

1469

LEVEL BOOK

373 A

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

" Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

Home Ave.	Euclid to	Lemon Grove Blvd.	1-7
Rosecrans	Atlantic to	Lyton	8-30
Alley Blk. 143	Univ. Hts.		31-36
r	r	E Plumosa Park	37-44
Location of Plaza Trail Marker			45
ok. of Serra Point- Conde Sta.	Pl. & Pine		46
Hospital Corps Athletic Field	Balboa		47-49 64-75
4 th Ave.	Univ. to	Wash.	76-78
Drain ditch 15' Sly. &	Kurtz to	Taylor	79

5.11

1.71

Mulher
Bliss
Northern 7-12-33
Kunagy

CT. in Paving
Book 1435-17=0+00
=0+00 this book 0.80 229.93

	+	T	-	Elev	
+25 on Paving				228.37	
+50 " "				227.93	
+68 " South edge				227.67	
+80				227.43	
+100				226.83	
+20 = E.V.C.				226.23	
+50				224.43	
+200				222.33	
+50				219.93	
+290.27 = B.C. Pt.				217.93	
T.P. 0.37	217.33	12.97		216.96	
+350				214.93	
+400				212.33	
+50				209.83	
+500				207.13	
+50				205.03	
T.P. 0.32	204.68	12.97		204.36	
+600				202.58	

204.68

1

6+40 P.V.C.		
3.7		200.98
+60		4.4 200.28
+80		5.0 199.68
7+00		5.7 198.98
+20		6.4 198.28
+40		7.0 197.68
+60		7.5 197.18
+80		8.0 196.68
8+00		8.6 196.08
+20		9.1 195.58
+40 = E.V.C.		9.5 195.18
9+00		10.6 194.08
+50		11.5 193.18
10+00		12.3 192.38
+09.64 = E.C.		12.4 192.28
T.P. 0.35	192.26	12.77 191.91
chk. 39.6' Rd & Book 1435-30		2.90 189.36
290	192.28	189.38 = Correct Elev.
10+50		0.5 191.78
11+00		1.3 190.98

192.28

Home Ave.

11+50	3.2	190.08
12+00	3.0	189.28
+50	3.8	188.48
13+00	4.6	187.68
+50	5.4	186.88
14+00	6.2	186.08
+50	7.0	185.28
15+00	8.1	184.18
+50	8.8	183.48
16+00	9.9	182.38
+50	10.6	181.68
17+00	11.2	181.08
T.P. 0.10	11.11	181.17
+50	1.0	180.27
18+00	1.9	179.37
+50	3.8	178.47
19+00	3.4	177.87
+50	4.1	177.17
20+00	4.9	176.37
+50	5.3	175.97

181.27

Home Ave.

2

31+00	5.9	175.37	
+50	6.6	174.67	
22+00	7.5	173.77	
+50	8.0	173.27	
23+00	8.6	172.67	
+50	9.3	171.97	
24+00	10.0	171.27	
T.P. 0.80	172.10	9.97	171.30
+50	1.4	170.70	
25+00	2.3	169.80	
+50	3.2	168.90	
26+00	3.9	168.20	
+50	4.8	167.30	
27+00	5.6	166.50	
+50	6.5	165.60	
28+00	7.5	164.60	
+50	7.9	164.20	
29+00	8.7	163.40	
+50	9.5	162.60	
30+00	10.2	161.90	

172.10

Home Ave.

160.84

Home Ave

3

30+50	10.9	161.2	T.P.	4.53	154.95	10.42	150.42
31+00	11.7	160.4	38+40 = PVC			4.5	150.45
T.P.	0.24	160.84	39+00			4.1	150.85
31+51.62 = B.C. Rt.	1.2	159.64	+50			4.0	150.95
32+00	1.8	159.04	40+00 = PVC			3.4	151.55
+50	2.6	158.24	+20			3.1	151.85
33+00	3.5	157.34	For Elev. Pacing on Fairmount Ave. see Book 1435-71				
+45.35 = E.G.	4.2	156.64	check B.M. 8D Book 1435-69			6.86	148.09
34+00	5.1	155.74	6.86	155.08		148.22	= B.M.
+50	5.7	155.14	40+80			1.8	153.28
35+00	5.6	155.24	41+00			2.0	153.08
+50	7.5	153.34	+20			2.0	153.08
36+00	8.3	152.54	+60			2.2	152.88
+16.84 = PVC	8.6	152.24	42+00			5.1	149.98
+56.84	9.2	151.64	+40			6.9	148.18
+96.84	9.9	150.94	+80 = PVC			8.7	146.38
37+36.84	10.5	150.34	43+00			9.6	145.48
37+54.81	} equation.	150.24	+20			10.3	144.78
37+37.97			+40			11.1	143.78
+60	10.6	150.24	+60			11.9	143.18
38+00	10.6	150.24					

	155.08	Home Ave
43+80		12.4 142.68
44+00		13.0 152.08
T.P. 1.25	143.33	13.00 142.08
+20		1.9 141.4
+40		2.4 140.9
+60		2.7 140.6
+80		3.2 140.1
45+00		3.7 139.6
+20 = E.V.C		4.0 139.3
+60		4.5 138.8
46+00		4.9 138.4
+50		5.8 137.5
47+00		6.3 137.0
+50		7.4 135.9
48+00		7.9 135.4
+50		8.5 134.8
49+00		9.4 133.9
+50		10.0 133.3
50+00		10.7 132.6
T.P.	0.52 133.20	10.65 132.68

	133.20	Home Ave
✓ 50+36.64		
51+36.64 = B.C. Lt.		0.8 132.4
+50		0.8 132.4
51+00		0.9 132.3
+50		1.3 131.9
52+00		2.0 131.2
+50		2.8 130.4
✓ +69.93 = E.C.		3.3 129.9
53+00		4.1 129.1
+50		4.5 128.7
54+00		5.3 127.9
+50		6.2 127.0
✓ 55+03.65 = B.C. Rt.		7.4 125.8
+60		8.1 125.1
56+00		8.4 124.8
+40		8.5 124.7
57+00		9.3 123.9
+50		10.0 123.2
58+00		10.9 122.3
T.P.	1.27 123.25	11.22 121.98
+50		1.4 121.9

123.25

Home Ave

59+00	1.9	121.4
15336 = E.R.	2.5	120.8
60+00	3.1	120.2
+50	3.8	119.5
61+00	4.1	119.2
+50	5.0	118.3
62+00	5.6	117.7
+50	6.3	117.0
63+00	6.8	116.5
+50	7.5	115.8
64+00	7.8	115.5
+50	8.8	114.5
65+00	9.4	113.9
T.P. 1.69	115.40	9.54 113.71
+50	2.0	113.4
66+00	2.8	112.6
+50	3.0	112.4
67+00	3.0	112.4
+50	3.4	112.0
68+00	3.8	111.6

115.40

Home Ave

+50	4.6	110.8
69+00	5.0	110.4
+50	5.7	109.7
1 + 8596 = B.C. Lt.	6.2	109.2
70+00	6.4	109.0
+50	6.8	108.6
71+00	7.3	108.1
+50	7.6	107.8
72+00	8.0	107.4
+50	8.1	107.3
T.P. 0.13	107.60	7.93 107.47
73+00	0.6	107.0
+50	1.6	106.0
74+00	2.1	105.5
+50	3.6	104.0
75+00	4.5	103.1
+50	5.5	102.1
76+00	6.2	101.4
+50	7.0	100.6
77+00	7.7	99.9

5

107.60

Home Ave

77+50	8.6	99.0
78+00	9.5	98.1
+50	10.4	97.2
79+00	11.5	96.1
T.P. 0.13	96.01	11.72 95.88
+50	1.1	94.9
+60.72 = E.S.	1.4	94.6
80+00	2.0	94.0
+50	3.1	92.9
81+00	3.6	92.4
+50	4.3	91.7
82+00	5.3	90.7
+50	5.8	90.2
83+00	6.8	89.2
+50	7.8	88.2
84+00	8.9	87.1
+50	10.0	86.0
85+00	10.7	85.3
+50	11.8	84.2
86+00	12.5	83.5

96.01

Home Ave.

6

T.P. 1.29	84.79	12.51	83.50
86+50		2.0	82.8
87+00		2.3	82.5
+50		2.9	81.9
88+00		3.5	81.3
+50		4.0	80.8
89+00		5.0	79.8
+50		5.6	79.2
90+00		6.0	78.8
+50		6.6	78.2
91+00		7.3	77.5
+50		7.9	76.9
92+00		8.5	76.3
T.P. 3.57	80.13	8.24	76.55
+50		4.2	75.9
93+00		4.2	75.9
chk. B.M. CT. & Lemay Grove Stij.		5.03	75.09
5.03	80.15		75.12 = B.M.
93+38.15 = End Bridge on Pav.		4.51	75.61
94+13.15 = South end Bridge "		4.96	75.16

Grade Book 175-49

Rosecrans St.
Cross Section Atlantic St to Lyman St.

index
c.s.k.

8-1-33
Moore
Sisson
Northern 8

Sketch Cont. Page 15

7+44.03

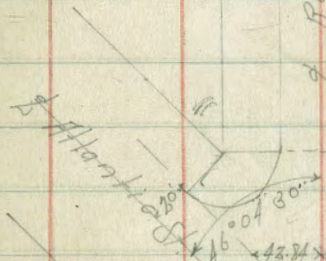
Moore

50' 50'

3+94.03

Safferson

Rosecrans St



1417.58'

160.60+0'

177.77'

Congress St

0+0

191.05'

233.89+19

BC 21

Rosecrans St.
Cross Section Atlantic to Lytton

9

240

LT	Z	PT
3.3	3.2	3.2
3.1	3.2	3.1
5.1	5.5	5.5
5.0	3.0	3.0
5.5	5.3	5.0
5.0	5.0	5.0
5.0	5.0	5.0

1450

LT	Z	PT
3.9	4.0	4.2
4.8	4.7	4.5
5.0	3.0	3.0
4.7	4.5	4.7
4.2	4.2	4.2
4.5	4.5	4.5
4.5	4.5	4.5

1+1758 - EC 02H

LT	Z	PT
3.6	3.5	3.6
5.1	5.2	4.9
5.0	3.0	3.0
4.8	4.8	4.8
4.7	4.7	4.7
4.6	4.6	4.6
4.3	4.3	4.3

0+6903 - Sty Concrete

LT	Z	PT
4.5	4.3	4.3
4.2	4.1	4.1
4.84	3.6	3.6
4.7	4.7	4.7
4.7	4.7	4.7
4.5	4.5	4.5

0+2777 - Sty of Proposing Atlantic St on Diag

LT	Z	PT
5.0	4.6	4.7
3.7	4.1	4.0
98.32	69.42	41.65
3.7	3.7	3.7
4.1	4.1	4.1
37.77	37.77	37.77
4.3	4.3	4.3
4.4	4.4	4.4
4.3	4.3	4.3

TP 3.92 8.65 3.87 4.73

8.65

BM 3.45 8.60 5.15

Mon Taylor
San Diego, Calif.
+ Rosecrans

5x0

Lt	Z	R
3.5	3.6	3.9
3.4	3.4	3.6
4.1	4.3	4.1
50	30	50

4x50

3.5	3.6	3.7	3.5	3.5	3.6	3.9
4.1	4.3	4.2	4.4	4.4	4.1	4.0
50	30	20	20	30	30	50

TP

4.52

7.89

5.28

3.37

2 Max Roser
+ Jefferson

7.89

3794.03 = 2 Jefferson

3.9	3.9	3.9	3.6	3.7	3.4	3.6
4.8	4.8	4.8	5.1	5.0	5.3	5.1
50	30	20	20	30	30	50

3x50

3.9	3.7	3.9	3.7	3.6	3.6	3.6
4.8	5.0	4.8	5.0	5.1	5.1	5.1
50	30	20	20	20	30	50

3x0

3.7	3.7	4.0	3.7	3.8	3.5	3.7
5.0	5.0	4.7	5.0	4.9	5.2	5.0
50	30	20	20	20	30	50

2x50

3.0	2.7	3.4	3.4	3.7	3.7	3.9
5.7	6.6	5.3	5.3	5.0	5.0	4.8
50	30	20	20	20	30	50

8.65

8.65

870

3.1	3.0	3.0	3.3	3.4	3.0	3.4
48/50	48/30	48/20	46	45/20	49/30	41/50

7744.03 = 1/2 Moore

3.2	3.6	3.5	3.5	3.4	3.2	2.6
47/50	43/30	44/20	44	45/20	47/30	51/50

770

3	3.4	3.6	3.5	3.5	3	3.6
46/50	45/30	42/20	44	46/20	46/30	42/50

6750

3.1	3.4	3.6	3.3	3.2	3.3	3.5
48/50	45/30	42/20	46	47/20	46/30	46/50

670

3.3	3.3	3.5	3.2	2.6	2.6	3.4
46/50	46/30	44/20	47	51/20	51/30	45/50

5750

3.6	3.7	3.7	3.4	3.4	3.1	3.3
43/50	42/30	42/20	43	45/20	48/30	46/50

7.89

7.89

10+94.03 $\frac{1}{2}$ Hancock

TP 4.49 7.16 5.22 2.67

10+50

10+0

9+50

9+0

8+50

7.89

	Lt.	S	Pt			
	2.4 $\frac{4.8}{50}$	2.2 $\frac{5.0}{30}$	2.4 $\frac{4.8}{20}$	2.4 4.8	2.4 $\frac{4.8}{20}$	2.6 $\frac{4.6}{50}$
	2.3 $\frac{5.6}{50}$	2.3 $\frac{5.6}{30}$	2.7 $\frac{5.4}{20}$	2.7 5.4	2.6 $\frac{5.2}{20}$	3.3 $\frac{4.6}{50}$
	2.7 $\frac{5.4}{50}$	2.7 $\frac{5.4}{30}$	3.1 $\frac{4.8}{20}$	2.6 5.3	3.0 $\frac{4.8}{20}$	2.6 $\frac{5.2}{30}$
	2.6 $\frac{5.2}{50}$	3.1 $\frac{4.8}{30}$	3.2 $\frac{4.7}{20}$	2.9 5.0	2.0 2.0	3.0 3.0
	2.5 $\frac{5.0}{50}$	2.9 $\frac{5.8}{30}$	3.1 $\frac{4.8}{20}$	3.0 4.9	2.9 $\frac{5.8}{20}$	3.1 $\frac{4.8}{50}$
	3.0 $\frac{6.0}{50}$	3.1 $\frac{6.2}{30}$	3.2 $\frac{6.4}{20}$	3.2 4.7	3.3 $\frac{6.6}{20}$	2.7 $\frac{5.4}{30}$
	3.0 $\frac{6.0}{50}$	3.1 $\frac{6.2}{30}$	3.2 $\frac{6.4}{20}$	3.2 4.7	3.3 $\frac{6.6}{20}$	3.2 $\frac{6.4}{50}$

7.89

1470

1.6	1.9	2.0	1.9	2.1	1.7	1.4
$\frac{5.1}{50}$	$\frac{5.3}{30}$	$\frac{5.2}{20}$	5.3	$\frac{5.1}{20}$	$\frac{5.5}{30}$	$\frac{5.1}{50}$

13750

1.1	2.2	2.2	2.1	2.1	2.0	1.4
$\frac{5.5}{50}$	$\frac{5.0}{30}$	$\frac{5.0}{20}$	5.1	$\frac{5.1}{20}$	$\frac{5.2}{30}$	$\frac{5.1}{50}$

1370

2.1	1.9	2.2	2.2	2.2	2.1	2.1
$\frac{5.1}{50}$	$\frac{5.3}{30}$	$\frac{5.0}{20}$	5.0	$\frac{5.0}{20}$	$\frac{5.1}{30}$	$\frac{5.1}{50}$

12750

2.2	2.3	2.2	2.1	2.3	2.3	2.4
$\frac{5.0}{50}$	$\frac{4.9}{30}$	$\frac{5.0}{20}$	5.1	$\frac{4.9}{20}$	$\frac{4.9}{30}$	$\frac{4.4}{50}$

1270

2.3	2.0	2.4	2.4	2.5	2.4	3.2
$\frac{4.9}{50}$	$\frac{5.2}{30}$	$\frac{4.8}{20}$	4.8	$\frac{4.7}{20}$	$\frac{4.8}{30}$	$\frac{4.0}{50}$

11750

2.5	2.2	2.5	2.4	2.4	2.4	3.1
$\frac{4.7}{50}$	$\frac{5.0}{30}$	$\frac{4.7}{20}$	4.8	$\frac{4.8}{20}$	$\frac{4.4}{30}$	$\frac{4.6}{50}$

7/16

7/16

17.70

1.0	2.3	1.9	1.9	1.3	1.4	0.6
$\frac{5.0}{50}$	$\frac{4.0}{30}$	$\frac{4.4}{20}$	4.4	$\frac{5.0}{20}$	$\frac{4.9}{30}$	$\frac{5.5}{50}$

16.450

1.9	1.4	1.4	1.4	1.3	1.3	0.6
$\frac{4.4}{50}$	$\frac{4.9}{30}$	$\frac{4.7}{20}$	4.7	$\frac{5.0}{20}$	$\frac{5.0}{30}$	$\frac{5.5}{50}$

16.70

1.4	1.1	1.5	1.8	1.4	1.3	1.1
$\frac{4.9}{50}$	$\frac{5.2}{30}$	$\frac{4.8}{20}$	4.5	$\frac{4.9}{20}$	$\frac{5.0}{30}$	$\frac{5.2}{30}$

15.750

1.6	1.5	1.8	1.4	1.3	1.3	1.3
$\frac{4.7}{50}$	$\frac{4.8}{30}$	$\frac{4.5}{20}$	4.9	$\frac{5.0}{20}$	$\frac{5.0}{30}$	$\frac{5.0}{50}$

15.70

1.6	1.7	1.5	1.5	1.4	1.4	1.4
$\frac{4.5}{50}$	$\frac{4.6}{30}$	$\frac{4.8}{20}$	4.8	$\frac{4.9}{20}$	$\frac{4.9}{30}$	$\frac{4.5}{50}$

BM

395

6.25

4.86

2.30

* Mon Kurtz

W 25 of Pasternak

6.25

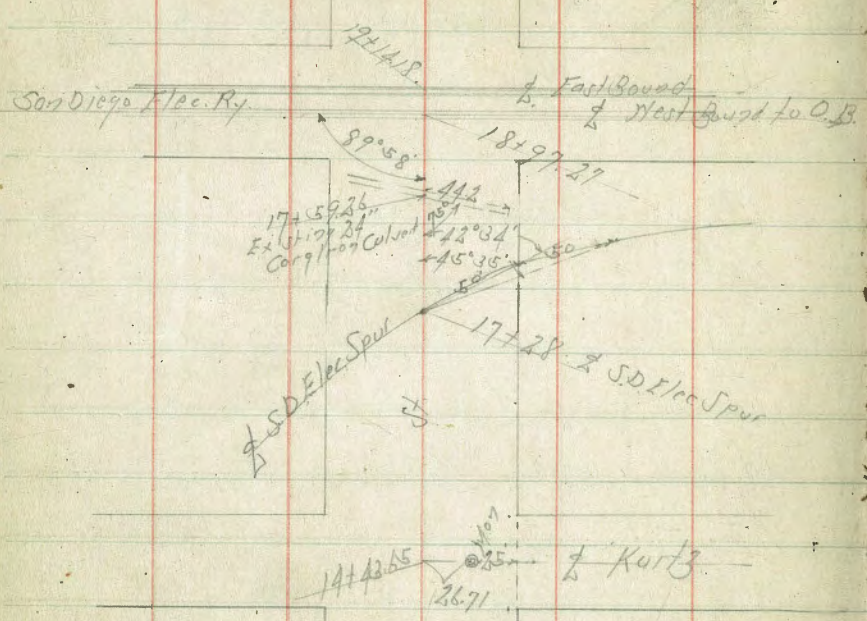
14.7.43.65 * Kurtz

7.16

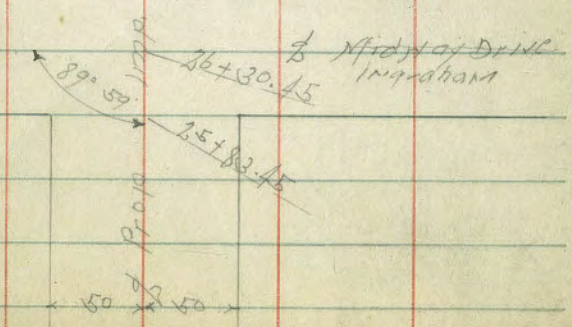
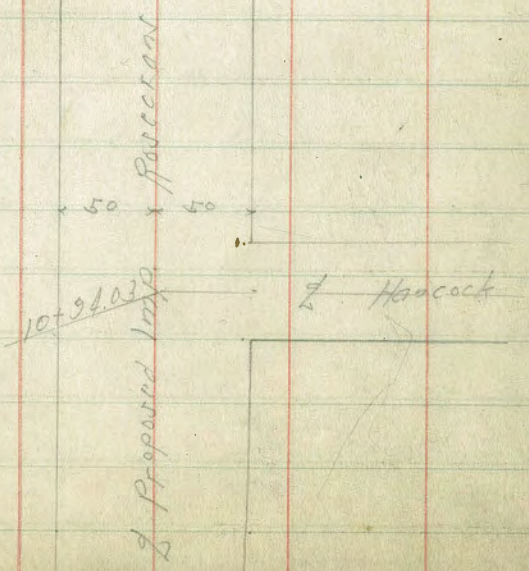
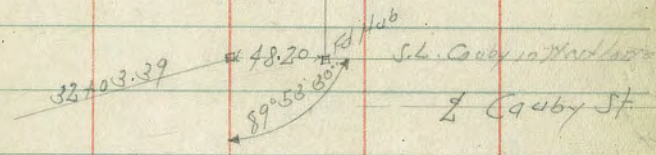
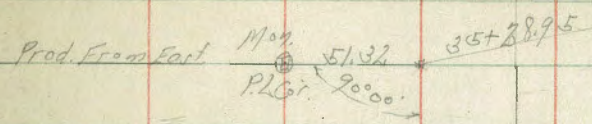
1.9	2.0	2.2	2.0	2.2	2.3	2.2
$\frac{5.3}{50}$	$\frac{5.7}{30}$	$\frac{5.0}{20}$	5.7	$\frac{5.0}{20}$	$\frac{4.9}{30}$	$\frac{5.0}{50}$

7.16

Rosecrans St
 Cross Section Atlantic to Ly. Hwy



Sketch Card Page 25



Ford Page 8

19+14.18 = 2 SD Elec East Bound Track

3.39	3.38	3.41
286 50 = Top Rail	287 Top Rail	284 50 = Top Rail

18+97.27 = 2 SD Elec West Bound Track

3.48	3.46	3.41
277 50 = Top Rail	279 Top Rail	284 50 = Top Rail

18+50

0.4	0.5	2.0	2.3	2.3	1.8	1.1
57 50	58 30	23 20	40	40 20	48 30	58

18+0

0.6	0.6	2.2	2.2	2.0	2.0	0.9
55 50	55 30	41 20	41	43 20	43 30	54 50

17+50

0.5	1.0	1.3	2.4	2.1	1.9	2.0	1.1	0.7
58 50	53 30	50 20	39	42 20	46 30	43 47 Top Rail	44 47 Top Rail	40 50

17+88 = 2 SD Elec Spur Taken on List of Track

2.22	2.35	2.31	2.16	2.42	2.29
103 50 = Top Rail	3.90 50 = Top Rail	3.94 Top Rail	4.07 Top Rail	6.23 50 = Top Rail	3.96 50 = Top Rail

6.25

6.25

22+0

	21		Z		PL	
0.4	0.6	0.5	0.9	0.6	0.7	0.4
$\frac{3.8}{50}$	$\frac{4.0}{30}$	$\frac{4.1}{20}$	3.7	$\frac{4.0}{20}$	$\frac{3.9}{30}$	$\frac{4.2}{50}$

21+50

0.6	0.7	0.6	0.8	0.3	0.7	0.8
$\frac{3.8}{50}$	$\frac{3.9}{30}$	$\frac{4.0}{20}$	3.8	$\frac{4.3}{20}$	$\frac{3.9}{30}$	$\frac{3.8}{50}$

21+0

0.4	0.4	0.6	0.6	0.6	0.7	0.9
$\frac{3.8}{50}$	$\frac{3.8}{30}$	$\frac{4.0}{20}$	3.8	$\frac{4.0}{20}$	$\frac{3.9}{30}$	$\frac{3.7}{50}$

TP

3.70 4.56 5.39 0.86

4.56

20+50

1.0	1.0	0.9	1.0	0.5	0.4	1.2
$\frac{5.3}{50}$	$\frac{5.3}{30}$	$\frac{5.4}{20}$	5.3	$\frac{5.8}{20}$	$\frac{5.5}{30}$	$\frac{5.1}{50}$

20+0

1.2	1.1	1.1	1.1	0.4	0.4	0.3
$\frac{5.1}{50}$	$\frac{5.2}{30}$	$\frac{5.1}{20}$	5.1	$\frac{5.5}{20}$	$\frac{5.5}{30}$	$\frac{5.0}{50}$

19+50

1.1	0.9	1.1	1.1	0.4	0.4	1.3
$\frac{5.2}{50}$	$\frac{5.4}{30}$	$\frac{5.2}{20}$	1.1	$\frac{5.5}{20}$	$\frac{5.7}{30}$	$\frac{5.0}{50}$

6.25

6.25

25+0

0.7	0.6	0.5	0.5	0.2	0.2	0.2
$\frac{3.9}{50}$	$\frac{3.8}{30}$	$\frac{4.1}{20}$	4.1	$\frac{4.8}{20}$	$\frac{4.1}{30}$	$\frac{4.6}{50}$

24+50

1.1	0.9	0.3	0.5	0.2	0.2	0.2
$\frac{3.5}{50}$	$\frac{3.7}{30}$	$\frac{4.3}{20}$	4.1	$\frac{4.8}{20}$	$\frac{4.1}{30}$	$\frac{4.6}{50}$

24+0

0.9	0.6	0.4	0.5	0.4	0.4	0.5
$\frac{3.7}{50}$	$\frac{3.8}{30}$	$\frac{4.2}{20}$	4.1	$\frac{4.2}{20}$	$\frac{4.2}{30}$	$\frac{4.6}{50}$

23+50

0.9	0.6	0.2	0.5	0.3	0.6	0.4
$\frac{3.7}{50}$	$\frac{3.8}{30}$	$\frac{4.6}{20}$	4.1	$\frac{4.3}{20}$	$\frac{3.8}{30}$	$\frac{4.2}{50}$

23+0

0	0.6	0.4	0.4	0.3	0.3	0.6
$\frac{3.6}{50}$	$\frac{3.8}{30}$	$\frac{4.2}{20}$	4.0	$\frac{4.3}{20}$	$\frac{4.3}{30}$	$\frac{4.0}{50}$

22+50

0.9	0.4	0.4	0.7	0.3	0.2	0.3
$\frac{3.7}{50}$	$\frac{4.2}{30}$	$\frac{4.2}{20}$	3.9	$\frac{4.3}{20}$	$\frac{4.1}{30}$	$\frac{4.3}{50}$

4.56

4.56

2770

0.0 0.1 0.2 0.1 0.2 0.2 0.0
 4.6 4.0 3.9 4.0 4.3 4.1 4.6
 50 30 20 20 30 30 50

26777.45 - S.L. Midway

0.43 0.23 0.04 0.23 0.00 0.26 0.53
 3.70 4.36 4.05 3.90 4.13 4.33 3.60
 30 30 20 20 20 30 30
 Topch Topch Topch Topch Topch Topch Topch

26730.15 - L. Midway

0.34 0.43 0.40
 3.75 3.70 3.73
 50 20 50
 Topch Topch Topch

BM

3.57 0.56

S.M.P.
 Reservoir
 Midway Dr.

TR 260 4.13 4.03 0.53

4.13

25783.45 - N.L. Midway

0.56 0.11 0.06 0.21 0.14 0.07 0.50
 4.00 4.67 4.50 4.25 4.42 4.63 4.06
 30 30 20 20 20 30 30
 Topch Topch Topch Topch Topch Topch Topch

25750

0.5 0.4 0.1 0.5 0.0 0.3 0.2
 4.5 4.3 4.5 4.1 4.6 4.3 4.8
 50 30 20 20 30 30 50
 4.56

4.56

30+0

4 5 7

-0.2 0.0 0.2 -0.4 -0.6 -0.6 -0.4

$\frac{4.3}{50}$ $\frac{4.6}{30}$ $\frac{3.9}{30}$ $\frac{4.5}{20}$ $\frac{4.7}{20}$ $\frac{4.7}{30}$ $\frac{4.5}{50}$

29+50

0.0 -0.3 0.0 -0.3 -0.4 -0.4 -0.5

$\frac{4.6}{50}$ $\frac{3.8}{30}$ $\frac{4.6}{30}$ $\frac{4.4}{20}$ $\frac{4.5}{20}$ $\frac{4.5}{30}$ $\frac{4.6}{50}$

29+0

0.1 -0.1 -0.3 -0.2 -0.4 -0.5 -0.3

$\frac{4.0}{50}$ $\frac{4.7}{30}$ $\frac{4.4}{30}$ $\frac{4.3}{20}$ $\frac{4.5}{20}$ $\frac{4.6}{30}$ $\frac{4.4}{50}$

28+50

0.2 0.2 -0.2 -0.1 -0.3 -0.3 -0.3

$\frac{3.9}{50}$ $\frac{3.9}{30}$ $\frac{4.3}{20}$ $\frac{4.2}{20}$ $\frac{4.6}{20}$ $\frac{4.6}{30}$ $\frac{4.4}{50}$

28+0

0.1 -0.1 0.0 -0.1 -0.3 -0.3 -0.3

$\frac{4.0}{50}$ $\frac{4.8}{30}$ $\frac{4.6}{30}$ $\frac{4.2}{20}$ $\frac{4.4}{20}$ $\frac{4.4}{30}$ $\frac{4.4}{50}$

27+50

0.3 0.1 0.1 0.0 -0.3 -0.3 -0.3

$\frac{3.8}{30}$ $\frac{4.0}{30}$ $\frac{4.0}{30}$ $\frac{4.1}{20}$ $\frac{4.4}{20}$ $\frac{4.4}{30}$ $\frac{4.4}{50}$

4.13

4.13

TP 3.74 - 3.95 3.92 0.21

3370

41 2 Rt
 $\begin{matrix} -0.6 \\ 47 \\ 50 \end{matrix}$ $\begin{matrix} -0.5 \\ 46 \\ 50 \end{matrix}$ $\begin{matrix} -0.4 \\ 47 \\ 50 \end{matrix}$ $\begin{matrix} -0.7 \\ 48 \\ 50 \end{matrix}$ $\begin{matrix} -0.4 \\ 45 \\ 50 \end{matrix}$ $\begin{matrix} -1.1 \\ 52 \\ 50 \end{matrix}$ $\begin{matrix} -0.8 \\ 49 \\ 50 \end{matrix}$

32750

$\begin{matrix} -0.3 \\ 44 \\ 50 \end{matrix}$ $\begin{matrix} -0.4 \\ 45 \\ 50 \end{matrix}$ $\begin{matrix} -0.9 \\ 50 \\ 50 \end{matrix}$ $\begin{matrix} -0.6 \\ 47 \\ 50 \end{matrix}$ $\begin{matrix} -0.4 \\ 45 \\ 50 \end{matrix}$ $\begin{matrix} -0.9 \\ 50 \\ 50 \end{matrix}$ $\begin{matrix} -0.7 \\ 48 \\ 50 \end{matrix}$

32703.39 = S.L. Corby

$\begin{matrix} -0.1 \\ 42 \\ 50 \end{matrix}$ $\begin{matrix} -0.2 \\ 43 \\ 50 \end{matrix}$ $\begin{matrix} -0.6 \\ 47 \\ 50 \end{matrix}$ $\begin{matrix} -0.41 \\ 45 \\ 50 \end{matrix}$ $\begin{matrix} -0.7 \\ 48 \\ 50 \end{matrix}$ $\begin{matrix} -0.6 \\ 47 \\ 50 \end{matrix}$ $\begin{matrix} -0.4 \\ 45 \\ 50 \end{matrix}$

31750

$\begin{matrix} -0.1 \\ 42 \\ 50 \end{matrix}$ $\begin{matrix} -0.5 \\ 46 \\ 50 \end{matrix}$ $\begin{matrix} -0.2 \\ 43 \\ 50 \end{matrix}$ $\begin{matrix} -0.7 \\ 48 \\ 50 \end{matrix}$ $\begin{matrix} -1.0 \\ 51 \\ 50 \end{matrix}$ $\begin{matrix} -0.9 \\ 50 \\ 50 \end{matrix}$ $\begin{matrix} -0.8 \\ 49 \\ 50 \end{matrix}$

3170

$\begin{matrix} -0.5 \\ 46 \\ 50 \end{matrix}$ $\begin{matrix} 0.1 \\ 48 \\ 50 \end{matrix}$ $\begin{matrix} -0.1 \\ 48 \\ 50 \end{matrix}$ $\begin{matrix} -0.4 \\ 45 \\ 50 \end{matrix}$ $\begin{matrix} -0.7 \\ 48 \\ 50 \end{matrix}$ $\begin{matrix} -0.7 \\ 48 \\ 50 \end{matrix}$ $\begin{matrix} -0.7 \\ 48 \\ 50 \end{matrix}$

30750

$\begin{matrix} -0.2 \\ 42 \\ 50 \end{matrix}$ $\begin{matrix} 0.0 \\ 46 \\ 50 \end{matrix}$ $\begin{matrix} 0.1 \\ 40 \\ 50 \end{matrix}$ $\begin{matrix} -0.3 \\ 44 \\ 50 \end{matrix}$ $\begin{matrix} -0.6 \\ 47 \\ 50 \end{matrix}$ $\begin{matrix} -0.6 \\ 47 \\ 50 \end{matrix}$ $\begin{matrix} -0.3 \\ 46 \\ 50 \end{matrix}$

4.13

4.13

4t 4 4t

3670

-0.4	-0.3	-0.5	-0.5	-1.2	-1.2	-1.1
$\frac{4.4}{50}$	$\frac{4.3}{30}$	$\frac{4.5}{20}$	4.5	$\frac{5.2}{20}$	$\frac{5.2}{30}$	$\frac{5.1}{50}$

35750

-0.8	-0.5	-0.5	-0.5	-0.9	-1.2	-1.0
$\frac{4.8}{50}$	$\frac{4.5}{30}$	$\frac{4.5}{20}$	4.5	$\frac{4.9}{20}$	$\frac{5.2}{30}$	$\frac{5.0}{50}$

BM

35.40

67 Mon
P. 6. 238

35x0

-0.6	-0.5	-0.5	-0.2	-1.0	-1.1	-1.1
$\frac{4.6}{50}$	$\frac{4.5}{30}$	$\frac{4.5}{20}$	4.2	$\frac{5.0}{20}$	$\frac{5.1}{30}$	$\frac{5.1}{50}$

34750

-0.5	-0.4	-0.4	-0.5	-0.8	-1.0	-0.8
$\frac{4.5}{50}$	$\frac{4.4}{30}$	$\frac{4.4}{20}$	4.5	$\frac{4.8}{20}$	$\frac{5.0}{30}$	$\frac{4.8}{50}$

3470

-0.7	-0.3	-0.3	-0.8	-0.5	-1.3	-0.8
$\frac{4.7}{50}$	$\frac{4.3}{30}$	$\frac{4.3}{20}$	4.8	$\frac{4.5}{20}$	$\frac{5.3}{30}$	$\frac{4.8}{50}$

33750

-0.5	-0.3	-0.6	-0.8	-0.5	-0.8	-0.8
$\frac{4.5}{50}$	$\frac{4.3}{30}$	$\frac{4.6}{20}$	4.8	$\frac{4.5}{20}$	$\frac{4.8}{30}$	$\frac{4.8}{50}$

39.5

39.5

38+50

	H	Z	P1				
	-1.1	-1.2	-1.2	-1.2	-1.1	-1.1	-1.1
	5/80	5/30	5/20	5/20	5/20	5/30	5/50

38+0

	-1.1	-1.0	-1.0	-1.1	-1.1	-1.2	-1.2
	5/50	5/30	5/20	5/1	5/20	5/30	5/30

37+22+3 B.C.P1

	-1.0	-1.0	-1.0	-1.18	-1.1	-1.1	-1.1
	5/50	5/30	5/20	5/13 20	5/20	5/30	5/50

37+50

	-0.9	-0.6	-0.6	-1.0	-1.1	-1.1	-1.2
	4.9/50	4.6/30	4.6/20	5/0	5/20	5/30	5/50

37+0

	-0.6	-0.5	-0.6	-0.6	-1.1	-1.1	-1.1
	4.6/50	4.5/30	4.6/20	4.6/10	5/20	5/30	5/50

36+50

	-0.5	-0.5	-0.5	-0.5	-1.0	-1.0	-1.1
	4.5/50	4.5/30	4.5/20	4.5/15	5/20	5/30	5/50

395

395

41+50

	LT	Z	RT			
	-1.5	-1.2	-1.3	-1.2	-0.8	-0.7
	12.0 50	12.7 30	12.8 30	12.7	12.8 30	12.8 30

41+0

	-1.4	-1.4	-1.5	-1.4	-1.2	-1.0	-0.9
	12.9 50	12.9 30	12.0 20	12.9	12.7 20	12.5 30	12.1 30

40+50

	-1.3	-1.3	-1.3	-1.4	-1.3	-1.1	-1.0
	12.8 50	12.8 30	12.8 30	12.9	12.8 20	12.6 30	12.5 30

40+0

	-1.4	-1.4	-1.3	-1.2	-1.2	-1.0	-0.9
	12.9 50	12.9 30	12.8 20	12.7	12.7 20	12.5 30	12.3 50

39+61.66 FC

	-1.3	-1.2	-1.2	-1.3	-1.4	-1.4	-1.3
	12.8 50	12.7 30	12.7 20	12.8 ⁰ 20 25/25	12.9 20	12.9 30	12.8 50

TP 11.94 11.51 1.38 -0.43

11.51

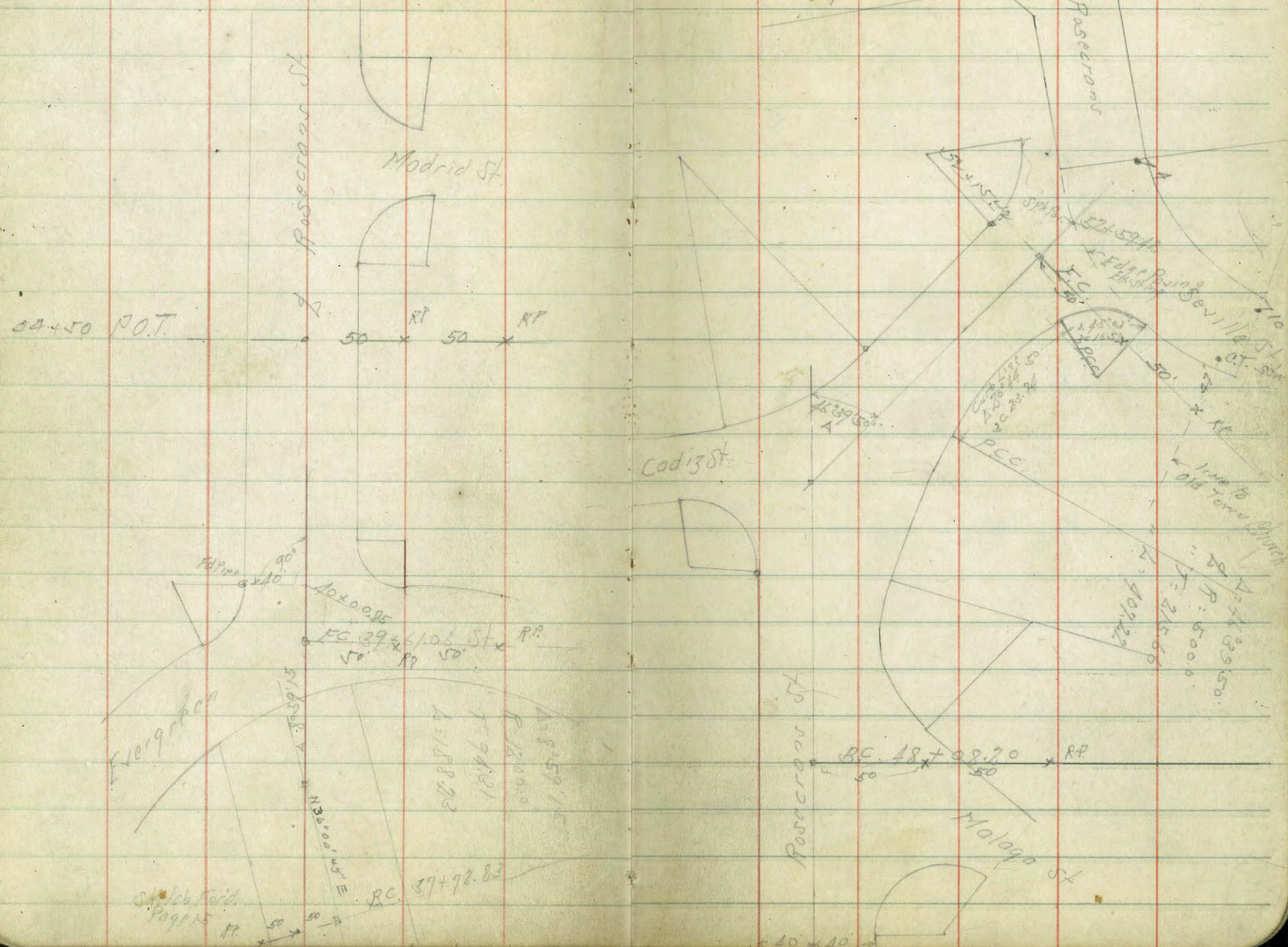
39+0

	-1.3	-1.3	-1.2	-1.2	-1.1	-1.1	-1.0
	5.3 50	5.3 30	5.2 20	5.2	5.1 20	5.1 30	5.0 50

395

395

Rosecrans St
 Cross Section Attached to by Hon



Elev 9m 400

Sketch of
 Page 15

A 8 59.15
 F 120.00
 T 94.81
 2 158.23

Rosecrans St

Malaga St

A 1 325.50
 F 5000
 T 215.56

BC 48+98.70 x RT

FC 29+51.06 St x RT

BC 57+92.83

P.C.C.

Cadiz St

by Hon St

Rosecrans

Madrid St

Rosecrans St

54+50 P.O.T.

44150

	4		5		11	
	12.4	12.7	12.6	12.31	12.3	13.0
	5.6	5.3	5.2	5.8	5.7	5.0
	3.0	3.0	3.0	2.5/1.6	3.0	3.0

4410

	4.2	6.4	8.1	6.9	9.8	10.2
	9.8	9.6	9.9	9.1	8.3	7.8
	3.0	3.0	3.0	3.0	3.0	3.0
	10.4	10.4	10.4	10.4	10.4	10.4

TP 8.36 17.99 1.88 9.63

17.99

43450

	2.2	3.1	3.5	4.7	5.4	5.9
	9.3	8.4	8.0	6.8	6.1	5.6
	3.0	3.0	3.0	3.0	3.0	3.0
	7.2	7.2	7.2	7.2	7.2	7.2

4340

	-0.9	-0.7	-0.5	0.2	0.7	1.1
	12.4	12.3	12.0	11.3	10.8	9.8
	3.0	3.0	3.0	3.0	3.0	3.0
	2.5	2.5	2.5	2.5	2.5	2.5

42450

	-1.2	-0.9	-1.0	-1.0	-0.9	-0.7
	12.7	12.4	12.5	12.5	12.4	12.2
	3.0	3.0	3.0	3.0	3.0	3.0
	0.2	0.2	0.2	0.2	0.2	0.2

4240

	-1.4	-1.3	-0.9	-1.0	-0.8	-0.8
	12.9	12.8	12.4	12.5	12.3	12.3
	3.0	3.0	3.0	3.0	3.0	3.0
	0.7	0.7	0.7	0.7	0.7	0.7

11.51

11.51

8-5 337

47+50

14.8	14.5	14.5	14.5	14.6	14.6	14.7
$\frac{32}{50}$	$\frac{35}{50}$	$\frac{35}{50}$	$\frac{35}{50}$	$\frac{34}{50}$	$\frac{34}{50}$	$\frac{33}{50}$

47+0

14.4	14.3	14.4	14.4	14.4	14.3	14.6
$\frac{36}{50}$	$\frac{37}{50}$	$\frac{36}{50}$	$\frac{36}{50}$	$\frac{36}{50}$	$\frac{37}{50}$	$\frac{38}{50}$

46+50

14.3	14.7	14.4	14.1	14.0	14.1	14.3
$\frac{37}{50}$	$\frac{33}{50}$	$\frac{36}{50}$	$\frac{39}{50}$	$\frac{40}{50}$	$\frac{39}{50}$	$\frac{37}{50}$

46+0

13.9	13.9	14.0	14.0	14.0	14.0	13.8
$\frac{41}{50}$	$\frac{41}{50}$	$\frac{40}{50}$	$\frac{40}{50}$	$\frac{40}{50}$	$\frac{40}{50}$	$\frac{38}{50}$

45+50

13.9	13.9	13.7	13.8	13.8	13.8	13.8
$\frac{41}{50}$	$\frac{41}{50}$	$\frac{42}{50}$	$\frac{42}{50}$	$\frac{41}{50}$	$\frac{41}{50}$	$\frac{41}{50}$

45+0

13.6	13.7	13.5	13.4	13.4	13.6	13.8
$\frac{44}{50}$	$\frac{43}{50}$	$\frac{45}{50}$	$\frac{46}{50}$	$\frac{46}{50}$	$\frac{48}{50}$	$\frac{48}{50}$

17.99

17.99

50+50

23.3	25.4	25.9	25.6	25.6	25.9	26.6
3.9	1.8	1.3	1.6	1.4	1.2	0.6
50	30	20	20	30	30	50

50+0

17.8	16.7	17.0	17.8	19.1	19.5	20.7
9.4	7.5	10.2	9.4	8.1	7.6	6.5
50	30	20	20	20	30	50

49+50

16.5	15.8	15.6	16.2	16.9	17.2	14.1
10.7	11.4	11.6	11.0	10.3	10.0	7.1
50	30	20	20	20	30	50

49+0

14.8	14.7	14.7	15.4	15.9	16.1	16.9
12.4	12.5	12.5	11.8	11.3	11.1	10.3
50	30	30	20	20	30	50

77

12.21 27.24 2.96 15.03

27.24

48+50

14.3	15.0	15.0	15.3	15.8	16.0	16.5
6.7	6.0	6.0	2.7	2.6	3.0	1.5
50	30	20	20	20	30	50

48+0820 BC.Pt

14.5	14.6	14.4	15.18	15.1	15.5	15.9
6.4	6.1	6.1	2.81	2.9	2.5	2.0
50	30	20	25.6	20	30	50

17.99

17.99

51735

31.2
8.2
50

30.7
8.8
30

29.5
100
20

31.3
8.2
5

26.7
128

36.9
126
77

32.6
6.9
21
Edg. Pt.

33.2
6.3
30

33.1
6.4
40

51720

30.2
9.3
50

31.0
8.5
30

27.8
11.7
20

24.7
14.8
15

27.6
11.7

32.4
7.1
20
Edg. Pt.

32.8
6.7
30

32.5
7.0
40

51706.51 - opp PCC 07 Pt.

29.6
9.9
50

30.3
9.2
38

26.4
13.1
34

26.4
13.1
30

24.4
15.1
20

25.4
14.1
16

31.2
8.3
12

31.61
7.85
20
Edg. Pt.

32.2
7.3
20

32.0
7.5
30

32.0
7.5
40

50780

28.5
11.0
50

22.9
16.6
46

22.9
16.6
48

26.5
11.0
40

29.2
10.3
30

29.6
9.9
20

29.9
9.6

30.0
9.5
20

30.0
9.5
30

30.1
9.6
30

50770

26.0
10.5
50

27.4
11.7
30

28.1
11.4
20

28.4
11.1

29.0
10.5
20

28.9
10.6
30

29.2
10.3
50

TP 1247 3946 0.25 26.99

27.24

39.46

27.24

BM

3.77

41.59

SW 82
Roserstadt
47 May
41.75

TP

715

45.36

1.25

38.21

52+59.42 - Fasting Price of Tater on Line of River

52+15.42 - F.C.

52+03 - opp PCC on Pt

57+58

39.46

44

45

47

37.17

36.94

36.75

36.63

36.50

36.90

37.17

37.59

36.10

2.77
10.5
27.9

2.52
30.07.19

2.91
20.07.19

2.83
70.07.19

2.96
70.07.19

2.56
20.07.19

2.89
20.07.19

1.87
15.07.19

1.36
15.07.19

35.7

36.0

36.2

36.0

31.6

33.3

35.8

37.1

37.3

3.8
10.0

3.5
30.0

3.3
20.0

3.8
8.0

7.9
6.0

3.7
5.0

4.0
30.0

4.7
40.0

34.9

35.2

35.6

35.3

31.2

31.2

35.7

36.7

36.9

4.6
40.0

4.3
30.0

3.9
20.0

4.2

8.3
2.0

8.3
8.0

3.8
8.0

2.8
28.0

2.6
20.0

32.5

32.5

32.5

32.4

28.3

28.3

33.2

33.8

34.8

7.0
70.0

7.0
30.0

7.0
20.0

7.1
70.0

11.2
10.0

10.6
20.0

6.2
22.0

5.7
30.0

4.7
40.0

39.46

40.46

9-21-33
Miller
Walker
Bliss

X 500. Alley Bk. 143. Univ. Hts.
Polk. to Howard.
bet. Georgia & Florida.

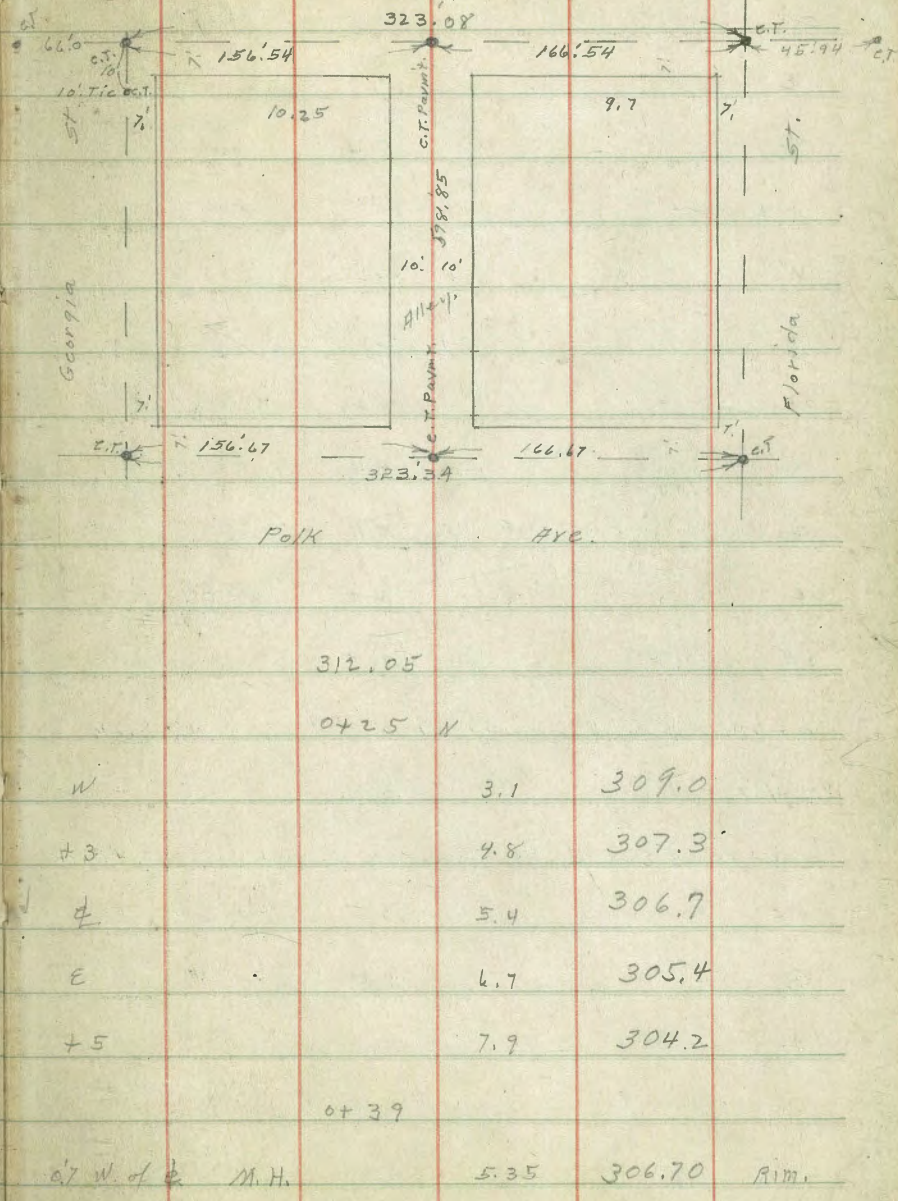
20' wide.
S.E. Polk
& Georgia

indexed
c.s.k.

319.85 NW 1400

31

B.M. RP	0.29	335.26	334.97
T.P.	0.01	322.33	322.32
14' S. of N. line = N. cl. line Polk.			
40' W. of W. line Alley		5.71	316.67 cmt. cl.
40' " " " "		6.38	315.95 gutter
T.P.	2.14	312.05	309.87
3' W. of W. line Alley P.C. cl. ret.		2.85	309.20 gutter
" " " " " " " "		2.18	309.87 cmt. cl.
W. line		3.41	308.64 gutter, pavmt.
±		5.21	306.84 " "
E. line		7.13	304.92 " "
3' E. of E. line P.C. cl. ret.		7.71	304.34 " "
3' " " " " " " " "		7.10	304.95 cmt. cl.
30' " " " " " " " "		12.05	300.00 " "
30' " " " " " " " "		12.64	299.41 gutter
0 + 00 = N. Line Polk			
E.		4.39	305.66 Pavmt. & cmt. cl.
+ 8		5.39	306.66 pavmt.
±		5.06	306.99 " "
W.		3.11	308.94 " "
W.		2.51	309.54 cmt. cl.



07 W. of ± M.H. 5.35 306.70 Rim.

312.05

0+48

-5	7.5	304.6
E	7.0	305.1
φ	5.4	306.7
+2	3.8	308.3
W	2.5	309.6

0+52

-0.5 cmt. step	3.05	308.97 ✓
W	3.4	308.7
φ	5.4	306.7
E	7.0	305.1
+5	7.5	304.6

✓ 0+64 = φ double garage on W. dirt floor 4.7 Back

W-4.7 floor	3.3	308.8
-------------	-----	-------

✓ 0+80 = S. End double garage on W. dirt floor 7.9 Back

-5	7.7	304.4
E	7.5	304.6
φ	5.2	306.9
W	2.8	309.3
+7.4 floor	1.9	310.2

312.05

Alley BIK 143.211.

32

1+00 = N. end above garage, 9' Back

W-9.0 floor	1.6	310.5
W.	2.8	309.3
φ	5.7	306.4
+6	7.0	305.1
E	7.4	304.7 ✓
+5	8.0	304.1

1+05

-5	7.9	304.2
E	7.3	304.8
φ	5.8	306.3
W	4.6	307.5

1+26

W.	5.5	306.6
φ	6.7	305.4
+9	7.1	305.0
+9 S. end W. side cmt. wall	6.6	305.5
E ground at E. face wall	7.4	304.7
+5	9.2	302.9

312.05

0+31 S. End House on E. 0.6 in Alley

9.4 E. of ϕ floor of House 5.95 306.10 ✓

0+32 = N. end ext. wall on E. 1.3 in Alley

8.7 E. of ϕ Top wall 6.61 305.44 ✓

1+45

✓ E+05 W. side House. 6.7 305.4

↓ ϕ 6.3 305.8

+7 5.4 306.7

W. 5.0 307.1

✓ 1+49⁵ = N End above House on E.

W. 5.0 307.1

↓ ϕ 6.5 305.6

+6 7.0 305.1

✓ +9.5 House N.W. cor. 8.5 303.6

E. 8.9 303.2

+7 9.5 302.6 ✓

T.P. 0.77 305.47 ✓ 7.37 304.68 ✓

✓ 1+71.5 S. End Garage on E. 4.0 Back, Entrance on N. End.

-7 4.2 301.3

E. 3.7 301.8

+1 2.0 303.5

305.47

Alley BIK 143.21.H.

33

+5 0.6 304.9

↓ ϕ 0.4 305.1

W. +0.8 306.3 ✓

✓ 1+90. N. End above garage

W. 0.0 305.5 ✓

↓ ϕ 1.5 304.0

+7 2.0 303.5

E. 3.3 302.2

+1 5.0 300.5

+10 dirt floor of garage 5.5 300.0

2+25 S. of garage on E ✓

-5 5.3 300.2

E 4.1 301.4

↓ ϕ 3.7 301.8

W. 2.0 303.5

2+31 garage on E. dirt floor 2.5 Back.

E-2.5 floor. 4.3 301.2

✓

305.47

✓ 2+61 = S. End garage on E. not in use	0.5 in alley	
9.5 E. of ϕ	5.2	300.3
✓ 2+80 = N. End above garage.	0.3 in alley.	
W.	3.0	302.5
+8	4.5	301.0 ✓
✓ ϕ on M.H. Rim	4.51	300.96 ✓
E	5.4	300.1
+5 on N. side garage.	7.3	298.2
✓ 3+04 S. End garage on E dirt floor on line		
-5	7.0	297.9
E	6.0	299.5
✓ ϕ	5.6	299.9
+5	5.0	300.5
W.	4.1	301.4
✓ 3+25 { N. End above garage S. " garage on E. entrance N. End on E. Line S. " W. edge emt. wall		
W.	4.2	301.3
+5	5.6	299.9
✓ ϕ	6.2	299.3
E	6.4	299.1 ✓
E. Top. emt. wall.	5.95	299.52 ✓

Alley BIK. 143.2.H.

305.47.

✓ 3+41 N. End above garage. N. entrance	one line dirt floor	
E-5. floor	7.4	298.1
E-0.5 East of wall	7.3	298.2 ✓
E. Top emt. wall	5.96	299.51 ✓
E. ground	6.7	298.8
✓ ϕ	6.5	299.0
+7	6.1	299.4
W.	4.8	300.7
	3+44 ^E	
E. N. End emt. wall	6.0	299.5
E. ground.	6.7	298.8
✓ 3+50 = S. End. 4 garages on W. emt floor	5.2 Back	
W-5.2 floor	5.2	300.3
W.	5.6	299.9
✓ 3+62 S. End. garage under construction on E. line		
W.	5.5	300.0
✓ ϕ	6.1	299.4
E	7.2	298.3 ✓
E. Top foundation wall	6.08	299.39 ✓
+5 on S. side garage	7.9	297.6 ✓

305.47. ✓

✓ 3+82 N. End above garage

E-5 8.5 297.0 ✓

E. on top foundation 6.08 299.39 ✓

E. 8.0 297.5

+4 6.7 298.8

✓ Φ 6.4 299.1

W. 5.7 299.8

✓ 3+89 = N. End 4 garages on W. cnt. floor 6.5 Back

W 5.8 299.7 ✓

W+ floor 5.40, 300.07 ✓

4+00

W. 6.8 298.7 ✓

✓ Φ 6.9 298.6 ✓

T.P. 9.81 308.43 6.85 298.62 ✓

E 10.8 297.6 ✓

+5 12.1 296.3 ✓

✓ 4+02 = S. End. double garage on E. cnt. floor 2.5 Back

E-2.5 floor 10.6 297.8 ✓

✓ 4+02 & double garages on W. dirt floor 8.5 Back.

W-8.5 floor 9.3 299.1 ✓

308.43

Alley BIK. 143. U.H.

35

4+21 = N. End above garage on E. 2.6 Back
E-2.6 floor 18.53 297.90 ✓

✓ 4+40 garage on W. dirt floor 4.0 Back

E-5 10.4 298.0

E 10.3 298.1

✓ Φ 10.2 298.2

+4 10.1 298.3

W. 9.4 299.0

+4.0 floor. 8.7 299.7

4+70 double garage on E cnt. floor 3.0 Back.

W 8.3 300.1

✓ Φ 9.3 299.1

E 9.4 299.0

+3.0 floor 9.4 299.0 ✓

✓ 5+05 garage on W. dirt floor 5.0 Back

-5. 8.1 300.3

E 9.2 301.2

✓ Φ 7.3 301.1

W 6.2 302.2

+5.5 floor 5.1 303.3

✓ 5+15 garage on W. dirt floor 5.0 Back

W-5.0 floor 4.2 304.2 ✓

308.43			308.43			Alley BK 143 UH.		
✓	5+19 garage on E. cmt. floor 3.2 Back							36
	E-4.0 floor	7.37	301.06 ✓	E.	5.7	302.7	308.43	
✓	5+28 S. end double garage on W. cmt. floor 2.5 Back			+5	5.7	302.5	TP. 308.09	
	W-2.5	4.28	304.15 ✓	5+98 ⁸⁵ = S. line			320.30	
	W	5.1	303.3	0.3 W. of E. line = cmt. cl.	5.80	302.63	0.34	
	+7	6.6	301.8	0.3 W. " " " = pavmt.	5.88	302.55	12.21	
↓	⊕	6.8	301.6	E+6	"	5.85	319.85 =	
	E.	7.1	301.3 ✓	⊕	"	5.58	319.85 B.M.B.P.	
✓	5+31 garage on E. cmt. floor 7.4 Back			0.2 W. of W. line pavmt	4.36	304.07	N.W. Howard & Georgia	
	E+3.2 W. edge cmt apron	7.25	301.18 ✓	0.25 W. of W " cmt. cl.	3.85	304.58		
	E+7.4 floor	7.13	301.30 ✓	"				
✓	5+49 N. end above garage on W. 2.5 Back			30' W. of W line gutter	1.85	306.58		
	-5	6.7	301.7 ✓	30' W " " " cmt. cl.	1.31	307.12		
	E	6.3	302.1 ✓	2' " " " " " "	3.82	304.61	at P.C. direct	
↓	⊕	6.2	302.2 ✓	" " " " " " "	4.41	304.02 ✓		
	W	4.7	303.7 ✓	W. pavmt.	4.59	303.84 ✓		
	+2.5 floor	4.25	304.18 ✓	⊕	"	5.53	302.90 ✓	
	5+65			E.	"	6.35	302.08 ✓	
	W.	4.2	304.2	+2	"	6.57	301.86 ✓	
	+3	4.4	304.0	+2 cmt. cl. at P.C. direct.	6.04	302.39 ✓		
↓	⊕	5.6	302.8	+60 " "	11.07	297.36 ✓		
				+60 pavmt.	11.66	296.77 ✓		

Indexed
C.S.K.

X Sec. Alley B.K.F. Plumosa Park

7-
Mills
Bliss
Paraguay

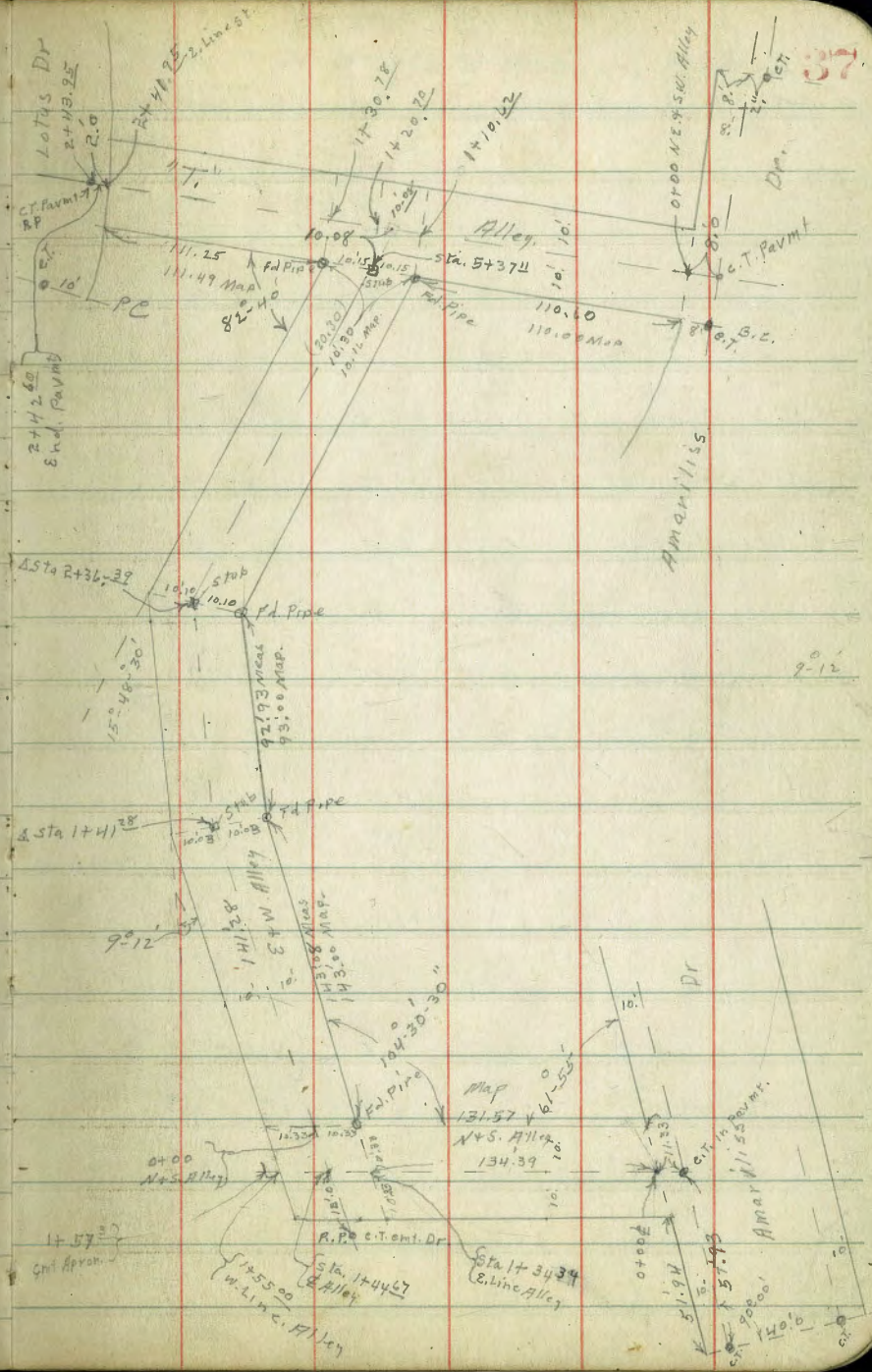
B.M. B.P.	11.42	120.03		108.61	S.S. Freeman & others
T.P.	12.79	132.05	0.77	119.26	
T.P.	12.73	142.94	1.84	130.21	
Set.					N.W. Lot 16
B.M. Top Hydt.			10.72	132.22	4 Hydrants
T.P.	10.06	148.50	4.50	138.44	
Set.					S. side Amarijiss E. side Alley B.K.F.
B.M. Top Hydt.	5.22	148.18	5.54	142.96	"

S. side line Amarijiss Dr.

11.33 Lt. = Alley Line Produced	7.63	140.55		Top of
"	8.23	139.95		gutter
"	7.64	140.50		payment
11.33 Rt	7.11	141.07		"
18.33 "	6.73	141.45		"
18.33 "	5.89	142.29		Top of

0+00 on S. line Amarijiss Dr. on d.

11.33 Rt.	5.75	142.43		entire
11.33 "	6.25	141.93		payment
"	7.05	141.13		"
11.33 Lt.	7.12	141.06		"
11.33 "	7.01	141.17		entire



148.18

0+07⁵⁰ ϕ at 90° 00'

2			
10.4 Rt. ent. dr. to Garage. N. End	6.15	142.03	
E.	6.2	142.0	
ϕ	6.3	141.9	
W. = 10 Rt.	5.8	142.4	

0+23³

W	5.2	143.0	
ϕ	5.5	142.7	
E	5.8	142.4	
10.4 Lt. ent. dr. to garage S. End	5.86	142.32	
30' Lt. of ϕ floor of garage.	5.85	142.33	

0+60

E	4.5	143.7	
ϕ	4.1	144.1	
W	3.4	144.8	

0+81

W.	2.5	145.7	
ϕ Top M.H.	2.9	145.3	
E	3.2	145.0	

148.78

Along Bldg E. Plumesa Park

0+93. Garage on E. 20.8' Back ent. floor

38

E-20.8 floor	3.23	144.95	
E-0.8 ent. apron	2.60	145.58	
ϕ	2.5	145.7	
W.	2.0	146.2	
T.P.	5.79	152.10	1.87

1714 garage on W. ent. floor 15.7' Back

W-15.7 floor	3.93	149.17	
W-1.7 edge ent apron	4.97	147.13	
W.	5.3	146.8	
ϕ	5.8	146.3	
E.	6.1	146.0	

1+33 = N. End. ent. dr on E. 1/2' Back at 90° 00'

E-1.2	5.71	146.39	
E.	5.8	146.3	
ϕ	5.4	146.7	
W.	4.8	147.3	

1+34³⁹ ϕ = N. Line E & W. Milling Products. (on diagonal)

W.	4.9	147.2	
ϕ	5.4	146.7	
E	5.8	146.3	

	152.10		
1+44 ² ϕ = ϕ E+W Alley Produced (on diagonal)			
E	5.5	146.6	
ϕ on Top M.H.	5.10	147.0	
W.	4.7	147.4	
1+52 = S. End. emt. dr. on E 1.3 Back			
E - 1.3 = S. End. emt. Dr.	5.10	147.0	
E - 25' floor	6.40	145.70	
1+55 = S. line E+W Alley Produced (on diagonal)			
W.	4.0	148.10	
ϕ	4.7	147.4	
E	5.0	147.1	
1+57 ² ϕ = N. End. emt. dr. Parallel to S. line E+W Alley			
9.2 Lt. = E. End. dr.	4.83	147.27	
ϕ on dr.	4.40	147.70	
12' Rt. = W. end dr. ^(E. Front) floor garage	3.85	148.25	
0+00 ϕ E+W Alley (on diagonal)			
S.	4.0	148.10	
ϕ	4.7	147.4	
N	4.9	147.2	

	152.10		Alley BIK E. Plumes Park
0+50			Rt Angles from here 39
N.	3.2	148.9	
ϕ	3.5	148.6	
+7.	3.3	148.8	
S	2.8	149.3	
	0+70		
S.	2.2	149.9	
+4	2.2	149.9	
+5	2.8	149.3	
ϕ	2.9	149.2	
+6	2.1	150.0	
N	2.1	150.0	
	0+87		
N.	1.5	150.6	
ϕ	1.5	150.6	
S.	1.7	150.4	
	1+00		
S.	1.4	150.7	
ϕ	1.2	150.9	
N	0.5	151.6	
T.P. ons.	8.24	159.34	1.00 151.10 Nail Pole

159.34
1741 28 ♀ Δ 9-12 Rt. on split

N 7.1 152.2

♀ stub 7.37 151.97

S 7.3 152.0

1770

S 6.2 153.1

♀ 6.6 152.7

N 6.3 153.0

2100

N 6.0 153.3

♀ 5.7 153.6

S 5.7 153.6

+2. on lawn in yard

5.7 153.6

2136 39 ♀ Δ 15-48-30" on split.

S 4.8 154.5

♀ Hub 5.17 154.17

N 5.0 154.3

2165

N 4.4 154.9

♀ 4.7 154.6

+5 4.8 154.5

S 3.9 155.4

+2 on lawn in yard 3.6 155.7

159.34 Alley BIK E. Plumasa Park

3100

40

S 4.0 155.3

+2 4.0 155.3

+4 4.9 154.4

♀ 4.8 154.5

N. 4.5 154.8

3130

N 4.2 155.1

+5 4.4 154.9

♀ 4.9 154.4

+8 4.9 154.4

S 4.1 155.2

3140

S 4.0 155.3

+1 4.6 154.7

+8 4.8 154.5

♀ 4.4 154.9

+3 3.7 155.6

N 3.6 155.7

159.34

3+65

N	3.5	155.8
φ	4.4	154.9
S	3.6	155.7

3+72 = E. End lattice fence on s. 0.9 in Alley

3+95

S+0.3 fence	3.4	155.7
φ	3.7	155.6
N	3.5	155.8

4+02 = W. End above fence 0.4 in Alley

T.P. 5.99 162.03 3.30 156.04

4+04 = E. End. garage on s. emt floor 5.6 Back

N-1 lawn in yard	6.1	155.9
N	5.9	156.1
φ	6.0	156.0
S	5.7	156.3

+2.2 N edge emt. apron 5.51 156.52

+5.6 floor 4.79 157.24

4+19 = W. End above garage 5.8 Back

S - 5.8 floor 4.76 157.27

S - 2.4 emt apron 5.48 156.55

162.03

Alley Bk. Plumosa Park

41

S	5.6	156.4
φ	5.6	156.4
N	5.8	156.2

4+40

N	6.3	155.7
φ	6.0	156.0
S	5.8	156.2

4+75 garage on N. emt. floor 5.8 Back

S	6.6	155.4
φ	7.0	155.0
N	7.4	154.6

+5.8 floor 7.12 154.8

5+05

N	6.3	155.7
φ	5.7	156.3
S	5.4	156.6

5+37" = E. Line "T" Alley on diagonal

S	4.8	157.2
φ	4.8	157.2
N	5.0	157.0

162.03

" Alley.

S. of Line Amariliss Drive

W. Top. el. 11.04 150.99

W. pavmt 11.80 150.23

♀ " 11.87 150.16

E. " 11.89 150.14

E. ent. el. 11.17 150.86

0+00 " Alley = S. Line Amariliss Dr

E. ent. el. 11.97 151.06

E. pavmt 11.24 150.77

♀ " 11.50 150.53

W " 11.20 150.83

W. ent. el. 10.72 151.91

0+02

W 6.5 155.5

+4 7.7 154.3

♀ 8.1 153.9

E 8.0 154.0

0+06

E 7.3 154.7

♀ 6.5 155.5

162.03

131K E. Plumosa Park.

42

5.3 156.7

0+30

W 4.7 157.3

♀ 5.7 156.3

E 5.8 156.2

0+36

E 5.7 156.3

+5 5.7 156.3

♀ 4.6 157.4

W 4.4 157.6

0+42

W 4.5 157.5

♀ 4.2 157.8

+2 6.0 156.0

+7 6.0 156.0

+8 4.4 157.6

E 4.7 157.3

162.03

0+47

E 4.8 157.2

♀ 4.0 158.0

W 4.5 157.5

0+80

W 4.8 157.2

♀ 4.5 157.5

E 4.8 157.2

1+10.62 ♀ at 90° 00' from N. line E+W. Alley

E 5.0 157.0

♀ 4.9 157.1

W 5.1 156.9

1+12 ctr garage on W. ext. floor 0.3 Back

W-03 floor 5.08 156.95

1+20.2 at 90° 00' from ♀ E+W. Alley

W 4.9 157.1

♀ 5.1 156.9

E 4.8 157.2

1+30.78 ♀ at 90° 00' from S. line E+W. Alley

E 4.8 157.2

♀ 4.9 157.1

162.03

Alley BIK E. Plumosa Park

43

W 5.0 157.0

1+65

W 4.6 157.4

♀ 4.1 157.9

E 4.2 157.8

2+00

E 3.3 158.7

♀ 3.1 158.9

W 2.9 159.1

2+41.25 = N. line Lotus Drive

W 1.8 160.2

♀ 2.1 159.9

E 1.7 160.3

2+42.60 Edge pavmt

E. on ext. el. 1.47 160.59

E. pavmt 1.71 160.32

♀ " 2.09 159.94

W. " 1.95 160.18

W. ext. el. 1.65 160.38

162.03 ✓
N. el. line Lotus Drive

W.	emt. el.		1.80	160.23	
W.	parmt.		2.41	159.62	
E.	"		2.31	159.72	
E.	"		2.22	159.81	
E.	emt. el.		1.67	160.36	
T.P.	2.75	161.61 ✓	3.17	158.86 ✓	
set					s.e. lotus
B.M. Top Hydt.			1.10	160.51 ✓	Jonguit
T.P.	0.64	152.49 ✓	9.76	157.85 ✓	
T.P.	8.68	152.75 ✓	8.42	144.07 ✓	
T.P.	0.41	141.56 ✓	11.60	141.75 ✓	
T.P. B.M. B.P.	1.46	129.60 ✓	13.41	128.14 ✓	5.2.21/11.1 + chatworth 128.13
T.P.	0.27	116.68 ✓	13.19	116.41 ✓	
T.P. original B.M.			8.06	108.62 ✓	= 108.61

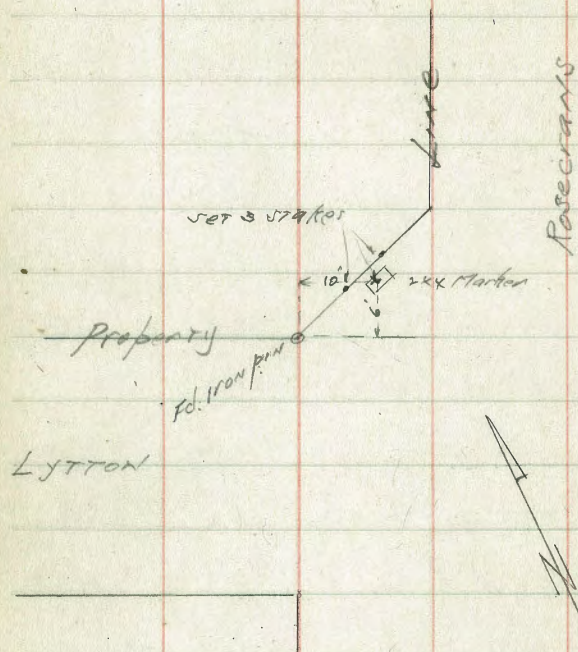
Plotted 11-16-33

Indexed
C.S.K.

Location of Playa Trail Marker

N.E. Cor. Rosecrans & Lytton

Moore
Sisson
Nashman
1/23/04



LYTTON

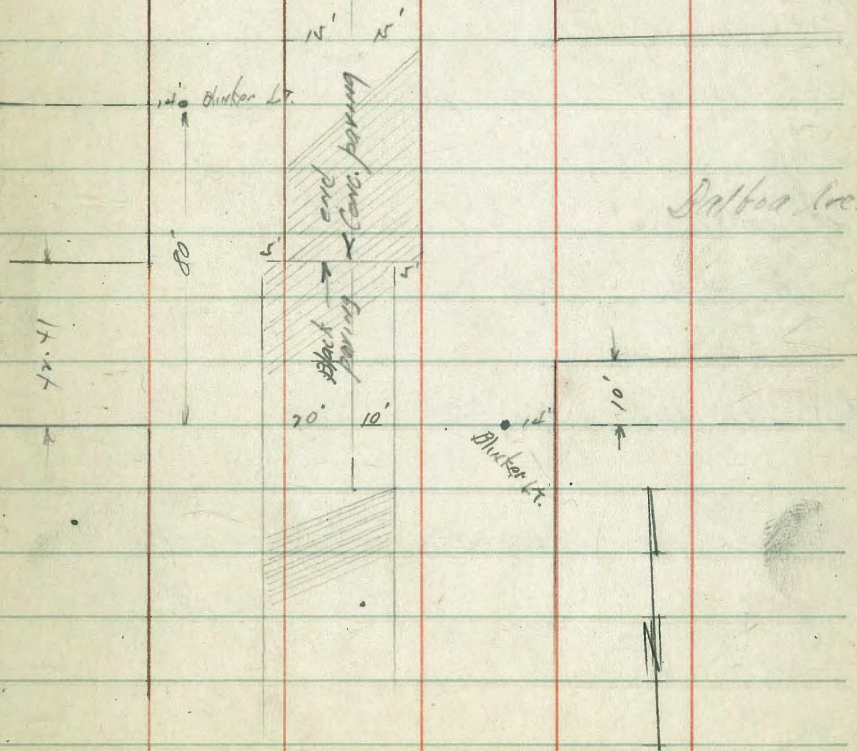
Indexed
C.S.K.

Moore
1/23/04

Location of Blinker Lights on N.W. & S.E. Cor.

Rose Cañon &
Balboa Ave.

Rose Cañon Rd.



Balboa Ave.

Check of Serra Point.

17000
Sisson
Northward
1/23/34

checked by def. + L. chords

def. $28^{\circ} 53' 37''$

L ch. 69.19 0.00 error pt. in ground

def. $7^{\circ} 15' 33''$

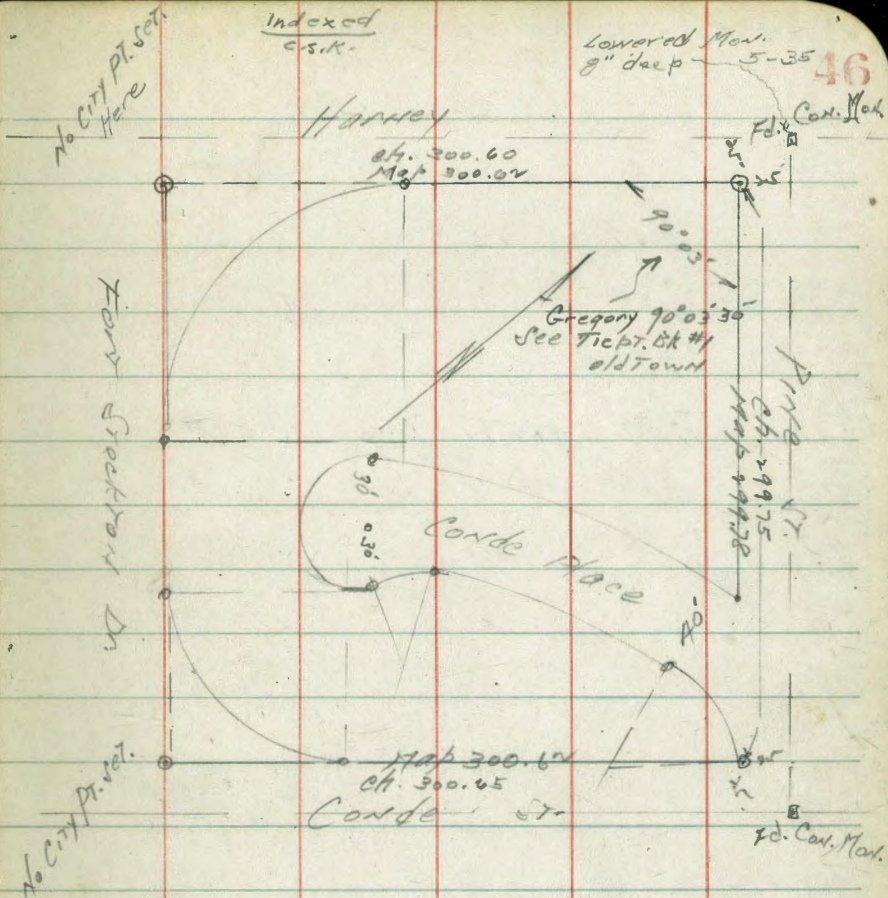
L ch. 121.41 0.00 " " " "

def. $40^{\circ} 16' 12''$

L ch. 279.1 0.01 " " " "

30 R. at end o.k.

Fd. all pipes, etc in place o.k.
C.S.K.



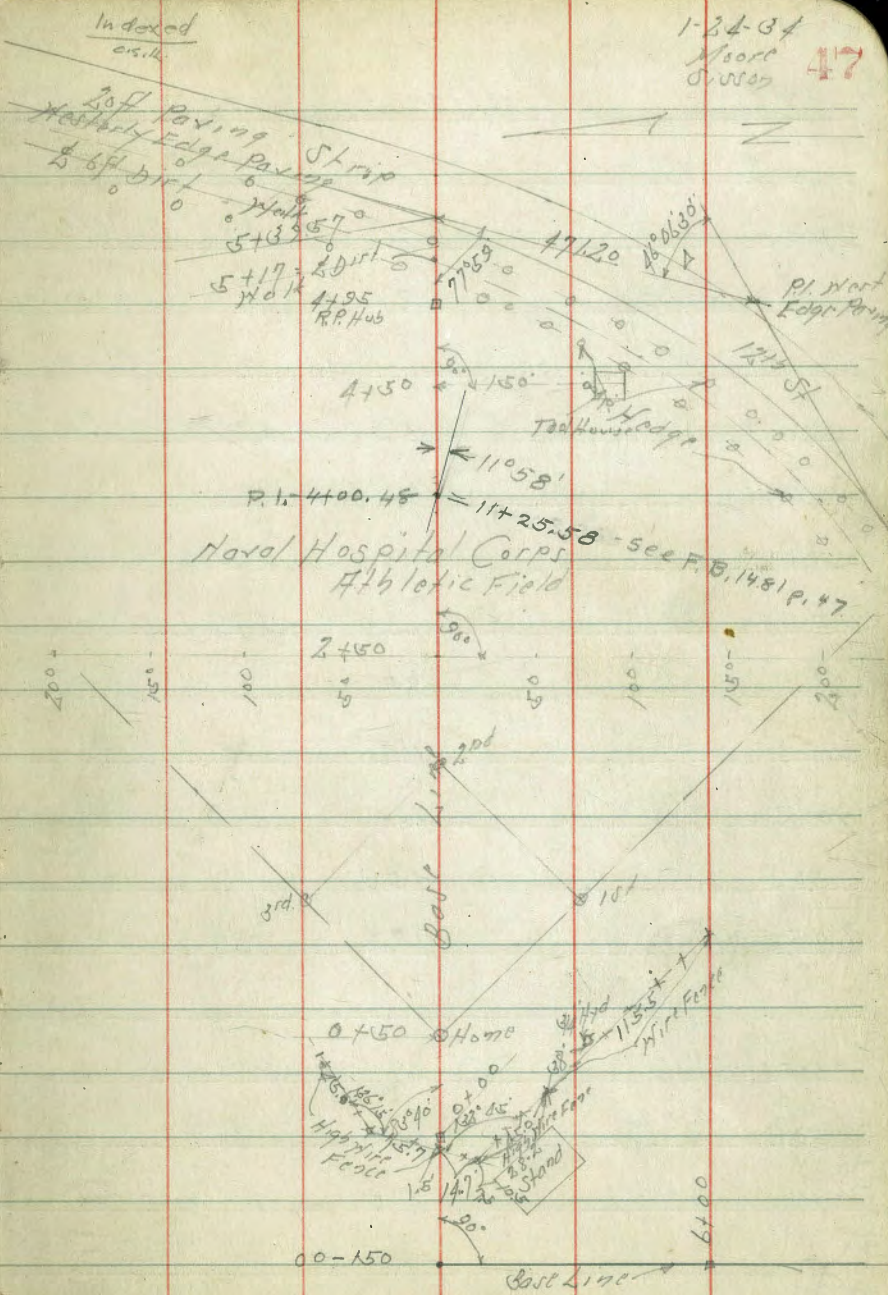
V-14-35 Moore-Sis-Northham

Conde Pl. rough graded. No Culvert drain.

Hospital Corps Athletic Field
Balboa Park

See Page 64-71

BM	11.46	116.93	105.47	NW BP H+1215H
TP	12.92	129.51	0.34	116.59
TP	12.38	141.65	0.21	129.27
TP	12.26	153.55	0.36	141.29
TP	12.42	165.74	0.23	153.32
TP	12.17	177.64	0.27	165.47
TP	12.56	190.18	0.02	177.62
TP	12.57	201.69	1.06	189.12
TP	11.63	206.85	6.47	195.22 on East Line Hub 0100
		0+50 = Home		
2		10.7		196.2
50 N = Top Canyon		10.0		196.9
50 S		12.2		194.7
75 S		13.2		193.7
		14.0		
150 S		16.2		190.7
100 S		12.3		193.6
50 S		11.5		195.4
1		10.0		196.9



206.85

50' N	8.7	198.2
100' N	7.6	199.3
125' N = Top Canyon	8.2	198.7

1+50

250' N	5.3	201.6
150' N	4.5	202.4
100' N	6.1	200.5
50' N	7.8	199.1

1/2	9.5	197.4
-----	-----	-------

50' S	11.2	195.7
-------	------	-------

100' S	13.0	193.9
--------	------	-------

150' S	15.3	191.6
--------	------	-------

175' S	17.4	189.5
--------	------	-------

2+0

200' S	18.0	188.9
--------	------	-------

150' S	14.5	192.4
--------	------	-------

100' S	12.5	194.4
--------	------	-------

50' S	10.8	196.1
-------	------	-------

1/2	9.1	197.8
-----	-----	-------

206.85

50' N	7.1	199.5
-------	-----	-------

100' N	5.7	201.2
--------	-----	-------

150' N	4.1	202.8
--------	-----	-------

200' N	3.5	203.4
--------	-----	-------

225' N = Rim Canyon	3.0	203.9
---------------------	-----	-------

2+50

250' N - Rim	2.7	204.2
--------------	-----	-------

225' N	1.7	205.2
--------	-----	-------

200' N	2.2	204.7
--------	-----	-------

150' N	3.5	203.4
--------	-----	-------

100' N	5.2	201.7
--------	-----	-------

50' N	6.9	200.0
-------	-----	-------

1/2	8.6	198.3
-----	-----	-------

50' S	10.3	196.6
-------	------	-------

100' S	11.9	195.0
--------	------	-------

150' S	13.8	193.1
--------	------	-------

200' S	16.7	190.2
--------	------	-------

250' S	19.5	187.4
--------	------	-------

206.85

310

250 S	18.3	188.6
200 S	15.5	191.4
150 S	13.2	193.6
100 S	11.6	195.3
50 S	9.8	197.1
∅	8.2	198.7
50 N	6.8	200.1
100 N	4.9	202.0
150 N	3.2	203.7
200 N	1.4	205.5
250 N = Rim Canyon	1.0	205.9

3150

290 N = Rim	1.4	205.5
250 N	0.8	206.1
200 N	1.5	205.4
150 N	3.6	203.3
100 N	4.8	202.1
50 N	6.8	200.1

206.85

∅

50 S	8.1	198.8
100 S	9.4	197.5
150 S	11.2	195.7
200 S	13.0	193.9
250 S	15.9	191.0
∅	17.8	189.1

410

250 S	17.9	189.0
200 S	15.4	191.5
150 S	13.4	193.5
100 S	11.2	195.7
50 S	9.4	197.5
∅	8.0	198.9
50 N	6.6	200.3
100 N	4.6	202.3
150 N	2.6	204.3
200 N	1.5	205.4
250 N	0.4	207.3
300 N = Rim of Canyon	0.5	207.4

206.85

+150

300H - Rim Canyon +2.5 209.4

250H +0.5 207.4

200H 0.3 206.6

150H 2.0 204.9

100H 4.3 202.6

50H 6.1 200.8

1/2 8.0 198.9

50'S 10.6 196.3

100'S 12.1 194.8

150'S 14.0 192.9

+95 = RP on Baseline

1/2 8.09 198.76

02 RP 163

70' wide
20' chs
7.5' hgs. X Sec. 4th Ave.
University to Washington

2-23-24
Miller
Walker
Bliss

292.13

index
C.S.K.

51

B.M.B.P.	7.57	292.09	284.52	N.W. 3 rd + Univ. Ave	1/4 pavmt	5.30	286.83
F.P. Fire Hydr.	2.23	292.13	289.90	S.E. 4 th + Univ. Ave	ch "	5.25	286.88
		17' S. of N. line Univ.			+10 "	5.16	286.97
E. - pavmt.		4.92	287.21		+10 cmt. ch	4.63	287.50
+10 "		4.96	287.17		E " "	4.62	287.51
+20 = ch. line		5.03	287.10		E. gutter	5.18	286.95
1/4 "		5.05	287.08	Tel. Co M.H.	E+10 "	5.13	287.00
1/4 Pavmt.		5.08	287.05				
1/4 "		5.20	286.93		0+00 = N. line Univ. Ave		
ch "		5.24	286.89		E. - cmt. walk	4.39	287.74
+10		5.36	286.77		+4.17 = E. edge cmt. walk	4.41	287.72
W		5.42	286.71		+9.5 = W. " " "	4.49	287.64
		10' S. of N. line Univ = N. ch. line			ch	4.62	287.51
W-5 gutter		5.89	286.24		gutter	5.18	286.95
W. gutter		5.84	286.29		1/4	5.07	287.06
W, cmt. ch		5.13	287.00		1/4	5.05	287.08
+10 " "		5.13	287.00		W	5.21	286.92
+10. gutter		5.72	286.41		gutter	5.54	286.59
ch pay		5.52	286.61		ch	5.14	286.99
1/4 "		5.42	286.71		+2.0 6 th light.		
1/4 "		5.35	286.78		+10.67 = E. edge cmt. walk	4.90	287.23
					W. W " " "	4.75	287.38

Walk on W. side
to W. line.

292.13

0+01

R. 8 E. of E. ch Elec Pole

0+10

W. on em t. walk	4.76	287.37
+ 9.33 E. edge walk	4.93	287.20
ch	5.08	287.05
gutter	5.64	286.49
"	5.03	287.10
ch	4.88	287.25
"	4.94	287.19
gutter	5.19	286.94
ch	4.66	287.47
+ 10.5 W. edge walk	4.49	287.64
+ 15.83 E " "	4.42	287.71
E	4.3	287.8
	0+25	
E	4.4	287.7
+ 4.17 E walk	4.43	287.70
+ 9.5 " "	4.46	287.67
ch	4.63	287.50
gutter	5.13	287.00

292.13

4th Ave

52

"	4.83	287.30
ch	4.77	287.36
"	5.02	287.11
gutter	5.52	286.61
ch	5.05	287.08
+ 10.67 E. walk	4.85	287.28
W. W "	4.71	287.42
	0+49	
	Water service on W.	
	0+49.5	
	Water service on E.	
	0+50	
W. - W walk	4.72	287.41
+ 7.33 E. walk	4.83	287.30
ch	4.97	287.16
gutter	5.42	286.71
ch	4.92	287.11
ch	4.71	287.42
"	4.79	287.34
gutter	5.14	286.99

292.13
0+50 (con)

ch.	4.56	287.57
+5.7 Cocos. Palm.		
+10.5 - W. Walk	4.39	287.74
+15.83 - E. "	4.34	287.79
E	4.3	287.8
	0+63	
Street Lamp Post on E.		
	0+22.5	
8' W. of End Tot. M.H.	4.78	287.35
	0+75	
E	4.2	287.9
+4.17 = E. Walks	4.27	287.86
+9.5 = W. "	4.33	287.80
gutter in Drive	4.95	287.18
+1	5.02	287.11
1/4	4.60	287.53
1/4	4.51	287.62
1/4	4.80	287.38
gutter	5.36	286.77
ent. ch.	4.90	287.23
+10.67 = E. Walk	4.77	287.36
W. on "	4.60	287.53

292.13
1+00

4th Ave
53

W. on walk	4.40	287.73
+9.33 = E. Walks	4.60	287.53
ent. ch.	4.79	287.34
gutter	5.27	286.86
1/4	4.77	287.36
1/4	4.54	287.59
1/4	4.65	287.48
gutter	4.98	287.15
ent. ch.	4.39	287.84
+5.5 Cocos. Palm.		
+10.5 W. Walk	4.28	287.85
+15.83 E. "	4.22	287.91
E.	4.2	287.9
1+09 1/2 = S. End. full width walk on E.		
E. ch.	4.40	287.73
+10.5 = W. walk to S	4.26	287.87
+15.83 = E. " " " "	4.15	287.98
E. on walk to N	4.04	288.09

292.13

1+14

Water service on E.

1+25

E. = E. edge walk 3.97 288.16

+ 4.17 " 4.06 288.07

+ 9.5 " 4.19 287.94

ch. 4.33 287.80

gutter 4.87 287.26

" 4.62 287.57

¢ 4.42 287.71

" 4.66 287.47

gutter 5.20 286.93

emt. ch. 4.73 287.40

+ 2. Street Light

+ 10.67 = E. emt. walk 4.56 287.57

W = W " " 4.37 287.76

T.P. 6.13 293.73 4.52 287.61

1+49

Water services on E & W.

1+49^E

5.5 E of E. ch. Cocos Palm.

293.73

1+50

W. - W. walk 5.97 287.76

+ 9.33 = E. " 6.07 287.66

ch 6.21 287.52

gutter 6.75 286.98

" 6.19 286.54

¢ 6.03 287.70

" 6.08 287.65

gutter 6.53 287.20

ch 5.83 287.90

+ 10.5 on walk 5.70 288.03

+ 15.83 " " 5.57 288.16

E " " 5.45 288.28

1+59^E = N. End. full width walk on W. & E.

E. - N. End walk 5.43 288.30

+ 4.17 = E. walk to X 5.59 288.14

+ 9.5 W. " " 5.67 288.06

ch. 5.85 287.88

gutter 6.46 287.27

" on Top, M.H. 5.97 287.76

¢ 5.98 287.95

4th Ave

54

293.73
1+59⁵ (con)

1/4		6.20	287.53
gutter		6.70	287.03
cb		6.18	287.55
+ 10.67 - E. walk		6.05	287.68
+ 16. - W. "		5.98	287.75
W. N. end walk		5.95	287.78
		1+61.5	
Water service on E.			
		1+75	
W.		5.8	287.9
+ 4 - W. walk		5.91	287.82
+ 9.33 E. "		5.98	287.75
cb		6.16	287.57
gutter		6.64	287.09
1/4		6.17	287.56
+		5.89	287.84
1/4		6.04	287.69
gutter		6.41	287.32
cb		5.84	287.89
+ 10.5 = W. walk		5.65	288.08

293.73

4th Ave

55

+ 15.83 - E. walk		5.53	288.20
E.		5.4	288.3
		1+90	
2' E. of E. cb. St. Lamp.			
		1+99	
5.5 E. of E. cb. Cocos. Palm.			
		2+00	
E.		5.2	288.5
+ 4.17 = E. Walks		5.42	288.31
+ 9.5 = W. "		5.52	288.21
cb		5.72	288.01
gutter		6.31	287.42
1/4		5.91	287.82
+		5.82	287.91
1/4		6.02	287.71
gutter		6.64	287.09
cb		6.10	287.63
+ 10.67 E. Walk		5.85	287.88
+ 16. = W. "		5.74	287.99
W.		5.6	288.1

293.73

2+04

Water service on W.

2+25

W.	5.4	288.3
+4 = W. walk	5.76	287.97
+9.33 = E. "	5.80	287.93
cl	6.00	287.73
gutter	6.54	287.19
"4	6.00	287.73
⊥	5.67	288.06
"4	5.86	287.87
gutter	6.24	287.49
cl	5.70	288.03
+10.5 = W. walk	5.52	288.21
+15.83 = E. "	5.43	288.30
E	5.2	289.5

2+32

Water service on E.

2+40

Water service on W.

293.73

2+49

5.5 E. of E. cl cocos. Palm.

2+50

E.	5.1	288.6
+4.17 = E. walk	5.34	288.39
+9.5 = W. "	5.40	288.33
cl	5.50	288.23
gutter	6.13	287.60
"4	5.76	287.97
⊥	5.60	288.13
"4	5.83	287.90
gutter	6.47	287.36
cl	5.84	287.89
+10.67 = E. walk	5.70	288.03
+16 = W. "	5.66	288.07
W.	5.5	288.2

2+52

2' W. of W. cl. = St. Lamp

2+75

W.	5.3	288.4
+4 = W. walk	5.61	288.12

4th Ave

56

293.73
2+75 (con)

+ 9.33 = E. Walk	5.68	288.05
el	5.75	287.98
gutter	6.27	287.46
"4	5.75	287.98
el	5.53	288.20
"4	5.72	288.01
gutter	6.04	287.69
el	5.54	288.19
+ 10.5 = W. walk	5.32	288.41
+ 15.83 = E. walk	5.28	288.45
E.	5.0	288.7

2+84

Water service on E.

2+89⁵

Water service on W.

2+99

5.5 E. of E. el. Cocon Palm.

3+00

E	5.0	288.7
+ 4.17 = E. Walk	5.22	288.51

293.73

4th Ave

57

+ 9.5 = W. Walk	5.29	288.44
el	5.47	288.26
gutter	6.00	287.73
"4	5.66	288.07
el	5.41	288.32
"4	5.63	288.10
gutter	6.20	287.53
el	5.66	288.07
5.5 W. of W. el. = Cocon Palm.		
+ 10.67 = E. Walk	5.49	288.24
+ 16. = W. "	5.49	288.24
W.	5.3	288.4

3+11⁵

2' E. of E. el. = St. Lamp.

3+18⁵

Water service on E.

3+25

W	5.3	288.4
+ 4 = W. Walk	5.42	288.31
+ 9.33 = E. "	5.45	288.28

293.73

3+25 (cont)

el	5.58	288.15
gutter	6.11	287.62
"4	5.59	288.14
⊕	5.41	288.22
"4	5.61	288.12
gutter	5.93	287.80
el	5.42	288.31
+10.5 = w. walk	5.22	288.51
+15.83 = e. "	5.15	288.58
E	4.8	288.9

3+44⁵

Water service on W.

T.P. 5.40 294.10 5.03 288.70

3+49

5.5 E of E. cl = Cocos. Palm.

3+50

E	5.3	288.8
+4.17 = E. walk	5.46	288.64
+9.50 = W. "	5.52	288.58
el	5.70	288.40

294.16

4th Ave

58

gutter	6.24	287.86
"4	5.84	288.26
⊕	5.68	288.42
"4	5.89	288.21
gutter	6.43	287.67
el	5.84	288.26
+10.67 = e. walk	5.65	288.45
+16 = w. "	5.62	288.48
W.	5.6	288.5

3+74

2. W. of W. cl. = street lamp.

3+75

W.	5.4	288.7
+4 = w. walk	5.61	288.49
+9.33 = e. walk	5.61	288.49
el	5.79	288.31
gutter	6.27	287.83
"4	5.77	288.33
⊕	5.63	288.47
"4	5.81	288.29

294.10

3775 (con)

gutter	6.19	287.91
el.	5.63	288.47
+ 10.5 = W. side Walk	5.47	288.63
+ 15.83 = E. " "	5.40	288.70
E.	5.1	289.0

37855

Water service on E

3790

Water service on W.

3799

5.5 E. of E. el. Cocon palm.

4700

E	5.2	288.9
+ 4.17 = E. Walk	5.29	288.51
+ 9.5 = W. "	5.37	288.73
el.	5.58	288.52
gutter	6.11	287.99
1/4	5.67	288.43
1/4	5.47	288.63
1/4	5.67	288.43

29410

4th Ave

59

gutter	6.27	287.83
el.	5.70	288.40
+ 10.67 = E. Walk	5.50	288.60
+ 16' = W. "	5.46	288.64
W.	5.3	288.8

47195

Water service on E.

4725

W.	5.1	289.0
+ 4' = W. Walk	5.38	288.72
+ 9.33 = E. "	5.46	288.64
el.	5.60	288.50
gutter	6.12	287.98
1/4	5.58	288.52
1/4	5.37	288.73
1/4	5.61	288.49
gutter	6.07	288.03
el.	5.56	288.54
+ 10.5 = W. Walk	5.30	288.80
+ 15.83 = E. "	5.22	288.88
E.	5.0	289.1

294.10

4+35.5

2' E. of E. cl. = Street Lamp

Water Service on W.

4+49

5.5 W. of W. cl. Cocos Palm.

4+50

E. 4.9 289.2

+4.17 = E. Walk 5.15 288.95

+9.5 = W. " 5.29 288.81

cl 5.44 288.66

gutter 5.97 288.13

" 5.57 288.53

ϕ 5.39 288.71

" 5.60 288.50

gutter 6.04 288.06

cl 5.50 288.60

+10.67 = E. Walk 5.32 288.78

+16.1 = W. Walk 5.28 288.82

W. 5.2 288.9

4+71

5.5 E. of E. cl. = Cocos Palm.

294.10

4+72

5.5 W. of W. cl. = Cocos Palm.

4+75

W. 5.1 289.0

+4' = W. Walk 5.29 288.81

+9.33 = E. Walk 5.35 288.75

cl 5.43 288.67

gutter 6.04 288.06

" 5.50 288.60

ϕ 5.32 288.78

" 5.50 288.60

gutter 5.94 288.16

cl 5.36 288.74

+10.5 = W. Walk 5.20 288.90

+15.83 = E. Walk 5.15 288.95

E. 5.0 289.1

4+81.2

Water Service on W.

4+97.5

2' W. of W. cl. Street Lamp Post.

4th Ave

60

294.10
5700

E.	4.9	289.2
+4.17 = E. walk	5.07	289.03
+9.5 = W. "	5.16	288.94
cl	5.26	288.84
gutter	5.89	288.21
ly	5.44	288.66
cl	5.32	288.78
ly	5.44	288.66
gutter	5.88	288.22
cl	5.35	288.75
+5.5 = Cocos Palm.		
+10.67 = E. walk	5.16	288.94
+16. = W. "	5.16	288.94
W.	5.1	289.0

5702

Water service on E.

5706

5.5 E. of E. cl. Cocos Palm.

57196

Water service on W.

294.10

4th Ave

5725 = S. End. Drive to oil station on W.

61

W.	5.0	289.1
+4. = W. walk	5.05	289.05
+9.33 = E. "	5.12	288.98
cl	5.27	288.83
gutter	5.81	288.29
ly	5.34	288.76
cl	5.21	288.89
ly	5.32	288.78
gutter	5.75	288.35
cl	5.21	288.89
+10.5 = W. walk	5.07	289.03
+15.83 = E. "	5.00	289.10
E	4.7	289.4

5733⁵

Water service on E

5747

E.	4.7	289.4
+4.17 = E. walk	4.92	289.18
+9.5 = W. "	4.98	289.12
cl.	5.15	288.95

294.10

5447 (con)

gutter	5.68	288.42
"	5.25	288.85
☐	5.09	289.01
"	5.35	288.75
gutter in drive	5.73	288.37
+10.67 = E. Walk	5.03	289.07
+16' = W. "	4.97	289.15
W.	4.9	289.2

5450

5.5 E. of E. ch. = Cocos Palm

5451

2' E. of E. ch. = Street Lamp Post

5456⁵

1' E. of E. ch. = Fire Hyd. T.

5459² = S. Line Washington St.

W.	4.9	289.2
+4 = W. Walk To S.	4.91	289.19
+9.33 = E. Walk " "	4.92	289.18
ch.	5.14	288.96
gutter	5.67	288.43

294.10

4th Ave.

62

"	5.42	288.68
☐	5.15	288.95
"	5.27	288.83
gutter	5.65	288.45
ch.	5.16	288.94
+10.5 = W. Walk To S.	4.96	289.14
+15.83 = E. " " "	4.88	289.22
E.	4.8	289.3

10' N = S. ch. Line Washington St

E-10 gutter	5.81	288.29
E "	5.75	288.35
E. ent. ch	5.10	289.00
+10 " "	5.14	288.96
+10 gutter	5.66	288.44
E ch. Line	5.41	288.69
"	5.19	288.91
☐	5.15	288.95
"	5.24	288.82
W. ch. Line	5.46	288.64

294.10

5. ch. Washington (con)

W. ch +10	gutter	5.66	288.44
" +10	emt ch	5.12	288.98
W	" "	5.12	288.98
W	gutter	5.72	288.38
+10	"	5.81	288.29

7. N. of 5. ch. line

W -10		5.50	288.60
W		5.48	288.22
+10		5.43	288.67
ch line		5.31	288.79
14		5.22	288.88
Φ		5.09	289.01
14		5.12	288.98
ch. line		5.15	288.95
+10		5.29	288.81
E		5.34	288.76
+10		5.44	288.66

294.10

12.5 N. of 5. ch. = 5.

E		5.11	
ch		4.99	289.11
Φ		5.00	289.10
ch		5.07	288.03
W		5.17	288.93
B.M.B.P.		5.08	289.02

4th Ave

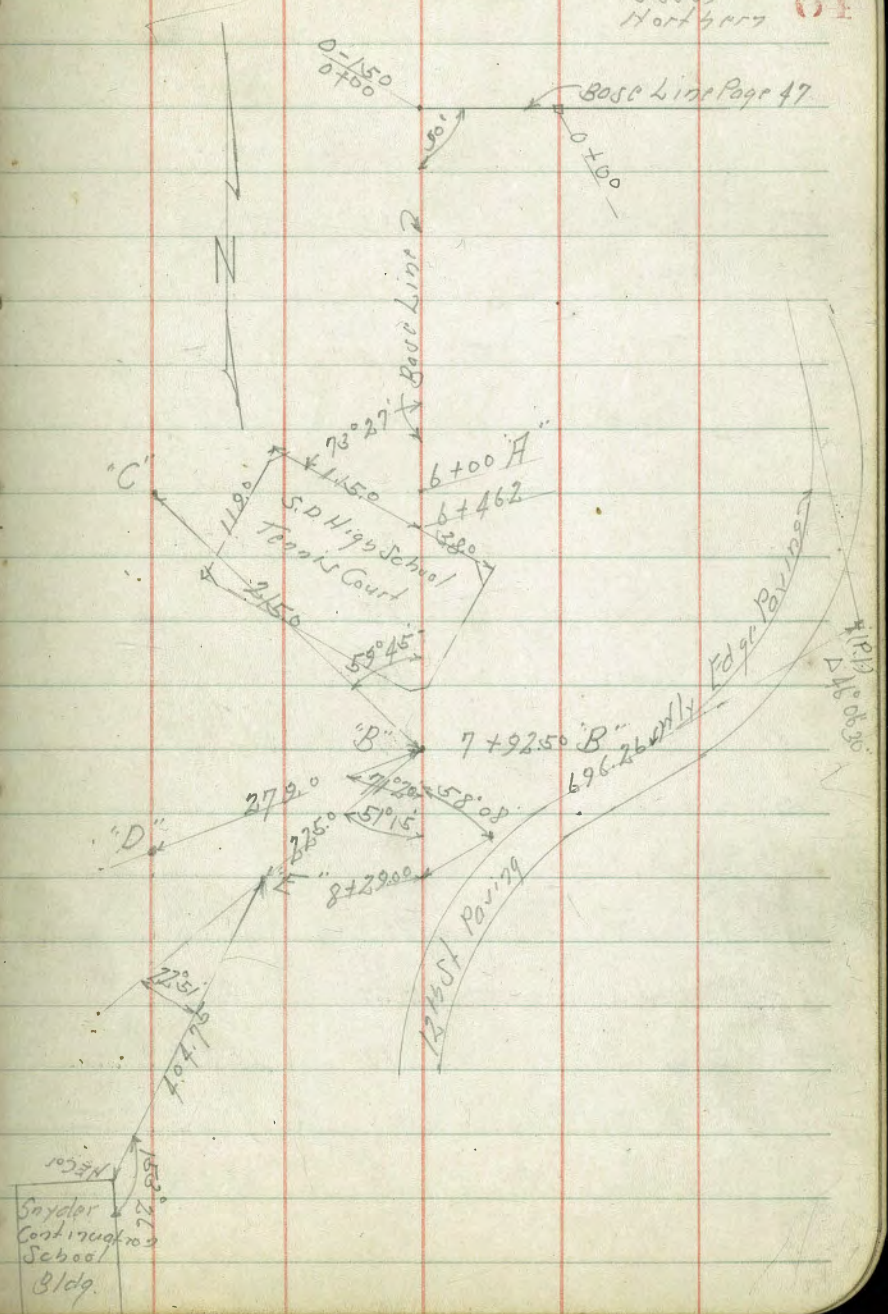
63

N.W. 4th Ave
Washington
289.01

Topog. North of Snyder Continuing School
 And Hospital Corps Athletic Field
 Balboa Park

5-5-34
 Moore
 Sisco
 North 61

See Sketch Page 47



Topog. Hospital Corps Athletic Field
Balboa Park

See Page 47-50

Hub 0.100
Base Line
Page 17

BM 0.34- 195.56 195.22

TP 0.10 182.72 12.94 182.62

TP 0.52 170.26 12.98 169.74

TP 1.05 159.48 11.83 158.43

0-450

50'S of Base Line 20.4 129.1

100'S " " " 19.2 140.3

150'S " " " 9.5 150.0

200'S " " " 12.2 147.3

250'S " " " 16.7 142.8

300'S " " " 21.2 138.3

350'S " " " 26.5 133.0

0-400

350'S of Base Line 21.2 138.3

300'S " " " 15.7 143.8

250'S " " " 9.2 150.3

200'S " " " 5.9 153.6

150'S " " " 4.9 154.6

100'S " " " 7.3 152.2

159.48

75'S of Base Line 10.7 148.8

50'S " " " 17.7 143.8

0-350

50'S of Base Line 7.1 152.4

100'S " " " 0.4 159.1

TP 12.49 170.92 1.05 158.43

150'S of Base Line 10.2 160.7

200'S " " " 12.3 158.6

250'S " " " 15.6 155.3

300'S " " " 21.2 149.7

350'S " " " 28.7 142.5

0-300

350'S of Base Line 26.0 144.9

300'S " " " 17.0 153.9

250'S " " " 10.7 160.2

200'S " " " 6.2 164.7

150'S " " " 3.1 167.8

100'S " " " 3.5 167.4

50'S " " " 11.8 159.1

5-5-34
Maori
Sings
Northern 65

170.92

0-250

Base Line	7.2	163.7
TP 1243	182.17	118
50 S of Base Line	11.2	171.0
75 S " " "	7.6	174.6
100 S " " "	7.6	174.6
150 S " " "	8.5	173.7
200 S " " "	11.8	170.4
250 S " " "	18.7	163.5
300 S " " "	25.5	156.7

0-200

300 S of Base Line	22.5	159.7
250 S " " "	15.1	167.1
200 S " " "	7.1	175.1
150 S " " "	1.1	181.1
100 S " " "	0.5	181.7
50 S " " "	1.4	180.8
B.L.	8.5	173.7
50 N of Base Line	20.6	161.6

TP 1260 19446 0(3) 181.86

194.46

0-150

50 N of Base Line	22.7	171.8
Base Line	12.2	182.3
50 S of Base Line	7.2	187.3
100 S " " "	6.9	187.6
150 S " " "	8.9	185.6
200 S " " "	15.5	179.0
250 S " " "	22.5	172.0
300 S " " "	32.8	161.7

0-100

300 S of Base Line	29.8	164.7
250 S " " "	21.5	173.0
200 S " " "	14.1	180.4
150 S " " "	7.0	187.5
100 S " " "	5.4	189.1
50 S " " "	4.5	190.0
Base Line	5.3	189.2
50 N of Base Line	12.9	181.6
100 N " " "	20.5	174.0

157

66

191.46

0-50

150 N of Base Line	19.3	175.2
100 N " " "	11.8	182.7
50 N " " "	5.5	189.0
Baseline	2.3	192.2
50 S of Base Line	2.8	191.7
100 S " " "	3.8	190.7
150 S " " "	6.3	188.2
200 S " " "	13.1	181.4
TP 160 183.56 ✓	12.50	181.96
250 S of Base Line	9.2	174.4
300 S " " "	16.5	167.1
	0+00	
300 S of Base Line	17.0	166.6
250 S " " "	9.1	174.5
200 S " " "	2.2	181.4
150 S " " "	7.8	186.4
100 S " " "	7.1	189.7

183.56

0+50

150 S of Base Line	7.55	189.1
200 S " " "	0.4	183.2
250 S " " "	9.3	174.3
300 S " " "	17.1	166.2
	1+0	
300 S of Base Line	17.3	169.3
250 S " " "	7.8	175.8
200 S " " "	7.0	186.6
	1+50	
220 S of Base Line	7.0	185.6
250 S " " "	3.1	180.5
300 S " " "	9.5	174.1
350 S " " "	14.5	169.1
	2+0	
350 S of Base Line	11.4	172.2
300 S " " "	6.3	177.3
250 S " " "	7.8	184.4

67

183.56

2+50

500' S of Baseline 2.9 180.7

350' S " " " 8.7 174.9

400' S " " " 11.4 172.2

3+0

400' S of Baseline 6.3 177.3

350' S " " " 3.7 179.9

300' S " " " 1.8 181.8

TP 11.72 193.45 1.83 181.73

3+50

300' S of Baseline 7.4 186.1

350' S " " " 9.3 184.2

390' S " " " 9.7 183.8
= 1/4 Edge Hedge

4+0

300' S of BL = Hedge 6.1 187.4

4+20

250' S of BL = Hedge 3.8 189.7

TP 11.86 203.73 1.58 191.87

BM 1.95 198.78

0.2 RP/115
1+95
Paper
19876

BM	6.93 -	202.15	195.22
		0+0	
50' N of Baseline		8.6	193.6
100' N " " "		12.7	188.5
150' N " " "		19.3	182.9
200' N " " "		26.9	175.3
		0+50	
50' N of Baseline		6.4	195.8
100' N " " "		9.4	192.8
150' N " " "		15.8	186.4
200' N " " "		25.1	177.1
		1+0	
150' N of Baseline		3.7	199.8
200' N " " "		8.1	194.1
250' N " " "		15.5	186.7
300' N " " "		25.2	177.0
		1+50	
250' N of Baseline		6.0	196.2
300' N of " " "		13.9	188.3

Hub to
Baseline
Page 47

	202.15		5-734
350' N of Baseline	26.0		176.2
	2+0		
250' N of Baseline	0.3		201.9
300' N " " "	7.3		194.9
350' N " " "	12.8		182.4
TP	12.79	207.79	7.15
		2+50	195.00
300' N of Baseline	10.2		197.6
350' N " " "	22.2		185.6
		3+0	
300' N of Baseline	7.2		200.5
350' N " " "	19.5		188.3
400' N " " "	35.3		172.5
		3+50	185
			181
			172
350' N of Baseline	11.4		196.4
400' N " " "	21.4		186.4
450' N " " "	36.2		171.6
		4+0	
350' N of Baseline	1.8		206.0
400' N " " "	10.8		197.0

207.79

450 H of Baseline 26.0 181.8

4+50

350 H of Baseline +28 210.6

400 H " " " 2.7 205.1

150 H " " " 14.7 193.1

500 H " " " 26.7 181.1

TP 10.19 217.85 0.13 207.66

5+0

100 H of Baseline 14.7 203.2

150 H " " " 13.4 204.5

200 H " " " 12.0 205.9

250 H " " " 10.2 207.7

300 H " " " 8.6 209.3

350 H " " " 7.6 210.3

400 H " " " 8.5 209.4

450 H " " " 14.8 203.1

500 H " " " 23.6 194.3

5+50

270 H - Hedge 10.3 207.6

300 H " " " 8.6 209.3

217.85

350 H of B.L. 6.9 211.0

400 H " " " 5.4 212.5

450 H " " " 6.3 211.6

500 H " " " 6.4 211.5

550 H " " " 9.5 208.4

600 H " " " 18.3 199.6

650 H " " " 22.5 195.4

5+80

350 H of B.L. - Hedge 7.2 210.7

5+90

400 H of B.L. - Hedge 5.3 212.6

6+03

450 H of B.L. - Hedge 4.5 213.4

6+14

500 H of B.L. - Hedge 3.9 214.6

6+25

550 H of B.L. - Hedge 3.0 214.9

6+0

600 H of B.L. 5.1 212.3

650 H " " " 12.3 205.6

70

2.7

9.5

217.85

6+46

600 H of BL - Hedge

2.0

215.9

6+50

650 H of BL

3.1

214.8

700 H " " "

10.8

207.1

6+63

650 H of BL - Hedge

1.9

216.0

6+90

700 H of BL - Hedge

2.1

215.8

TP 0.50 206.00 12.35 205.50

TP 0.04 193.29 12.75 193.25

TP 0.39 181.25 12.43 180.86

TP 0.21 168.67 12.79 168.46

"A" 9.0 159.7

"B" - My Hedge Hedge 9.6 159.1

TP 1.12 159.58 10.21 158.46

"C" 2.7 156.9

"D" 7.2 152.4

"E" 5.2 154.4

TP 0.92 147.67 12.83 146.75

147.67

TP 0.13 134.87 12.93 134.74

TP 0.37 122.50 12.74 122.13

TP 4.30 117.06 9.74 112.76

TP 2.82 114.42 5.46 111.60

BM 8.91 105.51

N.M.B.P

A+12/1/12
10547

71

Topog. North of Snyder Continuation School.
Balboa Park

No	Az.	Vert. Δ	Notes: - Az. Clockwise	
			Elev. A. 159.7	Hor. Dist.
✓ 1	120° 07'	H. B. S. 07-150 322° 16'	-4° 20'	287.3'
✓ 2	34° 10'		-4° 40'	232.4'
✓ 3	360° 00'		-3° 30'	217.2'
✓ 4	20° 50'		-3° 36'	211.2'
✓ 5	39° 54'		-2° 58'	258.4'
✓ 6	54° 07'		-0° 40'	299.0'
✓ 7	61° 06'		-0° 10'	385.0'
✓ 8	70° 05'		-0° 40'	340.0'
✓ 9	62° 45'		-4° 20'	250.6'
✓ 10	50° 03'		-7° 38'	175.0'
✓ 11	34° 00'		-8° 15'	249.5'
✓ 12	344° 22'		-14° 55'	119.6'
✓ 13	314° 58'		-13° 00'	767'
✓ 14	296° 24'	1/4 Edge 30' Road Road Level	-10° 28'	238'
✓ 15	309° 08'		-12° 06'	167.8'
✓ 16	343° 01'		-15° 45'	91.7'
✓ 17	50° 42'		-8° 00'	113.8'
✓ 18	73° 06'		-1° 28'	216.9'
✓ 19	74° 10'		+0° 45'	320.0'

5-7-34
Notes: - See McCarty's Notes For Snyder School

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Upper	Stadia	Lower	Diff. El.	Elev.
6.43	289'	3.54	-21.77	137.9
6.16	234'	3.82	-18.94	140.8
6.10	218'	3.92	-13.28	146.4
6.06	212'	3.94	-13.28	146.4
6.30	259'	3.71	-13.39	146.3
6.48	299'	3.49	-3.48	156.2
6.90	385'	3.05	-1.12	158.6
6.77	340'	3.27	-3.96	155.7
6.26	252'	3.74	-18.94	140.8
5.88	178'	4.10	-23.44	136.3
5.78	156'?	4.22	-24.70	135.0
5.65	128'	4.37	-31.9'	127.8
5.89	176'	4.13	-38.6'	121.1
6.23	246'	3.77	-44.0	115.7
5.88	175'	4.13	-36.0	123.7
5.49	99'	4.50	-25.8	133.9
5.58	116'	4.42	-15.92	143.8
6.11	217'	3.54	-5.54	154.2
6.60	320'	3.40	+4.28	164.0

No	Inst. at A	Hgt.	Vert	Elev. "A" 159.7 Hor. Dist.	Upper	Stadia	Lower	Diff. El.	Elev.
✓20	= Hly Edge 30' Road	70°57'	+2°01'	432.5'	7.15	433'	2.82	+15.25	175.0
✓21		80°57'	+1°58'	360.6'	6.81	361'	3.20	+12.39	172.1
✓22		89°20'	+2°25'	269.6'	6.34	270'	3.64	+11.45	171.2
✓23		94°56'	+2°25'	172.7	5.80	173'	4.07	+7.23	166.9
✓24		103°18'	+3°02'	70.8	5.35	71'	4.64	+3.75	163.5
✓25		270°22'	-1°50'	65.9	5.33	66'	4.67	-2.11	157.6
✓26		280°10'	-7°28'	139.7	5.71	142'	4.29	-18.28	141.4
✓27		277°56'	-6°50'	245.5	6.26	249'	3.77	-29.41	130.3
✓28		263°37'	-1°05'	145.0'	5.73	145'	4.28	-2.74	157.0
✓29	= No. W Cor. Tennis Court	262°49'	-1°00'	110.0'	5.55	110'	4.45	-1.92	157.8
✓30	= N E " " "	147°48'	-0°20'	66.0'	5.33	66'	4.67	-0.38	159.3
✓31		128°40'	+0°35'	111.0	5.55	111'	4.44	+1.12	160.8
✓32		111°54'	+3°01'	140.6	5.71	141'	4.30	+7.41	167.1
✓33	= Hly Edge Hedge	113°46'	+2°25'	189.7	5.95	190'	4.05	+8.00	167.7
✓34	= " " "	149°18'	+1°01'	157.0'	5.78	157'	4.21	+2.79	162.5
✓35		149°00'	+0°09'	147.0'	5.74	147'	4.27	+0.38	160.1

No.	Inst. A/B B.S. on H	Hgt	Vert	Elev. "B" 159.1 Hor. Dist.	Upper	Stadia	Lower	DIFF. Elev.	Elev.
✓ 1	SFCor Tennis Court	6° 00'	-0° 40'	21.0'	5.10	21'	4.89	-0.24	158.9
✓ 2	SH "	294° 16'	-0° 40'	158.0'	5.79	158'	4.21	-1.84	157.3
✓ 3		232° 50'	-1° 26'	84.0'	5.42	84'	4.58	-2.10	157.0
✓ 4	Wly Edge Parking	203° 37'	-1° 40'	99.3	5.50	100'	4.50	-8.11	151.0
✓ 5	" "	85° 50'	-0° 50'	72.0'	5.36	72'	4.64	-1.05	158.0

No.	Inst. A/C B.S. on B	Hgt	Vert	Elev. "C" 156.9	Upper	Stadia	Lower	DIFF. Elev.	Elev.
✓ 1		182° 52'	-18° 18'	18.0'	5.10	20'	4.90	-5.95	150.9
✓ 2		182° 52'	-13° 25'	71.7'	5.38	76'	4.62	-17.2	139.7
✓ 3		182° 52'	-12° 05'	126'	5.65	132'	4.33	-27.0	129.9
✓ 4		123° 18'	-13° 04'	121.6'	5.63	128'	4.35	-28.1	128.8
✓ 5		101° 14'	-10° 20'	86.0'	5.44	89'	4.55	-15.7	141.2
✓ 6		84° 53'	-0° 45'	98'	5.50	98'	4.52	-1.31	155.6

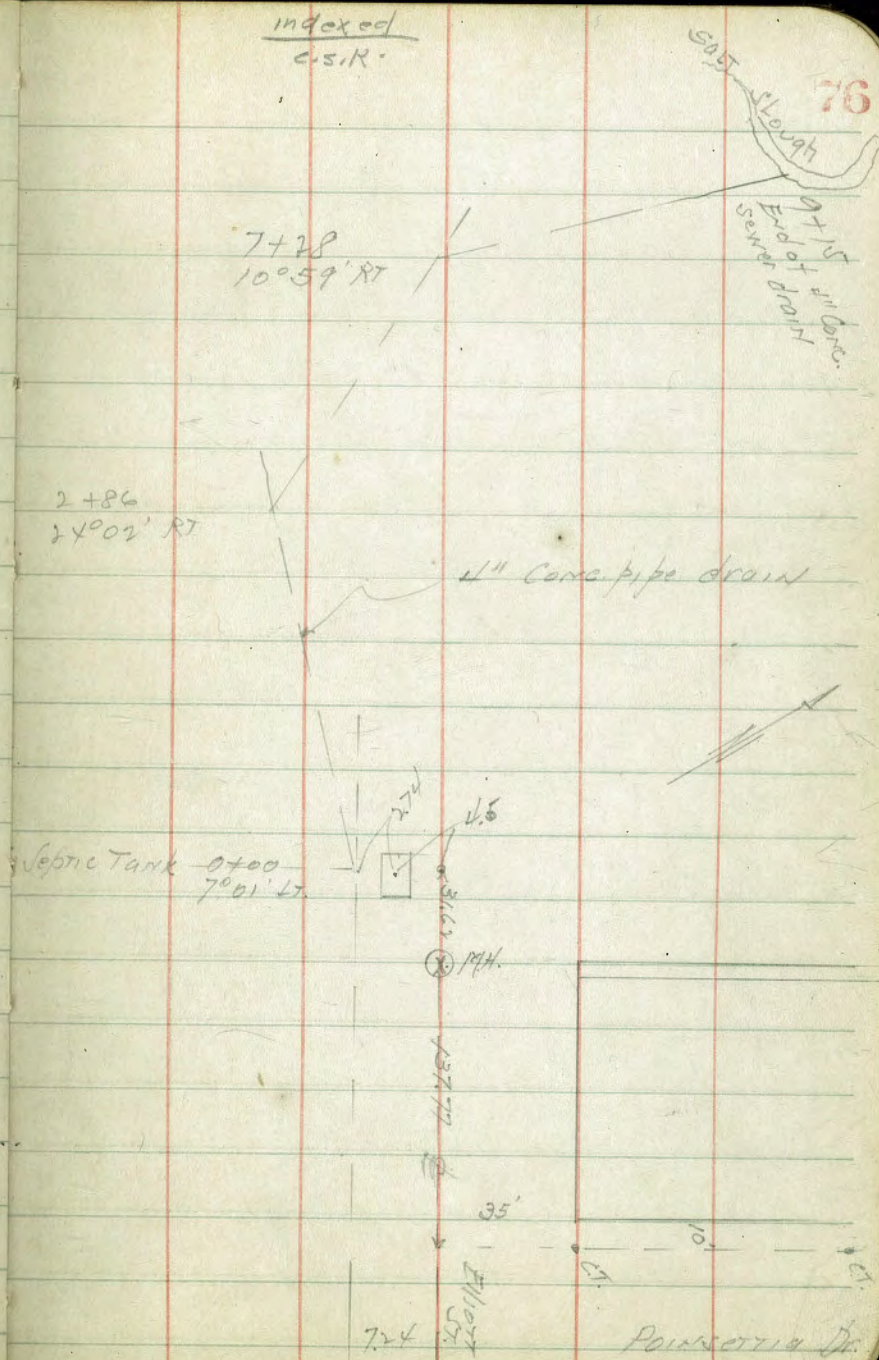
No.	Inst. A/D B.S. on B	Hgt	Vert	Elev. "D" 152.4	Upper	Stadia	Lower	DIFF. Elev.	Elev.
✓ 1		303° 20'	+0° 40'	53	5.27	53	4.74	+0.62	153.0
✓ 2		267° 45'	-18° 20'	63'	5.35	70'	4.65	-21.0	131.9
✓ 3		245° 43'	-24° 35'	82.8	5.50	100'	4.50	-37.8	114.6
✓ 4		181° 30'	-34° 10'	52'	5.38	76'	4.62	-35.3	117.1

\angle	125th A1 "D"	Azi.	Vert.	Elev. "D" 152.4 Hor. Dist.	Upper	Stadia	Lower	Diff. Elev.	Elev.
✓5		141° 44'	-20° 00'	93.6'	5.53	106'	4.47	-34.1	118.3
✓6		141° 44'	-32° 20'	50.7'	5.32	64'	4.68	-28.9	123.5
✓7		95° 35'	-16° 22'	60.8'	5.33	66'	4.67	-18.8	133.6
✓8		8° 32'	+2° 32'	49.9'	5.25	50'	4.75	+2.21	154.6

	125th A1 "E" B.S. 07 "B"			Elev. "E" 154.4'					
✓1		56° 40'	0° 00'	14'	5.07	14'	4.93	0.0	154.4
✓2		114° 25'	-11° 40'	38.3'	5.20	40'	4.80	-7.9	146.5
✓3		166° 06'	-7° 00'	84.7'	5.43	86'	4.57	-10.4	144.0
✓4		151° 54'	-4° 35'	238.5'	6.20	240'	3.80	-19.19	135.2
✓5		157° 25'	-5° 04'	244.1'	6.23	246'	3.77	-21.71	132.7

Location of Plumosa Park
 Septic Tank West of Elliott & Poinsettia
 and location of 4" Conc drain
 thru Loma Alta #2 to Salt Slough.

Moore 10-19-34



Transfer of C. + G. S. BM Serial #19
 Gran. Mon. to B.P. Swly curb Mason &
 San Diego Ave

Moore
 Sisson
 Northern

15-15-35

Indexed
 C.S.K.

77

+	π	-	el.
5.443	30.764		25.321 = Corrected

2.419 28.345 = B.P. BM
 USGS

U.S. ENGRS

el. ^ Old Town Serial #19 C + G. S. = D

Gran. Mon.
 Marked
 USGM

Swly curb return of Mason & San Diego Ave = 210'

N Ely from Gran. Mon. in front of old School in Old Town

28.345

- 6.17

8.688 30.913

22.225 = City Datum

check to SW 7' C.T. Twigg's
 San Diego Ave

223

28.683

28.802

diff. 0.117

- This el. brought from B.P. in Swly curb at

Moore & Witherby Sts.

N^o 18. Fairway & Green
Municipal Golf Course
in Balboa Park
for sprinkler system.
5-17-35
Miller
Walker
Bliss.

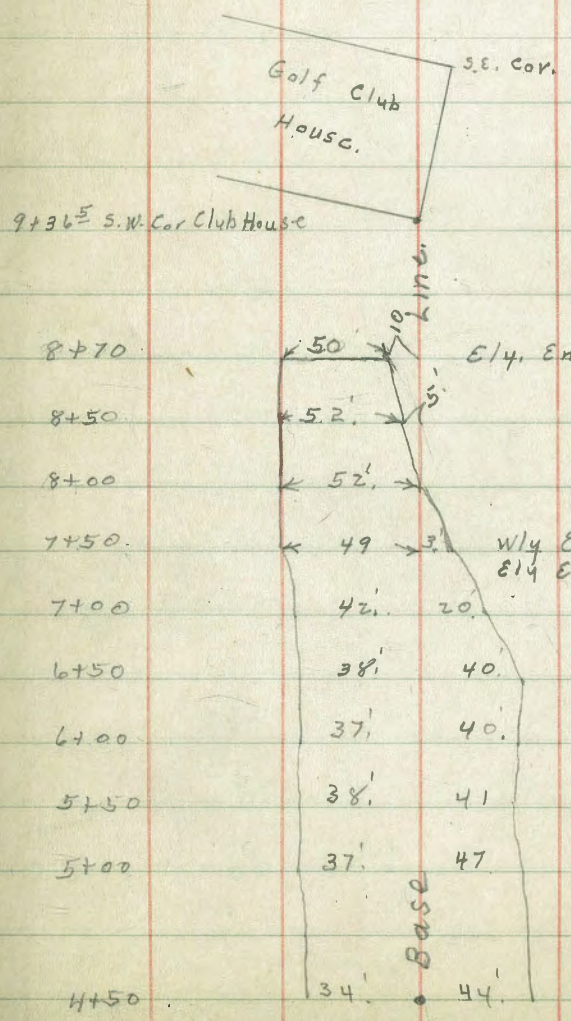
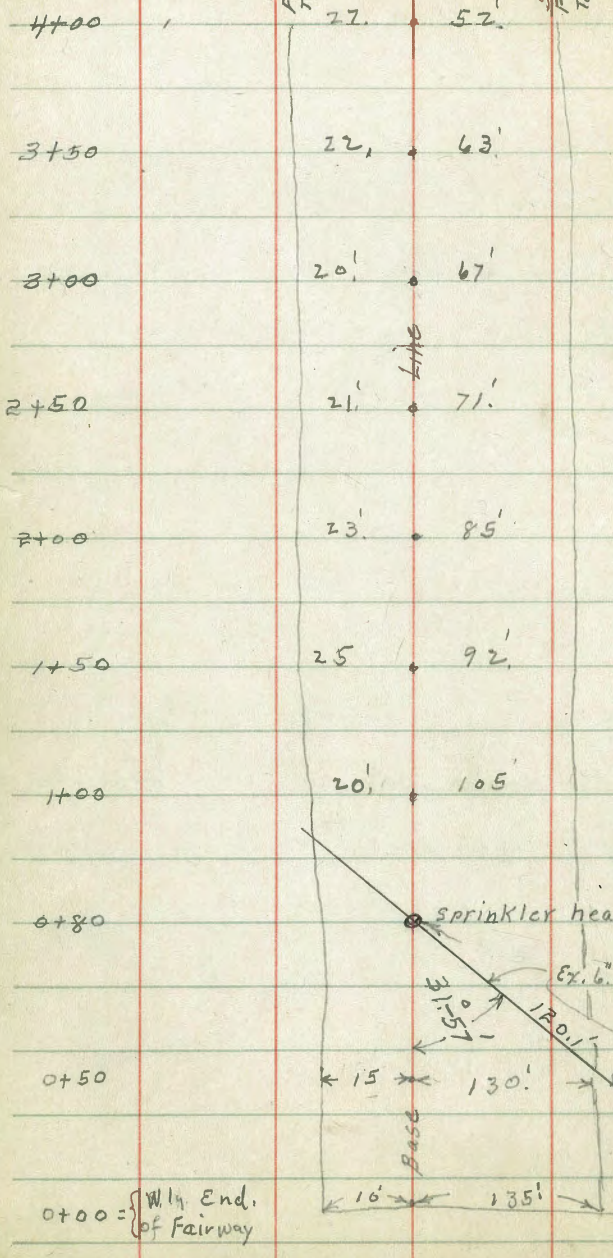
N.W. Side
Fairway &
Top slope

Indexed
C.S.K.

Sly. Edge
Fairway
Top slope

N.W. Edge
Fairway

Sly. Edge
Fairway



Indexed

CSIKI

Levels for Prop. drainage ditch
15' W of Kurtz to Taylor's
and Barnett ST ditch see 1424-29

6.38

79

Q.M. small Tel. Pole	3.50	7.17	3.07	near Kurtz Rosecrans	8.	4.1	2.2
00 = Vly Rosecrans		5.0	2.2	392 on line S. 7th St	8.50	4.5	2.1
0 + 50		5.0	1.6		9	4.4	2.0
0 + 50	JDEPT top soil abandoned	4.57	2.60		+ 50	4.5	2.1
1		5.7	1.5		10	5.8	0.6
+ 50		5.9	1.2		+ 50	5.9	0.5
2		5.2	2.0		11	6.0	0.4
4 50		5.4	2.0		+ 50	5.4	1.2
3		5.6	1.8		12	5.6	1.0
+ 50		5.1	2.1		+ 50	7.8	-1.4
4		4.5	2.6		12 + 22 bot ditch	8.7	-1.3
+ 50		4.4	2.8		30' corr.		
5		4.4	2.8		12 + 22 FL. I.P. CULV. outlet	9.0	-2.7 2
+ 50		3.8	3.3		4' LT of line		
6		4.6	2.6		put in recently by ST. Dept.		
T.P.	3.09	6.38	3.88	3.29			
+ 50		4.2	2.2				
7		4.3	2.1				
+ 50		3.9	2.5				

20.4
 20.1
 40.5

77-58

75
 94.52
 20.48

962.0
 83.5000000
 281.155
 538.50
 520770
 176800
 103590
 321.00

2+36.5

162.22

236.39
 141.29
 95.11

11° 58'

537.11
 236.39
 300.72

56.53
 906.83
 963.36
 102.22
 1125.58

10.00 2.83 7
 5.33 2.5 2.83
 4. 5.33 4.17
 20.00 10.67 5.33
 533 9.50
 16.00 10.50
 20.00

89-53-10
 5196

12.50
 5.33
 15.83
 4.17
 20.00

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

Page 21 - Elevations

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

