

1501

POSTS

LEVEL BOOK

No. 3807

MICROFILMED  
DEC 24 1964

ENGINEERING DEPARTMENT,  
CITY OF SAN DIEGO,  
CALIFORNIA.

963  
JK 100 J

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
IRVING PARK STATION  
CHICAGO, ILL.

X-Sections	54 <sup>th</sup> Univ. Ave. N.	1 - 24
Survey	Road opening Lot 26 La Mesa Hts	26 33
	Catechin Dr. Campo Ext.	
S D.	Public Library Sprinkling System	34 -
Sewer	Franklin Ave E. of Boundary	35 -
r	Sierra Vista Sub. Franklin East	37
x-sec.	FAY St. H. School S. of Westburn	39 - 44
" "	Blk 9 O.B. - Blk 23 Pt. Loma Hts	45 - 47
Curb Elev.	Atlantic St. Harasty to Courts	48 - 52
X-Sec.	Alley Blk-C Sterlingworth	53 - 55
" "	" " 28 Sub. Blk K+L Teralta	56 58
		59
x-sec.	Alley Blk 20 Fairmount Add.	60 64
" "	" " 3 Ocean Beach	65 67
" "	" " 24 Normal Hts	68 71
" "	" " 36 Ocean Beach	72 - 73
check Survey	Orange Crest Sub.	74 -
	Juan Street Addition	75 -
S.D.	Public Library	76 - 79

6-5-34 X Sec. 54<sup>th</sup> St.  
 2 University Ave. North.  
 Plat. Page 12.

50. Width  
 20. Pavmt.  
 10 Center

B.M. BP 10.05 320.07 310.02 + Univ.  
 B.M. spk. Pole N.W. 54<sup>th</sup> & Univ. 2.11 317.96 = 317.98

N. Line Univ. on Diagonal at L of 67-09

From Line of 54<sup>th</sup> St. 54.25 Width

E. -10	320.07 10.9	3091	✓
E	10.5	3095	✓
+7	9.3	3107	✓
+10 = E. cmt. cl.	11.05	30902	✓
gutter on pavmt.	11.47	30860	✓
+16.3 " "	11.14	30893	✓
☉ " "	10.63	30944	✓
+10.85 " "	10.63	30944	✓
+16.3 gutter " "	10.83	30924	✓
+16.3 cmt. cl.	10.11	30996	✓
+20	7.7	3125	✓
W.	8.2	3118	✓
+10	7.0	3130	✓

0+00 = { N. Line Univ on W. } at 90° 00'  
 { 21.07 N. of Univ on E. }

-10	7.0	313.0	✓
W	8.2	311.8	✓
+7	7.7	3123	✓
+11.3 = W. edge pavmt.	10.47	30960	✓
+15	10.37	30970	✓
☉	10.27	30980	✓
+10 Δ on E. edge Pavmt.	10.45	30962	✓
+14	10.2	3098	✓

320.07 Indexed  
 c.s.K.

1

+16	7.8	3122	✓
E	8.0	3120	✓
+10	8.6	3114	✓
0+08.			
10' W. of ☉ Δ on W. edge Pavmt. 9.89			
0+50			
-10	4.3	3157	✓
E.	3.4	316.6	✓
+9	2.9	317.1	✓
+10	7.1	3129	✓
+15. edge pavmt.	6.73	313.34	✓
☉	6.65	313.42	✓
+10 = pavmt.	6.77	313.30	✓
+15	7.0	313.0	✓
+16	2.6	317.4	✓
W.	2.3	317.7	✓
+10	2.3	317.7	✓

0+33

S. End Row. of Olive Trees. 18' W. of ☉

1+00			
-10	+3.4	323.4	✓
W.	+3.8	323.8	✓
+8	+3.3	323.3	✓
+10	3.0	317.0	✓
+15 Pavmt	2.89	317.18	✓
☉ "	2.74	317.33	✓

320.07 ✓  
 1+00 320.07  
 (con)

+10	paymt	2.81	317.26	✓
+14		2.9	317.1	✓
+16		+2.0	322.0	✓
E		+1.6	321.6	✓
+10		0.0	320.0	✓
T.P.	12.78	331.92 ✓	0.93	319.14 ✓

1+50 331.92

-10		8.1	323.8	✓
E		5.9	326.0	✓
+9		4.2	327.7	✓
+11		10.8	321.1	✓
+15	paymt.	10.60	321.5	✓
⊥	"	10.56	321.36	✓
+10	paymt.	10.73	321.19	✓
+14		11.4	320.5	✓
+16		3.8	328.1	✓
W		3.0	328.9	✓
+10		3.3	328.6	✓

2+00

-10		0.2	331.7	✓
W		+0.5	332.4	✓
+9		+0.7	332.6	✓
+11		6.9	325.0	✓
+15	paymt.	6.82	325.10	✓
⊥	"	6.64	325.24	✓
+10	"	6.77	325.15	✓

331.92 ✓  
 54<sup>th</sup> 5+ **2**  
331.92

+14		7.0	324.9	✓
+16		0.7	331.2	✓
E		2.9	329.0	✓
+10.		6.8	325.1	✓

should be on opp page 1+25

S. End Row. of Eucalyptus Trees 19.5 E. of ⊥

2+50

-10		4.3	327.6	✓
E		1.5	330.4	✓
+10		+0.7	332.6	✓
+11		2.9	329.0	✓
+15	paymt.	2.95	328.97	✓
⊥	"	2.78	329.14	✓
+10	"	2.84	324.08	✓
+14		2.3	329.6	✓
T.P.	12.75	344.25 ✓	0.42	331.50 ✓
+16		<u>344.25</u> 9.1	335.1	✓
W.		9.5	334.7	✓
+10		10.5	333.7	✓

3+00

-10		8.1	336.1	✓
W.		7.6	336.6	✓
+10		8.0	336.2	✓
+11		10.8	333.4	✓
+15	pay.	10.95	322.50	✓

344.25 ✓

3+00 (cont)

344.25 ✓

10.97

33378 ✓

♀ pay.

+10 "

11.21

33304 ✓

+14

11.4

33285 ✓

+15

10.8

33348 ✓

E

12.2

33205 ✓

+10

14.2

33005 ✓

3+25

-10

12.4

33185 ✓

E.

11.3

33195 ✓

+6

10.4

33385 ✓

+10

9.3

3349 ✓

+15 pay.

9.10

3351 ✓

♀ "

8.82

33545 ✓

+10 "

8.84

33541 ✓

+14

9.1

3351 ✓

+15

6.9

3373 ✓

W

6.1

3381 ✓

+10

6.6

3376 ✓

3+40 { W. End. Row Eucalyptus 19.5 E of ♀  
" " " Olive Trees 19.5 E of ♀

3+50

-10

5.3

3389 ✓

W.

5.0

3392 ✓

+10

5.8

3384 ✓

+11

7.4

3368 ✓

+15 = pay

7.03

33722 ✓

♀

7.02

33723 ✓

+10

7.30

3369 ✓

344.25 ✓

54<sup>th</sup> ST

3

344.25 ✓

+14

6.9

3373 ✓

+15

6.0

3382 ✓

E.

8.2

3360 ✓

+10

10.6

333.6 ✓

3+60

-10

8.6

3356 ✓

-4

6.5

3377 ✓

E

6.3

3379 ✓

+10

5.6

3386 ✓

+11

6.4

3378 ✓

+15

pay

6.56

33769 ✓

♀ "

6.33

33792 ✓

+10 "

6.47

33784 ✓

+14

6.8

3374 ✓

+15

5.6

338.6 ✓

W.

4.4

339.8 ✓

+10

4.2

340.0 ✓

3+75

-10

3.5

340.7 ✓

W.

3.6

340.6 ✓

+10

4.4

339.8 ✓

+11

6.1

338.1 ✓

+15.

pay

5.49

33876 ✓

♀ "

5.35

33887 ✓

+10 "

5.53

33872 ✓

+5

5.3

338.9 ✓

344.25 ✓

3+75 cont  
344.25  
5.9

E		338.3	✓
+10		338.0	✓
4+00			
-10		338.7	✓
E		340.0	✓
+10		340.8	✓
+15	pav	340.26	✓
±	"	340.46	✓
+10	"	340.31	✓
+15		339.9	✓
+6		340.9	✓
W		341.9	✓
+10		341.8	✓
4+25			
-10		343.1	✓
W		342.9	✓
+9		342.3	✓
+10		341.4	✓
+15	pav	341.72	✓
±	"	341.90	✓
+10	"	341.74	✓
+14		342.1	✓
+15		341.5	✓
E		340.2	✓
+10		339.3	✓

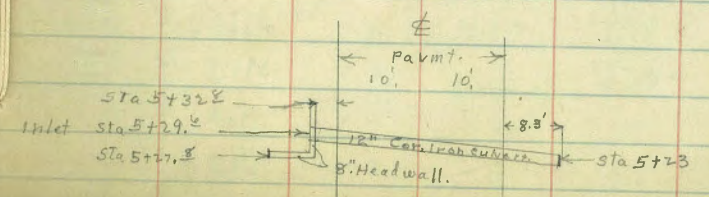
344.25 ✓

54<sup>th</sup> St

344.25

4

4+50			
-10		340.2	✓
E		340.9	✓
+10		342.9	✓
+15	pav	343.07	✓
±	"	343.22	✓
+10	"	343.12	✓
+15		342.6	✓
+16		343.6	✓
T.P.	12.67	356.72	✓
W		344.11	✓
+10		344.3	✓
5+00			
-10		347.0	✓
W		346.5	✓
+10		345.6	✓
+15	pav	345.7	✓
±	"	345.83	✓
+10	"	345.66	✓
+15		346.1	✓
+18		343.8	✓
E		342.8	✓
+10		341.8	✓



356.72

356.72

5+23

culvert.

18.3 E. of  $\phi$  Out. Let F.L. 12" 12.85 345.87 ✓

5+27.8

6.7 W. of  $\phi$  Top. Wing Wall 9.62 347.10 ✓

2.9 W. " " " " 9.61 347.11 ✓

5+29.6

3.6 W. of  $\phi$  Inlet F.L. 12" Culvert 11.73 344.99 ✓

5+32.8

2.9 W. of  $\phi$  N. End. Top Wing Wall. 9.37 347.35 ✓

5+50

-10 13.3 343.4 ✓

E. 12.0 344.7 ✓

+2 11.9 344.8 ✓

+10 8.5 348.2 ✓

+15 pay 8.52 348.20 ✓

$\phi$  " 8.35 348.37 ✓

+10 " 8.55 348.17 ✓

+15 8.3 348.2 ✓

+16 9.0 347.7 ✓

W 8.0 348.7 ✓

+10 7.1 349.6 ✓

6+00

-10 4.6 352.1 ✓

W 5.4 351.3 ✓

+9 6.4 350.3 ✓

+10 5.4 351.3 ✓

+15 pay 5.90 350.8 ✓

356.72

54<sup>th</sup> St. 5

356.72

$\phi$  pay

5.75 350.97 ✓

+10 "

5.95 350.77 ✓

+15

5.9 350.8 ✓

E

10.0 346.7 ✓

+10

11.1 345.6 ✓

6+50

-15

9.4 347.3 ✓

-10

8.7 344.0 ✓

E

7.2 349.5 ✓

+6

6.0 350.7 ✓

+10

3.2 353.5 ✓

+15 pay

3.02 353.70 ✓

$\phi$  "

2.81 355.91 ✓

+10 "

2.95 355.77 ✓

+15

2.5 356.27 ✓

+16

3.1 355.6 ✓

W

2.3 354.4 ✓

+10

1.1 355.6 ✓

T.P. 12.18

368.32

9.58 356.14 ✓

74.00

368.32

8.7

9.7 358.6 ✓

+6

10.0 358.3 ✓

W.

10.9 357.4 ✓

+10

11.38 356.94 ✓

+15 pay

11.19 357.15 ✓

$\phi$  "

11.41 356.91 ✓

+10 "

11.3 357.0 ✓

+15



368.32

7+00 (con)

368.32  
15.8

+22		357.5 ✓
E	16.1	357.2 ✓
+10	17.8	350.5 ✓
+15	18.2	350.1 ✓

7+50

-15	15.4	352.9 ✓
-10	14.5	353.6 ✓
E	13.0	355.3 ✓
+4	12.0	356.3 ✓
+10	8.4	359.9 ✓
+15	8.43	359.89 ✓
¢	8.17	360.15 ✓
+10	8.29	360.05 ✓
+15	8.6	359.7 ✓
+16	7.5	360.8 ✓
W.	5.8	362.5 ✓
+70	5.5	362.8 ✓
+10	4.2	364.1 ✓

8+00

-10	+2.4	370.7 ✓
	+0.9	369.2 ✓
W	+0.6	368.9 ✓
+9	0.8	367.5 ✓
+10	4.9	363.1 ✓
+15	5.15	363.17 ✓
¢	5.09	363.23 ✓
+10	5.29	363.03 ✓

368.32

54<sup>th</sup> ST 6368.32

+15	5.6	362.7 ✓
+22	7.6	360.7 ✓
E	8.2	360.1 ✓
+10	10.6	357.7 ✓
+15	11.2	357.1 ✓

8+50

-15	6.8	361.5 ✓
-10	5.1	363.2 ✓
E.	3.5	364.9 ✓
+7	1.7	366.6 ✓
+8	2.5	365.8 ✓
+15	2.40	365.9 ✓
¢	2.11	366.21 ✓
+10	2.08	366.24 ✓
+15	2.0	366.3 ✓
+16	+4.3	372.6 ✓
W	+5.2	373.5 ✓
+7	+5.5	373.8 ✓
+10	+6.4	374.7 ✓

8+75

-10	+8.2	376.5 ✓
W	+7.0	375.5 ✓
+8	+4.8	373.1 ✓
+10	0.4	367.9 ✓
+15	0.69	367.63 ✓
¢	0.78	367.54 ✓

368.32 ✓

	8+75 (Eon)	
	<u>368.32</u>	
+10	7.13	367.19 ✓
+17	1.4	366.9 ✓
+18	0.7	367.6 ✓
8.	2.3	366.0 ✓
+10	4.9	363.4 ✓
+15	5.7	362.6 ✓

9+00

-15	5.0	363.3 ✓
-1.0	4.0	364.3 ✓
E	1.8	366.5 ✓
+7	0.0	368.3 ✓
+15	0.09	368.23 ✓

T.P.	7.76	375.81 ✓	0.27	368.05 ✓
♀	Pay	<u>375.81</u>	7.77	368.64 ✓
+10	"		7.09	367.72 ✓
+16			6.7	369.1 ✓
+17			1.9	373.9 ✓
W			0.3	376.5 ✓
+			+1.0	376.8 ✓

last sect

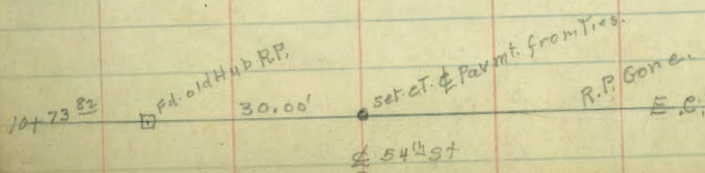
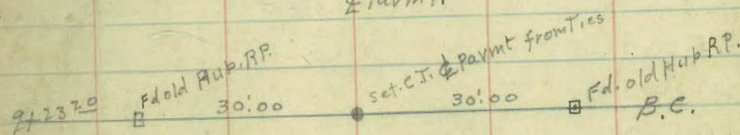
	9+23 <sup>2</sup>	P.C. Δ43°09'	R=200
-10	+0.2	376.0 ✓	
W	0.5	375.5 ✓	
+8	2.0	373.8 ✓	
+10	6.3	369.5 ✓	
+15	6.40	369.1 ✓	

375.81 ✓

54th St

		<u>375.81</u>	
♀	Pay.	6.45	369.36 ✓
+10	"	6.95	368.86 ✓
+15		6.6	369.2 ✓
E		9.2	366.6 ✓
+10		11.1	364.7 ✓
+15		11.8	364.0 ✓
		9+50	
-15		11.3	364.5 ✓
-10		10.4	365.6 ✓
E		9.0	366.8 ✓
+10		6.3	369.5 ✓
+15	Pay	6.46	369.35 ✓
♀	"	5.85	369.96 ✓
+10		5.68	370.13 ✓
+15		5.4	370.4 ✓
+20		3.6	372.2 ✓
W		3.1	372.7 ✓
+10		2.5	373.3 ✓

♀ Pavmt.



375.81

9+2.5

375.81

9.25

-10	Drive to House	4.6	371.2 ✓
W		4.8	371.0 ✓
+10		5.3	370.5 ✓
+15	pay	5.32	370.49 ✓
⊖	"	5.64	370.17 ✓
+10	"	6.22	369.59 ✓
+16		6.0	369.8 ✓
E		9.1	366.7 ✓
+10		10.7	365.1 ✓
+20		11.7	364.1 ✓

10+00

-20		12.0	363.8 ✓
-10		11.0	364.8 ✓
E		9.8	366.0 ✓
+5		9.0	366.8 ✓
+10		6.1	369.7 ✓
+15	pay	6.32	369.49 ✓
⊖	"	5.74	370.07 ✓
+10	"	5.40	370.41 ✓
+15		5.4	370.4 ✓
W		5.4	370.4 ✓
+10		5.7	370.1 ✓

10+25

-10		6.8	369.0 ✓
W		6.9	368.9 ✓
+6		5.5	370.3 ✓

375.81

54<sup>th</sup> St

8

375.81

+10		5.0	370.8 ✓
+15	pay	5.33	370.5 ✓
⊖	"	5.74	370.07 ✓
+10	"	6.37	369.44 ✓
+15		6.0	369.8 ✓
+21		9.5	366.3 ✓
E		9.9	365.9 ✓
+10		11.6	364.2 ✓
+20		12.6	363.2 ✓

10+50

-20		13.2	362.6 ✓
-10		11.6	364.2 ✓
E		10.9	364.9 ✓
+4		10.2	365.6 ✓
+10		6.1	369.7 ✓
+15	pay	6.38	369.43 ✓
⊖	"	5.77	370.04 ✓
+10	"	5.50	370.31 ✓
+15		5.0	370.8 ✓
+19		7.5	368.3 ✓
W		7.6	368.2 ✓
+10		7.7	368.1 ✓

10+73

E.C.

-10		7.6	368.2 ✓
W		7.6	368.2 ✓
+5		7.9	367.9 ✓

375.81 ✓

10+73 82 E.C. (Con)

375.81

+11		4.4	371.4 ✓
+14		4.3	371.5 ✓
+15	pav	5.48	370.93 ✓
♀	"	5.55	370.26 ✓
+10	"	5.97	369.82 ✓
+15		5.8	370.0 ✓
+20		9.9	365.9 ✓
E		10.7	365.1 ✓
+10		12.3	363.5 ✓
+20		13.6	362.2 ✓

11+00

-20		12.3	365.5 ✓
-10		11.3	364.5 ✓
E		10.6	365.2 ✓
+6		9.0	366.8 ✓
+11		5.3	370.5 ✓
+15	pav	5.39	370.42 ✓
♀	"	5.13	370.68 ✓
+10	"	5.19	370.60 ✓
+11		4.5	371.3 ✓
+14		4.4	371.4 ✓
+20		7.7	368.1 ✓
W.		7.5	368.3 ✓
+10		7.1	368.9 ✓

375.81 ✓

375.81

11+50

-10		4.9	370.91 ✓
W		5.6	370.7 ✓
+7		5.2	370.6 ✓
+12		3.1	372.7 ✓
+14		3.4	372.4 ✓
+15	pav	4.10	371.7 ✓
♀	"	3.94	371.87 ✓
+10	"	4.20	371.6 ✓
+14		4.0	371.8 ✓
+20		7.3	368.5 ✓
E		8.3	367.5 ✓
+10		8.3	367.5 ✓
+20		9.0	366.8 ✓

12+00

-15		4.7	371.1 ✓
-10		4.3	371.5 ✓
E		4.6	371.4 ✓
+7		3.9	371.9 ✓
+11		2.3	373.5 ✓
+15	pav	2.71	373.10 ✓
♀	"	2.39	373.42 ✓
+10	"	2.40	373.41 ✓
+15		1.3	374.5 ✓
+18		2.6	373.2 ✓
W.		2.5	373.3 ✓
+10		2.0	373.8 ✓

54<sup>th</sup> 51

9

375.81

386.14

386.14

54th St

10

13+25

386.14

0.0

0.7

1.7

5.8

6.13

5.90

5.99

6.1

3.4

3.0

2.6

13+42

1.2

2.0

2.4

5.3

5.43

5.47

5.83

5.4

1.0

0.2

+0.5

T.P. 10.60 386.14 0.27 375.54

12+50

-10 7.1 379.0

W 7.7 378.4

+9 8.5 377.6

+10 10.3 375.8

+15 pav 10.26 375.88

4 " 10.13 376.01

+10 " 10.31 375.83

+15 10.0 376.1

E 10.0 376.1

+10 9.9 376.2

13+00

-10 4.3 381.8

E 4.9 381.2

+10 5.1 381.0

+11 7.4 379.7

+15 pav 7.12 379.02

4 " 7.04 379.10

+10 " 7.23 378.91

+15 7.2 378.9

+14 3.6 382.5

W 2.7 383.4

+10 1.7 384.4

-10

W

+9

+10

+15 pav

4

+10

+14

+15

E

+10

-10

E

+6

+9

+15 pav

4

+10

+14

+16

W

+10

386.1

385.4

384.4

380.3

380.01

380.24

380.15

380.0

382.7

383.1

383.5

384.9

384.1

385.7

380.8

380.71

380.67

380.51

380.7

385.1

385.9

386.6

386.14 ~~386.14~~

13+44 S. side Drive to House on E.

-10		+0.5	386.6	✓
W		0.2	385.9	✓
+9		1.0	385.1	✓
+17		5.4	380.7	✓
+15	pav	5.81	380.33	✓
♀	"	5.43	380.71	✓
+10	"	5.39	380.75	✓
+15		5.2	380.9	✓
E		4.3	381.8	✓
+10		3.0	383.1	✓

13+56 N. side above drive

-10		2.9	383.2	✓
8		4.0	382.1	✓
+10		4.7	381.4	✓
+15	pav	5.23	380.91	✓
♀	"	5.26	380.78	✓
+10	"	5.79	380.35	✓
+14		5.7	380.4	✓
+16		1.0	385.1	✓
W		0.0	386.1	✓
+10		+0.8	386.9	✓

13+45

-10		+0.5	386.6	✓
W		0.2	385.9	✓
+9		1.5	384.6	✓
+11		5.6	380.5	✓

386.14

~~54+57~~ 11~~386.14~~

+15	pav	5.92	380.92	✓
♀	"	5.50	380.64	✓
+10	"	5.33	380.81	✓
+14		5.2	380.9	✓
+16		2.8	383.3	✓
E		2.6	383.5	✓
+10		2.4	383.7	✓
		15+92 <sup>10</sup>	B.C. Lt.	
-10		5.4	380.7	✓
E		5.6	380.5	✓
+10		5.2	380.9	✓
+11		6.4	379.7	✓
+15	pav	6.43	379.71	✓
♀	"	6.63	379.51	✓
+10	"	7.05	379.09	✓
+15		7.0	379.1	✓
+16		2.5	383.6	✓
W		1.6	384.5	✓
+10		0.6	385.5	✓

con. Page 15.

16+22.72

14+12.34 S. Line Orange

15+42.72 E.C.

$\Delta = 43.07$

$R = 200'$

$T = 79.08$

$L = 150.62$

13+92.10 B.C. Lt.

10+73.82 E.C.

$\Delta = 43.04$

$R = 200'$

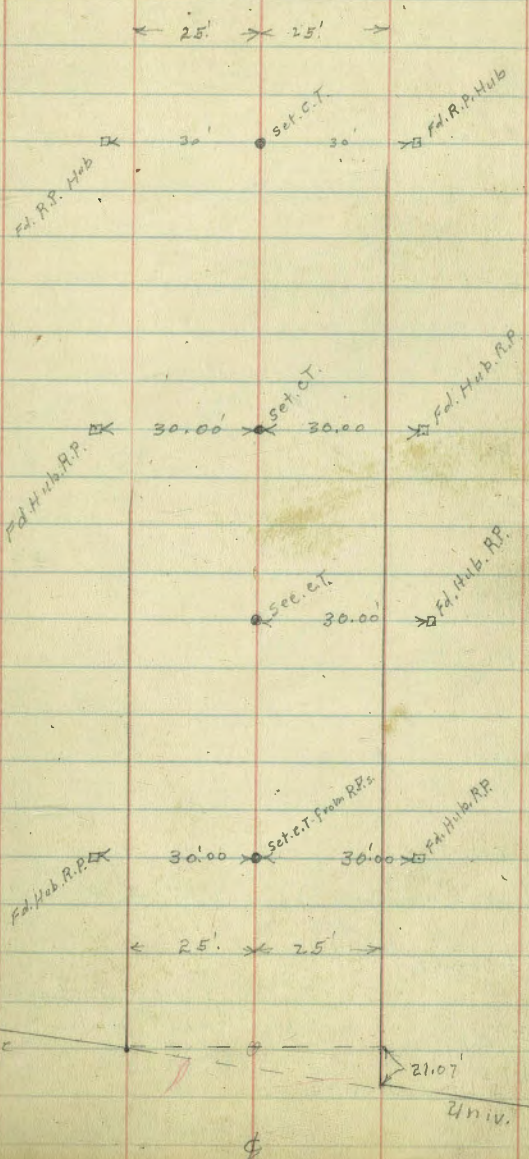
$T = 79.04$

$L = 150.62$

9+23.20 B.C. RT.

0+00

54th St



25+55<sup>10</sup> E.C.

Imp. Plans  
 $\Delta = 28.12'$   
 $R = 299.60'$   
 $T = 75.26'$   
 $L = 147.46'$

Imp. Plans  
 $\Delta = 28.10'$   
 $R = 300'$   
 $T = 75.26'$   
 $L = 147.48'$

24+07<sup>64</sup> P.C.Rt

18+64<sup>54</sup> E.C.

$\Delta = 28.10'$   
 $R = 300'$   
 $T = 75.26'$   
 $L = 147.48'$

17+21.0<sup>4</sup> P.C.Lt.

16+62<sup>22</sup> City Ties

16+52<sup>24</sup> N. Line Orange  
 Imp. Plans

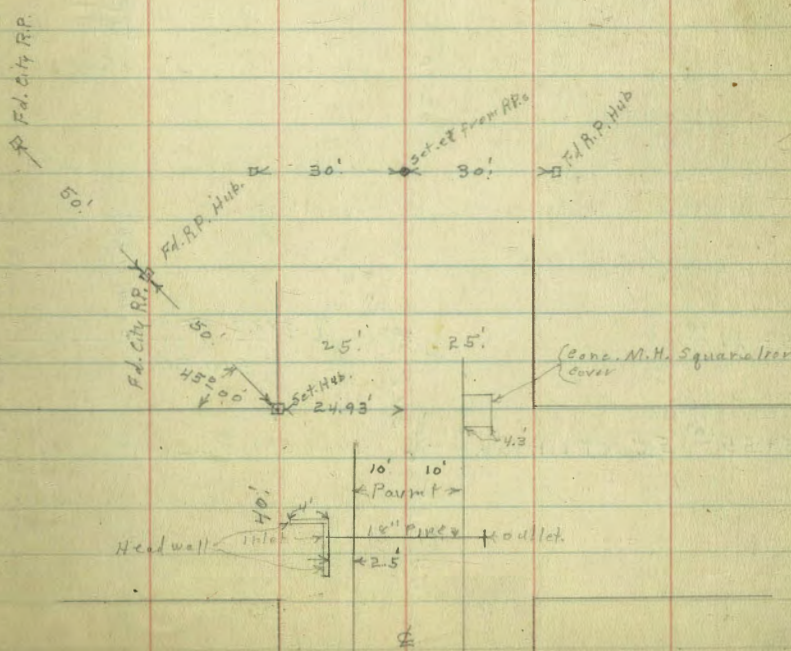
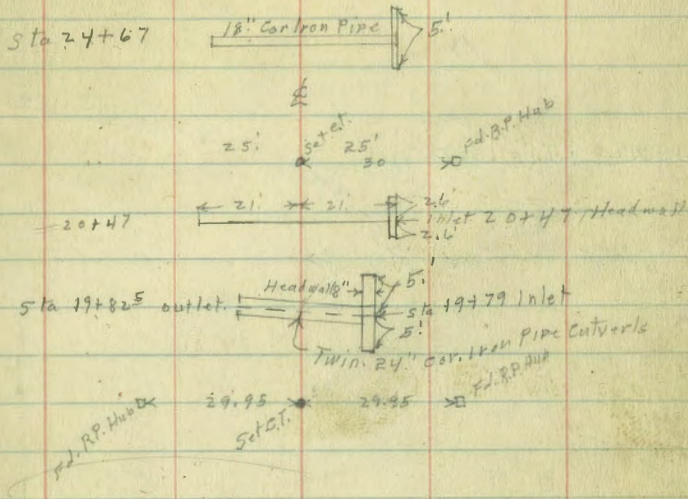
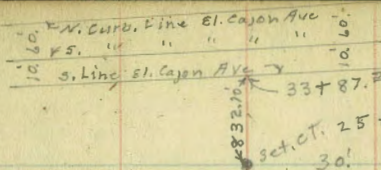
16+42<sup>25</sup> S. Orange

16+22<sup>27</sup> City Ties

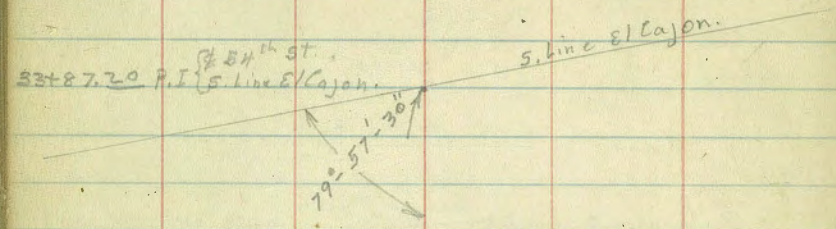
16+12<sup>24</sup> S. Line Orange  
 Imp. Plans

16+64<sup>23</sup> N. side M.H.  
 16+60<sup>25</sup> S. " M.H.

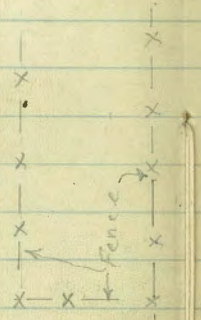
16+30<sup>2</sup> N. side Head wall  
 16+28.6 18" Cor. Iron Pipe Culvert  
 16+25 S end Head wall





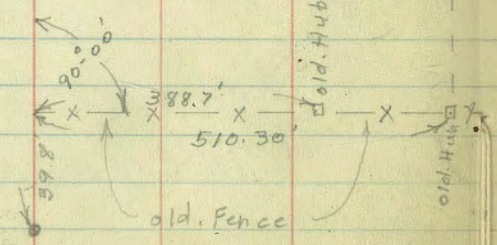


832.10'



25+94<sup>90</sup>

25+55<sup>10</sup> E.C. C.T.L.P. Pav.



54<sup>th</sup> St

386.14 ✓

14 + 25  
~~386.14~~  
3.6

-10		34.5 ✓
W	4.6	381.5 ✓
+9	5.5	380.6 ✓
+10	9.4	376.9 ✓
+15	9.09	377.05 ✓
±	8.66	377.48 ✓
+10	8.57	377.57 ✓
+15	8.0	378.1 ✓
E	9.2	376.9 ✓
+10	9.3	376.8 ✓

14 + 50

-10	11.8	374.3 ✓
E	11.3	374.8 ✓
+9	11.3	374.8 ✓
+10	10.0	376.1 ✓
+25	10.32	375.82 ✓
±	10.44	375.70 ✓
+10	10.87	375.27 ✓
+15	11.3	374.8 ✓
+16	7.7	378.4 ✓
W	7.0	379.1 ✓
+10	5.3	380.8 ✓

14 + 75

-10	7.8	379.3 ✓
W	8.7	377.4 ✓
+9	9.7	376.4 ✓

386.14 ✓

54<sup>th</sup> St.

15

~~386.14~~  
13.3

+10		374.8 ✓		
+15	pay	12.71	373.43 ✓	
±	"	12.27	373.87 ✓	
+10	"	12.12	374.02 ✓	
+15		11.7	374.4 ✓	
+19		14.2	371.9 ✓	
E		14.0	374.1 ✓	
+10		14.0	374.1 ✓	
T.P.	0.87	374.13	12.88	373.26 ✓

15 + 00  
~~374.13~~  
5.0

-10		369.1 ✓	
E		4.2	369.9 ✓
+7		3.4	370.7 ✓
+11		1.4	372.7 ✓
+15	pay	1.93	372.70 ✓
±	"	2.13	372.00 ✓
+10	"	2.59	371.54 ✓
+14		3.1	371.0 ✓
+16		+0.4	374.5 ✓
W.		+1.1	375.4 ✓
+10		+2.4	376.5 ✓

15 + 42<sup>72</sup>

-10		0.7	373.4 ✓
W		1.9	372.2 ✓
+10		3.6	370.5 ✓
+11		5.7	368.4 ✓

374.13

15+42.22 E.C. (con)

374.13

3.48

+15	Pav.		368.65	✓
±		5.07	369.06	✓
+10		5.08	369.05	✓
+14		4.5	369.6	✓
+18		6.3	367.8	✓
E		7.0	367.1	✓
+10		8.1	366.0	✓

15+75

-10		9.4	364.7	✓
E		9.1	365.0	✓
+7		7.9	366.2	✓
+10		6.8	367.3	✓
+15	Pav	6.98	367.15	✓
±	"	6.86	367.29	✓
+10	"	7.21	366.92	✓
+14		7.3	366.8	✓
+15		5.8	368.3	✓
W		3.9	370.2	✓
+10		2.8	371.3	✓

16+21.2

16.5 E. of ± = ctr Fire Hydr. 9.28 364.85 Top. Lower Flange

16+22.22 = S. Line Orange.

-10		5.4	368.7	✓
W		6.5	367.6	✓
+8		7.5	366.6	✓
+10		9.9	364.2	✓

374.13

54th St

16

374.13

+15	Pav		9.50	364.65	✓		
±			9.35	364.98	✓		
+10			9.73	364.40	✓		
+5			9.9	364.2	✓		
E			10.1	364.0	✓		
+10			10.8	363.3	✓		
T.P. B.M. B.P.	3.34	367.09	10.38	363.75	Top. Headwalls, W 54 <sup>th</sup> + Orange 363.75 ✓		
			16+25	367.09			
			3.31	363.78	✓		
			16+28.4				
			13.2 W. of ±	FL. Inlet 18" Culvert.	5.54	361.58	✓
			19.2 E. " "	FL. Outlet 18" "	6.45	360.64	✓
			16+30.3	N. Side E & W Headwall			
			12.5 W. of ±	E. End. Top of Headwall	3.35	363.74	✓
			16.5 W. " "	W. End " " "			
			16+30.				
-10			3.7	363.3	✓		
E			3.4	363.6	✓		
+10			3.3	363.7	✓		
+15	Pav		3.05	364.04	✓		
±	"		2.77	364.32	✓		
+10	"		2.89	364.20	✓		
+15			2.4	364.2	✓		
W			2.5	364.5	✓		
+10			1.6	365.4	✓		

367.09

16+59  
367.09  
2.1

364.9 ✓

365.9 ✓

362.7 ✓

362.90 ✓

362.98 ✓

362.79 ✓

362.6 ✓

362.3 ✓

361.9 ✓

16+60.4 s. side M.H.

10' E. of  $\phi$  = S.W. cor. M.H. 4.34

362.75 ✓

14.3 " " " = S.E. " M.H. 4.38

362.71 ✓

16+62.72

-10 4.9

362.1 ✓

E 4.7

362.3 ✓

+10 4.5

362.5 ✓

+15 Pav 4.44

362.65 ✓

 $\phi$  " 4.26

362.83 ✓

+16 " 4.46

362.63 ✓

+15 4.3

362.7 ✓

+14 2.9

364.1 ✓

W. 21

364.9 ✓

+10 1.2

365.8 ✓

16+64.2 N. side M.H.

10' E. of  $\phi$  = N.W. cor. M.H. 4.53

362.56 ✓

14.3 " " = N.E. " " " 4.47

362.62 ✓

367.09

17+00  
367.09  
2.5

364.5 ✓

365.4 ✓

362.7 ✓

360.4 ✓

360.4 ✓

360.80 ✓

360.75 ✓

360.8 ✓

360.5 ✓

359.6 ✓

359.3 ✓

359.9 ✓

17+21.06 P.C. Lt.

-10 7.9

359.1 ✓

E. 8.1

359.9 ✓

+10 7.8

359.2 ✓

+15 Pav 7.50

359.5 ✓

 $\phi$  " 7.56

359.53 ✓

+16 " 7.93

359.16 ✓

+15 7.9

359.1 ✓

+16 5.5

361.5 ✓

W. 4.5

362.5 ✓

+10 3.3

363.9 ✓

54th St.

17

367.09

17+50  
~~367.09~~  
4.7

-10		367.3	/
W		5.9	361.1 /
+9		7.0	360.0 ✓
+11		9.8	357.2 /
+15	pav	10.01	357.08 /
±	"	9.52	357.57 /
+10	"	9.35	357.74 /
+15		9.4	357.6 /
+17		8.8	358.7 /
E.		9.5	357.5 /
+10		10.6	356.4 /

17+75

-10		11.9	355.1 /
E		12.0	355.0 /
+10		11.0	356.0 /
+15	pav	10.99	356.10 /
±	"	11.18	355.91 /
+10	"	11.71	355.38 /
+14		11.5	355.5 /
+14		8.0	359.0 /
W		7.2	359.8 /
+10		6.0	361.0 /

367.09

54<sup>th</sup> St.

18

18+0  
~~367.09~~  
7.4

-10		354.6	✓
W		8.6	356.4 ✓
+9		8.9	358.1 ✓
+12		13.1	353.9 ✓
+15	pav	13.33	353.76 ✓
±	"	12.80	354.7 ✓
+10	"	12.61	354.48 ✓
+15		12.7	354.3 ✓
+18		12.0	355.0 ✓
E		12.0	355.0 ✓
+10		12.5	354.5 ✓
T.P.	9.76	355.63	12.22 354.87

18+25  
~~355.63~~  
3.0

-10		354.6	✓
E		3.0	354.6 ✓
+8		2.4	353.2 ✓
+9		2.9	354.7 ✓
+15	pav	2.80	354.8 ✓
±	"	3.07	354.56 ✓
+10	"	3.63	357.00 ✓
+15		3.6	357.0 ✓
+17		+1.0	356.6 ✓
W		+1.6	357.2 ✓
+10		+3.1	358.7 ✓

355.63 ✓

18+68.54 Ee

355.63

+0.3

355.9 ✓

-10

W

1.0

354.6 ✓

+7

1.6

354.0 ✓

+10

5.5

350.1 ✓

+15

Pav

5.88

349.75 ✓

E

"

5.52

350.11 ✓

+10

"

5.44

350.19 ✓

+15

5.0

350.6 ✓

E

6.4

349.7 ✓

+10

6.4

348.8 ✓

19+00

-10

8.5

347.11 ✓

E

9.0

346.6 ✓

+5

8.3

347.3 ✓

+10

6.3

349.3 ✓

+15

Pav

6.93

348.70 ✓

E

"

6.77

348.86 ✓

+10

"

6.97

348.66 ✓

+12

6.0

349.6 ✓

+17

6.2

349.4 ✓

+19

4.2

351.4 ✓

W.

3.3

352.3 ✓

+10

2.6

353.0 ✓

355.63 ✓

19+50.63

355.63

7.4

-10

W

8.1

348.7 ✓

+7

8.0

347.5 ✓

+10

6.9

347.6 ✓

+15

Pav

8.13

348.7 ✓

E

"

7.88

347.50 ✓

+10

"

7.88

347.75 ✓

+15

8.16

347.47 ✓

+23

7.5

348.1 ✓

E

10.2

345.4 ✓

+10

9.8

345.8 ✓

9.7

345.9 ✓

19+74

-10

9.8

345.8 ✓

E

10.0

345.6 ✓

+10.3 = S. End. Head wall

9.07

346.56 ✓

+12 ground

8.0

347.6 ✓

+15

Pav

8.30

347.3 ✓

E

"

8.11

347.5 ✓

+10

"

8.37

347.76 ✓

+14

7.5

348.1 ✓

W

8.5

347.1 ✓

+10

8.4

347.7 ✓

19+79

14.7 E. of E = F.L. Inlet { 24" Pipes

11.8

343.8 ✓

19+82

15' W. of E = F.L. outlet { 24" Pipes

12.4

345.2 ✓

54<sup>th</sup> St

19

355.63 ✓

19784

355.63

10.1

345.5 ✓

-10

-8 W. edge ditch

12.6

345.0 ✓

W " "

12.6

343.0 ✓

+7 " "

12.19

343.4 ✓

+8

9.4

346.7 ✓

+15 pav

8.41

347.7 ✓

±

8.18

347.6 ✓

+10

8.33

347.30 ✓

+14

8.0

347.6 ✓

+17.7 = N. End. Top Wing wall

8.99

346.4 ✓

E

10.1

348.5 ✓

+10

10.0

348.6 ✓

20+00

-10

10.6

345.0 ✓

E

10.9

344.7 ✓

+2

10.9

344.7 ✓

+11

7.7

347.9 ✓

+15 pav

8.30

347.3 ✓

±

8.14

347.49 ✓

+10

8.34

347.29 ✓

+12

7.8

347.9 ✓

+16

7.8

347.8 ✓

+21

10.9

344.7 ✓

W

10.9

346.7 ✓

+8 E. Bank.

10.5

345.1 ✓

+9 E. side ditch

12.6

343.0 ✓

355.63 ✓

54<sup>th</sup> St.

20

355.63

+15 W. edge ditch

12.4

343.2 ✓

+16 W. Bank

11.3

344.3 ✓

20+47 ± 18" Cor. Iron Pipe Culvert.

21' W. of E. = outlet FL

13.9

341.7 ✓

21' E " " = inlet. F.L.

10.7

344.9 ✓

21' 2 " " Top Head wall

13.8

341.8 ✓

20+50

-10

12.2

343.4 ✓

W

12.0

343.6 ✓

+4

12.4

343.7 ✓

+11

7.2

348.4 ✓

+15

pav

8.07

347.56 ✓

±

"

7.79

347.84 ✓

+10

"

7.92

347.71 ✓

+15

10.7

344.9 ✓

+21

11.4

344.2 ✓

E.

11.4

344.2 ✓

+10

11.4

344.2 ✓

21+00

-10

9.5

346.1 ✓

E

9.9

345.7 ✓

+6

9.2

346.4 ✓

+10

6.8

348.8 ✓

+15

pav

7.38

348.25 ✓

±

"

7.16

348.47 ✓

+10

"

7.23

348.40 ✓

355.63 ✓

21 + 00 (con)  
355.63  
6.7

+14			349.9	✓
+21		10.8	344.8	✓
W		12.3	343.3	✓
+10		12.7	342.9	✓

21 + 50

-10		10.0	345.6	✓
W		9.3	346.3	✓
+5		8.9	346.7	✓
+10		6.0	349.6	✓
+15	pay	6.63	349.00	✓
⊖	"	6.45	349.18	✓
+10	"	6.78	349.85	✓
+15		6.5	349.1	✓
E		6.6	349.0	✓
+10		6.5	349.1	✓
T.P.	11.61	361.31	5.93	349.70

21 + 90  
361.31

-10		9.6	351.7	✓
E		9.8	351.5	✓
+8		9.5	351.8	✓
+10		11.4	349.9	✓
+15	pay	11.84	349.47	✓
⊖	"	11.63	349.66	✓
+10	"	11.78	349.53	✓
+15		11.7	349.6	✓
W		12.0	349.3	✓
+10		12.1	349.2	✓

361.31 ✓

54<sup>th</sup> St

21

22 + 50  
361.31  
7.8

-10			353.5	✓
W		7.4	353.9	✓
+7		7.1	354.2	✓
+10		11.0	350.3	✓
+15	pay	11.00	350.3	✓
⊖	"	10.88	350.43	✓
+10	"	11.01	350.30	✓
+14		10.9	350.4	✓
+19		4.8	356.5	✓
E		4.5	356.8	✓
+10		3.8	357.5	✓

23 + 00

-10		1.0	360.3	✓
E		1.1	360.2	✓
+4		1.3	360.0	✓
+10		9.6	351.7	✓
+15	pay	10.33	350.98	✓
⊖	"	10.14	351.19	✓
+10		10.25	351.06	✓
+15		10.2	351.1	✓
+19		3.4	357.9	✓
W		3.6	357.7	✓
+10		3.9	357.4	✓



361.31 ✓

23+35

361.31

0.8

360.5 ✓

-10

W

0.1

361.2 ✓

+3

0.6

360.7 ✓

+10

9.6

351.2 ✓

+15 pav.

9.61

351.70 ✓

±

"

9.51

351.80 ✓

+10

"

9.75

351.56 ✓

+16

9.2

352.1 ✓

+21

0.7

360.6 ✓

E

0.6

360.7 ✓

+10

1.2

360.1 ✓

23+60

-10

3.6

359.7 ✓

E

3.4

359.9 ✓

+6

3.0

358.3 ✓

+10

9.0

352.3 ✓

+15 Pav

9.29

352.02 ✓

±

"

9.03

352.28 ✓

+10

"

9.08

352.23 ✓

+15

8.8

352.5 ✓

+20

1.8

359.5 ✓

W

1.6

359.7 ✓

+10

1.8

359.5 ✓

23+98

-10

6.0

355.3 ✓

W

5.9

355.4 ✓

361.31 ✓

54<sup>th</sup> st

22

361.31

+6

5.9

355.4 ✓

+9

8.0

355.3 ✓

+15

pav

8.25

353.06 ✓

±

"

8.33

352.98 ✓

+10

"

8.76

352.55 ✓

+15

8.4

352.9 ✓

+17

6.4

354.9 ✓

E

7.0

354.3 ✓

+10

7.0

354.3 ✓

24+02

-10

7.0

354.3 ✓

E

7.2

354.1 ✓

+8

6.7

354.6 ✓

+10

8.4

352.9 ✓

+15

pav

8.68

352.63 ✓

±

"

8.21

353.10 ✓

+10

"

8.13

353.18 ✓

+15

8.2

353.1 ✓

W

8.1

353.2 ✓

+10

8.0

353.3 ✓

T.P. RM, B.P. in Headwall

9.59

363.29

7.61

353.70

Rt of sta.

24+67

24+07 24

P.C. RT

363.29

10.0

353.2 ✓

-10

W

10.0

353.2 ✓

+10

10.0

353.2 ✓

+15

pav

9.95

353.34 ✓

363.29

24+07 44

363.29

±	Pav	10.08	353.21	✓
+10	"	10.63	352.66	✓
+15		10.3	352.9	✓
+16		9.4	353.8	✓
E		9.8	353.4	✓
+10		9.9	353.3	✓

24+25

-10		11.7	351.5	✓
E		11.3	351.9	✓
+4		10.9	352.3	✓
+6		9.7	353.5	✓
+11		9.5	353.7	✓
+15	Pav	10.45	352.84	✓
±	"	9.78	353.51	✓
+10	"	9.7	353.5	✓
W		10.1	353.1	✓
+10		10.1	353.1	✓

24+50

-5. Front. House		11.6	351.6	✓
W		11.1	352.1	✓
+6		10.5	352.7	✓
+11		9.1	354.1	✓
+15	Pav	9.24	354.05	✓
±	"	9.48	353.81	✓
+10	"	10.13	353.16	✓
+15		9.1	354.1	✓

363.29

54<sup>th</sup> St

23

363.29

+20		13.3	349.9	✓
E		13.3	349.9	✓
+10		13.3	349.9	✓
		24+67		
15.5 E of ± = FL. Pipe Culvert		12.43	350.86	✓ inlet
15.5 " " " Ctr. Headwall 5' Long.		9.63	353.66	✓

W End. Covered. appears to be on Radial line.

24+75

-10		13.1	350.1	✓
E		12.4	350.8	✓
+4		12.1	351.1	✓
+11		8.7	354.5	✓
+15	Pav	9.63	353.66	✓
±	"	9.06	354.23	✓
+10	"	8.82	354.47	✓
+15		8.4	354.8	✓
+20		12.3	350.9	✓
W		13.0	350.2	✓
+10		13.2	350.0	✓

25+00

-10		10.6	352.6	✓
W		10.4	352.8	✓
+10		6.9	356.3	✓
+15	Pav	8.69	355.20	✓
±	"	8.36	354.93	✓
+10	"	8.94	354.35	✓

363.29

25+00  
363.29

+15		8.2	355.0	✓
+23		12.1	351.1	✓
E		12.2	351.0	✓
+10		11.8	351.4	✓
		25+25 <i>first</i>		
-10		11.2	357.0	✓
E		11.1	354.1	✓
+4		10.9	352.3	✓
+10		7.2	356.0	✓
+15	PAV	8.02	355.27	✓
E	"	7.48	355.81	✓
+10	"	7.25	356.04	✓
+15		6.7	356.5	✓
+20		8.4	354.4	✓
W		9.2	354.0	✓
+10		10.0	353.2	✓
		25+55 <sup>10</sup> E.C.		
-10		8.5	354.7	✓
W		8.2	355.0	✓
+6		7.5	355.7	✓
+11		5.6	357.6	✓
+15	PAV	6.09	357.20	✓
E	"	6.33	356.96	✓
+10	"	6.86	356.43	✓
+15		6.1	357.1	✓
+20		7.3	353.9	✓

363.29

54 <sup>5</sup> 57

24

363.29

E		9.7	358.5	✓
+10		9.7	353.5	✓
		26+00		
-10		7.0	356.2	✓
E		7.0	356.2	✓
+5		6.6	356.6	✓
+12		3.2	360.0	✓
+15	PAV	3.80	359.4	✓
E	"	3.47	359.82	✓
+10	"	3.52	359.77	✓
+15		3.2	360.0	✓
+21		5.3	357.9	✓
W		5.3	357.5	✓
+10		5.2	358.0	✓
		26+40		
-10		2.0	361.2	✓
W		2.4	360.8	✓
+5		1.8	361.4	✓
+9		+0.2	363.4	✓
+15	PAV	0.48	362.81	✓
E	"	0.33	362.96	✓
+10	"	0.56	362.73	✓
+14		0.1	363.19	✓
+20		3.8	359.4	✓
E		4.8	358.4	✓
+10		4.9	358.5	✓
B.M. Headwall Sta 2467		9.59	353.70	✓ Page 22

Note: Cross sections cont on to E/Coron etc.  
See F.B. 1619 - Page 36  
by Walker 8-12-42



7-28-34

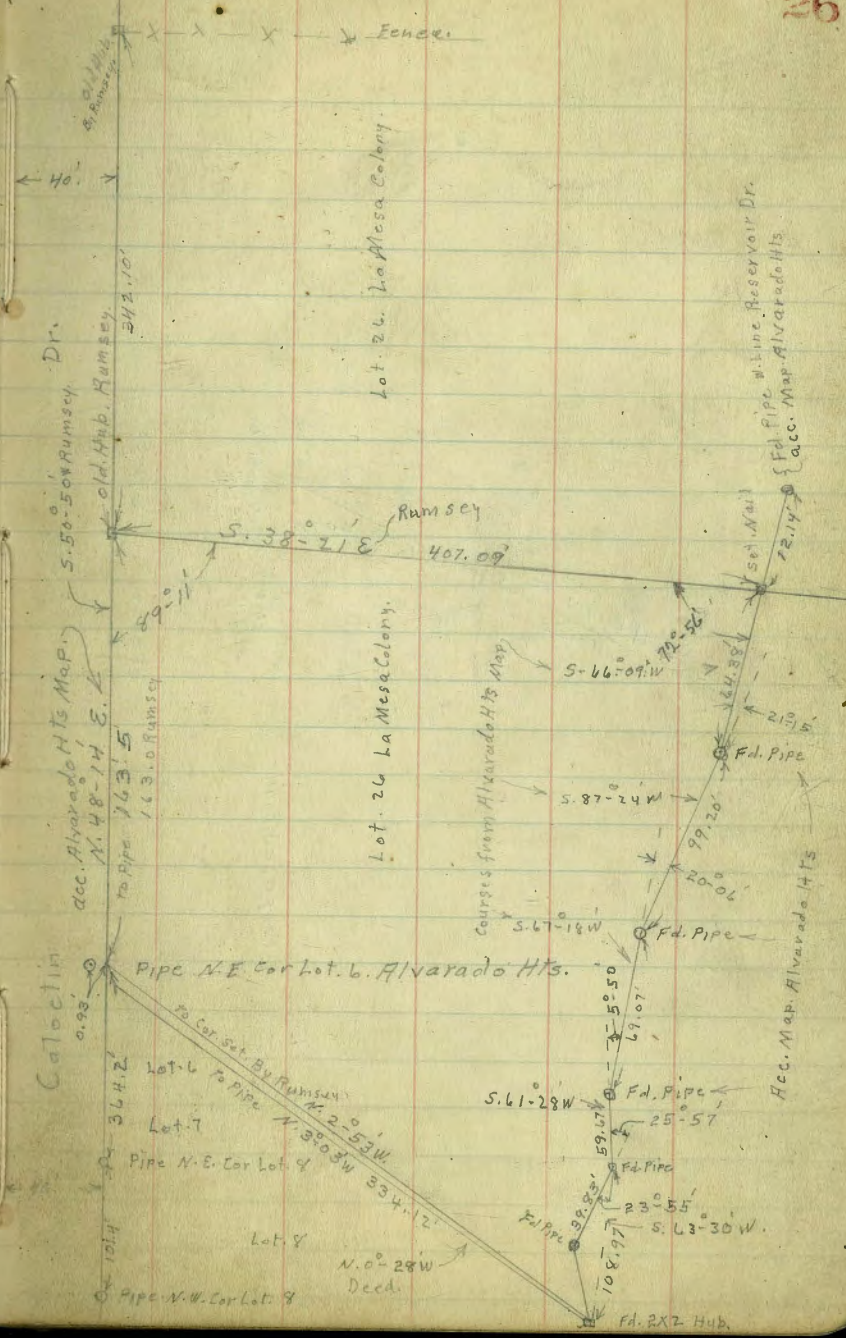
Mills  
Walker  
Bliss

Survey for Road Opening  
In Lot 26 La Mesa Hts.  
From Catalin Dr. To El Cajon Ave.  
(Campo Drive Extension)

Indexed  
c.s.K.

B.M. B.P.	1.59	454.05	452.46
5' S. of N. cb. El Cajon on pav.			
50' Bto $\phi$	opp. Prop. P.C.	2.18	451.87
25' " " "	= E. line	2.11	451.94
15' " " "	= E. cl.	2.11	451.94
$\phi$		2.05	452.00
15' Lt. of $\phi$	= W. cl.	1.97	452.08
25' " " "	= W. line	1.99	452.06
50' " " "	Opp. Prop. P.C.	1.94	452.11
0+00 = N. cl. line El Cajon Ave			
50' Lt.	gutter pav.	2.10	451.95
" "	Top emb. cl.	1.52	452.53
25' " "	" " "	1.52	252.53
" "	gutter pav.	2.14	451.91
15' " "	gutter pav	2.19	451.86
15' " "	Top emb. cl.	1.59	452.46
$\phi$	" " "	1.61	452.44
$\phi$	gutter pav	2.25	451.80
15' Rt.	" "	2.30	451.75
15' " "	Top emb. cl.	1.71	452.34
25' " "	" " "	1.76	452.29
25' " "	gutter Pav	2.35	451.70
50' " "	" " "	2.40	451.65
50' " "	Top emb. cl.	1.73	452.32

s.w. El Cajon +  
Rolando Blvd.





454.05

0706

50' RT	1.8	452.3
25' "	2.0	452.1
15' "	2.0	452.1
ϕ	2.0	452.1
15' Lt.	2.0	452.1
25' "	2.0	452.1
50' "	1.6	452.5

0714

65' Lt	6.9	447.2
50' "	6.6	447.5
25' "	8.4	445.7
15' "	8.8	445.3
ϕ	7.5	446.6
15' RT	6.5	447.6
25' "	5.3	448.8
50' "	4.6	449.5
60' "	3.6	450.5

0722 = N. Line Bl Cajon

60' RT	3.8	450.3
50' "	4.3	449.8
25' "	6.3	447.8
15' "	7.4	446.7
ϕ	8.8	445.3
15' Lt	9.3	444.8
25' "	9.1	445.0
50' "	8.3	445.8
65' "	8.1	446.0

454.05

0735 = P.C. 35' Curb Radius

	Carpo	Drive
50' Lt	9.6	444.5
25' "	10.2	443.9
15' "	10.5	443.6
ϕ	10.1	444.0
15' RT	8.1	446.0
25' "	7.4	446.7
50' "	5.2	448.9

0747 = P.C. 25' Prop Line Rad.

35' RT	7.4	446.7
25' " = Prop line at P.C.	8.1	446.0
15' "	9.1	445.0
ϕ	10.7	443.4
15' Lt	11.6	442.5
25' " Prop line at P.C.	11.5	442.6
40' "	11.4	442.7

0775

40' Lt	13.7	440.4
25' "	13.6	440.5
15' "	13.6	440.5
ϕ	12.5	441.6
15' RT	10.9	443.2
25' "	10.1	444.0
35' "	8.3	445.8

28

454.05

1+01.95 S. Line Alley

35' RT	10.3	443.8
25' "	11.5	442.6
15' "	13.1	441.0
ϕ	14.1	440.0
15' Lt.	14.6	439.5
25' "	14.5	439.6
35' "	14.9	439.2

1+21.95 = N. Line Alley

35' Lt.	14.5	439.6
25' "	15.1	439.0
15' "	16.1	438.0
ϕ	16.4	437.7
15' RT	15.0	439.1
25' "	12.7	441.4
35' "	11.4	442.7
T.P.	0.18	442.05
	1+50	12.18
		441.87

35' RT.	1.7	440.4
25' "	3.7	438.4
15' "	5.6	436.5
ϕ	6.3	435.8
15' Lt.	4.6	437.5
25' "	4.3	437.8
35' "	1.7	440.4

442.05

1+80

35' Lt.	3.4	438.7
25' "	3.8	438.3
19' "	4.2	437.9
15' "	5.8	436.3
ϕ	6.64	435.41
10' RT	8.2	433.9
15' "	7.6	434.5
25' "	6.0	436.1
35' "	3.3	438.8

2+00

35' RT	6.0	436.1
25' "	7.9	434.2
15' "	9.0	433.1
ϕ	7.5	434.6
15' Lt.	5.9	436.2
25' "	5.8	436.3
35' "	2.2	439.9

2+25

35' Lt	2.2	439.9
25' Lt	4.6	437.5
15' "	6.6	435.5
10' "	8.5	433.6
ϕ	8.8	433.3
12' RT	8.9	433.2
15' "	10.1	432.0
17' "	11.0	431.1

Campo Dr

29



442.05

2+25 (can)

21' RT	11.8	430.3
25 "	9.5	432.6
35 "	7.5	434.6

2+50

35' RT	9.7	432.4
30' "	11.8	430.3
25' "	11.1	431.0
15' "	10.9	431.2
φ	10.9	431.2
12' LT	9.4	432.7
15' "	8.0	434.1
20 "	6.4	435.7
25 "	6.4	435.7
35 "	5.5	436.6

2+75

35' LT	8.8	433.3
25' "	9.7	432.4
15' "	10.7	431.4
φ	11.5	430.6
15' RT	12.9	429.2
25' "	12.4	429.7
32' "	13.2	428.9
34' "	14.5	427.6
35' "	12.1	430.0

T.P. 5.37 435.22 12.20 429.85

Campo Drive

30

435.12

3+00

35' RT	7.1	428.1
25' "	6.8	428.4
15' "	7.0	428.2
φ	6.9	428.3
15' LT	6.4	428.8
25' "	6.3	428.9
35' "	5.7	429.5

3+25

35' LT	6.4	428.8
25' "	6.8	428.4
15' "	7.2	428.0
φ	8.0	427.2
15' RT	7.1	428.1
25' "	7.0	428.2
35' "	7.3	427.9

3+50

35' RT	8.4	426.8
30' "	6.9	428.3
25' "	6.6	428.6
15' "	6.2	429.0
φ	6.4	428.8
15' LT	5.5	429.7
25' "	5.3	429.9
35' "	5.4	429.8

T.P. φ Hub 12.07 442.95 4.34 430.88 3+72 94Δ

442.95

3+72 94 Δ 21-44' Lt. on split.

40' Lt.	8.5	434.5
25. "	8.3	434.7
15. "	9.2	433.8
2. "	11.0	432.0
Φ	12.0	431.0
15. Rt	11.9	431.1
25. "	12.6	430.4
40. "	14.6	428.4
	4+00	
35. Rt	8.5	434.5
25. "	8.2	434.8
15. "	8.1	434.9
2. "	8.2	434.8
Φ	7.3	435.7
15. Lt.	5.4	437.6
25. "	5.3	437.7
35. "	5.2	437.8
	4+25	
35. Lt	1.5	441.5
25. "	1.8	441.2
15. "	1.8	441.2
2. "	2.5	440.5
Φ	4.0	439.0
15. Rt	4.3	438.7
25. "	4.3	438.7
35. "	4.2	438.8

442.95

Campo Drive

31

T.P.	12.12	454.80	0.27	442.68
		4+50		
35. Rt			11.7	443.1
25. "			12.2	442.6
15. "			13.0	441.8
2. "			13.0	441.8
Φ			17.2	443.6
15. Lt.			10.7	444.1
25. "			10.7	444.1
35. "			10.3	444.5
		4+75		
35. Lt.			7.5	447.3
25. "			7.5	447.3
15. "			7.3	447.5
Φ			7.2	447.6
2. Rt.			8.4	446.4
15. "			8.9	445.9
25. "			9.0	445.8
35. "			9.5	445.3
		4+95		
35. Rt			5.7	449.1
25. "			6.4	448.4
15. "			6.9	447.9
8. "			7.0	447.8
Φ			5.8	449.0
15. Lt.			5.2	449.6

454.80

4+95 (con)

25' Lt. 5.4 449.4

35' " 5.9 448.9

5+10

35' Lt. 5.0 449.8

25' " 4.7 450.1

15' " 4.5 450.3

ϕ 4.3 450.5

15' RT 4.9 449.9

25' " 4.7 450.1

35' " 4.6 450.2

5+50

35' RT 2.9 451.9

25' " 2.9 451.9

15' " 3.0 451.8

ϕ 3.4 451.4

15' Lt. 3.7 451.1

25' " 3.9 450.9

35' " 4.1 450.7

6+00

35' Lt. 3.5 451.3

25' " 3.3 451.5

15' " 3.1 451.7

ϕ 2.8 452.0

15' RT 2.4 452.2

25' " 2.3 452.5

35' " 2.1 452.7

454.80

6+50

35' RT 2.2 452.6

25' " 2.1 452.7

15' " 2.3 452.5

ϕ 2.4 452.4

15' Lt. 2.7 452.1

25' " 2.7 452.1

35' " 2.7 452.1

7+16<sup>47</sup> = S. Line Catoctin Drive (on diagonal).

40' Lt. 1.9 452.9

25' " 2.0 452.8

15' " 2.0 452.8

ϕ 2.0 452.8

15' RT 2.1 452.7

25' " 1.9 452.9

40' " 1.9 452.9

20' N. of S. Line = ϕ Catoctin Dr. = ϕ Ex. Graded Rd.

100' RT 1.9 452.9

40' " 1.8 453.0

25' " 1.8 453.0

15' " 1.8 453.0

ϕ 1.7 453.1

15' Lt. 1.7 453.1

25' " 1.6 453.2

40' " 1.6 453.2

100' " 1.2 453.6

Campo Drive 32

454.80

T.P.  
Elec Pole 75699  
CHK. B.M. Nails in

7.68

460.72

1.76

453.04

1.75

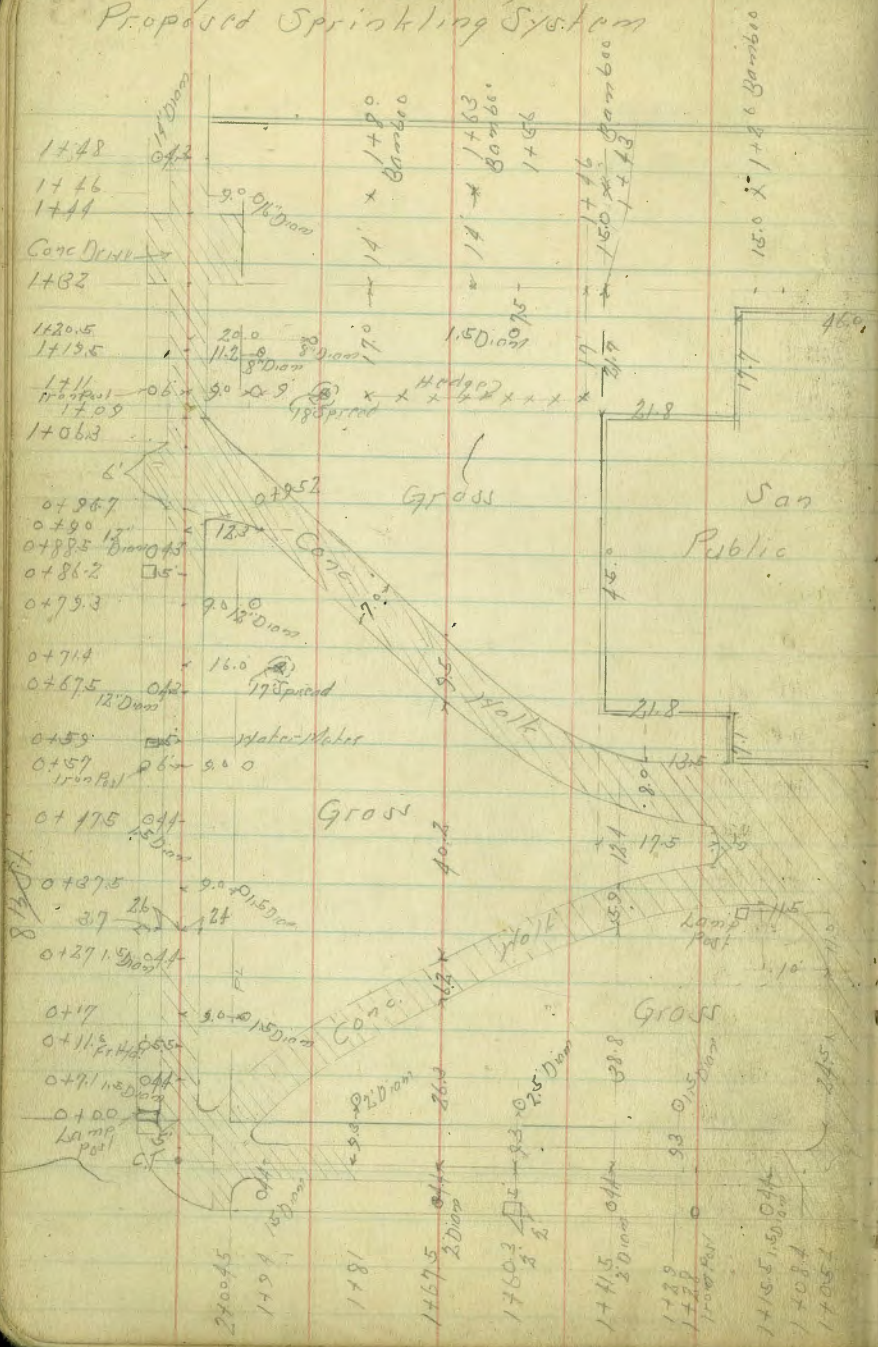
458.97

F.B. 1246. P. 5  
= 459.06

Campo Drive.

33

San Diego Public Library  
Proposed Sprinkling System

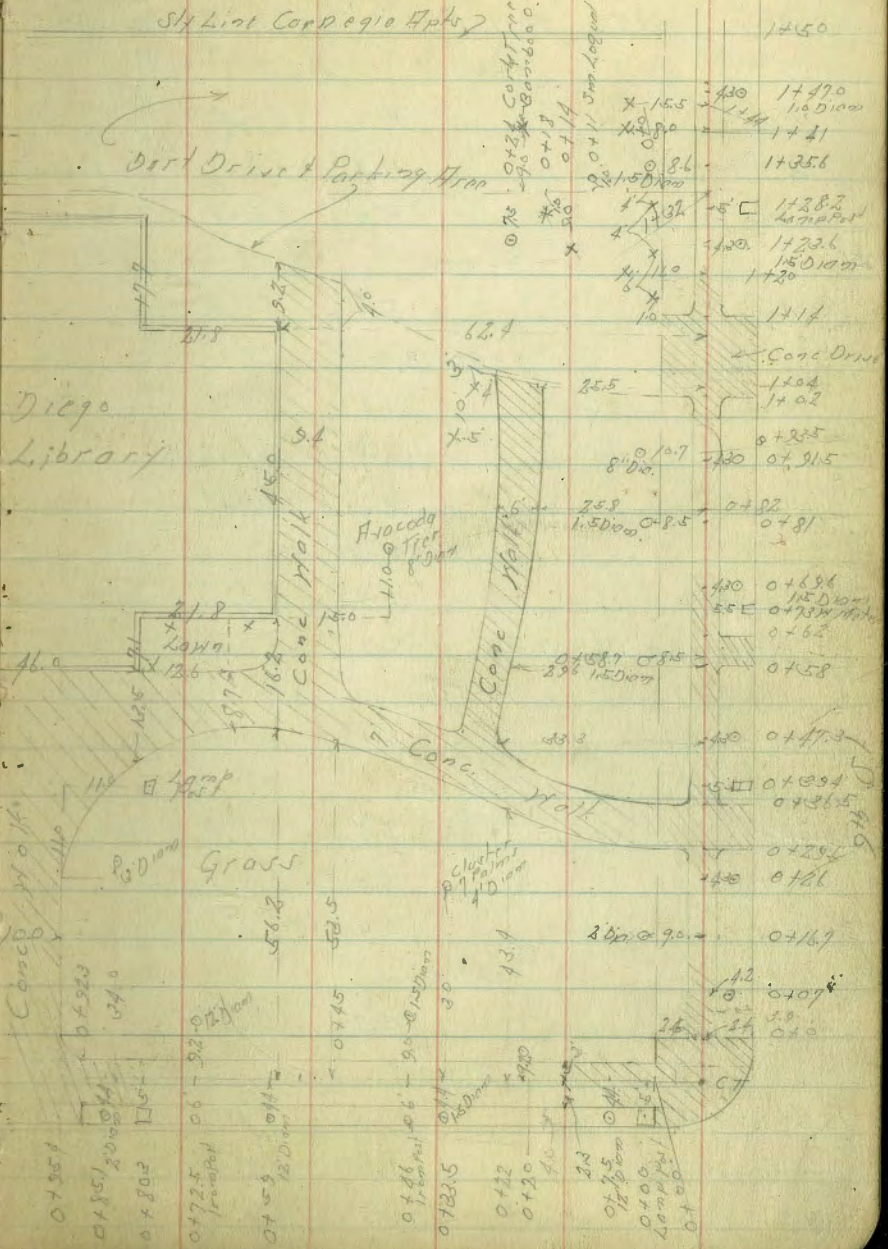


indexed  
c.s.k.

- Tree Palms
- Lamp Post
- x Small Shrubs

Aug 23-34  
510.00  
91.15  
North Lamp

34

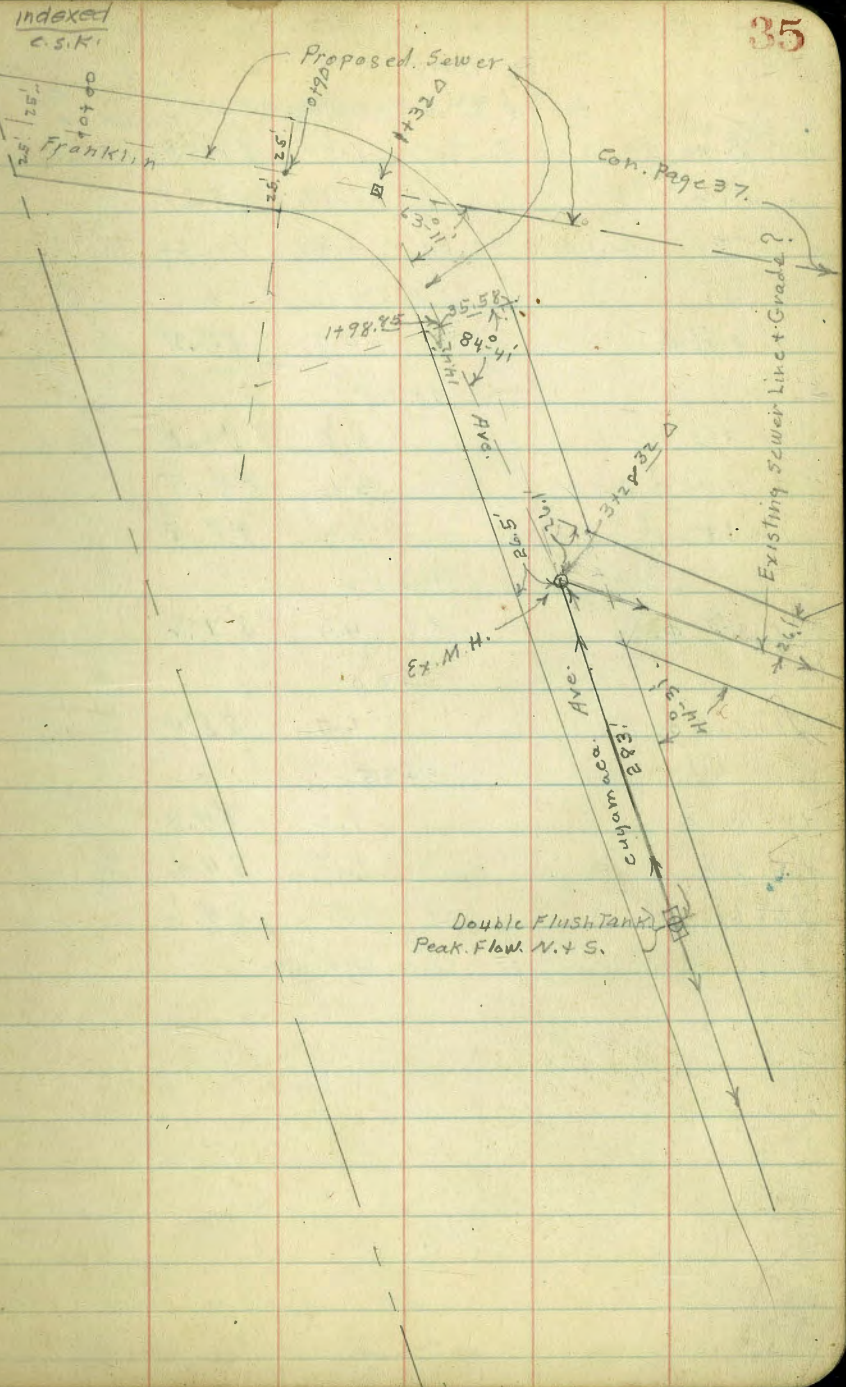


9-5-34  
 Miller  
 Walker

Prelim Sewer in Franklin Ave  
 E. of Old City Boundary.

BM. B.P.	0.98	90.48	89.50	N.E. Franklin + Cuyamaca.
		0+00		
N. ch		4.4	85.9	
φ		4.5	86.0	
S. ch		4.3	86.2	
		0+50		
φ		5.8	84.7	
		0+90 B.C.		
N. ch		6.5	84.0	
φ		6.4	84.1	
S. ch		6.5	84.0	
		1+32 A 13°-11' RT.		
on Hub		6.97	83.51	
5.2' Rt. on split = N. ch.		6.7	83.6	
		1+50		
φ sewer		6.1	84.4	
		1+98.85		
4.4 RT = ch		5.5	85.0	
φ sewer		6.0	84.5	
25.6 Lt. = ch		5.4	85.1	
		2+50		
φ sewer		3.7	86.8	
		3+00		
13.3' Rt = ch.		1.4	89.1	
φ proposed sewer		1.6	88.9	
15.8' Lt = ch.		1.5	89.0	

INDEXED  
 C.S.K.



90.48  
3+28 32 = Existing M.H. 1/2 S. of Franklin

90.48

36

→ 3+74.20

Rim

1.04

89.44

Franklin Ave

7.51

82.97

Top of 6" Sewer Pipe

F.L.

7.19

83.29

T.P.

2.64

92.14

0.94

89.50

3+50

1' S. of st.

2.7

89.4

4+00

14' Rt. = cl

3.1

89.0

7' S. of st.

3.6

88.5

16' Lt. = cl

3.2

88.9

4+50

1' S. of st.

4.9

87.2

5+00

1' S. of st.

6.7

85.4

5+35

14' Rt. = cl

7.2

84.9

1' S. of st.

7.5

84.6

16' Lt. = cl

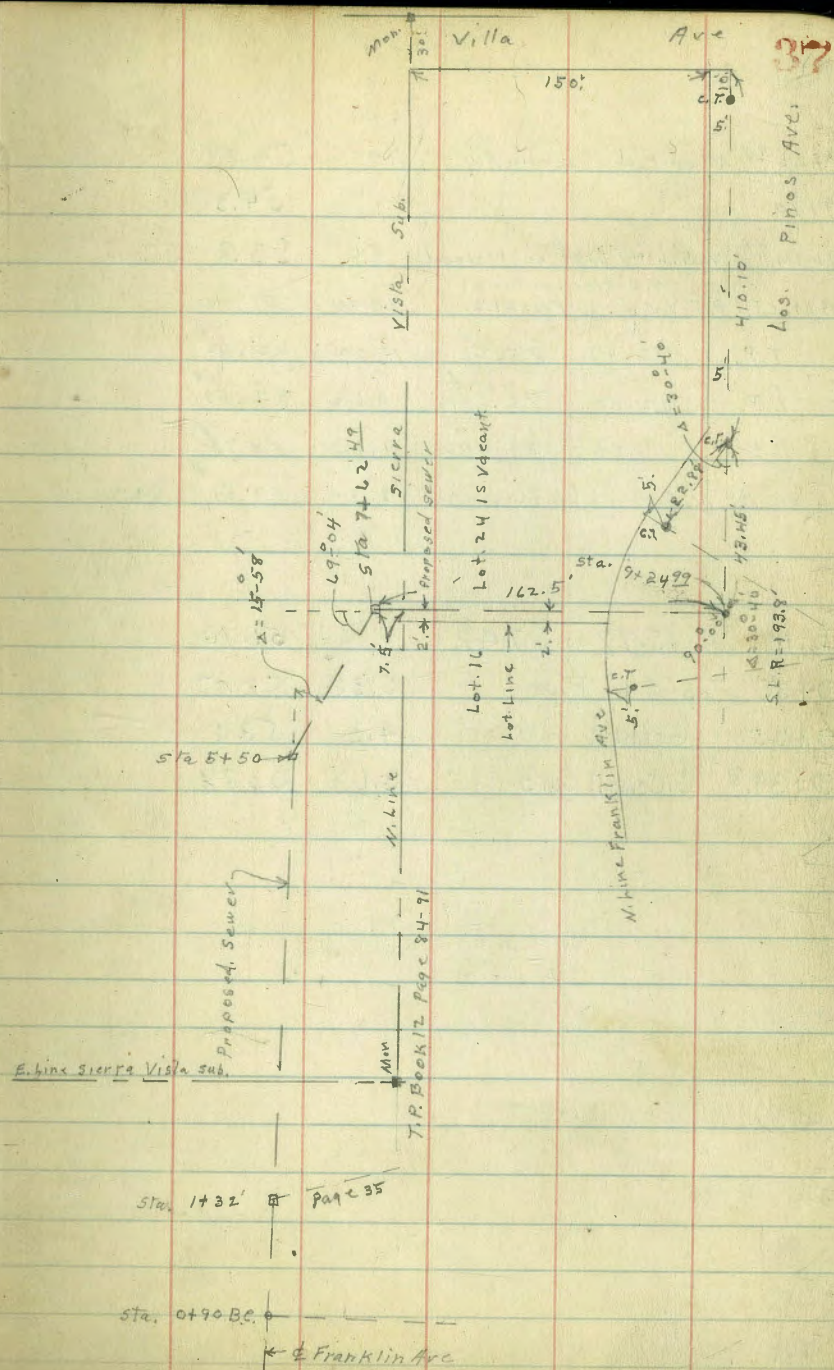
7.5

84.6

9-7-34 Prelim Sewers N. of N. Line  
 Miller Walker Sierra Vista sub. from Franklin East.

Plat Page 35

B.M. Hub Δ	3.44	86.95	83.51	Sta 1+32 Page 35
1+43 gutter			3.5	83.5
1+43 Top. ont. cl.			3.13	83.82
1+93			2.5	84.5
2+05			4.7	82.3
2+13			8.7	78.3
2+50			10.4	76.6
3+00			15.2	71.8
T.P.	0.76	74.91	12.80	74.15
3+50 bottom canyon			7.8	67.1
4+00 " "			9.4	65.5
4+50 " "			11.0	63.9
5+00 " "			12.5	62.4
T.P. 15° 58'				
5+50 Rt	3.82	65.11	13.62	61.29
5+50			5.0	60.1
6+00			6.4	58.7
7+00			5.3	59.8
7+40			4.6	60.5
7+62 1/2 69-04 Rt. on stub			2.45	62.66
7+68 50			3.5	61.6
1.5' E. of 7+68 50 = W. side Blue Pole				
7+69 29 = N. Line Sierra Vista Sub			5.4	59.7
T.P.	2.09	62.44	4.76	60.35
8+00			4.4	58.0
8+50			4.7	57.7





62.44

9+06 <sup>50</sup>	N. ent. d. Franklin Ave	7.55	54.89	
9+10		8.1	54.3	
9+24 <sup>29</sup>	N. 5' Line Los Pinos Produca-	8.6	53.8	
B.M. C.J. P.I.	{ N. 5' Line Los Pinos N. 5' " Franklin	10.74	51.70	
T.P.	12.99	75.21	0.22	62.22
T.P.	12.10	86.69	0.62	74.59
T.P.	6.86	91.85	1.70	84.99
chk B.M. B.P.	N. E. Frankl'n + Cayamaca	2.34	89.51	-89.50

B.M.	5.72	57.42	51.70
9+35	Top of 6' Pipe	5.35	52.07
9+35	Ground	4.3	53.1
9+39.8	S. Cement Curb	3.63	53.79

Cross Section Fay St. Ext. Bet. Track + La Jolla High School  
South of St. Marlboro

Indexed  
C.S.K.

No. 26-34 39

Sec 1427 Page 65-67-68-69

157.56

Station	Point	Elevation	Notes
B.M.	1248	157.56	145.08
	0+0	52.8	B.C. Pt. S.D. Elec RR
			A-37°45' D=8°00'
	0+0		St. Marlboro
✓ 1/2	Top RR	4.76	152.80
6"		6.0	151.6
26"		8.1	149.5
43"		10.8	146.8
	0+50		
✓ 1/2	Top RR	4.94	152.62
6"		6.1	151.5
33"		8.2	149.4
45"		9.2	148.4
	0+90.6		
✓ 1/2	Top RR	5.04	152.52
6"		6.2	151.4
15"		8.1	149.5
36"		8.6	149.0
42"		8.6	149.0
	1+15		
✓ 1/2	Top RR	5.05	152.61
6"		6.0	151.6
13"		8.2	149.3
35"		8.5	149.1
			157.56
	42.5"		Conc. Floor
	1+22		
✓	37"		18" Grating
	FL 6"		Drain
	1+57		
✓ 1/2	Top RR	5.05	152.51
6"		6.2	151.4
12"		8.4	149.2
35"		8.4	149.2
35"		8.01	149.55
40"		8.2	149.4
	2+0		
✓ 1/2	Top RR	5.18	152.38
6"		6.4	151.2
11"		8.3	149.3
33"		8.7	148.9
46"		8.41	149.15
56"		8.41	149.15
	2+54		
✓ 1/2	Top RR	5.63	151.93
6"		6.2	150.8
13"		8.3	149.3
33"		8.2	149.4
60"		7.80	149.76

15756

2747			
✓ 1/2	Top W Rail	5.76	151.80
6 W		6.8	150.8
13 W		8.1	149.5
32 W	F Edge Angle 3' Walk	7.66	149.90
39 W	NE Cor Spragr		

2782

✓ 1/2	Top W Rail	5.93	151.63
6 W		7.1	150.5
13 W		8.1	149.5
34 W	F Edge 3' Walk	7.68	149.88
40.5 W	NE Cor Bldg	7.7	149.9

370

✓ 1/2	Top W R	6.15	151.41
6 W		6.9	150.7
13 W		7.9	149.7
36 W	F Edge 3' Walk	7.67	149.59

3750

✓ 1/2	Top W R	6.90	150.66
9 W		7.0	151.6
13 W		8.0	149.6
38.5 W	F Edge Walk	9.64	147.92 149.92

3768

✓ 1/2	Top W R	7.21	150.35
9 W		7.2	150.4
13 W		7.7	149.9

15756

39 W	F Edge 3' Walk	8.00	149.56
3794			

✓ 1/2	Top W Rail	7.62	149.94
6 W		8.2	149.4
17 W	Top Cb	7.03	150.53
	Gutter	7.55	150.01
38 W	End 3' Walk	7.62	149.94
44 W	SE Cor Bldg	7.6	150.0

4719

✓ 1/2	Top W R	8.00	149.56
6 W		9.1	148.5
7 W		7.9	149.7
18 W	1/2 Naulilus on Pav	7.76	149.80
17 W	Top Cb	8.04	149.52
	Gutter	8.54	149.02

4728: Point of Switch

4725

1/2	Top W R	8.33	149.23
6 W		9.4	148.2
7 W		8.4	149.2
20 W	Top SCb	8.30	149.26
	Gutter	8.80	148.76

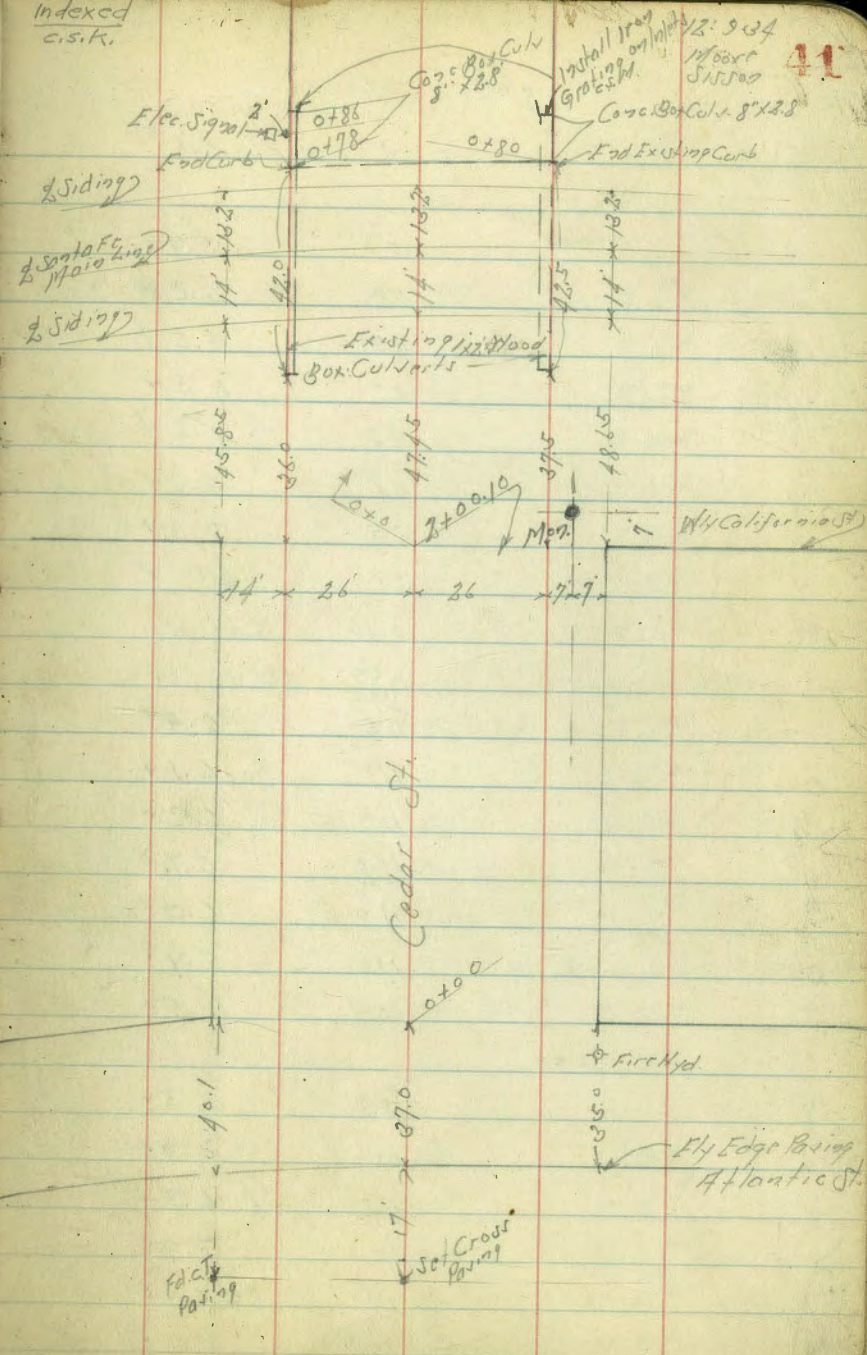
40

Cross Section Cedar St.  
Atlantic St. to California St

80' W. of  
14' Cb's  
13' Qts

Indexed  
c.s.k.

B.M	402	8.96	8.96	4.94	J.F.B.P Beech + Atlantic
S	0-2 Pavt.		3.93	5.03	x
d	" "		4.07	4.89	x
H	" "		4.19	4.77	x
0-15					
H			4.8	4.2	x
d			4.6	4.4	x
S			4.5	4.5	x
0-08					
S			3.8	5.2	x
Cb			4.3	4.7	x
1/4			4.2	4.8	x
1/2			4.6	4.4	x
1/4			4.5	4.5	x
Cb			4.3	4.7	x
H			4.1	4.9	x
0+0 = E. of Atlantic					
H			3.6	5.4	x
Cb			3.8	5.2	x
1/4			4.3	4.7	x
1/2			4.5	4.5	x
1/4			4.0	5.0	x
Cb			4.1	4.9	x
46			3.1	5.9	x



8.96

S		2.5	5.5 x
	0708		
S		3.1	5.9 x
XB		2.8	6.2 x
cb		4.5	4.5 x
1/4		3.7	5.3 x
1/2		4.4	4.6 x
1/4		4.1	4.9 x
cb		3.5	5.5 x
N		3.0	6.0 x
TP	12.23	17.89	3.30
	0750		5.66

		<del>17.89</del>	
N		11.5	6.4 x
cb		11.8	6.1 x
1/4		11.7	6.2 x
1/2		12.2	5.7 x
1/4		11.9	6.0 x
cb		12.0	5.9 x
S		10.4	7.5 x

	0790		
S		9.4	8.5 x
cb		10.0	7.9 x
1/4		11.2	6.7 x
+5		10.0	7.9 x
1/2		10.1	7.8 x
1/4		10.1	7.8 x

17.83

~~17.89~~

cb		16.7	7.2 ✓
N		10.4	7.5 ✓
	170		
N		9.7	8.2 ✓
cb		9.4	8.5 ✓
1/4		9.6	8.3 ✓
1/2		9.5	8.4 ✓
1/4		9.5	8.4 ✓
cb		10.3	7.6 ✓
+2		9.4	8.5 ✓
S		8.6	9.3 ✓

	1715		
S		8.2	9.7 ✓
cb		9.8	8.1 ✓
1/4		8.9	9.0 ✓
1/2		8.6	9.3 ✓
1/4		7.8	10.1 ✓
cb		7.8	10.1 ✓
N		8.0	9.9 ✓
+1	1/2 f Walk Case	7.9	10.18 ✓

	1750		
N		6.7	11.2 ✓
cb		6.4	11.5 ✓
1/4		6.6	11.3 ✓
1/2		7.1	10.8 ✓
1/4		6.9	11.0 ✓

42

17.89

17.89

cb	7.3	10.6 ✓
S	6.2	11.7 ✓
1775		
S	4.9	13.0 ✓
+5	6.0	11.9 ✓
cb	5.8	12.1 ✓
1/4	6.3	11.6 ✓
1/2	5.9	12.0 ✓
1/4	5.5	12.4 ✓
cb	5.2	12.7 ✓
N	5.7	12.2 ✓
210010 - 1/2 6 Col. f. St. - 040 Flood		
N	5.0	12.9 ✓
cb	3.8	14.1 ✓
1/4	4.9	13.0 ✓
1/2	4.9	13.0 ✓
1/4	4.7	13.2 ✓
cb	4.7	13.2 ✓
S	5.2	12.7 ✓
0+20		
S	3.7	14.2 ✓
+8	5.6	14.3 ✓
cb	4.7	13.2 ✓
+2	4.7	13.2 ✓
1/4	3.1	14.5 ✓
1/2	3.5	14.4 ✓

17.89

17.89

43

1/4	4.7	13.2 ✓
cb	4.8	13.1 ✓
N	4.2	13.7 ✓
0+86		
N	3.1	14.8 ✓
+9	3.1	14.8 ✓
cb	4.8	13.1 ✓
+1 = Outlet 1/2 2 Wood Box	4.85	13.04 ✓
Col. Floor Line		
+10	2.8	15.1 ✓
1/4	2.6	15.3 ✓
1/2	2.5	15.4 ✓
1/4	2.5	15.4 ✓
+6	2.2	15.6 ✓
cb	4.8	13.1 ✓
+5	3.2	14.7 ✓
S	2.9	15.0 ✓
0+875		
S	2.8	15.1 ✓
+8	3.0	14.9 ✓
cb	2.6	14.3 ✓
+1 Top Existing 1/2 2 Wood Box Col.	3.57	14.32 ✓
+1 Floor Line	4.89	13.00 ✓
+7	2.3	15.6 ✓
1/4	2.2	15.7 ✓
1/2	2.4	15.5 ✓
1/4	2.5	15.4 ✓

17.89

17.89

17.89

17.89

44

+3		2.7	15.2 ✓
+12	Top x 2 Yard Box Culs.	6.5	14.4 ✓
cb		3.5	14.4 ✓
+6		2.7	15.2 ✓
H		3.2	14.7 ✓
0+47.45 = $\frac{1}{2}$ W Sidings			
H	Top W Rail	1.92	15.97 ✓
$\frac{1}{2}$	" " "	2.04	15.85 ✓
$\frac{1}{2}$	" " "	2.20	15.69 ✓
0+61.45 = $\frac{1}{2}$ Main line			
S	Top W Rail	1.99	15.90 ✓
$\frac{1}{2}$	" " "	1.82	16.07 ✓
H	" " "	1.80	16.09 ✓
0+74.65 = $\frac{1}{2}$ East Sidings			
H	Top E Rail	1.61	16.28 ✓
$\frac{1}{2}$	" " "	1.61	16.28 ✓
$\frac{1}{2}$	" " "	1.76	16.13 ✓
0+78.07 = W			
0+80 " " = W End Pav. mp			
S		2.1	15.79 ✓
+4.5	Sly Conc. Walk	1.67	16.22 ✓
+9.5	Hly " "	1.68	16.21 ✓
cb + Pav.		1.83	16.06 ✓
$\frac{1}{4}$	o's Pav	1.73	16.16 ✓
$\frac{1}{4}$	" " "	1.67	16.22 ✓
$\frac{1}{4}$	" " "	1.65	16.24 ✓
cb + Pav		1.67	16.22 ✓

+4.5	Sly Conc. Walk	1.73	16.16 ✓
+9.5	Hly " "	1.65	16.24 ✓
H		2.0	15.89 ✓
1+0 =			
SCB	Top Head Wall	0.94	16.95 ✓
	Floor Line 8' x 28' Conc. Culs.	2.21	15.68 ✓
H	cb	0.81	17.08 ✓
	Floor Line 8' x 28' Conc. Culs.	2.62	15.27 ✓
TP	2.12	8.96	11.05
BM		4.02	4.94
SE BP. Beach + Atlantic 1.97			

Cross Section alley 20' wide  
 Blk 9 Ocean Beach  
 " 93 Pt. Loma Hts.

Vol. 1147	229.50	21808	SWBP
T.P. 177	7m. 7x 7.53	221.97	

W.L. Guizot = 0400

N Top of	1.61	222.13
N base	1.81	221.93
C "	1.67	222.07
S " Top of	1.06	222.68
	0.81	222.83

0+75

S	1.6	222.1
C	1.7	222.0
N	2.1	221.6

0+50

N	3.3	220.4
C	3.6	220.1
S	3.0	220.7

1+00

S	5.3	218.4
C	5.8	217.9
N	6.4	217.3

1+50

N	7.9	215.8
C	7.7	216.0
S	7.1	216.6

Indexed  
 G.H.K.

Map  
 Survey  
 Northway  
 1-9-35  
 45

Alley  
 Froude St.  
 6100

Ocean Beach

1.30  
 2x30-35  
 Div. line.

Pt Loma Hts.

Santa Cruz

Guizot St.



223.7x

	2+00		
S		8.5	215.2
C		9.0	214.7
N		9.4	214.3

2+00.15 - Div. line

N		10.0	213.2
C		9.8	213.9
S		9.3	214.4

2+50

S		9.6	214.1
C		10.2	213.5
N		10.5	213.2

3+00

N		11.7	212.6
C		11.3	212.4
S		10.8	212.9

3+50

S		14.7	210.0	
C		14.3	209.4	
N		15.2	208.3	
T.P.	0.61	214.21	10.14	213.60

214.1

46

3+65

N		7.6	206.6
C		6.3	207.9
S		5.8	208.4
+7		16.1	198.1
+16		23.8	190.4

3+85

-20		27.2	187.0
S		25.2	189.0
C		9.0	205.2
N		9.8	204.4

T.P.	0.74	203.12	11.83	202.38
------	------	--------	-------	--------

3+95

N		0.0	203.1
+2		0.0	203.1

T.P.	1.81	192.05	12.88	190.24
------	------	--------	-------	--------

+6		0.4	191.7
C		1.0	191.1

+8		6.7	185.4
----	--	-----	-------

S		6.8	185.3
---	--	-----	-------

+15		8.0	184.1
-----	--	-----	-------

4+10

-10		10.1	182.0
-----	--	------	-------

S		9.7	182.4
---	--	-----	-------

C		7.6	184.5
---	--	-----	-------

+4		5.3	186.8
----	--	-----	-------

N		+9.6	201.7
---	--	------	-------

192.05

J+W

N	8.0	184.1
+6	11.4	180.7
C	12.0	180.1
S	12.9	179.2
+10	11.1	181.0

J+50

S	14.8	177.3
C	15.2	176.9
N	15.0	177.1

J+95

N	17.8	174.3
C	17.7	174.4
J	16.5	175.6

J+N

S	9.9	182.2
C	12.7	179.4
T.P.	11.3	182.20
N	6.9	175.3
+10	11.6	170.4

J+50

-10	18.1	164.1
N	12.6	168.6
C	6.8	175.4
+7	2.2	179.9
J	2.1	180.1

182.20

5770

J	4.4	178.8
C	4.2	178.0
N	5.1	177.1
+10	7.1	175.1

5780

N	6.1	176.1
C	5.4	176.8
S	4.7	178.5

5795

J	4.0	178.9
C	4.0	178.2
N	6.7	175.5

5797

N	6.7	175.5
C	5.5	176.9
J	5.0	177.2

5498

S	10.9	171.3
C	12.0	170.2
N	12.9	169.3

6400 - E.L. Froude

N Total of having	12.60	169.60
C	13.08	169.12
S pav	11.93	170.27
S Top of	11.31	170.89
shook to other Rev. Grade	12.20	168.00
		167.90

17

Atlantic St Top of Curb Levels  
Harast by St to Court St.

BM	1.81	11.81	10.00
10.5' S of S.L. Harast by - Cb B.C.			
E Top Cb		0.81	11.0
H " "		1.91	9.90
S.L. Harast by			
H Top Cb		1.84	9.97
E " "		0.50	11.31
H.L. Harast by			
E Top Cb		1.65	10.16
H " "		2.92	8.89
10.5' N of H.L. Harast by - Cb B.C.			
H Top Cb		2.87	8.94
E " "		1.79	10.02
30' N			
E Top Cb		1.95	9.86
H " "		3.11	8.70
15' N			
H Top Cb		3.52	8.29
E " "		2.20	9.61
103' N			
E Top Cb		2.45	9.36
H " "		3.92	7.89
114' N			
H Top Cb - Sly End Santo Ferry		4.05	7.76

NE BP  
Harast by +  
Atlantic  
Reduced & plotted 4/19/35  
Mohler

Indexed  
c.s.k.

April 6-35  
18

			11.81
			135' N
H Top Cb		4.19	7.64
E " "		2.67	9.14
146' N			
E Top Cb - Sly End Santo Ferry		2.87	8.94
175' N			
E Top Cb		3.40	8.41
H Gutter in Drive		5.12	6.69
200' N			
H Top Cb		4.73	7.08
E Gutter in Drive		4.67	7.14
250' N			
E Top Cb		4.80	7.01
H Gutter in Drive		5.92	5.89
294' N = Cb B.C.			
H Top Cb		5.65	6.16
E " "		5.68	6.13
300' N = S.L. Clayton			
E Top Cb		5.78	6.03
H " "		5.69	6.12

11 81			
N.L. Clayton			
H	TopCb	5.99	5.87
F	"	5.89	5.97
E. H. of N.L. Clayton - Cb EC			
F	TopCb	5.94	5.87
H	"	5.99	5.87
50' H			
H	TopCb	6.12	5.69
F	"	6.17	5.64
100' H			
F	TopCb	6.50	5.31
H	"	6.32	5.49
TP	317 865	6.33	5.48
150' H			
H	"	3.37	5.78
F	"	3.36	5.79
200' H			
F	TopCb	3.55	5.10
H	"	3.59	5.06
250' H			
H	TopCb	3.77	4.88
F	"	3.84	4.81
294' H = Cb EC			
F	TopCb	4.01	4.64
H	"	4.04	4.61

865			
300' H = S.L. Sutherland			
H	TopCb	4.01	4.64
F	"	4.02	4.63
N.L. Sutherland			
F	TopCb	4.28	4.37
H	"	4.26	4.39
6' H of N.L. Sutherland			
H	TopCb	4.27	4.38
F	"	4.28	4.37
50' H			
F	TopCb	4.44	4.21
H	"	4.43	4.22
100' H			
H	TopCb	4.60	4.05
F	"	4.61	4.04
150' H			
F	TopCb	4.82	3.87
H	"	4.74	3.91
TP	411 839	4.87	4.28
200' H			
H	TopCb	4.67	3.72
F	"	4.75	3.64
250' H			
F	TopCb	4.90	3.49
H	"	4.83	3.56

Noted Pol  
on 11/20  
100' H of N.L.  
Sutherland

8.39

294 H = Cb BC

H Topcb	4.95	3.44
E	5.01	3.38

300 H = S-L Hoell

E Topcb	5.02	3.37
H	4.95	3.44

H-L Hoell

H Topcb	4.94	3.45
E	5.00	3.39

6 H of H-L Hoell = Cb BC

E Topcb	5.01	3.38
H	4.91	3.48

50 H

H Topcb	4.65	3.74
E Gutter 12 Dr.	5.58	4.81

100 H

E Topcb	4.64	3.75
H	4.33	4.06

150 H

H Topcb	3.98	4.41
E	4.27	4.17

200 H

E Topcb	4.35	4.04
H	4.16	4.23

8.39

250 H

H Topcb	4.33	4.06
E	4.72	3.67

294 H = Cb BC

E Topcb	4.83	3.56
H	4.46	3.93

300 H = S-L Estudillo

H Topcb	4.47	3.92
E	4.66	3.73

H-L Estudillo

E Gutter 4 Dr	5.55	4.84
H Topcb	4.77	3.62

6 H of H-L Estudillo

H Topcb	4.79	3.60
E Gutter 12 Dr.	5.61	4.78

7P 295 649 4.85 3.54

50 H

E Gutter drive	3.90	4.59
H Topcb	2.97	3.52

100 H

H Topcb	3.16	3.33
E	3.33	3.16

150 H

E Topcb	3.33	3.10
H	3.33	3.17

April 8-85

50

6.49

200 ft		
W Topcb	377	3.07
F	363	2.86
250 ft		
F Topcb	371	2.78
W	360	2.89
298 ft = C6 BC		
W Topcb	378	2.71
F	385	2.64
3035 ft = St. Wright		
F Topcb	390	2.69
W	379	2.70
H. Wright		
W Topcb	407	2.47
F	406	2.43
6 ft of H. Wright = C6 BC		
F Topcb	405	2.44
W	406	2.43
50 ft		
W Topcb	418	2.31
F	420	2.29
100 ft		
F Topcb	437	2.12
W	433	2.16

6.49

51

150 ft		
W Topcb	449	2.01
F	449	2.00
200 ft		
F Topcb	465	1.84
W	460	1.87
250 ft		
W Topcb	476	1.73
F	480	1.69
294 ft = C6 BC		
F Topcb	483	1.66
W	482	1.66
300 ft = St. Bordini		
W Topcb	487	1.67
F	481	1.68
H. Bordini		
F Topcb	486	1.63
W	487	1.67
6 ft of St. Bordini		
W Topcb	487	1.67
F	490	1.59
TP	478	6.39
488	1.61	
50 ft		
F Topcb	464	1.75
W	461	1.78

	100' H		
H	Topch	4.57	1.87
F		4.44	1.95
	150' H		
F	Topch	4.30	2.09
H		4.45	1.94
	200' H		
H	Topch	4.55	1.84
F		4.17	2.27
	250' H		
F	Topch	4.05	2.34
H		4.85	1.54
	294' H - C5 RC		
H	Topch	4.77	1.67
F		4.00	2.39
	300' H - S1/2 Conts		
F	Topch	3.99	2.40
H		4.81	1.58
TP	376	5.40	4.75
BN		5.59	-0.19

J.M. Manio  
 Cur  
 10/1/11  
 H. H. Manio  
 -0.18

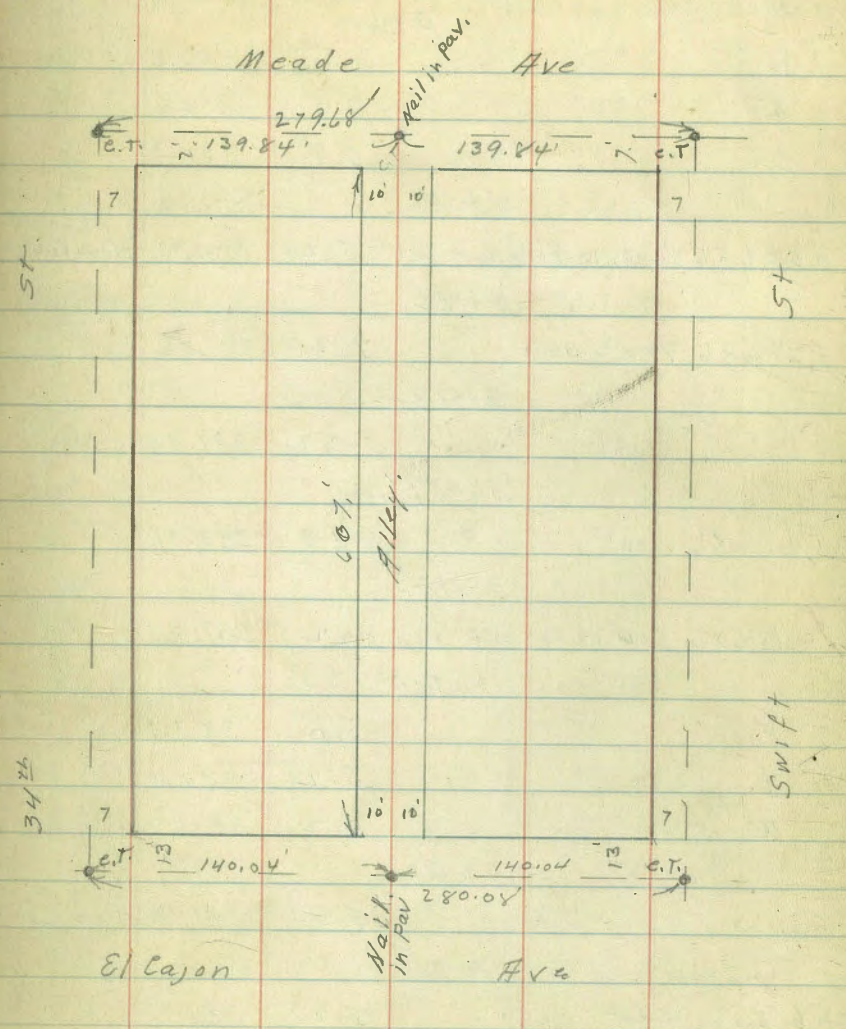
6-28-34  
Miller  
Walker  
Bliss

X See Alley B.K.C. Sterling Worth  
El Cajon to Meade bet  
34th & Swift.

Indexed  
C.S.K.

53

BM.BP.	7.79	387.06	379.27	s.w. Swift + El Cajon
25' S. of N. line El Cajon = N. cl. Line				
E-25 gutter	7.26	379.80		
E-25 ent. cl.	6.72	380.34		
E. " "	6.61	380.45		
E gutter	7.25	379.81		
♀ " "	7.27	379.79		
W " "	7.29	379.77		
W ent. cl.	6.75	380.31		
W+25 " "	6.91	380.15		
W+25 Gutter	7.32	379.74		
0+00 = N. line El Cajon.				
W. = N. End: ent. cl.	6.46	380.60		
W. N end pay	6.56	380.50		
♀ " "	6.82	380.24		
E. = N. End. "	6.67	380.39		
E. " " ent. cl.	6.49	380.57		
0+20' N				
E	6.2	380.9		
♀	6.0	381.1		
W.	6.0	381.1		
W. floor of office	5.77	381.29		





387.06

0+60

W	5.5	381.6
φ	5.5	381.6
E	5.8	381.3

0+76.

Fl. 6" X 6" Vent. in Building on W.	5.20	381.86	= Floor of cleaning shop
-------------------------------------	------	--------	--------------------------

0+82

Fl. 6" X 6" Vent. on W.	5.20	381.86	"
-------------------------	------	--------	---

0+88<sup>5</sup>

Fl. 6" X 6" Vent.	5.22	381.84	"
-------------------	------	--------	---

0+89<sup>7</sup>

Fl. 6" X 6" Vent.	5.20	381.86	"
-------------------	------	--------	---

0+95<sup>5</sup>

Fl. 6" X 6" Vent.	5.22	381.84	"
-------------------	------	--------	---

1+00 N

E	5.0	382.1	"
---	-----	-------	---

φ	5.2	381.9	"
---	-----	-------	---

W	5.2	381.9	"
---	-----	-------	---

1+01

Fl. 6" X 6" Vent.	5.24	381.82	Floor of shop
-------------------	------	--------	---------------

1+06<sup>5</sup>

Fl. 6" X 6" Vent.	5.21	381.85	" " "
-------------------	------	--------	-------

1+08 S. End. cmt. Drive on W.

W. on cmt. Drive	5.02	382.04
------------------	------	--------

W+0.6 " " "	5.34	381.72
-------------	------	--------

1+20 N. End. above Drive.

W. on cmt. Drive	5.05	382.01
------------------	------	--------

W+0.6	5.34	381.72
-------	------	--------

387.06

Alley BIK C. Sterlingworth

54

1+50 N = S. End. 4. Garages on E cmt floor 4.0 Back

W.	4.5	382.6
----	-----	-------

φ	4.8	382.3
---	-----	-------

E.	4.5	382.6
----	-----	-------

E + 4.0 = floor	4.25	382.81
-----------------	------	--------

1+82<sup>5</sup> = N. End. above 4. garages. on E.

E - 4.0 = floor	4.06	383.00
-----------------	------	--------

2+00

E.	3.8	383.3
----	-----	-------

φ	4.2	382.9
---	-----	-------

W.	4.5	382.6
----	-----	-------

2+50

W	4.2	382.9
---	-----	-------

φ	4.2	382.9
---	-----	-------

E	3.9	383.2
---	-----	-------

3+00

E.	3.7	383.4
----	-----	-------

φ	4.0	383.1
---	-----	-------

W.	3.9	383.2
----	-----	-------

3+04 to 3+47

Picket Fence on W. 0.8 in Alley

3+50

W.	3.3	383.8
----	-----	-------

φ	3.9	383.2
---	-----	-------

E	3.7	383.4
---	-----	-------

387.06

4700

E 3.0 384.1

E 3.1 384.0

W 3.1 384.0

T.P. 7.45 391.44 3.07 383.99

4450

W 6.7 384.7

E 6.8 384.6

E 6.7 384.7

5+00

E 5.95 385.49

E 6.1 385.3

W 6.0 385.4

5+10 E Double Garage on E. emt. floor R. 5' Back

5.76 385.68

E+2.5 = garage + floor 5.73 385.71

5+50

W 5.4 386.0

E 5.4 386.0

E 5.6 385.8

5+68 garage on W. emt floor 1.7 Back

W+1.7 = floor 4.40 387.04

5+95

E 5.0 386.4

E 5.0 386.4

W 5.0 386.4

391.44

Alley BIK. C. Sterlingworth.

55

6707 = S. line Meade

0.5 E. of W. Line = emt. el 5.36 386.08

0.5 E. " " = parmt 5.51 385.93

E " " 5.66 385.78

0.3 E. of E. Line " 5.40 386.04

0.3 E. of E. Line = emt. el 5.20 386.24

12. N. of S. Line = S. el. Line

E-25 gutter 5.87 385.57

E-25 emt. el. 5.22 386.22

E. emt. el 5.40 386.04

E. gutter 5.99 385.45

E " 6.05 385.39

W. " 6.21 385.23

W. emt. el 5.65 385.79

W+20 on emt. el. 5.80 385.64

W+20 gutter 6.50 384.94

T.P. 2.07 385.40 8.11 383.33

orig BM. 6.14 379.26 = 379.27

6-28-34 X. See Alley B1K. 28, Sob of Blks K & L Teratta  
 Miller Walker El Cajon to Orange bet. 40<sup>th</sup> & Central.  
 Bliss

Indexed  
 c.s.K.

See profile 2194  
 Grade established 6-16-25

B.M.B.P. 4.16.37 0.82 364.66 s.w. El Cajon + Central

20' N. of S. Line - s. ch. line of El Cajon

25' e. of E. Line	Gutter	6.35	364.47
25' " " "	emt. ch.	5.75	365.07
E. Line	" "	5.65	365.17
" "	Gutter	6.17	364.65
⊕	" "	6.19	364.63
W. line	" "	6.17	364.65
" "	emt. ch.	5.51	365.31
25' W. of W. line	" "	5.46	365.36
25' " " "	Gutter	6.07	364.75

0+00 = S. Line El Cajon

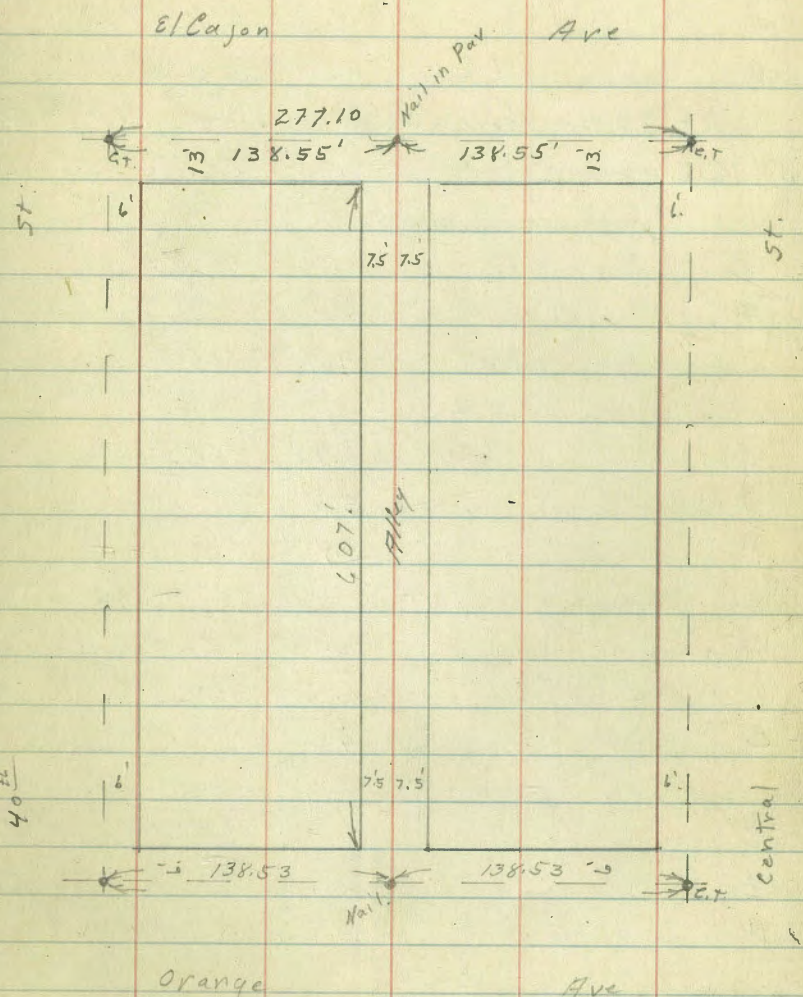
W. emt. ch.	5.27	365.55
W. Gutter Pav	5.41	365.41
⊕	5.69	365.13
E. gutter pav.	5.55	365.27
E. emt. ch.	5.43	365.39

0+08 S.

E	3.9	366.9
+B	5.2	365.6
⊕	5.3	365.5
W.	4.9	365.9

0+30

W.	4.3	366.5
⊕	4.6	366.2
E.	4.3	366.5



370.82

0+50

E 4.5 366.3

E 4.5 366.3

W 4.5 366.3

0+93 = Garage on W. drvt. floor 18.8' Back.

W-18.8 = floor 4.0 366.8

1+00.

W. 4.1 366.7

E 4.1 366.7

E 4.1 366.7

1+50

E 3.9 366.9

E 3.8 367.0

W 3.7 367.1

1+80

W 3.4 367.4

E 3.5 367.3

E 4.0 366.8

2+00

E 3.7 367.1

E 3.9 366.9

W 3.7 367.1

2+50

W 4.3 366.5

E 4.2 366.6

E 4.1 366.7

Alley Blk. 28

57

370.82

2+75

E 4.4 366.4

E 4.5 366.3

W 4.6 366.2

3+00

W. 4.7 366.1

E 4.7 366.1

E 4.3 366.5

T.P. 4.05 370.37 4.50 366.32

3+06 E emt. walk 0.5 W. of W. Line

W-0.5 emt. walk 4.07 366.30

3+50

E 3.9 366.5

E 4.2 366.2

W 4.1 366.3

4+00

W 4.4 366.0

E 4.5 365.9

E 4.3 366.1

4+50

E 4.0 366.4

E 4.4 366.0

W 4.5 365.9

370.37

5+07E {N. End. Existing cmt. Pavmt. Very Poor Condition  
N. End. 6. Garages on E. cmt. floors 4' Back.

W. N. End. Pavmt. 5.10 365.27

☿ " " " 5.35 365.02

E. " " " 4.94 365.43

E+4. = floor 4.42 365.95

5+41=☿ Double Garage on W. dirt floor 8.3' Back

E-4. floor 4.41 365.96

E. pavmt. 5.09 365.28

☿ " " 5.41 364.96

W. = W. edge Pavmt. 5.19 365.18

W.+4.8' = floor. 4.8 365.6

5+62 = S. End. 6. Garages on E.

W. = W. edge pav. 5.30 365.07

☿ pav. 5.55 364.82

E. " " 5.13 365.24

E+4. = floor 4.43 365.94

6+07' = {S. End. Ex. Pavmt.  
N. line. Orange Avc.

E. = N. End. cmt. cl. 5.85 364.52

E = S. " " pav. 5.99 364.38

☿ = " " " " 6.25 364.12

W = {N. " " " cl. } 6.04 364.31

14' S. of N. line = N. cl. line of orange

W. dirt gutter 6.6 363.8

W. cmt. cl. 6.27 364.10

☿ 6.8 363.6

E. Dirt. Gutter 6.7 363.7

E. cmt. cl. 6.23 364.14

Alley BIK.

58

370.37

T.P. 4.91 371.23 4.05 366.32

chk. orig. BM. 6.57 364.66 ✓

7-31-31  
Moore

Grade stakes  
along BIK C Sterlingworth  
El Cajon to 200 N.

	W	E
N. El Cajon +00	380.50	380.33
0 + 20 Break	380.99	380.96
0 + 40 "	381.24	381.24
0 + 50	381.53	381.53
1 + 20	381.84	381.84
1 + 60	382.11	382.11
2 + 00	382.40	382.40

379.27 SW Swift  
381.14 El Cajon  
387.41

59

W 80.40 80.99 81.24 81.53 81.82  
 $\frac{1.91}{}$   $\frac{0.27}{}$   $\frac{6.77}{}$   $\frac{5.88}{}$   $\frac{5.59}{}$   
 $+0.36$   $+1.0$   $+1.0$   $+0.17$

E 80.33 80.96 81.24 81.53 81.82  
 $\frac{7.03}{}$   $\frac{0.27}{}$   $\frac{6.17}{}$   $\frac{5.88}{}$   $\frac{5.59}{}$   
 $-0.37$   $-0.46$   $-0.22$   $+0.14$

W 82.11 82.40  
 $\frac{1.30}{}$   $\frac{1.01}{}$   
 $+0.20$   $+0.20$

E 82.11 82.40  
 $\frac{1.30}{}$   $\frac{1.01}{}$   
 $+0.70$   $+0.33$



0+43.3 ✓		
W	7.7	343.8
C	8.1	343.4
+7	8.4	343.1
E = NW Cor Studio Store	9.9	341.6
+10	9.9	341.6
0+60 ✓ sly edge 5' wide cem steps		
-10	9.1	342.4
E	8.1	343.4
+3	6.2	345.3
C	6.3	345.2
W NE Cor end of Top of cem steps 5' wide	5.8	345.63
+5.5 bot " "	9.8	341.63
0+75 ✓		
W	5.3	346.2
C	5.5	346.5
E	5.1	346.4
0+89		
W - 32 double gar divi floor	4.9	346.6
1+07 ✓		
E	4.9	346.6
C	5.1	346.4
W	5.2	346.3
+10 simple gar cem floor	5.01	346.46

1+30 ✓		
W	5.0	346.5
C	4.9	346.6
E	4.8	346.7
1+54 ✓		
E	4.6	346.9
C	4.9	346.6
W cem door step	4.57	346.90
1+73.5 ✓ ledge 5' wide		
W + 0.5 cem walk	4.53	346.94
W + 0.6 dirt	4.7	346.8
C	4.8	346.7
E	4.5	347.0
+1 ledge cem floor No garage	4.42	347.05
2+00 ✓		
E-1 ledge of above	4.45	347.02
E	4.6	346.9
C	5.0	346.5
W	4.7	346.8
2+40 ✓		
-1 NE cor average cem floor 28' wide	4.92	346.55 wly entrance
W	5.5	346.0
C	5.5	346.0
E & approx double cem gar floor level	5.18	346.29
+2	5.18	346.29



2+70 ✓

E	6.1	345.4
C	5.7	345.8
W	5.6	345.9

2+90 ✓  
 2 double for <sup>cont</sup> floor level

-5	5.5	345.94
W	6.2	345.3
C	6.5	345.0
E	6.4	345.1

3+25 ✓

E-4	9.8	341.7
E	8.8	342.7
C	7.9	343.6
W	7.1	344.4

T.T. 400 346.43 964 341.83

3+50 ✓

W	4.4	342.0
C Top S.M.H.	5.21	341.22
E	6.5	339.9
+5	7.7	338.7

3+75 ✓

-10	10.0	336.4
E	9.0	337.4
C	7.7	338.7

W 4+00 ✓

W	7.4	339.0
W	9.2	337.2
C	10.0	336.4

+9 & 12 shed  
 E+10  
 + 25 House Gess pool  
 4+25 ✓

+9 & 12 shed	10.9	335.5
E+10	11.7	334.7
+ 25 House Gess pool	11.5	333.9

No Sewer Connection

-10  
 E  
 +6  
 C  
 W  
 +5  
 4+50 ✓

-10	13.9	332.5
E	12.9	333.5
+6	10.7	335.7
C	10.2	336.1
W	9.9	336.5
+5	9.5	336.9

-10  
 W  
 C  
 +3  
 E  
 +15  
 4+70 ✓

-10	9.3	337.1
W	10.8	335.6
C	11.4	335.0
+3	11.6	334.8
E	14.2	332.2
+15	14.8	331.6

-15  
 E  
 +6  
 C

-15	13.1	333.3
E	12.6	335.8
+6	10.0	336.4
C	10.4	336.0

C + v	9.0	337.4
W	9.2	337.2
+v	8.5	337.9
4 + 80 ✓		
-v	7.6	338.8
W	7.8	338.6
C	8.0	338.4
E	8.7	337.7
+v	8.4	337.8
✓ + 100 ✓		
-v	7.3	339.1
E	7.7	338.7
C	7.2	339.2
W	7.1	339.3
+1 SE Cor garage Top Conc. foundation	5.78	340.65
✓ + 10 ✓		
W	6.7	339.7
+3	5.1	341.3
C	5.2	341.0
+v	7.9	339.1
E	6.7	339.7
✓ + 20 ✓		
E	4.4	342.0
C	4.6	341.8
W	6.1	340.3

NE Cor garage drift box	✓ + 30 ✓		
-1 Top <sup>conc.</sup> foundation gar.	5.49	340.94	North entrance
W	6.1	340.3	
C	4.5	341.9	
E	4.4	342.0	
✓ + 50 ✓			
E	3.8	342.6	
C	4.6	341.8	
W	5.4	341.0	
+5	5.3	341.1	
✓ + 75 ✓			
W	4.1	342.3	
C	3.2	343.2	
E	3.2	343.1	
✓ + 95 ✓			
E	3.2	343.2	
C	3.6	342.8	
W	3.7	342.7	
✓ + 99.3 SL Polk			
W Top et	3.69	342.74	
W par	4.05	342.38	
C "	3.96	342.47	
E "	3.71	342.72	
E Top et	3.35	343.08	
SL Polk + 6.5			
E par	3.86	342.57	SE line Polk

346.43

64

C pay

406

342.37

w/ "

425

342.18

T.P.

667

344.31

879

337.64

check to BM

361

340.70

340.68

0.02

Xsec alley 15' wide  
 Bk 3 Ocean Beach Park  
 S.S. Cliff Blvd & Ebor  
 Long Branch & Brighton

Moore  
 Oct. 1934

Indexed  
 C.S.K.

31.83

65

SW 7' 07	5.92	31.83	25.91	Long Branch S. S. Cliff H. B.
0+00 = Ely - Sunset Cliff Blvd.				
N Top of	5.49	26.34		
N Pav.	5.63	26.20		
E "	5.98	25.85		
S "	5.67	26.18		
S Top of	5.51	26.32		
0+20				
S	4.3	27.5		
C	4.6	27.2		
N	4.5	27.3		
0+34				
N	4.2	27.6		
C	4.4	27.4		
S	4.1	27.7		
+5 Sin Car. dirt floor	4.0	27.8		
0+46				
N	4.1	27.7		
+4.5 Sin gar dirt "	3.9	27.9		
0+57				
S	3.8	28.0		
C	4.1	27.7		
N Sin gar dirt floor ON LINE	4.2	27.6		

0+69				
N			3.9	27.9
C			3.8	28.0
S			3.7	28.1
+1 Sin. gar. dirt floor			3.8	28.0
0+86				
-2 Sin. gar. cement floor			2.85	28.98
S " " Hipod cement			3.34	28.51
C			4.6	28.2
N			3.6	28.2
T.P	4.03	33.84	20.7	29.81
1+11				
N - 10.3 double gar.			4.95	28.89
N			5.4	28.4
C			5.5	28.3
S			5.2	28.6
1+23				
S - 1.5 Sin. gar. Cement floor			4.92	28.92
S Cement Apron			5.79	28.55
C			5.5	28.3
N			5.4	28.4
1+49				
N			5.1	28.7
-7 Sin gar. dirt floor			5.1	28.7

J	1796	J.0	28.8
C		J.0	28.8
N		J.0	28.8
	+5.5 Six gar. dirt floor	5.1	28.7
	2+50		
N		4.8	29.0
C		4.8	29.0
J		4.7	29.1
	2+81		
-8	Six gar. Com foundation	4.49	29.35
S		4.7	29.1
-C		4.9	28.9
N		4.8	29.0
	3+00		
C	11.4 RIM	4.55	29.29
	3+13		
N		4.4	29.4
C		4.6	29.2
S		4.8	29.0
	+5.5 Six gar. com. floor	4.73	29.11
	3+25		
S	+1.5 fence in alley		
	3+50		
J		4.5	29.34

	+1.5 fence in alley		
C		4.5	29.3
N		4.4	29.4
	4+06		
N		4.1	29.7
C		4.1	29.7
J		4.1	29.7
	+4.5 Six gar. dirt floor	4.1	29.7
	T.P. 8.89 38.92 3.81	3.003	
	4+50		
J		8.8	30.1
C		8.9	30.0
N		9.0	29.9
	+6 Six gar Com floor	8.83	30.09
	4+58		
N		8.4	30.5
C		8.5	30.4
J	Com H/pan	8.10	30.82
	+2.5 Six gar. Com floor	8.01	30.91
	5+00		
J		7.5	31.4
C		7.6	31.3
N		7.4	31.5
	5+30		
N		6.5	32.4

C	6.9	32.0
S	6.8	32.1

√+VV

S	5.6	33.3
C	5.7	33.2
N	5.8	33.1
+6 S.W. cor. dirt floor	5.6	33.3

√+50

N	5.1	33.8
C	5.0	33.9
S	4.7	34.2

6+00 - w/ly Ebers

S Top ob	5.25	33.67
S part	5.64	33.28
C "	5.99	32.93
N "	5.64	33.28
N Top ob	5.44	33.48

J.P.	2.58	33.11	8.39	30.53
------	------	-------	------	-------

in to BM	7.21	25.90	25.91
----------	------	-------	-------

SW 7' CT  
 Long branch  
 S. Setchiff #2

Moore  
3-2-36

X SEC Alleys 15' wide  
BIK 24 Normal HTS

Indexed  
G.S.K.

68

SEBP 668 396.70 390.07

Adams &  
Wilson

Collier NOT PAVED

ST.

E & W alley xsec.

0-12

N pav. & cur. of 35th 5.23 391.52

C 5.20 391.58

S 5.21 391.54

00

S pav. 4.75 392.00

C " 4.98 391.97

N " 4.73 392.02

0+20

N - 1.5 S edge Conn Dr to W. garage 4.00 392.75

N 4.1 392.7

C 4.3 392.5

S 4.4 392.6

0+50

S 4.0 392.8

C 4.2 392.6

N 4.1 392.7

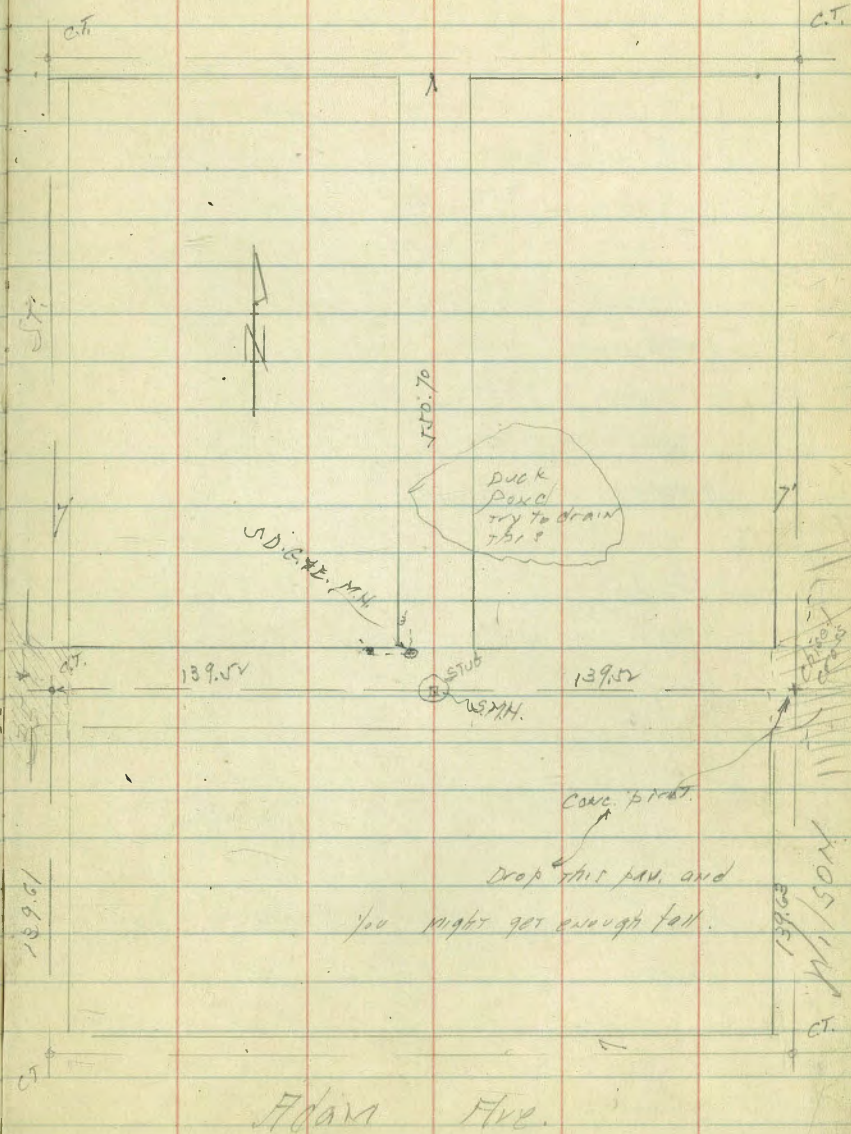
0+77

N - 1.8 above garage 3.82 392.93 18' deep

N 3.9 392.9

C 4.1 392.7

S 3.7 393.1



	1+00		
S		4.4	392.4
C		4.7	392.1
N		4.5	392.3
	1+25 = WL Nalley		
N		5.1	391.7
C		5.3	391.4
S		5.3	391.4
	1+28		
	1/2 N of C = Gas. Co. M.H.	5.38	391.37
	1+32.5 = WL Nalley		
S	ground	5.6	391.2
C	"	5.2	391.6
C	S.M.H. Fin	6.7	390.68
N	ground	5.3	391.5
	1+40.0 = EL Nalley		
N		5.2	391.6
C		5.4	391.4
S		5.5	391.3
	1+59		
S-1	= EL Wood Car. 10' wide	5.00	391.75
S	ground	5.4	391.4
C	"	5.1	391.7
N	"	5.2	391.6
	2+00		
N		4.8	392.0

S of face

S entrance  
con floor

C		5.0	391.8
S		4.7	392.1
	2+45		
S		5.0	391.8
C		5.0	391.8
N		4.9	391.9
	2+45.0 = WL Nalley		
N	00	5.66	391.09
N	par Conc.	5.79	390.96
C	"	6.00	390.25
S	"	5.73	391.02
S		5.60	391.15
	2+77.04 W gutter		
S	par	6.36	390.39
C	"	6.36	390.39
N	"	6.39	390.36
N	+100' par. fut.	6.07	390.68
	50' S of SL alley	6.52	390.22
	N + S alley x sec		
	00 = WL of E + W alley		
	0+50		
E		5.3	391.5
C		5.5	391.3
W		5.2	391.6



	1+00			
W		5.3	391.5	
C	= duck pond	5.6	391.2	
E		5.7	391.1	
	1+25			
E		5.6	391.2	
C	= duck pond	5.7	391.1	
W		5.7	391.1	
	1+50			
T.P.	7.0	398.19	5.66	391.09
W	Sedge Cem Apron		6.80	391.39
C			6.8	391.4
E			6.9	391.3
	1+70			
E		6.8	391.4	
C	Double Gar. Cem floor same El. 2' back	6.8	391.7	
W	S edge apron 2017	6.80	391.39	
	2+00			
W		6.4	391.8	
C		6.4	391.8	
E		6.3	391.9	
	2+50			
E		6.5	391.7	
C		6.0	392.2	
W		6.2	392.0	

	3+09			
W		4.9	393.3	
C		4.7	393.5	
E		4.7	393.5	
	+1.3 Cem. Apron 10' wide	4.71	393.48	
	+1.4 Gar. Cem floor	4.5	393.57	
	3+50			
E		5.0	393.2	
C		4.9	393.3	
W	Shed - alley 1.4	5.0	393.2	S.V. 14' long
	4+00			
W	Woodshed 1.4 in alley	4.6	393.6	8' wide
C		4.5	393.7	
E		4.6	393.6	
	4+50			
E		4.4	393.8	
C		3.7	394.5	
W		3.6	394.6	
	5+06			
W	19' Sing. gar. Cem floor	3.05	395.14	
W		3.2	394.9	
C		3.4	394.8	
E		3.5	394.7	
	+1.2 Singar dirt floor	3.8	394.4	

398.19

VTSV

E	4.2	394.10
E	4.0	394.2
W.	3.9	394.3
√+50.70 S.L. Collier Not Aired.		
W curb	4.54	393.65
W dirt	4.5	393.7
C "	4.61	393.6
E "	4.6	393.6
E cb	4.67	393.52

T.P.	3.94	396.90	5.23	392.96
------	------	--------	------	--------

√+62.70 = S curb Collier

EV. 35th Sub Collier Top cb	3.20	393.60	
" " " gut. pav.	3.52	393.38	
W.L. alley Top cb	3.85	393.05	S curb Collier
	4.3	392.60	
EL alley Top Collier	3.73	393.17	
	4.3	392.60	
W.L. Wilson Sub Collier	4.24	392.66	
dirt	4.6	392.30	
w cb Wilson S.L. Collier			
Top cb	4.16	392.24	
pav. gut. cent.	4.75	392.15	

71

396.90

T.P.	3.16	395.04	5.02	391.88
------	------	--------	------	--------

Ch. to BYT	adams wilson	4.98	390.06	390.07
------------	-----------------	------	--------	--------

5 floors  
5-17-97. Alley 15' wide  
Blk 96 Ocean Bay Beach

INDEXED  
C.S.M.

7.13

72

Dir	St. No.	Dist	Area	Notes	St. No.	Dist	Area
NW	5.19	713	1.94	Main Abbott	C		5.0
	wly Abbott = 00				S		5.5
S	Top cb	4.76	2.37				1.5
S	par	5.09	2.04				1.6
C	"	5.35	1.78				2.0
N	"	5.10	2.03				2.1
N	Top cb	4.77	2.36				2.3
	0 + 25				T.P.	4.25	7.25
N		4.7	2.4				2.10
C		4.9	2.2				3.00
S		4.7	2.4				
	0 + 69						
S		5.5	1.6				2.9
C		5.5	1.6				2.9
N	wly side of Gar. W. entrance	5.3	1.8	dist floor			2.9
	0 + 84						
N		5.4	1.9				2.9
C		5.3	1.8				2.9
S	Ely side of Gar. E. entrance	5.3	1.8	" "			2.9
	1 + 06						
S		5.7	1.4				2.9
C		5.8	1.3				2.9
N	Ely side Gar. "	5.4	1.7	" "			2.9
	1 + 50						
N		5.4	1.7				2.9

2 + 00

? 3 + 35 = beg. of sand

2 + 61

S E door floor E. Dwelling 2.0

+1 5.7 2.1

C 5.4 1.9

N 5.4 1.9

3 + 00 N 5.7 1.6

C 4.4 2.7

S 4.4 2.9

3 + 29 S 3.7 4.1

C 4.3 4.0

if possible  
make grade  
of alley  
3" below  
floor of  
dwelling

N		5.6	1.7	
+0.2	floor El. Dwelling	4.77	3.48	W.L. of 50' Long
+6.2	foundation	5.40	1.85	Dwelling
	3+50			

N		2.0	5.3
C		2.2	5.1
S		2.0	5.3

3+60 Top Sand Hill

S		2.0	5.3
C		1.5	5.8
N		2.0	5.3

3+75

N		2.0	3.3
C		4.2	3.1
S		2.5	3.8

3+92.0 = Ely W. Pittsford Ave.

S		5.8	1.5
C		5.8	1.5
N		5.8	1.5

T.P. 5.08 7.23 5.10 2.15

check back 5.28 1.95 1.94

Norel alley to be graded by St. Dept.

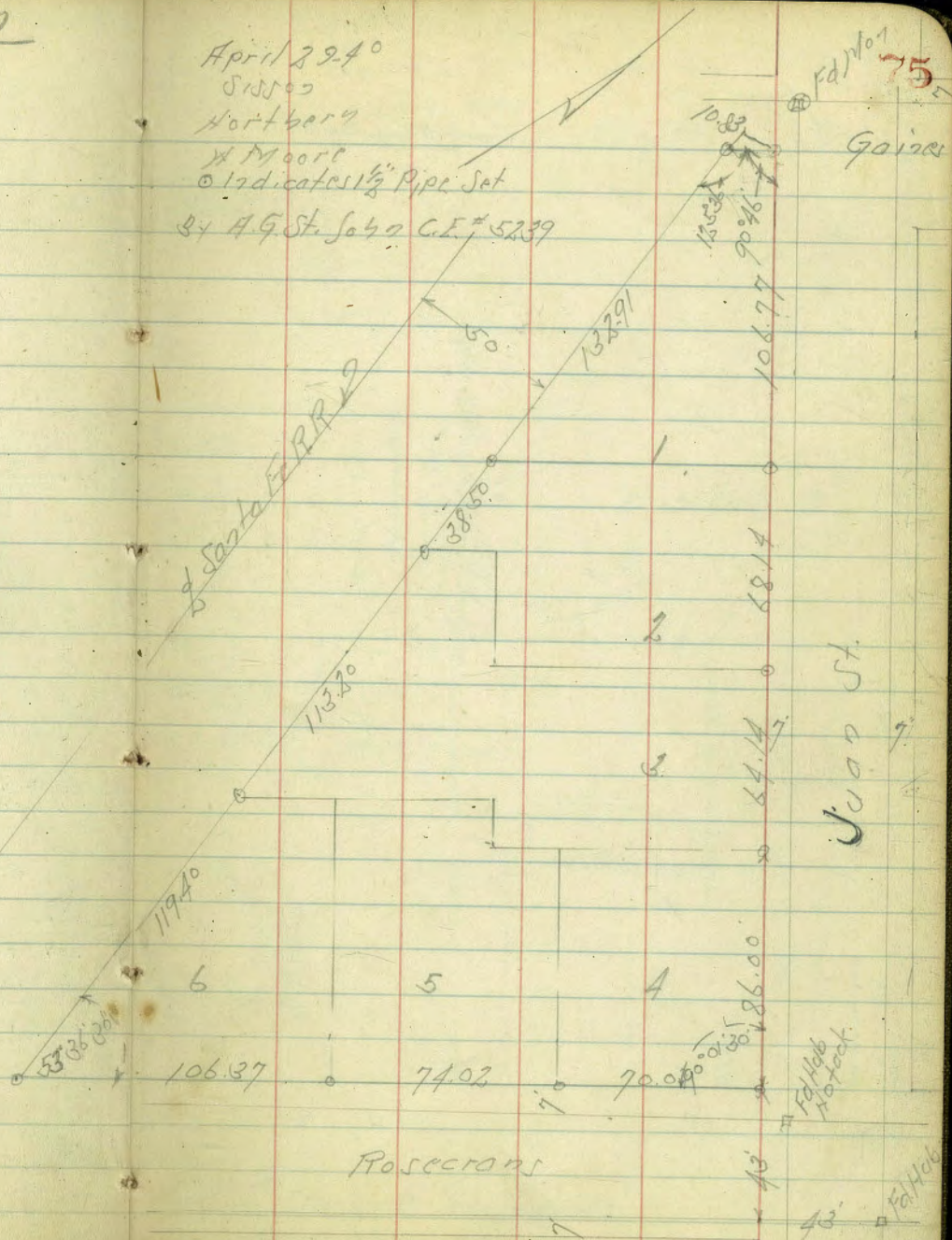


Juan Street Addition  
Check Survey

INDEXED  
E.F.B.

April 29, 40  
S.W.S.  
Northberry  
H. Moore  
Indicates 1 1/2" Pipe Set  
By A.G. St. John C.E.# 5239

Ed No 75  
Gaines





1+45.5 Nodge Pav

1+38 on Pav

1+15.3 ledge paving

T.P. 7.04 58.84 7.47 51.80

1+10.32

0+65.32

0+50

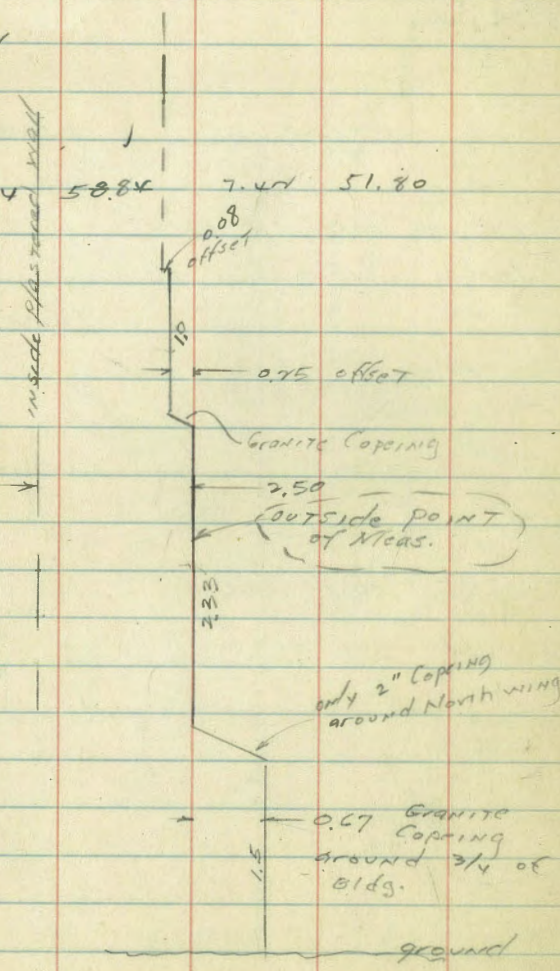
0+25

0+00

0-14 Top Curb

NWBP 2.67 59.22

56.55 9<sup>th</sup> + E St.  
CITY  
DATUM



Top of

(53.36)	(53.63)	(53.99)	(54.40)	(54.81)
5.28	5.21	4.85	4.40	4.62
		30	20	100

gutter & drive

(52.92)	(53.31)	(53.47)	(53.74)	(54.17)	(54.53)
6.42	5.53	5.37	5.10	4.67	4.31
	7.35		30	60	100

(53.0)	(53.78)	(54.37)	(54.69)	(54.99)
5.8	5.10	4.47	4.15	3.85
		20	5.4	77

58.84

(52.66)	(53.0)	(53.2)	(54.7)
6.56	6.2	5.0	4.5
14		30	5.41 NW corner W. wing

(51.7)	(52.1)	(52.9)	(52.9)
7.51	7.1	5.2	4.3
14		30	55.45 SW corner W. wing

(51.40)	(51.8)	(52.6)	(52.90)
7.87	7.4	4.6	4.34
14		50	87

(50.83)	(51.2)	(52.0)	(52.67)
8.23	7.8	5.2	4.55
14		50	100

(50.33)	(50.78)	(51.3)	(52.78)
8.89	8.49	6.9	5.44
14		50	100

(50.40)	(51.86)	(52.47)
8.87	7.36	5.75
	50	100

59.22

Levels Reduced. 1-6-92.



Levels S.D. Public Library

1-2-47.

See last page for floor pl.

1+50

1+28

1+10.40

0+65.4

0+50

0+25

0+00

0-14

Orig. B.M. P77

5.87

6.24

54.55

L.T.

"B"

PT.

curb

78

(55.67)	(55.9)	(57.6)	(58.54)	(58.19)
6.75	6.5	4.8	3.90	4.23
50	26	24		74
PAV	PAV			

(59.97)	(55.82)	(56.9)	(57.8)
7.45	6.60	5.5	4.6
50	255	24	
	PAV		

(59.97)	(54.47)	(55.45)	(56.16)	(57.80)	(57.36)
7.45	7.45	6.97	6.26	4.62	5.06
77x3	55x3	30 PAV.	15 PAV	70x	14 = gutter in Drive
PAV.	PAV				
NCCOR E WING					

(56.92)	(55.50)	(57.0)	(57.9)	(57.22)
7.50	6.92	5.4	5.0	5.20
55.8x	41	7		74
WALK SECOR E. WING				

(59.90)	(55.7)	(57.2)	(57.10)
7.54	7.2	5.2	5.22
50	25		14
WALK			

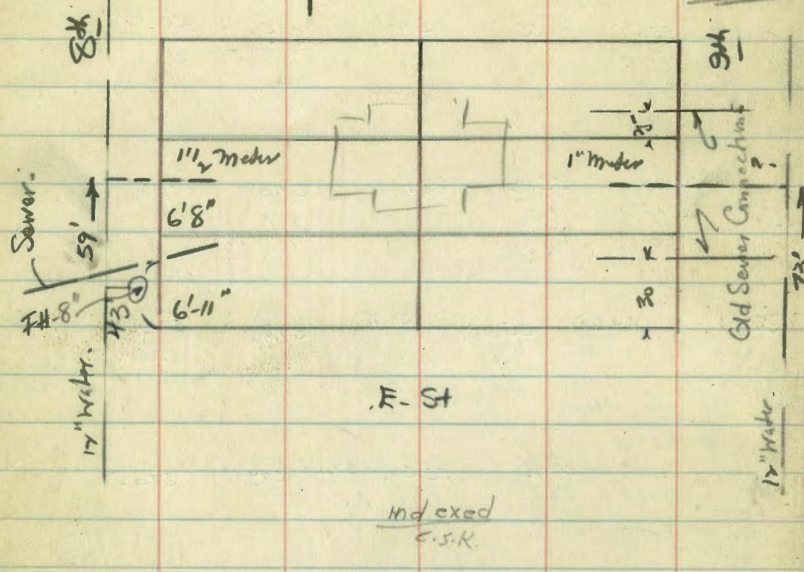
(55.3)	(56.2)	(57.0)	(56.88)
7.1	6.0	5.1	5.57
50	25		74

(59.92)	(56.83)	(56.51)
7.5	5.59	5.91 curb
50		74

(59.92)	(56.98)
7.50	5.94 curb
50	

6.24 ✓

Sewer & Water Books -  
#1-N  
Pg. 70



71-54

Indexed  
C.S.R.

385.84

79

E. Line Ill Topch	3.83	382.01
25' E. of the E. Line Ill in Gutter	4.37	381.47
Sec B N. Line of Meade & Ill.		
E. Prop. on Ground	3.4	382.4
E. Topch	3.80	382.04
W. Gutter	4.32	381.52
W. 1/4	4.27	381.50
W. 1/4	4.47	381.20
W. 1/4	4.66	381.18
W. Gutter	5.11	380.63
W. Topch	4.71	381.13
W. Line	4.4	381.4
TP	1.28	379.35
TP	0.51	368.22

See Book #1281-32

X Sections Meade & Illinois  
Towa + Meade

BM	262	385.84	383.22	SEBP
	225	386.09	370.52	Ohio + Meade
				BM
				TP in
				BM
				TP
				Char BM
				BM
				Topch NE Rio

Sec A N. cb Line Illinois Meade				
Gutter 25' W. W. Line Ill.	5.99	379.85	6.84	369.94
W. Line Ill in Gutter	5.40	380.44	6.49	376.13
W. Line Ill Topch	4.78	381.06		
W. cb Line Ill	5.14	380.70		
W. 1/4	4.86	380.98		
W. 1/4	4.60	381.24		
W. 1/4	4.43	381.41		
E. cb	4.54	381.30		
E. Line Ill in Gutter	4.37	381.47		

SEBP Ill +  
Record  
SE Ohio  
1 E. Capin. B.P.  
363.10 Record - Corrected  
To BM  
SEBP  
Ohio Meade  
373.52 Record

See FB 1285 P 32

N.W. Towan Meade

1-2-40

Library Floor Elev.

H.I. FROM P. 77

59.22 ✓

El. of 1 <sup>ST</sup> floor	0.32	58.90	✓
" " 2 <sup>nd</sup> "	+12.89	72.11	✓
" " fl. Basement <sup>MENS REST ROOM</sup>	11.50	47.70	✓
" " " Cent. fl. <sup>outside</sup> REST ROOM	11.87	47.35	✓
TOP 10" Lightwell Coping	3.99	55.23	
Bot. " " on west	7.04	52.18	

58.80 = H.I. P 77

El. Fl. Basement <sup>N. WING</sup>	11.20	47.60	✓
-------------------------------------	-------	-------	---

S.E. Cor. Carnegie Bldg - 0+0 0.09 back

0+50 on line

0+90 " "

1+00 S.E. Cor. Bldg Theatre <sup>Bldg.</sup> 0.00 over

1+50 on line

2+00 E.L. 8th St. Car " on line

Window sills on Carnegie apt extend over an average of 0.10

Bdry. Theatre Bldg at Tule Crossg. or South reinforced by 4"x6" which are over.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1%. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

from side stake to slope stake. If ground is not

IMPROVED TABLES

AND

INFORMATION

To find Target and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given 1 meter found by dividing tangent (or external), opposite, by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

El Cajon  
(Cactin) 63<sup>rd</sup> N.W. BP. 465.66

31.12

26.3  
7.5  
18.8

24.5

164.27  
1542.7

55.43  
21.8  
77.23

554.25  
10.85  
5.41  
16.3

2555.10  
832.10  
3387.20

15

0.3 West  
30.015