

NAME Causeway
X-Sections
Class _____ Course _____ Party _____

WATSON, VALLE & GOUGH

~~480~~
1461

FIELD NOTES

No. 403P

ESPECIALLY ADAPTED

TO THE USE OF

ENGINEERING STUDENTS

EUGENE DIETZGEN Co.

MANUFACTURERS

DRAWING MATERIALS

MATHEMATICAL AND SURVEYING INSTRUMENTS

MEASURING TAPES

CHICAGO SAN FRANCISCO NEW YORK
NEW ORLEANS PITTSBURGH

MICROFILMED

DEC 23 1964

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X-Sections - Barnett to RR, Trk - 1

Revised Alignment - 13-14

" X-Sections - 16-23

Light Standard Stations - Pages 24-25

Sta. + H.I. - Elev.

52400

51400

50400

49400

48400

47400

46400

45450

45400

44450

St. Chapman
June 13-14

| Left | | | | | | | | | | Right | | | | | | | | | |
|------|--|--|--|--|--|--|--|--|--|-------|--|--|--|--|--|--|--|--|--|
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Cont from Book 380 - 34

Sta. + HI - Elev.

62+00

61+00

60+00

59+00

58+00

57+00

56+00

55+00

54+00

53+00

5.09

HI
3.51

6.40

HI
~~4.67~~

4.67
+0.15
3.36
3.51

.8
5.6
5.0

1.3
5.1
5.0

1.5
5.9
5.0

| | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|
| -4 | -5 | -4 | 00 | -1 | -1 | | |
| 5.5 | 5.6 | 5.5 | 5.1 | 5.5 | 5.5 | | |
| 5.0 | 2.5 | 1.5 | | 1.0 | 5.0 | | |
| -2 | -1 | 2 | 5 | .6 | 00 | | -1 |
| 5.3 | 5.5 | 4.4 | 4.6 | 4.5 | 5.1 | | 5.5 |
| 5.0 | 2.5 | 1.5 | | 7 | 1.1 | | 5.0 |
| .3 | 00 | .7 | | .7 | .1 | .6 | .4 |
| 4.8 | 5.1 | 4.9 | 6 | 4.4 | 5.0 | 4.5 | 4.7 |
| 5.0 | 2.5 | 1.5 | 4.5 | 6 | 1.2 | 1.5 | 5.0 |

| | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|
| .6 | .3 | 1.0 | 9 | 1.1 | 2 | .6 | .7 |
| 5.8 | 6.1 | 5.4 | 5.5 | 5.3 | 6.2 | 5.8 | 5.7 |
| 5.0 | 2.5 | 1.5 | | 6 | 1.2 | 1.5 | 5.0 |
| .7 | .6 | 1.2 | 1.3 | 1.4 | .7 | .9 | 1.6 |
| 5.7 | 5.8 | 5.5 | 5.1 | 5.0 | 5.7 | 5.5 | 5.8 |
| 5.0 | 2.5 | 1.5 | | 6 | 1.2 | 1.6 | 5.0 |

| | | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| .7 | .8 | 1.3 | 1.2 | .9 | 1.0 | .6 | 1.3 | .9 |
| 5.7 | 5.6 | 5.1 | 5.4 | 5.5 | 5.4 | 5.8 | 5.1 | 5.5 |
| 5.0 | 2.5 | 1.5 | 5.4 | 6 | 1.0 | 1.4 | 3.6 | 5.0 |
| 1.2 | 1.0 | 1.6 | 1.4 | 1.3 | .8 | 1.1 | 1.5 | |
| 5.5 | 5.4 | 4.8 | 5.0 | 5.1 | 5.6 | 5.3 | 4.9 | |
| 5.0 | 2.5 | 1.5 | 5.0 | 1.0 | 1.3 | 2.7 | 5.0 | |

| | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|
| .8 | 1.0 | 1.6 | 1.4 | 1.6 | .9 | 1.7 | 2.1 |
| 5.6 | 5.4 | 5.8 | 5.0 | 4.8 | 5.5 | 4.7 | 4.3 |
| 5.0 | 3.0 | 2.5 | 1.5 | 5.0 | 1.0 | 1.2 | 3.5 |

| | | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 1.3 | 1.3 | .5 | 1.4 | 1.2 | 1.2 | .3 | 1.8 | 1.1 |
| 5.1 | 5.1 | 5.9 | 5.0 | 5.2 | 5.2 | 6.1 | 4.6 | 5.3 |
| 5.0 | 3.0 | 2.5 | 1.5 | 5.2 | 6 | 1.5 | 3.3 | 5.0 |

| | | | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|------|------|
| 1.5 | 1.7 | 1.1 | 1.8 | 1.7 | 1.7 | 1.0 | 1.1 | -1.0 | -1.0 |
| 5.9 | 5.5 | 6.3 | 5.6 | 5.7 | 5.7 | 6.4 | 6.3 | 8.4 | 8.8 |
| 5.0 | 3.0 | 2.5 | 1.5 | 5.7 | 1.0 | 1.5 | 3.0 | 4.2 | 5.0 |

5.82 = HI. 7.40

Left Right (2)

Sta. + H.I. - Elev.

68+50

68+00

67+50

67+00

66+50

66+00

65+50

65+00

64+00

63+00

Left

±

Right (3)

| | | | | | | | |
|------|------|-----|-----|-----|-----|-----|------|
| -2.3 | -1.9 | 3.2 | 1.5 | 3.4 | .8 | .8 | |
| 11.5 | 11.1 | 6.0 | | 5.8 | 8.4 | 8.4 | |
| 5.0 | 3.9 | 1.4 | 5.7 | 11 | 2.9 | 5.0 | |
| -2.0 | -1.5 | 1.7 | | 1.7 | -3 | -5 | -1.9 |
| 11.2 | 11.7 | 7.5 | 1.7 | 7.5 | 9.5 | 9.7 | 11.1 |
| 5.0 | 2.7 | 1.4 | 7.5 | 11 | 2.6 | 4.7 | 5.0 |

92.3

| | | | | | | | |
|------|------|-----|-----|-----|-----|------|--|
| -3.3 | -3.2 | 1.1 | | 1.1 | -4 | -2.0 | |
| 12.5 | 12.4 | 8.1 | 1.1 | 8.1 | 9.6 | 11.7 | |
| 5.0 | 3.3 | 1.3 | 8.1 | 9 | 4.4 | 5.7 | |

H.I.

7.65

| | | | | | | | |
|------|------|------|-----|------|-----|------|------|
| -1.8 | | | | | | | |
| 11.0 | | | | | | | |
| 5.0 | | | | | | | |
| -4.2 | -3.8 | -1.2 | 9 | -1.0 | .7 | -2.2 | -2.3 |
| 13.4 | 13.0 | 10.4 | 8.3 | | 8.5 | 11.4 | 11.5 |
| 3.3 | 3.1 | 2.3 | 1.4 | 8.2 | 2.3 | 4.4 | 5.0 |

| | | | | | | | |
|------|------|-----|-----|-----|------|------|------|
| -1.8 | -1.6 | .6 | | .4 | -1.0 | -2.8 | -2.8 |
| 11.0 | 9.8 | 8.6 | .4 | 8.8 | 10.2 | 12.0 | 12.0 |
| 5.0 | 2.6 | 1.6 | 8.8 | 10 | 2.2 | 3.4 | 5.0 |

| | | | | | | | |
|------|------|-----|-----|-----|------|------|-----|
| -2.6 | -1.6 | -7 | | .5 | -1.2 | -1.1 | .2 |
| 11.8 | 9.8 | 8.5 | .2 | 8.7 | 10.4 | 10.3 | 9.0 |
| 5.0 | 4.0 | 1.5 | 9.0 | 4 | 1.5 | 2.4 | 5.0 |

| | | | | | | | |
|------|------|-----|-----|-----|------|------|------|
| -1.3 | -9 | 2 | | 8 | -1.2 | -2.3 | -8 |
| 10.5 | 10.1 | 9.0 | .6 | 8.4 | 10.4 | 11.5 | 10.0 |
| 5.0 | 3.5 | 3.0 | 8.6 | 3 | 1.8 | 2.7 | 5.0 |

H.I.

3.71

7.85

7.65

| | | | | | | |
|-----|-----|-----|-----|-----|--|-----|
| -1 | -1 | .2 | | .5 | | -4 |
| 5.2 | 5.2 | 4.9 | .3 | 4.6 | | 5.5 |
| 5.0 | 2.5 | 5.0 | 1.8 | 6 | | 5.0 |

| | | | | | | |
|------|-----|-----|-----|-----|-----|-----|
| -1.0 | -5 | -2 | | 0.0 | -5 | -6 |
| 6.1 | 5.6 | 5.3 | 0.0 | 5.1 | 5.6 | 5.7 |
| 5.0 | 2.5 | 1.8 | 5.1 | 1.0 | 1.3 | 5.0 |

| | | | | | | |
|-------|------|-----|-----|-----|-----|-----|
| -0.20 | -1.6 | .1 | | -2 | 0.0 | -2 |
| 7.85 | 5.7 | 5.0 | 0.0 | 5.3 | 5.1 | 5.3 |
| 7.65 | 5.0 | 1.5 | 5.1 | 1.0 | 1.6 | 5.0 |

5.09

Sta. + H.I. - Elev.

Checked off Cortes' B.M.
- 0.10'

U.S.O. + G.S B.M. #61
See Book 380-13

70+00

69+30

69+00

68+90

68+70

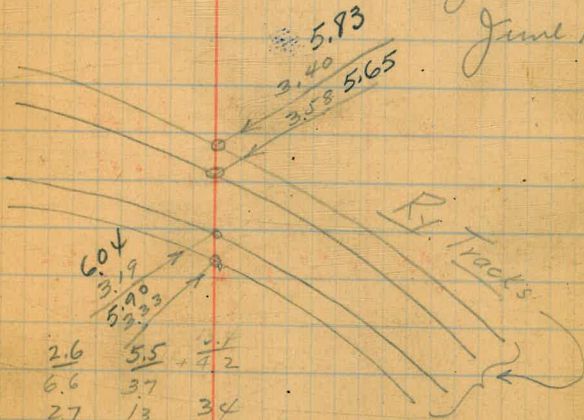
Left

4

Right (4)

See other notes of Chiltons'
for Continuation of this job

Og Shuyun
June 13-14



| | | | | |
|----|----|----|----|----|
| 1 | -1 | 26 | 55 | 72 |
| 98 | 93 | 66 | 37 | |
| 50 | 43 | 27 | 13 | 34 |

H.I. Toe of Fill

| | | | | | | | | | | |
|---------------|----|----|----|----|----|-----|----|----|----|----|
| 76 | 45 | 12 | 12 | 11 | 52 | -40 | 50 | 2 | 10 | 62 |
| 27 | 80 | 75 | 81 | 40 | 47 | 9.0 | 87 | 30 | | |
| 58 | 39 | 27 | 18 | 7 | 36 | 6 | 18 | 17 | 39 | |

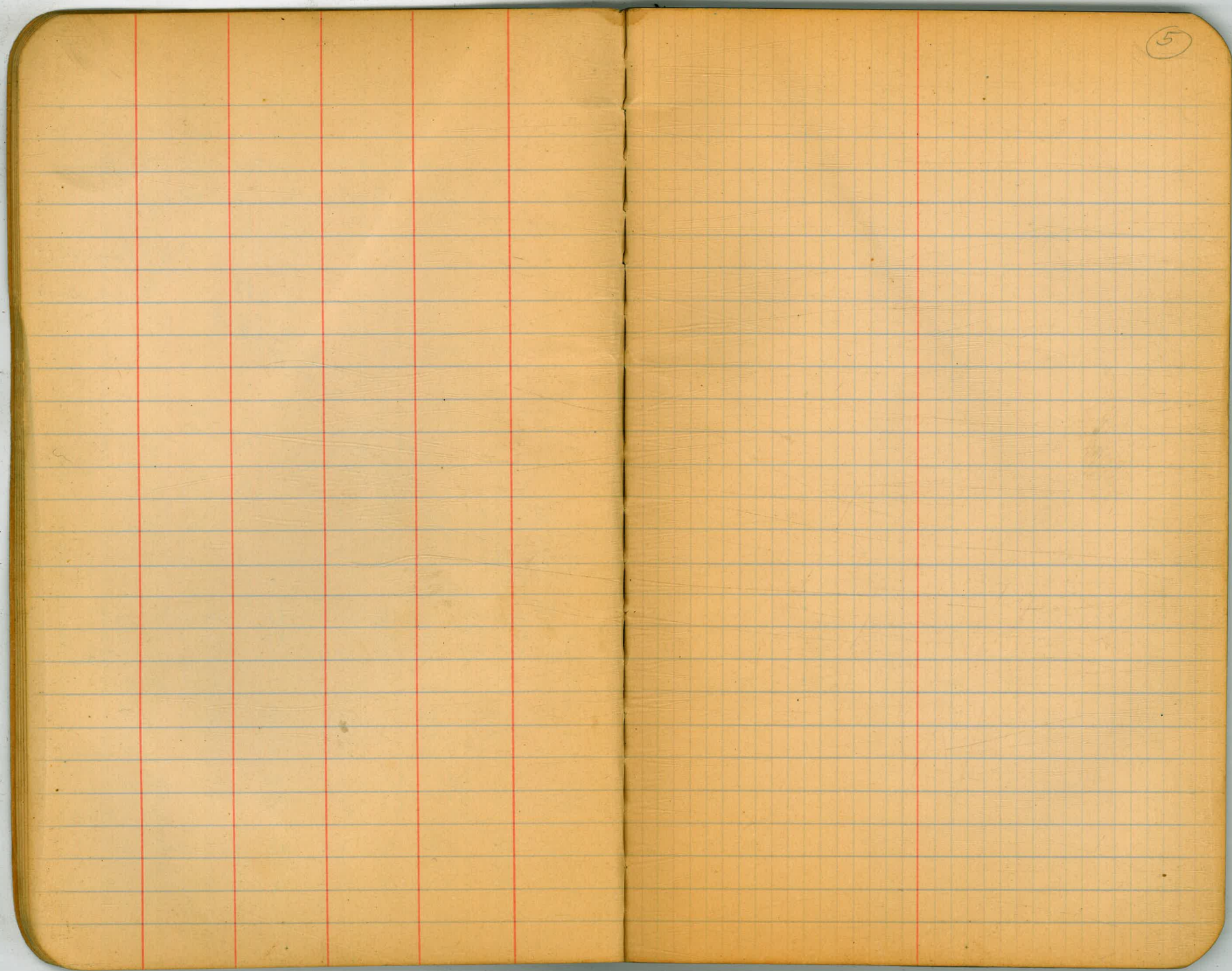
Toe Ry. Fill

| | | | | | |
|----|----|----|----|----|-----|
| 21 | 68 | 46 | 58 | 52 | 64 |
| 21 | 24 | 46 | 34 | 40 | 7.8 |
| 50 | 11 | 30 | 9 | 30 | 50 |

923

| | | | | | |
|----|----|-----|----|-----|-----|
| 21 | 68 | 45 | 60 | 6.9 | 6.7 |
| 21 | 24 | 47 | 37 | 2.3 | 2.5 |
| 50 | 11 | 3.1 | 5 | 11 | 50 |

| | | | | | | |
|------|----|----|-----|-----|-----|-----|
| -16 | .8 | 47 | 32 | 4.5 | 5.4 | 6.6 |
| 10.8 | 84 | 15 | 6.0 | 47 | 38 | 2.6 |
| 50 | 33 | 13 | 4.4 | 13 | 50 | 50 |



5

Altitude 10000 ft. - 10000 ft.

Left

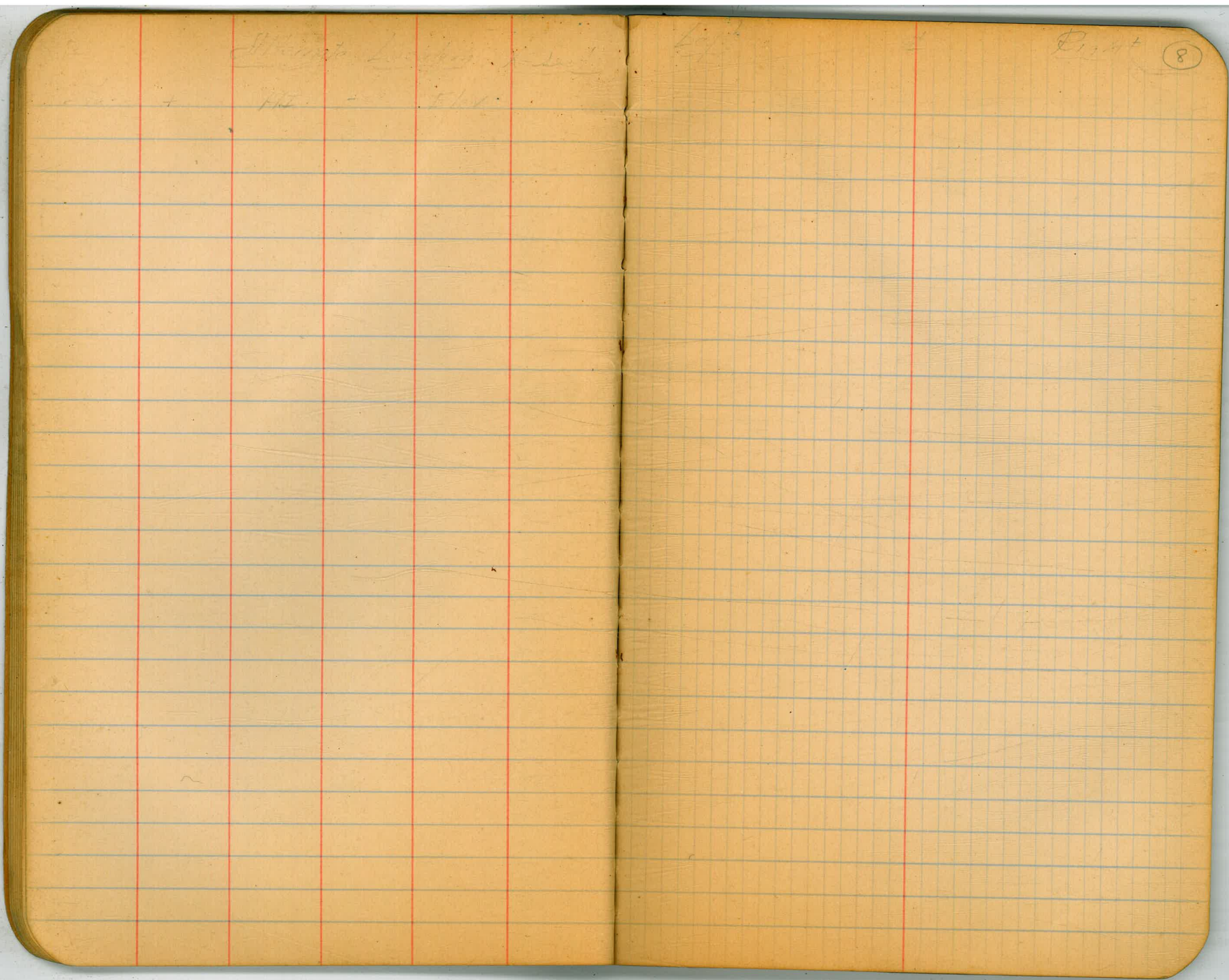
Right

⑥

Journal of ...

Page ②

...



Faint handwriting at the top of the left page.

Faint handwriting at the top of the right page, including the word "Print" and a circled number "8".

Alternate Location X-sections

Sta. + HI. - Elev.

Left

2

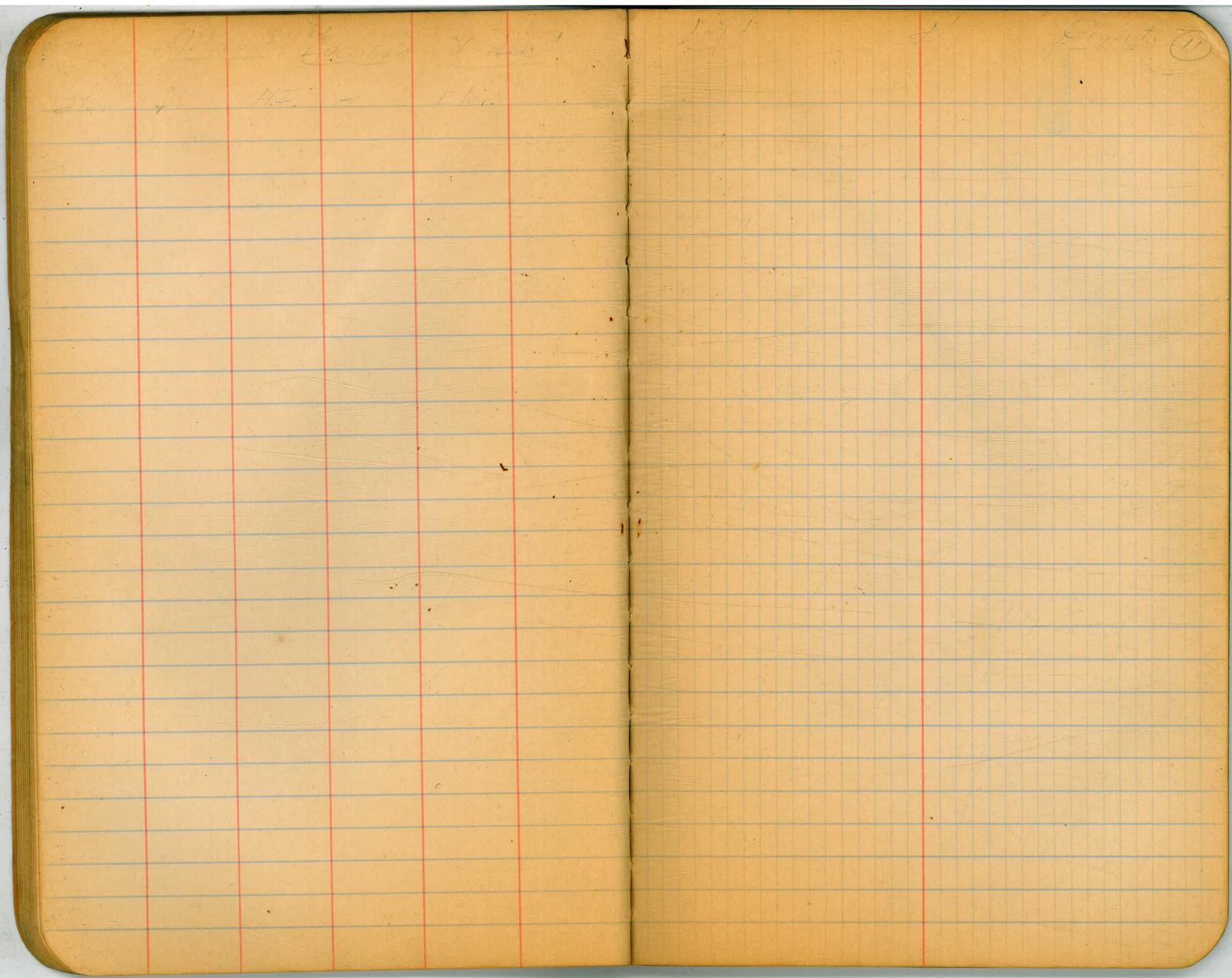
Right (9)

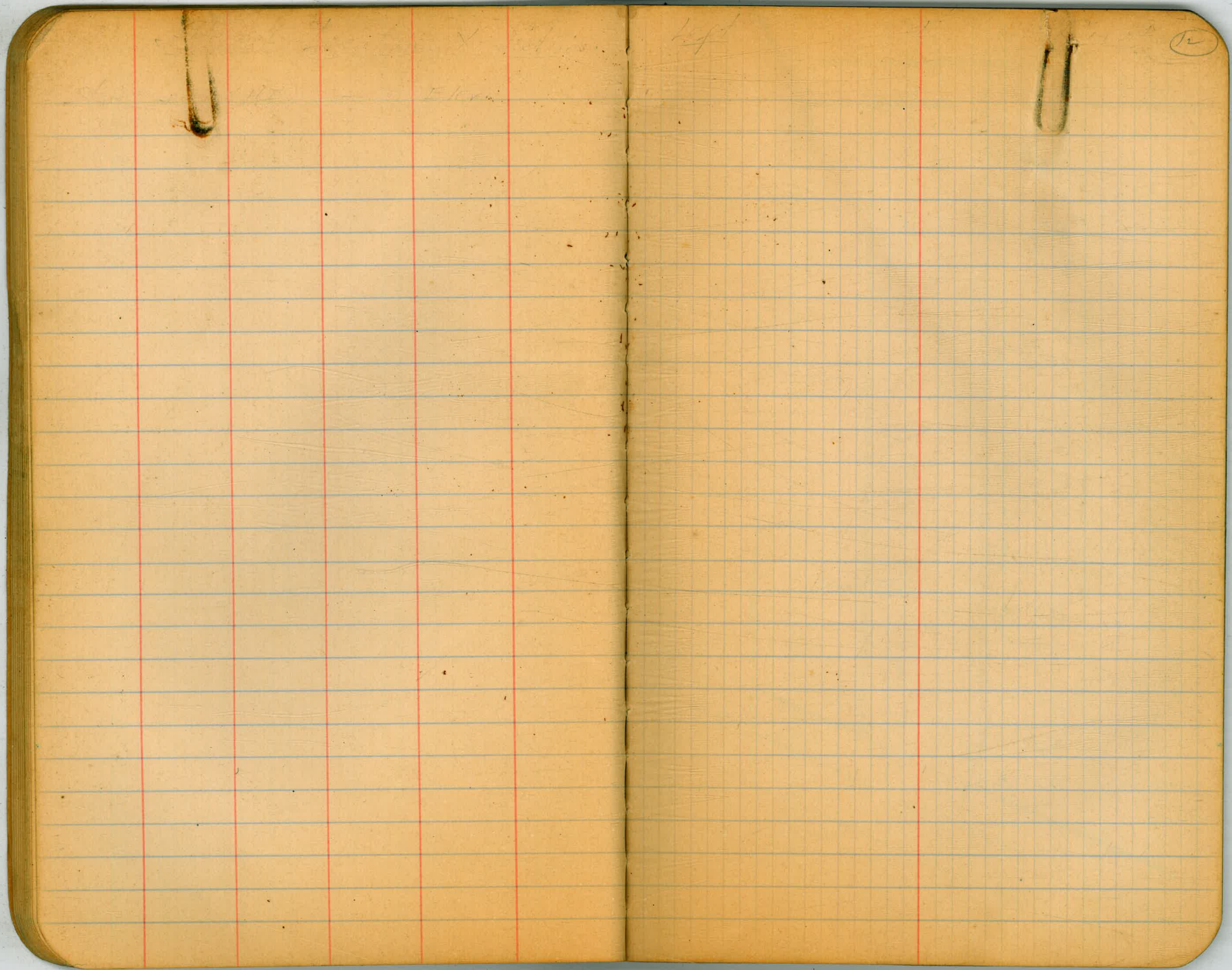
Algebra

184

Right

1. 115 - 5 km





Alternate Line

Sta.

Bearing

18+56.54 P.O.T.

9+22.72 P.O.T.

N. $53^{\circ}57'30''$ W.

0+50.62

0+00

15

(238)

Set. 2xv

70'

(237)

Set. 2x2

N.

$\angle = N. 03^{\circ}07'30'' W.$

35'

BARNETT.

0+00

St. 1x2 = 0+50.62

Ave

Fd. these Monuments
along the Northernly R/W Line
and Flagged same - Did not
Reference All should be O.K.

(316)

(317)

(318)

(319)

Noted Jan-10-1930
Og J

Alternate Line

Sta. Lt. L.Rt. Bearing

PI
32+93.63 35°51'-55"

N. 89°54'-21" W.

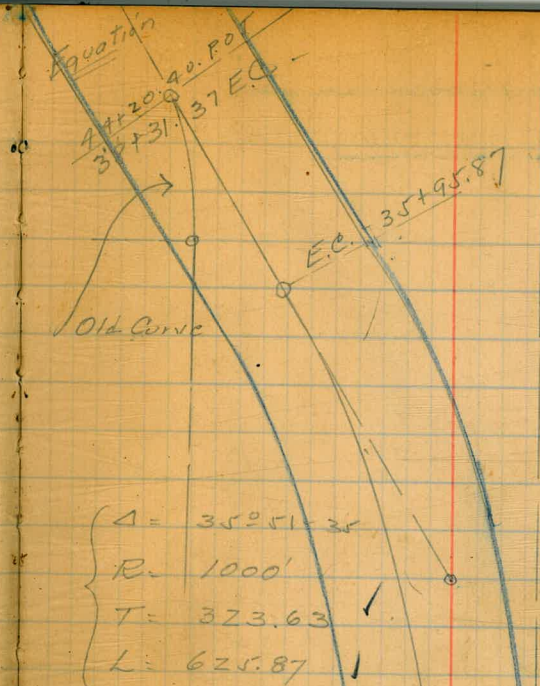
PI
28+89.85

1202'

N. 55°34'-45" W.

PI
27+89.45 1207'

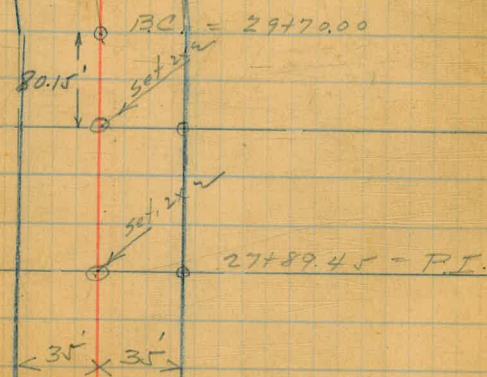
N. 53°57'-30" W.



$\Delta = 35251.35$
 $R = 1000'$
 $T = 323.63$
 $L = 625.87$

-Note-

From B.C. forward
 all controls are
 referenced 100'
 Northerly and
 100' Southerly
 from E of R.N.
 Jan-10-1930



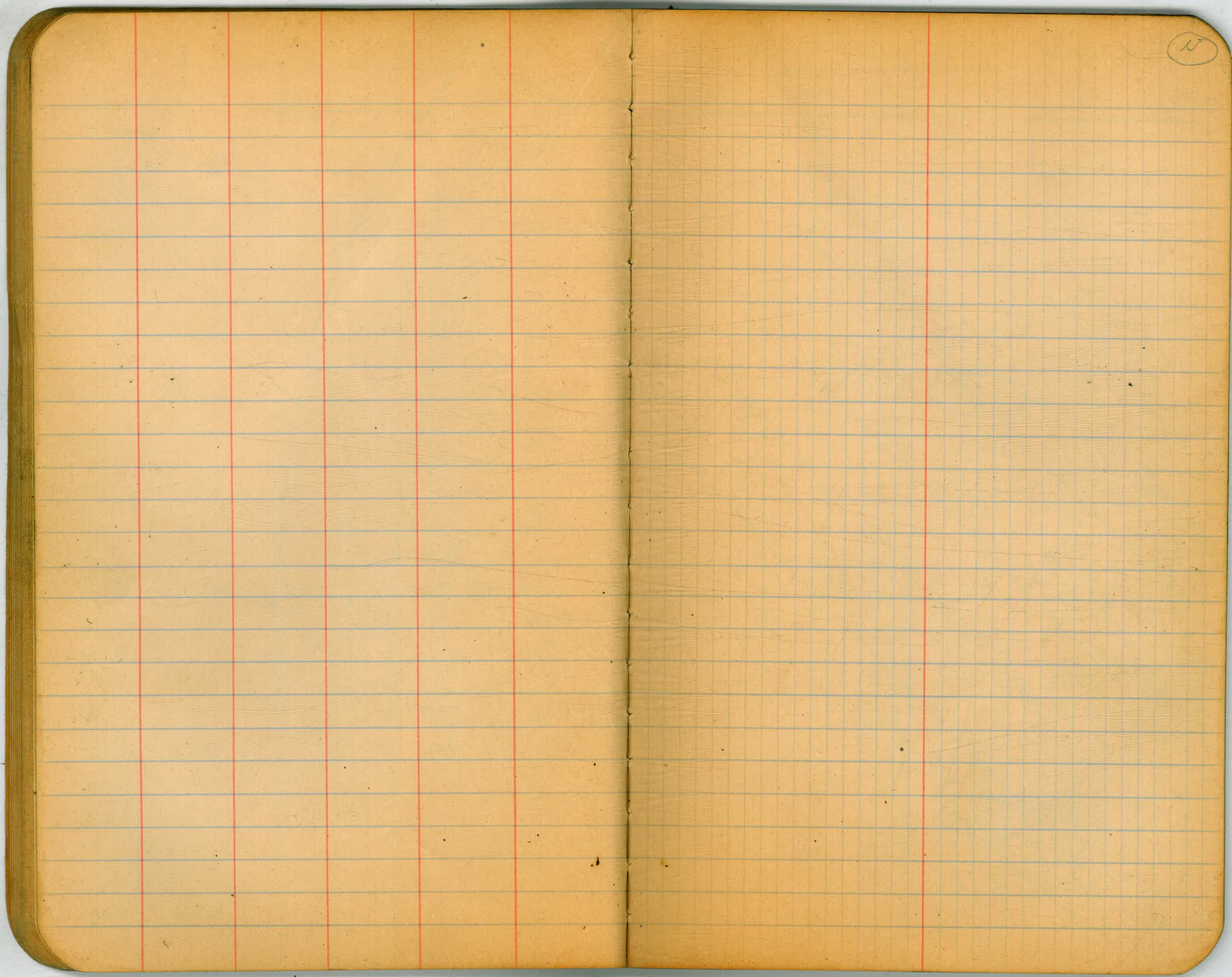
(238)

(316)

July-3-5
 Thompson
 Andersen
 de la Vaux
 Reed

(14)

(315)



Alternate Line - X-sec

sta + H.I - Elev

6.87

5.22 6.87

5.03 1.65

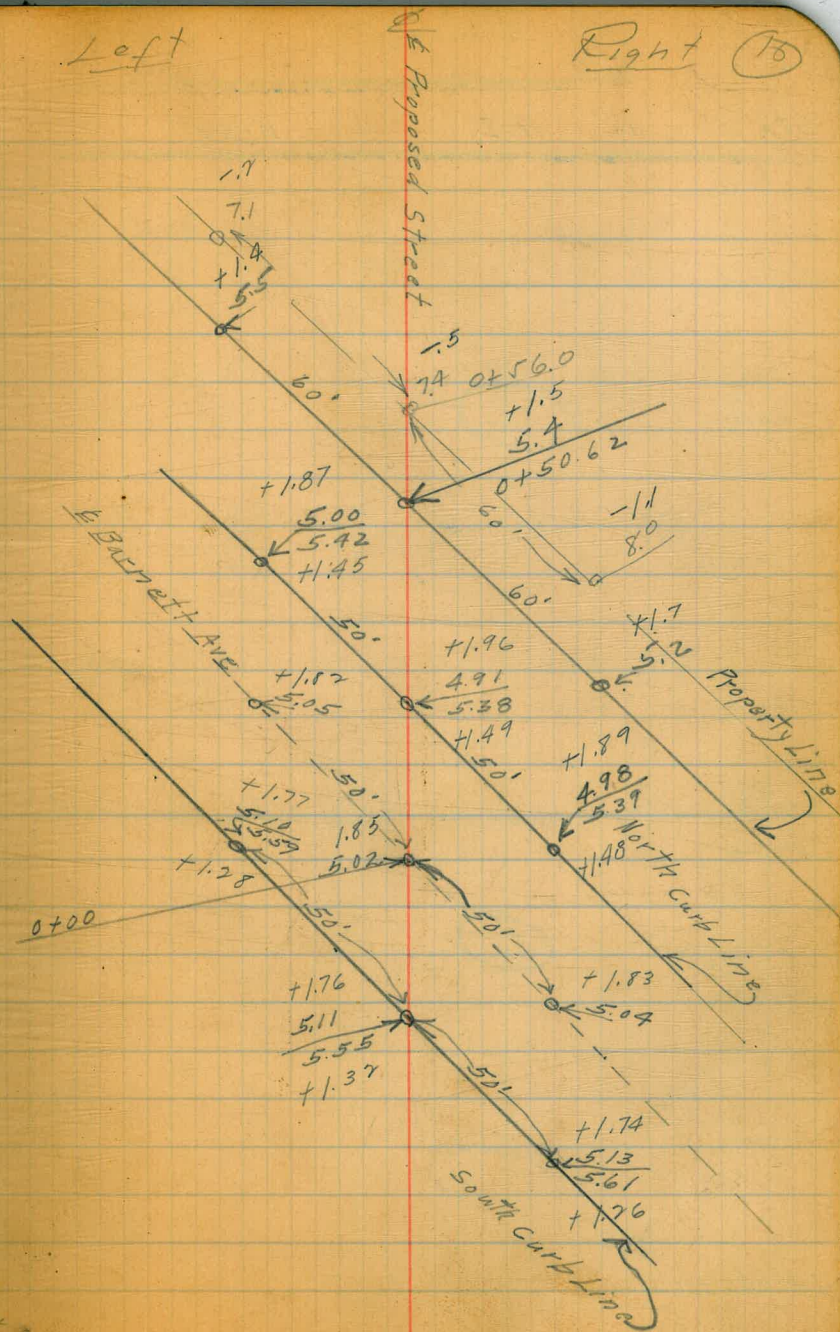
4.68 6.68

Temp BM

2.00 West Pot
Midway - Barnett

Left

Right (16)



Alternate Line X-sec.

Left

±

Right (17)

Sta + H.I - Elev

6+00

2

$\frac{-2.0}{66}$
50

$\frac{-2.2}{68}$

$\frac{-2.4}{70}$
50

5+10

(4.61)

$\frac{-2.5}{71}$
50

$\frac{-4.5}{61}$

$\frac{-1.1}{5.7}$
6

$\frac{+0.3}{4.3}$
25

$\frac{-0.1}{4.7}$
50

5+00

$\frac{-2.5}{71}$
50

$\frac{-2.2}{68}$
30

$\frac{-0.7}{53}$

$\frac{+0.2}{4.4}$
25

$\frac{+0.1}{4.5}$
50

4+50

305

4.61

$\frac{-1.3}{59}$
60

$\frac{+0.2}{4.4}$
50

0.0
4.6

$\frac{+0.6}{7.0}$
25

$\frac{+0.3}{4.3}$
50

0

5.31

1.56

$\frac{-0.2}{7.1}$
50

11.2
67

$\frac{+0.3}{6.6}$
35

$\frac{-0.1}{7.0}$
50

4+00

(6.87)

$\frac{-0.3}{7.2}$
50

$\frac{-0.2}{7.1}$

$\frac{+0.1}{6.8}$
50

3+00

2+00

$\frac{-0.8}{7.7}$
50

$\frac{-0.3}{7.2}$

$\frac{-0.4}{7.3}$
50

1+00

$\frac{-0.2}{7.1}$
35

$\frac{-1.1}{8.0}$

$\frac{-0.5}{7.4}$
50

Alternate Line X-sections

Sta. + H.F. - Elev.

13+00

5.01

12+00

11+00

4.24 5.01

10+00

384 0.77

9+00

4.61

8+00

7+00

6+15

Left

±

Right 18

$\frac{-0.3}{5.3}$
50

$\frac{-0.2}{5.5}$

$\frac{0.0}{5.0}$
50

$\frac{-0.2}{5.5}$
50

$\frac{-0.1}{5.1}$

$\frac{+0.3}{4.7}$
50

$\frac{-0.0}{5.0}$
50

$\frac{+0.2}{4.8}$

$\frac{+0.7}{4.5}$
50

$\frac{0.1}{4.5}$
50

$\frac{0.1}{4.5}$

$\frac{0.6}{4.0}$
50

$\frac{+0.1}{4.5}$
50

$\frac{+0.3}{4.3}$

$\frac{+0.7}{3.9}$
50

$\frac{+0.7}{4.2}$
50

$\frac{+0.7}{4.2}$

$\frac{+0.6}{4.0}$
50

$\frac{-0.6}{5.0}$

$\frac{-0.7}{5.3}$

$\frac{-0.8}{5.4}$
50

$\frac{-1.5}{6.1}$
50

$\frac{-1.4}{6.0}$

$\frac{-1.4}{6.0}$
25

$\frac{-2.1}{6.7}$
50

Alternate Line X-Sections

Left

±

Right (19)

Sta. t H.I. - Elev.

19400

$\frac{0.3}{5.0}$

$\frac{0.3}{5.3}$

$\frac{0.2}{5.0}$

18400

$\frac{0.4}{5.0}$

$\frac{0.5}{5.1}$

$\frac{0.9}{5.0}$

17400

$\frac{0.8}{5.0}$

$\frac{0.6}{5.0}$

$\frac{0.5}{5.0}$

16435

$\frac{-0.3}{5.0}$

$\frac{+0.6}{5.0}$

$\frac{1.0}{5.0}$

656

(5.57)

0

600 - 0.99 Watch-out

$\frac{-1.0}{6.0}$

$\frac{-1.0}{6.0}$

$\frac{-1.0}{5.0}$

15780

$\frac{0.0}{5.0}$

$\frac{0.6}{4.4}$

$\frac{0.2}{5.0}$

15425

(5.01)

$\frac{0.6}{4.4}$

$\frac{0.7}{4.3}$

$\frac{0.7}{5.0}$

15400

$\frac{0.0}{5.0}$

$\frac{0.0}{5.0}$

$\frac{0.2}{5.0}$

14400

Alternate Line y-sec

Left

±

Right (20)

Sta. + HI. - Elev.

| Sta. | + | HI. | - | Elev. |
|-------|------|------|------|-------|
| 27+00 | | | | |
| 26+00 | | | | |
| 25+00 | | | | |
| 24+00 | | | | |
| 23+00 | 4.34 | 5.69 | | |
| 22+00 | | | | |
| 21+00 | | | | |
| 20+00 | | 5.57 | 4.22 | 1.35 |

| | | |
|---------------------------|--------------------|---------------------------|
| $\frac{0.3}{5.7}$ 5.0 | $\frac{0.4}{5.3}$ | $\frac{0.5}{5.2}$ 5.0 |
| $\frac{-0.1}{5.8}$ 5.0 | $\frac{-0.3}{6.0}$ | $\frac{+0.3}{5.9}$ 5.0 |
| $\frac{0.1}{5.6}$ 5.0 | $\frac{0.3}{5.9}$ | $\frac{0.3}{5.7}$ 5.0 |
| $\frac{0.0}{5.7}$ 5.0 | $\frac{0.4}{5.3}$ | $\frac{1.0}{4.7}$ 5.0 |
| $\frac{0.3}{5.7}$ 5.0 | $\frac{0.6}{5.1}$ | $\frac{0.8}{4.7}$ 5.0 |
| $\frac{0.9}{4.8}$ 5.0 | $\frac{0.8}{4.9}$ | $\frac{0.7}{5.0}$ 5.0 |
| $\frac{0.5}{5.2}$ 5.0 | $\frac{0.5}{5.2}$ | $\frac{0.8}{4.9}$ 5.0 |
| $\frac{-0.1}{5.7}$ 5.0 | $\frac{+0.2}{5.9}$ | $\frac{-0.2}{5.8}$ 5.0 |

Alternate Line X-sec

Sta. + H.I. - Elev.

32+00

31+50

31+00

30+50

30+00

29+70 BL

28+89⁸⁵ 3.12

0

27+89²⁵

(5.51)

(5.51)

(5.69)

3.30 2.39

Left

±

Right

(21)

$\frac{0.5}{5.0}$
5.0

$\frac{0.5}{5.0}$
5.0

$\frac{0.3}{5.2}$
5.0

$\frac{-0.1}{5.6}$
5.0

$\frac{0.3}{5.2}$
5.0

$\frac{0.3}{5.2}$
5.0

$\frac{-0.2}{5.7}$
5.0

$\frac{0.8}{4.7}$
5.0

$\frac{0.5}{5.0}$

$\frac{0.9}{4.6}$

$\frac{0.2}{5.3}$

$\frac{-0.1}{5.6}$

$\frac{0.1}{5.4}$

$\frac{0.1}{5.4}$

$\frac{+0.3}{5.2}$

$\frac{0.7}{5.0}$

$\frac{0.3}{5.2}$
5.0

$\frac{0.7}{4.8}$
5.0

$\frac{0.2}{5.3}$
5.0

$\frac{+0.2}{5.3}$
5.0

$\frac{0.2}{5.3}$
5.0

$\frac{0.3}{5.2}$
5.0

$\frac{+0.1}{5.4}$
5.0

$\frac{0.9}{4.8}$
5.0

Alternate Line-X-sec

(22)

Sta + H.I - Elev

Left

±

Right

35+95 ^{0.7} ~~EL~~

$\frac{0.0}{5.2}$
5.0

$\frac{0.0}{5.2}$

$\frac{0.0}{5.2}$
5.0

35+50

$\frac{+0.1}{5.1}$
5.0

$\frac{-0.1}{5.3}$

$\frac{+0.1}{5.1}$
5.0

35+00

4.17

(5.24)

$\frac{-0.1}{5.3}$
5.0

$\frac{+0.1}{5.1}$

$\frac{+0.3}{4.9}$
5.0

0

4.44

1.07

34+50

$\frac{-0.1}{5.6}$
5.0

$\frac{+0.3}{5.2}$

$\frac{0.0}{5.6}$
5.0

34+00

$\frac{0.0}{5.5}$
5.0

$\frac{0.0}{5.5}$

$\frac{+0.1}{5.7}$
5.0

33+50

(5.51)

$\frac{+0.1}{5.4}$
5.0

$\frac{+0.0}{5.5}$

$\frac{-0.1}{5.6}$
5.0

33+00

$\frac{0.1}{5.4}$
5.0

$\frac{0.2}{5.3}$

$\frac{0.3}{5.2}$
5.0

32+50

$\frac{0.3}{5.2}$
5.0

$\frac{0.4}{5.1}$

$\frac{0.5}{5.0}$
5.0

Alternate Line X-sec

23

| Sta | + | H.I | - | Elev | Left | ± | Right |
|--------------------------------|------|------|------|-------|--------------------|-------------|--------------------|
| 44+20.40 P.O.T. 38+31.37 EC | | 5.74 | 6.0 | -0.26 | 0.9 4.8 5.0 | 0.4 5.3 | 4.6 5.0 |
| | | | | | 0.0 5.7 5.0 | 0.5 5.2 | 0.5 5.2 5.0 |
| 43+00 | | | | | -0.1 5.8 5.0 | +0.7 5.3 | +0.7 5.0 5.0 |
| 42+00 | | | | | -0.2 5.9 5.0 | 0.0 5.7 | +0.3 5.4 5.0 |
| 41+0.0 | 4.67 | 5.74 | | | 0.0 5.2 5.0 | 0.2 5.0 | 0.9 4.3 5.0 |
| 0 | | 5.24 | 4.17 | 1.07 | 0.2 5.0 5.0 | 0.3 4.9 | 0.8 4.7 5.0 |
| 40+00 | | | | | 0.1 5.1 5.0 | 0.2 5.0 | 0.3 4.9 5.0 |
| 39+00 | | | | | 0.2 5.0 5.0 | 0.2 5.0 | 0.2 5.0 5.0 |
| 38+00 | | 5.24 | | | 0.2 5.0 5.0 | 0.0 5.2 | 0.2 5.0 5.0 |
| 37+00 | | | | | 0.2 5.0 5.0 | 0.0 5.2 | 0.2 5.0 5.0 |
| 36+50 | | | | | | | |

check on
sta 35+00
old line

Light Standards.

Left.

Right.

About 20' from Ref.

1+05

1+82

2+59

3+36

4+13

4+90

5+67

6+44

7+21

7+98

8+75

9+52

10+29

11+06

11+83

12+60

13+37

14+14

14+91

15+68

16+45

17+22

17+99

18+75

19+53

- Light Standards -

24

Left

Right

Falls on Return.

21+07

20+30

22+61

21+84

24+15

23+38

25+69

24+92

27+23

26+46

28+80 = Middle Return

28+00 = Middle Return

30+40

29+60

Middle Return

32+00

31+20

33+50

32+75

Middle of Return

35+00

34+25

36+54

35+77

38+08

37+31

38+85

Light Standards

Left.

Right

39+62

40+39

41+16

41+93

42+70

44+19.97
38=31.39

Equation

Watch
out.

43+47

38+34

39+11

39+88

40+65

41+42

42+19

42+96

43+73

44+50

45+27

46+04

46+81

47+58

48+33

49+08

49+83

50+58

51+33

52+08

Light Standards

25

Left

Right

53+58

52+83

55+08

54+33

56+58

55+83

58+08

57+33

59+58

58+83

61+08

60+33

62+58

61+83

64+08

63+33

65+58

64+83

66+33

26

27

28

29

30

31

32

83

(34)

RT Const
← 40 → L ← 45 →

$\frac{6.4}{42.8}$

5.4

4.8

5.7

5.4

5.3

5.6

1.0

5.4

1.0

9

9

8

8

7

| | + | H.I. | - | EI | IF |
|--------|------|-------|---|-------|------|
| BM. #3 | 4.59 | +1.51 | | -3.08 | 61 |
| 29 | | | | | 2.3 |
| +50 | | | | | 2.35 |
| 30 | | | | | 2.4 |
| +50 | | | | | 2.45 |
| 31 | | | | | 2.5 |
| +50 | | | | | 2.45 |
| 32 | | | | | 2.4 |
| +50 | | | | | 2.35 |
| 33 | | | | | 2.3 |
| +50 | | | | | 2.25 |
| | | | | | 2.2 |
| 37 | | | | | 2.2 |

420.73 = L.C.

| | | |
|----------|------|---------|
| 39+95.77 | 130. | 0-00 |
| 40+50 | | 2-17 |
| 41+00 | | 4-23.4 |
| +50 | | 6-29.8 |
| 42 | | 8-36.2 |
| +50 | | 10-42.6 |
| 43 | | 12-49 |
| +50 | | 14-55.4 |
| 44 | | 17-02 |
| 44+23.90 | E.C. | 18-02 |

$$30+00 - 0-51.7'$$

$$+50 - 2-17.6'$$

$$31+00 - 3-43.6'$$

$$+50 - 5-09.5'$$

$$32+00 - 6-35.5'$$

$$+50 - 8-01.4'$$

$$33+00 - 9-27.4'$$

$$+50 - 10-53.3'$$

$$34+00 - 11-19.3'$$

$$+50 - 13-45.2'$$

$$35+00 - 15-11.2'$$

$$+50 - 16-37.1'$$

$$35+25.87 - 17-56'$$

$$\left\{ \begin{array}{l} 31+52.39 = 5-13 = \text{Ret} \\ 32+05.55 = 6-45 = \text{Ret} \end{array} \right.$$

$$\left\{ \begin{array}{l} 34+98.15 = 15-08 = \text{Ret} \\ 35+59.56 = 16-53.5 = \text{Ret} \end{array} \right.$$

$$\begin{array}{r} 70+12.93 \\ 65+19.28 \\ \hline 493.65 \end{array}$$

$$\begin{array}{r} 493.46 \\ 828.75 \\ \hline 1322.21 \\ 66.110 \\ 493.65 \\ \hline 1467.45 \end{array}$$

$$\left. \begin{array}{l} 104+32.67 \\ 111+50 \end{array} \right\} \text{NO. BR. } 109+14$$

$$(111+57)+35 = \neq \text{Intersect}$$

$$\left. \begin{array}{l} 73+93.50 \\ 81+58.83 \end{array} \right\} \text{80. BR. } 77+76$$