

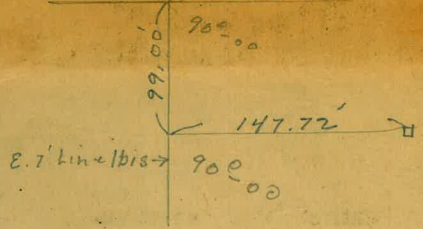
1497

ASTA

LEVEL BOOK

16.380 F

S. 7. line Montecito



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ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
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5/9/34
Miller
Walker
Blair

Levels on Existing Sewer
Index
CSK.

± 1 vy from 29th to 28th Sts.
in Delano Snyder Tract.

B.M.B.P.	1.69	284.76 ^v		283.07	5.8. Dale + 1 vy Sts
T.P.	2.15	274.29 ^v	12.62	272.14 ^v	
B.M.B.P.	5.07	270.15 ^v	9.21	265.08 ^v	5.8. 1 vy + 29 th Sts
0+00	± 1 vy + W. line 29 th St		7.12	263.03	pavmt.
0+50			11.81	258.84	"
T.P.	0.32	257.73 ^v	12.74	257.41 ^v	
1+00			4.34	253.39	pavmt
1+50			9.32	248.41	"
T.P.	0.02	244.80 ^v	12.95	244.78 ^v	
2+00			1.96	242.84	Pavmt.
2+50			7.68	237.12	"
2+83 ³	0.52 of par curve. M.H. Top. A		10.72	234.08	1.25's. of ±
2+83 ³	M.H. F.L.		16.69	228.11	
T.P.	1.47	233.33	12.94	231.86	
3+00			0.44	232.89	pavmt
3+50			3.31	230.02	"
4+00			6.10	227.23	"
4+50			8.85	224.48	
4+65 ²			9.80	223.53	
4+75 ²			10.65	222.68	
4+95 ⁴	Top. Catch Basin		12.61	220.72	
5+07 ³			12.16	221.17	
5+20	W. End. Pavmt.		11.71	221.62	
5+21	ground		14.0	219.33	
5+40 ²	Top. M.H.		19.15	214.18	
5+40 ²	F.L. M.H.		24.57	208.76	

5/9/34 X see Ivy St. 29th to 28th sts 45' wide
 5.0' wide
 10 Delano Snyder Tract. 8.75' 1/4s.

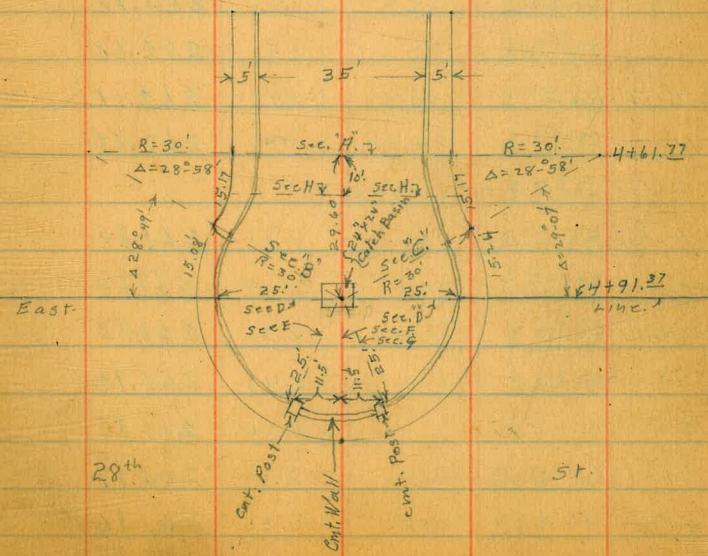
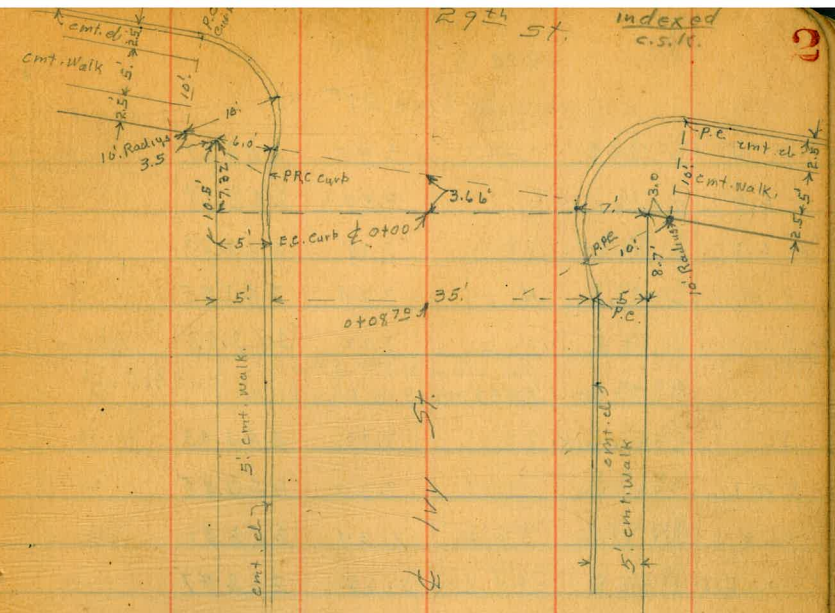
B.M. B.P.	1.69	284.76		283.07	S.E. Dale Ivy Sts
T.P.	2.15	274.29	12.62	272.14	
T.P. B.M. B.P.	5.07	270.15	9.21	265.08	set S.E. Ivy + 29 th Sts.

10' E. of W. line 29th = W. ch. line

30' S. of S. line Ivy Produced	7.39	262.76	Top. ch.
30' S " " " "	7.99	262.16	gutter pavmt.
4.63' S " " " "	7.79	262.36	" "
4.63' S " " " "	7.25	262.90	Top. of ch. at curb P.C.
S " " " "	7.74	262.41	Pavmt.
S. curb " " " "	7.66	262.49	" "
S. " " " " "	7.55	262.60	" "
☒ " " " " "	7.49	262.66	" "
N/4 " " " " "	7.48	262.67	" "
N. curb line " " " "	7.50	262.65	" "
N. " " " " "	7.43	262.72	" "
1.87' N. of N " " " "	7.42	262.73	gutter "
1.87' N " " " " "	4.94	263.21	Top. of ch. at curb P.C.
30' N. " " " " "	4.75	263.40	Top. ch
30' N. " " " " "	7.33	262.82	gutter pav

W. line 29th St

N. on walk	4.86	263.29
N. ch. line on walk.	4.96	263.19
+1.1 = cent. ch.	6.97	263.18
+1.1 gutter	7.36	262.79
"	7.29	262.86
☒	7.12	263.03



270.15 ✓

W. line 29th St

270.15 ✓

Ivy St. 3

S. 1/4	7.48	262.67
+ 6.8 = gutter	7.57	262.58
+ 6.8 = s. cnt. cl.	7.28	262.87
s. cl. line on walk	7.20	262.95
S. " " "	7.12	263.03
0+00 = {W. line 29 th St. obs. 2.32 W. of W. line on N}		at 90° 00'
S. on walk	7.12	263.03
S. cl. line " " "	7.30	262.85
+ 1.8 = cnt. cl.	7.34	262.81
gutter	7.68	262.47
1/4	7.61	262.54
⊕	7.44	262.71
1/4	7.67	262.48
+ 8.6 = gutter	7.89	262.26
+ 8.6 = Top cnt. cl.	7.55	262.60
N. cl. line	7.54	262.61
N	7.47	262.68
	0708 ²⁰	
N.	8.31	261.84
cl.	8.35	261.80
gutter	8.71	261.44
1/4	8.43	261.72
⊕	8.26	261.89
1/4	8.28	261.87
gutter	8.35	261.80
cl. at E.C. Curb.	8.01	262.14

S.	7.82	262.33
0+50		
S	11.97	258.18
cl.	12.10	258.05
gutter	12.40	257.75
1/4	12.33	257.82
⊕	12.23	257.92
1/4	12.41	257.74
gutter	12.67	257.48
cl.	12.29	257.86
N	12.17	257.98
T.P.	0.32	257.73
	1+00	12.74
		257.41 ✓
N.	4.66	253.07
cl.	4.73	253.00
gutter	5.06	252.67
1/4	4.82	252.91
⊕	4.69	253.04
1/4	4.90	252.83
gutter	5.00	252.73
cl.	4.64	253.09
S.	4.58	253.15
	1+30	
S	7.50	250.23
cl.	7.59	250.14
gutter	7.90	249.83

257.73 ✓

1730

1/4	7.81	249.92
✓ ♀	7.63	250.10
1/4	7.77	249.96
gutter	8.00	249.73
el	7.61	250.12
N.	7.53	250.20

1740

N	8.52	249.21
el	8.59	249.14
gutter	8.95	248.78
1/4	8.81	248.92
✓ ♀	8.66	249.07
1/4	8.82	248.91
gutter	8.92	248.81
el	8.60	249.13
S.	8.44	249.29

1750

S.	9.48	248.25
el	9.62	248.11
gutter	10.01	247.72
1/4	9.87	247.86
✓ ♀	9.74	247.99
1/4	9.84	247.89
gutter	10.02	247.71
el	9.64	248.09
N	9.54	248.19

257.73 ✓

Ny. ST

1

1760

N	10.66	247.07	
el	10.78	246.95	
gutter	11.12	246.61	
1/4	10.94	246.79	
✓ ♀	10.79	246.94	
1/4	10.96	246.77	
gutter	11.13	246.60	
el	10.72	247.01	
S	10.59	247.14	
T.P.	0.02	244.80	
		12.95	244.78 ✓

2700

S	2.19	242.61
el	2.36	242.44
gutter	2.68	242.12
1/4	2.55	242.25
✓ ♀	2.41	242.39
1/4	2.56	242.24
gutter	2.79	242.01
el	2.46	242.34
N.	2.30	242.50

2747³⁴ B.C. Δ = 9° 16' Alt. φ R = 400'

N	7.87	236.93
el	7.97	236.83
gutter	8.26	236.54
1/4	8.09	236.71
✓ ♀	7.82	236.98

2+47.34 (con) B.C.

1/4	7.96	236.84
gutter	8.09	236.71
cb	7.79	237.01
S.	7.66	237.14

Curve divided into 4 Parts
N. Line L = 68.33
4 = 64.69
5 = 61.04

Sta 2+63.51 Part. I Δ 2°19'

S	9.32	235.48
cb	9.47	235.33
gutter	9.77	235.03
1/4	9.57	235.23
1/4	9.47	235.33
1/4	9.63	235.17
gutter	9.80	235.00
cb	9.47	235.33
N.	9.34	235.46

Sta 2+79.48 Part 2 Δ = 4°38'

N.	10.69	234.11
cb	10.82	233.98
gutter	11.13	233.67
1/4	10.96	233.84
1/4	10.73	234.07
1/4	10.91	233.89
gutter	11.10	233.70
cb	10.80	234.00
S.	10.72	234.08

Sta 2+95.85 Part. 3 Δ = 6°57'

S	11.91	232.89
cb	11.97	232.83
gutter	12.29	232.51
1/4	12.04	232.72
1/4	11.93	232.87
1/4	12.10	232.70
gutter	12.26	232.54
cb	11.95	232.85
T.P.	1.47	233.33
N.	0.34	232.99

Sta 3+12.03 Part. 4 E.C. Δ 9°16'

N	1.35	231.98
cb	1.47	231.86
gutter	1.80	231.53
1/4	1.62	231.71
1/4	1.43	231.90
1/4	1.64	231.69
gutter	1.84	231.49
cb	1.50	231.83
S.	1.39	231.94

3+25

S	2.10	231.23
cb	2.24	231.09
gutter	2.56	230.77
1/4	2.39	230.94
1/4	2.15	231.18

233.33

3+25 (con)

1/4	2.32	231.01
gutter	2.54	230.79
cb	2.23	231.10
N	2.12	231.21

3+50

N	3.52	229.81
cb	3.54	229.77
gutter	3.89	229.44
1/4	3.66	229.67
✓ ♀	3.54	229.79
1/4	3.74	229.59
gutter	3.92	229.40
cb	3.60	229.73
S	3.46	229.87

4+00

S	6.18	227.15
cb	6.34	226.99
gutter	6.65	226.68
1/4	6.47	226.86
✓ ♀	6.33	227.00
1/4	6.43	226.90
gutter	6.65	226.68
cb	6.33	227.00
N	6.29	227.04

233.33

Ivy St

6

4+30

N	7.95	225.38
cb	8.03	225.30
gutter	8.33	225.00
1/4	8.06	225.27
✓ ♀	7.98	225.35
1/4	8.07	225.26
gutter	8.33	225.00
cb	7.97	225.36
S	7.80	225.53

4+61 P. C. See A. Page 2.

S	9.58	223.75
cb	9.74	223.59
gutter	10.05	223.28
1/4	9.84	223.49
✓ ♀	9.83	223.50
1/4	9.92	223.41
gutter	10.04	223.29
cb	9.76	223.57
N	9.66	223.67

For see "H" see 4+71 see page 7.

See B. Plat Page 2.

N	10.53	222.80	N. edge walk
+5 = N. cb	10.70	222.63	
gutter	11.01	222.32	
+12.5 = 1/4	11.66	221.67	
+25 = E. Iron Catch Basin Grating	12.61	220.72	

233.33 ✓

See C.

ctr on grating	12.61	220.72
+12.5 = 1/4	11.72	221.61
+25 = gutter	11.02	222.31
s. cb.	10.67	222.66
S. line on S. edge walk.	10.48	222.85

E. line 28th St. See "D" 4+91³⁷

s. line = W. End. ent. walk	11.24	222.09
s. cb.	11.35	221.98
gutter	11.61	221.72
+12.5 = 1/4	12.03	221.30
φ on C.B. Grating	12.61	220.72
+12.5 = 1/4	11.88	221.45
gutter	11.62	221.71
cb	11.39	221.94
N. on W. End. ent. walk	11.29	222.04

See E

W. ent. cb. N. End. wall	11.42	221.91
gutter	11.79	221.54
+12.5 = 1/4	12.06	221.27
ctr on C.B. Grating	12.61	220.72

See F = φ 1/4

ctr on C.B. Grating	12.61	220.72
+12.5 = 1/4	12.16	221.17
gutter Base of wall	11.71	221.62

233.33 ✓

See G.

W. ent. cb. S. End. wall	11.47	221.86
gutter	11.75	221.58
+12.5 = 1/4	12.15	221.18
ctr. on C.B. Grating	12.61	220.72

See H. Sta 4+77²⁷ This should be on Page 6.

N.	10.22	223.11
N. cb.	10.24	223.09
gutter	10.54	222.79
+1.5 = N. cb. line Produced	10.55	222.78
N. 1/4	10.61	222.72
φ	10.63	222.70
S. 1/4	10.63	222.70
S. cb. line	10.58	222.75
+1.5 = gutter	10.57	222.76
s. cb.	10.27	223.06
s. line	10.21	223.12

T.P.	11.36	243.22 ✓	1.47	231.86 ✓
T.P.	12.83	255.73 ✓	0.32	242.90 ✓
T.P.	12.65	268.34 ✓	0.02	255.71 ✓
BM			3.26	265.08 ✓
T.P.	12.16	280.23 ✓	6.27	268.07 ✓
T.P.	6.70	286.72 ✓	0.21	280.02 ✓
BM			3.64	283.08 ✓

S.E. 1/4

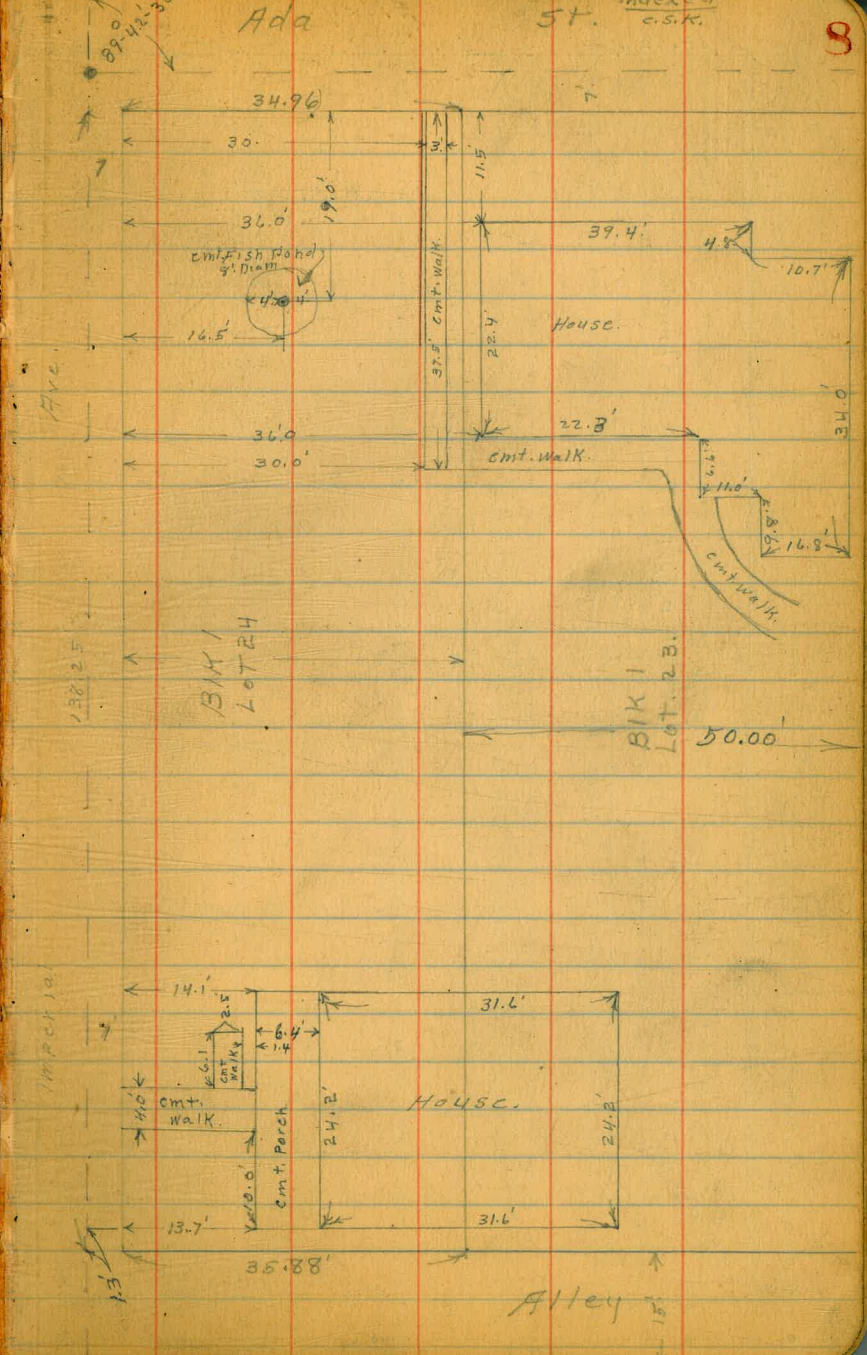
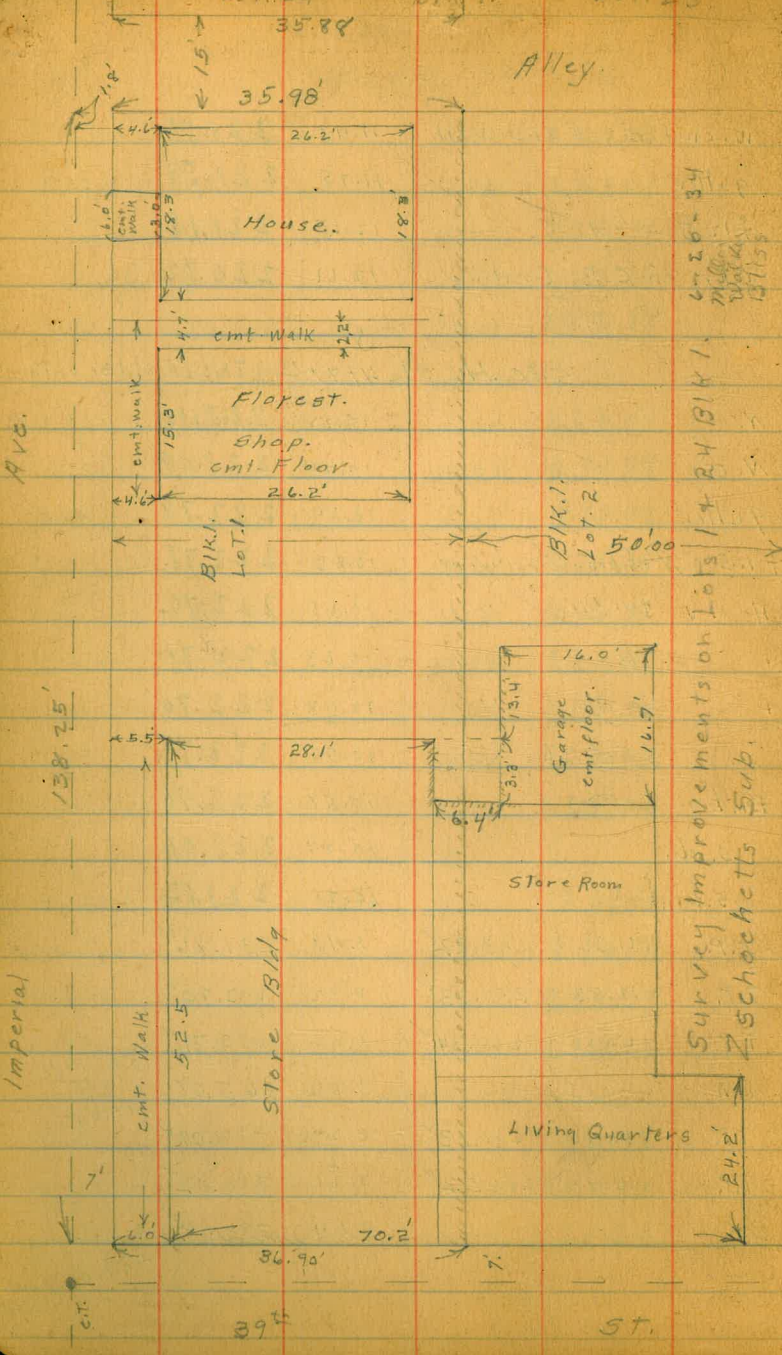
+ 29th

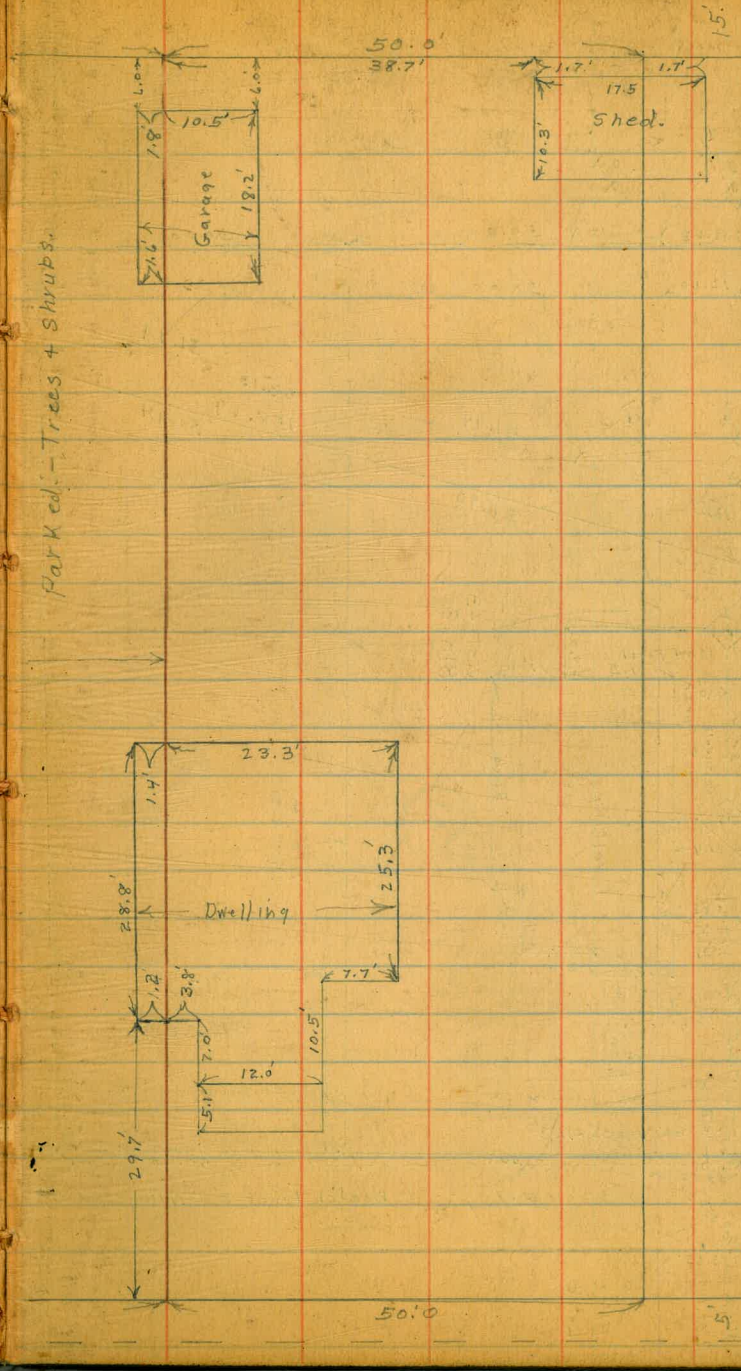
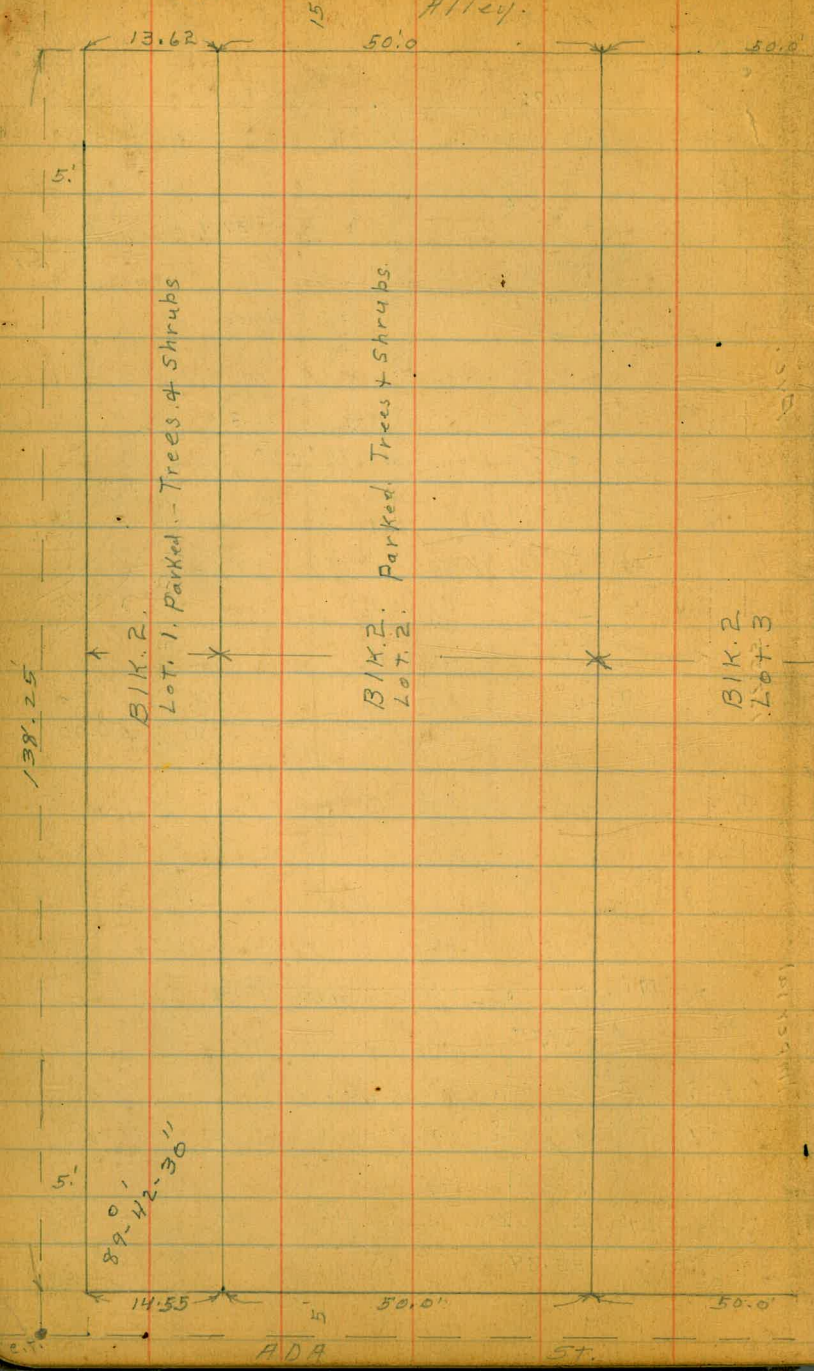
265.08

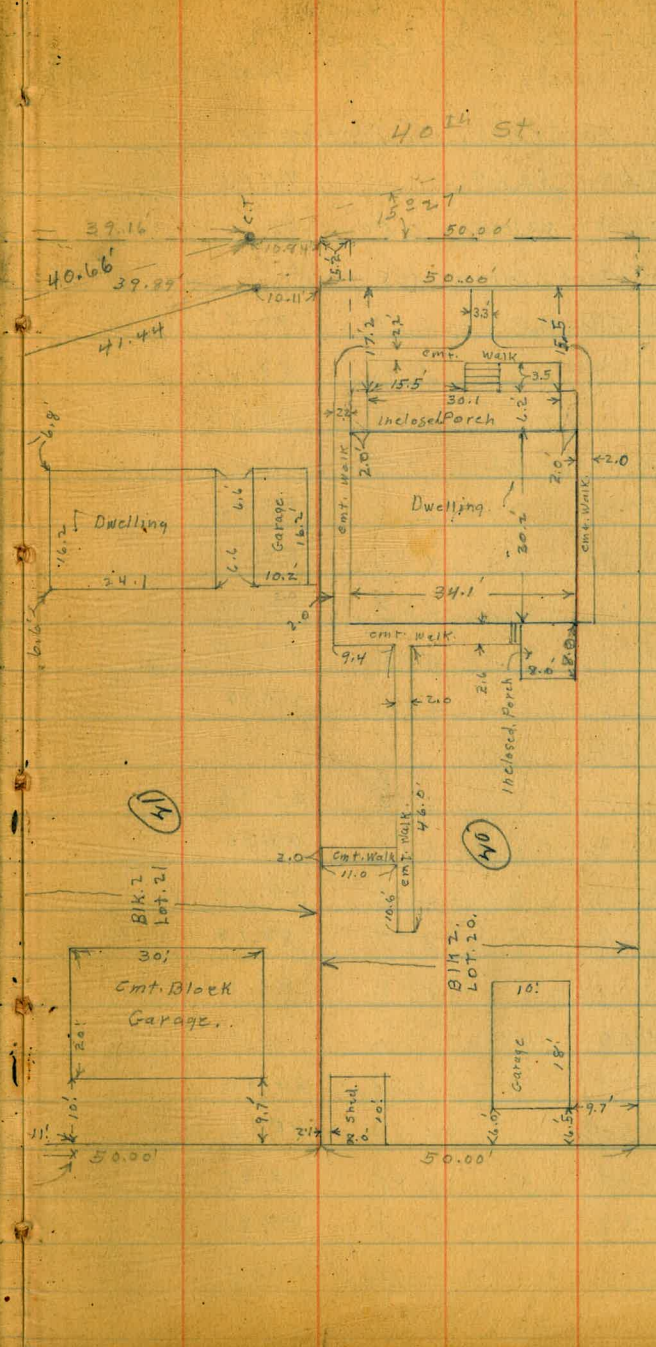
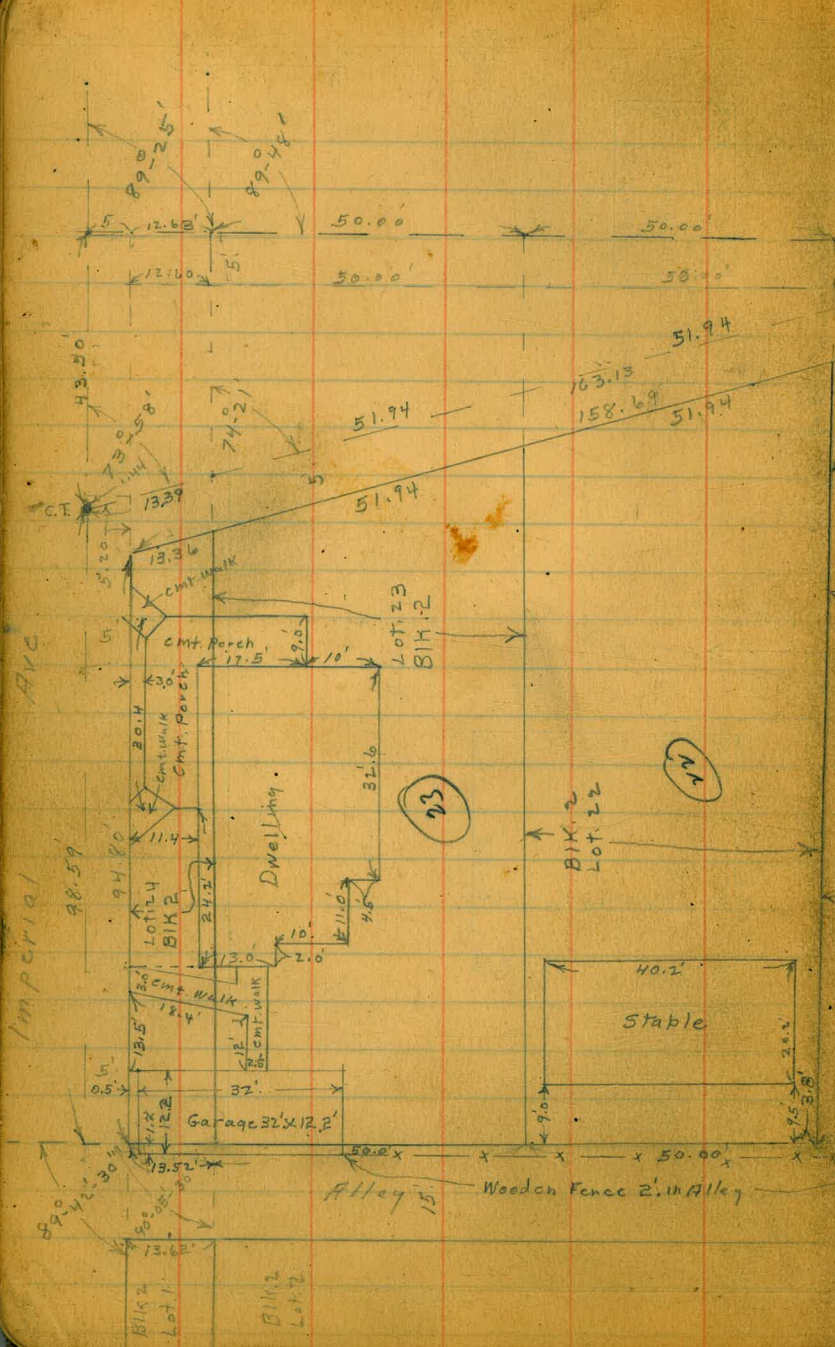
S.E. 1/4

+ Dale

283.07







Cross Section Electric Ave
Forward St. to Bird Rock Ave.

Roadway 50.0

Indexed
c.s.k.

93.05

Aug 15-34 11
Singer
Bliss
Hortberry

East Curb Line Stationing

BM	11.74	86.69	74.95
TP	6.86	93.05	0.50 86.19

5th St
Lafayette St
Forward

N. Curb Line of Forward

H.L. Electric on Pav	6.07	86.98
⊥	4.68	88.37
F.L.	4.20	88.85

0+00 H.L. Forward - Taken on Line Forward

FCb Top	4.13	88.92
Gutter on Pav	4.80	88.25
⊥	4.72	88.33
H Gutter	5.85	87.20
Top Cb	5.17	87.88

0+50

H Cb	5.13	87.92
Gutter on Pav	5.69	87.36
⊥	4.72	88.33
F Gutter	4.87	88.18
Top Cb	4.20	88.85

1+0

F Cb Top	4.25	88.80
Gutter on Pav	4.89	88.16
⊥	4.84	88.21
H Gutter	5.12	87.43
Top Cb	5.22	87.83

1+50

H Cb	5.33	87.72
Gutter on Pav	5.58	87.47
⊥	4.92	88.13
F Gutter	4.97	88.08
Top Cb	4.35	88.70

2+0

F Cb Top	4.46	88.59
Gutter on Pav	5.04	88.01
⊥	5.05	88.00
H Gutter	5.34	87.71
Top Cb	5.34	87.71

2+50

H Top Cb	5.43	87.62
Gutter on Pav	5.80	87.25
⊥	5.14	87.91
F Gutter	5.17	87.88
Top Cb	4.47	88.58

3+0

F Cb Top	4.52	88.53
Gutter on Pav	5.22	87.83
⊥	5.17	87.88
H Gutter	6.08	86.97
Top Cb	5.60	87.45

TP	4.60	92.44	5.21	87.81
----	------	-------	------	-------

9244

3+50 - Approx Cb FC

H Cb Top	5.02	87.41
Gutter on Pav	5.59	86.85
1/2 " "	4.61	87.83
F Gutter " "	4.70	87.74
Top Cb	4.03	88.41

4+0

F Cb Top	4.10	88.34
Gutter on Pav	4.77	87.67
1/2 " "	4.70	87.74
H Gutter " "	5.69	86.75
Top Cb	5.08	87.36

4+50

H Cb Top	5.09	87.35
Gutter on Pav	5.76	86.68
1/2 " "	4.74	87.70
F Gutter " "	4.81	87.63
Top Cb	4.13	88.31

5+0

F Cb Top	4.13	88.31
Gutter on Pav	4.84	87.60
1/2 " "	4.83	87.61
H Gutter " "	5.81	86.60
Top Cb	5.16	87.28

9244

5+50

H Cb Top	5.30	87.14
Gutter on Pav	5.92	86.52
1/2 " "	4.92	87.52
F Gutter " "	4.93	87.51
Top Cb	4.23	88.21

6+0

F Cb Top	4.80	88.14
Gutter on Pav	4.96	87.48
1/2 " "	4.99	87.45
H Gutter " "	5.96	86.48
Top Cb	5.37	87.07

6+50

H Cb Top	5.41	87.03
Gutter on Pav	6.07	86.37
1/2 " "	5.21	87.23
F Gutter " "	5.03	87.41
Top Cb	4.34	88.10

6+89 - S.L. Bird Rock Ave. Takes on Driv

F Cb Top	4.39	88.05
Gutter on Pav	5.06	87.38
1/2 " "	5.44	87.00
H Gutter " "	6.10	86.34
Top Cb	5.47	86.97

92.44

13

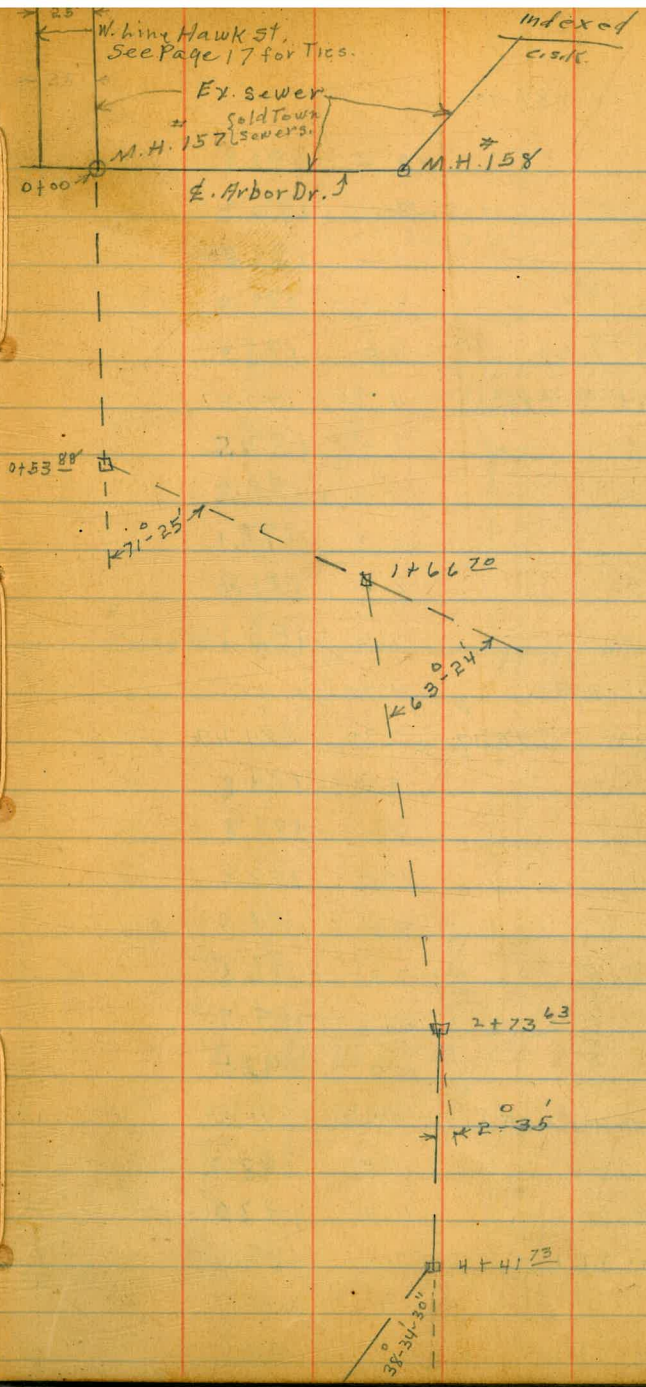
S Curb List of Bird Rock Ave

HL	as Pav	6.83	85.61	
L	"	5.50	86.94	
FL	"	4.50	87.94	
TP	1.97	84.47	2.94	82.50
BM		9.51	74.96	SN 80 La Jolla Blvd Forward 7495

9-21-34 Prelim Sewers from Arbor Drive
 Miller & Hawk St. to Serve Property E. Side 1615 St.
 Walker Bet. Lewis & Montecito Way,
 Bliss BIK. 36th Arnold & Choats

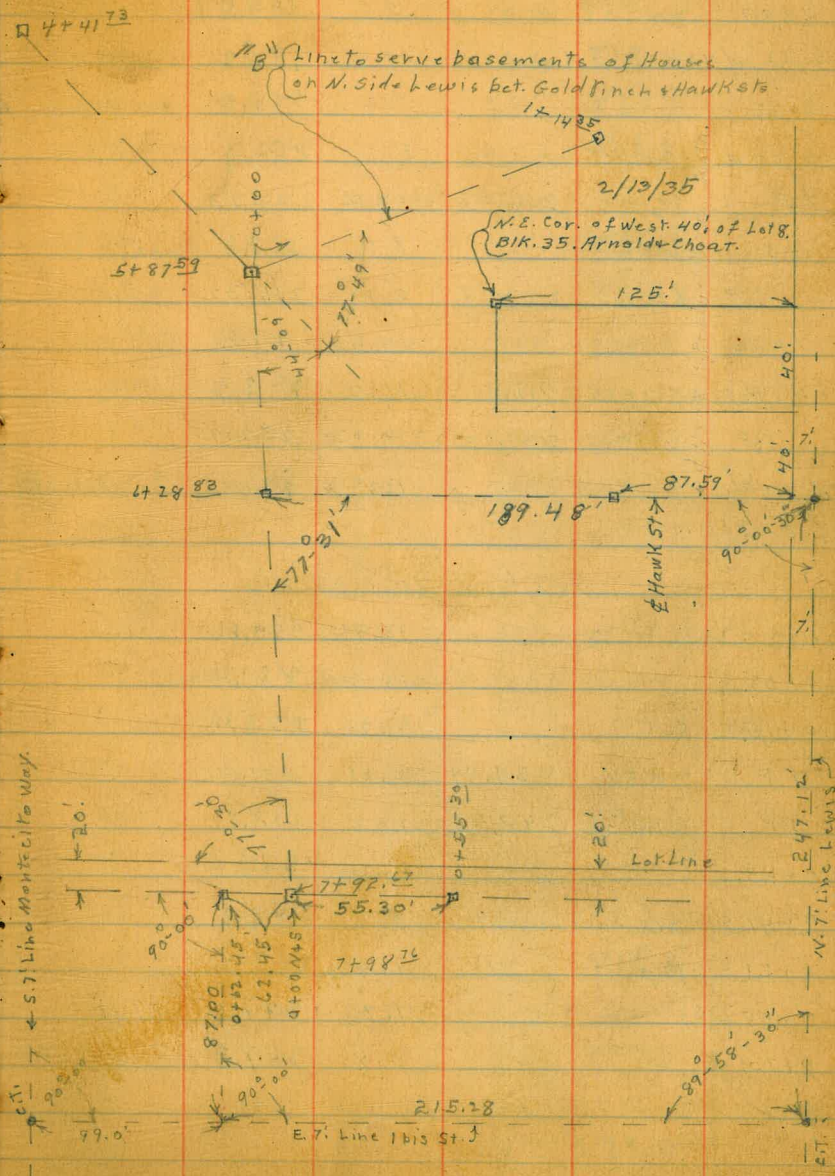
0+00 = Ex M.H. 157 Old Town Sewers
 & Arbor Dr. + 25' E. of W. Line Hawk St } 172.00 F.L. Plans

0+00 M.H.	9.26	181.26	172.00	F.L.
0+00				Top M.H.
0+00				ground
0+10		6.2	175.1	
0+25		10.2	171.1	
0+37		10.4	170.9	
0+53 ⁸⁸ Δ	71°-25' Lt.	4.75		
T.P.	4.83	181.34	4.75	176.51
0+85		3.0	178.3	
1+15		2.4	178.9	
1+45		0.5	180.8	
1+66 ⁷⁰ Δ	63°-24' Rt.	4.60		
T.P.	11.79	188.53	4.60	176.74
2+00		6.7	181.8	
2+50		5.6	182.9	
2+79 ⁶³ Δ	2°-35' Rt. (No. M.H.)	4.74	183.79	
3+00		6.7	181.8	
+33		10.0	178.5	
+50		8.5	180.0	
4+00		8.0	180.5	
4+41 ⁷³ Δ	38°-34'-30" Rt.	9.06		Φ Hub
T.P.	4.95	184.42	9.06	" "



184.42

4+75			2.5	181.9.
5+00			2.1	182.3
+50			1.6	182.8
5' Lt. of 5+50			3.4	181.0
9' " 5+50 ditch			9.0	175.4
T.P.	9.92	189.39	4.95	179.47
5+61			7.2	182.2
5+63 Ditch			10.6	178.8
5+70 "			10.3	179.1
5+72 "			8.0	181.4
5+80			6.3	183.1
5+87 ⁵⁹ Δ 44°09' Rt.			4.90	
T.P.	9.28	193.77	4.90	184.49
6+00			9.6	184.8
+12			8.0	185.8
+13 ditch			10.0	183.8
+18 "			9.8	184.0
+19			7.3	186.5
+25			6.1	187.7
+50			0.4	193.4
T.P.	12.24	205.61	0.40	193.37
+75			7.4	198.2
13 Lt. of 6+75 = Bank			11.7	193.9
18 Lt. of 6+75 = Ditch			17.0	188.6
7+00			4.9	200.7
6' Lt. of 7+00 = Ditch			11.1	194.5



205.61

N+S. Line 80' E. of 1b15

231.62

16

7+07			7.1	198.5
3' ht. of 7+07 = Ditch			10.4	195.2
7+25			7.6	204.0
2' ht. of 7+25 = Ditch			5.1	200.5
T.P.	12.58	216.51	1.68	203.93
7+50 = ϕ Ditch			8.0	209.5
T.P.	12.86	229.18	0.19	216.32
7+75			14.4	214.8
4' ht. of 7+75 = Ditch			16.0	213.2
T.P.	8.67	231.62	6.23	222.95

7+92⁶⁷ P.T. N+S. Line Δ 10.96 220.66 on stub
80' E. of 1b15 S

N+S. line 80' E. of 1b15

0+00 = 7+92 ⁶⁷ Δ			10.96	220.66	stub
0+05.5			10.2	221.4	
0+15.5			6.2	225.4	
T.P.	8.58	239.99	0.21	231.41	
T.P.	9.65	248.56	1.68	238.91	
0+45.5			4.2	244.4	
0+49.5 Top cobbles wall			3.1	245.5	
0+51.5 Top " "			1.4	247.2	
0+55 ³⁹ S			1.3	247.3	stub
0+70 S			0.8	247.8	

0+00 = 7+92 ⁶⁷ Δ			10.96	220.66	stub
0+05.5 N.			12.6	219.0	
0+15 N.			9.9	221.7	
0+30 N			4.7	226.9	
T.P.	8.58	239.99	0.21	231.41	
0+54 Top cobbles wall			3.5	236.5	
0+56 Top " "			0.8	239.2	
0+62 ⁴⁵ T.P.	9.10	248.01	1.08	238.91	stub
T.P.	12.96	260.16	0.81	247.20	
T.P.	12.16	271.48	0.84	259.32	
Top. Hydt. T.P.	6.22	276.06	1.64	269.84	S.E. 1b15 & Montecito
B.M. B.P.			0.55	275.51	S.W. Jackdaw & Montecito = 275.50

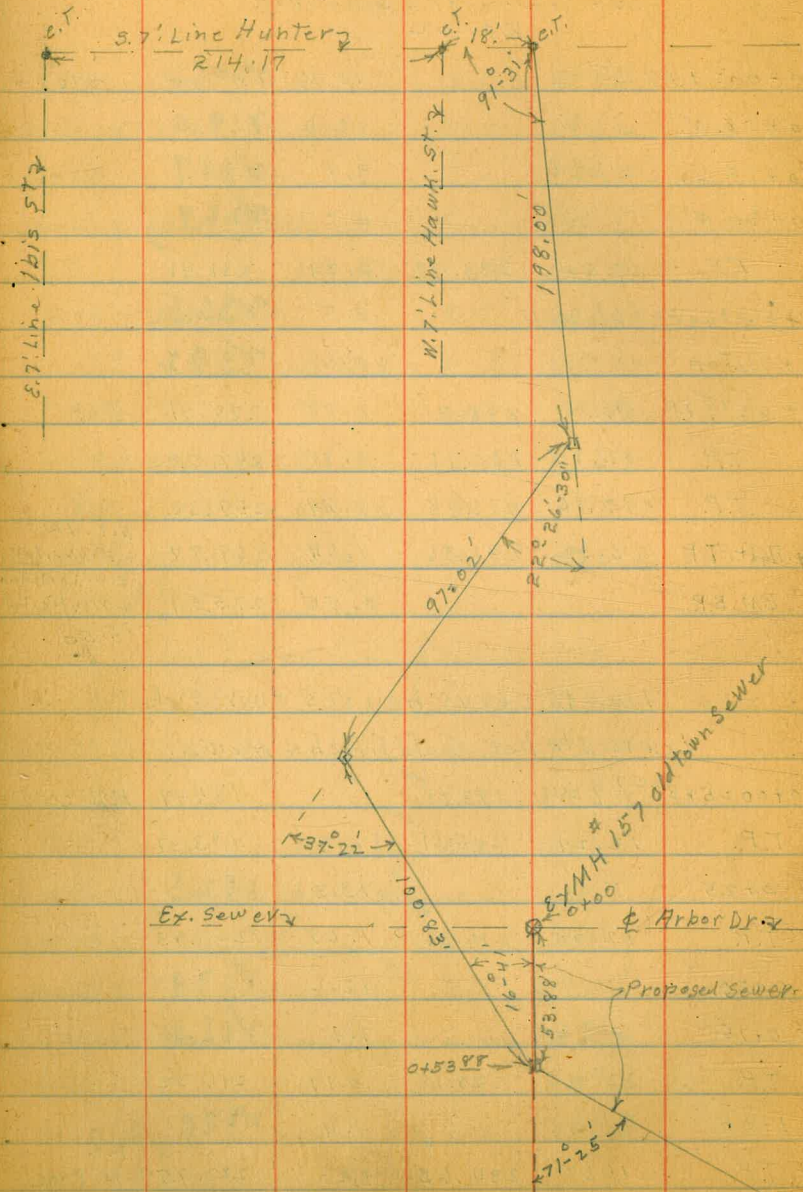
Line to serve houses on N. side

Lewis St. bet. Goldfinch & Hawk.

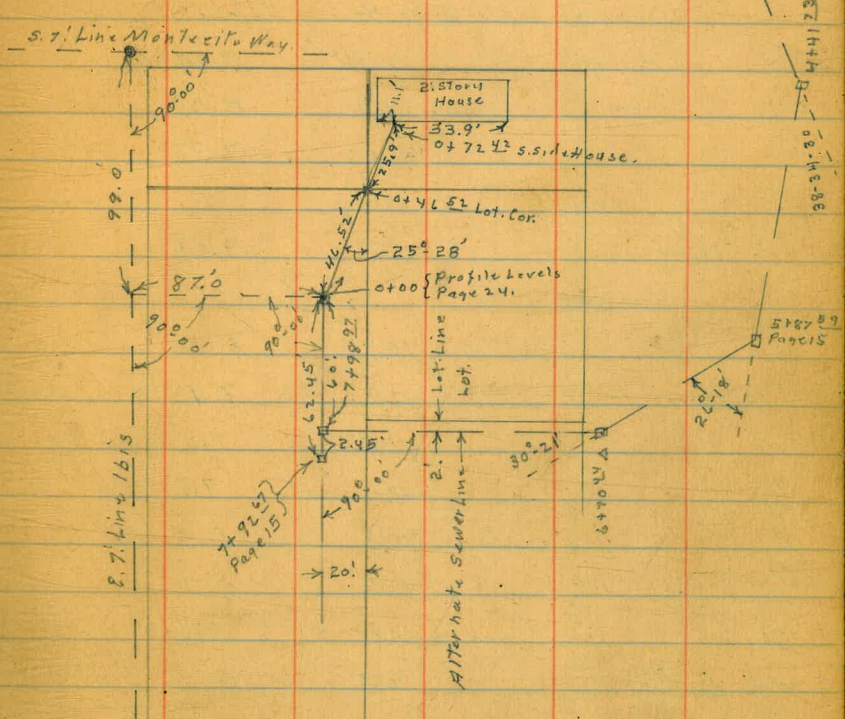
0+00 = 5+87 ⁵⁹ 9.28	193.77	184.49	Hub Δ
T.P.	12.24	205.61	0.40 193.37
0+25		13.3	192.3
T.P.	12.58	216.51	1.68 203.93
0+50		12.6	203.9
0+75		1.1	215.4
T.P.	12.86	229.18	0.19 216.32
1+00		1.4	227.8
T.P.	11.68	234.63	6.23 222.95
1+08		1.7	232.9
1+14 ³⁵ stub		1.03	233.3

T.P.
Opp. Page

Random Line from Hunter + Hawk to
Ex. MH Arbor Dr + Hawk



5+87 ⁵⁷ Δ Hub	15.96	200.45	184.49	Page 15
6+00		14.4	186.0	
+25		10.4	190.0	
+50		7.0	193.5	
3' RT of 6+50		8.4	192.0	
" " 6+50 = ditch		12.6	187.9	
6+70 ⁴⁴ Δ 30° 21' RT		4.61	195.84	
6' RT of 6+70 ⁴⁴		10.4	190.0	
9' " " 6+70 ⁴⁴ = ditch		11.6	188.9	
6+76		7.7	192.8	
6+84		4.0	196.5	
7+00		0.2	200.3	
8' RT of 7+00 = ditch		7.2	193.3	
T.P.	11.50	211.07	0.88	199.57
7+25		5.2	205.9	
7' RT of 7+25		7.6	203.5	
10' " " 7+25 = ditch		11.1	200.0	
7+50		1.1	210.0	
5' RT of 7+50 = ditch		5.0	206.1	
T.P.	10.82	221.16	0.73	210.34
7+75		7.5	213.7	
7' RT of 7+75 = ditch		9.8	211.4	
7+98 ⁷⁷ = Hub 2.45' N. of 7+92 ⁶⁷ Original line		2.05	219.11	
Hub. 7+92 ⁶⁷ Original Line		0.50	220.66	



Laurel St Cross Section
Atlantic St to Ketcher St

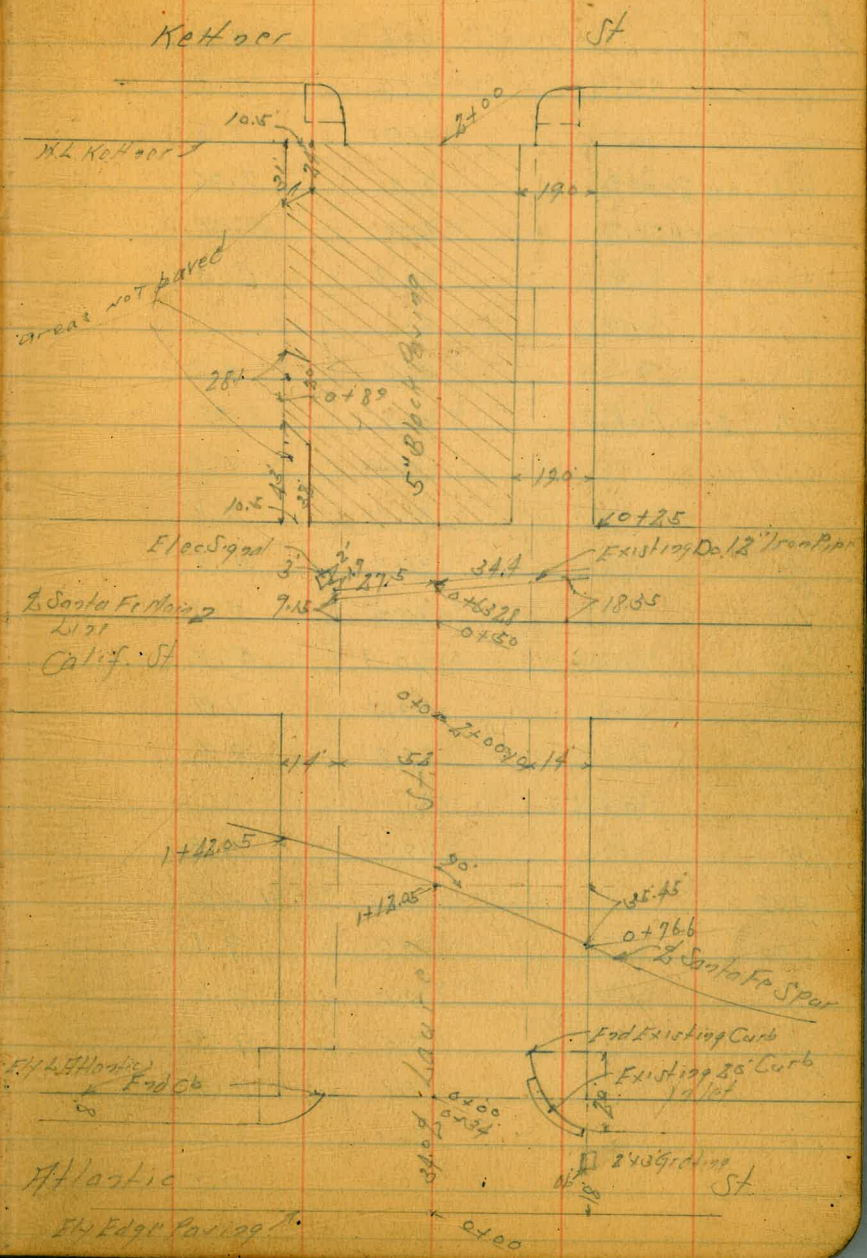
8" side
14 Cb
18" dia

B.M	7.46	19.69	12.23
TP	0.87	15.82	4.74 14.95
TP	10.37	18.77	7.42 8.40
0+00 - Fly Edge Paving Atlantic St			
N	on Paving	10.33	8.44
L	"	10.71	8.06
S	"	11.00	7.77
0+18			
0.6 S of S	on Grating	11.35	7.41
0+26			
S	Top Cb	10.77	8.00
	Gutter	11.7	7.1
	Cb	11.5	7.3
	1/4	11.1	7.7
	1/2	10.8	8.0
	3/4	10.7	8.1
	Cb	10.6	8.2
	N.L. Gutter	10.5	8.3
	Top Cb	10.00	8.77
0+34 - E.L. Atlantic - 0+00			
N		9.8	9.0
	+ 10 Top Cb	10.00	8.77
	Gutter	10.5	8.3
	Cb	10.6	8.2
	1/4	10.7	8.1

0.9 CT
14" layer
1.5" Atlantic

Indexed
e.s.k.

12-5-34
Moore
Sisson
Northey
19



18.77

1/2	10.6	8.2
1/4	11.0	7.8
Cb	11.5	7.3
+A on Grating	11.71	7.06
Top Cb	10.71	8.06
S	10.3	8.5
0+12		
S	10.1	8.7
Cb Top End Rail	10.72	8.05
Gutter	11.3	7.5
1/4	10.7	8.1
1/2	10.3	8.5
1/4	10.5	8.3
Cb	10.3	8.5
+5	9.4	9.4
N	9.2	9.6
0+50		
N	9.0	9.8
+12	8.8	10.0
Cb	9.7	9.1
1/4	9.5	9.3
1/2	9.5	9.3
1/4	9.8	9.0
Cb	10.0	8.8
S	9.3	9.5

18.77

0+76.6 = 2 Spur Track on So.

S Top High Rail	9.20	9.57
Cb	9.2	9.6
1/4	9.2	9.6
1/2	9.0	9.8
1/4	9.1	9.7
+8	9.4	9.4
Cb	8.8	10.0
N	8.7	10.1
1+120.5 = 2 Spur Track on E		
N	8.3	10.6
Cb	8.4	10.4
1/4	8.3	10.5
1/2 on Top High Rail	8.15	10.62
1/4	8.3	10.5
7/11	8.5	10.3
Cb	8.0	10.8
S	7.7	11.1
1+120.5 = 2 Spur Track on N		
S	6.3	12.5
Cb	6.8	12.0
+5	7.7	11.1
1/4	7.6	11.2
1/2	7.5	11.3
1/4	7.4	11.4
Cb	7.1	11.7

18.77

N Top High Rail	7.10	11.67
2 + 00.10 = 24.6 Calif. St. - 0 + 00		
N	2.9	14.9
cb	2.8	15.10
72	5.1	13.7
4	5.2	13.6
2	5.1	13.7
4	5.2	13.5
7	5.5	13.3
cb	4.8	14.0
S	5.0	13.8
0 + 25		
S	4.3	14.5
cb	2.9	14.9
4	4.1	14.7
2	2.9	14.9
4	4.1	14.7
78	4.2	14.6
cb	2.5	15.3
N	2.2	15.6
0 + 50 = 2 Sacto Fe Main high		
N Top Rail	2.80	15.97
1	2.91	15.86
S	2.03	15.74

18.77

0 + 83.28 - Existing D. 12 th Trap Pipe		
N End Floor Line	4.42	14.35
S End " "	4.90	13.87
0 + 75 = 0 + 0	Thread	
S	2.7	16.1
cb	2.2	16.6
4	2.3	16.5
1/2	2.0	16.8
4	2.1	16.7
cb	2.1	16.7
74	0.9	17.9
N	0.8	18.0
TP	10.93	27.46
2.24	16.53	0.800 of Elec Signal
0 + 25 = 14 1/2 of Black Paving		
N	9.1	18.1
cb on Pav.	9.54	17.92
4	9.38	18.08
2	9.30	18.16
4	9.41	18.05
78 - 1/2 Edge Pav	9.58	17.88
cb	9.9	17.6
S	10.2	17.3
0 + 10		
S	8.9	18.6
cb	9.0	18.5
75 1/2 Pav	8.93	18.53

27.46

1/4	8.82	18.64
1/2	8.70	18.76
1/4	8.83	18.66
cb	8.96	18.50
1/4	8.7	18.8
0+60		
1/4	7.9	19.6
cb	8.11	19.35
1/4	7.21	19.55
1/2	7.20	19.66
1/4	7.28	19.48
+8 - Sky Par	8.09	19.37
cb	7.9	19.6
1/4	7.7	19.8
0+80		
1/4	6.3	21.2
cb	6.8	20.7
+5 - Sky Par	6.81	20.65
1/4	6.75	20.71
1/2	6.75	20.71
1/4	6.88	20.58
cb	7.10	20.36
1/4	6.90	20.56
1+0		
1/4	5.4	22.1
cb	5.45	22.01

27.46

1/4	5.07	22.39
1/2	4.78	22.68
1/4	4.95	22.51
+8 - Sky Par	5.05	22.41
cb	5.0	22.5
1/4	5.0	22.5
1+20		
1/4	3.2	24.3
cb	3.0	24.5
+5 - Sky Par	2.95	24.51
1/4	2.81	24.65
1/2	2.56	24.90
1/4	2.70	24.76
cb	2.96	24.50
1/4	2.90	24.56
1+40		
1/4	0.40	27.06
cb	0.97	26.49
1/4	0.68	26.78
1/2	0.58	26.88
1/4	0.61	26.85
+8 - Sky Par	0.76	26.70
cb	1.0	26.5
1/4	0.7	26.8
TP	3.77	37.09
0.14		27.32

22

8709 ✓

1470

S	7.2	29.9
cb	7.5	29.6
+5 - Sky Pav	7.71	29.38
1/4	7.46	29.63
1/8	7.41	29.68
1/4	7.60	29.49
cb	8.35	28.74
H	8.50	28.59

240 - PL KeHoff

H 02 Conc Walk	3.83	33.26
cb Top End Ret.	4.38	32.71
Gutter	5.04	32.05
1/4	4.98	32.11
1/8	5.06	32.03
1/4	5.46	31.63
+8 - Sky Pav Framp	5.84	31.25
Gutter	6.05	31.04
cb Top End Ret.	5.97	31.62
S Conc Walk	4.22	32.17
BM	4.13	32.26

558 P

KeHoff

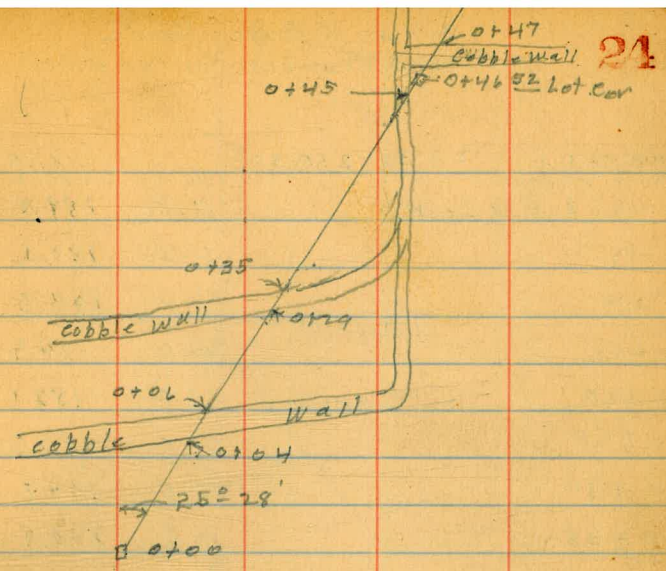
3229

Prelim. Sewer Levels
 BIK 36. Arnold + Cheats
 Plat Page 18.

12-10-34
 Miller
 Walker
 Blair

B.M.
 0+00 =
 = Stub 0+62 45019 Notes

	12.72	251.63	238.91	Page 16
0+04 Base cobbly wall	12.3	239.8		
0+06 Top " "	9.0	242.6		
0+29 Base " "	7.3	244.3		
0+35 Top " "	1.5	250.1		
0+45 " " "	1.5	250.1		
0+42.52 Base " " } Lot. cor.	2.5	249.1	Lot. cor	
0+47 Top " "	1.8	249.8		
0+54	0.4	251.2		
0+66	+ 3.2	254.8		
0+72.42 S. side House	+ 3.5	255.1	outlet	



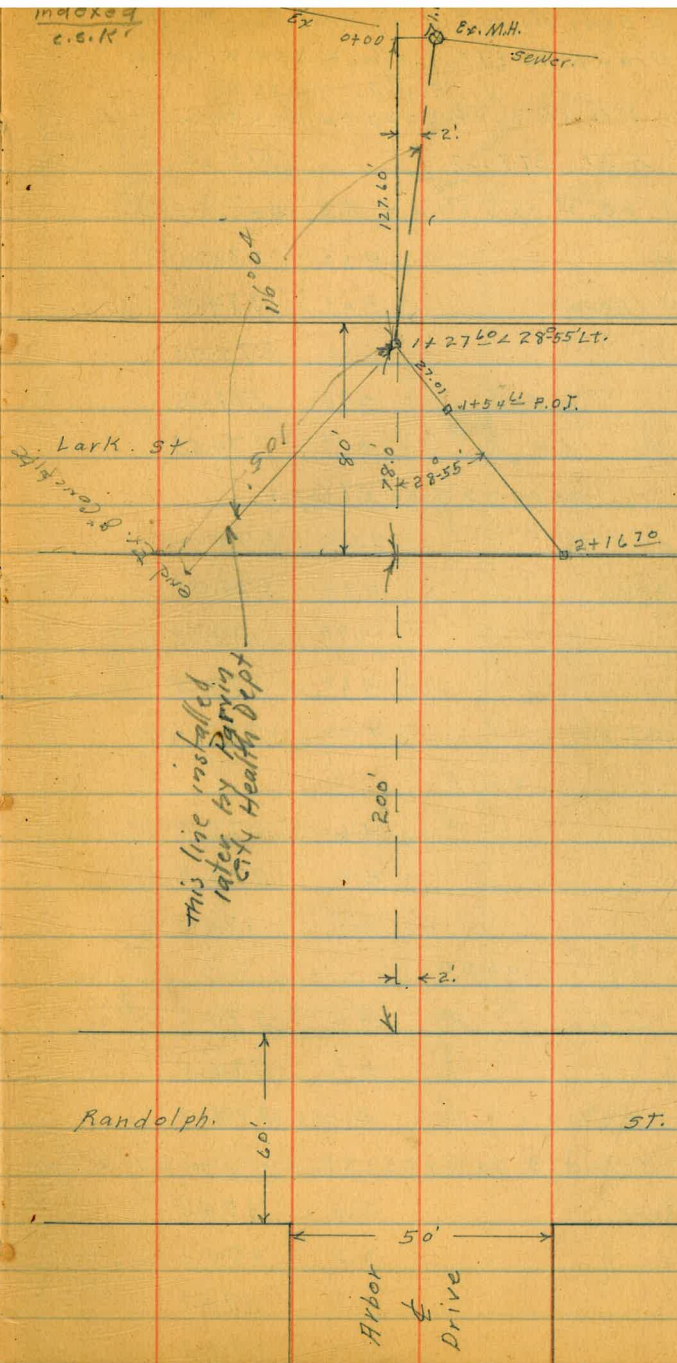
of plumbing seems to be. 4' West. of this point.

Sewer in Arbor Drive
To serve Francis Parker School

2-13-35
Miller
Walker
Bliss

INDEXED
C.E.K.

B.M. Ex M.H.	23.30	210.30		187.0	3' S. of top
Top. Ex M.H.			16.0	194.3	
0+00 = 3' N. of Ex M.H.			17.8	192.5	
0+04			17.8	192.5	
0+10			26.0	184.3	
0+16			26.0	184.3	
0+20			22.2	188.1	
0+25			17.0	193.3	
0+30			15.5	194.8	
0+38			9.5	200.8	
0+50			2.1	208.2	
T.P.	13.60	223.85	0.05	210.25	
T.P.	14.00	237.75	0.10	223.75	
0+85			8.8	229.0	
1+00			2.5	235.3	
T.P.	13.50	251.15	0.10	237.65	
1+27 ⁶⁰ Δ 28 ⁵⁵ Lt.			4.5	241.7	
T.P.	13.60	263.75	1.00	250.15	
1+48			6.6	257.2	
1+54 ⁶¹ P.O.T. Hub.			6.1	257.7	
1+80			7.2	256.6	
1+85			8.5	255.3	
1+90			6.2	257.6	
2+08			3.8	260.0	
2+16 ²⁰ W. line Lark.			4.0	259.8	



this line installed later by City Health Dept

Randolph St.

Arbor Drive

St.

2/19/35
Miller
Walker
Bliss

X Sec. Alley B.H. 40 Resub. Tera Ta (H&I)
Orange to El Cajon bet. 33rd + Felton
15' Wide
F.B. 1536 - Page 25. for Re.X Sec.

Indexed
C.S.K.

R. 426

26

B.M. B.P. 5.37 379.62 374.25 S.W. 33rd + El Cajon

20' N. of S. line = S. Curb -

E. cmt. ch.	4.62	375.00
E. gutter parvt.	5.01	374.61
♀ " "	5.17	374.45
W " " ant ch.	4.80	374.82
W. cmt. ch. ant $\frac{1}{2}$ ch.	5.19	374.43

0+00 = S. Line El Cajon.

N. S. End. cmt. ch.	4.62	375.00
W. " " pav.	4.74	374.88
♀ " " "	4.99	374.63
+ 7.3' " " "	4.60	375.02
+ 7.3 5' " cmt. ch.	4.46	375.16

0+15

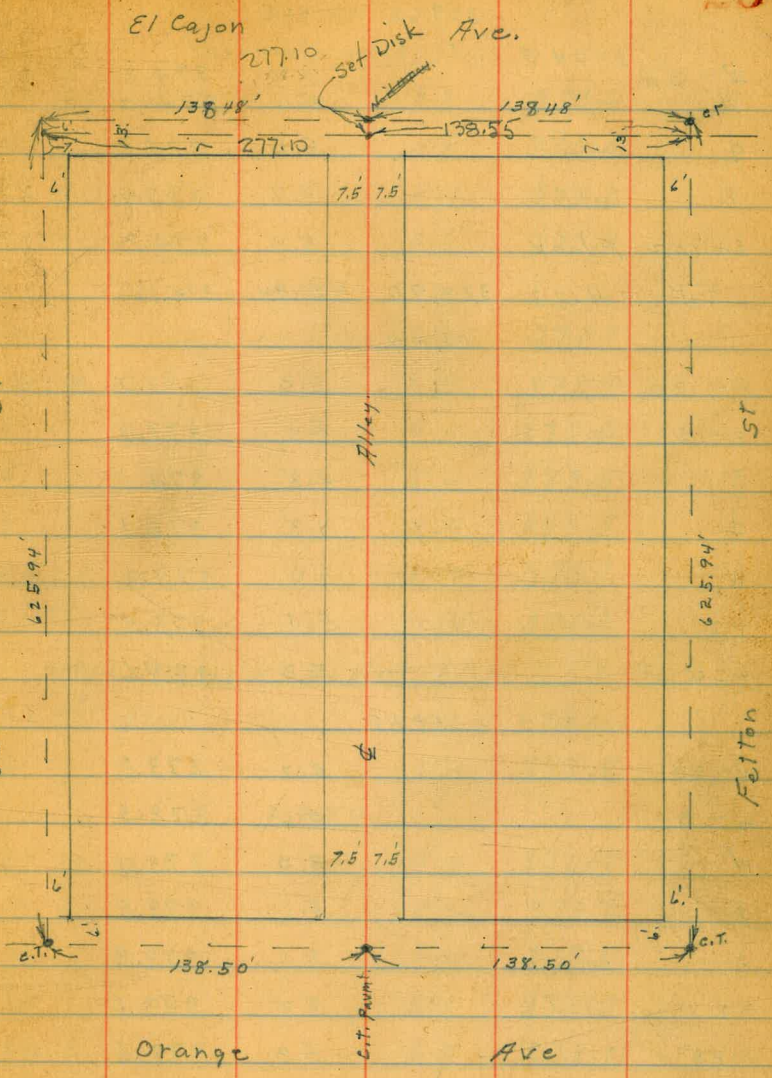
E.	4.6	375.0
♀	4.8	374.8
W.	4.8	374.8

0+50

W.	5.0	374.6
♀	5.1	374.5
E.	5.2	374.4

0+78 = N. End. 3. garages on E. dirt. floors 10.2' Back

E-102 floor	5.4	374.2
E.	5.5	374.1
♀	5.5	374.1
W.	5.4	374.2



379.62

378.90

W-30 1+04 S. End. above garages 5.4 374.2
 W. 5.6 374.0
 ♀ 5.6 374.0
 E 5.7 373.9
 2+10.2 Floor 5.4 374.2
 T.P. 4.72 378.90 5.44 374.18

♀
 W
 +2
 +30

5.3 373.6
 5.5 373.4
 5.7 373.2
 5.7 373.2

1+09

2+00

E-30 5.0 (373.0) 373.9
 E-3 5.4 373.5
 E 4.8 374.1
 ♀ 4.8 374.1
 W 5.0 373.9
 +2 5.4 373.5
 +30 5.3 373.6

W-30
 W-2
 W
 ♀
 E
 +5
 +15

6.2 372.7
 6.0 372.9
 5.5 373.4
 5.4 373.5
 5.4 373.5
 5.2 373.7
 4.8 374.1

1+40

2+16 Garage on E. dirt floor 6.5 Back

W-30 5.7 373.2
 W-3 5.6 373.3
 W. 5.0 373.9
 ♀ 5.1 373.8
 E 5.1 373.8
 +2 5.8 373.1
 +25 5.3 373.6

E-6.5' floor.
 E.

4.9 374.0
 5.4 373.5

2+30

E drainage ditch under House 5.8 373.1

E-10
 E.
 ♀
 W
 +2
 +30

5.0 373.9
 5.2 373.7
 5.4 373.5
 5.4 373.5
 5.8 373.1
 6.1 372.8

1+72

E. drainage ditch under House 6.0 372.9
 E. 5.2 373.7

378.90

2+80

- 30'	6.1	372.8
- 2.	5.9	373.0
W	5.5	373.4
⊕	5.6	373.3
E	5.4	373.5
+10	5.0	373.9

2+90

30' W. of W. Line	6.2	372.7
2' " " " "	6.0	372.9
W.	5.3	373.6

3+30

E-10	4.4	374.5
E	4.6	374.3
+4	5.4	373.5
⊕	5.4	373.5
W	5.2	373.7
+2	5.6	373.3
+25	6.1	372.8

3+65

N-30.	6.5	372.4
W-2.	5.8	373.1
W	5.4	373.5
⊕	5.3	373.6
+4	5.2	373.7
E	4.8	374.1
+10	4.6	374.3

378.90

4+00

E-10	4.7	374.2
E.	5.0	373.9
+2	5.6	373.3
⊕	5.8	373.1
W	5.8	373.1
+30	6.4	372.5
T.P.	4.25	377.34
	5.81	373.09

4+30

W-20'	4.8	372.5
W	4.5	372.8
⊕	4.5	372.8
E	4.1	373.2
+5'	3.7	373.6

4+58

W.	4.7	372.6
W+20'	4.9	372.4

4+65 garage on W. dirt floor 4' Back

E-10	4.2	373.1
E	4.7	372.6
⊕	4.7	372.6
W	4.6	372.7
W+4' floor.	4.7	372.6

377.34

4+98 garage on W. dirt floor 8' Back

W = 8' floor,	5.6	371.7
W.	5.2	372.1
⊕	5.1	372.2
E.	5.0	372.3

5+30

E-3	5.2	372.1
E	5.6	371.7
+3	6.0	371.3
⊕	6.3	371.0
W.	6.0	371.3
+20	6.3	371.0

5+60

W-10	6.9	370.4
W	7.0	370.3
⊕	6.9	370.4
+4	6.8	370.5
E	6.3	371.0
+3	6.1	371.2

6+06 ²⁴ = N. Line Orange Ave

0.15' W. of E = N. End cmt. cl.	7.62	369.72
" " " " pav.	7.68	369.66
+2.5' " "	7.99	369.35
⊕ " "	7.98	369.36
W. " "	7.95	369.39
W. W. End. cmt. cl.	7.83	369.51

377.34

411+4 BIK 40 Kesub Jeralta

29

14' S. of N. Line = N. ct. of Orange

W. cmt. cl.	8.11	369.23
W. gutter pav	8.80	368.54
⊕ " "	8.76	368.58
E " "	8.63	368.71
E. cmt. cl.	8.03	369.31
T.P.	8.14	374.56
chk original B.M.	2.31	374.25
	8.92	368.42
		374.25 ✓

Sewer Profile
 N end Blk 33 La Jolla Hermosa West
 between Beaumont & Waverly 42
 La Jolla Blvd
 Palomar

Indexed
 C.S.K.

Moore
 J. J. SON
 Northport
 2-2-35

30

NEBP	11.39	89.87		78.48
T.P.	12.69	101.39	1.17	88.70
T.P.	12.78	113.37	0.80	100.59
T.P.	12.55	125.13	0.79	112.58
0-61	Top 6" CI Covers	EL.	10.90	114.23
"	FL sewer		20.90	104.23
0+22	Top edge pal.		6.57	118.56
"	FL 8" Conc pipe	END	10.24	114.89
0+00	on stub		6.50	118.63
0+13	ground		5.1	120.0
0+13	1.5' S. end	Top Conc. ob.	5.88	119.25
T.P.	12.59	137.66	0.06	125.07
0+40			11.7	126.0
+75			6.0	131.7
1+00			2.4	135.3
T.P.	12.76	150.80	0.12	137.54
1+25			10.7	139.6
+50			6.8	143.5
+75			3.7	146.6
T.P.	12.75	162.95	0.10	150.20
2+00			11.3	151.7
+25			7.2	155.8
+50			3.4	159.6

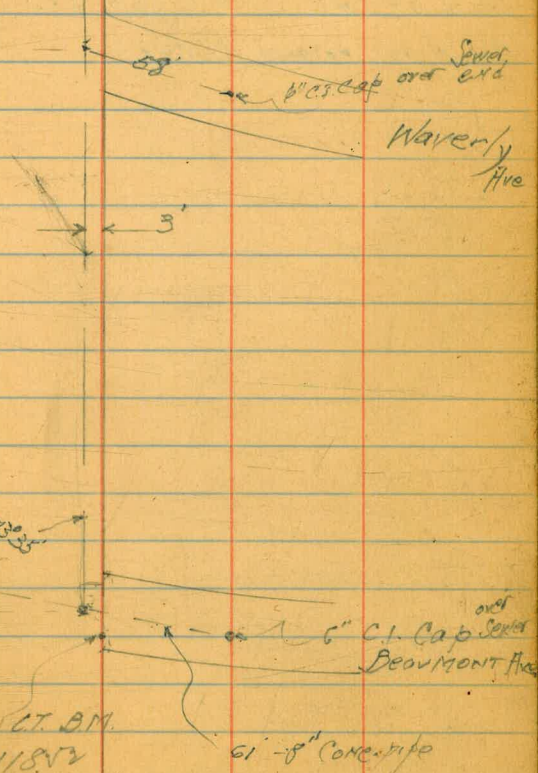
Set
 B.M.

3+08.60

0+00

20.35

Set B.M.
 118.52



next page

		162.95		
7.9	4.71	167.26	0.40	162.55
2+80			4.1	163.2
2+95	Top w/ly ob.	4.59		162.67
3+08.6	" paring &	4.19		162.36

Please check to profile

58' S of last Top 6" ci cap. 12.55 15471 pav. E.L.
 Could not remove ci. cap

Moore
Stinson
Northard
4/15/35

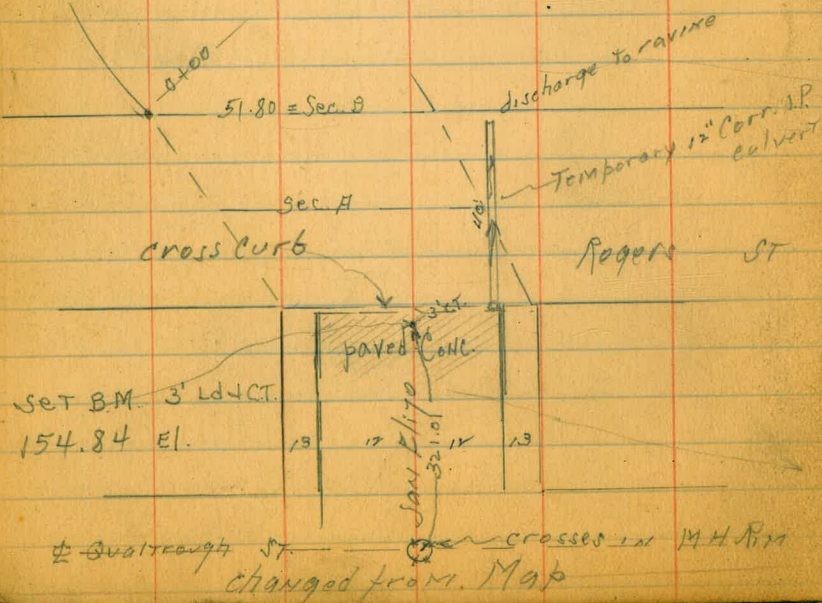
Indexed
G.S.R.

Line + levels on Armada Terrace
Thru PL 174 = Rogers N.Y.

Wly Line = Base Line.

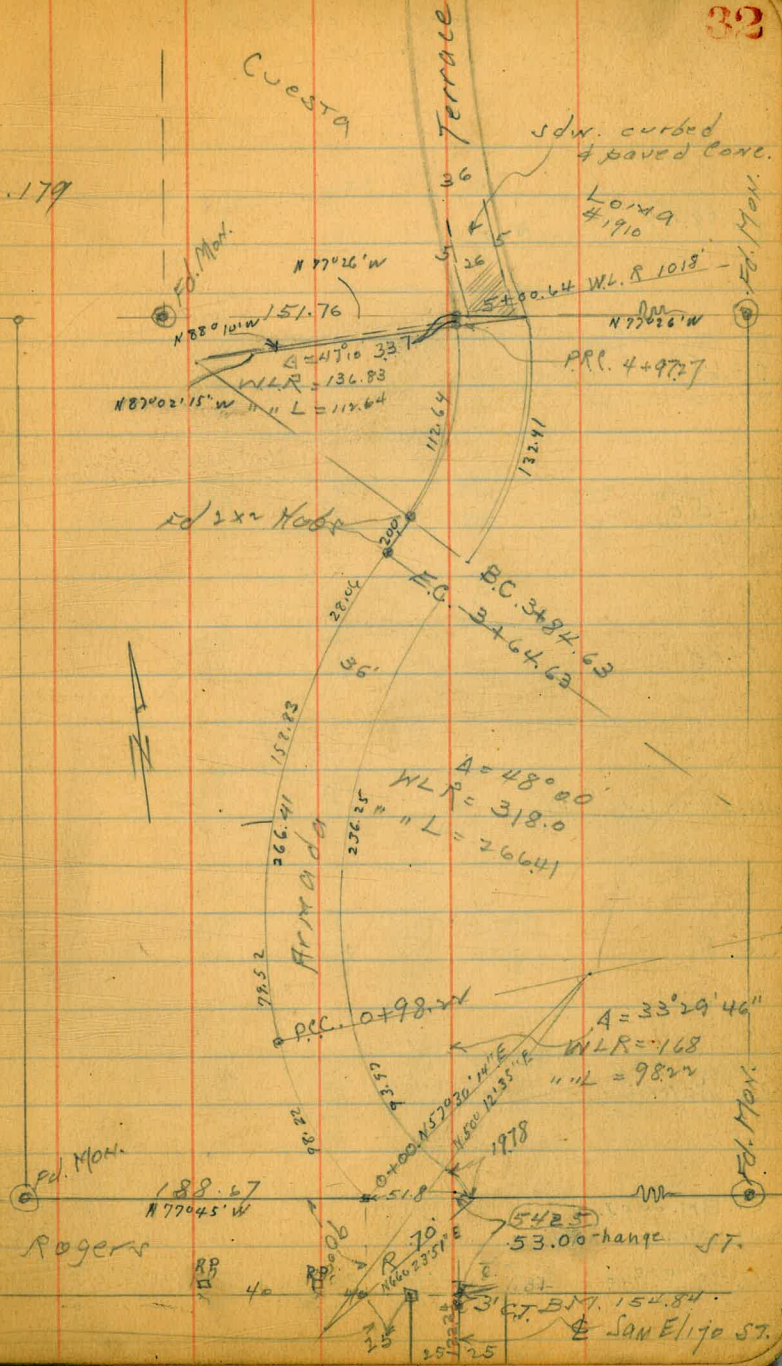
page 33 for levels

o = Set 2x2 Hubs



PL 179

Plotted A.E.B.



Levels on Armada Ter.
Rogers Nly.

Wk.

AT

33

0+98.22 PCC Hub

$\frac{152.03}{687}$	$\frac{148.2}{16.7}$	$\frac{148.7}{17}$	$\frac{144.8}{20.1}$	$\frac{144.2}{20.7}$
	$\frac{18}{18}$	$\frac{28}{28}$	$\frac{36}{36}$	$\frac{50}{50}$

0+65

$\frac{155.9}{9.0}$		$\frac{142.5}{22.4}$	$\frac{137.2}{32.2}$	$\frac{129.7}{35.2}$	$\frac{127.7}{37.4}$
		$\frac{18}{18}$	$\frac{36}{36}$	$\frac{51}{51}$	$\frac{60}{60}$

0+50

$\frac{156.1}{8.8}$	$\frac{152.2}{12.7}$	$\frac{147.9}{16.0}$	$\frac{142.7}{22.2}$	$\frac{127.1}{30.8}$	$\frac{125.5}{29.4}$
	$\frac{18}{18}$	$\frac{28}{28}$	$\frac{36}{36}$	$\frac{51}{51}$	$\frac{60}{60}$

0+00

$\frac{151.8}{13.1}$	$\frac{154.2}{13.7}$	$\frac{144.9}{23.0}$	$\frac{135.9}{29.2}$
	$\frac{78}{78}$	$\frac{36}{36}$	$\frac{51}{51}$

Sec. B - Nly Lino Rogers

$\frac{151.8}{13.1}$	$\frac{156.9}{13.0}$	$\frac{142.6}{17.3}$	$\frac{140.2}{24.0}$	$\frac{133.4}{31.5}$	$\frac{133.9}{31.0}$
	$\frac{75}{75}$	$\frac{40}{40}$	$\frac{31.8}{31.8}$	$\frac{64}{64}$	$\frac{75}{75}$

Sec A

$\frac{152.6}{12.3}$	$\frac{153.4}{11.5}$	$\frac{150.9}{13.0}$	$\frac{139.7}{11.2}$
	$\frac{24}{24}$	$\frac{33}{33}$	$\frac{50}{50}$

Sly Rogers

$\frac{155.4}{9.5}$	$\frac{155.27}{9.1}$	$\frac{155.22}{9.68}$	$\frac{154.82}{10.08}$	$\frac{153.83}{11.07}$	$\frac{154.73}{10.17}$	$\frac{153.6}{11.3}$
	$\frac{76}{76}$	$\frac{73}{73}$	$\frac{24}{24}$	$\frac{37}{37}$	$\frac{37}{37}$	$\frac{50}{50}$
		907	2 pm	907	37	06

Set. BM. on AT.
San Elijo

3' of SL
Rogers

157 40 R.P. Hub 7.27 16490 157.63

16490

limit of inlet

W.

N.

T.P. 198 163.40 3.48 161.42

163.40

3400

$\frac{163.5}{1.4}$	$\frac{163.9}{1.0}$	$\frac{161.5}{3.1}$	$\frac{159.3}{6.0}$	$\frac{155.3}{9.6}$
	10	18	36	50

+65

$\frac{162.3}{2.6}$	$\frac{156.7}{8.2}$	$\frac{157.9}{7.0}$	$\frac{155.4}{9.5}$
	18	36	50

+50

$\frac{160.9}{4.0}$	$\frac{159.8}{5.1}$	$\frac{156.3}{8.6}$	$\frac{142.8}{17.1}$	$\frac{139.6}{25.3}$
	13	18	36	60

+25

$\frac{166.8}{3.0}$	$\frac{158.6}{5.9}$	$\frac{153.8}{11.0}$	$\frac{143.5}{21.4}$
	18	36	50

2400

$\frac{161.9}{3.0}$	$\frac{158.0}{6.9}$	$\frac{153.9}{11.0}$	$\frac{149.8}{17.1}$
	18	36	50

1+50

$\frac{162.5}{2.4}$	$\frac{159.1}{5.8}$	$\frac{156.1}{8.8}$	$\frac{153.8}{11.0}$
	18	36	50

1+20

$\frac{162.1}{4.8}$	$\frac{157.3}{7.6}$	$\frac{155.1}{9.8}$	$\frac{152.7}{12.2}$
	18	36	50

164.90

164.90

0.44 = curb Face

W66 C ECB

$\frac{154.82}{8.58}$	$\frac{154.72}{8.58}$	$\frac{154.79}{8.61}$
-----------------------	-----------------------	-----------------------

$\frac{154.36}{9.04}$	$\frac{154.26}{9.20}$	$\frac{153.81}{9.49}$
-----------------------	-----------------------	-----------------------

W.L				
$\frac{156.22}{7.13}$	$\frac{154.3}{9.1}$	$\frac{154.3}{9.1}$	$\frac{153.6}{9.8}$	
	5	18	36	

$\frac{156.4}{7.0}$	$\frac{154.9}{8.5}$	$\frac{155.1}{8.13}$	$\frac{153.5}{9.9}$	$\frac{156.3}{12.1}$	$\frac{14.78}{15.6}$	$\frac{145.0}{18.4}$
	11	13	18	23	36	50

$\frac{156.5}{6.9}$	$\frac{156.1}{7.1}$	$\frac{154.1}{9.3}$	$\frac{150.5}{14.9}$	$\frac{148.5}{14.9}$
	13	18	36	50

$\frac{158.2}{4.7}$	$\frac{157.1}{6.3}$	$\frac{152.2}{6.7}$	$\frac{152.2}{10.7}$	$\frac{150.1}{13.3}$
	2	18	36	50

$\frac{161.5}{1.9}$	$\frac{152.2}{4.4}$	$\frac{152.6}{4.8}$	$\frac{154.2}{8.7}$	$\frac{152.8}{10.6}$
	3	18	36	50

$\frac{162.4}{1.0}$	$\frac{160.4}{3.0}$	$\frac{159.6}{3.8}$	$\frac{155.9}{7.4}$	$\frac{153.3}{10.1}$
	2	18	36	50

5+00.64 Taken on Pueblo Line

+97.27 PRC

+50

4

3+84.63 PC

2+64.63 EC

3+50

163.40

163.40

9 + 70.67 EC

9 + 00

8 + 80

8 + 60

8 + 40

T.P. 0.46 156.27 759 155.81

8 + 02.46 = PCC

7

16340

W/25 C EC

$\frac{149.37}{11.90}$ $\frac{144.41}{11.86}$ $\frac{144.44}{11.83}$

$\frac{151.40}{4.87}$ $\frac{151.31}{4.96}$ $\frac{151.35}{4.92}$

$\frac{152.99}{9.30}$ $\frac{152.89}{3.30}$ Sand pile

$\frac{154.19}{2.08}$ $\frac{154.29}{1.98}$ $\frac{154.38}{1.89}$

$\frac{155.13}{11.4}$ $\frac{155.11}{11.6}$ $\frac{155.22}{1.05}$

$\frac{156.27}{\text{---}}$

$\frac{155.82}{7.58}$ $\frac{155.82}{7.58}$ $\frac{155.85}{7.55}$

$\frac{155.40}{8.00}$ $\frac{155.22}{8.08}$ $\frac{155.20}{8.20}$

16340

17 + 20.42 Taken diag. on Pueblo Line

17 + 00

11 + 68.76 PC

11 + 00

T.P. 005 130.65 1289 130.60

10 + 00

T.P. 0.17 143.49 12.95 143.32
156.27

858 11888 11.77	1181 11812 12.48	1175 11265 13.00
-----------------------	------------------------	------------------------

120.00 10.65	119.85 10.80	119.81 10.84
-----------------	-----------------	-----------------

122.98 7.67	122.91 7.74	122.82 7.83
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130.34 0.31	130.43 0.22	130.32 0.33
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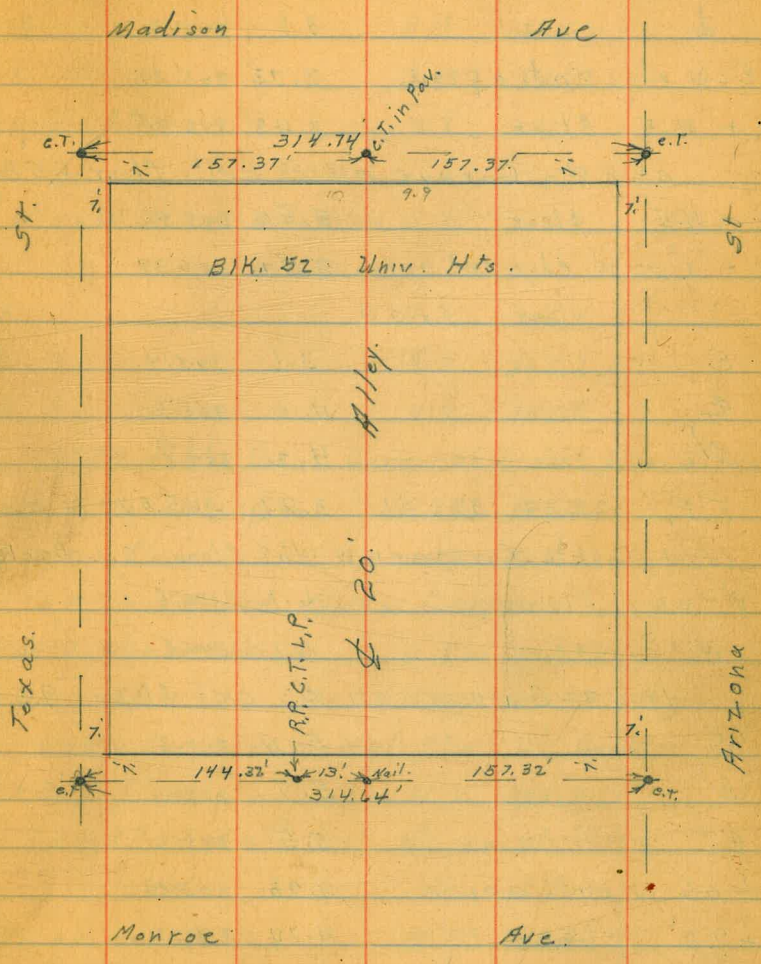
130.65
⚡

141.14 2.35	141.22 2.22	141.24 2.25
----------------	----------------	----------------

143.49
⚡

5- -35 X Sec. Alley BIK. 52. Univ. Hts. ^{in 40x69} _{c-s-R.} Mad + Texa. S.E. 346.03
 Miller Walker Bldg
 Monroe to Madison bet. Texas + Arizona.

B.M. B.P.	10.00	348.96	338.96	S.E. Texas + Monroe.
14.5 of N. line = N. ch. Monroe. AVE				
W-20	ent. ch.	6.77	342.19	
W-20	gutter	7.5	341.5	
W.	"	6.7	342.3	
W.	ent. ch.	6.37	342.59	
Φ	gutter	6.4	342.6	
E	"	6.1	342.8	
E.	ent. ch.	5.45	343.51	
+20	" "	4.74	344.22	
+20	gutter	5.3	343.64	
0400 = N. line Monroe. AVE.				
0.2 W. of E. =	ent. ch. Ret.	5.20	343.76	
	gutter	5.2	343.8	
	Φ	6.0	343.0	
0.1 E. of W. =	gutter	6.1	342.9	
" " " "	ent. ch. Ret.	6.16	342.80	
0407, N.				
W.		5.4	343.6	
Φ		5.4	343.6	
E		4.8	344.2	
0430				
E		4.1	344.9	
Φ		4.4	344.6	
W		4.9	344.1	



0+56 N. Garage on E. cmt. floor 4.5' Back		
W	4.1	344.9
¢	3.8	345.2
E = W. edge cmt. apron.	3.75	345.21
+ 4.5' floor	3.48	345.48
0+88 = Garage on E. cmt. floor 4.5' Back		
E - 4.5' floor	3.50	345.46
E - 1.1' W. edge cmt apron	3.57	345.39
	1+00	
E	3.6	345.4
¢	4.0	345.0
W	4.2	344.8
T.P.	5.59	350.66
1+14 Double Garage on W. dirt floor 0.6 Back		
W - 0.6 floor	6.1	344.6
W	6.1	344.6
1+43 = Garage on E. cmt floor 9.5' Back		
W.	5.4	345.3
¢	5.7	345.0
E	5.5	345.2
+ 7.5' = cmt. apron.	4.93	345.73
+ 9.5' floor	4.74	345.92
1+66 Garage on W. dirt floor on. Line		
E	5.1	345.6
¢	5.4	345.3
W. floor,	5.7	345.0

2+04 Garage on E. dirt floor 0.4 Back		
W.	5.4	345.3
¢.	5.4	345.3
E.	5.0	345.7
+ 0.4' floor.	4.8	345.9
2+08.		
5' W. of W. line E. side House	4.8.	345.9 floor
2+50		
E.	4.3	346.4
¢	5.0	345.7
W	4.9.	345.8
2+54 S. Edge Double Garage on W. cmt. floor 3' Back		
W+0.9' E. edge cmt. apron	4.78	345.88
W+3'0' floor	4.73	345.93
2+72 = N. End. above Garage.		
W+0.9' E. edge cmt. apron	4.76	345.90
W+3'0' floor	4.72	345.94
2+82 Garage on W. dirt. floor 3' Back		
W+3' floor	4.4	345.9
2+97 S. End. cmt. ch. on W. line		
3+00		
W. on cmt. ch.	4.50	346.16
W.	4.7	346.0
¢ on M.H. Cover.	4.33	346.33
E.	4.0	346.7
3+25 = N. End. cmt. curb on W. line		
W.	4.3	346.7

350.66

3+30 garage on W. dirt floor 1.2 Back				
W-1.2 floor	4.3	346.4		
3+39 garage on W. dirt floor 1.2 Back				
W-1.2 floor	4.1	346.6		
3+49 garage on W. cmt. floor 1.3' Back				
E	3.6	342.1		
♀	4.0	346.2		
W cmt. apron	4.04	346.62		
W+1.3' floor	3.95	346.71		
3+59 garage on W. cmt. floor 1.3' Back				
W. cmt. apron	3.97	346.69		
W+1.3' floor	3.80	346.86		
3+68 garage on W. cmt. floor 0.8' Back				
1' E. of W. line cmt. apron	3.87	346.79		
W+0.8' floor.	3.90	346.76		
3+89 Double garage on W. dirt floor 4' 0" Back				
W+4' floor	3.1	342.6		
	4+00			
W.	3.6	342.1		
♀	3.1	342.6		
E	2.8	342.9		
4+08. Garage on E. cmt. floor 20' Back				
4' E. of E. = cmt. apron.	1.74	348.92		
20' " " " = floor	0.46	350.20		
4+19 garage on W. dirt floor 0.3' Back.				
W+63 floor	3.2	342.5		
T.P.	9.11	357.11	2.66	348.00

357.11

Alley BIK 52. J.H.

40

4+31 Garage on W. cmt. floor 0.3' Back.				
0.7' in alley cmt. apron	9.50	347.61		
0.3 Back = floor.	9.38	347.73		
{ Garage on W. cmt. floor 0.1' Back				
4+40 { " " E. dirt " 5' 0" Back				
E-5' floor	8.4	348.7		
E	8.7	348.4		
♀	9.1	348.0		
+9.2 cmt. apron	9.42	342.69		
W+70.1' floor.	9.34	347.77		
4+78 S. End 3 Garages on W. cmt. floor. 2.4' Back				
W+08 cmt. apron.	7.63	349.48		
W+2.4 floor	7.30	349.81		
	4+88			
W+08' apron	7.50	349.61		
W+2.4 floor	7.20	349.91		
4+81 { Garage on E. cmt. floor 3.3' Back				
W-2.4 floor	6.60	350.51		
W-0.8 cmt. apron.	6.97	350.14		
W	7.1	350.1		
♀	7.6	349.5		
E.	7.1	350.0		
E+1.6 cmt. apron	6.90	350.2		
E+3.7 floor	6.64	350.47		

357.11

5+05 = Garage on E. emt. floor	4' Back.		
E-4.0 floor	5.15	351.96	
E. emt. apron.	5.82	351.29	
+4	6.6	350.5	
⊥	7.0	350.1	
W	6.9	350.2	
+0.8 emt. apron.	6.84	350.27	
+2.4 floor	6.60	350.51	
5+11 N. End 3 Garages on W.	2.4 Back		
W+0.8' emt. apron	6.73	350.38	
W+2.4 floor	6.55	350.56	
5+31 garage on W. emt floor	2.4 Back		
W-2.2 floor	5.78	351.33	
W-0.5 emt. apron.	5.95	351.16	
W	6.0	351.1	
⊥	5.9	351.2	
+7	5.5	351.6	
E.	4.9	352.2	
5+42 garage on W. emt. floor	2.2 Back		
E	4.2	352.9	
+2.	4.9	352.2	
⊥	5.5	351.6	
W	5.6	351.5	
+0.5 emt. apron	5.61	351.50	
+2.2 floor	5.49	351.62	

357.11

Alley B/K 52. U.H.

5+60

W	4.5	352.6
⊥	4.8	352.3
+4	4.6	352.5
+5	3.0	354.1
E.	2.7	354.4

5+90

E	2.0	355.1
+5.	2.4	354.7
⊥	3.0	354.1
W	3.4	353.7

5+99 S. line Madison Ave.

W. emt. el.	3.19	353.92
W. pav.	3.26	353.85
⊥ "	2.89	354.22
E. "	2.30	354.81
E. emt. el.	1.83	355.28

14' N. of S. line = S. curb

E. emt. el.	1.80	355.31
E. gutter pav.	2.49	354.62
⊥ " "	3.27	353.84
W. " "	3.95	353.16
W. emt. el.	3.63	353.48
B.M. B.P.	11.12	345.99

S. E. Texas
+ Madison
346.03

11

X-sections proposed road
 from Park Blvd. to 11th St
 and Russ Blvd.

Alignment in Book 1495
 Page 53.

2+50

2+00

1+50

1+00.

0+50

B.M. 12.26 201.60 189.34

Station 3+37 Non hub
 Book 1495 P 59

May 27-35
 Loudon
 Lesey
 Grabowski

Indexed
 C.S.K.

$\frac{9.4}{21}$
 191.2 ✓ ✓

8.9
 192.7 ✓

$\frac{8.2}{23}$
 193.4 ✓

$\frac{7.1}{43}$
 194.5 ✓

$\frac{7.5}{25}$

194.1 ✓

7.2

194.4 ✓

$\frac{7.2}{18}$ $\frac{4.5}{26}$ $\frac{5.6}{40}$

194.4 ✓ 197.1 ✓ 196.0 ✓

$\frac{5.7}{26}$

195.9 ✓

5.1

196.5 ✓

$\frac{4.5}{40}$

197.1 ✓

$\frac{3.8}{27}$
 197.8 ✓

3.8

197.8 ✓

$\frac{3.2}{40}$
 198.4 ✓

$\frac{1.8}{27}$
 199.8 ✓
 Edge
 Struck

1.3

200.3 ✓

$\frac{1.4}{33}$
 200.2 ✓

L+

⊕

R+

T.P. 1.19 179.83 11.92 178.64

5+12

$$\frac{9.1}{50} \\ 181.5 \checkmark$$

$$9.3 \\ 181.3 \checkmark$$

$$\frac{17.7}{21} \\ 172.9 \checkmark$$

$$\frac{19.3}{50} \\ 171.3 \checkmark$$

5+00

$$\frac{9.3}{40} \\ 181.3 \checkmark$$

$$9.0 \\ 181.6 \checkmark$$

$$\frac{8.9}{12} \\ 181.7 \checkmark$$

$$\frac{16.8}{31} \\ 173.8 \checkmark$$

$$\frac{18.5}{50} \\ 172.1 \checkmark$$

4+50

$$\frac{5.8}{36} \\ 184.8 \checkmark$$

$$\frac{7.1}{11} \\ 183.1 \checkmark$$

$$\frac{8.2}{7} \\ 182.4 \checkmark$$

$$8.4 \\ 182.2 \checkmark$$

$$\frac{8.9}{17} \\ 181.7 \checkmark$$

$$\frac{8.7}{40} \\ 181.9 \checkmark$$

4+00

$$\frac{6.0}{36} \\ 184.6 \checkmark$$

$$\frac{4.6}{22} \\ 186.0 \checkmark$$

$$\frac{4.1}{6} \\ 186.5 \checkmark$$

$$4.5 \\ 186.1 \checkmark$$

$$\frac{4.6}{13} \\ 186.0 \checkmark$$

$$\frac{4.0}{23} \\ 186.6 \checkmark$$

3+50

$$\frac{1.1}{27} \\ 189.5 \checkmark$$

$$\frac{2.2}{13} \\ 188.4 \checkmark$$

$$2.2 \\ 188.4 \checkmark$$

$$\frac{1.9}{28} \\ 188.7 \checkmark$$

3+37⁴ B.C.

$$\frac{0.6}{40} \\ 190.0 \checkmark$$

$$\frac{1.1}{24} \\ 189.46 \checkmark$$

$$\frac{1.7}{11} \\ 188.9 \checkmark$$

$$\frac{1.4}{30} \\ 189.2 \checkmark$$

3+30⁷⁴ E.C.

$$\frac{0.3}{40} \\ 190.26 \checkmark$$

$$\frac{0.6}{28} \\ 190.0 \checkmark$$

$$0.7 \\ 189.9 \checkmark$$

$$\frac{1.0}{28} \\ 189.56 \checkmark$$

T.P. 1.22 190.56 12.26 189.34

3+00

201.60

$$\frac{11.0}{26} \\ 190.6 \checkmark$$

$$10.7 \\ 190.9 \checkmark$$

$$\frac{10.6}{8} \\ 191.1 \checkmark$$

$$\frac{8.4}{19} \\ 193.2$$

$$\frac{9.5}{26} \\ 192.1$$

$$\frac{9.5}{44} \\ 192.1$$

T.P. 1.90 158.33 13.10 156.43

7+00

Edg. Ext
road

→ $\frac{7.8}{40}$ $\frac{6.0}{38}$ $\frac{6.3}{32}$ $\frac{17.0}{12}$ $\frac{18.0}{9}$ $\frac{19.0}{20}$ $\frac{21.0}{36}$ $\frac{19.0}{40}$ $\frac{16.5}{50}$
 161.7 ✓ 163.5 ✓ 163.2 ✓ 152.5 ✓ 151.5 ✓ 150.5 ✓ 148.5 ✓ 150.5 ✓ 150.5 ✓ 153.0 ✓

6+50

Edg. Exist
road.

→ $\frac{3.3}{43}$ $\frac{1.5}{40}$ $\frac{2.1}{34}$ $\frac{12.8}{73}$ 13.1 $\frac{13.1}{9}$ $\frac{11.5}{19}$ $\frac{11.0}{44}$ $\frac{11.0}{50}$
 166.2 ✓ 168.0 ✓ 167.4 ✓ 156.2 ✓ 156.4 ✓ 156.4 ✓ 158.0 ✓ 158.5 ✓ 158.5 ✓

6+00

$\frac{4.4}{12}$ 5.8 $\frac{5.7}{15}$ $\frac{6.6}{33}$ $\frac{6.7}{50}$
 165.1 ✓ 165.7 ✓ 163.8 ✓ 162.9 ✓ 162.8 ✓

T.P. 1.20 169.53 11.50 168.33

6+00

Edg. Exist
road

→ $\frac{4.2}{52}$ $\frac{3.5}{47}$ $\frac{1.6}{36}$ $\frac{2.1}{29}$
 175.63 ✓ 176.33 ✓ 176.33 ✓ 177.73 ✓

5+50

$\frac{+1.0}{46}$ $\frac{+2.2}{23}$ $\frac{7.9}{7}$ 8.2 $\frac{8.6}{15}$ $\frac{7.5}{29}$ $\frac{10.7}{51}$
 186.83 ✓ 182.03 ✓ 171.93 ✓ 171.63 ✓ 171.23 ✓ 170.33 ✓ 169.13 ✓

5+25

$\frac{+3.3}{50}$ $\frac{+3.0}{22}$ $\frac{5.4}{7}$ ✓ 6.6 ✓ $\frac{7.6}{76}$ ✓ $\frac{8.9}{43}$ ✓ $\frac{9.3}{54}$ ✓

177.83

183.1 ✓ 182.83 ✓ 174.43 ✓ 173.23 ✓ 172.23 ✓ 170.93 ✓ 170.53 ✓

9+50

+5.7	3.8	7.9	10.2		10.2	9.0	9.2	15.3	15.3
40	20	10	8	9.9	15	17	28	46	50
✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
154.1	144.6	140.5	138.2	138.5	158.2	159.4	159.2	153.1	135.1

9+00

+2.4	4.8	5.9	5.6	5.9		4.8	11.4	11.4	12.2
40	23	22	13	1	4.7	11	25	40	50
✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
150.8	144.1	142.5	142.8	142.5	143.2	145.6	157.0	157.0	156.2

8+50

+0.8	1.2	1.3	1.7	0.0	0.2	1.8	8.7	9.7	10.3	12.0	12.0
40	35	28	17	15	5		10	17	34	35	50
✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
149.2	147.2	147.1	146.7	148.4	148.2	146.6	159.7	158.7	158.1	156.4	156.1

8+25⁰⁴ E.C.

+1.0	+1.2	0.2	+2.6	+1.3			6.6	7.7	8.3	11.4	11.4	7.4
45	34	22	20	11	4.4		5	10	30	35	40	50
✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
149.36	149.56	148.6	151.0	149.7	144.0	141.8	140.7	140.1	157.0	157.0	141.0	

8+00

+4.4	+3.9	+4.4	+5.0		6.1	7.0	11.0	11.1	7.0
48	27	25	16	3.5	9	26	32	22	50
✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
152.8	152.3	152.8	153.4	144.9	142.3	141.4	157.2	157.3	141.1

T.P. 2.32 148.36 12.29 146.04

7+50

158.33

Edg Ext	2.0	0.0	0.7	10.3		12.3	17.2	17.0	13.1	12.4
road 20	37	34	28	10	11.3	14	23	30	33	41
	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	156.33	158.33	157.63	148.0	147	146.0	141.1	141.3	145	145.2

T.P. 1.46 140.88 10.19 139.42
12+50

$\frac{+0.1}{50}$	$\frac{1.0}{49}$	$\frac{4.5}{21}$	9.4	$\frac{13.0}{20}$	$\frac{18.0}{50}$
149.2 ✓	148.6 ✓	145.1 ✓	140.2 ✓	136.6 ✓	131.6 ✓

12+00

$\frac{+7.8}{50}$	$\frac{+7.0}{48}$	$\frac{+1.7}{32}$	$\frac{1.8}{9}$	4.3	$\frac{12.8}{34}$	$\frac{15.9}{50}$
157.4 ✓	156.6 ✓	151.2 ✓	147.8 ✓	145.3 ✓	136.8 ✓	133.2 ✓

11+50

$\frac{+7.8}{50}$	$\frac{+6.6}{20}$	2.8	$\frac{10.6}{25}$	$\frac{17.3}{50}$
157.4 ✓	156.2 ✓	146.8 ✓	159.0 ✓	132.3 ✓

TP 2.18 149.61 9.73 147.43
11+00

stake at 11+50
Tennis Court Fedd. →

$\frac{+1.0}{38}$	$\frac{0.8}{25}$	$\frac{6.7}{15}$	11.5	$\frac{27.0}{41}$	$\frac{28.9}{45}$	$\frac{31.0}{47}$	$\frac{31.0}{50}$
158.2 ✓	156.4 ✓	150.5 ✓	145.2 ✓	130.2 ✓	128.3 ✓	126.2 ✓	126.2 ✓

10+50

$\frac{+1.4}{47}$	$\frac{0.5}{37}$	$\frac{6.4}{22}$	$\frac{9.4}{11}$	13.4	$\frac{19.3}{13}$	$\frac{26.4}{28}$	$\frac{26.2}{48}$	$\frac{25.0}{50}$
158.6 ✓	156.7 ✓	156.8 ✓	147.8 ✓	143.8 ✓	137.9 ✓	130.8 ✓	131.0 ✓	132.2 ✓

TP 10.04 157.16 1.24 147.12
10+02⁰⁹ B.C.
148.36

$\frac{+10.2}{50}$	$\frac{+5.3}{38}$	$\frac{1.3}{16}$	8.8	$\frac{12.5}{8}$	$\frac{14.3}{10}$	$\frac{14.3}{20}$	$\frac{14.3}{30}$	$\frac{13.3}{32}$	$\frac{13.1}{40}$
158.6 ✓	155.2 ✓	147.1 ✓	139.6 ✓	135.9 ✓	134.1 ✓	134.1 ✓	134.1 ✓	135.2 ✓	135.3 ✓

14+50

T.P. 4.14 99.70 11.97 95.56

T.P. 0.91 107.53 13.10 106.62

14+40

14+00

13+50

T.P. 1.06 119.72 12.53 118.66

T.P. 1.64 131.19 11.33 129.55

13+15

13+00

140.88

$\frac{+10.0}{50}$
109.7 ✓

$\frac{+8.8}{7.4}$
108.5 ✓

2.4
97.3 ✓

$\frac{1.7}{8}$
98.0 ✓

$\frac{5.8}{20}$
93.9 ✓

$\frac{7.0}{50}$
92.7 ✓

$\frac{9.8}{50}$
109.9 ✓

11.2
108.5 ✓

$\frac{25.6}{28}$
94.1 ✓

$\frac{26.0}{50}$
93.7 ✓

$\frac{4.4}{50}$
115.3 ✓

$\frac{9.3}{41}$
110.4 ✓

$\frac{11.5}{20}$
108.7 ✓

11.2
108.5 ✓

$\frac{8.4}{32}$
111.3 ✓

$\frac{13.2}{50}$
106.5 ✓

$\frac{+12.0}{50}$

$\frac{+11.0}{40}$

$\frac{6.6}{9}$

7.5

$\frac{9.3}{50}$

131.7 ✓

130.7 ✓

113.1 ✓

110.7 ✓

110.4 ✓

$\frac{0.8}{50}$
140.1 ✓

$\frac{4.0}{29}$
136.9 ✓

11.3
129.6 ✓

$\frac{29.5}{31}$
111.4 ✓

$\frac{30.4}{50}$
110.5 ✓

$\frac{+2.4}{50}$

$\frac{0.3}{40}$

9.2

$\frac{10.1}{13}$

$\frac{28.6}{40}$

$\frac{29.2}{50}$

143.3 ✓

140.6 ✓

131.7 ✓

130.8 ✓

112.3 ✓

111.7 ✓

17+50

$$\begin{array}{r} 4.2 \\ 50 \\ \hline 97.7 \\ \checkmark \end{array}$$

$$\begin{array}{r} 6.1 \\ 4.6 \\ 50 \\ \hline 85.8 \\ \checkmark \end{array}$$

$$\begin{array}{r} 7.8 \\ 84.1 \\ \checkmark \end{array}$$

$$\begin{array}{r} 8.7 \\ 29 \\ 50 \\ \hline 83.2 \\ \checkmark \end{array}$$

$$\begin{array}{r} 8.8 \\ 50 \\ \hline 83.1 \\ \checkmark \end{array}$$

17+00

$$\begin{array}{r} 1.7 \\ 50 \\ \hline 90.2 \\ \checkmark \end{array}$$

$$\begin{array}{r} 6.7 \\ 39 \\ 50 \\ \hline 85.2 \\ \checkmark \end{array}$$

$$\begin{array}{r} 6.4 \\ 85.5 \\ \checkmark \end{array}$$

$$\begin{array}{r} 7.2 \\ 36 \\ 50 \\ \hline 84.7 \\ \checkmark \end{array}$$

$$\begin{array}{r} 8.4 \\ 38 \\ 50 \\ \hline 83.5 \\ \checkmark \end{array}$$

$$\begin{array}{r} 8.4 \\ 50 \\ \hline 83.5 \\ \checkmark \end{array}$$

16+50

$$\begin{array}{r} +3.1 \\ 50 \\ \hline 95.0 \\ \checkmark \end{array}$$

$$\begin{array}{r} 2.8 \\ 43 \\ 50 \\ \hline 91.1 \\ \checkmark \end{array}$$

$$\begin{array}{r} 3.3 \\ 29 \\ 50 \\ \hline 89.6 \\ \checkmark \end{array}$$

$$\begin{array}{r} 5.3 \\ 19 \\ 50 \\ \hline 86.6 \\ \checkmark \end{array}$$

$$\begin{array}{r} 6.4 \\ 85.5 \\ \checkmark \end{array}$$

$$\begin{array}{r} 6.6 \\ 41 \\ 50 \\ \hline 85.3 \\ \checkmark \end{array}$$

$$\begin{array}{r} 7.7 \\ 50 \\ \hline 84.2 \\ \checkmark \end{array}$$

16+00

$$\begin{array}{r} +0.3 \\ 50 \\ \hline 92.1 \\ \checkmark \end{array}$$

$$\begin{array}{r} 0.5 \\ 19 \\ 50 \\ \hline 91.4 \\ \checkmark \end{array}$$

2.9

$$\begin{array}{r} 4.4 \\ 41 \\ 50 \\ \hline 87.5 \\ \checkmark \end{array}$$

$$\begin{array}{r} 6.1 \\ 44 \\ 50 \\ \hline 85.8 \\ \checkmark \end{array}$$

$$\begin{array}{r} 6.1 \\ 50 \\ \hline 85.8 \\ \checkmark \end{array}$$

T.P 1.52 91.87 9.35 90.35

15+50

$$\begin{array}{r} +2.4 \\ 50 \\ \hline 102.1 \\ \checkmark \end{array}$$

$$\begin{array}{r} 6.7 \\ 12 \\ 50 \\ \hline 93.0 \\ \checkmark \end{array}$$

8.2

$$\begin{array}{r} 12.2 \\ 44 \\ 50 \\ \hline 87.5 \\ \checkmark \end{array}$$

$$\begin{array}{r} 13.3 \\ 50 \\ \hline 86.4 \\ \checkmark \end{array}$$

$$102.11 \checkmark$$

$$93.0 \checkmark$$

$$91.5 \checkmark$$

$$87.5 \checkmark$$

$$86.4 \checkmark$$

15+00

99.70

$$\begin{array}{r} +9.6 \\ 50 \\ \hline 109.3 \\ \checkmark \end{array}$$

$$\begin{array}{r} +8.0 \\ 39 \\ 50 \\ \hline 107.7 \\ \checkmark \end{array}$$

$$\begin{array}{r} 2.5 \\ 15 \\ 50 \\ \hline 97.2 \\ \checkmark \end{array}$$

7.0

$$\begin{array}{r} 11.3 \\ 50 \\ \hline 88.4 \\ \checkmark \end{array}$$

$$109.3 \checkmark$$

$$107.7 \checkmark$$

$$97.2 \checkmark$$

$$92.7 \checkmark$$

$$88.4 \checkmark$$

B.M.

5.00 check. Hub sta
18+43²³

(83.07)
Book 1495
Page 58

19+00

Edg. road
to school

+8.4
-7.50
Shrubby bank → 7 5.0
96.5 ✓ 84.4 ✓ 83.1 ✓
83.10

6.3
50
81.8 ✓

18+43²³ L.

+6.6 + 5.2 3.3
50 33 12 5.00

Road to school

94.7 ✓ 93.3 ✓ 84.8 ✓ 83.1 ✓

6.0
50
82.1 ✓

T.P.

2.62 88.10 6.39 85.48

17+97⁸⁷ E.C.

91.87

1.4
50

2.4
48

6.4

8.6
14

9.3
50

85.5 ✓

83.3 ✓

82.6 ✓

90.5 ✓

89.5 ✓

±

83.3

Mission Valley Road Ext.
 East of College Ave. to F1 Cajon Ave

index d
 c.s.k.

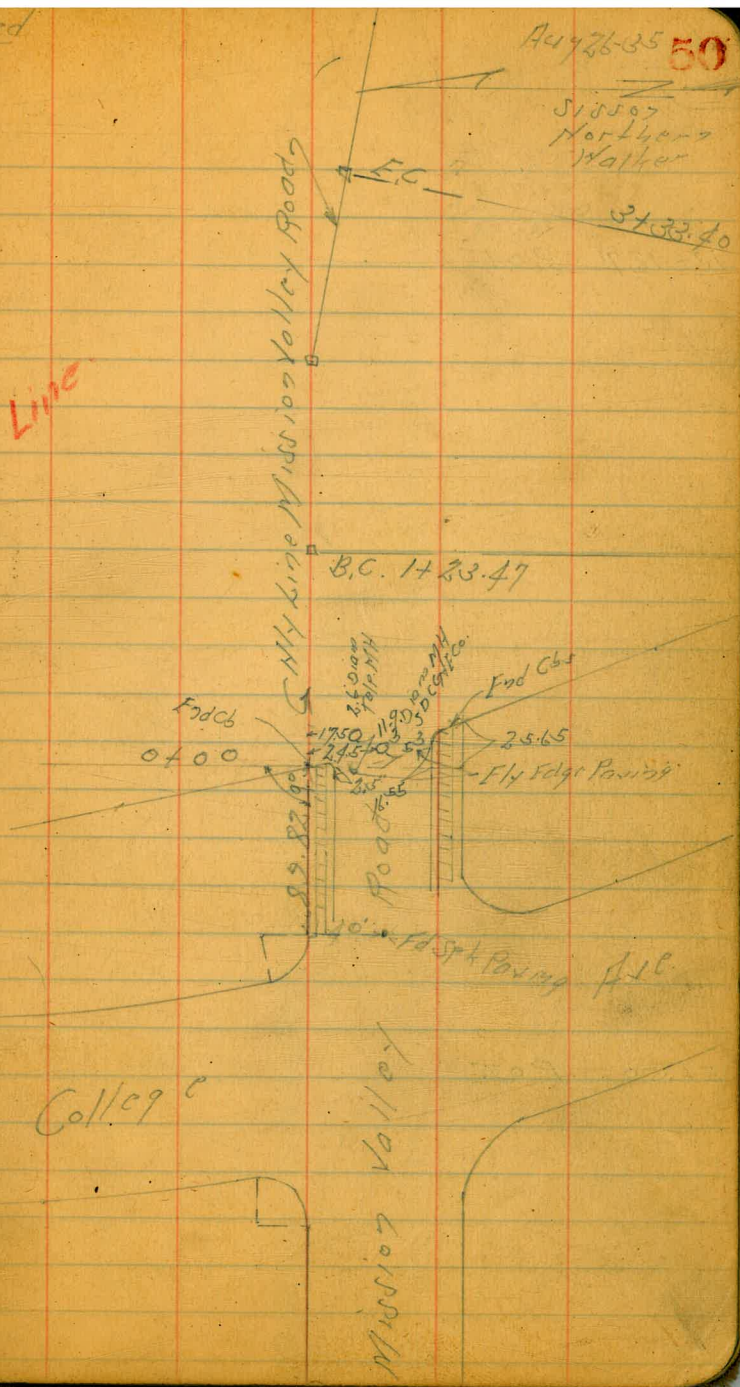
Aug 26-35 50

North Line Stationing Rt.

+33.40	F.C.		1° 51'
0+0	A	9° 42'	1° 04' 76"
+50	P	124°	2° 55' 45"
2+0	T	105.21	1° 46' 14"
+50	L	209.93	0° 36' 83"
1+23.47	B.C.	0.13862	

First Line

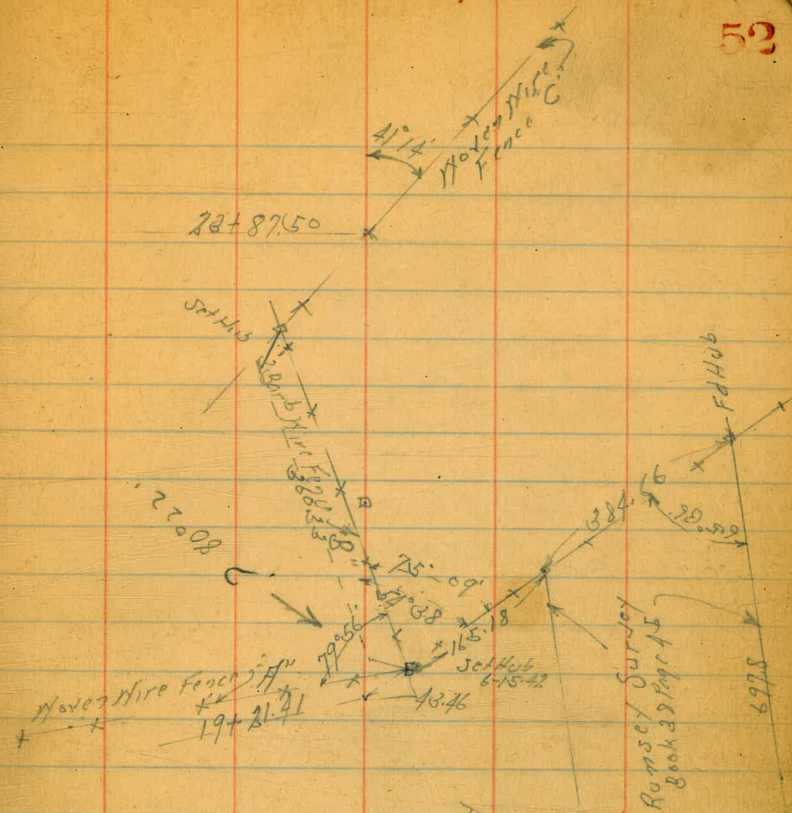
0+00



137 12.71 P.O.T.

57 50 P.O.T.

21+00.10 P.O.T.



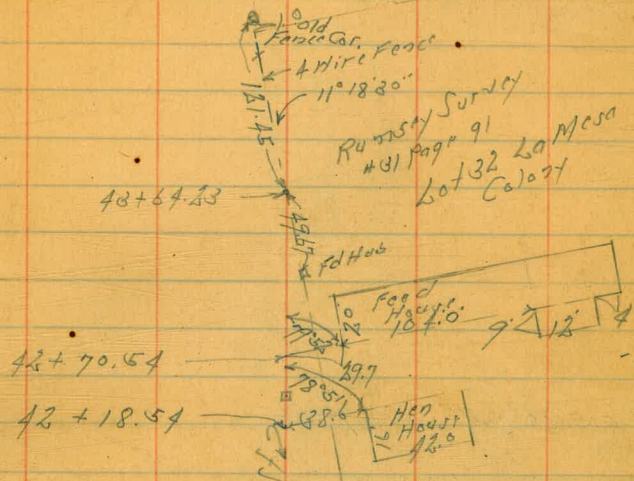
My line P.O.P. 2

 Lot 12 Colony
 La Mesa Colony

Fd Hub

42+36.24 P.O.T.

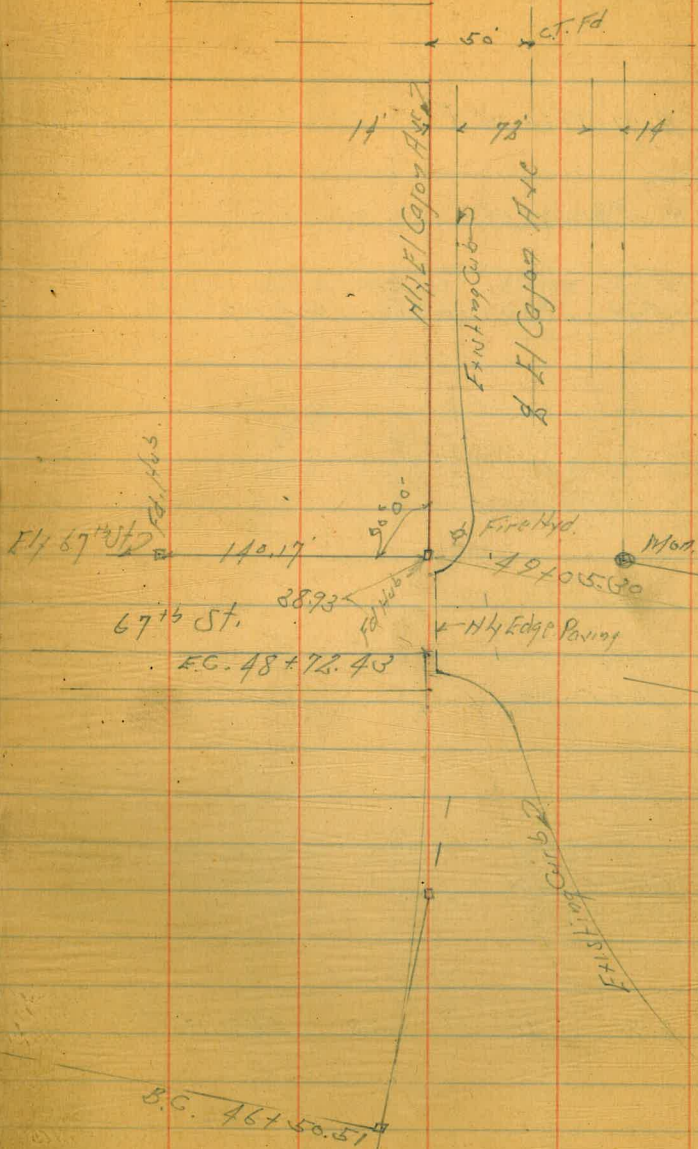
36+18.93 P.O.T.



64

49+05.30 = Ely of 67th St.

48+72.43 E.C.	5° 28.83	
+50	1° 55.55	A 10° 57' 40"
48+0	3° 41.46	R 1160.0
+50	2° 27.38	T 111.30
47+0	1° 13.29	L 231.92
46+50.51 B.C.	0 1.4817	



Cross Section Mission Valley Road Ext.
East of College Ave. to El Cajon Ave.

8-28-35
Susan
Walter 56

on R. D. Tap. M.H.

450.79
10.62

on R. D. JOGIE M.H.

450.81
10.60

see sketch page 50

Edge End of Paving Takes on 5199.

451.01	450.33	450.98	450.84	451.46
10.40	110.8	10.73	15.57	9.95
26' Topch	26' Gut		26' Gut	26' Topch

0+00

450.41 ✓

451.31	451.01	450.31	445.41	450.91	450.45	451.05	451.41
10.1	10.4	11.1	11.0	10.50	10.96	10.86	10.8
40	28	37	21		26' Gut	26' Topch	40

00-547 = Cb F.C. on S.

450.31	449.79	449.16	449.80	449.29	449.98	450.11
11.1	11.62	12.25	11.61	12.12	11.43	11.3
40	26' Cb	26' Gut		26' Gut	26' Topch	40

00-898 = Cb F.C. on N

449.91	449.50	448.96	449.11	448.67	448.47
11.5	11.91	12.25	12.00	12.24	12.94
40	26' Cb	26' Gutter	on Pav	26' on Pav	40 on Pav

B.M. 8.90 461.41 1.58 452.51

J.E. Top Ht.
Mission
Point College

B.M. 0.45 454.03 458.64

N.W. Top Ht.
Mission
Point College
W. of Linda
Pass

Lt

L

Rt

0+85

457.41	457.01	455.11	453.41	454.81	453.91
10	44	6.3	8.0	6.6	7.5
10	30	12		33	40

0+70

453.51	453.01	454.01	452.91	454.81	453.81
7.9	8.1	7.1	8.5	6.6	7.6
10	30	15		12	40

0+50

452.41	452.01	452.81	452.41	452.41	453.81	454.51
9.0	9.4	8.6	9.0	9.0	7.6	6.9
10	30	30		15	8	40

0+45

452.41	451.81	452.51	451.91	452.11	453.11	453.11	451.61
9.0	9.6	8.9	9.5	9.3	8.15	8.6	9.8
10	35	18		15	8	25	40

0+30

453.21	451.31	451.01	451.81	451.21
8.2	10.1	10.4	9.6	10.2
10	35		25	40

0+25.6

450.81	450.71	450.91	451.61
10.6	10.7	10.5	9.8
18		35	40

461.41

461.41

Lt

L

Rl

+25

454.816.6
40455.21

6.2

454.916.6
40

2+0

454.716.7
40455.116.3
20457.31

4.1

455.116.3
15455.016.4
30455.715.7
40

+75

454.816.6
40454.41

7.0

454.516.9
25456.914.5
40

+150

454.816.6
40455.216.2
30456.514.9
20455.01

5.5

454.217.2
12454.317.1
40

+2347

BCP

454.377.04
40 on Hub454.117.2
6.0454.417.0
35455.016.4
32455.216.2
40

1+0

456.614.8
40456.614.8
38454.317.1
12454.41

7.0

453.817.6
40

461.41

461.41

Lt L Rt

TP 4.08 459.79 5.70 455.71 ^{07 F.C. H₂O} 3+33.40

+50

454.21 455.41 457.51 457.61 455.31 455.41 456.21
7.2 6.0 3.9 3.8 6.1 6.0 5.2
40 25 10 20 30 40

+33.40 F.C.

455.71 454.91 455.61 455.71 457.51
5.7 6.5 5.8 5.7 3.9
40 35 30 40

+20

456.41 455.31 455.51 457.51 457.01 455.41 455.61
5.0 6.1 5.9 3.9 4.4 6.0 5.8
40 32 15 10 20 40

+80

455.61 455.51 455.41 457.11
5.8 5.9 6.0 4.3
40 30 40

+60

456.21 455.81 455.81 457.01 457.81 455.51 456.31
5.2 5.6 5.6 4.4 3.6 5.9 5.1
40 20 6 10 30 40

+40

455.81 457.81 458.21 455.81 456.81 455.61 455.31
5.6 3.6 3.2 5.6 4.6 5.8 6.1
40 30 10 15 30 40

461.41

461.41

Lt.

S

Pt

+50

450.99	451.19	450.89	450.89	450.89	449.19	449.19
8.8	8.6	8.9	8.9	8.9	10.6	10.6
50	40	30		30	40	50

570

453.19	453.19	452.59	452.59
6.6	6.6	7.2	7.2
40	30		40

+50

453.89	454.79	453.69	453.79	454.59	454.09
5.9	5.0	6.1	6.0	5.2	5.7
40	30	10		30	40

+25

454.89	454.69	453.99	454.39	455.89	455.29	454.49
4.9	5.1	5.8	5.4	5.9	4.5	5.3
40	35	10		35	35	40

410

454.29	454.69	454.29	454.69	455.19	454.69
5.5	5.1	5.5	5.1	4.6	5.1
40	40		30	30	40

375

453.99	455.09	457.39	457.49	455.09	454.59	455.69
5.8	4.7	2.4	2.3	4.7	5.2	4.1
40	35	15		30	30	40

159.79

159.79

Lt. Z PI

+75

428.54	427.14	427.34	428.74	434.54	439.64	440.84	442.94	443.54
26.0 80	22.4 80	22.2 40	20.8 25	15.0	9.9 25	8.7 40	6.6 50	6.0 60

+50

432.94	432.14	432.04	433.24	433.04	432.94	438.94	441.24
16.6 95	17.4 40	17.5 30	16.3 25	16.5	16.6 10	10.6 40	8.3 55

+25

439.04	437.94	437.44	438.54	440.24	441.94
10.5 80	11.6 40	12.1	11.0 25	9.3 40	7.6 55

6+0

447.84	444.34	443.54	442.34	442.74	443.24	444.84
4.7 60	5.2 40	6.0 20	7.2	6.8 20	6.3 40	4.7 55

5+75

448.74	448.14	449.04	448.34	448.54	447.24	447.74
0.8 55	1.1 40	0.5 30	1.2	1.0 10	2.3 40	1.8 50

4P

1.85 449.54 18.10 447.69

449.54

459.79

Lt Z Rt

+25

<u>443.73</u>	<u>445.73</u>	<u>448.73</u>	<u>450.53</u>	<u>451.13</u>	<u>451.43</u>	<u>453.53</u>
17.4	15.4	12.4	10.6	10.0	9.7	7.6
60'	40'	20'		20'	40'	150'

870

<u>440.93</u>	<u>442.83</u>	<u>445.73</u>	<u>446.43</u>	<u>447.53</u>	<u>448.53</u>	<u>451.23</u>
20.2	18.3	15.4	14.7	13.6	12.6	9.9
60'	40'	20'	461.13	10'	40'	155'

TP 12.07 461.13 0.48 449.06

+75

<u>432.34</u>	<u>436.54</u>	<u>437.84</u>	<u>439.94</u>	<u>441.14</u>	<u>443.34</u>	<u>445.84</u>	<u>447.74</u>
17.2	13.0	11.7	9.6	8.4	6.2	3.7	1.8
75'	55'	40'	20'		20'	40'	50'

+50

<u>425.24</u>	<u>432.54</u>	<u>433.44</u>	<u>436.14</u>	<u>437.04</u>	<u>439.74</u>	<u>442.64</u>	<u>446.44</u>
21.3	17.0	16.1	13.4	12.5	9.8	6.9	3.1
80'	53'	40'	20'		20'	40'	80'

+25

<u>419.34</u>	<u>427.74</u>	<u>431.34</u>	<u>435.54</u>	<u>440.54</u>	<u>443.04</u>	<u>445.34</u>
30.2	21.8	18.2	14.0	9.0	6.5	4.2
100'	40'	30'		130'	40'	80'

770

<u>422.04</u>	<u>421.74</u>	<u>427.74</u>	<u>430.14</u>	<u>435.04</u>	<u>438.54</u>	<u>440.34</u>	<u>443.24</u>
27.5	27.8	21.8	19.4	14.5	11.0	9.2	6.3
85'	65'	40'	30'		20'	40'	80'

449.54

449.54

Lt.

Z

R1

+50

<u>457.95</u>	<u>457.85</u>	<u>460.35</u>	<u>460.05</u>	<u>458.95</u>	<u>459.75</u>
6.2	6.3	3.8	4.1	5.3	4.1
40	30		15	25	40

1040

<u>459.05</u>	<u>457.95</u>	<u>458.65</u>	<u>460.85</u>	<u>459.15</u>
5.1	6.1	5.5	3.3	5.0
40	30		20	40

+150

<u>457.85</u>	<u>457.65</u>	<u>458.55</u>	<u>460.95</u>	<u>460.15</u>
6.3	6.5	5.6	3.2	4.0
40	20		30	40

TP

4.04

464.15

1.02

460.11

3 Nails Pole
R1 8+70

464.15

510

<u>454.13</u>	<u>454.73</u>	<u>455.93</u>	<u>457.23</u>	<u>457.83</u>	<u>458.93</u>
7.0	6.4	5.2	3.9	3.3	2.2
50	40	25		20	40

+75

<u>450.23</u>	<u>453.13</u>	<u>454.93</u>	<u>455.93</u>	<u>457.53</u>	<u>458.03</u>
10.9	8.0	6.7	5.2	3.6	3.1
60	40	20		10	40

8+50

<u>447.43</u>	<u>449.73</u>	<u>450.93</u>	<u>453.83</u>	<u>455.03</u>	<u>456.53</u>	<u>456.73</u>	<u>456.33</u>
13.7	11.4	10.2	7.3	6.1	4.6	4.9	4.8
60	40	30		20	30	40	50

461.13

461.13

Lt. & Pt.

750

<u>458.35</u>	<u>458.55</u>	<u>459.55</u>	<u>459.25</u>	<u>458.75</u>	<u>459.75</u>	<u>459.55</u>	<u>460.55</u>
5.8	5.6	4.6	4.9	5.4	4.4	4.6	3.6
40	25	15		15	20	30	40

712.71

4.35 459.80 07.12.11

1310

<u>458.15</u>	<u>458.15</u>	<u>459.15</u>	<u>459.95</u>	<u>458.65</u>	<u>458.75</u>
6.0	6.0	5.0	4.8	5.5	5.4
40	30	20	5		40

750

<u>458.35</u>	<u>458.85</u>	<u>457.65</u>	<u>458.65</u>	<u>458.15</u>
5.8	5.8	6.5	5.5	6.0
40	15		18	40

1210

<u>455.95</u>	<u>457.15</u>	<u>456.85</u>	<u>458.35</u>	<u>458.15</u>
8.2	7.0	7.6	5.8	6.0
40	25		20	40

750

<u>456.75</u>	<u>457.25</u>	<u>457.15</u>	<u>459.75</u>	<u>458.75</u>	<u>459.15</u>
7.4	6.9	7.0	4.7	5.4	5.0
40	30		20	24	40

742 = Pow. Po/r 13 Pt. o/lz

1170

<u>457.55</u>	<u>458.95</u>	<u>458.35</u>	<u>457.85</u>	<u>459.25</u>	<u>459.55</u>
6.6	5.2	5.8	6.3	4.9	4.6
40	25		15	25	40

464.15

464.15

Lt.	g	Rt.
-----	---	-----

<u>458.11</u>	<u>458.91</u>	<u>459.01</u>
5.2	4.7	4.3
40		40

<u>457.81</u>	<u>458.31</u>	<u>458.61</u>
5.5	5.0	4.7
40		40

<u>457.81</u>	<u>458.21</u>	<u>458.51</u>
5.5	5.1	4.8
40		40

<u>457.71</u>	<u>458.11</u>	<u>458.61</u>
5.6	5.2	4.7
40		40

7P	4.00	463.31	4.84	459.31	Mark Pole 14.14 34.14 of 8	463.31
----	------	--------	------	--------	----------------------------------	--------

<u>457.75</u>	<u>457.95</u>	<u>458.65</u>	<u>459.05</u>
6.4	6.2	5.5	5.1
40		20	40

+14 = Power Pole 34.14 of 8

<u>458.55</u>	<u>458.35</u>	<u>458.75</u>	<u>459.05</u>	<u>458.95</u>	<u>460.15</u>	<u>460.15</u>
5.6	5.8	5.4	5.1	5.2	4.0	4.0
40	30	15		15	30	40

1470

464.15

464.15

L

S

R1

+50

$$\begin{array}{r} \underline{457.31} \\ 6.0 \\ 40 \end{array}$$

$$\begin{array}{r} \underline{457.31} \\ 6.0 \end{array}$$

$$\begin{array}{r} \underline{457.01} \\ 6.3 \\ 40 \end{array}$$

1840

$$\begin{array}{r} \underline{457.61} \\ 5.7 \\ 40 \end{array}$$

$$\begin{array}{r} \underline{457.61} \\ 5.7 \end{array}$$

$$\begin{array}{r} \underline{457.81} \\ 5.5 \\ 40 \end{array}$$

+50

$$\begin{array}{r} \underline{457.91} \\ 5.4 \\ 40 \end{array}$$

$$\begin{array}{r} \underline{458.21} \\ 5.1 \end{array}$$

$$\begin{array}{r} \underline{458.71} \\ 4.6 \\ 40 \end{array}$$

1840

$$\begin{array}{r} \underline{458.51} \\ 4.8 \\ 40 \end{array}$$

$$\begin{array}{r} \underline{458.91} \\ 4.4 \end{array}$$

$$\begin{array}{r} \underline{459.31} \\ 4.0 \\ 40 \end{array}$$

+50

$$\begin{array}{r} \underline{458.41} \\ 4.7 \\ 40 \end{array}$$

$$\begin{array}{r} \underline{458.91} \\ 4.4 \end{array}$$

$$\begin{array}{r} \underline{459.31} \\ 4.0 \\ 40 \end{array}$$

1740

$$\begin{array}{r} \underline{458.51} \\ 4.8 \\ 40 \end{array}$$

$$\begin{array}{r} \underline{458.81} \\ 4.5 \end{array}$$

$$\begin{array}{r} \underline{459.51} \\ 3.8 \\ 40 \end{array}$$

463.31

463.31

L. S. R

2410

<u>451.26</u>	<u>452.06</u>	<u>453.06</u>	<u>453.56</u>	<u>454.16</u>
7.5	6.7	5.7	5.2	4.6
40	25		30	40

+50

<u>452.46</u>	<u>453.36</u>	<u>453.66</u>	<u>454.16</u>	<u>453.86</u>
6.3	5.4	5.1	4.6	4.9
40	30		15	40

2370

<u>452.66</u>	<u>452.46</u>	<u>452.46</u>
6.1	6.3	6.3
40		40

+65

<u>449.66</u>	<u>450.16</u>	<u>450.76</u>	<u>450.86</u>
9.1	8.6	8.0	7.9
60	40		40

+35 = Prop Cult.

<u>438.26</u>	<u>438.46</u>	<u>438.56</u>	<u>439.46</u>	<u>440.26</u>	<u>441.76</u>	<u>445.56</u>	<u>443.96</u>	<u>444.96</u>
20.5	20.3	20.2	19.3	18.5	17.0	12.2	14.8	13.8
60	40	30	30		20	30	40	65

22710

<u>442.46</u>	<u>442.16</u>	<u>443.96</u>	<u>444.66</u>	<u>444.36</u>	<u>445.16</u>	<u>446.26</u>
16.3	16.6	14.8	14.1	14.4	12.6	13.5
80	40			30	40	60

458.76

458.76

27+0

Lt.	L	Rt
<u>451.66</u>	<u>452.16</u>	<u>452.06</u>
7/40	6.6	6.7/40

+50

<u>451.66</u>	<u>452.16</u>	<u>452.86</u>	<u>453.86</u>	<u>454.16</u>
7/40	6.3/30	5.9	4.9/30	4.6/40

26+0

<u>452.06</u>	<u>452.86</u>	<u>453.56</u>	<u>454.56</u>
6.7/40	5.9/30	5.2	4.2/40

+50

<u>452.76</u>	<u>453.56</u>	<u>454.26</u>
6.0/40	5.2	4.5/40

25+0

<u>452.46</u>	<u>453.26</u>	<u>453.66</u>
6.3/40	5.5	5.1/40

24+50

<u>451.76</u>	<u>452.26</u>	<u>453.26</u>
7.0/40	6.5	5.5/40

458.76

458.76

Lt Lt Rt

30 +0

<u>441.85</u>	<u>442.35</u>	<u>442.95</u>	<u>442.75</u>	<u>443.75</u>	<u>444.35</u>
9.1 60	8.6 40	8.0	8.2 10	7.7 40	6.6 55

+50

<u>437.55</u>	<u>437.65</u>	<u>438.95</u>	<u>439.95</u>	<u>440.45</u>	<u>441.55</u>
13.4 65	13.3 40	12.0	11.0 25	10.5 40	9.4 60

29 +0

<u>437.25</u>	<u>438.15</u>	<u>439.65</u>	<u>440.85</u>	<u>441.55</u>	<u>442.55</u>
13.7 65	12.8 40	11.3	10.1 30	9.4 40	8.4 60

+50

<u>440.95</u>	<u>441.95</u>	<u>442.95</u>	<u>443.95</u>	<u>445.15</u>	<u>445.95</u>
10.0 60	9.0 40	8.0 10	7.0	5.8 40	5.0 50

28 +0

<u>445.75</u>	<u>446.75</u>	<u>447.75</u>	<u>448.95</u>	<u>449.55</u>
5.2 80	4.2 40	3.2	2.0 35	1.4 40

TP

2.24 450.95 10.05 448.71

450.95

27 +50

<u>449.96</u>	<u>451.06</u>	<u>451.96</u>
8.8 70	7.7	6.8 40

458.76

458.76

+50

<u>451.38</u>	<u>450.48</u>	<u>450.48</u>
3.6	4.5	4.5
40.		40.

3570

<u>451.18</u>	<u>450.78</u>	<u>450.68</u>	<u>451.58</u>
3.8	4.2	4.3	3.4
40.		25.	40.

+50

<u>451.68</u>	<u>451.38</u>	<u>451.58</u>
3.3	3.6	3.4
40.		40.

3410

<u>451.78</u>	<u>451.98</u>	<u>451.68</u>	<u>451.48</u>
3.2	3.0	3.3	3.5
40.	20.		40.

TP 2.83 454.98 0.50 452.15

454.98

+50

<u>450.45</u>	<u>450.95</u>	<u>452.15</u>
2.2	1.7	0.5
40.		40.

3370

<u>449.95</u>	<u>450.55</u>	<u>450.95</u>
2.7	2.1	1.7
40.		40.

452.65

452.65

TP 0.76 419.90 12.66 419.14

3870

Lt	L	Rt
418.80	417.30	416.80
13.0	14.5	15.0
75	40	30
416.30	415.80	415.30
15.5	16.6	16.3
30	40	75

+50

426.80	426.00	425.80	425.00	425.00	425.50	425.70
5.0	5.8	6.0	6.8	6.8	6.3	6.1
65	40	20	30	30	40	65

TP 2.15 431.80 12.89 429.65

3770

Lt	L	Rt
436.44	436.04	435.24
6.1	6.5	7.3
60	40	25
434.34	434.44	434.14
8.2	8.1	8.4
25	30	40

TP 0.71 442.54 13.15 441.83

+50

444.68	444.88	443.48	443.58	443.68
10.3	10.1	11.5	11.4	11.3
50	40	40	50	50

+20

449.38	447.88	448.58	448.18
5.6	7.1	6.4	6.8
40	20	40	40

+18.93

5.62 449.36 0.74/16
17 Lt.

3670

450.08	449.58	449.38
4.9	5.4	5.6
40	40	40

154.98

454.98

TP 9.92 456.50 0.10 446.58

12+0

TP 12.10 446.68 0.71 434.58

+50

41+0

TP 12.41 435.29 0.53 422.88

+75

+50

+25

40+0

423.41

Lt

L

Rt

444.28 444.38 444.38 444.28 444.08 443.38 443.18
2.4 2.3 2.3 2.4 2.6 2.3 2.5
60 40 20 20 20 40 60

446.68

432.79 433.79 434.99 434.09 434.89
2.5 1.5 0.3 1.2 0.4
80 40 70 40 70

422.69 423.99 423.49 426.59 425.69 424.89 424.89 424.99
12.6 11.3 11.8 8.7 9.6 10.4 10.4 10.3
80 60 40 15 20 30 40 80

435.29

419.41 420.21 420.51 420.71 421.61 421.71 420.81 420.91
4.0 3.2 2.9 2.7 1.8 1.7 2.6 2.5
80 40 20 20 20 40 60 80

417.71 416.71 418.11 417.01 418.31 419.11 418.11 417.91 417.51
5.7 6.5 5.3 6.4 5.1 4.8 5.3 5.5 5.9
80 85 40 20 15 20 40 80

412.11 413.21 414.41 415.31 415.01 415.21 414.91 414.31
11.3 10.3 9.0 8.1 8.4 8.2 8.5 9.1
90 75 40 20 20 20 40 20

405.31 407.21 410.41 411.21 412.41 412.41 411.91 412.01
18.1 18.2 12.0 12.2 11.0 11.0 11.5 11.4
90 60 40 20 20 20 40 90

423.41

BM 2.80 453.75 ^{5.11.84}
~~453.75~~
 453.70

TP 6.97 457.55 5.92 450.58

+50

449.80 450.90 451.60
 6.7 5.6 4.9
 40 40 40

45+0

451.00 451.80 452.70
 5.5 4.7 3.8
 40 40 40

+50

452.00 452.50 452.80
 4.5 4.0 3.7
 40 40 40

44+0

451.70 452.40 452.90
 4.8 4.1 3.6
 40 40 40

+50

452.40 452.30 452.50
 4.1 4.2 4.0
 40 40 40

43+0

452.30 452.00 452.20
 4.2 4.5 4.3
 40 40 40

42+50

450.50 450.50 450.10 449.40 449.20
 6.0 6.0 6.7 7.1 7.3
 50 40 40 40 50

456.60

456.50

Lt Z R+

Lt.

2

Rt.

452.24	452.54	453.09	453.52	453.89	454.06
7.75	7.45	6.90	6.47	6.10	5.93
40 on Ho	38 1/2 on Ho	30 on Ho	on Ho	20 on Ho	40 on Ho

+72.43 EC
 TP 6.29 459.99 3.38 453.70

452.88	452.98	453.10	453.48	453.42	453.88
4.2	4.1	3.9	3.6	3.66	3.20
40	30		12.3 Top	13.3 Gut	40 on Ho

+50

452.78	452.78	452.68	453.38	453.42	452.80	453.13
4.3	4.3	4.7	3.7	3.66	4.28	3.95
40	20		30	32.2 Top	32.2 Gut	40 on Ho

48+0

452.48	452.18	452.28	452.08	452.48	452.70	452.08
4.6	4.9	4.8	5.0	4.6	4.38	5.00
40	20		20	40	58.5 Top	58.5 Gut

+50

451.18	451.58	451.38
5.9	5.5	5.7
40		40

47+0

449.88	450.08	450.68	450.88	451.48
7.2	7.0	6.4	6.2	5.6
40	20		20	40

+50.51 B.C. Lt.

449.78	449.78	450.28	450.98	452.08
7.3	7.3	6.8	6.1	5.0
40	20		20	40

46+0

BM 2.38 457.08 453.70
 S.H. 84
 F. 10/10/27
 67454

457.08

Lt Z Rt

+50

<u>455.59</u>	<u>455.91</u>	<u>455.25</u>	<u>455.79</u>	<u>455.77</u>	<u>455.37</u>
4.4 40	4.08 23.8- Topch	4.74 23.8-Gut	4.20 20.07Par	4.22 20.07Par	4.62 40.07Par

50+0

<u>455.69</u>	<u>455.61</u>	<u>455.03</u>	<u>455.43</u>	<u>455.91</u>	<u>454.89</u>
4.3 40	4.38 18.8-Topch	4.76 18.8- Gut	4.56 20.07Par	4.58 20.07Par	5.10 40.07Par

+75

<u>455.29</u>	<u>455.47</u>	<u>454.81</u>	<u>455.18</u>	<u>455.14</u>	<u>454.71</u>
4.7 40	4.52 15.4-Topch	5.18 15.4- Gut	4.81 20.07Par	4.85 20.07Par	5.28 40.07Par

+50

<u>454.79</u>	<u>455.19</u>	<u>454.59</u>	<u>454.87</u>	<u>454.87</u>	<u>454.57</u>
5.2 40	4.80 11.2- Topch	5.40 11.2- Gut	5.10	5.10 20.07Par	5.40 40.07Par

+25

<u>454.99</u>	<u>454.89</u>	<u>454.94</u>	<u>454.32</u>	<u>454.46</u>	<u>454.51</u>	<u>454.34</u>
5.0 40	5.1 20	5.05 9.0- Topch	5.67 9.0- Gut	5.53	5.48 20.07Par	5.65 40.07Par

19+0

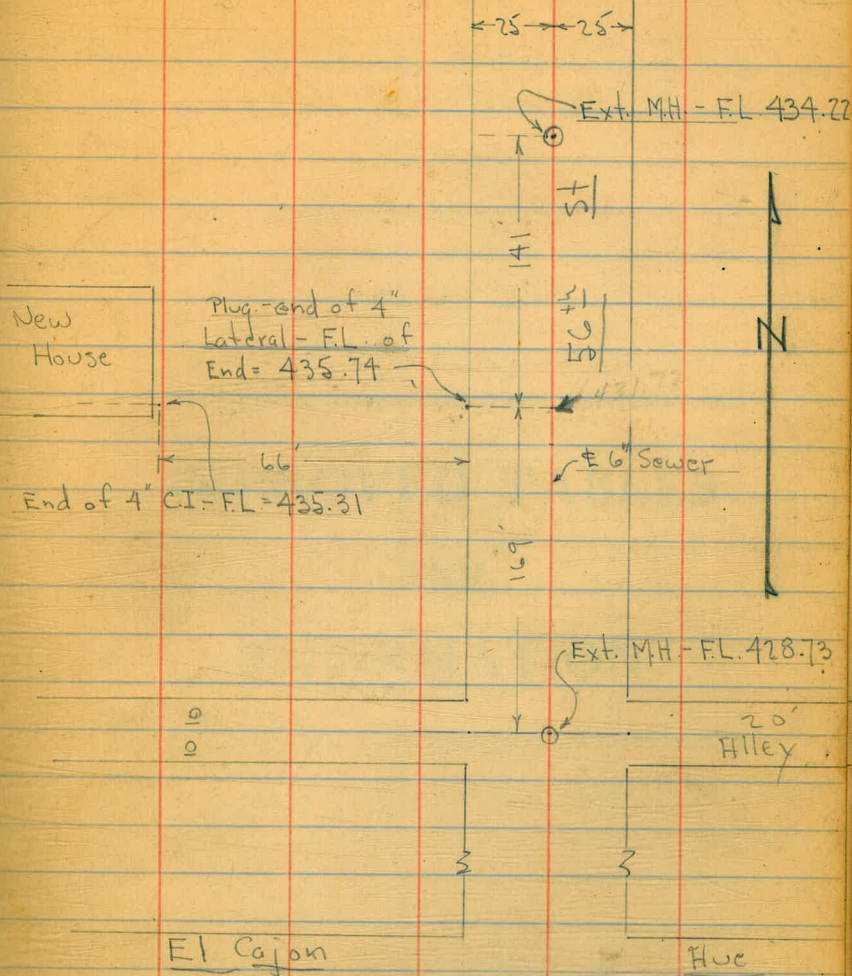
<u>452.99</u>	<u>452.99</u>	<u>453.66</u>	<u>454.04</u>	<u>454.31</u>	<u>454.22</u>
7.0 40	7.00 38.0- 20.07Par	6.33 20.07Par	5.95 20.07Par	5.68 20.07Par	5.77 40.07Par

15999

459.99

Elev. of Sewers + M.H.'s and Laterals on 56th St. - N. of El Cajon

BM	11.54	<u>449.31</u>	437.77	NE. 56 th + El Cajon
FL. - M.H. at Φ 20' Alley	20.58		428.73	
FL. - M.H. 310' N.	15.09		434.22	
FL. - end of 4" Lateral at W.L. 56 th	13.57		435.74	
FL. - End of 4" C.I. at House	14.00		435.31	



El Cajon		±		Hue	
Lt.			Rt.		
455.89	456.12	455.51	455.97	456.13	455.67
4/0	3.87 25.8 Toplet	4.48 25.8 Gut	4.02 57' Pat	3.86 25.99 Pat	4.32 40' on Pat

457.99

459.99

277.10
138.55

-87-57-30
90-00-30

11
12
13

29. 33.9
11.5 11.1
17.5 45.0
16.5
34.0

147.63 1st 40' Tie
357.11 346.03
11.11 67 70
46.00 12 15

75 128.5
6 17.5
13.5 125.0
62.94 13.5
19. 5
606.94

65-17
114.04
181.21

128 | 3000
 256
 440
 384
 560
 512
 480

30.4
24.2
54.6
9
45.6
32.6
13.6
13
100
230
45
275