

NAME _____

Class _____ Course _____ Party _____

1459

CAUSEWAY

FIELD NOTES

No. 403P

ESPECIALLY ADAPTED

TO THE USE OF

ENGINEERING STUDENTS

EUGENE DIETZGEN Co.

MANUFACTURERS

DRAWING MATERIALS

MATHEMATICAL AND SURVEYING INSTRUMENTS

MEASURING TAPES

CHICAGO SAN FRANCISCO NEW YORK
NEW ORLEANS PITTSBURGH

X-Sections for Johnson - Jan. 16 -

sofa

→ Pages - 6-9

Final X-Sections of Dredging - 10

Final X-sectioning Btw. br. 142 - 17-22

82+20 to 104+32

MICROFILMED

DEC 23 1964

Sta	+	H.I	-	Elev BM's
				-3.19

	+9.53	+6.34		
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70+15				
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70+10				
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69+50				
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69+00				
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68+50				
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68+00				
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67+50				
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67+00				
-------	--	--	--	--

	+6.34			
--	-------	--	--	--

Left

±

Right

2

-3.0		
93		
45		

-3.0	
93	
74	

-3.0	
93	
40	

+0.4		
61		
30		

+0.8	
55	
5.5	

+1.3	
50	
25	

+1.1		
52		
30		

+2.0	
48	
7.3	

+1.1	
48	
25	

+1.0		
54		
30		

+1.2	
51	
5.1	

+1.2	
51	
25	

+1.0		
52		
30		

+1.0	
53	
5.3	

+1.0	
53	
25	

+0.8		
52		
30		

+1.1	
52	
5.2	

+0.8	
52	
25	

+0.6		
57		
30		

+0.7	
56	
5.6	

+0.6	
57	
25	

+0.8		
52		
30		

+0.8	
55	
5.5	

+0.8	
52	
25	

Sta	+	H.I	-	Elev	BM's
		+6.34			
66+50					
66+00					
65+50					
65+00					
64+25					
64+20					
64+00					
63+50		+6.34			

Left

4

Right

3

+1.7 51 30	+1.4 49	+1.0 57 25
+1.2 51 30	+1.8 4.5	+0.9 57 25
+1.3 52 30	+1.8 4.3	+1.2 57 25
+1.2 48 30	+1.9 4.4	+1.4 49 25
+1.4 49 30	+2.0 4.3	+1.8 45 25
-1.0 73 30	-1.0 7.3	-1.8 81 25
-1.6 79 32	-1.7 8.0 6.3	-1.8 82 25
-1.6 82 32	-2.3 9.6	-1.7 81 25

Sta + H.I. - Elev. BM's

63+00 +6.34

62+50

62+00

61+50

61+00 +6.34

T.P.

-6.64 -0.30

+3.96 +3.66

60+50

60+00

59+26

Left

-1.5
72
32

-1.6
82
32

-1.4
77
32

-0.9
72
32

-1.0
77
32

-0.9
45
32

-0.7
41
32

-0.9
46
32

-1.5
72
7.8

-1.6
82
8.0

-1.2
76
6.3

-0.4
6.7

-0.4
6.7
6.3

H.I. + 3.7

-0.3
4.0

-1.0
4.7
2.0
1.1

-1.2
4.9

Right

4

-1.6
72
27

-1.7
82
27

-1.4
72
27

-1.2
75
27

-1.0
74
27

-1.1
48
27

-1.0
43
27

-0.8
45
27

Sta + H.I. - Elev BM's

59+18 + 3.66

59+00

58+50

59+00

57+60 + 3.66

Left

- 2.9
 $\frac{6.5}{3.2}$

- 2.4
 $\frac{6.1}{3.0}$

- 2.4
 $\frac{6.1}{3.0}$

- 2.6
 $\frac{6.3}{3.0}$

$\frac{7.3}{3.0}$

±

H.I. 3.7

- 3.7
6.8

- 2.8
6.5

- 2.4
6.1

- 2.1
5.8

7.2

Right

5

- 3.1
 $\frac{6.8}{2.7}$

- 3.3
 $\frac{7.0}{2.5}$

- 2.4
 $\frac{6.1}{2.5}$

- 2.5
 $\frac{6.5}{2.5}$

$\frac{7.3}{2.5}$

Prob. 0.4 fill
above N.S.

Add $60 \times 10 \times 2.5 = 55$ cu. yds
for part fill of slough

Sta.	+	HI	-	Elev
B.M.				-3.19
	4.66	+1.47		

70+15

70+20

70+75

71+00

71+35

71+85

72+00

72+50

73+00

73+10

73+35

+1.47

Left

West

E

Right

East.

6

Opposite Sta. 70+00

+0.4			+1.2		+1.2
1.0			-0.3		-0.3
3.0					2.5
-2.0			-1.6		-2.4
3.5			3.1		3.4
3.0					2.5
-5.0			-4.3		-5.0
6.5			5.8		6.5
4.5					5.0
-5.1	-4.0	-3.6			-4.8
6.5	5.5	3.1	-3.7		6.5
4.5	2.1	2.0	5.2		5.0
-5.3	-4.8	-4.0			-3.7
6.8	6.2	5.5	-3.2	-5.0	6.8
4.5	2.8	2.5	4.7	3.0	4.0
-6.6	-5.4	-3.5			-5.3
8.1	6.2	5.2	-3.0	-4.5	6.8
4.5	2.5	1.4	4.5	3.0	4.0
-6.7		4.9			-6.0
8.2		6.4	-4.5	-5.1	7.3
4.5		2.0	6.0	3.5	4.0
-5.6	-4.8				-4.9
7.1	6.3		-4.3	-3.8	6.4
4.0	3.5		5.8	2.7	2.8
-5.6	-4.8				-4.6
7.1	6.2		-4.2	-3.7	6.1
4.5	4.0		5.7	3.0	3.2
-5.2	-3.9	-3.4			-4.3
6.7	5.4	4.2	-3.3	-3.0	5.8
4.0	2.5	2.0	4.8	2.5	2.7
-4.3	-3.2				-4.1
6.8	4.2		-2.8	-3.1	5.6
4.0	1.5		4.3	4.6	5.7
				2.0	2.5
					4.0

Sta	+	H.I	-	Elev	BM's
73+80		+1.47			

Left

±

Right

7

Note:

This last section probably not included

-6.6	-5.9	-5.1		-4.4
8.1	7.3	6.6	-4.3	5.2
2.5	1.5	1.0	5.8	4.0
M.S. →				

as it lies beyond limits of earthwork

Sta	I	H.I	-	Elev	B.M.'s
	9.22			-3.19	No 7
		+6.03			
65+00					
64+00					
63+00					
62+00					
61+00					
T.P.			4.41	1.62	
60+00	1.94	+3.56			
59+30					
59+20					
59+00					
58+50					
58+00		+3.56			

Left

West

E

Right 8
East.

1.2		1.2
48	+1.8	48
30	4.2	25
1.2		1.0
48	1.8	50
30	4.2	25
1.1		1.2
49	1.6	48
30	4.4	25
1.0		1.0
52	1.6	50
30	4.4	25
0.7		0.8
53	1.3	52
30	4.7	25
-0.1		-0.2
37	-0.1	38
30	3.7	25
-0.3		-0.8
32	1.1	44
30	-0.8	25
	4.4	
	3.0	
-1.4		-1.6
51	-1.6	52
30	5.2	25
	3.2	
-1.7		-1.8
53	-1.8	52
30	5.4	25
-1.1		-1.5
47	-1.3	52
30	4.9	25
-2.0		-2.2
56	-2.0	58
30	5.7	25

Sta	+	H.I	-	Elev	BM's
	+41				
57+50		+3.56			
= 56+63					
57+00	✓	56+70			
56+30		55+50			
56+00		55+70			
55+30		54+50			
55+00		54+70	+3.56		
54+50		53+70			

Left

4

Right

9

-2.4					
6.0	-1.6				-2.2
3.0	5.2				5.8
					2.5
-2.8					
6.4	-2.8	-2.8	-1.6	-1.9	
3.0	6.4	6.4	5.2	5.5	
		1.0	1.2	2.5	
-3.7					
7.3	-3.8	-3.4	-2.4	-2.1	
3.0	7.4	7.0	6.2	5.7	
		1.8	2.0	2.5	
-3.4					
7.0					-2.2
3.0					6.2
					2.5
-2.4					
6.0					-2.0
3.0					5.2
					2.5
-2.5					
6.1	-2.4				-2.7
3.0	6.0				6.5
					2.5

Wedge End of Grading = Original Surface

55+50 - 55+00 = 50' x 2' = 100' of cut to fill

200' x 2' = 400' of cut to fill

21'

- Final X-sec. -

Sta. + HI. - Elev.

450

46

450

45

450

44

450

43

450

44

BC
4149187

Westerly

±

Easterly 10

FINAL X-Sec

Sta. + H.I. - Elev.

1

52

100

57

100

50

100

49

100

48

100

47

Westerly

±

Easterly 11

Final X-sec

Grade

Westerly

Easterly

12

Sta.	+ H.I.	- Elev.	W. Curb	E. Curb
58+43				
58+05	+5.84		2.83	2.83

T.P.	3.58	2.90	+ 2.94		
56	0°55'	+6.52		3.16	2.66
57	1°38'			3.06	2.48
58	2°21'			3.02	2.40
59	3-04			2.97	2.33

54+03				2.93	2.25
53+97					
53+35					

Note -
The apparent error of stationing for slough was probably account instead of the Semi-Tang of true E of Curve. Therefore Quantities could be computed fairly close if the original sections were set back 53+97 + 53+70 (See Keys notes on this also)

Approximated this station as end of Johnson's work

Top of Earth Bank

Bottom Slough

Far Edge of Slough

Edge slough

11 1/2	10 1/2	9 0	8 1/2	+0.9	+1.3	+1 1/2	-2 1/2	-4 1/2	-5 0
104	102	40	38	32	4.2	29	33	45	55
10.9	10.2	96	92	85	+20	45	45	82	91
107	105	50	49	38	32	28	25	34	41
96	93	F18	49	+1.3	F.09	46	88	95	
63	35	30	32	4.0	25	28	36	50	N.S
10 1/2	9 3/4	F-2 1/2	50 1/2	+1.5	F-1 1/2	52	92	92	10 1/2
65	33	30	28	5.0	25	28	38	38	42
10 1/2	9 1/2	F-1 1/2	52	+1.9	F-1 1/2	52	93	92	10 1/2
60	35	30	26	4.7	25	27	32	40	55
10 1/2	9 1/2	F-1 1/2	52	+1.7	F-1 1/2	54	92	92	10 1/2
63	37	30	31	4.8	25	25	33	55	N.S
98	92	F-1 1/2	52	+1.6	F-0 1/2	54	92	10 1/2	10 1/2
63	37	30	32	4.9	25	27	34	40	50
10 1/2	9 1/2	F-2 1/2	52	+1.5	F-1 1/2	56	99	10 1/2	10 1/2
47	37	30	32	5.0	25	25	30	50	N.S

$10 - 3.7 = 6.3$
 $10 - 3.3 = 6.7$
 $10 - 3.8 = 6.2$

- Add -
 $45 \times 10 \times 0.6 = 270$
 10 cu yds for side slough
 - 8.0
 14.5

Elev. Bottom Slough opposite 53.50 (53+97)
 Use for Sections 53+70

Final X-sec

Grade

Westerly

±

Easterly

Sta.	+	H.I.	-	Elev.	W. Curb	E. Curb
63		+6.70			2.17	2.17
T.P.			3.37	+3.33		

	2.46	+5.79				
62+85					2.15	2.15

6v					2.27	2.27
----	--	--	--	--	------	------

6t					2.41	2.41
----	--	--	--	--	------	------

60					2.55	2.55
----	--	--	--	--	------	------

Chrom BM #6
 $8.75 - 2.96 = -2.91$
 $+ 5.84 = \text{Corrected H.I.}$

59					2.69	2.69
----	--	--	--	--	------	------

Westerly	Easterly
-4.0 10.6 5.0 N.S.	-3.6 10.3 4.0
-1.4 8.2 3.5	+1.4 5.5 3.2
(F-9) 2.5	+1.8 4.9
	(F-12) 3.0
	+1.2 -1.9 -3.8
	5.5 3.5
	8.9 3.8
	10.5 4.5 N.S.

10.5 = H.S. Edge Slough

-4.0 9.7 5.0 N.S.	-3.6 9.2 4.4	-2.1 7.9 3.7	+1.0 4.8 3.4	(F-12) 3.0	+1.1 4.3	(F-12) 2.5	+0.9 4.2 3.0	-2.0 7.8 3.4	-4.3 10.1 4.5	-4.3 10.1 5.0 N.S.
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-3.7 9.5 5.3 N.S.	-3.1 9.2 4.5	-2.2 8.0 4.0	+0.9 4.9 3.4	(F-15) 3.0	+1.1 4.3	(F-12) 2.5	+0.8 5.2 2.6	-2.6 8.4 3.3	-4.1 9.9 3.8	-4.5 10.3 5.0 N.S.
----------------------------	--------------------	--------------------	--------------------	---------------	-------------	---------------	--------------------	--------------------	--------------------	-----------------------------

-3.4 9.2 6.3 N.S.	-3.0 9.1 4.0	+1.0 4.8 3.0	(F-12) 3.0	+1.1 4.3	(F-17) 2.5	+1.4 4.6 2.5	-4.1 9.9 4.0	-4.7 10.5 6.5 N.S.
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-2.2 9.4 5.0 N.S.	-3.4 9.2 4.0	-2.3 8.1 3.7	+1.3 4.5 3.1	(F-12) 3.0	+1.3 4.5	+1.1 4.2 2.4	(F-16) 2.5	-2.3 8.1 2.9	-3.6 9.4 3.3	-4.0 9.8 5.5 N.S.
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Final X-Sections

Westerly

2

Easterly 15

Grade

Sta. + H.I. - Elev. W. } E
Curb } Curb.

BM #7

989 +6.70

-3.19

71

244 244

70

42
251 251

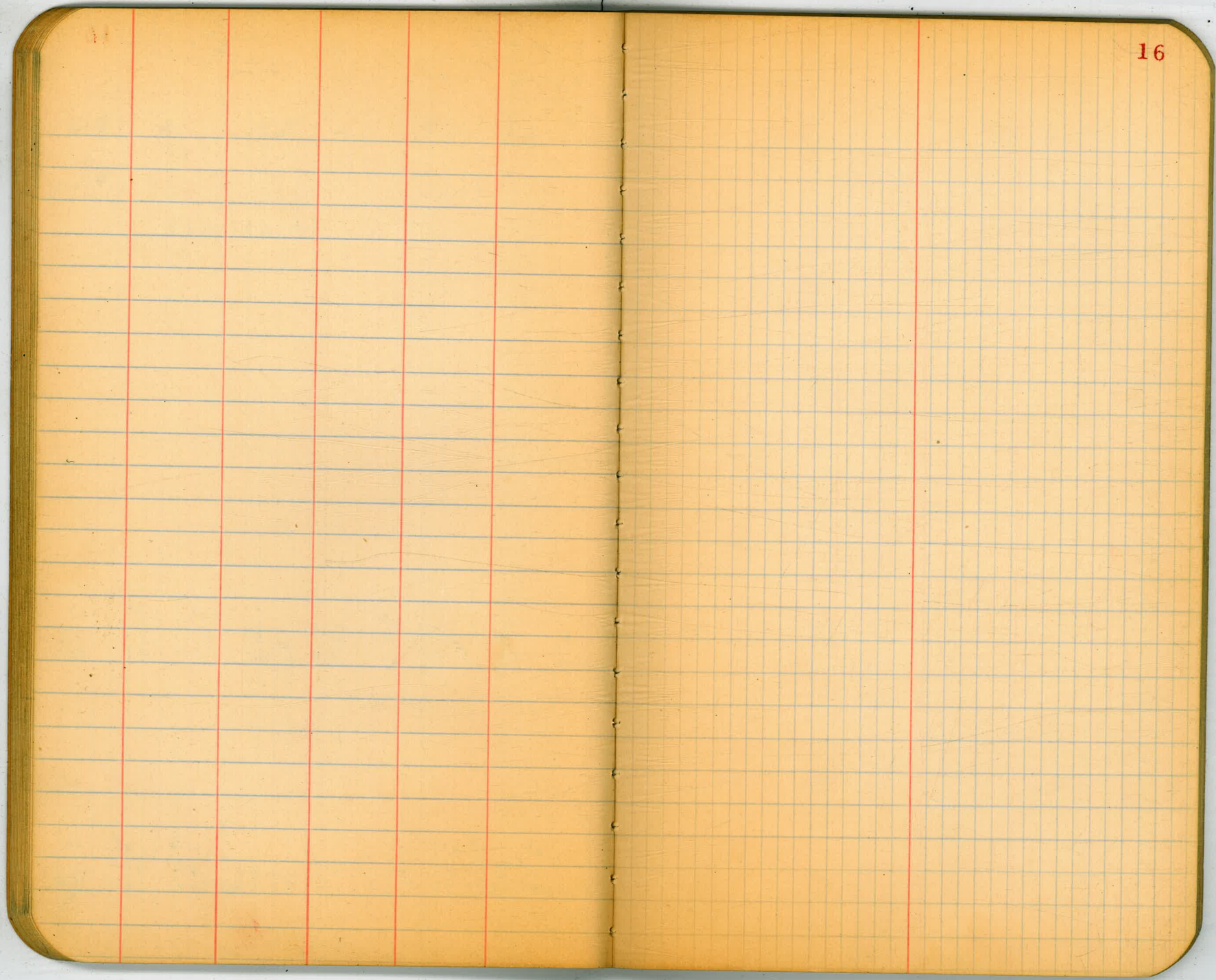
-4.1	-2.2	0.0		+1.2	-3.8	-4.3
108	89	68	68	55	105	112
65	35	30	28	5.4	30	41
						50

69

+6.70

4.1
257 257

-3.8	-1.8	+1.4		+1.6	+1.8	-3.1	-3.1
105	85	53	53	30	49	102	102
798	41	38	30	5.1	25	40	50
(N.S)							



West

±

East

Sta + H.I - Elev BM's

82+59 +6.38

-47 -41 -16 +17 -25 +21 +18 -18 -42 -55
 111 105 80 47 89 46 82 106 119
 60 50 33 30 10 4.3 26 30 40 50

82+50

-46 -17 -07 -22 -25 +12 +12 -21 -40 -53
 110 81 71 86 46 45 85 104 117
 50 30 27 20 8.9 9 24 30 40 50

82+40

-49 -17 -03 -35 -35 -35 -26 -27 -50 -56
 113 81 67 99 91 90 91 114 120
 45 22 18 5 9.9 5 10 22 40 45

82+30

-53 -40 -26 -25 -48
 117 104 92 112
 40 25 10 8.9 25

82+20 +6.38

-74
 13.8

T.P. 4.00 2.38

3.78 6.16

T.P. 3.21 2.95

3.33 6.28

T.P. 2.56 3.72

3.90 +7.62

T 8.66 -1.04 = -1.01

CK on BM
 See Page 22

West

±

East

19

Sta	+	H.I	-	Elev	BM's													
86+00		+6.38				✓	-5 ⁹	-3 ⁷	-1 ⁸	+2 ²	+2 ⁵	+1 ⁹	-2 ⁰	-4 ²	-5 ⁰			
							12 ³	9 ⁸	8 ²	4 ²		4 ⁵	8 ⁹	10 ⁶	11 ⁴			
							50	40	33	28	3.9	29	35	50	60			
85+50						✓	-5 ⁸	-4 ⁸	-2 ¹	+1 ⁹	+2 ¹		+2 ⁰	-1 ⁹	-4 ⁵	-5 ²		
							12 ³	11 ²	8 ⁵	4 ⁵		4 ⁴	8 ³	10 ⁹	11 ⁶			
							60	50	34	30	4.3	31	36	50	60			
85+00						✓	-5 ⁶	-4 ⁶	-1 ⁷	+2 ¹	+2 ¹	+2 ²	-2 ⁴	-4 ⁷	-5 ⁸			
							12 ⁰	11 ²	8 ¹	4 ³		4 ²	8 ⁸	10 ⁸	12 ²			
							55	50	34	31	4.3	25	30	40	50			
84+50						✓	-5 ⁰	-3 ⁹	-1 ⁹	+2 ²	+2 ⁰	+1 ²	-2 ⁴	-3 ⁴	-4 ⁸			
							11 ⁴	10 ³	8 ³	4 ²		5 ⁰	8 ⁸	9 ⁸	11 ²			
							60	50	38	31	4.4	29	34	40	50			
84+00						✓	-4 ⁶	-4 ¹	-2 ⁰	+2 ²	+2 ⁰	+2 ²	-1 ⁹	-3 ⁵	-4 ⁴			
							11 ⁰	10 ⁵	8 ⁴	4 ¹		4 ²	8 ³	9 ⁹	10 ⁸			
							56	50	38	32	4.4	27	33	41	50			
83+50						✓	-5 ⁰	-4 ³	-2 ³	+1 ⁸	+1 ⁹	+1 ⁸	-2 ³	-4 ⁰	-4 ⁷			
							11 ⁴	10 ⁷	8 ⁷	4 ⁶		4 ⁶	8 ⁷	10 ⁹	11 ¹			
							55	50	36	32	4.5	25	32	40	50			
83+00						✓	-5 ⁰	-4 ²	-2 ⁰	+2 ⁵	+2 ⁰	+2 ²	-2 ³	-4 ²	-5 ³			
							11 ⁴	10 ⁶	8 ⁴	3 ¹		4 ²	8 ⁷	10 ⁶	11 ⁷			
							56	50	38	29	4.4	26	32	40	50			
82+65		+6.38				✓	-4 ⁷	-4 ¹	-1 ⁸	+2 ²	+2 ¹	+1 ²	-1 ⁸	-4 ²	-5 ⁵			
							11 ¹	10 ⁵	8 ³	4 ²		4 ⁵	8 ²	10 ⁶	11 ⁹			
							60	50	36	33	4.3	24	30	40	50			

West

East 20

Sta + H.I - Elev BM's

Sta	H.I	Elev	BM's
91+00	+6.23	✓	-4 ⁸ -4 ⁸ -2 ¹ +1 ⁶ +2 ¹ +1 ² -1 ⁸ -3 ⁰ -4 ⁵ -5 ⁴ 11 ⁰ 10 ¹ 8 ² 4 ⁶ 4.1 4 ⁵ 8 ⁰ 9 ² 10 ² 11 ⁰ 60 50 35 30 27 32 37 50 60
90+50		✓	+1 ⁶ 4.6 -4 ² -3 ⁴ -1 ⁶ -0 ² +1 ² +2 ⁸ +1 ⁶ -2 ⁰ -3 ¹ -4 ⁸ -5 ² 10 ⁷ 9 ⁶ 7 ⁸ 6 ⁴ 4 ³ 4 ⁶ 8 ² 9 ² 11 ⁰ 12 ¹ 60 50 35 34 29 29 32 38 50 60
89+50		✓	+1 ² 4.3 -5 ⁸ -4 ³ -1 ² +2 ² +2 ⁴ +1 ⁶ -2 ⁰ -3 ⁹ -6 ⁰ -6 ³ 12 ² 10 ⁵ 8 ¹ 4 ⁰ 4 ⁶ 8 ² 10 ¹ 12 ² 12 ⁵ 60 50 37 32 26 31 38 50 55
88+50		✓	+1 ⁷ +1 ⁴ -1 ⁹ -4 ⁹ -6 ¹ -5 ⁰ -4 ⁵ -1 ⁷ +1 ⁸ 4.5 4 ⁰ 8 ¹ 11 ¹ 12 ³ 11 ⁸ 10 ⁷ 8 ¹ 4 ⁴ 27 31 50 60 56 50 35 32
88+00	+6.23	✓	-5 ⁸ -5 ⁶ -4 ⁰ -1 ² +1 ⁸ +2 ¹ +1 ⁶ -2 ¹ -4 ² -5 ³ -5 ⁸ 12 ⁰ 11 ³ 10 ² 8 ¹ 4 ⁴ 4 ⁶ 8 ² 10 ⁴ 11 ³ 12 ⁰ 60 52 45 34 30 26 31 40 50 60
T.P.		3.85	2.38
87+50	4.00 +6.38		+2 ¹ 4.3
87+00		✓	-5 ⁸ -5 ³ -1 ⁸ +2 ⁴ +2 ⁴ +2 ³ -1 ² -4 ⁶ -5 ⁵ 12 ² 11 ⁷ 8 ² 4 ⁰ 4 ¹ 8 ² 11 ⁰ 11 ⁹ 60 50 35 31 4.0 29 34 50 60
86+50	+6.38		+2 ² 4.2

West

±

East

Sta + H.I - Elev BM's

	2.04	+5.79		
99+00				
98+00				
97+00				
96+00				
95+00				
94+00		+5.79		
T.P.			2.80	2.99
93+00	3.24	+6.23		
92+50				
92+00				
91+50				

✓	-55	-45	-15	+26	+35	+30	-16	-50	-59
	114	103	73	35		22	74	108	112
	60	50	31	27	2.3	25	27	50	60
✓	-60	-44	-16	+30	+25		+20	-14	-53
	118	103	74	38			38	72	110
	65	50	29	22	3.3		24	27	50
✓	-57	-44	-17	+33	+16		+17	-18	-56
	115	102	75	35			41	76	111
	65	50	29	26	4.2		24	26	50
✓	-59	-48	-25	+18	+28		+17	-16	-52
	117	106	83	40			41	74	119
	65	50	30	28	3.1		24	26	50
✓	-52	-46	-17	+17	+24		+19	-16	-53
	117	104	75	41			39	74	111
	65	50	27	25	3.4		25	26	50
✓	-56	-44	-21	+16	+23		+14	-16	-55
	114	102	79	45			44	74	114
	65	50	29	26	3.5		25	27	50
✓	-58	-43	-18	+13	+23		+13	-18	-42
	120	105	82	49			42	80	104
	60	50	32	29	4.0		25	29	40
✓	-56	-51	-19	+14	+24		+18	-13	-24
	118	113	81	48			44	75	86
	60	50	30	27	3.8		26	29	32
✓	-57	-50	-38	-20	+12		+17	-22	-37
	119	113	102	82			45	82	92
	55	50	40	31	4.0		26	31	40

Sta.	
BC 4141.87	0-00
42	1-50
+50	1-32.8
43	2-15.5
+50	2-58.5
44	3-41.5
+50	4-24.5
45	5-07.5
+50	5-50.5
46	6-33.5
+50	7-16.5
47	7-59.5

$$\begin{array}{r} 4141.87 \\ 39+4935 \\ \hline 19252 \end{array}$$

47+50	8-42.5
48	9-25.5
+50	10-08.5
49	10-51.5
+50	11-34.5
50	12-17
+50	13-00
51	13-43
+50	14-26
52	15-09
+50	15-52
53	16-35

53+50

17-18

54

18-01

+50

18-44

55

19-27

+50

20-10

56

20-53

56+63.80

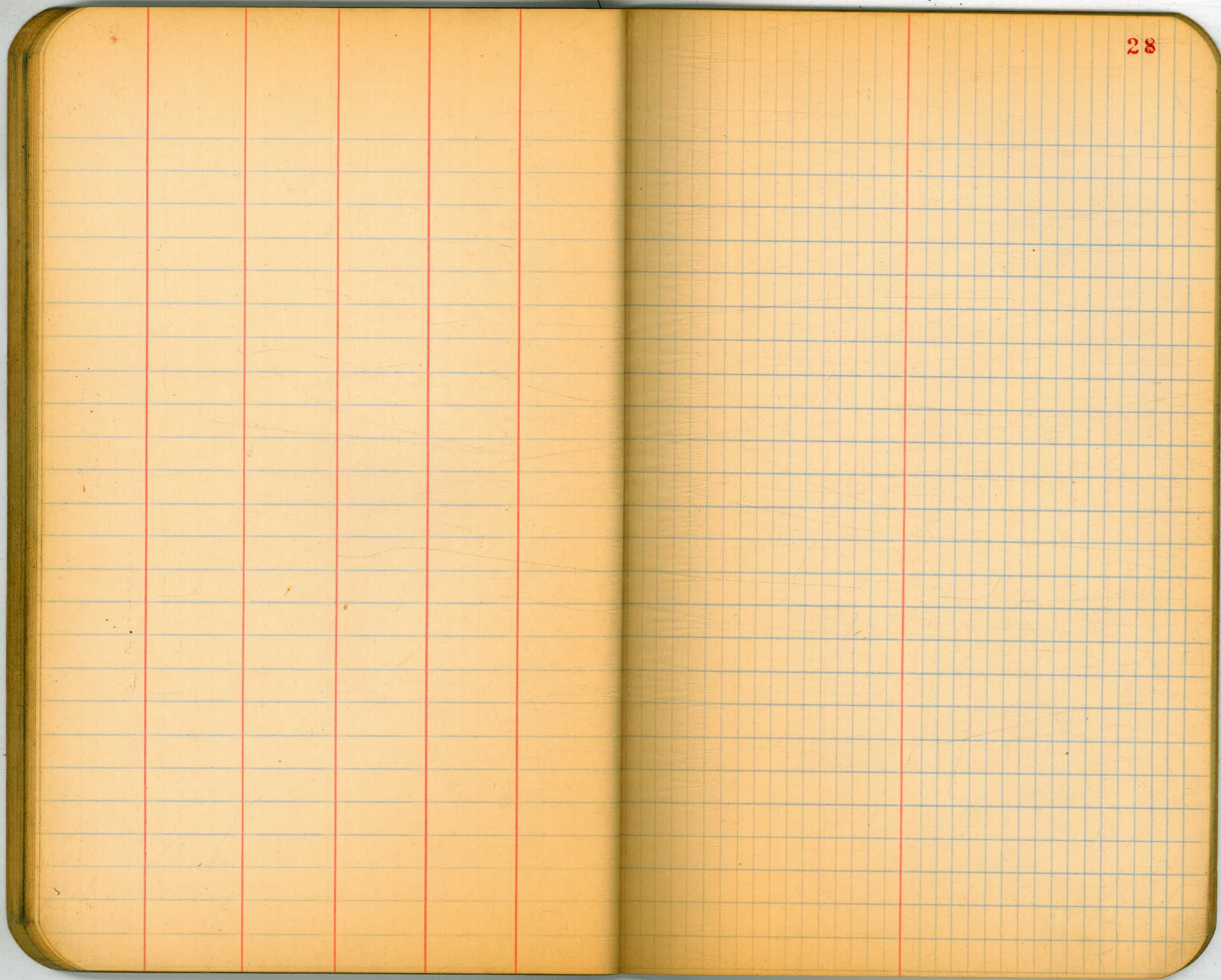


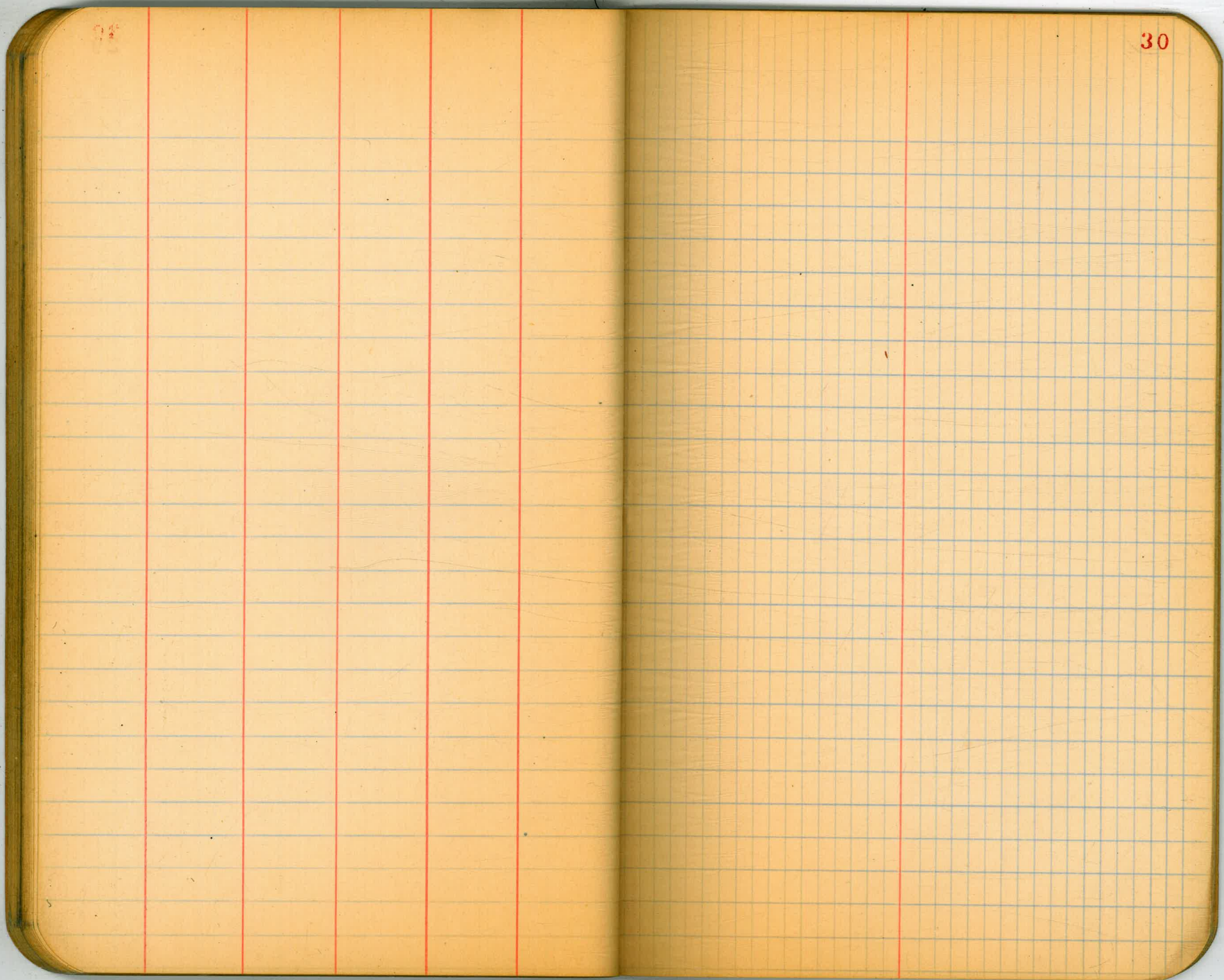
Equation =

21248

57+41.757

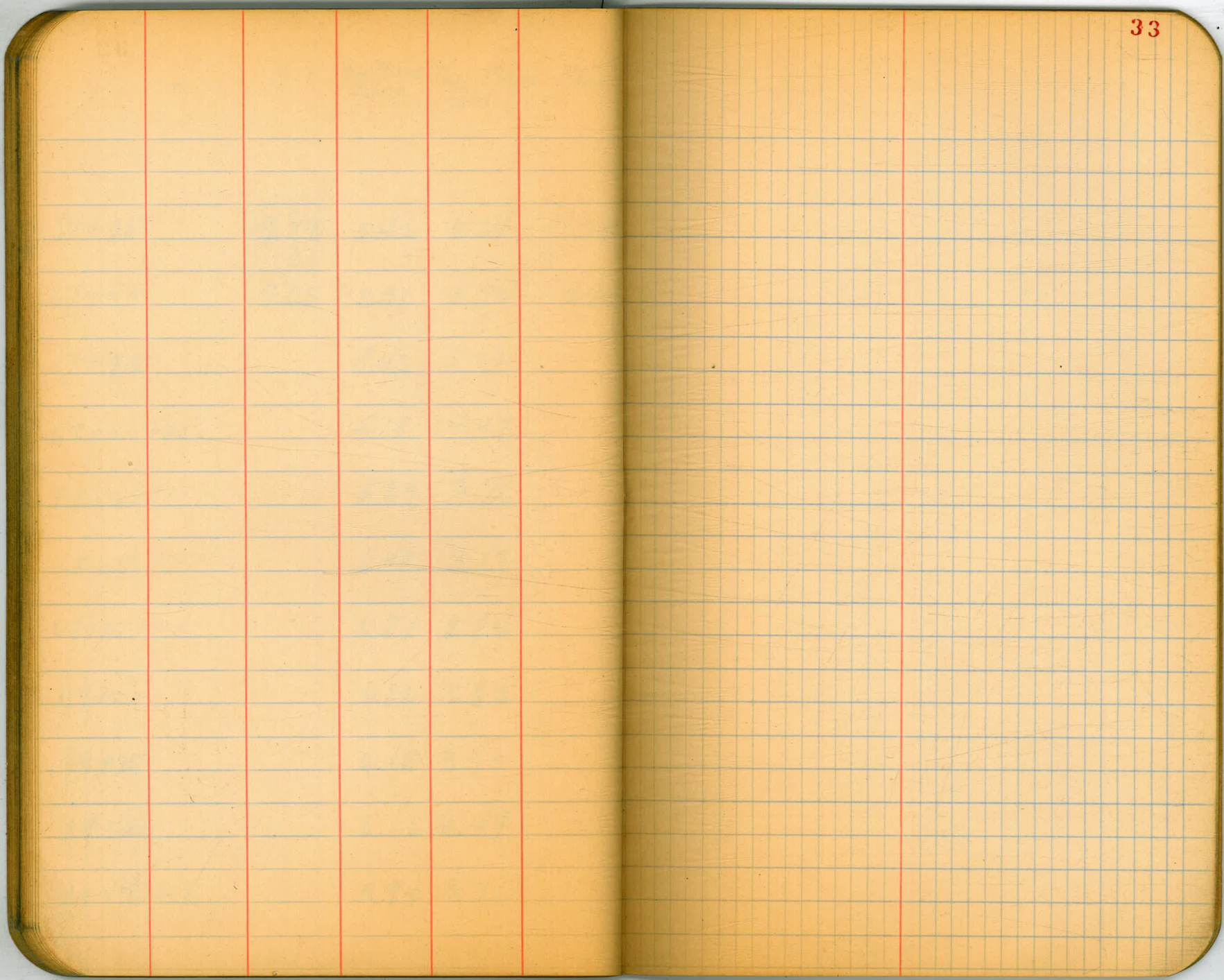






H. I.	Top Base Elev.	Top Base Rod	Elev.
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67+25	9.56	3.42	6.14	4.25
67+50	9.65	3.91	5.74	4.74
67+75		4.42	5.23	
68+00+25		5.18	4.47	
68+25+50		5.89	3.76	
68+50+75		6.48	3.17	
68+75+100		6.81	2.84	
69+00		6.82	2.83	
69+25		6.45	3.20	
69+50		6.16	3.49	
69+65 track		5.94	3.71	



54 to 56 Field Study

56 + 63.80 Back
= Equation = E.C.
57 + 41.75 Forward
62 + 90 = Monumenta
74 + 00 = Bridge # 1

63 + 100.34 = P.O.T. - Feb. 3-20

875
579.
- 2.96

875
296
5.84

16

12.58

11.58
.86
694.8
92.64

6995.188
16.59

6995.
16.
16

409

16.36
6
5.13

21.49

43-38 = 5

330
4
3
81
3
243