-00'	158'	-0°-57'	158.0	-2.62	83.03
81	222°-37'	120'	-1°-12'	120.0	-2.52	83.13
82	197°-37'	94'	-0°-48'	94.0	-1.33	84.32
83	163°-33'	72'	-0°-12'	72.0	-0.25	85.46
84	233°-15'	72'	-0°-50'	72.0	-0.11	85.54
85	233-25	51'	-1°-47'	51.0	-1.58	84.07 Plotted to here
86						
87						
88						

7-11-34
 Miller
 Walker
 Bliss

Police Target Range.

Grades 160's. of N. line
 = S. End. Range.

85.34
 1.70
 83.64

Grade 78.36 BM. Mon & 40th S. line BIK.35.

81.5
 3.9
 5.9
 -2.0

85.34
 85.65 BM. Mon E. End BIK.35.

81.6
 3.8
 5.8
 -2.0

89.52
 85.65 BM. Mon E. End BIK.35.
 Target Pit
 Grade at N. Edge Pit. 10' S. of N. line
 Stake 1' offset. 9'

Top Pit. Bottom Pit.

82.0
 8.4
 5.4
 -2.0

0+00 = E. line 87.31
 5.50
 92.81

82.4
 3.0
 5.1
 -2.1

E. End Pit 87.07
 0+30 W 81.16
 2.45
 2.35
 C.O. 10 F. 1.40 81.62
 8.90
 2.35
 C. 6.01

82.8
 2.6
 4.2
 -1.6

0+55 86.86
 2.66
 2.20
 C.O. 46 F. 1.04 80.62
 8.90
 2.20
 C. 6.76

83.2
 2.2
 3.2
 -1.4

0+70 86.66
 2.86
 2.82
 C. 1.84 80.08
 2.82
 2.65
 C. 9.01

83.6
 1.8
 2.8
 -1.0

Low. PM 86.66
 2.86
 2.82
 C. 1.84 80.08
 2.82
 2.65
 C. 9.01

84.0
 1.4
 2.1
 -0.7

1+05 86.45
 3.07
 2.92
 C.O. 15 F. 1.35 80.20
 7.90
 2.92
 C. 6.70

84.4
 1.0
 1.1
 -0.1

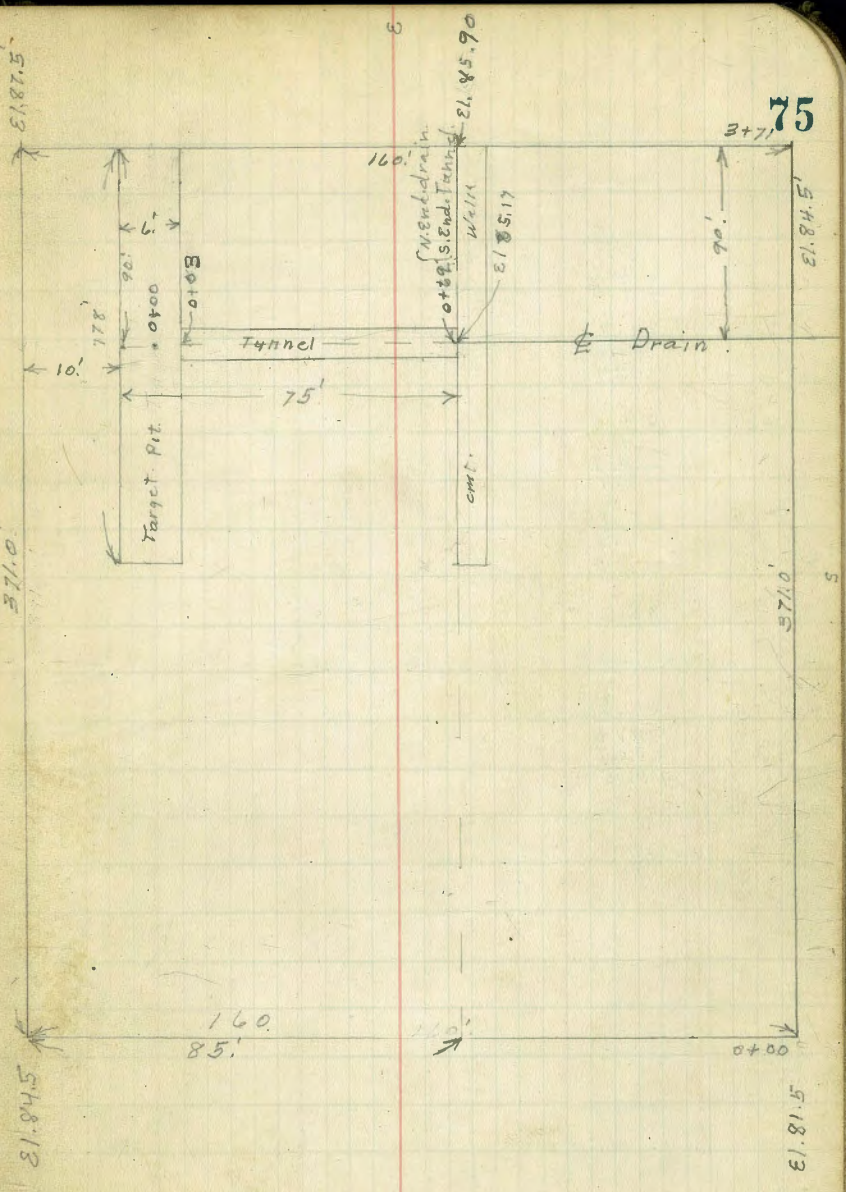
1+30 86.25
 3.27
 2.71
 C.O. 56 F. 0.94 80.05
 9.47
 2.71
 C. 6.76

84.5
 0.9
 1.1
 -0.2

1+55 86.04
 3.49
 3.24
 C.O. 24 F. 1.26 80.20
 7.34
 3.24
 C. 6.10

W. End Pit. 1+78 85.84
 3.68
 3.35
 C.O. 33 F. 1.17 80.34
 7.19
 3.35
 C. 5.83

13.0
 76.5 Wash. outlet Culvert
 85.8
 7
 78.8 Bottom Pit.
 2-3 fall



Police Range

10' s. of N. Line

0+00 = W. Line

84.3
 85.34
 1.70
 83.64
 6.11

0+29

84.5
 5.2
 89.75
 6.11
 83.64
 5.88
 +1.5

0+55

84.7
 5.0
 89.52
 3.87
 85.65 Mon E. Cor B1K35
 5.1
 -0.1

0+80

84.9
 4.8
 89.7
 -0.1

1+05

85.1
 4.6
 89.7
 0.0

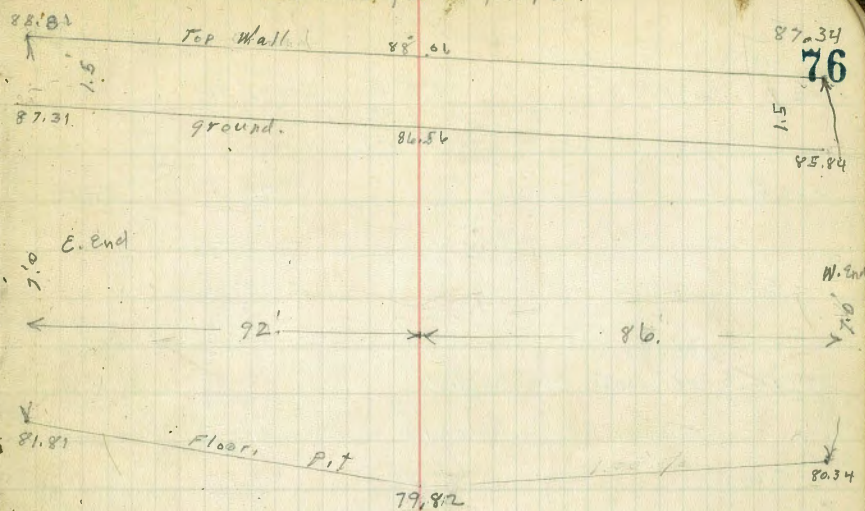
1+30

85.3

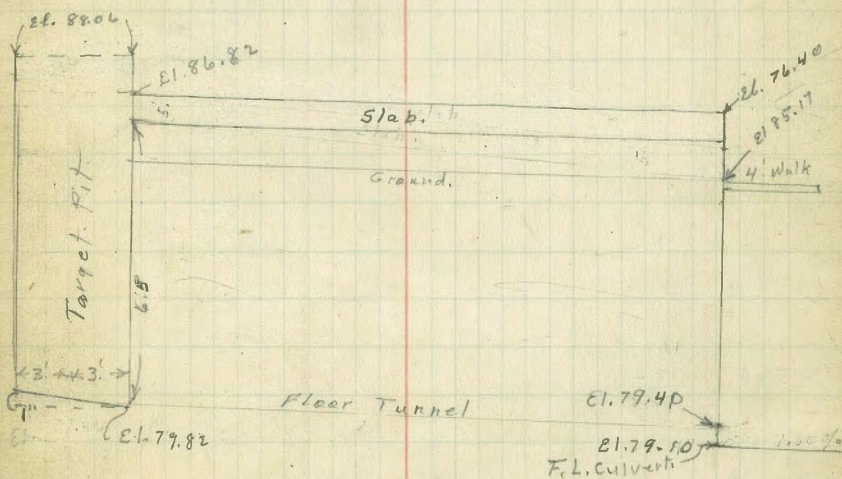
1+55

85.5
 4.2
 89.7
 +0.5

Grades for Target Pit.



Grades for Tunnel 4.5' Headroom.



Grades, Floor Tunnel

s. side

0+03 Target Pit

85.65
1.82
87.47

79.82
7.65
0.64
C. 7.01

0+25

79.69
7.78
1.33
C. 6.45

0+50

79.54
7.93
1.73
C. 6.20

0+72 (W. Edge Walk)

Floor Tunnel

Culvert

79.40
8.07
2.20
C. 5.87

0+72

79.10
8.37
2.20
C. 6.17

1+00

78.93
8.54
2.73
C. 5.81

1+25

78.78
8.69
3.74
C. 4.91

1+50

78.63
8.94
4.43
C. 4.41

1+75

78.48
8.99
4.35
C. 4.64

2+00

78.33
9.14
4.94
C. 4.20

2+25

78.18
9.29
4.94
C. 4.31

2+50

78.03
9.44
4.44
C. 5.00

2+75

77.88
9.59
4.56
C. 5.03

3+00

787.47

77.72
9.75
4.26
C. 5.69

3+35

77.50
9.97
9.22
C. 0.75

E. side Tunnel
Top. Walk

85.19
2.28
2.20
C. 0.08

W. side Tunnel
Top. Walk

85.15
2.32
2.25
C. 0.07

Rest
78.65
78.78
9.87
4.66
+ 5.21

78.63
8.02
5.61
+ 4.41

10.2
77.3

Finish stakes Pist. Range
on line 85: S. of N. line

BM.
0+00: W. line

BM

78.36

$\frac{82.90}{5.75}$
 $\frac{10.29}{88.65}$

$\frac{84.7}{4.0}$

0+25

$\frac{83.10}{5.55}$ ✓

83.10

0+50

$\frac{83.30}{5.35}$ ✓

83.30

0+75

$\frac{83.50}{5.15}$ ✓

83.50

1+00

$\frac{83.70}{4.95}$ ✓

83.70

1+25

$\frac{83.90}{4.75}$ ✓

83.90

1+50

$\frac{84.10}{4.55}$ ✓

84.10

1+75

$\frac{84.30}{4.35}$ ✓

84.30

2+00

$\frac{84.50}{4.15}$ ✓

84.50

2+25

$\frac{84.70}{3.95}$ ✓

84.70

2+50

$\frac{84.90}{3.75}$ ✓

84.90

2+75

out $\frac{85.10}{3.55}$

85.10

$\frac{85.15}{3.50}$

3+00

$\frac{85.30}{3.35}$ ✓

85.30

$\frac{3.43}{10.07}$

3+25

$\frac{85.50}{3.15}$ ✓

85.50

3+50

$\frac{85.70}{2.95}$ ✓

85.70

3+75: E. line

$\frac{85.90}{2.75}$ ✓

85.90

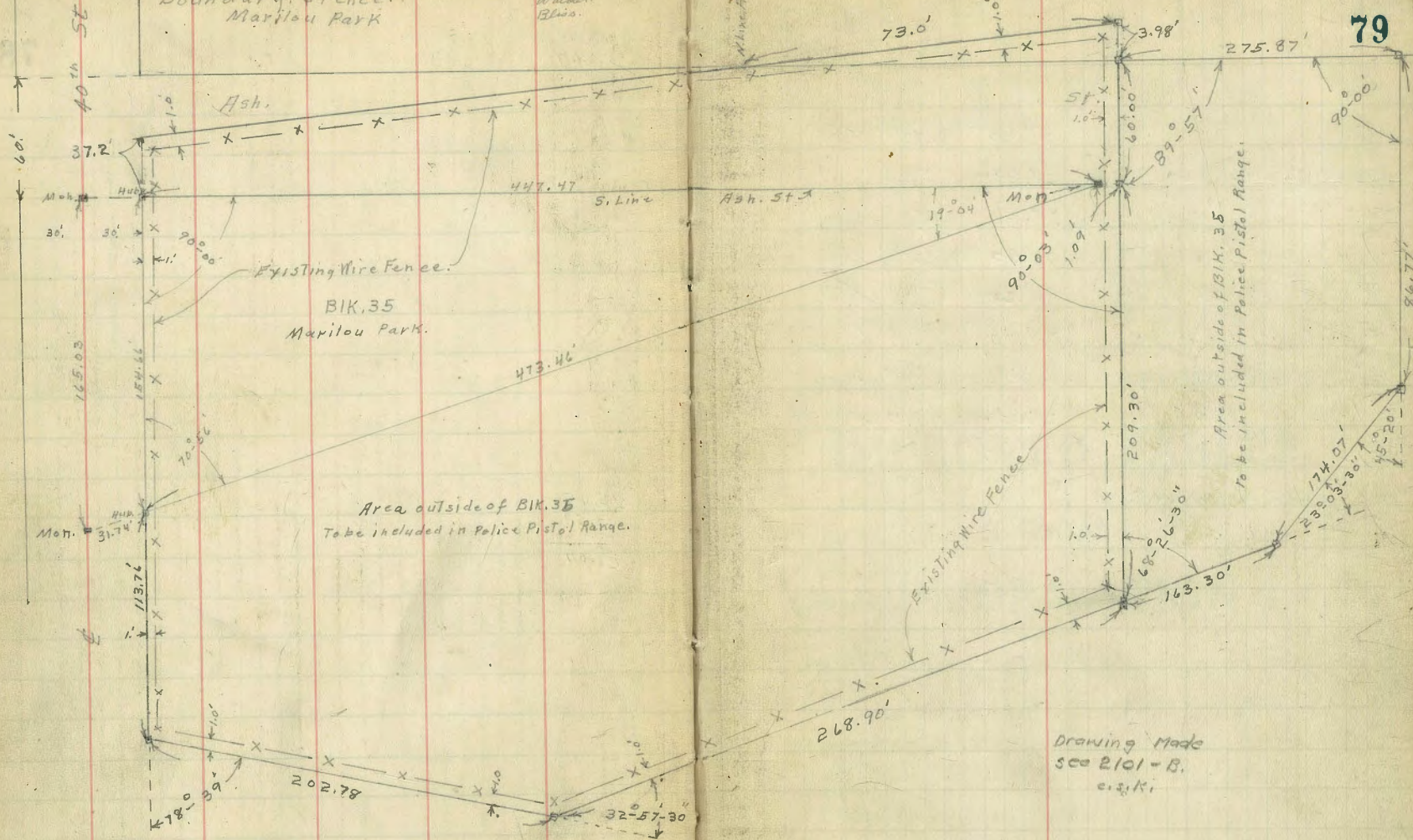
Survey Police Pistol Range.

Boundary & Fence.
Marilou Park

1-12-35

Miller
Walker
Bliss.

Indexed
c.s.K.



MOVING ACCOUNT 107102
Kettner & Kalmia

29.02
7.47
36.49

NWBP
June per
Kettner

1+75	29.22	7.27	✓
2+00 = SL Kalmia = 00	29.33	7.16	
0+15	29.41	7.08	✓
0+36 Brk	29.50	6.99	✓
0+40 Sedge Cr water	29.30	7.19	✓
+58 N " " "	29.30	7.19	✓
+80 NL Kalmia	29.24	7.15	✓
+96	29.38	7.11	✓
1+12	29.42	7.07	✓
+17 = end new solar			

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

**IMPROVED TABLES
AND
INFORMATION**

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

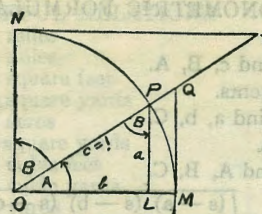


TABLE II

TRIGONOMETRIC FORMULAE.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

S.W. 24th + A. 174.91

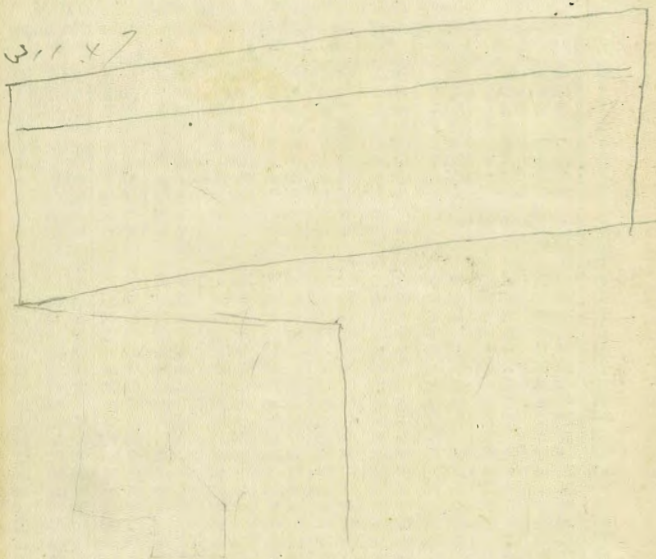
39 + 38.48 = BC

397.33 = T

300 R

A 88° 31'

311 x 7



249.9

$$\begin{array}{r} 115.39 \\ 50.11 \\ \hline 15.2 \\ 7.40-30 \end{array}$$

$$\begin{array}{r} 00894 \\ 00891 \end{array}$$

$$\begin{array}{r} 100894.0 \\ 40.2584 \end{array}$$

20.5
2.0
7.0
7.0
3.0
13.5
56.0

$$\begin{array}{r} 896 \\ 17 \end{array}$$

SL to 1/2 + 8 = changed curb

0.70
0 + 0.5
0 + 11.5

$$\begin{array}{r} 178 \\ 90 \\ \hline 86 \end{array} \quad \begin{array}{r} 80.34 \\ 88 \\ \hline 79.46 \end{array} \quad \begin{array}{r} 81.81 \\ 79.41 \\ \hline 2.35 \end{array}$$

$$\begin{array}{r} 912.35 \\ 10261 \\ \hline 30 \\ 7830 \end{array} \quad \begin{array}{r} 12261 \\ 22 \\ \hline 1305 \\ 522 \\ \hline 1525 \end{array}$$

$$\begin{array}{r} 178 \\ 30 \\ \hline 2148 \\ .74 \end{array} \quad \begin{array}{r} 2478 \\ 89 \end{array}$$

$$\begin{array}{r} 88 \\ 72 \\ \hline 160 \end{array} \quad \begin{array}{r} 160 \\ 960 \\ 24 \end{array}$$

1402-53

80.34
23
80.11
25
79.86
25
79.61
15
79.46
22
79.22
65
80.37
65
81.02
79
81.81