

1503

DEPT

LEVEL BOOK

No. 389F

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DEC 24 1964

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
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See ~~Map~~ on E. Side.
 Mt. View Park West of
 old City Boundary. 20' Wide
 Boundary St.

6-21-34
 Miller
 Walker
 Blass
 N.W. Hoth
 + Ocean View Blvd.

B.M. 7. C.T. 0.57 82.75 82.18

± Ocean View Blvd.

-10.43	± Pavmt.	14.44	68.31
E.	" "	14.20	68.55
± Alley	" "	14.09	68.66
W.	on "	13.95	68.80
+10.43	" "	13.83	68.92

10.43' N. = N. Edge Pavmt. Produced West.

-10.43	on Pavmt.	13.93	68.82
W	N. edge Pavmt.	14.08	68.67
± Alley	N. edge Pavmt.	14.17	68.58
E.	" " "	14.30	68.45
+10.43	" " "	14.47	68.28

15' N of ± Parallel to Ocean View

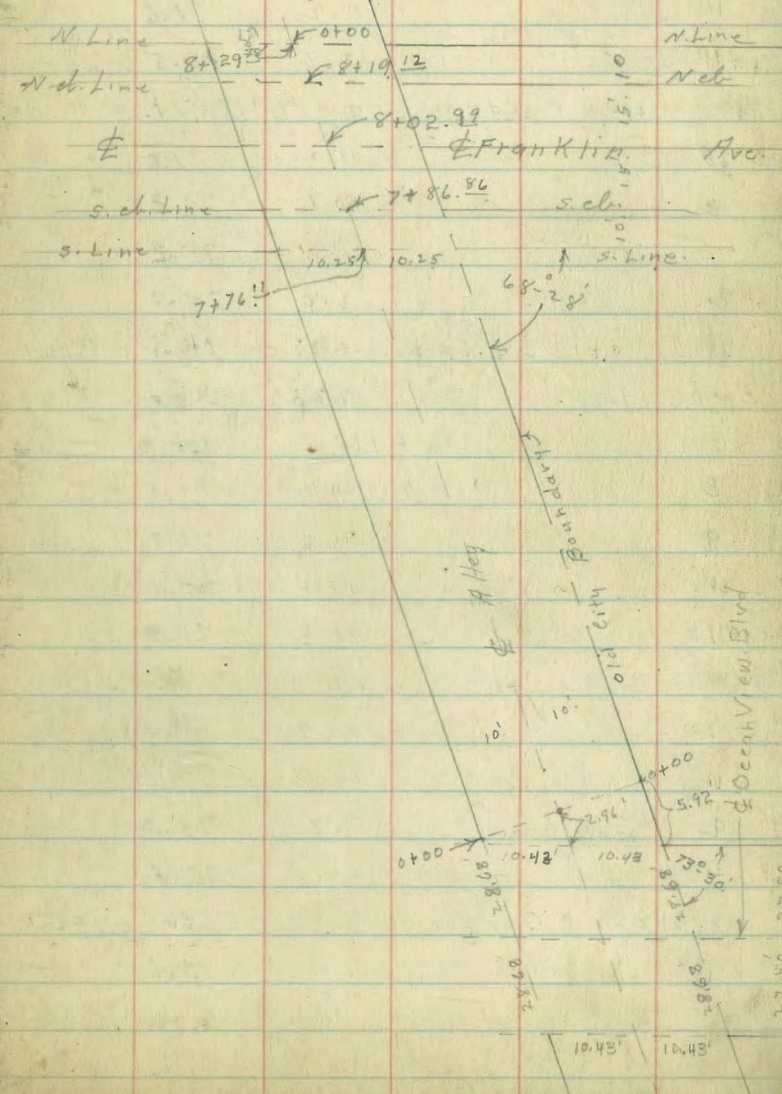
-10.43		14.6	68.2
E		14.5	68.3
±		14.3	68.5
W		14.1	68.7
+10.43		14.0	68.8

20' N. of ± Parallel to Ocean View

-10.43		13.8	69.0
W.		12.3	70.5
±		11.1	71.7
E		14.0	68.8
+10.43		14.0	68.8

Abt 1934

Indexed
 disk
 10.3
 15.
 20
 24.6
 29.
 31.64 = 00



82.75

28.68' N. of ϕ = N. Line Ocean View Blvd

-10.43	10.9	71.9
E	10.9	71.9
ϕ	10.7	72.1
W	11.2	71.6
+10.43	12.3	70.5

31.64 N. of ϕ = 0+00 Plat. Page 1 at 90°-00

W	11.2	71.6
ϕ	10.6	72.2
+5	9.6	73.2
E.	8.0	74.8

0+13 = ϕ Garage on E. cmt. floor 0.8 Back

E - 0.8 floor 8.90 73.85

0+16

E	9.0	73.8
ϕ	9.3	73.5
W.	10.4	72.4
+10	11.3	71.5

0+21

-10	10.9	71.9
W	10.0	72.8
ϕ	7.7	75.1
E	6.4	76.4

0+26 = ϕ Garage on E. Dirt floor 0.6 Back

4.4 76.4

82.75

Atty W. of Old Boundary
Boundary St.

0+40

E	6.1	76.7
ϕ	7.2	75.6
W	8.2	74.6
+10	9.1	73.7

0+71

-10	7.3	75.5
W	5.5	77.3

+8.5 Pepper Tree 18" Diam

ϕ	4.3	78.5
E	3.8	79.0

1+00

E	3.5	79.3
---	-----	------

ϕ	3.7	79.1
--------	-----	------

W	4.2	78.6
---	-----	------

+10	5.6	77.2
-----	-----	------

1+50

-10	4.1	78.7
-----	-----	------

W	3.0	79.8
---	-----	------

ϕ	2.1	80.7
--------	-----	------

+5	1.2	81.6
----	-----	------

E	0.9	81.9
---	-----	------

T.P.	10.93	92.05	1.63	81.12
------	-------	-------	------	-------

2+00

E	6.9	85.2
---	-----	------

ϕ	8.7	83.4
--------	-----	------

W	10.7	81.4
---	------	------

+10	12.2	79.9
-----	------	------

92.05

2+50

-10.	10.3	81.8
W	8.5	83.6
+7	7.8	84.3
±	6.8	85.3
E	5.0	87.1

2+75. Garage on E. line emt. floor.

E Floor.	5.88	86.17
3' W. End. emt. Apron	6.20	85.85

2+88

E	6.2	85.9
±	7.2	84.9
W	9.7	82.4
+10	11.0	81.1

3+00

-10	11.3	80.8
W	10.5	81.6
±	10.0	82.1
E	8.1	84.0

3+25

E	8.0	84.1
+7	7.0	83.1
±	10.1	82.0
W	10.9	81.2
+10	11.5	80.6

3+50 Garage on E. line Dirt. floor.

-10	10.6	81.5
W.	9.8	82.3

92.05

Alley W. of old City Boundary.
Boundary St.

3

±	9.0	83.1
E. floor	8.0	84.1

3+65 Garage on E. line Wooden floor

-0.1	6.7	85.4
E	7.0	85.1
±	8.0	84.1
W.	8.5	83.6
+10.	9.1	83.0

3+96

-10	6.4	85.7
W.	5.5	86.6
±	5.2	86.9
E.	4.5	87.6

4+02

7' E. of ± old Cesspool top. caved in should be filled

4+05

E.	1.4	90.7
±	1.5	90.6
+8	1.9	90.2
W.	2.6	89.5
+3	4.2	87.9
+10	4.7	87.4
T.P.	11.90	102.72
	1.23	90.82

102.72

4+30 Garage on E. Line cmt. floor

E. floor 10.50 92.22

3' W. = End. cmt. apron 10.76 91.96

4+38

-10 10.1 92.6

W 10.7 92.0

Φ 10.6 92.1

E. 10.6 92.1

4+50

E 7.3 95.4

Φ 8.0 94.7

W 8.0 94.7

+10 8.4 94.3

4+65

-10 7.4 95.3

-5 7.0 95.7

W 5.5 97.2

Φ 5.0 97.7

E 5.1 97.6

4+67 Garage on E. cmt. floor 0.3 Back.

E. -0.3 floor 4.70 98.02

4+78

E 4.3 98.4

Φ 4.0 98.7

W 4.1 98.6

+5 6.4 96.3

+10 6.4 96.3

102.72

Alleyway City Boundary
Boundary St.

5+00

5.5 97.2

5.5 97.2

1.9 100.8

1.2 101.5

1.6 101.1

5+50

1.4 101.3

1.3 101.4

1.2 101.5

4.2 98.5

4.2 98.5

6+00

3.6 99.1

3.6 99.1

2.2 100.5

1.0 101.7

0.6 102.1

0.4 102.3

6+35

E. 1.5 101.2

Φ 1.5 101.2

+8 1.6 101.1

W 2.6 100.1

+10 3.0 99.7

102.72

6+60

-10		3.8	98.9
W		4.4	98.3
±		5.7	97.0
E		5.9	96.3
+10		7.7	95.0

6+80

-10	in yard	10.5	92.2
-2	in yard	9.5	93.2
E		7.8	94.9
±		6.2	96.5
W		4.8	97.9
+10		4.4	98.3

6+85

-10		4.4	98.3
W		5.2	97.5
±		6.4	96.3
+4		7.7	95.0
+6		10.4	92.3
E		11.7	91.0
+1	in yard	12.5	90.2
+10	" "	14.5	88.2

6+91

-10	in yard	15.4	87.3
-1	" "	12.4	90.3
E		9.7	93.0
±		7.8	94.9

102.72

Alley W. of old City Boundary
Boundary St 5

W		6.2	96.5	
+10		4.2	98.5	
T.P.	6.08	98.45	10.35	92.37

7+15

-10		7.05	99.0
W		2.0	96.5
±		5.0	93.5
E		7.3	91.2
+1	in yard	9.6	88.9
+10	" "	10.3	88.2

7+55

-10	in yard	12.8	85.7
-2	" "	11.8	86.7
E		9.9	88.6
±		7.5	91.0
W		4.3	94.2
+10		1.2	97.3

7+65

-10		5.5	93.0
W		7.5	91.0
±		9.0	89.5
E		11.0	87.5
+4	in yard	13.3	85.2
+10		13.8	84.7

98.45

7+76 ^u ϕ = S. Line Franklin See on St. Line			
-10.75		15.0	83.5
E		14.4	84.1
ϕ		14.1	84.4
W		13.2	85.3
+10.75		12.3	86.2
ϕ 7+86 ⁸⁴ = S. cl. Line			
-10.75		13.4	85.1
W.		14.2	84.3
ϕ		14.8	83.7
E		15.0	83.5
+3	W. End. cmt. cl.	15.2	83.3
+10.75	" "	15.46	82.99
ϕ 8+02 ²² on ϕ Franklin			
-10.75		15.3	83.2
E		15.0	83.5
ϕ		14.5	84.0
W		13.9	84.6
+10.75		13.0	85.5
8+19 ¹² ϕ = N. cl. Line			
-10.75		12.6	85.9
W		13.5	85.0
ϕ		14.5	84.0
E		14.8	83.7
+0.5	W. End. cmt. cl.	15.28	83.17
+10.75	" "	15.41	83.04

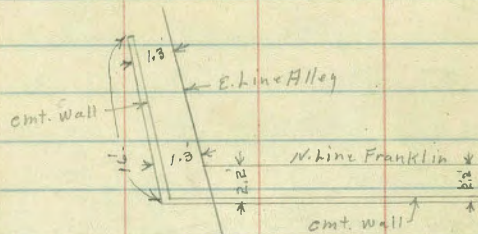
98.45

Alley W. of City Boundary

Boundary St.

8+29¹⁸ ϕ = N. Line Franklin see on St. Line 6
= 0+00

-10.75		12.5	86.0
E		12.4	86.1
+1.2	Top Wall	12.3	86.2
+1.3	Base "	13.7	84.8
ϕ		13.2	85.3
W		12.2	86.3
+10.75		11.4	87.1



0+30

-10		10.5	88.0
W.		10.7	87.8
ϕ		11.0	87.5
E.		10.1	88.4
+10		10.3	88.2
0+50			
-10		5.0	93.5
E		5.2	93.3
ϕ		6.7	91.8
W		7.6	90.9
+10		8.3	90.2

98.45

0+65

-10		4.7	93.8
W		3.9	94.6
♀		1.7	96.8
E	1h. yard	1.0	97.5
T.P.	13.03 110.81 ✓	0.67	97.78

0+80

-10		14.3	96.5
W		13.0	97.8
♀		11.3	99.5
+9		10.6	100.2
E	1h. yard	13.2	97.6
+10	" "	13.2	97.6

1+00

E		7.0	103.8
♀		7.4	103.4
W		7.3	103.5
+10		8.0	102.8

1+20

-10		5.5	105.3
W		5.1	105.7
♀		5.1	105.7
E		5.3	105.5

1+50

E		4.0	106.8
♀		4.1	106.7
W		3.5	107.3

110.81

Way W. of old City Boundary
Boundary St. 7

+10		3.5	107.3
	2+00		
-10		2.4	108.4
W		2.5	108.3
♀		2.4	108.4
E		2.6	108.2

2+50

E		2.3	108.5
♀		1.8	109.0
W		1.5	109.3
+10		1.1	109.7
T.P.	6.20 115.50 ✓	1.51	109.30

3+00

-10		6.0	109.5
W		6.5	109.0
♀		7.3	108.2
E		7.6	107.9

3+50

E		7.0	108.5
♀		7.0	108.5
W		6.6	108.9
+10		6.6	108.9

3+94

6' E. of ♀ Acacia Tree 8" Diam.

115.50

4+00

-10	5.9	109.6
W	6.1	109.4
φ	6.5	109.0
E	6.7	108.8

4+50

E	7.1	108.4
φ	6.5	109.0
W	5.9	109.6
+10	5.5	110.0

4+76¹³ = N. End. Mt. View Park.

-10	4.9	110.6
W = P.I. E. = N. Line Alley 40 th St.	5.6	109.9
φ	6.5	109.0
E	6.7	108.8
+10	6.9	108.6

5+15

-10	5.4	110.1
E	5.1	110.4
φ	4.8	110.7
W	4.3	111.2
+10	4.1	111.4

5+20¹

20' E. of φ = S. Edge Pavmt 5.45 110.05 Imperial Ave.

5+24²

10' E. of φ = S. Edge Pav. 5.12 110.38

115.50

Alley W. of Old City Boundary,
Boundary St R5+27¹

φ = S. edge pavmt 4.91 110.59

5+31²

20' E. of φ on Pav. 5.42 110.08

5+34³

10' W. of φ = S. edge Pav 4.52 110.98

5+37³

10' E. of φ on Pav. 5.14 110.86

5+46²

20' W. of φ = S. edge Pav. 4.05 111.45

5+46⁷

φ on pav. 4.96 110.54

5+53²

10' W. of φ on pav 4.36 111.14

5+65³

20' W. of φ on pav. 3.54 111.96

T.P. 11.71 125.72 1.49 114.01

T.P. 1.34 125.62 1.44 124.28

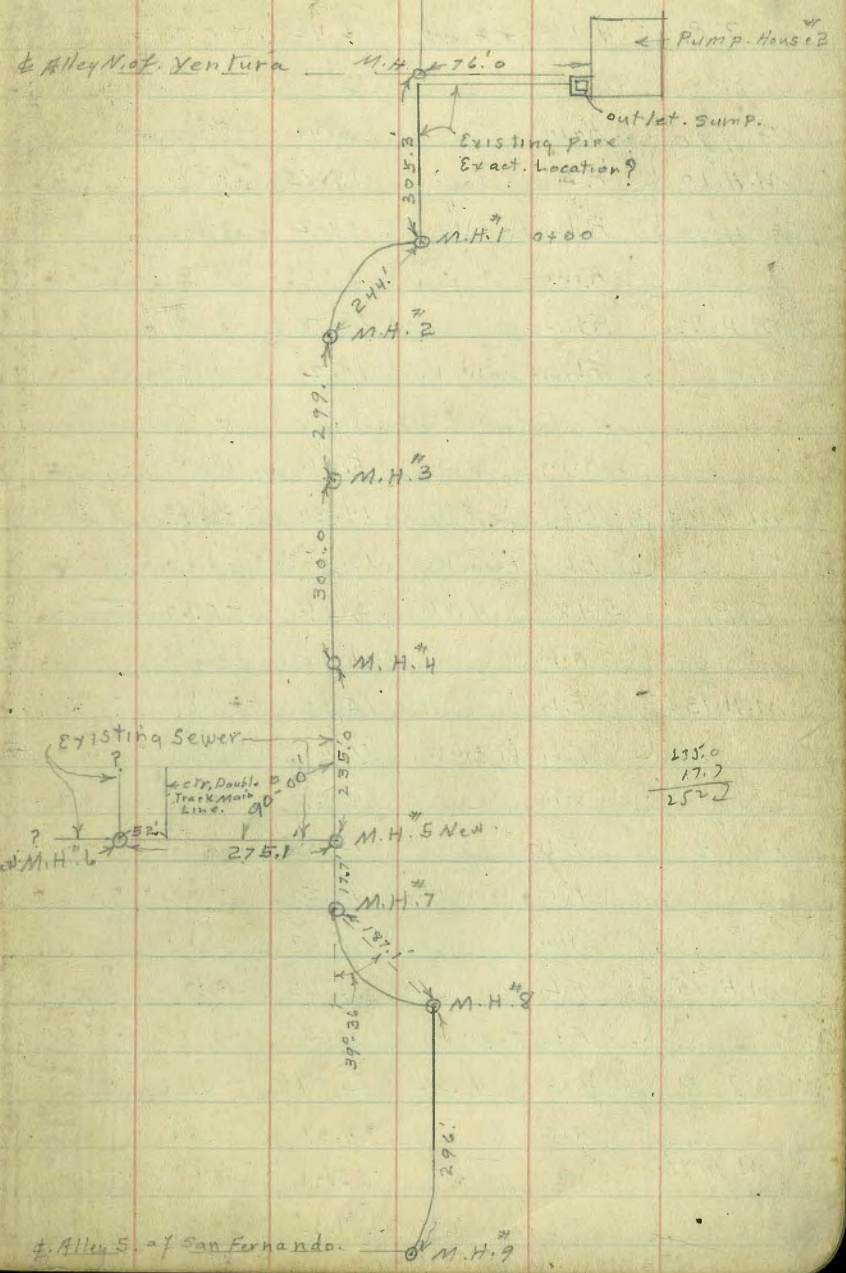
B.M. B.P. S.E. 39th + Imperial 7.05 118.57 = 118.38

7-4-34
Miller
Walker

Levels on Mission Beach Sewer
Bay Side Lane.

B.M. B.P.	0.24	+ 7.75	+ 7.51	Sea Wall
T.P.	7.59	+ 5.88	9.46	- 1.71
S.W. Cor. M.H. Rim outlet Pump #2 = B.M.			6.98	- 1.10
F.L. outlet at Pump #2			11.02	- 5.14
M.H. 1. Bonita Bay } Rim			5.96	- 0.08
F.L. M.H. 1 = 0+00			12.82	- 6.94
M.H. 2 {at E.C. W. side } Bonita Bay } Rim			4.77	+ 1.11
F.L. M.H. 2 = 2+48			12.97	- 7.09
T.P.	4.52	5.63	4.77	+ 1.11
5+48 = M.H. 3 Rim			4.60	+ 1.03
M.H. 3 F.L.			13.01	- 7.38
8+48 M.H. 4 Rim			4.63	+ 1.00
M.H. 4 F.L.			13.57	- 7.94
T.P.	5.18	6.18	4.63	+ 1.00
New { M.H. 5 Rim			5.10	+ 1.08
West { M.H. 5 F.L. W.N. + S.			14.50	- 8.32
Plan 10+96 11+007 Meas. { M.H. 6 Rim			5.60	+ 0.58
At B.C. S.W. Cor Bonita Bay } M.H. 6 F.L.			11.80	- 5.62
M.H. 7 { Rim			5.08	+ 1.10
M.H. 7 F.L.			14.53	- 8.35
M.H. 7 ground.			6.4	- 0.25
12+82 M.H. 8 at E.C. - Rim			5.10	+ 1.08
M.H. 8 F.L.			14.91	- 8.73
M.H. 8 ground			7.0	- 0.85
M.H. 9 at Alley S. of San Fernando Rim			6.42	- 0.24
M.H. 9 F.L.			15.34	- 9.16
M.H. 9 F.L. from W.			12.4	- 6.27

Indexed
C.S.K.



6.18

T.P.	4.68	+4.44	6.42	-0.24
M.H.#10	Rim		5.42	-0.98
	F.L.		13.85	-9.41
	F.L. from W.		10.2	-5.76
M.H.#11	Rim		5.36	-0.92
	F.L.		13.98	-9.54
	F.L. from W.		10.2	-5.76
M.H.#12	Rim		5.06	-0.62
	F.L.		14.38	-9.94
	F.L. from W.		10.0	-5.56
T.P.	5.48	4.86	5.06	-0.62
M.H.#13	Rim		5.20	-0.34
	F.L.		15.30	-10.44
	F.L. from W.		11.2	-6.34
M.H.#14	Rim		5.20	-0.34
	F.L.		15.38	-10.52
	F.L. from W.		10.5	-5.64
M.H.#15	Rim		5.07	-0.21
	F.L.		15.65	-10.79
	F.L. From W.		10.5	-5.64
T.P.	4.53	4.32	5.07	-0.21
M.H.#16	Rim		4.57	-0.25
	F.L.		15.21	-10.89
	F.L. from W.		9.2	-4.88

10.12
10.8

San Fernando Pl

Ensenada Ct.

Dover Ct.

Devon Ct.

San Gabriel Pl.

Deal Ct.

Coronado Ct

Cohasset Ct.

Capistrano Pl.

Alley O M.H.#9

Alley O M.H.#10

Alley O M.H.#11

Alley O M.H.#12

Alley O M.H.#13

Alley O M.H.#14

Alley O M.H.#15

Alley O M.H.#16

206.8

199.8

194.9

204.

185.2

186.7

190.

4.32

# M.H. 17	Rim	3.79	+0.53
	F.L.	15.32	-11.00

 spk. Pole N.E.
 Bayside Lane +
 Capistrano Pl.

2.56 +1.76

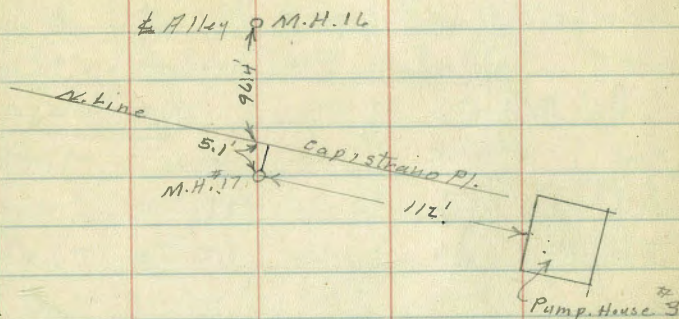
R.F.S. & M.B.B.

T.P. T.P. 4.70 4.27 4.75 -0.43 Alley North of Capistrano

T.P. 5.84 4.35 5.76 -1.49

T.P. 9.51 8.75 5.11 -0.76

B.M. B.P. Top Seawall San Fernando 1.19 7.56 = 7.57



Readings on Open - Sewer Ditch at Mission Beach.

Bay Side Lane Between San Gabriel Place + Deal Court.

High Water

Low Water

Time	Height
10.03 A.M.	5.7
10.34 P.M.	4.6

Time	Height
3.47 A.M.	1.2
4.27 P.M.	0.8

High Tide

3 M. M. H. 13 P.M. 4.93 ✓ #4.59 ✓

12.11	-7.52 ✓	Ditch A
9.97	-5.38 ✓	" B
9.12	-3.53 ✓	Bay C

10.015	-7.425 ✓	A
9.90	-5.31 ✓	B
7.92	-3.33 ✓	Bay C

12.05	-7.46 ✓	A
9.845	-5.255 ✓	B
7.835	-3.265 ✓	C

11.985	-7.395 ✓	A
9.86	-5.21 ✓	B
7.78	-3.19 ✓	C

9.30 A.M.

" " "

" " "

10.03 A.M. (High Tide)

" " " "

" " " "

10.30 A.M.

" " "

" " "

11 A.M.

" " "

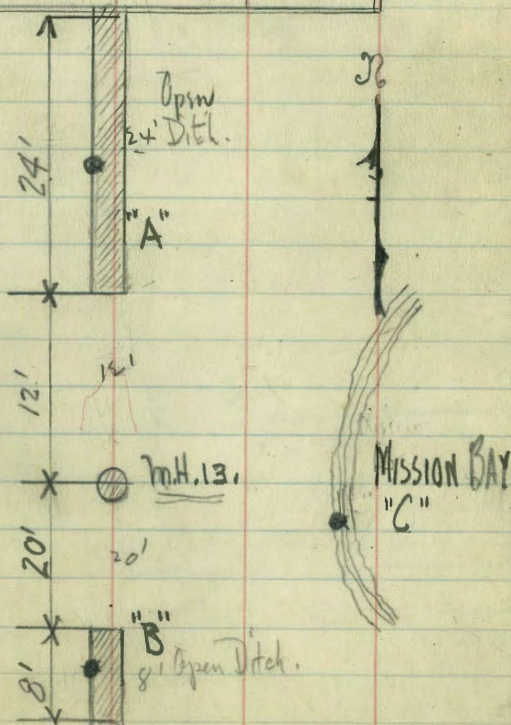
" " "

Weather < 100° - Sun Shining

Sept. 11, 1934. Kenny.

Time	Ditch "A"	Ditch "B"	Bay "C"
9.30 A.M.	-7.52 ✓	-5.38 ✓	-3.53 ✓
10.03 A.M.	-7.425 ✓	-5.31 ✓	-3.33 ✓
10.30 "	-7.46 ✓	-5.255 ✓	-3.265 ✓
11.00 "	-7.395 ✓	-5.21 ✓	-3.19 ✓
11.50 "	-7.34 ✓	-5.155 ✓	-3.37 ✓
12 M	-7.35 ✓	-5.12 ✓	-3.70 ✓
12.30 P.M.	-7.36 ✓	-5.09 ✓	-4.06 ✓
1.00 P.M.	-7.38 ✓	-5.075 ✓	-4.4 ✓

Henderson

Bottom "A" Ditch - 9.95
Top pipe - 8.55
Bottom Ditch "B" - 7.41

4.59

11.93 -7.34 ✓ A
 9.745 -5.155 ✓ B
 7.96 -3.37 ✓ C

2.6 Bottom Ditch. 1.2 Pipe

11.94 -7.35 ✓ A
 9.71 -5.12 ✓ B
 8.29 -3.70 ✓ C

1.0 Bottom

Onny says water in ditch is much lower at low tide.

11.95 -7.36 ✓ A
 9.68 -5.09 ✓ B
 8.65 -4.06 ✓ C

11.97 -7.38 ✓ A
 9.665 -5.075 ✓ B
 8.99 -4.40 ✓ C

11.50 A.M.

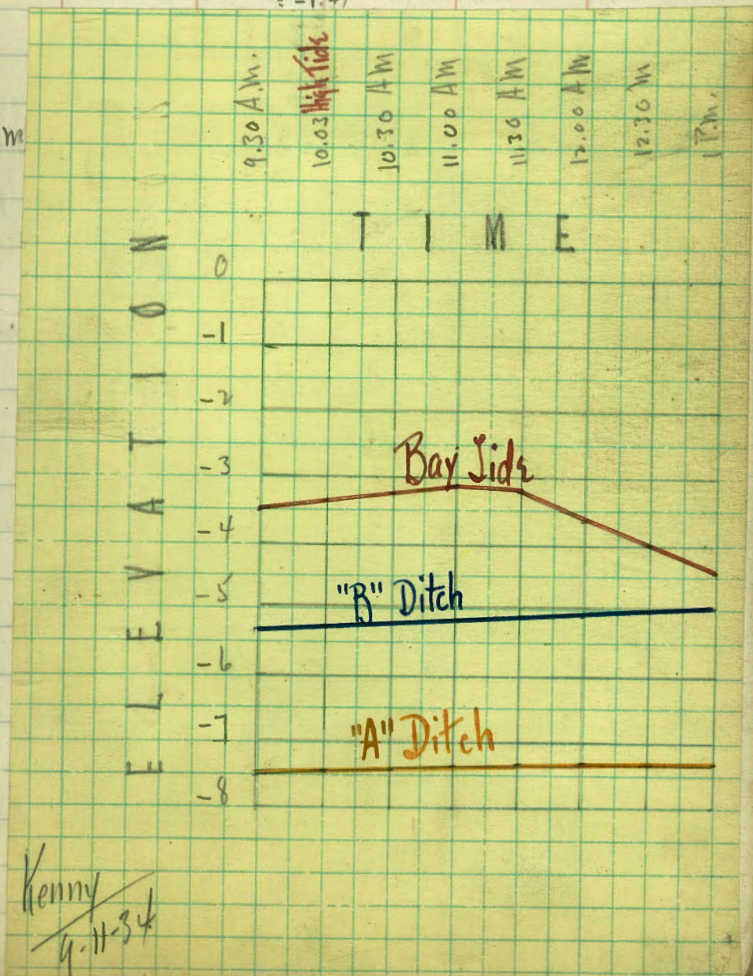
12 M.

Bottom Ditch -9.95 Top Pipe -8.65

" " = -7.41

12:30 P.M.

1 P.M.

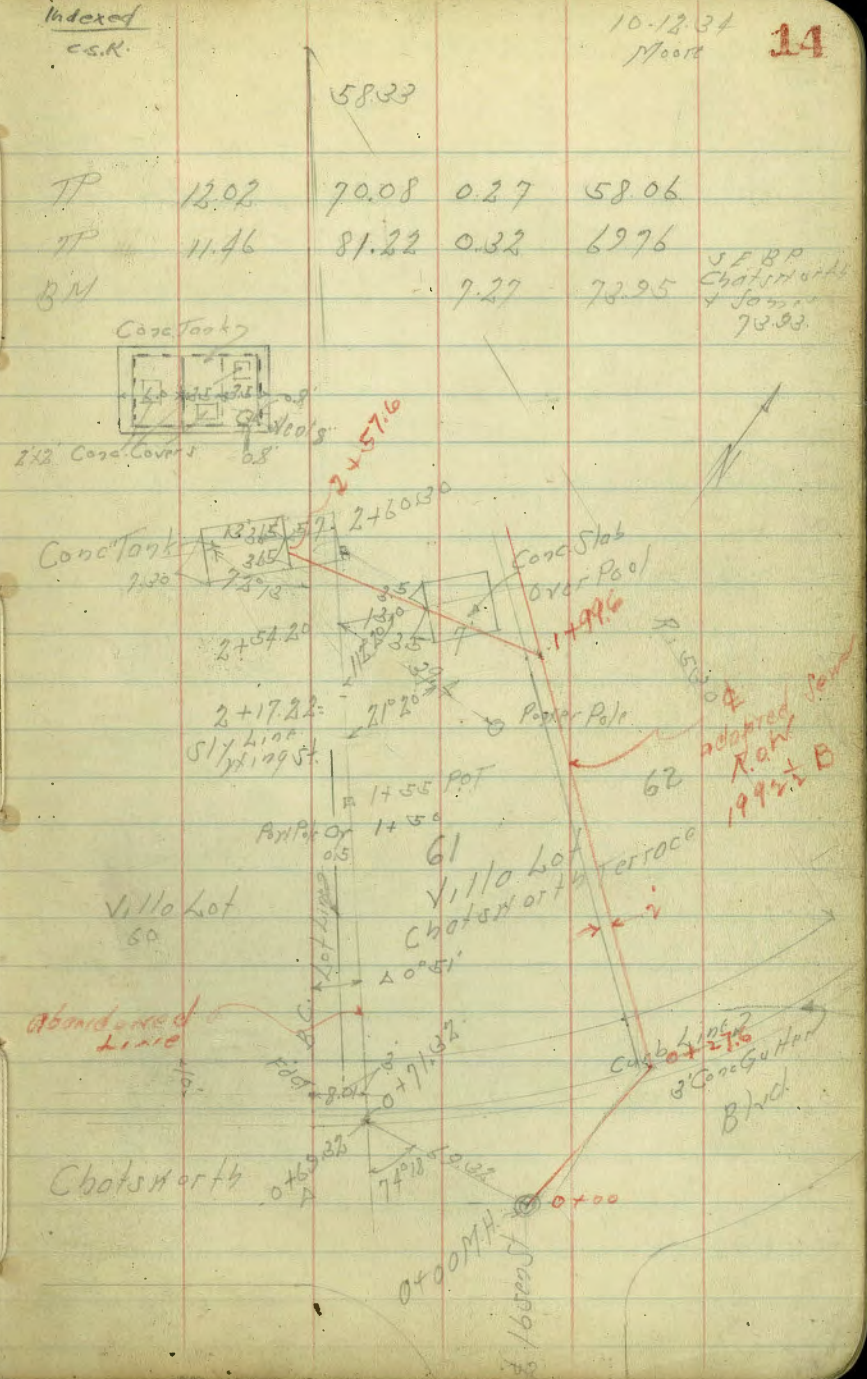


Proposed Sewer Through Villa Lot of 81
Chatsworth Terrace

Indexed
C.S.R.

10-12-34
Moore 14

BM	7.50	81.83 ✓		73.93	STOP Chatsworth + Jam
0+00 Rim MH			3.97	78.36	
Chatsworth Poles			8.13	73.70	
Flax Heap			3.25	78.58	
0+24.6 on Pavng			2.40	78.43	
0+69.32			2.56	78.27	
0+71.32 Gutter			2.57	79.26 ✓	
Top cb			2.41	79.39	
0+77.82 - Edge Walk			1.12	80.6	
1+0			0.7	81.1	
1+30			1.2	80.6	
1+55 POT on Stub			1.43	77.40 ✓	
TP	0.07	69.82	12.08	69.75 ✓	
1+75			7.4	62.4	
TP	0.27	58.33	11.76	58.06 ✓	
2+0			6.8	51.5	
2+17.22 - Sky Line Ming			11.0	47.3	
2+40			13.8	44.5	
2+54.2			13.4	44.9	
2+60.3			12.6	44.7	
Top Conc Slab			15.28	43.10	
Top Conc Tank			14.78	43.55	
Bottom "			20.21	38.12	



Grades Mission Beach Sewer Boys delaware
From Pump House #2 to Pump House #3

Indexed
c.s.R.

Oct. 25-34
Moore 15

BM	LLS	5.55	-1.10	SW Cor. MH Pines outlet Pump #2 Page 9	6.137				
0+1013 Pump Ho #2			-3.27	8.82 c2.17 on R.R. 6.55	4+48.36 4+44.47	9°25'5"	9°04'	-3.28	10.01 c5.33 4.68
					4+81.18 4+75.79	14°08.25"	13°36'	-3.93	10.06 c5.47 4.39
					5+14.00 5+66.81	18°51'	18°08'	-3.97	10.10 c5.72 4.38
0+78.13 B.C. 8' Rad			-3.27	8.93 c2.31 6.81	5+46.82 5+37.89	23°38.75"	23°40'	-4.01	10.14 c5.71 4.43
0+90.70 F.C.			-3.33	8.94 c2.33 6.62	5+73.63 5+68.85	28°16.50"	27°12'	-4.05	10.18 c5.83 4.63
1+0			-3.40	8.95 c2.17 6.43	6+12.45 5+99.87	32°53.25"	31°41'	-4.10	10.23 c4.82 4.97
+50			-3.47	9.02 c2.61 6.41	6+45.27 6+30.89 F.C. MH #2	37°42'	36°16'	-4.14	10.27 c4.89 5.59
2+0			-3.54	9.09 c3.72 5.37	+50			out	
+08 Top P. #214			-2.58						
+50			-3.62	9.17 c4.52 4.65	7+0			-4.21	10.34 c4.99 4.35
3+0			-3.69	9.24 c4.74 4.50	+50			-4.28	10.36 c4.72
BM 7.23 6.13			-1.10	Pump Ho #2	TP	5.08	5.52	5.69	0.41
+50			-3.76	9.83 c5.03 4.86	8+0			-4.35	9.87 c4.99 4.88
+82.73 MH #1 B.C.			-3.80	9.93 c5.11 4.82	+50			-4.42	9.94 c4.99 4.95
8 Parts 4+15.55 4+12.75			-3.84	9.97 c5.21 4.76	9+0			-4.49	10.01 c5.12 4.89

Σ = 0.0147

Σ = 0.0037

5.527

9+11.20 - MH #3
-4.55

+50 out

10+0
-4.63

+50
-4.62

11+0
-4.76

+50
-4.83

12+0
-4.90

+44.35 - MH #4
-4.96

+50 out -4.99

13+0
-5.04

+50
-5.11

14+0
-5.18

+50
-5.25

10.07
4.96 c5.11

10.15
4.51 c5.64

10.21
4.73 c5.48

10.28
4.81 c5.47

10.35
4.85 c5.50

10.42
4.84 c5.58

10.48
4.93 c5.55

10.56
4.77 c5.82

10.63
4.93 c5.70

10.70
5.04 c5.66

10.77
4.83 c5.94

0.51
4.82
4.82
8M 0.60 BPEC6 opp. Nori Pump
Hour

5.52

TP

14+79.6 - MH #5

+97.20 MH #7 BC

6.31
6.27

15+31.01
15+13.65

6.31
6.27

+64.82
+44.70

12.12
12.54

+98.63
+75.76

19.48
19.21

16+32.44
16+06.82

26.24
26.47

+66.25
+37.88

30.00
32.14

17+00.06
+68.24 FC MH #8

39.36
38.41

5.97

5.45

3.32

TP

5.97

5.45

3.32

19+0

3.40

5.01

0.51

Pump RP

10.74

-5.29

10.76
5.66 c5.70

-5.31

10.80
4.96 c6.44

-5.35

10.85
4.76 c6.39

-5.40

10.89
4.87 c6.52

-5.44

10.93
4.92 c6.61

-5.48

10.98
4.88 c6.70

-5.53

11.02
4.98 c6.66

0 -5.57

11.09
4.95 c6.74

-5.64

11.16
4.62 c6.59

-5.71

11.23
4.83 c6.40

-5.78

0.08

5.25
3.31 c5.94

-5.85

5.00/0.0286

5.00/0.0286

11.02.86

5.00/0.0286

19 + 0.60 BC 4 Park 21.85 C 21.85		-5.86	$\frac{9.26}{3.50}$ C 5.76	24 + 0.80 MH #11		-6.54	$\frac{9.94}{4.37}$ C 5.47
+31.45	2° 22' 45"	-5.82	$\frac{9.29}{3.49}$ C 5.80	+50		-6.60	$\frac{10.00}{4.23}$ C 5.77
+53.30	4° 45' 30"	-5.92	$\frac{9.32}{3.65}$ C 5.97	25 + 0		-6.67	$\frac{10.07}{3.87}$ C 6.20
+75.15	7° 08' 15"	-5.95	$\frac{9.35}{3.75}$ C 6.20	TP 1.03 2.40 5.02		-6.63	$\frac{11.13}{5.03}$ C 6.11
+97.00 EC MH #9 9° 31'		-5.98	$\frac{9.38}{3.91}$ C 5.97	+98.75 = MH #12		-6.81	$\frac{11.20}{5.06}$ C 6.14
20 + 50		-6.05	$\frac{9.45}{4.38}$ C 5.17	26 + 50		-6.88	$\frac{11.27}{4.52}$ C 6.75
21 + 0		-6.12	$\frac{9.52}{4.27}$ C 5.25	27 + 0		-6.95	$\frac{11.34}{4.67}$ C 6.67
+50		-6.19	$\frac{9.59}{5.04}$ C 4.55	+50		-7.02	$\frac{11.41}{4.54}$ C 6.87
22 + 0.90 = MH #10		-6.26	$\frac{9.66}{4.46}$ C 5.20	28 + 0.30 = MH #12		-7.09	$\frac{11.48}{4.62}$ C 7.46
+50		-6.33	$\frac{9.73}{4.73}$ C 5.00	+50		-7.15	$\frac{11.54}{4.74}$ C 6.80
23 + 0		-6.40	$\frac{9.80}{4.90}$ C 5.41	29 + 0		-7.22	$\frac{11.61}{4.81}$ C 7.10
+50		-6.47	$\frac{9.87}{5.00}$ C 4.87	+50		-7.29	$\frac{11.68}{5.00}$ C 6.68
	3.40				1.89		

29+88.45 - MH 14

-7.34

11.73 c 7.02
4.71

34+50

S-00137

-7.97

12.05 c 8.67
3.38

30+0

-7.36

11.75 c 6.85
4.90

+68.1 MH "17"

-8.00

12.08 c 8.60
3.98

TP 5.15 4.39 4.84

-0.76

5.76
30+50

35+34.4

-8.07

12.15 c 8.33
3.82

+50

-7.43

11.57 c 6.67
4.84

31+0

-7.49

11.57 c 6.82
4.76

+80.4 - Pump No. 3

-8.15

12.23 c 9.06
3.17

+50

-7.56

11.64 c 6.83
4.81

BM 2.32 4.08

+1.76

Spk. Pole NE
Borvid Lane
Capistrano Ph.

+75.3 - MH "15"

-7.60

11.68 c 7.37
4.31

MH "9"

-5.48

32+0

-7.63

11.71 c 7.27
4.44

50 W of MH

-5.24

8.64 c 5.40
3.23

+50

-7.70

11.78 c 7.16
4.62

100 W of MH

-5.00

8.40 c 4.41
3.99

33+0

-7.77

11.85 c 7.22
4.63

340

S-00136

+50

-7.84

11.82 c 7.58
4.34

+66.8 - MH "16"

-7.86

11.84 c 7.51
4.43

34+0

-7.51

11.99 c 8.02
3.37

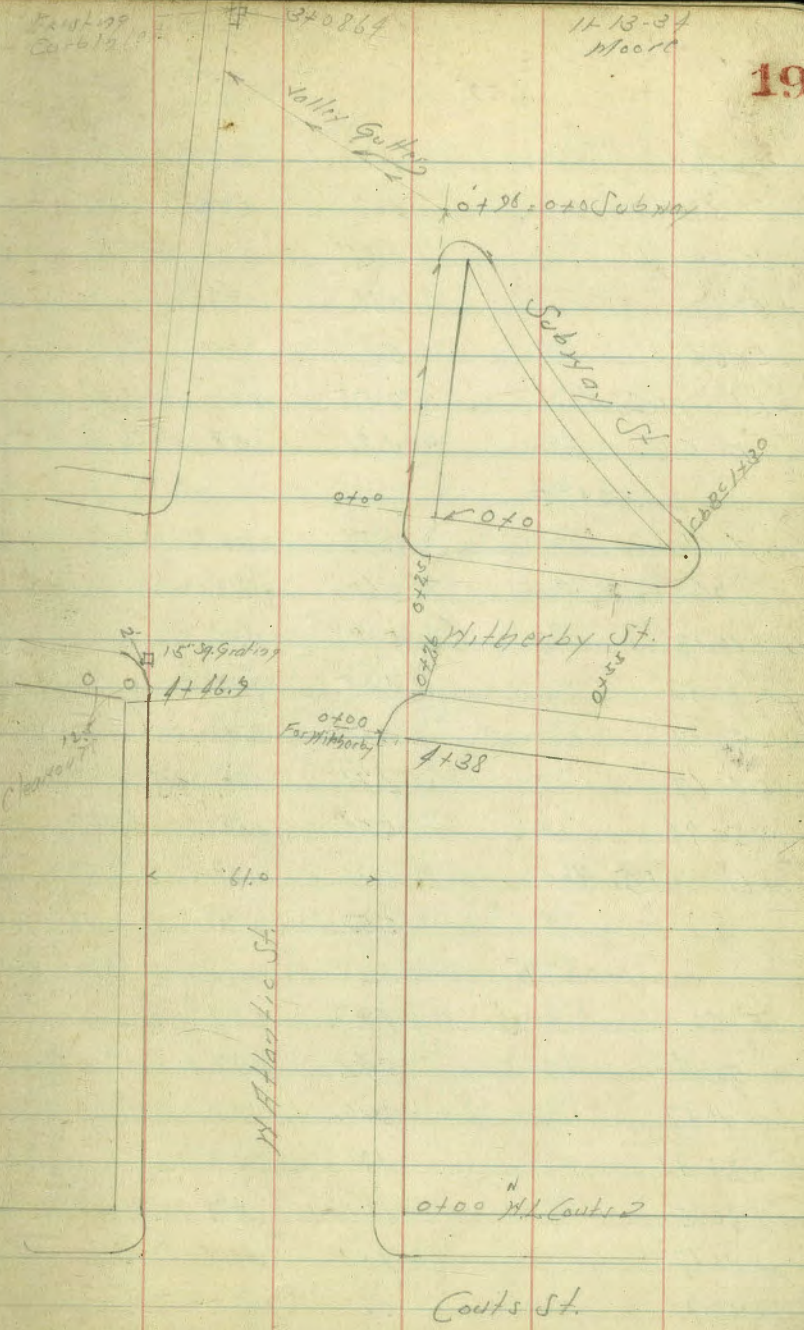
S-00137

Cross Section of Atlantic St.
Couts St. to North

Indexed
C.S.R.

B.M.	5.95	5.77	-0.18	
TP	504	653	4.22	1.55
	0+0 - N.H. Couts			
F. Cb Top		4.15		2.44
Gutter		4.81		1.28
+10.17		4.64		1.95
+20.33		4.47		2.12
+30.50 = Z		4.33		2.26
+40.67		4.63		1.96
+50.84		4.96		1.63
+61 = H Gutter		5.31		1.28
H Cb Top		4.75		1.84
	0+25			
H Cb Top		4.72		1.87
Gutter		5.45		1.14
+10.17		5.10		1.49
+20.33		4.76		1.83
+30.50		4.43		2.16
+40.67		4.60		1.99
+50.84		4.86		1.73
+61 = F Gutter		5.11		1.48
F Cb Top		4.41		2.18
	0+50			
F Cb Top		4.53		2.06
Gutter		5.25		1.34

S.H. North Cb.
Borough
Atlantic



+10.17	491	1.68
+20.33	467	1.92
+30.50	452	2.07
+40.67	486	1.73
+50.84	521	1.33
+61 = H Gutter	555	1.04
H Cb	481	1.78

0725

H Cb	486	1.73
H Gutter	560	0.99
+10.17	519	1.40
+20.33	485	1.74
+30.50	459	2.00
+40.67	471	1.88
+50.84	501	1.58
+61 = F Gutter	531	1.28
	459	2.00

140

F Cb	472	1.87
Gutter	542	1.17
+10.17	516	1.49
+20.33	486	1.79
+30.55	471	1.88
+40.67	491	1.65
+50.84	520	1.39
+61.0 = H Gutter	558	1.01

H Cb Top	482	1.77
	1725	
H Cb Top	486	1.73
Gutter	556	1.03
+10.17	517	1.42
+20.33	500	1.59
+30.50	482	1.77

+40.67	490	1.69
+50.84	520	1.39
+61 = F Gutter	549	1.10
F Cb Top	486	1.79

1750

F Cb Top	482	1.77
Gutter	555	1.04
1 +10.17	524	1.35
2 +20.33	497	1.62
3 +30.50	490	1.69
4 +40.67	500	1.59
5 +50.84	525	1.34
6 +61 = H Gutter	558	1.01
H Cb Top	484	1.75

1775

H Cb Top	487	1.72
Gutter	556	1.03
1	528	1.31
2	508	1.51

3	4.90	1.69
4	5.00	1.59
5	5.32	1.27
6 = F Gutter	5.58	1.01
ECb Top	4.87	1.72
2.10		
ECb Top	4.94	1.65
Gutter	5.60	0.99
1	5.34	1.25
2	5.02	1.57
3	4.91	1.68
4	5.07	1.52
5	5.24	1.35
6 = H Gutter	5.54	1.04
H Cb Top	4.80	1.79
2.725		
H Cb Top	4.77	1.82
Gutter	5.50	1.09
1	5.23	1.36
2	5.05	1.54
3	4.97	1.62
4	5.12	1.47
5	5.51	1.09
6 = F Gutter	5.76	0.83
Cb Top	5.08	1.51

2.750		
F Cb Top	5.26	1.33
Gutter	5.93	0.66
1	5.59	1.00
2	5.22	1.27
3	5.08	1.51
4	5.13	1.46
5	5.26	1.33
6 = H Gutter	5.50	1.09
H Cb Top	4.76	1.83
2.75		
H Cb Top	4.80	1.79
Gutter	5.48	1.11
1	5.25	1.34
2	5.14	1.45
3	5.10	1.49
4	5.27	1.32
5	5.66	0.93
6 = F Gutter	6.01	0.58
ECb Top	5.45	1.14
3.70		
F Cb Top	5.44	1.15
Gutter	6.05	0.54
1	5.67	0.92
2	5.27	1.32
3	5.06	1.53

1	5.13	1.46
5	5.21	1.28
6 = W Gutter	5.49	1.10
W Cb Top	4.78	1.81
3+20		
W Cb Top	4.84	1.25
Gutter	5.52	1.07
1	5.29	1.30
2	5.18	1.41
3	5.21	1.48
4	5.40	1.19
5	5.70	0.89
6 = E Gutter	6.05	0.54
E Cb Top	5.44	1.15
3+40		
E Cb Top	5.50	1.09
Gutter	6.12	0.46
1	5.73	0.86
2	5.35	1.24
3	5.17	1.42
4	5.17	1.42
5	5.33	1.26
6 = W Gutter	5.53	1.06
W Cb Top	4.88	1.21

3+60		
W Cb Top	4.84	1.25
Gutter	5.54	1.05
1	5.31	1.28
2	5.22	1.36
3	5.22	1.32
4	5.38	1.21
5	5.71	0.88
6 = E Gutter	6.16	0.43
E Cb Top	5.54	1.05
TP 4.87 5.90	5.56	1.03
3+80		
E Cb Top	4.87	1.03
Gutter	5.44	0.46
1	5.01	0.89
2	4.70	1.20
3	4.52	1.38
4	4.56	1.34
5	4.67	1.23
6 = W Gutter	4.89	1.01
W Cb Top	4.22	1.68
410		
W Cb Top		
Gutter in Drive	4.37	0.93
1	4.74	1.16
2	4.60	1.30

5.90

3	460	1.30
4	468	1.22
5	500	0.90
6 = FGutter	540	0.50
FCb Top	480	1.10
	4120	
FCb Top	473	1.17
Gutter	530	0.60
1	491	0.99
2	468	1.22
3	460	1.30
4	462	1.28
5	481	1.09
6 = H Gutter in Dr	502	0.88
	4130	
Hcb	439	1.51
Gutter	506	0.84
1	480	1.10
2	462	1.28
3	460	1.30
4	468	1.22
5	497	0.93
6 = FGutter	531	0.59
FCb Top	478	1.12

5.90

4 + 38 = 42. Mitberby on Diag.
4 + 46.9 = 50.9

F Gutter	530	0.60
1	495	0.95
2	470	1.20
3	463	1.27
4	467	1.23
5	482	1.08
6 = H Gutter	507	0.83
Grating SW Gutter	514	0.76
	S cb of Mitberby	
H Gutter	511	0.79
1	493	0.97
2	481	1.09
3	471	1.19
4	480	1.10
5	506	0.84
6 = FGutter	531	0.59
	511	
FGutter	531	0.59
1	511	0.79
2	489	1.01
3	477	1.13
4	481	1.09
5	490	1.00
6 = H Gutter	508	0.82

23

5.90

H. L. Witherby

H Gutter	5.08	0.82
1	4.93	0.97
2	4.81	1.02
3	4.81	1.09
4	4.85	0.95
5	5.15	0.75
6 = F Gutter	5.36	0.54

H 11

F Gutter	5.40	0.50
1	5.31	0.59
2	5.11	0.79
3	4.94	0.96
4	4.90	1.00
5	5.03	0.87
6 = H Gutter	5.17	0.77

H Gurb

H Gutter	5.32	0.58
1	5.08	0.82
2	5.00	0.90
3	4.99	0.91
4	5.20	0.70
5	5.36	0.54
6 = F Gutter	5.43	0.47

5.90

H. L. Witherby on Ding

FL on Conc. Dr.	4.95	0.95
+7 = Gutter	5.51	0.39
1	5.41	0.49
2	5.22	0.68
3	5.02	0.88
4	4.98	0.92
5	5.20	0.70
6 = H Gutter	5.39	0.51

0 + 20

H Gutter in Dr.

H Gutter in Dr.	5.41	0.49
1	5.16	0.74
2	5.03	0.87
3	5.03	0.87
4	5.27	0.63
5	5.50	0.40

6 = F Gutter	5.68	0.22
FL on Conc. Dr.	5.04	0.86

0 + 40

FL on Conc. Dr.	5.08	0.82
F Gutter	5.69	0.21
1	5.45	0.45
2	5.20	0.70
3	5.01	0.89
4	5.07	0.83
5	5.22	0.68

21

5.90

6 - W Gutter in Dr	5.49	0.41
0+760		
W Gutter 120 ft	5.51	0.39
1	5.20	0.70
2	5.10	0.80
3	5.01	0.89
4	5.10	0.80
5	5.37	0.53
6 - E Gutter	5.60	0.30
E L in Conc Dr	5.10	0.80
0+75		
E L in Conc Dr	1.95	0.95
+7 - E Gutter	5.50	0.40
1	5.33	0.57
2	5.09	0.81
3	4.98	0.92
4	5.08	0.82
5	5.21	0.69
6 - W Gutter in Dr	5.57	0.33
0+86		
W Cb Top	4.90	1.00
Gutter	5.62	0.28
1	5.32	0.58
2	5.12	0.78
3	5.06	0.84
4	5.18	0.72

5.90

25

5	5.41	0.49
6 - E Gutter	5.55	0.35
E L in Paving	5.40	0.50
1+08.94		
E L	5.10	0.80
Cb	5.32	0.58
1	5.55	0.35
2	5.41	0.49
3	5.18	0.72
4	5.12	0.71
5	5.33	0.57
6 - W Gutter	5.64	0.26
W Cb	4.91	0.99
1+21.88		
W Gutter	5.61	0.29
1	5.35	0.55
2	5.31	0.59
3	5.35	0.55
4	5.58	0.32
5	5.46	0.50
6 - E Cb	5.05	0.85
+7 - E L	4.85	1.05
1+34.82		
E L	4.71	1.19
+7 - E Cb	4.81	1.09
1	5.10	0.80

5.96

2	5.53	0.39
3	5.54	0.36
4	5.54	0.36
5	5.49	0.41
6 - H Gutter Dr	5.74	0.16
1 + 47.76		
H Gutter in Dr	5.70	0.20
1	5.65	0.25
2	5.66	0.24
3	5.49	0.41
4	5.10	0.80
5	4.88	1.02
6 - EC66	4.69	1.21
77 - F.L.	4.62	1.28
1 + 60.70		
F.L.	4.66	1.24
77 - EC66	4.51	1.39
1	4.68	1.22
2	4.95	0.95
3	5.25	0.65
4	5.65	0.25
5	5.78	0.12
6 - H Gutter	5.78	0.12
H CB Tap	5.09	0.81

5.90

1 + 73.64		
H Gutter in Dr	5.80	0.10
1	5.76	0.14
2	5.34	0.56
3	5.12	0.78
1 + 98.64		
H Gutter in Dr	5.83	0.07
2 + 23.64		
H Gutter	5.90	0.0
2 + 48.64		
H Gutter	6.00	-0.10
2 + 73.64		
H Gutter	6.11	-0.21
2 + 98.64		
H Gutter	6.27	-0.37
3 + 08.64 = Existing Cb Inlet on Grating		
H Gutter on Grating	6.44	-0.54

Levels Sly Gutter of Subway St.

	5.9° Bt. Ford			
	0+0 = 0+36 Atlantic			
Gutter	0+20	5.49	0.41	
Gutter	0+40	5.43	0.47	
Gutter	0+60	5.33	0.57	
Gutter	0+80	5.35	0.55	
Gutter	1+0	5.24	0.66	
Gutter	1+20	4.96	0.94	
Gutter	1+30 = Cb EC	4.85	1.05	
TP	4.41	6.00	4.31	1.59

Cross Section Withby St
East of W. Atlantic

27

	6.00		
	0+0 Sly Line Withby		
Gutter	0+10	5.59	0.41
Gutter	0+20	5.49	0.51
Gutter	0+25 = Cb EC	5.57	0.43
Gutter	0+35	5.67	0.33
Gutter	0+45	5.73	0.27
Gutter	0+55	5.64	0.36
Gutter	0+70 Sly Line Withby	5.45	0.55
Gutter	0+10	5.48	0.60
Gutter	0+20	5.43	0.57
Gutter	0+26 = Cb EC	5.55	0.45
Gutter	0+35	5.57	0.43
Gutter	0+35	5.56	0.44

6.00

~~0+25~~

~~Gutter~~

~~5.50~~

~~0.50~~

~~0+55~~

~~Gutter~~

~~5.31~~

~~0.69~~

TP

5.30

6.09

5.21

-0.79

BM

6.23

-0.14

Starting

-0.18

Cross Section With curb St.
Foot of E.L. Atlantic

11-20-34
Moore 29

BM	4.68	6.23	1.55
	0-966 on H		
	0+0 on S =		
			E.L. Atlantic
S.Cb-6.75-Existing	5.23	1.00	
Gutter	5.64	0.59	
S.Cb Lint	5.66	0.52	
1/4	5.58	0.65	
1/2	5.57	0.66	
1/4	5.64	0.59	
H.Cb L	5.73	0.50	
7.3-Existing Gutter	5.71	0.52	
" Curb Top	5.24	0.99	
	0+0 on S		
H.Cb	5.30	0.93	
Gutter	5.83	0.46	
1/4	5.56	0.67	
1/2	5.45	0.78	
1/4	5.53	0.70	
S.Cb L	5.72	0.51	
7.5.7-Gutter	5.66	0.57	
Existing Cb Top	5.23	1.00	
	0+20		
S.Cb Top	5.21	1.02	
Gutter	5.79	0.44	
1/4	5.40	0.83	
1/2	5.25	0.98	

TP Page 19

	6.23		
1/4	5.42	0.81	
Gutter	5.88	0.35	
H.Cb	5.33	0.90	
	0+40		
H.Cb	5.02	1.21	
Gutter	5.54	0.69	
1/4	5.12	1.11	
1/2	4.99	1.24	
1/4	5.19	1.04	
Gutter	5.59	0.64	
S.Cb	5.01	1.22	
	0+60		
S.Cb	4.57	1.66	
Gutter	5.19	1.04	
1/4	4.81	1.42	
1/2	4.66	1.57	
1/4	4.77	1.46	
Gutter	5.21	1.02	
H.Cb-End Rd	4.71	1.62	
	0+80		
H.L	4.81	1.42	
H.Cb L	4.73	1.50	
1/4	4.54	1.69	
1/2	4.45	1.78	
1/4	4.61	1.62	
Gutter	5.01	1.22	
S.Cb	4.40	1.83	

Additional Sections
Atlantic St. N of Whitcomb

BM	414	5.69	1.55
	0736		
10' F of FL		4.80	0.89
27' F " "		4.29	1.40
40' F " "		4.61	1.08
56' F " " = Edge Pav		5.22	0.47
	1708.94		
18' F of FL		4.41	1.28
33' F " "		4.53	1.16
48' F " " = Edge Pav		5.00	0.69
	1721.88		
11' F of FL		4.45	1.24
26' F " "		4.55	1.14
40' F " " = Edge Pav		4.82	0.87
	1734.82		
4' F of FL		4.47	1.22
18' F " "		4.90	0.99
33' F " " = Edge Pav		4.96	0.73
	1747.96		
12' F of FL		4.74	0.95
26' F " " = Edge Pav		5.08	0.61
	1760.70		
6' F of FL		4.64	1.05
20' F " " = Edge Pav		5.02	0.67

TP Page 19

5.69

1773.64

5' F of FL		4.67	1.02
15' F " " = Edge Pav		4.95	0.74
FL		4.54	1.15
FCB L		4.36	1.33
1		4.28	1.41
2		4.58	1.11
	1798.64		
-6		5.02	0.67
FL		4.85	0.84
CB		4.60	1.09
1 1617		4.40	1.29
2 2023		4.47	1.22
3 20.50 d		4.60	1.09
4 40.67		4.86	0.83
5 50.84		5.26	0.43
	2126.64		
FL		5.22	0.47
+1.1 = Edge Edge Pav		5.13	0.56
CB		4.87	0.82
1		4.62	1.07
2		4.45	1.24
3		4.62	1.07
4		4.96	0.73
5		5.36	0.33

11-20-34

30

5.69

278.64

FL	4.50	1.19
+2	5.46	0.23
Cb - Edge Pass	5.15	0.54
1	4.86	0.83
2	4.63	1.06
3	4.62	1.07
4	4.98	0.71
5	5.40	0.29

273.64

FL	4.5	1.19
Cb	5.40	0.29
+4 - Edge Pass	5.15	0.54
1	4.26	0.73
2	4.70	0.99
3	4.53	1.16
4	4.96	0.73
5	5.50	0.19

278.64

FL	4.5	1.2
Cb	5.4	0.4
+5.8 - Edge Pass	4.98	0.71
1	4.85	0.84
2	4.59	1.10
3	4.46	1.23
4	5.00	0.69

5.69

31

5

5.53 0.16

270.864 - Existing Cb. lat. 10.2

FL 4.8 0.9

Cb 5.34 0.35

1 4.26 0.83

2 4.65 1.04

3 4.52 1.17

4 5.04 0.65

5 5.58 0.11

6 - 11 Gutter on Grading 6.24 -0.48

Flank Line at Top Box 7.96 -2.27

Flank Line Existing Clean Out 8.63 -2.94
S.W. Cor. of Lot 10 + 11 + 12Ment This from North
Flank Line Existing Clean Out 8.31 -2.62
12.5 W. of N.L. Atlantic

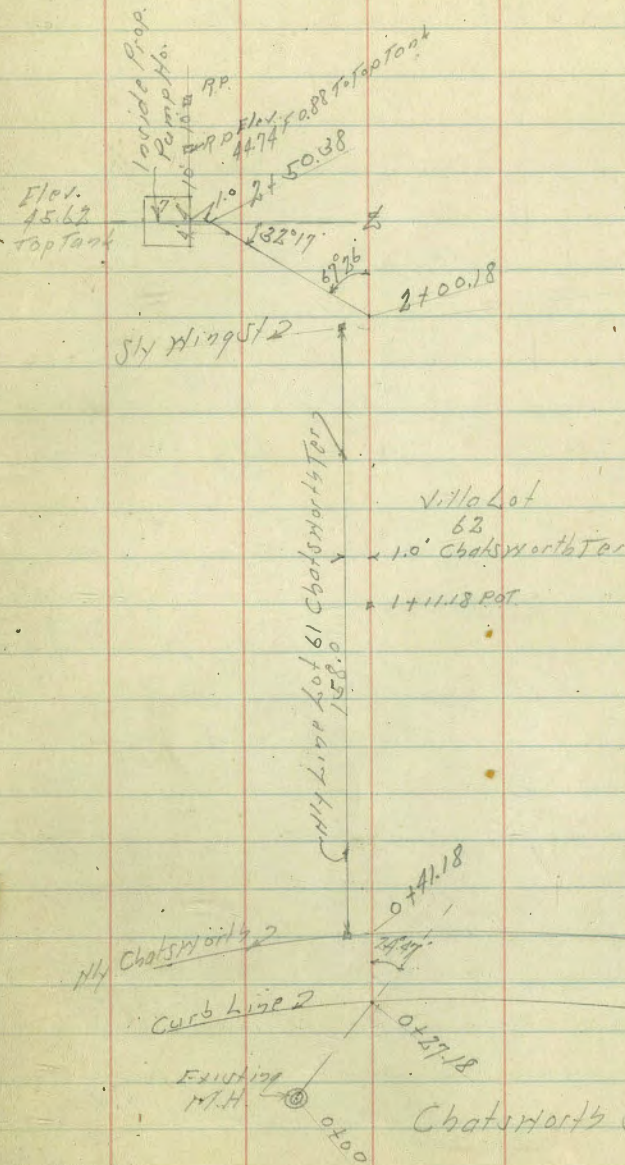
Proposed Sewer Through Villa Lot 62
Chatsworth Terrace

Indexed
C.S.K.

12-7-34
Moore
Sisson
Hartman

32

BM	7.83	81.76	78.93	S.F.B.P. Chatsworth 44 Jan 22 25
0+0	- Existing M.H.	3.92	78.34	
+27.18	Δ Lt 24°47' Gutter Topcb.	4.94	76.82	
+33.78	- 1/4 Conc Walk	3.95	77.81	
+41.18	- 1/4 Chatsworth	3.5	78.3	
+50		3.3	78.5	
+70		1.6	80.2	
+12		1.5	80.3	
+20		6.5	75.3	
TP	0.23	69.44	12.55	69.21
+30		1.7		67.7
+40		8.2		61.2
TP	0.22	59.02	12.64	56.80
+60		3.6		53.4
+80		9.4		47.6
2+00.18	Δ Lt 67°26'	12.8		44.2
+25		12.4		44.6
+51.38	- Inside Prop. Pump Ho.	12.4		44.6
BM		12.28		44.74



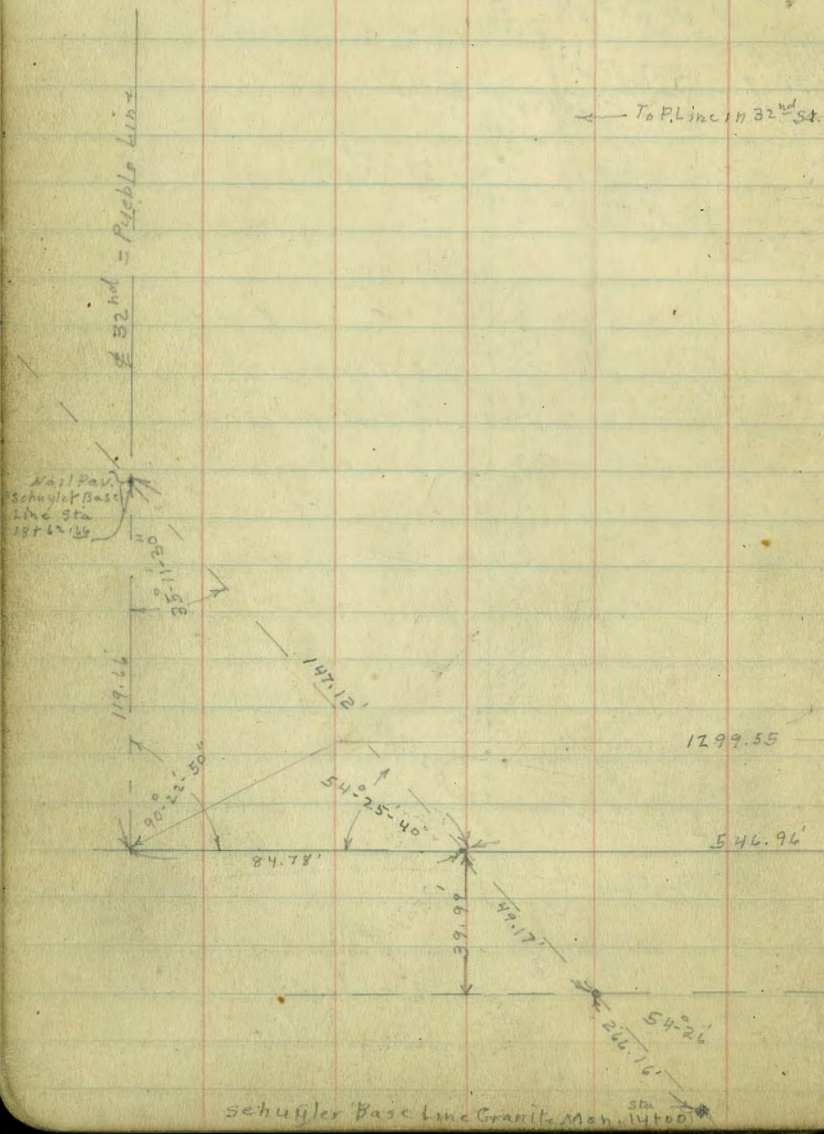
07/10' NRP
Hub
Prop. Pump Ho.

1-2-35
M.H.
W.H.
B.H.

Survey P.L. 1167.

Indexed
C.S.K.

To P. Line in 32nd St.



Schuyler Base Line Granite Mon. Sta. 14700

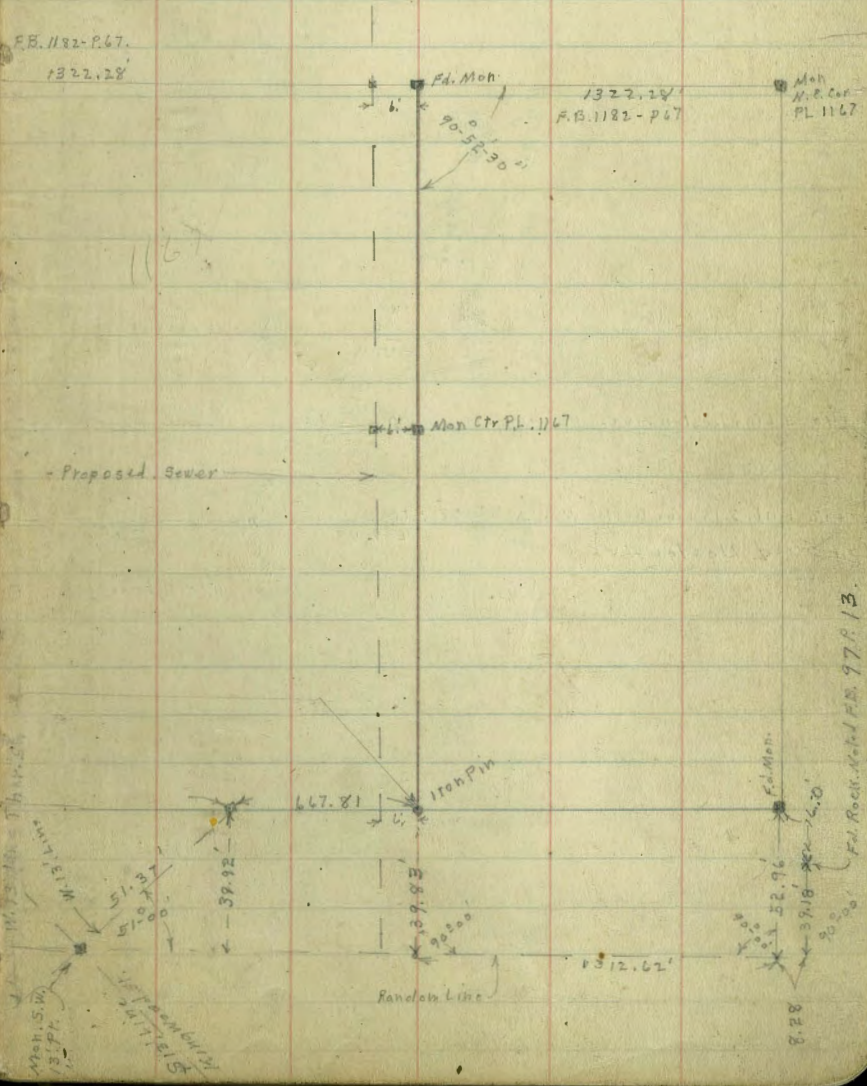
Plotted on the sheets.
C.S.K.

1-13 52.94

33

F.B. 1182-247.
1322.28

Proposed Sewer



F.d. Rock. Mon. Sta. 978.13

613.57

Plotted on tie sheets
e.s.k.

12+98⁵⁵ Hub. N. Line P.L. 1167 $\angle 0^{\circ}18'17''$

10+26⁷⁴

W. 13' Line S.W. 1/4

Men.
662.45
T.P. 12

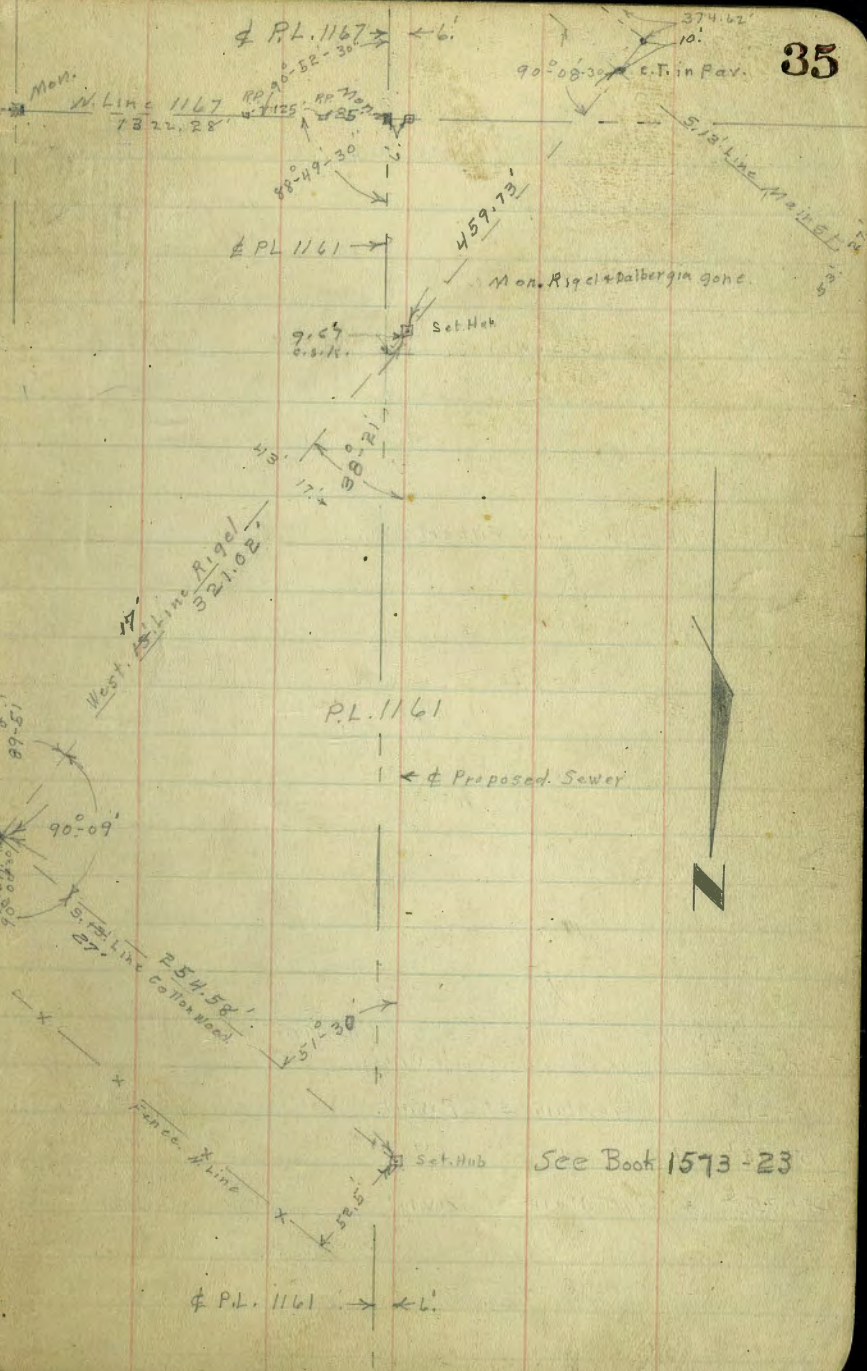
531
89-51

380.26

6+16⁵⁹ Hub. S. 13' Line Cottonwood St

Men.
90-04

S. 13' Line Black



23+36 P.I. Ex. 8" Sewer in Alley.

Plotted on tie sheets
c.s.k.

20+89 P.I. Ex. 16" Sewer

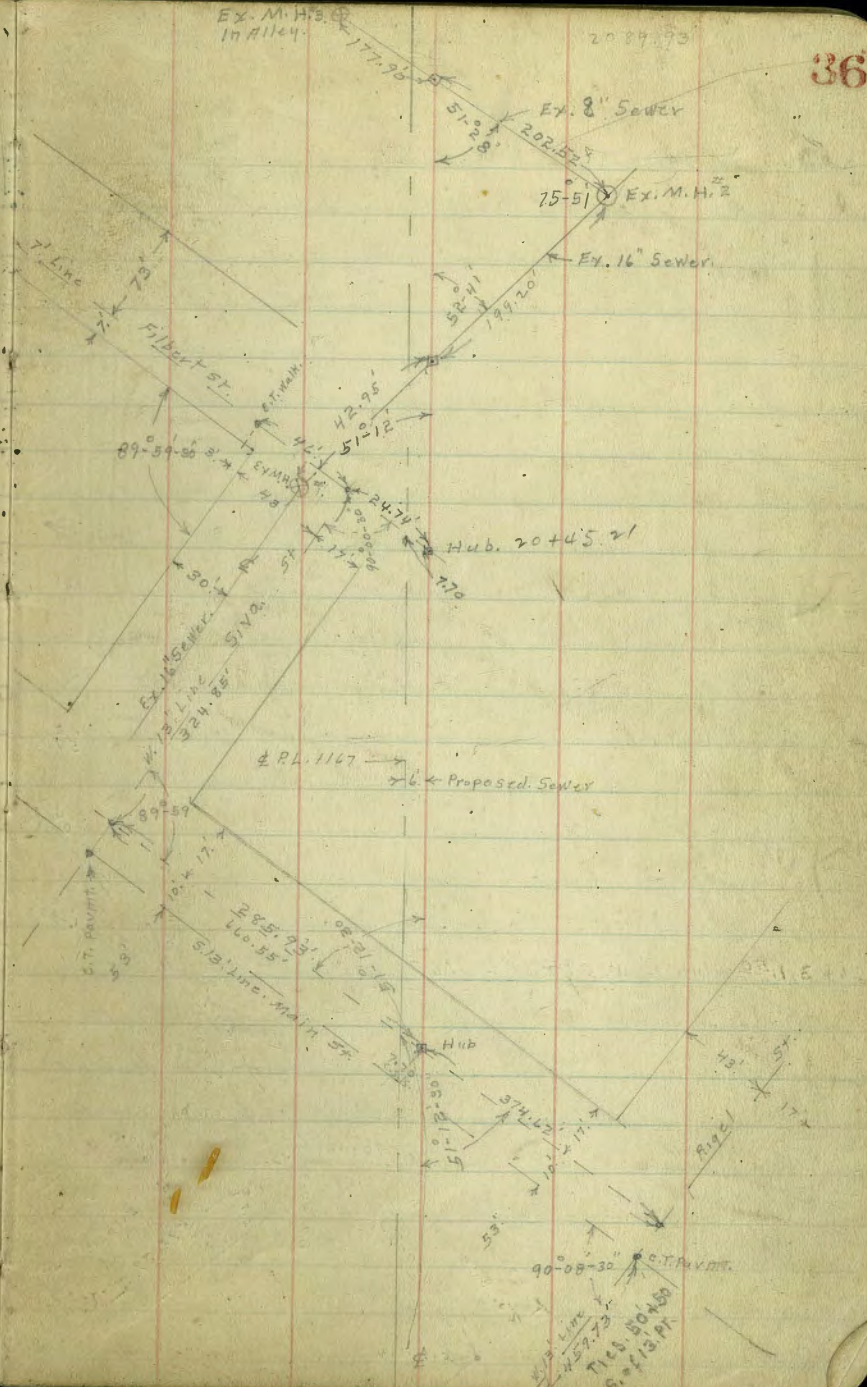
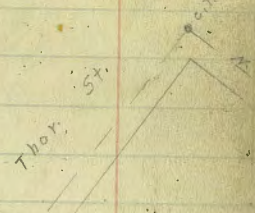
20+45 Hub. on N. 7' line Filbert St.

16+28 P.I. offset line 23' S. of Main St.

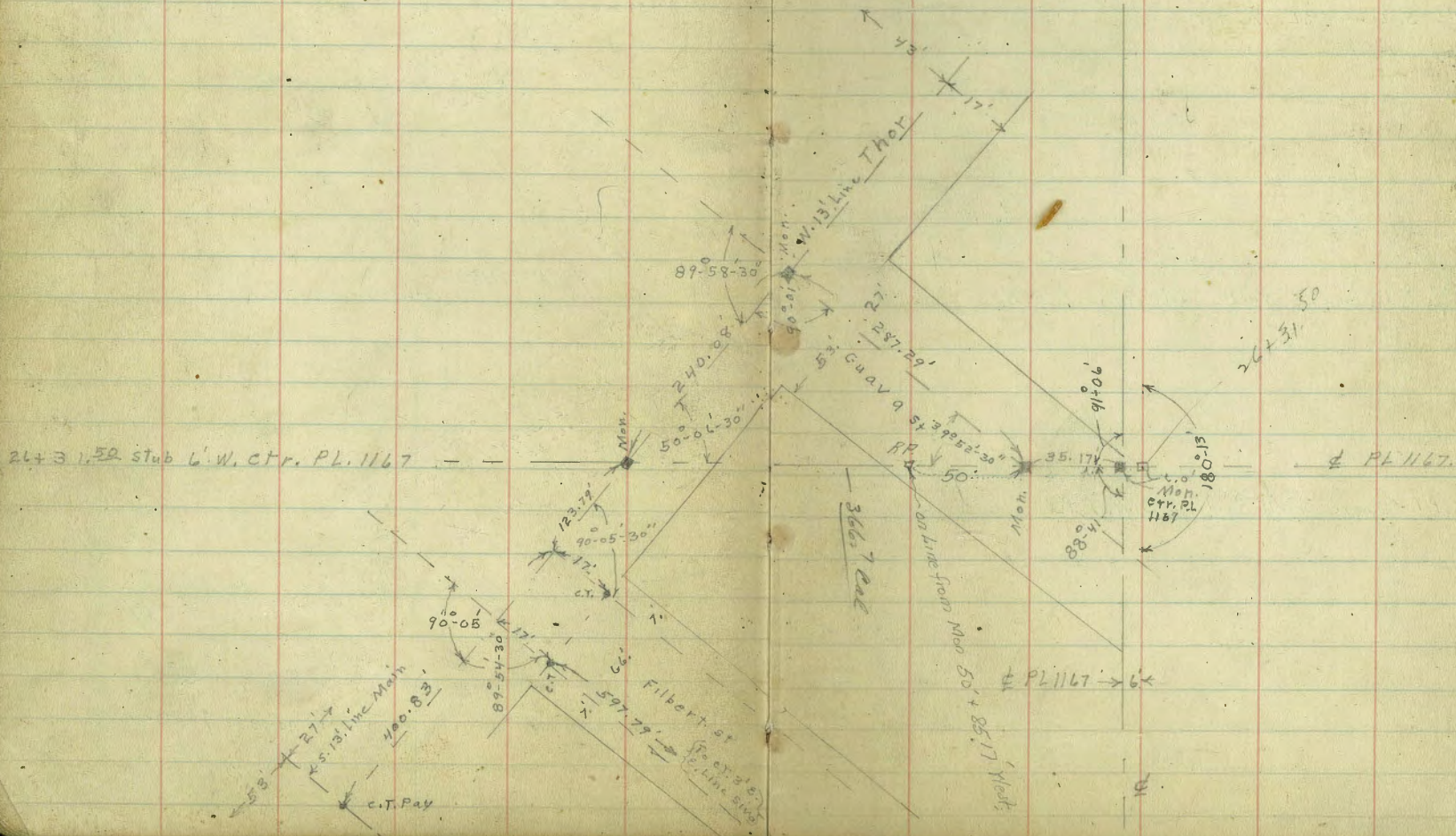
16+21 S. Edge Main St. Pavmt

15+98 S. " " " "

15+75 N. Edge Main St. Pavmt



Plotted on tie sheets.
c.s.Kr



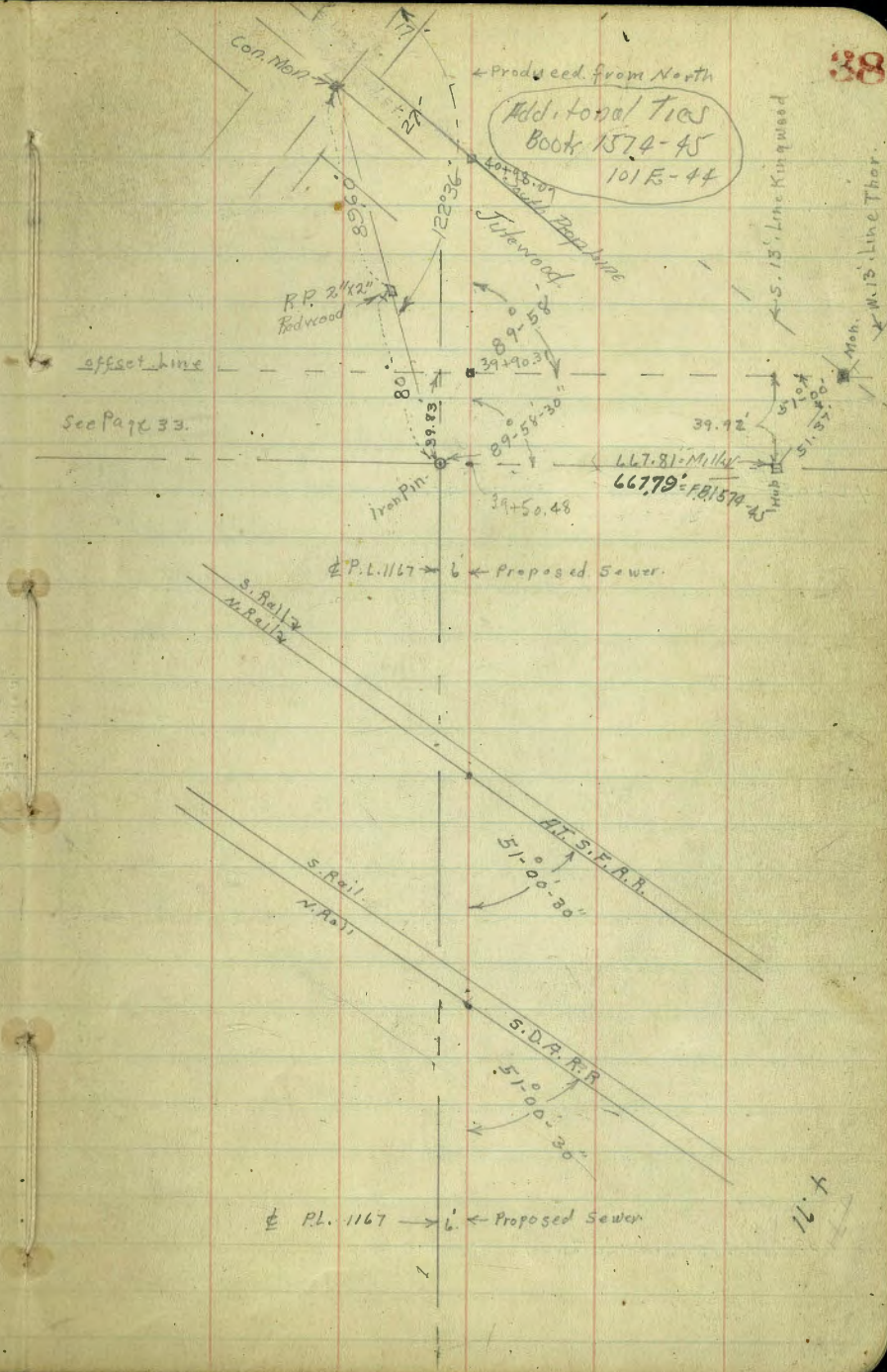
40+98⁰⁷ P.I. S. Line Jutewood St.

39+90²¹ Stub on offset line

39+50⁴⁸ S. Line P.L. 1167

38+75⁴³ P.I. Gauge North Rail A.T.S.F.R.R.

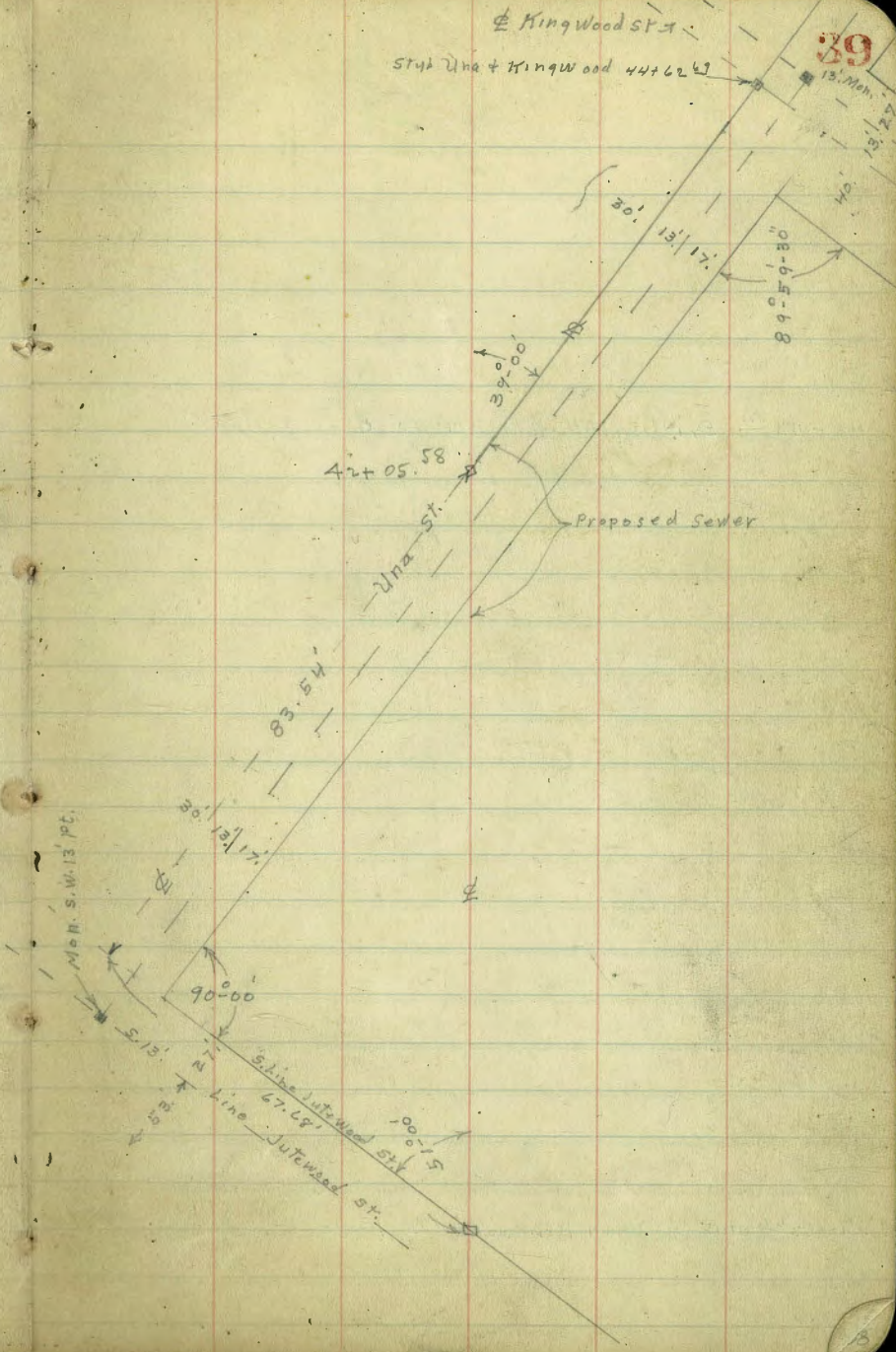
37+46²⁶ P.I. Gauge North Rail S.D.A.R.R.



42+05⁵⁸ stub of Una L 39°00' Rt.

Angle 38°06' R to MH
at Sta 48+43.34
Calc'n

40+98.02 P.I. S. Line Jutwood St. stub



Kingwood St.

Stub Una + Kingwood 44+62.43

39

13. Mem.

30.13'

41.11'

89.59'

39.00'

42+05.58

Proposed Sewer

Una St.

83.54'

30.13'

90°00'

Mem. S.W. 13' pt.

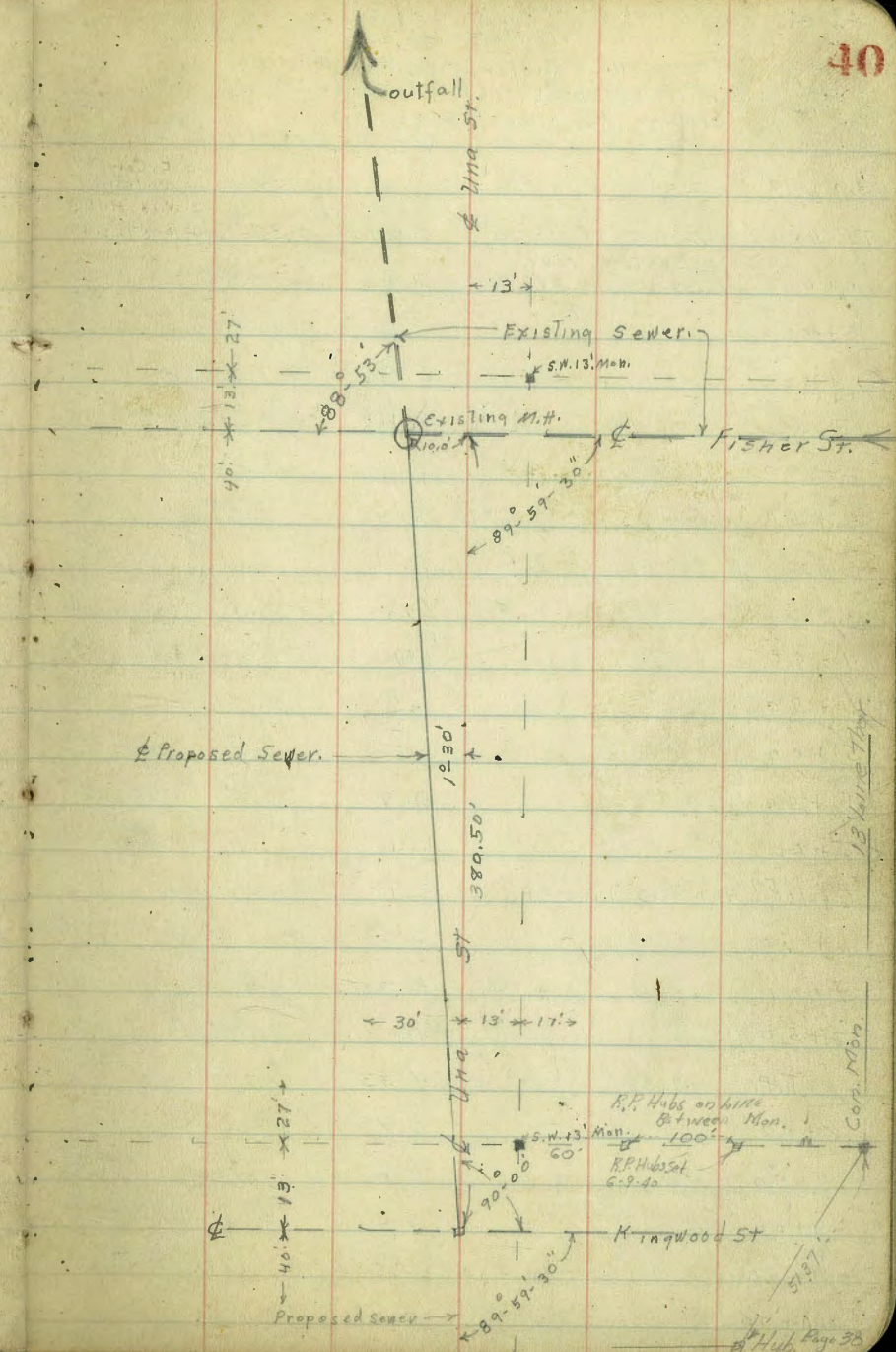
57.69'

S. Line Jutwood St.
47.69'

40+98.02

48+43³² Existing M.H. ϕ Fisher 10' E. of ϕ Una.

44+62⁶⁹ stub ϕ Una + Kingwood \angle 1° 30' Lt.



12 Kingwood

Cor. Man.

Hub Page 38

Prelim Sewer. L.W. of E of.
 Pueblo Lots 1161 + 1167.
 from 34th + Boston Ave to B14109.
 Partition Map. P.L. 1168. Proposed
 Sewage Treatment Plant.

B.M. B.P.	2.40	9.22	6.82	
T.P. 4x4	5.95	6.30	8.87	0.35
0+00 =	E Boston Ave 15.38' W. of E 34 th St.		4.8	1.5
0+50		5.8	0.5	
1+00		5.3	1.0	
1+50		5.6	0.7	
2+00		5.7	0.6	
2+50		5.5	0.8	
3+00		5.1	1.2	
3+50		5.8	0.5	
4+00		5.9	0.4	
4+50		6.0	0.3	
5+00		6.3	0.0	
5+50		5.9	0.4	
6+00		6.4	-0.1	
6+16 ⁵⁹	Hub 3.13. Line Cottonwood	6.10	0.20	
6+50		6.0	0.3	
7+00		5.7	1.1	
7+50		4.0	2.3	
T.P.	7.38	9.15	4.53	1.77
8+00		5.8	3.4	
8+50		6.0	3.2	
9+00		6.4	2.8	
9+50		6.5	2.7	
10+00		7.2	2.0	

S.E. Cor 34th
 + National
 S.W. 13th + Hub 34th
 + Boston

10+26 ²⁴	Hub. W. 13 th Line R. 9 cl.	8.25	+0.90
10+50		10.1	-0.9
10+75		10.7	-1.5
10+80	N.E. Side Cottonwood Drainage Ditch	11.5	-2.3
11+00		11.6	-2.4 -1.4 X
11+06	S.W. side Crt. Drainage Ditch	10.7	-1.5
11+19	Top Dyke	1.4	+7.8
11+23		5.1	4.1
11+50		7.2	2.0
12+00		7.8	1.4
12+50		8.1	1.1
12+98 ⁵⁵	Hub { S. Line P.L. 1161 N. Line P.L. 1167	8.14	0.97
13+50		8.1	1.1
14+00		8.2	1.0
14+50		8.2	1.0
15+00		8.4	0.8
15+25		8.5	0.7
15+50		7.1	2.1
T.P. Hub			
16+28 ⁴⁰	4.16 6.36	6.95	2.20
15+75 ⁵	N. Edge Main St. Pav	3.82	2.54
15+98 ²	" " " "	3.62	2.70
16+21 ⁸	S. " " " "	4.00	2.36
16+28 ⁴⁰	Hub on line 23' S. of Main St	4.16	2.20
16+32		4.2	+2.2
16+43		7.1	-0.7
17+00		7.6	-1.2

9.15^v Indexed
 8.15.14.

17+50	8.3	- 1.9	✓
18+00	8.0	- 1.6	✓
18+50	7.4	- 1.0	✓
19+00	7.3	- 0.9	✓
19+50	6.8	- 0.4	✓
20+00	6.8	- 0.4	✓
20+06	8.0	- 1.6	✓
20+32	7.2	- 0.8	✓
20+45 ²¹ Hub. N. 7' line Filbert.	6.31	+ 0.05	✓
20+89 ²³ Hub. Ex. 16" Sewer.	5.72	0.94	✓
Ex. M.H. #1 { 42.95 to Lt. of 20+89 ²³ on E. line Filbert St. " & Siva. }	6.69	- 0.33	Top. M.H.
	15.61	- 9.25	FL.
Ex. M.H. #2 199.20 to Rt. of 20+89 ²³	6.78	- 0.42	Top. M.H.
	16.34	- 9.98	FL.
21+00	5.1	1.3	✓
21+50	5.5	0.9	✓
21+78	4.1	0.3	✓
21+88	0.0	6.4	✓
T.P.	8.12	14.18	✓
22+00	6.5	7.7	✓
22+50	5.4	8.8	✓
23+00	5.1	9.1	✓
23+36 ⁸⁸ P.I. Ex. B" Sewer Stub 14' Alley.	5.70	8.48	✓
177.9' to ht. of 23+36 ⁸⁸ - Ex. M.H. #3	6.42	7.76	Top. M.H.
	20.17	- 6.29	FL.

14.18

23+50	5.1	9.1	✓		
24+00	5.2	9.0	✓		
24+50	4.8	9.4	✓		
25+00	3.5	10.7	✓		
25+25	2.9	11.3	✓		
25+40	1.6	12.6	✓		
25+50	1.9	12.3	✓		
25+75	1.2	13.0	✓		
T.P.	6.23	19.69	0.72	13.46	✓
26+00	5.4	14.3	✓		
T.P.	6.01	21.94	3.76	15.93	Mon. Ctr. P.L. 1167.
CHK. B.M. SW. 13' Man. Filbert + T. Hor.	11.77	10.17	= 10.18	✓	
26+31.50 Hub. C. W. of Man. ctr. P.L. 1167.	6.29	15.65	✓		
26+50	6.0	15.9	✓		
27+00	5.6	16.3	✓		
27+50	5.5	16.4	✓		
28+00	5.9	16.0	✓		
28+50	6.2	15.7	✓		
29+00	6.9	15.0	✓		
29+50	6.7	15.2	✓		
30+00	7.3	14.6	✓		
30+50	8.1	13.8	✓		
T.P.	0.50	14.81	7.63	14.31	✓
31+00	2.0	12.8	✓		
+50	2.4	12.4	✓		

32+00	2.6	12.2 ✓
+50	3.4	11.4 ✓
33+00	3.9	10.9 ✓
+50	4.9	9.9 ✓
34+00	5.4	9.4 ✓
+50	6.0	8.8 ✓
35+00	6.6	8.2 ✓
+50	7.6	7.2 ✓
36+00	8.1	6.7 ✓
+32	9.0	5.8 ✓
+50	7.3	7.5 ✓
+57	10.2	4.6 ✓
37+00	11.4	3.4 ✓
+32	10.8	4.0 ✓
+37	12.2	2.6 ✓
+46	10.2	4.6 ✓
+46.24 N. Rail S.D. A	9.57	5.24 ✓
+62	12.0	2.8 ✓
+70	9.5	5.3 ✓
+85	10.6	4.2 ✓
38+00	10.5	4.3 ✓
+50	10.2	4.6 ✓
+58	9.3	5.5 ✓
+71	5.1	9.7 ✓
+75.67 N. Rail A.T.S.F.	4.48	10.33 ✓
+85	5.1	9.7 ✓

39+00	10.3	4.5 ✓
T.P. 7.95 13.03 ✓	9.73	5.08 ✓
39+50.48 S. Line P.L. 1167	9.4	3.6 ✓
40+00	9.6	3.4 ✓
+50	9.5	3.5 ✓
+98.02 S. Line Jute Wood stub	9.31	3.72 ✓
41+50	8.6	4.4 ✓
42+05.58 stub	7.83	5.20 ✓
42+50	5.2	7.8 ✓
43+00	4.6	8.4 ✓
+50	3.5	9.5 ✓
44+00	4.2	8.8 ✓
44+62.69 stub of Una + Kingwood	4.54	8.99 ✓
45+00	4.5	8.5 ✓
+10	4.9	8.1 ✓
+50	4.9	8.1 ✓
46+00	5.3	7.7 ✓
+50	5.4	7.6 ✓
47+00	5.8	7.2 ✓
+50	6.1	6.9 ✓
48+00	6.3	6.7 ✓
+50	6.5	6.5 ✓
48+43.22 S.E. of Una. E.V. M.H. & Fisher St.	6.9	6.1 ✓ ground.
48+43.22 " " " "	7.14	5.89 ✓ M.H. Rim.
48+43.22 T.P. S.W. 13' M.H. " " F.L.	22.81	-9.78 = -9.92 ✓ Cons. Notes
Una + Fisher	5.05	10.89 7.19 5.84 ✓

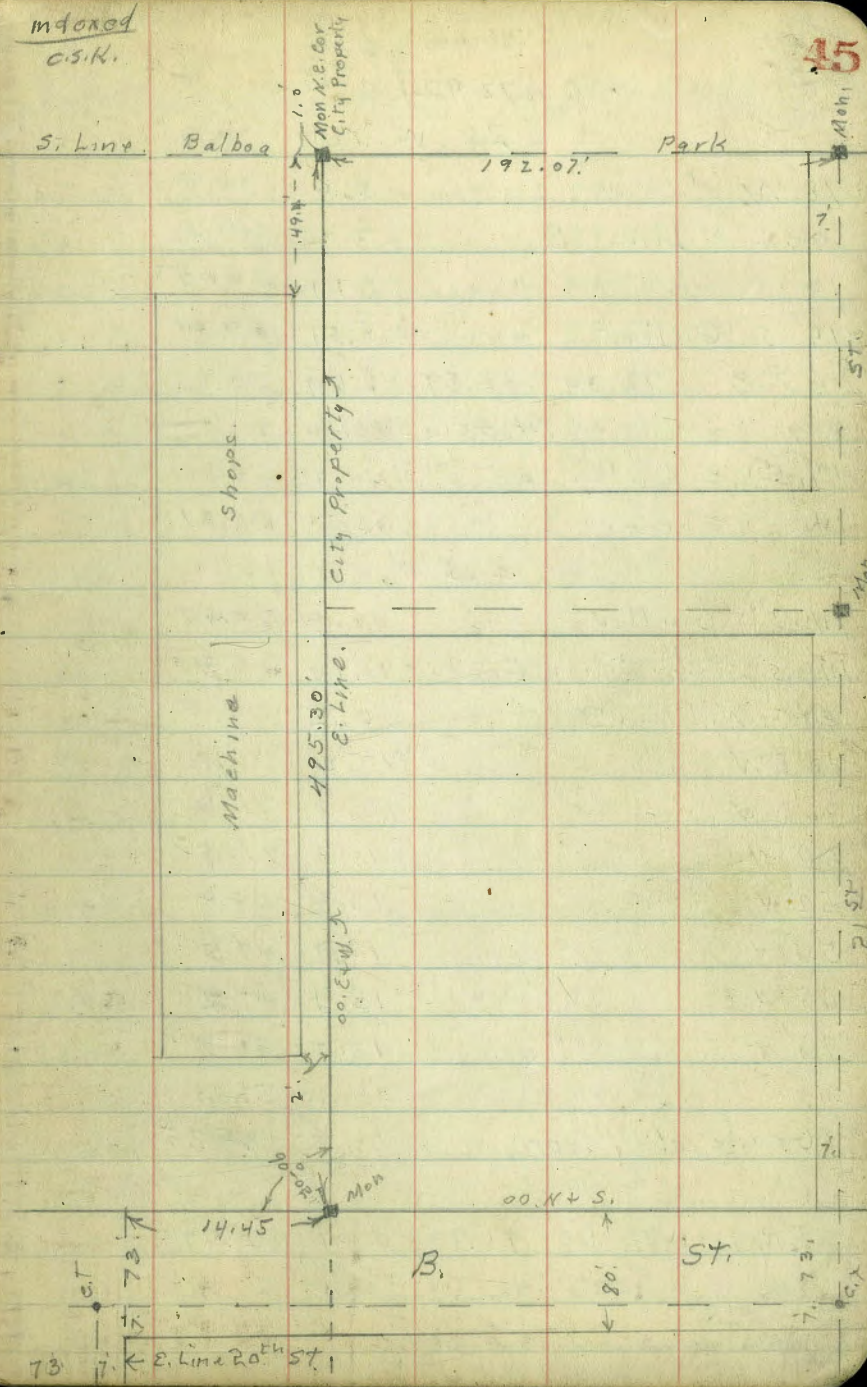
10.89 ✓

T.P. S.W. 13. MoH	2.73	8.13 ✓	5.49	5.40 ✓	Thor + Fisher
B.M. B.P.			5.95	2.18 ✓	S.W. 32nd Fisher
				2.13	

6-26-35
 Miller
 Walter
 Blair

Contours BJK 12 Culverwell
 Area e. of City Barns.
 0+00 N + S. = N. Line B. St.
 0+00 E + W. = E. Line City Property.

R.M. B.P	0.96	71.19	70.23	8.E. 20 th + B Sts.
76'. W. = Existing asphalt Pavmt.				
300' N.		6.85	64.34	
250' N		7.31	63.88	
200' N		7.20	63.99	
175' N		6.70	64.49	
150' N		6.24	64.91	
100' N		5.82	65.37	
50' N		5.34	65.81	
00' N = N Line B		4.60	66.59	
14' S. Gutter		4.97	66.22	
T.P.	2.69	72.92	0.96	70.23
52'. W. = W. Side Machine Shops.				
Grade of flood			65.15	
28.5' W.				
14.5' S = Gutter		5.52	67.40	
00 = N Line B.		5.09	67.83	
18' N.		5.00	67.92	
36' N		4.90	68.02	
52' N		5.36	67.56	
78' N	5' End. Shop.	4.10	66.9	
28' W.				
56' N.		5.4	67.5	
52' N		3.4	69.5	
36' N		3.0	69.9	



72.92

28' W. con

18' N	3.0	69.9
00 = N line B	3.2	69.7
14' S. ch	3.27	69.05
14' S Gutter	5.51	67.41
T.P.	12.34	82.57
	2.69	70.23

14.5' W = E. line 20th

14' S. = Gutter	14.56	68.01
14' " = ch.	12.36	70.21

2.5' W.

14' S = Gutter	12.08	70.49
14' S = ch. Brkin Grade	11.60	70.97
00 = N. line B.	10.2	72.4
18' N	10.4	72.2
36' N	10.8	71.8
50' N	11.3	71.3
52' N	13.8	68.8
54' N	15.1	67.5
65' N.	15.4	67.2
78' N. S. End. Shops.	15.7	66.9

2' W. = E. Sid. Shops

Grade of floor 65.35

T.P.	14.60	96.90	0.27	82.30
------	-------	-------	------	-------

96.90

14' S. of N. line B. st. = N. ch. line

46

25' E Gutter	19.60	77.30
25' E cnt. ch	19.26	77.54
50' E. Gutter	13.50	83.40
50' E cnt. ch	13.00	83.90
75' E. Gutter	7.30	89.60
75' E cnt. ch.	6.95	89.95
100' E. Gutter	1.20	95.70
100' E. cnt. ch.	0.80	96.10

0+00 = N. line B.

100' E	0.8	96.1
75' "	7.2	89.7
50' "	13.3	83.6
25' "	19.3	77.6
13' E	22.4	74.1
00 E & W.	24.4	72.5

18' N of 00

00 E & W.	24.5	72.4
25' E	23.0	73.9
50' E	20.3	76.6
75' E	17.2	79.7
100' E	12.0	84.9
125' E	7.0	89.9
150' E.	2.0	94.9

96.90
30' N of 0100

150' E	7.6	89.3
125' E	13.3	83.6
100' E	16.0	80.9
75' E	17.8	79.1
50' E	20.6	76.3
25' E	22.0	74.9
0+00 E+W	24.8	72.1

45' N of 00

0400 E+W	25.3	71.6
25' E	23.0	73.9
50' E	21.3	75.6
75' E	18.3	78.6
100' E	15.8	81.1
125' E	15.0	81.9
125' E	12.1	84.8
150' E	7.7	89.2

80' N of 0100

150' E	0.0	96.9
125' E	10.0	86.9
100' E	18.0	78.9
75' E	19.1	77.8
50' E	22.8	74.1
25' E	23.7	73.2
00 E+W	25.7	71.2

T.P.	0.27	82.57	14.60	82.30
T.P.	12.38	86.97	8.84	73.69

86.07
140' N of 00

00 E+W	18.4	67.7
25' E	17.0	69.1
50' E	16.4	69.7
75' E	15.5	70.6
100' E	14.8	71.3
125' E	9.0	77.1
150' E	2.0	84.1
175' E	+7.3	93.4
192' E	+13.2	99.3

200' N of 00 = 200' N of Line B

192' E	+1.6	87.7		
175' E	5.4	80.7		
150' E	11.7	74.4		
125' E	16.6	69.5		
100' E	17.6	68.5		
T.P.	4.54	78.23	12.38	73.69

75' E	10.7	67.5
50' E	11.0	67.2
25' E	12.2	66.0
00 E+W	12.8	65.4

250' N of 0100

0+00 E+W	12.7	65.5
25' E	12.9	65.3
50' E	12.8	65.4
75' E	12.0	66.2
100' E	11.5	66.7

125' E			11.2	67.0	
150' C			8.8	69.4	
175' E			5.0	73.2	
192' E			1.8	76.4	
	300' N. of 0100	= S. line	A. St		
192' E			7.2	71.0	
175' E			9.1	69.1	
150' E.			11.8	66.4	
125' E			12.0	66.2	
100' E			12.0	66.2	
75' C			12.0	66.2	
50' E			12.4	65.8	
25' E			12.5	65.7	
00 E+W			13.1	65.1	
T.P.	574	79.43	4.54	73.69	
orig BM			9.21	70.22	70.23

xsec of Poe St
Willow to 200' Ely.

70' wide
18' cbs
8.5' 1/4"

Howe
12-18-34

indexed
c.s.Kr

18738

SWBP	959	187.38	172.79	Willow 200	S	0+03	3.7	183.7
					cb		2.8	184.6
	0-10				1/4		2.1	185.3
S top cb		8.78	178.60		+7		1.9	185.5
S gut		9.59	177.79		C		8.0	179.4
cb pav.		8.70	178.68		1/4		8.5	178.9
1/4 "		8.46	178.92		cb		8.2	179.2
C "		8.29	179.09		N		5.0	182.4
1/4 "		8.15	179.23			0+25		
cb "		8.01	179.34		N		4.1	183.3
N gut		8.23	179.15		+15		6.8	180.6
N top cb		7.45	179.93		cb		10.2	177.2
	0+00 Ely Willow				1/4		10.3	177.1
N		6.4	180.98		C		10.3	177.1
+10 = Top end cb		7.30	180.08		+1		4.0	183.4
+10 = gut		8.07	179.31		1/4		4.3	183.1
cb pav.		8.06	179.32		cb		5.0	182.4
1/4 "		8.17	179.26		S		5.7	181.7
C "		8.25	179.13			0+50		
1/4 "		8.43	178.95		S		11.4	176.0
cb "		8.67	178.71		cb		10.5	176.9
+8 gut		8.95	178.43		1/4		9.2	178.2
+8 top cb		8.20	179.18		C		8.8	178.6
S		8.4	179.0		+1		12.6	174.8
					1/4		12.8	174.6

187.38

175.68

50

Npb		12.3	175.1	
+V		8.1	179.3	
N		7.5	179.9	
	0+60			
N		9.6	177.8	
+13		9.7	177.7	
cb		12.6	174.8	
1/4		12.8	174.6	
+7		12.4	175.0	
C		10.6	176.8	
1/x		11.8	175.6	
cb		12.8	174.6	
J		14.3	173.1	
	0+85			
-10		21.7	165.7	
J		21.2	166.2	
cb		19.7	167.7	
1/x		14.7	172.7	
C		12.3	175.1	
1/4		12.9	174.5	
cb		12.9	174.5	
N		11.1	176.3	
+5		11.5	175.9	
T.P.	133	175.68 ^v	13.03	174.35

		1700		
-10			5.1	170.6
N			4.8	170.9
cb			2.8	172.9
1/4			3.8	171.9
C			4.2	171.5
1/x			8.5	167.2
cb			11.4	164.3
S			13.2	162.5
+15			14.7	161.0
		1720		
-15			19.5	156.2
S			18.5	157.2
cb			16.3	159.4
1/x			15.8	159.7
C			14.5	161.2
1/4			12.7	163.0
cb			12.2	163.5
N			11.1	164.6
+10			10.5	165.2
		1729 top cut to N.		
-10			12.9	162.8
N			13.1	162.6
T.P.	0.88	163.78	12.78	162.90
cb			3.5	160.3
1/4			4.8	159.0

163.78

C	5.6	158.2
1/4	6.2	157.6
cb	6.9	156.9
V	8.7	155.1
+20	9.9	153.9
1+35 bot. cut to N		
S-20	11.5	152.3
S	10.1	153.7
cb	8.6	155.2
1/4	8.2	155.6
C	7.3	156.5
1/4	6.2	157.6
cb	5.0	158.8
+8	4.8	159.0
N	7.0	156.8
+50	7.1	156.7
1+65 Shoulder fill to N.		
N-50	7.4	156.4
N	9.2	154.6
+7	10.2	153.6
cb	15.5	148.3
1/4	16.5	147.3
C	17.1	146.7
1/4	17.7	146.1
cb	18.3	145.5
S	19.3	144.5

163.78

51

S+20		20.3	143.5		
T.P.	0.92	151.63	130.7	150.71	
1+35 Top fill to N					
S-20		16.2	135.4		
S		14.1	137.5		
cb		13.5	138.1		
1/4		13.5	138.1		
C		13.7	137.9		
1/4		12.7	138.9		
cb		12.1	139.5		
N		10.8	140.8		
+20		6.7	144.9		
-2+00					
-20		14.0	137.6		
N		15.7	135.9		
cb		17.9	133.7		
1/4		18.8	132.8		
C		19.0	132.6		
1/4		19.1	132.5		
cb		19.8	131.8		
S		20.5	131.1		
+20		20.7	130.9		
T.P.	12.76	163.47	0.92	150.71	
T.P.	12.51	175.74	0.24	163.23	
T.P.	10.35	181.59	0.50	175.24	
check to BM			7.80	177.79	177.79

xsec Alley 20 wide
 BIK 25 Ft. Loma HTS.
 Between Santa Barbara + Guizote
 Narrogansett + Del Monte

Flora
 12-20-24
 indexed
 C.S.K.

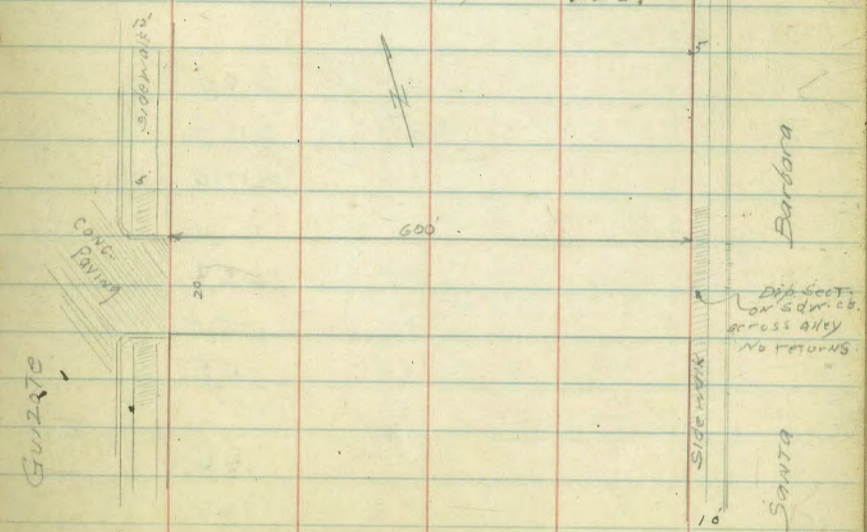
31.08

52

NEBP	q13	237.61	237.48
T.P.	298	231.08	228.10
	0-10		
S	Top 16	240	228.68
S	CONC. gut	342	27.66
N	"	462	26.46
N	Top 16	362	27.46
	opp nly Santa Barbara		
N	conc sdw	348	27.60
C	"	330	27.78
S	"	216	228.92
	0+10		
S		1.5	229.6
C		2.2	28.9
N		3.0	28.1
	x50		
N		3.90	27.2
C		4.1	28.0
S		2.3	28.8
	1+00		
S		3.4	27.7
C		4.0	27.1
N		4.5	226.6

Santa Barbara
 Del Monte

	1450		5.7	225.4
			5.2	259
			4.7	264
	1+61			
S	-20 Sing. garage floor	310		280 227.22
	2+00			
S			6.2	24.9
C			6.7	24.4
N			7.2	23.9
	2+50			
N			8.8	22.3
C			8.0	23.1
S			7.7	223.4



Del Monte

231.08

3+00

S	9.5	221.6
C	9.6	21.5
N	9.9	21.2

3+50

N	11.6	19.5
C	10.9	20.2
S	10.7	20.4

4+00

S	12.6	18.5
C	13.0	18.1
N	13.4	217.7

T.P.	1.39	219.33	131.4	217.94
------	------	--------	-------	--------

4+50

N	3.3	216.0
C	2.9	216.4
S	2.3	217.0

5+00

S	3.9	215.4
C	4.3	15.0
N	4.8	14.5

5+50

N	5.9	13.4
C	5.6	13.7
S	5.3	214.0

219.33

5+75

S	5.6	213.7
C	6.6	12.7
N	6.6	212.7

6+00 Ely Guizot

N	Top ob	9.8	209.75
N	par	9.7	209.61
C	par	9.9	209.36
S	par	9.8	209.92
S	Top ob	8.9	210.39

T.P.	9.7	219.03	10.0	209.31
check to SWB	²⁰¹⁷⁰⁰⁰⁰ Guizot	1.0	218.01	215.03

53

Photocopy

Levels on Muir St. Paving
W of Abbott St.

Moors
12-20-24

Indexed
c.s.k.

8.35

54

NWBP 0.41 = 8.35 1.94

Muir
Abbott

S cb 7.6 0.8

1/4 7.6 0.8

+3 7.6 0.8

N Top cb 7.00 1.35

C 6.5 2.2

N gutter par 7.63 0.72

1/4 4.9 3.5

1/4 " 7.43 0.82

N cb 3.9 4.5

C " 7.51 0.84

1/4 " 7.57 0.78

N cb 6.8 1.6

S gutter " 7.72 0.63

1/4 7.2 1.2

S Top cb 7.07 1.28

C 7.9 0.5

3+25 = w/ly expanding

1/4 7.8 0.6

S Top cb 7.15 1.20

S cb 7.6 0.8

S gut par. 7.80 0.55

4+25 = High tide 1.00

1/4 " 7.85 0.50

S cb 8.0 0.4

C " 7.90 0.45

1/4 7.9 0.5

1/4 " 7.82 0.53

C 8.0 0.4

N gut " 7.80 0.55

1/4 8.0 0.4

N Top cb 7.07 1.28

N cb 7.8 0.6

3+50

N cb 5.0 3.4

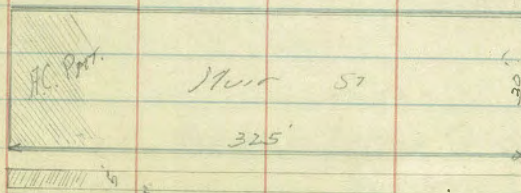
1/4 5.2 3.2

C 6.1 2.3

1/4 7.3 1.1

S cb 7.5 0.9

Sidewalk



St.

Abbott

1-15-36
Miller
Walker
Bliss

X See Alley BIK 48 W.D. Herbert's Add
E + W. Alley

B.M. BP 3.96 371.68 367.72 S.W. El Cajon
+ 39th St.

10' W. of E. Line 39th St. = E. Curb Line

S-25	Top. curb.	4.70	366.98
S-25	gutter pav	5.31	366.37
S.	" " "	4.62	367.06
S	Top. ch	5.18	366.50
±	pav	5.05	366.63
+75=N	gutter pav	5.11	366.57
+75=N	Top. ch.	4.64	367.04
N+25	" "	4.57	367.11
N+25	gutter pav	5.10	366.58
N+50	" "	4.96	366.72

0+00 = E. Line = 39th St.

N. E. End	Top. ch.	4.63	367.05
N. E. End	pav	4.94	366.74
±	" "	4.84	366.79
+75=S	" "	4.77	366.91
+75=S	E " Top. ch.	4.44	367.20

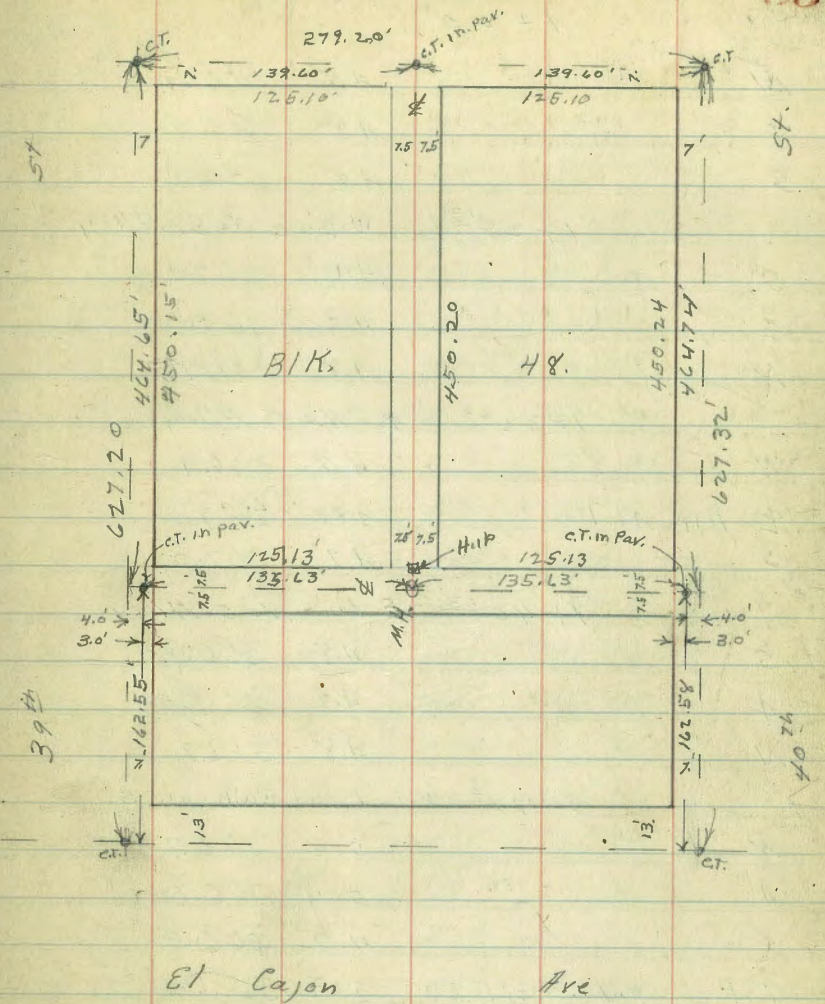
0+50

S	4.5	367.2
±	4.5	367.2
N	4.5	367.2

Indexed
C.S.K.

Meads Ave

55



Recorded on Tie Rints Sheets 3572-73

9/18/42

(Next Cross Sections FB 1658-P-77)
Sept. 25-1945

371.68

1+00

N	4.8	366.9
⊕	4.8	366.9
S	4.8	366.9

1+25¹³ = W. line N+S. Alley

S	4.6	367.1
⊕	4.7	367.0
N	4.8	366.9

1+32⁶³ = ⊕ N+S. Alley

N	4.8	366.9
⊕ Rim M. 11	4.80	366.9
S	4.7	367.0

1+40¹³ = E. Line N+S. Alley.

S	4.8	366.9
⊕	4.7	367.0
N	4.8	366.9

1+77³ = W. End. cmt. Walk, on S.

N	5.0	366.7
⊕	5.1	366.6
S	4.9	366.8

T.P. = N 4.94 371.60 5.02 366.66

+1.9 = N. Edge cmt. Walk 4.57 367.11

2+00

S-1.9 = N. Edge cmt. Walk,	4.59	367.01
S.	4.7	366.90
⊕	4.8	366.80
N	4.8	366.8

371.60

2+41⁴⁰ = Jog. in cmt. walk on S

N	4.8	366.8
⊕	5.0	366.6
+7.3 ground	4.7	366.9

+7.3 N. edge walk to E.	4.40	367.20
+7.5 = S on walk	4.40	367.20
+1.8 N edge walk to E. W	4.36	367.24

2+47.4 = E. End. cmt. walk on S.

S. on walk	4.30	367.30
+0.2 N. edge E. End. cmt. walk	4.30	367.30

+0.2 ground 4.7 366.9

⊕ 5.0 366.6

N 4.8 366.8

2+65²⁶ = W. line 40⁷⁶ ST.

N Top. cb. W. end. 4.76 366.84

N gutter Pav. " " 4.94 366.66

⊕ " " " 5.14 366.46

S " " " 5.00 366.60

S Top. cb. " " 4.91 366.69

10' E = W. cb. line

S-45 Top. cb. 5.18 366.42

S-45 gutter Pav. 5.74 365.86

S " " 5.66 365.94

S Top. cb. 5.09 366.51

⊕ Pav. 5.64 365.94

N gutter " 5.64 365.94

N Top. cb. 5.05 366.55

N+45 " " 4.94 366.64

N+45 Gutter Pav. 5.55 366.05

56

371.60
N + S. Alley

T.P. 5.70 372.61 4.69 366.91

0+00 = N. line + E + W. Alley.

E 4.7 366.9

Φ 4.7 366.9

W. 4.7 366.9

0+50

W 6.0 366.6

Φ 5.4 367.2

E 5.8 366.8

0+75

E 5.8 366.8

Φ 5.8 366.8

W 5.9 366.7

1+00

W 5.4 367.2

Φ 5.4 367.2

E 5.6 367.0

1+15

E 5.6 367.0

Φ 5.2 367.4

W 5.2 367.4

1+50

W 5.7 366.9

Φ 5.8 366.8

E 5.7 366.9

372.61

1+79⁵⁰ = S. End Double Garage on W. ent. floor 3.0' Back

E 5.5 367.1

Φ 5.6 367.0

W 5.4 367.2

+0.1 = E. edge ent. Apron 5.39 367.22

+3.0 = ent. floor 5.15 367.46

1+98.50 = N. End. above garage

W-3.0 ent. floor 5.05 367.56

W-0.1 E. edge ent. apron 5.36 367.24

W 5.3 367.3

Φ 5.3 367.3

E 5.3 367.3

2+00 = S. edge ent. walk from W.

5.3 W. of Φ = { S. Edge } ent. walk 5.28 367.33

7.5 " " " = W. 5.08 367.53

2+02 = { N. Edge above walk }
{ S. End. ent. walk on W. }

W. = N. edge above walk 5.04 367.53

+1.6 = E. edge S. End. ent. walk 5.20 367.41

2+06.20 = { N. End. above walk }
{ S. " Double garage on W. ent. floor 0.6 Back }

W-0.6 ent. floor of Garage 4.90 367.71

W. on ent. apron 4.94 367.67

+1.6 = E. Edge N. End. ent. walk 5.13 366.48

+2.2 = E. " S. " ent. apron 5.16 367.45

Φ 5.0 367.6

E 5.0 367.6

57

372.61
 2+24.50 { N. End. Double garage on W.
 S. " " cmt. walk on W.

E 5.0 367.6
 ♀ 5.0 367.6
 + 5.2' = E. Edge { cmt. walk
 cmt. apron 5.14 367.47
 W apron & walk 4.87 367.74
 + 0.6 = cmt. floor 4.82 367.79

2+29 = Jog in E. Edge of cmt. walk on W.

W = E. edge of walk to N 4.65 367.96
 W + 2.6 = E. Edge " to S. 4.88 367.73

2+45'

W = E. Edge cmt. walk 4.64 367.95

2+48.3 = N. End. cmt. walk on W
 S. " " cmt. steps + porch on W 4.6' in Allen

W. on walk 4.62 367.99
 + 0.6 E. = E. edge walk 4.62 367.99
 ♀ 4.7 367.9
 E, 4.9 367.7

2+57.5 = N. End cmt. Porch on W.

T.P. 5.12 373.18 4.55 368.06

2+65.4 = S. Edge cmt. walk on W.

1.6 E. of W. line = { S. edge }
 { E. End } walk

{ N. Edge Walk. on W. 5.16 368.02
 S. End. Triple Garage on W. cmt. floor 0.3' Back
 2+69 = { S. " " " " " " " " 7.2' " " "
 E-7.2' = cmt. floor 4.97 368.21
 E-5.1' = W. edge cmt. apron 5.15 368.03
 E 5.3 367.9

♀ 5.2 368.10
 + 6 = { E. edge N. End walk.
 E. edge cmt. apron 5.16 368.02
 W. on cmt. apron 4.96 368.22
 + 0.3 cmt. floor 4.91 368.27
 2+98 { N. End. Triple garages on E & W.
 S. side cmt. walk on W.

W-0.3 cmt. floor 4.98 368.20

W. on cmt. apron. 5.04 368.14

+ 1.5 = { E. Edge cmt. apron
 E. End. " walk. 5.14 368.04

♀ 5.1 368.1

E 5.2 368.0

+ 5.1 5.10 368.08

+ 7.2' 4.98 368.20

2+99.8 = W. Edge cmt. walk.

1.5 E. of W. = { E. End }
 { W. Edge } walk 5.12 368.06

3+50

E-0.5 = W. End. ♀ cmt. Walk, 4.88 368.30 2' Wide

E 4.7 368.5

♀ 4.7 368.5

W 4.9 368.3

T.P. 5.04 373.39 4.83 368.35

3786 = S. Side double garage on W. cmt floor 4.8 Back

W-4.8	cmt. floor.	4.57	368.82
W-1.4	E. Edge cmt. apron	4.80	368.59
W.		4.9	368.5

3798 N. Side above garage

W-4.8	cmt. floor	4.50	368.89
W-1.4	E. edge cmt. apron	4.73	368.66
W		4.8	368.6
±		4.9	368.5
E		4.8	368.6

4702 = S. Side garage on E. cmt. floor 4' Back

E-4	= cmt. floor	4.22	369.17
E = W. End	cmt. apron	5.20	368.19
E. ground		4.9	368.5

4710 = N. Side above garage

E-4'	= cmt. floor	4.19	369.20
E = W. edge	cmt. apron	5.10	368.29
E. ground		5.0	368.4

4740

E		4.9	368.5
±		4.8	368.6
W		4.8	368.6

4750 = S. Line Meads Ave

W.	cmt. cl. S. End	4.79	368.60
W.	Pay	" "	4.97 368.42
±	" "	" "	5.16 368.23
E.	" "	" "	4.99 368.40
E	cmt. cl. " "	4.78	368.61

14' N. of S. Line = S. cl. Line

E-32.	cmt. cl.	4.98	368.41
E-32.	gutter Pav	5.52	367.87
E.	" "	5.44	367.95
E	cmt. cl.	4.96	368.43
±	pav.	5.42	367.97
W.	"	5.37	368.02
W	cmt. cl.	4.93	368.46
± 32.	" "	4.84	368.55
± 32	pav.	5.26	368.13

T.P. 5.55 372.60 6.34 367.05

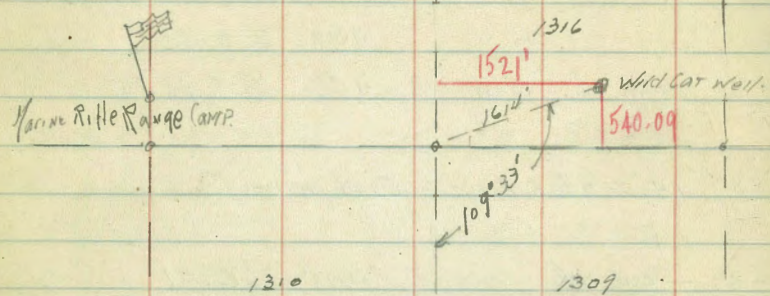
Orig B.M. 4.87 367.73 = 367.72

Year
3/20/36

Indexed
e.s.k.

60

Location of old casing of the J.P. Mills
Wild Cat oil well PL 1316



Levels & Location of Proposed
 6' wide Path to Ocean from Spindrift Dr.
 S. of Spindrift Inn
 3-20-86.

Level	North	South	Distance	Elevation	Notes
JESP	12.76	N. 32	256	11.45	✓
TP (100'S)	3.72	15.33	371	11.41	✓
0+10 = 6'					
N			388	11.45	✓
S			362	11.71	✓
0-5.33 inside edge wall					
N			361	11.72	✓
S			332	12.01	✓
0+00					
N	on NW Hub		331	12.02	✓
S			2.9	12.4	✓
0+07					
2' N of NL Garage floor El.			33	12.0	✓
N			34	11.9	✓
S			2.6	12.7	✓
0+31					
2' N of NL E of 4' wide window			0.5	14.8	Window sill ✓
N			5.0	10.3	✓
S			5.1	10.2	✓
0+40					
3' N of NL E 3' wide window			0.10	15.2	✓
N			4.4	10.9	✓
S			4.8	10.5	✓
0+46					
3' N of NL E 4' wide window			+0.4	15.7	✓

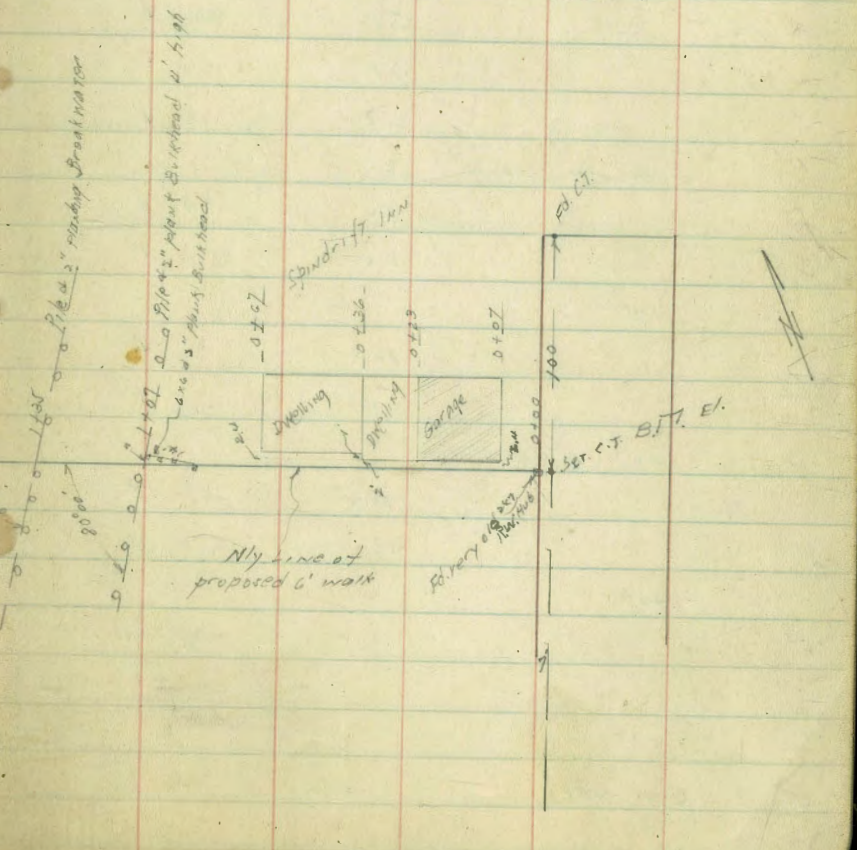
Indexed
 c.s.k.

N. 33

Pencilled on TPS 2179

61

Level	North	South	Distance	Elevation	Notes
N				10.9	✓
S				10.4	✓
0+59					
2.5' N of NL E of 4' window			+0.4	15.7	Window sill ✓
N			4.5	10.8	✓
+2			2.9	12.4	✓
S				12.9	✓



15.33

0+67			
v. x N = Nly Cor Dwelling	2.5	12.8	✓ Floor Et.
" " " "	4.3	11.0	✓ Top 200 mud fill
N	4.1	11.2	✓
+x	2.6	12.7	✓
✓	2.5	12.8	✓

0+85

✓	5.0	10.3	✓
+x	3.1	12.2	✓
✓	2.9	12.4	✓

0+94 edge cliff

✓	8.2	6.9	✓
✓	4.2	11.1	✓

0+95

✓	12.3	3.0	✓
✓	12.3	3.0	✓

1+07 at High Boulevard

N sand	16.3	-1.0	✓
S	16.3	-1.0	✓

1+34

N sand	18.4	-3.3	✓
S			

1+35

Top Breakwater	17.3	-2.0	✓
----------------	------	------	---

15.33

62

1+36

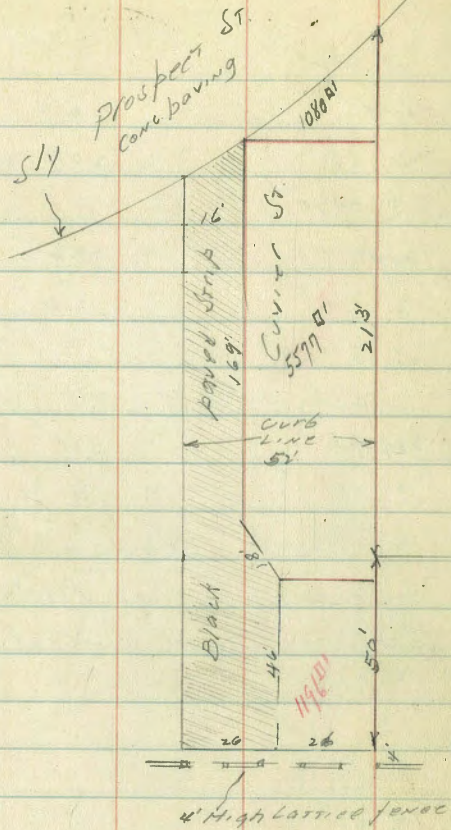
N SAND		20.4	-5.1	✓
S "		20.4	-5.1	✓
	1+99.75			
N SAND		21.4	-6.3	✓
S "		21.4	-6.3	✓

TP	21.5	13.77	371	11.62
check to BM BP			11.21	2.56 2.56

Note! Grade at 6' north should be low enough so that "Peeping Toms" could not gaze into the windows of Spindrift Inn. Apts.

Meas. for area for
proposed paving on
Draper + Currier
Sly from Prospect

Moore
S. 25
North
3-20-36

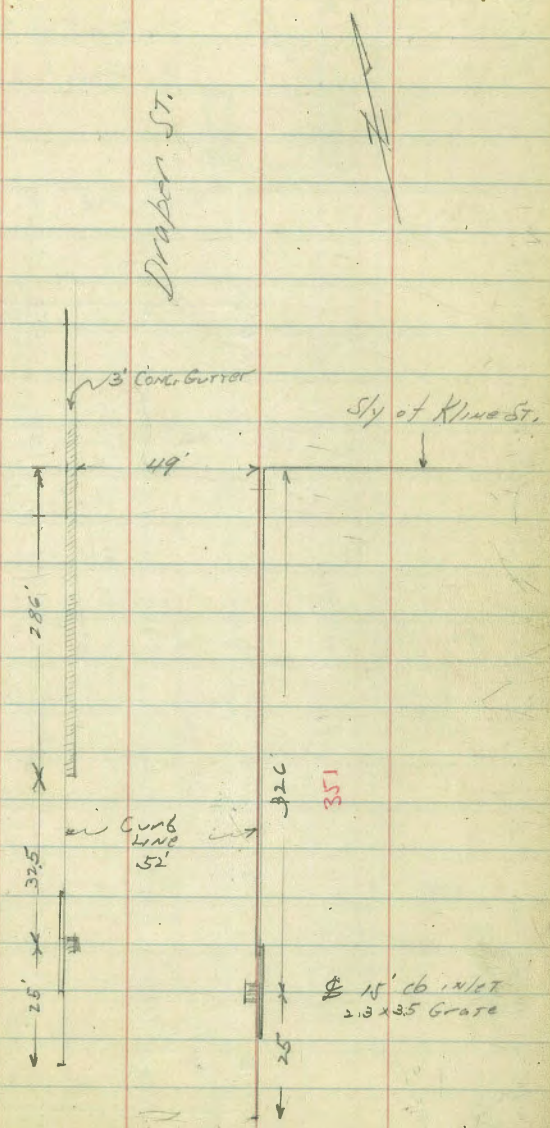


1080
5577
1196
7853 sq ft. Total Area Unshaded Portion.

City Frontage
20x26 = 520
17x26 = 442
46x26 = 1196
111x26 = 2886
50x26 = 1300
Total = 6344

Indexed
C.S.R.
Deduct 26x23 = 598
313 = 2385.5
858
872
17377 sq ft.

351 x 52 = 18,252
872
17377 sq ft.



19' cb inlet
3x3 Grate
lots 21-26 incl = City Property.
City Property
25x26 = 150x23 = 3450 sq ft.

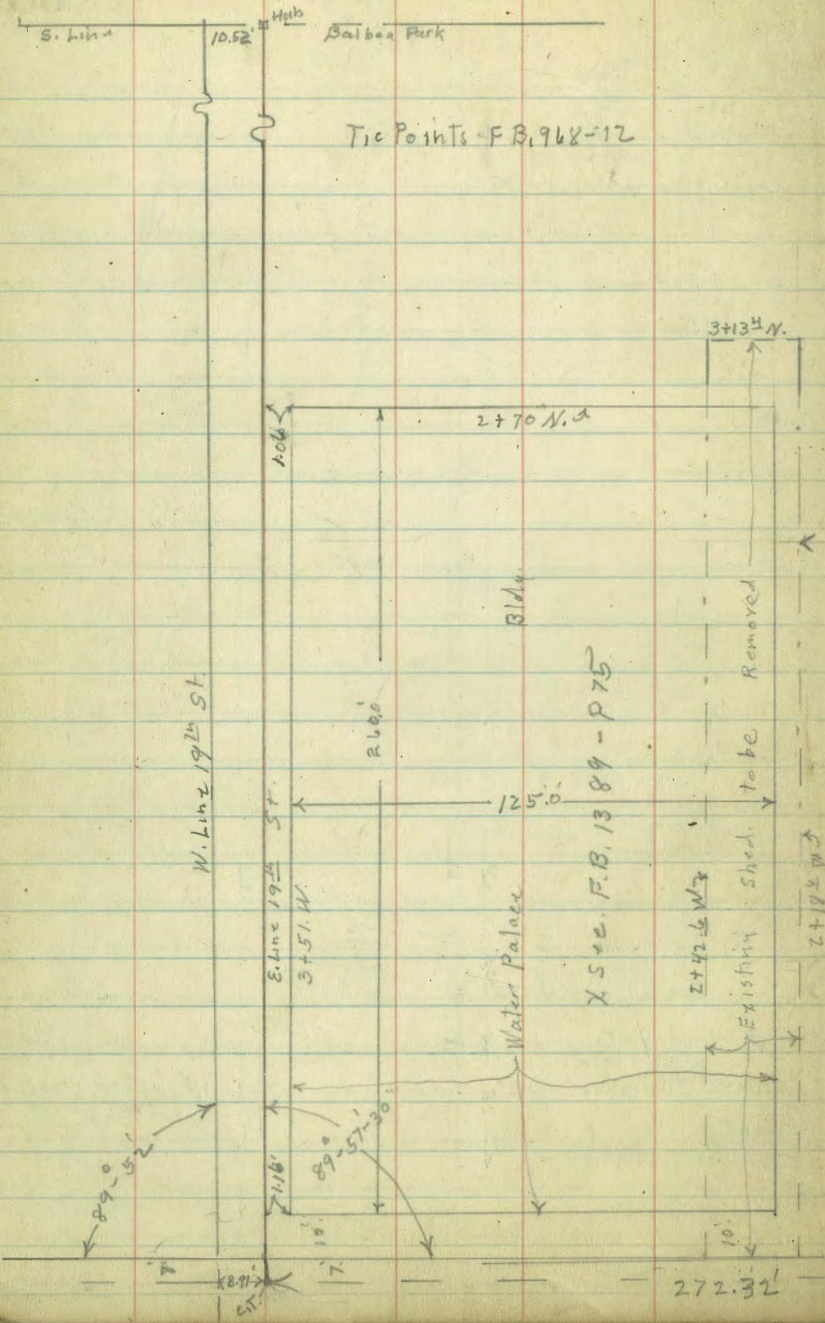
15' cb inlet
2.9 x 3.5 Grate

1-12-27
27th St
13-140

X Sec Ared at City Shops See Pages 20 + B Sts

Indexed
C.S.K.

2-Story Bldg under Construction.



Tie Points - F.B. 968-12

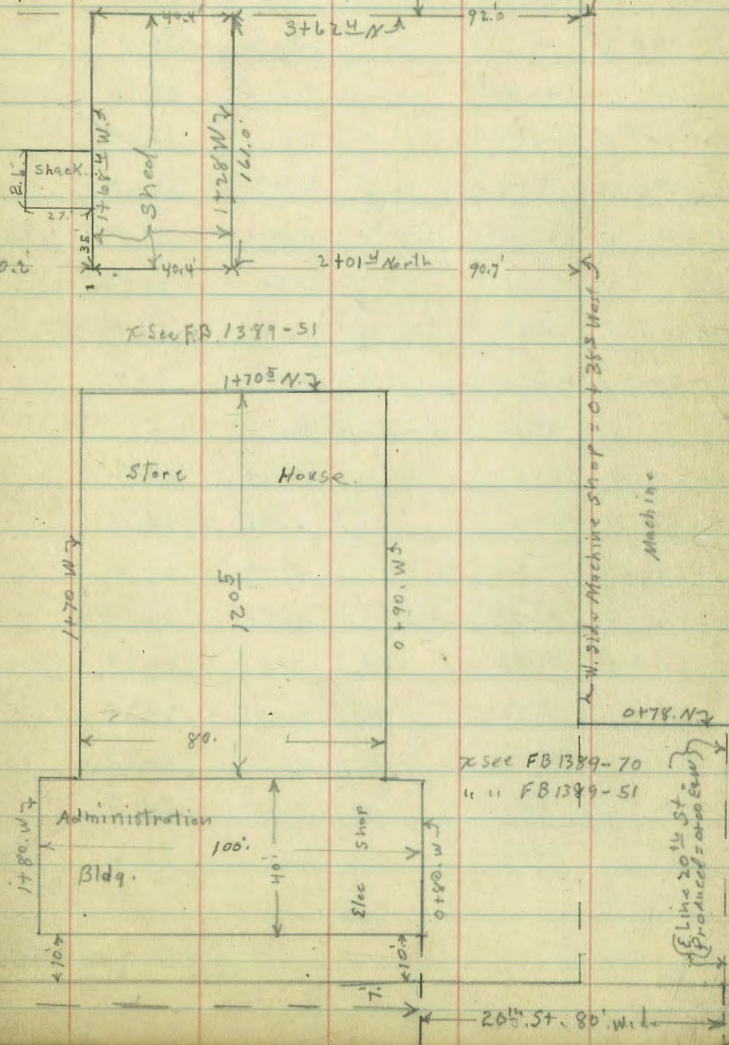
X Sec. F.B. 1389-975

X Sec. F.B. 1387-51

X Sec F.B. 1389-63

X Sec F.B. 1389-51

X Sec F.B. 1389-70
" " F.B. 1389-51



B.M. B.P. 1.08 71.31 70.23

T.P. 5.76 69.60 7.47 63.84

S.E. Cor
20th + B. St^s

2+01⁴ N

2+25 N

2+50 N

2+69⁵ N

2+82 N

3+50 N

3+25 N

3+00 N

2+82 N

2+69⁵ N

2+50 N

2+25 N

2+01⁴ N

T.P.

2+01⁴ N

2+25 N

2+50 N

2+75 N

3+00 N

3+25 N

3+50 N

69.60

0+60 W.

5.50 64.10

5.46 64.14

5.38 64.22

5.46 64.14

5.17 64.43

5.18 64.42

5.16 64.44

5.30 64.30

5.22 64.38

5.57 64.03

5.74 63.86

5.77 63.83

5.66 63.94

0+64 W.

4.52 68.36 5.76 63.84

0+90 W.

4.64 63.72

4.68 63.68

4.61 63.75

4.41 63.95

4.27 64.09

4.15 64.21

4.19 64.17

0+38³ W. = W. side Machine Shop.
Readings on par. outside Shop. unless indicated

2+01.4 N. = floor

2+25 N

2+50 N

2+69⁵ N

2+69⁶ N

2+82 N

3+00 N

3+25 N

3+50 N

3+50 N floor.

0+47 W.

3+50 N

3+25 N

3+00 N

2+82 = W. Edge Ctr Valve Box. C.I. Lid.

2+69⁶ N

2+69.5

2+50

2+25

2+01⁴

4.48 65.14

4.49 65.11

4.43 65.17

4.40 65.20

5.21 64.39

4.97 64.63

4.66 64.94

4.61 64.99

4.64 64.96

4.40 65.20

4.84 64.76

4.85 64.75

4.86 64.74

4.88 64.72

5.31 64.29

5.31 64.29

5.33 64.27

5.44 64.16

5.46 64.14

1+18 W

3+50 N	4.61	63.75
3+25 N	5.00	63.36
3+00 N	5.13	63.23
2+75 N	5.44	62.92
2+50 N	5.50	62.86
2+25 N	5.41	62.95

1+28 W = E. Side Shed.

2+25 N	5.76	62.60
2+50 N	5.57	62.79
2+75 N.	5.53	62.83
3+00 N	5.31	63.05
3+25 N.	4.94	63.42
3+50 N	4.65	63.71

1+30 N. inside enclosed shed

3+00 N. floor	4.86	63.50
3+10 N "	4.47	63.89
3+25 N "	4.00	64.36
3+50 N "	4.00	64.36

T.P. 3.29 67.13 4.52 63.84

1+68 W = W. side shed.

2+20 N.	5.16	61.97
2+25 N	4.97	62.16
2+36 N	4.97	62.16

1+78 W.

2+36 N	4.80	62.33
2+25 N	4.69	62.44
2+20 N	5.10	62.03

1+88 W

2+20 N	4.40	62.53
2+25 N	4.60	62.53
2+36 N	4.64	62.49

2+05 W.

2+36 N	4.57	62.56
2+25 N.	4.63	62.50

2+18 W = E. side shed.

2+25 N	4.87	62.26
2+36 N.	4.55	62.58

2+42 W. = W. side shed. inside.

2+25 N.	4.90	62.33
---------	------	-------

T.P. 5.36 68.05 4.44 62.69

2+42 W.

2+50 N	5.0	63.0
2+75 N	4.6	63.4
3+00 N	4.5	63.5
3+13.4 N W. car shed inside	4.5	63.5

68.05
2+18 W = E. side shed.

67

2+50 N	5.3	62.7
2+75 N	5.0	63.0
3+00 N	4.6	63.4
3+13 ⁴ N = N.E. Cor. shed.	4.4	63.6
3+20 N = W. edge of yard.	4.0	64.0

2+05 W

3+4 W = W. edge of yard.	4.6	63.4
3+25 N	4.9	63.1
3+00 N	5.0	63.0
2+75 N	5.1	62.9
2+50 N	5.4	62.6

1+88 W

2+62 N	5.2	62.8
2+75 N	5.3	62.7
3+00 N	5.2	62.8
3+25 N	4.7	63.3
3+50 N	4.4	63.6

3+50 N	4.4	63.6
3+25 N	4.7	63.3
3+00 N	5.2	62.8
2+75 N	5.5	62.5
2+62 N	5.6	62.4

chk. stub P.P.N.E. Cor. Water Palace 5.15 62.90 = 62.90

G-172-P,55

1-15-37

Miller
Walker
Bliss2. See Area N. of B. St. 4 W. of
Existing shed
See Plat. Page 64

68

BM	2.65	77.80	75.20	2+00 N. con	
3+51 W		12.0		2+90 W	10.1
2+90 W		12.5		3+40 W	9.6
2+43 W		12.2		3+44 W	6.0
	0+50 N.			3+51 W	5.3
2+43 W		11.6		2+33 N	
2+90 W		11.4		3+51 W	3.5
3+51 W				3+44 W	3.1
	1+00 N			3+41 W	5.5
3+51 W				3+33 W	10.0
2+90 W		11.3		2+90 W	9.3
2+43 W		11.4		2+40 N	
	1+50 N			2+43 W	9.8
2+43 W		10.8		2+70 W	9.0
2+90 W		10.6		2+90 W	9.2
3+51 W		10.7		W	9.5
	1+58 N			3+20 W	3.5
3+51 W		9.1		3+41 W	3.4
3+48 W		10.7		3+51 W	3.3
	1+80 N			2+65 N	
3+44 W		10.0		3+51 W	2.8
3+51 W		6.7		3+11 W	2.6
	2+00 N			3+00 W	9.0
2+43 W		10.3		2+90 W	9.0
2+58 W		10.3		2+63 W	8.0
2+60 W		9.1		2+58 W	9.5
				2+43 W	9.0

2 + 25 N.

2 + 43 W.	8.6
2 + 60 W.	9.0
2 + 64 W.	4.8
2 + 77 W.	4.0
2 + 80 W.	2.5
2 + 90 W.	2.5
3 + 11 W.	2.5
3 + 51 W.	2.5

2 + 85

2 + 43 W.	5.0
2 + 46 W.	3.1
2 + 90 W.	2.4
3 + 40 W.	1.7
3 + 51 W.	2.3

3 + 00 = S. Line A. St.

3 + 51 W.	1.9
3 + 45 W.	1.4
2 + 90 W.	2.0
2 + 48 W.	2.6
2 + 43 W.	4.4

Moore. X sec alley 20' wide
 9-13-37 Blk 4 Sub. Lot 7-17
 " N Teralta

bet. Wabash + 34th - Polk + Orange
 NW 8th 8.88 375.54 366.66 ^{33^d} Orange

Sly Orange = 00

W ob 4.92 370.62
 W par. 5.02 370.52
 C 5.18 370.36
 E " 4.66 370.88
 E ob 4.58 370.96

0+20

E 4.6 370.9
 C 4.8 370.7
 W 4.7 370.8

0+43

W 5.2 370.3
 W-4 Sim. Gar. dirt 5.2 370.3

0+64

W 5.3 370.2
 C 5.2 370.3
 E N edge cem. apron 4.88 370.66
 +3 " " Gar. 3 car. 4.61 370.93

0+76

-4 Sim gar. dirt 5.3 370.2
 W 5.3 370.2

0+89

-3 Sedge 3 car. ^{cem} gar floor 4.61 370.73
 E " " cem. apron 4.90 370.64

Index
 C.S.K.

375.54

70

C 5.4 376.1
 W 5.5 370.0

1+00

W 5.7 369.8
 C 5.8 369.7
 E 5.3 370.2

T.P. 3.59 372.76 6.37 369.17

1+37

E-3.5 E Sim gar. cem. 2.71 370.05

E 3.2 369.6
 C 3.6 369.2
 W 3.3 369.5

1+45

E-2.5 N edge double gar 3.39 369.37 cem fl.

E-1 " " cem. apron 3.58 369.18

1+65

W 3.8 369.0
 C 4.1 368.7
 E 3.7 369.1

+1 Sedge apron 3.69 369.07

+2.5 " " double gar 3.46 369.30 cem fl.

2+00

E 4.3 368.4
 C 4.5 368.3

W		4.5	368.3
	2+25		
-4	Sin. gar. cem.	4.83	367.93
-4		4.83	367.93
W		5.1	367.6
C		5.1	367.6
E		4.4	368.2
	2+50		
E		5.4	367.4
C		5.4	367.4
W		5.6	368.2
	2+81		
W		5.7	367.1
C		5.7	367.1
E		5.5	367.3
+4	Sin. gar. cem.	5.35	367.41
	3+00		
E		6.0	366.8
C		6.3	366.5
W		6.5	366.3
	3+13		
-4.5	Sin. gar. dirt	6.7	366.1
W		6.7	366.1
	3+37		
W		7.2	365.6
C		7.1	365.7

E		7.1	365.0	
+3	Sin. gar. dirt	7.2	365.6	
	3+46			
-4	Sin. gar. cem.	6.87	365.89	
E		7.5	365.5	
C		7.5	365.3	
W		7.6	365.2	
+1	" " dirt	7.4	365.2	
	4+07			
W		8.2	364.6	
C		7.9	364.9	
E	Sin. gar. cem.	7.9	364.9	
	4+50			
E		8.8	364.0	
C		9.4	363.4	
W		9.5	363.3	
TP.	2.54	365.83	9.47	363.29
	4+80			
W		3.2	362.6	
C		2.6	363.2	
E		2.0	363.8	
+3	E double gar.	1.9	363.9	Level floor 18' wide
	5+07			
E		2.9	362.9	

C		3.6	362.2	
W		3.4	362.4	
+7 E	gar. dirt	4.4	361.4	South entrance
	5+40			

W		5.4	360.4	
C		5.3	360.5	
E		4.3	361.5	

5+68.50 = N/4 Polk Ave.

Ecb		5.72	360.11	
E	PAV.	6.05	359.78	
C	"	6.42	359.41	
W	"	4.46	359.37	
W	cb	6.38	359.45	

T.P.	0.53	363.05	3.31	362.52	
T.P.	9.21	359.79	12.47	350.58	
check to NWBP	swift		0.98	358.81	358.86
	W/4				0.05

Proposed Drain at
Subway & Witherby St.

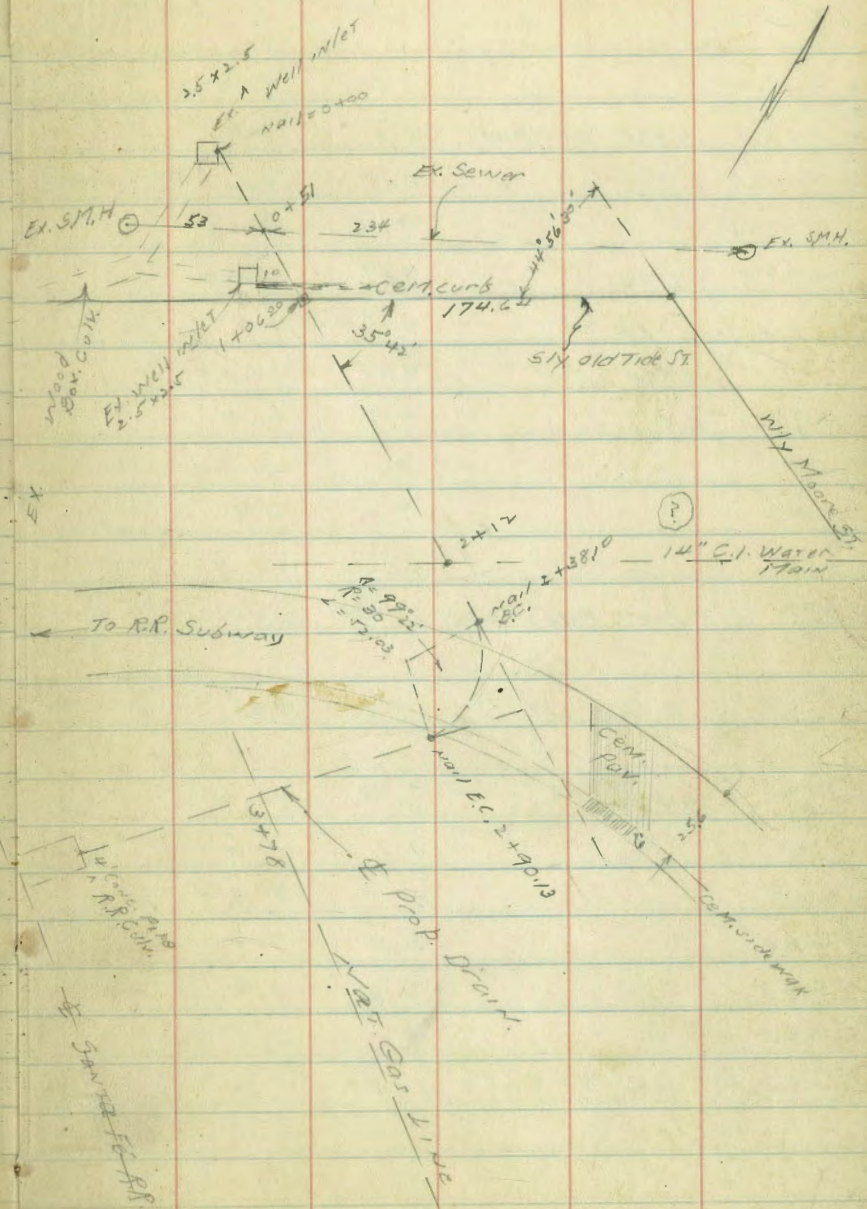
Moore
J. 5500
Northern
9-13-27

Indexed
C.S.K.

BM B.P. in C.C. W. side on Curve W of W.C. at Moore St.	0.37	28.10	27.73	Moore Subway
T.P.	6.63	22.95	12.38	15.72
El. FL. S.M.H. on Moore St.	5.61	16.74		
El. FL. S.M.H. 287 Wly from above MH	14.29	5.86		
0+00 FL. of Ex. Inlet	14.7	7.68		
" Top wooden Box	11.7	10.7		
0+37 Wly edge old Pav.	9.8	12.6		
0+51 INT of Sewer	9.30	13.05		
0+89 Gutter Conc.	8.71	15.64		
" Top curb	7.28	15.07		
" 10 Wly of above FL. of BOX	14.24	8.11		
" " " Gutter end	9.5	12.9		
" " " Top Curb	7.80	14.55		
1+00	7.5	14.9		
1+10	8.4	14.0		
1+50	8.3	14.1		
2+00	7.6	14.8		
2+12 on ground	7.5	14.9		
2+12 Top Water Main	12.88	9.47	Look up size	
2+38.10 B.C.	6.0	16.4		

See P 145

R.R. Curb



2 + 51.10		8.6	13.8
2 + 52.5	edge Conc. Pav.	8.8	13.6
2 + 64.10	"	9.89	12.46
2 + 77.10	"	9.64	12.69
2 + 79.9	S 90T	9.87	12.48
"	Top cd	9.97	12.98
2 + 88	Sedge SW	9.88	12.52
2 + 90.13	E.C.	9.1	13.3
2 + 93		7.1	15.3
2 + 00		7.3	15.1
3 + 50		10.1	12.3
3 + 78	TOP Nat. Gas Man	19.95	2.40
T.P.	0.06 11.71	10.70	11.65
3 + 78	ground	0.7	11.0
4 + 00		1.1	10.6
4 + 25		2.5	9.2
4 + 60		4.0	7.7
4 + 80		7.8	3.9
5 + 00		9.0	2.7
5 + 36	FL. S. Fe ⁺ R.R. Culv.	10.35	1.34

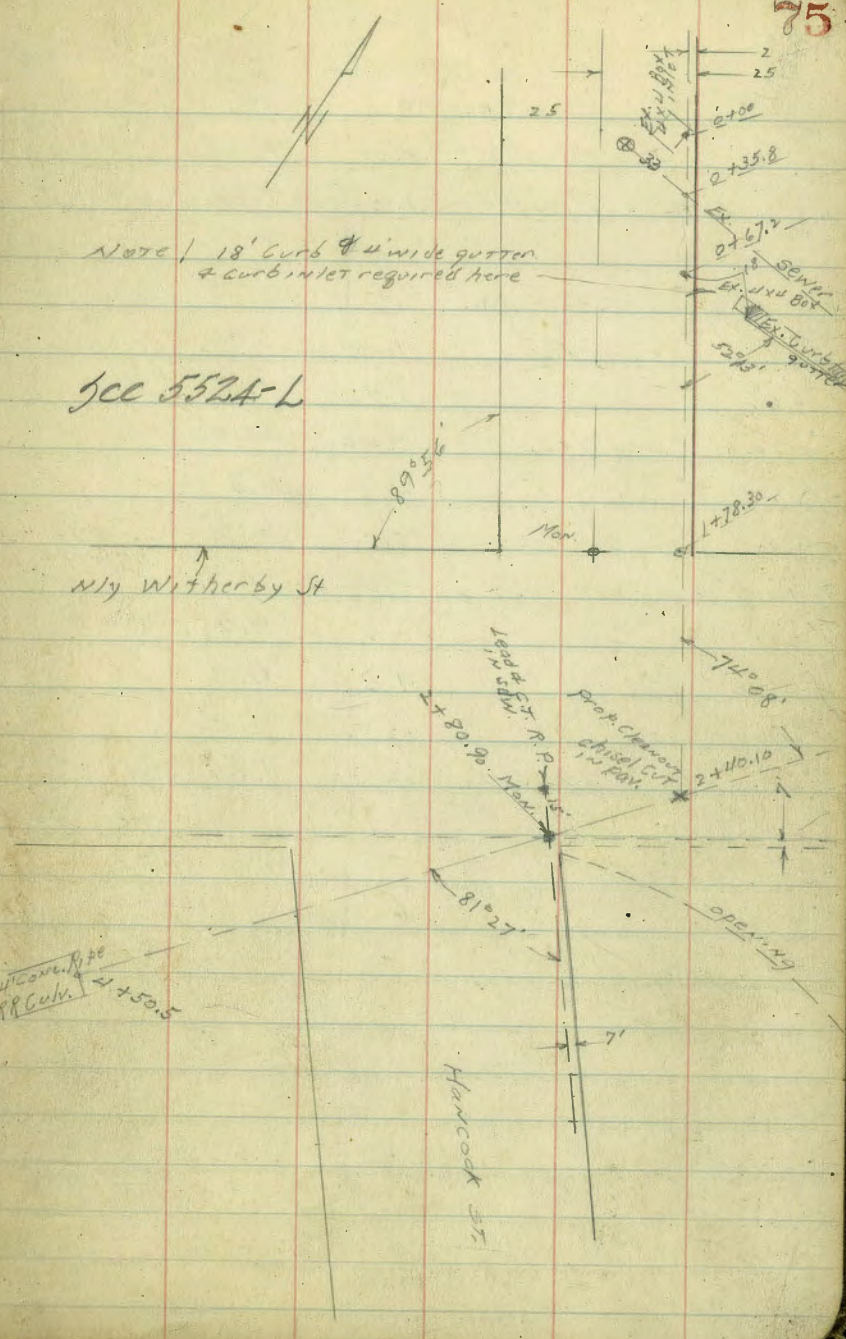
call Gas Co. for size

Moore
10-2-37
Prop. Drain #2
Subway & Witherby

Sta.	Dist. from Moore	Dist. from Witherby	Notes
0+00	0.32	27.73	FL. 4x4 Box inlet
"	0.14	15.72	TOP
0+05		12.0	TOP
0+28.8	3.85	12.01	N. edge Pav.
0+35.8	3.63	12.23	INT. EX. SEWER on pav.
0+41.8	3.09	12.77	Sedge Pav.
0+67.2	3.1	12.8	INT. of curb on ground
76'	7.64	8.22	Left of 0+67.2 FL. 4x4 Box End 4' wide
18'	3.02	9.84	" " " " gutter End
"	1.31	14.55	" " " " TOP curb
24'	1.08	14.78	" " " " " "
"	2.48	13.38	" " " " gutter
34'	2.13	13.74	" " " " " "
"	0.70	15.16	" " " " TOP curb
1+00	3.6	12.3	
1+50	3.6	12.3	
1+78.30	3.57	12.29	on stub Nly Witherby
2+00	2.9	13.0	
2+03	5.0	10.9	INT. WATER LINE on ground
2+10	7.4	8.5	
2+17.5	7.95	7.91	N. edge Subway Pav.
2+40.10	7.91	7.95	Proposed CLEANOUT on pav.

NOTE / 18' Curb & 4" wide gutter & curb inlet required here

see 552A-L



15.86

2+48	gutter pav.	8.60	7.26	
" "	1/4 top curb	8.12	7.74	of Subway
10' 2047	2+48 " "	7.30	8.56	Note! Build curb under here
" "	" " gutter pav.	7.77	8.09	
2+60	Sedge sidewalk	9.00	6.86	
2+68		8.9	7.0	
2+80.9	on 7' Man	5.40	10.46	
2+85		4.6	11.3	
2+92	INT. Gas Line	5.7	10.2	on top ground.
3+00		5.2	10.7	
3+35		4.2	9.7	
3+70		9.6	6.3	
4+00		12.6	3.3	
4+50.5	FL. of pipe curb	14.52	1.34	

Drainage at Pacific & Witherby.
See Plat. Book 1521 P. 78

BM. 6.11 7.24 1.13 N.E. Witherby Pacific

See A' at 90°-00 to Pacific at Point A'

N. Gutter at "A"	pay	6.77	0.52
+ 15.25 s = N. 14 "	"	6.34	0.86
+ 30. E s = Pacific	"	6.04	1.20
+ 45.25 s = S. 14 "	"	6.18	1.06
+ 61. s = S. gutter indium	"	6.75	0.49

Levels from Point "B" To Nly End. Concrete

Box Culvert - in Kurts St. S. of Witherby

0+00 = B' gutter Pav mt	6.74	0.50
0+50	6.25	0.99
1+00	5.70	1.54
+50	5.37	1.87
2+00	5.23	2.01
+50	5.34	1.90
3+00	5.35	1.39
3+50	4.4	2.6
4+00	4.5	2.7
+45	4.0	3.2
+50	2.5	4.7
+63	3.5	3.7
+66	8.4	-1.2
Nly End. inlet 72"x24" Box. Culvert	8.62	-1.38

See also G.B. 186, P. 64

~~± sewer levels on Vna St.~~

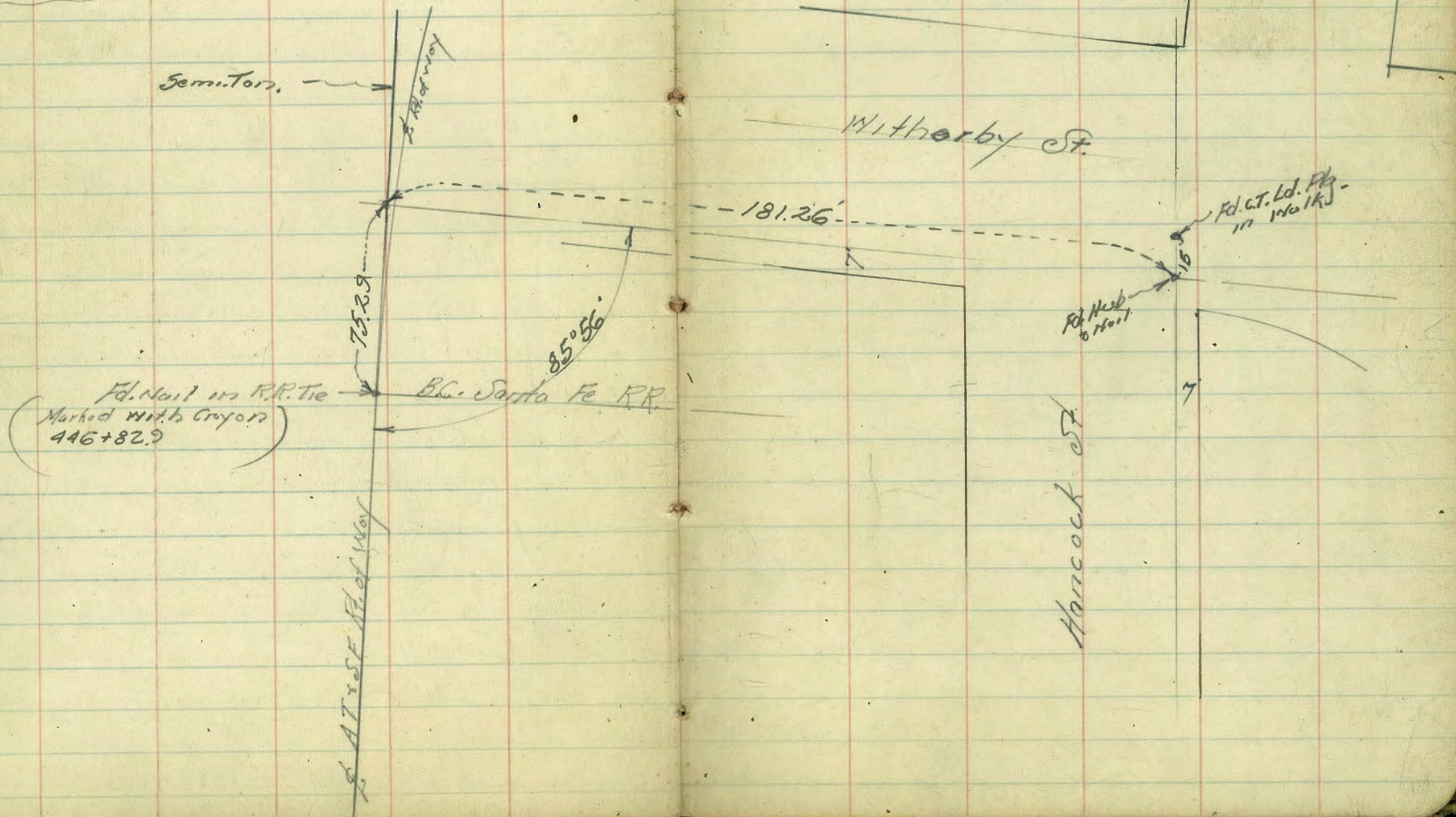
~~Void~~

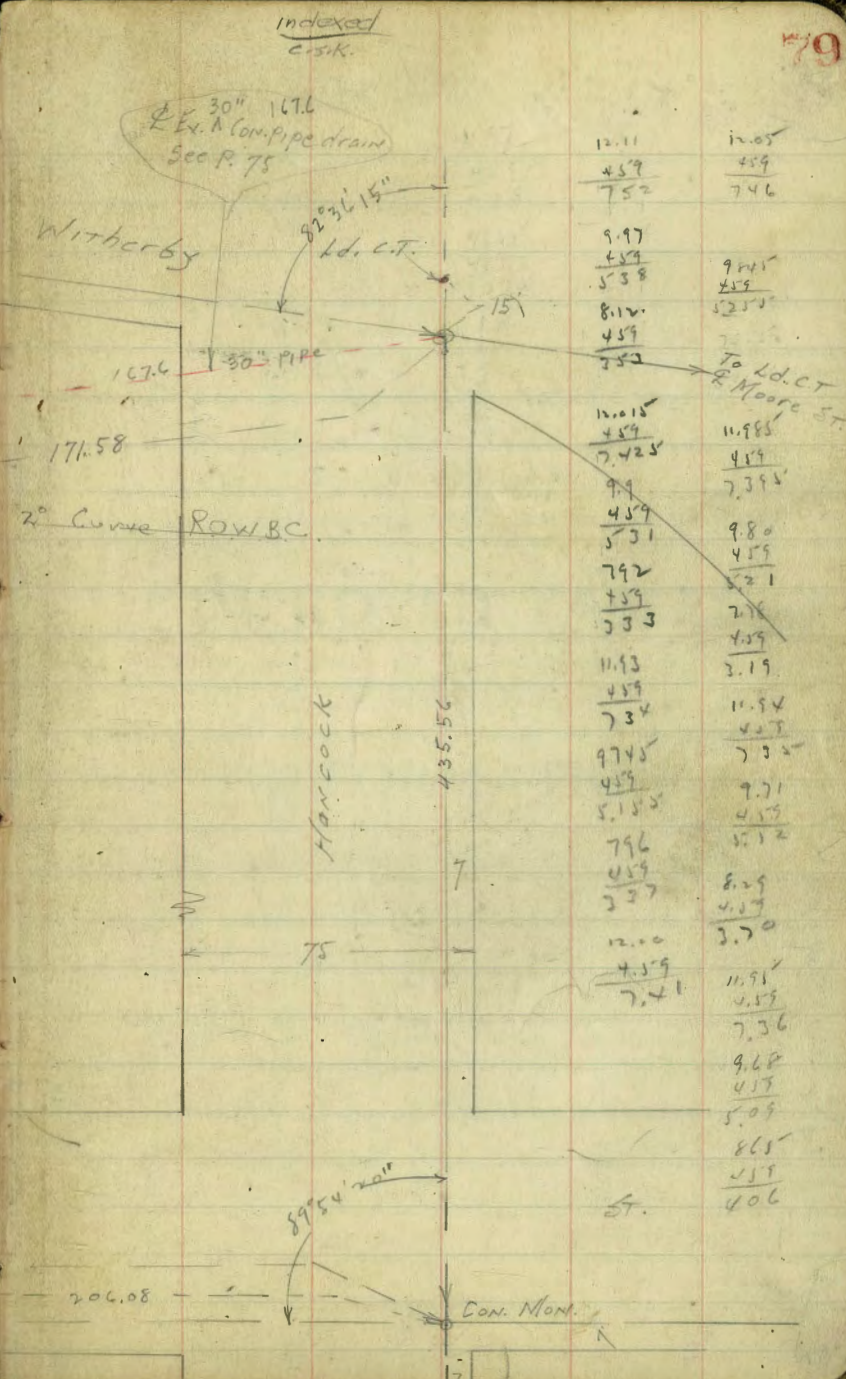
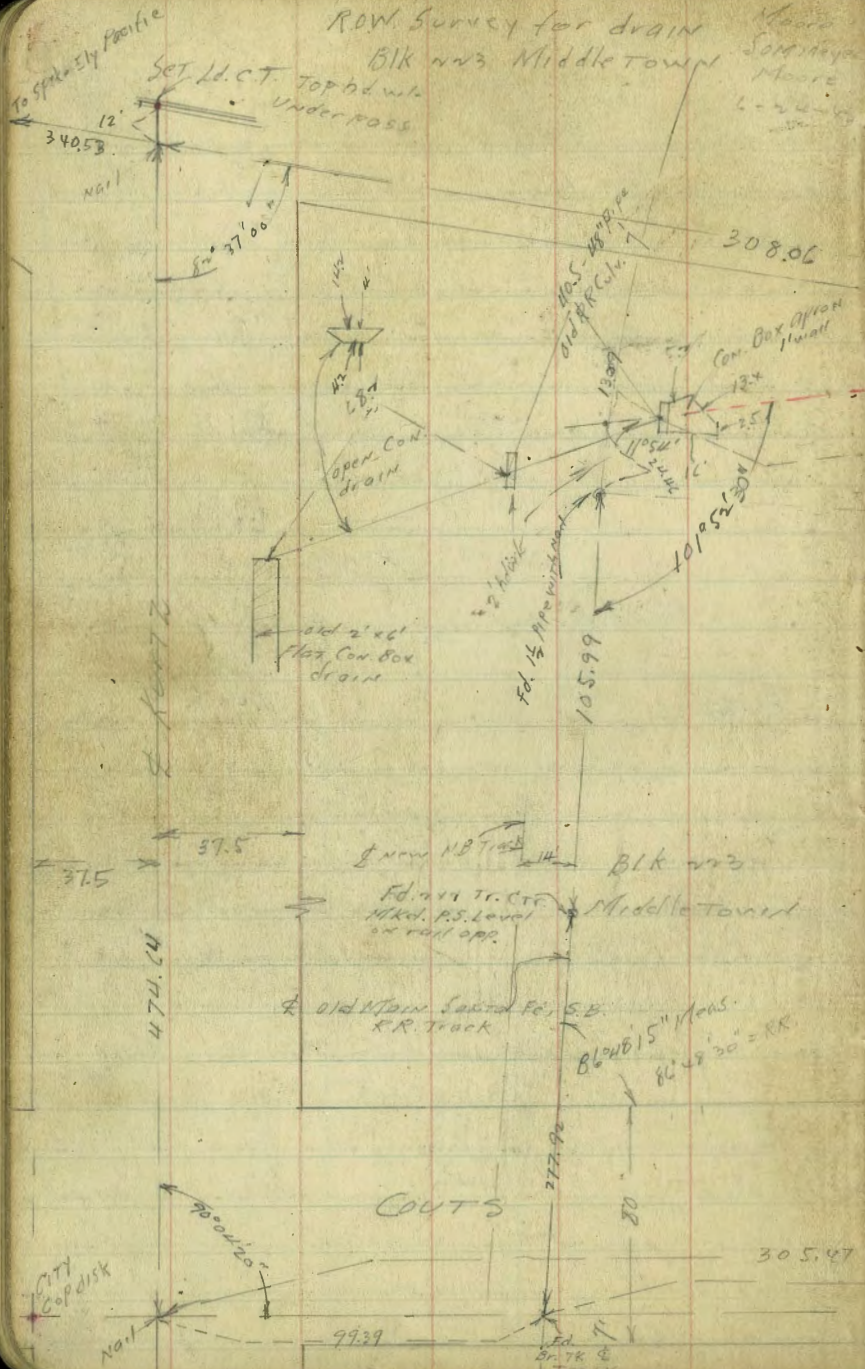
BM curb	1.53	19.56	18.05	SE. Pt. Vna + Dalbergia
T.P.	3.55	16.13	7.00	12.58
T.P.		10.14	4.01	

Walker
Johnson
Pope
Crawford
4-26-99

Ties To Santa Fe R.R.
at Witherby St.

78





28.39
 25
 42.11
 95.50

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in both

from side stake to slope stake. If ground is not

**IMPROVED TABLES
 AND
 INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree divide by degree of curve and add correction found in column of corrections. Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg	
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43	
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42	
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41	
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40	
										1.2203				
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	.2647	7753	1.2276	39	
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.3111	862	.2723	38	
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3597	969	.3190	37	
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.4106	8073	.3680	36	
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4641	175	.4193	35	
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.5204	274	.4733	34	
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5798	371	.5301	33	
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.6426	465	.5900	32	
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.7090	557	.6534	31	
59	572	.6643	587	.6753	601	.6864	616	.6977	631		646	.7205	30	
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29	
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28	
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27	
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26	
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25	
65	9063	1.445	075	1.609	088	1.775	100	1.943	112	2.113	124	2.286	24	
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23	
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22	
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21	
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20	
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19	
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18	
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17	
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16	
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15	
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14	
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13	
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12	
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11	
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10	
80	9348	5.6713	9353	5.7694	9358	5.8708	9363	5.9758	9368	6.0844	9372	6.1970	9	
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8	
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7	
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6	
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5	
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4	
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3	
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2	
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	1	
89	999	57.290	999	68.750	999	85.940	999	114.58	1.000	171.88	1.000	343.77	0	
60'	cos	60'	cos	50'	cos	40'	cos	30'	cos	20'	cos	10'	cos	deg

TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48	86	56-9.12
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40	87	57-5.04
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32	88	58-0.96
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24	89	58-8.88
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16	90	59-4.80
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08	91	60-0.72
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00	92	60-8.64
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92	93	61-4.56
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84	94	62-0.48
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76	95	62-8.40
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68	96	63-4.32
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60	97	64-0.24
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52	98	64-8.16
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44	99	65-4.08
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36	100	66-0.00
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28	101	66-7.92
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20	102	67-3.84



177.03 ✓
88.97

177.60
90.57
89.03
2.26
4.52
76.42
38.21
89.59-30
150
140

714
15167
2.81

380.16
378.57
1.59
79.2
135
214.2

79082
39051

37462
245.93
660.55

1236
22
1450

276
134
142

NE 237.10 Del Monte

Near 1860s T. NW SP 194

4.86
4.47
4.03

SW 218.03

68.87
62.39
1.48
53
95