

1471

LEVEL BOOK

373 A

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

Tables for Excavations and Embankments.

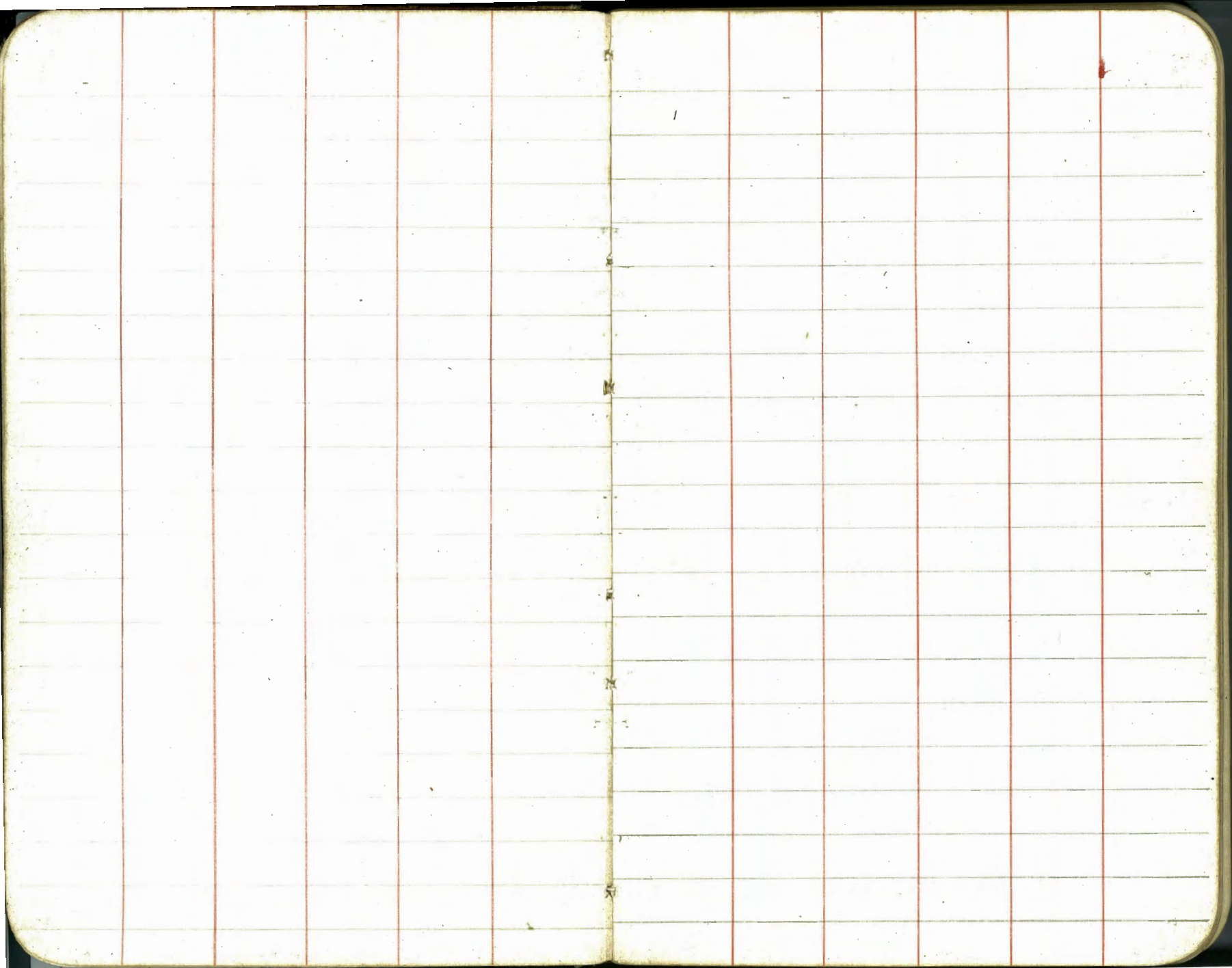
DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.



Garnet St. Cross Section
Pendleton to Atlantic St.

8-7-33
Moore
Singer
Northboro

2146 = Calverton Pt

26.08 22.18

14.30 18.20
41' Top Basin 442.5' Top
10' 10'

see sketch

210

32.8 30.3 28.8 29.36 29.36 29.25 28.0 27.7
76 101 11.6 11.02 11.02 11.13 12.1 12.7
40 35 20 10' edge 10' edge 20 40

1776 21' Pt Large Tree

37.4 31.4 30.6 30.75 30.82 30.64 29.6 31.1
20 90 9.8 9.63 9.56 9.90 10.8 9.3
40 35 20 10' edge 10' edge 20 40

1750

1708 21' Pt Large Tree

37.1 33.7 32.6 32.25 32.25 32.12 32.1 31.2
23 17 7.8 8.13 8.13 8.26 8.3 9.2
40 35 20 10' edge 10' edge 20 40

170 21' Pt Small Tree

36.3 34.2 33.78 33.62 33.62 32.8 34.6 31.8
4 6.3 6.65 6.76 6.76 7.6 5.8 8.6
40 20 10' edge 10' edge 20 20 40

0750

0425 24' Pt Small Tree

045 22' Pt Fire Hydrant

040 = E.L. Pendleton

37.4 35.80 35.06 35.10 35.42 34.92 34.71 35.33 34.9
3.0 4.58 5.32 5.28 5.26 5.46 5.67 5.05 5.5
40 20' top 20' gutter 10' edge 10' edge 20 20' top 40

BM 246 40.38

36.92

HXB.P.
Garnet Pendleton

4148.39

22.46 Lt ✓
 21.6 (22.8) 21.1 21.53 21.70 22.89 22.5 22.2 20.0 16.2
 10.6 9.7 11.1 10.63 10.46 9.77 9.7 10.0 12.2 15.0
 40 20 10 22-Edge 16.8-Edge

4113.53

23.1 22.6 23.4 22.5 22.66 22.90 23.62 23.5 22.5
 9.1 9.6 8.8 9.7 9.50 9.26 8.51 8.7 9.7
 40 30 20 10 57-Edge 143-Edge 20 40

4402

20' Lt. Large Tree

25.3 24.1 23.84 24.03 24.54 24.1 22.1
 6.9 8.1 8.32 8.13 7.62 8.1 10.1
 40 20 9-Edge 11-Edge 20 40

3178.66

314380 BC Lt

29.5 26.4 24.5 24.94 25.12 25.28 24.8 23.5
 2.7 6.0 7.7 7.22 7.04 6.88 7.1 8.7
 40 35 20 10-Edge 10-Edge 20 40

370

30.3 27.3 26.1 26.39 26.45 26.40 25.7 24.7
 1.9 4.8 6.1 5.77 5.71 5.76 6.5 7.5
 40 35 20 10-Edge 10-Edge 20 40

JP

483

32.16

1305

27.33

32.16

2+150

40.38

28.2 27.8 27.89 27.86 27.74 26.8 26.0
 12.2 12.6 12.47 12.52 12.64 13.5 14.4
 20 24 30 10-Edge 10-Edge 20 24 40.38

6471 - 34 Pt - Power Pole

17.7 18.7 15.6 15.94 16.07 16.02 15.9 12.4

6450

5.4 4.4 7.5 7.14 7.01 7.06 7.2 10.7
40 20 12 12 10 20 30 40

6432

39 Pt. Tree 18 Lt. Tree

18.7 19.3 17.1 17.27 17.51 17.2 17.2 13.5

640

4.4 3.8 6.0 5.81 5.57 5.40 5.8 9.6
10 20 12 12 10 20 30 40

BM

3.59 23.08 3.72 19.51

Mon 15th

545298 EC

23.08

5461

26 Pt Tree

19.51 19.7 20.0 17.9 18.46 19.40 19.2 13.9

545298

EC

3.72 3.5 3.2 5.3 4.77 3.83 4.1 9.3
45 00 10 40 20 10 12 20 30 40

20.2 20.6 18.7 19.45 19.50 20.59 20.6 13.9

541812

3.0 2.6 1.5 3.78 3.73 2.70 2.6 9.3
20 20 10 05 12 15 27 40

20.5 21.8 19.8 20.38 20.51 21.53 21.5 16.3

478325

2.7 1.4 3.4 2.85 2.72 1.7 1.7 14.4
40 20 16 10 15 18 29 40 40

TP

3.13 23.23 12.06 20.10

23.23

32.16

			Lt	Z	Pt						
8+60	20 Lt - Tree	22 Pt - Tree	15.7	16.7	16.8	11.9	12.04	12.17	12.07	11.7	10.3
8+50			7.1 40	6.4 30	6.3 20	11.2 10	11.04 Edgr	10.91 10	11.01 20 Edgr	11.4 30	12.9 40
8+04.20			4.9	17.2	16.9	12.2	12.22	12.31	12.21	12.1	10.5
7+93	38 Pt. Power Pole	22 Lt - Twp. Pole	8.2 40	5.9 30	6.2 20	10.9 10	10.86 Edgr	10.77 10	10.87 20 Edgr	11.0 30	12.1 40
7+84.2	Existing Culvert		12.26	17.3	17.2	12.3	9.82	12.34	12.42	12.33	8.82 (8.72) 10.0
7+79	32 Pt. Large Tree	18 Lt - Tree	10.82 40 Ft. Col. Box	5.8 30	5.9 20	10.8 10	13.28 7 max 27-41	10.71 Edgr	10.66 10	10.75 20 Edgr	14.25 30 39.50 40
7+64.2			15.0	17.6	17.5	12.9	12.74	12.87	12.76		11.6
7+50			8.1 40	5.5 30	5.6 20	10.3 10	10.34 Edgr	10.21 10	10.33 20 Edgr		11.5 40
7+08	27 Pt. Tree		15.4	17.7	17.6	12.9	13.15	13.20	13.10	13.1	12.0
7+0			7.7 40	5.4 30	5.5 20	10.2 10	9.93 Edgr	9.88 10	9.98 20 Edgr	10.0 30	11.1 40
			16.7	18.2	18.2	14.4	14.61	14.67	14.54	14.0	12.0
			6.1 40	4.9 30	4.9 20	8.7 10	8.47 Edgr	8.41 10	8.54 20 Edgr	9.1 30	11.1 40
							23.08				

23.08

23.08

		Lt.	Lt.	Lt.	Lt.	Lt.	Lt.	Lt.	Lt.	
1170		16.2	14.3	13.8	12.3	12.31	12.41	12.26	11.5	9.0
10792	16 Lt. Top Pole	1.1 40	3.0 30	3.5 20	5.0 10	5.04 20-Edge	4.96 16	5.09 20-Edge	5.8 30	8.3 40
10783	37 Pt. Tree 17 Lt. Tree									
10764	37 Pt. Post or Pole	16.5	15.5	14.6	12.3	12.28	12.43	12.28	11.6	9.0
10750		0.8 40	1.8 30	2.7 20	5.0 10	5.07 Edge	4.92 10	5.07 20-Edge	5.7 30	8.3 40
10709	18 Lt. Tree 37 Pt. Tree									
1070		17.1	15.1	14.7	12.5	12.28	12.35	12.23	11.8	9.5
		0.2 40	1.2 30	2.6 20	4.8 10	5.12 Edge	5.00 10	5.12 20-Edge	5.5 30	7.8 40
9750		16.4	15.7	12.3	12.20	12.28	12.15	11.6	9.8	
9713	18 Lt. Top Pole	0.9 40	1.6 30	5.0 10	5.15 Edge	5.07 10	5.20 20-Edge	5.7 30	7.5 40	
9736	36 Pt. Tree									
9732	37 Pt. Post or Pole 19 Lt. Tree									
TP	515 17.35 10.88 12.20					17.35				
970		16.9	16.4	16.2	12.3	12.15	12.25	12.12	8.8	
		6.2 40	6.7 30	6.9 20	10.8 10	10.93 Edge	10.83 10	10.96 20-Edge	14.3 40	
	23.08					23.08				

BM 6.96 11.17
 14.7 Lt
 48 Lt
 18+29.38 FC
 1/2 G. and the
 1/2 Pic

18+29.38 FC

18+0
 17+88 16 Lt = Telp Pole

17+60 32 Ft = Tree

17+50
 17+37 4 Lt - top Tree 22 Lt - Small Tree

17+15 36 Ft - Parasitic Pole

17+0

TP 4.97 18.13 4.16 12.16

16+83 7 Lt - Tree 28 Lt - Telp Pole

16+50
 17.32

Lt Lt Rt
 11.7 12.7 13.1 13.14 13.05 12.93 13.6 10.1 4.0 -1.0
 6.4 5.4 5.0 4.99 5.08 5.20 4.5 8.0 1.1 1.1
 25 26 15. 26. Edgy 40 -0.9 100 Bot Chm
 19.0 100 Bot Chm

11.8 12.4 13.0 13.23 13.03 12.94 12.4 10.1 0.0 2.0
 6.3 5.7 5.1 4.90 5.10 5.39 5.7 8.0 8.1 1.1
 25 26 48 Edgy 148 242 Edgy 40 55 100 Bot Chm

12.1 12.3 13.1 13.32 13.03 12.60 12.0 10.0 9.9 4.9
 6.0 5.8 5.0 4.81 5.10 5.53 6.1 8.1 8.2 1.1
 25 26 8.5 Edgy 13.5 20.5 Edgy 40 8 100 Bot Chm

12 Lt 12.1 13.1 13.23 12.94 12.56 11.1
 5.7 6.0 5.0 4.90 5.19 5.57 7.8
 25 26 17.2 Edgy 12.3 22.2 Edgy 100

18.13

13.2 12.5 13.2 13.12 12.89 12.50 12.2 10.6
 4.6 4.8 4.1 4.20 4.43 4.82 5.1 6.7
 35 20 11.2 Edgy 11.2 21.2 Edgy 30 65
 17.32

19+50

7.9 7.9 4.9 4.5 1.3 ✓ 0.6 ✓ 0.1 ✓ 4.9 4.1 6.1 10.0
 $\frac{10.2}{100}$ $\frac{10.2}{80}$ $\frac{13.2}{45}$ $\frac{13.4}{25}$ $\frac{16.8}{20}$ 17.5 18.0 $\frac{13.2}{30}$ $\frac{14.0}{55}$ $\frac{12.0}{75}$ $\frac{8.1}{100}$

19+29

17' Lt - Twp. Pole

8.5 7.0 6.1 ✓ 3.2 0.8 ✓ 0.4 ✓ 4.5 4.8 4.2

19+25

$\frac{9.6}{80}$ $\frac{11.1}{45}$ $\frac{12.0}{20}$ 14.9 17.3 17.7 $\frac{13.6}{45}$ $\frac{13.3}{75}$ $\frac{13.9}{100}$

19+0

10.3 12.1 8.5 ✓ 8.3 5.8 ✓ 1.8 ✓ -0.5 ✓ 4.0 3.5

$\frac{7.8}{75}$ $\frac{8.0}{15}$ $\frac{9.6}{20}$ $\frac{9.8}{10}$ 12.3 16.3 $\frac{18.6}{25}$ $\frac{14.1}{50}$ $\frac{14.1}{80}$

18+79

Opp N.W. Cor. Bridge

12.7 10.8 11.3 ✓ 9.1 - 7.0 ✓ 4.6 - 0.3 - 0.2 4.4 2.1

$\frac{7.4}{85}$ $\frac{7.3}{45}$ $\frac{6.8}{20}$ 9.0 11.1 $\frac{13.5}{25}$ $\frac{13.4}{30}$ $\frac{15.9}{80}$ $\frac{13.7}{64}$ $\frac{14.0}{100}$

18+76

10.9 10.9 11.4 ✓ 12.9 ✓ 13.29 4.6 $\frac{-0.47}{-0.6}$ -0.9 4.5 2.2

$\frac{7.2}{85}$ $\frac{7.2}{45}$ $\frac{6.7}{20}$ 5.2 $\frac{13.4}{25}$ $\frac{13.5}{30}$ $\frac{18.5}{80}$ $\frac{19.0}{60}$ $\frac{12.6}{65}$ $\frac{15.9}{100}$
 2nd Deck

18+55

Opp S.W. Cor. Bridge

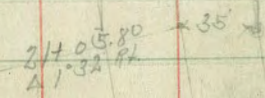
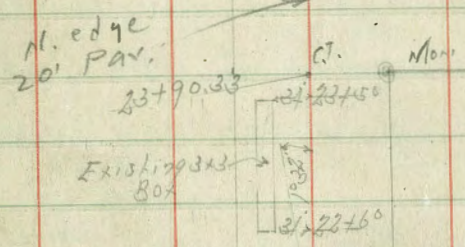
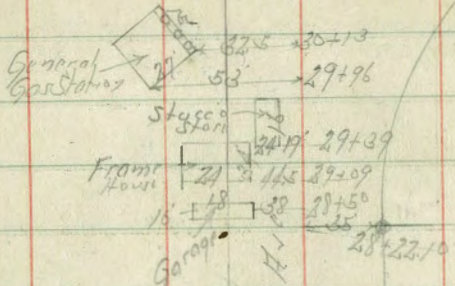
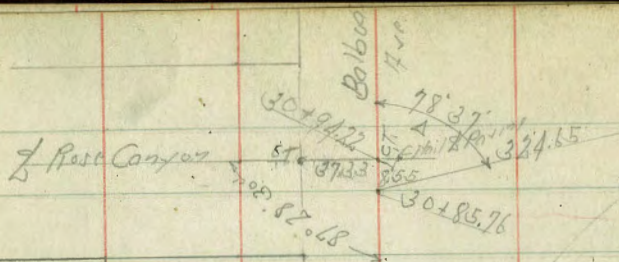
18.13

11.7 13.2 13.4 13.29 13.16 7.9 3.8 - 1.2 - 1.2 3.3

$\frac{6.4}{45}$ $\frac{1.9}{20}$ 4.7 1.84 4.97 $\frac{10.2}{25}$ $\frac{14.2}{50}$ $\frac{19.3}{80}$ $\frac{12.2}{75}$ $\frac{14.5}{100}$

18.13

2nd Deck Bridge

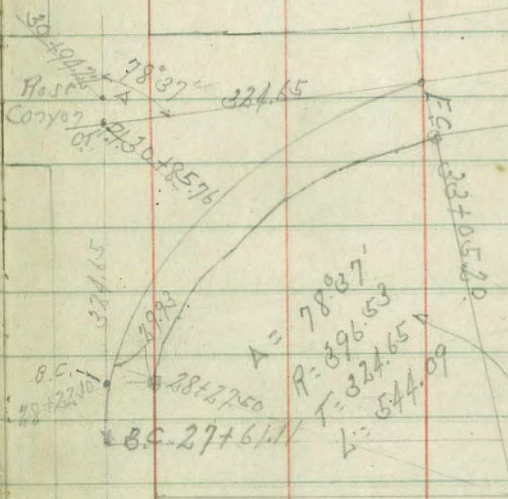


Grand Ave

Grand Ave

Bond St

Bond St



Balboa Fl

Good Ave

Magnolia Ave

NOT USED
NO OPENING

A.C. 18+29.38

22+45 7' Lt. Tree 30 Rt. Tree Lt S Rt

22+25 50 Lt. Tree 40 Rt. Tree

22+10 22' Lt = Telp Pole

TP 4.87 17.59 4.52 12.72

10.4 8.4 8.6 12.9 12.9 13.08 13.17 13.06 12.6 10.7

22+0 6.8 8.8 8.6 4.3 4.3 4.6 4.07 4.18 4.6 P.Pole 6.5
5.5 4.5 20 15 2 2.5 13.5 2.5-Edge 30 32 40

21+77 50 Lt. Tree

21+70 6' Lt. Tree 31' Rt. Tree

21+55 50 Lt. Tree 11.5 8.0 8.8 12.5 12.6 13.05 13.18 13.04 10.3

21+50 5.7 9.2 8.4 4.7 4.6 4.19 4.06 4.22 6.9
5.0 3.5 20 7 8.7-Edge 13.7 23-Edge 4.0

9.4 10.7 7.6 8.4 12.6 12.99 13.14 13.02 11.0

21+0580 = Δ Rt 1°32' 7.8 6.5 7.6 9.6 8.8 4.6 4.25 4.10 4.22 6.2
7.5 5.0 5.0 4.0 20 2.5-Edge 2.5-Edge 3.5

20+95 4' Lt. Tree 32' Rt. Tree

20+80 18' Lt = Telp Pole 7.9 2.6 10.5 6.7 12.8 12.9 12.99 13.14 13.03 13.0 10.1

20+80 32' Rt. Pencil Pole 9.3 14.6 6.7 10.5 4.4 4.3 4.25 4.10 4.21 4.7 7.1
9.0 8.0 3.0 3.5 1.8 2.5-Edge 1.5 2.5-Edge 3.2 2.0

20+72 50 Lt. Lgt Tree

3.1 7.0 7.1 2.0 7.2 6.9 11.3 12.3 13.02 13.14 13.09 10.1 9.9

20+60 1.1 10.7 10.1 15.2 10.0 10.3 5.9 4.9 4.22 4.10 4.15 7.1 7.3
1.00 2 8.0 7.5 3.0 3.0 2.0 2.5-Edge 1.5 2.5-Edge 2.0 8.5

17.24

17.24

23+46

11.7 13.2 ✓ 13.20 ✓ 13.34 ✓ 13.21 ✓ 12.3 ✓ 10.6 ✓
 5.9 5.9 4.1 4.39 4.25 4.38 5.3 7.0
 5.0 38 20 20-Edge 38 40

23+25 - A Pairing

12.4 12.4 ✓ 13.16 ✓ 13.28 ✓ 13.21 ✓ 11.6 ✓ 10.5 ✓
 5.2 5.2 4.22 4.31 4.38 6.0 7.1
 5.0 20 20-Edge 30 40

23+21 10 Lt-Tree 28 Rt-Tree

11.1 9.8 9.6 ✓ 12.9 ✓ 13.1 ✓ 13.14 ✓ 13.29 ✓ 13.18 ✓ 12.5 ✓ 10.5 ✓

23+15

6.5 7.8 8.0 1.7 4.5 1.45 4.30 4.41 5.1 6.9 7.1
 5.0 15 20 7 10 6.2-Edge 10.2 20.2-Edge 25 34 40

23+0

11.3 9.3 8.8 ✓ 12.4 ✓ 13.1 ✓ 13.14 ✓ 13.26 ✓ 13.16 ✓ 12.3 ✓ 10.2 ✓
 6.3 8.3 8.9 5.2 4.5 4.25 4.33 4.43 5.3 7.4
 5.0 40 20 7 23-Edge 10.3 20.3-Edge 30 40

22+60

7.81
 9.78
 13.1 12.5 ✓ 12.9 ✓ 13.11 ✓ 13.26 ✓ 13.13 ✓ 12.8 ✓ 10.7 ✓

22+50

11.7 8.8 8.1 9.5 5.1 4.7 4.48 4.32 4.46 1.8 6.9
 6.4 8.8 9.5 5.1 4.7 4.48 4.32 4.46 1.8 6.9
 5.0 40 20 5 13-Edge 11.3 21.3-Edge 35 46

17.59

17.59

				Lt.	Z	Rt					
28+47	28 Rt. Tree										
28+30	10 Lt. Tree 30 Lt. Tree			13.6	13.7 ✓	13.61 ✓	13.71 ✓	13.62 ✓	14.4 ✓	13.79 ✓	13.8 ✓
28+22+10	- Opp BC SL Ground			4.8 4.5	4.7 20	4.76 Edge	4.66 10	4.75 20-Edge	4.0 30	4.58 35	4.6 40
27+08	? 10 Lt. Tree			13.6	13.7 ✓	13.56 ✓	13.55 ✓ ^{13.65}	13.44 ✓	14.3 ✓	12.8 ✓	
28+0				4.8 4.5	4.7 20	4.81 Edge	4.72 10	4.93 20-Edge	4.1 30	5.6 40	
27+82	34 Rt. Power Pole										
27+70	28 Rt. Tree 36 Lt. Telp Pole			13.3	13.5 ✓	13.50 ✓	13.61 ✓	13.52 ✓	13.8 ✓	12.4 ✓	
27+50				5.1 4.5	4.9 20	4.82 Edge	4.76 10	4.85 20-Edge	4.6 30	6.0 40	
				12.5	12.7 ✓	13.47 ✓	13.56 ✓	13.43 ✓	13.7 ✓	11.3 ✓	
27+0				5.9 4.5	5.7 20	4.90 Edge	4.81 10	4.94 20-Edge	4.7 30	7.1 40	
26+95	10 Lt. Tree 28 Rt. Tree										
TP	4.91 18.37 4.13 13.46					18.37					
26+18	34 Rt. Power Pole			12.2	12.5 ✓	13.42 ✓	13.53 ✓	13.42 ✓	13.4 ✓	11.4 ✓	
26+50				5.4 4.5	5.1 20	4.12 Edge	4.06 10	4.17 20-Edge	4.2 30	6.2 40	
26+45	28 Rt. Tree										
26+20	9 Lt. Tree										
	17.59					17.59					

BM		2.44	19.75	NE No. 30/boon Post Canyon							
					Lt	Z	Rt				
					18.49	18.44	18.42	18.20	18.30	18.27	18.7
30+7922	-H Edge Pring Rose Canyon				3.70	3.75	3.77	3.99	3.89	3.92	3.5
30+69	40' Lt - Telp Pole				4.50 20	4.75 20	4.77 20	4.99	4.89 10	4.92 20-Edge	4.5
30+50					17.2	17.4	17.40	17.68	17.63		18.9
					5.0 4.5	4.8 20	4.79 Edge	4.51 10	4.56 20-Edge	4.3 30	4.3 40
30+40	11.5 Lt - General Petroleum Sign				17.2	16.8	16.45	16.52	16.36	16.6	
30+0					5.0 4.5	5.4 20	5.74 Edge	5.67 10	5.83 20-Edge	5.6 40	
TP	6.31	22.19	2.49	15.88			22.19				
29+96	28' Pt - Trac				15.8	15.7	15.42	15.54	15.43	15.2	
29+55					3.6 4.5	2.7 20	2.95 Edge	2.83 10	2.94 20-Edge	3.2 20	
29+07	38' Lt - Telp Pole				14.0	14.4	14.42	14.47	14.36		14.0
29+0	33' Pt - Power Pole				4.4 4.5	4.0 20	3.95 Edge	3.96 10	4.01 20-Edge		4.4 40
					13.67 (13.7)	13.9	13.86	13.93	13.81	14.7	14.7
28+50					17	4.5 20	4.51 Edge	4.94 10	4.56 20-Edge	3.7 30	3.7 40
	18.97				38-400 2x18		18.37				

32+50

Lt.				Rt.	
15.7	16.5	16.9	16.2	15.1	15.7
$\frac{6.6}{40}$	$\frac{5.8}{20}$	$\frac{5.4}{20}$	$\frac{6.1}{20}$	$\frac{7.2}{40}$	$\frac{6.6}{59.7=5.1\%}$

32+0

16.9	17.2	17.0	16.6	15.2	15.5
$\frac{5.4}{40}$	$\frac{5.1}{20}$	$\frac{5.3}{20}$	$\frac{5.7}{20}$	$\frac{7.1}{40}$	$\frac{6.8}{58.5=5.1\%}$

31+50

17.5	17.6	17.6	16.7	16.0	16.5	15.7
$\frac{4.8}{50}$	$\frac{4.7}{30}$	$\frac{4.7}{20}$	$\frac{5.6}{20}$	$\frac{6.3}{20}$	$\frac{6.8}{40}$	$\frac{6.6}{57=5.1\%}$

31+0

18.5	18.0	16.0	16.0	15.5	15.5	15.4
$\frac{4.8}{50}$	$\frac{4.3}{30}$	$\frac{6.3}{20}$	$\frac{6.3}{20}$	$\frac{6.8}{20}$	$\frac{6.8}{30}$	$\frac{6.9}{57.4=5.1\%}$

JP 7.47 22.34 3.81 14.87

22.34

30+50

17.7	16.3	15.6	15.0	14.8	15.3
$\frac{1.0}{40}$	$\frac{2.4}{20}$	$\frac{3.1}{20}$	$\frac{3.7}{20}$	$\frac{3.9}{20}$	$\frac{3.1}{32=5.1\%}$

30+0

16.6	15.7	15.3	14.6	14.7
$\frac{2.1}{20}$	$\frac{3.0}{20}$	$\frac{3.4}{20}$	$\frac{4.1}{20}$	$\frac{4.0}{47=5.1\%}$

18.68

18.68

H

L

R

BM

237

19.77

NE 1/4
S1/2 Sec 4
T12N R10E

33705.20 - FC

14.6

15.7

16.1

15.7

14.9

14.9

77
7066
20

66

66
2071
4071
80-100

2234

2234

See Alley Bk 53. Univ. Hts
 Monroe to Madison Bet. Arizona & Hamilton
 New Notes See Page 77.

9-21-33
 Mills
 1311 ss.
 Kahayy.
 SE. Hamilton
 + Madison

Indexed
 C.S.K.

B.M. B.P. 3.04 382.03 378.99

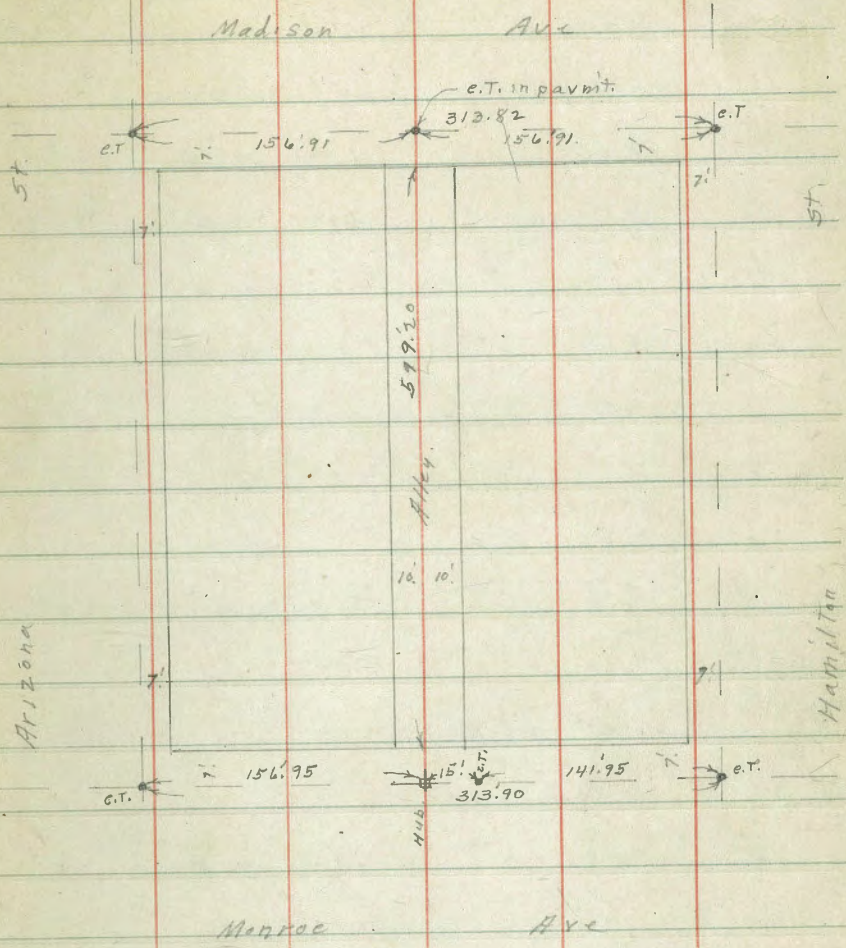
14' N of S Line = S. ch. Line Madison			
-10' E.	gutter	7.45	374.58
-10' E.	on ent. ch.	4.78	75.25
E.	" " "	6.98	75.05
E.	paymt	7.71	74.32
±	"	8.06	73.97
W.	"	8.51	73.52
W.	on ent. ch.	7.91	74.12

0+00 = S Line Madison

9.85 W. of ±	Top. ent. ch.	7.61	74.42	
"	"	7.73	74.30	
±	"	7.58	74.45	
9.90 E. of ±	"	7.23	74.80	
"	ent. ch.	6.80	75.23	
T.P.	5.90	380.49	7.44	374.59

0+10 South

E.	5.0	375.5
±	5.3	75.2
W.	5.5	75.0



380.49

0+37 1/2 emt. walk on W.

W. emt. walk 4.74 75.95

0+44 garage on W. emt. floor 3.6 Back

W-3.6 floor 4.82 75.67

W. emt. apron 4.85 75.64

1/2 4.6 75.9

E. 4.3 76.2

0+73 garage on W. emt. floor. 2.6 Back

E 4.5 76.0

1/2 4.6 75.9

W. 5.1 75.4

+2.6 floor 5.23 75.26

0+80 1/2 W. end picket fence on W. 0.6 in Alley

1+00

W 4.9 75.6

1/2 4.8 75.7

E. 4.6 75.9

1+26 garage on W. emt. floor 2.6 Back

E 4.7 75.8

1/2 4.7 75.8

W 5.0 75.5

+2.6 floor 5.2 75.3

380.49

Alley BIK 53. U.H.

1+59 { Picket fence on W. Line
garage on E. dirt floor 3.6 Back

23

W. 4.8 75.7

1/2 4.8 75.7

E. 4.6 75.9

+3.6 floor 4.6 75.9

1+93 { garage on E. dirt floor 4.5 Back
" " W. " " 2.3 "

E-4.5 floor 4.8 75.7

E 4.8 75.7

1/2 4.9 75.6

W 5.2 75.3

+2.3 floor 5.2 75.3

2+30

W. 5.7 74.8

1/2 5.6 74.9

E. 5.6 74.9

2+59 N. end garage on W. emt. floor 0.5 in Alley

E. 5.8 74.7

1/2 ~~Gone and~~ New Garage Built 6.0 74.5

+9.5 floor 6.40 74.10

~~gone~~ 2+71 1/2 S. end garage on W. 0.5 in Alley
W " Board Fence on W. 0.4 in alley

2+82 N. End. Board. Fence.

		380.49		378.84		Alley BIK. 53. U.H.
W	3+00 { s. End. above W. 11' cmt. el. on W. line on cmt. el.		5.70	24.79	4+07 { garage on E. dirt floor " " W. cmt. "	2:0 Back 4:3 Back
W			6.3	24.2	E-2.0 floor	5.1 223.7
φ			6.2	24.3	W-4.3 floor.	5.79 230.5
E.			5.8	24.7		4+50
T.P.	3.66	378.84	5.31	375.18	E	5.8 73.0
	3+06 garage on E. cmt. floor 17.8 Back				φ	6.0 72.8
E-17.8	floor.		3.68	25.16	W.	5.9 72.9
	3+43 garage on E. cmt. floor 5.5 Back				T.P.	3.96 376.52 6.28 372.56
E-5.5	floor		4.78	74.04	4+95 garage on W. cmt. floor 6.1 Back	
E-3.3	cmt. apron		4.98	73.86	W.-6.1 floor.	4.43 72.09
E			5.2	73.6		5+00
φ			5.10	73.8	W.	4.7 71.8
W			4.9	73.9	φ	4.4 72.1
W. on cmt. el.			4.27	74.47	E.	3.8 72.2
	4+00 s. End cmt. el. on W. line				5+04 garage on E. dirt floor 3.1 Back	
W. Top. el.			4.53	74.31	E-3.1 floor	3.5 73.0
W.			5.4	73.7	5+09 garage on W. cmt. floor 4.4 Back	
φ			5.4	73.4	W.-4.4 floor.	4.68 71.84
E.			5.2	73.6	5+17 garage on E. dirt floor 3.3 Back	
					E-3.3	4.1 72.4
					Flagstone Repair.	

376.52

5+50

E	4.1	72.4
♀	4.6	71.9
W	5.1	71.4

5+75

W.	5.6	70.9
♀	5.1	71.4
E.	4.3	72.2

5+99.2 = N. Line Monroe

9.9 E. of ♀ cmt. ch.	5.53	70.99
" " " " ground	5.6	70.9
♀ " "	6.2	70.3
+9.85 W. " "	6.3	70.2
+9.85 cmt. ch.	6.26	70.26

14' S. = W. ch. Line

40' W. of W. = cmt. ch.	8.55	67.97	B&K
" " " " ground	7.6	66.9	
W. " "	7.4	69.1	
W. cmt. ch.	6.58	69.94	
♀ ground	7.0	69.5	
E. " "	6.5	70.0	

376.52

Alley BIK 53 L.H.

25

E. cmt. ch.	5.79	70.73	
40' E " "	4.58	71.94	
40' " ground.	5.3	71.2	S.E. Monroe
B.M. B.P.	1.27	375.25 =	+ Hamilton
		375.30	

Plotter
RFB

Xsec Gaines
Colusa to Benicia

50 wide

17000
V. 5104
Northton
14/21/33

17.20

100' w'

150' w'

200' w'

250' w'

300' w'

Taylor &
Bridge

2.17

22.24

20.07

SWBP

S

6.4

40.5

T.P.

6.27

19.00

9.57

12.73

✓ C

5.5

41.7

T.P.

11.37

25.91

4.6

14.54

N

4.9

42.3

T.P.

10.88

46.37

0.42

25.49

N

5.6

41.6

Set BM
Top F.H.

11.69

47.62

0.44

45.93

NE COR
M. Idrod
Camp Kearney Rd

✓ C

6.4

40.8

T.P.
RR
set spike
pole.

12.23

47.87

12.18

25.44

SW COR
Riley & Benicia

S

7.2

40.0

T.P.
BM nail
pole

5.57

47.20

6.24

41.63

Gaines
Colusa

S
✓ C

8.1

39.1

WL Colusa = 00

N

6.4

40.8

S

5.1

42.1

250' w'

C

4.0

43.2

N

7.4

39.8

N

2.4

44.0

✓ C

8.1

39.1

50' w'

S

9.0

38.2

N

4.0

43.2

300' w'

S

4.8

42.4

S

10.0

37.2

S

5.7

41.5

✓ C

9.1

38.1

N

8.5

38.9

4720

W50 W

N	9.6	37.6
✓ C	9.9	37.3
S	10.5	36.2
✓ Joon		
S	11.6	35.6
✓ C	11.4	35.8
N	14.1	33.1

413 LN = EL Donahue

N	15.2	32.0
C	11.8	35.4
S	11.8	35.4

Xsec Cairnes, east 50' wide

EL. Cdusa = 00

N	4.6	42.0
✓ C	5.5	41.7
S	7.4	40.0
0750		
S	6.9	40.3

4720

27

✓ C

5.4 41.8

N

4.2 43.0

1700

N

5.3 41.9

✓ C

7.4 39.5

S

8.1 39.1

T.P.

0.45

34.77

12.91 34.29

1750

S

12.0 31.5

✓ C

10.4 24.4

N

9.8 25.0

1460

N

13.6 21.2

✓ C

14.2 20.6

S

11.7 19.1

7400 = W L Donahue Jr

S

14.5 20.3

✓ C

12.2 21.5

N

12.5 22.2

Set T.P. 50' N of N

9.38 25.39

57.38

C			4.6	52.8	
S			5.8	51.6	
	7700 = WL Fresno				
H			2.9	54.5	
C			1.8	55.5	
T.P.	616	63.36	0.18	57.00	mill in post
N			5.7	52.7	
	7750 = EL Fresno				
N			2.1	61.3	
C			4.1	59.3	
S			6.4	52.0	
	8700				± Grade By O'Connell, C.W.A. Exp.
S			4.6	58.8	
C			1.8	61.6	53.35
N			0.3	63.1	
	8750				
N			6.3	52.1	
C			12.0	51.4	52.0
S			16.7	42.2	

64.36

± Grade
29

8790 = WL Carbon

S			16.3	47.1	
C			9.9	53.5	50.90
	T.P. Norkob		5.51	59.85	
	9+17.5 = 24°01' RT - 400' ± R.				
N			4.7	58.7	
C			13.2	50.2	50.18
S			19.1	44.3	
	9750				
C					38.35 49.30
	10700				
C					35.85 47.95
	10750				
C					37.35 46.60
	11700				
C					47.90 45.35
	11750				
C					52.30 43.90

Xsec of Gashen 50' wide
 Gaines to Yurta

63.36

T.P. rock 0.05 50.78 14.63 50.73

J.L. Gaines = 00

W 3.7 42.1

C 6.1 44.7

E 12.6 38.2

T.P. 001 47.83 12.96 47.82

50'S

E 5.6 32.2

C 5.5 32.3

W 4.7 34.1

100'S

W 7.4 30.4

C 9.0 28.8

E 9.3 28.5

150'S

E 13.4 24.4

C 13.4 24.4

W 12.7 25.6

T.P. 040 24.90 12.33 24.50

24.90

30

200'S

W 3.4 21.5

C 4.5 20.4

E 4.1 20.8

250'S

E 6.9 18.0

C 7.4 17.5

W 6.9 18.0

300'S = NL Yurta

W 7.0 15.9

C 9.0 15.9

E 8.3 16.6

1/2 sec Goshen
Gaines to Riley

50 wide

T.P. Hub 1286 72.71 59.85

N.L. Gaines = 00

W 72.71 / 14.9 52.5

✓ C 13.4 59.3

E 22.4 50.3

+ 30 bottom draw 30.9 41.8

50' N

- 25 bot. draw 29.0 43.7

E 15.3 57.41

✓ C 2.6 70.1

W 10.1 69.6

T.P. 1201 85.12 0.60 72.11

100' N

W 85.12 / 8.8 76.32

✓ C 13.0 72.12

E 30.5 54.6

+ 10 bot. draw 37.0 48.1

150' N

- 10 bot. draw 33.0 51.1

N.W. Cor.

Gaines & Foster

E

C

W

T.P.

✓ C

E

+ 15 bot. draw

150' N

- 25 bot. draw

E

✓ C

W

200' N - S.L. Riley

E

✓ C

W

T.P.

85.12

85.12

22.5

62.82

5.0

80.1

4.8

81.3

0.05

84.77

97.98

10.0

87.9

13.3

84.6

23.4

74.5

36.9

61.0

28.0

69.9

12.5

85.6

6.3

91.6

4.7

93.2

2.8

95.1

0.0

97.9

+ 1.5

99.5

1.01

96.67

XSec of Fresno 50' wide
Riley to Yuma

10580

S.L. Riley = 00
E 0.4 105.4
C 1.0 104.8
W 1.2 104.5

50'S

W 9.6 96.2
C 9.1 96.7
E 8.1 92.7

T.P. 006 93.18 12.68 93.12

100'S

E 5.8 89.4
C 5.3 87.9
W 5.4 87.8

150'S

W 14.7 78.5
C 13.2 80.0
E 12.7 80.5

T.P. 003 80.87 14.24 80.84

80.87

200'S

E 8.9 72.0
C 10.4 70.5
W 11.0 69.9
T.P. 023 68.70 12.40 68.47

150'S

W 6.4 62.3
C 4.7 64.0
E 5.2 65.5

300'S = N.L. GAINES

E 7.6 61.2
C 10.1 58.6
W 11.1 57.6

T.P. nail 0.22 57.60 11.52 57.18 57.20

S.L. GAINES = 00

W 3.1 54.5
C 1.7 55.9
E 0.7 56.9

50'S

E 4.7 52.9

57.60

FRODO

↓ C		5.0	32.6
W		6.2	51.4
	100'S		
W		9.0	48.6
↓ C		8.1	49.5
E		10.0	42.6
	150'S		
E		11.1	46.5
↓ C		10.1	47.5
W		11.5	46.1
	200'S		
W		13.2	44.4
↓ C		12.1	45.5
E		12.3	45.3
T.P.	0.8	12.88	44.77
	250'S		
E		2.0	43.3
↓ C		2.2	43.1
W		2.7	42.6

45.25

33

300'S - NL YUMA

W		6.3	39.0
↓ C		5.5	39.8
E		4.2	41.1
T.P.	0.17	32.66	12.76

Xsec Eureka 50' wide Yuma to Riley

NL YUMA = 00

E		18.1	14.6
↓ C		18.2	14.5
W		19.2	13.5

50 N

W		16.2	16.5
↓ C		15.4	17.3
E		15.0	12.2

100 N

E		3.4	28.1
↓ C		6.1	26.6
W		5.9	26.8
T.P.	12.88	44.39	1.15

44.39

150' N

W	7.7	36.2
↓ C	8.3	36.1
E	7.3	32.1

400' N

E	2.6	41.8
↓ C	4.0	41.4
W	5.8	40.6

250' N

W	2.2	42.2		
↓ C	1.4	43.0		
E	1.2	43.2		
T.P.	11.07	55.00	0.46	43.93

300' N = V.L. Gaines

E	9.7	45.2
↓ C	10.9	44.1
W	11.5	43.8

N.L. Gaines = 00

W	9.0	46.0
↓ C	8.2	46.8

55.00

Eureka

34

E

7.4 42.6

50' N

E	4.6	51.4
↓ C	5.2	49.8

W

7.5 47.5

100' N

W	5.7	49.3
↓ C	3.8	51.2

E

0.5 54.5

T.P. 12.04 66.55 0.49 54.51

150' N

E	8.1	58.5
↓ C	12.0	54.6

W

12.3 53.3

200' N

W	7.2	59.4
↓ C	4.0	62.6

E

3.2 63.4

T.P. 12.12 78.59 0.08 66.47

7859

Eureka

250' N

E 6.4 22.2

C 9.3 69.3

W 11.9 66.8

300' N = S L Riley

W 2.8 25.8

C 1.3 22.3

E + 2.2 80.8

T.P. 0.5N 65.8N 1289 65.70

T.P. 0.05 53.55 1282 53.50

1/2 sec of Donahue 50' wide

S. L. Riley - 00

E 6.8 46.8

C 12.1 41.45

W 14.6 38.95

T.P. 0.07 41.5N 12.10 41.45

50' S

W 6.2 35.3

E 6.6 34.9

41.5N

Donahue

35

E 3.7 32.8

100' S

E 6.4 35.1

C 9.9 31.6

W 9.9 31.6

150' S

W 12.8 28.7

C 12.1 29.4

E 11.3 30.2

200' S

E 12.4 29.1

C 14.2 27.3

W 15.3 26.2

T.P. 119 2016 12.55 28.97

250' S

W 5.5 24.7

C 5.0 25.2

E 3.7 26.5

300' S = ML GAINES

E 4.7 25.5

30.16

Donahue

↓ C		6.7	23.5
W		7.7	22.5
	SLGAINASE=00		
W		9.7	20.5
↓ C		8.8	21.4
E		6.6	22.6
	50'S		
E		9.4	20.8
↓ C		10.9	19.3
W		11.5	18.7
	100'S		
W		12.1	18.1
↓ C		12.3	17.9
E		11.4	18.5
T.P	7.75	25.11	17.36
	150'S		
E		8.2	16.9
↓ C		8.2	16.9
W		9.2	15.9

25.11

36

200'S

W		10.3	14.8
↓ C		9.1	16.0
E		3.5	21.6
	250'S		
E		10.9	14.2
↓ C		11.3	13.8
W		11.3	13.8

300'S = NL YUMA

W		14.8	10.3
C		14.5	10.6
E		14.1	11.0

25.11

Xsec of Colusa roadside Yuma to Lauretta

NL Yuma

E	15.7	9.4
✓ C	17.0	8.1
W	17.4	7.7

50' N

W	15.2	9.9
✓ C	15.1	10.0
E	14.8	10.3

100' N

E	11.5	13.6
✓ C	11.8	13.3
W	11.7	13.4

150' N

W	0.0	25.1
✓ C	2.0	23.1
E	5.4	19.2
+10	10.4	14.2

T.P. 12.68 37.30 0.49 346^N

37.30

Colusa

37

200' N

-10	12.5	24.8
E	9.3	28.0
✓ C	5.7	31.6
W	5.1	34.2

250' N

W	0.7	36.6
✓ C	1.5	35.8
E	2.5	33.5
T.P.	12.30	49.1

300' N = 51 GAINES to east

E	9.0	40.1
✓ C	8.7	40.4
W	8.9	40.2

NL GAINES to east = 00

W	6.8	42.3
C	6.8	42.3
E	6.5	42.6

54.5' N = NL GAINES to West

E	4.1	45.0
---	-----	------

4911

60.56

Colusa

38

0.5	C		4.9	44.2
	W		5.0	44.1
		100' N		
	W		3.3	45.8
0.5	C		2.8	46.3
	E		2.2	46.9
T.P.		1243	60.56	0.98
		150' N		48.13
	E		10.9	49.7
0.5	C		11.2	49.4
	W		12.2	48.4
		200' N		
0.5	W		9.1	51.5
	C		8.7	51.9
	E		7.9	52.7
		250' N		
	E		4.3	56.3
0.5	C		5.4	55.0
	W		6.4	54.2

300' N = SL Riley

	W		4.1	56.5
0.5	C		3.0	57.6
	E		2.1	58.5
	T.P.	11.43	71.28	0.71
		SL Riley = 00		
	E		10.6	60.7
0.5	C		12.0	59.3
	W		12.7	58.6
		50' N		
	W		10.8	60.5
0.5	C		10.2	61.1
	E		8.9	62.4
		100' N		
	E		6.9	64.4
0.5	C		8.4	62.9
	W		9.7	61.6
		150' N		
	W		8.0	63.3
0.5	C		6.9	64.4

or SL
Garage

7/28

62.5W

Riley

39

E 5.4 65.9
 290 N = SL Lauretta
 E 1.8 69.5
 C 3.1 68.2
 W 2.9 62.4
 T.P. 247 62.3W 11.43 59.85

150' N
 N 12.2 50.1
 T.P. 066 50.1 12.77 49.55
 C 4.3 45.9
 S 9.3 40.9
 200 N

Xsec of Riley 50' wide Colusa to Doravue
 EL Colusa = 00

S 11.2 39.0
 C 7.9 42.3
 N 6.2 44.0

N 1.6 60.7
 C 2.5 59.8
 S 3.9 58.4

Nail pole 10.20 51.55 41.35 Gaines Colusa
 T.P. 25W 45.8W 8.25 43.30
 T.P. 5.76 46.01 5.57 40.25

50' E
 S 2.1 60.2
 C 1.3 61.0
 N 4.04 62.7

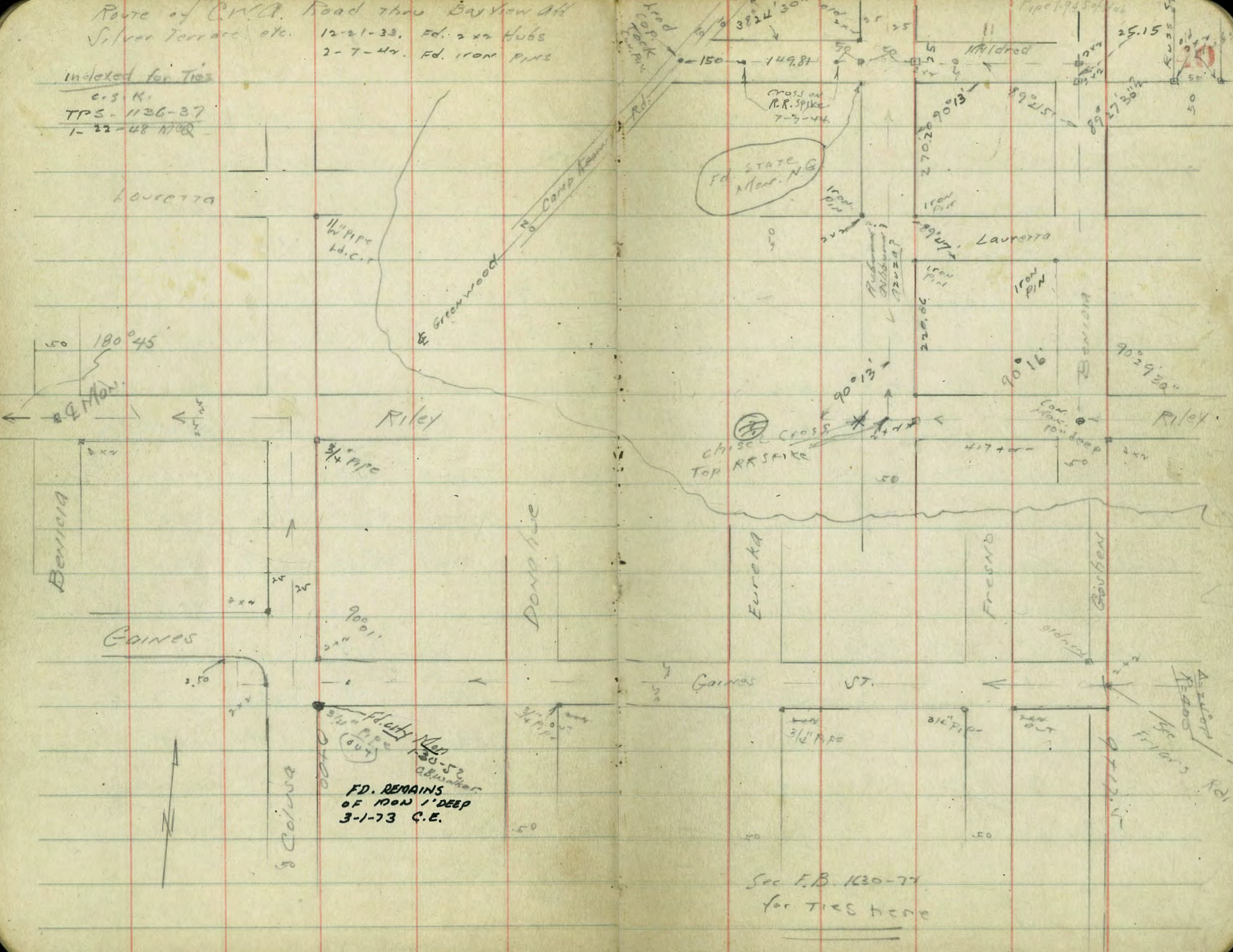
ch to B.P.
 T.P. 1.43 54.53 12.91 33.10 F.H. Ruby + Camp 12.87
 T.P. 0.35 21.95 12.96 21.59
 T.P. 5.96 18.91 8.99 12.95

100' E
 N 0.0 62.3
 C 5.5 56.8
 S 6.6 55.7

T.P. 6.76 22.88 2.79 16.14
 check to B.P. Taylor Bridge 2.80 20.08 20.07

Route of C.M.A. Road thru Bay View Off
 Silver Terrace etc. 12-21-33. Fd. 2 x 2 Hubs
 2-7-44. Fd. IRON PINS

Indexed for Ties
 C.S.K.
 TPS-1136-37
 1-22-48 N.P.R.



See F.B. 1130-74
 for TIES here

sec of Riley St.
Colusa to Azusa

50' wide

5514

Station	W of RL of Colusa	W of RL of Benicia	W of RL of Colusa	W of RL of Benicia	W of RL of Colusa	W of RL of Benicia
11.85	55.14	43.29	Riley + Benicia	S	11.3	42.8
50' W of RL of Colusa				300' W		
N	0.0	55.1	S	12.8	42.3	
C	0.3	54.8	C	10.0	45.1	
S	0.5	54.6	N	8.5	46.6	
100' W				550' W		
S	2.8	52.3	N	8.7	46.4	
C	2.5	52.6	C	10.3	44.8	
N	1.3	53.8	S	16.8	35.3	
150' W				413.4 W = E.L. Benicia = 50' wide		
N	4.6	51.5	S	12.2	42.9	
C	5.0	50.1	C	11.5	43.6	
S	5.3	49.8	N	10.3	44.8	
200' W				T.P. 0.31 43.60 11.85 43.29 of RL		
S	7.6	47.5	WL Benicia = 00			
C	7.4	47.7	N	0.0	42.6	
N	6.6	48.5	C	0.7	42.9	
250' W				S		
N	7.1	48.0	50' W			
C	9.6	45.5	S	2.2	46.4	

4360

✓ C	17	41.9
N	0.9	42.7
160' W		
N	2.5	41.1
✓ C	3.6	40.0
S	4.0	39.6

150' W

✓ S	4.7	38.9
+V	6.1	32.5
✓ C	5.3	38.3
+10	3.8	39.8
N	3.2	40.4

200' W

✓ N	3.2	40.4
+15	5.1	38.5
+20	7.8	35.8
✓ C	7.2	36.2
+20	8.4	35.2
S	6.0	37.6

4360

Piley

42

950' W		
S	7.3	36.3
+5	10.1	33.5
✓ C	9.9	33.7
+10	10.0	33.6
+15	6.3	32.3
N	6.3	32.3

300' W

N	7.7	36.9
+10	10.6	33.0
+15	11.5	32.1
✓ C	11.5	32.1
+20	12.1	31.5
S	9.4	34.2

350' W

S	10.7	32.9
+8	13.5	30.1
✓ C	13.0	30.6
+10	13.3	30.3
+15	10.1	30.5
N	9.1	34.5

400 W

43.60

N 10.9 32.7

+15 12.2 31.4

+20 15.0 28.6

C 15.0 28.6

+15 15.2 28.4

S 12.4 31.2

417 W = EL AZUZA 50 m wide

S 14.1 28.5

+10 16.4 27.2

C 16.0 27.6

+5 16.0 27.6

+15 13.1 30.5

N 12.8 30.8

T.P 517 3608 12.69 30.91

1/2 sec of Azusa
300' S of SL Riley to Mildred

36.08

44

300' S of SL Riley

E	5.8	30.3
↓ C	4.2	30.9
W	4.8	31.3

250' S

W	6.7	29.4
↓ C	6.3	29.8
E	6.8	29.3

200' S

E	7.9	28.2
↓ C	8.0	28.1
W	8.2	27.9

150' S

W	10.3	25.8
↓ C	10.3	25.8
E	9.1	27.1

100' S

E	9.7	26.4
↓ C	11.1	25.0

36.08

W

12.6 23.5

50' S

W

9.6 26.5

↑ 10

11.7 24.4

C

11.6 24.5

↑ 20

10.8 25.3

E

8.6 27.5

SL Riley

E

6.6 29.5

↑ 5

10.1 26.0

↓ 0

10.8 25.3

↑ 15

10.7 25.4

W

7.0 29.1

W L Riley

W

5.7 30.4

↑ 10

9.9 26.2

↓ C

9.8 26.3

↑ 15

9.1 22.0

E

5.2 30.9

56.08

50 N

F	4.6	31.5
+10	9.2	26.7
C	9.4	26.2
+15	8.9	27.2
W	7.4	28.2

100 N

W	15.7	20.4
+15	11.4	24.7
C	10.8	25.3
+15	10.3	25.8
E	13.3	22.8

118 N = 2" corr 1 pipe

N + 4 = inlet F.L.	13.9	23.2
" + 4 = outlet F.L.	15.5	20.6

150 N

F	11.9	24.2
C	10.8	25.3
W	12.6	23.5

56.08

200 N

W	11.1	25.0
+10	8.3	27.8
C	8.6	22.5
E	9.4	26.2

215.3 N = SL Lauretta

E	7.6	28.5
C	7.7	28.4
W	7.9	28.2

NL Lauretta

W hub	3.47	32.61
C	2.0	32.1
E	4.6	31.5

50 N

E	1.1	35.0		
T.P.	12.57	48.57	0.08	36.00
C	12.1	36.5		
W	10.5	38.1		

100 N

W	6.2	42.4
+5	7.9	40.7

A20.70

45

48.57

↓ C			7.9	40.7
-----	--	--	-----	------

E			9.1	39.5
---	--	--	-----	------

150N

E			2.4	45.2
---	--	--	-----	------

↓ C			2.2	44.2
-----	--	--	-----	------

W			4.1	44.5
---	--	--	-----	------

200 N

W			1.6	42.0
---	--	--	-----	------

↓ C			1.5	42.1
-----	--	--	-----	------

E			0.4	48.2
---	--	--	-----	------

T.P.	11.88	60.7	0.28	48.29
------	-------	------	------	-------

250N

E			8.5	51.7
---	--	--	-----	------

↓ C			9.5	50.7
-----	--	--	-----	------

W			9.9	50.3
---	--	--	-----	------

270N - 5L 151 dred

W hub			8.6	51.53
-------	--	--	-----	-------

↓ C			8.2	52.0
-----	--	--	-----	------

E			6.8	53.9
---	--	--	-----	------

60.17

02020

46

NL 171 dred

E			1.9	58.3
---	--	--	-----	------

↓ C			4.9	56.3
-----	--	--	-----	------

W			4.9	55.3
---	--	--	-----	------

1500 Mildred 50' wide
 92020 west to Camp Keany Rd.

6017

WL 92029 = 00

N 4.9 55.3
 √ C 8.0 52.2
 S Sub 8.6x 51.53

50' W

S 11.4 49.0
 √ C 10.9 49.3
 +10 10.6 49.6
 N 8.4 52.0

100' W

N 11.5 48.7
 +10 13.2 49.17
 √ C 12.9 46.3
 S 13.9 46.3

T.P. 125 48.7N 1270 47.47

150' W

S 4.9 43.8
 √ C 4.7 44.0
 +15 4.8 43.9
 N 2.8 45.9

48.7N

200' W

N 5.2 43.5
 +10 6.7 42.0
 √ C 6.8 41.9
 S 6.8 41.9

250' W

S 8.5 40.2
 √ C 8.3 40.4
 N 7.6 41.1

300' W

N 7.6 41.1
 √ C 9.1 39.6
 S 9.4 39.3

335' W on E Mildred = Ely edge paving

S on paving 40' S of E 14.56 36.16

C " " 10.13 38.59

N " " 40' W of E 7.73 40.99

Ch. B.M. Hyd.

4.85 43.87 43.87

47

X sec of Benicia 20' wide
Caines to Lavetta

40.75

RR of the pole 0x6 43.75 43.49
NL Gaines = 00

S. L. Riley
Benicia

W

3.3 40.5

2 x 7.5 x 1 = SL Riley

E 11.8 32.0
C 16.7 27.1
W 21.0 22.8

W

1.6 42.2

C

1.1 42.7

E

0.5 43.0

50' N

T.P.

10.66 53.95 0.46 42.79 DM

W 20.4 23.4
C 19.6 24.2
E 17.4 26.4

NL Riley = 00

E

8.7 45.3

C

9.4 44.6

100' N

W

10.0 44.0

E 16.5 27.3
C 14.5 27.3
W 12.4 30.4

50' N

W

8.0 46.0

C

7.1 46.9

150' N

E

6.6 47.4

W 8.1 35.6
C 7.9 35.9
E 8.9 34.9

100' N

E

4.6 48.4

C

4.9 49.1

200' N

W

5.6 48.4

E 4.4 39.6
C 3.4 40.6

150' N

W

3.4 50.6

5395

DONICIA

49

↓ C 2.8 51.2

E 2.2 51.8

T.P. 4.4 57.73 0.66 53.29

2nd N = SL Lauretta 50 miles

E 2.9 54.8

↓ C 3.5 54.2

W 4.3 53.4

NL Lauretta

W 1.6 56.1

↓ C 0.6 52.1

E 0.6 52.1

Xvec Lauretta
 Bexicia To 300' W of WL Azuza

45.19

50

S.L. Lauretta = 00 57.73

N 1.6 56.1

C 2.9 54.8

S 4.3 53.4

50' W

S 6.0 51.7

C 4.8 52.9

N 4.0 53.2

100' W

N 8.6 49.1

C 8.7 49.0

S 8.3 49.4

T.P. 020 45.19 12.7x 44.99

150' W

S 1.9 43.3

C 2.2 43.2

N 4.1 41.1

200' W

N 7.9 37.3

C 9.6 35.6

S

250' W

S

C

N

300' W

N

C

S

350' W

S

C

N

417' W = EL Azuza

N

C

S

W/L Azuza = 00

S

C

N

10.2 35.0

12.1 33.1

11.5 33.7

10.2 35.0

12.4 32.8

13.9 31.3

15.0 30.2

16.2 29.0

14.5 28.7

13.6 31.6

12.7 31.5

14.8 30.9

16.6 28.6

17.0 28.2

15.1 30.1

12.6 32.6

4519

50' W

N	9.5	35.7
C	11.6	33.6
S	13.5	31.7

100' W

S	10.6	34.6
C	9.4	35.8
N	8.4	36.8

150' W

N	9.5	35.7
C	9.6	35.6
S	10.4	34.8

200' W

S	10.9	34.3
C	10.6	34.6
N	10.4	34.8

250' W

N	11.3	33.9
C	11.3	33.9
S	11.6	33.6

4519

Lauretta

51

300' W

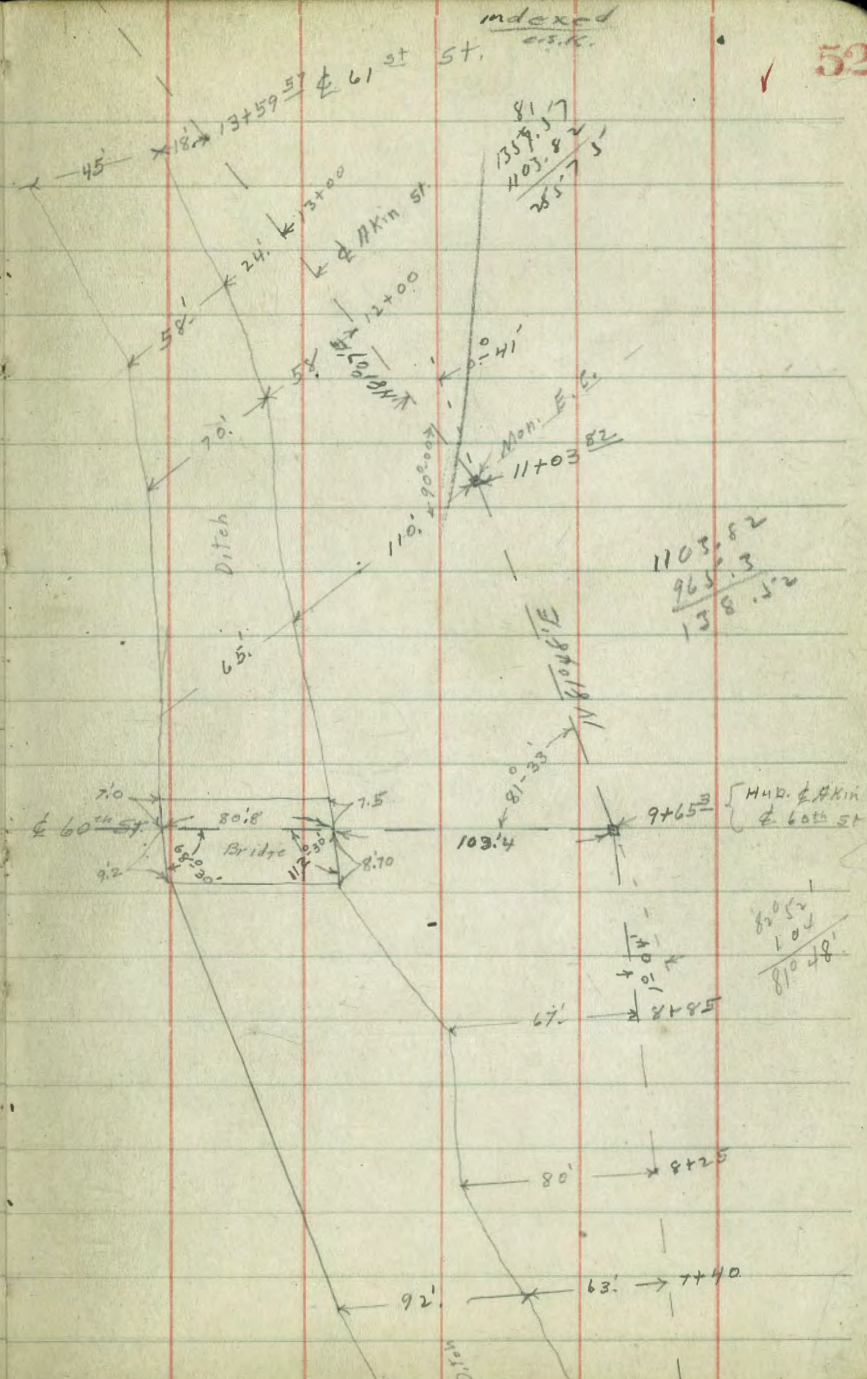
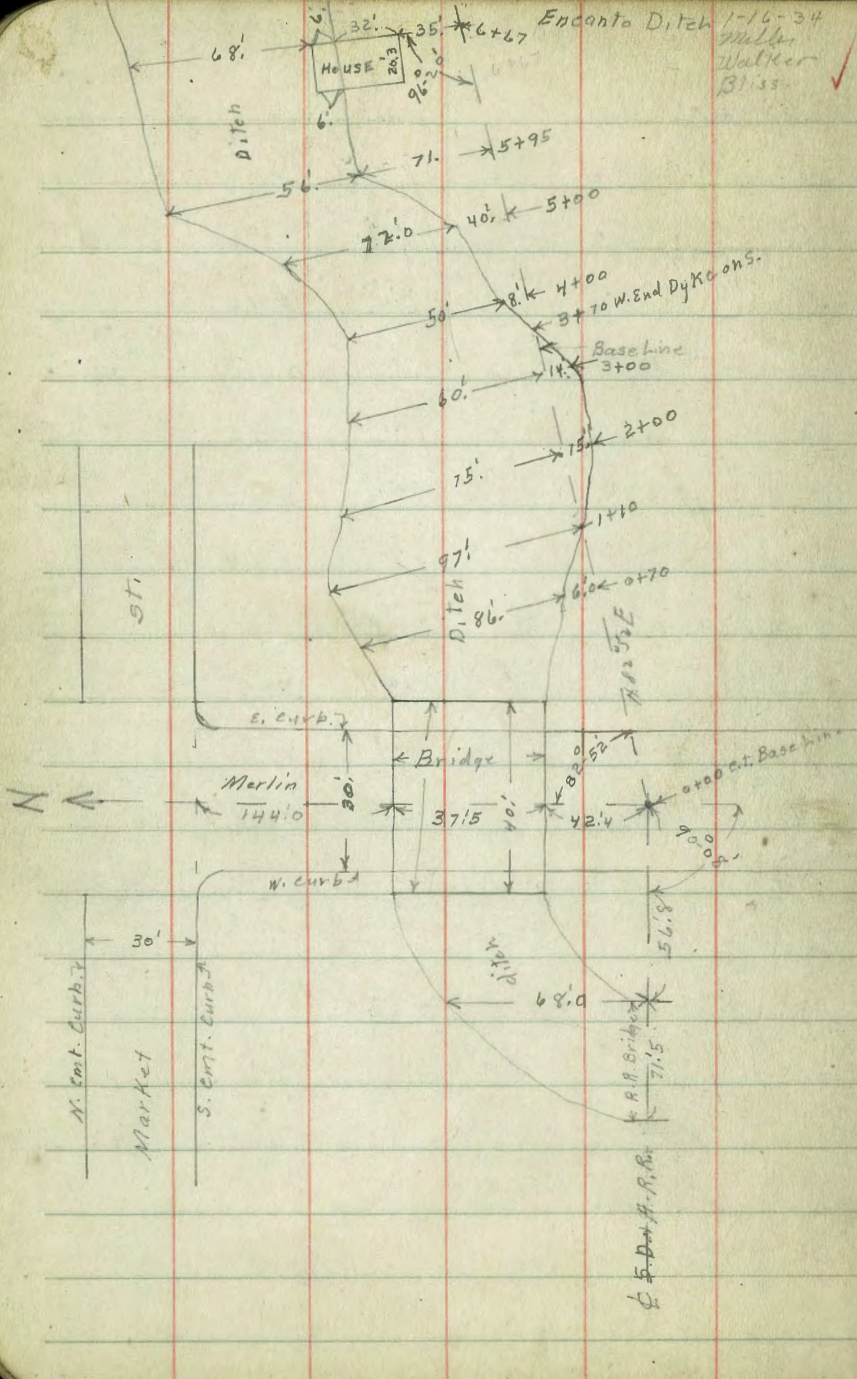
S	12.2	33.0
C	11.9	33.3
N	11.7	33.5

350' W

N	12.6	32.6
C	12.7	32.5
S	12.7	32.5

400' W

S	12.9	32.3
C	13.1	32.1
N	13.1	32.1



indexed

ens. K.

81.7
1359.5
403.8
265.75

1103.82
965.3
138.52

50.5
10.0
81.08

Encanto Ditch

92°08' N
Base Line

Fergus N 00°39' W

Mon 17+51.2
5.85
E AKens. St.

30' 20'
Ditch
Base Line

41' 8' 14+55

N. line AKIN
S. line AKIN

30' 20'
ST. AKIN

61st St N 00°39' W

45' 18' 13+59.57

Ditch
N 61°00' E
20' 20'

62hd 28' 48°23'
16' 23+72.86
144.62
81°46'
5' Granite Mon.

53

24' 23+52
25' 20'
23+40
12'
E. End Welling
& Cobble Wall

237.76
2190.18
182.68

227 80
24' 12'
22+55
14'
20' 22+30

84°33'
21+90
Hub Δ

2194.18
1932.37
257.81

39' 59'
Ditch
Base Line
21+55
15'

S. End Welling
& Cobble Wall
25' 25'

40' 21+30
26' 20+90
19' 20+00
34'

Hub Δ 19+32

1932.37
1751.13
181.24

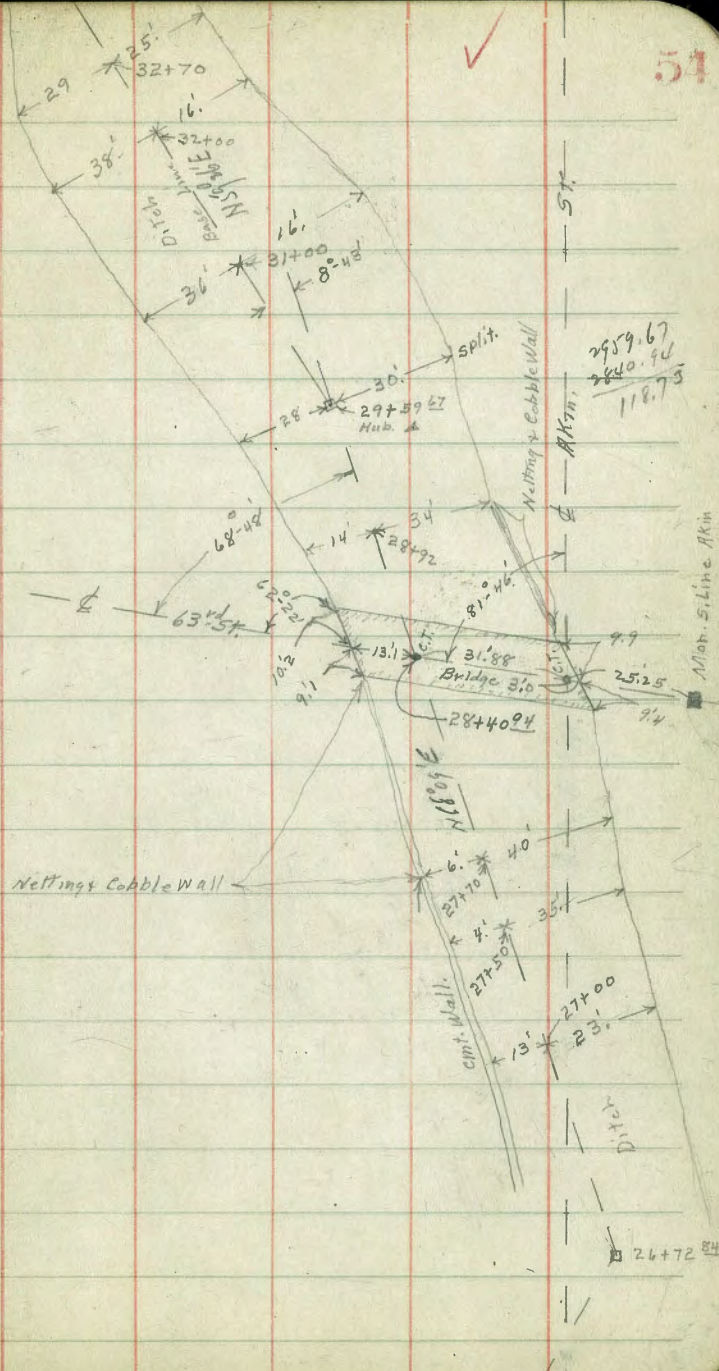
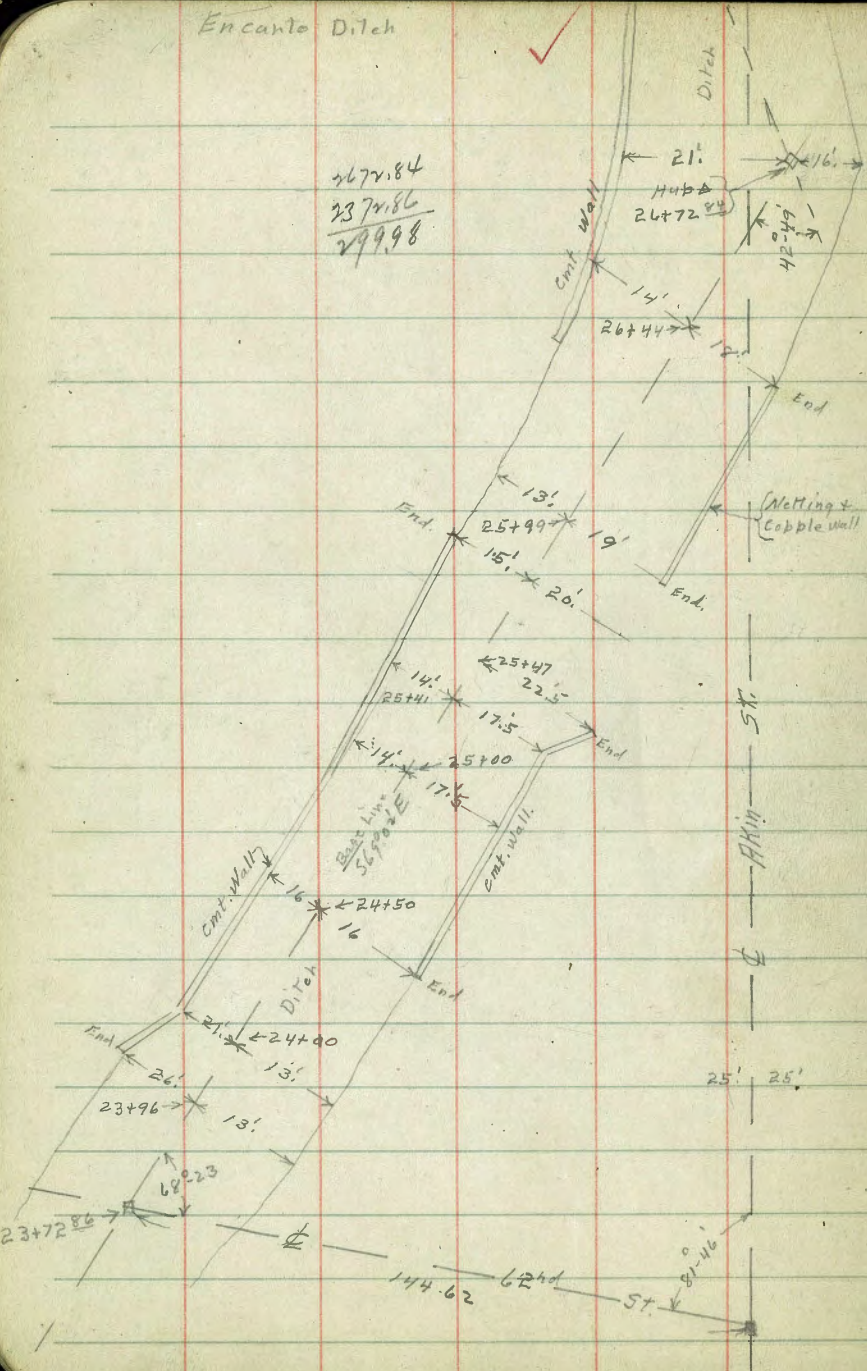
N 76°25' E
17' 34'
45-34'
51'

19+00
18+60
20' 46'

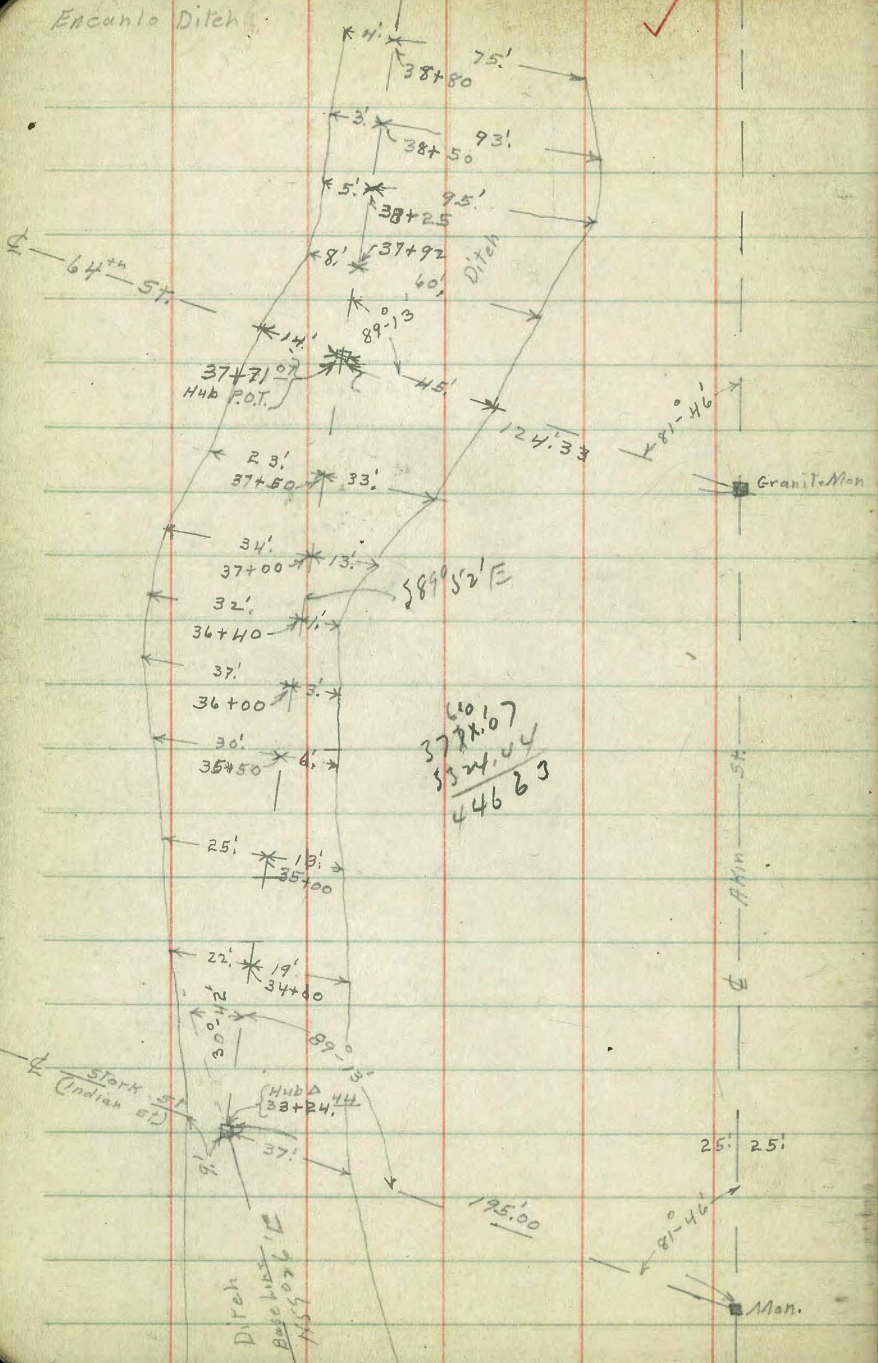
Busc. line
18+00
81°46'
17+51.3
Ditch

Fergus 5' 81°46' 17+51.3

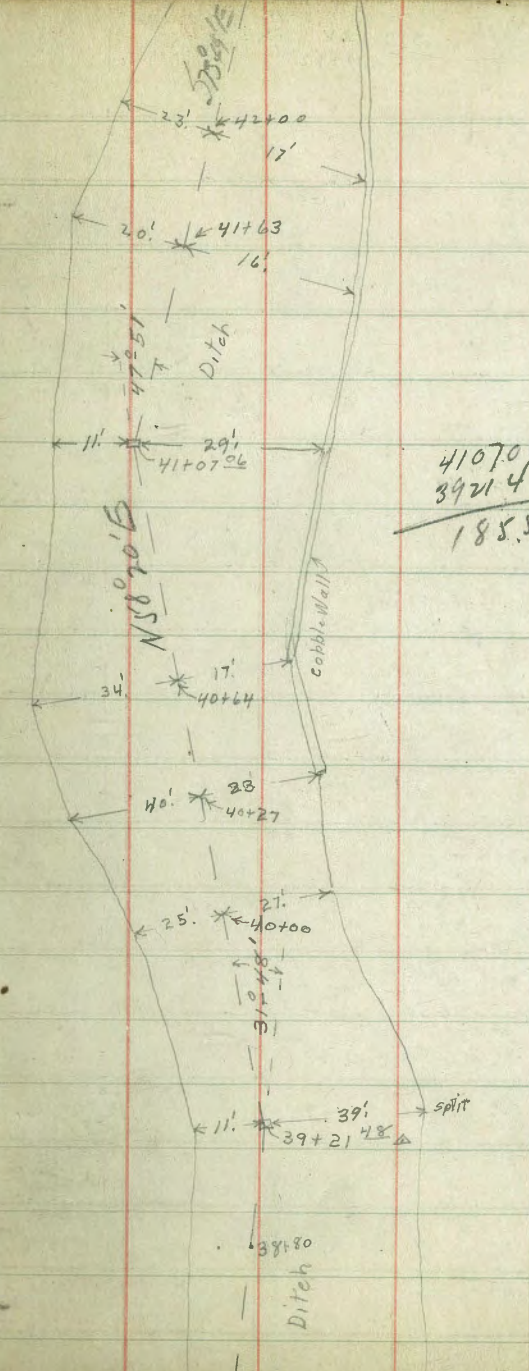
$$\begin{array}{r} 2672.84 \\ 2374.86 \\ \hline 299.98 \end{array}$$



$$\begin{array}{r} 2959.67 \\ 2840.94 \\ \hline 118.73 \end{array}$$



$$\begin{array}{r} 60 \\ 3772.67 \\ 5324.44 \\ \hline 44663 \end{array}$$



$$\begin{array}{r} 4107.06 \\ 3921.48 \\ \hline 185.58 \end{array}$$

$$\begin{array}{r} 3921.48 \\ 3771.07 \\ \hline 15041 \end{array}$$

Encanto Ditch

28' 5' ✓
47+62

26' 10' ✓
47+00

18' 9' ✓
46+00

26' 19' ✓
45+23.26
HUB A

28' 15' ✓
45+00

25' 15' ✓
44+50

25' 17' ✓
44+00

25' 20' ✓
43+50

27' 8' ✓
43+00

13.0 27.2 22.8 ✓
43+14.25

19' 19.2 ✓
43+00

21' 15' ✓
42+50

19' 15' ✓
42+00

4314.26
4107.06
207.20

179.54 to SL
172.84

90°00'
5247.16
4803.96
723.20
227.68'

AKIN

25' 25'

90°00'
50.06
81.18
43'

✓

56

38' 7' ✓
52+47.16

36' 9' ✓
51+90

41' 6' ✓
51+00

37.5 12' ✓
50+30.50
66th St Bridge

35' 12' ✓
50+00

38' 3' ✓
49+00

35' ✓
48+71

30' 2' ✓
48+00

42' 43'
S. Line Imperial
Woodman Ave

Ditch

1523.96
4914.26
209.70

181.94E

181.94E

Base Hill

Chapel Wall

Ditch

47

7

47

7

See Page 63 →

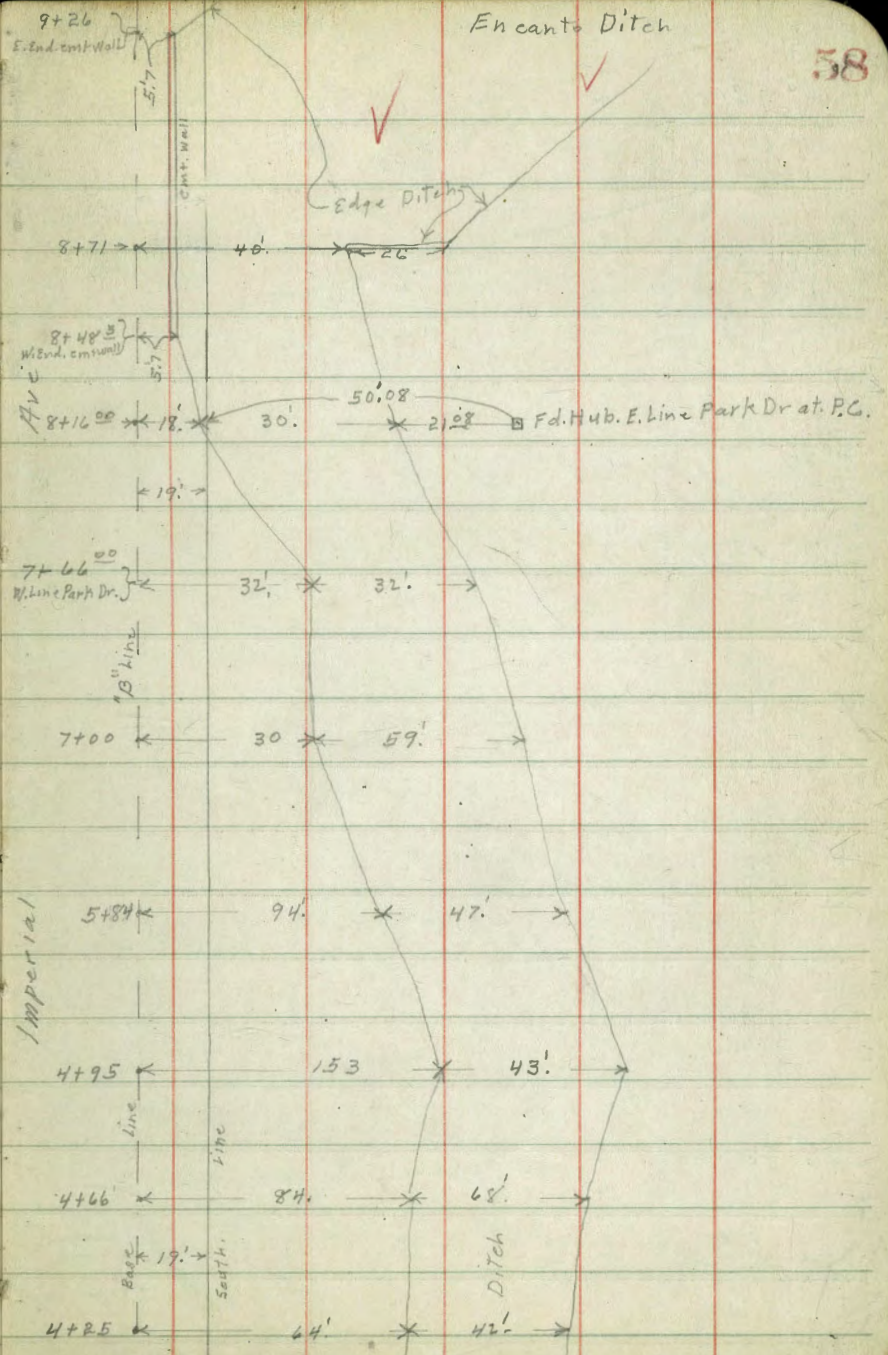
60+00 ← 10' × 17' →

Base line

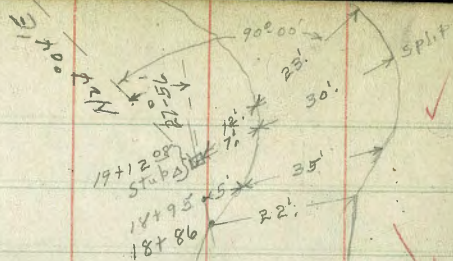
Cut Ditch

58+00 ← 12' × 15' →

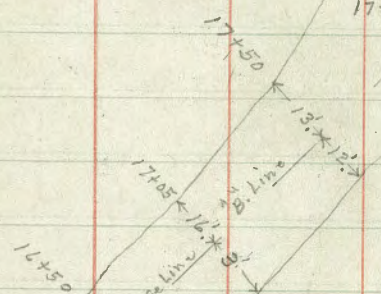
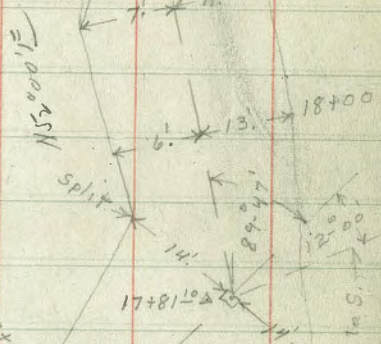
✓



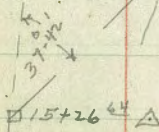
Enganto Dileh



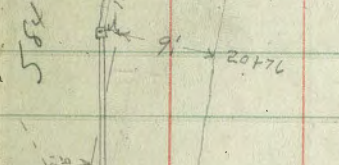
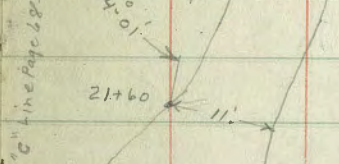
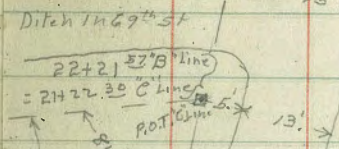
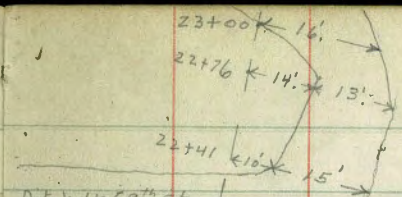
$$\begin{array}{r} 142.00 \\ 175.10 \\ \hline 130.98 \end{array}$$



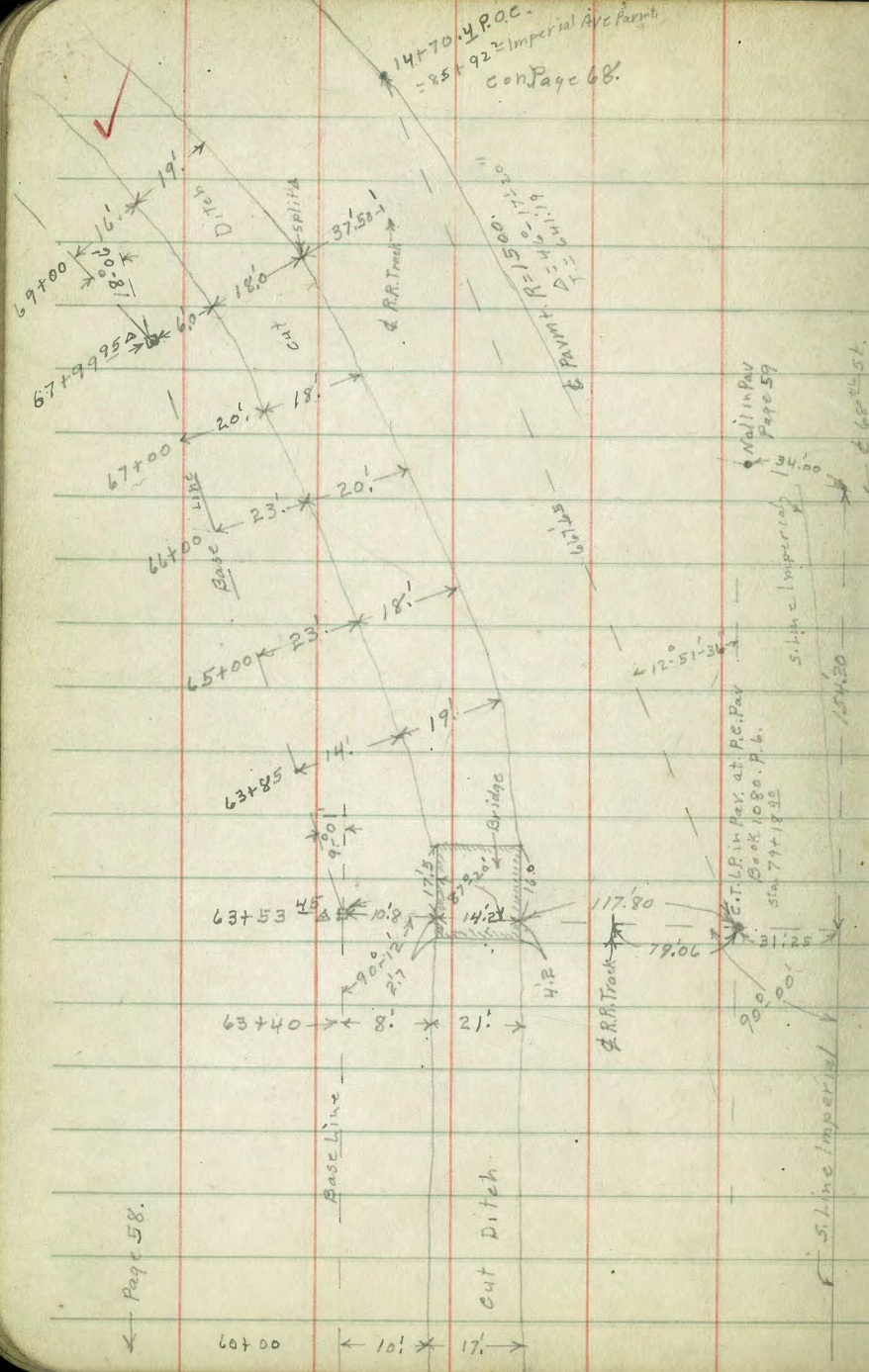
$$\begin{array}{r} 1526.10 \\ 1526.10 \\ \hline 25446 \end{array}$$



60



$$\begin{array}{r} 2056.13 \\ 1912.08 \\ \hline 144.05 \end{array}$$



Page 58.

69+00 ← 101' × 17''

Baseline

Cut Ditch

RR Track

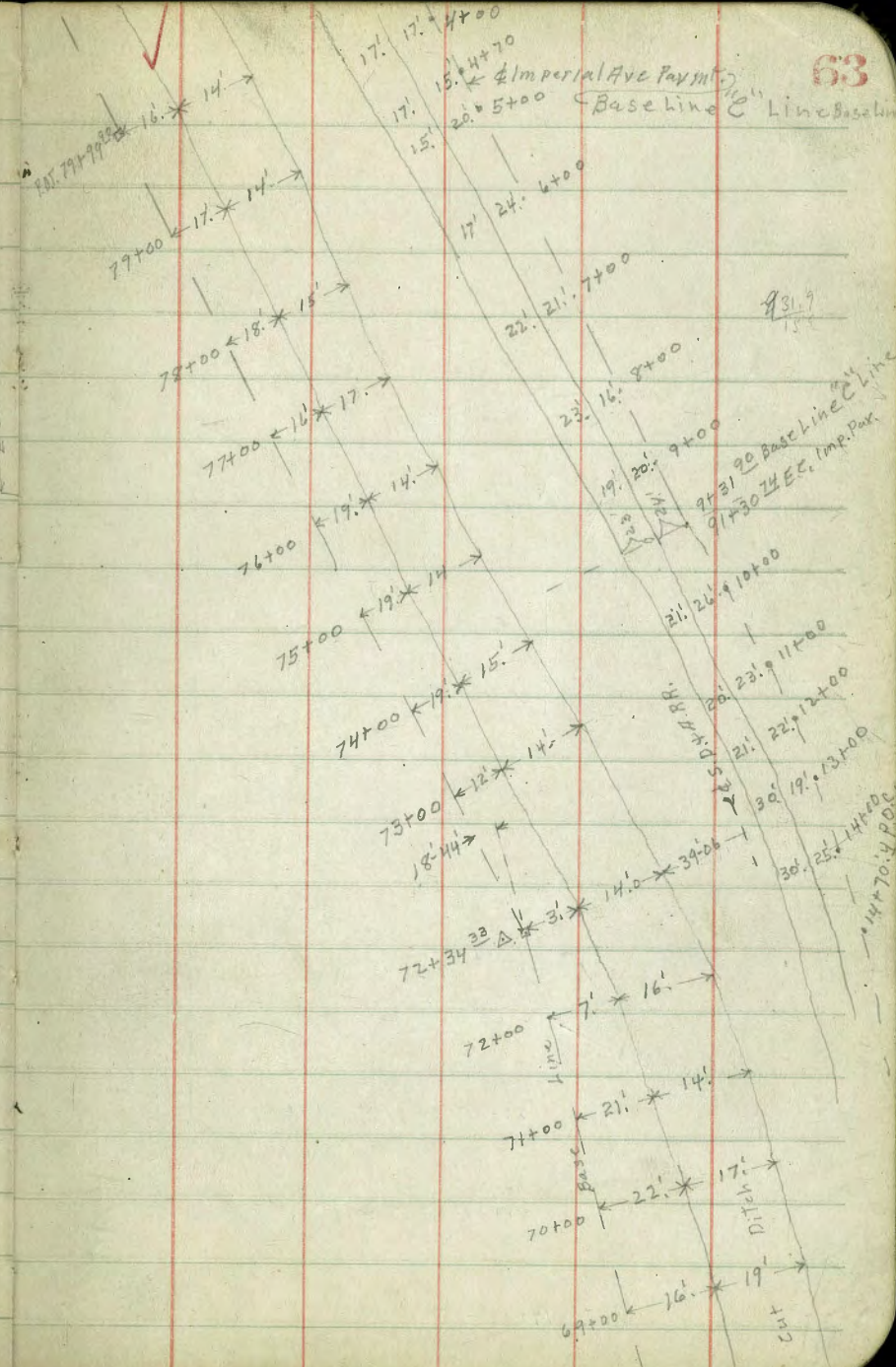
S. Line Imperial

C.P. (C.P. at P.C. Par)
Book 1080, P. 6.
Sta. 79+14.2

Main Pav
Page 59

S. Line Imperial

14+70.4 P.C.
= 85+92 Imperial Ave Parant
con Page 68.



14+70.4 P.C.
= 85+92 Imperial Ave Parant
con Page 68.

Main Pav
Page 59

S. Line Imperial

Baseline
Line Baseline

831.9

9731.90 Baseline
91730.74 E.C. Imp. Par

14+70.4 P.C.

69+00 ← 101' × 17''

Baseline

Cut Ditch

RR Track

S. Line Imperial

2-1-34
Miller
Walker
Bliss

Profile Levels of Existing
Drainage Ditch in Encanto.
Plat. Page 52
Main Ditch

B.M. Nailin R.P.	3.29	165.00	165.00	161.71	N. E. Merlin A + Imperial Ave.
92' W. of 0+00 ϕ Ditch + ϕ B. R. Bridge	16.4		148.6	✓	
92' W. of 0+00 Top Rail R. R. "	5.09		159.91	✓	
61' N. of 0+00 ϕ Merlin Drain Bridge floor.	4.17		160.83	✓	
61' N. of 0+00 ϕ " " ϕ Ditch.	14.0		151.00	✓	Under Bridge
30' N. of 3+00 ϕ Ditch	10.0		155.00	✓	
T.P.	9.40	165.23	9.17	155.83	✓
107' N. of 6+67 = ϕ Ditch		165.23	4.2	161.0	✓
T.P.	7.64	170.74	2.13	163.70	✓
144' N. of 9+65 ϕ 60 th St. + ϕ Ditch		170.74	5.3	165.4	✓
144' N. of 9+65 ϕ Floor Bridge	+2.85		173.59	✓	
93' N. of 12+00 ϕ Ditch	2.8		167.9	✓	
T.P.	7.83	176.92	1.65	169.09	
40' N. of 13+59 ϕ 61 st St. + ϕ Ditch		176.92	7.7	169.0	✓
20' N. of 14+55 ϕ Ditch	6.2		170.7	✓	
27' S. of 17+51 ϕ Ditch + Fergus St.	3.4		173.5	✓	
T.P.	10.47	185.15	2.24	174.64	
43' Rt. of 18+60 ϕ Ditch	9.8	185.15		175.5	✓
8' Rt. of 19+32 ϕ 45 th St. on Baseline	7.8		177.3	✓	

185.15

20' Rt. of 21+90 ϕ A	5.7	185.15		179.4	✓
6' Lt. of 23+72 ϕ 62 nd St. P.O.T. Baseline	3.6			181.5	✓
T.P.	7.01	189.47	2.69	182.46	✓
2' Rt. of 25+41 ϕ Ditch	6.1	189.47		183.3	✓
2' Lt. of 26+72 ϕ Ditch 42 nd St.	5.0			184.4	✓
9' Rt. of 28+40 ϕ 63 rd St.	2.5			186.9	✓
9' " " 28+40 ϕ 63 rd St. Floor Bridge	+7.8			197.0	✓
T.P.	9.73	198.23	0.97	188.50	
1' Rt. of 29+59 ϕ Ditch 43 rd St.	7.2	198.2		189.0	✓
10' Lt. of 31+00 = ϕ Ditch	7.0			191.2	✓
14' Rt. of 33+24 ϕ Ditch + stop St. 43 rd St.	4.5			193.7	✓
12' Lt. of 35+00 = ϕ Ditch	3.1			195.1	✓
T.P.	11.08	207.08	2.23	196.00	
15' Rt. of 37+71 P.O.T. ϕ Ditch 64 th St.	8.4	207.08		198.6	✓
45' Rt. of 38+25 = ϕ Ditch	5.3			201.7	✓
36' Rt. of 38+80 = ϕ Ditch	4.9			204.1	✓
14' Rt. of 39+21 ϕ 31 st St. 44 th St. = ϕ Ditch	5.1			201.9	✓
9' Rt. of 41+07 ϕ 47 th St. = ϕ Ditch	3.2			203.8	✓
T.P.	9.47	212.80	3.75	203.33	

35

Encanto Ditch

	212.80			
1. Rt. of 43+14 ²⁶ { { ϕ Ditch { ϕ 65 th St.	212.8	7.5	205.3	✓
1. Rt. of 43+14 ²⁶ { { Floor Bridge	+2.7		215.5	✓
4. Lt. of 45+23 ²⁶ Δ B4 ^o 52' Lt. = ϕ Ditch	4.6		208.7	✓
14. Lt. of 48+00 = ϕ Ditch	1.1		211.7	✓
T.P.	13.02	225.03	0.79	212.01
		225.03	11.1	215.9
28. Lt. of 50+30 ⁵⁰ ϕ Ditch				✓
28. Lt. of 50+30 ⁵⁰ Floor Bridge	3.20		221.8	✓
T.P.				
BM. R.R. Spk Pk. 11.20	231.74	4.49	220.54	4. R.R. at 220.56
26. N. of st. 52+47 ²⁴ R.R. ²⁴ { { Woodman Ave { Produced from S.	231.74	15.4	216.3	ϕ Ditch
18. Rt. of 53+34 ϕ Ditch to E.	13.7		218.0	✓
6.7. Rt. of 53+34 = { { ϕ Ditch to S. { at R.R. Bridge	14.0		217.7	✓ +
Top Rail Ctr. R.R. Bridge	2.75		228.99	✓
Set. BM. on c.T. cont. walk on S.T. line Imperial + W. line Woodman Ave	1.34		230.40	✓
16. Rt. of 55+00 = ϕ cut. Ditch	11.3		220.4	✓
24. Rt. of 56+00 = ϕ " "	9.8		221.9	✓
T.P.	13.19	239.17	5.76	225.98
		239.17	11.1	228.0
19. Rt. of 58+00 = ϕ cut. Ditch				✓
18. Rt. of 60+00 = ϕ " "	7.8		251.3	✓
T.P.	12.88	247.99	4.06	235.11

247.99

12. Rt. of 63+53 ⁴⁵ = ϕ cut. Ditch	9.1	247.99	238.8	✓
18. Rt. of 63+53 ⁴⁵ Δ 9'-0" Lt. floor Bridge	+1.3		249.7	✓
T.P.	10.95	257.90	1.04	246.95
		257.9	18.0	239.9
32. Rt. of 65+00 = ϕ cut. Ditch				✓
33. Rt. of 66+00 " " "	16.5		241.4	✓
29. Rt. of 67+00 " " "	14.5		243.4	✓
15. Rt. of 67+99 ⁹⁵ Δ 18'-06" Lt.	13.1		244.8	ϕ cut. Ditch
25. Rt. of 69+00 = ϕ cut. Ditch	12.0		245.9	✓
30. Rt. of 70+00 " " "	10.6		247.0	✓
28. Rt. of 71+00 " " "	9.9		248.0	✓
10. Rt. of 72+34 ³³ Δ 18'-44" Lt.	8.2		249.7	ϕ cut. Ditch
T.P.	10.80	264.07	4.63	253.27
		264.07	12.5	251.5
26. Rt. of 74+00 = ϕ cut. Ditch				✓
26. " " 75+00 = " " "	11.4		252.6	✓
26. " " 76+00 = " " "	10.4		253.6	✓
24. " " 77+00 = " " "	8.6		255.4	✓
25. " " 78+00 = " " "	7.6		256.4	✓
24. " " 79+00 = " " "	6.5		257.5	✓
23. " " 80+00 = " " "	5.3		258.7	✓
T.P.	7.94	271.13	0.88	263.19
				stab 79+99 ²⁰

271.13

Encanto Ditch

271.13

21' Rt of 81+00 = Cut Ditch	10.9	260.7	✓
20' " " 82+00	9.6	261.5	✓
20' " " 82+85 ⁵⁶ N. City Boundary	8.6	262.5	✓ N. End
T.P.	9.24	272.43	7.94 263.19
B.M. City Boundary Men E. Line Imperial	2.71	269.72	
T.P.	0.17	266.05	4.55 265.88
T.P.	0.29	260.19	7.15 258.90
T.P.	1.30	253.20	7.29 252.90
Set B.M. Top Fire Hydr S.W. Cor 68' + Imperial	4.89	248.31	

Profile for Ditch Bet. Imperial Pavmt. & S.D.R.R. Plat Page 63+64

"C" Line = Imperial Ave Pavmt.

67

B.M. City Men	0.55	270.27	269.72	E. line Imp Ave = 100 + 62.4 + Imperial Ave Pavmt N. City Boundary
28' W = Rt. of 0+00 = Cut Ditch	6.0	270.27	264.27	✓
27' " " 1+00	6.8		263.4	✓
45' " " 2+00	8.1		264.1	✓
36' " " 3+00	8.9		261.3	✓
25' " " 4+00	10.4		259.8	✓
27' " " 5+00	11.7		258.5	✓
T.P. Nail Header	2.49	264.75	8.01 262.26	Sta 5+00
32' W. Rt of 6+00 = Cut Ditch	7.7	264.75	257.0	✓
32' " " 7+00	8.8		255.9	✓
27' " " 8+00	10.3		254.4	✓
30' " " 9+00	11.9		254.8	✓
36' " " 9+31 ²⁰ E.C. " "	12.0		252.7	✓ = 91 + 30 ²⁴ E.C. Imperial Ave Pavmt.
36' " " 10+00	12.5		252.2	✓
T.P.	5.50	258.08	12.17 252.58	
33' Rt. of 11+00 = Cut Ditch	6.8	258.08	251.2	✓
32' " " 12+00	7.5		250.5	✓
34' " " of 13+00	8.3		249.7	✓
40' " " 14+00	10.3		247.7	✓
35' " " 14+55	11.2		246.8	✓

Levels in Encanto Ditch
 Woodman Ave. East.
 S. of Imperial Ave. "B" Line Page 57

245.37

245.37

39

BM Imperial	4.75	235.15	230.40	Page 66.
22.6 Lt. of 0+80 = N. End. Bridge	16.1	235.15	219.0	4. Ditch
12.3 " " 0+80 = ctr. Bridge	6.1		229.0	on paymt.
21 " " 0+80 = S. End. Bridge	16.0		219.1	4 Ditch
27. Rt. " 0+80 = 4 Ditch	15.8		219.3	at L
32 " " 2+00 = " "	13.8		221.5	
54 " " 3+16 = " "	13.9		221.2	W. Line Park Dr
74 " " 3+66 = " "	12.3		222.8	E. Line Park Dr
118 " " 4+66 = " "	11.8		223.3	
175 " " 4+95 = " "	11.1		224.0	
T.P.	11.85	245.37	1.63	233.52
60. Rt. of 7+00 = 4 Ditch	78.4	245.37	226.9	
44 " " 7+66 = 4 " "	17.2		228.1	W. Line Park Dr
33 " " 8+16 = " "	18.2		227.1	E. Line Park Dr
5.7 " " 8+48 ⁵ = Top Wall N. End.	10.1		235.2	
23 " " 8+71 = 4 Ditch	17.5		227.8	
5.7 " " 9+26 = Top. Wall E. End.	8.6		236.7	
9+48 ⁸⁷ = A on Base Line	296-53			Rt.
30. Rt. of 10+00 = 4 Ditch	14.2		231.1	
3. Lt. " 11+00 = " "	16.1		229.2	

20 Lt. of 11+80 = 4 Ditch	15.3	230.0	
11 " " 12+49 ⁴² Δ Base Line	15.2	230.1	on split Δ
T.P. Stupa 9.01	244.96	9.42	235.95
9. Lt. of 13+63 = 4 Ditch	14.1	234.96	230.8
3 " " 14+50 = " "	13.8		231.1
16.7 Rt. " 15+48 ²⁴ on 4 68 th St	12.8		237.1
16.7 " " 15+48 ²⁴ " " " "	4.33		240.63
Base line at 16+50 = 4 Ditch	12.0		237.9
17+81 ¹⁰ Δ Base Line = " "	9.7		235.2
2. Rt. of 18+68 = " "	9.7		235.2
22 " " 19+12 ²⁸ Δ = " "	8.5		236.4
12 " " 20+56 ¹³ Δ = " "	8.1		236.8
14 " " 22+34 = P.I. Ditch to N.	6.6		238.3
T.P. Stub [22+21 ⁵² Pot. B. Line 21+22 ³⁰ "C" Line	1.34	243.62	Page 66.
T.P.	9.71	253.33	243.62
Base line at 23+10 4 Ditch	13.0	253.33	240.3
25. Lt. of 23+20 " "	12.8		240.5
11. Rt. " 23+20 4 cut. Ditch	11.6		241.7
36 " " 23+76 " " "	9.9		243.4
44. Lt. of 23+76 4 Ditch	10.8		244.5

253.33

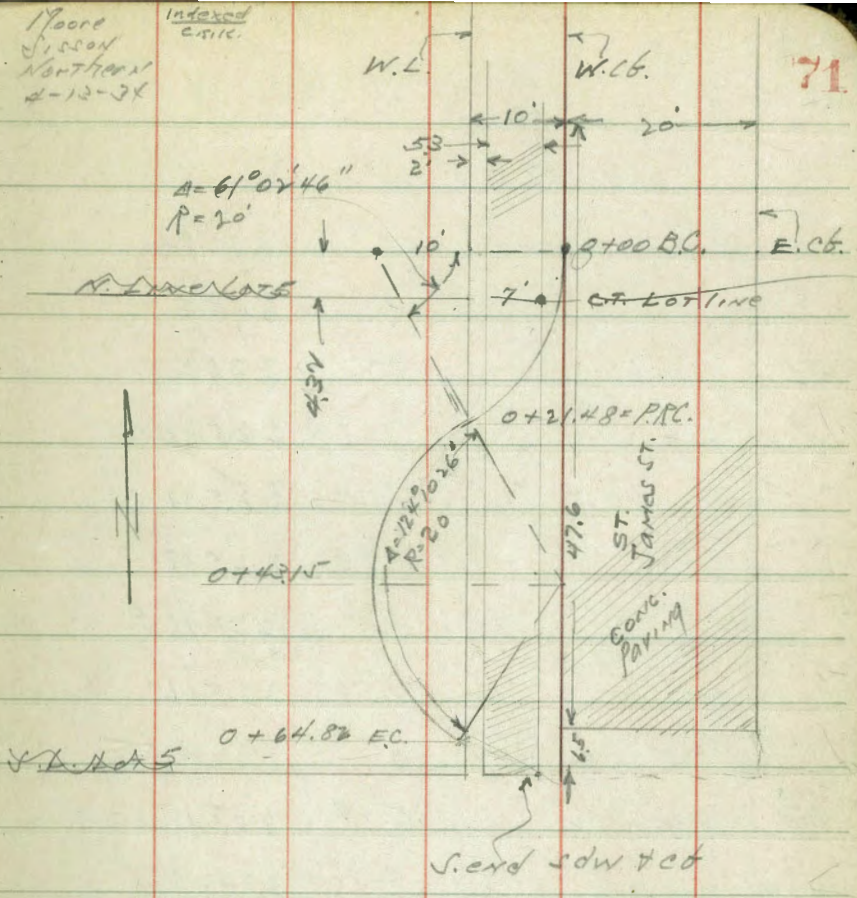
253.33

20

Baseline at 24+26 = ϕ Ditch	10.3	$\sqrt{43.0}$ ✓
38' Pt. of 24+90 = ϕ "	9.4	$\sqrt{43.9}$ ✓ at P.T. of cut. ditch
34' " " 25+50 = " "	10.8	$\sqrt{42.5}$ ✓
Baseline at 25+89 = " "	9.2	$\sqrt{44.1}$ ✓
stub 26+00 \approx 4	5.28	$\sqrt{48.05}$

Levels on Opening on
 Lot 5 Bk 3 Inspiration Hts.
 Note! Sec. taken at Mt. A with St. James

	0.97	244.95	243.98	SWBP Marked St. James
T.P.	1.33	233.46	228.24	237.13
0+00 = B.C. W curb of St. James				
W.L. St. James	4.47	228.99		
+ 2 w/ edge curb walk	4.78	228.68		SW of Mt. Lots
+ 7.5	5.06	228.40		
W of top	5.12	228.34		
gut	5.99	227.47		
+ 10 = § St. James	5.78	227.68		
+ 20 E gut	6.09	227.37		
+ 20 E of top	5.29	228.17		
0 + 21.48 = P.R.C.				
10.32 W of W.C.B.	6.2	227.5		
W of top	6.38	227.08		
gut	7.24	226.24		
§ St. James	7.05	226.41		
gut	7.30	226.16		
E of top	6.62	226.84		



233.46

0 + 43.15 = Crr curve

10' W of WL St. James	7.7	230.8
2 " " " "	3.9	229.5
WL	7.2	226.2
W of top	7.63	225.83
gut	8.35	225.11
E	8.29	225.17
gut	8.48	224.98
E of top	7.80	225.66

0 + 64.84 = EC.

9.7 W of Wcb	8.29	225.17	on Hub
W top of	9.00	224.46	
E	9.2	224.2	
+5	9.6	223.8	
E of dirt	12.0	221.5	
+10	16.3	217.2	
T.P.	12.76	224.89	1.33
of to BM	0.91	223.98	223.98 SW BP

Levels & Location of paving etc.

Moore
Sisson
Northern
v. 11-38

Indexed
C.S.K.

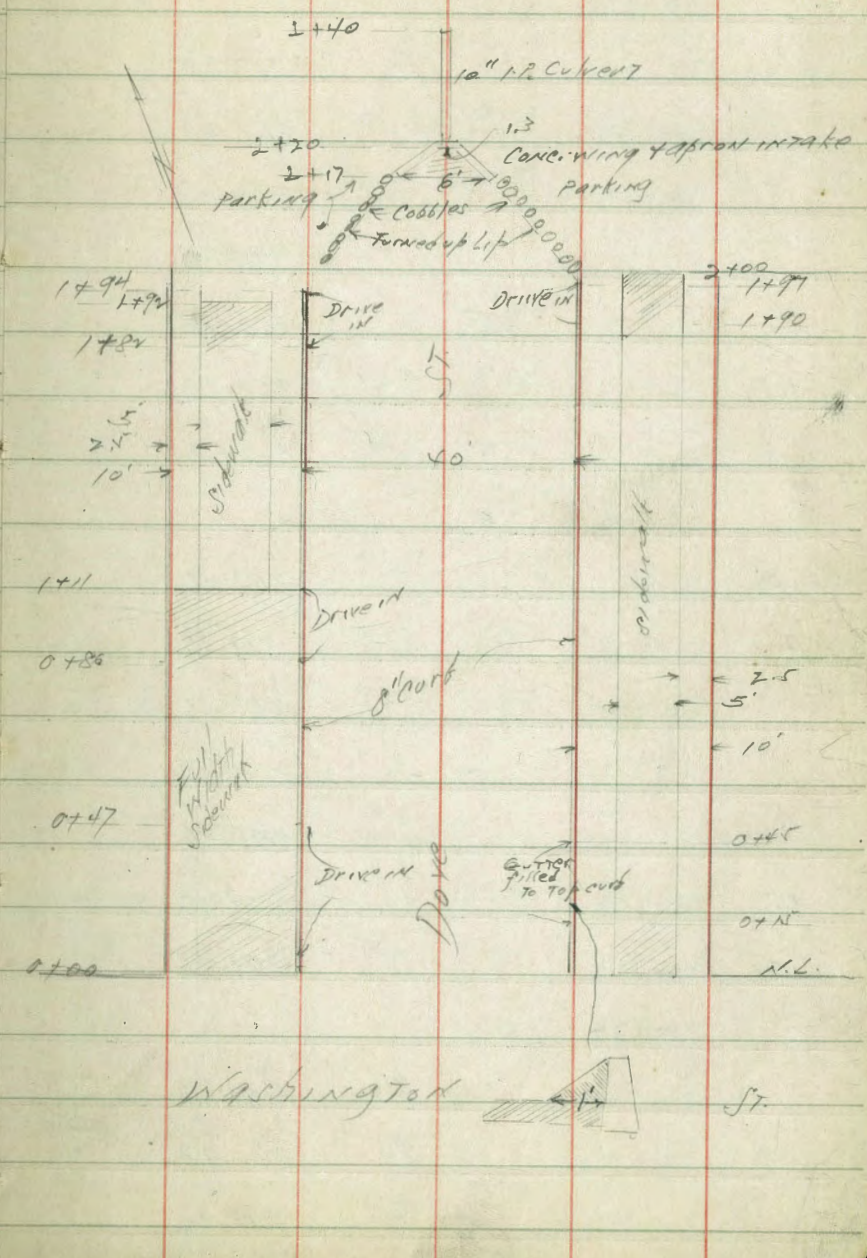
NOTE: on Dove st of Washington

2" Paving = A. Conc. non-skid surface

Eagle + Washington 7.37 270.42 263.06 NEAP

0+00 = N.W. Washington

w cb	5.95	264.48
gut	6.66	263.77
1/4	6.43	264.00
c	6.24	263.99
1/4	6.76	263.67
E gut	7.37	263.06
w cb	6.98	263.45
0+50 = N.W.		
E cb	7.47	262.96
gut	7.85	262.58
1/4	7.37	263.06
c	7.06	263.37
1/4	7.10	263.33
gut	7.45	262.98
w cb	6.92	263.51



270.43

0+80

W cb	7.55	262.88
gut	8.03	262.40
1/4	7.63	262.80
C	7.50	262.93
1/4	7.77	262.66
gut	8.21	262.22
E cb	7.75	262.68

1+00

E cb	8.17	262.26
gut	8.68	261.75
1/4	8.27	262.16
C	8.01	262.42
1/4	8.17	262.26
gut	8.53	261.90
W cb drive	8.51	261.92

1+20

W cb	9.16	261.27
gut	9.51	260.92
1/4	9.17	271.26

270.43

C	8.98	261.45
1/4	9.18	261.25
gut	9.53	260.90
E cb	9.17	261.26

1+50

E cb	10.91	259.52
gut	11.35	259.08
1/4	10.91	259.52
C	10.75	259.68
1/4	10.92	259.51
gut	11.33	259.10
W cb	10.95	259.48
T.P.	3.27	261.17

1+94 = W cb & 1+97 Ecb. taken diag.

W cb - v lip	4.22	256.95
gut	4.45	256.72
1/4	4.12	257.05
C	3.93	258.24
1/4	4.08	257.09
gut	4.42	256.65
2 v lip	4.36	256.81

Dove
No. of Wash.

74

261.17

Dove St

75

2+09

4 Dove	4.78	256.39
8' W gut	5.00	256.17
11' W lip	4.75	256.42
8' E gut	4.98	256.19
11' E lip	4.68	256.49

2+30 Culvert 10" I.P.

inlet F.L.	6.07	255.10
------------	------	--------

2+40

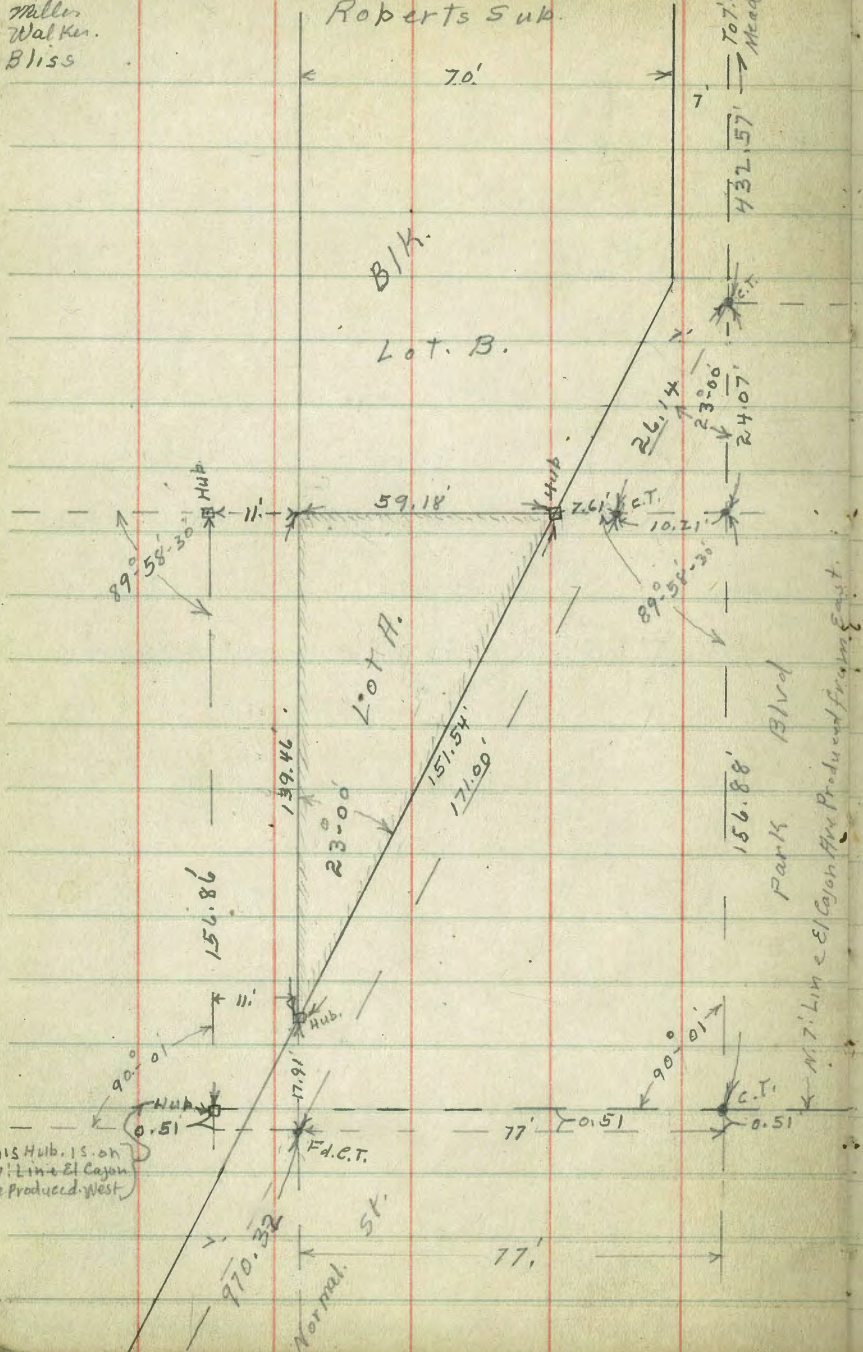
outlet F.L.	12.00	249.17
-------------	-------	--------

T.P. 1203	270.43	327	257.80
-----------	--------	-----	--------

737	263.06	263.06
-----	--------	--------

7-1-35
Miller
Walker
Bliss

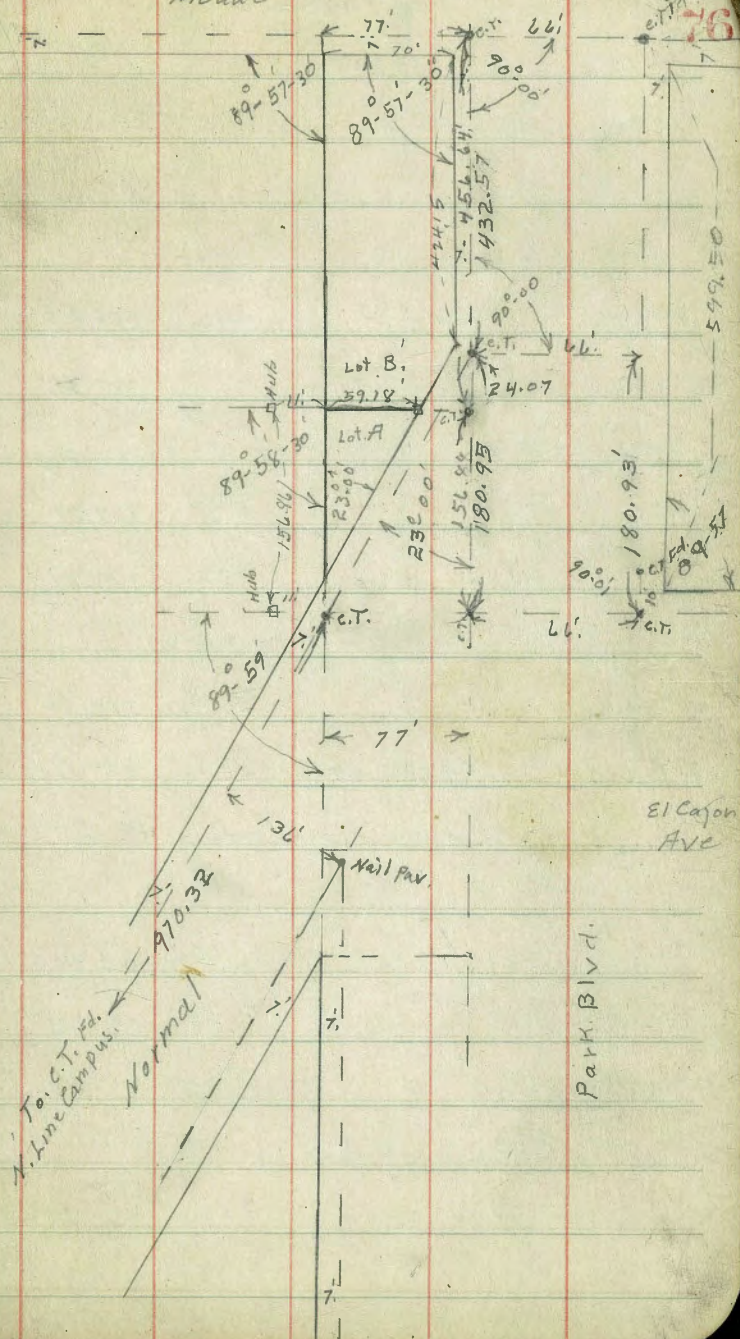
Survey Lot. A. B1K B1K2
Roberts Sub.



Indexed
C.S.K.

Meade

Ave.



76

El Cajon Ave

Park Blvd.

2-9-39 Re. X See Alley B11K 53 U.H.
See Page 22

miller
Walker
Bliss

BM 4.15 379.80 375.65

Old. 1+59 garage on E. dirt floor 3.6 Back

E-3.6 = floor 3.8 376.0 = 75.9 ✓

New 2+24 garage on W. Cmt. floor 12 Back

W-12 = floor 4.93 374.87

W Line - E. End. out apron 4.99 374.81

New. 2+10 N. End. Garage on W. cmt floor on W. Line

W. Line floor 5.49 374.31

+ 2.2 E. End. cmt. apron 5.73 374.02

2+76 S. End. above garage

W Line = floor 5.54 374.26

2.2 E. of W Line = E. End. apron 5.61 374.19

2+82 N. End. Board. Fence 0.4 E. of W. Line

5+16 N. End. New. Garage on E. cmt. floor 7' Back

1' E. of E = W. end. cmt. apron 6.99 372.81

7' E. of E = floor 6.85 372.95

5+36 S. End. above garage

1' E. of E = W. End. cmt. apron 7.12 372.68

7' " " = floor 6.85 372.95

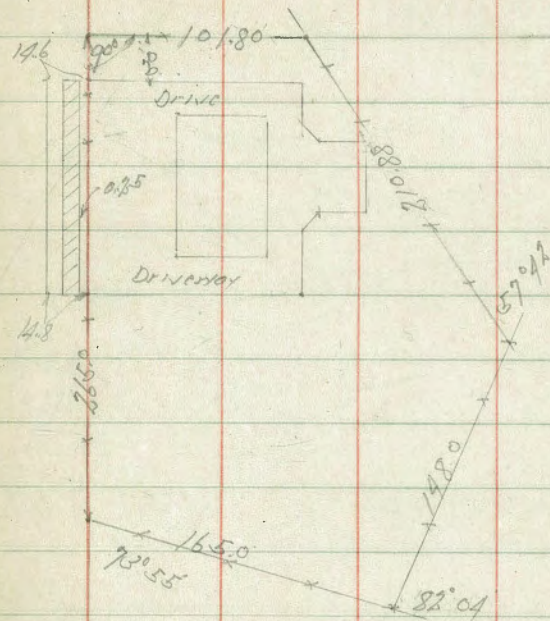
77

373.2
372.8

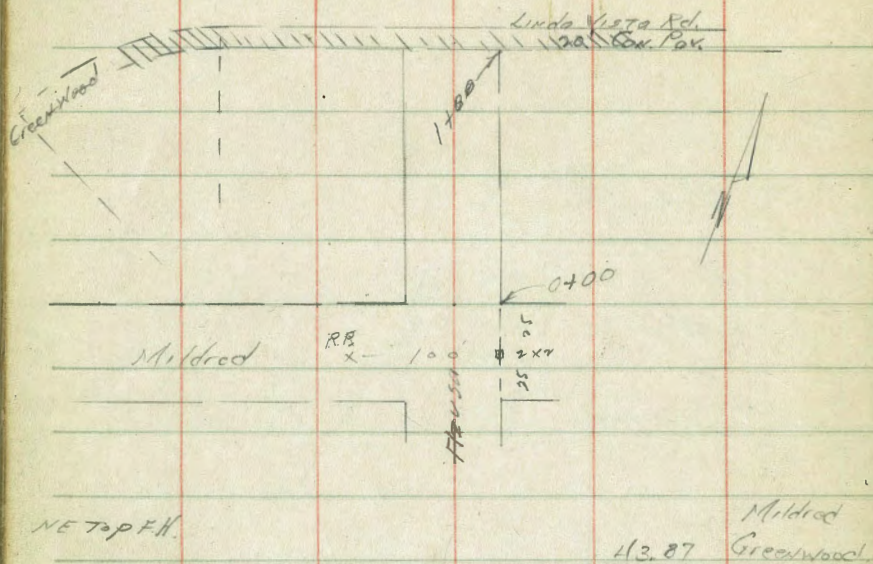
Proposed Fence
San Diego Fire Alarm Station
Balboa Park

April 11-42
Sisson
Northcott
H. Moore

78



x sec Azusa St. 50' wide
Mildred Nly to Hwy. 10' curbs



See FB 1630-37

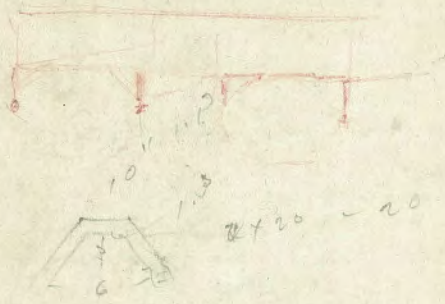
89-60	1.01029	1.01033	50.06	179.62
81-49	178.	178	701191	115
8-11	808232	808264	57	53
14	707203	707231	708337	178.
89-60	101029	101033	505955	
81-12	179.83162	179.83874	57.68	
8-48				27

45.23.96	1359.57	
4314.26	1103.87	108
209.70	255.70	
7		

87.62

33
 40
 14
 22.73
 1177.27
 1526.64
 37.30
 1563.94
 86.06
 1650.00
 136.50
 136.50
 20.
 11.07
 19.13
 10.067
 110
 100.67
 100.67
 110.7425

245.1
 25
 220.1
 293.0
 50
 343.0



603.59
 96.5
 320.
 604.59
 416.5

599.57
 H1MH + 8.5

223.9
 181.5
 42.4
 91-10.2
 163-32
 44.99
 43.0748
 30.20
 11.07
 19.13
 81-45
 9014
 9.82
 51.13
 48.67
 144.
 37.5
 103.82
 1725
 30-42
 89-13
 21-48
 78.52
 28563
 38084
 408403
 100.67
 100.67
 110.7425

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

81-45-30