

NAME _____

Class _____ Course _____ Party _____

1460

FIELD NOTES

No. 403 P

ESPECIALLY ADAPTED

TO THE USE OF

ENGINEERING STUDENTS

EUGENE DIETZGEN Co.

MANUFACTURERS

DRAWING MATERIALS

MATHEMATICAL AND SURVEYING INSTRUMENTS

MEASURING TAPES

CHICAGO SAN FRANCISCO NEW YORK
NEW ORLEANS PITTSBURGH

- INDEX -

Barnett - Northely - Slope Stakes - 2 -

Cut-off Wall - Topog - — 34

Grades for Curb + Pav. at R.R. Crossing - 32

MICROFILMED

DEC 23 1964

0+11 - East.

0+56 - West

Barnett - North - Rod

Sta.	+ or -	H.I	Elev.		Grade		
			W	E	W	E	
Rt. 0+35.61					1.80	0.97	1.23
0+50 W+E.					1.76	0.93	1.16
0+91.36	0.18	1.15	0.97	1.80	1.63		
1+14.50 = Rt.							
1+00 Rt.			0.94	1.77	1.60	0.77	0.93
1+29.08	0.10	0.94	0.84	1.67	1.51	0.68	0.80
+50	0.8	0.85	0.77	1.60	1.45	0.62	0.70
2+00	5.80	0.60	0.60	1.43	1.30	0.47	
+50			0.43	1.26	1.15	0.32	
3+00		0.46	1.09	0.99		0.16	
+50		0.09	0.95	0.86		0.03	
4+00		-0.08	0.75	0.71		-0.14	
+50		-0.23	0.60	0.56		-0.27	
5+00		-0.40	0.43	0.40		-0.42	
+50		-0.57	0.26	0.25		-0.58	

Westerly - Easterly
Cuts or Fills

Westerly	Easterly
0.26	-2.7 C-0.29
0.23	C-0.19
F-0.39	-1.8
0.16	C-0.29
0.17	0-0.26
0.8	-1.8 C-0.31
	-1.8 C-0.07
✓	-1.9 C-0.51
	-1.5 C-0.81
	-1.7 C-0.87
	-1.5 C-0.60
	-1.5 C-0.60
	-0.9 C-0.71
	-0.9 C-0.51
	-0.7 C-0.51
	-0.4 C-0.56
	-0.1 C-0.40
	-2.6 C-1.41
	-0.5 C-0.59
Grade - 28	-1.9 C-1.15
	B.M. Elev. = -1.66

BARNETT		North	Red
Sta.	+ or -	H.I. Elev.	Grade
		N-E.	Red
	4.92	4.32	
6+00		-0.74	0.09 0.10 -0.73
Break.		4.42	
6+25		-0.83	0.00 0.00 -0.83
		4.39	
7+00		-0.80	0.03 1 -0.80
		4.39	
7+00		-0.75	0.08 1 -0.75
		4.29	
7+00		-0.70	0.13 1
		4.24	
8+00		-0.60	0.18 1
		4.19	
7+00		-0.60	0.23 1
		4.13	
9+00		-0.54	0.29 1
		4.07	
7+00		-0.49	0.34 1
		4.03	
10+00		-0.44	0.39 1
		4.00	
7+00		-0.39	0.44 1
		4.00	
11+00		-0.34	0.49 1

West.	East.
4.81 4.86 -0.05 4.38 4.33 4.73	3
- 1.1 -1.1 C-0.13	-2.3 - 1.2 C-1.06
- 1.3 -1.3 C-0.28	-1.5 - 1.2 C-1.08
- 1.3 -1.3 C-0.19	-1.3 - 1.2 C-1.12
- 0.5 -0.5 C-0.3	-0.8 - 0.7 C-0.71
+0.6 +0.5 C-0.92	-0.1 Grade C-0.19
+ 0.5 +0.4 C-0.52	+0.5 + 0.6 C-0.93
+ 0.7 Grade C-0.76	+0.7 + 0.8 C-0.53
+ 0.2 +0.1 C-0.49	+0.4 + 0.5 C-0.65
- 0.1 C-0.04	+0.3 C-0.91
- 0.2 C-0.22	+0.4 C-0.77
- 0.2 = BM. C-0.28 Elev. = 0.27	+0.4 C-0.65
- 0.3 C-0.20	+0.1 C-0.92

BARNETT North Rod

Sta.	+ or -	H.I.	Elev.	Grade W-E	
11+50			(-0.29)	0.54 ✓	4.4
12+00	83 69 18		(-0.23)	0.60 ✓	4.3
12+50			(-0.18)	0.65 ✓	4.3
13+00			(-0.13)	0.70 ✓	4.4
1+50			(-0.08)	0.75 ✓	4.4
14			(-0.03)	0.80 ✓	4.4
1+50			(+0.02)	0.85 ✓	4.4
15			(+0.08)	0.91 ✓	4.0
1+50			(+0.12)	0.96 ✓	4.0
16			(+0.18)	1.01 ✓	4.0
1+50			(+0.23)	1.06 ✓	4.5
17			(+0.28)	1.11 ✓	4.5

W.

E

4

56.5
62.7
-0.2
53.3
-0.8
48.5

-0.4 C-065	Scale C-074
-0.7 C-069	-0.5 C-078
-0.8 C-045	-0.6 C-089
-0.8 069	-0.7 C-104
-1.1 C-102	-0.7 C-114
-0.8 C-083	-0.7 C-060
-0.7 C-068	Scale C-025
-0.7 C-033	-0.7 C-046
-1.0 C-045	-0.9 C-083
1.7^{BM} C-034	-1.7 C-062
Elev. = 070	
-0.9 C-079	Scale C-016
-0.4 C-040	-0.7 C-052

BARNETT North Rod

Sta.	+ or -	HI.	Elev.	Grade.	Rod
				W-E	
17+50		(5.60)	(0.33) 1.16	✓	4.1
18			(0.38) 1.21	✓	4.1
18+50			(0.43) 1.26	✓	4.1
19			(0.49) 1.32	✓	4.1
19+50			(0.54) 1.37	✓	4.1
20+00			(0.59) 1.41	✓	4.1
20+23.7 ✓ = Ret. H.			(0.62) 1.45	✓	4.1
20+69.7 ✓ = Ret. only			(0.67) 1.50	✓	4.1
21+50.7 ✓ = Ret. H. 0 - 496 + 5.13 5.77			(0.67) 1.50	1.50	4.1
21+50			(0.63) 1.46	✓	4.1
22+00			(0.58) 1.41	✓	4.1

Westerly

5.65

Easterly 5

-0.7 C-087	-0.6 C-012
-0.7 C-036	-0.4 C-080
-0.8 C-041	-0.6 C-080
-1.0 C-045	-1.1 C-123
-0.8 C-040	-0.7 C-066
-1.4 C-096	-1.3 C-096
-1.7 C-176	-1.5 C-080
-	-0.8 C-081
(0.9 / 12) = Elev. = 0.64	-0.8 C-084
-0.9 C-101	-0.6 C-051
-0.5 C-093	-0.5 C-097

BARNETT Northerly

Sta.	Cor-	H.I.	Elev.	Grade	Rod
22+50			(0.53)	1.36	4.4
		5.77			
23+00			(0.47)	1.30	4.5
23+50			(0.41)	1.25	4.5
24+00			(0.37)	1.20	4.6
24+50			(0.31)	1.15	4.6
25+00			(0.26)	1.09	4.74
+50			(0.21)	1.04	4.79
26+00			(0.16)	0.99	4.84
⊙	-5.12		(0.10)	0.93	4.90
750	+5.00	5.65			
27+00			(0.05)	0.88	4.95
+50			(0.01)	0.84	4.99
27+89.45	Ret. E & W.		(-0.03)	0.80	5.03
⊙	-4.70	(5.00)	(-0.95)		(+0.98)

Westerly

100
3.48
+1.52
4.13
5.65

-0.4	C-0.62
-0.6	C-0.80
-0.6	C-0.61
-0.9	C-1.87
-1.1	C-0.50
-0.8	C-0.22
-0.8	C-0.50
-1.1	C-0.72
-0.8	C-0.71
-0.4	C-0.74
-0.2	C-0.61
Grade	(C-0.23)

B.M. - Elev. = +0.95

Easterly

-0.4	C-0.22
-0.3	C-1.05
-0.5	C-0.99
-0.4	C-0.52
-1.3	C-0.92
-0.7	C-0.91
-1.2	C-0.74
-0.7	C-0.50
-0.3	(B.M. Elev. = 0.65)
-0.3	C-0.76
-0.1	C-1.03
+0.2	(C-0.53)

2x2 Hub. Near
N.W. Cor. Bldg. Sta. 27+50

BARNETT NORTHERLY

Sta. + or -	H.I.	Elev.	Grade	Rod
28+89.85 = Ret. East. & West.				
		(-0.03)	0.80	5.03
29+30		(+0.01)	0.84	4.99
29+70 = B.C.	(0.00)	(+0.05)	0.88	5.32
	(3.92) (29.07)			
30+00	(0-51.5)	(+0.08)	0.91	5.29
+25	(1-34.5)	(+0.11)	0.94	5.26
+50	(2-17.4)	(0.14)	0.97	5.23
+75	(3-00.4)	(0.17)	1.00	5.20
31+00	(3-43.4)	(0.19)	1.02	5.11
	(2.78) (24.2)			
+25	(4-26.5)	(0.21)	1.04	5.16
	(28.23) (24.15)			
Ret. 31+52.39	(5-13.4)	(0.24)	1.07	5.13
	(23.32) (21.90)			
31+75	(5-52.3)	(0.27)	1.10	5.10
	(31.57) (26.59)			
Ret. 32+05.55	(6-44.7)	(0.29)	1.12	5.08
	(30.06) (26.84)			
32+25	(7-18.5)	(0.31)	1.14	5.06
32+50	(8-01.2)	(0.34)	1.17	5.03
32+75	(8-44)	(0.37)	1.20	5.00
33+00	(9-27.2)	(0.40)	1.23	4.97
	(25.78) (24.22)			
33+25	(10-10)	(0.42)	1.25	4.95
33+50	(10-53)	(0.45)	1.28	4.92
+75	(11-36)	(0.47)	1.30	4.90
34+00	(12-19)	(0.50)	1.33	4.87

Westerly

-0.9	(C0.77)
	(C0.52)
-0.5	(C0.59)
-0.7	(C0.71)
	(C0.68)
-0.8	(C0.35)
	(C0.27)
-0.6	(F0.10)
	(F0.18)
-0.7	(C0.70)
	(F0.03)
-0.5	(C0.38)
	(F0.12)
-0.8	(C0.08)
	(C0.28)
-0.9	(C1.20)
	(C1.20)
-0.9	(C1.12)
	(C1.08)
-1.0	(C0.97)

Easterly

1031
30
30930

-0.6	(C0.93)
	(C0.13)
-0.6	(C0.48)
-0.6	(C1.28)
	(C0.41)
-0.7	(C0.35)
	(C0.24)
-0.6	(C0.22)
	(C0.13)
	(C0.21)
-0.5	(C0.29)
	(C0.31)
-0.5	(C0.82)
	(C0.79)
	(C0.64)
-0.7	(C0.60)
	(C0.94)
-1.1	(C0.16)
	(C0.20)
-1.3	(C0.52)

1121
27
727
2062
2787
2820
2823

BARNETT NORTHERLY

Sta.	+ or -	H.I.	Elev.	Grade	
34+25	13-07	2078 2422	0.53	1.36	6.12
34+50	13-45	2078 2422	0.55	1.38	7.43
34+75	14-28	2357 2443	0.58	1.41	
Rt.	15-07.5	2357 2443	0.60	1.43	
34+98.15		2169 2401			
35+W	15-54	2078 2422	0.63	1.46	1.53 1.80 0.73 5.41 6.14
35+50	16-36.8	2078 2422	0.65	1.48	6.14 0.10 1.0 7.14
Rt.	16-53.1	9.27 9.27			
35+75	17-20	11.52 14.96	0.66	1.49	
35+75	17-55.5	2.150 20.19	0.68	1.51	
35+95.8			0.70	1.53	
36+50			0.77	1.60	4.54
37		24.27 24.22 26.01 5.98	0.82	1.65	4.49
+50			0.87	1.70	4.44
38			0.92	1.75	4.39
0	-4.91		0.15		
+50	+5.63	5.78	0.97	1.80	4.34

Westerly

- 1.7	C047
- 1.7	C024
- 1.7	C051
- 1.7	C080
-	F018
-	F005
- 1.7	F020
-	F04
- 1.3	F0019
- 1.2	C-0.18
- 1.1	C-0.59
- 1.4	F-0.06
- 1.6	B.M. C041 Elev. = 0.15
- 1.4	C-0.31

Easterly

- 1.1	C027
- 1.1	C070
-	C0.55
-	C0.82
- 1.1	C0.60
- 1.7	C0.67
-	C0.20
-	C0.58
- 1.2	C-0.50
- 1.0	F-0.30
- 1.3	C-0.87
- 1.1	C-0.20
- 1.1	C-0.39
- 1.1	F-0.02

BARNETT - Northwesterly

Sta.	+ or -	H.I.	Elev.	Grade	Red
39			1.03	1.86	478
+50		5.78	1.08	1.91	473
40			1.13	1.96	418
+50			1.19	2.02	412
41			1.24	2.07	407
+50			1.29	2.12	402
42			1.34	2.17	397
+50			1.39	2.22	451
43	0 -5.60 +5.84	6.00	1.44	2.27	446
+50			1.50	2.33	440
			1.57	2.40	433
			1.57	2.40	
39			1.63	2.46	427

$44 + 19.97 = \uparrow$
 $38 + 31.37 = \downarrow$

Westerly

521

Easterly

9

- 14	C-0.42	- 11	C-0.81
- 10	C-0.58	- 12	C-0.24
- 19	C-0.20	- 11	C-0.75
- 19	F-0.08	- 11	C-0.85
- 20	C-0.94	- 15	C-0.06
- 20	C-1.00	- 16	F-0.04
- 21	C-0.87	- 13	C-0.61
- 21	C-0.36	- 10	C-0.26
- 21	BM C-0.81 Elev. = 0.18	- 13	C-0.90
- 21	C-0.67	- 16	C-0.84
- 16	C-0.94	- 12	C-0.99
- 14	C-1.02	- 13	C-0.91

614
 420
 1.90
 4.83
 6.73

BARNETT Northerly

Sta	+ or -	HI.	Elev	Grade	Rad.
39+0		6.00	1.68	2.51	4.22
39+90.77	0-00		1.73	2.56	4.17
40+25	1-13.8		1.76		4.14
40+50	2-17		1.78	2.61	4.12
40+75	3-20.2		1.80		4.10
41	4-23.4		1.82	2.65	4.08
+25	5-26.6		1.84		4.06
+50	6-29.8		1.87	2.70	4.03
+75	7-33		1.89		4.01
42	8-36.2		1.91	2.74	3.99
+25	9-39.6		1.93	2.77	4.42
+50	10-42.6		1.96	2.79	4.40
+75	11-45.8		1.98		4.38
43	12-49		2.00	2.83	4.36
+25	13-52.2		2.02		4.33
+50	14-55.4		2.05	2.88	4.31
+75	15-58.6		2.07		4.29
44	17-02		2.09	2.92	4.27
44+23.90	18-02		2.11	2.94	4.25
44+50			2.13	2.96	4.23

29.97
27.97
26.14
23.86
25.00
23.80

Westerly

Easterly 10

-17	C-0.49	-1.3	C-0.90
-15	C-1.13	-1.8	C-0.81
-19	C-0.67	-1.2	C-0.12
-19	C-0.44	-1.2	C-0.34
-19	C-0.30	-1.1	C-1.00
-19	C-0.76	-1.1	C-0.96
-19	C-0.76	-1.7	C-0.67
-19	C-0.84	-1.7	C-0.49
-14	C-0.80		C-0.62
-14	C-1.02	-1.2	C-0.94
-14	C-0.19		C-0.77
-14	C-0.86	-1.6	C-0.85
-18	C-0.69		C-0.39
-18	C-0.68	-1.5	C-0.85
-16	C-0.70		C-0.38
-16	C-0.90	1.5	C-0.69
1.6	C-0.74		C-0.68
1.6	C-0.91	1.6	C-0.34
-1.6	C-1.16	2.2	C-0.79
-1.6	C-0.91	-2.1	C-0.73

673
407
2.66
4.53
7.19

Cont. Mon
B.M. Elev. = 1.47

Sta.	+ or -	H.I.	Elev.	West. Grade	R.I. 7.19		
45700				2.17	3.00	4.19	
150		+1.47 +1.34 6.81		2.14	2.95	4.24	
46				2.07	2.90	4.29	
150				2.02	2.85	4.34	
47				1.97	2.80	4.39	
150				1.94	2.75	4.44	
48				1.87	2.70	4.49	
150				1.81	2.64	4.55	
49 ^o	-4.48 +4.35			6.68	17.6	25.9	4.20
150				1.71	2.54	4.25	
50				1.66	2.49	4.30	
150				1.61	2.44	4.35	

x/westerly

±

Easterly. 11

	4.46	
- 1.6	C-0.58	- 2.3 C-0.83
- 1.4	C-0.56	- 0.9 C-0.60
- 1.2	C-0.73	- 1.6 C-0.78
- 1.0	C-0.55	- 1.9 C-0.83
- 1.0	C-0.68	- 1.1 C-0.65
- 0.7	C-0.45	- 0.9 C-0.93
- 0.7	C-0.68	- 0.6 C-1.10
- 0.5	C-0.45	- 0.5 C-1.12
- 0.2	C-0.79	- 0.3 B.M. Elev. = 2.33
Grade	C-0.21	- 0.4 C-0.78
+ 0.1	C-1.03	- 0.5 C-0.99
- 0.8	C-0.58	- 0.7 C-0.74

719
448
771
408
679

Sta	Hor -	HT	Elev.	West Grade	Pod (6.73)
51400		(6.68)	(1.56)	2.39	(4.40)
51450			(1.51)	2.34	(4.39)
51498.09			(1.45)	2.28	(4.45)
52450			(1.40)	2.23	(4.92)
53			(1.35)	2.18	(4.97)
53+5766	- 5.30 + 4.80	(6.18)	(1.30)	2.13	(5.02)
54			(1.25)	2.08	(5.07)
750			(1.20)	2.03	(5.14)
55			(1.15)	1.98	(5.17)
750			(1.09)	1.92	(5.23)
56			(1.04)	1.87	(5.28)
750			(0.99)	1.82	(5.33)

Westerly

6.80

Easterly

12

- 0.5	(C-0.63)	- 0.8	(C-0.63)
- 1.1	(C-0.80)	- 0.6	(C-0.90)
- 1.0	(C-0.15)	- 1.2	(C-0.99)
- 0.5	(C-0.80)	- 1.9	(C-0.54)
- 0.5	(C-0.96)	- 2.0	(C-0.51)
- 0.8	(C-0.41) IBM Elev. = 1.38	- 0.9	(C-0.40)
- 0.8	(C-0.61)	- 0.7	(C-0.74)
- 1.9	(C-1.02)	- 0.2	(C-0.75)
- 1.2	(C-1.09)	Grade	(C-0.52)
- 1.0	(C-1.07)	- 1.3	(C-0.77)
- 0.5	(C-0.74)	- 0.2	(C-0.62)
- 0.8	(C-0.52)	- 0.3	(C-0.50)

Sta	+ or -	H.I.	Elev.	West Grade	Rod	Westerly	Easterly
57		6.18	0.95	1.77	5.38	-0.9 C-0.56	-0.4 C-0.20
50			0.89	1.74	5.43	-0.8 C-0.78	-0.6 C-0.3
58			0.84	1.67	5.48	-0.8 C-0.68	-0.7 C-0.48
50 ^o	-5.27 +4.65	5.53	0.79	1.62	3.89	-0.6 C-0.45 B.M. Elev. = 0.91	-0.7 F-0.17
59			0.73	1.56	3.95	-1.1 C-0.60	-1.0 F-0.06
50			0.68	1.51	4.00	-1.3 C-0.64	-1.0 C-0.44
60			0.63	1.46	4.05	-1.4 C-0.48	-0.6 C-0.84
50			0.58	1.41	4.10	-1.5 C-0.85	-0.7 C-0.94
61			0.53	1.36	4.15	-1.5 C-1.08	-1.0 C-0.74
50			0.48	1.31	4.20	-1.7 C-1.09	-1.1 C-0.19
62			0.43	1.26	4.25	-1.6 C-0.98	-1.3 C-0.99
62+50			0.37	1.20	4.31	-1.6 C-0.65	-1.4 C-0.65

586
094
4925.32
4.10
1.22
4.64
5.86

Sta.	+ or -	H.I.	Elev.	Grades			
				W.	E	W	E
67+50				3.90	4.73	4.46	
		H.I.		Road Readings			
		8.20		W.	E		
0+65				2.59	3.85	5.40	6.08
1+00				4.09	4.91	5.17	5.53
1+40				4.50	4.28	4.91	4.91
1+60.83	2.82 ✓			3.78	3.82	4.91	4.91
2+00	3.00 ✓			4.42	4.38	4.78	4.77
2+50	3.23 ✓			3.73	3.42	4.60	4.54
3+00	3.46 ✓			4.47	4.78	4.60	4.54
				3.28	3.40	4.37	4.23
				5.03	3.40	4.14	4.14
				5.12	4.80	4.14	3.92
3+50	7.60 ✓					3.91	3.67
4+00	3.92 ✓					3.68	3.31
4+50	4.15 ✓					3.45	3.00
5+00	4.38 ✓					3.22	2.69
5+50	4.61 ✓					2.99	2.39
6+00	4.84 ✓					2.76	2.08
6+13 R.R.	4.90 ✓					2.70	2.00
Ret around						1.80	1.80

Westerly

±

Easterly 15

630
176
8.06
7.35

0.71
595
6.66

C-053

-7.0			
35			
-7.6	F-0.17	F-0.13	-7.1
35.4	F-0.04	F-0.29	28
-3.1	F-0.26		-3.7
21.8	F-0.23	C-0.3	17.6
-2.3			-2.2
21.3	C-0.69	C-0.59	15.3
-2.1			-1.6
19.4	C-0.42	C-0.37	17.2
-1.8			-1.3
18.8	C-0.25	C-0.55	13.4
-1.2			-1.5
17.6	F-0.06	C-0.52	13.8
-1.5			-1.3
18.3	F-0.04	C-0.43	12.6
-1.6			-0.7
17.8	C-0.09	C-0.91	12.4
-1.4			-1.4
17.4		C-0.64	12.0
		F-0.31	

Westerly

666

Easterly

Stn.	+ or -	H.I.	Elev	W. E.	W. E.
		(7.60)			
6753			250	1.67	✓
6763 = Ret. Rt.	5.12	✓	2.48	(4.66) 2.70 2.86 1.78	1.65 117
Return Around					0.97
7700	5.18	✓	2.47	(4.62) 2.04	1.59 1.21
7750	5.29	F0.65	2.33	(4.56) 2.10	1.50 1.27
	(6.84)				
8703.75 = Ret. Lt.	4.59	✓	2.25	(4.50) 2.76	1.42 1.33
Ret. Around			2.20		1.37
8753.75 = Ret. Lt.	4.55	✓	2.29	(4.44) 2.22	1.46 1.39
Ret. Around			2.20		1.37
9700	4.53	✓	2.31	(4.38) 2.28	1.48 1.45
9750	4.41	✓	2.36	(4.32) 2.54	1.53 1.51
10700	4.43	✓	2.41	(4.26) 2.40	1.58 1.57
10700	4.39	✓	2.45	(4.20) 2.46	1.62 1.63
10765 (S.B.)	4.34	✓	250	(4.16) 2.50	1.67 1.67
11700	4.40	✓		(4.22) 2.44	1.61

-12 172	CO.22	Blank
		CO.90 -12 12.6
		F0.32
-13 175	F0.06	CO.56 -07 12.2
-12 172	CO.52	CO.38 -08 12.2
		CO.43
-15 178	CO.33	CO.43 -15 13.2
	CO.65	
-12 168	CO.20	CO.69 -14 12.7
	CO.08 CO.63	
-11 174	CO.26	CO.74 -16 13.6
-15 178	CO.27	CO.44 -12 14.0
-12 162	CO.45	CO.42 -22 14.2
-21 192	CO.50	CO.20 -22 14.6
-21 196	CO.45	CO.27 -12 14.2
-25 210	CO.50	CO.29 -18 14.8

Sta.	+ or -	H.I.	Elev	Int Grade	
11472.57 (2 nd oik)		4.49 ✓	<u>4.31</u> 2.35	1.52	
12400	<u>6.89</u>	4.57 ✓	<u>4.39</u> 2.27	1.44	
1300		4.65 ✓	<u>3.64</u> 2.19	1.36	
13400		4.46 4.74 - F0 72	<u>3.73</u> 2.10	1.27	
1450	<u>6.15</u>	4.13 ✓	<u>3.81</u> 2.07	1.19	
14700		4.22 ✓	<u>3.90</u> 1.93	1.10	
14458.57 Rd. Lt		4.31 ✓	<u>3.99</u> 1.84	1.01	
Rd Around		4.55 ✓	1.60	0.77	
14488.57			<u>4.00</u> 1.80	0.97	
15718.57 Rd. Lt		4.35 ✓	<u>4.03</u> 1.80	0.97	
Rd Around		4.55 ✓	1.60	0.77	
15450		4.30 ✓	<u>3.98</u> 1.85	1.02	
16400		4.23 ✓	<u>3.91</u> 1.97	1.09	

Welderly

190-T.P.
4.04
5.94 - H.I.

Right 17

-24 193	C-060	666 ✓35 1.31 452 5.83	C-0.15	-18 142
-24 192	C-087		C-0.14	-24 144
-22 202	C-072		C-0.35	-27 162
-24 206	C-050		C-0.53	-30 156
-26 204	C-035		C-0.65	-12 158
-25 198	C-083		C-0.49	-23 140
-28 206	C-093		F-0.07	-27 156
	F-0.60			
			C-0.26	-24 152
-22 194	C-083		F-0.10	-26 154
	F-1.08			
-27	C-1.27		C-0.50	
-21	C-0.42		C-0.40	-30 166

Sta.	H.F.	Elev.	Cont Seals
16400	4.18 ✓ 4.15 6.15 1.07 5.08	✓	386 197
17400	4.13 ✓	✓	381 202
1750	4.08 ✓	✓	375 207
18400	4.02 ✓ 6.13	✓	370 213
1850	3.77 ✓ 3.26	✓	2.18 495 135
19400	3.92 ✓ 4.06	✓	2.23 480 140
1950	4.37 ✓	✓	2.28 475 145
20400	4.32 ✓ 6.65	✓	2.33 490 150
1950	4.26 ✓	✓	2.39 464 136
20+82.38 = (0-10 ft)	4.22 ✓	✓	2.43 460 160
21+2339 Ref. Pt.	4.18 ✓	✓	2.47 456 164
Ref. Around	4.18 ✓	✓	2.47 164 456
21+48	4.15 ✓	✓	2.50 167 453

-38 22°	C-0.35	C-0.15	-38 174
-38 218	C-0.61	F-0.08	-37 178
-38 218	C-0.86	C-0.38	-39 182
-38 234	C-0.58	F-0.26	-36 176
-37 226	C-0.65	C-0.27	-40 178
-45 248	C-0.14	C-0.32	-39 178
-47 242	C-0.71	C-0.50	-40 182
-47 244	C-0.70	C-0.37	-42 184
-39 228	C-0.19	C-0.36	-38 176
-38 230	C-0.25	C-0.43	-38 176
-38 226	C-0.08	C-0.94	-52 228
	F-0.29		-52 213
	- Blank -	C-0.30	

594-HI. 2
483
7.11
509
6.20

5.83
476
1.07
Temp 13.77
18400
on East.

Sta.	Cor-	H.I.	Elev.	Cont. Seal
21+23.39	Rt. Lt.	4.15	✓	2.50
	Ret. Ground	4.15	✓	2.50
21+00		4.21	✓	2.44
150	665	4.26	✓	2.39
23+00		4.32	✓	2.33
150		4.37	✓	2.28
24+00		4.43	✓	2.22
150		4.48	✓	2.17
25+00		4.54	✓	2.11
150	(653)	4.47	✓	2.06
26+00	to S.B.	4.53	✓	2.00
150		4.48	✓	2.05
27+00		4.42	✓	2.10

(453)
 1.67
 1.67
 (459)
 1.67
 (464)
 1.56
 (470)
 1.50
 (467)
 1.45
 (473)
 1.39
 (478)
 1.34
 (484)
 1.28
 (489)
 1.23
 (495)
 1.17
 (490)
 1.22
 (485)
 1.27

Westarky 6.20
 4.84
 1.36
 4.76
 6.12
 Exuly 19

-6.3
 29° C-0.17
 -5.5
 27° C-0.10
 -3.7
 23° C-0.39
 -3.7
 23° C-0.13
 -4.1
 23.4 Grade F-0.14
 -4.2
 23.6 C-0.10 F-0.15
 -4.6
 24.2 C-0.30 F-0.22
 -4.6
 24.0 C-0.04 F-0.17
 -4.6
 24.2 C-0.21 C-0.68
 -5.0
 25.8 F-0.26 C-0.39
 -4.8
 24.0 Grade C-0.68
 -4.6
 24.2 C-0.17 C-0.63
 -4.2
 23.8 C-0.07 C-0.75

-4.7
 20.8
 -3.9
 18.0
 -4.0
 18.0
 -4.6
 19.2
 -4.8
 19.6
 -4.7
 19.6
 -4.4
 19.2
 -4.5
 19.4
 -4.3
 18.8
 -4.3
 18.6
 -4.7
 19.4
 -4.7
 19.6

Sta	+ or -	H.I.	Obs.	Cont Grades
27750	6.50	4.38	✓	2.15
28750		4.33	✓	2.20
290		4.28	✓	2.25
29450		4.23	✓	2.30
290		4.18	✓	2.35
30450		4.13	✓	2.40
30416 = (0'10' LT)		4.11	✓	2.45
30450		4.29	✓	2.45
31450 = S.B.		4.24	✓	2.50
290	674 H.I.	4.29	✓	2.45
32450		4.34	✓	2.40
290		4.39	✓	2.35
33450		4.44		2.30

Westerly	612 4 509	629	Easterly	20
	1.03		632	
	5.29		1.59	
			73	
4 4 240	C-0.33		C-0.48	-47 196
	C-0.21		C-0.53	-53 204
	C-0.78		C-1.25	762 - 11 194
	F-0.25		F-0.44	
	C-0.03		Grade	
	C-0.30		F-0.13	
	C-0.37	T.P. on West 30416	F-0.41	
	F-0.28	elevs 171	F-0.65	
	F-0.73		F-0.51	
	C-0.11		C-0.13	
	C-0.10		F-0.32	
	F-0.16		F-0.50	
	C-0.09		C-0.66	

Sta	+ or -	H.I.	Cor.	Cont Index	
27+50		4.38	✓	2.15	(480) 1.3✓
28+00	6.53	4.33	✓	2.20	(475) 1.37
29		4.28	✓	2.25	(470) 1.42
29+00		4.23	✓	2.30	(465) 1.47
30		4.18	✓	2.35	(460) 1.52
30+00		4.13	✓	2.40	1.57
30+16 = (0-10' Lt)		4.11	✓	2.42	
30+50		4.29	✓	2.45	
31+00 = S.B.		4.24	✓	2.50	
31	674 H.I. 84	4.29	✓	2.45	
31+00		4.34	✓	2.40	
32		4.39	✓	2.35	
33+00		4.44		2.30	

Westerly

612 4
509
1.03
5.29
639

Easterly 20

632
1.59
73

6.74
472

202 T.P.
4.90

692 H.I.

6.92
4.58

2.34 T.P.

6.86
4.58

2.28 T.P.

14

Inspector

WATSON, VAHLE & CO

Daily Report of Work Done

Name of Job

KIND OF

3.89	3.06	3.08	3.08
4.28	3.16	3.08	3.08
4.27	2.78	3.08	3.08
5.33	2.55	3.08	3.08
1.81	2.52	3.08	3.08
3.35	2.52	3.08	3.08

5.56

4.78
79
3.99

3.61
2.60 H.I
5.92

1.68 T.P
5.16

6.84 H.I
5.46

1.38 T.P
4.77

6.15 H.I
4.53

4.52 T.P
1.62

5.83
6.65 H.I
4.90

1.70 T.P
4.83

6.53 H.I
4.82

1.71 T.P
1.703
6.74 H.I

6.74
4.72
2.02 T.P
4.90
9.2 H.I

14

6.9
4.58
2.34 T.P

6.86
4.58
2.28 T.P

3.61

7.60
4.54
3.06

7.60
4.54
3.06

6.74
2.42
4.32

Signed

Inspector

5.65
1.34
4.31

5.65
2.53
3.12

5.36
6.62
1.26

0.88
3.27
4.35

5.65
1.34
4.31

Job No

From

To

By

Date

Time

Rate

Total

Remarks

Sta.	tor-	H.F.	Elev.	Cur sides
33 + 100	6.74	4.49 ✓		2.25
34 + 100		4.54 ✓		2.20
100		4.59 ✓		2.15
35		4.64 ✓		2.10
100		4.69 ✓		2.05
36 + 100 (3/3)		4.74 ✓		2.00 2.00 W E
100	6.92	4.83 ✓	4.88 ✓	2.09 2.04
37 + 100		4.74 ✓	4.83 ✓	2.18 2.09
100		4.65 ✓	4.79 ✓	2.27 2.13
38 + 100	6.90	4.53 ✓	4.72 ✓	2.37 2.18
100	6.88	4.42 ✓	4.66 ✓	2.46 2.32
39 + 100	6.88	4.33 ✓	4.61 ✓	2.55 2.27

Westly

Eastly

21

Westly	E	Eastly
	6.29 5.42 0.87 5.27 6.14	
F-0.14		C-0.31
C-0.04		C-0.14
F-0.06		C-0.64
F-0.40		C-0.72
C-0.20		C-1.00
F-0.14		C-1.00
F-0.12		C-0.69
F-0.49		C-0.61
F-0.39		C-0.43
F-0.09		Grade
C-0.49		C-0.09
C-0.50		C-0.26

Sta.	+ or -	HT.	Elev.	Cont Grades	
				W	E
39150	6.84	422	454	294	232
40400		413	450	273	236
+50		405	445	281	241
41400		395	441	291	245
41428.90 Lot. Cw		50.7			
414487 (P.C.) 0-00		386	436	300	250
+75 0-28.5				298	246
42 0-50				296	243
+25 1-11.5				294	239
+50 1-33				293	236
+75 1+54.5				291	233
43 2-15.5				290	230
+25 2-37				288	226
+50 2+58.5				287	223
+75 3-20.0				285	220
44 3-41.5				283	217
+25 4-03				281	213
+50 4-24.5				280	210
+75 4-46				278	207
45 5-07.5				277	204

Westly

Eastly 22

C-0.56	234 414 646	C-0.13
C-0.47		C-0.64
F-0.18		C-0.36
C-0.34	T.P. on 41+41.87 West Elev = 2.28	C-0.26
C-0.17		F-0.17
F-0.60		C-0.23
C-0.26		C-0.10
C-0.72		C-0.51
C-0.72		C-0.46
C-1.00		C-0.66
F-0.37		C-0.79
F-0.50		C-0.80

+25	5-28.5	275	2.00
45+50	5-50.5	274	1.97
+75	6-12.0	272	1.94
46	6-33.5	270	1.91
+25	6-55	268	1.87
+50	7-16.5	267	1.84
+75	7-38	265	1.80
47	7-59.5	264	1.77
+25	8-21	262	1.74
+50	8-42.5	261	1.71
+75	9-04	259	1.67
48	9-25.5	257	1.64
+25	9-47	255	1.60
+50	10-08.5	254	1.57
+75	10-30	252	1.53
G. Brock 49+0286	10-54	250	1.50
+25	11-13	251	1.53
+50	11-34.5	253	1.56
+75	11-56	255	1.60
50	12-17	257	1.63
+25	12-38.5	259	1.66
+50	13-00	261	1.69
+75	13-21.5	263	1.72
51	13-43	264	1.76
+25	14-04.5	265	1.79
+50	14-26	267	1.82

West		East 23
	646	
	516	
F-063	1.30	C-0.78
	512	
F-050	6.42	C-0.81
F-049		C-0.43
F-058		C-0.99
F-044		C-0.77
F-044		C-1.09
F-049	6.42	C-0.66
F-065		C-0.60
F-055		C-0.63
F-060		C-0.57
F-058		C-0.68
F-032		C-0.81
F-024		C-0.79

+25	14-47.5	2.69	1.85
52	15-09	2.71	1.89
+25	15-30.5	2.73	1.92
+50	15-52	2.75	1.95
+75	16-13.5	2.77	1.98
53	16-35	2.78	2.00
+25	16-56.5	1.80	2.05
+50	17-18	2.81	2.08
+75	17-39.5	2.83	2.11
54	18-01	2.84	2.15
+25	18-22.5	2.86	2.18
+50	18-44	2.87	2.21
+75	19-05.5	2.89	2.25
55	19-27	2.91	2.28
+25	19-48.5	2.93	2.32
+50	20-10	2.94	2.35
+75	20-31.5	2.96	2.38
56	20-53	2.97	2.41
+25	21-14.5	2.99	2.45
56+63.80			
= Equation	21-48	3.00	2.50
57+41.75			
58			
+50			

642

C-0.21	C-0.77
F-0.02	C-0.18
C-0.03	F-0.22
C-0.11	C-0.60
grade	C-0.04
F-0.03	C-0.26
C-0.04	C-0.52
C-1.49	F-0.07
C-0.80	C-0.52
F-0.24	F-0.19
F-0.40	C-0.45
F-0.27	C-0.53

642
4.97
1.45
4.78
6.13

Sta.	W.E	W. E		
59		$\frac{431}{192}$ $\frac{466}{157}$	F-0.20	$\frac{182}{33}$ $\sqrt{1.5}$ C-0.15
+50		$\frac{439}{184}$ $\frac{469}{154}$	F-0.71	Grade
60		$\frac{446}{177}$ $\frac{473}{150}$	C-0.28	C-0.26
+50		$\frac{454}{169}$ $\frac{476}{147}$	F-0.52	C-0.42
61		$\frac{462}{167}$ $\frac{479}{144}$	C-0.02	C-0.17
+50		$\frac{470}{153}$ $\frac{482}{141}$	C-0.36	C-0.32
62		$\frac{477}{146}$ $\frac{485}{138}$	C-0.36	C-0.65
+50		$\frac{482}{138}$ $\frac{488}{135}$	C-0.52	$\frac{623}{446}$ $\frac{1.77}{438}$ $\frac{6.15}{}$ C-0.72
G.B. 62485	2.15 2.15	$\frac{491}{132}$ $\frac{491}{132}$	F-0.03	C-0.67
63		$\frac{489}{134}$	C-0.96	C-0.75
+50		$\frac{484}{139}$	C-0.36	C-0.64
64		$\frac{470}{145}$	F-0.07	C-0.45
+50		$\frac{463}{150}$	C-0.93	C-0.09

	166 83 √49		W. } E.	459 156
65		.7		
+50	538 33 5.71	+20		454 1.61
66		.05		448 1.67
+50				443 1.72
67				437 1.78
+50			✓	432 1.83 1.66
68		2.21	2.54	1.71 (4.05)
+50		2.26	2.59	1.76 (4.00)
69		2.31	2.64	1.81 (3.95)
+50	9.13	2.36	2.69	1.86 (3.90)
70		2.31	2.64	1.81 (3.95)
+50		2.26	2.59	1.76 (4.00)
710	HI = 5.76	2.21	2.54	1.71 (4.05)
+50		2.16	2.49	1.66 (4.10)
72		2.11	2.44	1.61 (4.15)
+50		2.06	2.39	1.56 (4.20)
72+93.50 B.V.C.		2.02	2.35	1.52 (4.24)
73+25		2.30	2.63	1.80 (3.96)
+50		3.00	3.33	2.50 (3.26)
+75		4.00	4.33	3.50 (2.26)

	232	576 410 1.66
	6.15	
C-0.41	319 895	F-0.29
C-0.48	5.76	F-0.15
F-0.44		C-0.06
F-0.45		C-0.48
F-0.34		C-0.67
F-0.72		C-0.80
F-0.16		C-0.87
F-0.46		C-0.09
F-0.25		C-0.15
C-0.02		C-0.50
F-0.23		F-0.20
		C-0.09
F-0.31		F-0.48
		F-0.20
		F-0.87
		F-0.30
		F-0.76
		F-0.46
		F-0.90
		F-1.94

Government Property

Right

Sta. + or - H.I. Elev. Base Line

3+00

28.5

39.7
12

Interpolate on Out

2+85

37.7

47.7
50

51.5
100

55.1
150

2+50

43.9

49.7
50

54.7
100

56.0
150

2+20

47.0

54.7
35

56.5
50

56.0
100

57.7
150

2+00

50.7

58.7
50

58.7
100

60.0
150

1+50

43.6

58.7
50

60.5
100

61.5
150

1+00

58.4

61.5
50

61.7
100

0+50

61.7

60.4
50

63.1
100

0+00 = (S.W. Corner of U.S. Gov. Prop) 54.2

B.M. +11.00 (66.47) 55.47

Elev. of Top of Lot Corner (Run by R. Keys)

28
±
Base
Line

Left.

Sta. + or - H.I. Elev.

3+00

2+85

44.69

2+70

2+20

2+00

1+50

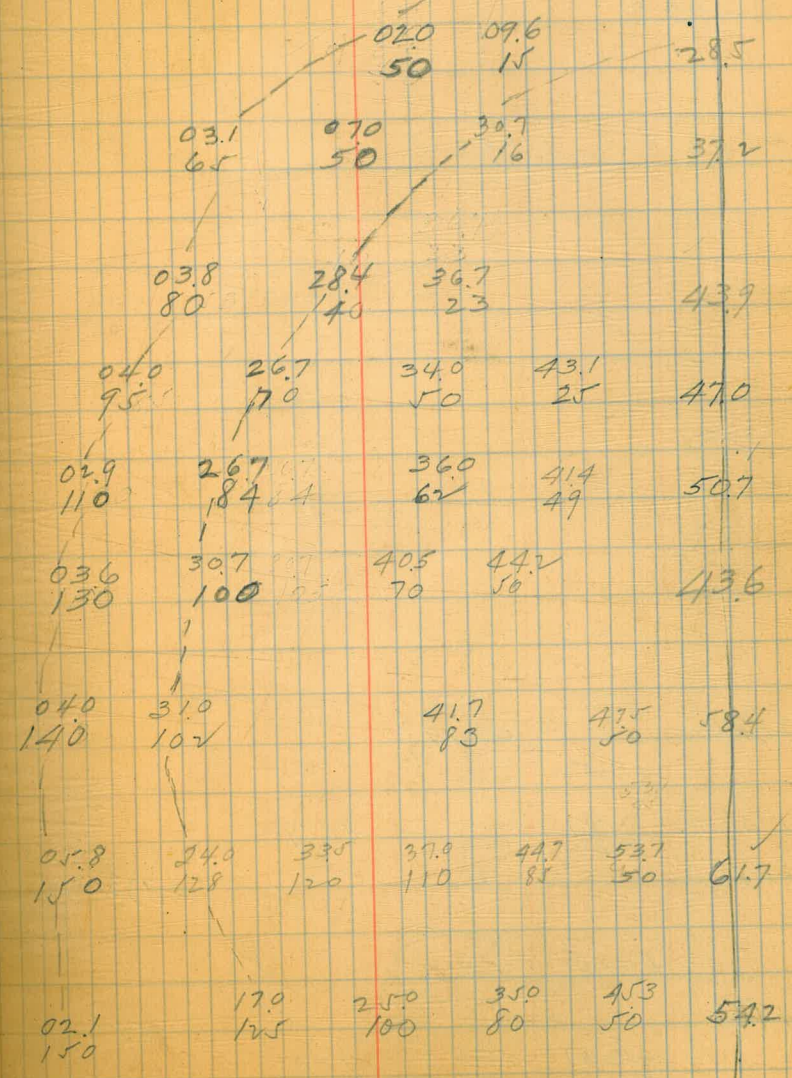
1+00

0+50

0+00

(= S.W. Cor. U.S. Gov. Prop.)

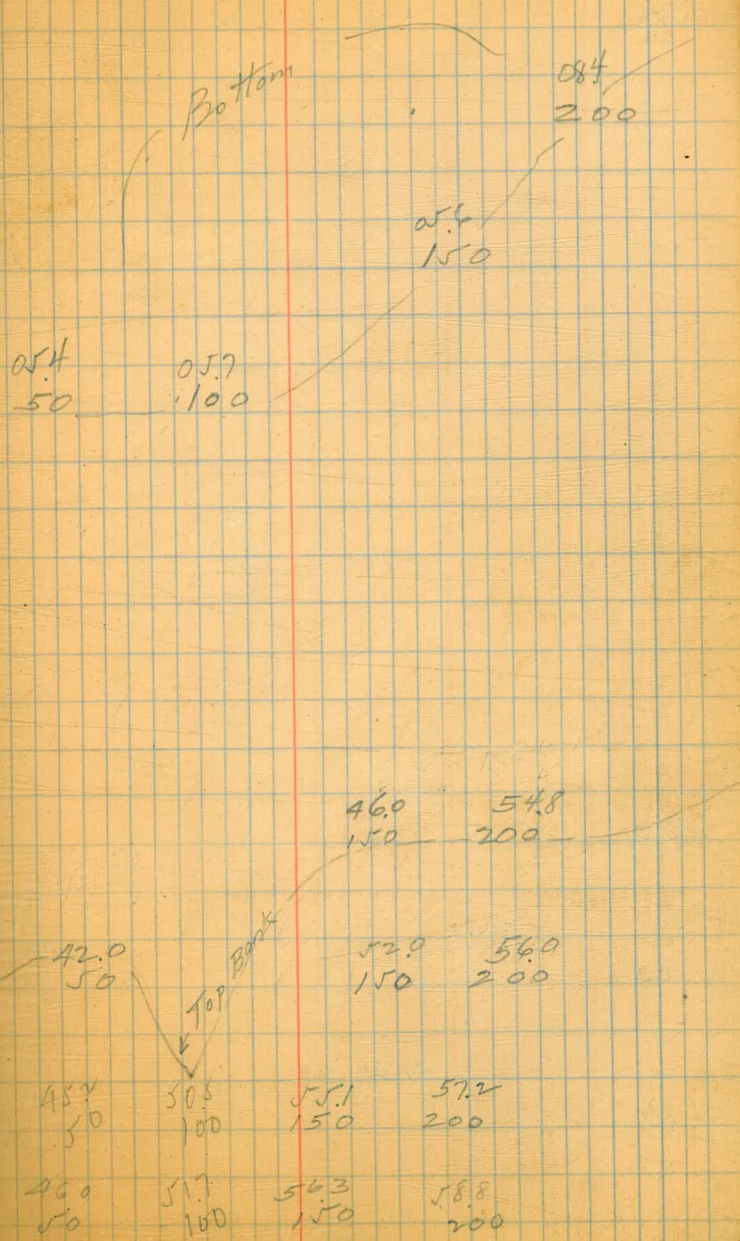
66.47



Government Prop d.

Sta.	+ or -	H.I.	Elev.	Baseline
4+10				
3+98		(9.70)		
3+86				
3+60		(44.69)		
	+2.50			
	-12.97		42.19	
3+50				39.3
	+1.16	(55.16)		
3+40				35.1
	-12.47		54.00	
3+26				35.6

Right



32

Sta.

+ or -

H.I.

Elev.

3+86

3+50

3+40

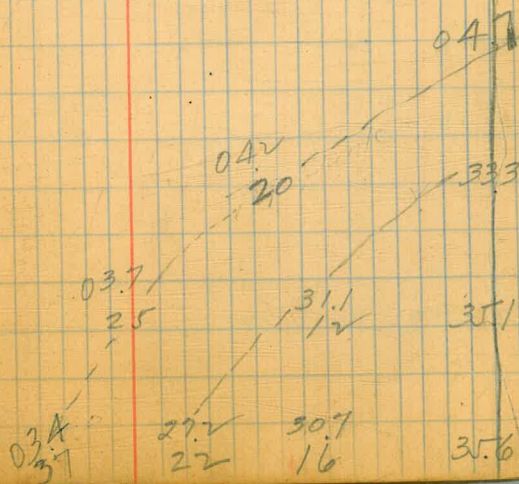
3+26

44.69

Left.

30

Baseline



X-Sections of
Private Property
South of Lot #2

$\frac{d}{=}$
Base line
Produced
back.

-0+64

210

-(0+27)

450

0+00 = (S.W. Cor. Govt. Prop.) 54W

West Side
of
Govt Line Produced Back

31

120	08.5	04.0	01.0
50	80	125	154

31.2	210	12.0	01.2
50	80	125	154

✓ 45.3	✓ 350	✓ 250	✓ 170	✓ 02.5
50	80	100	125	154

Curb
Shades

East

Sta

E. W

N.W. Curb Return -

0+08.2 End Curb at Trk. 9.06 6.33 2.73

1/2 Arc. 6.41 6.41 2.65

Return on Loma Blvd. 6.50 2.56

1+60.83 9.06 4.80 4.78 4.23

1+40.00 5.10 5.10 3.76

1+0.0 5.55 5.53 3.63

0+65 5.91 3.18

0+50 6.12 6.10 2.90

0+47 6.40

0+25 6.60

End Curb 70+09 6.70 1.23 3.69 5.37

70+00 9.06 6.70

End Curb 69+65.48 6.81 5.45

69+50 6.78 1.33 3.61

69+00 6.70 1.03 5.37 3.69

68+75 6.60 1.33 5.07 3.79

68+50 6.40 5.07 3.99

F1 12

F2 48

F2 37

F1 18

F1 10

F1 36

F1 94

F1 40

F0 44

F2 78

E0

F0 44

F0 68

F1 53 = F0 69 Top Rail

F1 30 = F0 79 Top Rail

F0 84

F0 30

F0 82

Carl
Hall

E. W.

68+25

906

6.10¹³³ 477.

429^v

F0⁸¹

68+00

5.70¹³³ 437

469^v

F1¹²

67+83

5.40

F1⁰⁸

67+50

4.73 390

566^v

67+00

3.77 299

662^v

+25

66+50

280

66+25

2.37

66+00

200

65+75

167

65+50

140

65+25

122

65+00

110

E.

6.30
2.37

8.67 = H.I.

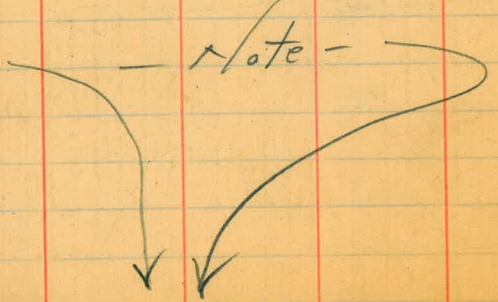
33

Dope for Cut-off Wall

Station	H.I.	L-Rt.	Stadia Dist.	Actual Rod
		45°09'	54'	3.27
		45°09'	54'	7.27
		59°06'	46'	9.48
		59°06'	59'	6.8
		75°20'	40'	9.48
	H.I.	75°20'	65'	7.5
	(6.53)	90°54'	79'	7.0
		90°54'	52'	9.5
		103°30'	61'	9.5
		103°30'	105'	6.9
		127°50'	96'	10.0
		134°03'	135'	10.3
		124°38'	185'	10.2
		125°42'	282'	10.4

Top. South End Ht. Wall
 Natural - Surface
 F.L. & South Barrel
 Natural Surface - Rf-R/W
 F.L. & North Barrel
 Natural Surface - Rf-R/W
 " " - Rf-R/W
 Natural Surface Slough
 " " "
 Natural surface Rf-R/W
 N.S. Slough
 N.S. "
 N.S. "
 N.S. "

Note - 5.7 Rod on Bottom Rip Rap - 17' - Beyond Fence -



Set up on 1467.46 - Back Sight on 0+00 - Wound up Gun to Rt.

Sta.	H.I.	West Side	W Rod	East Side	East Rod	West + or -	East + or -
65+19.28	9.24	1.10	8.1	$\frac{65+25}{1.20}$	8.0	$\frac{-1.5}{12}$	$\frac{65+25}{-2.2}$ 12
50		1.20	8.0	1.40	7.8	$\frac{-2.6}{16}$	$\frac{-3.6}{17}$
+75		1.35	7.9	1.67	7.6	$\frac{-2.8}{16}$	$\frac{-3.3}{17}$
66		1.60	7.6	2.00	7.2	$\frac{-4.1}{16.5}$	$\frac{-2.0}{12}$
³⁰ 66+26.08		1.90	7.3	2.37	6.9	$\frac{-5.5}{19.5}$	$\frac{-4.0}{19.1}$
+00	1-00	2.22	7.0	2.80	6.4	$\frac{-3.6}{17}$	$\frac{-5.8}{49}$
+75	2-02.4	2.60	$\frac{6.6}{6.6}$	3.28	6.0	$\frac{-3.2}{18}$	
67	3-04.8	2.98	6.3	3.76	5.5	$\frac{-4.4}{20}$	$\frac{-6.1}{48.5}$
+25	4-07.2	3.36	5.9	4.24	5.0	$\frac{-4.3}{20}$	
+50	5-09.6	3.74	5.5	4.72	4.5	$\frac{-5.0}{22}$	$\frac{-6.8}{50}$
+75	6-12	4.12	5.1	5.20	4.0	$\frac{-6.1}{21}$	
68	7-14.4	4.50	4.7	5.70	3.5	$\frac{-6.0}{21}$	$\frac{-7.1}{49}$

		HI.	West Side	W 4.3 Rod	East Side	East Rod 3.1	West -8 22	-6 48 East + or -
68+25	8-16.8	9.29	4.90		6.10		+ or -	
+50	9-19.4	9.24	5.20	4.0	6.40	2.8	-8 23	-4 47
+75	10-21.6		5.47	3.8	6.60	2.6	-8 23	0 40
69	11-24		5.70	3.5	6.70	2.5	-6 22	
+25	12-26.4		5.80	3.4	6.74	2.5	-2 15	
+50	13-28.8		5.90	3.3	6.78	2.4	+1 12	
+75	14-31.2		6.00	3.2	6.81 =	69+66		
E.C. 69+95.75	15-23 ✓		6.00	3.2				
70+25	16-35.4 ✓							
+50	17-37.8 ✓							
+75	18-40.2 ✓							
71	19-42.6 ✓							
+25	20-45 ✓							

Corrected B.M.

1.474 = 1700. - Sta. 444 = 2.90

7175640 - 22.04

27) 325
27
55
14
100

-2.8 on Lower = East.
-2.5 on Upper = West.

- Mr. Watson -

- ① Staked the Culvert at sta. 5+50± but did not extend the pipe outside of our R/W. account of possibility of getting in Dutch.
- ② Would suggest Headwalls on both ends to protect shoulder
- ③ Staked the upper flow line at -2.5 Elev. and lower flow line at -2.8 Elevation.

{ Upper Flow is on West Side
Lower " is " East "

729.08
116.99
1309

53
175
1500.86
1225

625
500
120
48

