

1504

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DEC 24 1964

ENGINEERING DEPARTMENT,
CITY OF
SAN DIEGO,
CALIFORNIA.

MADE IN U. S. A.

Our Leather Bound Engineers Note Books
are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page
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Book, Right Hand Page 4x4
to the inch, Center Line Red.
- No. 384 MINING TRANSIT
BOOK. Left Hand Page as in this
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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

7-2-34
 mill.
 Walker.
 Bliss.

X See. Portion of BIK 497
 old. San Diego.
 for Tennis Courts.

B.M. B.P	1.11	263.03		263.92	N.W. Pine + Ampudia
T.P.	0.47	252.61	12.89	252.14	
T.P. Hub	3.94	248.76	7.79	244.82	N.E. Cor. BIK 497
0+00 N+5 = S. Line Pine St.					
0+00 E+W = $\frac{1}{2}$ Arista St		3.8		245.0	
25' W		5.0		243.8	
50' W		5.2		243.6	
50' W	7' S.		4.4	242.4	
75' W	10' S		8.0	240.8	
75' W			5.5	243.3	
100' W			6.8	242.0	
100' W	13' S		9.4	239.4	
125' W			6.5	242.3	
125' W	10' S		9.7	239.1	
150' W			5.5	243.3	
150' W	10' S		10.6	238.2	
175' W			4.7	244.1	
175' W	10' S		9.6	239.2	
200' W			3.4	245.4	
200' W	8' S.		7.8	241.0	

Indexed
 c.s.K.

1

FT. Stockton Dr.

$\frac{1}{2}$

Conde

St.

325'

Hub.

BIK 497

324.82
 0+00 N+5.

St.

PINE

0+00 E+W.

Hub.

$\frac{1}{2}$ Arista
 St.

248.76
0+00 N+S = S. line Pine

248.76
25' S.

225' W		2.1	246.7
225' W	12' S	3.3	245.5
250' W		1.3	247.5
250' W	13' S	3.1	245.7
275' W		0.7	248.1
275' W	8' S	1.3	247.5
300' W		1.1	247.7
325' W	N.W. Cor. BK 497	1.5	247.3
325' W	13' S	2.9	245.9
25' S. of S. line Pine			
325' W		2.3	246.5
300' W		1.9	246.9
275' W		4.2	244.6
250' W		5.6	243.2
225' W		7.0	241.5
200' W		9.6	239.2
175' W		11.1	237.7
150' W		12.0	236.5
125' W		11.0	237.8
100' W		10.6	238.2

75' W		8.5	240.3
50' W		6.5	242.3
25' W		5.5	243.3
0+00 E+W		4.9	243.9
	50' S.		
0+00 E+W		5.2	243.6
12' W		4.9	243.9
12' W	54' S	5.0	243.8
12' W	63' S	8.3	240.5
25' W		5.9	242.9
25' W	57' S	6.4	242.4
25' W	63' S	9.0	239.8
50' W		8.4	240.4
50' W	63' S	9.7	239.1
75' W		10.4	238.4
75' W	66' S	11.0	237.8
100' W		12.8	236.0
100' W	59' S	13.1	235.7
100' W	65' S	11.7	237.1
100' W	70' S	13.0	235.5

248.76

50' S.

125' W.			13.1	233.7
125' W	63' S		15.5	233.3
150' W.			14.1	234.7
175' W.			13.8	235.0
200' W.			12.9	235.9
225' W			11.8	237.0
250' W			10.7	238.1
275' W.			9.0	239.8
300' W			7.0	241.8
325' W.			4.7	244.1
		75' S.		
325' W			10.0	238.8
300' W.			12.3	236.5
275' W			14.2	234.6
T.P.	4.57	240.49	12.84	235.92
250' W			7.3	233.2
225' W			8.3	232.2
200' W			9.3	231.2
175' W			9.4	231.1
150 W			9.3	231.2

B1K.497.

O.S.D.

3

240.49
75' S.

125' W			5.5	235.0
125' W	90' S		7.0	233.5
100' W			5.0	235.5
100' W	90' S.		7.2	233.3
75' W			4.7	235.8
50' W.			4.4	236.1
25' W.			2.4	238.1
0+00 E+W.			+0.9	241.4
		100' S.		
0+00 E+W.			0.0	240.5
25' W			4.5	236.0
50' W			7.1	233.4
75' W			8.7	231.8
100' W			10.7	229.8
125' W.			11.5	229.0
150' W			12.6	227.9
175' W			13.2	227.3
200' W.			13.0	227.5
225' W.			13.5	227.0
225' W	94' S.		11.1	229.4

240.49

100' S. Con.

240.49

125' S.

235' W		11.5	229.0
235' W	<u>107' S</u>	14.4	226.1
250' W		11.0	229.5
250' W	<u>110' S</u>	13.7	226.8
275' W		10.3	230.2
300' W		9.3	231.2
325' W		7.6	232.9
	125' S.		
325' W		13.1	227.4
300' W		14.2	226.3
275' W		14.9	225.6
250' W		15.9	224.6
225' W		16.6	223.9
200' W		16.0	224.5
175' W		15.7	224.8
150' W		16.0	224.5
125' W		15.0	225.5
100' W		14.3	226.2
75' W		12.2	228.3
50' W		9.9	230.6

25' W		6.1	234.4
10' W		3.6	236.9
0+00 E+W.		0.8	239.7
	150' S		
0+00 E+W.		0.7	239.8
7' W		1.6	238.9
12' W		4.5	236.0
20' W	131. S. = Pepper	24" Diam at Base.	
25' W		7.0	233.5
50' W		10.7	229.8
75' W		13.6	226.9
100' W		15.2	225.3
125' W		17.2	223.3
150' W		18.1	222.4
175' W		18.4	222.1
200' W		18.5	222.0
225' W		17.8	222.7
250' W		18.3	222.2
275' W		18.0	222.5
300' W		18.3	222.2

240.49

180' S.

325' W 18.0 222.5

175' S.

325' W 21.5 219.0

300' W 21.5 219.0

275' W 21.2 219.3

250' W 21.0 219.5

225' W 21.0 219.5

200' W 21.0 219.5

175' W 20.6 219.9

165' W = W. Rim canyon 20.2 220.3

154' W in " 22.4 218.1

150' W " " 27.8 212.7

150' W 169' S N. Rim canyon 22.4 218.1

145' W in canyon 22.4 218.1

144' W E. Rim canyon 23.1 217.4

125' W 20.6 219.9

100' W 17.1 223.4

75' W 14.4 226.1

50' W 11.0 229.5

240.49

175' S.

25' W 6.6 233.9

0+00 E+W 1.6 238.9

200' S.

0+00 E+W 0.0 240.5

25' W 5.2 235.3

50' W 10.2 230.3

75' W 15.0 225.5

100' W 18.7 221.8

125' W 20.3 220.2

137' W E. Rim canyon 22.8 217.7

146' W in " 29.6 210.9

150' W " " 35.6 204.9

159' W Bottom " 37.4 203.1

175' W W. Rim " 24.6 215.9

190' W 22.0 218.5

200' W 22.7 217.8

225' W 22.6 217.9

250' W 22.6 217.9

275' W 22.6 217.9

B.K. 497. O.S.D.

5

240.49

200' S. (con)

300' W 24.6 215.9

325' W 25.1 215.4

T.P. 12.81 252.61 0.69 239.80

T.P. 12.90 265.03 0.48 252.13

Original B.M. 1.11 263.92

7-3-34

X Sec. Portion of BIK 493 old San Diego
for Tennis Courts

B.M. B.P.	3.85	253.87		250.02	N.E. Hickory + Arputia
B.M. inside Cor. Return		6.65		247.22	S.E. Arputia + Presidio
T.P.	0.07	245.26	8.64	245.19	
T.P. Top					S.E. Arista
Hydt	0.57	234.56	11.27	233.99	+ Presidio
T.P. set.	3.09	225.02	12.63	221.93	
B.M. B.P.		5.62		219.40	± Whitman w.d. Arista

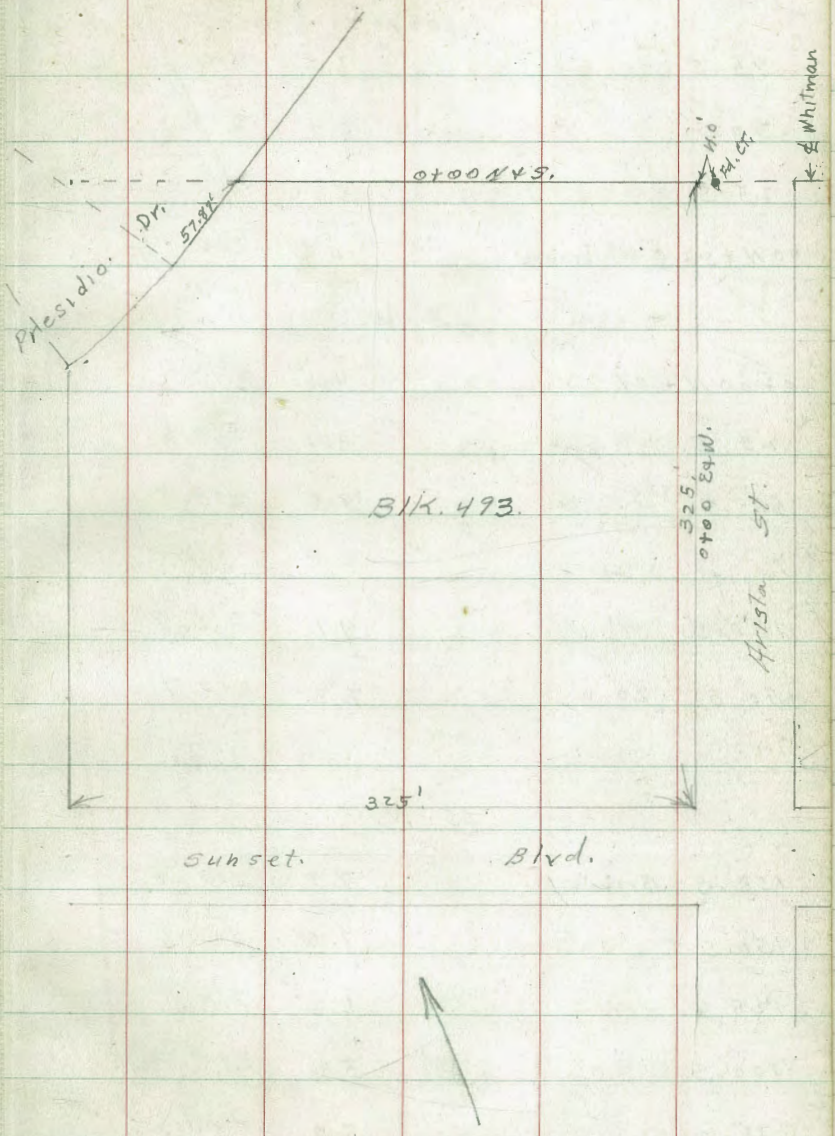
4' E. of 0+00 = W. Edge cmt. Walk

0+00 N+S = ± Whitman	5.54	219.48			
25' S	6.34	218.68			
50' S	7.05	217.97			
75' S	7.75	217.27			
100' S	8.42	216.60			
125' S	9.15	215.87			
150' S	9.84	215.18			
157.5' S = S. End. cmt. Walk	10.04	214.98			

0+00 E+W = W. Line Arista

150' S	9.4	215.6			
125' S	7.8	217.2			
100' S	7.0	218.0			

Indexed
C.S.K.



225.02

0+00 E+W. com

BM.	75'.S		6.5	218.5
BM.	50'.S		5.7	219.3
T.P.	25'.S		5.1	219.9
T.P. To Hydt	0+00 N+S = $\frac{1}{2}$ Whitman		4.9	220.1
T.P. set. BM.	0+00 N+S.	3'.W.	4.1	220.9
	25'.S.		4.4	220.6
0+00	50'.S		5.5	219.5
25				
50	150'.S	9'.W	9.1	215.9
75	150'.S	20'.W	7.3	217.7
100				
125		25'.W.		
150	158'.S	Brink	7.7	217.3
157.5	150'.S		7.0	218.0
	125'.S		6.2	218.8
15	100'.S.		5.6	219.4
12	75'.S		5.3	219.7
10	50'.S		4.7	220.3
	25'.S		4.3	220.7

B/K 493. C.S.D.

8

225.02

25'.W.

0+00 N+S		3.7	221.3
	50'.W.		
0+00 N+S.		4.6	220.4
25'.S		4.0	221.0
50'.S		4.6	220.4
75'.S		5.1	219.9
100'.S		5.2	219.8
125'.S		5.5	219.5
150'.S		6.6	218.4
141'.S = Brink		6.9	218.1
	75'.W.		
149'.S = Brink		6.7	218.3
150'.S		5.6	219.4
125'.S		5.6	219.4
100'.S		5.5	219.5
75'.S		5.4	219.5
50'.S		5.4	219.6
25'.S		5.9	219.1
0+00 N+S.		7.9	217.1
25'.S	67'.W	5.0	220.0

225.02
100' W

0+00 N+ S.		12.7	212.3
11' S		12.2	212.8
25' S		9.8	215.2
50' S		7.4	217.6
75' S		6.1	218.9
75' S	109' W	6.8	218.2
100' S.		6.1	218.9
100' S	113' W	6.7	218.3
125' S		6.3	218.7
125' S	115' W	7.0	218.0
150' S		6.7	218.3
150' S	113' W	7.9	217.1
168' S	= Brink	7.6	217.4
	125' W		
175' S	= Brink	15.3	209.7
150' S.		11.1	213.9
125' S.		9.7	215.3
100' S		10.5	214.5
75' S.		11.6	213.4
50' S		14.8	210.2

225.02

B/K. 493 O.S.D.

9

25' S.	125' W	16.5	208.5	
25' S	112' W	14.2	210.8	
0+00 N+ S.	112' W	15.5	209.5	
0+00 N+ S	125' W	17.0	208.0	
0+00 N+ S.	150' W	18.2	206.8	
25' S	150' W	19.4	205.6	
50' S	150' W	19.5	205.5	
75' S.	135' W	17.4	207.6	
75' S	150' W	19.2	205.8	
100' S	150' W	19.1	205.9	
125' S	150' W	18.4	206.6	
150' S.	150' W	18.7	206.3	
165' S	150' W	19.2	205.8	
175' S	150' W	19.4	205.6	
T.P.	12.06	236.54	0.54	224.48
T.P.	13.21	249.42	0.33	236.21
T.P.	5.95	253.92	1.45	247.97
Original B.M.		3.90		250.02

Levels for Storm Drain S. E. & N. of Φ Alleys. from Texas + El Cajon. To Univ. Ave. bet. Florida + Alabama.

S-2-24 Miller Walker Bliss

Allys 126-177-173-194 univ. Hts

319.56

Indexed elev.

10

BM. BP	6.37	324.41	318.04	4 Texas	6+31		10.8	308.8	
0+00 =	W. line Texas. 5' N. of Φ E. W. Alley		5.17	319.24	W. edge Pav.	6+31 -	7.1 E. of Φ	308.33	F.L.
0+50		5.6	318.8		6+50		11.0	308.6	
1+00		6.2	318.2		7+00		9.3	310.3	
1+45	Δ 90° 00' ht. 5' E. of Φ N + S. Alley		6.2	318.2		7+50		309.9	
T.P.	1.81	319.56	6.66	317.75	8+00		9.3	310.3	
1+60 =	S. line E. + W. Alley		2.0	317.6		+50		310.9	
2+00		2.6	317.0		9+00		8.4	311.2	
+50		3.1	316.5		T.P.	4.39	315.07	310.68	
3+00		3.5	316.1		9+50		4.1	311.0	
3+34.5 =	N. line Howard		3.12	316.44	N. edge Pav.	10+00		311.1	
3+48.5 =	N gutter		3.10	315.86		10+13.5 =	N. line Polk		3.8
3+74.5 =	Φ		2.74	316.82		10+48.5 =	5' N. of Φ " Δ 90° 00' ht.		3.5
4+00.5 =	S. gutter		3.54	316.02		10+63.5 =	5' N. of Φ Polk. W. line Alley		4.5
4+14.5 =	S. line Howard		2.68	316.88	S. edge Pav.	11+00		308.2	
4+50		2.2	317.4		11+50		10.2	304.9	
5+00		4.4	315.2		12+03.5 =	E. line Louisiana on pav		13.6	301.5
+50		6.0	313.6		12+17.5 =	E. gutter		13.7	301.4
6+00		7.1	312.5		12+43.5 =	Φ		13.3	301.8

Polk Ave. Ungraded.

315.07

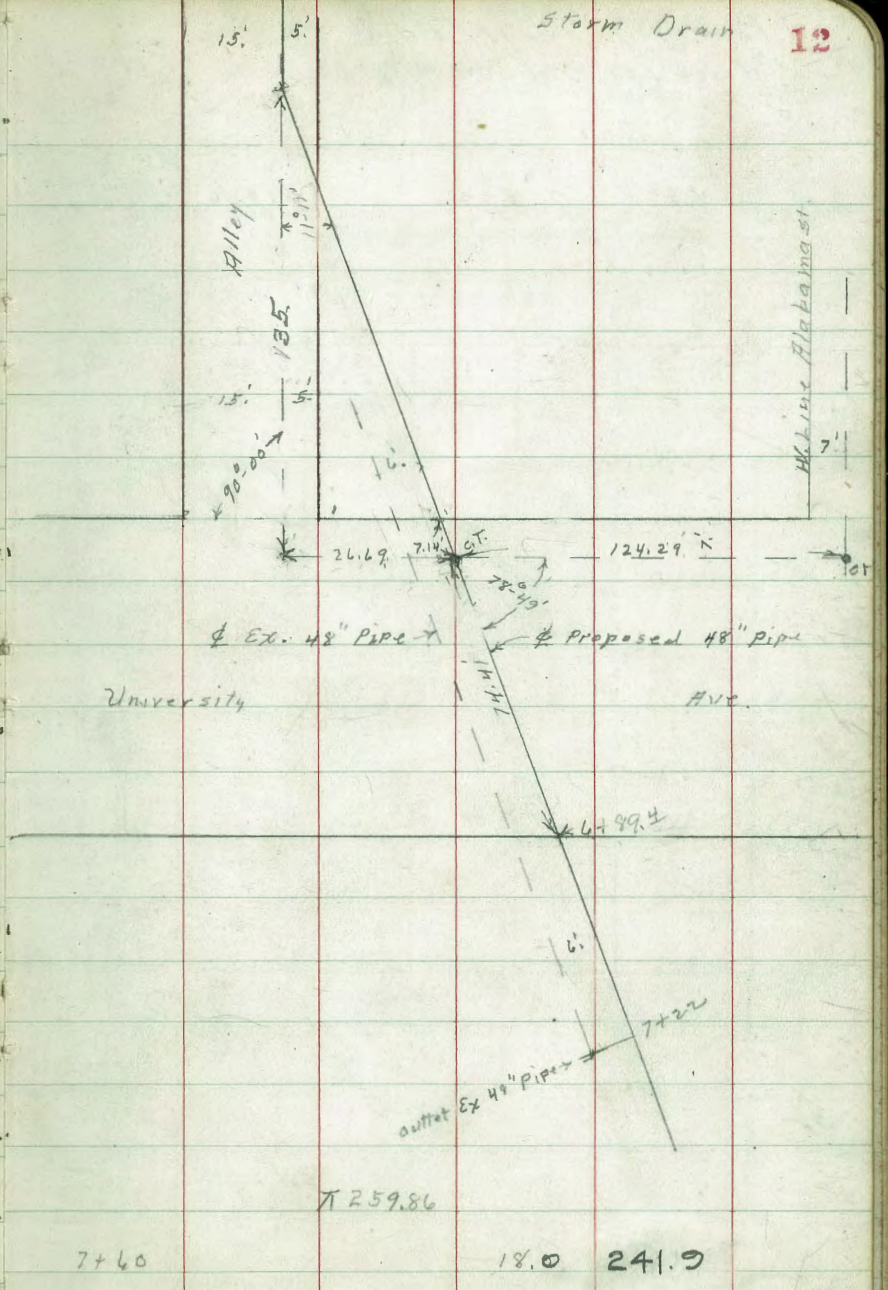
Alley bet. Alabama + Florida
Lincoln To Univ

Storm Drain.

11

12+69 ^E = W gutter	14.0	300.1	B.M. BP	3.02	288.88	285.86	S.E. Lincoln + Miss	
12+83 ^E = W Line Louisiana	13.6	301.5	T.P.	0.62	276.59	12.91	273.77	
ch. R.M.B.P.	5.10	309.77	S.E. Polk + Mississippi	S. E. of S. line Lincoln + S. Edge Pavmt.		3.36	273.23	
T.P.	0.80	309.34	6.53	308.54	0+25	2.9	273.7	
5' E. of Alley bet. Louisiana					0+65	4.8	271.8	
+ Mississippi from Polk to Lincoln					1+00	8.4	268.2	
0+00 = S. Line Polk Ave	2.40	306.94	S. edge Pav	+50		13.2	263.4	
+50	2.6	306.7		+75		14.4	262.2	
1+00	4.7	304.6		2+00		13.3	263.3	
+50	5.6	303.7		2+40		10.1	266.5	
2+00	6.5	302.8		2+90		10.1	266.5	
+50	8.1	301.2		3+00		11.0	265.6	
3+00	9.0	300.3		3+20		13.2	263.4	
+50	10.9	298.4		T.P.	0.47	264.02	13.04	263.55
4+00	12.5	296.8		3+50		8.6	255.4	
T.P.	0.33	297.48	12.19	297.15	3+80	12.6	251.4	
4+50	3.3	294.2		4+00		13.8	250.2	
5+00	5.3	292.2		+50		13.5	250.5	
5+50	6.4	291.1		4+77.6	Δ 11'-11" Lt.	14.8	249.2	
6+06 = N. End. Pav. 6' S. of N. line Lincoln	6.02	291.46		T.P.	4.27	255.71	12.58	251.44
ch. R.M.B.P. S.E. Lincoln + Mississippi	11.60	285.88	= 285.86					

		255.71		
5+00			6.7	249.0
5+50			6.8	648.9
6' Rt. of 5+58	Top Ex Pipe		7.8	247.9
5+70			6.2	249.5
5+82			3.1	252.6
T.P.	12.58	264.02	4.27	251.44
T.P.	9.00	272.29	0.73	263.29
BM. B.P.			6.34	265.95 = 265.96
6+08	N. Line Univ		0.4	271.9
6+22 ³	N. cl.		0.75	271.54
6+22 ³	gutter		1.47	270.82
6+482	= ϕ		1.68	270.61
6+75 ²	= gutter		3.02	269.27
6+75 ¹	= S. cl.		2.54	269.75
6+86			2.8	269.5
6+89 ⁴	= S. Line Univ		6.1	266.2
T.P.	0.15	259.86	12.58	259.71
7+14			7.9	252.0
7+22			17.0	242.9
6' Rt. of 7+22	{ S. End. outlet Ex. 48" Culvert.		19.7	240.2



Proposed Tennis Courts
Block 493 Old San Diego

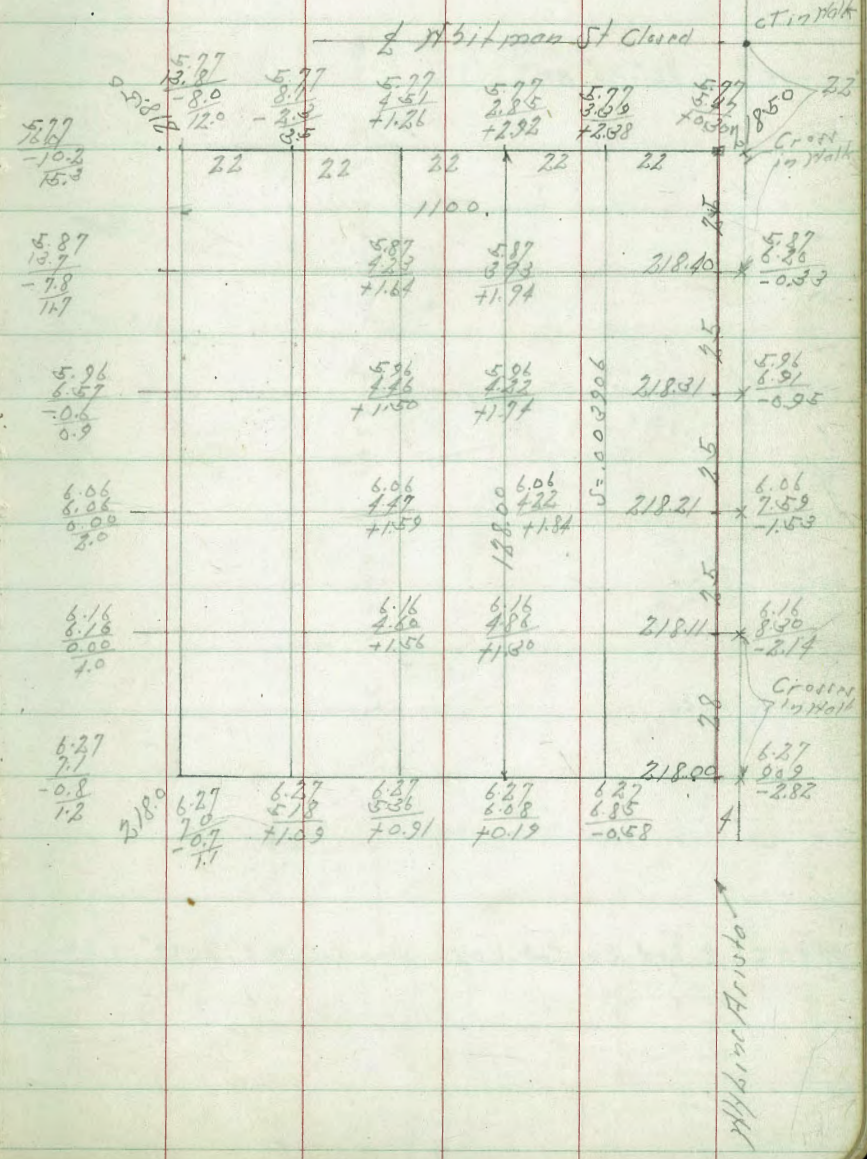
8-23-34
S. J. J. J.
Bliss
Hortberg

13
ct.

B.M. 4.87 22427 219.40

B.P. Co.
2 Whitman
McClintock
1927

Finished Grade
Cuts off St 4th
Fills Set Top Slope 1/2" 1'



11-2 -34 "N." ST. Storm Drain
 Miller
 Walker Logan Ave to Harrison
 Blaw

indexed
 c.s.Kr

0+98.15 L 16°40' RT.

1564'

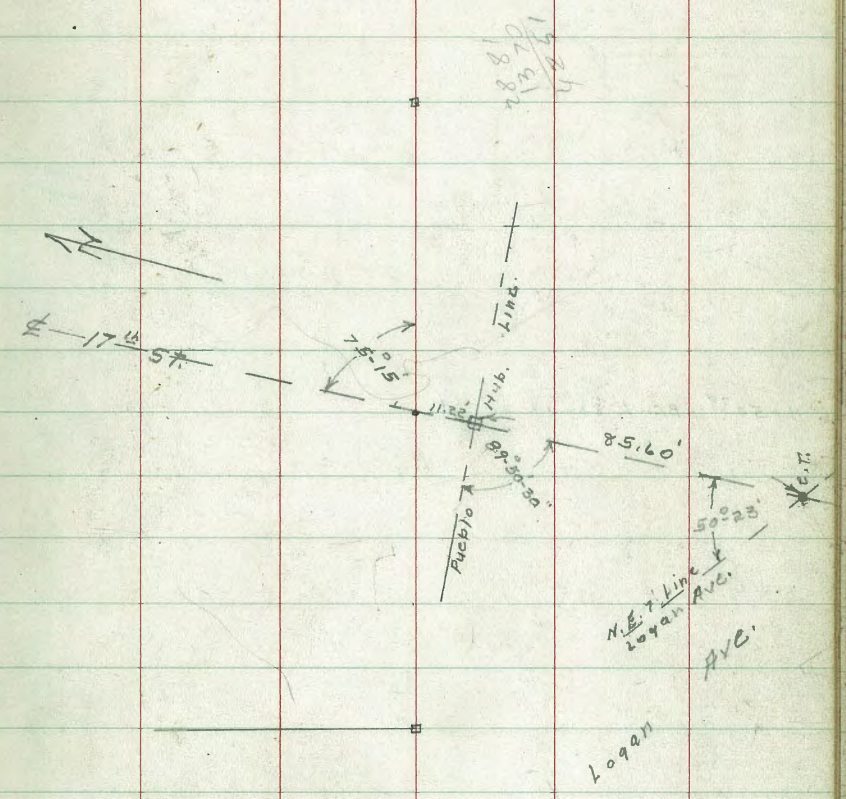
0+82.51 P.I. of 17th ST.

5370

change 0+00 to 6+27.93 see page 23.

0+28 P.I. E.C.

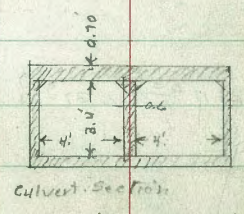
0+00 C.T. 2. End. Ex. Ent. Box Culvert. B.C. A 19°-17' Lt.



L = 19-17'
 A = 85.60'
 T = 14.54
 L = 28.81

P.I. Hub

Ex. Box Culvert.



Culvert Section

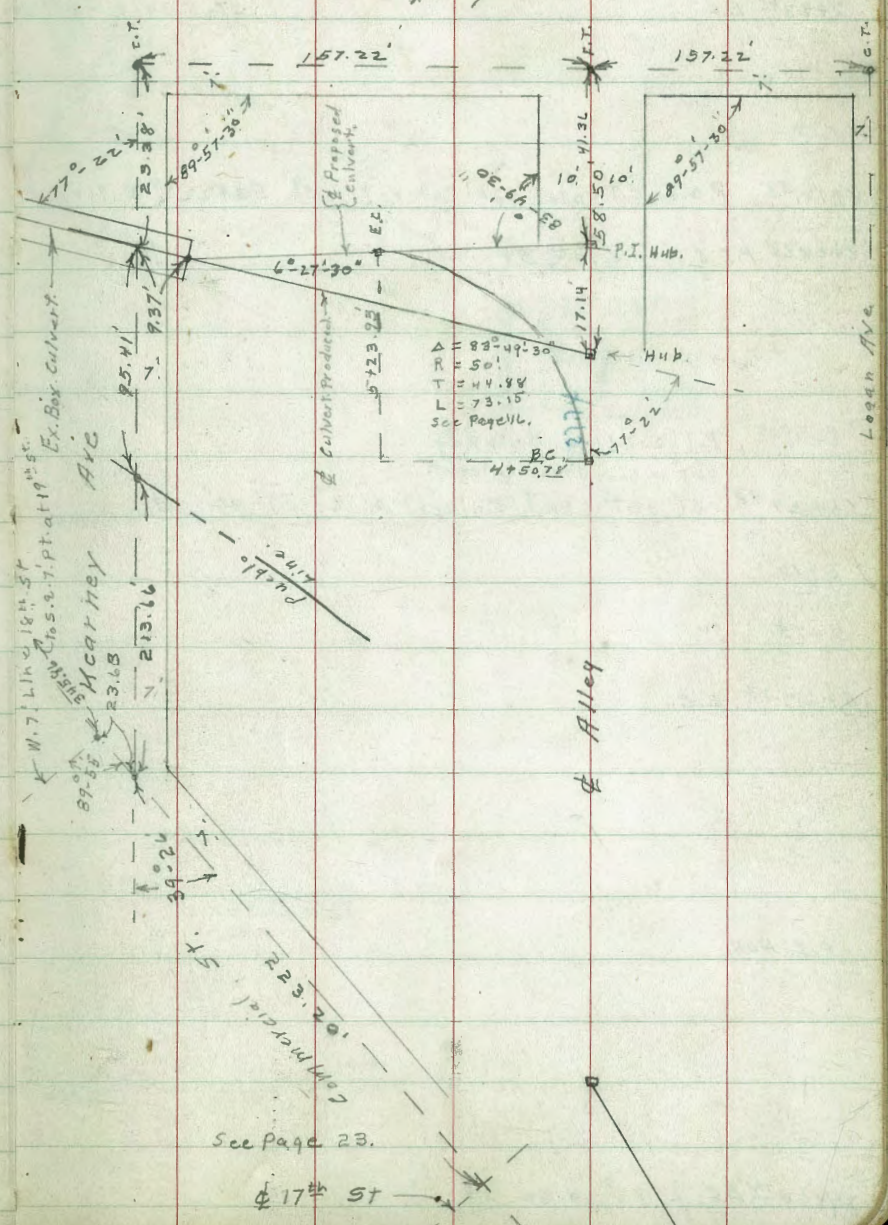
Sigsby St.

4+50.28 B.C. $\angle 82^{\circ}49'30''$ Lt.

239.25

2+11 ⁵⁰ $\angle 37^{\circ}03'$ AT

113.38

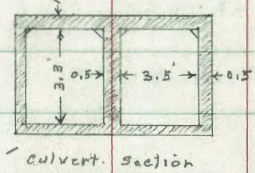
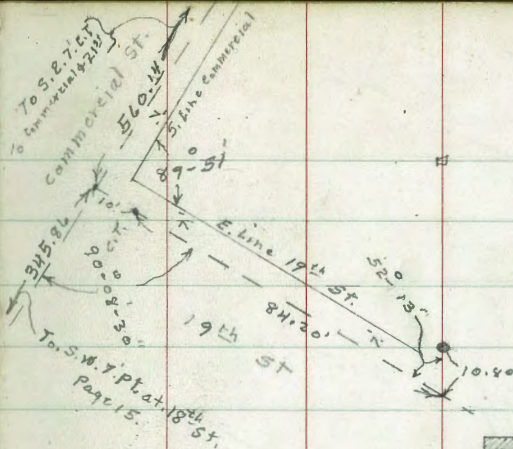


8+23⁰⁰ B.C.

Sta 53+18⁰⁰ B. 26 P. 10

8+19⁵⁸ P.O.T. C.T. Inlet End. Culvert. Sta 53+22⁰⁵ B. 26 P. 10

8+08²⁸ P.I. E. 7' line 19th St



6+37⁰⁰ P.I. S. 7' line Kearney.

- C.T. in board over culvert.

6+27²³ - C.T. outlet End. Culvert Δ 6° 27' 30" Rt.

Sta 55+14⁰⁰ B. 26 P. 10

6+10

5+75

5+23²³ E.C.

P.I. Hub

$L = 83-49-30$
 $R = 50.00$
 $T = 44.88$
 $L = 73.15$

4+50²⁸ B.C. Δ 83° 49' 30" Lt

11+94⁴² E.C.

P.I. H46

7

 $\angle = 44^{\circ} 51' 30''$
 $R = 100'$
 $T = 47.29'$
 $L = 78.32'$
11+16¹² B.C. $\angle 44^{\circ} 52' 30''$ Rt

112.90

10+03²⁰ E.C.

P.I. H44

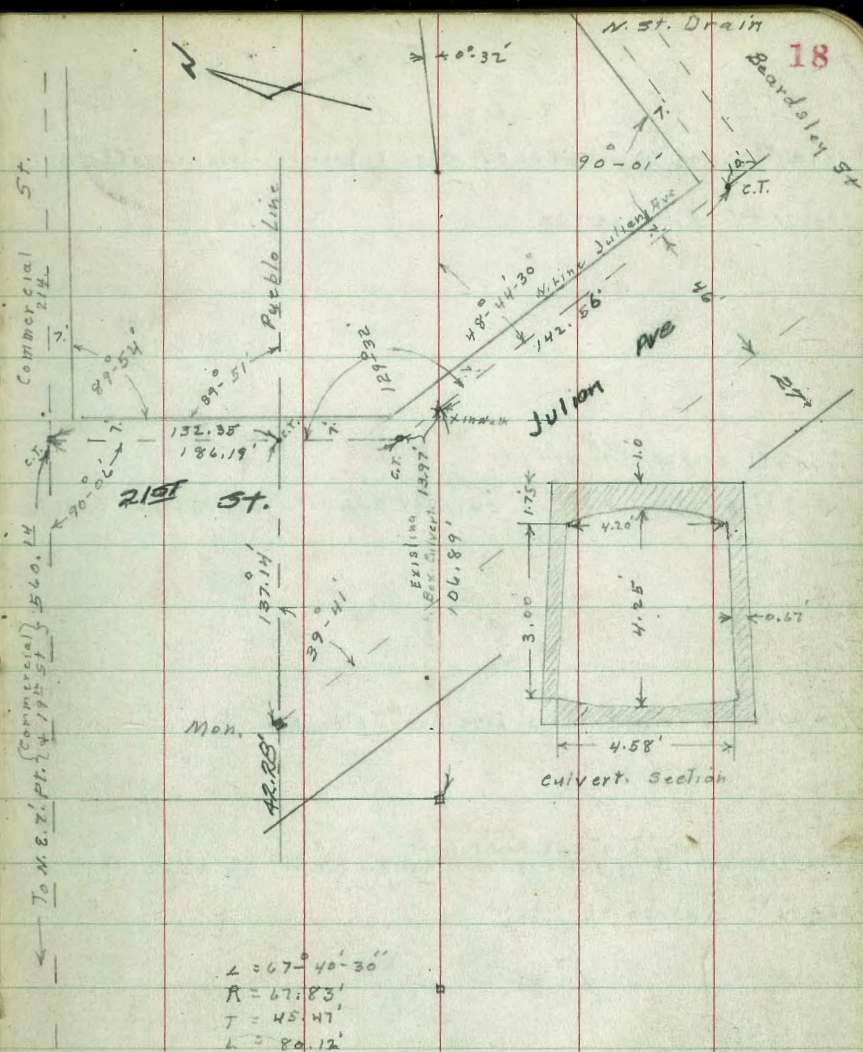
 $\angle = 51^{\circ} 27'$
 $R = 200'$
 $T = 96.36'$
 $L = 179.60'$
8+23⁶⁰ $\angle 51^{\circ} 27'$ Rt8+19⁵⁵ c. to End. Culvert

14+75³⁷ = sta 46+66⁸⁴ B. 968 P. 9, Inlet. original culvert.

14+57³⁷ P.I. of culvert + N.E. 7' line Julian Ave

13+50⁴⁸ E.C. : N. End. Out let. 4' x 4' Cont. Box Culvert. Sta 47+91²⁵ B. 968 P. 9.

12+70²⁴ B.C. 67°-40'-30" LT.



181

69-901

7592

18

19+06.43 W. End. Outlet. Ex. Cmt. Box. Culvert = Sta 42+33 B. 948. P. 8

18+97.14 Δ 6-22 Lt

167.73

17+29.41 stub Δ 37-47 Lt

17+27.77 E. End. Inlet 4.8' x 5' cmt. Box Culvert, Sta 44+15 B. 948. P. 8

16+70.22 P.I. Culvert + W. 13' Line Beardlee St.

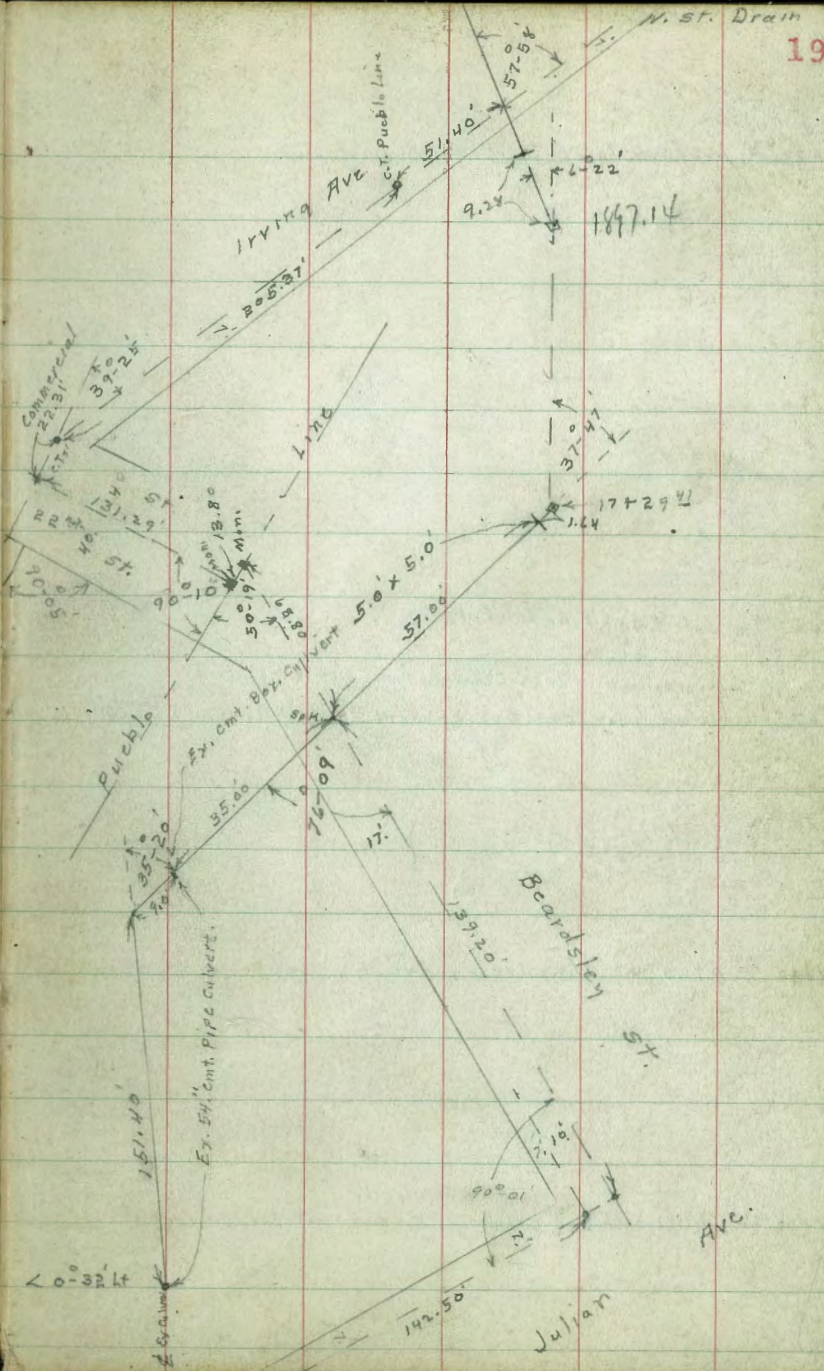
16+85.27 connection [54" Cmt. Box Culvert
5.0' vert x 5.0' Horiz. Cmt. Box. Culvert Sta 45+07 B. 948. P. 8

16+26.77 Δ 35-20 Rt

157.40

163.77
147.33
160.40

14+75.37 W. End. 54" Cmt. Pipe Culvert,
E. End. Cmt. Box. Culvert Sta 46+63 B. 948. P. 9



21+73⁸² Headwall Inlet 3. Pipe Culverts.

28.52
Cor. Iron Pipe
Covered with
Concrete

21+00

16.81
cmt. Pipe

23.82
~~26.81~~
30.53

3368.48
2035.14
1333.29

20+43¹⁹ W. End. 3. Cmt Pipe Culverts

8.0

20+35¹⁹ { connection with 2-36" Cement Pipes + 1-18" cmt. Pipe
E. End. Inlet cmt. Box Culvert. Sta 41+05²⁵ B. 969. P. 8.

102.66
26.11
128.77

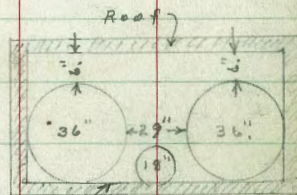
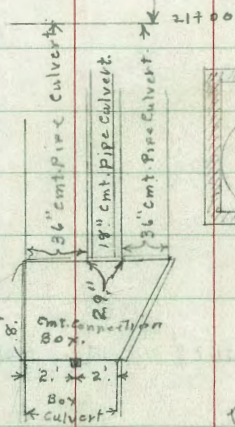
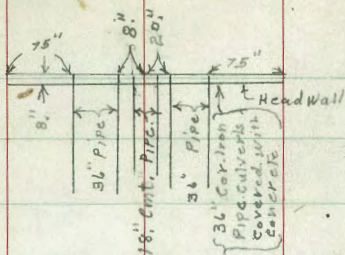
19+22³³ P.T. s. W. T. line Irving Ave. X in walk.

26.11

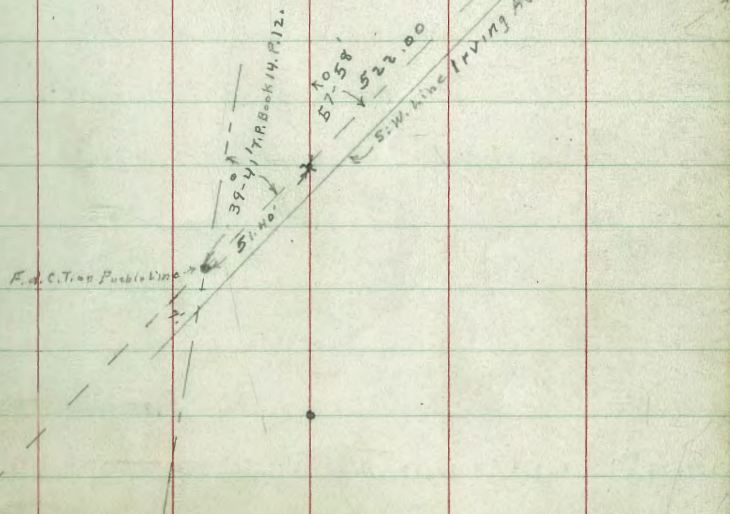
19+06⁴² outlet W. End Existing {4.0 wide} 5.0 High Cmt. Box Culvert.

N. St. Drain

20



Hub. over culvert.
Δ 2' = 21' AT.



87-60
37-41
50-17

N. St. Drain 21

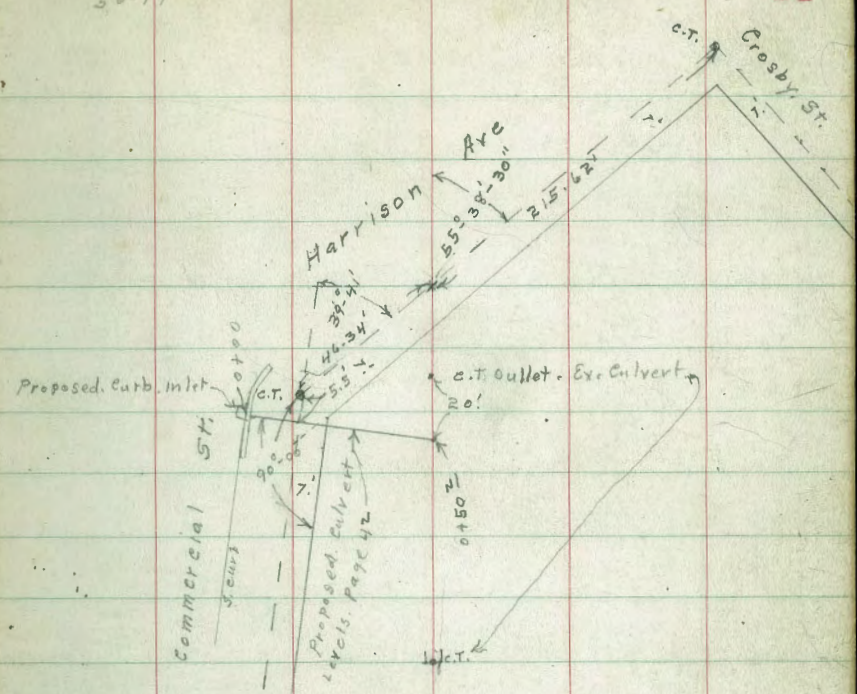
23+91 ²⁵ P.I. S.W. 7' line Harrison Ave x in Walk

2277

23+68 ⁴⁸ W. End. outlet { 4.2' High
4.0' Wide } cmt. Box Culvert. c.T. End. Culvert.

1966

21+73 ⁸² Inlet. Culverts. Headwall.



Alignment Change N. St. Drain

2+16.99 $\Delta 39^{\circ}40'$ P.I. ϕ Alleys.
 2+07.25 Sewer M.H. 1.205.0 ft ϕ .

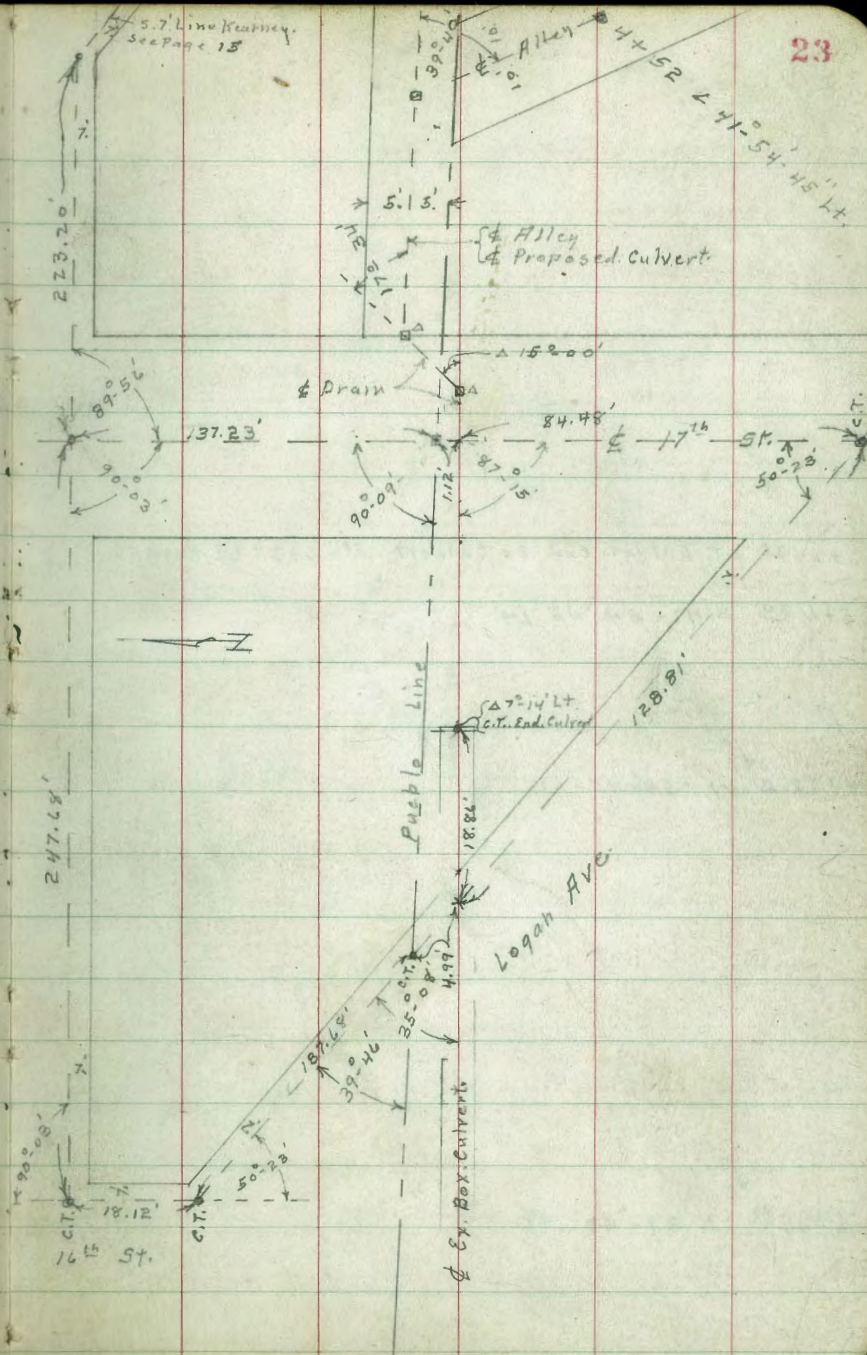
1+21.32 ϕ Alley + E. line 17th St $\Delta 17^{\circ}34'$ Rt.

1+04.59 $\Delta 15^{\circ}00'$ Lt.

0+80.53 P.I. ϕ Drain + ϕ 17th St.

84.53

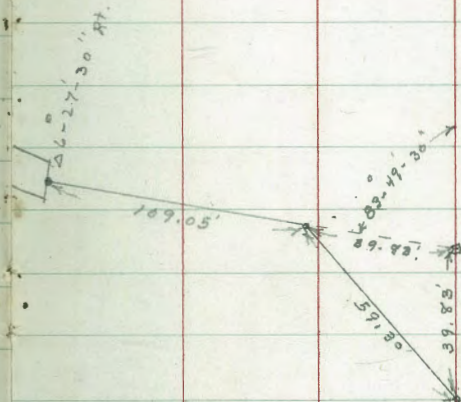
0+00. Inlet Ex. double box culvert. $\Delta 7^{\circ}14'$ Lt.



6+2035 C.T. Outlet. End. 8x Culvert. Sta 6+27 93 Page 16.

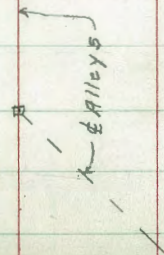
5+1130 Δ 41°-54'-45" Lt

4+52 Δ 41°-54'-45" Lt.



Handwritten scribbles and numbers, possibly '256'.

2+1622 Δ 39°-40' Rt.



13+63⁴⁰ Connection Ex. Box Culvert

5/14/44

13+12²⁶ 17' N. 95' line Julian Ave. \angle 8-32' RT.

12+24²² P.O.T.

2/9/23

10+93²³ Δ 16-44' RT.

11/1/48

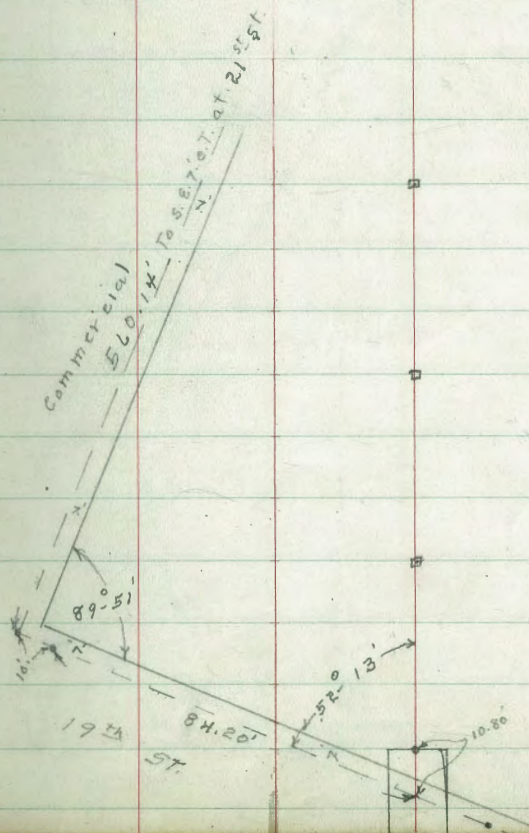
9+62²⁵ 31-34' RT.

10/2/21

8+55⁰⁴ Δ 20-31' RT.

3/1/46

8+19²⁸ C.T. Inlet. by Culvert. page 17



X. Sec. "N" St. Drain
Logan to Harrison Aves.

12 - - 34
12.52
13.45

15.92

27

A.M. B.P.	3.40	15.92	12.52	N.E. 16 th Commercial.	6' RT.	15.92 2.5	13.4
0+00 = E. End. Inlet		Ex. Box Culvert at Logan Ave.				0+50	
6' Lt.		15.92 3.6	14.3		6' RT.	3.2	14.7
4' " Top. Box		3.76	12.14		6'	3.0	14.9
4' " Fch.		7.82	8.08		7' Lt.	6.8	9.1
6' "		7.91	7.99		6' "	6.9	9.0
4' RT. "		7.84	8.06		T.P.	4.98	20.71
4' " Top. Box		3.67	12.13			0.19	15.73
6' "		3.5	12.4			0+75	
0+07 = End. Apron + Wing Walls..						20.71	
6' RT		3.8	12.1		6' RT	7.4	13.3
3.4' " Top. W.W.		3.81	12.09		6' Lt	7.4	13.3
3.4'		7.67	8.23		10' Lt	7.7	15.0
6' Lt.		7.71	8.19			10.7	10.0
6' Lt Top. W.W.		7.62	8.28			1+04	
		3.81	12.09		11' "	10.5	10.4
	0+25				8' Lt. Top. M.H.	7.66	13.05
6' Lt		7.3	8.6		8' " FL. M.H.	14.36	6.35
6'		7.10	8.4		6' "	7.5	13.2
6' RT		3.0	12.9		6' RT.	7.2	13.5
						7.1	13.6

	20.71		
	1+0459 Δ	15° 00' Lt.	
6' Rt.	$\frac{20.71}{7.1}$		15.6
♀	7.1		13.6
6' Lt.	7.2		13.5
10' "	10.5		10.2

1+21³³ E. Line 17th st. ♀ Alley Δ 17° 34' Rt.

6' Lt.	10.4		10.3
3' "	7.4		10.3
2' "	7.4		13.3
♀	6.9		13.8
6' Rt.	6.9		13.8

1+50

6' "	5.9		14.8
♀	6.1		14.6
11' Lt.	10.0		10.7
6' "	10.0		10.7

1+60

6' Lt.	9.8		10.9
♀	9.8		10.9
3' Rt.	5.8		14.9
6' "	5.7		15.0

20.71		N. St. Drain	28
1+95	$\frac{20.71}{5.3}$		15.4

6' Rt.		5.8	14.9
♀		9.1	11.6
2' Lt.		9.1	11.6
6' "		9.1	11.6

2+07²⁰

6' Lt.		9.1	11.6
♀		9.1	11.6
1.20 Rt. Top. M.H.		7.61	13.10
1.20 " F.L. M.H.		12.94	7.77
6' "		6.2	14.5

2+16²⁹ Δ 29° 40' Rt. ♀ Alleys. on split

8' Rt.		5.8	14.9
6' Rt.		9.0	11.7
♀ on Hub		9.02	11.69
1' Lt.		9.0	11.7
3' "		6.8	13.9
8' "		5.7	15.0

2+50

6' Lt.		6.2	14.5
2' "		9.1	11.6
♀		9.1	11.6

20.71

20.71

2' Rt

9.0

11.7

4' "

5.8

14.9

6' "

5.8

14.9

3+00

6' Rt

4.8

15.9

4' "

5.2

15.5

1' "

8.5

12.2

4

8.5

12.2

4' Lt

8.5

12.2

5' "

4.8

15.9

6' "

4.8

15.9

3+30

6' Lt

5.3

15.4

3' Lt

8.2

12.5

4

8.2

12.5

2' Rt

8.2

12.5

3' "

6.8

13.9

6' "

5.6

15.1

20.71

3+40

26.71

6' Rt

6.4

14.31

3' "

8.0

12.7

4

8.0

12.7

3' Lt

8.0

12.7

5' Lt

5.4

15.3

6' "

4.8

15.9

3+90

6' Lt

5.3

15.4

2' "

7.7

13.0

4

7.7

13.0

2' Rt

7.7

13.0

4' "

5.1

15.6

6' "

5.1

15.6

4+20

6' Rt

5.3

15.4

2' "

7.4

13.3

4

7.4

13.3

6' Lt

7.3

13.4

N. St. Doin

29

20.71
 4+52 Δ 41°-54'-45" Lt. on Split

20.71
 $\frac{7.2}{13.5}$
 6' Lt 4.4 16.3
 6' Rt 3.2 17.5
 T.P. 4.27 22.48 2.50 18.21

4+61 22.5
 6' Rt 4.8 17.7
 4.8 17.7
 3' Lt. 8.6 13.9
 6. " 8.8 13.7

4+66
 6' Lt 8.6 13.9
 4.8 13.9
 2' Rt. 8.7 13.8
 4. " 7.2 15.5
 6. " 4.4 18.1

4+74
 6' Rt 8.4 14.1
 4.8 14.5
 1. Lt. 5.0 17.5
 6. " 5.0 17.5

22.48 N. St. Drain 30

4+77 $\frac{14.8}{4.8}$
 6' Lt 4.8 18.7
 4.8 17.3
 1' Rt. 7.7 14.8
 6. " 8.4 14.1

4+93
 6' Rt 7.3 15.2
 5. " 7.3 15.2
 4. " 5.0 17.5
 4.4 18.1
 6. Lt 4.4 18.1

5+08
 6' Lt 3.6 18.4
 4.3 18.2
 1' Rt. 7.9 14.6
 6. " 7.9 14.6

5+11³⁰ Δ 41°-54'-45" Lt.

6' Rt 1.6 20.9
 4. " 7.6 14.9
 4. " 7.6 14.9
 1' Lt 7.5 12.0

22.48				22.48				N. St. Drain 31	
		5+11.30				6+00			
		<u>22.5</u>				<u>44.5</u>			
		3.8				4.3			
2' Lt			18.7	6' Lt				21.2	
6' "		3.6	18.9	4' "			6.9	14.6	
		5+25		♀			6.9	15.6	
6' Lt.		2.4	20.1	2' Rt			6.9	15.6	
2 "		2.7	19.8	4' Lt			1.3	21.2	
1' "		7.2	15.3	6' "			1.3	21.2	
♀		7.2	15.3	T.P.	8.07	27.77	2.78	19.20	
♀		7.2	15.3	CHK. BM. BP.			4.27	23.50	N.E. Kennen + Sigby
♀	Bottom of	House stringers	2.4	6+20.35					W. End. Outlet Ex. Box Culvert
5' Rt.		7.2	15.3				<u>27.77</u>		
6' "		2.4	20.1	6' Rt			6.3	21.5	
		5+70		4' Rt. Top. Box			7.53	20.24	
6' Rt		1.3	22.2	3.75 Rt. F.L.			12.20	15.57	
4'		1.3	21.2	♀ F.L.			12.20	15.57	
3' "		6.3	16.2	3.75 Lt. F.L.			12.20	15.57	
♀		6.3	16.2	4' " Top. Box			7.33	20.44	
2' Lt		6.3	16.2	6' Lt.			7.3	20.47	
3' "		1.6	20.9	T.P.	6.91	30.87	3.91	23.96	
6' "		1.6	20.9						

30.87

8+19.5⁸ E. End Inlet Ex Box culvert. Page 25

6' Lt		30.87 7.0	√3.87
4' "	Top. Culvert	6.91	√39.8
3.75' "	F.L.	11.22	19.66
⊕	F.L.	11.22	19.65
3.75' Rt	F.L.	11.22	19.65
4' Rt	Top. Culvert	6.91	√39.6
6' "		7.5	√3.5

8+23

6' Rt		9.1	√1.7
3' "		11.1	19.9
⊕		11.1	19.9
5' Lt		11.1	19.7
6' "		8.7	24.1

8+55.04 L 20°-31' Rt on split.

6' Lt		7.9	√2.9
⊕		9.8	√1.0
1' Rt		10.6	√0.2
5' "		10.6	20.2
6' "		9.9	√1.9

30.87

N. St. Drain 32

8+75

30.9

6' Rt		8.2	√1.7
2' "		10.4	√0.5
⊕		10.4	√0.5
2' Lt		10.4	√0.5
3' Lt		9.2	√1.7
6' "		8.1	√2.8
		9+00	

6' Lt		8.0	√0.9
4' "		9.9	√1.0
⊕		10.0	√0.9
6' Rt		7.8	√3.1

9+20

6' Rt		6.4	√4.5
⊕		8.5	√1.4
2' Lt		9.7	√1.2
6' "		9.7	√1.2

9+35

6' Lt		9.4	√1.5
⊕		9.4	√1.5
3' Rt		7.0	√3.9
6' "		6.2	√4.7

30.87

9+62 Δ 31-34 RT. on split-L6' RT $\frac{30.9}{2.1}$ 21.8

♀ Hub 9.05 21.9

1' Lt. 9.0 21.9

2' " 7.7 23.2

6' " 6.4 24.5

9+70

6' Lt 7.1 25.8

3' " 8.9 22.0

♀ 8.9 22.0

5' RT 9.0 21.9

6' " 7.7 23.2

9+95

6' RT 9.0 21.9

♀ 9.0 21.9

5' Lt 8.8 22.1

6' " 7.9 23.0

10+15

6' Lt 7.3 23.6

3' " 8.4 22.1

♀ 8.4 22.1

30.87

N. St. Drain

33

30.9

1' RT 8.8 22.1

6' " 6.4 24.5

10+50

6' RT 4.8 26.1

♀ 6.6 24.3

1' Lt 7.9 23.0

6' " 7.9 23.0

10+65

6' Lt 5.7 26.2

♀ 6.2 24.7

6' RT 5.8 25.1

10+85

6' RT. 5.0 25.9

♀ 6.2 24.7

6' Lt 6.8 24.1

T.P. 11.94 35.47 7.34 23.53

35.47

10+93 $\Delta 16$ 44' RT on split of L
35.5
10.4

6' LT

75.1

2' "

9.1 76.4

±

9.3 76.7

3' RT

9.3 76.7

6' "

8.3 77.7

11+08

6' RT

4.0 31.5

±

8.0 72.5

6' LT

9.5 76.0

11+15

6' LT

11.6 73.9

±

8.0 77.5

6' RT

6.0 79.5

11+21

6' RT

8.2 27.3

±

8.5 29.0

3' LT

8.8 26.7

4' "

11.7 23.8

6' "

11.7 23.8

35.47

N. St Drain 34

11+35

35.5

11.3

6' LT

74.2

±

9.6 75.9

2' RT

7.9 77.6

6' "

7.9 77.6

11+52

6' RT

7.6 77.9

±

11.0 74.5

5' LT

11.0 74.5

6' "

7.4 78.1

11+62

6' LT

8.1 77.4

±

10.9 74.6

4' RT

10.9 74.6

6' "

9.5 76.0

11+79

6' RT

10.9 74.6

±

6.2 79.3

6' LT

3.9 31.6

	35.47				35.47	5.11	N. St. Drain	35	
6' RT	11+9	$\frac{38.5}{2.1}$	33.4		12+25	$\frac{38.5}{4.0}$	31.5		
±		4.4	31.1			6.6	28.9		
6' LT		6.7	28.8			5.9	29.6		
19' Lt. Top. 14" Sewer Main		9.05	26.45			5.5	30.0		
		Sewer Pipe Exposed			J.P.	8.50	38.86	5.11	30.36
9.05								$\frac{38.9}{12+31}$	31 P.I. Puck to Line
8.88		8.117							
0.17 fall in 8'		$\frac{.02125}{.02125} = 2.125$	0%						
		12+00			6' Lt	9.1	29.8		
6' Lt.		0.9	34.6		±. ctr. 5'x5' Toilet	(Connected To 14" Sewer.)	9.1	29.8	
±		3.3	32.2		3' Rt	9.1	29.8		
6' Rt.		5.9	29.6		5' "	7.5	31.4		
		12+15			6' "	7.5	31.4		
6' Rt		7.0	28.5						
±		6.8	28.7						
6' Lt		6.1	29.4						
		12+24							
6' Lt		5.5	30.0						
±		5.9	29.6						
6' Rt		6.6	28.9						

12+21²

± Top. 14" Vitrified Sewer Pipe 11.50 27.36

12+40

6' Rt 7.1 31.8
± 7.3 31.6
6' Lt 8.7 30.2

38.86

12+60

38.86

7.6

31.3

6' Lt

±

7.2

31.7

6' Rt.

7.2

31.7

12+91⁸

6' Rt

6.4

32.5

± Top. Ex. ent. cl.

7.00

31.9

6' Lt.

6.9

32.0

13+12⁹⁶ Δ 8-32 Rt

6' Lt

5.7

33.2

±

6.3

32.6

3' Rt Top. ent. cl.

6.11

32.75

6' "

5.9

33.0

13+47⁶3' Lt. W. edge pav. 21st St.

4.94

33.92

13+50²± = W. edge pav. 21st St.

5.06

33.80

13+52⁴3' Rt. = ^{f = gutter} W. edge pav. 21st St.

5.19

33.67

3' Rt. Top. ent. cl.

4.35

34.51

38.86

38.86

N. St. Drain

36

13+63⁴⁸ P.I. ± Ex. Box. Culvert

3' Lt on pav

4.19

34.67

±

" "

4.45

34.21

2' Rt. FL Ex. Culvert.

12.67

26.19

3' Rt gutter Pav.

4.63

34.73

3' Rt Top. cl.

3.82

35.04

T.P. 11.48

49.11

1.23

37.63

T.P.

0.71

40.96

8.86

40.25

17+27⁷³ E. End. (Inlet) Ex. Box Culvert.

Page 19.

6' Rt

40.96

2.0

38.96

3' Rt. Top. Headwall.

2.38

38.58

2.5 " F.L.

10.31

30.65

± F.L.

10.31

30.65

2.5 Lt F.L.

10.20

30.76

3' " Top. Headwall

2.33

38.63

6' Lt

2.6

36.3

	40.96		
17+29	41' L	37	0.47 Lt. on split L
			40.96
6' LT		2.0	38.9
3.2" = Wing wall		2.7	38.2
3.0"		10.4	30.5
ϕ		10.6	30.5
3' RT		10.4	30.5
3.1" = Wing wall		3.8	37.1
6' "		3.2	37.7
	17+35	5	8" sewer
Top. C.I. Pipe		3.68	37.28
	17+45		
6' RT		7.4	33.5
3' "		9.4	31.5
ϕ		9.7	31.2
6' LT		6.5	34.4
	17+70		
6' LT		5.3	35.6
ϕ		7.1	33.8
3' RT		9.3	31.6
6' "		9.3	31.6

	40.96	N. St. Drain	37
	18+00	40.96	
6' RT		7.6	33.5
ϕ		6.0	34.9
6' LT		5.4	35.5
	18+50		
6' LT		5.2	35.7
ϕ		5.2	35.7
3' RT		5.7	35.2
6' "		7.9	33.0
	18+68		
6' RT		7.8	33.1
3' "		7.6	33.3
ϕ		5.1	35.8
6' LT		4.0	36.9
	18+75		
6' LT		5.0	35.9
ϕ		7.6	33.3
6' RT		8.0	32.9

		40.96		
		18+90		
		40.96		
6' RT		7.7	33.7	
∅		8.1	32.8	
5' LT		8.1	32.8	
6' "		5.0	35.9	
	18+97.4	6-22'	LT. on split.	
6' LT.		4.0	36.4	
5' "		8.0	32.9	
∅		8.0	32.9	
6' RT		7.2	33.7	
	19+06.4	W. End (Outlet) Ex Box Culvert.		
6' RT		2.6	38.5	
4' "		2.8	38.1	
3.8' "		6.8	34.1	
∅	Flow Line	6.87	34.09	
∅	Top. Culvert	1.04	39.92	
2' Lt.	FL	6.80	34.16	
2' "	T.	6.4	39.56	
6' "		2.7	38.2	
T.P.	12.93	52.86	1.03	39.93

		52.86		
	21+73.8	E. End (Inlet) Ex Pipe Culverts		
		52.86		
6' Lt.	Top. Headwall	8.71	44.15	
6' "		11.0	41.8	
2' "	FL 36" Pipe	12.90	39.96	
∅	FL 18" Pipe	12.90	39.96	
3' RT	FL 36" "	12.90	39.96	
6' "		12.9	39.9	
6' RT.	Top. Headwall	8.70	44.16	
		21+90		
6' RT		11.7	41.1	
3' "		12.6	40.2	
∅		11.1	41.7	
6' Lt.		9.6	43.2	
		22+20		
6' Lt.		8.5	44.3	
3' "		10.2	42.6	
∅		10.7	41.1	
3' RT		11.6	41.2	
6' RT.		10.5	42.3	

52.86

22+70

52.86
8.8

44.0

6' RT

10.0

47.8

4' "

11.1

41.7

2' "

4 10.2

42.6

Φ

9.4 43.4

4' LT

8.0 44.8

6' "

23+28

7.1 45.7 ✓

6' LT

9.3 43.5 ✓

4' "

9.7 43.1 ✓

Φ

11.1 41.9 ✓

2' RT

9.4 43.4 ✓

4' "

7.4 45.4 ✓

6' "

23+50

7.1 45.7 ✓

6' RT

10.6 42.2 ✓

Φ

9.2 43.6 ✓

2' LT

8.3 44.5 ✓

6' "

52.86

23+68 48 W. End (outlet) Ex. Box Culvert.

52.86
7.2

45.6 ✓

6' LT

6.41 46.45 ✓

2.7 " Top Culvert

10.78 47.1 ✓

2' "

11.30 41.56 ✓

Φ F.L.

10.6 42.2 ✓

2' RT

6.40 46.46

2.7 RT Top Culvert

7.60 45.2 ✓

6' RT

3.84 49.02 N.E. 24th
+ Commercial

BM. B.P.

39

1-16-35
 200 ft
 1/2 in
 1/2 in

Culvert Profile 1.5' E. of W. d. Line 24th St.
 from N. Line Commercial S. to Proposed Storm Drain

B.M. B.P.	3.87	52.89	57.04	49.02	N. E. 24 th + Commercial
0+00 = N. Line Commercial Produced from East					
W. cmt. ch.			3.55	49.34	✓
gutter	PAV.		4.24	48.65	✓
1.5' E.	"		4.19	48.70	✓
0+14 ⁵ = N. End. Ex. Curb. Inlet					
W. cmt. ch.			3.79	49.10	✓
gutter			4.49	48.40	✓
1.5' E.			4.48	48.41	✓
0+17 ⁵ = Ex. ch. Inlet					
W. cmt. ch.			3.82	49.07	✓
gutter on grating			4.61	48.78	✓
1.5' E. "	"		4.58	48.31	✓
F.L. 18" outlet pipe			8.06	44.83	✓
0+20 ⁵ S. End. Ex. ch. inlet					
W. cmt. ch.			3.83	49.06	✓
gutter			4.55	48.34	✓
1.5' E.			4.54	48.35	✓

				52.89	52.89	40
0+31.5 = N. ch. Line Commercial to W.						
W. ch. line	PAV.			4.38	48.51	✓
1.5' E.	"			4.38	48.51	✓
10' W. = W. end.	"			4.63	48.26	✓
10' W. = W. "	cmt. ch. met.			3.82	49.07	✓
0+45 = N. Rail						
1.5' E. of W. ch.				4.55	48.34	✓
0+50 = S. Rail						
1.5' E. of W. ch.				4.52	48.37	✓
0+81.5 = N. End. Ex. Grating						
1.5' E. of W. ch.	Top. grating			5.95	46.94	
1.5' " " " "	F.L. Pipe			10.32	42.57	
0+84 = S. ch. Line Commercial						
1.5' E. of W. ch.	F.L. 18" outlet pipe			10.40	42.49	
1.5' " " " "	Ex. grating			6.02	46.87	
1.5' " " " "	cmt. ch.			5.26	47.63	
4' " " " "	" " "			5.23	47.66	E. End. Ex Curb. Inlet
4' " " " "	gutter PAV.			5.93	46.96	
11.5' " " " "	" " "			5.91	46.98	
11.5' " " " "	cmt. ch.			5.20	47.69	

52.89

0 + 84. (con)

~~52.89~~

1.0 W. of W. ch. = gutter Pav 6.00 46.89 ✓

W. end. Ex
Curb. Intec

1.0 " " " " S. cent. ch. 5.30 47.59 ✓

8.5 W " " " " " " 5.51 47.38 ✓

Curb.
SUNK.

8.5 " " " " gutter Pav 6.08 46.81 ✓

0 + 94

1.5 E. of W. ch. 5.1 47.7 ✓

11.5 " " " " 4.8 48.0 ✓

8.5 W " " " " 4.8 48.0 ✓

1 + 00

1.5 E. of W. ch. 3.1 49.7 ✓

11.5 " " " " 3.0 49.8 ✓

8.5 W " " " " 2.9 49.9

1 + 20

1.5 E. of W. ch. 7.4 45.4 ✓

11.5 " " " " 7.0 45.8 ✓

8.5 W " " " " 4.7 48.1 ✓

1 + 34

1.5 E. of W. ch. 3.6 49.2

11.5 " " " " 6.2 46.6

8.5 W " " " " 2.1 50.7

52.89

1 + 47

~~52.89~~

1.5 E. of W. ch. 2.5 50.3 ✓

11.5 " " " " 6.0 46.8 ✓

8.5 W " " " " 2.6 50.2 ✓

1 + 60

1.5 E. of W. ch. 6.9 45.9 ✓

11.5 " " " " 8.1 44.7 ✓

8.5 W " " " " 4.9 47.9 ✓

1 + 70

1.5 E. of W. ch. 7.9 44.9 ✓

11.5 " " " " 7.8 45.0 ✓

8.5 W " " " " 8.7 44.1 ✓

1 + 79 + 07

4. Main Culvert 10.9 42.0 ✓

41

Culvert Profile for Curb Inlet & Culvert
S.W. Cor. Commercial + Harrison Ave.

Plat Page 21

X 52.89 Page 41.

00 = S. Curb. Commercial

10' RT. (W) of d. cmt. d	52.89 4.29	48.60	✓
10' " " " " gutter	5.12	47.77	✓
± " "	4.98	47.91	✓
± cmt. d	4.15	48.74	✓
10' Lt. (E) on Curb. Return	4.07	48.82	✓ cmt. d
10' " " " " "	4.83	48.06	gutter

0+10.5 = S. side cmt. walk

10' Lt.	3.83	49.06	
±	3.89	49.80	
10' RT.	4.00	48.84	

0+18

10' RT	3.8	49.0	
±	3.5	49.3	
10' Lt	3.5	49.3	

0+25

10' Lt	3.6	49.2	
±	1.9	51.0	
10' Rt	2.3	50.5	

52.89

0+37

~~52.9~~
4.9

48.0

10' Rt

φ

3.6

49.3

10' Lt

5.5

47.4

0+45

10' Lt

10.1

42.8

φ

9.4

43.5

10' Rt

9.3

43.6

0+50 = φ Main Culvert

φ

10.4

42.5

X Sec Main Culvert. from Sta 20+02
To sta 21+73 ~~82~~ Plat Page 20.

52.89

44

π 52.89 Page 41

20+02

~~52.89~~

15' LT

21+00

~~52.9~~

2.9

50.0 ✓

♀. E. Gutter Irving Ave

3.99

48.90

♀

2.9

50.0 ✓

♀. " Cmt. Curb " "

2.95

49.94

15' RT

2.5

50.4 ✓

20+25

~~52.9~~

21+20

15' RT.

2.3

50.6

15' RT

2.2

50.7 ✓

♀

2.6

50.3

♀

2.5

50.4 ✓

15' LT.

2.5

50.4

15' LT.

2.8

50.1 ✓

20+35 ¹⁹ End. Original Culvert. L 2'-2" RT.

21+35

15' LT

2.5

50.4

15' LT

2.0

50.9 ✓

5' "

3.5

49.4

3' LT

2.7

50.2 ✓

♀

2.5

50.4

♀

3.3

49.6 ✓

5' RT

2.0

50.9

5' RT

4.1

48.8 ✓

20+65

15' "

4.2

48.7 ✓

15' RT

3.2

49.7

21+55

5' "

4.2

48.7

15' RT

7.1

48.8

♀

3.6

49.3

7' "

4.4

48.5

5' LT

2.8

50.1

♀

3.4

49.5

15' "

2.7

50.2

15' LT

2.9

50.0

52.89

21+65

 $\frac{52.9}{3.8}$

3.8

49.1 ✓

15' LT

±

6.2

46.3 ✓

5' RT

7.3

45.6 ✓

15' "

5.2

47.7 ✓

21+73 ⁸²

15' RT

6.9

46.0 ✓

± Top. emb. Headwall

8.74

44.15 ✓

10' LT

8.1

44.8 ✓

15' "

6.0

46.9 ✓

45

5-29-35
Walker
Bliss

X see Alley BIK 6
Watkins + Biddle

Indexed
C.S.K.

From 32nd St. West. Bet. Ivy + Juniper

BM. B.P. 4.13 289.72 ✓ 282.99 + Ivy
T.P. 5.58 288.18 ✓ 6.52 282.60

Alley Paved. from E. Line 31st + 370.4 East

0 + 00 = E. Line 31st

3 + 70.4 = E. End. Pav

S. pav. 5.70 287.48
E " 5.89 287.79
N " 5.65 287.53

3 + 70.4 W. face ent. el.

N Top. ent. el. 5.15 283.03 ✓
E " " " 5.35 282.83 ✓
S " " " 5.07 283.11 ✓

3 + 70.4 W. face. ent. el.

1.25 S. of E. = S. edge ch. inlet.

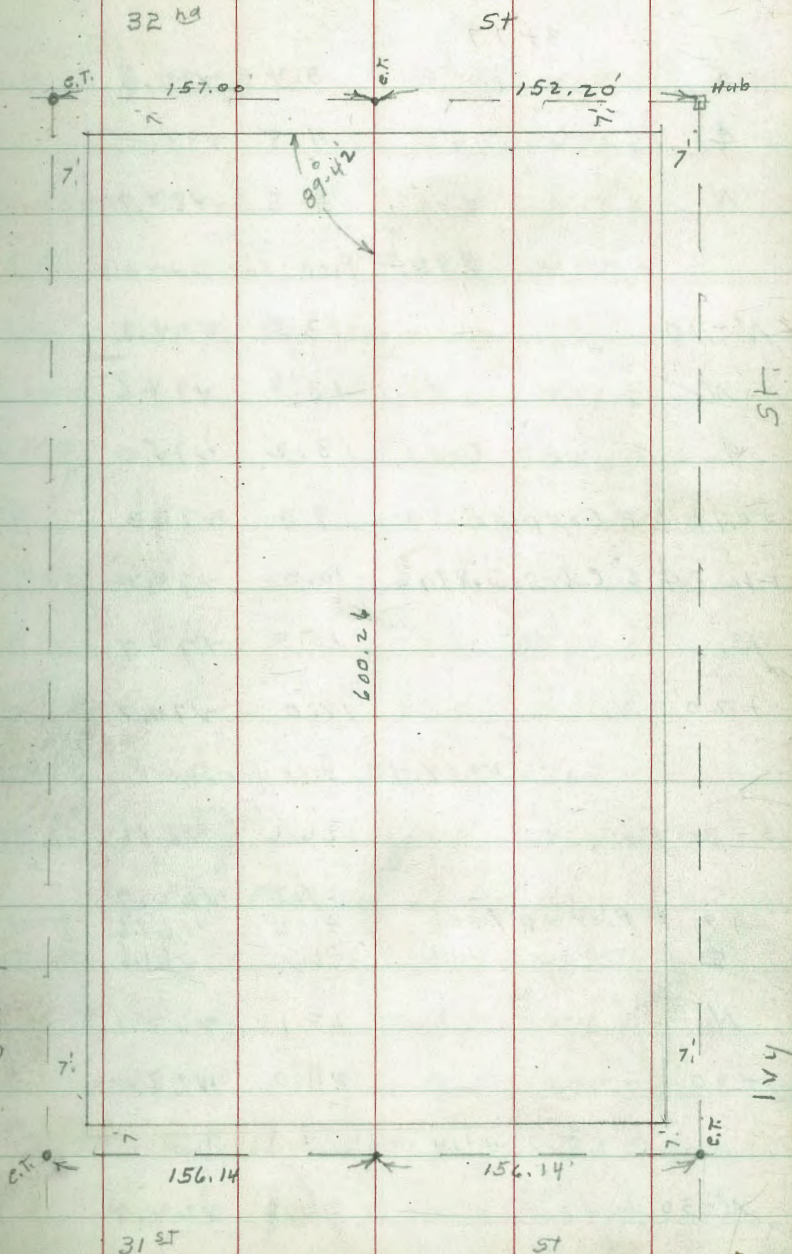
1.25 N " " = S " " "

3 + 71 { W. End 12' Cor. Iron Culvert.
E. Side ch. inlet

E F.L. 7.3 280.9

PLOT 10-10-41
(Pacific 2008)

Juniper



288.18
3+77

S 5.4 487.8
E 4.8 483.4
N 5.5 482.7

390⁶ Pier for Sewer pipe

N-10 13.5 474.2
N 13.6 474.6
E 13.2 475.0

+0.4 = E 2" Gas pipe 9.9 478.3
+11' = E 6" C.I. Sewer Pipe 10.0 478.7

S 15.5 472.7
+20' 18.0 470.7

4+08.10 Pier for Sewer

S-30 24.6 461.6
S 27.5 460.7
+9' E Pier = E Pipe 26.6 461.6 ground
E 26.6 461.6

N 25.1 463.1
+30 24.0 464.2

4+14 Culvert location

N-30 26.0 464.7
N 26.7 461.5

288.18

Alley BIK 6,
Watkins + Biddle 47

d 27.7 460.5
S 29.8 458.4
+30 31.8 456.4

+40 32.7 455.5

4+26 Pier for Sewer

S-40 29.6 458.6
S-8' 26.3 461.9
S 23.7 464.5

+9 = E Pier 23.6 464.6 ground

E 23.6 464.6
N 21.4 466.8

+20 20.3 467.9
+30 19.0 469.2

4+41 Pier for Sewer

N-10 10.4 477.8
N 11.4 476.4
E 12.5 475.7

+1 = E Pier 12.6 475.6 ground

S 15.4 472.8
+20 14.7 471.5

288.18

T.P. 7.96 286.64 ✓ 9.50 278.68

4+47

S-15 13.9 277.7

S 10.3 276.3

+9. Top, 6" C.I. Sewer Pipe 8.03 278.61

+9.7 2" Gas Pipe

φ 8.0 278.6

N 7.2 279.4

+10 6.9 279.7

4+55

N 5.9 280.7

φ 6.2 280.4

S 7.3 279.3

+10 8.2 278.4

4+70

S 5.0 281.6

φ 5.1 281.5

N 4.4 282.2

5+06 Garage on N. emt. floor 77' Back ✓

S 3.7 282.9

φ 3.6 283.0

286.64

Alley BIK L. Watkins + Biddle 48

N. 2.7 283.9

+7. S. End emt. aprons 2.25 284.39 ✓

+17. floor 1.60 285.04 ✓

{ S. End. Garage on S. line emt. floor east Entrance.
5+18.5 } W " emt Drive Way.

N. 2.5 284.1

φ 3.3 283.3

S. = { floor of Garage
N. W. Cor emt. Dr 3.72 284.94 ✓

from 5+12 to 5+45. Lattice fence on N. 1.5 in Alley

at sta 5+83 E. End fence it is 0.5 in Alley.

T.P. 4.77 288.29 ✓ 3.12 283.52

5+28

9.2 S. of φ = N. Edge emt. Drive 5.09 283.40 ✓

5+47

9.0 S. of φ = { S. End. emt. Drive
N. Edge emt. Drive 4.75 283.54 ✓

5+44

S. line = N. edge emt. walk 4.75 283.54

{ W. side emt. Porch.
5+54 } E. End emt. walk

S. line = N. Edge emt. walk 4.60 283.69 + ground ✓

0.4 N. of S. line = N " " porch 3.33 284.96

φ 4.0 284.29

	288.29		
	5+54 (con)		
N.	3.7	784.6	
	5+60 = 2. End. Curb. Poreh.		
0.4 N. of S. Line = N. end. Poreh	3.35	784.94	Top. Poreh
S. line	4.4	783.9	ground.
	5+80		
N.	3.3	785.0	
+ S	3.8	784.5	
±	4.5	783.8	
S.	4.4	783.9	
	6+00 ²⁶ = W. Line 32 nd St		
S	4.7	783.6	
±	5.2	783.1	
+ 2	4.2	784.1	
N.	3.7	784.6	
3.9' E. of W. line on N. } = { W. End. Curb. Returns			
3.4' " " " " " S. } = { W. Edge Pavmt.			
N. line Top. emt. el.	4.42	783.87	
N. " G. pav	4.70	783.59	
± " "	5.21	783.08	
S. line pav. + Top. of el.	5.03	783.76	

	288.29				Alley Bldg. Watkins & Biddle 49
13.7 E. of W. line on N. } = W. Curb Line				32 nd St.	
13.4 " " " " " S }					
S. line Top. emt. el.	5.22	783.07			
S. " pav.	5.71	784.58			
± " "	5.49	784.80			
N. line " "	5.09	783.70			
N. " Top. emt. el.	4.49	783.80			
T.P.	10.57	297.17	1.69	286.60	
R.M. B.P. S.E. Juniper + Bancroft.	3.63	293.54		293.58	

393.91

51

3+30		9.7	384.2	
3+70	S. Line Waxerly St.	10.51	383.40	Hub
3+78		11.2	382.7	
4+00		25.4	368.5	
4+13		29.0	364.9	
4+21	Wash.	33.0	360.9	Bottom of Wash
BM. B.P. S.E. Adams + Boundary		2.85	391.06 = 390.96	

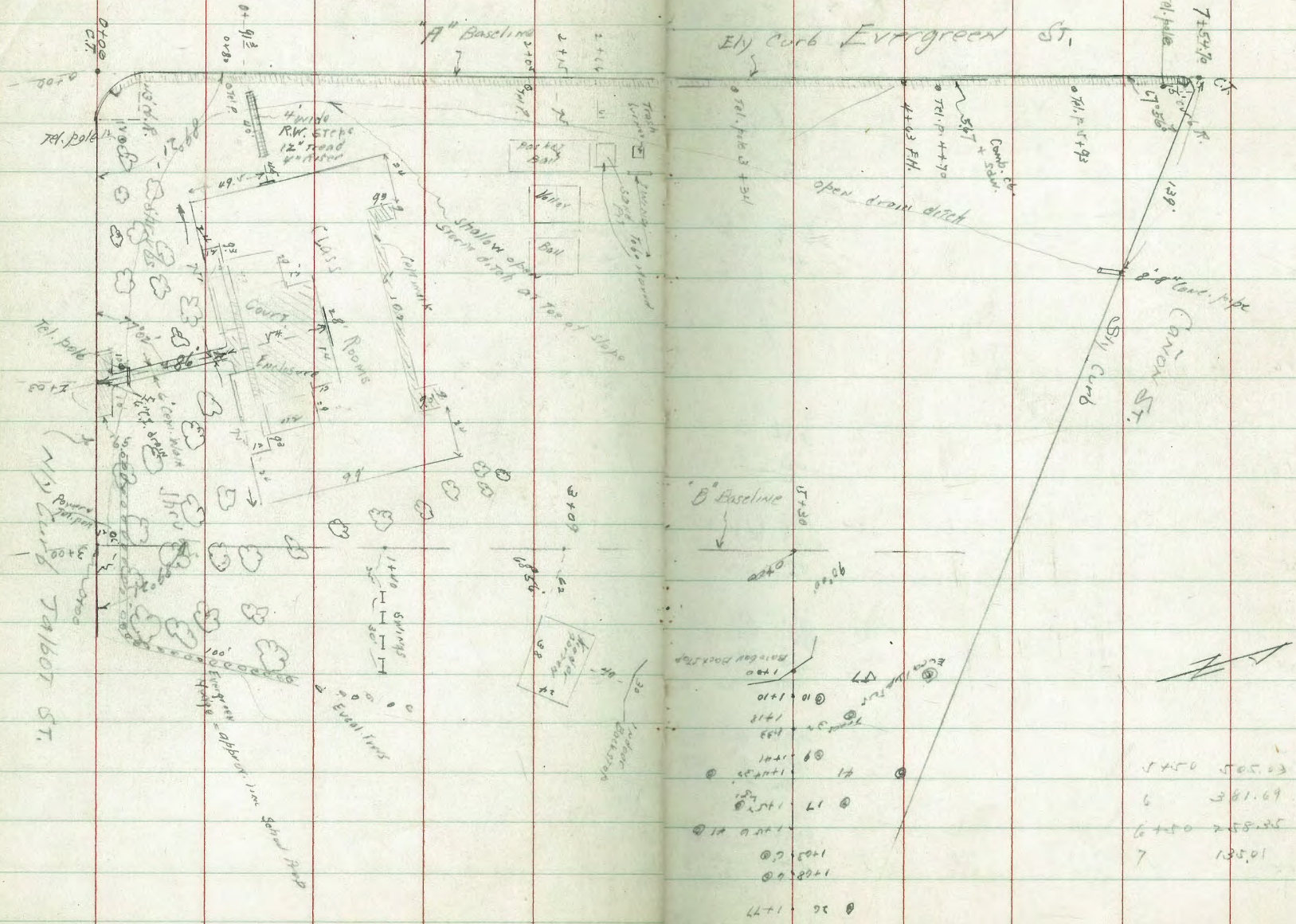
Location of Impms etc. and
 Contours of Caberto Grade School
 Roseville, Pt. Loma.

Moore
 4-25-05
 10-11-05
 2-15-36

indexed
 C.S.K.

52

EN Curb Evergreen St.



- 1700
- 1710
- 1718
- 1733
- 1741
- 1745
- 1751
- 1757
- 1760
- 1763
- 1768
- 1777

5	545.5	505.03
6	381.69	
6	150	258.35
7		135.01

"Curb
Baseline →

			522	396	411	386	372	339	318
2+06	233 26	2.6 10	10.0 25	15.0 45	13.5 50	16.0 120	17.4 170	20.7 155	22.8 250
2+00	51.5 3.05 26	51.5 3.1 10	39.9 12.7 21	40.1 14.5 75	39.9 12.7 100	38.7 15.9 150	37.8 16.8 200	35.7 19.2 220	36.6 18.0 250
1+00	50.9 3.0 18	50.7 4.4 15	40.7 14.4 70	41.3 12.6 Floor El.	40.3 14.3 120		39.9 14.7 175	35.0 19.5 250	
0+86							38.58 15.97 CEM WALL	35.00 19.5 250	
0+50	50.34 4.1 28		48.6 6.0 35	40.6 14.0 60	40.4 14.4 100	38.6 16.0 175		35.9 19.6 250	
0+35	49.69 4.86 207	50.2 4.35 NCC	48.2 6.4 35	46.5 10.1 35	40.1 14.5 100	38.5 16.1 175		35.0 19.6 250	
0+25	49.9 4.89 207	49.4 4.4 1.5 28	48.4 6.4 35	45.8 9.8 60	40.4 12.4 100	38.5 16.1 175		34.9 19.7 250	
0+10	49.7 4.83 207	49.9 4.77 11.6	48.4 6.4 35	47.4 9.4 60	44.1 10.5 100	38.6 16.0 175		34.9 19.7 250	
0+00	49.61 4.94 207	49.5 4.94 30.901	48.3 6.25 35	47.8 10.37 10.66	44.1 10.5 100	38.6 15.87 175	38.19 16.36 2.03.6	34.75 19.5 250	

NWBP 2.78

54.55

51.77

Evergreen
20/607

54.55

46¹ 46³ - 44³ 39⁸ 38³

840 8.3 10.3 14.8 16.2 FL. 8" pipe = dev. 17.00 90T.
1350 15 50 100 1350 16

43⁵ 43⁴ 41⁶ 41⁶ 39⁴ 38⁸ 37⁴ 39⁴ 38² 36⁴ 34² 32¹

1100 11.2 100 12.0 15.3 15.8 17.2 15.4 16.4 18.2 19.7 21.9
15 50 70 100 100 110 110 120 150 200 250 300 350 400

47⁰ 46⁰ 43⁰ 38⁶ 37¹ 38⁴ 37² 35² 33¹ 31²

530 6.6 11.0 10.0 12.2 10.2 17.4 19.4 21.5 23.4
20 40 70 97 100 110 150 200 250

50⁶ 49⁸ 43² 41⁴ 38⁶ 37² 38⁸ 36⁶ 33² 31⁹ 29⁹

400 11.4 11.4 13.2 16.0 17.4 15.8 18.0 20.7 22.7 24.7
20 25 40 75 80 80 100 150 200 250

52⁶ 52³ 44⁶ 41⁵ 35² 37⁹ 39⁴ 36⁸ 35⁸ 33² 31¹ 30

200 2.3 10.0 13.1 15.4 16.7 15.2 17.8 18.8 21.4 23.5 24.6
25 30 40 66 70 75 90 100 150 200 250

52⁸ 52⁸ 43⁶ 40⁶ 38⁴ 39⁶ 36⁵ 35⁶ 35² 31³ 29⁶

180 1.8 11.0 14.5 16.2 15.0 18.1 19.0 21.0 23.3 25.0
20 30 45 60 65 75 100 150 200 250

T.P. Top 16 3+84 142 54.62 135 53.20 54.62

53.21 53⁷ 38⁹ 40⁷ 36⁹ 35⁴ 33⁴ 31⁹ 30⁶

150 0.9 15.7 13.9 17.7 19.2 21.2 22.7 24.5
25 40 50 75 100 150 200 250

52⁵ 46⁵ 39⁴ 40⁴ 39² 35⁴ 35.9 33⁶ 31⁵

20 8.1 15.2 13.8 15.2 19.2 20.7 21.0 23.1
20 45 50 60 130 170 180 250

54.55

7

6+50

6

5+50

4+84

4+40

T.P. Top 16 3+84

3+84

2+90

54.55

54.55

2+80

"B" Baseline
 $\frac{0.0}{2.0}$ $\frac{0.0}{1.0}$ $\frac{4.4}{2.2}$ 31.67 30.67 27.67
 8.4
 96 approx line

1+50

33.07 31.07 28.77
 $\frac{0.0}{4.0}$ $\frac{0.0}{3.0}$ $\frac{2.0}{2.0}$ 31.07 30.07 27.77
 7.2
 70

1+00

32.07 31.07 30.27
 $\frac{0.0}{4.0}$ $\frac{0.0}{2.0}$ $\frac{2.0}{1.0}$ 31.07 30.07 29.27
 5.8
 53 approx line

0+80

33.37 31.97 27.27
 $\frac{2.7}{2.5}$ 2.1

0+60

32.07 30.87
 Flag Pole 4.0 5.2
 37 approx line

0+15

32.37 31.27
 3.7 4.8
 18 approx. EL School Prop.

0+00

31.57
 4.50 Tot eb

T.P 3.01 36.07 9.52 3396 36.07

T.P 0.25 42.58 1239 22.23

7+33 Approx.

"A" Baseline
 45.1 35
 9.5 15
 9.5 = 67%

45.1
 11.04 = 6 EC.

5d. 62

5d. 62

check to SWBP CANON ROSACRANZ
 T.P. 2.18 26.90 6.26 20.64 20.95
 7.51 24.72 0.01

6
 +50

5

4 +50

4

3 +50

T.P.

5.19 32.23 9.03 27.04

3 +00

2 +50

36.07

"B"
 30 33 25 57
 1.9 $\frac{3.64}{81.7.06}$
 27 13 28 13 27 13 26 53 25 13 25 08
 3.1 $\frac{4.1}{50}$ $\frac{5.1}{100}$ $\frac{5.7}{150}$ $\frac{7.1}{200}$ $\frac{7.5}{205.0}$
 28 13 27 43 26 43 25 63 24 13 23 83
 3.6 $\frac{4.8}{50}$ $\frac{5.8}{100}$ $\frac{6.6}{150}$ $\frac{8.1}{200}$ $\frac{8.4}{225}$
 28 43 27 13 26 13 25 53 23 93 23 83
 3.8 $\frac{5.1}{50}$ $\frac{6.1}{100}$ $\frac{6.7}{150}$ $\frac{8.3}{200}$ $\frac{8.4}{212}$
 28 13 26 93 25 63 24 93 24 03
 4.1 $\frac{5.0}{50}$ $\frac{6.6}{100}$ $\frac{7.3}{150}$ $\frac{8.2}{195}$
 28 53 27 13 26 23 25 13
 3.7 $\frac{5.1}{50}$ $\frac{6.0}{100}$ $\frac{7.1}{150}$

32.23

29 67 27 67 26 07 25 07
 6.4 $\frac{8.1}{50}$ $\frac{10.0}{100}$ $\frac{11.0}{142}$ 11/21/07
 30 07 28 57 26 77
 6.0 $\frac{7.5}{50}$ $\frac{9.3}{112}$ 11/21/07

36.07

5-20-37
Miller
Walker
B. Ross

Maple St. X Sec.
32nd to Bancroft.

Graded 56' 0" wide
10' 0" deep
10' 0" deep
10' 0" deep
(80' wide
20' deep
20' deep)

indexed
visit.

302.38

N. + S = 10' from Property lines = limit of grading

S.W. 32nd
+ Maple

BM.	1.27	302.38	301.11	S	2.5	299.9
		00-10 = E. Curb. Line 32 nd St				0+50
S.	Top. ent. d.	2.58	299.80	S	+1.4	303.8
S.	gutter pav.	3.09	299.29	+2	3.1	299.3
+10 cl.	" "	3.33	299.05	d	4.1	298.3
"	" "	3.76	298.62	+2	4.5	297.9
±	" "	4.19	298.19	"	4.3	298.1
"	" "	4.65	297.73	±	4.5	297.9
cl	" "	5.42	296.96	"	5.1	297.3
N	" "	6.05	296.33	d	5.3	297.1
N	Top ent. d.	5.27	297.11	N.	4.8	297.6
		0+00 = E. Lin - 32 nd St.				1+00
N		5.0	297.4	N	5.5	296.9
N	ent. d. E. End	5.09	297.29	cl	5.7	296.7
G.	pav " "	5.60	296.78	"	5.6	296.8
"	" " "	4.71	297.67	±	5.1	297.3
±	" "	3.98	298.40	"	5.0	297.4
"	" " "	3.56	298.82	+8'	5.4	297.0
G.	" " "	3.30	299.08	d	4.8	297.6
				+6	4.4	298.0
S cl.	" "	2.54	299.80	S	3.3	299.1

302.38

1+50:

S		3.7	298.2	
+4		5.2	297.2	
cl		5.7	296.7	
+2		6.2	296.2	
"4		6.0	296.4	
±		6.1	296.3	
"4		6.3	296.1	
+8		6.8	295.6	
cl		6.3	296.1	
+7		5.9	296.5	
N		4.9	297.5	
	2+00=			
N		7.0	295.4	
T.P.	6.01	301.15	7.24	295.14
cl		5.9	295.30	
+1		6.4	294.8	
"4		6.1	295.1	
±		6.0	295.2	
"4		6.0	295.2	
+8		5.9	295.3	

301.15

Maple

58

cl		5.5	295.2
+8		4.9	296.3
S		3.5	292.7
	2+03.22 on N. cl. Line 2+08.22 on S. cl. Line		} = W. edge Pav + W. End. cnt. cl Returns
	S. on cnt. walk Return solid to curb. cnt. cl	5.22	296.83
	W. End	5.64	295.51
G pav.	" "	6.30	294.85
"4	" "	6.12	295.03
±	" "	6.11	295.04
"4	" "	4.31	294.84
G	" "	6.56	294.59
cnt. cl.	" "	6.02	295.13
+5	S. edge cnt. walk W. End.	5.95	295.20
+10 N	N. " " " "	5.83	295.32
	6+20 = W. curb. of Bancroft St		
N.	Top. cnt. cl	6.16	294.94
N.	gutter pav.	6.85	294.30
cl	" "	6.76	294.39
"4	" "	6.71	294.44
±	" "	6.58	294.57

301.15

W. ch. of Bancroft. (Con)

1/4 pay 6.47 294.68

ch pay 6.39 294.76

S. Line " 6.27 294.88

S " Top. amt. ch 5.58 295.57

B.M. B.P

7.07 294.04

N. E. Nutmeg

+ Bancroft

294.08

Maple

59

Moore
7-10-37

Xsec of Mason, Twiggs and
Sunset. around Blk 450 Old Town

L.T. = Wily

P.T.

60

Xsec of Mason

Indexed
e.s.k.

2+00

Juan to Sunset

21.4	21.0	19.4	19.8	24.7	26.9	27.0	26.8
$\frac{9.2}{25}$	$\frac{9.6}{25}$	$\frac{11.2}{15}$	$\frac{10.8}{11}$	5.9	$\frac{2.7}{5}$	$\frac{3.6}{15}$	$\frac{3.8}{25}$

1+50

20.1	20.6	21.5	22.9	25.0	26.2	26.5	26.2
$\frac{10.5}{25}$	$\frac{10.0}{25}$	$\frac{9.1}{15}$	$\frac{7.7}{6}$	5.6	$\frac{4.4}{5}$	$\frac{4.1}{15}$	$\frac{4.4}{25}$

1+00

20.1	20.8	21.0	22.4	25.6	26.2	26.1	25.8
$\frac{10.5}{25}$	$\frac{9.8}{25}$	$\frac{9.6}{15}$	$\frac{8.2}{7}$	5.0	$\frac{4.4}{5}$	$\frac{4.5}{15}$	$\frac{4.8}{25}$

0+50

23.2	22.2	23.7	25.7	25.7	25.9
$\frac{8.4}{25}$	$\frac{8.4}{15}$	$\frac{6.9}{10}$	4.9	$\frac{4.9}{15}$	$\frac{4.7}{25}$

0+10

24.0	23.7	25.46	25.50	25.42	25.64
$\frac{6.6}{25}$	$\frac{6.9}{15}$	$\frac{5.6}{5 \text{ Pav}}$	$\frac{5.2}{5 \text{ Pav}}$	$\frac{5.20}{15 \text{ Pav}}$	$\frac{4.98}{25}$

0+00 = NLY JUAN

24.6	24.95	24.45	24.94	25.27	25.69	26.10
$\frac{6.0}{25}$	$\frac{5.67}{15.5}$	$\frac{6.17}{15.5}$	5.68	$\frac{5.35}{15 \text{ Pav}}$	$\frac{4.93}{25 \text{ Pav}}$	$\frac{4.52}{25 \text{ Pav}}$

T.P. 6.76 30.62 1.00 23.86

30.62

SW.B.P. 2.64 24.86 22.22

San Diego
Mason

LT = Wly

Z

PT.

62

MASON

Nly Sunset

23.6	24.1	25.8	30.10	32.4	32.3	32.3
$\frac{18.0}{25}$	$\frac{17.5}{25}$	$\frac{15.8}{15}$	$\frac{11.5}{14.25}$	$\frac{9.2}{6}$	$\frac{9.2}{15}$	$\frac{9.3}{25}$

E Sunset

20.0	21.1	23.1	28.0	31.1	31.1	31.0
$\frac{21.6}{25}$	$\frac{20.5}{25}$	$\frac{18.5}{15}$	13.6	$\frac{10.5}{7}$	$\frac{10.5}{15}$	$\frac{10.6}{25}$

T.P. 11.77 41.65 0.74 29.28

41.65

3+00 = Sly Sunset

18.0	19.6	23.2	26.4	27.4	29.7	29.9	29.9
$\frac{12.6}{25}$	$\frac{11.0}{25}$	$\frac{7.4}{15}$	$\frac{4.2}{9}$	3.2	$\frac{0.9}{6}$	$\frac{0.7}{15}$	$\frac{0.7}{25}$

2+75

17.1	19.1	23.1	24.8	26.3	28.7	28.8	28.7
$\frac{13.5}{25}$	$\frac{11.5}{25}$	$\frac{7.5}{15}$	$\frac{5.8}{10}$	4.3	$\frac{1.9}{2}$	$\frac{1.8}{15}$	$\frac{1.9}{25}$

2+50

19.6	18.1	20.8	23.6	25.6	27.9	28.1	27.9
$\frac{11.0}{25}$	$\frac{12.5}{25}$	$\frac{9.8}{15}$	$\frac{7.0}{8}$	5.0	$\frac{2.7}{5}$	$\frac{2.5}{15}$	$\frac{2.7}{25}$

30.62

30.62

Xsec of Sunset
Mason To Twiggs

Indexed
c.s.K.

LT

Z

PT

63

T.P. 12.52 66.34 0.39 53.82

52.8	52.6	52.1	52.3	50.4	51.0	51.4	50.4
$\frac{1.4}{25}$	$\frac{1.6}{15}$	$\frac{2.1}{14}$	19	$\frac{3.8}{14}$	$\frac{3.2}{15}$	$\frac{2.8}{23}$	$\frac{3.8}{25}$

1750

46.0	45.2	44.5	44.6	43.2	43.8	43.5	42.2
$\frac{8.2}{25}$	$\frac{9.0}{15}$	$\frac{9.7}{14}$	9.6	$\frac{11.0}{14}$	$\frac{10.4}{15}$	$\frac{10.7}{23}$	$\frac{12.0}{25}$

1700

T.P. 12.81 54.21 0.25 41.40

$\frac{54.21}{Z}$

38.4	37.6	36.8	37.3	36.1	36.6	36.4
$\frac{3.2}{25}$	$\frac{4.0}{15}$	$\frac{4.8}{14}$	43	$\frac{5.5}{14}$	$\frac{5.0}{15}$	$\frac{5.2}{25}$

0750

30.78 28.73

0+03 = 12" Culv. pipe F.L.

$\frac{10.87}{25}$ $\frac{12.92}{25}$

0+00 = Fly Mason

41.65

$\frac{41.65}{Z}$

					LT.		Σ		PT.		
					71.3	71.0	70.4	70.6	68.9	69.6	69.4
3700					$\frac{6.9}{25}$	$\frac{7.2}{15}$	$\frac{7.8}{14}$	7.6	$\frac{9.0}{14}$	$\frac{8.6}{15}$	$\frac{8.8}{25}$

T.P. 12.36 78.21 0.49 65.85

78.21
7

					64.9	64.3	63.6	64.1	62.4	62.9	62.9
2440					$\frac{6.4}{25}$	$\frac{2.0}{15}$	$\frac{2.7}{14}$	2.2	$\frac{3.9}{14}$	$\frac{2.4}{15}$	$\frac{3.4}{25}$

					63.2	62.2	61.5	61.9	60.3	60.7	60.4
2420					$\frac{3.1}{25}$	$\frac{4.1}{15}$	$\frac{4.8}{14}$	4.4	$\frac{6.0}{14}$	$\frac{5.6}{15}$	$\frac{5.9}{25}$

					60.3	60.0	59.1	59.4	57.7	58.2	57.9
2400					$\frac{6.0}{25}$	$\frac{6.3}{15}$	$\frac{7.2}{14}$	6.9	$\frac{8.6}{14}$	$\frac{8.1}{15}$	$\frac{8.4}{25}$

					57.1	57.0	56.3	56.7	55.0	55.4	54.9
1780					$\frac{9.2}{25}$	$\frac{9.3}{15}$	$\frac{10.0}{14}$	9.6	$\frac{11.0}{14}$	$\frac{10.9}{15}$	$\frac{11.4}{25}$

66.34

66.34
7

LT

~~E~~

RT

4+64 Note! Sewer broken thru

78.77
72.8
Top of 8" sewer → 8
should be lowered

4+44.25 27° RT

Δ = 90°
LR = 100

82.5	81.9	81.5	79.7		77.6	79.0
$\frac{3.5}{25}$	$\frac{4.1}{17}$	$\frac{4.5}{16}$	6.3	—	$\frac{8.4}{24}$	$\frac{7.0}{25}$

4+12.83 18° RT

86.8	83.0	82.7	82.1	80.8	79.0	79.4	78.1
$\frac{+0.8}{25}$	$\frac{3.0}{23}$	$\frac{3.2}{17}$	$\frac{3.9}{14}$	5.2	$\frac{7.0}{12}$	$\frac{6.6}{13}$	$\frac{7.9}{25}$

3+81.42 9° RT

81.4	80.6	80.1	79.3	77.7	78.0	77.2	77.8
$\frac{4.6}{25}$	$\frac{5.4}{18}$	$\frac{5.9}{17}$	6.7	$\frac{8.3}{13}$	$\frac{8.0}{14}$	$\frac{8.8}{23}$	$\frac{8.2}{25}$

T.P. 7.96 86.05 0.12 78.09

$\frac{86.05}{5}$

3+50 = BC RT

77.8	77.0	76.4	76.1	74.7	75.0	74.8
$\frac{0.4}{25}$	$\frac{1.2}{14}$	$\frac{1.8}{15}$	2.1	$\frac{0.5}{12}$	$\frac{3.2}{15}$	$\frac{3.2}{25}$

78.21

$\frac{78.21}{1}$

LT

indexed
6.5.16
RT

66

Twigg
Sunset to Sun

T.P 0.45 61.89 12.49 67.44

62.3	61.9	60.8	60.8	59.9	60.3	62.1
$\frac{11.6}{25}$	$\frac{12.0}{18}$	$\frac{13.1}{15}$	13.1	$\frac{14.0}{15}$	$\frac{13.6}{23}$	$\frac{11.8}{25}$

5+52.08

70.3	70.6	66.2	65.7	64.4	64.6
$\frac{3.6}{25}$	$\frac{3.3}{20}$	$\frac{7.7}{17}$	8.2	$\frac{9.5}{19}$	$\frac{9.3}{25}$

5+52.08

68.9	69.4	71.9	71.5	70.4	71.0
$\frac{+5.0}{35}$	$\frac{+4.5}{20}$	$\frac{2.0}{16}$	2.4	$\frac{3.5}{18}$	$\frac{2.9}{25}$

5+07.08 EC on Twigg 45° RT

T.P 0.66 73.93 12.78 73.27

73.93
8

4+75.66 36° RT

79.2	78.1	77.8	77.0	75.3	77.7	78.8
$\frac{6.8}{35}$	$\frac{7.9}{16}$	$\frac{8.2}{15}$	9.0	$\frac{10.7}{19}$	$\frac{8.3}{20}$	$\frac{7.2}{35}$

86.05

86.05
7

T.P. 3.02 52.11 12.80 49.09

6+84.08

6+35.08

= outlet of wash from
" to be diverted to TUN
at next St. South

6+07.08

SEE THIS

5+86.08

5+72.08

61.89

LT

E

PT

67

Twigg

52.41	51.3	49.4	49.1	48.2	48.5	47.9
cen. 9.48	10.6	12.5		13.7	12.4	14.0
Wash 2.5	1.8	1.3	12.8	1.5	1.6	2.5
	TOP					
	52.4					

48.7	49.4	50.4	50.1	50.3	49.2	49.8	49.4
12.2	12.5	11.5	11.8		12.7	12.1	12.5
3.5	2.5	2.0	1.5	11.6	1.4	1.5	2.5

52.44	51.56	51.7	52.0	51.3	51.6	51.1
9.45	10.33	10.2		10.4	10.3	10.8
2.5	2.3	1.5	9.9	1.5	1.6	2.5
5' wide	Upper	Lower	stop			

52.56	53.9	54.5	53.8	53.1
9.33	8.0	7.4	8.1	8.8
2.5	1.2		1.5	2.5
E 8' com. Dr.				

53.6	56.1	56.9	56.0	56.4
8.3	5.8	5.0	5.9	5.5
2.5	2.0		1.5	2.5

61.89
E

LT

£

PT TW 1995 68

S.W. 7' CT.

check to B.M. SP. + TW 1995 10.87 28.71 28.68 0.03

T.P. 014 39.58 12.67 39.44

7+32.08 = Nly of Juan

49.3	48.75	48.37	47.74	47.05	47.47	46.9
<u>2.8</u>	<u>3.36</u>	<u>3.74</u> <small>amt</small>	<u>4.37</u> <small>pay</small>	<u>5.04</u>	<u>4.04</u>	<u>5.2</u>
25	15.2	15.2 <small>pay</small>		15.2 <small>amt pay</small>	15.2	25

52.1	52.1	48.5	47.7
<u>0.0</u>	<u>0.0</u>	<u>3.6</u>	
25	15	12	44

7+30.08

52.11

52.11

9-21-37
Miller
Walker
Blair
Sisson

X sec. Mason. St. Sunset
To Presidio Road.
See Plat. Page 61

1+25

36.0	39.0	38.1	39.5	43.0	43.0	43.2	43.0
19.0	16.0	15.9	15.5	12.1	12.1	12.8	12.0
35	28	25	15	5		15	25

T.P. — 12.33 — 55.06 — 0.34 — 42.73 —

————— 55.06 —————

1+00

31.7	34.3	39.4	40.6	40.7	40.9	40.7
11.4	8.5	3.7	2.5	2.4	2.2	2.4
35	25	8	3		15	25

0+75

30.5	31.5	33.3	36.0	38.0		38.4	38.3
12.6	11.6	9.8	7.1	5.1		4.7	4.8
28	25	19	11			15	25

0+50

28.5	30.1	31.6	34.8	36.2	36.1	36.2
14.6	13.0	11.5	8.3	6.9	7.0	6.9
35	25	15		5	15	25

0+25

27.1	28.3	30.0	32.6	34.2	34.1	33.9
16.0	14.8	13.7	10.5	8.9	9.0	9.2
35	25	15		5	15	25

0+00 = N1/4 Line Sunset

BM, ♀ Hub — 12.97 — 43.07 —

————— 30.10 —————
N1/4 Sunset
Page 62

————— 43.07 —————

0.19 BM. 12.55 30.10

T.P. 0.35 42.65 12.76 42.30

2+36.5 ϕ = E. Edge 20.5 strip pay. on curve

2+20.3 ϕ Existing Pav. on curve

2+16 ϕ = W. Edge 20.5 strip Pav. Not at 90°00' on curve

2+02

1+90

1+74³ Sly End. Existing Pav.

1+50

55.06

42.15 44.79 47.46 48.54 50.02 51.39 52.26 54.21 55.13 70
12.91 10.27 7.60 6.52 5.04 3.67 2.80 0.85 0.03
75 50 25 15 15 15 25 50 59.5

42.18 44.90 47.66 48.76 50.23 51.52 52.31 54.27 55.07
12.84 10.16 7.40 6.30 4.83 3.54 2.75 0.79 0.01
75 50 25 15 15 15 25 50 59

42.21 44.93 47.69 48.81 50.24 51.36 52.02 54.77 54.11 55.05
12.85 10.13 7.37 6.25 4.82 3.64 3.04 2.29 0.94 0.01
75 50 25 15 15 25 25 37 50 59

46.3 47.8 49.39 49.82 50.73 51.15 51.40
8.8 7.3 5.67 5.24 4.33 3.91 3.66
35 25 6.3 W. Edge Pav. 25 30 6.8 Edge Pav.

42.8 45.6 46.3 49.0 49.3 49.79 48.84 49.56 49.74 49.74
12.3 9.5 8.8 6.1 5.8 6.27 6.22 5.50 5.32 5.32
35 25 23 20 4 15 25 25 25 25
W. Edge Pav. 8. Edge Pav.

41.3 44.2 46.5 48.5 48.1 47.53 47.87 47.86 47.86
13.8 10.9 8.0 6.6 7.0 7.53 7.19 7.20 7.20
35 25 19 17 1.3 W. Edge Pav. 15 Pav. 25 Pav. 25.5

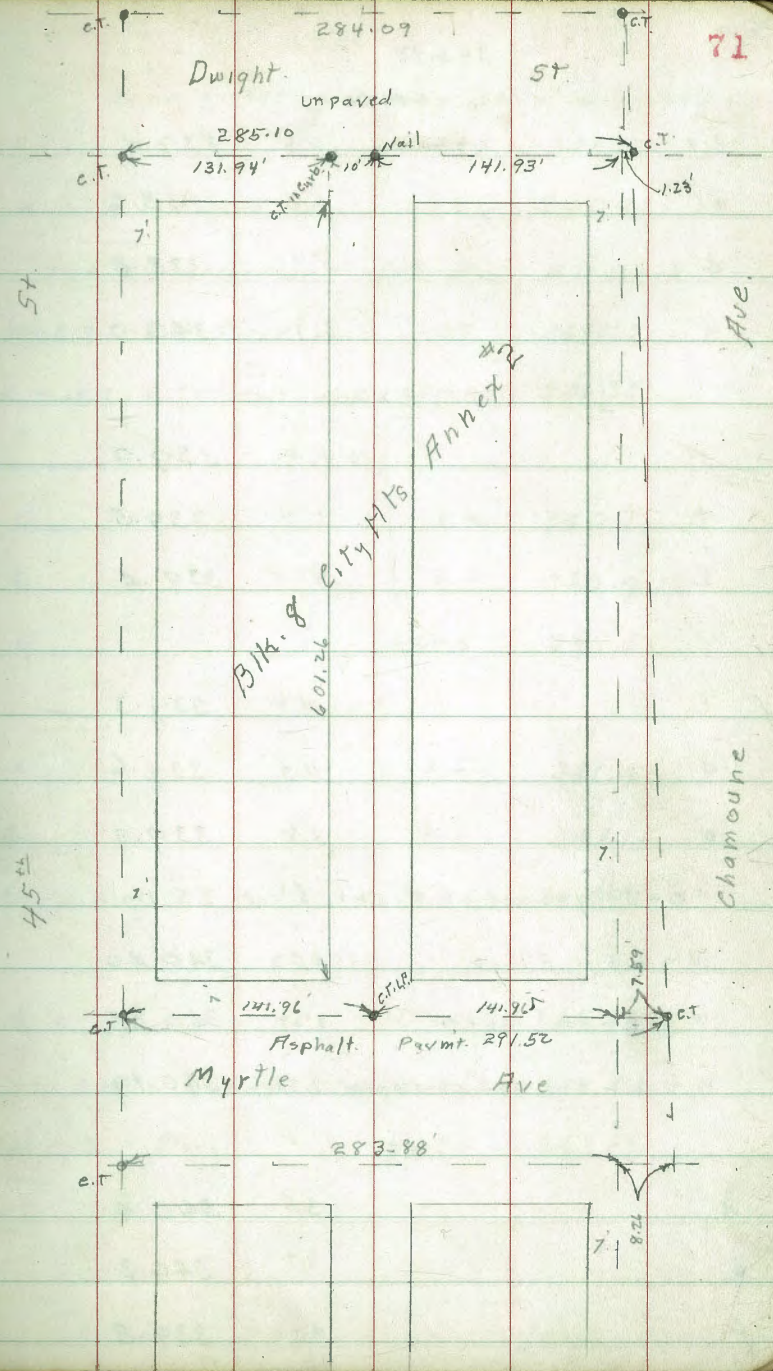
40.4 42.1 44.0 45.6 45.3 45.5 45.1
14.7 13.0 11.1 9.5 9.8 9.6 10.0
35 25 13 8 15 25

55.06

10-9-35
Miller
Walker
Bless.

X See Alley B14. 8: City Hts. Annex "2
indexed
C.S.K.

B.M. B.P.	11.35	335.35		324.00	N.W. Dwight & Chamoune.
T.P.	12.52	347.39	0.48	334.87	
T.P.	1.89	343.93	5.35	342.04	
B.M. B.P.			8.08	335.88	N.W. Myrtle & Chamoune
14' S. of 0+00 = N. ch. line Myrtle					
E-25 Top ed			6.58	337.35	
E-25 gutter			7.02	336.91	
E "			6.58	337.35	
E. Top ed			6.18	337.75	
E pav.			6.46	337.47	
W gutter			6.34	337.59	
W. Top ed			5.82	338.11	
+ 25 " "			5.46	338.47	
+ 25 gutter			6.01	337.92	
0+00 = N. line Myrtle					
W. curb. N. End.			5.61	338.32	
W. pav N. End			5.82	338.11	
E " " "			5.99	337.94	
E. " " "			5.94	337.99	
E. ch. " "			5.87	338.06	



343.93

0+10

E	4.5	339.4
+5	5.3	338.6
±	5.1	338.8
W	3.9	340.0

0+25

W	4.0	339.9
±	4.4	339.5
E	4.5	339.4

0+50

E	4.6	339.3
±	4.3	339.6
W	3.8	339.9

0+57 garage on W. ent. floor 2.5' Back

W - 2.5 = Floor 3.53 340.40

W. ch. ent. apron 3.64 340.25

W + 1.2 = E. End. conc. apron 3.74 340.19

1+00

W	3.5	340.4
±	3.7	340.2
E	4.1	339.8

343.93

1+20 garage on W. conc. floor 0.5' Back

W - 0.5 floor 2.80 341.13

W. = E. End. conc. apron 3.0 340.9

1+34 garage on W. ent. floor 5.7' Back

W - 5.7 ent. floor 2.38 341.55

W - 4.7 E. End. ent. apron 2.60 341.33

1+50

E 3.2 340.7

± 3.0 340.9

W. 2.8 341.1

2+00

W 2.5 341.4

± 2.8 341.1

E 3.0 340.9

2+31

± = Top. M.H. 2.50 341.43

2+32 garage on W. ent. floor 13' Back

W - 13. = floor 1.70 342.23

343.93

2+50

E 2.3 341.6

E 2.2 341.7

W 2.0 341.9

2+64 garage on W. dirt floor 14' Back

W-14 = floor 2.0 341.9

2+73 garage on E. cnt. floor 10' Back

E-2. = W E. cnt. apron 2.10 341.83

E-10. = floor. 2.02 341.91

T.P. 5.13 347.09 1.97 341.96

3+00

W. 4.5 342.6

E. 4.9 342.2

E. 4.9 342.2

3+09 garage on E. dirt floor 8' Back

E-8' = floor. 4.6 342.5

3+50

E 4.0 343.1

E 3.9 343.2

W 3.6 343.5

347.09

73

3+92 E Double garage on E dirt floor 4.3' Back

E-4.3 = floor 3.5 343.6

4+00

W 3.3 343.8

E 3.4 343.7

E 3.3 343.8

4+10 garage on E. dirt floor 0.2' Back

E-0.2 = floor 3.4 343.7

4+50

E 3.1 344.0

E 2.8 344.3

W 3.2 343.9

{ Garage on E dirt floor on E. line
 4+58 " " W " " 5.6' Back

E. floor 4.0 343.1

W-5.6' " 3.1 344.0

4+80 = S. End House on W. 0.6 in Alley.

5+00

W. 3.3 343.8

E 3.8 343.3

E. 4.0 343.1

5+01 = N. End above House on W. 0.6 in Alley.

347.09

5+25

E	4.2	342.9
E	3.8	343.3
+5	3.1	344.0
W	2.7	344.4

T.P.	2.42	344.95	4.56	342.53
------	------	--------	------	--------

5+42 garage on W. ent. floor 2.5 Back

W-2.5 floor	0.88	344.07
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5+50

W	1.3	343.6
E	2.5	342.4
E	2.8	342.1

5+56 garage on W. ent. floor 2.7 Back

W-2.7 floor	0.8	344.1
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5+65

E	3.4	341.5
+2	4.1	340.8
E	3.8	341.1
+1	3.8	341.1
+2	2.5	342.4
W.	2.0	342.9

344.95

5+70 S. end cmt. wall on W. 04 in Alley

W+04 Top wall	2.29	342.56
---------------	------	--------

5+90

W. Top wall	3.07	341.88
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W+ 0.4 E. edge wall	3.07	341.88
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W+ 04	4.6	340.3
-------	-----	-------

+6	5.3	339.6
----	-----	-------

+7	6.3	338.6
----	-----	-------

E	6.8	338.1
---	-----	-------

+7	6.8	338.1
----	-----	-------

E	5.0	339.9
---	-----	-------

5+98

E	5.6	339.3
---	-----	-------

+3	7.5	337.4
----	-----	-------

E	7.7	337.2
---	-----	-------

+5	7.5	337.4
----	-----	-------

+9.6	6.3	338.6
------	-----	-------

+9.6 Top wall	3.46	341.49
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W	3.46	341.49
---	------	--------

74

344.95

75

6+01²⁶ = S. Line Dwight St. Unpaved

W. on ent. d. & dirt 8.09 336.86

W+0.4 Face of curb. 8.09 336.86

± 8.2 336.7

E. dirt. 8.6 336.3

E. Line. Ent. curb. 9.75 335.20

+ 14 = S. curb line Dwight St.

E. curb. 10.09 334.86

E. dirt gutter 10.5 334.4

± " " 9.3 335.6

W " " 8.8 336.1

E. curb. 8.19 336.76

T.P. 0.38 332.90 12.35 332.60

chk orig B.M. 8.98 324.00 ✓

12-9-57

Miller
Bliss

Sunset + Twigs - X. S. e.

indexed
C.S.K.

76

3+00

71.5 70.9 70.5 70.3 69.9 69.9 69.4

7.4 8.0 8.4 8.6 9.0 9.0 9.5
25 16 15 15 15 20 25

T.P. 11.50 78.94 0.22 67.44

78.94

2+50

65.7 65.1 64.8 64.7 64.0 64.7 64.6 64.0

2.0 2.6 2.9 3.0 3.7 3.0 3.1 3.7
25 18 14 15 16 16 21 25

2+15

62.5 61.4 60.6 60.5 59.7 60.5 60.6 59.9 59.6

5.2 6.3 7.1 7.2 8.0 7.2 7.1 7.8 8.1
25 15 14 15 15 16 25 22 25

T.P. 12.59 67.66 0.50 55.07

67.66

1+60

54.7 54.4 53.6 53.2 52.8 53.3 53.2 52.2

0.9 1.2 2.0 2.4 2.8 2.3 2.4 3.4
25 18 14 15 16 20 25

1+10

47.6 46.9 46.0 45.9 45.6 45.8 44.4

8.0 8.7 9.6 9.7 10.0 9.8 11.2
25 15 14 15 20 25

T.P. 12.75 55.57 0.32 42.82

55.57

0+60

40.1 39.1 38.7 38.3 38.5 37.6

3.0 4.0 4.4 4.8 4.1 5.5
25 15 15 15 22 25

0+10

33.2 32.6 32.4 31.6 31.4

9.9 10.5 10.7 11.5 11.7
25 15 15 15 25

0+00: E. Line Mason

4. Mason N. line
Sun set.

P.M. H4b

13.04 43.14

30.10

32.4 32.0 31.3 30.6 29.9

10.7 11.1 11.8 12.5 13.2
25 15 15 15

43.14

T.P. 0.90 55.07 11.95 54.17

77

5+82⁰⁸

54.18 54.62 54.6 55.2 54.9 55.4 55.1
 11.94 13.50 11.5 10.9 11.2 10.7 11.0
_{25 Top wall} _{25 E. side Drive} ₁₅ ₁₄ ₁₅ ₂₅

5+62⁰⁸

58.1 59.1 58.8 58.7 58.4 59.3 59.2
 8.0 7.0 7.3 7.4 7.7 6.8 6.8
₂₅ ₁₉ ₁₅ ₁₃ ₁₅ ₂₅

T P 0.03 66.12 12.85 66.09

66.12

5+32⁰⁸

70.3 70.4 69.8 65.3 65.3 64.9 64.2 65.3 65.4
 8.6 8.5 7.1 13.6 13.6 14.0 14.7 13.6 13.5
₂₅ ₂₀ ₁₈ ₁₇ ₁₅ ₁₄ ₁₅ ₂₅

5+07⁰⁸

e.c. E. of Jaan on Twigg St.

78.9 71.1 70.8 70.4 70.3 71.1 71.3
 0.0 7.2 8.1 8.5 8.6 7.8 7.6
₂₅ ₁₇ ₁₅ ₁₅ ₁₅ ₁₇ ₂₅

4+75⁶³

77.9 76.9 76.4 75.5 75.2 75.4
 7.0 2.0 2.5 3.4 3.7 3.5
₂₅ ₂₄ ₁₅ ₁₅ ₂₅

4+44²⁵

81.9 78.4 78.4 77.6 77.3 77.3 77.0
 7.0 0.5 0.7 1.3 1.6 1.6 1.9
₂₅ ₂₄ ₁₅ ₁₃ ₁₅ ₂₅

4+12⁸³

78.6 78.5 77.9 77.8 77.6 77.3
 0.3 0.4 1.0 1.1 1.3 1.6
₂₅ ₁₇ ₁₅ ₁₅ ₁₅ ₂₅

3+81⁴²

78.5 78.2 77.6 77.3 77.0 76.8
 0.4 0.7 1.3 1.6 1.9 2.1
₂₅ ₁₆ ₁₅ ₁₅ ₁₅ ₂₅

3+50 B.C.

76.9 76.5 75.9 75.5 75.1 74.8
 2.0 2.4 3.0 3.4 3.8 4.1
₂₅ ₁₆ ₁₅ ₁₅ ₁₅ ₂₅

78.94

78.94

7+32⁰⁸ N. Line Juan.7+02⁰⁸chk. elev
53.06
-53.1

2.01
26
P.R.

52.5	51.7	51.0	49.5	48.9	48.2	48.0
2.6	3.4	4.1	5.6	6.2	6.9	7.1
25	16	15	12		15	25

6+42⁰⁸

50.3	50.2	50.1	50.2	50.2
4.8	4.9	5.0	4.9	4.9
25	15		15	25

6+22⁰⁸

51.2	51.0	51.1	50.2	50.2
3.9	4.1	4.0	4.9	4.9
25	15		15	25

6+02⁰⁸

51.8	52.3	52.8	52.3	52.3
3.3	2.8	2.3	2.8	2.8
25	15		15	25

55.07

55.07
E

IMPROVED TABLES
OF
INFORMATION

12-10
250

INSTRUCTIONS FOR USE OF TABLES
City Engineer's Office
San Diego, Calif.

IMPROVED TABLES
AND
INFORMATION

74.3
41.6
16.0

6.14
8.88
15.00
12.30
2.7
14.26
5.54
8.68

.0145
185.7
7.70
1.85
8.50
7.40
1.00
11.10

12.97
8.88
21.85

50 6.86

0.146
25
7.30
4.38
5.110
12.30
12.8
7.3
13.53
14.26
7.3
14.99

100 13.53
6.86
6.67

100 1.66

6.06
1.66
+4.40

135 2.44

150 12.90
7.07
5.73

145 12.30
6.96
5.34

131
3278
3095
1689L
753-7582

325.43 13.4 15.8 18.2 7.79 243.92
308. 12.64 4.99 14.58
21.6 8.73 100 128.80 133.81
25 11.23 246.83 89.51 2.5
204.02 23.63 90.09 5.0
(12.58) 223.20 23.50
251.44 13.5 27.77
48 251 4.27
7 32 7.53 12.20
5.07

162 24
56

149.18 83.92
85. 57.7
144.18 2.0188
15.14
29.00

119.7
156
13.50
93.91
390.96
2.95

144.14 31.82
83.92 144.78
228.10 176.00
370.00
141.90

49.2
3.9
53.1

413.6 3.30
1.25
4.57 4.55

2035.19
19 32.53
1 02.66