

1506

PASTS

FIELD BOOK

No. 385F

MICROFILMED
DEC 24 1964

CITY OF
CALIFORNIA
ENGINEERING DEPARTMENT
SAN DIEGO.

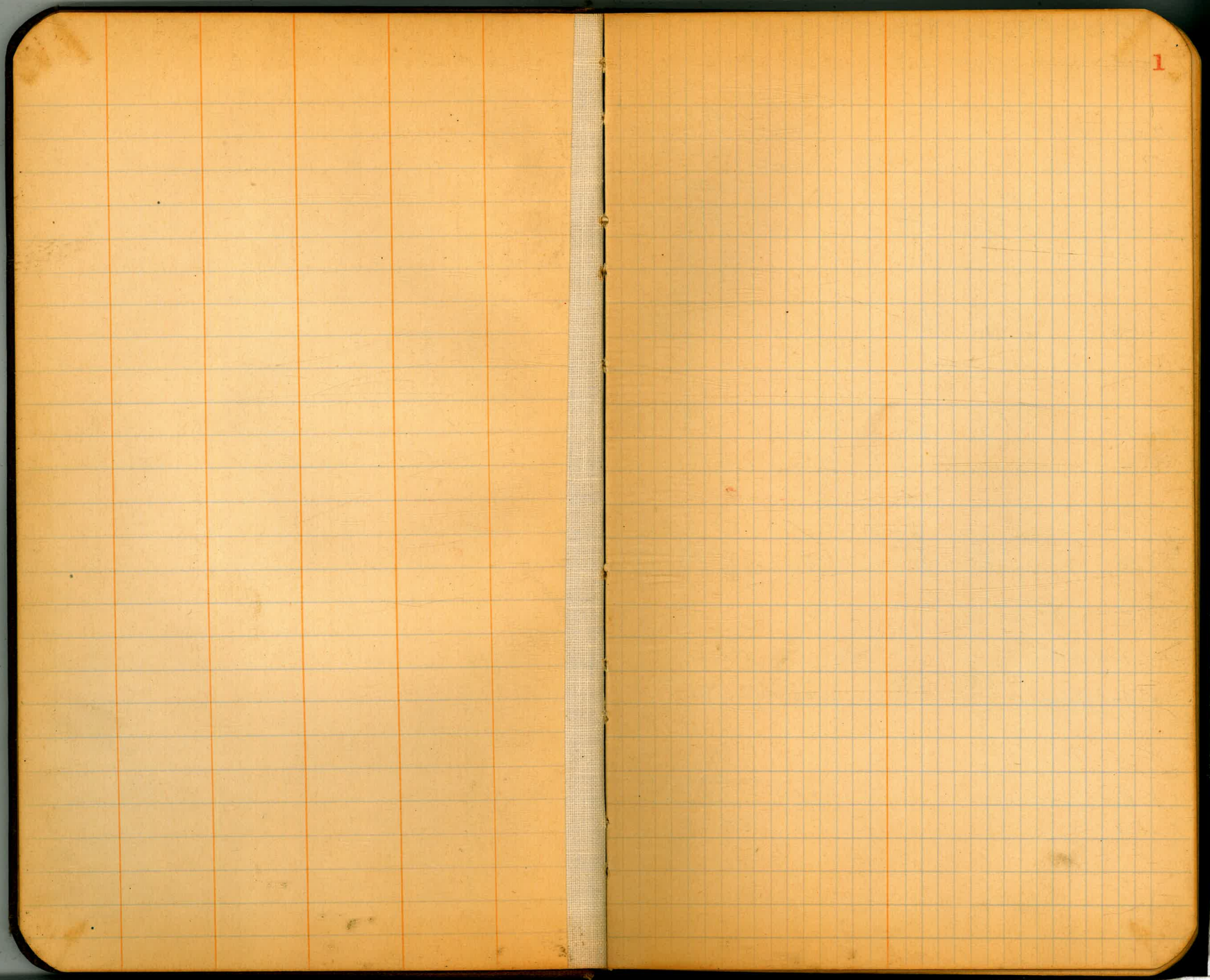
Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.



1

Pacific Beach Paths
Felspar + Ocean Blvd.

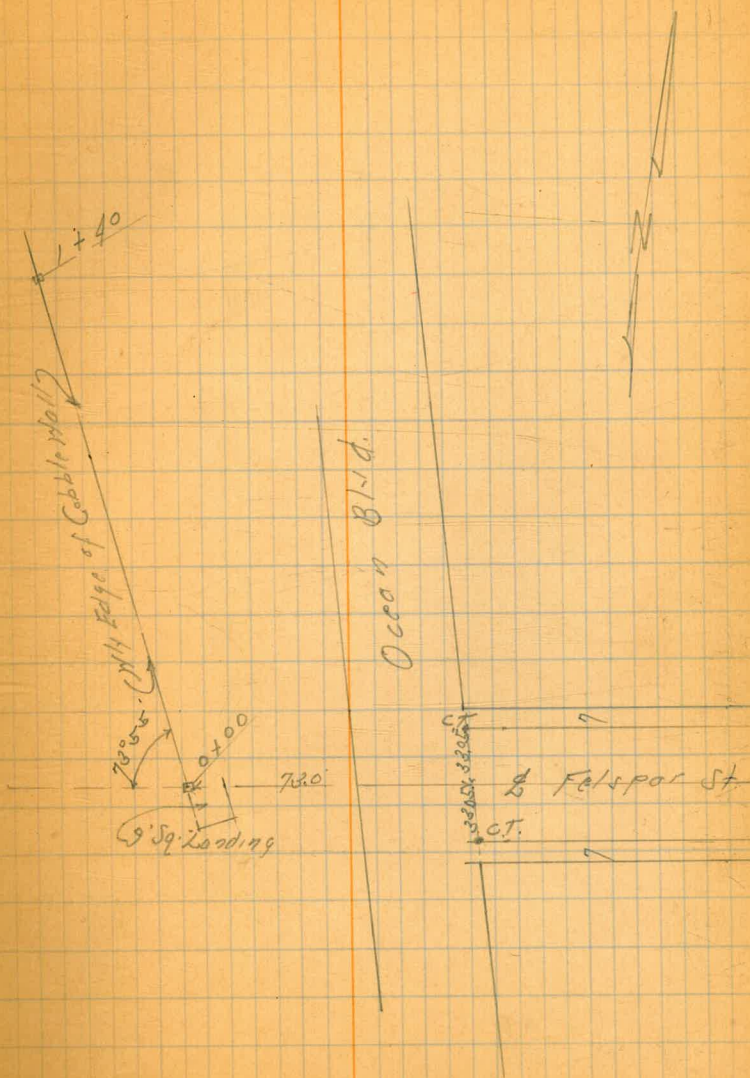
	Cut Slopes 1/2:1		Fill Slopes 1/2:1		
BM	4.20	23.72	19.52		BP, NW Felspar Mission Blvd
TP	0.08	11.12	12.67	11.05	East
0+0	Max		Subgrade		
	F 20.7 31.1	-9.9 10.8	21.00	11.7	C 1.8 2.5
+50	F 12.2 18.3	-8.6 8.8	14.75	8.1	C 6.4 12.2
	F 5.7 8.6	2.6 8.2	8.50	15.2	C 11.2 16.1
+40	C 0.5 0.3	7.6 7.1	3.50	20.22	C 18.7 18.4
	F 20.4 30.6	-9.9 10.5	21.00	2.7	0.0 2.7
S.W. Cor Landing			21.00	2.7	0.0
S.E. Cor Landing			21.00	2.7	C 0.9 9.5

S = 12.50%

Indexed - C.S.K.

Aug. 8-34
Moore
Sisson
Hartberg

2

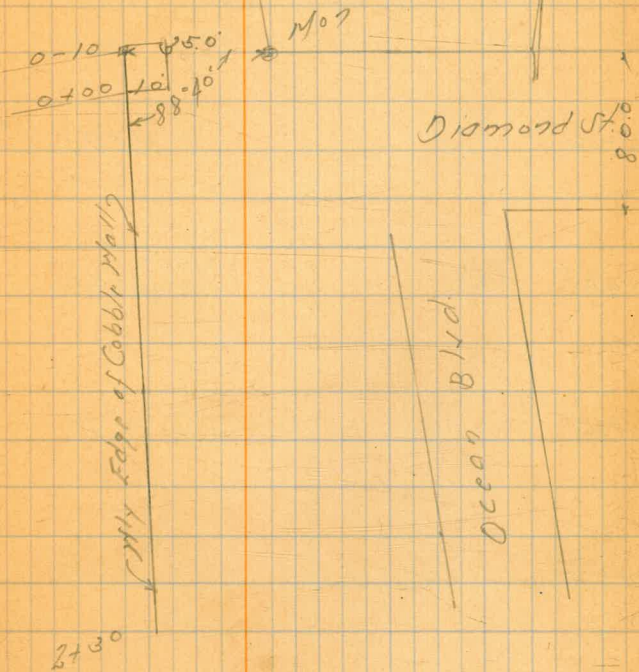


Pacific Beach Paths
Diamond St + Ocean Blvd.

Indexed
C.S.K.

Aug 7, 34
Moore
Sivons
Northboro

3



Pacific Beach Pat 41

Diamond St + Ocean Blvd

4

Cut Slope 1/2:1 Full Slope 1/2:1
 BM 5.40 26.32 20.92
 S.W.B.P.
 Diamond
 #10010784

West

East

TP 2.92 35.57 3.67 32.65

TP 0.56 23.31 12.82 22.75

TP 0.96 11.66 12.61 10.70

0-10 32.90

-21.3 F 316 2.67 0.0
 10.3 47.4 2.67 0.0

2.67 0.0
 2.67 0.0

0+0 32.65

-21.0 F 313
 10.3 47.0

2.92 0.0
 2.92 0.0

+50 26.40

-14.7 F 242
 9.5 38.3

9.2 C 5.6
 9.8 2.8

1+0 20.15

5 = 12.50%

-8.5 F 178
 9.3 26.7

15.4 C 11.5
 4.1 5.8

+50 12.90

-2.2 F 110
 8.8 16.5

21.7 C 10.8
 10.9 15.4

2+0 7.65

4.0 F 15
 5.5 2.3

27.9 C 18.0
 9.9 9.0

+30 3.90

7.8 C 2.0
 5.8 1.0

7.8 C 8.0
 10.2 7.0

Pacific Beach Paths
 Low St And Ocean Blvd.
 N°1 Location Lt.
 See Page 9 For N°2

1+75 End

1+03.05 EC

44° 43'

Δ 89° 26'

+75

R 50.0

42° 58.30'

T 49.51

L 78.05

+50

38° 38.87'

0+25 BC

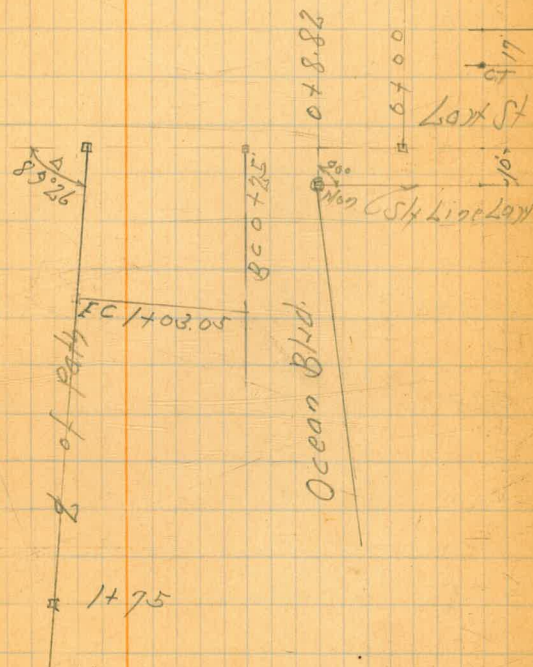
14° 19.25'

0+0

Indexed
 C.S.K.

5

Aug. 9-34
 Moor



Pacific Beach Palms
 6014 St And Ocean Blvd

BM 0.15 33.96 33.815 NEBP
 TP 0.72 21.84 12.84 21.12 6014 + Ocean Blvd

0+0 31.60

+25 28.00

+50 24.40

+75 20.80

+103.05 16.76

+25 13.60

+50 10.00

+75 6.40

Σ = 144

Lt.

L

Rt.

6

2.1 0.9
 2.7 3.0

2.1

2.1 0.0
 2.1 3.0

6.0 0.11
 4.9 3.6

6.0 0.12
 4.9 3.6

8.6 0.35
 6.7 4.8

8.6 0.16
 8.0 3.8

13.2 0.0.9
 12.3 3.5

13.2 0.0
 13.2 3.0

5.1 0.6.9
 12.0 4.1

5.1 0.120
 17.1 2.0

8.2 0.0
 8.2 4.0

8.2 0.10.1
 18.3 1.92

11.8 0.0.3
 11.5 3.2

11.8 0.37
 15.5 3.5

15.4 0.1.9
 13.5 4.0

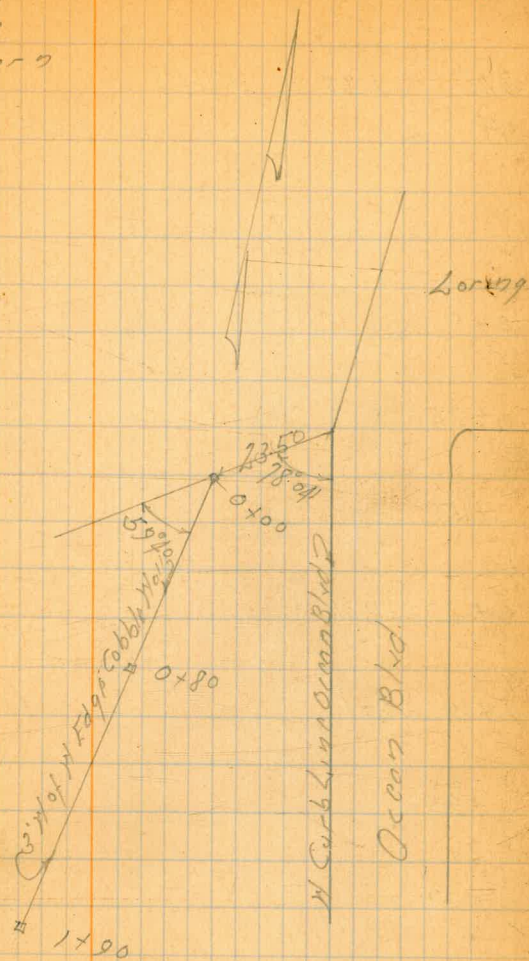
15.4 0.0
 15.4 3.0

Pacific Beach
Loring St And Ocean Blvd
No. 1 Location

Aug. 9-34
Moore
Sisson
Hortner

Indexed
C. S. K.

7



Grades
Loring x Ocean Blvd.

8

BM 1.29 47.49 46.20
TP 12.05 35.44

SE RP
Loring x
Ocean Blvd.

N

East

0+0 47.10

0.4 0.0
0.4 7.0 0.4 0.0
0.4 1.4

+25 39.72

7.8 F 5.6
13.4 5.4 7.8 C 5.7
2.1 12.9

+50 32.35

15.1 C 2.5
12.6 11.3

+80 -Brk 23.50

+100 -Brk 21.70

+25 16.62

+50 11.54

+75 6.45

+90 3.40

S=2.295

S=20.83

Pacific Beach Path
 Ocean Blvd. North of Low
 No 2 Location RT

1+82 End

1+50.06 E.C.

15° 45'

A 31° 30'

1+22.57

R 100.0 7° 52' 30"

T 28.20

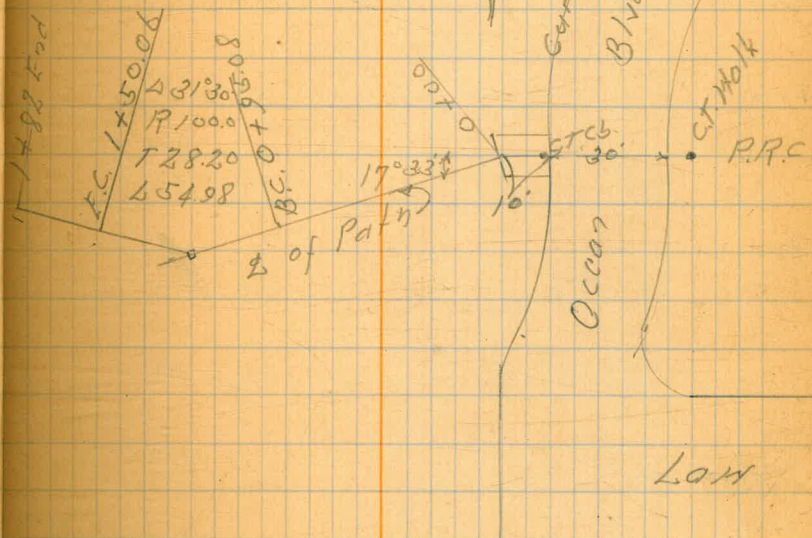
L 54.98

0+95.08 B.C.

0+00 = 16 W of NCB Ocean Blvd.

Indexed
 C.S.K.

Aug 12 34⁹
 Survey
 Northham
 Bliss



Grades Ocean Blvd
North of Lam

BM	0.17	33.98	33.81	NE BP to top of Ocean Blvd.
TP	0.55	21.69	12.84	21.14
TP	2.25	11.09	12.85	8.84

0-10: Top cb 2.25 31.23

0+0 31.00

+2.5 27.21

+5.0 23.42

+7.5 19.63

+95.05 BC 16.59

+122.57 12.42

+150.06 FC 8.25

+82 3.40

Aug 13-34 10
S. 0.00
North of
Blvd

11 2 5

3.0 c 0.4
2.6 3.2

3.0 0.0
2.0 3.0

6.8 c 4.2
2.8 5.1

6.8 c 3.5
6.3 7.8

10.6 c 6.5
4.1 6.3

10.6 c 3.2
7.4 7.6

14.3 c 5.6
8.7 5.8

14.3 c 2.0
11.3 9.5

17.4 c 2.5
9.9 6.8

17.4 c 5.0
12.1 5.7

2.3 c 6.7
2.6 6.4

2.3 c 2.6
5.7 4.8

13.4 c 3.1
10.3 7.6

13.4 c 1.3
12.1 3.7

7.7 0.0
7.7 3.0

7.7 0.0
7.7 3.0

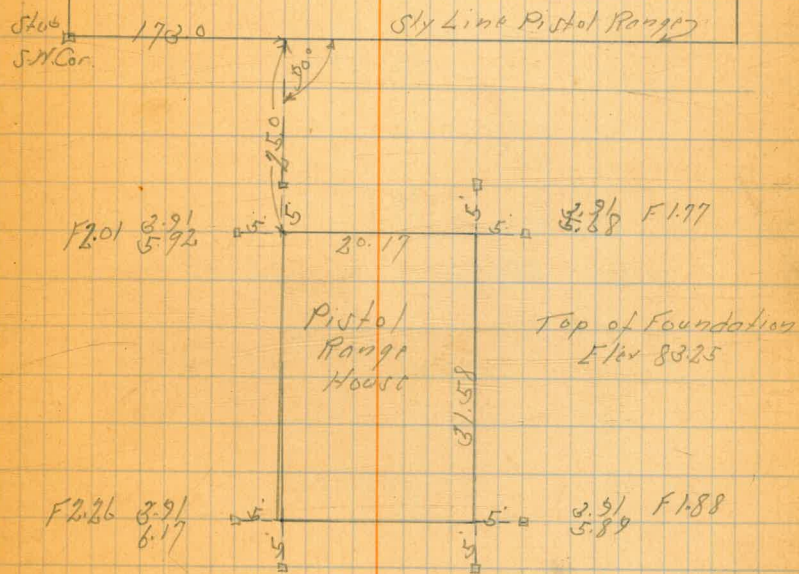
San Diego Police Department
Pistol Range

B.M. 1.51 87.16 85.65 Mo 2.24
Cor 8/4/35

indexed
c.s.K.

11

Aug 17-34
515807
81.55
Northborn



Dwight St Water Grades
 From Alley West of Chamouse to
 West Line of Euclid Ave.

indexed
 E.S.K.

8-31-34
 Moore 12
 Sisson
 Hartberg

BM 1268 38668 324.00 NW CP
 Dwight St
 Chamouse

0+50 = 10" SL Dwight
 5' F of 2' Alley 45"
 Chamouse 5.0 c3.7
 7.3 Before Edge Pipe
 331.70

30' S 0+50 Gate 322.50 4.2 c4.2
 0.8

1+0 = Bk 8.6 c2.9
 5.7 322.10

1+50 = Bk 13.8 c3.6
 10.2 322.90

1+80 = W.L. Chamouse 15.2 c3.7
 12.2 320.20

TP 10.31 324.79 12.20 324.48

2+40 = FL " 10" Gate 14.7 c3.7
 11.6 320.10

3+0 14.5 c3.8
 16.7 320.30

4+81.5 10" x 6" Tee to S. 12.6 c4.1
 9.9 322.80

30' S of 3+81.5 14.7 c3.9
 11.8 323.10

334.79

37.4V = 1/2 Block "A"
 0.20 Line Block "A" 13.3 C4.0 321.50

440 14.8 C3.7 323.50

451.52 = 1/2 46 1/2 J1
 1/2 F=0.170 2.5 C3.8 325.30

570.152 = FL 46 1/2 J1 8.1 C3.9 326.70

574.152 7.4 C3.9 327.40

578.152 = Brk 6.7 C3.9 328.10

610.15 = 1/2 Block "B"
 0.70 Block "B" 5.1 C4.0 328.70

6150 = Brk 4.5 C4.0 330.30

TR 9.58 343.82 0.55 334.24

343.82

7+12 = 10" x 6" C.I. Tee $\frac{12.0}{8.2}$ C8.8 331.80

30' 5 of 7+12 6" Gate $\frac{12.0}{8.2}$ C8.8 331.80

7+01.50 = F.L. Wash Ave $\frac{12.2}{8.4}$ C8.8 331.60

7+51.50 = F.L. Wash Ave $\frac{11.1}{7.3}$ C8.8 332.70

8+0 $\frac{10.4}{8.6}$ C8.8 333.10

7+31.40 $\frac{10.4}{8.4}$ C8.7 333.70

4.50 = 1/2 Black C" $\frac{9.2}{8.2}$ C8.7 333.50

10" Gate Jo.

9+01.5 10" Gate = F.L. Wash St. $\frac{9.5}{8.7}$ C8.8 334.30

343.82

9+51.50 = Y.L. 47¹/₂ St North ^{8.9} C3.8
5.1 334.90

10+44 = Exsting Gate ^{8.8} C3.6
5.2 335.00

30.5 of 9+90 out

10+01.50 = F.L. 47¹/₂ North ^{8.6} C3.7
4.9 335.20

10+50 out 9.0 334.80

10+87 ^{8.3} C3.6
3.7 334.50

11+21.50 = Block D ^{10.6} C3.8
6.8 333.20

11+61.50 ^{11.7} C3.7
8.0 333.10

343.82

12+0			12.5 c26 8.9	331.30
------	--	--	-----------------	--------

13+50 = 22½ Bend			12.8 c12 11.6	331.00
------------------	--	--	------------------	--------

TP	0.34	332.59	11.57	332.25
----	------	--------	-------	--------

780			13.1 c12 11.9	319.50
-----	--	--	------------------	--------

TP	0.19	319.89	12.89	319.70
----	------	--------	-------	--------

13+10			8.4 c18 7.6	310.50
-------	--	--	----------------	--------

TP	8.27	315.98	12.18	307.71
----	------	--------	-------	--------

13+40			13.0 c26 10.4	303.00
-------	--	--	------------------	--------

13+60			15.5 c23 13.2	300.50
-------	--	--	------------------	--------

13+85 = 22½ Bend			16.0 c52 10.8	300.00
------------------	--	--	------------------	--------

14+00			8.0 c45 3.5	308.00
-------	--	--	----------------	--------

315.98

TP 12.65 328.56 0.07 315.91

TP 911 334.47 3.20 325.86

14144 = 22½° Bend 9.5 c7.5 327.00

15191 = Firsting 8' Gate 6.3 c4.0 328.20
= N. L. Euclid 2.3

Block "H" Bella Crest Water Grades
Landis St to Dwight St.

Indexed
C.S.R.

0+0 = Schicklandis 339.50

+50 338.93

+100 338.36

+200 = Brk 337.80

+300 337.60

+400 = Brk 337.40

+500 337.00

+600 = Brk 336.60

3740

335.00

3790

333.40

4140

331.80

4490 - Brk

330.20

5140

327.75

5490 - Brk

326.30

6125

323.95

6460 - Brk out

800
5

6756 - Main night st

322.00

Block "B" Belle Crest Water Garden
Landis St to Dixie St.

Indexed
c.s.K.

20

0+0 = S Line Landis 342.80

1+7 = Brk 344.30

1+67 = Brk 344.30

1+17 343.05

1+67 = Brk 341.80

2+17 340.95

2+67 340.10

3+17 339.20

3+67 - Brk

338.00

4+17

337.60

4+67 - Brk

336.90

5+17

336.00

5+67 - Brk

335.10

6+27 - H. L. Dwight

333.20

6+77 - Main Dr 96/ St

332.20

Block "C" Belle Crest Water Grades
Londis St to Dwight

Indexed
C.S.K.

22

0+0 - S.L. Londis 335.70

+10 338.20

+30 - Brk 340.00

+80 - Brk 341.50

1+30 - Brk 343.30

+80 - Brk 343.30

2+30 - Brk 344.30

2+80 - Brk 343.30

3+30 - Brk 341.40

3+80 - Brk 341.70

4+30 - Brk 341.10

4+80 - Brk 340.50

5+30 - Brk 338.80

5+80 - Brk 337.40

6+30 - Brk = N.L. Dwight St 336.60

+77 = Main Dwight St 334.40

Block "D" Belle Crest Water Grades
Londis St to Dwight St.

Indexed
CISIK.

9-4-34

24

0+0 - S.L. Londis

335.70

0+19.5

336.40

0+69.5

335.80

1+19.5

334.80

+69.5

334.80

2+19.5

334.40

+69.5

332.90

3+19.5

330.40

3 + 69.5

330.70

4 + 19.5

330.60

+ 69.5

331.40

5 + 19.5

335.60

+ 69.5

336.20

6 + 19.5

337.00

+ 29.5 - H.L. D.M. 1967

336.60

+ 69.5

333.70

Block "E" Bell's Crest Water Grades
Lardis to Roselawn Ave.

Indexed
C.S.R.

26

010 = 5¹/₂ Lardis 339.90

+29 339.85

+78 = 8¹/₄ 339.80

+28 338.80

+78 337.80

2+28 = 8¹/₄ 336.80

+78 336.03

3+28 335.26

3+78 = B-k

334.50

4+14

333.70

4+50 = B-k = M. Barlow

332.90

Stadium La Jolla High School
 Contd. ^{from} page 37

Moore
 6-22-35

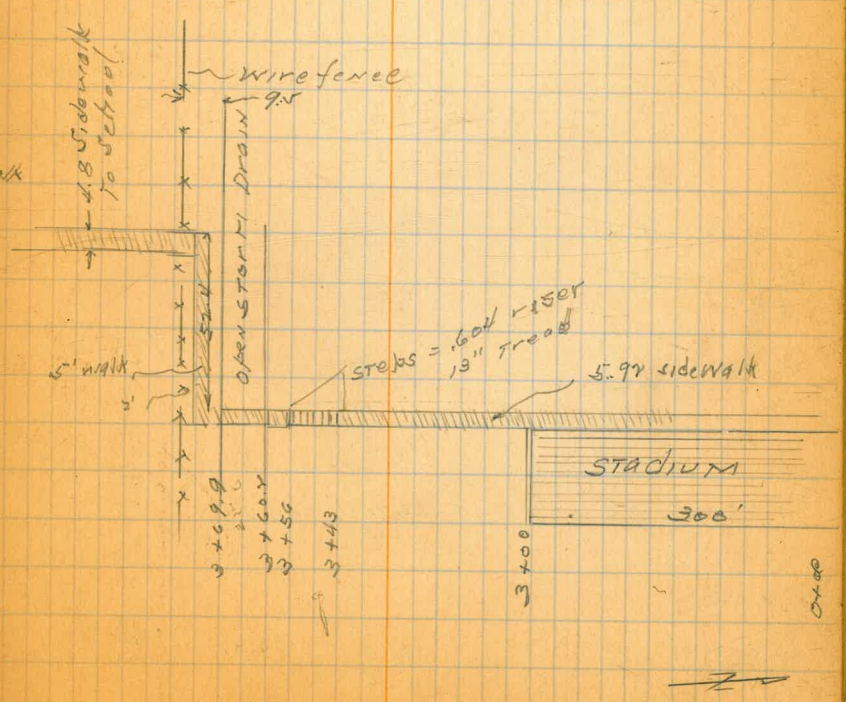
28

S.E.R.H.

El. walk
 at east edge

Prall = Supt.

3+69.9 = S edge drain	Steps offset 4' w of WL		
3+60.2 = N edge open Conc. Drain		144.90	190 5.03 -1.15
+56 Top Step		144.85	1.95 3.18 -1.23
+43 = Walk bottom of bottom step		137.0	980 980 0.0
+23		137.10	970 1014 -44.0
3+00		137.20	= 137.13 = .07 High
172	146.80	144.08	T.P. p 34



0+00



Curb Grades S.E. Cor.
Moorland Drive And Frosters St.

BM	7.51	25.43			S.F.B.P. Moorland & Frosters
0+0 - S End of Imp.	Gutter 17.60 1.22 7.15		Top Curb 18.15	17.92 7.28 7.27 TopCb	
+08.83			17.55 7.27	18.12 7.31 7.31	
+17.66			17.50 7.32	18.10 7.33	
+26.49			17.51 7.31	18.10 7.33	
+35.32 - B.C.			17.52 7.30	18.10 7.33	
+44.66			17.62 7.20		
+54.01			17.75 7.07	18.35 7.08	
+63.35			17.96 6.86		
+72.70 - B.C.			18.20 6.62	18.90 6.53	
+81.21			18.58 6.24	19.25 6.18	

Indexed
C.S.K.

Sept. 13, 34
Moore
Sisson
Hardy
29

	Gutter	TopCb	
0+82.72	19.00 5.82	19.65	5.78
+98.23	19.53 5.29	20.10	5.03
+66.74 - E End of Imp.	20.12 4.65	20.62	4.81 4.79 TopCb

Curb Grades 9-22-34

BM 21.44 S.P.H.
3.38 Moorland
24.82 Frosters

Curb Grades N.W. Cor.
Moorland Drive And Frontero St.

	25.43 Bl Ford Gutter	Top Curb	6.02
0+00 = N End of Imp	18.90 5.92	19.41	
	24.82 Bl Ford		
+0856	18.94 5.88	19.49	5.94 5.86 on Walk
+1713	18.99 5.83	19.58	5.85
+2569	19.03 5.79	19.65	5.78
+3426 B.C.	19.07 5.75	19.74	5.69
+4451	19.13 5.69	19.82	5.61
+5477	19.18 5.64	19.85	5.58
+6502	19.13 5.69	19.80	5.63

	25.43 Gutter	Top Cb	5.91
0+75.28	19.07 5.75	19.72	
TP 4.69	24.91	5.71	19.72
+85.53	18.86 5.96	19.55	4.86
+95.79 = B.C.	18.64 6.18	19.25	5.16
1+10.67	18.14 6.68	18.71	5.20
1+25.54 = N End of Imp	17.60 7.22	18.08	6.33 6.29 on Cb.
B/M 6.44	24.36		17.92
Set B/M		2.92	21.44

B.P.M.I.
Moorland
+ Frontero

Moorland Drive And Frontier
£ Gradus

31

£

24.82 Blford

0+45

17.58

7.24 Fo.04
7.28

+55.5

17.49

7.33 Fo.23
7.56

+66

17.40

7.42 Fo.32
7.74

+77.5

17.34

7.48 Fo.43
7.91

+86

17.41

7.41 Fo.58
7.99

+91.8

17.50

7.52 Fo.66
7.98

17.04.5

17.52

6.90 Fo.29
7.19

+20.92

18.61

6.21 Co.05
6.16

Stadium LaSalle High School

0-25		153.00	1.90m 0.89 F10.5 11.3 15.8
0100 = N Edge Aisle H	Top Rail 10.8 153.14	6.6 F17.4 26.1 153.65	Top of Top Step 0.18 F1.70 1.88
+26.165	3M 145.08 11.94 157.02	3.87 F1.44 2.81 3.25 F1.8 2.63	153.57
+52.33 = 1/2 Aisle B		3.53 F1.36 4.89	153.49
+76.745		3.60 F1.21 4.81	153.42
+101.16 = 1/2 Aisle C		3.67 F1.27 4.94	153.35
+125.575		3.75 F1.30 5.05	153.27
+150.00 = 1/2 Aisle D		3.82 F1.00 4.88	153.20
+174.405		3.89 F0.72 4.61	153.13
+198.82 = 1/2 Aisle E		3.97 F0.91 4.88	153.05
+223.235		4.04 F0.88 4.92	152.98
+247.65 = 1/2 Aisle F		4.11 F0.88 4.99	152.91
+273.82		4.19 F0.75 4.94	152.83
3+00 = S Edge Aisle G	Top Rail 153.15 9.27 F0.53	6.9 F16.0 24.0 152.75	1.08 F0.87 1.95

10-2-34			
Mount Sisson Northers			
Bot of Col. Step 11.36			
138.03			
Rushville St			
S. Rushville			
9.44			
137.95			
137.87			
137.80			
137.73			
137.65			
137.58			
137.51			
137.43			
137.36			
137.29			
137.21			
137.13			

page 28 for
EXTRA WORKS



153.83T

3+40

152.63

1.2° F 0.53

1.73

3+67.28

152.55

1.28 F 0.83

2.11

3+79.30 P.V.C. - opp. Fence =
52 Northburg

152.51

1.32 F 0.79

2.11

3+89.30

152.41

2.78 F 0.68
6.4 Fire Hyd.

3+99.30 F.V.C.

152.18

3.01

4+59.30

150.70

146.33T

-6.2 F 15.4

9.2 23.1

3 Germ

1.3 F 7.1

8.4 10.7

1.3 F 6.0

7.3 9.0

201 152.02 Top Hyd.

3.17
155.19

2.8 F 4.3

7.1 6.5

3.0 F 5.5

6.5 6.3

4.5 F 1.6

6.1 2.4

Sub Grade East Edge Side Walk

11-2-34

34

B.M.	1.72	146.80	145.08		2+73.82	146.80	136.88	9.92 9.07	0.85	
o + o			137.70	9.10 8.75	0 + 0	137.13	136.80	9.67 10.24 70.67	10.00 8.70	0.30
+26.16			137.62	9.18 8.71						
+52.33			137.54	9.26 8.93						
+76.74			137.47	9.33 8.55						
+01.16			137.40	9.40 8.60						
+25.57			137.32	9.48 8.50						
+50.00			137.25	9.55 8.95						
+74.10			137.18	9.62 8.79						
+98.82			137.10	9.70 8.77						
2+23.23			137.03	9.77 8.66						
+47.65			136.96	9.84 8.82						

Stadium La Jolla High School
Borrow Pit

San Diego Elec. R.R. East Rail Stationing

Roadway 34' left of E Rail 1/2

Grades

TP 1.90 172.39 11.00 170.49

+50

151.48

21°

152.00

+50

152.13

TP

12.01 181.49 0.48 169.48

17°

152.25

TP

12.86 169.96 0.00 157.10

+50

152.38

01° = 379.3 Stadium Sub

152.50

BM

508 157.10

153.02

10-9-37

Moore
Sisson
Hortner

San Diego
Curve to R.

35

300 C28.1 C31.2 182.9 179.9 173.5 156.6 151.5 152.38
1.6 18.2 58.3 +1.4 1.6 8.0 24.9 30.0 27.11
60 60 28 11 4

29.5 C26.0 C26.5 181.0 177.0 173.3 152.7 151.9 152.79
1.5 18.5 52.5 0.5 4.5 8.2 28.8 29.6 28.70
60 60 46.5 30 11 4

29.4 C19.4 172.9 171.5 170.5 153.4 152.5 152.89
10.0 18.7 8.6 10.0 11.0 28.1 29.0 28.60
60 43.7 34 16 4
181.49

17.7 C10.4 163.1 162.7 162.0 152.9 152.4 152.90
7.3 39.2 8.9 7.3 8.0 17.1 17.6 17.06
60 39.2 35 26 4

169.96

152.4 157.1
4.7 0.0 153.1 152.4 152.0 153.00
4.7 34 4.0 4.7 5.1 4.10
60 34 4

152.5 157.1
4.6 0.0 152.5 152.1 153.17
4.6 34 4.6 5.0 3.93
34 4

157.10

East Hill Baye Linc
Curve to Pt

Grades

+10 149.90

11.5 0.0
11.5 34

149.9
11.5
34

150.1 150.06
11.3 11.37
4

+55

151.9
9.5
60

150.9
10.5
34

150.3
11.1
18

151.1
10.3
4

150.95
10.48

161.43

TP 1.16 161.43 12.12 160.27

155.3
17.1
60

150.8
21.6
55

152.1
20.3
38

158.6
13.8
36

157.3
15.1
30

150.8
21.6
17

151.3
21.1
4

151.06
21.33

+50

150.43

+40

50.0105
5

150.53

21.9
12.9
38.5

C 9.0
38.5

12.7
55.4

163.8
8.6
60

159.5
12.9
38.5

157.5
14.9
17

150.4
22.0
15

151.4
21.0
4

151.23
21.16

+30

150.95

21.7
34

C 10.0
20.0
56.5

172.4
20.6
60

169.0
3.4
33.0

164.2
8.2
20

152.4
20.0
11

151.7
20.7
4

151.82
20.57

172.39

172.39

Stadium LaSalle High School
 Top East Edge of Center Footing

10.6?

Nov. 26/34

37

0+00	145.67
+26.165	145.59
+32.83	145.51
+76.745	145.44
1+01.16	145.37
+25.575	145.29
1+50	145.22
+74.405	145.15
+98.82	145.07
2+23.235	145.00
+47.65	144.93
+73.82	144.85
3+00	144.77

B.M. 145.08
 6.07
 151.15

B.M. 145.08
 10.63
 155.71

147.29 ^{stake} 145.0
 8.20
 155.49

5.48 F1.8 9.85 C2.32
 7.3 7.50

5.56 F1.0 9.80 C2.15
 8.2 7.75

5.64 F1.2 9.88 C1.50
 6.8 8.48

5.71 F1.0 10.05 C1.97
 6.7 8.08

5.78 F0.8 10.12 C2.22
 6.6 7.90

5.86 F0.9 10.20 C1.99
 6.8 8.21

5.93 F0.6 10.48 C2.07
 6.5 8.43

6.00 F0.7 10.56 C1.75
 6.7 8.81

6.08 F0.8 10.64 C2.21
 6.9 8.73

6.15 F0.9 10.71 C2.44
 7.1 8.27

6.22 F0.5 10.78 C2.25
 6.7 8.63

6.30 F0.9 10.86 C2.68
 7.2 8.18

6.38 C0.1 10.94 C2.42
 6.3 8.52

Stadium La Jolla High School

Feb. 13, 35

38

010	138.66	7.84 8.84	F1.00	
+26.16	138.58	7.92 8.32	F1.00	
+43.33	138.50	8.00 9.00	F1.00	
+76.74	138.43	8.07 9.07	F1.00	
+101.16	138.36	8.14 9.14	F1.00	
+25.57	138.28	8.22 9.22	F1.00	8.97
+450	138.21	8.29 9.29	F1.00	8.54
+74.40	138.14	8.61 9.61	F1.00	
+98.82	138.06	8.69 9.69	F1.00	
21 2323	137.99	8.76 9.76	F1.00	
+47.65	137.92	8.83 9.83	F1.00	
+73.82	137.84	8.91 9.91	F1.00	
270	137.76	8.95 9.99	F1.00	

BM 145.08
1.42
146.50

145.08
1.67
146.75

Foy Ave. Extension
 From S.L. Westbourne to 401.385.
 Between S.D. Elec Tracks & LaSalle High School
 West Curb Line Sta.

Station	Angle	Dist	Grade	Elevation	Notes
B.M. 8.80		152.88		145.08	Page 32
B.C. = 0-53		52.80		152.66	
0+0	2° 12.18'	3.90	Curb Grade	152.50	1.38 F0.4
+08 = Fire Hyd.	2° 31.139'	out		152.45	1.43
+50	4° 16.882'	3.72		152.18	1.70 F1.6
	Δ 37° 47'				
+10	R 689.04	6° 21.582'	4.04	151.86	2.02 F2.6
	T 235.80				
+50	L 454.38	8° 26.882'	4.36	151.54	2.34 F2.3
	St 2.494				
+20	10° 30.982'	4.68		151.22	2.66 F1.7
		Σ = 0.0639			
+50	12° 35.682'	5.00		150.90	2.98 F1.1
+30	14° 40.382'	5.32		150.58	3.30 F0.6
+50	16° 45.082'	5.64		150.26	3.62 0.0
+79 = P.C.C.	17° 57'	5.82		150.08	3.80 00.30
		5.97			
		00.35			
+91 Cb.F.C.		5.90		150.00	
		3.91			
401.38 E.C.	18° 53.50'				

For East Side See Page 52

Feb. 25, 1935
 Moore 39

East Edge of W Road Level
 With West Curb

145.08
 10.82
 155.90



Note: - Top of Wall
 152.05
 14.10
 151.53
 157.15
 150.51

RP
 Stus 70.0

RP
 Stus 30

85.0-53

1.83

2.35

2.7 F1.4

3.1 F0.9

W. Foy

CONSTRUCTION of
Islevar Septic Tank
Unit #2

Moore
10-16-34

under direction of
Mr. Parvin S.D. Health Dept.

Top skv F.H.	5.62	247.68		242.06	Landis Rose Lawn.
T.P.	0.32	247.19	10.81	236.87	
T.P.	4.25	229.86	15.8	235.61	
T.P.	0.81	230.49	10.18	229.68	
T.P.	0.11	217.71	12.89	217.60	
M.H. Rim			11.00		
" FL			15.58	202.13	FL
T.P.	0.86	205.64	12.93	204.78	
M.H. Rim			10.73		
" FL			18.48	287.26	FL
T.P.	0.89	293.64	12.89	292.75	
NW Cor Tank on ground			7.4		
NE " " " "			4.4		
SE " " " "			7.4		
SW " " " "			9.9		
SE 10' R.P. Hub			4.57	289.07	287.00
T.P.	0.82	289.89	4.57	289.07	

Gr. Top Tank C 207 on 10' SE R.P. = Top Gr. Tank

				FL. Grade	CON-STUBS EL	CUTS
0+00 = Outlet Tank EL				282.22		
0+03 Break	FL.	4.8	285.1	282.20	4.32	285.57 C3.37
0+22		11.9	278.0	274.77	10.25	278.94 C4.17
T.P.	0.05	277.05	12.89	277.00		
0+50		7.0	270.0	266.32	5.82	271.23 C4.91
T.P.	0.07	264.22	12.90	264.15		

See pages 41 & 42

					FL. Grade	CUT STUBS	EL STUBS	CUTS
		264.20						
0+75			5.8	260.4	257.88	2.62	261.60	C 272
1+00			12.4	251.8	249.44	11.02	253.20	C 276
T.P.	0.02	251.64	12.60	251.62				
+55			7.1	244.5	241.0	5.87	245.77	C 279
+55			13.8	237.8	235.58	12.75	238.89	C 281
T.P.	0.25	238.94	12.95	238.69				
+90			10.0	228.9	226.91	9.60	229.74	C 283
T.P.	3.45	229.49	12.90	226.04				
2+08 APT. 0+0			4.3	225.0	223.0	3.89	225.60	C 286
+50					222.8	6.7 3.7	228.0	
1+0					222.6	6.9 3.8	231	
+50					222.4	7.6 3.9	232	
2+0					222.2	7.9 3.7	242	
+50					222.0	7.5 4.2	23.3	
T.P.	7.87	238.14	4.22	225.27				
+75					221.9	11.2 8.0	232	
3+0					221.8	11.3 8.1	245	
+25					221.7	11.4 7.7	237	

223.14

3750

2216

11.5 c3.7
8.7

410

2214

11.2 c3.8
7.5

450

2212

11.0 c3.7
8.5

579

2210

12.1 c3.5
8.2

450

2208

12.3 c3.3
8.0

610

2206

12.5 c3.7
8.8

450

2204

12.7 c4.1
8.6

S.E.R.H. Lark St. Side Walk West Side
S.L. Washington to E. Douglas

12-1-34
Moore

44

BM	1.41	271.35	269.94	J.F.B.P. Washington + Lark	
S.L. Washington			270.50		0.85 0.2100 Ret
50.5			269.08		2.27
100.5			267.67		2.68
150.5			266.24		5.11
200.5			264.83		6.52
250.5			263.41		7.94
300.5			262.00		9.35
325.5 = E. Douglas			261.75		9.60

Server Grades Through Villa Lot 62
 Chatsworth Terrace
 Chatsworth to Existing Septic Tank

12-9-87
 March 45

B.M.	8.77	82.70		73.23		8.20 c 882
0+0	- Existing M.H.			74.50		7.88
	Chatsworth Blvd.					
+27.18	A			74.77		7.93 c 806
						4.87
+50				75.00		7.70 c 858
						4.17
+10				75.50		7.20 c 4.70
						2.50
+14.8	Bk			75.65		7.05 c 868
						6.37
TP	1.03	70.90	12.83	69.87		12.90 c 801
						9.89
+40				58.00		
TP	0.54	58.86	12.58	58.32		11.96 c 859
						8.37
+70				46.9		
TP	2.98	51.30	10.54	48.32		8.80 c 187
						6.93
2+00.18	A Lt			42.50		
+51.38				42.00		9.80 c 266
						6.54

Alley Grades Block 55 LaSalle Park
 For Proposed Hall on West Side

1-3-35
 Moore

46

BM	0.29	88.20		87.91	5.80 Eodril P. 1901
TP	0.12	75.61	12.71	75.49	
TP	10.85	74.02	12.44	63.17	
0+64				69.08	4.91 5.71 F0.77
+70				69.23	4.99 5.53 F0.74
+80				69.43	4.59 5.68 F1.09
+90				69.62	4.40 7.13 F3.03
+50				70.07	3.95 7.26 F3.81
+64				70.20	3.82 6.85 F3.03
Top Hall N.L. Eads on East		59.5		68.07	(68.07)

Curb Grades
UNION OIL STA.
ATLANTIC & BEACH

1/55
Moore

47

ct. 91.

P.C.

5.20 4.74
4.8702 Cb

BM 4.94 S.F. 8P
5.20 Beach & Atlantic
10.14

#1

5.22 4.97

#2

5.14 5.02

#3

5.10 5.04

E.C. #4 = 6' N. of N.L. Beach

5.10 5.04

51 " " "

5.17 4.97

100 " " "

5.25 4.88

Miramar Ave
N. of Pearl St

1-28-35
48

	EL.
00 = N. Pearl	181.50
0 +10	182.30
+30	183.60
+50	184.40
+70	184.70
+90	184.50
1 +10	183.80
+30	182.70
+50	181.10
+70 P/C	179.00
+05	174.85
+40 P/C	170.70
+60	168.60
+80	166.60
2	165.0
+20	163.90
+40	163.20
+60	162.70
4	162.10
+50	161.50
+90	161.00

BM	0.45	185.46	185.01	SE. 8 th College Excluding
TP	0.23	172.94	12.75	172.71
TP	1.08	161.64	12.38	160.56
TP			0.17	161.47

16250 cont/600

Beryl
Ingraham to 280 E of Jewell

	NL	SL
EL Ingraham	128.70	127.70
+40	133.30	132.7
+80	137.8	136.8
1 +20	142.4	141.4
+60 PVC	147.0	146.0
2	151.0	150.0
+40	153.3	152.3
+80 PVC	154.9	153.9
+20	155.4	154.4
+60	155.9	154.9
4	156.5	155.5
+40	157.0	156.0
+80	157.5	156.5
5 +20 W2 Jewell	158.0	157.0
0 +60 EL	159.0	158.0
+40		
+80		
1 +20		
+60		
2		
+40		
+80 DRK.	163.0	162.0

For St. Dept.
Borrow 177

Moore

49

128.70	N 28.7	37.8	37.8	42.4	47.0	51.0
11.64		19.2	14.9	10.8	7.3	3.8
140.34		9.5	6.1	1.6	10.4	7.2
139.79		+9.7	+8.0	+3.7	+7.4	+6.1
12.97						
152.76	S 27.7	37.3	36.8	41.4	46.0	50.0
6.64		8.0	5.4	11.3	6.7	2.7
159.40		2.5	1.6	1.7	6.9	2.4
156.90		+4.2	+0.9	+0.2	-0.2	-0.7
161.10						
170.04	N 57.3	54.9	55.4	55.9	56.5	57.0
	11.5	9.9	9.2	8.9	8.3	7.8
	5.0	6.6	5.0	5.0	3.0	2.1
	+6.1	+4.9	+6.2	+5.9	+6.9	+4.7
	S 52.3	53.9	54.4	54.9	55.5	56.0
	9.4	10.9	10.4	9.9	9.3	8.8
	1.2	12.8	11.4	11.0	10.4	11.3
	-0.8	-1.3	-1.0	-1.7	-2.1	-2.4
	N 57.5	58.0				
	7.2	12.0				
	0.4	13.6				
	+6.8	+8.2				
	S 56.5	57.0				
	8.8	7.8				
	11.0	10.6				
	35.7	34.8				

SUMMIT A. 12 wide
CONST.

0+00	M. Not NL 258.17	N.L. 257.97	at R 258.27	SE 258.06	-1.12
0+12	M. Not NL 258.10	257.90	at R	Gr. Corv	NL 0.0
0+15 R		257.80 ^{0.0}	257.85	257.90	-0.11
0+18				257.85	+0.50
0+50		257.30 0.0		257.30	+0.48
0+70	at dip	256.30 0.0		256.30	OUT
0+90	v	255.10 0.0		255.10	OUT
1+05.65 = PC. LT.		253.90 0.0			
1+12.69 = PC. RT.				253.15	+0.12
1+18.35		252.70 0.0	OUT	252.55	+0.05
1+31.06		251.89 0.0		252.0	+0.11
1+48.74 = Ev. Pav.		251.20		251.89	+0.69

20.0'

258.26 Top Hyd
8.65
262.91
8.65
258.26
2.41
256.67

30'
24'
7.7'

Dover St. Water gauge
70/607 to Jennings
For Water Dept.

Moore
2-14/35

0+00 = SL to bot = Gate Valve	214.1
+17 R. Return = F.H. Cbgr. 219.2	215.6
+50	216.8
+90	218.0
1+30	220.8
+70	222.2
2+10 = EVC	226.4
+50 = NL Kex	229.4
+90 = "70c"	232.6
3+10 = SL Kex	234.2
+70 P.V.C.	239.0
4+10	242.0
+50	244.5
+90	246.5
5+30	248.8
+60 NL JOHN	249.4
6+00 = "Tree"	250.6
+20 "L JOHN"	251.1
+50	251.9
7	253.5
+50	255.0
8	256.7
+50	258.3
+70 NL Jennings = Gate Valve	259.1

State B.M.

13 Sch

cb. gr. F.H. at River R.

52

217.04	215.1	215.6	219.20	216.8	218.6	210.8
0.35	9.6	9.1	0.0	7.9	6.1	3.9
37.44	6.1	6.1	0.0	5.0	5.6	1.6
15.01	13.2	13.0	0.0	2.9	3.5	5.3
44.33						
4.76						
0.87						
23.89						
11.66						
23.24	223.2	226.2	229.4	232.6	234.2	239.0
1.17	12.4	9.9	6.1	15.2	13.8	9.0
6.24	9.6	6.0	6.1	12.4	11.8	7.7
37.30	44.8	43.0	43.1	45.2	42.7	47.3
12.70						
48.00						
0.97						
47.63	244.0	244.5	246.5	248.3	249.2	250.5
1.17	6.0	7.3	10.3	11.4	10.6	9.7
2.70	2.2	1.9	10.3	11.4	10.6	6.1
49.87	12.8	13.4	12.5	12.2	12.2	12.2
10.51						
49.41						
69.94	251.1	251.9	253.5	255.0	256.7	258.3
	8.7	7.9	6.3	4.3	1.30	11.4
	4.9	4.0	2.7	0.8	9.6	8.0
	13.8	13.9	13.8	4.4	13.4	12.2
	259.1					
	10.6					
	17.4					
	1.2					
	6.7					
	263.04					
	262.0					

SECOR
Mr. Jann + Dover

Fay Ave Extension
From S.L. Westbourne to 402.5 S
East of S.D. Elec. Track

21 Roadway
From 6.5 F of E Track

W Edge
East Road

BM	11.85	156.91	145.08	Page 32
0+0	S.L. Westbourne		153.00	3.9 F0.8 47
+50			152.88	4.0 F0.7 47
+100			152.76	4.2 F0.4 48
+150			152.64	4.3 0.0 43
+200			152.52	4.4 F0.3 47
+250			152.47	4.4 0.0 47
+300			152.27	4.6 F0.2 48
+350			151.82	5.0 F0.5 5.5
+400			151.32	5.6 0.02 5.7
4+02.5			150.30	6.6 F0.2 6.8

S = 0.024

Forrest Road See Page 35

2-27-35
Moore

52

Note East Gutter
0.40 Below W Edge

at S.L. Westbourne

Fay Ave grades	S.L. Westbourne	Nly to P.L.
W Top of	at below Top rail W rail track. at below	W gutter
00 - 25 = P.L.	153.60	153.10
00 = Nend Stadium		152.33
+50		153.00 ✓
		152.80 ✓
+50		152.92 ✓
		152.66 ✓
1		152.84 ✓
		152.53 ✓
+50		152.76 ✓
		152.50 ✓
2		152.78 ✓
		152.26 ✓
+50		152.60 ✓
		152.12 ✓
3		152.52 ✓
		152.01 ✓
+50	152.60	152.42 ✓
		151.85 ✓
+68 E grade to inlet		152.42
+80 Sly Westbourne	152.5	152.40
		151.60 ^{grade}
		151.90

BM 14508
11.73
156.81

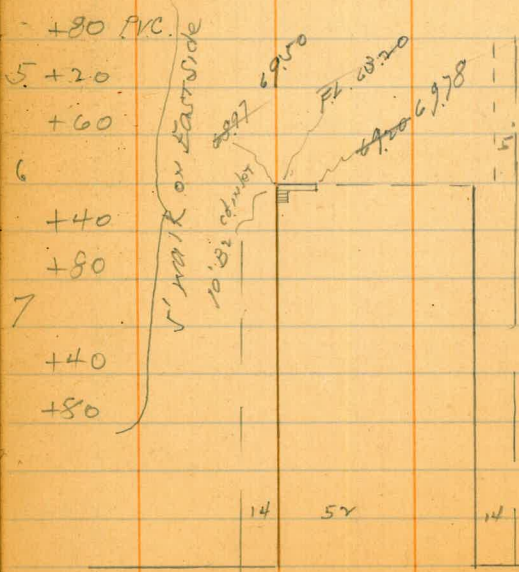
Moore
Dixon
Northern
5-25.

Clover St. Pearl N.Y. CUT & FILL

Pearl 4
NEAR 107th St.

53

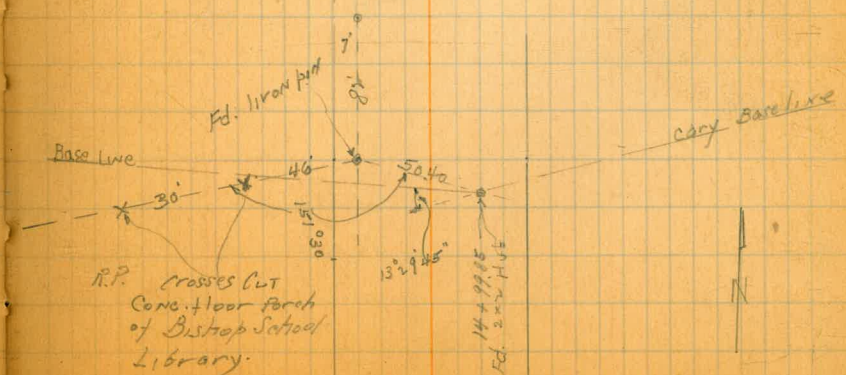
	W.C.	E.C.	
N.L. Pearl = 00	78.04	79.55	65.00 12.89 77.93 0.21 77.74 4.89
+50	76.97	78.44	82.23 7.18 75.15 4.07
1	75.90	77.34	79.22 16.23 63.99 7.53
+50	74.84	76.23	76.57 2.64 73.88 6.09
2	73.77	75.13	79.97 11.21 68.76 3.46
+50	72.70	74.02	72.22 7.21 65.01
3	71.64	72.92	64.99
+50	70.57	71.81	
4	69.50	70.70	
+25 = N.Y. end St.	68.97	70.12	
+50		69.57	
+80 P.V.C.		68.90	
5 +20		68.20	
+60		67.70	
6		67.40	
+40		67.90	
+80		69.30	
7		70.30	
+40		72.20	
+80		73.60	



Pearl St

W	77.0 5.3 6.2 -0.9	75.9 6.4 7.3 -0.9	74.8 7.5 8.1 -0.6	73.8 8.5 8.9 -0.4	72.7 9.6 9.4 +0.2	71.6 10.7 9.9 +0.8	70.6 11.7 10.7 +1.0	69.5 12.7 10.9 +1.2	69.0 13.2 11.2 +1.0
E	78.4 3.9 3.7 +0.7	77.3 4.0 4.5 +0.8	76.2 4.1 5.0 +1.1	75.1 4.2 4.4 +1.8	74.0 4.3 6.3 +1.6	72.9 4.4 7.3 +2.3	71.8 4.5 8.1 +2.4	70.7 4.6 9.9 +1.7	70.1 4.7 8.2 +0.9
E	69.6 9.6 8.4 +1.2	P.V.C. 68.9 10.3 8.9 +1.4	68.2 11.0 9.3 +1.7	67.7 11.5 9.8 +1.7	67.4 11.8 10.2 +1.6	67.9 12.1 7.7 +0.9	69.3 12.5 7.8 -0.6	70.3 12.7 6.7 -0.5	72.2 12.8 4.7 +3.1
E	73.6 6.4 2.8 +3.6								

See NEXT Page



Iron pin
NEW Car Library
Clover's B.M.

Carrier St
 Pearl N 425
 C-grade change

Mode
 6-18-35

54

	w cb	E cb	7774 TP 4.25 82.29 1.86 75.43 4.13 79.56
NL Pearl = 00	78.04	79.55	
+50 NY	77.04	78.54	
1	76.03	77.53	
+50	75.02	76.52	
2	74.02	75.52	
+50	73.01	74.51	
3	72.01	73.51	
+50	71.0	72.50	
4	70.0	71.50	
+25 = END ST.	69.50	71.00	

Set rough grade 6-18-35

	0+50	1	+50	2	+50
W	77.04 5.3 6.1 -0.8	76.03 6.3 7.2 -0.9	75.02 7.3 8.1 -0.8	74.02 8.3 9.2 -0.6	73.01 9.3 10.2 -0.0
E	78.54 4.3 5.2 +0.6	77.53 5.3 6.2 +0.7	76.52 6.3 7.2 +0.9	75.52 7.3 8.2 +1.4	74.51 8.3 9.2 +1.1
S		+50	4	+25	
W	72.0 10.3 9.9 +0.4	71.0 11.3 10.7 +0.6	70.0 12.3 11.7 +0.6	69.5 13.1 12.6 +0.5	
E	73.50 8.8 7.7 +1.1	72.50 9.8 8.7 +1.1	71.50 10.8 9.7 +0.9	71.0 11.8 10.7 +1.1	

Ch. grade inlet

w end cb	69.50 10.06 10.65 -0.59	69.78 = End of inlet 9.78 8.78 +1.0	63.20 Fl. Box. 16.36 10.65 +5.11
----------	----------------------------------	--	---

CUT OFF to Left
Pac Ave to Balboa

Moore
Sisson
Northern
6-5-45

20 PAVING CONSTR. by CITY ST. DEPT.

4 + 79.45 = E.C. 19° 11.75'

Levels next page.

+50 15° 49.26'

4 10° 05.45'

+50 4° 21.66'

3 + 11.94 = B.C. LT.

2 + 99.95 = E.C. 20° 06.30'

+50 16° 45.25'

2 13° 24.20'

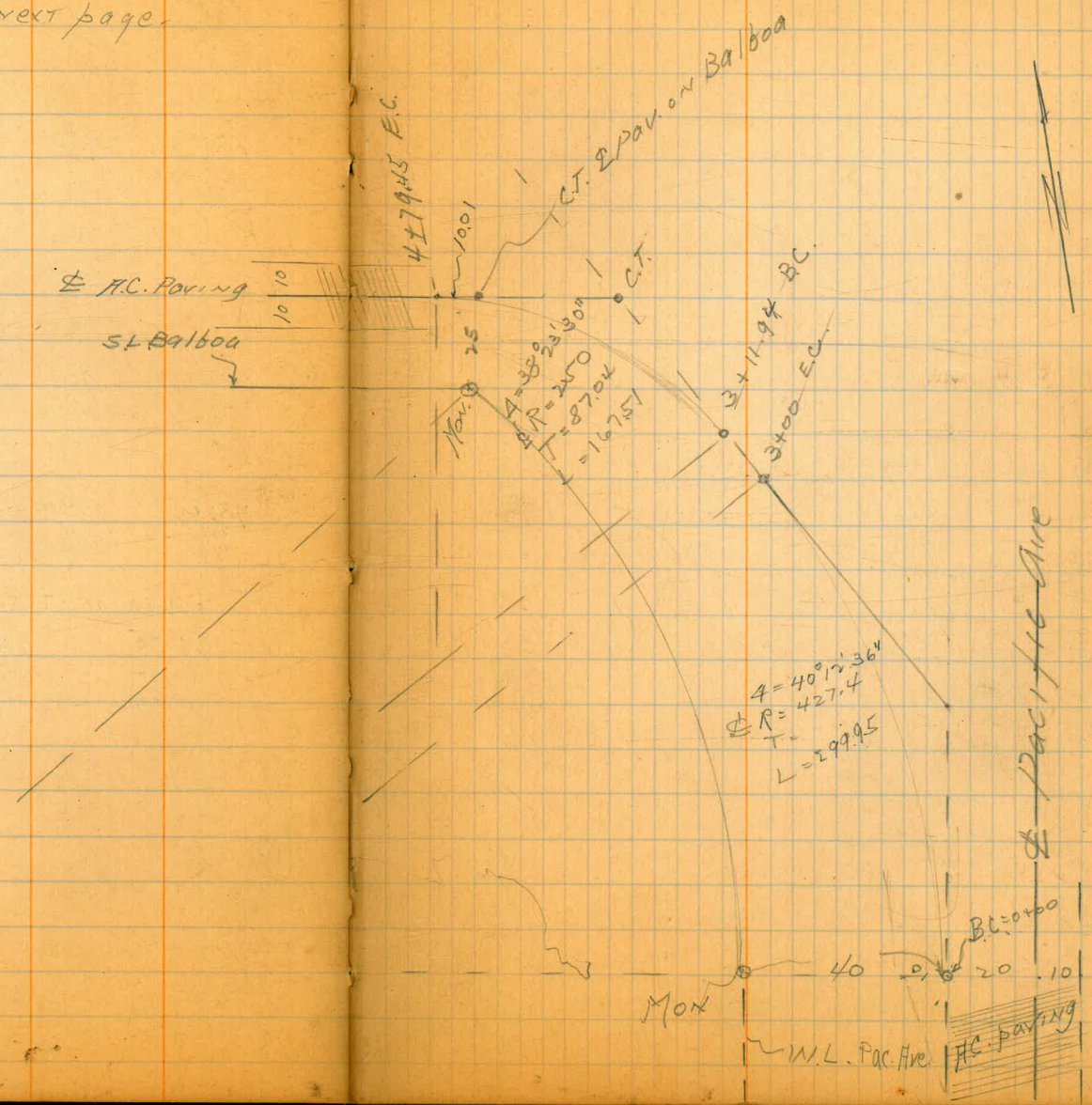
+50 10° 03.15'

1 6° 42.10'

0 + 50 3° 21.05'

0 + 00 = B.C. LT.

Indexed
C.S.K.



rod El. NEMOX. 1978
 9r yr 251004 +
 positio 21.45

edge par. 10 LT. edge par. K
 Grade 10 RT. - edge par.

56

CUT stakes set 25' RT & LT of Φ

at grade pt. 10' " " " "

wly + Ely edge of 20'
 paving

4 + 79.45 EC

+50

4

71⁵

1430

3 + 80

+50

3 + 11.94 BC

2 + 99.94 EC

+50

2

+50

1

0 + 50

495

16.50

0 + 00 BC

535

16.10

	7.80	13.65		
	$\frac{8.03}{0.23}$			
	7.55	13.90	14.30	
	$\frac{7.10}{+0.15}$	14.05 OUT	14.05 OUT	14.00 OUT
	7.13	14.30	14.70	15.00
	$\frac{7.27}{-0.14}$			$\frac{6.44}{6.28}$ + 0.17
	6.81	14.60	15.00	15.40
	$\frac{7.14}{-0.33}$			$\frac{6.00}{5.00}$ + 1.0
	6.71	14.70	15.10	15.50
	$\frac{7.01}{-0.30}$			$\frac{5.90}{5.30}$ + 0.10
	6.29	15.10	15.50	15.90
	$\frac{6.40}{-0.11}$			$\frac{5.50}{5.01}$ + 0.09
	5.87	15.50	15.90	16.30
	$\frac{6.20}{-0.33}$			$\frac{5.07}{5.04}$ + 0.03
	5.44	16.00	16.40	16.80
	$\frac{5.85}{-0.40}$			$\frac{4.64}{4.61}$ + 0.03
	5.21	16.20	16.60	17.00
	$\frac{6.14}{-0.90}$			$\frac{4.44}{4.50}$ - 0.05
	5.14	16.30	16.50	
	$\frac{5.74}{-0.60}$			
	5.54	16.00	16.10	
	$\frac{5.60}{-0.06}$			

Tennis Court Bleachers
La Jolla Hi-School.

S.E.R.F.

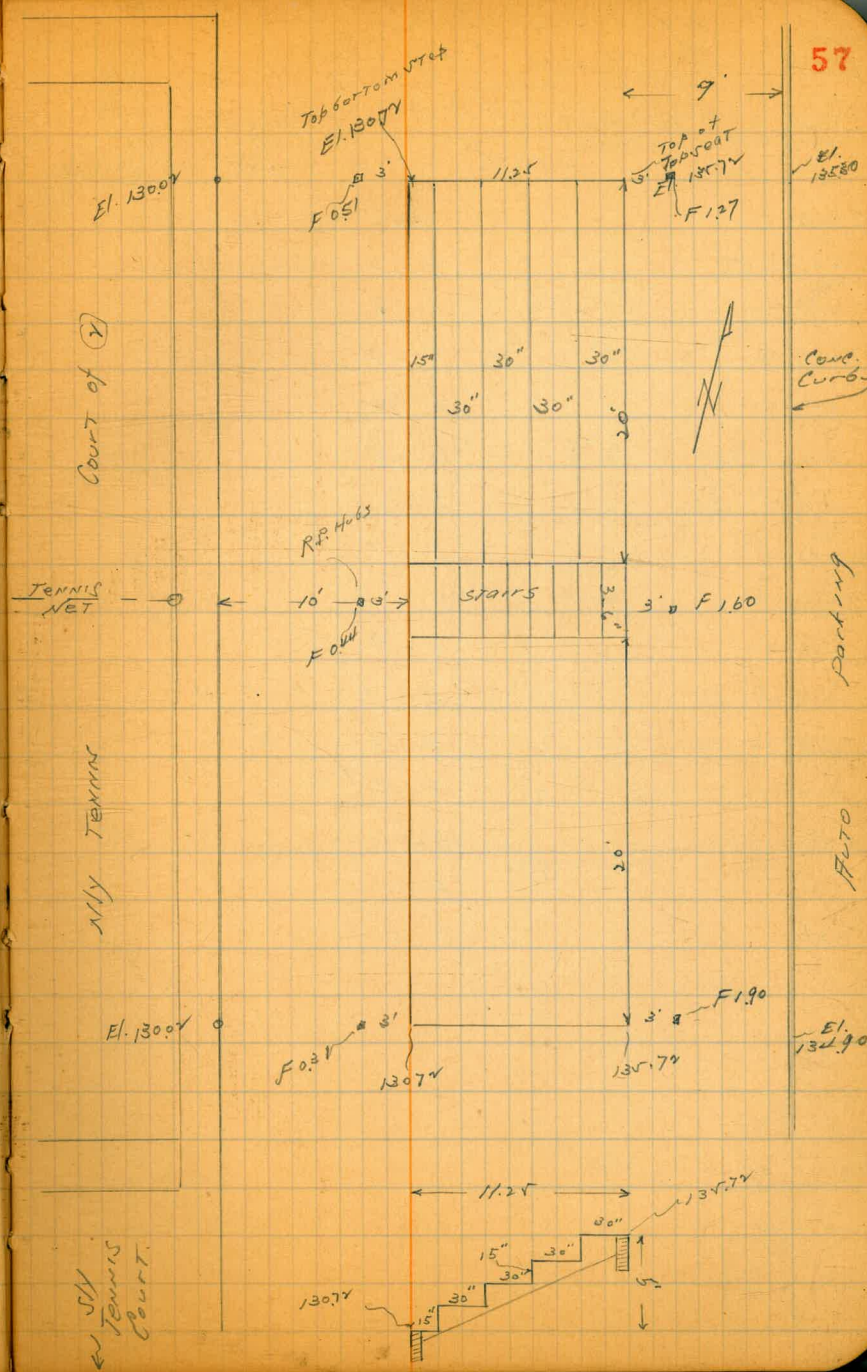
Moore
7-2-34

B.M.	058	144.46	145.08
T.P.	271	138.22	9.95
			135.57

Top rd. wall
end of curb
Ray & W. Course

130.72	750	750	135.72	2.50	2.50
7.50	794	781	5.20	2.10	4.40
5.01	0.44	0.21	3.77	1.60	-1.90
-0.41			-1.27		

820	2.47	337
1300.2	1318.0	1279.0



May
11-6-38

Alley Bk 3
Paving grades
N & S W alley

Douglas
W. 1100

SL Douglas 500	270.45	270.88
+10	271.0	271.3
+20	271.2	271.5
+30	271.4	271.5
+40	271.0	271.3
1 + 00.9 = W. of Edw	269.0	269.30
1 + 15.9 = SL " " "	268.6	268.80
1 + 53.9	267.40	267.60
1 + 91.9	266.20	266.40

270.53
4.94
275.47
6.23
269.17 TP
5.17
272.25
3.81
268.44 TP
272.95

E & W alley

SL Brk 400	266.36	266.43
0 + 20	266.70	266.80
0 + 70	267.28	267.47
+80 Brk	267.40	267.60
1 + 20	267.55	267.70
+60	267.70	267.80
+80	268.0	268.10
2 + 06.5	268.6	269.0

269.14
2.81
272.95

60

W	70.45 4.9	71.0 4.97 0.00	71.2 4.97 0.00	71.4 4.97 0.00	71.0 4.97 0.00	69.0 6.37 5.47 +0.90	68.6 6.37 5.47 +1.0	67.4 2.85 0.00	66.20 6.04 5.80 +0.24
E	70.84 +1.55	71.3 4.07 2.07 +1.0	71.5 3.87 2.90 +1.0	71.5 3.87 2.87 +1.0	71.3 4.07 3.07 +1.0	69.3 6.07 5.07 +1.0	68.8 6.07 5.07 +1.0	67.6 4.65 4.14 +0.50	66.4 5.85 5.84 +1.0

N	66.43 6.54 1.00	66.80 6.14 5.14 +1.0	67.15 5.80 4.63 +1.15	67.50 5.45 4.55 +0.90	67.80 5.10 4.20 +0.90	68.10 4.85 3.85 +1.0	68.6
---	-----------------------	-------------------------------	--------------------------------	--------------------------------	--------------------------------	-------------------------------	------

S	66.36 6.54 6.53 +0.01 pav	66.60 6.35 5.35 +0.97	66.95 6.00 4.90 +1.10	67.20 5.75 4.87 +0.75	67.50 5.45 4.55 +0.90	67.80 5.10 4.20 +0.90	68.6
---	------------------------------------	--------------------------------	--------------------------------	--------------------------------	--------------------------------	--------------------------------	------

N	66.80 2.75 5.11 +1.0	67.47 5.48 4.63 +0.85	67.60 5.34 4.54 +1.0	67.70 5.25 4.55 +0.70	67.80 5.15 4.31 +0.84	68.10 4.84 2.94 +2.0
---	-------------------------------	--------------------------------	-------------------------------	--------------------------------	--------------------------------	-------------------------------

S	66.70 6.25 5.35 +0.90	67.28 5.67 4.94 +0.74	67.40 5.54 4.84 +1.0	67.55 5.40 4.92 +0.48	67.70 5.25 4.84 -0.20	68.0 4.94 5.64 -0.10
---	--------------------------------	--------------------------------	-------------------------------	--------------------------------	--------------------------------	-------------------------------

Bayside Lane +
 Alley Paving BX NT - 154

March
 11-7-25

SWSP San Juan
 Sea Wall

7.07
1.13
8.90
9.28
- 1.08
4.22
4.06
3.14



Lane

San Juan Pl.

Bldg

155

Trowan



Bayside Lane

W	-1.74	-1.71	-2.03	-2.08
	3.14	3.14	3.14	3.14
	5.06	5.13	5.17	5.22
	4.06	4.12	4.17	4.22
	+1.0	+1.0	+1.0	0.0
E	5.06	5.13	5.17	5.22
	5.21	5.27	5.34	5.39
	-0.11	+0.11	+0.17	-0.11

Alley

N	-1.65	-1.87	-1.99
	3.14	3.14	
	4.79	4.96	
	4.88	4.64	
	-0.09	+0.32	
S	-1.09	-1.86	-2.03
	3.14	3.14	
	4.83	5.00	
	4.39	4.00	
	+0.04	+1.0	

Sewer Grabs
 BIK 389 Pac. Beach

11-15-55
 Tim Carroll
 W.P.

DMH #1 = 00

+36
 +74
 1 + 08

1 + 44 = M.H. #2

1 = 478.75
 2 + 13.50
 2 + 48.25

2 + 83.0 = M.H. #3

00 = DMH #4

0 + 45.94
 0 + 91.88
 1 + 37.82

1 + 83.75 = M.H. #2

00 = D.D. M.H. #5

0 + 46.89
 0 + 93.78
 7 + 40.07

1 + 87.5 = M.H. #3

-10.20
 -8.0
 -7.75
 -7.50
 -7.25
 -7.0
 -6.75
 -6.50
 -6.25
 -6.0
 -2.0
 -3.25
 -4.50
 -5.75
 -7.0
 -3.56
 -4.17
 -4.78
 -5.39
 -6.00

+9.24
 +7.04
 +0.77
 +6.04
 +6.64
 +5.91
 +5.70
 +5.64
 +5.29
 +4.51
 +4.71
 +5.14
 +4.64
 +5.10
 +5.24
 +5.01
 +4.41
 +4.39

-1.73 NEBP Pac. + Mission
 6.68
 4.95

-1.73
 6.06
 4.33

-7.07
 11.48
 4.77
 +6.63

-6.57
 10.90
 4.77
 +6.12

-6.93
 11.26
 4.80
 +6.46

-6.43
 10.76
 4.80
 +5.96

E cb grades on Girard St
S of Pearl

Sta 7+00 to 10+27 = FB 1526-11

E cb. grades

7+00	142.5
+50	144.58
8+00	146.64
+50	148.74
9+00	150.80
+40 Break	152.50
10+00	155.35
+27 = Δ in Cobble ditch draw	156.68

158.75 DMBP Center of Girard NW Cor
cut-off.

23

142.5 TOP CB EL.
15.5
158.0

= Pav grade 14' W of E CB

141.8	142.9	146.0	148.0	150.1	151.5
	10.1	8.0	6.0	5.9	2.2
	11.0	10.2	9.0	8.4	4.3
	0.9	2.2	3.0	2.5	2.1

154.7

0.7
1.6
2.3

4574 St Grading Gr. 30'
Market to Hillsop

±

64

+50

$$\begin{array}{r} 65 \\ 4.6 \\ + 7.9 \end{array}$$

163.2

$$\begin{array}{r} 3 \\ 6.2 \\ 8.7 \\ + 7.9 \end{array}$$

3

$$\begin{array}{r} 7.5 \\ 6.0 \\ + 7.5 \end{array}$$

162.7

$$\begin{array}{r} 3 \\ 7.9 \\ + 7.4 \end{array}$$

+50

$$\begin{array}{r} 83 \\ 7.3 \\ + 7.0 \end{array}$$

161.4

$$\begin{array}{r} 81 \\ 7.3 \\ + 8.8 \end{array}$$

2

$$\begin{array}{r} 88 \\ 6.2 \\ + 5.0 \end{array}$$

160.9

$$\begin{array}{r} 86 \\ 8.2 \\ + 6.4 \end{array}$$

+50

$$\begin{array}{r} 82 \\ 5.4 \\ + 8.7 \end{array}$$

160.5

$$\begin{array}{r} 9.0 \\ 10.0 \\ - 7.0 \end{array}$$

1

$$\begin{array}{r} 97 \\ 9.6 \\ + 0.1 \end{array}$$

160.0

$$\begin{array}{r} 9.5 \\ 11.0 \\ - 1.5 \end{array}$$

+50

$$\begin{array}{r} 10.1 \\ 10.7 \\ - 0.6 \end{array}$$

159.6

$$\begin{array}{r} 9.9 \\ 11.1 \\ - 7.4 \end{array}$$

0+00 = Nly Market

BMBP 10.65 169.50

#158.85

NW Market +
45 TH

159.1

$$\begin{array}{r} 10.45 \\ 0.1 \end{array}$$

grade change
raised

65

⊕

+80

$$\begin{array}{r} 9.4 \\ 9.4 \\ - 8.1 \\ \hline \end{array}$$

160.0

$$\begin{array}{r} 9.2 \\ 9.2 \\ - 0.0 \\ \hline \end{array}$$

161.4 ✓

+40

$$\begin{array}{r} 7.8 \\ 7.4 \\ + 8.2 \\ \hline \end{array}$$

161.6

$$\begin{array}{r} 7.6 \\ 7.4 \\ - 0.3 \\ \hline \end{array}$$

161.3 ✓

6

$$\begin{array}{r} 6.1 \\ 6.3 \\ + 0.3 \\ \hline \end{array}$$

163.3

$$\begin{array}{r} 5.9 \\ 6.1 \\ - 0.2 \\ \hline \end{array}$$

163.4 ✓

F.P. 4.39 169.21 4.68 164.54

163.3

+60 ✓

$$\begin{array}{r} 4.8 \\ 4.7 \\ + 8.1 \\ \hline \end{array}$$

164.9

$$\begin{array}{r} 4.3 \\ 4.2 \\ + 0.1 \\ \hline \end{array}$$

at 5 of
here

5 + 20

$$\begin{array}{r} 3.9 \\ 3.2 \\ + 8.7 \\ \hline \end{array}$$

165.8

$$\begin{array}{r} 3.7 \\ 3.4 \\ + 7.3 \\ \hline \end{array}$$

+80

$$\begin{array}{r} 3.6 \\ 3.4 \\ + 1.2 \\ \hline \end{array}$$

166.1

$$\begin{array}{r} 3.4 \\ 3.6 \\ + 7.3 \\ \hline \end{array}$$

+40

$$\begin{array}{r} 4.0 \\ 2.5 \\ + 1.2 \\ \hline \end{array}$$

165.7

$$\begin{array}{r} 3.8 \\ 1.1 \\ + 3.7 \\ \hline \end{array}$$

1

169.50

$$\begin{array}{r} 5.0 \\ 2.9 \\ + 2.1 \\ \hline \end{array}$$

164.7

$$\begin{array}{r} 2.8 \\ 1.6 \\ + 2.2 \\ \hline \end{array}$$

+40

$\frac{3.9}{2.3}$
+ 1.1

165.5

$\frac{3.7}{1.3}$
+ 1.9

E
grade change 66
→

10

$\frac{1.6}{2.9}$
+ 1.7

164.8

$\frac{1.4}{2.3}$
+ 2.3

OK

+50

$\frac{5.8}{1.3}$
+ 0.5

163.6

$\frac{5.9}{0.9}$
+ 0.9

163.9

9

$\frac{4.9}{6.0}$
+ 0.9

162.5

$\frac{4.0}{2.3}$
+ 2.3

162.9

+50

$\frac{8.0}{7.9}$
+ 0.1

161.4

$\frac{7.8}{5.2}$
+ 2.6

161.9

8

$\frac{9.3}{9.0}$
+ 0.3

160.1

$\frac{9.1}{7.8}$
+ 1.3

161.1

+60

$\frac{10.0}{9.9}$
+ 0.1

159.4

$\frac{9.8}{8.7}$
+ 1.1

160.3

7+40 = 12" Col/s

FL

157.7 0.17

0.17 158.5

7+20

161.21

$\frac{10.2}{10.1}$
+ 0.1

159.2

$\frac{10.0}{9.7}$
+ 0.3

161.0

check to north fence post
 same Hill top 6' E of last line 715 165.56 165.86

+50 = SW Hill top

$$\begin{array}{r} 9.7 \\ 8.3 \\ + 1.7 \\ \hline \end{array}$$

168.5

$$\begin{array}{r} 8.5 \\ 8.4 \\ + 2.1 \\ \hline \end{array}$$

27

$$\begin{array}{r} 8.6 \\ 7.6 \\ + 1.6 \\ \hline \end{array}$$

164.6

$$\begin{array}{r} 8.8 \\ 8.8 \\ + 4.1 \\ \hline \end{array}$$

+60

$$\begin{array}{r} 7.9 \\ 6.1 \\ + 1.8 \\ \hline \end{array}$$

165.3

$$\begin{array}{r} 7.7 \\ 3.9 \\ + 3.9 \\ \hline \end{array}$$

11+20

$$\begin{array}{r} 7.4 \\ 6.1 \\ + 1.3 \\ \hline \end{array}$$

165.8

$$\begin{array}{r} 7.2 \\ 4.4 \\ + 2.8 \\ \hline \end{array}$$

T.P. 6.11 173.01 231 166.90

10+50

$$\begin{array}{r} 3.6 \\ 1.8 \\ + 1.8 \\ \hline \end{array}$$

165.8

$$\begin{array}{r} 3.4 \\ 1.3 \\ + 2.1 \\ \hline \end{array}$$

269.21

Alley Parking 13-5-55
 8-9-10-11 So. La Jolla Moore

A

Grade changed to 17007
 Now April on West See Profile

1+00

$\frac{1}{C}$

+80 Brk

+60 Brk

T.P. 584 51.99 4.01 46.17

+50

+40 Brk

+20 Brk

0+00 = Nth Bonnar

Top 6 10.02 50.18 54.16 on West

W 4840 = 52 E Alley

E

68

47.10

4.84
 5.03
 - 0.14

46.50

5.49
 5.53
 - 0.104

45.60

6.39
 6.40
 - 0.01

45.00 = Top curbing

5.00
 4.01
 + 1.17

44.30
 5.83
 4.29
 + 7.19

42.40
 7.78
 5.51
 + 2.27

40.15

40.15

Top 8

47.30

4.29
 5.17
 + 2.15

46.70

5.29
 3.06
 + 2.23

45.80

6.19
 3.69
 + 2.50

44.50

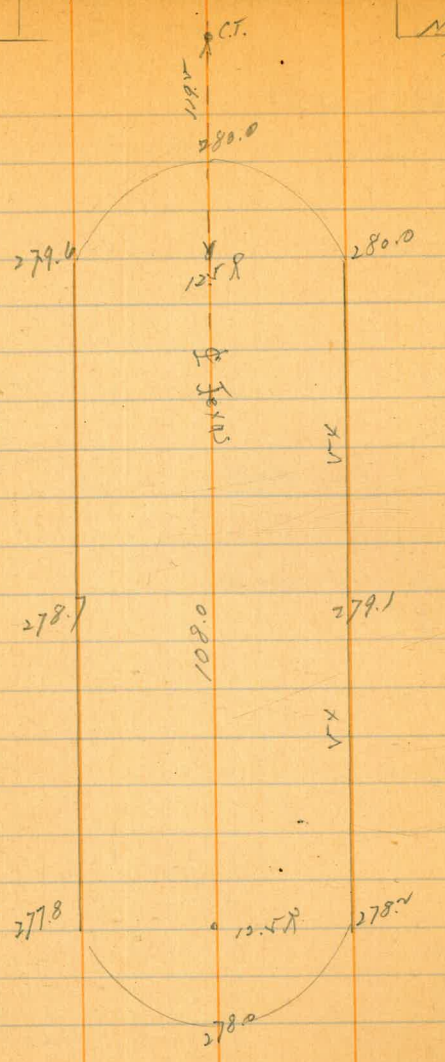
5.68
 3.40
 + 2.28

42.60

7.58
 4.56
 + 3.02

40.80

-1



Ny Upas

NW Upas
Arizona
269.2
10.14
279.10

Parking Curbs
Texas & Upas

Moore
12/9/34

$\frac{280.0}{3.1}$	$\frac{280.0}{3.1}$	$\frac{279.1}{4.0}$	$\frac{278.7}{5.4}$	$\frac{278.0}{5.1}$	$\frac{277.8}{5.3}$
$\frac{278.7}{4.4}$	$\frac{279.6}{3.5}$				

38th St Curb grades
W-side S of Wightman

0	Ely Wightman	318.90
+50		318.40
1		317.90
+50		317.40
2		316.90
+50	BRK	316.40
3	"	314.80
+50	"	311.40

319.70 NW1 Wightman +2570
3.59
323.29

70

Survey Lot 1 Blk 11 Mission Hills
for Mr Sample.

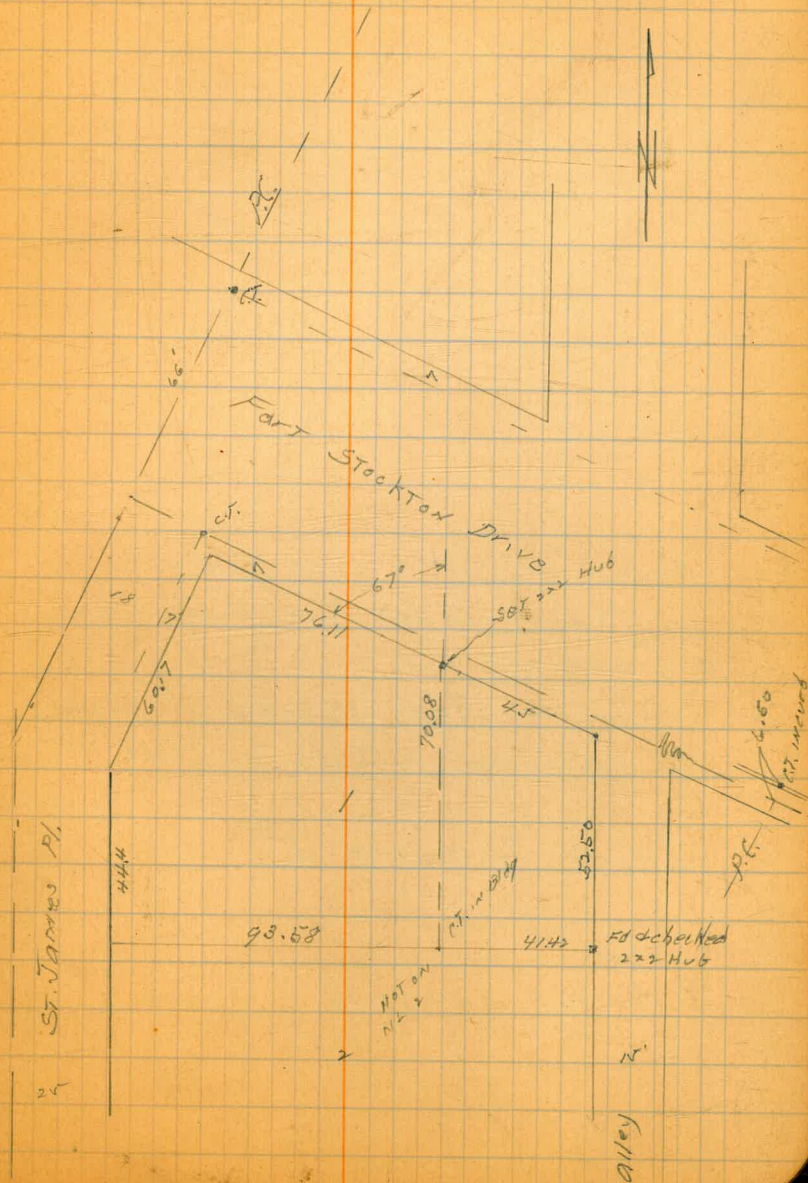
Moore
Sisson
Northern

12-14-35

Indexed

C.S.K.

71



Moore
1-8-36

Mason St. curbs
Bet. San Diego + Congress
in front of Old Town Library
Grade change see profile Mason St.

Nly Congress 18.50

0 + 75 19.0

1 + 125 19.25

1 + 50 = B.M. 19.50

Reset U.S.B.M. Old Town
on Mason St. bet. San Diego Ave.
+ Congress St.

Granite Mark. Moved 1' N.Wly
to position inside of Curb.

4.135 rod

Reset to same El.

Moore
Northern
Sierra 1-8-36.

72

2225 Swly San Diego + Mason B.P.B.M.
2225
2225
4.73

18.50
6.43
diff

19.0
5.73
1

19.25
5.48
1

19.50
5.23
1

Moore
1-21-36
Comfort Sta. Const.
Foot of Diamond at Ocean
new grade

M.H. #15=00	0+00	21.00 ✓	
	0+70 = Ev. Pipe.	21.79 ✓	21.84 ✓
	1+00	21.78	21.93 (6.18)
	1+35 = St. Diatr.		22.01 (7.39)
	1+75 = 2 "	21.87	22.10 (7.58)
	2+04 = M.H. to Const 3' x 4' x 6' Diamond St.	22.18 ✓	22.18 ✓
	2+07 6" No. 6	22.45	
	2+75	22.74	
	3+00	23.03	
	3+30	23.32	
	3+50	23.61	
	4+00	23.78	
	4+84 = Fly Comfort Sta.	23.80	

Floor El. 25.50

30.92
6.12
37.06 X

1.56
C 7.00 To floor el.
from rail in post
at SE Cor Sta.

15.77
C 6.80

15.18
C 7.00

22.18
C 7.58

14.88
5.70
C 9.18

14.61
5.55
C 9.36

14.32
5.14
C 9.20

14.03
5.00
C 9.23

13.74
4.85
C 9.03

13.46
4.64
C 9.01

13.28
4.21
C 9.07

Comfort Sta.

2+84

Ocean Ave.

N. Curd

Diamond

5' curb

0+00 = Ex. M.H.

2+04

Pump

M.H. to Const

Moore
1-24-34

N + S alley BIK 242 W.H.

for St. Dept
S.A. Hyd. Cyprus part 2d.

74

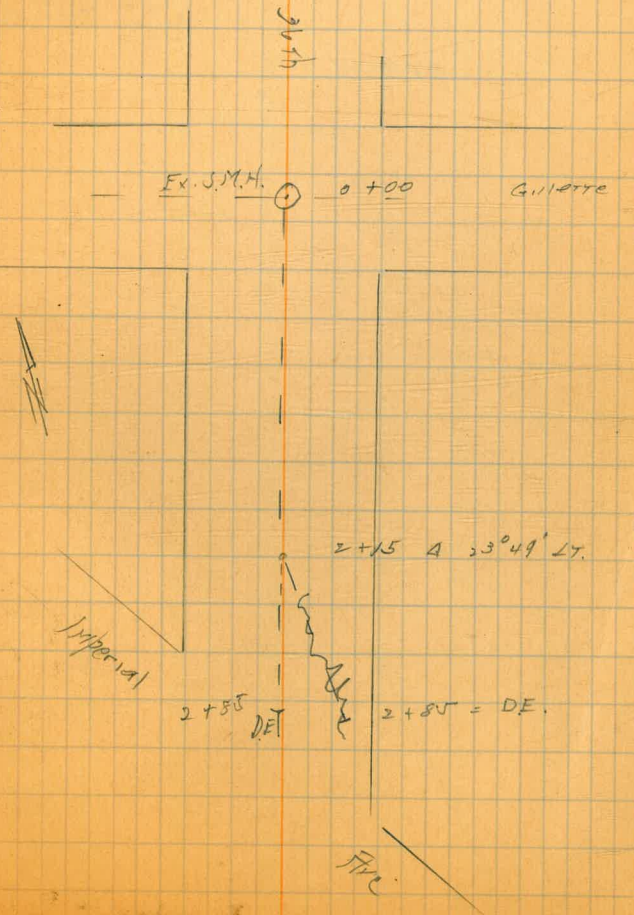
	W	E		W				
SL PENN:00	294.60	294.80	$\begin{array}{r} 300.84 \\ 0.21 \\ \hline 301.05 \\ 6.37 \\ \hline 294.68 \\ 3.05 \\ \hline 298.33 \end{array}$	$\begin{array}{r} 294.85 \\ 3.48 \\ \hline 294.41 \\ 3.91 \\ 3.61 \\ \hline +0.10 \end{array}$	$\begin{array}{r} 293.98 \\ 4.35 \\ 4.58 \\ \hline -0.33 \end{array}$	$\begin{array}{r} 293.50 \\ 4.83 \\ 4.52 \\ \hline +0.31 \end{array}$	$\begin{array}{r} 293.50 \\ 4.83 \\ 5.13 \\ \hline -0.30 \end{array}$	
0 +50	294.24	294.44		$\begin{array}{r} 295.10 \\ 3.23 \\ \hline 294.65 \\ 3.68 \\ 2.52 \\ \hline +1.14 \end{array}$	$\begin{array}{r} 294.20 \\ 4.13 \\ 2.72 \\ \hline +7.40 \end{array}$	$\begin{array}{r} 4.63 \\ 3.05 \\ \hline +1.58 \end{array}$	$\begin{array}{r} 4.63 \\ 3.03 \\ \hline +1.10 \end{array}$	
1 +54.5 N alley W	293.50	293.70		$\begin{array}{r} 293.70 \\ 4.63 \\ 2.76 \\ \hline -5.13 \end{array}$	$\begin{array}{r} 293.90 \\ 4.43 \\ 6.13 \\ \hline -1.70 \end{array}$	$\begin{array}{r} 294.10 \\ 4.33 \end{array}$	$\begin{array}{r} 5.08 \text{ red} \\ 4.28 \\ \hline 0.0 \\ \hline \text{S alley W} \end{array}$	
+74.5 SL " "	293.50	293.70		$\begin{array}{r} 293.97 \\ 4.46 \\ 2.90 \\ \hline +0.56 \end{array}$	$\begin{array}{r} 294.04 \\ 4.29 \\ 5.29 \\ \hline 0.0 \end{array}$	$\begin{array}{r} 294.20 \\ 4.13 \end{array}$		
2 +24.5	293.70	293.87						
4 +74.5	293.90	294.04						
3 +24.5 = NL Cyprus	294.10	294.20						

Moore
12-1-06

Sewer CONST. on
36th, Gillette S. 28'

	F.L.	CUTS
00 - Ex. MH ^{36th} Gillette	33.26 ✓	
+40 Sly	35.26	5.61
+80 = Brk	37.26	7.78
1 +30 = Brk	53.50	6.50
1 +80	61.50	7.75
2 +15 = A 23° 49' LT. ^{LINE} change	67.10	7.32
2 +50	72.70	10.63
2 +85 = DE.	78.30	7.34

23.26	78.30
18.53	6.54
<u>41.79</u>	84.84
0.82	2.51
41.97	<u>87.05</u> X
12.95	
64.10	
0.14	
12.27	
76.77	
0.17	
72.60	
12.30	
88.95	



Set Fire Plug
Swly Cor. Congress & Rosecrans

BMBP 4.95 9.57 4.62 San Diego Taylor

4.80 - cb grade
graderod 4.77
5.77
F 1.0

Congress

F.H.

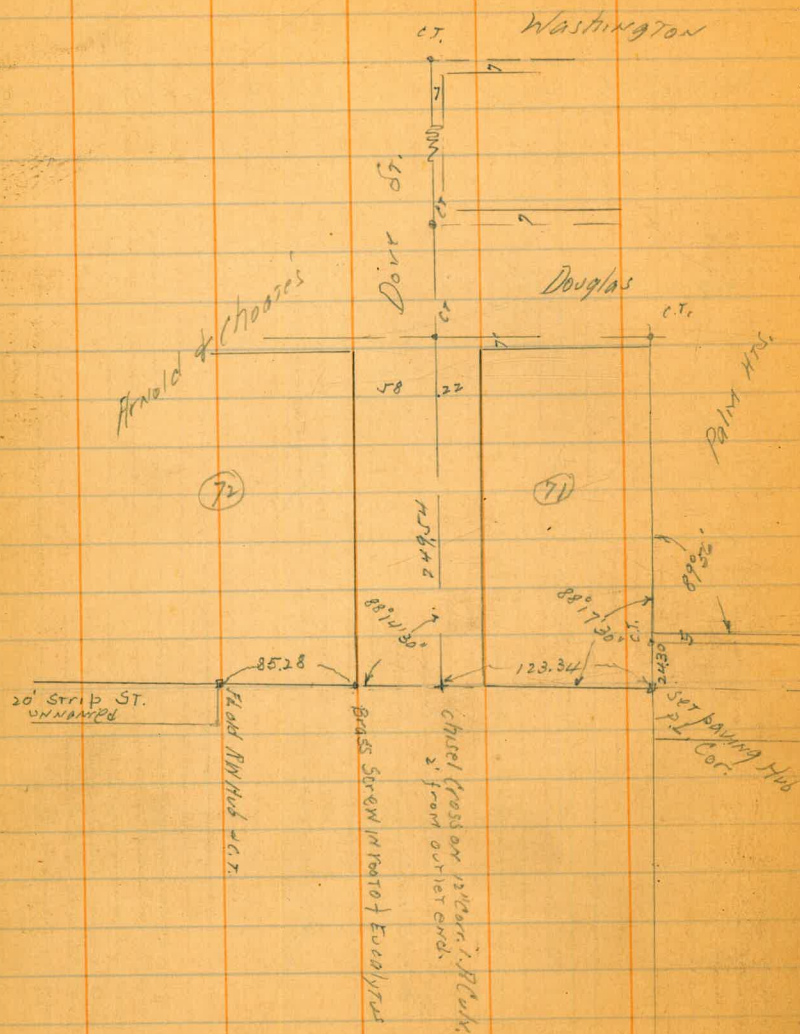
12

Rosecrans

Rosecrans 76

Tie pts. Dove St. and S.L.
of Arnold + Choates add

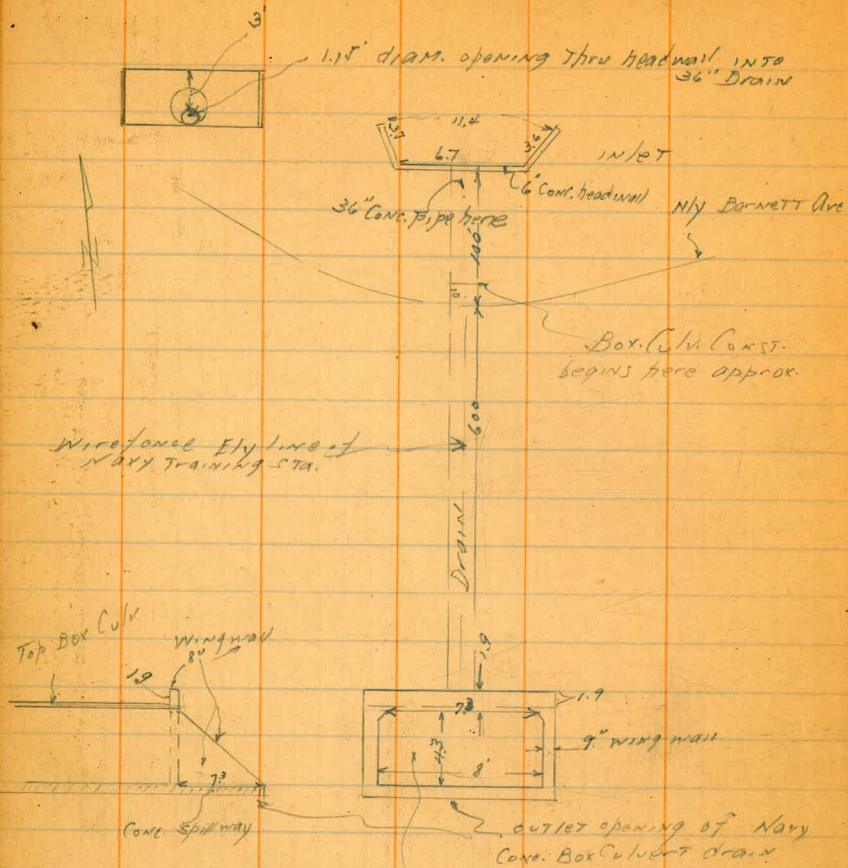
Moore
3-13-36



indexed plotted on Tie sheet
CIS:K

77

INDEXED
CISK.



2" Wood plank Gate EXISTING:
hung by 3 iron strap hinges to eye bolts
but does not function properly
at highest tide Bay water flows
IN over top of plank gate.

78

Plan for proposed Tidal Gate for
Conc. Box Drain at Ely Boundary line of
Navy Training Sta.

To Control Tidal Water Nly of
Barnett Ave

Moored 4-20-36

Address -

Lt. Com. Browne, Maintenance Officer
Navy Training Sta.
S. P. Col.

Proposed Sewer Block C O.L. Steel Sdb

BM	3.65	33.22		29.57	BP N Run 1/2 Bridge 1 1/2" per 191' E of 33rd St
TP	7.39		10.69	22.53	Top F. House Steel + 33rd St
(29.92)					
0-240	Exist MH 1/2 33rd St		9.81	20.11	0.75 Rim
			16.32	13.60	Flow Line 24" S Channel
0+0			7.81	22.11	0.75 H46
+20			1.8	28.1	
		42.56		29.50	
TP	13.06	35.17	0.42	22.11	
+44			1.5	4.11	
		52.75		41.10	
TP	11.65	45.36	1.46	30.71	
+58			4.2	48.6	
+56	0.5 R 1/2 of 1/2 Fruit Tree				
+65			1.1	51.7	
		61.57		52.72	
TP	8.85	54.18	0.03	45.33	
+93	6.5' Lt of 1/2 - 1' Fruit Tree				
+97	4' R 1/2 " - 2" Peach Tree				
1+0			7.8	53.8	
+35	34' Lt of 1/2 N 1/2 Cor.		2.7	58.9	Frame House 0.75 Floor
+46	97' Lt of 1/2 N 1/2 "		0.00	61.57	Frame House 0.75 Floor

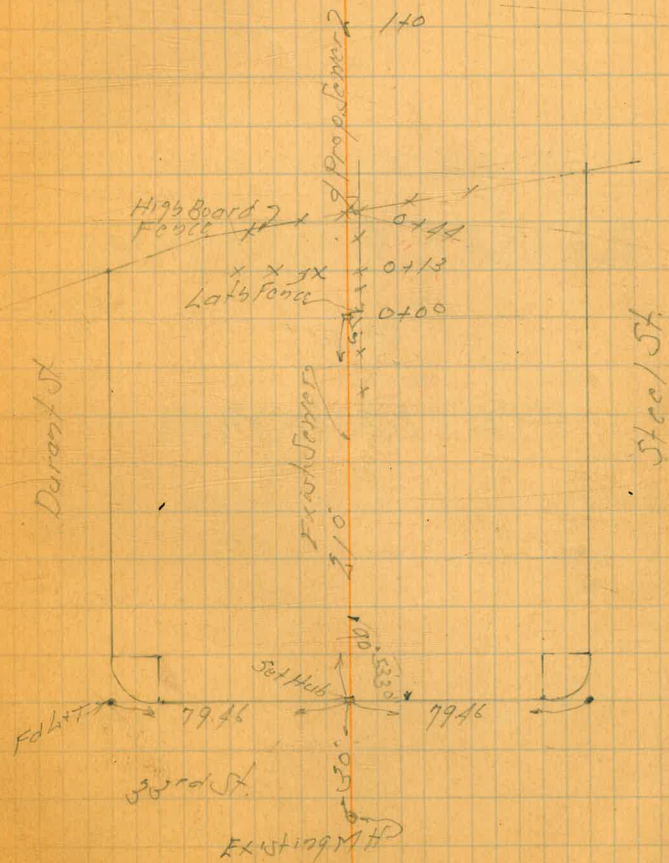
Continued FB. 1708 - P 74
Backed up to 0+80

Indexed
e.s.k.

Oct. 14-47
Sisson
McCoy
Allen
W.O. 60 189

79

See. F.B. 1708 - P. 74 + 75



Bench Levels Rosecrans St
Homer + Lythons Sts

Oct 14. 47
Sines
1700 ft X
#1100
No 25001

BM	7.06	58.56		57.50	NW BP Rosecrans & Homer
BM	0.21	48.96	9.81	48.75	NW BP Rosecrans & Homer 48.80
BM	9.34	50.97	7.33	41.63	SW BP Rosecrans & Lythons 41.76
TP	11.38	61.43	0.92	50.05	
BM			0.22	61.21	SW BP Lythons & Rosecrans 61.18

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 $\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not

IMPROVED TABLES
AND
INFORMATION

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Point of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

52.72
12.24
64.96
084
64.12

42.06

~~4.287~~
4.135