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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
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10-29-34 Relocation of Road Connecting
Miller Alabama + Upas + Powder House Canyon
Walker Road (Florida St. Extension)
Bliss

3+24 P.O.T. Hub

2+90.65 Hub. B.C. F.B. 1480 P.I. 2+90.28 Hub. 13.0.08 W. of &

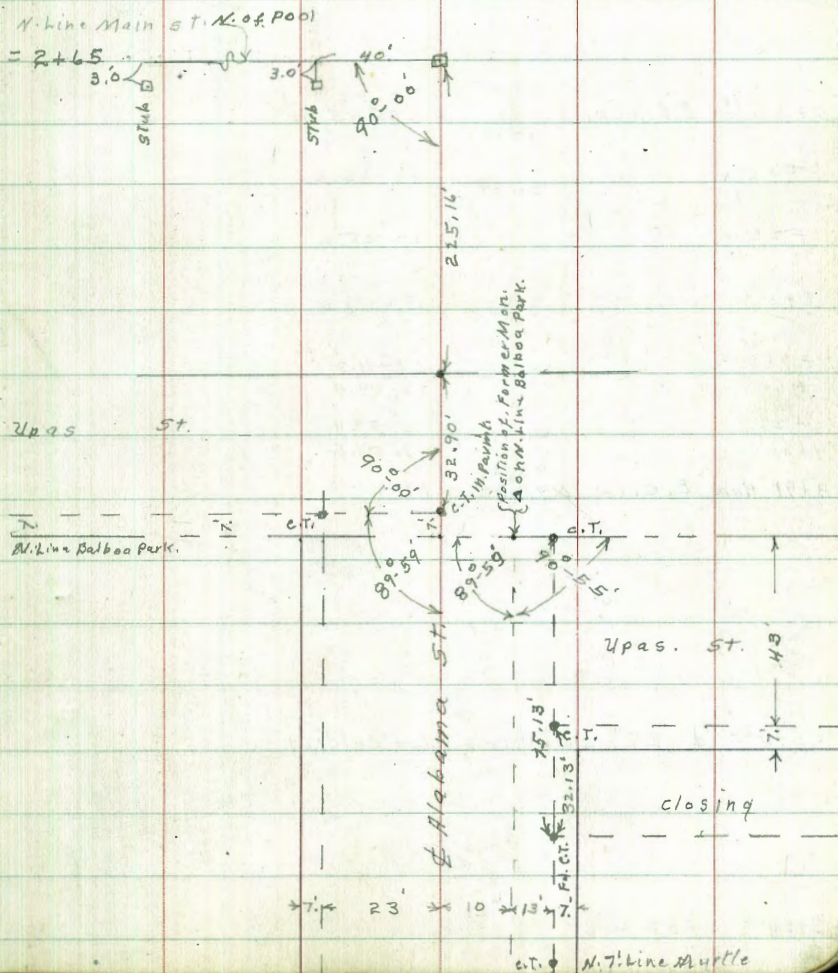
2+25.16 Hub. & B.C. Road South of Recreational Area.

0+00 Nail F.B. 1480 P.I. S Edge Ex Pav

C.T. 17. Pav. 7' S. of N. Line Upas. St.

indexed
C.S.K

1



9+20⁴⁸ E.C. Hub
 8+82⁴² E.C. Hub F.B. 1480 P. 2.
 8+75
 8+50
 8+25
 8+00
 +75
 +50
 +25
 +00
 6+67⁰⁶ B.C. Hub

chd
 20.46
 Def L:
 30-15'
 27-54'
 24-54'
 21-50'
 18-51'
 15-51'
 12-53'
 9-54'
 6-53'
 3-56'

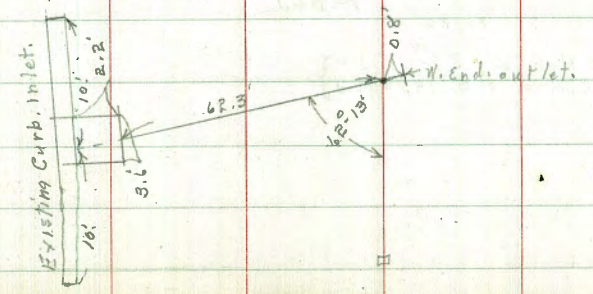
10.34
 P.I. Hub.
 $\Delta = 60-30$
 $R = 240'$
 $T = 139.96'$
 $L = 253.42'$

5+65⁷¹ E.C. Hub.
 +50
 +25
 3+00
 +75
 +50
 +25
 +00
 3+91 Hub B.C. Hub

chd
 15.70
 24.97
 27-25.2'
 22-18.3'
 17-11.3'
 12-04.4'
 6-52.4'
 1-50.5'
 $\Delta 10-30$
 Lt.
 $\Delta 71-30$
 Rt.

P.I. Hub
 $\Delta = 71-30$
 $R = 140'$
 $T = 100.79'$
 $L = 174.71'$

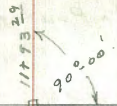
3+74²⁶ 4 22" Sheet Iron Pipe Culvert



3+24 P.O.T. Hub

14+79.30

□ Powder House Canyon Road.



	Chd	Def L
13+89 ⁵³ E.C.	14.49	53°-07.45'
+75	24.87	47°-14.4'
+50	24.87	37°-05.9'
+25	24.87	26°-57.4'
13+00	24.87	16°-48.9'
+75	16.40	6°-40.4'
12+58 ⁵⁵ B.C. Hub	∠ 106°-15'-30" RT.	

$\Delta = 106^{\circ} - 15' - 30''$
 $R = 70.62$
 $T = 94.12$
 $L = 130.97$

PJ Hub

	Chd	Def L
12+05 ¹⁴ E.C. Hub	8.13	13°-59'
12+00	24.99	13°-23.7'
+75	24.99	10°-31.8'
+50	24.99	7°-40'
+25	24.99	4°-48'
11+00	16.88	1°-56.1'
10+83 ¹¹ B.C. Hub	∠ 27°-58' LT	
= 10+55 ⁴⁵ B.C. Hub	F.B. 1480 P. 3	

$\Delta = 27^{\circ} - 58'$
 $R = 250'$
 $T = 62.26'$
 $L = 122.03'$

□ RT Hub

X Sec. Proposed Road from Upas
 & Alabama to Powder House Canyon Road.

indexed
 C.S.M.

264.88

1+50

4

BM.B.P.	5.38	264.88	259.50	N.W. Cor Upas & Alabama.	20' Lt		3.7	261.2	graded Rd
	0+00 =	{ 39.90 s. of N. line Upas. s. edge existing Pavmt.			10' "		3.8	261.1	" "
20' Rt.	Top ent. ch	4.87	260.01		¢		3.8	261.1	" "
20' "	gutter	pavmt.	5.40	259.48		10' Rt	4.0	260.9	" "
10' "	"	"	5.06	259.82		20' "	5.0	259.9	" "
¢	"	"	4.73	260.15	F.B. 1440				
								2+00	
10' Lt	"	"	4.45	260.43		20' Rt.	5.4	259.5	" "
20' "	"	"	4.07	260.81		10' "	4.6	260.3	" "
		0+50				¢	4.2	260.7	" "
20' Lt			3.7	261.2	graded Road	10' Lt	4.0	260.9	" "
10' "			3.9	261.0	" "	20' "	4.1	260.8	" "
¢			3.9	261.0	" "				
								2+50	
10' Rt			4.3	260.6	" "	20' Lt	4.6	260.3	" "
20' "			4.9	260.0	" "	10' "	4.6	260.3	" "
		1+00				¢	4.7	260.2	" "
20' Rt.			4.7	260.2	" "	10' Rt	4.9	260.0	" "
10' "			4.2	260.7	" "	20' "	5.6	259.3	" "
¢			3.8	261.1	" "	20' "	4.9	260.6	" "
10' Lt			3.7	261.2	" "				
20' "			3.5	261.4	" "				

264.88

2+75

264.88

3+60

5

20' Rt		5.0	259.9	edge Berm	20' Lt.	edge Berm	4.6	260.3	graded Rd.
10' "		5.2	259.7	graded Rd.	10' "		10.2	254.7	
ϕ		4.9	260.0	" "	ϕ		15.0	249.9	
10' Lt		4.9	260.0	" "	10' Rt		16.3	248.6	
20' "		4.7	260.2	" "	20' "		16.0	248.9	
	3+00				40' "		16.8	248.1	
20' Lt		5.0	259.9	" "		3+72			
10' "		5.0	259.9	" "	40' Rt.		18.5	246.4	
ϕ		5.1	259.8	" "	20' "		17.8	247.1	
10' Rt.		4.9	260.0	" "	10' "		17.8	247.1	
12' "	edge Berm.	5.0	259.9	" "	ϕ		16.0	248.9	
20' "		9.6	255.3		10' Lt.		11.8	253.1	
30' "		10.9	254.0		20' "		6.6	258.3	
	3+26				25' "	edge Berm.	4.6	260.3	
35' Rt		13.4	251.5		<hr/>				
20' "		12.5	252.4		Curb inlet 4.2.3' 2.0' ϕ				
16' "		10.2	254.7		Flow Line		9.84	255.04	
ϕ	edge Berm	4.8	260.1	graded Rd.	Top grating		6.39	258.49	
10' Lt		5.1	259.8	" "	" Curb.		5.53	259.35	
20' "		5.0	259.9	" "	Sta 3+24 ²⁴ 0.8' Rt. of ϕ End Culvert.		17.0	247.9	Flow Line

26488			26488				
3+77			4+06				
25' Lt.	Edge Berm	5.0	259.9	47' Lt	edge Berm	3.8	261.1
20' "		7.7	257.2	31' "		11.7	253.2
10' "		13.3	251.6	20' "		13.5	251.4
ϕ		17.0	247.9	10' "		16.1	248.8
7' Rt.		23.8	241.9	ϕ		16.9	248.0
10' "		23.9	241.0	10' Rt.		21.7	243.8
20' "		18.7	246.2	20' "		26.4	238.5
40' "		19.8	245.1	24' "		27.8	237.1
				25' "	Wash	33.0	231.9
	3491 B. C. Rt.			29' "	"	33.2	231.7
50' Rt		21.6	243.3	32' "		27.8	237.1
25' "		25.3	239.6	55' "		25.6	239.3
20' "	Wash	31.6	233.3	57' "		23.6	241.3
14' "		28.4	236.5				
5' "		18.2	246.7				
ϕ		17.0	247.9				
10' Lt		15.1	249.8	67' Rt.		27.5	237.4
20' "		13.4	251.5	52' "		32.0	232.9
34' "	edge Berm	4.5	260.4	50' "	Wash.	35.7	229.2
				39' "	"	35.0	229.9
				36' "		30.0	234.9
				20' "		21.8	243.1

264.88

4+25 (con)

10' Rt		18.4	246.5
ϕ		16.3	248.6
10' Lt		14.3	250.6
20' " "		13.3	251.6
60' "		6.0	258.9
70' "	edge of Berm	2.4	262.5

4+50

40' Lt		10.5	254.5	
30' "		12.7	252.2	
T.P.	3.64	255.85	12.71	252.17
20' Lt		5.0	250.9	
10' "		6.7	249.2	
ϕ		8.1	247.8	
10' Rt		10.0	245.9	
20' "		13.5	242.3	
52' "		25.4	230.5	
53' "	Wash.	28.0	227.9	
57' "	"	28.6	227.3	
58' "		26.5	229.4	
70' "		24.0	231.9	

255.85

4+75

43' Rt		18.2	237.6		
30' "		13.0	242.8		
20' "		11.6	244.2		
10' "		9.8	246.0		
ϕ		8.2	247.6		
10' Lt		6.7	249.1		
20' "		5.4	250.4		
30' "		3.7	252.1		
T.P.	2.64	255.08	3.45	252.40	P.I. Hub.
		5+00			
30' Lt		3.8	251.3		
20' Lt		5.3	249.8		
10' "		6.0	249.1		
ϕ		7.8	247.3		
10' Rt		9.1	246.0		
20' "		10.2	244.9		
40' "		14.5	240.6		

			255.08		
			5+25		
10	40' RT			15.4	239.7
φ	20' "			12.7	242.4
10	10' "			11.3	243.8
20	φ			10.1	245.0
60	10' LT			8.9	248.2
70	20' "			7.5	247.6
	30' "			6.5	248.6
40	T.P.	1.39	244.94	11.53	243.55
30			5+65 ⁷¹	E.C.	
T.	30' LT			1.0	243.9
20	20' "			2.0	242.9
10	10' "			3.0	241.9
φ	φ Hub.			4.09	240.85
10'	10' RT			5.1	239.8
20'	20' "			6.1	238.8
52'	40' "			8.2	236.7
53'			6+00		
57	40' RT			14.5	230.4
58	25' "			10.6	234.3
70'	20' "			9.5	235.4

			244.94		
10' RT				8.6	236.3
φ				7.6	237.3
10' LT				6.3	238.6
20' "				4.5	240.4
30' "				3.7	241.2
			6+30		
30' LT				5.6	239.3
20' "				6.8	238.1
30' "				8.0	236.9
φ				9.3	235.6
10' RT				10.7	234.2
20' "				11.7	233.2
30' "				14.8	230.1
			6+67 ²⁶ BC	4.60-30' LT	
30' RT				17.2	227.7
20' "				14.7	230.2
10' "				12.6	232.3
φ Hub				11.11	233.83
10' LT				9.5	235.4
20' "				8.5	236.4
30' "				7.7	237.2

244.94

7+00

30' Lt.	8.9	236.0
20' "	10.0	234.9
10' "	11.0	233.9
♀	12.4	232.5
10' Rt.	14.4	230.5
20' "	16.4	228.5
30' "	17.6	227.3

7+25

30' Rt.	19.9	225.0
20' "	18.2	226.7
10' "	16.0	228.9
♀	13.6	231.3
10' Lt.	12.3	232.6
20' "	11.1	233.8
30' "	10.2	234.7

7+50

30' Lt.	12.3	232.6
T.P.	0.46	232.74
20' Lt.	1.3	231.4
10' "	2.7	230.0

232.74

9

♀	4.1	228.6
10' Rt.	5.8	226.9
20' "	7.7	225.0
30' "	10.0	222.7
7+75		
30' Rt.	15.4	217.3
20' "	12.0	220.7
10' "	9.6	223.1
♀	7.1	225.6
10' Lt.	5.2	227.5
20' "	3.5	229.2
30' "	2.2	230.5

8+00

30' Lt.	6.2	226.5
20' "	7.3	225.4
10' "	9.5	223.2
♀	12.0	220.7
10' Rt.	14.3	218.4
20' "	17.5	215.2
30' "	20.1	212.6

232.74

T.P. 0.02 220.06 12.70 220.04

8+25

40' Rt 13.0 207.1

20' " 8.9 211.2

10' " 7.0 213.1

ϕ 5.2 214.9

10' Lt. 3.3 216.8

20' " 1.7 218.4

30' " 1.0 219.1

8+50

30' Lt. 9.5 210.6

20' " 10.0 210.1

10' " 10.8 209.3

ϕ 12.0 208.1

10' Rt. 13.4 206.7

20' " 14.9 205.2

40' " 18.0 202.1

220.04

10

8+75

40' Rt 22.7 197.4

20' " 19.7 200.4

10' " 18.8 201.3

ϕ 18.1 202.0

10' Lt. 18.0 202.1

20' " 17.9 202.2

40' Lt. ϕ Wash. 17.8 202.3

8+82

40' Lt 16.0 204.1

30' Lt. 17.2 202.9

20' Lt. ϕ Wash. 21.3 198.8

10' Lt. " " 22.1 198.0

ϕ " " 23.5 196.6

4' Rt. " " 23.8 196.3

10' " 20.3 199.8

20' " 20.8 199.3

40' " 24.5 195.6

220.06

9+00

40' RT		27.0	193.1
32' " W. Bank cut drainage ditch		26.0	194.1
30' " ♀	" " "	29.0	191.1
28' " E. " "	" " "	26.5	193.6
20' "		24.3	195.8
10' "		22.0	198.1
♀		20.0	200.1
10' Lt.		18.4	201.7
20' "		16.6	203.5
40' "		12.2	207.9
	9+20 ⁸⁴ E.C.		
25' Lt.		10.0	210.1
20' "		12.1	208.0
10' "		14.8	205.3
♀		18.3	201.8
10' RT		21.8	198.3
20' "		24.4	195.7
37' RT E. Bank cut drainage ditch		27.2	192.9
39' " ♀	" " "	30.2	189.9
41' " W " "	" " "	28.0	192.1

220.06

9+50

40' RT		32.0	188.1	
34' RT = W. Bank cut drainage ditch		30.7	189.4	
33' " ♀	" " "	32.7	187.4	
32' " E. Bank " "	" " "	29.2	190.9	
20' "		27.3	192.8	
10' "		24.4	195.7	
♀		20.1	200.0	
10' Lt.		17.1	203.0	
20' "		11.6	208.5	
25' "		9.5	210.6	
	9+75			
25' Lt.		15.5	204.6	
20' "		16.4	203.7	
10' "		21.5	198.6	
♀		24.9	195.2	
T.P.	0.10	207.24	12.92	207.14
T.P.	8.85	203.35	12.74	194.50
10' RT		10.6	192.8	
20' "		12.4	191.0	
28' " = E. Bank cut ditch		13.6	189.8	
29' " = d	" "	16.0	187.4	

11

203.35
9+75 (con)

30' Rt. = W Bank cut. Ditch	13.5	189.9
46' " = Top Bank P.H.C. Rd.	17.0	186.4
10+00		
H3 Rt. = Top Bank P.H.C. Rd.	18.2	185.2
27' " = W Bank cut. Ditch	16.0	187.4
26' " ϕ " " "	17.4	186.0
25' " E " " "	15.5	187.9
20' "	14.5	188.9
10' "	12.5	190.9
ϕ	11.0	192.4
10' Lt.	8.8	194.6
20' "	5.9	197.5
25' "	3.7	199.7
10+50.		
25' Lt.	7.1	196.3
20' "	9.0	194.4
10' "	11.3	192.1
ϕ	13.6	189.8
10' Rt.	15.6	187.8
22' " E Bank cut. ditch	14.9	186.5

203.35

12

18 Rt. ϕ cut. ditch	18.9	184.5
20' " W Bank " "	17.3	186.1
33' " Top Bank P.H.C. Rd.	19.3	184.1
10+83 $\frac{1}{2}$ B.C. \angle 27-58' Lt.		
27' Rt. Top Bank P.H.C. Rd.	20.7	182.7
20' "	19.7	183.7
15' " = W Bank out ditch	18.9	184.5
13' " = ϕ " "	20.0	183.4
11' " E " " "	18.2	185.2
10' "	17.9	185.5
ϕ	16.0	187.4
10' Lt.	12.6	190.8
20' "	8.1	195.3
25' "	6.0	197.4
11+00		
25' Lt.	4.8	198.6
20' "	7.0	196.4
10' "	11.5	191.9
ϕ	15.7	187.7
10' Rt = E Bank cut. ditch	18.9	184.5

203.35

11400 (con)

11' Rt	⊕	cut ditch	20.9	182.5
12' "	W Bank	" "	19.6	183.8
20' "			20.7	182.7
24' "	Top Bank	P.H.C.Rd.	20.9	182.5

T.P.	4.35	195.49	12.21	191.14
------	------	--------	-------	--------

11425

21' Rt	Top Bank	P.H.C.Rd.	13.3	182.2
11' "	W Bank	cut ditch	11.8	183.7
9.5' "	⊕	" "	13.8	181.7
8' 4"	⊕	" "	11.0	184.5
⊕			8.3	187.2
10' Lt			3.5	192.0
20' "			+1.4	196.9
25' "			+4.4	199.9

11450

25' Lt			+3.6	199.1
20' "			+1.0	196.5
10' "			4.1	191.4
⊕			8.1	187.4
16' Rt	E. Bank	cut ditch	11.4	184.1

195.49

13

11' Rt	⊕	cut Ditch	14.4	181.1
12' Rt	W Bank	" "	11.8	183.7
22' "	Top Bank	P.H.C.Rd.	14.8	180.7

11475

25' Rt	= Top Bank	P.H.C.Rd.	15.1	180.4
20' "			13.6	181.9
17' "	W Bank	cut ditch	13.1	182.4
16' "	⊕	" "	15.4	180.1
15' "	E. Bank	" "	12.4	183.1
10' "			11.2	184.3
⊕			8.0	187.5
10' Lt			4.0	191.5
20' "			0.2	195.3
25' "			+2.3	197.8

11490

25' Lt			+0.9	196.4
20' "			1.6	193.9
10' "			5.3	190.2
⊕			8.6	186.9
10' Rt			11.3	184.2

195.49

185.59

14

11+90 (con)

18' Rt. = E. Bank cut. ditch 13.6 181.9

19' " = ϕ " " 16.2 179.3

20' " = W " " " 14.1 181.4

29' " = Top. Bank P.H.C. Rd. 16.7 178.8

12+05¹⁴ E.C.

33' Rt. = Edge P.H.C. Rd 18.6 176.9

25' " = W. Bank cut. Ditch 16.7 178.8

24' " = ϕ " " 17.7 177.823' " = ϕ " " 16.2 179.3

20' " " " 15.3 180.2

10' " " " 13.0 182.5

 ϕ Hub 10.22 185.27

10' Lt. 6.4 189.1

20' " 2.5 193.0

25' " 0.6 194.9

12+15 = S. End. cut. Drainage Ditch

12+25

25' Lt. 5.8 189.7

20' " 6.4 189.1

10' " 9.2 186.3

T.P. 1.00 185.59 10.90 184.59

 ϕ

3.3 182.3

10' Rt

6.3 179.3

20' "

8.7 176.9

36' "

11.8 173.8

40' " Berm P.H.C. Rd.

9.5 176.1

43' " gutter " " " "

10.2 175.4

12+58⁵⁵ B.C. Δ 106⁰ - 15' 30" Rt.70.62 Rt ϕ P.H.C. Rd 10.8 174.8

53' Rt. E gutter. P.H.C. Rd. 11.0 174.6

50' " E. Berm " " " " 10.2 175.4

43' " " " " " 13.3 172.3

20' " " " " " 11.6 174.0

10' " " " " " 10.3 175.3

 ϕ " " " " " 9.07 176.52

10' Lt. 6.9 178.7

20' " 4.4 181.2

25' " 2.7 182.9

185.59

12+75

30' Lt.		5.6	180.0
20' "		8.7	176.9
10' "		10.5	175.1
⊕		10.7	174.9
10' Rt		11.5	174.1
20' "		12.5	173.1
44 "		13.5	172.1
51' " E. Berm P.H.C. Rd.		10.2	175.4
53' " E. Guller P.H.C. Rd.		11.3	174.3
	13+00		
42' Rt		13.8	171.8
20' "		13.5	172.1
10' "		13.4	172.2
⊕		13.0	172.6
10' Lt.		12.9	172.7
20' "		12.4	173.2
30' "		11.8	173.8
	13+25		
30' Lt		14.5	171.1
20' "		15.0	170.6

185.59

15

10' Lt		15.0	170.6
⊕		15.0	170.6
10' Rt		15.0	170.6
20' "		14.9	170.7
36' "		14.8	170.8
	13.50		
20' Rt.		15.2	170.4
10' "		15.2	170.4
⊕		14.6	171.0
10' Lt.		14.6	171.0
20' "		17.4	168.2
40' "		17.5	168.1
	13+61		
50 Lt.		15.6	170.0
25' "		14.8	170.8
20' "		17.7	167.9
10' "		14.5	169.1
⊕		16.0	169.6
10' Lt.		13.1	172.5
20' " E. Berm P.H.C. Rd.		10.7	174.9

185.59

13+69.

20' Rt.	in P.H.C. Rd.	11.5	174.1
10'	" gutter area "	12.5	173.1
±	E Berm " " "	11.5	174.1
10' Lt.		13.2	172.4
20' "	Toe slope	14.4	171.2
50' "		15.4	170.2

15+75.

50' Lt.	Toe slope	15.0	170.6
29' Lt	Berm P.H.C. Rd	11.5	174.1
20' "		11.5	174.1
10' "		12.9	172.7
±		12.0	173.6

13+89⁵² E.C. = ± P.H.C. Rd.

±		11.9	173.7
50' Lt	± P.H.C. Rd	12.7	172.9
100' "	" " " "	13.8	171.8
# B.M. 2		6.97	178.62

R.B. 1480P4

= 178.60

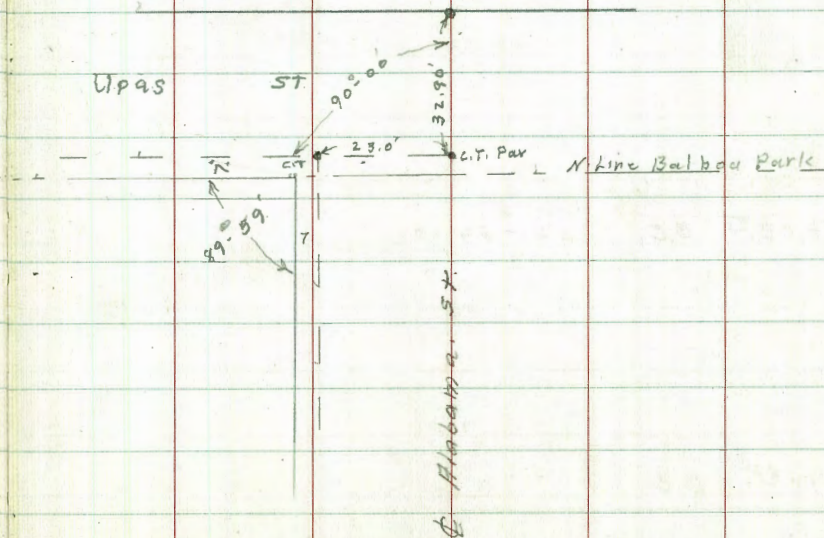
11-2-34 "B" Alternate Line
 Miller
 Walker
 Bliss.
 From Alabama + Upas to P.H.C. Rd.

Indexed
 C.S.K.

Station	Deflection	Chord
4+78.45 E.C.	26°-28'	14.44
4+00		24.423
+50		19-55.8'
3+00		15-09.3'
+50		10-22.8'
2+00	49.95°	5-36.3'
	58.65	
1+41.22	B.C. \angle 52° 56' AT	

$\Delta = 52^{\circ} 56'$
 $R = 300.00'$
 $T = 149.36'$
 $L = 277.16'$

0+00 Nail. E.B. 1480 S. edge Ex. Pav



7+95⁶⁶ E.C.

$$\begin{aligned} \Delta &= 41-54 \\ R &= 400' \\ T &= 153.14 \\ L &= 292.52 \end{aligned}$$

□ P.J. Hub

5+03.92 B.C. $\angle 41-54$ lt.

418⁴⁵ E.C.

7-5-34
 Miller
 Walker
 1920

C Alternate Lim.
 From Alabama & Upas. to P. H. C. R.R.
 Thence to Upas. & Park Blvd.
 Following Alignment F.B. 1291 P 40.

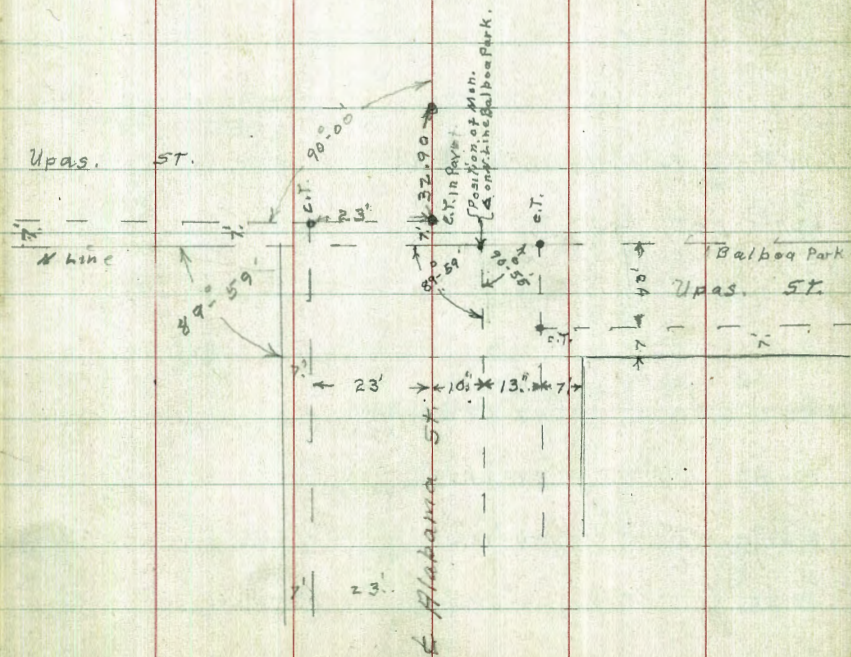
Indexed
 C.S.K.

19

	Def L	chd
4+18 ⁴⁵	26-28	37.52
4+00	24-42.3	18.44
+50	19-55.5	49.95
3+00	15-09.3	49.95
+50	10-22.8	49.95
2+00	5-36.3	49.95
1+41.79 BC		58.65

$\Delta = 87^{\circ} 36' 24''$
 $R = 300'.00$
 $L = 458.71'$
 $T = 287.72'$
 Def 5.729 per %

2000 West S. Edge Existing Pavmt. F.B. 1480.



	Def L	Ent
10+58.6 EC	10-52	
10+25	8-58	31.14
10+00	7-32	24.99

+75	6-06.2	
+50	4-40.2	
+25	3-14.3	24.99
9+00	1-48.3	31.49

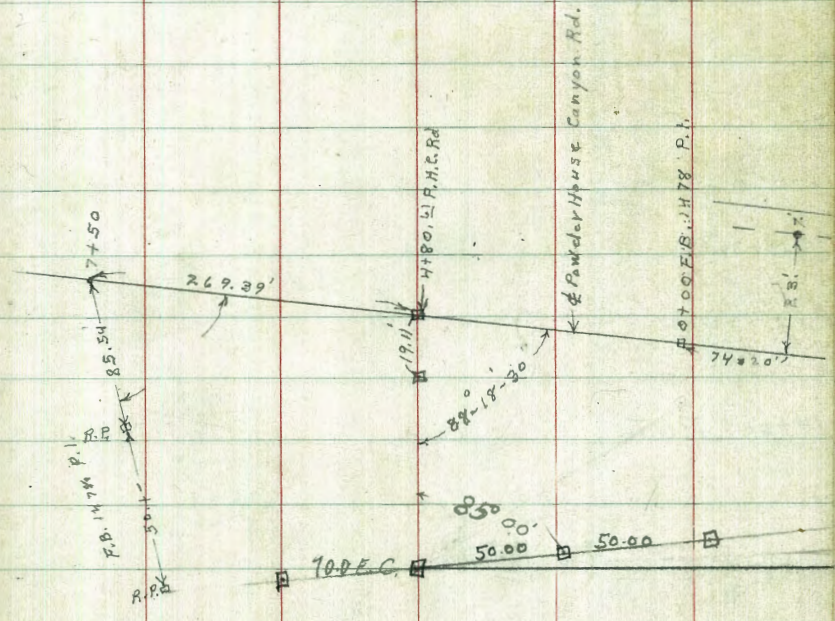
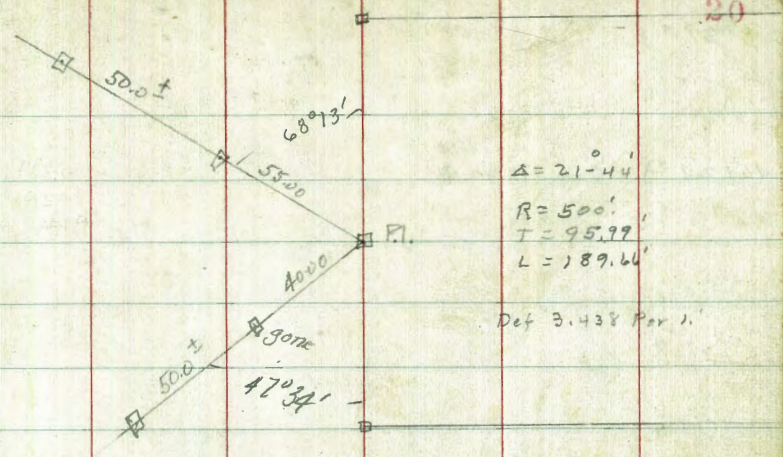
8+68.50
 95.99
964.49
 8+68.63
 95.86

8+68.50 B.C. \angle 21-44 Rt

7+48.28 P.I. Powder House Canyon Rd.

7+29.67 P.O.T.

	Def L	Ent
6+00 E.C.	42-48.2	49.95
+50	39-01.7	49.95
5+00	34-15.2	49.95 ✓
4+50	29-28.7	31.52 ✓

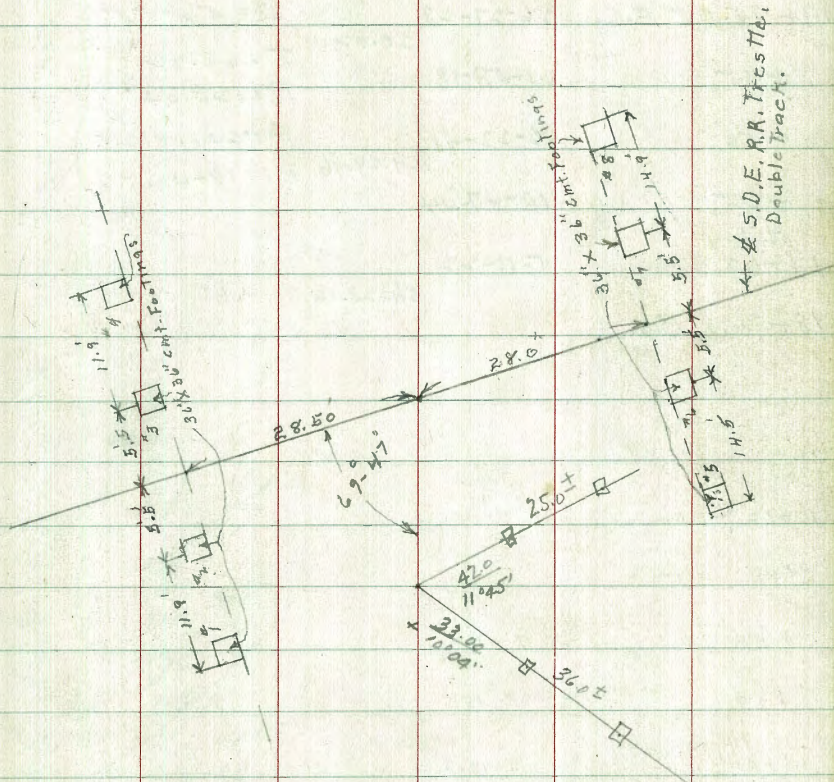


16+24⁵³ B.C. \angle 77° 00' P.I.

15+36.84

14+00 P.O.T.

10+58¹⁴ E.C.



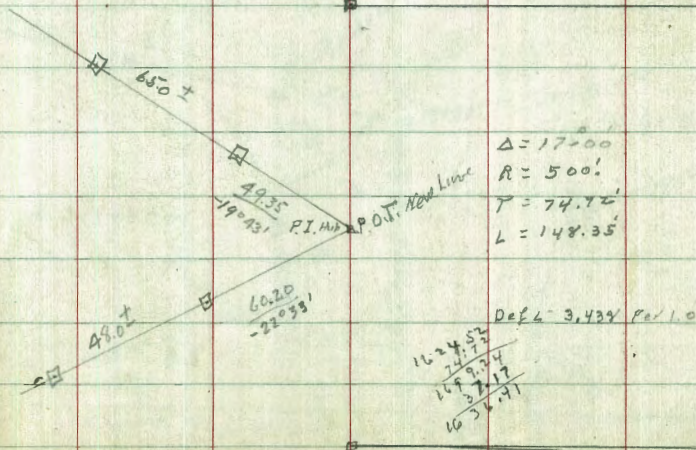
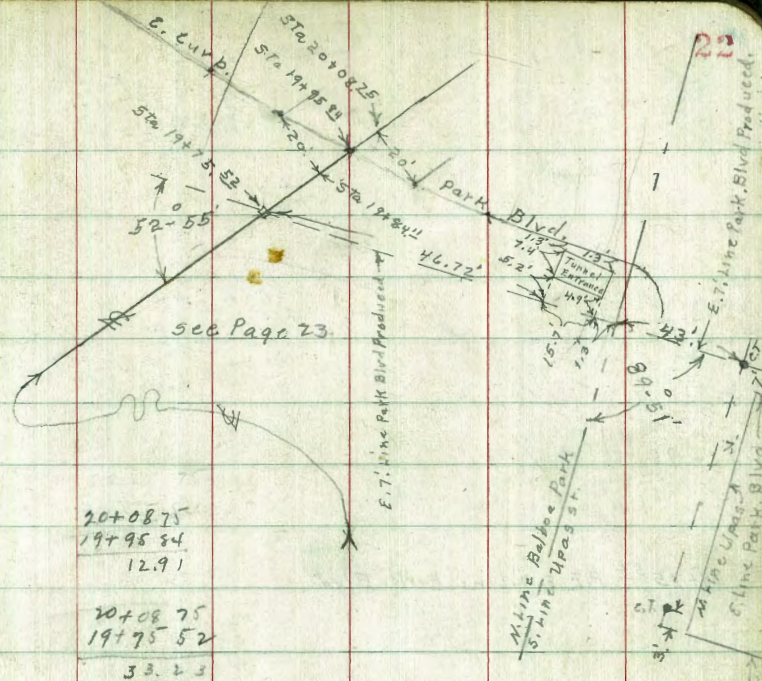
20+04.75 P.I. Line 20' Rt. + E. cl. Park Blvd
 19+95.84 P.I. of + E. cl. Park Blvd
 19+84.11 " " Line 20' Lt. + E. cl. Park Blvd
 19+75.52 P.I. of + E. Line Park Blvd.

19+95.05 E.C.	26-27-28	$\Delta = 52-55$
+75	21-58-18	$T = 63.72$
+50	16-22-41	$R = 128.04$
+25	10-47-04	$ARC = 118.25$
19+00	5-11-22	$PI = 19+40.52$
18+76.8 B.C.		Partridge

ch=24.96
 ch=23.16

Note: For New
 Park Blvd Connection
 See Book 1520 Pages 49-50
 See Book 1520 Pages 54
 " E. Line

17+72.57 E.C.	Def L 8'-30"
+50	7'-11.4"
+25	5'-45.5"
17+00	4'-19.5"
+75	2'-53.6"
16+50	1'-27.6"
16+24.5 B.C.	$\angle 17^{\circ} 00'$ RT.

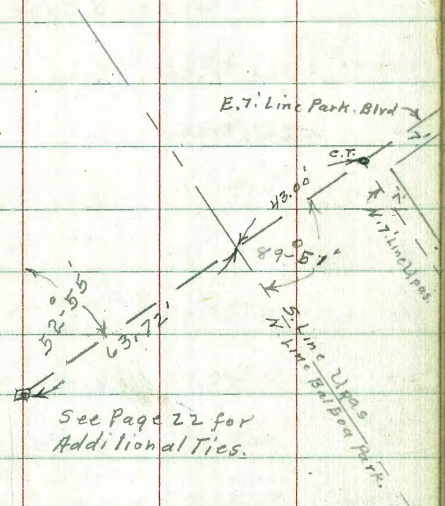


90-1430

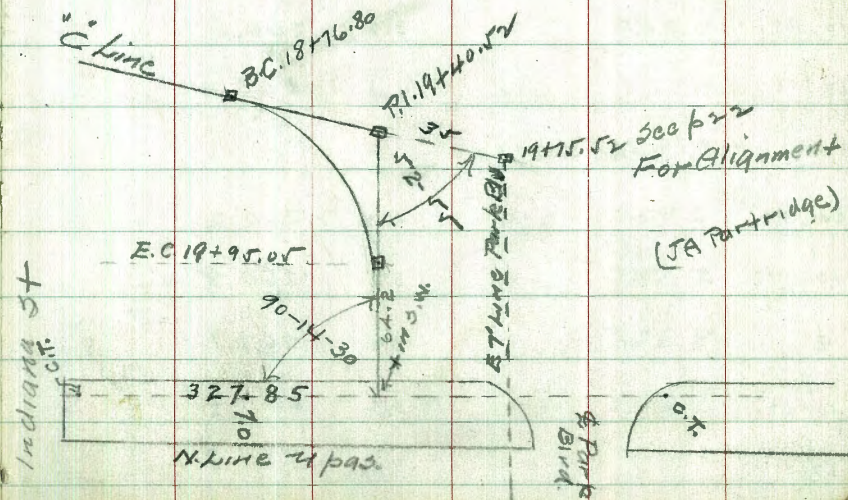
19+95.84

19+75.52 P.I. E. 7th Line Park Blvd.

17+72.87 E.C.



Layout "C" Line Running into Upas.



X see "C" Line Road.
from Upas + Alabama to Upas + Park Blvd.

INDEXED
E.S.M.

264.35

24

BM, R.P.	H. 85	264.35	259.50	N.W. Upas + Alabama	20' Lt.	graded Road	1 + 41 29 B.C. 287 - 36-24" Rt.	3.3	261.1
	0+00 = S. Edge Existing Pavmt				10' "	"	"	3.3	261.1
20' Rt. S. End. Ex. Ck.		4.34	260.01		±	"	"	3.3	261.1
20' " S. End. Ex Pav		4.87	259.48		10' Rt.	"	"	3.5	260.9
10' " " " " "		4.53	259.82		20' "	"	"	4.4	260.0
± " " " "		4.20	260.15				2+00		
10' Lt. " " " "		3.92	260.43		20' Rt.	"	"	5.4	259.0
20' " " " "		3.54	260.81		10' "	"	"	4.5	259.9
	0+50				±	"	"	3.8	260.6
20' Lt. graded Road		3.2	261.2		10' Lt.	"	"	3.7	260.7
10' " " "		3.4	261.0		20' "	"	"	3.5	260.9
± " " "		3.4	261.0				2+50		
10' Rt. " "		3.8	260.6		20' Lt.	"	"	4.3	260.1
20' " " "		4.4	260.0		10' "	"	"	4.4	260.0
	1+00				±	"	"	5.1	259.3
20' Rt. " "		4.2	260.2		10' Rt.	Berm	"	4.8	259.6
10' " " "		3.6	260.8		13' "	"	"	7.2	257.2
± " " "		3.3	261.1		20' "	"	"	7.6	256.8
10' Lt. " "		3.2	261.2		30' "	"	"	8.3	256.1
20' " " "		3.1	261.3						

264.35

2+64

30' RT	8.7	255.7
20' "	8.2	256.2
10' "	7.7	256.7
6 "	7.2	257.2

4' Berm.	4.6	259.7
20' Lt graded Road	4.8	259.5
20' " " "	4.6	259.7

2+73

20' Lt	"	"	4.6	259.7
10' "	"	"	4.6	259.7
"	Berm		4.8	259.5
4'			8.0	256.3

10' RT	8.4	255.9
20' "	9.0	255.3
30' "	9.3	255.0

3+00

30' RT	10.7	253.6
26' "	10.5	253.8
10' "	10.3	254.0
4'	10.2	254.1

264.35

25

10' Lt	9.9	254.4
20' "	9.4	254.9
33' " Berm	4.5	259.8
F.P.	2.86	254.30
	12.91	251.44

3+50

30' Lt	5.0	249.3
20' "	4.9	249.4
10' "	4.8	249.5

4'	4.6	249.7
10' RT	4.4	249.9
20' "	4.5	249.8
30' "	4.3	250.0

4+00

30' RT	10.0	244.3
20' "	10.0	244.3
10' "	10.0	244.3

4'	9.7	244.6
10' Lt	10.0	244.3
20' "	10.3	244.0
30' "	10.0	244.3

254.30
4+20

242.58

26

30' Lt			15.5	238.8	±			11.7	230.9
20' "			13.8	240.5	10' Rt.			10.2	232.4
10' "			13.0	241.3	20' "			9.0	233.6
±			13.1	241.2	30' "			8.3	234.3
10' Rt.			12.7	241.6	T.P.	0.15	229.67	13.06	229.52
20' "			12.4	241.9			5+50		
30' "			11.9	242.4	40' Rt			3.9	225.8
T.P.	0.92	242.58	12.24	241.66	20' "			3.6	226.1
		4+50			10' "			4.0	225.7
30' Rt.			3.8	238.8	±			6.2	223.5
20' "			3.9	238.7	10' Lt.			8.1	221.6
10' "			4.5	238.1	20' "			10.2	219.5
±			5.9	236.7	30' "			12.8	216.9
10' Lt.			5.7	232.9	T.P.	0.27	217.20	12.74	216.93
20' "			7.2	235.4			6+00 E.C.		
30' "			10.7	231.9	30' Lt.			11.9	205.3
		5+00			20' "			8.4	208.4
30' Lt			17.9	224.7	20' "			7.3	209.9
20' "			15.5	227.1	10' "			6.2	211.0
10' "			13.1	229.5	± Hüb.			5.82	211.38

217.20
6+00 E.C. (con.)

205.22

27

10' RT		5.1	212.1
20' "		4.7	212.5
30' "		5.0	212.2
	6+25		
30' RT		9.1	208.1
20' "		9.2	208.0
10' "		9.5	207.7
⊕		9.8	207.4
10' LT		10.0	207.2
20' "		10.9	206.3
30' "		12.7	204.5
T.P.	0.37	205.22	12.35
	6+50		
30' Lt.		3.8	201.4
20' "		3.6	201.6
10' "		3.2	202.0
⊕		2.6	202.6
10' RT		2.8	202.4
20' "		2.6	202.6
30' "		2.5	202.7

30' RT		8.5	196.7
20' "		8.4	196.8
10' "		8.5	196.7
⊕		8.5	196.7
10' Lt.		8.3	196.9
20' "		8.5	196.7
30' "		8.2	197.0
	6+96		
30' Lt.		10.5	194.7
20' "		11.5	193.7
10' "		12.0	193.2
⊕		12.8	192.4
10' RT		12.0	193.2
20' "		11.0	194.2
30' "		10.5	194.7
T.P.	0.70	192.94	12.98
	7+10		
30' RT		5.6	187.3
20' "		5.8	187.1
10' "		5.8	187.1

192.94

7+10 (con.)

ϕ	5.9	187.0
10' Lt	5.9	187.0
20' "	5.6	187.0
30' "	4.8	188.1

7+30 { at. 2 of 88'-18"-30" from ϕ } E. Berm
Parallel to P.H.C. Rd P.H.C. Rd

50' Lt	6.2	186.7
20' "	4.0	186.9
10' "	5.6	187.3
ϕ	5.4	187.5
10' Rt	5.1	187.8
20' Rt.	4.9	188.0
50' "	4.4	188.5

7+32 = E. Gutter P.H.C. Rd.

50' Rt	5.6	187.3
20' "	6.3	186.6
10' "	6.5	186.4
ϕ	6.7	186.2
10' Lt	6.9	186.0
20' "	7.1	185.8
50' "	7.5	185.4

192.94

7+34 = E. edge P.H.C. Rd.

50' Lt.	6.9	186.0
20' "	6.5	186.4
10' "	6.3	186.6
ϕ	6.2	186.7
10' Rt	6.0	186.9
20' "	5.8	187.1
50' "	5.2	187.7

7+48²⁴ ϕ P.H.C. Rd.

100' Rt	3.8	189.1
50' "	4.8	188.1
20' "	5.5	187.4
10' "	5.7	187.2
ϕ	5.9	187.0
10' Lt	6.2	186.7
20' "	6.4	186.5
50' "	6.9	186.0
100' "	7.7	185.2

28

19294
7+64 = W. gutter P.H.C. Rd

50' Lt	7.0	185.9
20' "	6.6	186.3
10' "	6.4	186.5
¢	6.3	186.6
10' Rt	6.0	186.9
20' "	5.8	187.1
50' "	5.1	187.8

7+67 = W. Berm P.H.C. Rd, Sec. Parallel to P.H.C. Rd.

50' Rt.	4.3	188.6
20' "	4.9	188.0
10' "	5.1	187.8
¢	5.3	187.6
10' Lt	5.5	187.4
20' "	5.8	187.1
50' "	6.0	186.9

7+72

50' Lt.	8.7	184.2
30' "	7.3	183.6
20' "	9.5	183.4
10' "	9.2	183.7

192.94

¢	8.9	184.0
10' Rt	9.2	183.7
20' "	8.8	184.7
30' "	8.5	184.4
50' "	8.2	184.7
30' Rt	8.1	184.8

8+00

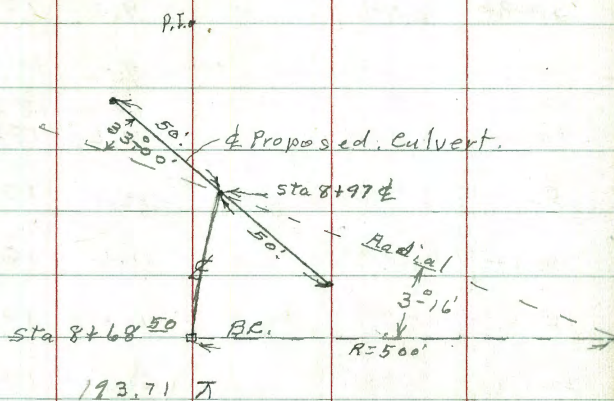
20' "	8.1	184.8
10' "	8.3	184.6
¢	8.3	184.6
10' Lt	8.5	184.4
20' "	8.7	184.2
30' "	9.3	183.6

8+50

30' Lt	9.2	183.7
20' "	8.8	184.1
10' "	9.0	183.9
¢	8.4	184.5
10' Rt.	8.1	184.8
20' "	8.0	184.9
30' "	7.4	185.5

29

culvert. location



culvert. Profile & Wash

		192.94		
T.P.	10.07	193.71	9.30	183.64
		8+68 ⁵⁰	B.C. L 21	44 Rt.
30' Rt			8.9	184.8
20' "			8.9	184.8
10' "			8.9	184.8
¢ Hub			9.38	184.33
10' Lt			9.2	184.5
20' "			9.7	184.0
30' "			10.1	183.6
		8+87		
30' Lt			9.8	183.9
20' "			9.3	184.4
10' "			9.0	184.7
¢			9.0	184.7
10' Rt.			9.8	183.9
17' "	10 wash		11.4	182.3
20' "	" "		11.4	182.3
27' "	" "		11.2	182.5
30' "			9.8	183.9

40' Rt.	Wash 7' wide	11.3	182.4
20' "	" 7' "	11.5	182.2
¢	at. sta 8+97 Wash 10' wide	12.0	181.7
20' Lt.	Wash 10' wide	12.0	181.7
40' Lt.	" 9' "	12.4	181.3

193.71

9+00

30' Rt		9.1	184.6
20' "		9.2	184.5
12' "		10.2	183.5
60' "	in wash	11.6	182.1
ϕ	" "	12.1	181.6
10' Lt	" "	11.6	182.1
18' "	" "	11.5	182.2
20' "		9.6	184.1
30' "		9.6	184.1
		9+10	
30' Lt	in wash	11.8	181.9
20' "	" "	11.9	181.8
10' "	" "	11.9	181.8
7' "	" "	11.9	181.8
5' "		10.3	183.4
ϕ		9.8	183.9
10' Rt		9.3	184.4
20' "		9.2	184.5
30' "		9.3	184.4

193.71

9+25

30' Rt		9.0	184.7	
20' "		9.4	184.3	
10' "		9.5	184.2	
ϕ		9.2	184.5	
10' Lt		9.0	184.7	
20' "		8.8	184.9	
30' "		8.6	185.1	
		9+50		
25' Lt		6.5	187.2	
22' "		5.0	188.7	
20' "		5.0	188.7	
10' "		3.8	189.9	
ϕ		3.5	190.2	
10' Rt		4.3	189.4	
20' "		4.5	189.2	
30'		6.1	187.6	
T.P.	12.07	204.99	0.79	192.92

31

204.99

9+75

30' Rt.	13.0	192.0
20' "	12.5	192.5
10' "	12.0	193.0
⊕	11.7	193.3
10' Lt	11.9	193.1
20' "	12.6	192.4
27' "	14.5	190.5
30' " Wash	16.7	188.3

10+00

30' Lt	10.4	194.6
20' "	9.0	196.0
10' "	8.4	196.6
⊕	8.7	196.3
10' Rt	9.8	195.2
20' "	10.8	194.2
30' "	11.5	193.5

10+25

30' Rt	6.9	196.1
20' "	5.0	200.0
10' "	4.6	200.4

204.99

32

⊕	4.5	200.5
10' Lt	5.5	199.5
20' "	6.6	198.4
30' "	8.4	196.6

10+58¹⁶ F.C.

30' Lt	4.9	200.1
20' "	3.2	201.8
10' "	1.9	203.1

⊕ Hub T.P. 13.28 217.19 1.08 203.91

10' Rt	11.7	205.5
20' "	11.1	206.1
30' "	9.6	207.6

11+00

30' Rt	4.0	213.2
20' "	5.2	212.0
10' "	7.1	210.1

⊕

10' Lt	9.2	208.0
10' Lt	11.4	205.8
20' "	13.4	203.8
30' "	16.5	200.7

217.19

11+50

40' Lt			13.2	204.0
30' "			12.4	204.8
20' "			9.5	207.7
10' "			7.4	209.8
⊕			5.1	212.1
10' Rt			3.0	214.0
20' "			0.5	216.7
T.P.	12.41	229.01	0.59	216.60
30' Rt			9.9	219.1
		12+00		
30' "			6.4	222.6
20' "			9.7	219.3
10' "			12.0	217.0
⊕			14.4	214.6
10' Lt			16.9	212.1
20' "			19.2	209.8
35' "			20.7	208.3
		12+55		
35' Lt			17.0	212.0
20' Lt			12.8	216.2

229.01

33

10' Lt			9.2	219.8
⊕			5.6	223.4
10' Rt			1.7	227.3
T.P.	12.74	241.18	0.57	228.44
20' Rt			10.3	230.9
30' "			6.8	234.4
		13+15		
30' Rt			+3.2	244.4
20' "			0.7	240.5
10' "			6.3	234.9
⊕			10.9	230.3
10' Lt			15.4	225.8
20' "			19.6	221.6
30' "			21.2	220.0
40' "			23.6	217.6
		13+50		
40' Lt			20.1	221.1
30' "			18.7	222.5
20' "			16.5	224.7
10' "			11.9	229.3

		241.18				252.67		
♀		13+50 (cow)	6.3	234.9	30' Rt		+7.0	259.7
10' Rt			1.0	240.2		14+50		
20' "			+5.0	246.2	30' Rt		+7.0	259.7
30' "			+11.0	252.2	20' "		+2.7	255.4
T.P.	12.09	252.67	0.60	240.58	10' "		1.5	251.2
		13+90			♀		7.0	245.7
30' Rt			+5.2	257.9	10' Lt.		11.0	241.7
20' "			+2.1	254.8	20' "		15.6	237.1
10' "			1.8	250.9	45' "		22.5	230.2
♀			7.0	245.7		15+00		
10' Lt			11.6	241.1	47' Lt		22.5	230.2
20' "			17.6	235.1	20' "		13.1	239.6
45' "			28.7	224.0	10' "		10.2	242.5
		14+15			♀		5.8	246.9
45' Lt.			26.1	226.6	10' Rt		1.6	251.1
20' "			16.6	236.1	20' "		+2.0	254.7
10' "			11.8	240.9	30' "		+5.3	259.0
♀			6.0	246.7				
10' Rt.			0.4	252.3				
20' "			+4.0	256.7				

		252.67			264.09			
		Cmt. Footings of S.D.E.R.R. Bridge S. of ϕ See Plat Page 21				15+50		
Footing #1	E. side Bridge	13.26	239.41	30' Rt.		2.7	261.4	
"	" 1 ground.	13.8	238.9	20' "		6.2	257.9	
"	" 2 Top.	13.30	239.37	10' "		10.9	253.2	
"	" 2 ground	14.0	238.7	ϕ		14.3	249.8	
"	" 3 Top.	13.30	239.37	10' Lt.		18.5	245.6	
"	" 3 ground.	14.7	238.0	20' "		22.1	242.0	
"	" 4 Top. W. side Bridge	13.30	239.37	42' "		28.0	236.1	
"	" 4 ground	14.8	237.9		15+85			
		Cmt. Footings S.D.E.R.R. Bridge N. of ϕ			40' Lt		26.0	238.1
T.P.	13.09	264.09	1.67	251.00	20' "	19.5	244.6	
Footing #5	E. side Bridge	0.65	263.44	10' "		17.6	246.5	
"	" 5 ground.	2.2	261.9	ϕ		14.6	249.5	
"	" 6 Top.	0.65	263.44	10' Rt		10.5	253.6	
"	" 6 ground.	3.2	260.9	20' "		7.6	256.5	
"	" 7 Top.	2.64	261.45	30' "		4.1	266.0	
"	" 7 ground	4.3	259.8		15+95			
"	" 8 Top W. side Bridge	2.64	261.45	30' Rt		3.4	260.7	
"	" 8 ground	5.3	258.8	20' "		6.6	257.5	
				10' "		10.5	253.6	
				ϕ		15.1	249.0	

244.09

15+95

10' Lt 17.6 246.5

20' " 19.0 245.1

30' " 26.6 237.5

40' " 25.3 238.8

16+02

40 Lt 23.3 240.8

30' " 21.3 242.8

20' " 24.0 240.1

10' " 21.8 242.3

♀ 17.8 246.3

10' Rt 11.3 252.8

20' " 7.3 256.8

30' " 3.7 260.4

16+10

30' Rt 4.7 259.4

20' " 7.7 256.4

10' " 10.5 253.6

♀ 13.3 250.8

10' Lt 15.8 248.3

20' " 17.0 247.1

40' " 21.2 242.9

244.09

See Book 1520 P 54

36

16+24 ⁵² B.C. \angle 17°00' Rt.

9.98 254.11

♀ Hub

16+50

40' Lt 15.8 248.3

20' " 9.5 254.6

10' Lt 6.8 257.3

♀ 3.9 260.2

10' Rt 0.5 263.6

20' " 72.4 266.5

30' " 74.3 268.4

T.P. 12.44 276.43 0.14 263.95

16+80

30' Rt 76.2 282.6

20' " 72.6 279.0

10' " 1.8 274.6

♀ 7.1 269.3

10' Lt 11.6 264.8

20' " 16.4 260.0

45' " 25.0 251.4

See AB 1663 P 1

276.43

17+05

45' Lt	22.3	254.1
20' "	12.4	264.0
10' "	8.4	268.0
☒	3.4	273.0

10' Rt	+1.3	277.7
20' "	+6.3	282.7
30' "	+9.6	286.0

17+50

30' Rt	+9.4	285.8
20' "	+5.3	281.7
10' "	+0.6	277.0
☒	3.4	273.0

10' Lt	7.6	268.8
20' "	11.8	264.6
45' "	19.0	257.4

17+72⁸⁷ E.C.

45' Lt	18.0	258.4
20' "	8.8	267.6
10' "	4.8	271.6

☒ Hub T.P.	13.38	288.71	1.10	275.33
------------	-------	--------	------	--------

288.71

10' Rt	8.5	280.2
20' "	4.2	284.5
30' "	+0.5	289.2

18+00

30' Rt	+2.8	291.5
20' "	+0.9	289.6
10' "	3.1	285.6

☒	7.7	281.0
---	-----	-------

10' Lt	13.0	275.7
20' "	17.6	271.1
31' Lt	22.2	266.5
40' "	31.6	254.1
60' "	33.3	255.4

18+25

50' Lt	23.6	265.1
40' "	28.2	260.5
25' "	26.5	262.2
20' "	22.3	266.4
10' "	15.7	273.0

☒	9.1	279.6
---	-----	-------

288.71

18+25 (both)

10' RT	2.7	286.0
20' "	+1.4	290.1
40' "	+3.8	292.5

18+63

40' RT	+5.0	293.7
25' "	+4.5	293.2
20' "	+3.0	291.7
10' "	7.0	281.7
⊕	13.3	275.4
10' LT	17.0	271.7
20' "	19.5	269.2
27' "	19.0	269.7
40' "	10.8	277.9

18+80

40' LT	4.5	284.2
30' "	9.7	279.0
20' "	12.8	275.9
10' "	11.1	277.6
⊕	5.0	283.7
T.P.	9.75	297.66
	0.80	287.91

297.66

10' RT	7.9	289.8
20' "	3.9	293.8
40' "	3.6	294.1

17+00

40' RT	3.5	294.2
20' "	3.8	293.9
10' "	4.5	293.2
⊕	10.4	287.3
10' LT	12.4	285.3
20' "	11.1	286.6
30' "	8.0	289.7
40' "	6.0	291.7

17+17

40' LT	6.5	291.2
20' "	6.6	291.1
10' "	6.6	291.1
⊕	5.6	292.1
10' RT	4.2	293.5
20' "	4.0	293.7
40' "	2.9	294.8

297.66

19+75

40' RT	2.2	295.5
20' "	3.2	294.5
10' "	3.0	294.7
⊕	3.5	294.2
10' LT	3.2	294.5
20' "	3.2	294.5

40' " = E. ch. Park Blvd	3.33	294.33
40' " E. gutter	3.89	293.77

19+84.11

20' LT = E. gutter	3.64	294.62
20' " = E. ch.	3.04	294.62
10' "	3.0	294.7
⊕	2.8	294.9
10' RT	2.8	294.9
20' "	2.8	294.9
40' "	2.0	295.7

19+95⁸⁴

40' RT	2.0	295.7
20' "	2.0	295.7
10' "	2.6	295.1

297.66

39

⊕ = E. ent. ch. Park Blvd 2.58 295.08

⊕ = E. gutter 3.18 294.48

20+0 V 25

20' RT = E. ent. ch. 2.19 295.47

20' " = E. gutter 2.74 294.92

20+14.5

28.5' RT = E. ent. ch. Park Blvd 1.95 295.71

28.5' R = E. gutter 2.52 295.14

RM. B.P.

1.88 295.78
= 295.80s.w. 21 pas +
park Blvd

12-21-34
Miller
Walker
Bliss

"D" Alternate Line
from Alabama & Upas to P.H. Canyon Rd.

indexed
c.s.k.

40

4+99³⁰ P.O.T. Nail

3415 E.C. Def L.
36-05.8

3+00 34-22.6 ✓

2+50 28-38.8 ✓

2+00 22-55 ✓

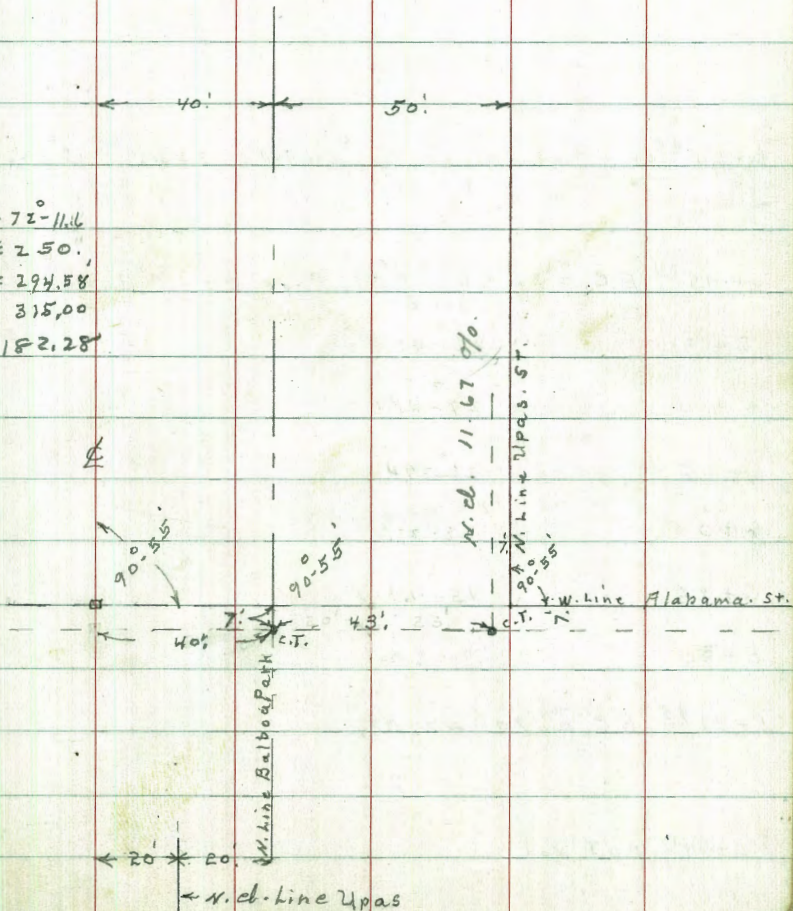
1+50 17-11.2 ✓

1+00 11-27.5 ✓

0+50 5-43.7 ✓

0+00 = W. line Alabama. B.C. L 72-11.2 Lt.

$\Delta = 72-11.6$
 $R = 250'$
 $LE = 294.58$
 $L = 315.00$
 $T = 182.28$



6+64⁴⁵ P.I. of Powder House Canyon Rd. = 7+48⁷⁸ "C" Line Page 20

6+45²⁴ E.C. = 7+29⁶⁷ P.O.T. Page 20 "C" Line

Def L.

6+36 32-40.4

6+26 29-48.5

6+15 26-39.4

6+00 22-21.6

5+75 15-11.9 ✓

5+50 8-02.2

5+21²⁵ B.C. L 70° 42' RT.

4+99³⁰ P.O.T. Nail

4+80 P.H.C. Rd.

4 Powder House Canyon Rd.

0+00 P.H.C. Rd. F.B. 1128 P.I.

88-18-20

$\Delta = 70.42$ RT.

$R = 100'$

$T = 20.93'$

$EX = 22.60$

P.T. Hub.

100' Rad
Hub.

12-26-34. X Sec. "D" Line

262.41

42

B.M. BP	R. 91	262.41	259.50	N.W. Upas & Alabama	20' Lt		4.2	258.2
	10' E. of 0+00 = W. ch. line	Alabama			40' "		4.2	258.2
40' Rt. =	N. Line Park	3.01	259.40	gutter pav		0+50		
40' "	" " "	2.48	259.93	cont. ch	40' Lt		5.9	256.5
20' " =	N. Curb. line Upas. East of Alabama.	2.41	260.00	" "	20' "		6.4	256.0
20' "		3.00	259.41	gutter pav	⊥		7.2	255.2
⊥		2.92	259.49	" " S. End	20' Rt.		8.2	254.2
⊥		2.40	260.01	cont. ch. S. End	40' "		9.5	252.9
20' Lt.		2.5	259.9			1+00		
40' "		2.4	260.0		40' Rt		12.1	250.3
	0+00 = B.C. Lt. = W. Line Alabama				20' "		10.7	251.7
40' Lt		3.2	259.2		⊥		9.8	252.6
20' "		3.2	259.2		20' Lt.		9.0	253.4
⊥		2.8	259.6		40' " = N. edge	Grove of Trees.	8.2	254.2
20' Rt		2.6	259.8			1+50		
40' "		2.6	259.8		40' Lt		11.2	251.2
	0+15				20' "		12.1	250.3
40' Rt		6.0	256.4		⊥ = N. edge, Grove of Trees		13.1	249.3
20' "		5.5	256.9		20' Rt		15.2	247.2
⊥		3.6	258.8		40' "		17.6	244.8

262.41

T.P. 0.04 249.87 12.58 249.83

1+75

40' RT = N. edge Grove Trees 8.2 241.7

20' " 6.4 243.5

ϕ 3.8 246.1

20' Lt 2.2 247.7

40' " 0.9 249.0

2+00

40' Lt 3.2 246.7

20' " 5.2 244.7

ϕ 7.7 242.2

20' Rt. 10.2 239.7

40' " 11.4 238.5

2+25

40' Rt. 18.8 231.1

20' " 15.0 234.9

ϕ 11.7 238.2

20' Lt 9.3 240.6

40' " 6.7 243.2

249.87

2+50

40' Lt 10.6 239.3

20' " 13.3 236.6

T.P. 0.17 237.22 12.82 237.05

ϕ 3.8 233.4

20' Rt. 7.8 229.4

40' " 11.0 226.2

2+75

40' Rt. 16.7 220.5

20' " 14.7 222.5

ϕ 9.2 228.0

20' Lt 4.6 232.6

40' " 1.1 236.1

3+15 E.P.

40' Lt 5.0 232.2

20' " 10.1 227.1

T.P. 1.92 226.54 12.60 224.62

ϕ Hub. 4.89 221.67

20' Rt. 9.9 216.6

40' " 13.6 212.9

	224.54			
	3+50			
40' Rt	17.0	209.5		
20' "	13.1	213.4		
⊕	8.8	217.7		
20' Lt	3.9	222.6		
40' "	+1.0	227.5		
	4+00			
40' Lt	3.6	222.9		
20' "	8.7	217.8		
⊕	13.1	213.4		
20' Rt	18.0	208.5		
40' "	21.2	205.3		
	4+50			
40' Rt	24.3	202.2		
20' "	21.2	205.3		
⊕	17.7	208.9		
20' Lt	13.6	212.9		
40' "	8.6	217.9		
T.P.	3.95	218.17	12.32	214.22

	218.17			
	5+00 = S. Side Grove of Trees			
40' Lt	3.3	214.9		
20' "	8.2	210.0		
⊕	12.6	205.6		
20' Rt	15.8	202.4		
40' "	18.7	199.5		
	5+21 ²⁵ B.C. L 70-42 Rt.			
40' Rt	19.9	198.3		
20' "	17.7	200.5		
⊕	12.7	205.5		
20' Lt	9.9	209.3		
40' "	4.7	213.5		
	5+50			
40' Lt	9.0	209.2		
20' "	12.0	206.2		
T.P.	0.43	206.03	12.57	205.60
⊕	3.5	202.5		
20' Rt	7.2	198.8		
40' "	9.4	196.6		

206.03

5+75

40' Rt	10.6	195.4
20' "	8.0	198.0
☐	6.3	199.7
20' Lt	3.7	202.3
40' "	1.5	204.5

6+00

40' Lt	6.8	199.2
20' "	8.0	198.0
☐	9.4	196.6
20' Rt	11.5	194.5
40' "	14.6	191.4

6+15

40' Rt	18.4	187.6
20' "	18.0	188.0
☐	15.3	190.7
20' Lt	11.1	194.9
40' Lt	9.0	197.0

6+26

40' Lt	11.8	194.2
T.P	0.42	193.87
	22.58	193.45

193.87

6+26 (con.)

20' Lt	4.6	189.3
10' "	6.5	187.4
☐	6.7	187.2
20' Rt	5.6	188.3
40' "	5.3	188.6

6+36

40' Rt	5.6	188.3
20' "	5.9	188.0
☐	6.6	187.3
20' Lt	6.9	187.0
40' "	5.1	188.8

6+45³⁴ E.C. = E. Berm. P.H.C. Rd.

40' Lt	6.3	187.6
20' "	6.8	187.1
☐	6.3	187.6
20' Rt	5.8	188.1
40' "	5.4	188.5

Hub. ☐ 8+68⁵⁰ Page 30 9.54 184.33

45

Richmond St. Extension

indexed
c.s.k.

J.A. Partridge
C.R. Otis
C.F. Weir

1/18/35

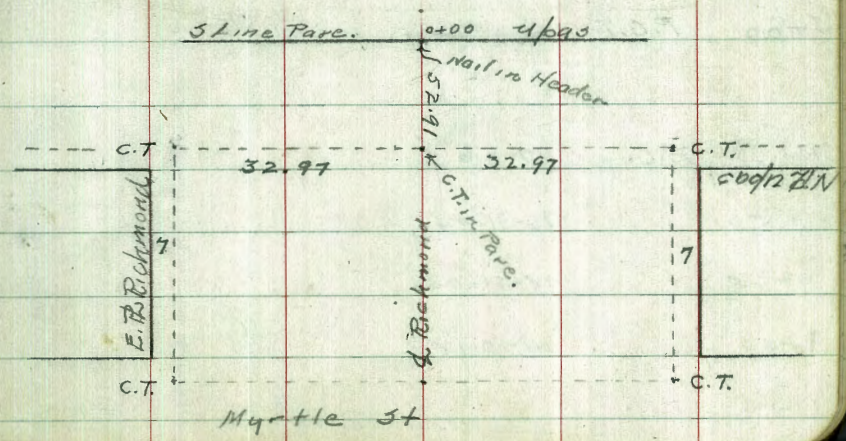
Sta	Defl.	
+75	12-59-21	
+50	11-48-3	
+25	10-37-39	
2+00	9-26-48	$\Delta = 34-12 \text{ Rt}$
+75	8-15-57	$TB = 606.42$
+50	7-05-06	$T = 186.56$
1+25	5-54-15	$\text{Arc} = 361.97$
1+00	4-43-24	$00-02.834 \text{ per. ft.}$
0+75	3-32-33	
0+50	2-21-42	
0+25	1-10-51	



P.I.
1-26-56
 $\Delta = 34-12 \text{ Rt.}$

S. R. Upas

B.C. Rt.
0+00 = Prolongation of Richmond South to Int. of S.
Parcment line of Upas.

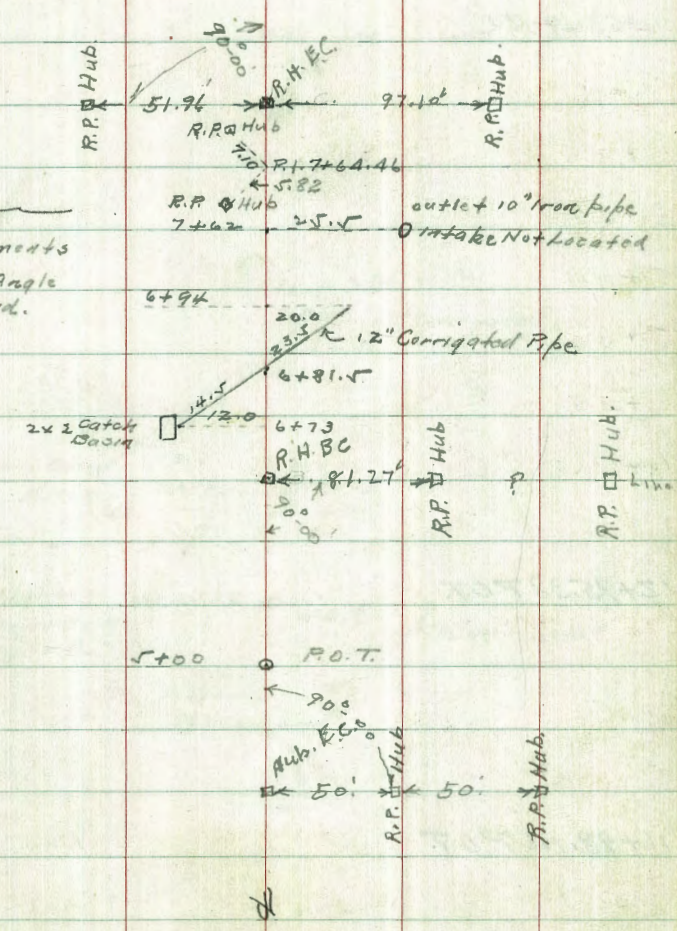


Richmond St. Extension

Sta	Defl.	
9+00.85 E.C.	7-28	$\Delta = 14-56$ RT
+50	6-04-58	EX = 9
8+00	4-43-19	$T_C = 1052-63$
+50	3-21-40	$T = 137.96$
7+00	2-00-01	$ARC = 274.35$
+50	0-38-22	
6+26.5 B.C.		
5+00	P.O.T.	
3+61.97 E.C.	17-06	
+50	16-31-56	
+25	15-21-03	
3+00	14-10-12	

Note:
Tie Measurements
Taken Right Angle
To Chord.

6+26.5
3+61.97
264.53
156.56
137.96
589.05

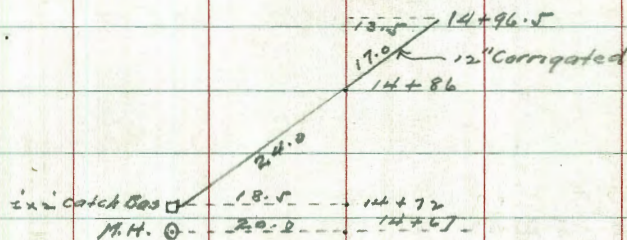
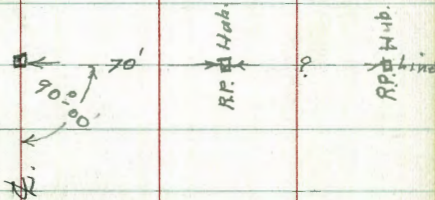


Sta Defl.

67+00 1-25-43

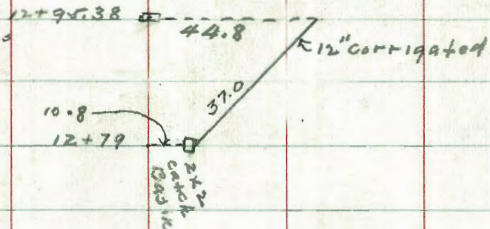
16+63.49 B.C

70.5
21.5
49.0

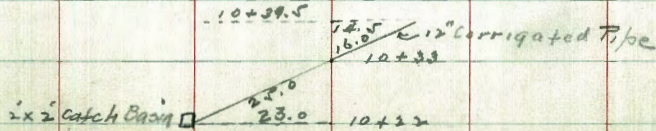


12+95.38 P.O.T.

Note: Tie Distances
Taken Right Angles
To Tangent.



11+98.14 P.O.T.



Richmond St. Extension

22+10.
20+75.75
134.25

22.10
2P 87.18
21.82

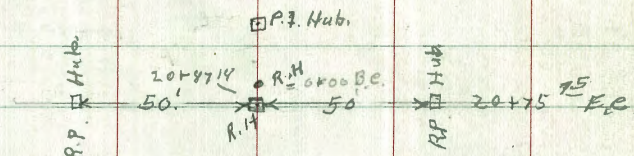
22+10
20+87.18
1+22.82

22+10 Hub W. Side Cayada Way (End)

R.P. Hub Elev 160.99

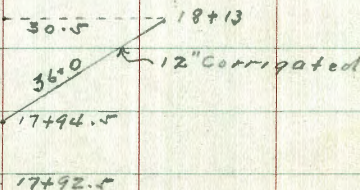
21+98.9 Int. Richmond St. Ext + Cayada Way

21+87¹⁸ P.I.
20+87¹⁸ B.C = 0+00
20+75.75 E.C 16-08



+50	N-07-31	Δ = 32-16 Rt.
20+00	13-10-07 ✓	EX = 30
+50	11-12-43 ✓	R = 731.71
19+00	9-15-19 ✓	T = 211.66
+50	7-17-55 ✓	412.07 ARC = 12.26
18+00	5-20-31 ✓	Ref per ft 140.882
17+50	3-23-07 ✓	" " " 140.946

Note: The Distances Taken Right Angle To Chord Bet Sta. 17+50 and 18+50



Int. Catch Basin

Richmond St. Extension
E. Levels and X Sections

1/22/35

Partridge
Otis
Weir

Indexed
C.S.K.

Lt.

E

Rt

Sta.	B.S.	H.I.	F.S.	Elev
	1.57	291.52 297.37		289.95 (295.80)
B.M.	v. 0.6	286.27 292.12	7.31	284.21 290.06

N.W. Cor.
Herbert
W. End SE
Ret

(286.97)
Upas.
Richmond
Upas.

(286.97) (cont'd) (Upas)

0+00	B.C. Rt. C.T. Header Board		3.1	283.15 289.0
------	-------------------------------	--	-----	----------------------------

on Pavement +0.2
20 00 on
20 Pavement

0+25			2.6	283.65 289.5
------	--	--	-----	----------------------------

0+50			2.4	283.85 289.7
------	--	--	-----	----------------------------

+0.7 +0.7 -0.1 -0.3 00 -0.3
40 21 15 15 18.6 40

~~284.55~~ ~~284.55~~ ~~283.75~~ ~~283.35~~ ~~283.85~~ ~~283.55~~

0+75			2.6	283.65 289.5
------	--	--	-----	----------------------------

1+00			2.8	283.45 289.3
------	--	--	-----	----------------------------

+1.0 +0.9 -0.2 -0.3 00 -0.4
40 30 15 12.3 15 40

~~284.45~~ ~~284.35~~ ~~283.25~~ ~~282.95~~ ~~283.45~~ ~~283.05~~

Richmond St. Ext

Sta B.S H.I. F.S Elev Lt. \pm Rt

286.27
~~292.15~~

1+25 3.1 ~~289.0~~ 283.15

1+50 3.4 ~~288.7~~ 282.85

+1.6 / 40
~~284.45~~
283.95
+1.1 / 29
~~284.4~~
282.85
0 / 5
~~284.7~~
282.35
-0.5 / 15
~~288.2~~
281.75
-1.1 / 40
~~281.6~~

1+75 3.6 ~~281.5~~ 282.65

2+00 3.9 ~~288.2~~ 282.35

+1.0 / 20
~~284.4~~
283.35
+1.0 / 21
~~284.4~~
283.35
0 / 5
~~284.4~~
282.35
0 / 3
~~284.4~~
282.35
0 / 7
~~288.2~~
282.35
+0.3 / 5
~~288.2~~
282.65
+0.5 / 40
~~288.7~~
282.85

2+25 4.2 ~~287.4~~ 282.05

2+50 4.6 ~~289.5~~ 281.65

+1.0 / 20
~~288.7~~
282.65
+0.8 / 15
~~288.7~~
282.45
+0.8 / 13
~~288.7~~
282.45
-0.1 / 10
~~287.4~~
281.55
-0.4 / 11
~~287.4~~
281.25
+0.2 / 15
~~287.4~~
281.85
+0.2 / 40
~~287.4~~
281.85

Richmond St. Ext.

Sta	B.S	I.I.	F.S	Elev	L+	+	R+
		286.27 292.12					
2+75			5.1	281.15 287.0			
3+00			5.6	280.65 286.5	+1.0 40	+0.3 15	+0.2 8
					-0.3 4	-0.5 15	+0.5 24
						+0.3 40	
					281.65	280.95	280.85
					280.35	280.15	181.15
					280.95		
3+25			6.2	280.05 285.9			
3+50			6.8	279.45 285.3	+1.1 40	+1.0 15	+1.1 4
					+0.2 15	00 24	+0.7 30
						+0.7 40	
					280.55	280.45	280.55
					279.65	279.45	280.15
					280.15		
3+61.97	^{on} E.C. Hob		6.00	280.25 286.1			
4+00			6.5	279.75 285.6	+0.3 40	+0.2 15	00 10
					-1.3 10	-1.1 15	-1.0 30
						-0.6 40	
					280.05	279.95	279.75
					279.75	278.45	278.65
					278.75	278.75	279.15

Richmond St. Ext.

Sta.	B.S.	H.I.	F.S.	Elev.	Lt	±	Rt
		286.27 292.12					
4+50			7.5	278.75 284.6	+1.1 +0	+0.2 15	00 -2.2 -1.6 -1.3 6 10 15 40
					279.85	278.95	278.95 276.53 277.15 277.45
5+00 P.O.T.			9.1	277.15 283.0	+2.2 4.0	+0.6 15	-0.3 -3.2 -2.3 -2.0 -1.9 -1.4 2.6 6.0 10 15 35 40
					279.35	277.75	276.85 273.95 274.85 275.15 275.25 275.75
T.P.	0.00	273.60 279.45	12.67	273.60 279.45			
5+50			3.2	270.45 276.3	+6.8 4.0	+4.0 15	+3.4 15
					277.25	271.45	273.85 271.85 271.75 271.45
							Deer Park Cor. Fence
6+00			6.0	267.65 273.5	+7.6 4.0	+4 15	-0.7 3
					275.25	273.15	271.65 266.95 268.65 258.65 257.65 261.35
							Edge Road
6+26.5 B.C.Rt.			7.7	265.95 271.8			+1.0 -9.0 -1.0 -6.3 15 30 50 6.2
6+50			9.3	264.35 270.2	+7.3 31	+6 18.5	+3.6 0.0 15 8.6
					271.35	270.35	267.95 264.35 265.35 244.95 247.15 245.8
							Deer Park Fence W. Edge Road

Richmond St. Ext.

Sta.	B.S	H.I.	F.S	Elev.
		273.60 274.45		
6+73	catch Basin on 12' left	Grate	11.05	262.55 268.10
T.P.	0.96	261.50 267.35	13.06	260.54 266.39
6+94	20' RT F.L. Pipe		3.2	258.15 264.0
7+00			0.5	261.05 266.9
7+50			4.2	257.35 263.2
8+00			8.0	253.55 259.4
8+50			11.3	250.25 256.1
T.P.	0.34	248.78 254.63	13.06	248.44 254.29

L
Rt

Deer Park Fence

+8.6	+1.2	00						
43	15	12						
<hr/>								
269.65	262.25	261.05						

Edge Road

00	-2.8	-17	-23		
1015	15	37	60.5		
<hr/>					
261.05	258.25	257.05	258.05		

Deer Park Fence

+16.6	+14.3	+12	+3.2	00			
53	39	26	13	11			
<hr/>							
273.95	269.65	269.35	269.55	257.35			

Edge Road

+0.4	-12	-20			
14	33	58			
<hr/>					
257.75	245.35	257.35			

Deer Park Fence

+23	+21	+17.6	+10	+5.0	-0.6	+0.5	+0.7	-12	-18	-21.7
46	36.4	19	14	8	7	15	22	43	66	73
<hr/>										
276.55	274.35	271.15	269.35	278.55	250.95	253.55	254.55	241.55	235.55	251.85

Edge Road

+26	+24.0	+13	+4.0	-0.5	00	+0.5	-12	-20	
73	45	24	13	10	15	20	41	64	
<hr/>									
276.25	274.25	263.25	254.25	249.75	250.25	250.75	238.25	250.25	

Richmond H. Ext.

Sta	B.S	H.I	F.S	Elev.
		235.84 244.69		
11+37			10.5	225.35 231.7
11+50			8.4	227.45 233.3
11+98.14 P.O.T.			5.31	230.53 236.38
12+50			6.6	229.25 235.1
12+95.38 P.O.T.			9.94	225.90 231.75
T.P.	0.18	223.28 229.13	12.74	223.10 228.95

4 4 Rt

Edge Road	Edge Road	Edge Rd.	Edge Rd.
+26 44	+13 16.5	+10.1 8	-2.8 15
-2.5 27	-13 44	-18.5 66	
224.65	224.95	214.45	208.95
+26 60	+13 31.5	+5.8 15	-2.5 2.5
-10.4 6.5	-10 15	-8.8 31.5	14.8 40
228.05	220.15	220.55	215.75
+23 45	+13 25.5	+7.8 15	-1.5 3.5
-12.5 10.2	-12.2 15	-10.8 57.3	17.2 45
227.75	212.25	237.05	218.45
+26 62	+13 29.5	+6.4 15	-12.6 8.5
-12.4 15	-11 37	-18.7 54	-24 70
251.95	238.95	232.35	213.35
			213.55
			214.95
			207.25
			201.95

Richmond St. Ext.

Sta	B.S.	I.I.	F.S.	Elev.	Lt.	±	Rt
		223.28 229.13					
12+79	Top Grating Catch Basin		8.35	214.93 220.98			
12+95.38	F.L. Pipe 44.8 Rt		12.08	211.20 217.05			Edge Rd.
13+25			3.4	219.85 225.7			
							Edge Rd.
13+50			12.6	210.65 216.5			
T.P.	1.30	212.21 218.06	12.37	210.91 216.76			Edge Road
14+00			5.2	207.05 212.9			
							Edge Road
14+50			8.9	203.35 209.2			
							Edge Rd
15+00			11.9	200.35 206.2			

$\frac{+26}{55}$ $\frac{+13}{27}$ $\frac{+8.0}{15}$ $\frac{-4.0}{4}$ $\frac{-9.1}{6.3}$ $\frac{-8.7}{15}$ $\frac{-7.6}{53}$ $\frac{-16.6}{45.3}$ $\frac{-20.6}{49.4}$ ✓
~~215.85~~ ~~232.85~~ ~~227.85~~ ~~215.85~~ ~~210.15~~ ~~211.25~~ ~~212.25~~ ~~209.25~~ ~~199.25~~

$\frac{+26}{46.5}$ $\frac{+13}{17}$ $\frac{+9.3}{50}$ $\frac{-1.4}{1.0}$ $\frac{-0.7}{15}$ $\frac{+0.2}{30}$ $\frac{-8.8}{47}$ $\frac{-13}{58}$ ✓
~~236.85~~ ~~223.85~~ ~~219.95~~ ~~209.25~~ ~~209.95~~ ~~210.85~~ ~~201.85~~ ~~198.65~~

$\frac{+26}{47}$ $\frac{+13}{19}$ $\frac{+9.0}{17}$ $\frac{+2.6}{11.0}$ $\frac{-1.2}{9.0}$ $\frac{0.0}{15}$ $\frac{0.0}{21}$ $\frac{-2.4}{25.6}$ $\frac{-5.7}{37.2}$ $\frac{-12}{49.7}$ ✓
~~233.05~~ ~~220.05~~ ~~216.05~~ ~~209.85~~ ~~205.85~~ ~~207.05~~ ~~204.65~~ ~~201.35~~ ~~195.05~~

$\frac{+13}{65}$ $\frac{+5.2}{24.6}$ $\frac{0.0}{19}$ $\frac{+0.4}{15}$ $\frac{+0.8}{6.6}$ $\frac{+0.2}{10}$ $\frac{-3.5}{18}$ $\frac{-6.8}{31}$ $\frac{-12}{44}$ ✓
~~216.35~~ ~~208.35~~ ~~203.35~~ ~~203.75~~ ~~204.15~~ ~~203.55~~ ~~199.85~~ ~~196.55~~ ~~191.35~~

$\frac{+23}{64}$ $\frac{+13}{39}$ $\frac{+9.7}{30}$ $\frac{0.0}{22.6}$ $\frac{+0.5}{15}$ $\frac{0.0}{6.5}$ $\frac{-4.0}{13.5}$ $\frac{-6.0}{20.5}$ $\frac{-7.5}{27}$ $\frac{-12}{34}$ $\frac{-9.0}{49}$ ✓
~~223.35~~ ~~213.35~~ ~~209.55~~ ~~200.35~~ ~~200.85~~ ~~200.35~~ ~~196.35~~ ~~194.35~~ ~~190.85~~ ~~188.35~~ ~~177.55~~

Richmond St. Ext.

Sta.	B.S.	I.I.	F.S.	Elev.	Lt.	Rt
		212.21 218.06				
T.P.	0.74	200.25 206.10	12.70	199.51 205.36		
14+67	M.H. 20 Lt			202.36 208.21		
14+72	Top Grading Catch Basin 13.5 Lt			201.86 207.71	Hand	
14+96.5	F.L. Pipe 13.5 Rt			197.36 203.21	Level	
15+50			2.7	197.55 203.4		
16+00			6.0	194.25 200.1		
16+50			8.9	191.35 197.2		
17+00			11.9	188.35 194.2		
T.P.	0.86	188.60 194.45	12.51	187.74 193.59		

Edge Road

+13	+7.4	00	+0.5	00	-4.8	-11	-8.0
50	27	23	16	9.5	18	48.5	60
210.55				197.55	192.75	186.55	189.55

Edge Rd.

+25	+13	+8.2	00	00	00	-5.0	-10.3	-7.5
62.5	34	24	19	15	10.7	18.7	33.7	60.7
219.25				194.25	189.25	183.95	186.75	

Edge Bank

+26	+13	+6.5	-0.7	-0.3	-6.6	-9.0	-6.5
58.5	25	15	13	15	25	40.8	50
217.95				197.85	190.65	184.15	184.85

Edge Bank

+26	+13	+7.1	-0.4	00	00	-3.8	-7.4	-7.0
66	30	12	8	15	22	29	40.3	50
214.35				195.45	187.95	184.55	180.95	181.35

Sta.	B.S	H.I	F.S	Elev	Lt.	±	RT								
		188.60 194.44													
17+50			3.7	184.95 190.8	+26 58.7	+13 27	+6.8 -0.2 10 5.5	+0.2 15	+0.2 24	-2.7 28.5	-4.8 48	-1.1 70			
					110.95	197.95	191.75	185.15	181.15	182.25	179.15	183.95			
	Top Grading Catch Basin	4.3 Lt	6.44	182.16 188.01											
18			7.1	181.55 187.4	+26 65	+13 23	+10.5 15	+4.8 7.5	0.0 4.5	+0.7 15	+0.7 24.5	-2.6 32.5	-3.0 54.5	-0.3 65	
					207.65	194.55	192.05	186.35	181.55	182.25	178.95	179.55	181.55		
18+13	F.L. Pipe		10.1	178.55 184.4											
18+50	30.5 RT		9.8	178.85 184.7	+26 71.5	+13 34.5	+3.0 13.5	0.0 10.5	0.0 14	+0.5 15	-0.5 19.7	-2.3 26	-2.1 44.6	-0.2 55.4	
					204.85	191.85	181.85	178.85	178.85	179.35	178.35	176.35	176.35		
T.P.	0.39	176.25 182.10	12.74	175.86 181.71											
19+00			1.5	174.75 180.6	+23 77.4	+13 47.4	+9.0 29	+2.0 19	+0.7 17.6	+0.7 15	0.0 5.0	+1.6 7.0	-0.7 21.5	+0.3 38	+2.4 46
					197.75	187.75	185.75	178.75	175.45	175.45	174.75	176.35	174.05	175.05	177.15
19+50			4.7	171.55 177.4	+13 50	+6.8 28	+2.1 21	+0.8 20	+0.8 15	0.0 1.5	+2.3 3	+2.7 8	+1.0 12	+0.8 50	+3.8 42.5
					184.55	178.35	173.65	172.35	172.35	171.55	173.85	174.25	172.55	172.35	175.35

Edge Rd

Edge Rd

Edge Rd
Top Bank

Richmond St Ext.

Sta B.S. H.I. F.S. Elev

176.25
+82.10

20+00 7.1 169.15
~~175.0~~

20+50 9.7 166.55
~~172.4~~

20+75.75 E.C. 11.1 165.15
~~171.0~~

21+00 12.4 163.85
~~169.7~~

21+50 Boot Log 13.8 162.45
~~168.3~~

21+98.9 Int. Richmond St Ext. 160.65
S. on Canyonada Way ~~166.4~~

22+05 Hub End Boot Log 15.7 160.55
S. Side Canyonada Way ~~166.4~~

168.3
1.9
166.4

Lt E Rt

+10.0 +7.7 +11.8 +0.6 0.0 +1.5 +1.4 +0.8 +3.6
4.8 41.4 17.8 15 5.0 6 14 25 46.3
~~179.15~~ ~~176.85~~ ~~170.95~~ ~~179.75~~ ~~169.15~~ ~~170.65~~ ~~170.55~~ ~~169.95~~ ~~172.75~~

+4.0 +3.7 +1.7 0.0 -0.2 +1.4 +2.0 +1.6 +1.0 +3.0
5.0 38.3 15 13 8.5 10 14 32 37 51.5
~~170.55~~ ~~170.35~~ ~~168.25~~ ~~166.55~~ ~~166.35~~ ~~167.95~~ ~~168.55~~ ~~168.15~~ ~~167.55~~

-0.3 +0.4 +0.8 -0.6 +0.3 +1.2 +2.7 +2.6
5.0 33 13.5 11.2 10 11.4 39.5 40
~~163.55~~ ~~164.25~~ ~~164.65~~ ~~163.25~~ ~~164.15~~ ~~165.05~~ ~~166.65~~ ~~166.45~~

-1.7 -0.6 -1.0 -0.5 0.0 +0.3
5.0 5.0 15 15 26 5.0
~~160.75~~ ~~161.85~~ ~~161.45~~ ~~161.95~~ ~~162.45~~ ~~162.35~~ ~~161.05~~
S. on Canyonada ← 5.0 → N. on Canyonada

Richmont St. Ext
 Check Levels Back To N.W. Cor.
 Herbert and Upas.

		176.25 182.70				
B.M. 1.		0.60	175.65 181.50	2 Nails 09 R 35 Rt	12 Scrub Sta 19+25	(172.67 = Using)
	12.43	188.28 194.13	0.40	175.85 181.70		
	12.19	200.11 205.96	0.36	187.92 193.77		
B.M. 2	12.03	210.35 216.20	1.79	198.32 204.17	Edge Bridle Path 90' Rt Sta 15+35	
	12.92	222.57 228.42	0.70	209.65 215.50		
B.M. 3	12.77	233.86 239.71	1.48	221.09 226.94	Edge Bridle Path 125' Rt Sta 11+75	
	12.48	246.05 251.90	0.29	233.57 239.42		
	12.89	258.56 264.41	0.38	245.67 251.52		
	12.95	271.01 276.86	0.50	258.06 263.91		
B.M. 4	12.10	282.67 288.52	0.44	270.57 276.42	55 FT TB Sta. 5+60	
	8.87	290.24 296.09	1.30	281.37 287.22		
	7.01	294.00 299.85	3.25	286.99 292.84		
			4.09	289.91 295.76	289.95 Herbert and Upas.	

Note: Elevations on this page not
 corrected — 5.85 high

EV. 286.93 Albert and Upas

Canyada Way Running From
 Richmond St. Extension Sta. 21+87.18
 To 11th Ave.

J. Partridge
 H. Wade
 R. Bower

Indexed
 C.S.R.

Sta Defl.

6+39 P.O.T

1+64.93 E.C. 40-50

+50 37-08-06

+25 30-56-45

1+00 24-45-24

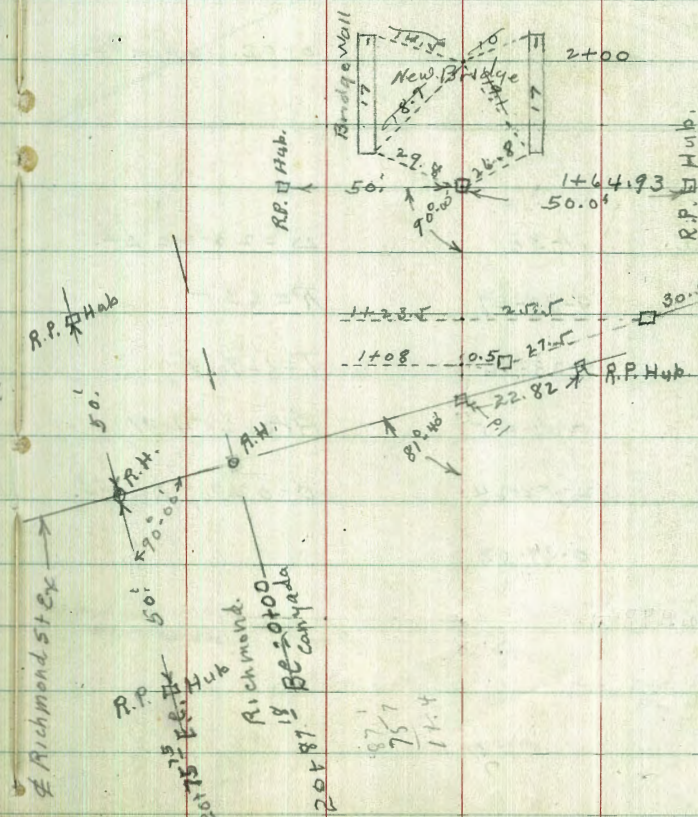
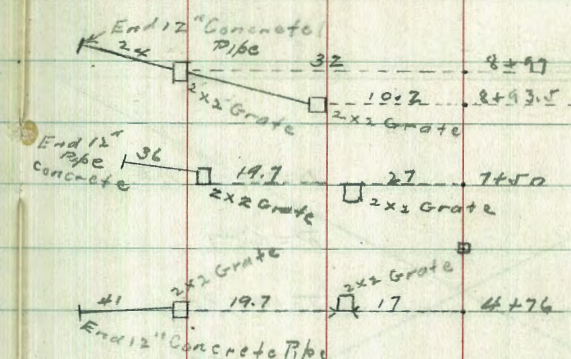
+75 18-34-03

+50 12-22-42

0+25 6-11-21

0+00 Canyada Way = (B.C.)
 20+87.18 Richmond St. Extension

$\Delta = 81-40 \text{ Lt}$
 $T = 100.0$
 $R = 114.71$
 $\text{Arc} = 164.93$
 $\text{Defl.} = 14.854 \text{ per Ft.}$
 $\text{Def per Ft } 89.1287''$

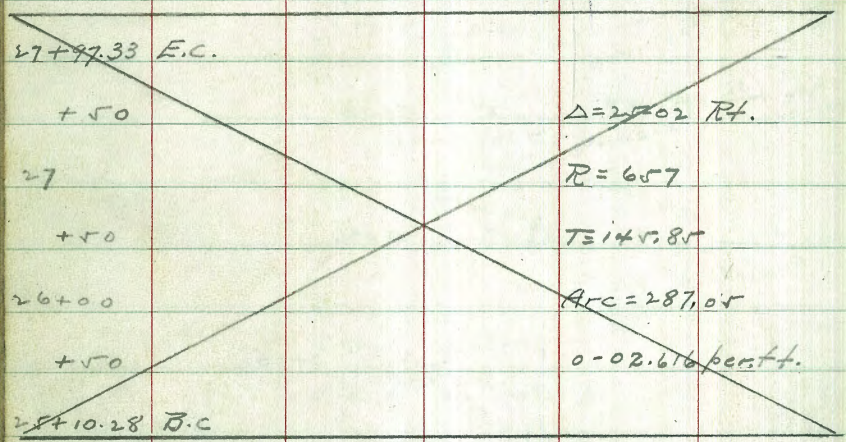


87.7
 75.4
 11.4

Canyada May-

J. Partridge
C. Walker
W. Bliss

Sta. Def't.

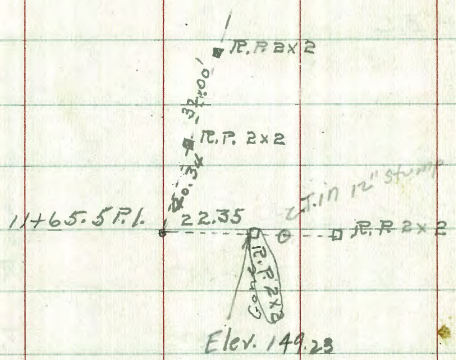


27+97.33	E.C.		$\Delta = 250.2$ Ft.
+50			$R = 657$
27			$T = 145.85$
+50			$Arc = 287.05$
26+00			$0 - 02.616$ per ft.
+50			
25+10.28	B.C.		

12+91.22	E.C.	11-30	$\Delta = 230.0$ Ft.
+50		9-38-27	$R = 635$
12+00		7-23-06	$T = 129.19$
+50		5-07-45	$Arc = 254.91$
11+00		2-52-24	$0 - 02.707$ per Ft.
+50		0-37-03	
10+36.31	B.C.		

1036.31
129.19
1165.50

11+65.50
161.70
1063.80

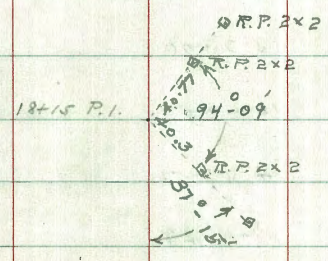
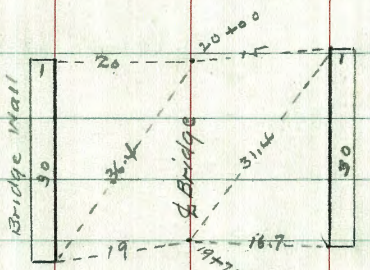


+ 30.8 10403 17.6 W End 12" Concrete Pipe etc Pipe

Cangada Way

1653.59
1671.41
1815.00

Sta	Defl	
+75	11-34-43 ✓	$\Delta = 40-00 \text{ Rt.}$
+50	9-52-39 ✓	$R = 421$
+25	8-10-34 ✓	$T = 153.23$
21+00	6-28-30 ✓	$\text{Arc} = 293.91$
+75	4-46-25 ✓	$0-04-083 \text{ per Ft.}$
+50	3-04-21 ✓	
+25	1-22-16	
20+04.85 B.C.		
19.74 03		
30.82		
19+74.03 E.C.	8-30 ✓	$\Delta = 17-00 \text{ Lt}$
+50	2-51-35	$R = 1080.0$
19+00	6-32-02	$T = 161.41$
+50	5-12-29	$\text{Arc} = 320.44$
18+00	3-52-56	$0-01-59 \text{ per Ft.}$
+50	2-33-23	$\text{Def. } 95.46''$
17+00	1-13-50	
16+53.59 B.C.		



Cangada Way

2510.28
145.55
2664.73

Sta Defl.

27+97.33 E.C. 12-31 Δ=25-02 Rt.

+50 10-27-06

2657

27+00 8-16-18

T=145.85

+50 6-05-30

Arc=287.05

26+00 3-54-42

0-02.616 per. Ft.

+50 1-43-54

25+10.28 B.C.

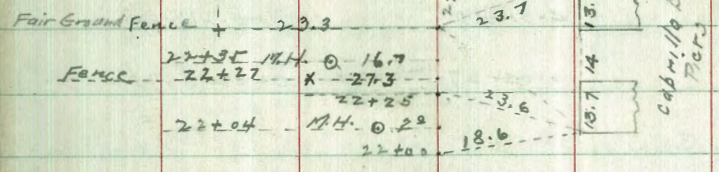
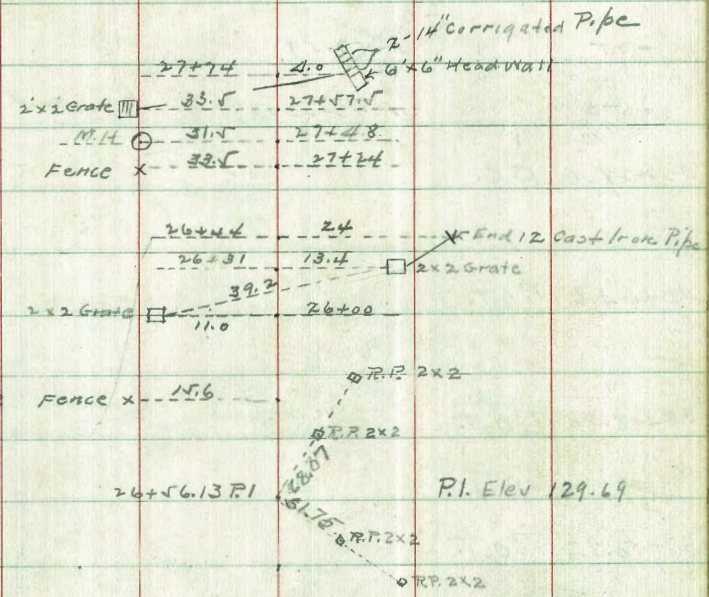
22+98.76 E.C. 20-00-00

+75 18-23-01

+50 16-40-57

+25 14-58-52

22+00 13-16-48



35987
107.6
35063

Sta	Defl.	ch
+75	3-59-59	
+50	1-49-23	ch 20.86

42+29.06 B.C.

40+64.6 P.O.T.

38+18.88 P.O.T.

37+50.92 P.O.T.

35+12.33 E.C. 6-30 Δ 17-00 Lt.

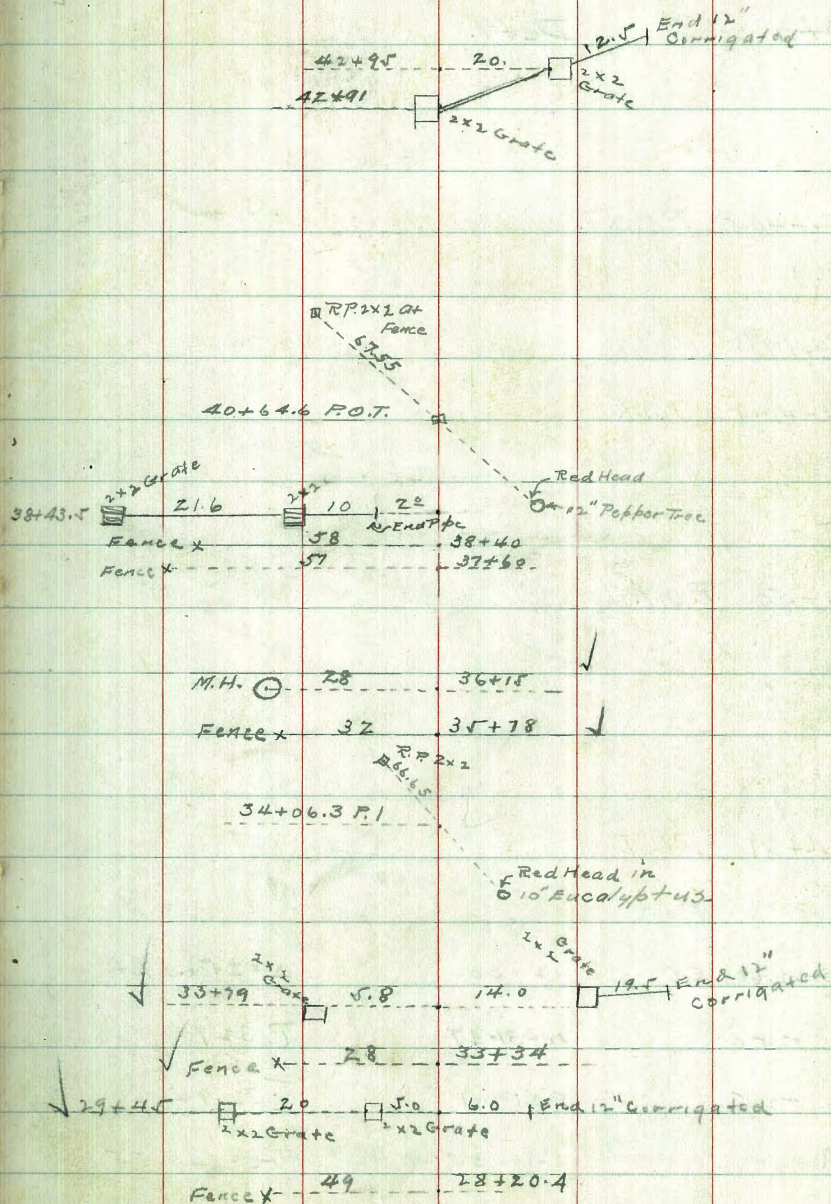
35+00 8-00-30 R=720

+50 6-01-09 T 107.6

34+00 4-01-48 Arc 213.63

33+50 2-02-27 0-02.387 per Ft.

32+98.70 B.C.



Sta

Defl.

96.09
48.04

54+40.52 P.O.S.T.

54+17⁹⁶ BC.

44
72.61
27.39
72.94
10 0.33

51+50 P.O.T.

15.7

44+81 P.O.T.

43+72.61 E.C.

12-30

$\Delta = 25^{\circ}00' Lt$

+50

10-31-47

R 329

+25

8-21-11

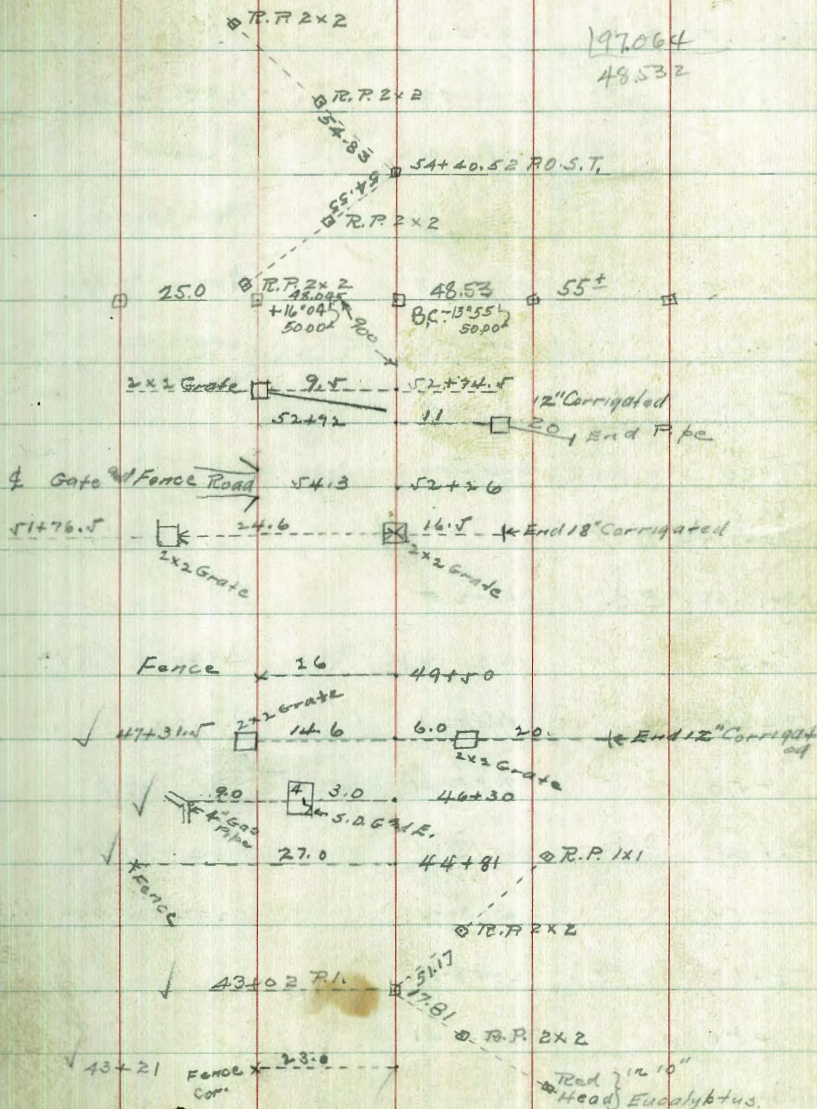
T. 72.94

43+00

6-10-35 ch 49.88

Arc = 143.55

0-05.224 per Ft.

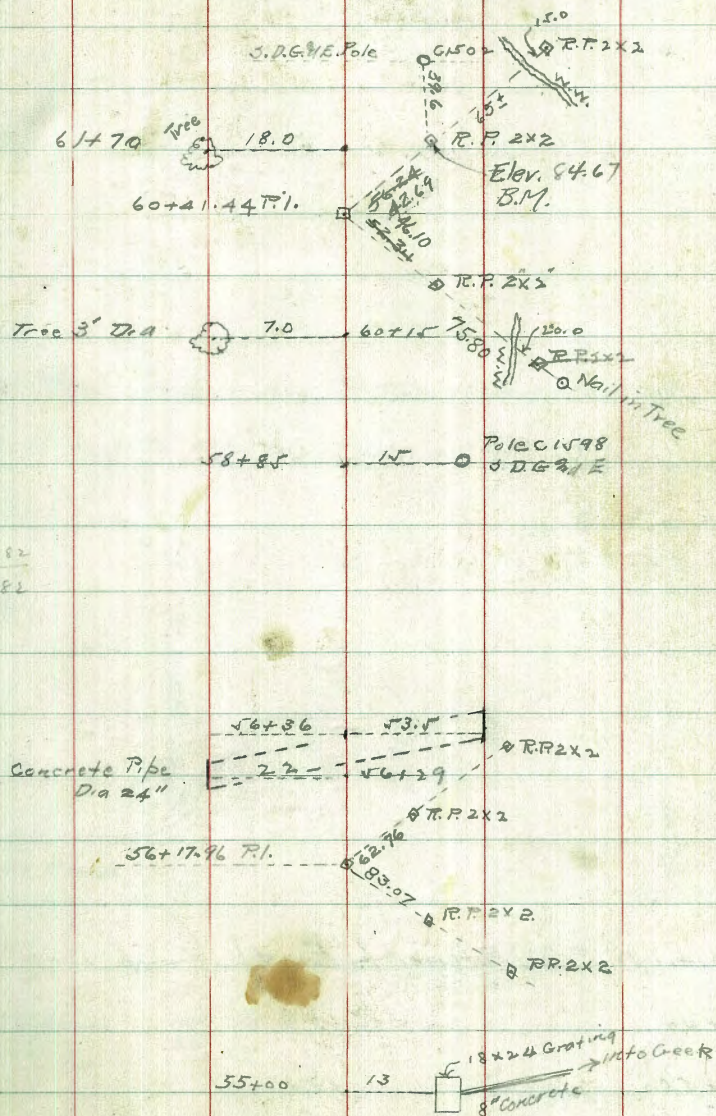


Canyada Way-

Sta.	Defl.	
62+40.51 E.C.	4-46	
62+00	4-16-58	$\Delta = 9-32$ Lt.
+50	3-41-08	T 200
61+00	3-05-18	$R = 2398.46$
+50	2-29-28	$ARC = 399.07$
60+00	1-53-38	0-00-43 per Ft. 0.716 M "
+50	1-17-48	
59+00	0-41-58	
58+41.44 B.C.		
58+10.62 E.C.	13-25	
+50	11-20-41	$\Delta = 56-50$ Rt.
57+00	9-38-11	T 200
+50	7-55-41	$R = 838.43$
56+00	6-13-11	$ARC = 392.66$
+50	4-30-01	0-02.05 per Ft.
55+00	2-48-11	
+50	1-05-41	
54+17.96 B.C.		

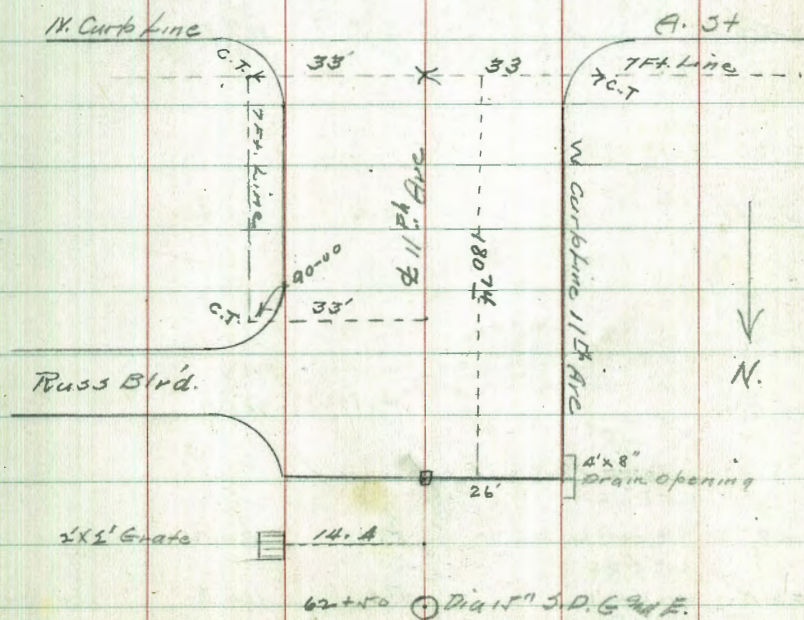
Note: for New Location
See Book 1520 Page 48

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Canyada Way

Note. ϕ of Canyada Way is The Prolongation of
 ϕ of 11th Ave To P.I. Sta. 60+41.44 (P.I. 68)



67+14.1 N. Edge Pavement (End) ✓

66+46

62+50

62+50 \odot Dia 15" S.D. 6th F.

Canyada Way Levels & Section

Partidge
Weir
Bower

index
c.s.k.c

Sta	B.S.	I.I.	F.S.	Elev
		175.915		175.65
	0.265	181.765		181.50
	2.30	165.285	12.93	162.985
		171.135		168.835
20+87.18	Richmond St. Ex + =			
0+00	B.C. Canyada Way		0.70	164.59
0+25			2.1	162.2
0+50			3.5	161.8
0+75			3.6	161.7
1+00			4.1	161.2
1+08	0.5 Right on Grate		5.1	160.2
1+23.5	2.5 Rt on Grate End Pipe F.L.		7.0	160.3
			7.7	157.6

Richmond St Extension Pg. 61
B.M. 11-35' Rt Sta 19425'

(Note Gutter = Sides of Present Road)

Lf	+	+	+	+	Gutter	Gutter	+	+	+	+	+
0.2	1.0	1.8	1.2	-0.3	-0.1	+1.6	+1.2	+1.2	+2.3		
50	30	15	13	11	9	11.7	15	50	50	50	50
164.8	165.6	165.9	165.8	164.1	164.9	166.3	165.8	165.8	166.9		

+	+	+	Gutter	Gutter	+
0.2	0.8	1.8	0.0	+1.0	+0.2
50	15	50	3	13	25
161.6	162.6	163.6	161.8	162.8	162.0
					162.6

-	-	-	Gutter	Gutter	-	-
1.4	0.8	0.5	-0.6	-0.1	-0.7	-0.2
50	30	15	2.5	15	59	50
159.8	160.4	160.7	160.6	161.1	160.5	161.0

Canyada Way

Sta	B.S.	H.I.	F.S.	Elev	ft	ft	ft
	165.285 171.135						
1+25			4.4	160.9			
1+50			4.8	160.5	Gutter -1.8 -1.6 -0.3 0.0 50 30 15 7.0 158.7 158.9 160.2 160.1	Gutter 0.0 -0.6 -1.6 -4.0 -5.7 -1.3 0.0 15 30 39 44 49 50 60 160.1 159.9 158.9 156.5 156.8 159.2 160.5	creek -1.8 -1.6 -0.3 0.0 50 30 15 7.0 158.7 158.9 160.2 160.1
2+00	OH 3" ϕ Bridge		5.5	159.8	creek -3.5 -4.0 -7.0 -6.0 -2.5 70 59 58 33 28 156.3 155.8 152.8 153.8 157.3	Gutter -1.7 +0.2 16 14 158.1 160.0	Gutter 0.0 -0.3 -0.1 +0.5 10 15 30 50 159.8 159.5 157.7 160.3
2+50			7.5	157.8	Gutter -1.6 -1.2 +0.3 50 31 17 156.2 159.0 158.1	Gut. 0.0 +0.9 +1.3 +2.8 +5.0 +8.0 2 15 27 29 40 50 157.8 158.7 159.1 160.6 162.8 165.8	
3+00			8.2	157.1	Gut. Gutter -1.5 -0.2 -1.2 -0.8 +2.0 +6.1 +11 50 25 22 15 15 34 50 155.6 156.9 155.9 156.3 159.1 163.2 168.1		
3+50			8.8	156.5	Gutter Gut. -1.4 -1.3 -0.8 +1.0 +1.8 +6.0 +11.1 50 26 6 10 15 3.2 50 155.1 155.2 155.7 157.5 158.3 162.5 167.6		

Canyada May

Sta	B.S.	H.I.	I.S.	Elev	LT	Q	TOT
		165.285 171.150					
T.P.	5.61	160.265 166.115	10.63	154.655 160.505			
4+00			3.90	157.37			
4+50			2.6	157.7			
4+76	17.7+ } 36.7+ } Topgrate		6.3	154.0			
			6.3	154.0			
4+76	Endplate 77.7+ } FL.		10.05	150.22			
5+00			2.7	157.6			
5+50			3.7	156.6			
6+00			3.5	156.8			

Gut. Gut.

$$\begin{array}{ccc|ccc} -2.7 & -2.2 & -1.8 & +3.0 & +6.4 & +10.5 \\ \hline 50 & 34 & 11 & 8 & 25 & 50 \end{array}$$

$$153.7 \quad 154.2 \quad 154.6 \quad 159.4 \quad 162.8 \quad 166.9$$

Gut. Gut.

$$\begin{array}{ccc|ccc} -4.0 & -3.5 & -1.8 & +1.3 & +3.0 & +5.6 & +8.7 \\ \hline 50 & 38 & 16 & 4 & 15 & 30 & 50 \end{array}$$

$$153.7 \quad 154.2 \quad 154.3 \quad 159.0 \quad 162.7 \quad 163.3 \quad 166.4$$

Gut. Gutter

$$\begin{array}{ccc|ccc} -4.3 & -4.0 & -4.3 & -4.7 & -3.6 & -1.2 & +2.8 & +4.2 & +8.1 \\ \hline 70 & 50 & 42 & 22 & 19 & 6 & 19 & 30 & 50 \end{array}$$

$$152.3 \quad 153.6 \quad 153.3 \quad 152.9 \quad 154.0 \quad 156.4 \quad 162.4 \quad 161.8 \quad 165.7$$

W. Bank
Creek
Gut. Gut.

$$\begin{array}{ccc|ccc} -3.8 & -3.6 & -4.2 & -2.4 & +2.2 & +4.5 & +8.4 \\ \hline 76 & 48 & 26 & 15 & 15 & 30 & 50 \end{array}$$

$$152.8 \quad 153.0 \quad 152.4 \quad 154.2 \quad 158.8 \quad 161.1 \quad 165.0$$

W. Bank
Creek
Gut.

$$\begin{array}{ccc|ccc} -4.6 & -4.6 & -5.0 & -4.0 & -1.8 & +1.8 & +3.5 & +7.0 \\ \hline 75 & 51 & 30 & 29 & 15 & 15 & 30 & 50 \end{array}$$

$$151.2 \quad 152.2 \quad 151.8 \quad 155.8 \quad 158.0 \quad 158.6 \quad 160.3 \quad 163.8$$

Cargada Way

Sta	B.S.	H.I.	F.S.	Elev		Lt.	¢	Rt.
		160.265						
		166.115						
6+39	P.O.T.		3.5	156.8				
B.M. #1			7.60	152.66	1x1 stake			
				158.51	55' Lt + 5' Rt			
6+50			4.0	156.3				
7+00			5.90	154.4				
7+50			7.1	153.2				
7+50	27' x 2' Top Grate 46' x 45' Heights 82.7 Lt - Fl. Pipe		10.1 10.1 13.2	150.2 150.2 147.1				
T.P.	1.285	154.66	6.89	153.375				
		160.51		159.225				
8+00			3.3	151.4				
8+50			4.9	149.8				

W. Bank Creek

Out.	Out.						
-5.8	-5.0	-5.6	-4.5	-2.2	+1.8	+3.7	+7.0
77	52	33	32	15	15	30	49
150.5	151.3	150.7	151.8	154.1	158.1	160	163.3

W. Bank Creek

Out.	Out.						
-4.6	-2.8	-3.7	-3.8	-3.0	-7.5	+0.3	+2.2
84	56	53	31	30	15	4	30
149.8	151.6	150.7	150.6	151.4	152.9	154.7	156.6
							158.5
							163.2

W. Bank Creek

Out.	Out.						
-4.1	-2.8	-3.8	-3.0	-1.2	+2.2	+8.6	
87	50	31	30	15	15	50	
149.1	150.4	149.4	150.2	152.0	153.4	161.8	

W. Bank Creek

Out.	Out.						
-3.2	-2.0	-2.5	-2.5	-1.8	-1.7	+1.2	+4.2
82	50	45	24	23	15	13	30
148.2	149.4	148.9	148.9	149.6	149.7	151.6	153.6
							159.8

W. Bank Creek

Out.	Out.						
-2.4	-0.5	-0.9	-1.3	-0.4	+1.1	+1.8	+7.5
77	44	39	17	15	15	23	50
149.4	149.3	148.9	148.5	149.4	150.4	151.6	157.3

Canyada Way

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Sta B.S. H.I. F.S. Elev

Lt. E. Rt.

8+93.5 10.2 Lt } Top
 8+97 42.2 Lt } Grate
 End Pipe
 F.L.

9+00 5.6 148.3

9+50 5.5 149.2

T.P. 1.57 150.03
~~154.81~~ 6.20 ~~154.81~~

10+00 1.1 148.9

10+03 17.6 Rt } F.L. Pipe
 30.8 Lt }

10+36³¹ B.C. 1.1 148.9

W. Bank
Creek

-3.8	-2.2	-0.2	-0.6	-0.5	0.0	+0.7	+1.8	+4.6
65	5.8	38	53	13	10	15	30	50
45.3	146.9	148.9	148.5	148.2	149.1	149.8	150.9	153.7

W. Bank
Creek

-2.4	-0.6	-0.5	-0.5	+0.8	+2.0
40	24	5	5	35	50
146.8	148.6	148.7	148.8	150.0	151.4

-3.6	-0.3	-0.5	0.0	+0.5	+2.0
30	23	18	6.0	15	50
145.3	148.6	148.4	148.9	149.4	150.9

Cangada May

Sta.	B.S.	H.I.	F.S.	Elev		L+		R+	
		150.03 148.89							
10+50			1.4	148.6		W. Bank Creek $\frac{-4.5}{39}$	E. Gut. Cangada May $\frac{0.0}{20}$ $\frac{-0.9}{16}$	$\frac{+2.0}{25}$ $\frac{+3.1}{50}$ $\frac{+4.3}{75}$	W. Gut. Quince St. Road $\frac{+4.5}{96}$
						144.1	146.6 147.7	150.6 151.7 152.9	153.1
11+00			2.8	147.2		W. Bank Creek $\frac{-3.5}{56}$	Gut. $\frac{-3.3}{41}$ $\frac{0.0}{17}$ $\frac{-0.3}{15}$	$\frac{+1.6}{25}$ $\frac{+2.0}{55}$	W. Gut. Quince St. Rd $\frac{+2.0}{55}$
						143.7	143.9 147.2 146.9	148.8 149.2	
11+50			4.2	145.8		$\frac{-3.0}{50}$	Gut. $\frac{-0.4}{15}$ $\frac{-0.9}{13}$	Gut. $\frac{0.0}{15}$ $\frac{-0.2}{29}$ $\frac{+7.6}{50}$	
						142.8	145.4 144.9	145.8 145.6 153.4	
B.M. Z			2.38	147.65 143.50	1x1 Huk 25' RT				
12+00			5.2	144.8	11880	$\frac{-2.2}{50}$	Gut. $\frac{-2.2}{35}$ $\frac{-0.8}{13}$	Gut. $\frac{-0.3}{15}$ $\frac{+4.7}{32}$ $\frac{+10.1}{50}$	
						142.6	142.6 144.0	144.5 149.5 154.9	
12+50			6.4	143.6	High Water Flooded Land	$\frac{-1.2}{50}$	Gut. $\frac{-1.1}{25}$ $\frac{-0.4}{14}$	Gut. $\frac{-0.4}{8}$ $\frac{+3.0}{15}$ $\frac{+7.6}{41}$ $\frac{+10}{50}$	
						142.4	142.5 143.2	143.2 147.6 152.2 156.6	
12+91.22 F.C.			7.5	142.5		$\frac{-1.0}{50}$	Gut. $\frac{-1.0}{38}$ $\frac{-0.3}{15}$	Gut. $\frac{-0.3}{9}$ $\frac{+4.0}{29}$ $\frac{+9.3}{50}$	
13+00						141.5	141.5 142.2	142.2 146.5 151.8	

Canyada Way

Sta.	B.S.	H.I.	F.S.	Elev
		150.03 148.88		
13+50			8.2	141.8
14+00			9.1	140.9
14+50			9.6	140.4
T.P.	1.82	142.25 148.06	9.64	140.39 146.24
15+00			2.5	139.8
+50			2.9	139.4
16+00			3.3	139.0

High Water Flood Land

Lt			Rt		
		Ent			Ent
-0.9	-1.4	-0.5	-0.4	+4.0	+11.0
50	30	17	9	23	50
140.9	140.4	141.3	141.4	145.8	152.8
		Ent			Ent
-1.2	-1.2	-0.4	0.0	+1.0	+4.0
50	26	11	11	12	24
139.7	139.7	140.5	140.9	141.9	144.9
		Ent			Ent
-1.0	-1.0	-0.3	-0.6	+0.4	+4.0
50	24	13	11	12	30
139.4	139.4	140.1	139.8	140.8	144.4
		Ent			Ent
-1.0	-0.4		0.0	+4.3	+13.3
50	14		11	28	50
138.8	139.4		139.8	144.1	153.1
		Ent			Ent
-0.6	-0.4		0.0	+5.4	+13.5
50	14		10	26	50
138.8	139.0		139.4	144.8	152.9
		Ent			Ent
0.0	0.0		-0.2	+5.6	+14
50	16		7	27	50
139.0	139.0		138.8	144.6	153.0

Canyada Way

Sta	B.S.	I.I.	F.S.	Elev	Lt.	Rt.
		142.21 148.06				
16+53.59	B.C.		3.9	138.3	$\begin{array}{r} -0.6 \\ \hline 50 \\ \hline 137.7 \end{array}$	$\begin{array}{r} \text{Gut} \\ -0.6 \quad 0.0 \\ \hline 30 \quad 15 \\ \hline 137.7 \end{array}$ $\begin{array}{r} \text{Gut} \\ -0.3 \quad +4.3 \\ \hline 8 \quad 26 \\ \hline 138.0 \end{array}$ $\begin{array}{r} +14.6 \\ \hline 50 \\ \hline 152.9 \end{array}$
17+00			4.2	138.0	$\begin{array}{r} -1.1 \\ \hline 50 \\ \hline 136.9 \end{array}$	$\begin{array}{r} \text{Gut} \\ -0.9 \quad 0.0 \\ \hline 35 \quad 15 \\ \hline 137.1 \end{array}$ $\begin{array}{r} \text{Gut} \\ +0.3 \quad +2.0 \\ \hline 11 \quad 28 \\ \hline 138.3 \end{array}$ $\begin{array}{r} +9.5 \quad +14 \\ \hline 40 \quad 50 \\ \hline 140.0 \end{array}$ $\begin{array}{r} 147.5 \quad 152.9 \end{array}$
17+50			4.5	137.7	$\begin{array}{r} -1.0 \\ \hline 50 \\ \hline 136.7 \end{array}$	$\begin{array}{r} \text{Gut} \\ -0.9 \quad 0.0 \\ \hline 22 \quad 15 \\ \hline 136.8 \end{array}$ $\begin{array}{r} \text{Gut} \\ -0.3 \quad +4.0 \\ \hline 9 \quad 24 \\ \hline 137.7 \end{array}$ $\begin{array}{r} +9.1 \\ \hline 50 \\ \hline 141.7 \end{array}$ $\begin{array}{r} 137.4 \quad 141.7 \quad 146.8 \end{array}$
18+00			4.8	137.4	$\begin{array}{r} +0.4 \\ \hline 50 \\ \hline 137.8 \end{array}$	$\begin{array}{r} \text{Gut} \\ -0.3 \quad -0.3 \\ \hline 27 \quad 14 \\ \hline 137.1 \end{array}$ $\begin{array}{r} \text{Gut} \\ 0.0 \quad +4.4 \\ \hline 13 \quad 21 \\ \hline 137.4 \end{array}$ $\begin{array}{r} +6.0 \\ \hline 50 \\ \hline 143.4 \end{array}$ <p style="text-align: right;">intersect Road</p> $\begin{array}{r} 137.4 \quad 141.8 \quad 143.4 \end{array}$
18+50			5.3	136.9	$\begin{array}{r} -2.2 \\ \hline 50 \\ \hline 134.7 \end{array}$	$\begin{array}{r} \text{W. Bank} \\ \text{Creek} \\ -1.2 \quad -1.2 \\ \hline 24 \quad 14 \\ \hline 135.7 \end{array}$ $\begin{array}{r} \text{Gut} \\ -0.9 \quad 0.0 \\ \hline 25 \quad 14 \\ \hline 136.0 \end{array}$ $\begin{array}{r} \text{Gut} \\ -0.2 \quad +1.7 \\ \hline 15 \quad 40 \\ \hline 136.7 \end{array}$ $\begin{array}{r} +5.5 \\ \hline 50 \\ \hline 142.4 \end{array}$ $\begin{array}{r} 136.7 \quad 138.6 \quad 142.4 \end{array}$
19+00			5.4	136.8	$\begin{array}{r} -1.0 \\ \hline 44 \\ \hline 135.8 \end{array}$	$\begin{array}{r} \text{W. Bank} \\ \text{Creek} \\ -1.2 \quad -1.2 \\ \hline 24 \quad 15 \\ \hline 135.6 \end{array}$ $\begin{array}{r} \text{Gut} \\ -0.5 \quad 0.0 \\ \hline 15 \quad 14 \\ \hline 136.3 \end{array}$ $\begin{array}{r} \text{Gut} \\ 0.0 \quad 0.0 \\ \hline 14 \quad 27 \\ \hline 136.8 \end{array}$ $\begin{array}{r} +1.2 \\ \hline 50 \\ \hline 138.0 \end{array}$ $\begin{array}{r} 136.8 \quad 136.8 \quad 138.0 \end{array}$

Canyada Way

Sta B.S. H.I. F.S. Elev

Lt.

Rt.

142.21

~~148.06~~

139.42

~~146.29~~

136.96

~~142.81~~

T.P. 2.46

5.25

W. Bank
Creek

Gut

Gut

19+50

2.4

137.0

-3.3

-1.3

-0.4

-0.4

-1.0

-0.2

34

27

15

14

31

50

1337

1357

136.6

136.6

136.0

136.8

19+74.03 ^{or} E.C. Bridge

2.4

137.0

20+00 ^{or} Bridge S. End.

2.5

136.9

+0.2

-1.0

-0.2

0.0

0.0

-3.3

50

39

20

15

27

50

137.1

135.9

136.7

136.9

136.9

133.6

20+04.85 B.C.

136.9 ^{H.}
_{L.}

B.M. #3

1.50

137.92

~~143.77~~

E. Side

Bridge

+0.3

-1.0

-0.2

+0.3

+0.15

S.W. Cor

Parapet Wall

50

31

16

27

47

137.2

135.9

136.7

137.2

137.4

20+25

2.8

136.65

~~144.5~~

20+50

3.3

136.1

Gut.

Gut.

+5.3

+3.0

-0.4

-0.2

0.0

0.0

50

27

16

14

29

50

141.4

139.1

135.7

135.9

136.1

136.1

20+75

3.5

135.9

Sta.	B.S.	I.I.	F.S.	Elev
------	------	------	------	------

139.42

~~135.37~~

21+00

3.8

135.6

Fence	Gut	Gut.	Gut.	Gut.
+7.0	+3.0	-0.2	0.0	+1.3
39	18	13	14	15
142.6	138.6	138.4	135.6	136.9

21+25

4.1

135.3

(Note:
T.B. = Top Bank)

21+50

4.3

135.1

Fence	Gut.	Gut.	Gut.	T.B. Lilly Pond
+8.7	+6.3	-0.3	-0.4	-1.0
29	19	13	14	50
143.8	141.4	136.8	134.7	134.1

21+75

4.5

134.9

Fence	Gut.	Gut	Gut	T.B. L. Pond
+8.7	+5.2	-0.3	-0.2	-0.3
26	17	14	13	46
143.3	139.8	136.3	134.4	134.3

22+00

4.8

134.6

22+04

2 Ft. Lt
M.H.

4.64

134.78

See Pg 1 - Book 1520

Δ = 57-12 RT

1+93-68 P.1 EX=28

-12	-145
37	726

DIRECTIONS FOR USE OF TABLE

TABLE No. 1

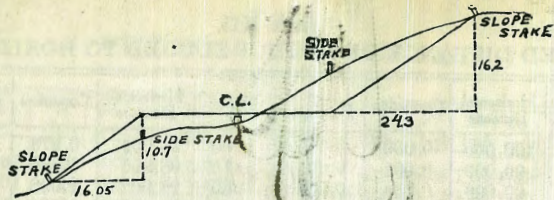
Distances of slope stake from side of roadway...
stake for any width roadway, slope 1:1 to 1:2
If ground is nearly level, the cut or fill at any
stake is located by the double entry method in
left column and top row. The number in body

IMPROVED TABLES

AND

INFORMATION

To find the angle of a curve, or to find the
any other degree, divide by degree of curve and
add correction found in column of correction.
Degree of curve with a given I may be found
by dividing tangent (or versine) by given
given tangent (or versine).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

Handwritten notes on the right page of the notebook:

- 62
- 39-02
- 26-02
- 12-34
- 52220
- 60/2001.420
- 25
- 43-48
- 39-02
- 4-45

1479-64

26+86.13

66

97.89

180.74 = 11 Ave

5440.52

5438.41

79.55

56+17.96 P.1

164.24

1182

166.06

5.25

160.81

2.46

163.27

105.545

1.0169

94.855

1.035

95.890

7.46

88.43

5.415

93.845

0.265

181.50

181.765

12.93

168.835

2.30

171.135

10.63

160.505

5.61

166.115

6.89

159.225

1.285

160.510

6.20

154.310

1.57

155.88

9.64

146.24

10.05

156.29

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155.51

8.78

164.29

.77

163.52

.32

170.83

.02

171.85

0.35

181.50

166.115

7.60

158.515

155.88

2.38

153.50

35

163.27

1150

161.77

1

116.715

2.66

119.375

7.05

112.365

1.54

113.905

8.23

105.675

1.865

107.540

1.33

106.210

8.03

114.200

11.125

103.115

3.43

105.545

181.50

1291.

13324

37.15

94.09

49

87

136

212

5136

72

260.15

21

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7

13.00

50.79

32.67

211.62

1125

55

625

625

625

625

625

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625

2/65.94

32.97

182.10

13.8

168.30

2/65.91

32.955

14+95.86
19+74.52
20.32