

1495

LEVEL BOOK

No. 330 F

MICROFILMED  
DEC 24 1964

ENGINEERING DEPARTMENT,  
CITY OF SAN DIEGO,  
CALIFORNIA.

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
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**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
IRVING PARK STATION  
CHICAGO, ILL.

Pershing Drive Extension

See change - page 6

5+14<sup>30</sup> Hub

$\Delta$  35° 34' 15" RT.

3/23/34  
Miller  
Walker  
Bless.

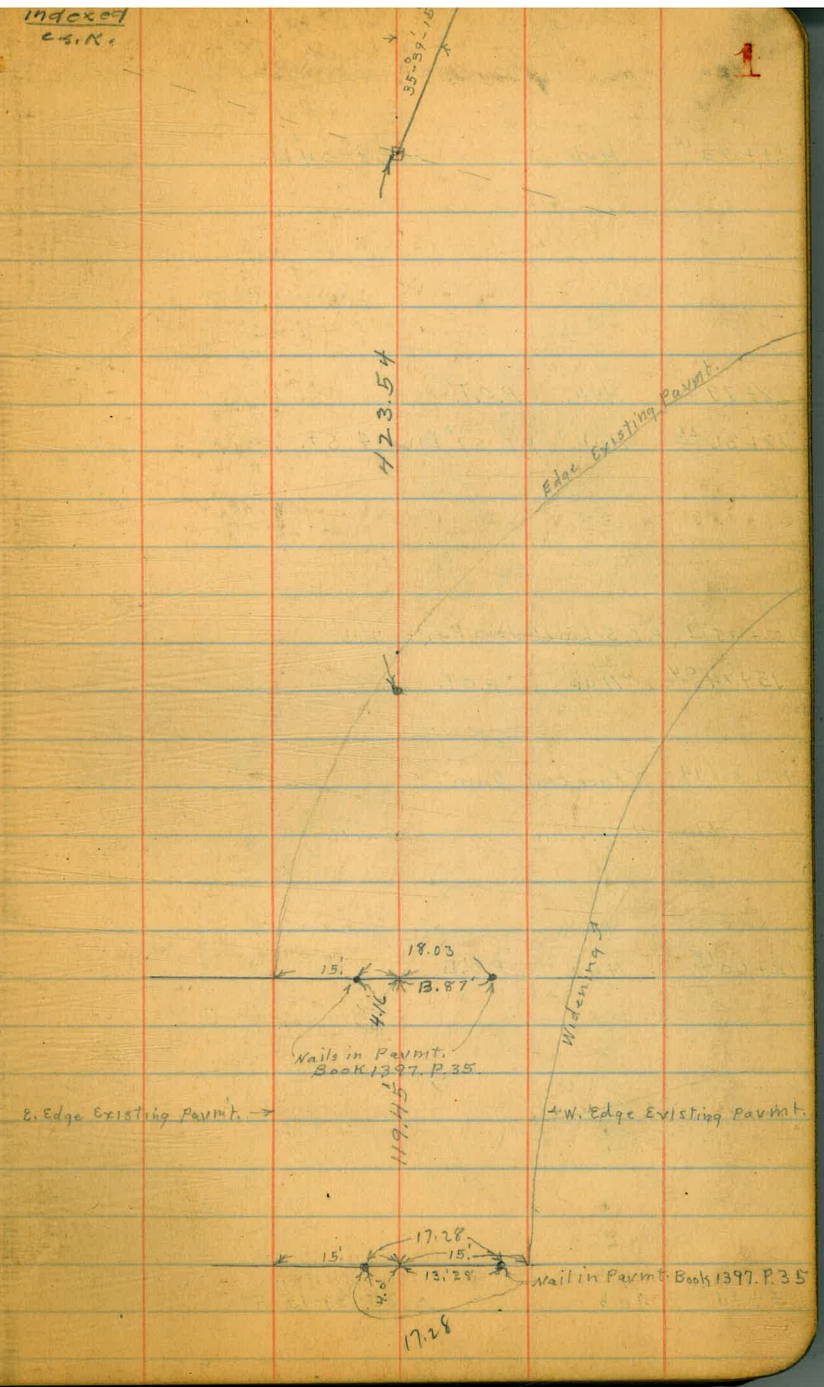
INDEXED  
C.S.K.

1

0+91.90 E. Edge Pavmt.  
0+90.76 Nail in Pavmt.  
1.14

0+00

B.C. Widening Curve on W.



21+53<sup>14</sup> Hub  $\Delta 38^{\circ}04' Lt.$

18+79<sup>01</sup> Hub. P.O.T.

18+36<sup>26</sup> Hub. P.I. S.7' Line A. St.

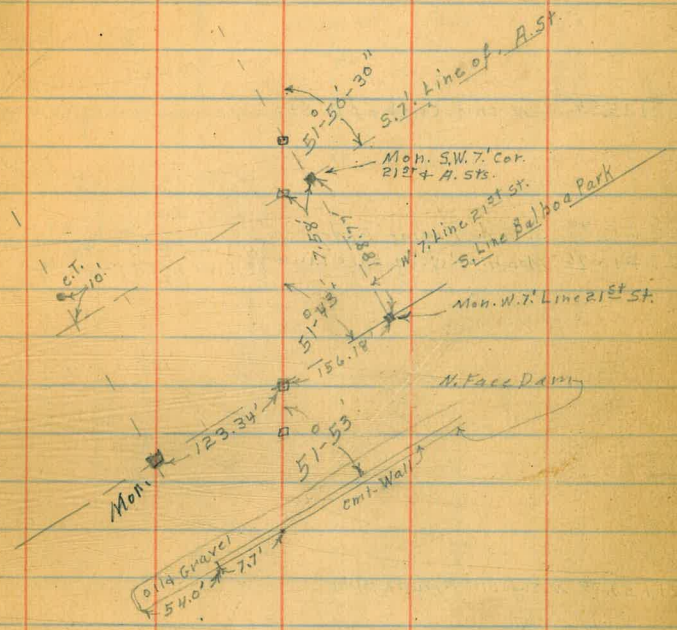
15+95<sup>79</sup> P.I. S. Line Balboa Park Hub

15+74<sup>04</sup> Hub P.O.T.

15+54<sup>44</sup> N. Face cmt. Dam.

12+60<sup>18</sup> Hub. P.O.T. ✓

5+14<sup>30</sup> Hub  $\Delta 35^{\circ}39'15'' Rt.$



25.04  
72.40  
12.64

2 1/2

22+83.96 X in Walk on s. 7' Line of B. St Δ  
22+77.04 = s. Curb of B. St.

22+25.04 N. cmt. Curb of B. St.

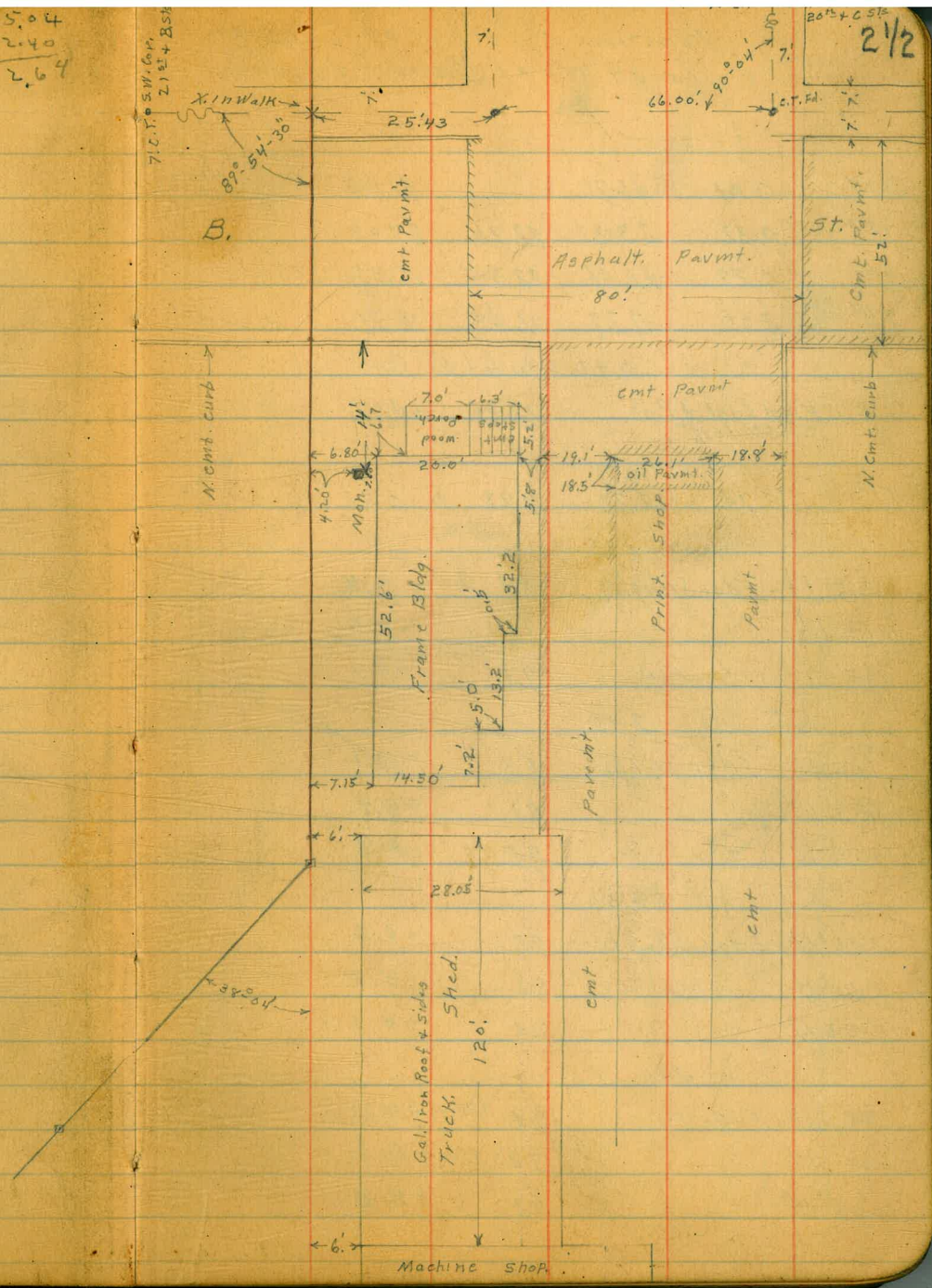
22+12.40 S. End. Frame Bldg.  
22+16.26 Mon 4.20' W. of Base Line

{ N. Line B St. +  
E. Line of City Property.

21+59.80 N End. old Frame Bldg

21+57.18 S. End. Truck Shed.  
21+53.14 Hub Δ 38-04 Lt.

18+79.01 Hub P.O.T.



Location & Levels of Culverts  
& Slough N. of Barnett & Lytton

Indexed  
C.S.K.

4-29-34  
Moore 3

BM	0.01	41.76	41.75	5th BP Rogersquit 24 1/2
TP	0.32	29.32	12.76	29.00
TP	0.29	16.66	12.95	16.37
TP	2.06	7.27	11.45	5.21

0+0 = 1/2 let 48" Pipe

4 1/2 Flat Lye 4" Pipe  
closed 10/18 12.24 -4.97

TP 3.74 3.22 7.79 -0.52

1+0

55' Lt - Edge Slough 6.4 -3.2

60' Lt 8.2 -5.0

65' Lt 7.3 -4.1

2+0

105' Lt - Edge Slough 6.3 -3.1

108' Lt 8.1 -4.9

113' Lt " " 7.5 -4.3

2+50

145' Lt - Edge Slough 7.2 -4.0

150' Lt 8.2 -5.0

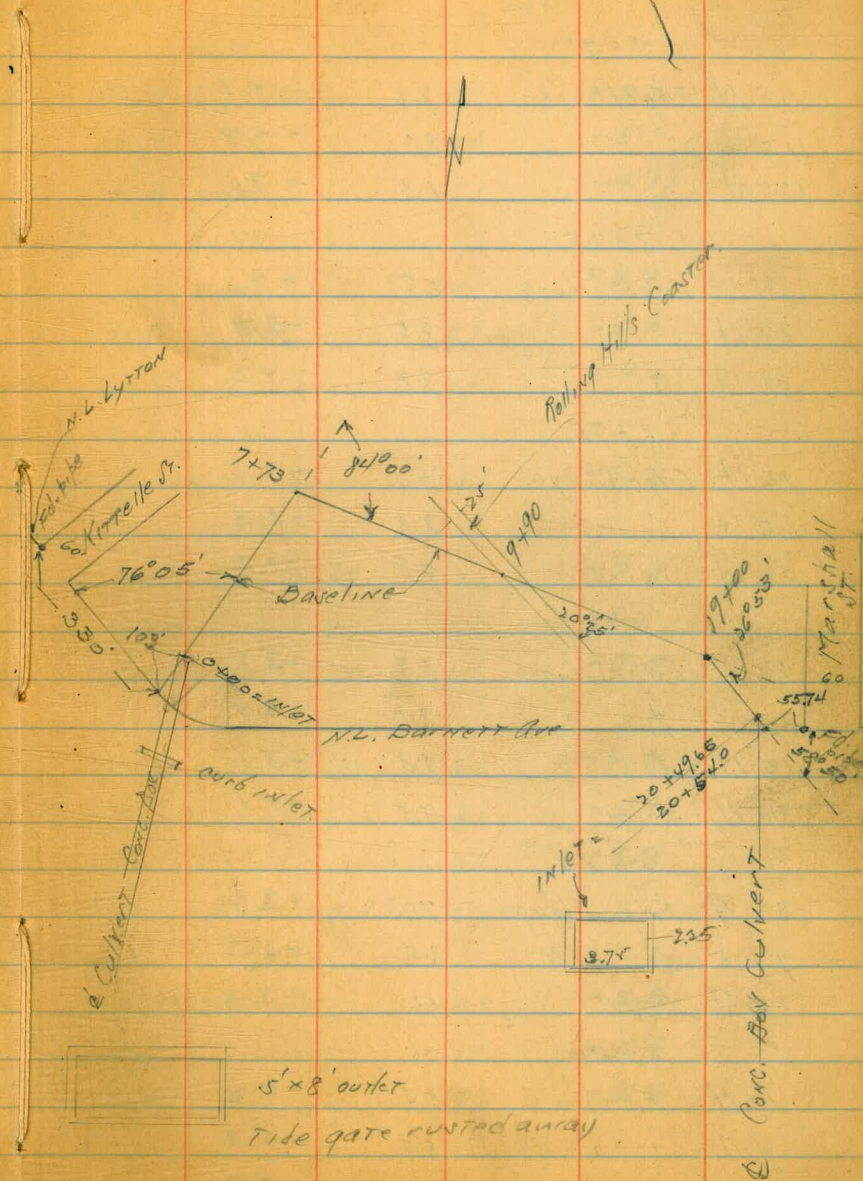
155' Lt " " 7.3 -4.1

3+0

93' Lt - Edge Slough 7.3 -4.1

100' Lt 8.2 -5.1

105' Lt 7.2 -5.0



3-22

3+50

110 Lt - Edge Slough	7.3	- 4.1
115 Lt	8.0	- 4.8
120 Lt	6.8	- 3.6

3+75

40 Lt - Edge Slough	5.8	- 2.6
17 Lt	8.5	- 5.3
52 Lt	7.2	- 4.0

4+75

15 Lt - Edge Slough	5.7	- 2.5
25 Lt	8.5	- 5.3
33 Lt	7.2	- 4.0

5+0

25 Lt - Edge Slough	6.3	- 3.1
35 Lt - 1/2	8.1	- 4.9
65 Lt - 1/2	8.3	- 5.1
75 Lt - Edge	7.3	- 4.1

5+75

80 Lt - Edge Slough	7.0	- 3.8
75 Lt - 1/2	8.5	- 5.3
65 Lt - Edge	6.6	- 3.4

5+50

10 Lt	7.4	- 4.2
1/2	8.5	- 5.3
10 Rt	6.1	- 2.9

3-22

6+0

25 Rt - Edge Slough	6.4	- 3.2
20 Rt	8.4	- 5.2
10 Rt - Edge	7.3	- 4.1

6+50

30 Rt - Edge Slough	7.1	- 3.9
22 Rt	8.2	- 5.0
15 Rt	7.4	- 4.2

6+65

1/2 - 1/2 Slough	8.3	- 5.1
------------------	-----	-------

7+0

40 Lt - Edge Slough	7.0	- 3.8
18 Lt	8.3	- 5.1
55 Lt - Edge Slough	6.7	- 3.5

7+50

27 Lt - Edge Slough	7.5	- 4.3
37 Lt	8.3	- 5.1
46 Lt	7.1	- 3.9

TP	4.02	1.89	5.95	- 2.13
----	------	------	------	--------

8+0

7 Rt - Edge Slough	5.5	- 3.6
14 Rt	6.9	- 3.0
20 Rt	5.7	- 3.8

1.89

8+50

7' Rt = Edgr Slough	5.4	-3.5
15' Rt	6.8	-4.9
22' Rt	5.5	-3.6

9+90

92' Rt Edgr Slough	5.7	-3.8
100' Rt	6.6	-4.7
108' Rt	5.7	-3.8

11+0

160' Rt Edgr Slough	5.6	-3.7
168' Rt	6.7	-4.8
175' Rt	4.4	-2.5

12+0

155' Rt Edgr Slough	5.8	-3.9
165' Rt	6.5	-4.6
170' Rt	5.0	-3.1

13+20

200' Rt Edgr Slough	5.4	-3.5
210' Rt	6.2	-4.3
220' Rt	3.4	-1.5

TP 2.31 1.70	2.50	-0.61
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13+35

1/2 = Edgr Slough	5.6	-3.9
-------------------	-----	------

13+45

1/2 = Slough	6.2	-4.5
--------------	-----	------

1.70

13+55

1/2 = Edgr Slough	5.1	-3.4
-------------------	-----	------

14+0

92' Lt Edgr Slough	5.8	-4.1
--------------------	-----	------

100' Lt	6.8	-5.1
---------	-----	------

105' Lt Edgr	5.8	-4.1
--------------	-----	------

15+0

80' Lt = Edgr Slough	5.9	-4.2
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90' Lt	6.8	-5.1
--------	-----	------

97' Lt	5.5	-3.8
--------	-----	------

15+10

1/2 = Edgr Slough	6.0	-4.3
-------------------	-----	------

15+20

1/2 = Slough	6.8	-5.1
--------------	-----	------

15+30

1/2 = Edgr Slough	5.1	-3.4
-------------------	-----	------

15+50

70' Rt Edgr Slough	5.5	-3.7
--------------------	-----	------

80' Rt	6.6	-4.9
--------	-----	------

90' Rt	5.9	-4.2
--------	-----	------

16+0

73' Rt Edgr Slough	5.8	-4.1
--------------------	-----	------

80' Rt	6.5	-4.8
--------	-----	------

87' Rt	5.8	-4.1
--------	-----	------



170

16+50

1/2	- Edge Slough	5.9	-4.2
-----	---------------	-----	------

16+60

1/2	- 1/2 Slough	6.6	-4.9
-----	--------------	-----	------

16+70

1/2	- Edge Slough	5.9	-4.2
-----	---------------	-----	------

17+0

20 Lt	- Edge Slough	6.0	-4.3
-------	---------------	-----	------

30 Lt		6.6	-4.9
-------	--	-----	------

40 Lt		5.9	-4.2
-------	--	-----	------

17+90

1/2	- Edge Slough	5.7	-4.0
-----	---------------	-----	------

18+0

1/2	- 1/2 Slough	6.5	-4.8
-----	--------------	-----	------

18+10

1/2	- Edge Slough	5.2	-3.5
-----	---------------	-----	------

TP	9.40	6.83	4.27	-2.57
----	------	------	------	-------

18+50

35 Rt	- Extreme High Water Mark	11.3	-4.4
-------	---------------------------	------	------

100 Lt	- Storm Pile	9.7	-2.9
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20+496.5 = End Conc. Box Culvert 2.85 x 3.75

1/2	Flax Line	11.8	-4.35
-----	-----------	------	-------

TP	2.91	6.61	3.13	3.70
----	------	------	------	------

BM			4.95	1.66
----	--	--	------	------

NERP  
Bar 20 ft +  
Width 1.50

893  
222  
1178

5

5 1/2

5/14/34  
 Muller  
 Walker  
 Bliss

Change in Alignment.  
 Pershing Dr. Extension  
 original Page 1  
 "B" Line

Def Ls.

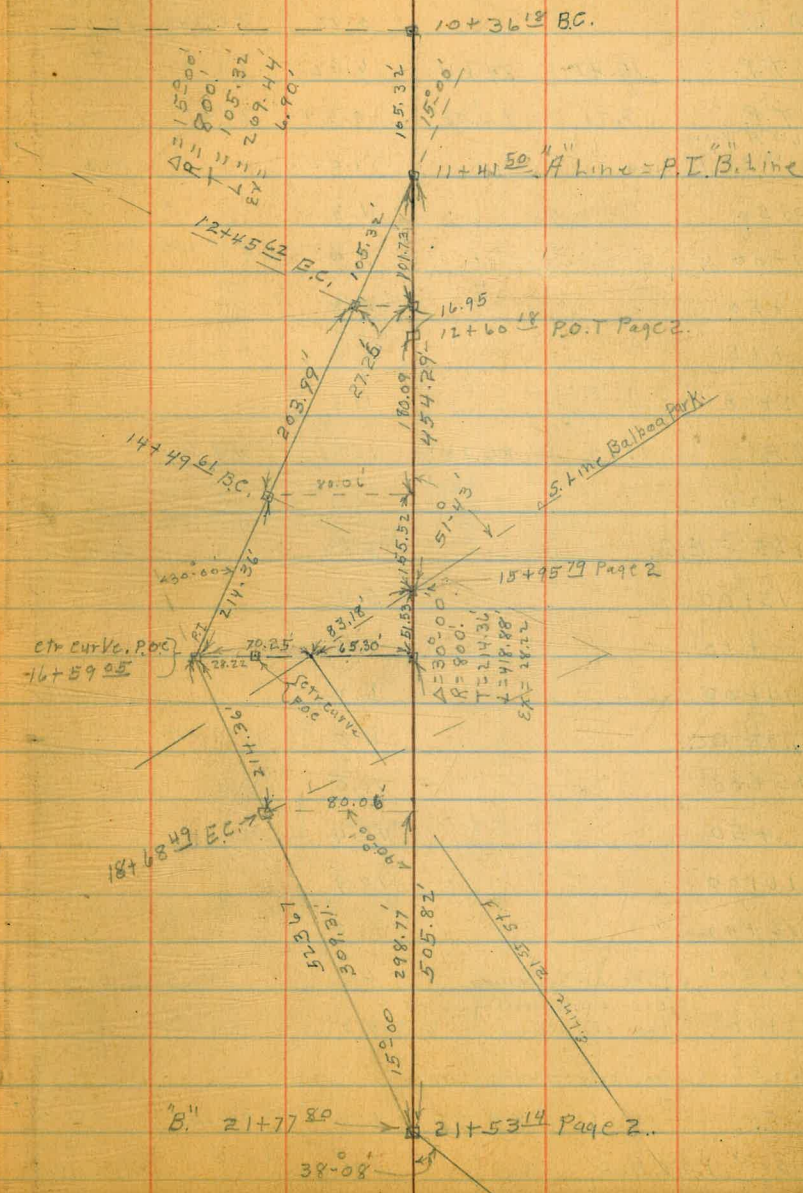
10+36 <sup>14</sup> PC	
10+50	0°-29.69'
	1-47.43
11+00	2°-17.12'
	1-47.43
11+50	4°-04.55'
	1-47.43
12+00	5°-51.98'
	1-38.02'
12+45 <sup>61</sup>	7°-30'

Def Ls.

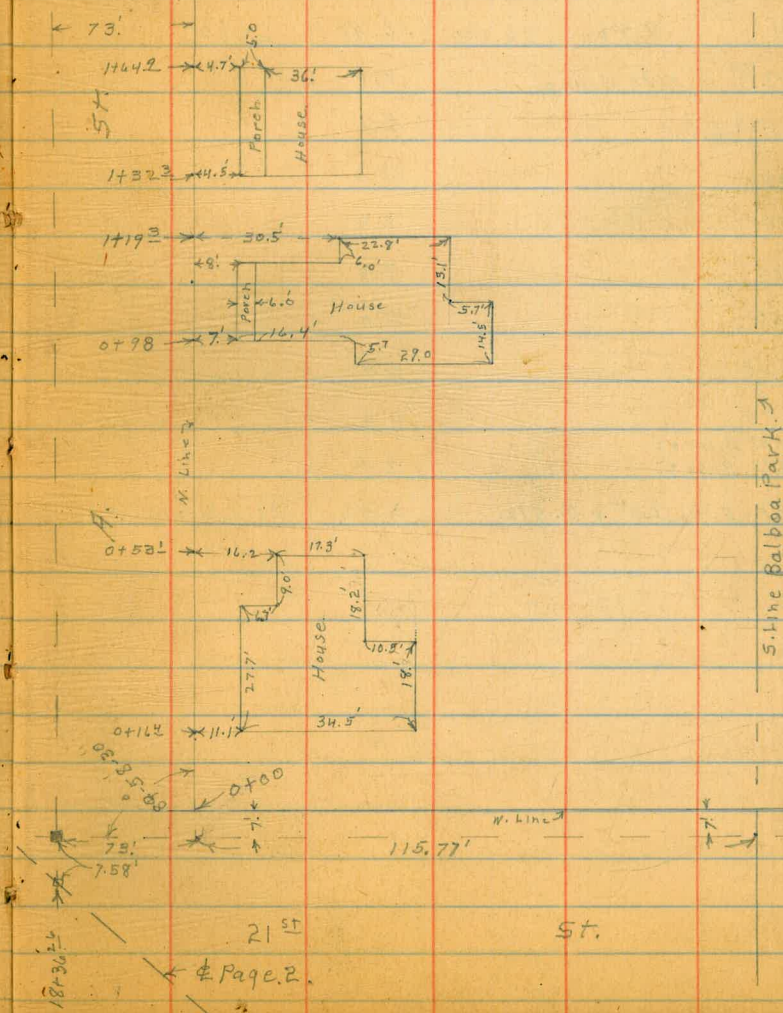
14+49 <sup>61</sup> BC	
15+00	1°-48.27'
	1-47.43
15+50	3°-35.70'
	1-47.43
16+00	5°-23.13'
	2-06.87
16+59 <sup>25</sup> Ctr Curve	7°-30'
	1-27.98'
17+00	8°-57.98'
	1-47.43
17+50	10°-45.41'
	1-47.43
18+00	12°-32.84'
	2-27.16
18+68 <sup>49</sup> EC	15°-00'

Def Ls.

17+76	11°-21.29'	N side Hous.
18+154 <sup>9</sup>	13°-05.12'	S. side Hous.



B.M. Top Fire Hydrant	2.96	76.09	73.13	5 E. 20th + B. Sts.
B.M. B.P.		5.85	70.24	5 E. 20th + B. Sts.
T.P.	15.47	84.64	6.92	69.17
T.P.	7.71	92.08	0.27	84.37
10+36 15" A Line				
10+36 15" B.C. B. Line		1.02		Hub
10+50		1.3		
11+00		3.0		
+50		4.8		
+65		5.8		
12+00		11.1		
T.P.	1.62	80.78	12.92	79.16
+20		4.9		
12+45 6" E.C.		5.63		Hub
13+00		5.4		
+50		5.6		
14+00		6.2		
14+49 4" B.C.		8.5		
15+00		10.0		
+50		10.4		
16+00		10.9		
16+42		11.0		
16+50 1" Face cmt. Dam		6.9		
16+50 3" Base of oil screening Lip		4.9		
16+57 Top. oil screenings Lip		1.7		
T.P.	4.66	83.71	1.73	79.05
16+59 05" P.O. C. Hub		4.91		ctr Curve



83.71

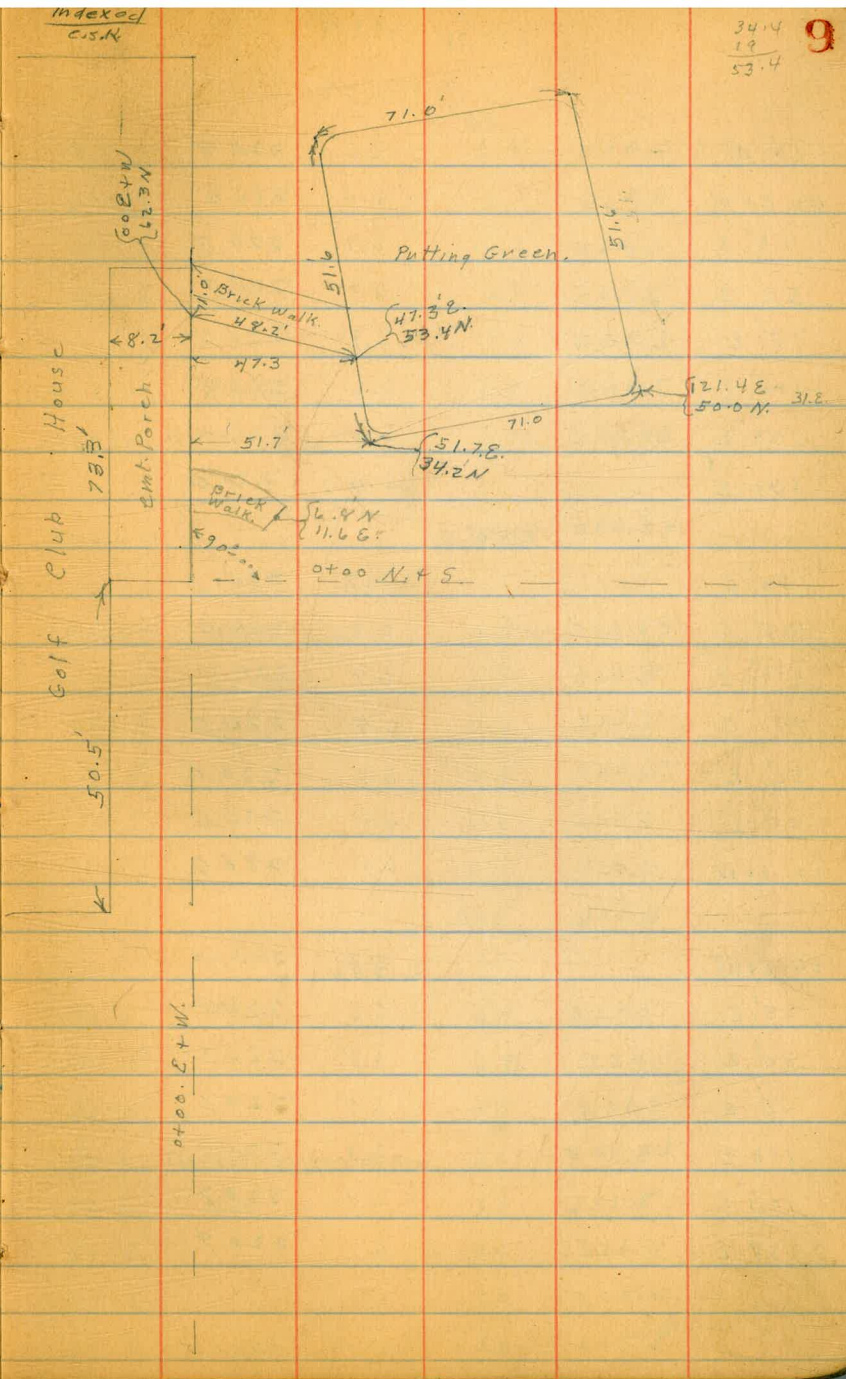
16+67			4.8	
16+81			14.2	
17+00			14.6	
+50			16.1	
+76 = N. side House			16.4	
T.P.	8.82	76.12	16.41	67.30
18+15 <sup>49</sup> S. side House.			8.8	
18+68 <sup>49</sup> E.C.			9.6	
19+00			10.0	
+50			9.5	
20+00			9.5	
+50			8.0	
21+00			5.8	
+50			4.2	
21+77 <sup>80</sup> B. Line =			4.0	
21+53 <sup>14</sup> Page 2.				
R.M. B.P. S. E. 20 <sup>th</sup> + B. Sts.			5.86	70.26 = 70.24

5-18-34 2 sec. Parking Area E. of  
Municipal Golf Club House

34.4  
19  
53.4  
9

B.M. B.P.	10.13	218.08		207.95
Stub 28 <sup>th</sup> + Date			1.96	216.12
T.P.	5.88	223.75	0.21	217.97
T.P.	6.07	223.52	6.20	217.45
T.P.	4.54	227.38	0.68	222.84
		125' S.		
20' W.			5.5	221.9
0+00 E+W			5.4	222.0
25' E			5.0	222.4
50' E = N. Edge Ex Road			4.4	223.0
75' E	"	"	3.4	224.0
100' E	"	"	3.2	224.2
125' E			3.9	223.5
150' E			4.7	222.7
		100' S.		
150' E			5.4	222.6
125' E			5.3	222.1
100' E			4.5	222.9
75' E			5.2	222.2
50' E			6.0	221.4
25' E			6.1	221.3
0+00 E+W.			6.3	221.1
11' W			6.5	220.9

S.W. Dale  
& Granada



227.38

75' S

10' W	6.6	220.8
00. E+W	6.4	221.0
25' E	6.7	220.7
50' E	6.7	220.7
75' E	6.9	220.5
100' E	6.6	220.8
125' E	6.4	221.0
150' E	6.4	221.0

50' S

150' E.	7.1	220.3
125' E	6.8	220.6
100' E	6.9	220.5
75' E	6.8	220.6
50' E	6.8	220.6
25' E	6.8	220.6
00. E+W	6.8	220.6

25' S

00. E+W	6.9	220.5
25' E.	6.6	220.5
50' E	6.8	220.6
75' E	6.8	220.6
100' E	6.7	220.7
125' E	6.7	220.7
139' E	6.7	220.7

227.38

00. N+ S

128 E.	6.8	220.6
100' E	6.7	220.7
75' E	6.8	220.6
50' E	6.9	220.5
25' E	7.1	220.3

00. E+W	ground.	6.9	220.5
00. E+W	= 5' E, Cor. ent. Porch	6.92	220.46

6.8 N.

11.6 E =	{ 2' End. Brick walk 9' Wide	7.15	220.23
----------	---------------------------------	------	--------

25' N

00. E+W	= 8' Edge Porch.	6.91	220.47
00 E+W	ground	6.9	220.5
+ 25' E		7.1	220.3
50' E		6.9	220.5
75' E		6.8	220.6
100' E		6.7	220.7
131' E		6.8	220.6

34.2 N

131' E		6.9	220.5
100' E		6.9	220.5
75' E		6.9	220.5
56' E	Top ent. Wall putting green	5.57	221.81
56' E	Lawn " "	5.9	221.5
51.7 E		7.0	220.4
25' E		7.0	220.4
00. E.	ground.	7.0	220.4

10

227.38

50' N.

131' E		6.9	220.5
121' 4 E		6.8	220.6
117' E	Top amt. wall Pulling green	5.38	222.00
117' E	Lawn " "	5.8	221.6
48' E		7.0	220.4
25' E		7.0	220.4
00. E+W.	ground	7.0	220.4
00. E+W.	E. Edge Porch.	6.89	220.49
	53.4 N.		
47.3 E	S. Edge Brick walk at E. End	6.94	220.44
47.3 E	ground.	7.2	220.2
	57' N		
25' E.	ground.	7.3	220.1
	62.4 N.		
00. E+W.	S. Edge Brick walk E. Edge amt. Porch	6.93	220.47
00 E+W.	ground.	7.1	220.3



5-31-34 Levels N.E. Cor. Univ. + Normal  
 Miller  
 Walker  
 Bloss.

12  
 7.33  
 5.33  
 7.33  
 26.00

Univ Ave

B.M. B.P. 4.94 307.62 307.62 302.68 S.W. Univ + Herbert.

100' E. of E. line Normal

N. ent. cl Univ	4.67	302.95	✓
gutter	5.34	301.48	✓
8' S.	4.93	301.69	✓
18.8 S = N. Rail.	4.75	302.87	✓

50' E. of E. line Normal

N. ent. cl Univ	4.87	302.75	✓
gutter	5.58	302.04	✓
8' S.	5.15	302.27	✓
18.8 N. Rail	5.03	302.59	✓

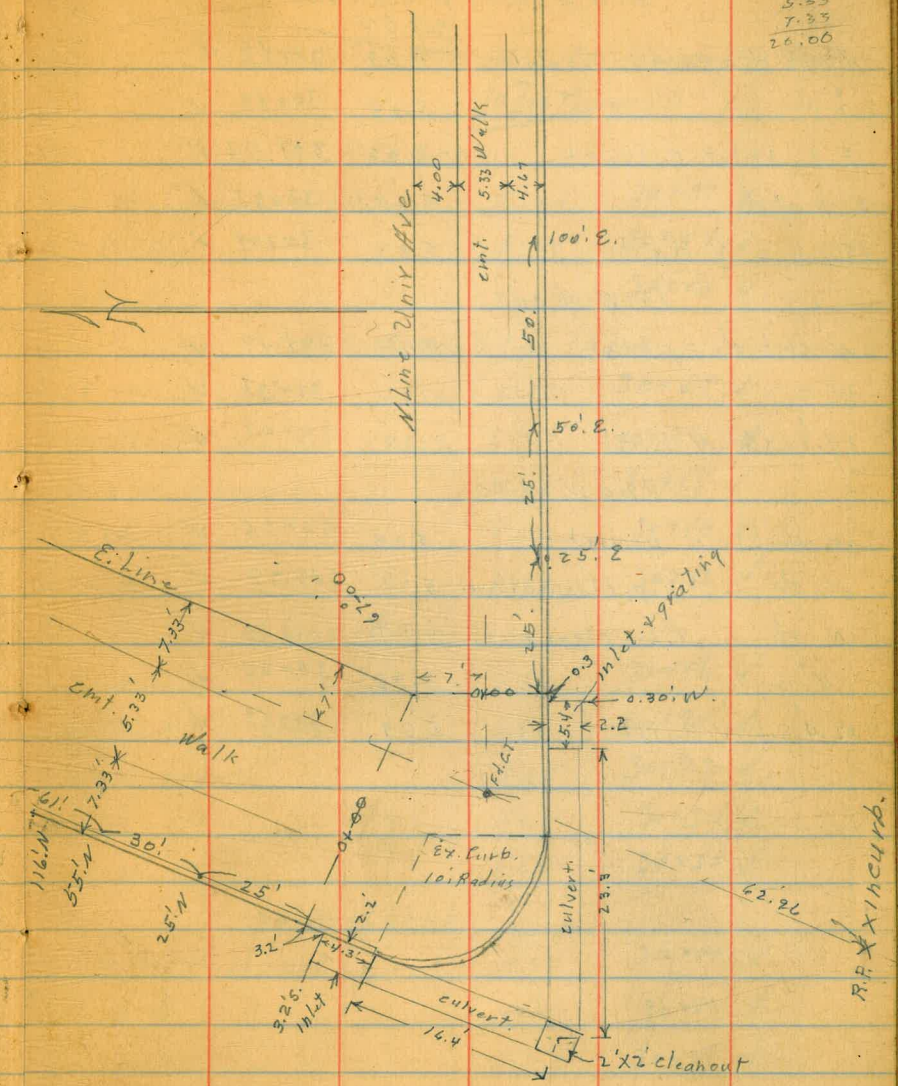
25' E. of E. line Normal

N. ent. cl. Univ	5.01	302.61	✓
gutter	5.69	301.93	✓
8' S.	5.46	302.16	✓
17.9 S = N. Rail	5.17	302.45	✓

0+00 = 90° 00' From N.E. Cor Univ + Normal

0.3' W. of 0+00 = E. end. in let.

N. ent. cl.	5.71	302.51	✓
gutter to E. + Top grating	5.78	301.84	✓
" under grating	6.07	301.55	✓
2.2' S. " "	6.07	301.55	✓
2.2 S. pavmt. to E.W. + S. + Top grating	5.76	301.86	✓
8' S. of el.	5.44	302.18	✓
16.1 S " " = N. Rail	5.33	302.29	✓



307.62

5.7' W. of 0+00 = W. End. Inlet

	307.62		
N. ent. cl. Pavmt. = Top grating	5.09	30253	✓
2.2' S. = " = " "	5.04	30258	✓
F.L. Inlet culvert.	6.08	30154	✓
8' S. of cl.	5.29	30253	✓
15.7' S. = N. Rail	5.33	30229	✓
15' W. of 00			
N. ent. cl. = pavmt.	5.13	30249	✓
8' S.	5.26	30236	✓
14.9' S. = N. Rail	5.35	30227	✓
29' W. of 00			
N. cl. Line pavmt.	5.28	30234	✓
N. cl. " Top. cleanout cover	5.25	30237	✓
N. cl. " F.L. cleanout.	6.59	30103	✓
8' S.	5.38	30224	✓
12.4' S. = N. Rail.	5.39	30223	✓

307.62  
Normal. St. Levels

13

0+00 = 90° 00' from N. E. Cor Univ + Normal.

307.62

17' S. of 0+00

E. cl. Line on pavmt	5.25	30237	✓
8' W.	5.18	30244	✓
16' W.	5.22	30260	✓

7.5' S. of 0+00 = S. End. Inlet

E. ent. cl. = pav.	5.17	30245	✓
gutter = F.L. Inlet	6.20	30142	✓
2.2' W. = pavmt.	5.07	30255	✓
8' W.	5.12	30250	✓
16' W.	5.09	30253	✓

3.2' S. of 0+00

E. ent. cl.	5.16	30246	✓
gutter + F.L. Inlet.	5.88	30174	✓
2.2' W. pavmt.	5.85	30177	✓
8' W.	5.28	30234	✓
16' W.	5.08	30254	✓

25' N. of 0+00

gutter - cl. gone	5.60	30201	✓
8' W.	5.40	30222	✓
16' W.	5.23	30239	✓

307.62

14

55' N. of 0+00

307.62 ✓

E. emf. el	4.52	30310	✓
gutter	5.29	30233	✓
8' W.	5.20	30202	✓
16' W.	5.03	30259	✓

116' N. of 0+00.

E. emf. el	3.95	30367	✓
gutter	4.63	30299	✓
8' W.	4.63	30299	✓
16' W.	4.51	30311	✓

The image shows an open notebook with two facing pages. The pages are cream-colored and feature light blue horizontal ruling. Each page has two vertical red margin lines, one on each side of the center fold. The notebook is lying flat on a grey surface. At the bottom of the frame, there is a white strip, possibly a piece of paper or tape. The number '15' is printed in red in the top right corner of the right-hand page.

Proposed Road  
 Pershing Drive to Municipal Golf Course  
 Club House

Rt.

Indexed  
 C.S.R.

Sept 12-34  
 Moore  
 S. 4002  
 Northland 16

9+56.85 P.O.T. Nail

4+58.15 P.O.T.

2+69.65 EC 15° 27'

+50 14° 19' 42.5"

A 30° 54'

2+0 R 500.0 11° 27' 54"

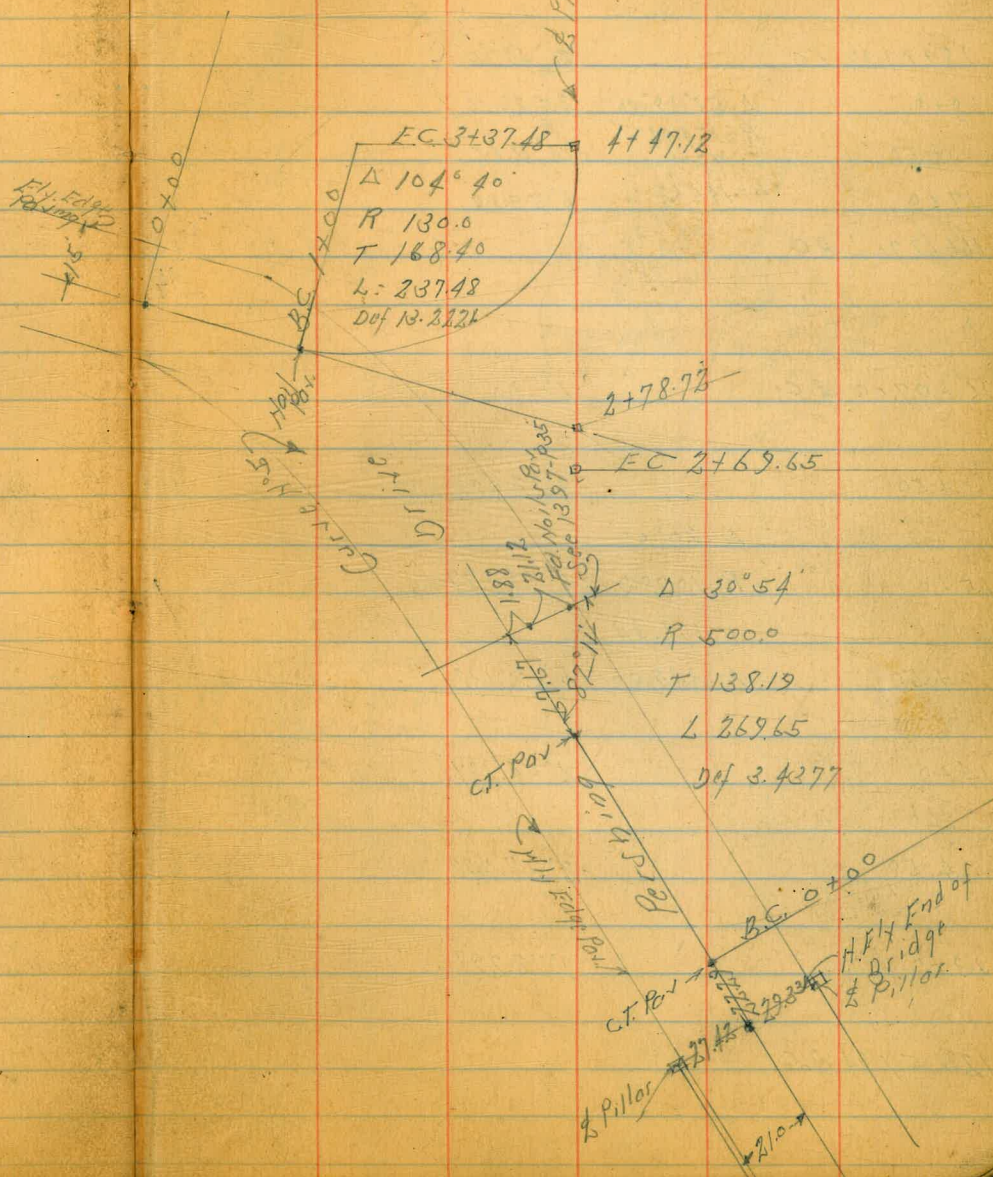
T 138.19

+50 L 269.65 8° 35' 65.5"

1+0 5° 43' 77"

+50 2° 51' 88.5"

0+00 BC



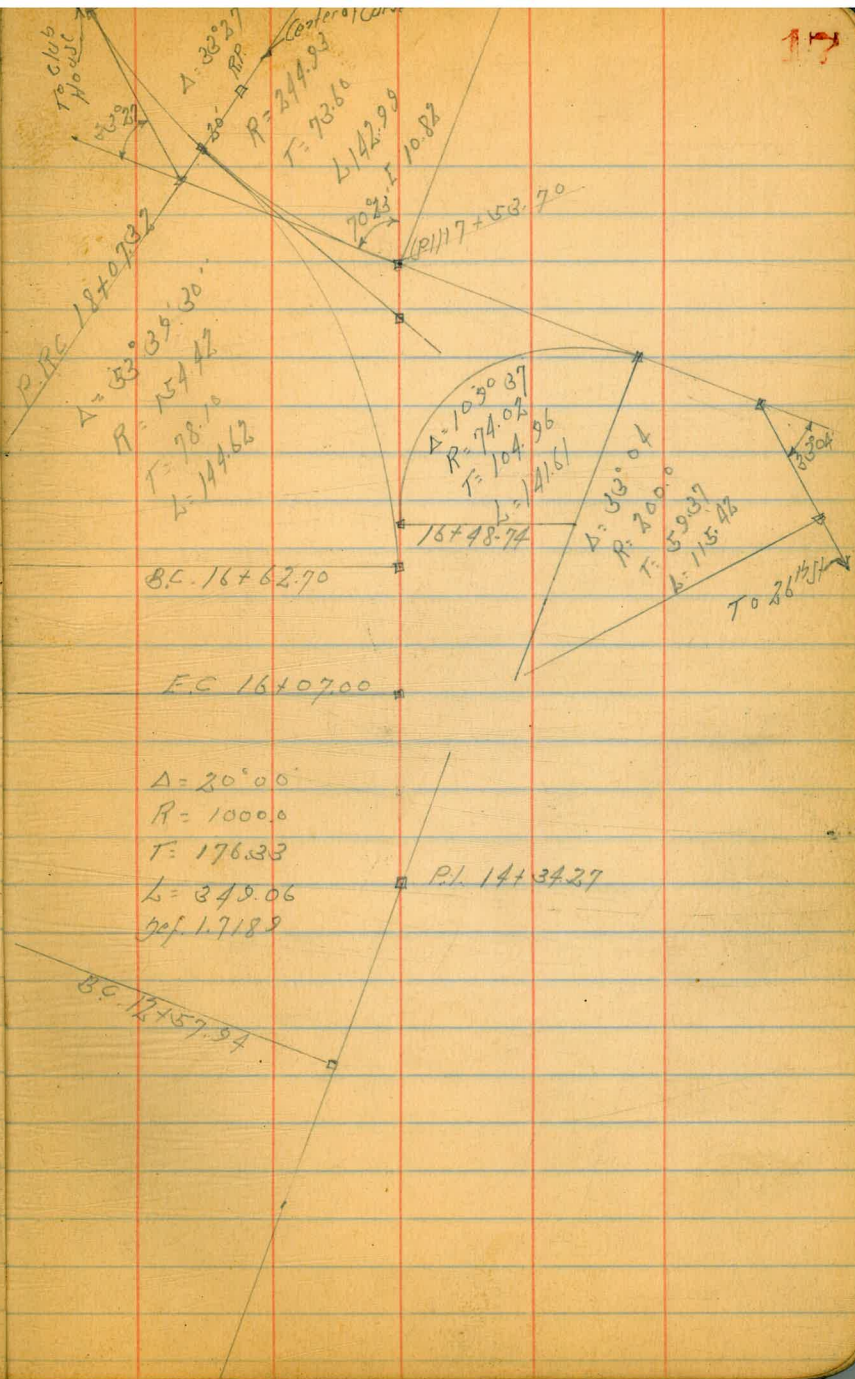
EC 3+37.48 4+47.12  
 $\Delta$  104° 40'  
 R 130.0  
 T 168.40  
 L 237.48  
 Def 13.2121

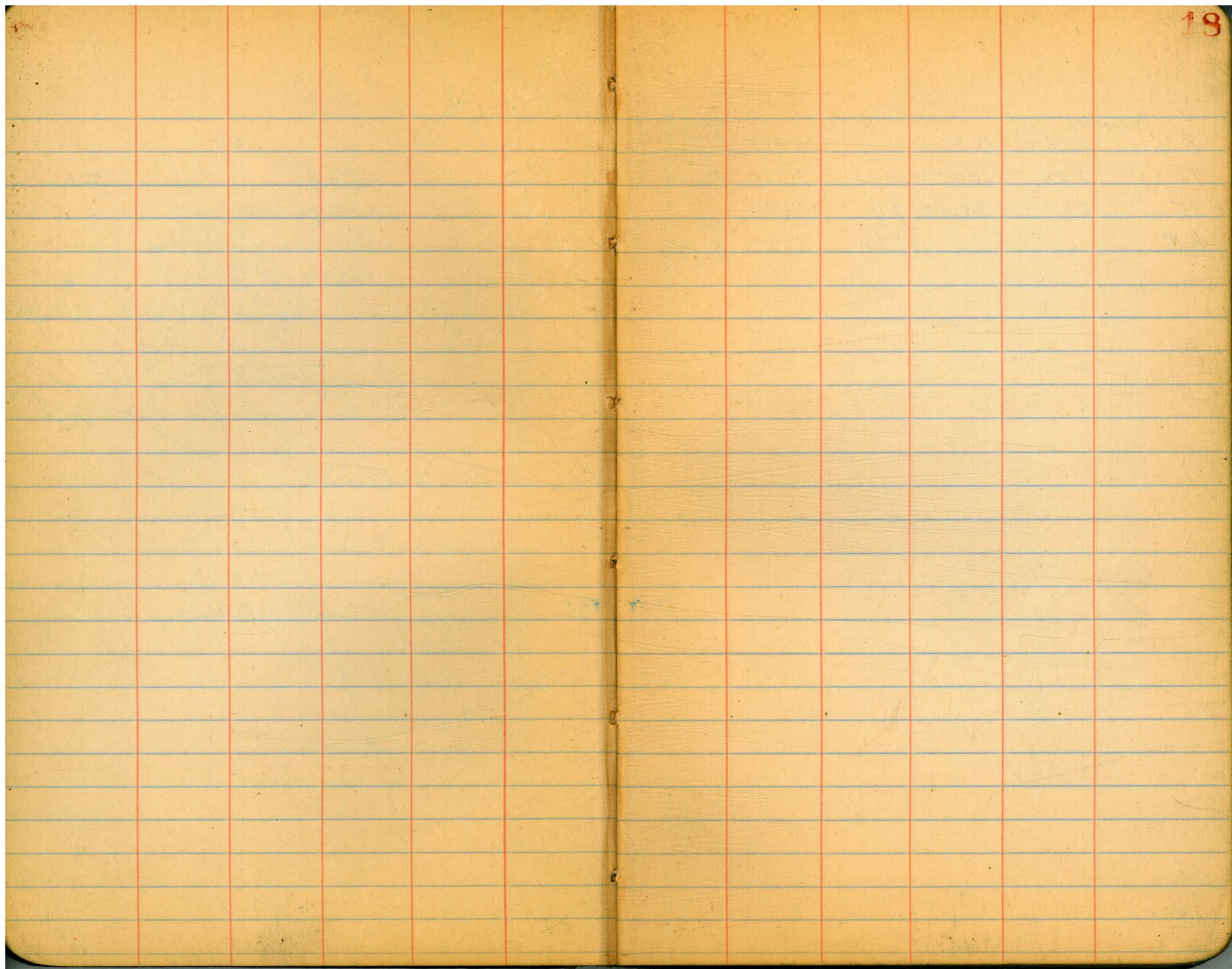
2+78.72  
 EC 2+69.65

$\Delta$  30° 54'  
 R 500.0  
 T 138.19  
 L 269.65  
 Def 3.4277

BC 0+00  
 H.F. End of  
 Bridge  
 & Pillar

18+07.32 E.C.  $26^{\circ}42.75'$   
 18+0  $\Delta: 53^{\circ}39'30''$   $25^{\circ}28.16'$   
 +50  $R=154.42$   $16^{\circ}11.65'$   
 $T=78.10$   
 17+0  $L=144.62$   $6^{\circ}55.15'$   
 16+62.76 B.C.  
 16+07.00 E.C.  $10^{\circ}00'$   
 +50  $8^{\circ}22.022'$   
 $\Delta 20^{\circ}00'$   
 15+0  $R 1000.0$   $6^{\circ}56.097'$   
 $T 176.33$   
 +50  $L 349.06$   $5^{\circ}30.132'$   
 14+0  $4^{\circ}04.187'$   
 +50  $2^{\circ}38.242'$   
 13+0  $1^{\circ}12.297'$   
 12+57.91 B.C.





B.M.	0.26	109.03		108.77	Hub Guard 3004946
TP	2.59	100.50	11.12	97.91	on SF Cor Pipe Fence
TP	2.11	95.50	7.11	93.39	
BM			6	7.79	Spk Power Ho Jet Power Ho Cement Forbing 87.59



Levels Proposed Road  
Pershing Drive to Municipal Golf Course  
Club House

9-13-04 **20**

Lt.

S

Rt.

+69.65 F.C.

89.3  
88

+50

88.7  
88

2+0

88.1  
7.7

+50

88.1  
7.7

+47 = Edge Pav.

88.3  
7.37

1+0

87.08  
8.42 on Pav.

+50

86.6  
8.81 on Pav.

0+00

B.C.

85.5  
8.95 on Pav.

95.50 B/Ford.

95.50

+50

+2.5 = Prop. C/v

+75

540

+58.15

TP      5.17      100.55      0.12      95.38

440

+50

340

95.50

2

10.4  
90.2

11  
88.95

11  
88.0  
301.10

85.5  
115.5

2.5  
98.1  
100.65

✓

6.1  
91.9

6.7  
91.8

5.2  
90.3  
96.50

+

TP	12.53	134.20	0.17	121.67
----	-------	--------	------	--------

+50

115.5
6.0

121.84

TP	12.95	121.84	0.85	108.85
----	-------	--------	------	--------

104.7

5.0

109.20

8+0

TP	11.79	109.70	2.64	97.91
----	-------	--------	------	-------

Top Pipe  
Force  
12.47+0

98.7

1.0

+50

96.7

0.0

7+0

+50

93.3

2.0

6+0

93.3

2.0

5+60

92.0

0.6

100.55

100.65

+70

10.7

8  
120.7  
10.7  
131.41

TP 9.73 131.41 12.97 121.68

+50

8.4 126.3

+30

8.8 131.9

TP 0.62 134.65 6.93 134.03

134.65

10+0

1.7 139.3

+75

0.2 140.8

+50

1.4 142.96

TP 9.02 140.96 2.26 131.94

140.96

9+0

134.20

2.8 141.4  
134.20

2

TP 12.03 155.18 0.35 143.15

1210

142.9  
0.6  
143.50

TP 12.73 143.50 0.64 130.77

+65

132.9

+60

130.6

+50 - 1/2 Canyon Road

125.9

+25

124.9

1170

119.6

10+90 = Prop. Calc 12.93

118.78  
12.93  
131.71

131.41

+50

+25

13+0

TP	12.74	192.14	0.69	179.40
----	-------	--------	------	--------

+75

TP	12.65	180.09	0.16	167.44
----	-------	--------	------	--------

+57.24 B.C.

+50

12+35

TP	12.48	167.60	0.06	155.12
----	-------	--------	------	--------

155.18

8  
0.6/191.8

5.4/188.7

9.2/182.5

192.14

4.2/176.9

180.09

166.18  
1.42  
0.1/Hub

6.1/161.5

11.6/156.0

167.60



+75

+60

+50

+25

TP 10.51 210.72 354 200.28

15x0

+50

14x0

TP 11.85 203.82 0.17 191.97

192.14

8

14.6 196.3

11.6 199.5

11.4 199.4

8.6 201.9

210.72

11.5 201.3

11.6 200.6

7.2 196.6

203.82

+50

5

2120.8

1740

2128.9

+62.70 BCLH

216.38  
6.18  
02/1/03

+55

215.7

16+4870 BCPH

213.37  
9.19  
07/1/03

TP 12.75 222.86 0.68 210.11

222.86

+20

200.0  
10.0

16+070 FC

195.3  
15.5

210.79

210.79



B.M.

4.79 218.07

0.7 Conc. Head  
Wall Cul. (217.95)  
(Coverts)

18707.32 P.R.C.

222.75  
0.11 0.5706

1810

0.3 222.6

222.86

222.86

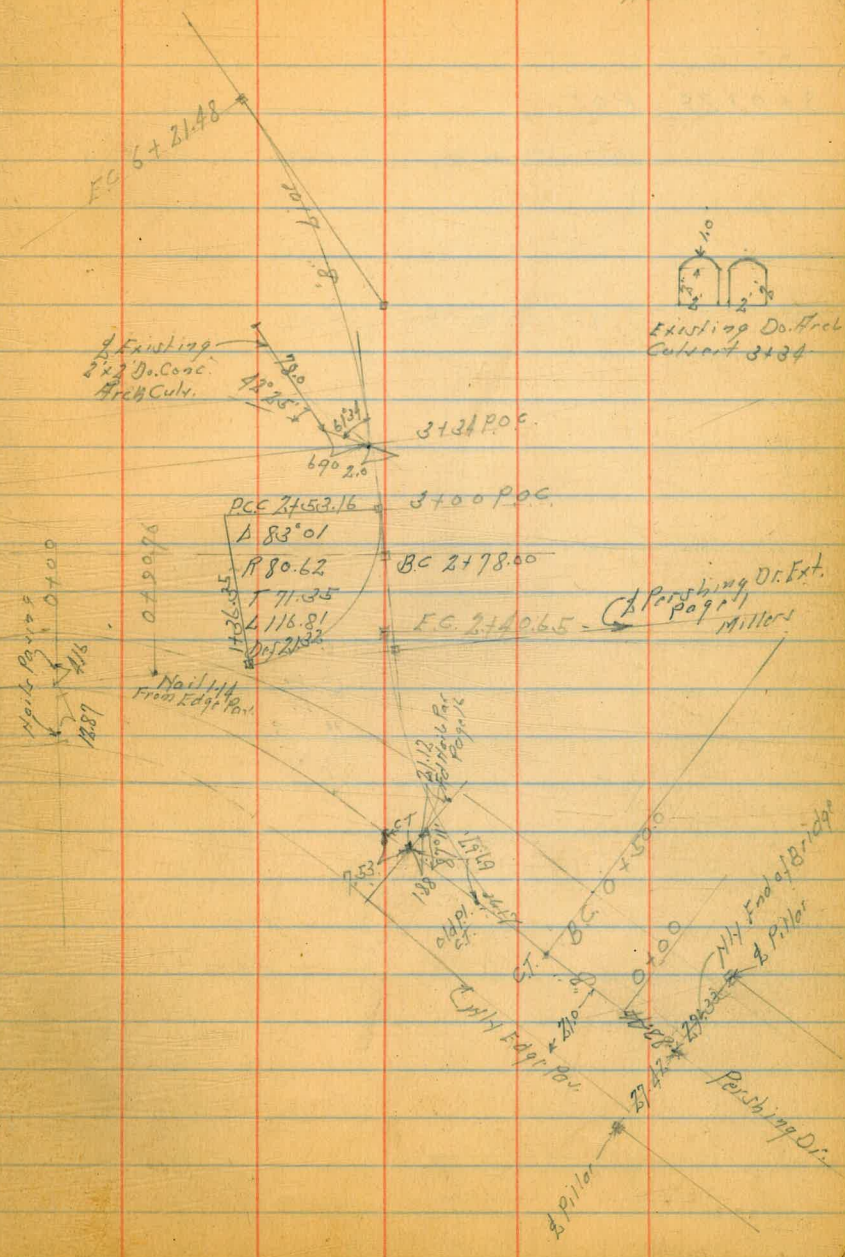
B Line  
Pershing Drive to Municipal Golf Course  
Club House

Lt. Rt.

6721.48	FC.		16° 24'
670			15° 22.433
750		Δ 32° 48'	12° 59.198
		R 600.0	
570		T 176.59	10° 25.963
750		L 343.48	8° 12.728
470		Def 2.8647	5° 49.493
750			3° 26.258
370			1° 03.023
2778.00	BC.		
2740.65	FC		27° 18.50'
270		Δ 54° 37'	21° 29.145
		R 300.0	
750		T 103.26	14° 19.63
		L 190.65	
		Def 8.5943	
170			7° 09.715
0750.0	BC.		

Indexed  
c.s.R.

9-21-84  
Moore  
S. 1107  
Northcutt



8+09.29 P.O.T.

940 19' - Pipe Tree

8475 17' - Pipe Tree

8480 21' - Pipe Tree

RT

12+82.17 P.O.T

10+36.86 F.C.

10+0

+50

9+35.34 B.C.

A 5° 49'  
R 1000.0  
T 50.81  
L 101.52  
Df 1.7182

2° 54' 50"  
1° 51' 14"  
0° 25' 19"

"B" Line

Proposed Drain

55° 52'

10+52.10

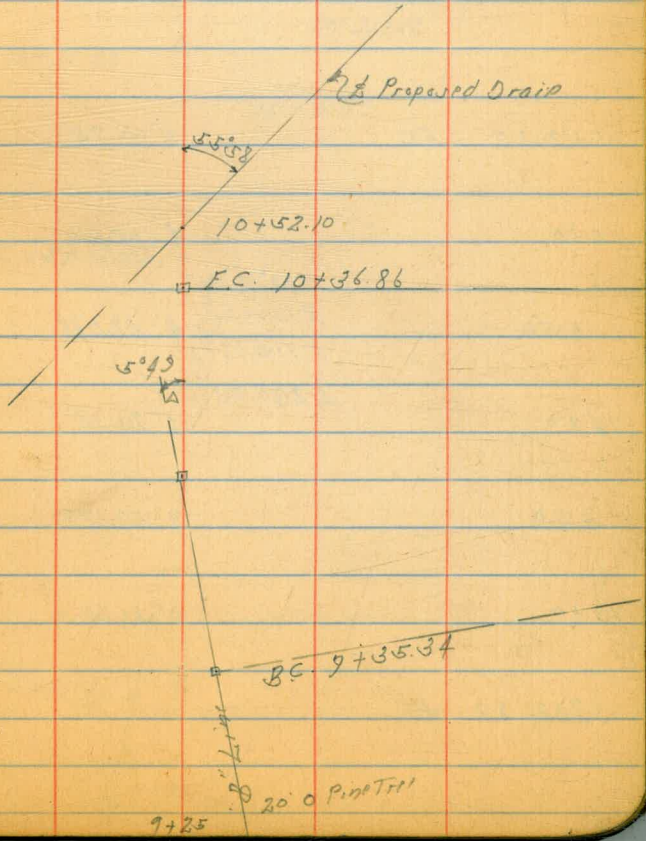
F.C. 10+36.86

5° 49'

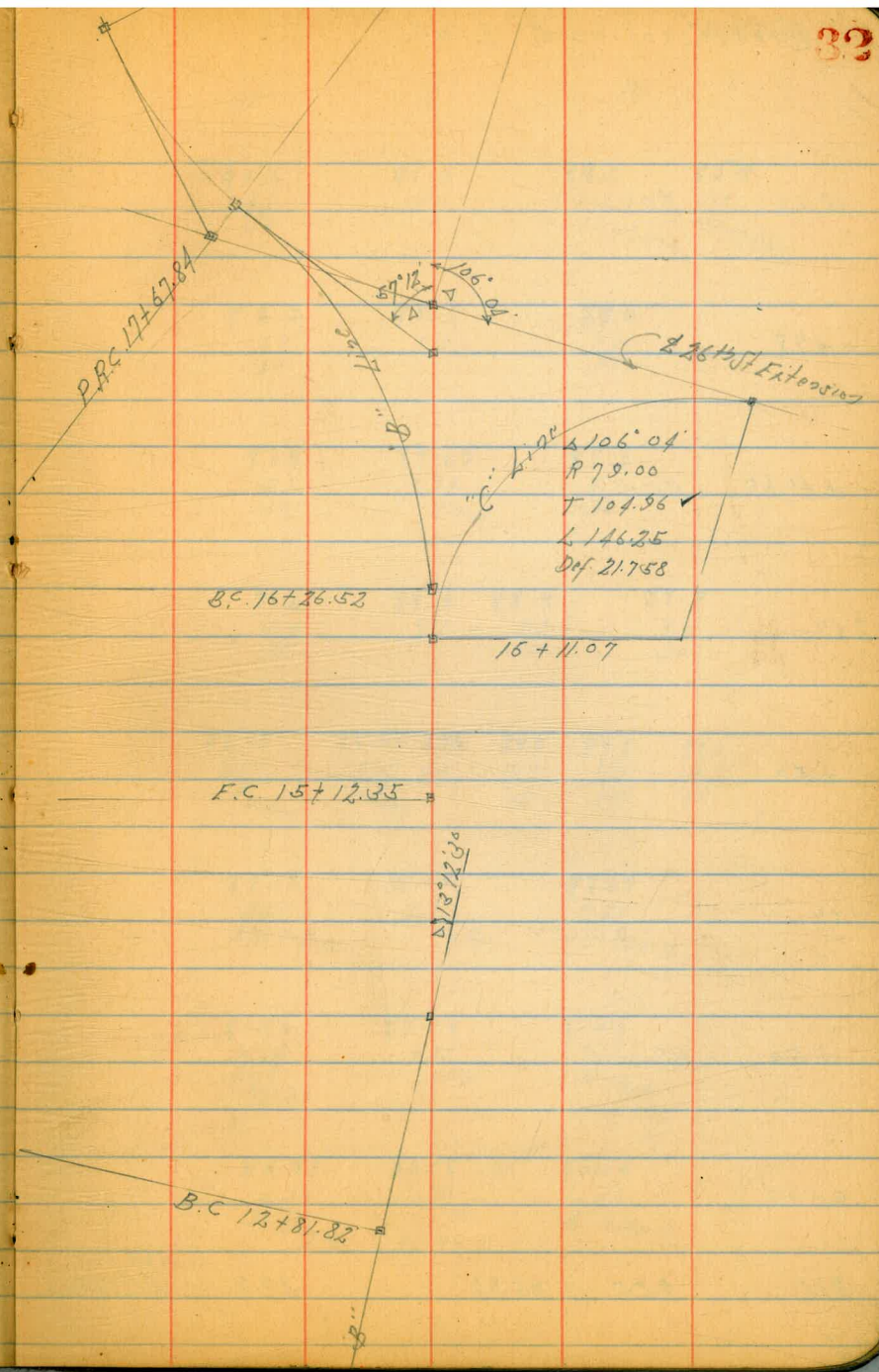
BE 9+35.34

20° P. in T. 11

9+25



17+67.84	PRC	28°36'
+50	A 57°12'	29°59.35'
	R 141.56	
17+0	T 77.18	14°52.23'
+50	L 141.32	4°45.11'
	Dof 12.1423	
16+26.52	B.C.	
15+12.35	F.C.	6°36.25'
15+0		6°15.08'
+50	A 113°12.30'	
	R 1000.0	4°49.085'
	T 115.98	
14+0	L 230.53	3°23.14'
+50		1°57.195'
13+0		0°31.25'
12+81.82	B.C.	



Cross Section B Line

Sept 25-34 33

				Lt	L	Rt	
3+0	P.C.			92.3 4.7 30	91.3 5.7	89.5 7.5 30 1/4 Cor.	85.4 1.6 50 1/4 Cor.
+78				92.2 4.8 30	90.5 6.5	89.0 8.0 35	
+40.65	E.C.			91.9 5.1 30	89.67 7.29 07 Hus	88.3 8.7 35	
2+0				91.6 5.4 30	89.9 7.1	88.8 8.2 10	89.7 2.9 30
+50				88.49 8.47 30 07 Par.	89.68 7.28 0.8 Edge	89.6 7.4 15	89.5 7.7 25
1+0				87.11 9.85 27.6 Edge Par.	88.00 8.96 07 Par.	87.47 8.48 15.8 Edge Par.	
+50	B.C.			86.82 10.14 20.8 Edge Par.	87.14 9.82 07 Par.	87.25 9.71 20 Edge Par.	
0+00				86.47 10.47 20.8 Edge Par.	86.68 10.28 07 Par.	86.54 10.46 20.2 Edge Par.	
BM	92.5	96.96	87.71	Spx Calc Set Point Corner & Par. Lines			

L1

L

R1

+15

93.6	92.3	87.9	86.9	90.0	91.4	90.3	89.5
3.1	4.7	2.1	10.1	7.0	5.6	6.7	7.5
5.0	4.0	3.0	1.5	1.8	0.0	2.5	5.0

+10

94.5	93.4	90.7	91.3	90.0	89.4
7.5	3.6	6.3	5.7	7.0	7.6
4.5	3.4	2.0		2.5	5.0

+75

93.8	91.0	91.2	91.0	88.2	88.1	90.5	89.2
3.2	6.0	5.8	6.0	8.8	8.9	6.5	7.8
7.0	2.5		7.2	1.8	3.0	3.5	5.0

+65

93.3	91.1	91.1	91.6	87.7	87.2	94.2	99.0
3.7	5.2	5.9	5.4	9.0	2.8	2.8	12.0
4.0	2.8		8.0	1.5	2.5	2.8	5.0

+50

91.5	90.9	91.1	86.8	87.2	97.0	98.0
5.5	6.1	5.9	10.2	2.8	2.0	7.0
3.5		6	1.5	2.4	3.7	1.5

+40

91.5	91.2	86.8	86.6	91.8	91.4
5.5	5.8	10.2	10.4	5.2	5.6
3.5	7	3.0	3.3		5.0

+30

91.5	91.3	85.6	86.6
5.5	5.7	11.4	10.4
3.5	5		5.0

50% Creek

37 18

92.1	91.4	86.0	85.9
4.9	5.6	11.0	11.0
3.0		1.5	5.0

50% Creek

96.96

96.96

L L R

Cont Page 37

TP 8.72 106.61 2.78 97.89

+2148 F.C. 93.6 93.8 95.3 96.5 97.2 100.3  
71 6.9 5.1 4.7 3.5 2.9  
50 40 36 4.7 Edg Grv 35 50

6+0 92.6 91.5 90.2 92.3 93.2 93.7 95.8 96.1 99.0  
8.1 9.2 10.5 8.4 7.5 7.0 4.9 4.6 1.7  
130 125 108 104 50 35 49 35 50

+50 92.6 90.9 90.6 92.1 92.2 93.7 94.9 95.7 94.5 95.8 96.6  
8.1 9.8 10.1 8.6 8.5 7.0 5.8 5.0 6.2 4.9 4.1  
135 100 85 81 35 70 35 35 38 43 Edg Grv

5+0 91.2 90.2 89.5 89.7 91.9 91.9 92.5 93.6 92.8 92.8  
9.5 10.5 11.2 11.0 8.8 8.8 8.2 7.1 7.9 7.5 Edg Grv  
95 90 78 84 35 30 0.0 35 40 45

+50 92.4 89.0 88.1 89.9 91.5 92.1 90.7 90.8  
8.3 11.7 12.6 10.8 9.2 8.6 10.0 9.8  
65 55 40 35 25 25 30 Edg 50  
100.67 oak Grv

TP 8.91 100.67 5.20 91.76

3+34 Existing Culvert 86.6 85.6  
10.4 11.4  
12/101 00/101  
Hori Line Hori Line

4+35 92.7 88.7 88.0 91.4 91.4 90.6 89.9  
4.2 8.2 8.0 5.6 5.6 6.4 7.1  
60 50 32 15 25 50



Cross Section NE Leg 18/11  
Pershing Dr

See Page 29

Lt                      S                      Pt.

+53.16 = 3100

92.2                      91.3                      89.6  
18                      5.7                      7.1  
30

210

92.5                      90.8                      89.2  
15                      6.2                      7.8  
30

+50

94.4                      92.9                      92.59  
26                      4.1                      4.32  
30    33 Edg. Par.

+3536 BC

94.9                      93.7                      93.98                      93.25  
21                      2.3                      2.98                      3.71  
35    20 Edg. Par.                      30 in Par.

170

96.4                      97.0                      96.78                      95.80  
+0.6                      0.0                      0.18                      1.16  
30    2.5 Edg. Par.                      20 in Par.

96.96

96.96

+75

Lt	Z	Rt
119.9	131.4	139.8
23.5	120	3.6
50	25	
		148.1
		152.4
		+4.7
		+2.0
		20
		30

+50

Lt	Z	Rt
118.0	126.4	135.9
25.4	170	8.5
50	25	
		139.9
		148.9
		+5.5
		3.5
		15
		143.38

12.84 143.38 0.76 130.54

+25

Lt	Z	Rt
111.1	119.1	129.6
20.2	122	1.7
50	25	
		131.2
		137.5
		+6.3
		3.5
		15
		35

8+0

Lt	Z	Rt
106.8	112.9	121.5
21.5	18.4	9.8
50	25	
		126.1
		129.9
		+5.2
		1.4
		25
		40
		131.30

TP 12.50 131.30 0.15 118.80

+50

Lt	Z	Rt
101.0	105.1	109.6
18.0	13.2	2.4
50	25	
		113.9
		119.6
		+0.6
		5.0
		25
		50
		118.25

TP 12.81 118.25 0.97 106.14

7+0

Lt	Z	Rt
97.2	103.5	107.3
2.4	3.1	10.7
50		25
		111.6
		+5.0
		5.0

6+50

Lt	Z	Rt
96.6	96.8	97.8
10.0	9.8	8.8
50	20	
		99.7
		103.6
		6.2
		3.0
		25
		50

106.61

106.61

TP 0.69 132.36 10.39 131.67

+25

119.0	117.0	124.0	129.4	135.8
23.1	25.1	18.1	12.7	6.3
50	25		20	40

10 + 0

129.0	124.8	131.3	136.2	138.4
22.1	17.2	10.8	5.9	3.9
50	25		20	30

+75

123.2	131.7	137.9	143.3	145.3
18.9	10.1	4.2	1.2	13.2
50	25		20	30
		142.06		

TP 0.36 142.06 6.08 141.70

+50

128.8	135.7	143.7	147.2	149.6
12.0	12.1	4.1	0.6	1.2
50	25		20	30
		147.78		

TP 4.57 147.78 0.17 143.21 <sup>stake</sup> 9 + 0.2

+3534 B.C.

128.0	135.5	144.5	149.7	152.2
15.1	7.2	1.1	7.2	8.8
50	25		20	30

+25

126.5	135.7	145.8	150.4	154.6
16.2	7.7	7.4	17.0	11.2
50	25		20	30

9 + 0

122.6	132.0	142.7	148.4	153.0
20.8	11.4	0.7	15.0	7.6
50	25		20	30

143.38

143.38

B Line

9-26-34  
11+50

Lt                      Rt.

+50

144.6	141.6	138.9	134.8	128.6	130.6
6.2	2.2	11.9	16.0	21.6	20.2
40'	20'		20'	40'	60' - Conn. Rd.
150.77					

TP 13.06 150.77 0.12 137.71

+23

137.3	135.4	128.6	126.0	127.1	128.7
70.5	2.4	2.2	11.8	10.7	2.1
50'	30'	5'	24 Road	25'	50'

11+0

128.8	125.9	123.2	124.7	125.6	122.7
20	11.9	14.6	13.1	12.2	15.1
50'	35'	32'	Conn. Rd.	25'	50'
24 Road					

10+80

121.6	122.6	123.8	122.1	121.2	117.2	122.5
16.2	15.2	14.0	15.7	16.5	20.6	15.3
53'	25'	15'		25'	37'	50'
25' Conn. Rd.						
137.83						

TP 12.44 137.83 6.97 125.39

10+52.10 - Proposed Drain See Page 31 Tables on Drawings

114.4	117.8	117.4	119.9	119.5
18.0	14.5	15.0	12.5	12.9
20'	30'		30'	25'

+5210

121.6	119.6	117.4	122.7	129.9
10.8	12.8	15.0	2.7	2.5
55'	30'		25'	50'

10+26.86 EC

117.4	116.4	120.5	126.0	131.4
15.0	16.0	11.9	6.4	1.0
50'	18'		20'	50'

132.36

132.36

1370

193.4	191.9	186.4	175.7
5.8	7.9	128	23.5
35		30	50

+81.82 BC

190.3	188.67	185.5	171.8
8.9	10.56	13.7	27.4
35	20	20	50

TP 1229 199.23 0.02 186.94

199.23

12+43.69 ROT

181.0	177.7	176.4	164.2
6.0	9.26	10.6	22.8
40	15	15	45

TP 1197 186.96 0.42 174.99

186.96

TP 12.28 175.41 0.41 163.13

+15

175.3	176.7	164.3	159.1	154.5
+11.8	+8.2	+0.8	1.1	2.0
40	25		35	50

1270

165.5	161.5	163.2	158.1	157.8	152.0	149.5
+2.0	2.0	0.3	5.4	5.7	11.5	1.0
40	30	17	9.6		30	50

163.54

TP 1300 163.54 0.23 150.54

1170

152.2	148.6	145.9	141.5	136.3
+1.4	2.2	1.9	9.3	14.5
40	25		25	55

150.77

150.77

+80

LT	L	RT	RT
218.0	700.9	195.0	193.2
1.0	18.3	2.0	25.8
40.		35	50

+50

217.3	199.3	185.8	176.5
4.7	18.7	33.2	42.5
40.		25	50
	219.05		

TP 12.06 219.05 0.33 206.99

+12.35 F.C.

217.4	212.6	206.2	192.1	181.3
+10.1	+5.3	1.1	15.2	26.0
25.	15.		25.	45

15+0

216.4	207.0	192.1	180.4
+8.1	0.3	15.2	26.9
35		25	45

+50

213.8	204.6	196.7	188.3
+6.5	2.7	19.6	19.0
30		25	40

14+0

207.7	201.5	194.5	186.5
+0.4	5.8	12.8	20.8
30		30	45
	207.32		

TP 9.00 207.32 0.91 198.32

13+50

199.9	196.7	192.9	190.5	184.6
+0.7	2.5	6.3	8.7	14.6
30		30	40	50

199.23

199.23

+67.84 PRC

+50

17+0

+50

TP 7.70 224.79 1.96 217.09

+26.52 BC

16+11.07

219.05

St. 2 Ft.

220.9 222.6 222.1 224.5  
3.9 2.8 2.7 0.3  
20/25 15 17 20/25

220.6 222.2 221.8  
4.2 2.6 3.9  
30 20-Dirt/Gull

220.2 220.2 220.9  
4.6 4.6 3.9  
25 25

219.1 218.6 217.5 216.0  
5.7 6.2 7.3 8.8  
36 15 30  
224.79

218.2 217.0 212.8  
0.8 2.0 4.2  
35 30

218.2 218.7 216.5 214.0 210.0 209.8  
0.8 0.3 0.5 5.1 9.0 9.2  
35 25 15 20 20

219.05

Lt.

S

Rt.

BM

6.86

217.93

0.07 C 6.05  
Hood Pfall  
217.95

+ 57.32 FC

216.1	217.1	217.23	217.0	217.0
8.7	7.7	7.56	7.8	7.8
17.0	13		13	23

177.0

219.8	219.3	215.9	214.2
5.0	5.5	8.9	10.6
25		15	25

167.50

219.0	217.4	213.5
5.8	7.1	11.3
25		25

224.79



12-10-34  
Miller  
Walker  
Bliss

X Sec. Area North of Russ Blvd.  
Bet. 26<sup>th</sup> St. & 27<sup>th</sup> St.

Indexed  
c.s.N.

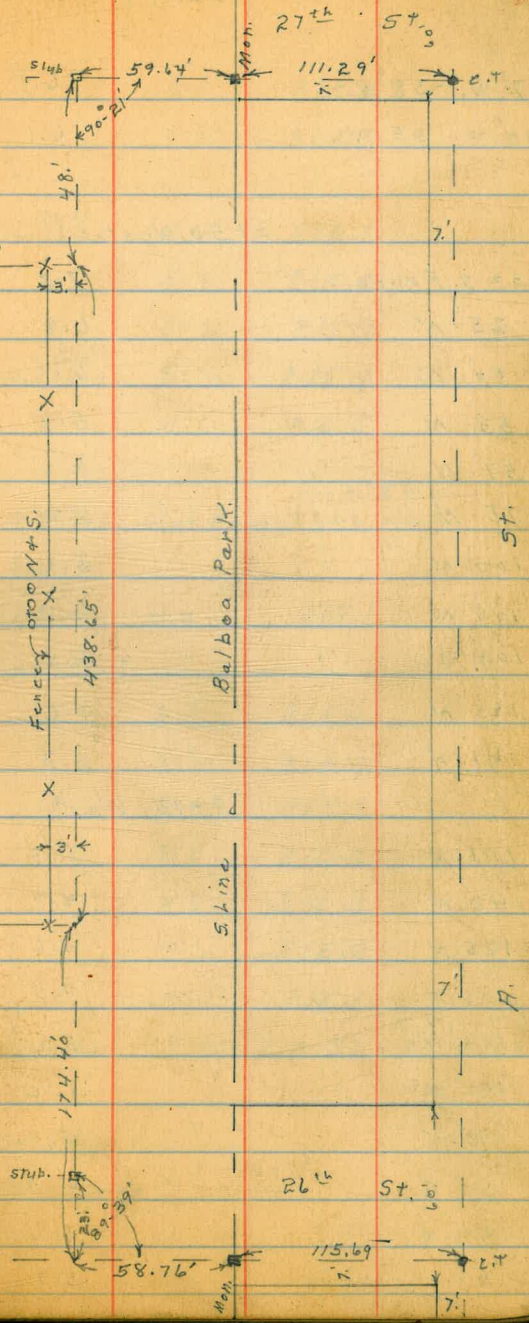
59.64  
90-21 S.W.

41

B.M.B.P.	5.23	214.08	208.85	N.W. 27 <sup>th</sup> + A. St.
T.P.	9.61	221.08	2.61	211.47
0+00 E.+W. = E. Fence				
S. Fence		9.6		211.5
25' N		8.9		212.2
50' N		8.6		212.5
75' N		8.6		212.5
100' N		8.7		212.4
125' N		8.7		212.4
141' N	E. End.	8.7		212.4
S. Side Bleachers				
0+25 West				
141' N		6.9		214.2
125' N		7.0		214.1
100' N		7.0		214.1
75' N		7.0		214.1
50' N		7.0		214.1
25' N		7.6		213.5
00 S. Fence		8.1		213.0
45' W - 105' N	NE. Cor. Horse shoe Court	5.1		216.0
45' W - 109' N		5.7		215.4
42' W - 105' N		6.1		215.0
42' W - 100' N		6.1		215.0
45' W - 100' N		5.1		216.0
41' W - 75' N		6.1		215.0
43' W - 75' N		5.3		215.8
40' W - 58' N	SE. Cor. Horse shoe Court	5.2		215.9

Fence 0+00 E+W.

Playground Area.



221.08

37' W. - 58' N. 6.1 215.0

40' W. 55' N. 6.1 215.0

0+50 West.

00 = S. Fence 7.3 213.8

25' N 6.8 214.3

50' N 6.1 215.0

55' N 5.8 215.3

57' N 5.1 216.0

75' N 5.2 215.9

100' N 5.2 215.9

105' N 4.9 216.2

109' N 5.5 215.6

125' N 5.6 215.5

141' N 5.3 215.8

0+75 West.

146' N 5.3 215.8

140' N 4.7 216.4

125' N 4.6 216.5

106' N 4.5 216.6

105' N 5.2 215.9

100' N 5.2 215.9

75' N 5.2 215.9

55' N 4.9 216.2

54' N 5.6 215.5

50' N 5.7 215.4

221.08

45

25' N 6.1 215.0

00 = S. Fence. 6.9 214.2

80' W 54' N = S.W. Cor. <sup>Horse shoe court.</sup> 5.0 216.1

80' W 50' N 5.7 215.4

82' W 75' N 5.2 215.9

85' W 100' N = N.W. Cor. <sup>Horse shoe court.</sup> 5.2 215.9

85' W 102' N 4.6 216.5

94.3' W. 70.5' N. = N.W. Cor. Club House. { 10.2' E+W. 20.3' N+S.

93' W. 50.3' N. = S.W. " " " " { " " " "

Wooden Floor of <sup>Club</sup> House. 4.0 217.1

1+00 West.

00 = S. Fence 6.5 215.6

25' N 6.2 214.9

50' N 6.0 215.1

75' N 5.1 216.0

100' N 4.8 216.3

125' N 4.2 216.9

139' N 4.4 216.7

T.P. 1.42 219.03 3.47 217.61

N.W. Cor. Top of oven.

98' W 103.7' N. Drinking Fountain

121' W. 40' N. center of oven { 5.0' E+W. 3.3' N+S

## Location of Cypress Trees

		Diam	
102' W - 73' N.		12"	✓
100' W 82.5 N		10"	✓
96' W 76' N		6"	✓
94' W 84' N		5"	✓
88' W 76' N		12"	✓
105.7 W 98.5 N		10"	✓
93' W 103' N.		8"	✓
102' W 105' N		10"	✓
111' W 103' N		10"	✓
109' W 112' N		12"	✓
94' W 111' N		7"	✓
96' W. 118' N		8"	✓
103' W 120' N		9"	✓
117' W 112' N		14"	✓
127' W 105' N		10'	✓
117' W 104' N		9'	✓
131' W. 99' N		12"	✓
140' W 98' N		14'	✓
115' W 97' N		10"	✓
123' W 93' N		12"	✓
138' W 92' N		10"	✓
130' W 92' N		6'	✓
121' W 82' W		10'	✓
124' W 78' N		12"	✓
118' W 74' N		24"	✓
142' W 64' N		14"	✓

## Location Cypress Trees.

		Diam	
142' W	72' N.	10"	✓
147' W	78' N	8"	✓
149' W	85' N	12"	✓
158' W	87' N.	10"	✓
154' W	80' N.	6"	✓
163' W	81' N.	12"	✓
155' W	74' N.	12"	✓
158' W	67' N.	12"	✓

## Eucalyptus Trees.

96' W	41' N.	10'	✓
97' W	40' N	14"	✓
102' W	36' N	6"	✓
106' W	32' N	4'	✓
101' W	27' N	3"	✓
88' W	31' N	8"	✓
94' W	26' N	6"	✓
107' W	23' N	3'	✓
100' W	19' N	8"	✓
91' W	16' N	10"	✓
126' W	33' N	12"	✓
114' W	32' N	5"	✓
121' W	28' N	6"	✓
113' W	26' N	6"	✓
126' W	16' N	3"	✓

Eucalyptus Trees.

Diam

✓

123. W	9. N	4"	✓
113. W	6. N	14"	✓
137. W	22. N	9"	✓
129. W	25. N	9"	✓
133. W	32. N	8"	✓
143. W	43. N	8"	✓
152. W	40. N	16"	✓
145. W	34. N	6"	✓
154. W	31. N	7"	✓
164. W	30. N	4"	✓
149. W	27. N	6"	✓
161. W	24. N	3"	✓
146. W	20. N	8"	✓
155. W	19. N	8"	✓
166. W	22. N	6"	✓
162. W	14. N	5"	✓
145. W	12. N	3"	✓
153. W	5. N	4"	✓
139. W	2. N	6"	✓
170. W	39. N	10"	✓
176. W	34. N	10"	✓
185. W	33. N	14"	✓
172. W	27. N	5"	✓
181. W	25. N	4"	✓
190. W	27. N	4"	✓
174. W	19. N	6"	✓

Eucalyptus Trees.

Diam

✓

183. W	19. N	6"	✓
170. W	12. N	4"	✓
179. W	11. N	4"	✓
188. W	14. N	5"	✓
176. W	5. N	10"	✓
185. W	4. N	5"	✓
197. W	31. N	4"	✓
204. W	28. N	8"	✓
198. W	23. N	4"	✓
209. W	21. N	6"	✓
192. W	20. N	6"	✓
203. W	17. N	3"	✓
198. W	13. N	7"	✓
213. W	14. N	4"	✓
207. W	9. N	8"	✓
228. W	5. N	8"	✓
226. W	12. N	12"	✓
216. W	27. N	10"	✓
238. W	19. N	8"	✓
235. W	10. N	12"	✓
242. W	4. N	10"	✓

219.03

1+25 West.

139'.N	2.3	216.7
125'.N	2.1	216.9
100'.N	2.5	216.5
75'.N	3.1	215.9
63'.N	3.6	215.4
58'.N	4.3	214.7
50'.N	4.5	214.5
43'.N	4.2	214.8
25'.N	4.5	214.5
00 = S. Fence	4.5	214.5

1+50 West.

00 = S. Fence	5.0	214.0
25'.N	4.4	214.6
41'.N	4.1	214.9
50'.N	4.6	214.4
58'.N	4.2	214.8
62'.N	3.6	215.4
75'.N	3.2	215.8
100'.N	2.8	216.2
125'.N	1.9	217.1
132'.N	2.8	216.2
139'.N	2.8	216.2

1+75 West

139'.N	3.2	215.8
134'.N	3.2	215.8
130'.N	2.6	216.4

219.03

48

125'.N	2.6	216.4
100'.N	3.1	215.9
75'.N	3.6	215.4
60'.N	3.9	215.1
55'.N	4.4	214.6
50'.N	4.6	214.4
42'.N	4.7	214.3
38'.N	4.3	214.7
25'.N	4.6	214.4
00 = S. Fence	5.3	213.7

2+00 West.

00 = S. Fence	5.6	213.4
25'.N	5.2	213.8
50'.N	4.5	214.5
75'.N	3.9	215.1
100'.N	3.2	215.8
125'.N	3.0	216.0
130'.N	3.1	215.9
140'.N	3.8	215.2

1+78 West.

139'.N = S. side W. End Bleachers.

219.03

2+25 West.

140' N	4.3	214.7
135' N	4.0	215.0
130' N	3.2	215.8
125' N	3.2	215.8
100' N	3.8	215.2
75' N	4.3	214.7
50' N	5.2	213.8
25' N	5.7	213.3
00 = S. Fence	6.3	212.7

2+50 West

00 = S. Fence	7.1	211.9
25' N	6.0	213.0
50' N	5.7	213.3
75' N	5.2	213.8
100' N	4.7	214.3
125' N	4.7	214.3
140' N	4.7	214.3

2+44' West.

125' N	3.9	215.1
--------	-----	-------

219.03

2+60' West

140' N	4.9	214.1
125' N	5.0	214.0
100' N	5.3	213.7
75' N	5.6	213.4

2+70' West

140' N	E. Side Basket Ball Court.	4.4	214.6
125' N	" " " " " "	4.5	214.5
100' N	" " " " " "	4.5	214.5
85' N	S.E. Cor " " "	4.6	214.4
75' N	" " " " " "	4.7	214.3
70' N		5.9	213.1

2+75 West

85' N	S. Side B.B. Court	4.5	214.5
75' N		4.8	214.2
65' N		6.2	212.8
50' N		6.5	212.5
25' N		7.1	211.9
00 = S. Fence		7.4	211.2

3+00 West.

00 = S. Fence	8.1	210.9
25' N	7.6	211.4
50' N	7.2	211.8
54' N	7.3	211.7
60' N	5.0	214.0
75' N	5.0	214.0
85' N = S. Side B.B. Court.	4.8	214.2

49

219.03

3+25 West.

85' N = S. side B.B. Court.	4.4	214.2
75' N	4.4	214.2
58' N	5.2	213.8
52' N	7.4	211.2
50' N	7.4	211.2
25' N	8.3	210.7
00 = S. Fence	8.7	210.3

3+50 West.

00 = S. Fence	8.5	210.5
25' N	8.8	210.2
50' N	8.4	210.6
55' N	8.4	210.6
63' N	4.9	214.1
75' N	5.1	213.9
85' N S.W. cor. B.B. Court.	5.0	214.0

3+75 West.

85' N	5.1	213.9
75' N	5.4	213.6
70' N	5.5	213.5
61' N	8.8	210.2
56' N	8.9	210.1
25' N	9.5	209.5
00 = S. Fence	9.6	209.4

70' W.	3+83 W.	8.7	210.3
--------	---------	-----	-------

219.03

50

73' N	3+83 W.	5.4	213.6
85' N	3+83 W.	5.2	213.8

4+00 West.

88' N		5.4	213.6
75' N		8.6	210.4
65' N		9.7	209.3
50' N		10.0	209.0
25' N		10.0	209.0
00 = S. Fence		10.4	208.6

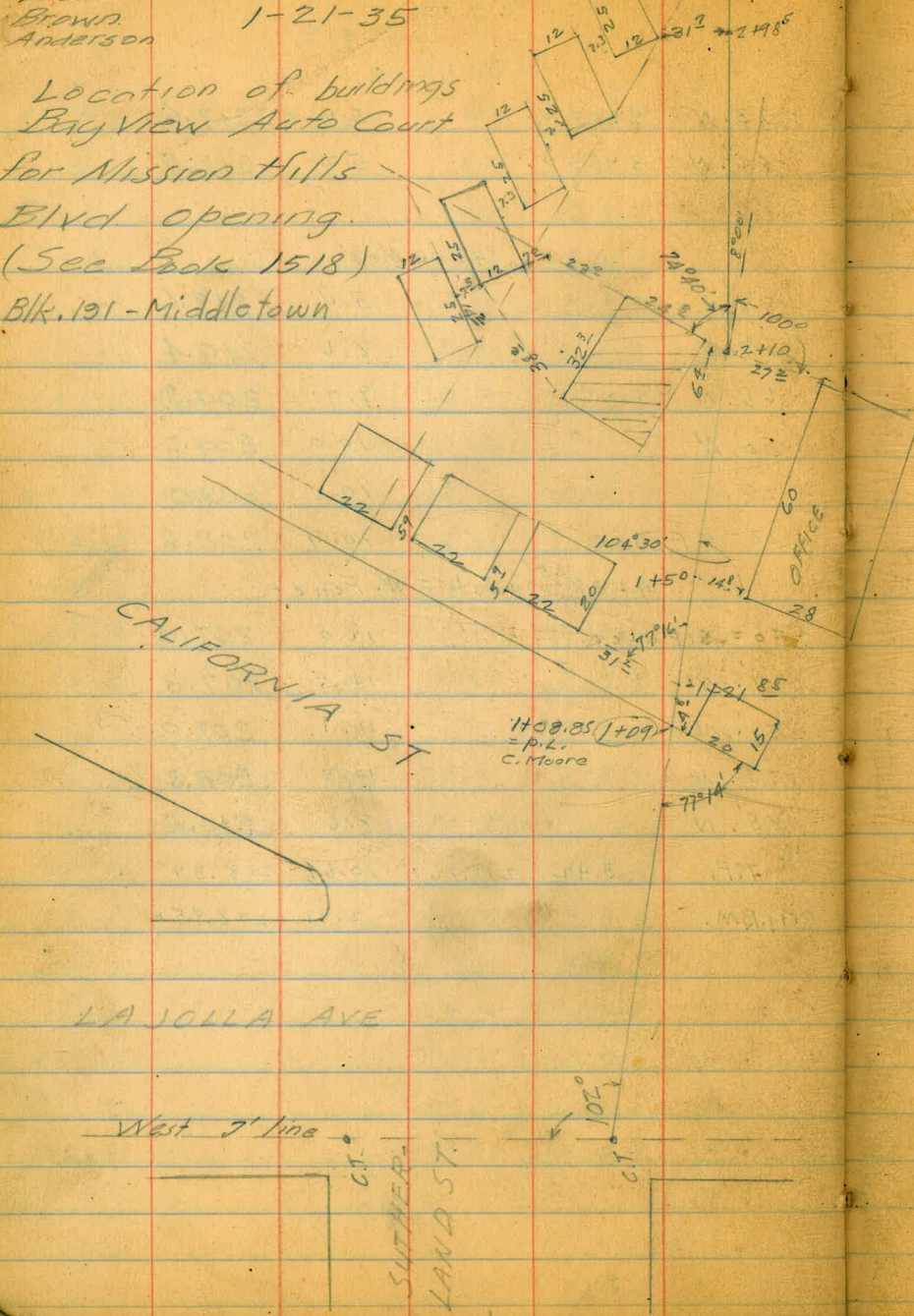
4+38<sup>65</sup> West = W. Fence

00 = S. Fence.		12.0	207.0
25' N		11.7	207.3
50' N		11.1	207.9
75' N		10.7	208.3
85' N		8.6	210.4

T.P.	3.42	211.76	10.69	208.34
orig. B.M.			2.91	208.85 ✓

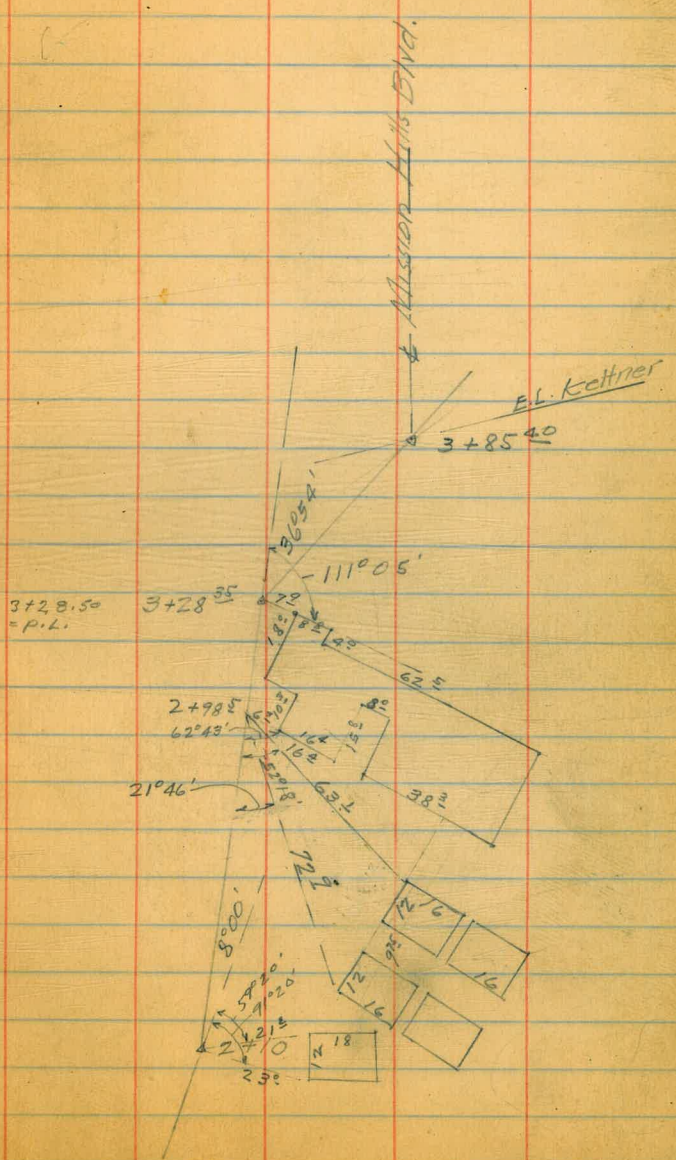
Louden  
Brown  
Anderson  
1-21-35

Location of buildings  
Bay View Auto Court  
for Mission Hills  
Blvd opening.  
(See Book 1518)  
Blk. 191 - Middletown

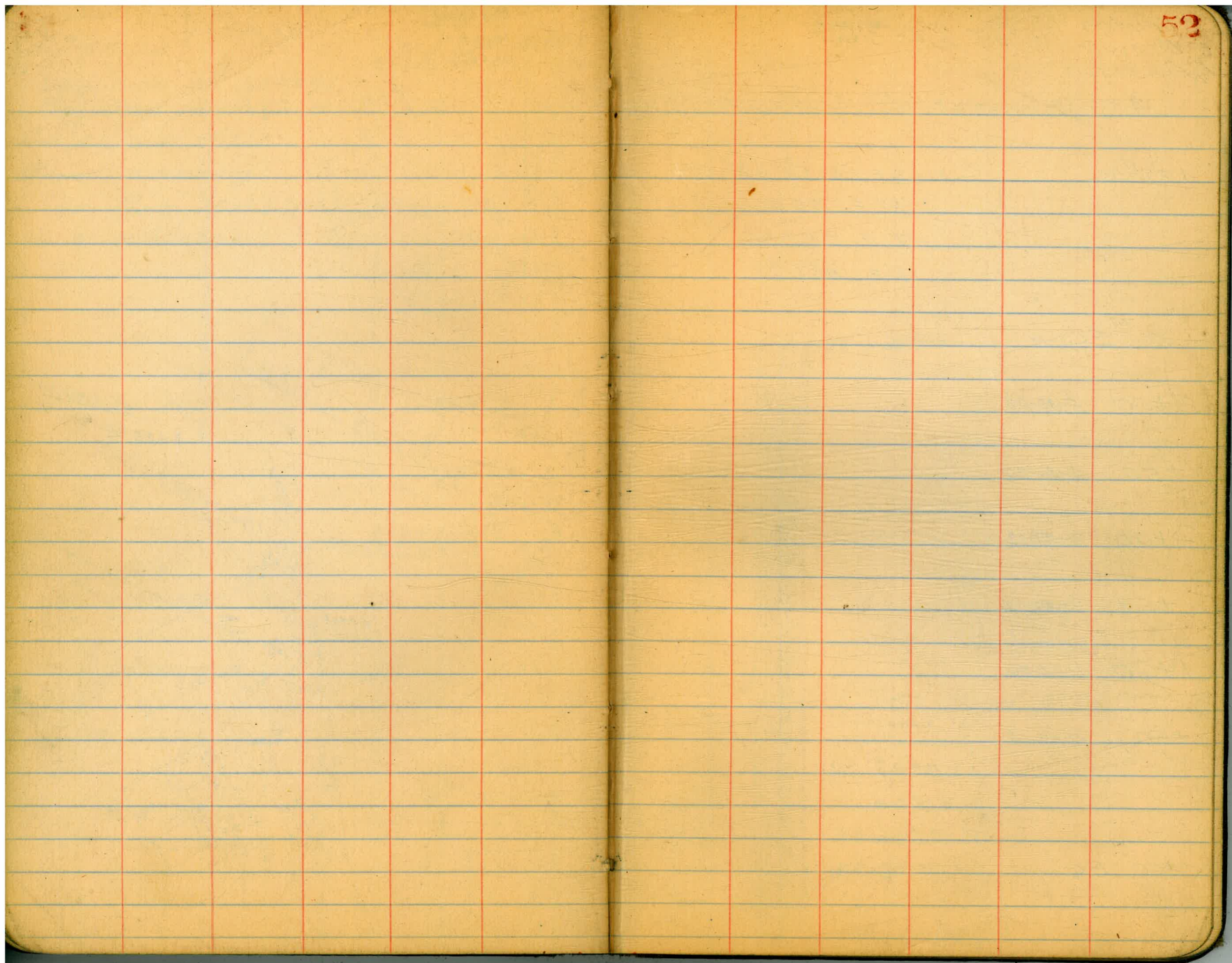


Indexed  
c.s.K.  
Plotted - 2102-B

1518  
51







Louden  
Brown  
Anderson.

1-22-35

Indexed  
c.s.K.

53

Alignment Proposed Road from Park Blvd. to 11th St.

+37<sup>11</sup> B.C.

$\Delta = 55^{\circ} 54' 45''$  Rt.

$R = 500$

$T = 265.35$

$L = 487.93$

hub

+30<sup>74</sup> E.C. 6-19

3+00 5-43-48

+50 4-46-30

2+00 3-49-12

+50 2-51-54

1+00 1-54-36

+50 0-57-18

$\Delta = 12^{\circ} 38'$  Rt.

$R = 1500$

$T = 166.05$

0+00 B.C.

$L = 330.74$

80' hub

30

PARK BLVD ALIGNMENT

(See Page 57)

80' hub

9+00

+50

+25<sup>29</sup> EC

27-57-22

hub

8+00

26-31-15

+50

23-39-22

10+200  
5425  
1.9705

63  
3  
127  
12

7+00

20-47-29

+50

17-55-36

6+00

15-03-43

+50

12-11-50

5+00

9-19-57

+50

6-28-04

4+00

3-36-11

3+50

0-44-18

15+00 23-46-25

+50 21-23-11

14+00 18-59-56

+50 16-36-42

13+00 14-13-27

+50 11-50-13

12+00 9-26-58

+50 7+03-44

11+00 4-40-29

+50 2-17-15

+02<sup>09</sup> 96

$\Delta = 75^{\circ} 59' 30''$  Lt  
R = 600  
T = 468.73  
L = 795.78

hub

10+00

9+50

Note: For relocation from  
Sta. 10+02<sup>09</sup> to ~~11~~ 11<sup>st</sup> see  
page 74 this book

+01<sup>60</sup>

23+00

22+00

21+00

20+00

19+00

18+43<sup>23</sup>  $\triangle$  2° 41' 30" Lt

+97<sup>87</sup> EC 37-59-45

+50 35-42-38

17+00 33-19-23

+50 30-56-09

16+00 28-32-54

15+50 26-09-40

Russ St.



Double 17' pepper 80% hub

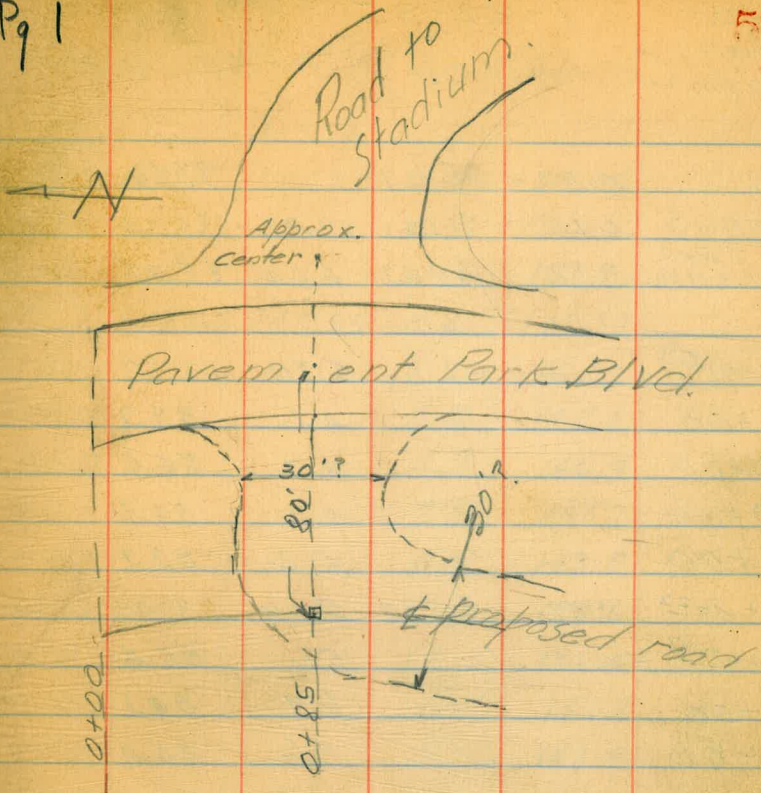
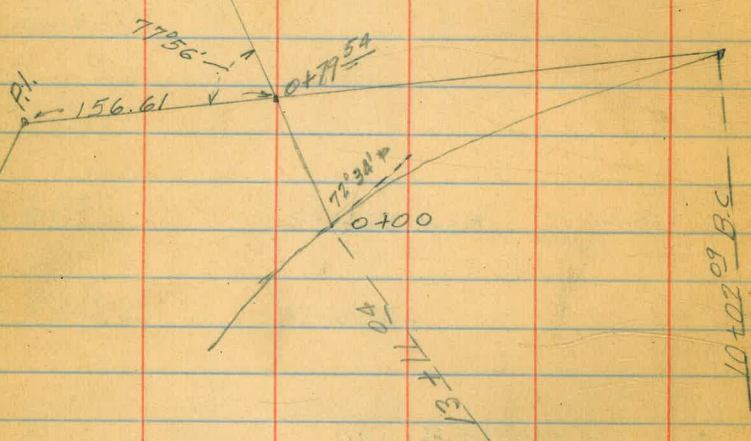
hub

30' pepper. 0 7% +40

2'  $\odot$  22'  $\odot$  42' EUC. <sup>30' EUC.</sup>

See book 1533 - Pg 1

57



Connection to Park Blvd

B.M.	11.70	201.04	189.34	hub 3+37 1/2
B.M.	5.43	204.12	2.35	198.69
Edge		Pav. at 0+85	6.20	197.9 ✓
"		Pav 40' South of 0+85	7.79	196.33
"		Pav 47 North of 0+85	4.40	199.7 ✓

1-22-35

Loudon  
Grown  
Anderson

Center-line profile of alignment P 53-56

BM	0.59	98.07	97.48	BRNIN 12th & B	T.P.	12.98	136.30	0.06	123.32
T.P.	6.46	91.61	12.92	85.15	13+11		6.3	130.0	See P. 57
SE 7/8ack Russ. ellth.	2.70	88.27	6.04	85.57	13+00		4.6	131.7	
					T.P.	12.66	148.55	0.41	135.89
23+01 <sup>60</sup>		5.70	82.57		12+50		8.23	140.32	temp P.M.
22+00		4.6	83.7		12+00		3.3	145.3	
21+00		3.7	84.6		11+50		1.7	146.9	
20+00		4.2	84.1		11+00		2.9	145.7	
19+00		5.2	83.1		10+50		4.8	143.8	
18+43 <sup>22</sup>	7.92	90.99	5.20	83.07 on hub	10+02 <sup>09</sup> BC		9.0	139.6	
17+97 <sup>87</sup> E.C.			5.6	85.4	9+75		12.2	136.4	Road.
17+50			6.9	84.1	9+10		6.7	141.9	"
17+00			5.6	85.4	9+00		5.2	143.4	
16+50			5.6	85.4	8+50		2.0	146.6	
16+00			2.0	89.0	8+25 <sup>09</sup>	12.82	156.75	1.62	143.93 on hub
T.P.	11.43	101.07	1.35	89.64	8+00		12.8	144.0	
15+50			9.6	91.5	7+50		9.7	147.1	
15+00			8.4	92.7	T.P.	11.48	167.91	0.32	156.43
14+50			3.8	97.3	7+00		16.8	151.1	
T.P.	12.93	112.34	1.66	99.41	6+50		11.3	156.6	
14+40			3.9	108.4	6+00		4.1	163.8	
14+00			3.9	108.4	T.P.	12.98	179.62	1.27	166.64
13+50			2.0	110.3					
T.P.	12.34	123.38	1.30	111.04					

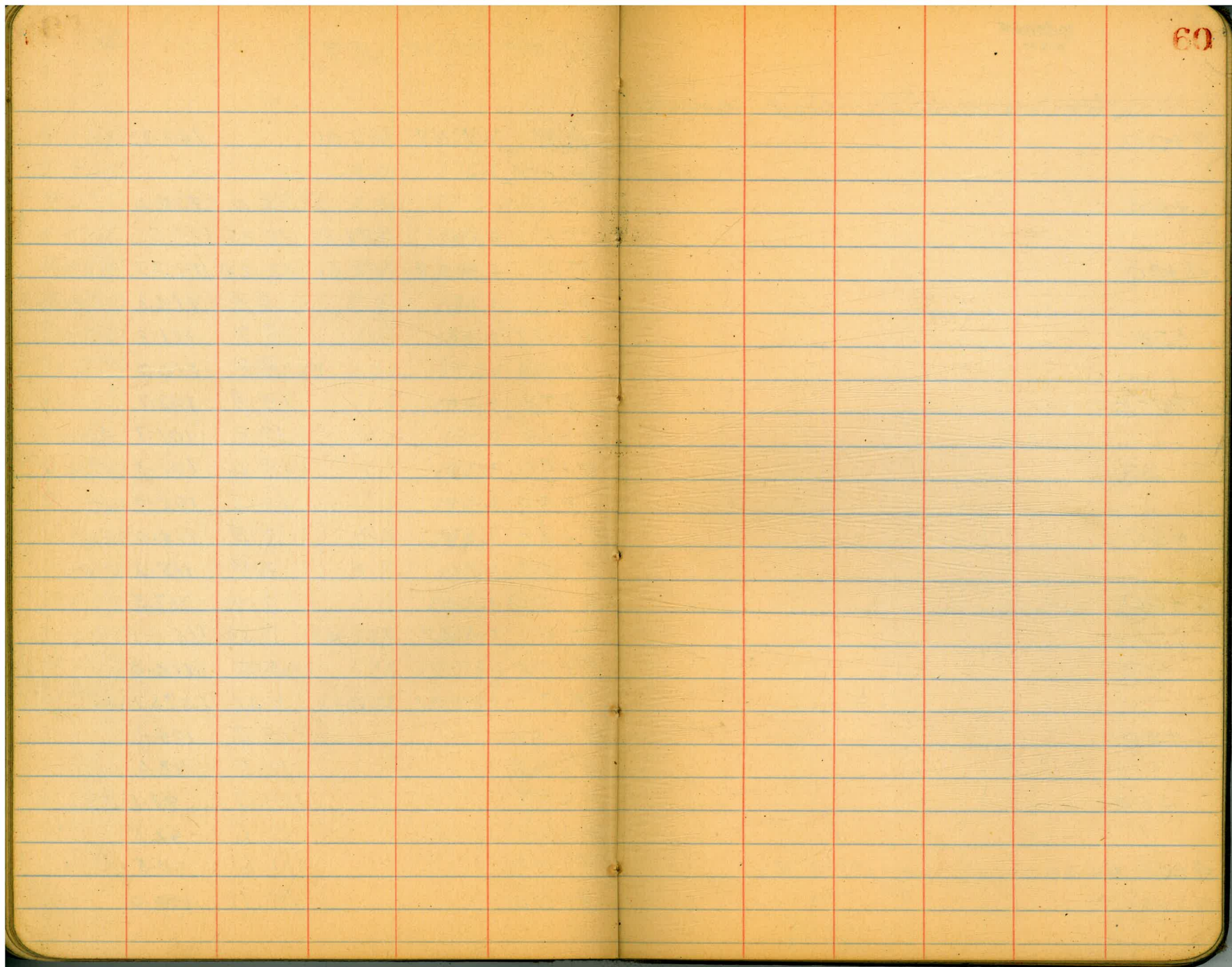
± Profile 11th St Connection (see Page 57)

59

179.62

5+50		7.5	172.1	B.M	1.69	142.01	140.32
5+00		3.0	176.6	13+112 <sup>4</sup>			
T.P.	12.70	189.96	2.36	0+00		12.0	130.0
4+74		8.4	181.6	T.P.	1.85	131.51	12.35 129.66
4+50		7.8	182.2	T.P.	0.28	119.51	12.28 119.23
4+00		3.9	186.1	0+50		3.3	116.2
3+50		1.6	188.4	0+79 <sup>5</sup>		8.3	111.2
3+37 <sup>11</sup>	bc/2.25	201.59	0.62	1+50		8.8	110.7
3+30 <sup>74</sup>	FC		11.8	1+74		15.8	103.7
3+00		10.6	191.0	2+15		17.8	101.7 Road
2+50		8.8	192.8	2+40		18.2	101.3 Road
2+00		7.2	194.4	2+50		17.5	102.0
1+50		5.5	196.1	2+80		5.5	114.0
1+00		3.7	197.9	3+00		3.9	115.6
0+50		1.3	200.3	4+00		2.2	117.3
0+00		+0.3	201.9	T.P.	5.47	121.48	3.50 116.01
T.P.	1.17	204.02	1.74	5+00		5.5	116.0
at P.V.				T.P.	0.21	110.08	11.61 109.87
opp 0+60		4.48	199.58	5+50		5.4	104.7
				5+68		11.5	98.6
				5+87		13.0	97.1 Road
				6+00		12.6	97.5 "
				7+00		11.6	98.5 "
				8+00		10.1	100.0 "





Alignment using existing road from Park Blvd. to 11th St.

5+00

+50

4+00

+50

+30<sup>74</sup> E.C.

3+00

+50

2+00

+50

1+00

+50

0+00 B.C.

$$\Delta = 12^{\circ}38' \text{ Rt.}$$

$$R = 1500$$

$$T = 166.05$$

$$L = 330.74$$

Same as on Page 53

+50

+21<sup>05</sup> E.C.

9+00

+50

8+00

+50

7+00

+93<sup>11</sup> P.C.C

$\Delta = 34^{\circ}26'30''$  Rt.

+50

$T = 117.53$

$R = 379.19$

6+00

$L = 227.94$

+50

5+03<sup>55</sup> B.C.

$\Delta = 40^{\circ}13'30''$  Rt.

$R = 270$

$T = 98.87$

$L = 189.56$

← of existing road

+66

Approx. 4 Hth. St.

+50

15+00

+50

14+00

+50

13+00

+50

12+00

+50

11+00

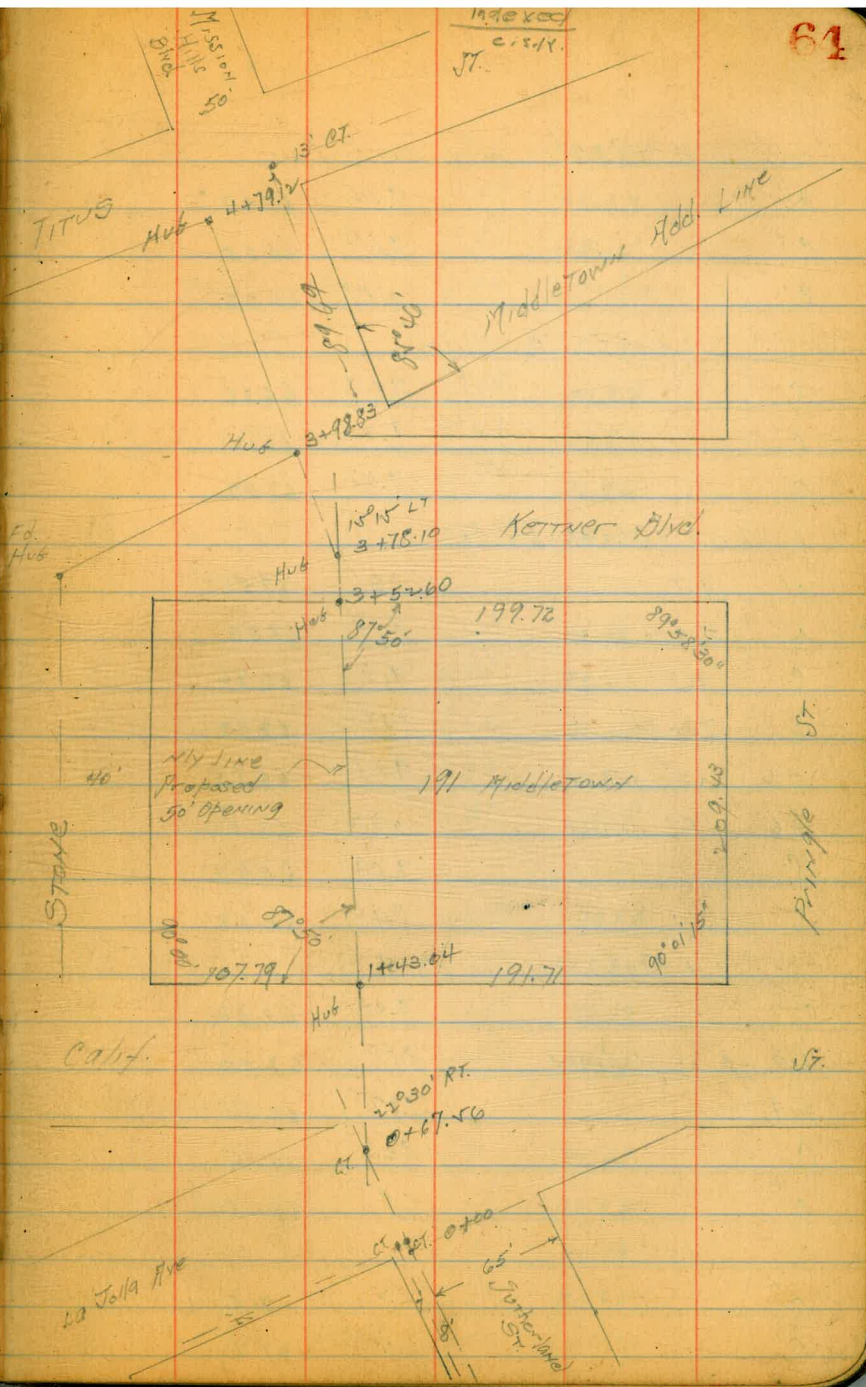
+50

10+00

Levels on Proposed 50' Opening  
of Mission Hills Blvd.  
Thru Blk 191 Middletown

NEPT	8.93	76.12	67.19
	0+00 w/ly L. La Jolla Ave		
o-1 Top cb	9.12		67.00
" gut	9.93		66.19
N.L.	9.91		66.21
C	9.86		66.26
S.L.	10.71		65.91
+1 gut	10.71		65.41
+1 Top cb	10.11		66.01
	0+12 w. curb		
S	10.63		65.49
+ N Top 24" grate	10.42		65.70
" FL. drain 30" diam.	16.30		59.82
C	10.17		65.95
N	9.80		66.32
	0+37.5 w. La Jolla Ave		
N	9.19		66.93
C	9.50		66.62
S	9.84		66.28
	0+63 curb line La Jolla Ave		
S	10.85		65.67
+6 Top grate	10.50		65.62
" FL. drain	14.16		61.96
C	10.06		66.06
N	9.88		66.24

Seaboard  
Levels  
La Jolla Ave



0+80.04 wly curb Calif.

N		9.65	67.07
C		9.84	66.28
S		10.19	65.93

1+05.54 @ Calif.

S		9.46	66.66
C		9.00	62.12
N		8.23	62.79

1+21.04 Fly Cb.

N	gut	8.61	67.51
N	Top cb	7.79	68.33
C	gut	9.13	66.99
C	Top cb	8.54	67.78
+6	2" grade	9.07	66.75
+6	FL drain	12.32	63.80
S		9.69	66.43
S		8.94	67.18

1+43.04 Fly / no Calif.

S		8.44	67.68
+10	@ open drain	8.58	67.54
+19		8.14	68.00
C		8.06	68.06
N		6.87	69.25
	1+50		
N		4.5	71.6
C		6.4	69.9

C+8

		7.8	68.36
+17	@ open drain	7.88	68.24
S		7.97	68.15
T.P.	8.00 80.30	7.84	72.30

1+78

S		9.25	70.95
+6	@ open drain	9.03	70.67
C		7.85	72.45
N		6.29	74.01

2+00

N		5.10	75.20
C		6.78	73.52
+21	@ open drain	8.10	72.20
S		7.85	72.95
T.P.	8.73 87.10	1.91	78.27
	2+50		

S		10.94	76.18
+8	@ open drain	11.25	75.85
C		10.01	77.09
N		8.98	78.12

3+00

N		5.91	81.17
+18	open drain	7.18	77.92
C		7.0	80.10
S		5.90	81.20
T.P.	12.39 95.99	2.50	82.60

	W+52.60		
S		8.6	87.9
C		10.4	85.6
N	open drain	12.5	83.5
	W+78.10 A		
N	1/8 open drain	11.1	84.9
N	15 " " "	11.4	84.6
N		11.2	84.8
C		8.9	82.1
	+13	7.9	88.1
S		5.2	90.8
	3+98.5 <sup>3</sup> Line of Mhd.		
S		1.8	94.2
	+14	2.2	93.8
C		6.4	89.6
N		7.0	89.0
	W+XV		
-10		4.8	91.2
N		2.4	92.6
T.P.	11.53 106.35	1.17	94.84
	+10	8.8	97.6
C		8.4	98.0
S		5.9	100.5
	4+55		
S		5.7	100.7
C		7.5	98.9

Mass of paper cut from  
 100.35 on 100.35  
 100.35

N		8.4	98.0
	W+79.0 <sup>W</sup> wly line 7170		
N		6.7	99.7
	+7.7 Top ob	6.52	99.83
	" 907 par.	6.96	99.39
C	par.	6.20	100.15
	+18.3 907	5.98	100.37
	" Top ob	5.53	100.82
S		3.7	102.7
	W+89.0 <sup>W</sup>		
S	par.	2.70	103.65
C	"	5.43	100.92
N	"	6.87	99.48
	5+104.1 <sup>W</sup> 2 7170		
N	par.	5.77	100.58
C	"	4.19	102.16
S	"	2.58	103.77
T.P.	016 9403	12.50	93.85
T.P.	121 8334	11.90	82.3
T.P.	144 7437	12.39	70.95
check BM		5.15	67.22

67.19  
0.03

2/20/34 Prelim. Sewers.  $\phi$  Orange Ave  
 from Ex. M.H.  $\phi$  Alley bet Euclid & 48<sup>th</sup>  
 East. to  $\phi$  Alley bet. Estrella & 49<sup>th</sup>

B.M., B.P.	6.80	349.76	342.96	S.E. 48 <sup>th</sup> + Orange
0+00 = Ex. M.H. $\phi$ Alley E. of Euclid	4.46 9.45	345.30	Top. Rim	
0+00 = " " " " " "	13.91	335.85	F.L.	
0+50	5.2	344.6		
1+00	6.0	343.8		
1+35	{ W. line 48 <sup>th</sup> St W. Edge Pav.	6.31	343.45	
1+47	6.66	343.10		
1+65	$\phi$ 48 <sup>th</sup> St	6.38	343.38	
1+83	6.68	343.08		
1+95	{ E. line 48 <sup>th</sup> St E. Edge Pav.	6.36	343.40	
2+00	6.3	343.5		
+50	5.8	344.0		
3+00	5.3	344.5		
3+30 = stub $\phi$ N. + S Alley	4.90	344.86	FL Grade 337.50	
3+50	4.7	345.1		
4+00	4.1	345.7		
+50	3.4	346.4		
+95 $\phi$ Estrella	3.3	346.5		
5+00	3.3	346.5		
750	3.8	346.0		
6+00	4.3	345.5		
+30	5.2	344.6		
6+60 stub $\phi$ N. + S Alley	6.89	342.87	FL Grade 339.15	
T.P., Stub	6.89	342.87		

Prelim Sewer in Alley  
 South of Orange Ave  
 bet. Estrella & 49<sup>th</sup> St

Blk. 30  
 Fairmount Add.

T.P.	10.79	353.66	342.87	opp. page FL Grade 339.15
0+00 = stub $\phi$ Alley	{ Orange Ave $\phi$ Alley	10.79	342.87	
0+23	11.4	342.3	339.26	
0+40	10.1	343.6		
0+70	7.2	346.6		
1+00	5.1	348.6	339.65	
+50	4.9	348.8	339.90	
2+00 stub P.O.T.	5.13	348.53	340.15	
+50	6.3	347.4	340.40	
3+00	7.3	346.4	340.65	
+30	8.6	345.1	340.70	
3+50	8.8	344.9	340.90	
4+00	11.3	342.4	341.15	
T.P.	5.73	346.59	13.00	340.66
4+44	6.1	340.5		
79.5 E. of 4+44 = { N.W. Cor. } House	4.2	342.4	ground	
" " " " "	3.25	343.34	floor, of House	
82.5 W. of 3+97 = { N.E. Cor. } House	4.25	342.34	" " "	
" " " " "	5.5	341.1	ground.	
T.P.	6.41	351.06	1.94	344.65
85.5 W. of 3+25	6.9	344.2	plumbing outlet of House	floor
" " " " "	8.4	342.7		ground
T.P.	1.09	349.97	2.14	348.88



0+00 stub of Orange	5.11	344.86	337.50
0+24	6.1	343.9	
0+40 = S. Line Orange	5.3	344.7	
0+85	6.1	343.9	
1+00	6.6	343.4	338.0
+50	9.1	340.9	338.25
2+00	12.0	338.0	338.50
+50	14.7	335.9	
Houses to E. + W. of 2+00	Can not get in		
80' E. of 1+50 vacant lot.	9.2	340.8	
80' W. " 1+50 " "	9.5	340.5	

0+00 = stub of Orange	5.11	344.86	337.50
0+20	5.8	344.2	
0+35	5.0	345.0	
0+50	3.5	346.5	
1+00	1.4	348.6	
1+50	1.6	348.4	
2+00	0.9	349.1	
2+50	6.6	349.1	338.75
3+00	1.8	348.2	339.00
3+30	3.9	346.1	
3+50	4.4	345.6	
3+75	8.3	341.7	
T.P.	4.97	353.31	
78.7' W. of 3+19 =		S.E. Cor. of House	
" " "		"	ground
" " "		"	floor
78.7' W. " 3+11 =		N.E. Cor. House	
" " "		"	"
" " "		"	ground
21.1' E. of 3+15		Plumbing Outlet	"
" " " "		"	floor
77.5' E. of 2+57 =		W. side House at Bath Room opp. Vent. in Roof	"
" " " "		"	ground
T.P.	2.45	351.77	
orig. B.M.			342.96

Indexed  
C.S.K.

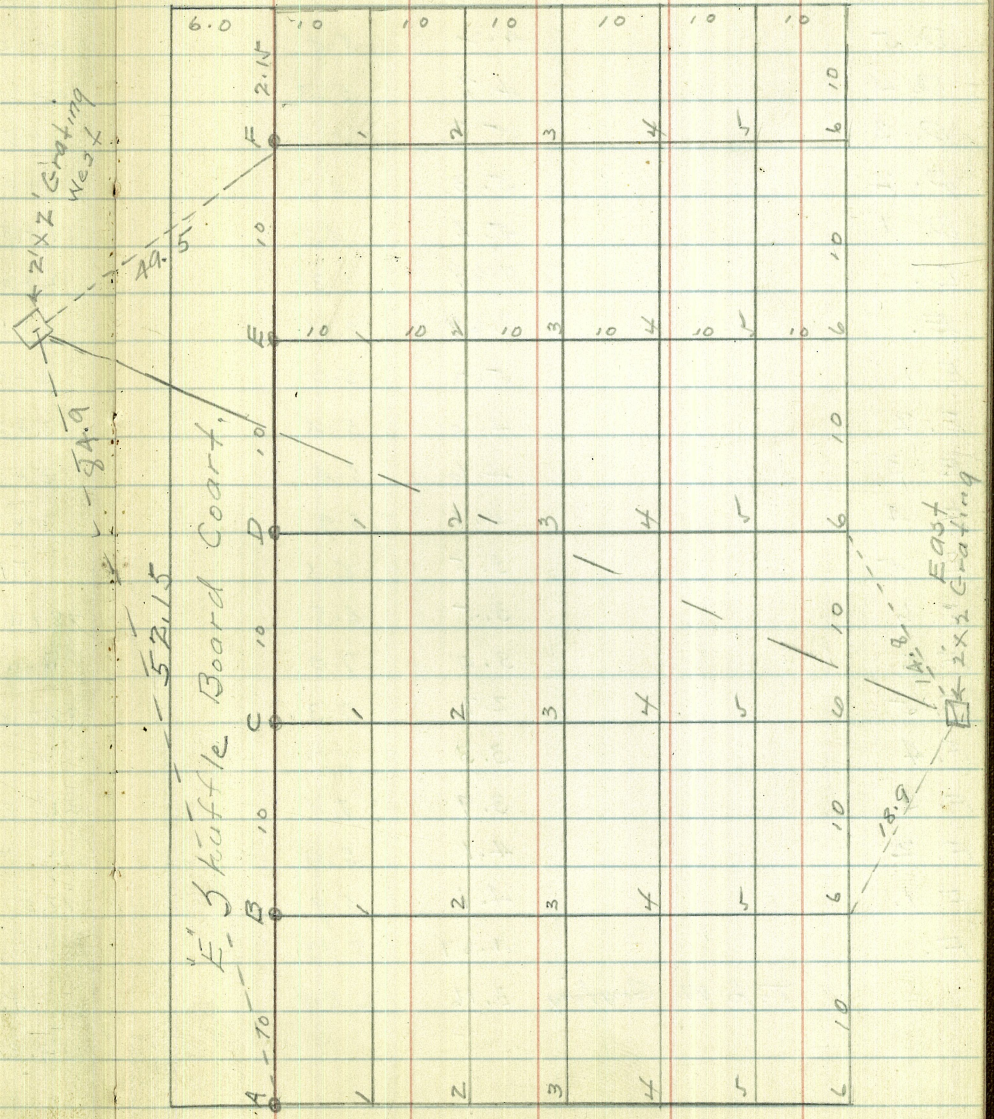
# Balboa Horse Shoe Mill Chess Checker Club Grounds at 8<sup>th</sup> Ave and Date St.

N.  
↑

(Partridge  
Bower  
Weir) 3/21/35

69

3+9	Assumed H.I. 10.00	Red	
A		7.65	2.35
A.1.		7.0	3.0
A.2		6.6	3.4
A.3		6.4	3.6
A.4		6.2	3.8
A.5		5.9	4.1
A.6		5.6	4.4
B.6		5.1	4.9
B.5		5.5	4.5
B.4		5.6	4.4
B.3		5.9	4.1
B.2		6.0	4.0
B.1.		6.7	3.3
B.		7.65	2.35
C.		7.66	2.34
C.1.		6.3	3.7
C.2		5.6	4.4
C.3		5.4	4.6
C.4		5.2	4.8
C.5		4.8	5.2
C.6		4.5	5.5
	Top E Grating	5.1	4.9
D.6		4.0	6.0



Sta.	Pod.	
D. 5	4.2	5.8
D. 4	4.7	5.3
D. 3	5.2	4.8
D. 2	5.3	4.7
D. 1	5.8	4.2
D.	7.69	2.31
E.	7.69	2.31
E. 1	5.0	5.0
E. 2	4.6	5.4
E. 3	4.6	5.4
E. 4	4.1	5.9
E. 5	3.5	6.5
E. 6	3.5	6.5
F. 6	3.0	7.0
F. 5	2.7	7.3
F. 4	3.3	6.7
F. 3	3.9	6.1
F. 2	4.1	5.9
F. 1.	4.1	5.9
F.	4.67	5.33
Top W. Grating	3.16	6.84

San Diego Roque Shuffle Board Club.

at 6<sup>th</sup> Ave and Redwood.  
X Section N. of Courts \* 4-5-6

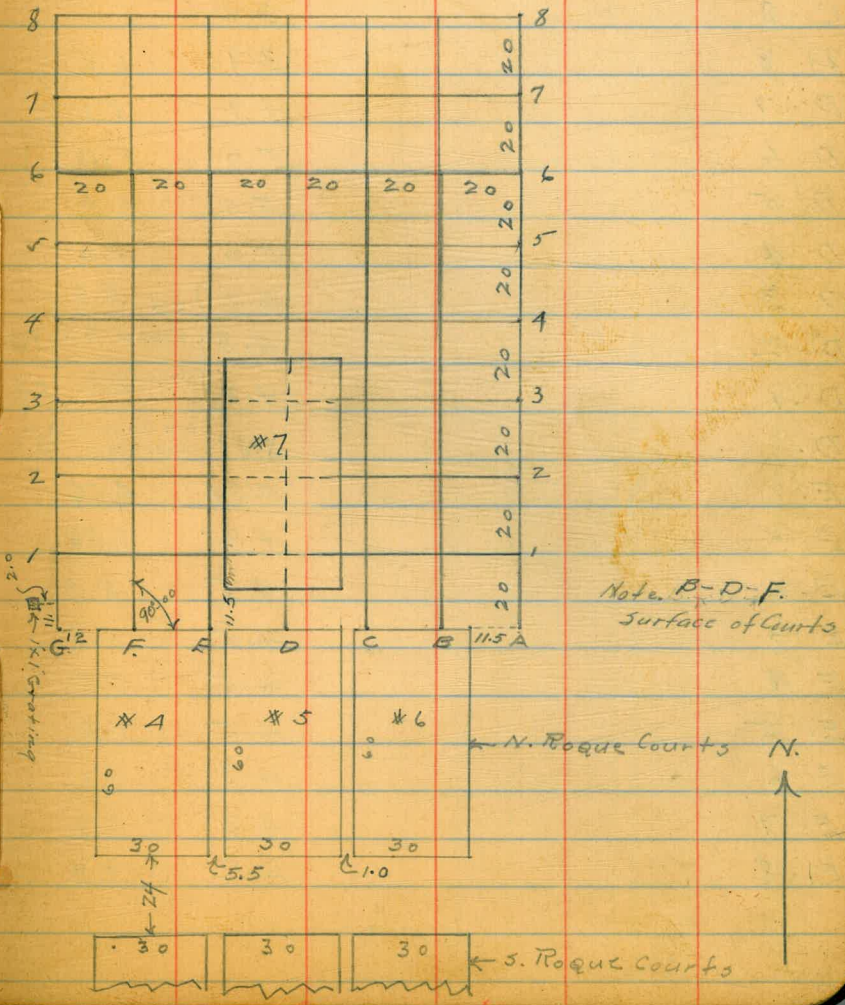
(Partridge Bowers Weir) 3/21/35

Indexed  
c.s.M.

Sta	Assumed H.I.	Red	
A	10.00	4.7	5.3
A.1.		4.1	5.9
A.2.		3.8	6.2
A.3		2.9	7.1
A.4		3.4	6.6
A.5		3.8	6.2
A.6		3.5	6.5
A.7		3.4	6.6
A.8		3.5	6.5
B.8		3.4	6.6
B.7.		4.6	5.4
B.6		4.6	5.4
B.5		4.5	5.5
B.4		4.5	5.5
B.3		4.3	5.7
B.2		4.1	5.9
B.1		4.4	5.6
B.		5.81	4.19
C		5.32	4.68
C.1.		4.6	5.4
C.2.		4.5	5.5
C.3		4.5	5.5
C.4		5.0	5.0

Note \*4-5-6-7 = Roque Courts 30'x60" is Playing Area and Does Not Include Concrete Wall

All Lines Are Parralel at 90°00



Note B-D-F Surface of Courts

surface of Court \* 6 4.19

N. Roque Courts N.

S. Roque Courts

assumed H.I.  
10.00

Sta	Rod	
C. 5	5.0	5.0
C. 6	4.9	5.1
C. 7	4.9	5.1
C. 8	3.6	6.4
D. 8	3.8	6.2
D. 7	4.9	5.1
D. 6	5.0	5.0
D. 5	5.0	5.0
D. 4	5.0	5.0
D. 3	4.8	on 5.2
D. 2	4.8	Court * 7 5.2
D. 1	4.8	Surface 5.2
D.	5.81	on Court * 5 Surface 4.19
E.	5.34	4.66
E. 1	4.35	5.65
E. 2	4.5	5.5
E. 3	4.5	5.5
E. 4	4.5	5.5
E. 5	4.5	5.5
E. 6	4.3	5.7
E. 7	4.3	5.7
E. 8	4.2	5.8

Sta	Assumed H.I. 10.00	Rod	
F. 8		4.1	5.9
F. 7		4.3	5.7
F. 6		4.4	5.6
F. 5		4.3	5.7
F. 4		4.4	5.6
F. 3		4.6	5.4
F. 2		4.7	5.3
F. 1		4.6	5.4
F. .		5.72	on Court WA Surface 4.28
G.		4.3	5.7
G. 1		4.8	5.2
G. 2		4.4	5.6
G. 3		4.3	5.7
G. 4		4.2	5.8
G. 5		4.1	5.9
G. 6		3.7	6.3
G. 7		4.3	5.7
G. 8		3.8	6.2

Relocation of Road from  
Park Blvd. to Canyon Way  
from Sta 10+02<sup>09</sup> to 15' W of 11<sup>54</sup>

H.L. Landweer  $\pi$  71  
Frank Smith cb  
W.H. Adams "  
W. Albin stakes

12+50 10°38'22"

12+00 8°10'35"

11+50  $\Delta$  78°41' Lt  
R 581.54

5°42'48"  
T 476.69  
L 798.62

11+00 3°15'01"  
Def. per. ft 177.3435"

10+50 0°41'14"

10+34<sup>02</sup> B.C.

□ set hub

10+02<sup>09</sup> old B.C.

□ hub

18+25<sup>04</sup> EC

16+12<sup>4</sup> Side line Int. <sup>28°28'40"</sup>

16+00 27°52'52"

15+50 25°25'05"

15+00 22°57'18"

14+76<sup>40</sup> P.C. Refon Rt. <sup>21°47'33"</sup>

14+50 20°29'31"

14+00 18°01'44"

13+50 15°33'57"

13+00 13°06'09"



16400

1650

15400

$18+32 \overset{64}{=} \overset{62+41}{62+40} \overset{39 \text{ Back}}{51} \overset{39^{\circ}20'30''}{\text{EC}}$  Canyada Way  
 Ahead

18400 37°44'01"

17450 35°16'13"

17400 32°48'26"

16450 30°20'39"

REFLECTED TABLETS  
 REFLECTED TABLETS  
 REFLECTED TABLETS

□ set up

## DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

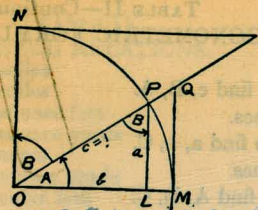


TABLE II

### TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

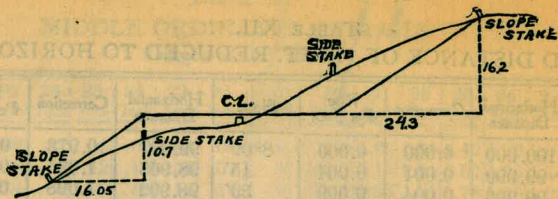
$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

15.85  
75  
100

.0566666  
.0523599 - 3  
.0043068  
0040724 - 14  
2344 47

3-14-48  
1-37-24

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8508000

2000

107

1843.22

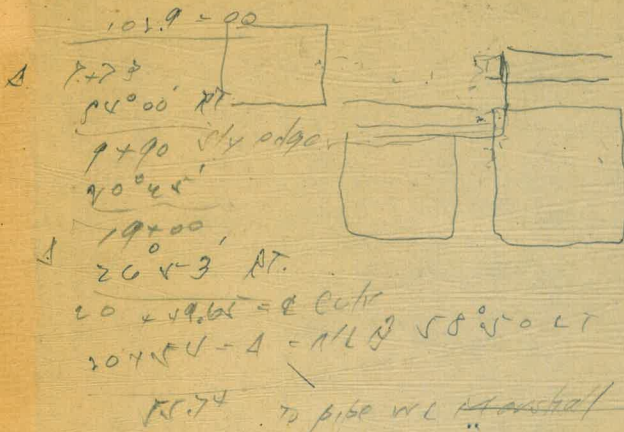
1797.87

45.35

$$\begin{array}{r}
 22.29 \\
 138.17 \\
 \underline{67.07} \\
 228.15
 \end{array}$$

28	12	13	1.7	0.0	0.2		8.7	97	103	12.0	12.0
40	35	28	17	15	5		10	17	34	35	50

V50  
76°05'



$$\begin{array}{r}
 483 \\
 31.3 \\
 \hline
 514.3 \\
 1574.04 \\
 19.60 \\
 \hline
 1554.44
 \end{array}$$
