

1516

FIELD BOOK

1935

MICROFILMED
DEC 24 1964

ENGINEERING DEPARTMENT,
CITY OF
CALIFORNIA,
DIEGO.

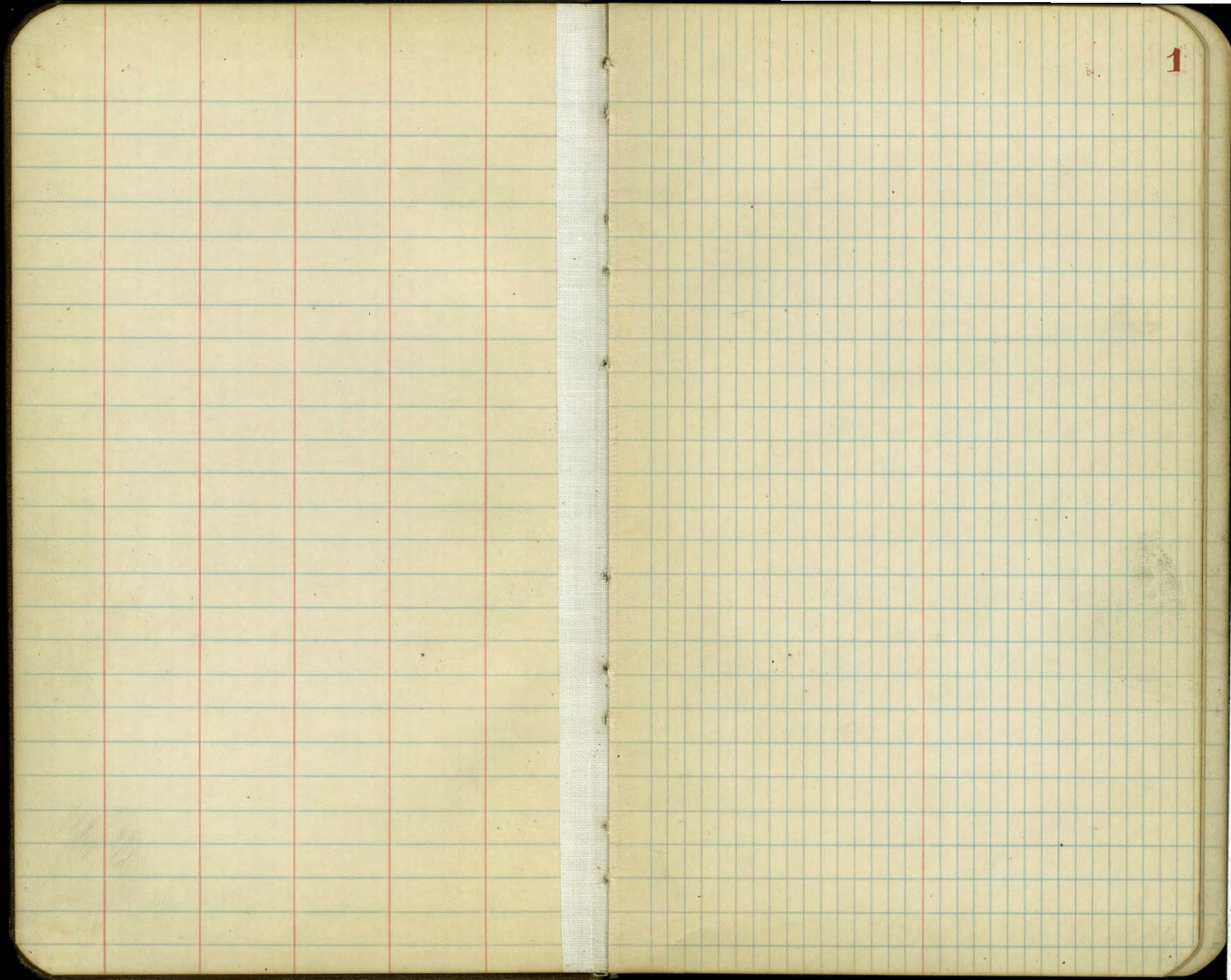
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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
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1

Alignment 12th St. Extension
Russ Blvd. to Calle Colon.

RT

4+01.77	PCC.	11° 55.26'
+50	A 23° 50' 36"	9° 16.74'
3+0	P 561.79	6° 43.79'
+50	T 118.60	4° 10.84'
2+0	L 233.77	1° 37.89'
1+68.00	BC.	

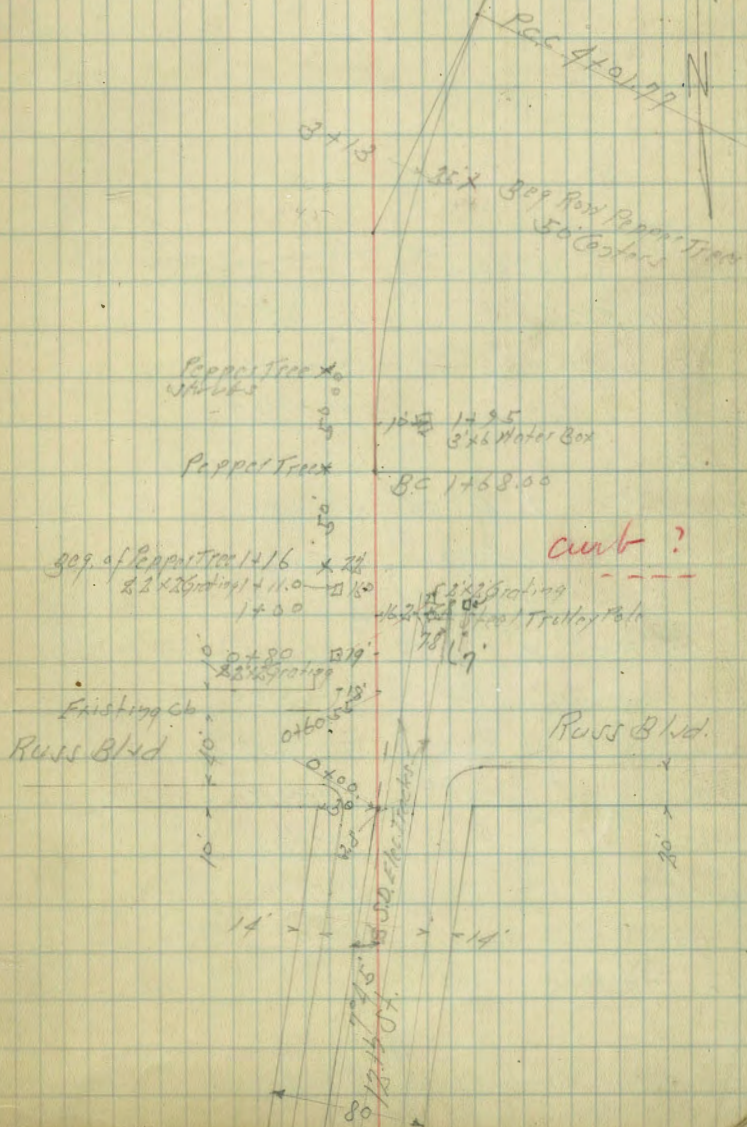
0+00

Indexed
C.S.K.

RAIN
Very Windy
11:00 to 4:00
Heavy Traffic

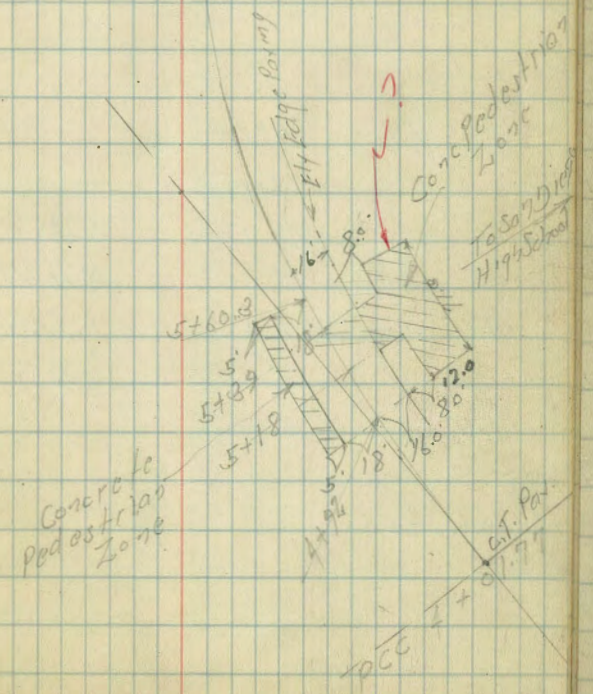
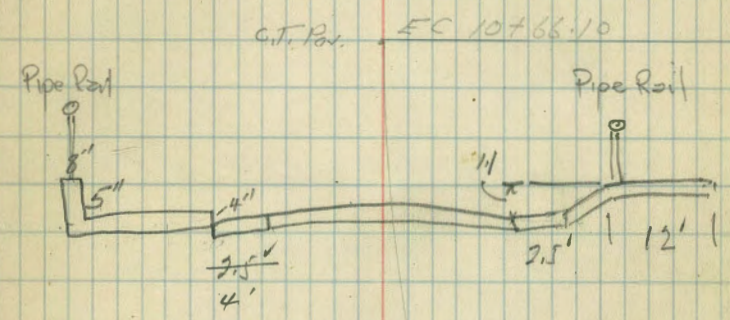
March 19-35
Moore
J. S. S. H.
Northern

2



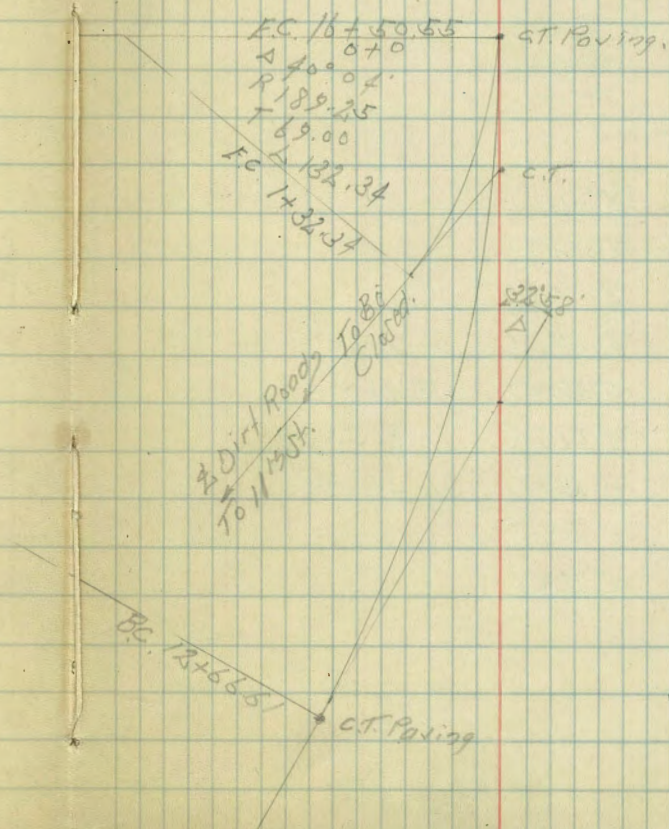
171

666.10	F.C.	20° 02'
+50		19° 32.84'
10+0		18° 02.38'
+50		16° 31.91'
9+0	A 40° 04'	15° 01.45'
+50	R 950.0	13° 30.98'
8+0	T 346.40	12° 00.52'
+50	P.O.C. L 664.33	10° 30.05'
7+0		8° 59.59'
+50		7° 29.12'
6+0		5° 58.66'
+50		4° 28.19'
5+0		2° 57.73'
+50		1° 27.26'
4+01.77	P.C.C.	



L7.

+50.55 E.C.	16° 29'	
16+0	14° 18.41'	
+50	12° 09.66'	Δ 32° 58'
15+0	10° 00.91'	R 667.30
+50	7° 52.16'	T 197.45
14+0	5° 43.41'	L 382.94
+50	3° 34.76'	
13+0	1° 26.01'	
12+66.61 B.C.		



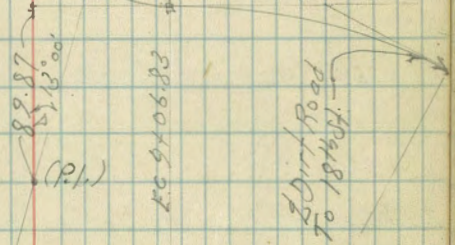
Lt

+28.54	EC	6°30'	
21+0		6°02.74'	
+50		5°14.99'	
20+0		4°27.25'	A 13°00'
+50		3°39.50'	R 1800.0
19+0		2°51.76'	T 205.09
+50		2°04.01'	L 408.41
18+0		1°16.27'	
+50		0°28.52'	
17+20.13	BC.		

EC 21+28.54

C.T. Pnt.

BC 0+0
 L 90°05'
 R 67.68
 T 67.78
 L 106.41



BC 17+20.13 C.T. Pnt.

PL

+61.07	EC		12° 14.75'
+50			11° 55.73'
32+0			10° 30.32'
+50			9° 04.92'
32+0	A	24° 29' 36"	7° 39.52'
+50	R	1006.12	6° 14.12'
31+0	T	218.38	4° 48.72'
+50	L	430.06	3° 23.32'
30+0			1° 57.92'
+50			0° 32.52'

+30.96	PCC		15° 28.58'
29+0			14° 14.83'
+50			12° 16.18'
28+0	A	30° 57' 10"	10° 17.53'
+50	R	724.15	8° 18.88'
27+0	T	200.50	6° 20.73'
+50	L	391.19	4° 21.58'
26+0			2° 22.93'
+50			0° 24.28'
25+39.77	BC		

C.T. Pav.

EC 22+61.87

A 24° 29' 36"

C.T. Pav.

PCC 29+30.96

A 30° 57' 10"

C.T. Pav.

BC 25+39.77

Lt.

40+00.61 EC 4°26.25'

450 3°28.96'

A 8°52.30'

39+0 2°32.43'

R 1520.0'

T 117.95'

450 1°35.89'

L 235.42'

32+0 0°39.36'

37+65.19 BC

EC. 40+00.61

C.T. Pav.

8°23.81'

BC. 37+65.19

C.T. Pav.

35+30.75

73.444

C.T. Pav.

8°19.1'

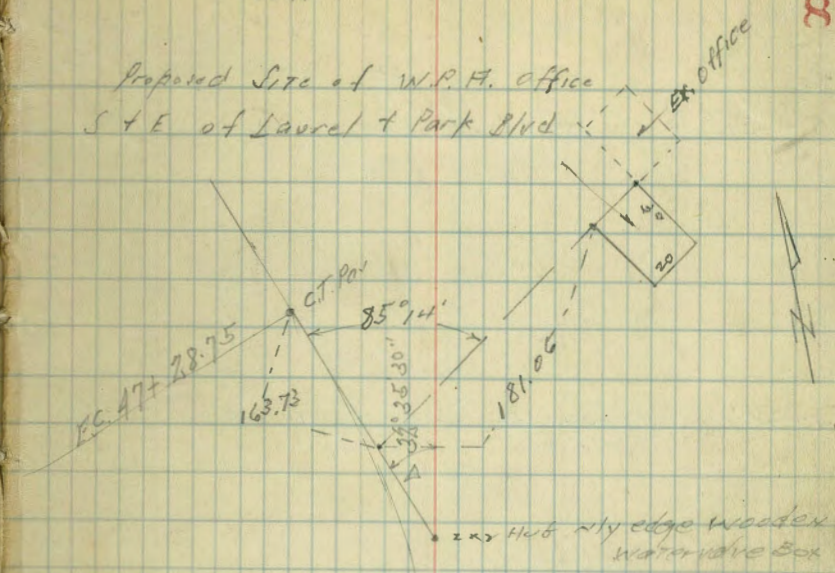
See Page 10 For Sketch

To Parking
To Navy Hospital

4970.38
4728.75
261.43

Lt

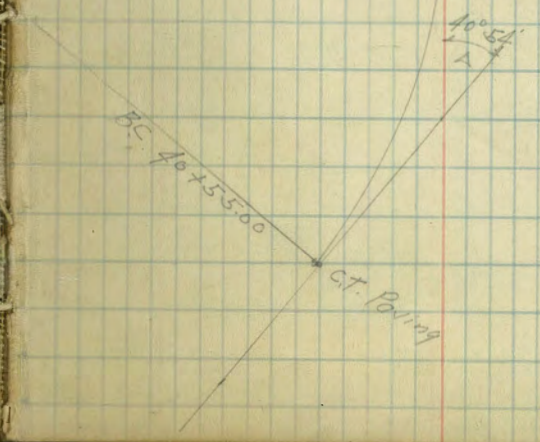
Proposed Site of W.P.H. Office
S + E of Laurel + Park Blvd



+28.75 F.C.	16° 17.75'	
47+0	15° 08.64'	
+50	13° 08.55'	
46+0	11° 08.47'	A 32° 35.30'
+50	9° 08.38'	R 715.67
45+0	7° 08.30'	T 209.22
+50	5° 08.21'	L 407.09
44+0	3° 08.12'	
+50	1° 08.04'	

+21.66 P.C.C.	2° 27'	
43+0	18° 47.32'	A 40° 54'
+50	14° 57.25'	R 373.56
42+0	11° 07.19'	T 139.20
+50	7° 17.12'	L 266.66
41+0	3° 27.06'	C 261.04
40+55.00 B.C.		

P.C.C. 43+21.66 C.T. Poin



55+44.00 RT
Nly edge full paved plaza

53+33.60 Sly edge full width paving of Plaza
and end of existing 30' wide H.C. Pav.

+16.33 EC 8°21.75'

51+0 Δ 16°43'30" 7°25.553'

R 500.0

+50 T 73.50 4°33.65'

L 145.95

50+0 1°41.76'

49+70.38 BC

Existing Curbs

1295.295'

H.C. PAVING

2 Laurel St

59'

19.19 ST. 54+46.62

H.C. PAVING

ST. EC. 51+16.33

16°43'30"

C.T. Pav.

BC. 49+70.38

Cross Section 12th St Extension

Indexed
C.S.N.

March 21-35

Rt Moore
Sisson
Northern **12**

Lt

Δ

Fall
Heavy Traffic

+50

118.1
11.3
20'
117.9
11.5
17'
118.14
11.30
14.6
17.7 Bv

118.33
11.11
15.3
14. Bv
118.67
10.77
20.7
Top of Rail

129.44

TP 12.83 129.44 0.40 116.61

115.6
115.26
115.33
115.74

115.87
115.88
112.71

+10

1.4
20'
1.75
1.7
1.68
1.58

1.14
18'
1.13
18.3
4.30
Top of Rail

Top of Straberry

Top of Rail

+20

112.76
8.05
112.85
2.18
1.09
Top of Grating

+65.5 = End of Cb. on Lt

113.20
3.63
18'
112.98
4.03
18'
112.26
2.77
15.1
17.7 Bv

113.66
3.35

+50

112.46
5.11
20'
11.90
4.55
15'

113.16
2.87
3.77
7.5
3.37
20'

0+0

109.94
7.09
18'
109.56
7.15
18'
Top of Cb

110.55
6.36
07.00
111.28
5.72
18'
Top of Rail

BM 11.54 117.01

117.80
105.47
12th St

117.01

570

134.47
5.43
Top 1000
18.7
Gutter
134.37
5.55
14.7
Fly Pn
134.55
6.30
132.80

134.55
6.16
Edge Pn
20.0
134.2
5.15
135.0

+50

132.4
7.7
20.0
131.9
8.2
17.0
132.13
7.97
14.3
Fly Pn
132.13
7.67

132.17
7.0
15.8
Fly Pn
132.1
8.0
132.5
7.6
20.0

4101.77 P.C.C.

130.1
10.0
20.0
129.7
10.4
17.0
129.8
10.29
14.2
Fly Pn
130.12
9.98
140.10

129.76
10.25
15.7
Fly Pn
129.8
10.2
19.0
130.1
10.0

TP 10.87 140.10 0.21 129.23

+50

127.4
2.0
20.0
127.2
2.2
17.0
127.40
2.94
14.3
Fly Pn
127.71
1.72

127.41
2.0
15.8
Fly Pn
127.2
2.2
18.0
127.6

340

Note: Box Sta 340
25' out same as 20' out

125.2
4.2
20.0
125.0
4.4
17.0
125.20
4.24
18.5
Fly Pn
125.54
3.90

125.27
4.17
15.6
Fly Pn
125.0
4.4
16.0

+50

123.3
6.1
20.0
123.6
6.8
17.0
123.25
6.19
14.8
Fly Pn
123.25
6.19

123.27
6.46
15.4
Fly Pn
122.7
6.7
20.0

240

121.1
8.3
20.0
120.4
9.0
17.0
120.55
8.79
13.0
Fly Pn
120.82
8.62
129.41

120.57
8.27
13.3
Fly Pn
120.6
8.8
20.0
121.21
8.23
27.4
Top Pn

129.44

Lt

2d

Rt

+50

146.6
6.2
20

146
6.7
18

146.20
6.55
15.3
Fly Pnl

146.25
6.80

146.15
6.60
14.8
Fly Pnl

146.1
6.7
18

146.8
6.0
20

7+0

144.3
8.5
20

143.8
9.0
18

143.89
8.86
15.1
Fly Pnl

144.11
8.64

143.86
8.89
15.1
Fly Pnl

143.8
9.0
18

144.1
8.4
20

+79 - Existing 2x2 lot on Rt

142.61
10.14
19
on Grating

139.61
13.14
Fly Pnl

+71 - Existing lot on Lt 2x2

138.09
14.66
Fly Pnl

142.09
10.66
18.5
on Grating

141.84
10.91

141.56
11.19
15.3
Fly Pnl

141.5
11.2
19

142.1
10.9
22

+50

141.9
10.9
20

141.6
11.2
18

141.62
11.2
14.8
Fly Pnl

152.75

141.56
11.19
15.3
Fly Pnl

141.5
11.2
19

142.1
10.9
22

IP 12.92 152.75 0.27 139.83

6+0

139.5
0.6
20

139.1
1.0
18

139.29
0.81
14.6
Fly Pnl

139.56
0.54

139.27
0.83
15.3
Fly Pnl

139.1
1.0
20

139.7
0.6
22

5+50

137.07
3.03
18
Top Hole Gut

136.76
3.24
18
Gut

136.91
3.19
14.3
Fly Pnl

137.21
3.89

136.86
3.14
15.5
Fly Pnl

136.8
3.3
20

137.3
3.2
22

140.10

140.10

J-22-35
 Pt. Fair 15
 Heavy Traffic

Lt. 2

+50					161.2	160.6	160.7	160.76	160.70	160.6	161.0	✓
					5.6 20	4.5 18	4.4 15.0 Fly Bar	0.79	4.05 15.0 Fly Bar	4.2 18	2.8 20	P
10+0					158.6	158.1	158.19	158.46	158.22	158.1	158.7	✓
					6.2 20	6.7 18	6.56 15.0 Fly Bar	1.29	6.53 15.0 Fly Bar	6.7 18	6.1 20	P
+67	21.5 Lt. 2" Stand Pipe											
+50					156.0	155.7	155.75	156.09	155.67	155.6	156.2	✓
					8.8 20	9.1 18	9.00 15.0 Fly Bar	9.66	9.08 14.7 Fly Bar	9.2 18	8.6 20	P
9+0					153.7	153.3	153.32	153.57	153.31	153.2	153.8	✓
TP	12.75	164.75	0.75	152.00	11.1 20	11.5 18	11.43 15.2 Fly Bar	11.15	11.44 14.8 Fly Bar	11.6 18	11.0 20	P
								164.75				
+50					151.2	150.8	150.93	151.16	150.88	150.7	151.0	✓
					1.6 20	2.0 18	1.82 15.3 Fly Bar	1.59	1.82 14.8 Fly Bar	2.1 18	1.8 20	P
8+0					149.0	148.5	148.47	148.76	148.49	148.4	149.1	✓
					3.8 20	4.3 18	4.28 15.2 Fly Bar	2.99	4.26 14.7 Fly Bar	4.4 18	3.7 20	P
								152.75				

152.75

152.75

+66.61 BC Lt

+50

12+0

+50

TP

11+0

10+66.10 EC

164.75

1248 176.97 026 164.49

161.7	161.91	161.50	161.70	161.45	161.4	161.8
2.9	3.2	3.25	3.05	3.30	3.4	3.0
20	18	15.0	15.0	15.1	18	20
		Wly Par		Wly Par		
163.1	163.1	163.18	163.10	163.11	163.0	163.4
12	17	1.57	1.35	1.4	1.8	1.4
20	18	15.0		15.2	18	20
		Wly Par		Wly Par		
165.0	165.21	165.62	165.91	165.58	165.5	165.9
11.0	11.5	11.25	11.13	11.39	11.5	11.1
20	18	15.0		15.7	18	20
		Wly Par		Wly Par		
168.4	168.1	168.12	168.39	168.06	167.9	168.4
8.6	8.9	8.85	8.58	8.91	9.1	8.6
20	18	14.7		15.3	18	20
		Wly Par		Wly Par		
170.6	170.6	170.58	170.84	170.60	170.5	171.0
6.4	6.39	6.39	6.13	6.37	6.5	6.0
20	17	14.6		15.3	18	20
		Wly Par		Wly Par		
171.1	171.1	171.35	171.67	171.10	171.3	171.7
5.9	5.7	5.67	5.30	5.57	5.7	5.9
20	17	14.9		15.2	18	20
		Wly Par		Wly Par		

✓ P

✓ P

✓ P

✓ P

✓ P

✓ P

1570

1813	1808	1808	18125	18089	1808	1812
7.6	8.1	7.95	7.66	8.02	8.1	7.7
20	18	14.3		16	19	20
		Wly Pav				

+50

1796	1792	1793	17961	17937	1792	1797
9.6	9.7	9.42	9.30	9.54	9.7	9.2
20	19	15.3		14.3	18	20
		Wly Pav		Fly Pav		

1470

1779	1773	1771	17789	17760	1771	1771
11.0	11.6	11.22	11.02	11.31	11.4	11.0
20	19	16.5		13.9	17	20
		Wly Pav		Fly Pav		

188.91

TP

12.25 188.91" 0.31 176.66

+50

1752	1754	1751	17527	17550	1754	1759
1.4	1.6	1.49	1.20	1.42	1.6	1.1
20	17	16.4		13.8	17	20
		Wly Pav		Fly Pav		

+03 Existing Culv 2'x2 Grating

1731	1728	1731	17333	17308	1729	1734
3.2	4.34	3.96	3.64	4.07	4.1	3.6
20	20	14.6		18.5	18	20
		Wly Pav		Flowline		
		0.2 Grating		0.2 Grating		

1370

176.97

176.97

P ✓ P ✓ P ✓ P ✓ P ✓ P ✓

+72 20' Lt - 2" FireHyd.

+50.55 EC = Existing Inlet on Rt.

185.81	185.72	185.58	185.45	185.1	185.02	183.04
3.2	3.7	3.1	3.26	3.50	3.23	5.87
20'	18'	15.2		15'	19'	FL 10" Pipe
		Wly Pav.		FLy Pav.	2x2 Grating	

+20 - Existing Inlet on Lt 2x2 Grating 10" Pipe

181.1	184.17					
7.90	4.74					
FL	19'					
	2x2 Grating					

16+0

178	183	183	184.2	184.1	184.7	
4.8	5.2	5.00	4.70	4.72	4.2	
20'	18'	15.2		19'	20'	
		Wly Pav.		FLy Pav.		

+65 - Existing Inlet on Rt 2x2 Grating

184.29	181.02	
6.52	7.88	
19'	FL 6" Pipe	
2x2 Grating		

15+50

182.8	182.41	182.66	182.8	182.3	182.8	
6.7	6.50	6.25	6.63	6.6	6.1	
20'	17.7		15.4	18'	20'	
	Wly Pav.		FLy Pav.			

188.91

188.91

+50

1921	1916	1911	1921.5	191.84	191.7	1921
9.8	10.3	10.13	9.77	10.08	10.2	9.8
20	18	15.3		15.2	18	20
		11/4 Pa.		11/4 Pa.		

1870

1904	1900	19004	19004	18958	1900	1901
11.5	11.9	11.88	11.56	11.94	11.9	11.5
20	18	15.1		15.3	18	20
		11/4 Pa.		11/4 Pa.		

+50

1887	1883	1888	1883	1883	1884	1887
13.2	13.6	13.45	13.11	13.44	13.5	13.2
20	18	15.3		15	18	20
		11/4 Pa.		11/4 Pa.		

TP 13.27 201.92 ✓ 0.26 188.65 ✓

201.92 ✓

+20.13 BC. 47

1878	1878	1874	1870	1877	1873	1876
1.1	1.5	1.44	1.11	1.44	1.6	1.3
20	18	15.2		14.5	18	20
		11/4 Pa.		11/4 Pa.		

1770

1871	1867	1863	1871.6	1868	1868	1870
1.8	2.4	2.08	1.75	2.11	2.1	1.9
20	18	15		15	18	20
		11/4 Pa.		11/4 Pa.		

18891 ✓

18891

Cont Page 22

TP 1301 214.78 0.15 201.77

2140

BM #2

7.50

2040

7.50

1910

201.92

198.53
PP Jot X 198.53
40' R 19.125

201.92	201.92	201.92	201.92	201.92	201.92	201.92
194.5	194.5	194.5	194.5	194.5	194.5	194.5
2.4	2.7	2.65	2.44	2.39	2.09	
20	18	15	15	15	20	
		fly Par		fly Par	on Par	
197.6	197.6	197.6	197.6	197.6	197.6	197.6
4.3	4.7	4.55	4.27	4.54	4.5	
20	18	15	15	15	20	
		fly Par		fly Par		
195.1	195.1	195.1	195.1	195.1	195.1	195.1
6.2	6.5	6.41	6.17	6.53	6.6	
20	18	15	15	15	20	
		fly Par		fly Par		
193.8	193.8	193.8	193.8	193.8	193.8	193.8
7.8	8.36	7.93	8.24	8.4	8.0	
20	15	15	15	18	20	
	fly Par		fly Par			

201.92

P ✓

P ✓

F

P ✓

P ✓

Levels Cut off to 18th St

See Sketch Page 5

21

1+06.41 = 2+06.83 2.2 199.7

1+02 Top E Rail 2.15 199.77

+80 Top W Rail 2.07 199.85

+65 1.8 200.1

+53.2 2.6 199.3

0+0 1.21 200.71

201.92 Bt Ford.

2340

08.3	08.0	08.01	08.21	08.02	08.0	08.4
6.5 20'	6.8 18'	6.72 15.2 Fly Pav	6.57	6.76 15.1 Fly Pav	6.8 18'	6.4 20'

750

00.6	06.4	08.47	06.70	06.51	06.5	07.1
8.2 20'	8.4 17'	8.21 15.1 Fly Pav	8.08	8.27 15.2 Fly Pav	8.3 18'	7.7 20'

2240

05.2	04.7	04.85	05.07	04.98	04.7	04.54
9.6 20'	10.1 18'	9.93 15.2 Fly Pav	9.71	9.86 15.1 Fly Pav	9.9 18'	9.4 20'

750

03.4	02.9	02.99	03.17	03.07	03.0	03.8
11.4 20'	11.9 18'	11.79 15.1 Fly Pav	11.59	11.71 15.1 Fly Pav	11.8 17'	11.2 20'

+ 28.54 FC

02.5	02.2	02.28	02.41	02.25	02.3	03.0
12.2 20'	12.6 18'	12.55 15.0 Fly Pav	12.37	12.53 15.1 Fly Pav	12.5 18'	11.8 20'

21422 = Existing Inlet 16.5 ft 15" x 15" Grating

21478'

12.77
18.5
02 Grating

21478 -

LH

R

RT

22

Lt

Rt

RA

23

+39.77 BC PA

14.05	14.3	14.24	14.43	14.23	14.2	14.6
0.3 20	0.15 18	0.52 15.2 Fly Par	0.35	0.55 15.2 Fly Par	0.6 18	0.2 20

25+0

13.9	13.5	13.58	13.73	13.56	13.4	13.7
0.9 20	1.1 18	1.2 15.2 Fly Par	1.05	1.22 15.2 Fly Par	1.4 18	1.1 20

+7.5 - Existing 12' x 18" Grating 19' Lt.

10.63	10.75	10.83	10.93	10.83	10.6	10.5
4.15 Fly Par	2.0 19	2.03	2.03	2.03	2.03	2.03

25+0

12.8	12.4	12.46	12.58	12.46	12.8	12.6
2.0 20	2.4 18	2.32 15.2 Fly Par	2.20	2.22 15.2 Fly Par	2.5 18	2.2 20

24+0

11.3	10.9	11.09	11.24	11.16	11.1	11.5
3.5 20	3.9 18	3.69 15.2 Fly Par	3.54	3.62 15.1 Fly Par	3.7 18	3.3 20

23+50

0.92	0.94	0.954	0.978	0.953	0.95	1.0
5.0 20	5.4 18	5.24 15.2 Fly Par	5.00	5.25 15.1 Fly Par	5.3 18	4.8 20

214.78'

214.78'

					LT	Z	RT				
+50					17.9 6.8 20	17.6 7.1 18	17.60 6.98 15.6 Fly Par	17.75 7.14 14.7 Fly Par	17.59 7.2 18	18.0 6.7 20	P ✓
27+0					17.0 7.7 20	16.7 8.0 18	16.83 7.90 15.6 Fly Par	16.96 7.77 14.9 Fly Par	16.78 8.0 18	17.1 7.6 20	P ✓
+50					16.2 8.5 20	15.9 8.8 18	16.03 8.70 15.3 Fly Par	16.16 8.57 14.9 Fly Par	16.03 8.8 18	16.3 8.4 20	P
26+0					15.6 9.1 20	15.2 9.5 18	15.26 9.48 15.2 Fly Par	15.47 9.26 15.0 Fly Par	15.27 9.46 18	15.6 9.1 20	P ✓
25+50					14.7 10.0 20	14.4 10.3 18	14.43 10.30 15.2 Fly Par	14.61 10.12 15.2 Fly Par	14.3 10.4 18	14.7 10.6 20	P ✓

TP

10.20

224.73

0.25

214.55

224.73

214.78

	LT	RT	PT	
+50	22.3 2.4 20	21.9 2.8 18	22.03 2.70 15.6 Fly Par	22.21 2.52 2.67 14.6 Fly Par
+30.96 PCC	21.8 2.9 20	21.4 3.3 18	21.48 3.25 15.6 Fly Par	21.65 3.68 3.30 14.6 Fly Par
29+0	20.9 3.8 20	20.2 4.5 18	20.60 4.13 15.6 Fly Par	20.55 3.95 4.18 14.8 Fly Par
+93 - Existing Culvert 1.5 x 1.5 Grating	17.63 7.10 FL 10" Pipe	20.18 4.55 19.5 embanking		20.18 4.90 19 Grating 8" Pipe
+50	19.6 5.1 20	19.3 5.4 18	19.40 5.33 15.6 Fly Par	19.60 5.13 5.33 14.8 Fly Par
28+0	18.6 6.1 20	18.3 6.4 18	18.59 6.34 15.5 Fly Par	18.57 6.16 6.33 14.7 Fly Par
224.73 ✓				224.73 ✓

750

3270

750

3170

750

TP

3070

11.75 236.04 0.44 224.29 ✓

224.73

32.4	32.1	32.18	32.43	32.18	32.0	32.6
3.6	3.9	3.86	3.61	3.86	4.0	3.4
20	18	15.3 Fly Par		14.9 Fly Par	18	20
30.7	30.8	30.49	30.84	30.44	30.4	31.0
5.3	5.7	5.55	5.46	5.60	5.6	5.0
20	18	15.4 Fly Par		14.9 Fly Par	18	20
270	286	287	28.94		286	27.1
7.0	7.4	7.32	7.10	7.36	7.4	6.9
20	18	15.6 Fly Par		14.7 Fly Par	18	20
27.3	26.8	26.97	27.4	27.19	26.9	27.4
8.7	9.2	9.07	8.90	9.05	9.1	8.6
20	18	15.7 Fly Par		14.6 Fly Par	18	20
25.3	25.2	25.32	25.50	25.34	25.2	25.6
10.7	10.8	10.72	10.54	10.70	10.8	10.4
20	18	15.6 Fly Par		14.9 Fly Par	18	20
23.9	23.6	23.6	23.75	23.56	23.4	24.0
0.8	1.2	1.13	0.98	1.17	1.3	0.7
20	18	15.6 Fly Par		14.6 Fly Par	18	20
			224.73			

Lt

Δ

PT

P ✓

P ✓

P ✓

P ✓

P ✓

P ✓

+32 Existing Inlet

36.14
12.58
FL

38.14
10.58
19.3
on grading

+12 Existing Inlet

37.7

37.3

37.40

37.64

37.38

34.38

34+0

11.0
20

11.4
18

11.32
15.0
Fly Pav

11.08

11.43
15.4
Fly Pav

11.5
18

11.3
20

36.5

36.1

36.07

36.27

35.97

35.9

36.2

+61.02 FC

12.2
20

12.6
18

12.65
15.2
Fly Pav

12.45

12.75
15.2
Fly Pav

12.8
18

12.5
20

TP 13.01 248.72 ✓ 0.33 235.71 ✓

248.72 ✓

+50

0.1
20

0.5
18

0.32
15.1
Fly Pav

0.10

0.40
15.4
Fly Pav

0.6
18

0.2
20

34.3

33.8

33.72

34.19

33.91

33.8

34.3

33+0

1.7
20

2.2
18

2.12
15.2
Fly Pav

1.85

2.13
15.2
Fly Pav

2.2
18

1.7
20

236.04 ✓

236.04 ✓

P

✓

P

✓

P

✓

P

P

P

✓

3770

50.2	47.8	47.76	47.98	47.61	47.5	48.0
18.0 25	19.4 20	19.45 15.3 Wly Pav	12.23	12.60 15.2 Fly Pav	12.7 18	12.2 20

TP 12.22 260.21 0.73 247.99

46.6	46.3	44.01	46.21	45.84	45.7	46.13	46.1
0.1 25	2.1 20	2.71 15.2 Wly Pav	2.51	2.88 15.2 Fly Pav	3.0 18.6 Gutter	2.59 18.6 TopCb	2.6 20

+50

3670

46.3	44.4	44.29	44.46	44.09	44.0	44.38
2.4 25	4.3 20	4.43 15.2 Wly Pav	4.27	4.68 15.3 Fly Pav	4.7 18.5 Gutter	4.34 18.5 TopCb

BM #3

4.01 244.71 27.8' Lt 35+50 Nail Top Cont Nail

+50

42.6	42.50	42.60	42.12	42.05
6.1 20	6.22 15.2 Wly Pav	6.12	6.60 15 on Pav	6.67 20 on Pav

3570

39.80	39.2	39.10	39.29	38.85	38.6	39.06	39.1
7.8 20	10.9 7.8 20	9.77 7.93 15 Wly Pav	7.82	8.35 15 on Pav	8.37	8.51 20 on Pav	8.51 20

34750

8.99	9.5	9.62	9.43	9.87	10.1	9.66	9.6
20 TopCb	20	15.7 Wly Pav		15.7 Fly Pav	28.4	18.4 TopCb	20

248.72

248.72

3910

54.5	54.8	54.8	54.8	54.8	54.83
65 25	57.2 15 Fly Par	58.5	55.2 15 Fly Par	65.8 20 Fly Par	P

+82

540	53.90	5420	54.07	53.97	
62 25	6.31 15 Fly Par	6.01	6.17 15	6.24 20 Fly Par	P

+60 Peppertrees Ends on East

+50

53.1	52.87	53.18	52.87	52.8	53.3
7.1 25	7.32 15.2 Fly Par	7.03	7.34 15.1 Fly Par	7.4 18	6.9 20

3810

521	51.6	51.12	51.43	51.4	51.0	51.4
8.1 25	8.6 20	9.10 15.2 Fly Par	8.78	9.07 15.1 Fly Par	9.2 18	8.8 20

+65.19 BC Lt

512	54.2	49.96	52.27	49.88	49.7	50.2
9.0 25	9.8 20	10.25 15.2 Fly Par	9.99	10.33 15.2 Fly Par	10.5 18	10.0 20

37150

50.9	47.8	49.8	47.4	49.35	47.3	47.8
9.3 25	14.4 20	16.73 15.2 Fly Par	10.47	10.86 15.2 Fly Par	10.9 18	10.4 20

26021

26021

4140

TP 1272 272.66 0.27 259.94 ✓

+5500 BCL

+50

40 + 0061 FC

+50

39 + 23

260.21 ✓

41

61.1

11.6
25

596

0.6
25

594

0.8
25

577

2.5
25

55.9

4.3
25

61.4

11.52
15
Fly Pw

5970

0.51
15.6
Fly Pw

59.51

0.70
15.5
Fly Pw

5771

2.50
15
Fly Pw

56.12

4.09
15
Fly Pw

42

61.51

11.15

273.66 -

597

0.24

59.81

0.40

5815

2.06

56.47

3.74

4.50

260.21 ✓

PT

61.71

10.95
14.3
Fly Pw

60.18

0.03
14.6
Fly Pw

59.99

0.27
14.0
Fly Pw

5803

2.18
15.4
Fly Pw

4.35

4.07
15
Fly Pw

57.71

4.81
154.69
20 = Fly King

30

61.4

11.2
20

59.9

0.3
20

59.8

0.4
20

577

2.5
20

56.2

4.0
20

57.71

4.69
20 = Fly King

450

Lt
2
500
69.92.84
1.96
Fly Par
69.822
70.19
~~66.19~~
2.472.33
1.57
Fly Par
70.332.9
1.0
70.0

421.66 P.C.C.

2
25
68.93.90
1.51
Fly Par
68.763.57
69.093.34
1.52
Fly Par
69.323.9
1.0
69.0

4340

2
25
68.14.63
1.51
Fly Par
68.034.38
68.284.18
1.51
Fly Par
68.984.3
1.0
68.4

450

2
50
66.36.39
1.55
Fly Par
65.276.15
66.615.86
1.50
Fly Par
66.806.0
1.0
66.7

4270

2
50
68.48.14
1.50
Fly Par
64.527.81
64.857.51
1.50
Fly Par
65.157.6
1.0
65.1

41750

2
50
62.59.88
1.50
Fly Par
62.789.45
63.219.22
1.47
Fly Par
63.449.6
1.0
63.1

272.66

272.66

LT

Z

PH

78.4	78.63	78.86	78.61	78.5
5.4 25	5.14 14.4 Fly Paw	4.91	5.16 15.9 Fly Paw	5.2 20
77.6	77.78	77.96	77.76	77.5
6.2 25	5.99 14 Fly Paw	5.81	6.01 16.2 Fly Paw	6.6 20
76.5	76.53	76.68	76.41	76.4
7.2 25	7.24 13.7 Fly Paw	7.09	7.36 16.2 Fly Paw	7.4 20
75.0	75.22	75.38	75.08	75.0
8.8 25	8.55 13.6 Fly Paw	8.39	8.69 16.5 Fly Paw	8.8 20
73.3	73.32	73.68	73.51	73.3
10.5 25	10.45 13.9 Fly Paw	10.09	10.26 16.3 Fly Paw	10.5 20
71.7	71.67	72.03	71.94	71.7
1.0 25	0.97 14.2 Fly Paw	0.63	0.72 16.8 Fly Paw	1.0 20
272.28	272.66	272.66		

+50

4670

+50

4570

+50

TP 11.49 283.77 0.38 272.28

4440

272.66

P ✓
P ✓
P ✓
P ✓
P ✓
P ✓
P ✓

4910

80.6	80.89	81.06	80.77	80.8
3.3	3.88	2.71	3.00	3.0
15	15	15	15	20
W/P	W/P		FLY/P	

450

80.3	80.52	80.67	80.49	80.2
3.5	3.25	3.10	3.28	3.6
15	15	15	15	20
W/P	W/P		FLY/P	

4810

79.8	80.17	80.33	80.12	80.1
4.0	3.60	3.44	3.65	3.7
15	15	15	15	20
W/P	W/P		FLY/P	

450

79.3	79.76	79.89	79.72	79.8
4.5	4.01	3.88	4.05	4.0
15	15	15	15	20
W/P	W/P		FLY/P	

42875 EC.

79.3	79.55	79.70	79.55	79.5
4.5	4.22	4.07	4.22	4.2
15	15	15	15	20
W/P	W/P		FLY/P	

4710

79.0	79.27	79.45	79.22	79.2
4.7	4.48	4.32	4.55	4.6
15	15	15	15	20
W/P	W/P		FLY/P	

283.77

283.77

4K 8 Pt

716.33 EC

81.8
5.6
20
21.7
5.7
25
81.5
5.9
25
81.3
6.1
25
81.0
6.4
25
81.0
2.8
25

82.25
5.5
15.4
Fly Pt
82.14
5.26
15.4
Fly Pt
81.84
5.56
15.4
Fly Pt
81.58
5.82
15.4
Fly Pt
81.27
6.13
15.4
Fly Pt
81.12
2.65
15.4
Fly Pt

82.40
5.00
82.36
5.04
82.05
5.35
81.72
5.68
81.50
5.90
81.37
2.40

82.17
5.90
1.26
Fly Pt
82.12
5.28
1.26
Fly Pt
81.81
5.59
1.57
Fly Pt
81.46
5.94
1.57
Fly Pt
81.22
6.18
1.57
Fly Pt

82.2
5.2
20
82.1
5.5
20
81.8
5.6
20
81.4
6.0
20
81.1
6.3
20
81.0
2.8
20

P ✓

P ✓

P ✓

P ✓

P ✓

P ✓

51+0

750

50x0

770.38 BC Pt.

TP 6.24 28740 2.61 281.16 ✓

49+50

282.77 ✓

283.77 ✓

BM 9.97 28308 ^{NW 3/4} ^{County} ^{Park Blvd} ²⁸³²⁸

TP 9.31 29305 366 28374 ✓

+33 - 1/4 Eder Full Width Pavise
1/2 of slope and end of 30' strip paving

53+0

+50

52+0

51+50

28740 ✓

28740 ✓

82.60	82.68	82.84	83.00	83.00
1.80 25 on Pav.	4.72 15 on Pav.	4.56	4.40 15	4.40 20 on Pav. ✓
82.4	82.55	82.92	82.85	83.0
5.0 25	4.75 15 on Pav.	4.48	4.55 12.7 on Pav.	4.4 ✓
82.3	82.55	82.85	82.67	82.8
5.1 25	4.85 15 on Pav.	4.55	4.73 14.6 on Pav.	4.6 ✓
82.1	82.49	82.69	82.48	82.5
5.2 25	4.91 15 on Pav.	4.71	4.92 14.6 on Pav.	4.9 ✓
82.0	82.32	82.49	82.27	82.3
5.4 25	5.08 15 on Pav.	4.91	5.13 14.6 on Pav.	5.1 ✓

+ 89.30 - Sly Edge Full Width end of existing
Paving End Project
35.1 strip paving

20.46	89.89	89.89	89.84	89.81	89.86	89.88	90.44
3.58	3.16	3.20	3.21	3.24	3.19	3.17	3.18
36	36	29.5	35	35	19.8	29.5	38
TopCb	TopCb	TopCb	TopCb	TopCb	TopCb	TopCb	TopCb

+ 79.30 - opp New Cb B.C

90.16	89.86	89.80	89.71	90.30
3.59	3.19	3.25	3.24	3.25
29.5	15.3	14.8	19.8	29.5
TopCb	TopCb	TopCb	TopCb	TopCb

+ 50

90.29	89.67	89.50	89.52	90.10
3.76	3.38	3.25	3.53	3.23
29.5	15.3	14.8	19.8	29.5
TopCb	TopCb	TopCb	TopCb	TopCb

55x0

99.02	89.40	89.65	89.27	89.85
3.03	3.65	3.36	3.78	3.20
29.5	15.3	14.8	19.8	29.5
TopCb	TopCb	TopCb	TopCb	TopCb

+ 50

89.78	89.12	89.41	88.85	89.50
3.27	3.92	3.64	4.20	3.55
29.5	15.3	14.8	19.8	29.5
TopCb	TopCb	TopCb	TopCb	TopCb

58x0

89.51	88.87	89.18	88.71	89.30
3.54	4.18	3.87	4.44	3.75
29.5	15.3	14.8	19.8	29.5
TopCb	TopCb	TopCb	TopCb	TopCb

293.05

293.05

see page 40 for sketch
 Laurel to Calle Colon

BM #2		12.69	198.48	5 PM 1911/29 Post 40' 19185 198.53
TP	0.50	211.17	11.56	210.67
TP	0.53	222.23	12.77	221.70
TP	0.36	234.47	12.56	234.11
BM #3		1.97	244.70	Hail Top Conc. Hail 278 at 334.50 244.71
TP	0.29	246.67	12.95	246.38
TP	0.18	259.33	12.45	259.15
TP	0.30	271.60	11.84	271.30
TP	1.74	283.14	5.90	281.40
TP	4.22	287.30	9.97	283.08
		293.05		

Sketch of existing F.C. paving
and old + new curbs on 14th St Ext.
between Laurel + Calle Colon.

59+87.30 End of Project and end of 35.1
strip paving

59+79.30 new cb P.C.

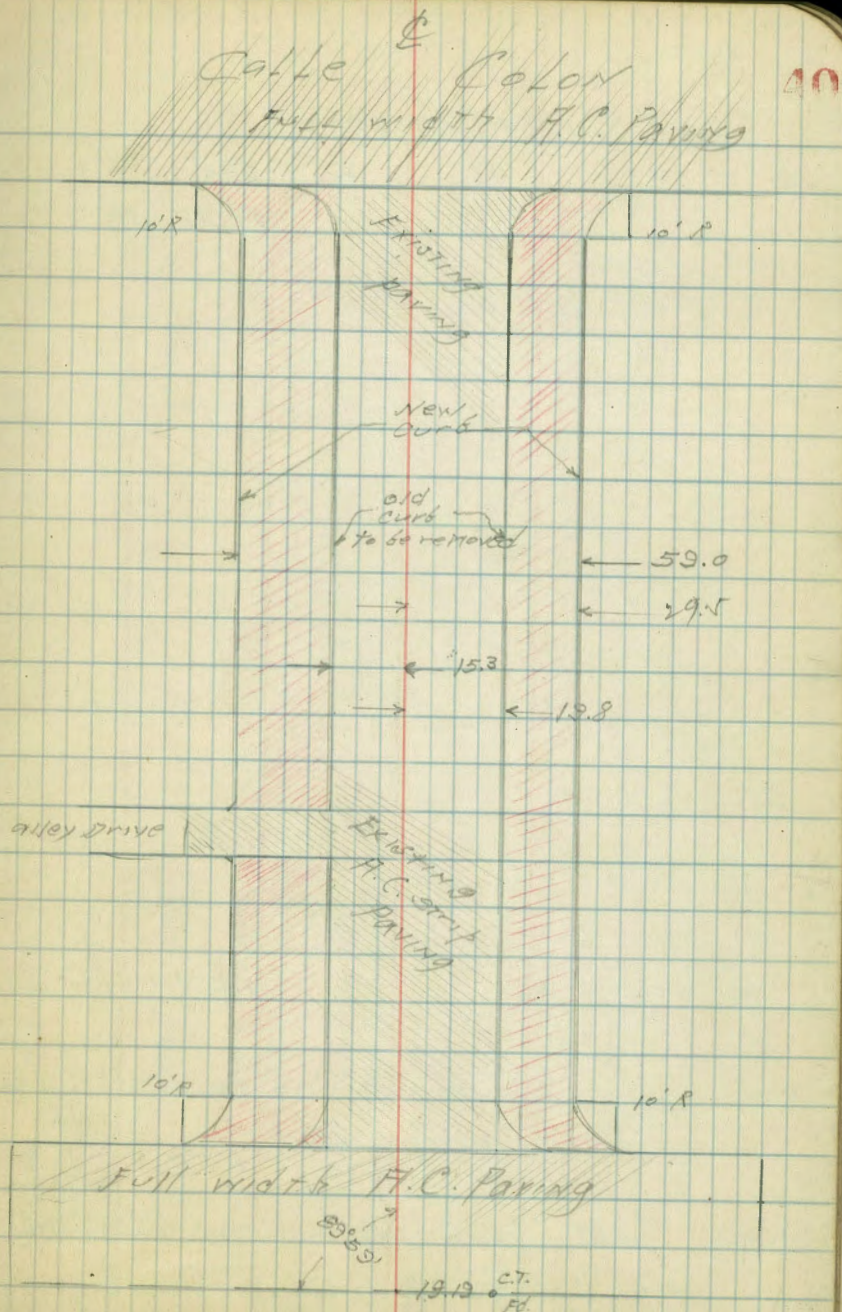
area in red hatching
NOTE - already subgraded
for 6" paving

56+93.5
56+80

55+54 New curb P.C.

55+44 beginning of 35.1 strip paving

54+46.00 @ Laurel St.



Rail Elevations

$\frac{3}{2}$	+	HJ	-	Elev
				WR WR ER ER
450				123.76 274 309 297 311
200				123.41 5.32 5.53 5.27 5.40
1450	8.08	126.56		118.52 7.98 7.98 7.86 7.86

Gutter below Tracks 6.79

± Pave at 1450 118.42

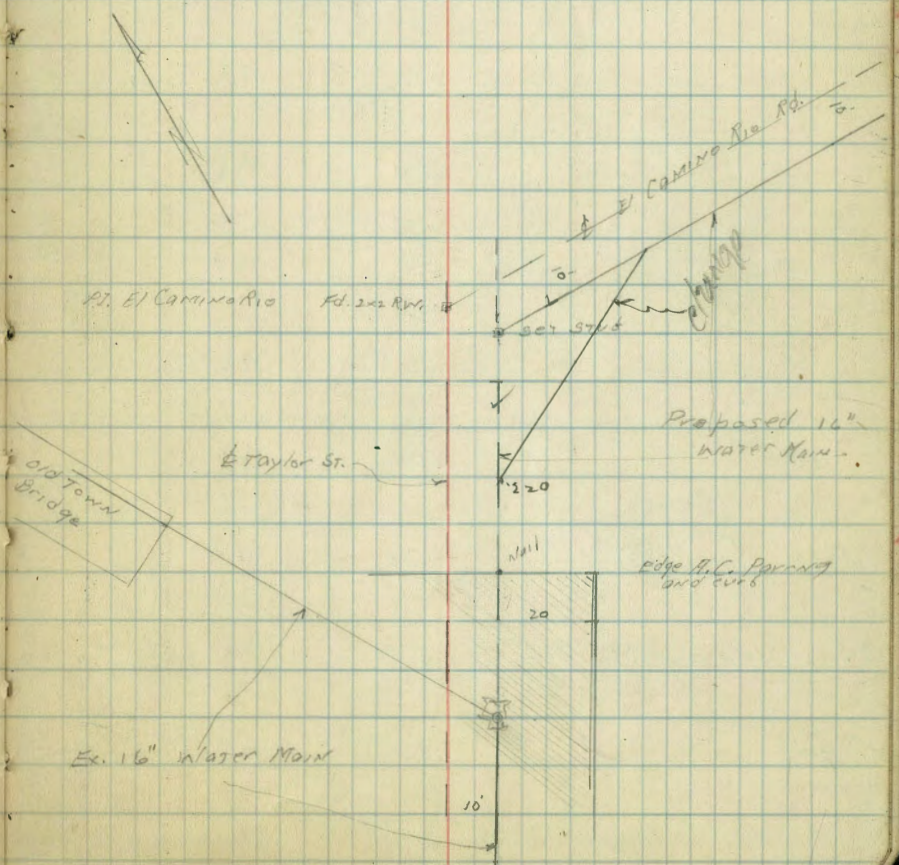
(1450)	Gutter	Shldr	Put	Gutter
	9.1	7.6	2.4	7.9

4.6

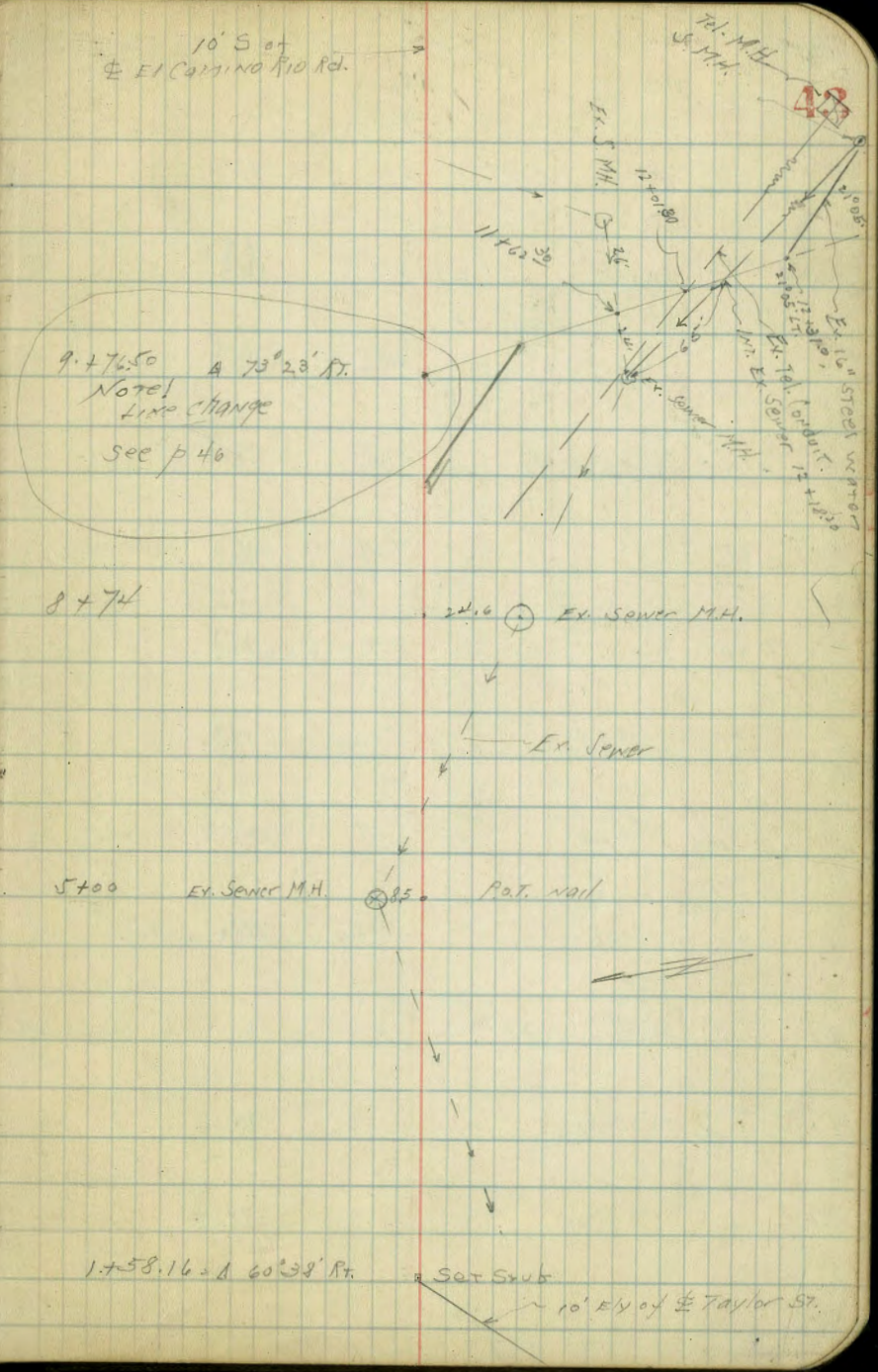
Moore
1/29/36
Proposed 16" Water Main
on Camino Del Rio, Taylor to Smith.
to connect to Ex. 16" Steel line from Pine St.

Indexed
c.s.k.

T.P.	8.11	22.92	6.55	14.81
+50			1.0	20.4
✓			6.8	14.6
+50			7.3	14.1
3			7.0	14.4
+50			7.0	14.4
✓			6.5	14.9
1 + 58.16 = Δ 60° 38' 17"	Stub =	6.31	18.05	
1 + 700		5.3	16.1	
0 + 4y edge Pav.		3.94	17.42	
0 + 00 = Tin Cap in Pav. = Ex. Tee		4.77	16.59	on post
BM B.P.	129	21.36	20.07	SW Cor Old Town Bridge

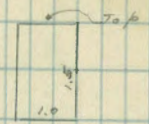


9		10.4	22.5
+50		10.3	12.6
8		10.3	12.6
+50		9.9	13.0
+40		5.1	17.8
7		5.4	17.5
+50		5.5	17.4
6		5.1	17.8
+50		5.2	17.5
8.5 ² 27	5100 FL. MH.	11.68	11.24
8.5	LT of 5100 Rim MH	3.80	19.1
5100		3.2	19.7
	22.92		
	↑		



~~21.2~~
~~21.7~~

9	T.P.	10.17	28.97	20.5	18.80
	+50			2.1	18.8
	+01			4.6	16.5
11	Top Conc. wall		3.17		17.68
	+98			5.9	15.0
	+90			7.2	13.7
	+50			8.1	14.8
6	B.M. BP Top Conc. wall old pump plant		6.57	12.34 ✓	$\frac{14.3}{0.02}$
10			8.2		12.6
8	T.P.	8.09	20.85	10.76	12.16
	+76.5 Δ 73°23' RT.			10.76	12.16
	+50			10.5	12.4
			22.92		
			7		



Detail Tel. Conduit

Note! Possibly, may need 5 or 6 hundred feet more to replace old 16" steel beyond STA. 12+250. Survey to be made by Water Dept.

	Δ 21°05' LT.				
12	+31 JUNCTION EX. 16" steel		9.04	19.93	Top of 16" pipe
12	+31. ground		5.0	26.0	
12	+01.30 Int. Tel. Conduit		8.55 6.3	20.42 42.7	= Top Tel. Conduit = ground
24	Rt of 11+62.3 M.H. F.L.		14.09 = Drop 13.76	14.58 15.21	15.32 E.L. FL
26	LT of 11+62.3 M.H. F.L.		13.54	15.43	Sewer at intersection
11	+62.30 Int. Sewer		10.1	18.9	ground
			28.97		
			7		

+55	ground	11.8	42.6
N +55	Top 16" Steel	2.85	41.57
+35		6.3	38.1
+21	13' Ft. FL SMH	11.32	33.1
+21	ground	6.0	38.4 ✓
15 + 16.80	Top old 16" Steel	8.60	35.8 ✓

15 + 16.80 = A 50° 13' LT 5.9 38.5

T.P. 6.38 4.42 1.08 38.0 ✓

N 1.8 37.3

+50 4.7 34.4

14 7.4 31.7

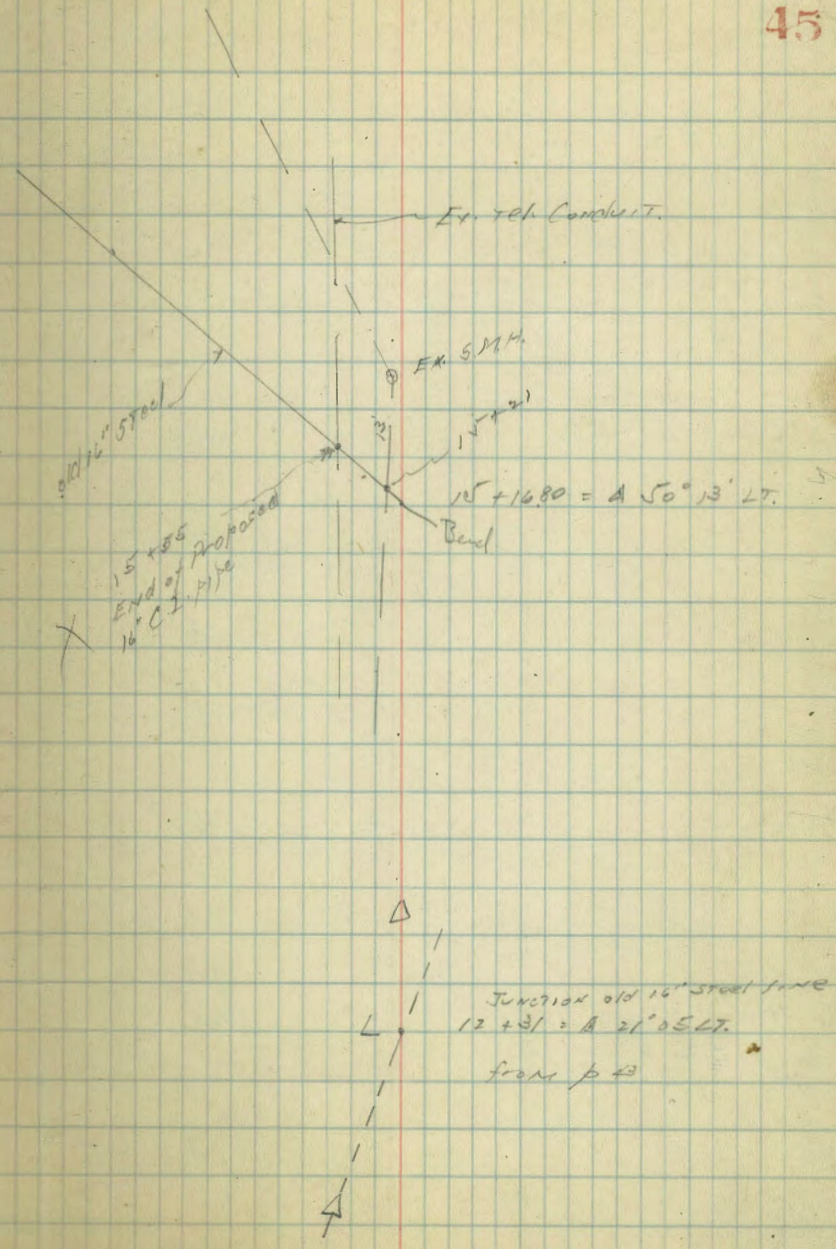
+50 9.7 29.4

13 12.0 27.1

12 + 50 14.6 24.5

T.P. 19.19 39.1 ✓ 19.93

Top old 16" Steel at 519.12731



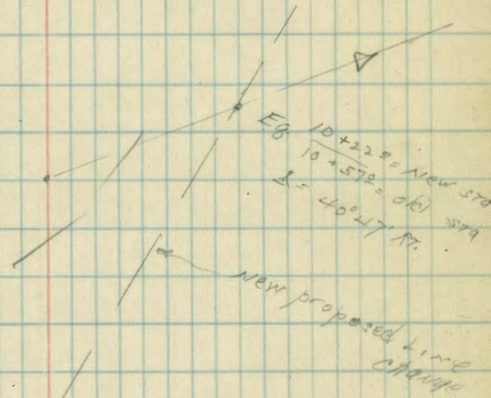
10+57 = Eq. old
 10+27 = Δ 30° 47' RT
 = New

	4.57	12.9
10	5.0	12.4
+60	5.5	11.9
+50	1.7	15.7
+40	4.1	15.3
9	4.4	15.0
8+790 Δ 32° 36' RT. STUB	4.75	12.6
BM BP 304	17.35	14.31

Top Conc. wall

9+1650
 old Δ 73° 23' RT

8+790
 Δ = 32° 36' RT



1022
 879
 143

					C + 5	2.7	179.9	
SWBP	0.11	218.14	218.03	dot Monte Guizot	S	2.2	180.4	
T.P.	0.50	205.59	13.05		0 + 50			
T.P.	0.99	193.47	13.11		S	3.3	179.3	
T.P.	2.12	182.58	13.01		C	4.0	178.6	
					N	4.4	178.2	
	0-12				0 + 75			
S	PAV.		6.49		N	5.3	177.3	
N	"		7.79		C	5.0	177.6	
	0 + 100 WL Guizot				S	Fence on line	4.5	178.1
N	cb		7.10			1 + 80		
N	PAV		7.18		S	Fence on line	6.4	176.2
C	"		7.09		C	6.6	176.0	
S	"		6.40		N	6.6	176.0	
S	cb		5.79			1 + 50		
	0 + 01				N	9.9	172.7	
S			1.9		C	9.4	173.2	
+ 5			2.1		S	Fence on line	9.0	173.6
+ 6			6.5			1 + 86		
C			6.8		S	9.9	172.7	
+ 8			6.5		N	11.5	171.1	
N			3.0		C	12.0	170.6	
	0 + 25				N	12.2	170.4	
N			3.8			+ or double bar. 4" wide	11.9	170.7
C			4.1			2 + 00		
+ 4			4.0		N	Fence on line	12.9	169.7

dirt floor
level

182.58

C		12.6	170.0
+6		12.2	170.2
S		10.7	171.9
T.P.	0.67	170.58	172.7
		169.91	
	2+50		
S		0.5	170.1
+2		1.0	169.6
+5		3.9	166.9
C		3.7	165.9
N	Fence on line	3.0	162.6
	2+70		
N	Fence on line	5.3	165.3
C		6.2	164.4
+6		6.2	164.4
+8		1.7	168.9
S		1.6	169.0
	3+00		
S		11.0	159.6
C	M.H. Rim	11.4	159.14
N	Fence on line	11.5	159.1
T.P.	0.75	158.85	12.48
		158.10	

158.85

48

		3+25	
N	Fence on line	3.7	155.2
C		3.7	155.2
+7		3.7	155.2
S		2.7	156.2
	3+50		
S		3.6	155.3
+6		5.0	153.9
C		5.5	153.4
N	Fence on line	5.7	153.2
	4+00		
N		9.4	149.5
C		8.9	150.0
+7		8.9	150.0
S		6.4	152.5
	4+13		
S		9.5	149.4
C		10.2	148.7
N		10.6	148.3
	+0.50 ² S.W. Cor.	10.5	148.4
			dir floor 10' wide
T.P.	0.85	146.87	12.83
		146.02	
	4+50		
N		2.0	144.9
C		2.1	144.8
S		2.2	144.7

	J+96		
S		8.0	138.9
	J+00		
S		8.5	138.4
C		8.3	138.6
N		8.9	138.0
	J+25		
N		12.1	134.8
C		11.5	135.4
S		11.3	135.6
T.P.	0.38	134.46	12.79
	J+50		
S		2.5	132.0
C		3.0	131.5
N		3.6	130.9
	J+75		
N		8.3	126.2
C		8.0	126.5
S		7.9	126.6
	J+97		
S		10.3	124.2
+3		12.1	122.4
C		13.0	121.5

C+5		13.6	120.9
N		13.1	121.4
T.P.	0.97	122.43	13.00
	J+99.4		= EL Froude
N	curb	2.60	119.83
N	par.	2.66	119.77
C	r	2.39	120.04
S	r	1.19	121.24
S	curb	0.74	121.69
	G + 11.4		= F cb Froude
S	par.	1.64	120.79
N		3.34	119.09

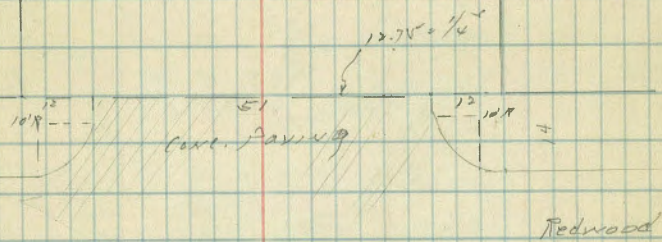
T.P.	1.96	111.43	12.96	109.47
Check To NEM	Now part Froude	3.04	108.39	108.38
				0.01

Node
3-21-34
Curb. E. Redwood + Union
Paving "

Indexed
C.S.K.

50

10' CT. S. Cor	234	209.25	207.11	Redwood Union
N. C. Redwood				
FL Union	cb	441	204.84	
" "	qvt. pav	5.09	204.16	
E. Cb	pav	5.41	203.84	
E 1/4	"	5.37	203.88	
C	"	5.59	203.66	
W 1/4	"	6.07	203.18	
W. Cb	"	6.77	202.48	
WL Union	qvt	7.10	202.15	
" "	cb	6.43	202.82	
N. L. Redwood				
W. Cb	"	6.56	202.69	
"	qvt pav	7.29	201.96	
1/4	"	6.55	202.70	
C	"	6.18	203.07	
1/4	"	6.11	203.14	
E. Cb	qvt "	6.28	202.97	
"	cb	5.59	203.66	
T.P.	0.28	208.17	100	208.19
T.P.	0.59	196.26	1280	195.67

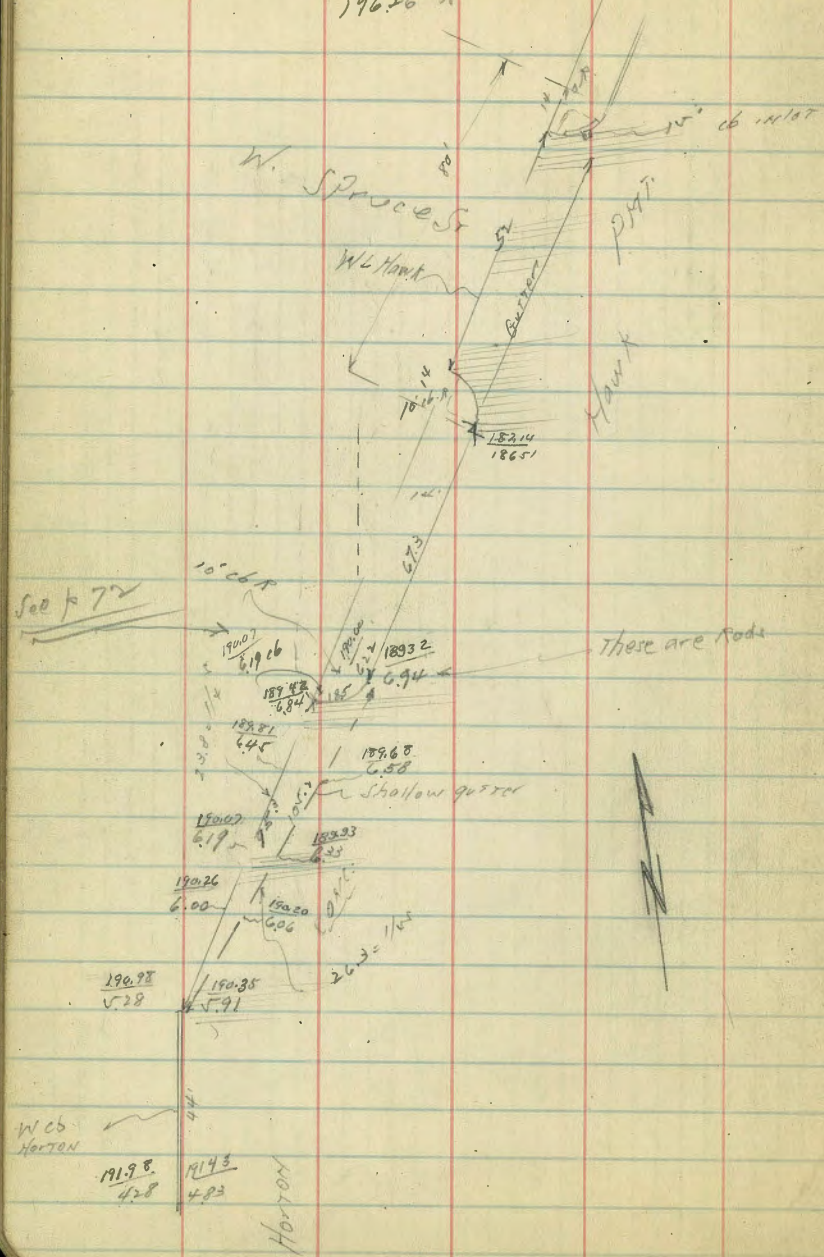


Moose
12-31-26

Curb & Pav. E.L.
Horton - Hawk
196.26 T

See p 72

Spruce at Hawk
T
196.26
W side
indexed
c.s.R.



W cb Hawk				
SL Spruce cb	9.14		187.14	
" " gut	9.75		186.51	
Scb pav	10.17		186.09	
S 1/4 "	10.41		185.85	
" " 13 1/4 "	10.58		185.68	
N 1/4 "	10.65		185.62	
N cb	10.45		185.61	
NL Spruce gut pav	10.43		185.73	
" " cb "	9.74		186.50	
W.L. Hawk				
N cb	9.74		186.50	
" " gut	10.41		185.85	
NL pav	10.04		186.22	
" "	9.84		186.42	
S 1/4 "	9.81		186.45	
S cb gut	9.88		186.38	
" cb	9.23		187.03	
T.P. 22.07	20274	0.59	195.67	
T.P. 2.08	21028	0.14	207.60	
check to BM 03		3.18	207.10	207.11

274.12

1 + 88.5			
W - 9 dble gar. dirt floor	3.7	270.4	
W	3.7	270.4	
C	4.3	269.8	
E	4.4	269.7	
+7 dble gar. " "	4.3	269.8	
1 + 85			
E - 2 Sin. gar. dirt floor	4.8	269.3	

T.P. 3.66 274.63 5.15 268.97

1 + 86			
W - 8 Sin. gar. dirt floor	3.4	269.2	
1 + 87			
W - 8 Sin. gar. " "	3.5	269.1	
W	3.8	268.8	
C	4.1	268.5	
E	4.1	268.5	

1 + 63			
E - 4.5 dble gar. Cem. floor level	4.36	268.27	
E	4.4	268.2	
C	4.2	268.4	
W	4.0	268.6	
+8 $\frac{1}{2}$ Triple gar. dirt floor	3.8	268.8	

1 + 80			
W - 5.7 Single dble gar.	3.67	268.96	Cem. floor
W	4.2	268.4	

272.63

54

C	4.2	268.4	
E	4.5	268.1	
1 + 97			
E	4.9	267.7	
C	4.7	267.9	
W	4.2	268.4	
+8 N.L. dble gar	3.75	268.82	Cem. floor
2 + 91			
W - 5.5 Sin. gar	4.27	268.36	" "
H. valley Cem. apron ^{13'} wide	4.50	268.1	
C	5.6	267.0	
E	5.8	266.8	
2 + 60			
E - 8 Sin. gar. dirt floor	7.1	265.5	
F	7.0	265.6	
C	6.6	266.0	
W	6.0	266.6	
2 + 69.5 = E M.H.			
W	6.7	265.9	
C R. Sand M.H. ✓	7.16	265.47	
F	7.9	264.7	
3 + 00			
E	9.0	263.6	
C	5.8	263.8	
W	7.8	264.8	

272.62

3+20 = Head of draw

W		9.9	262.7
C		10.0	262.6
E		9.4	263.2

T.P.	1.01	261.48	22.46	260.17
------	------	--------	-------	--------

3+40

- 15 Top edge School playground + 5.4 266.7

F 2.5 259.0

C 5.2 256.3

+ 6 Poplar tree 15" diam

W 4.0 257.5

+ 10 1.9 259.6

3+80

- 10 10.7 250.8

W 12.6 248.9

C 11.8 249.7

E 6.9 254.6

+ 7 1.5 260.0

4+16 Sly Univ Ave.

E 7.2 254.3

E 13.2 248.3

C 16.2 245.3

W 17.7 243.8

+ 10 18.2 243.3

55

261.48

T.P. 11.77 271.94 1.31 260.17

T.P. 3.70 274.15 1.49 270.45

check to B.M. 4.17 269.98

269.97
201

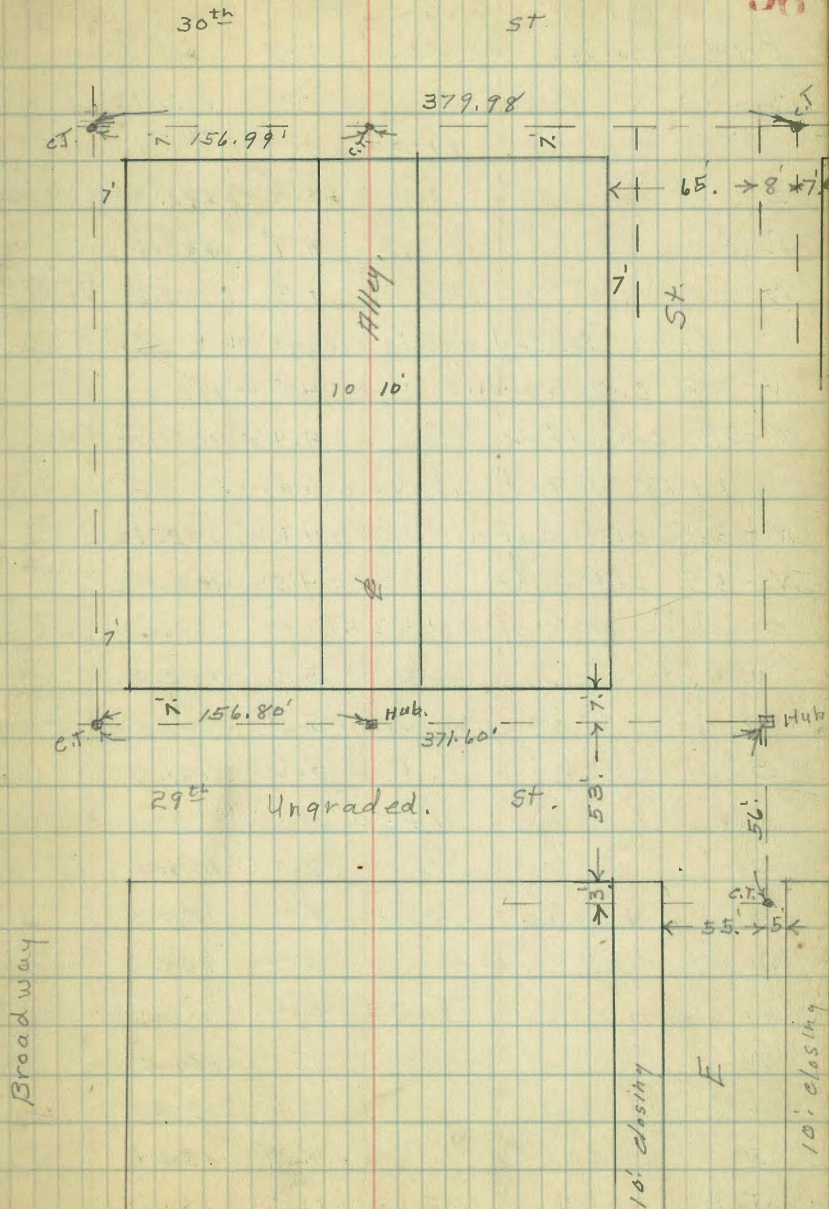
X. Sec. Alley Bk 86
 E.W. Morse's Sub.
 29th to 30th Sts Bet Bdw. + E.

8-19-36
 Miller
 Wal Ker
 Bliss
 Northern

Indexed
 as is.

56

BM. P.P.	2.40	197.48	195.04
10' E. of W. Line = W. cb. Line of 30 th St			
N. ent. cl		3.93	193.55
N. gutter		4.45	193.03
± "		4.63	192.85
S. "		4.77	192.71
S. ent. cl		4.28	193.20
0+00 = W. Line 30 th St.			
s. ent. cl	W End	4.15	193.33
S. pav.	" "	4.27	193.21
± "	" "	4.45	193.03
N "	" "	4.07	193.41
N. ent. cl.	" "	3.66	193.82
0+15			
N		3.2	194.3
±		3.7	193.8
S		3.6	193.9
0+30			
S		3.7	193.8
±		3.7	193.8
N		3.7	193.8
0+81			
N.		4.3	193.2
±		4.5	193.0
+9.5	garage	4.6	192.9 dmt floor



197.44
0+95

0.5 N. of S. garage cmt. floor 4.98 192.50

1.2 " " " 5.06 192.42

1+00

S 5.2 192.3

⊕ 4.9 192.6

N 4.3 193.2

1+03 E. End. double garage on N cmt. floor ^{Back} 5.5

N-3.5 cmt. apron 4.52 192.96

N-5.5 cmt. floor 4.48 193.00

1+18 W. End. above garage

N-3.5 cmt. apron 4.64 192.82

N-5.5 cmt. floor 4.55 192.93

1+25

WN 5.5 192.0

⊕ 5.4 192.1

S 5.6 191.9

1+50

S 8.1 189.4

⊕ 8.0 189.5

N 8.4 189.1

1+75

N 13.1 184.4

⊕ 12.6 184.9

S 12.9 184.6

T.P. 0.46 185.13 12.81 184.67

185.13

Alley BIK 86. E.W. Morse.

57

1+95

S 5.8 179.3

⊕ 5.1 180.0

N 5.2 179.9

2+03

N-5 7.4 177.7

N 8.0 177.1

⊕ 8.2 176.9

+6 8.6 176.5

S 11.2 173.9

+5 11.2 173.9

2+30

S 12.7 172.4

⊕ 12.7 172.4

N 13.2 171.9

+5 14.4 170.7

2+42

-5 17.5 167.6

N 17.4 167.7

+5 13.5 171.6

⊕ 13.2 171.9

S 13.5 171.6

+5 18.6 166.5

T.P. 0.45 173.14 12.44 172.69

173.14

2755

-40		13.0	160.1
S		11.4	161.7
±		11.0	162.1
N		10.6	162.5
+10		10.7	162.4

T.P. 0.18 160.76 12.56 160.58

2790

-10		11.3	149.5
N		11.5	149.3
±		11.9	148.9
S		11.7	149.1
+10		11.7	149.1

T.P. 2.53 150.62 12.67 148.09

3225

-10		9.4	141.2
S		9.0	141.6
± M.H. Rim Top.		8.67	141.95
N		8.2	142.4
+10		7.8	142.8

3260

-10		11.4	139.2
N		12.4	138.2
±		14.0	136.6
S		12.8	137.8
+10		12.6	138.0

150.62

3790

-10		12.1	138.5
S		12.2	138.4
±		10.5	140.1
N		10.7	139.9
+10		10.1	140.5

3796

M.H. Top. Rim. 9.35 141.27

4705

-10		8.9	141.7
N		8.6	142.0
±		8.3	142.3
S		7.8	142.8
+10		8.2	142.4

4725

-10		6.5	144.1
S		5.7	144.9
±		5.1	145.5
N		5.2	145.4
+10		5.1	145.5

4750 = E. End. Foot. of City Dump.

-10		1.2	149.4	Nat. ground
N		2.1	148.5	" "
±		3.3	147.3	" "
S		4.1	146.5	" "
+10		4.9	145.7	" "
T.P.	11.96	161.91	0.67	149.95

Alley BIK 876. E.W. Morse

58

161.91

172.39

Alley B/k 26 e.w. Morse

59

4773 = Top of City Dump Nat ground. ? Deep.

-10	5.4	156.5
S	1.0	160.9
E	0.0	161.9
N	0.0	161.9
+10	0.0	161.9

5+48

T.P. 12.07 172.39 1.59 160.32

4+96 E. end shed. on N 5.5 in Alley.

-10	9.0	163.4
N	9.0	163.4
E	9.4	163.0
S	9.4	163.0
+10	9.4	163.0

on N 5.5

5+55 = E. end garage on S. dirt floor on line
S. on floor 2.3 170.1

5+71 W end. above garage 1' Box K

S-1 on floor	2.1	170.3
S	2.1	170.3
E	2.5	169.9
N	2.8	169.6
+5	3.0	169.4

5+00 W. Natural ground.

-10	9.2	163.2
S	9.2	163.2
E	9.2	163.2
N	9.2	163.2
+10	9.2	163.2

T.P. 9.23 179.88 1.74 170.65

5+88

N	9.4	170.5
E	9.2	170.7
S	7.9	172.0

5+22 W End. above shed. on N 5.5 in Alley

N-10	5.7	166.7
N	5.7	166.7
E	7.1	165.3
S	7.1	165.3
+10	7.1	165.3

6+00²⁰ = E. Line 29th St

S	7.0	172.9
E	7.7	172.2
N	8.2	171.7

RM Mon N.W. 29th

4.57 175.31 ✓

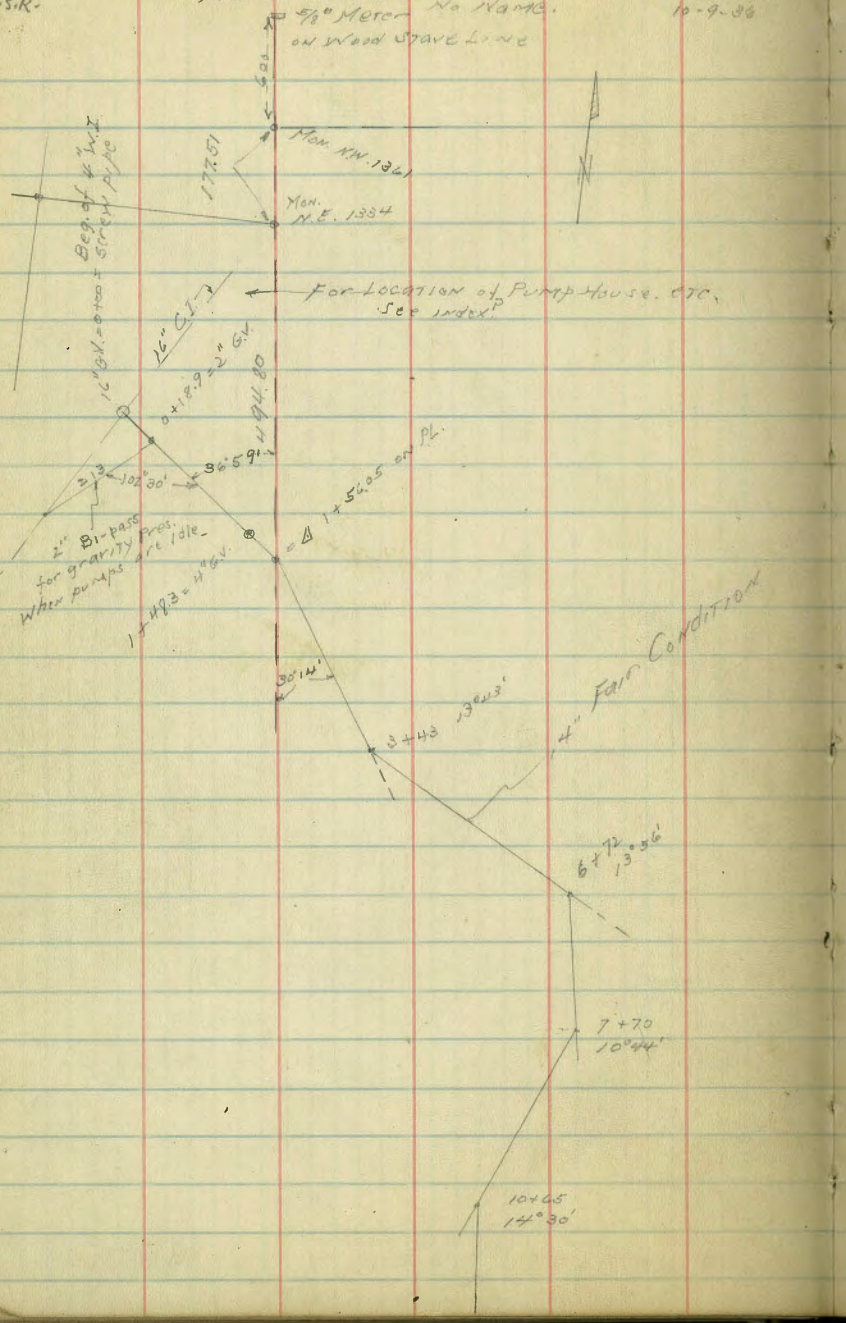
INDEXED
C.S.R.

Location of Sorrento Valley WATER LINES

Moore
Lisson
Northern
10-9-36

5/8" Meter No Name.
on Wood Stake Line

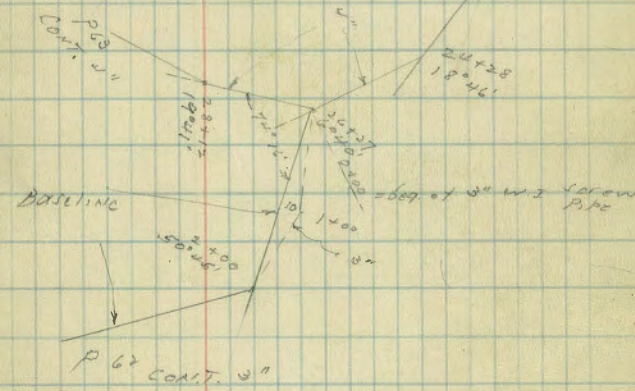
To Terry Pines Res.



For Location of Pump House, etc.
See Index

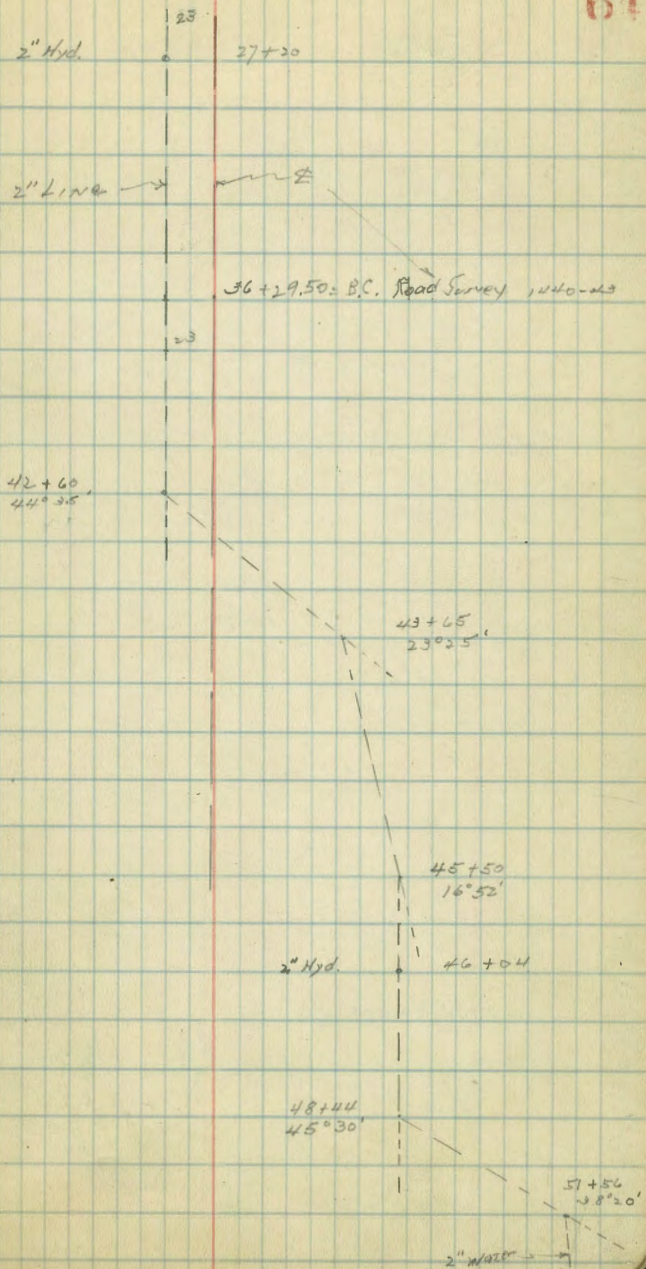
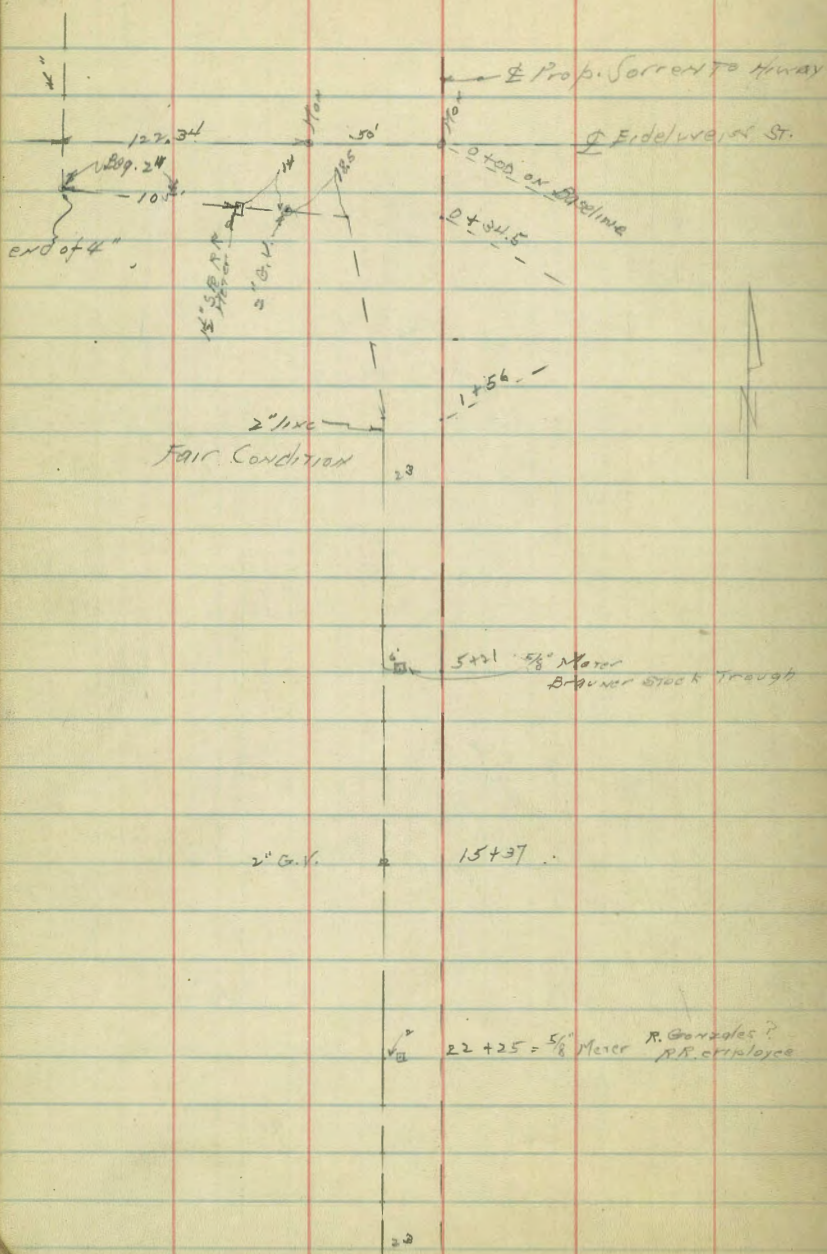
2" Bypass
for gravity
When pumps
are idle.
1+493 = 486'

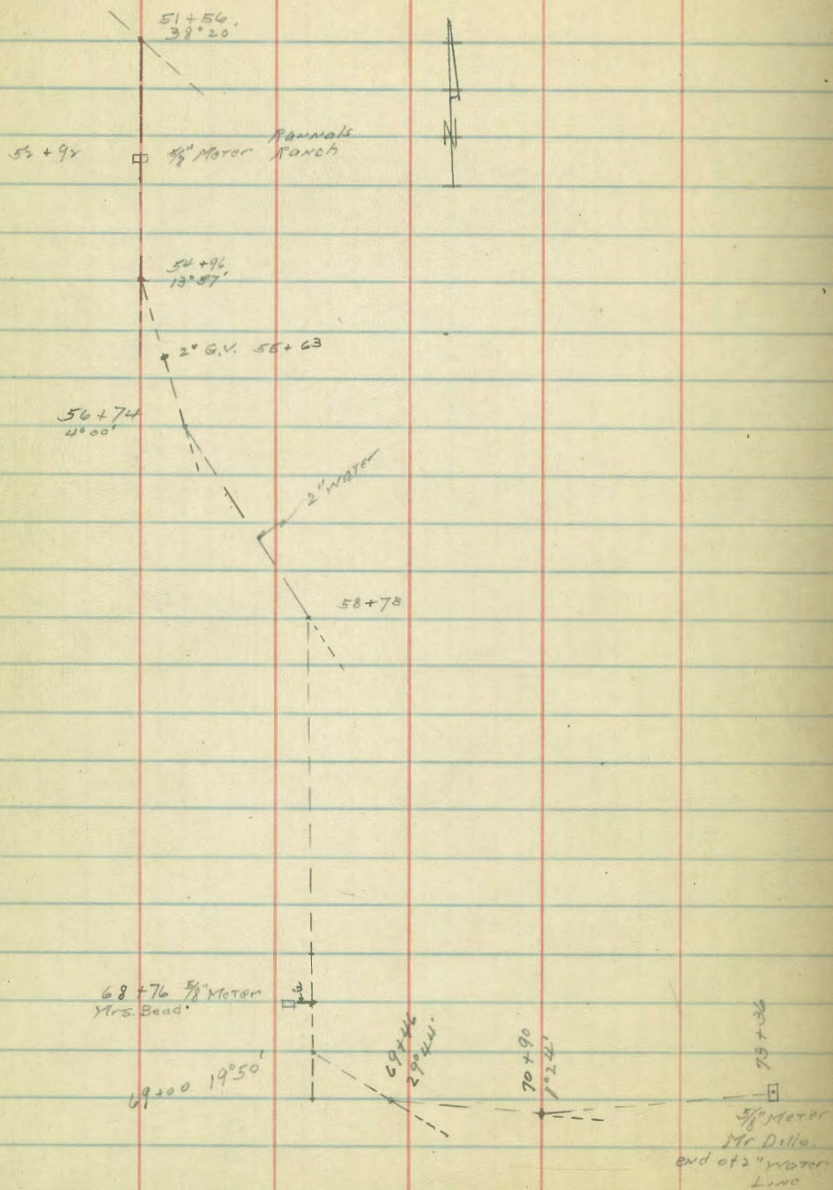
4" Fair Condition



Mr. Levi

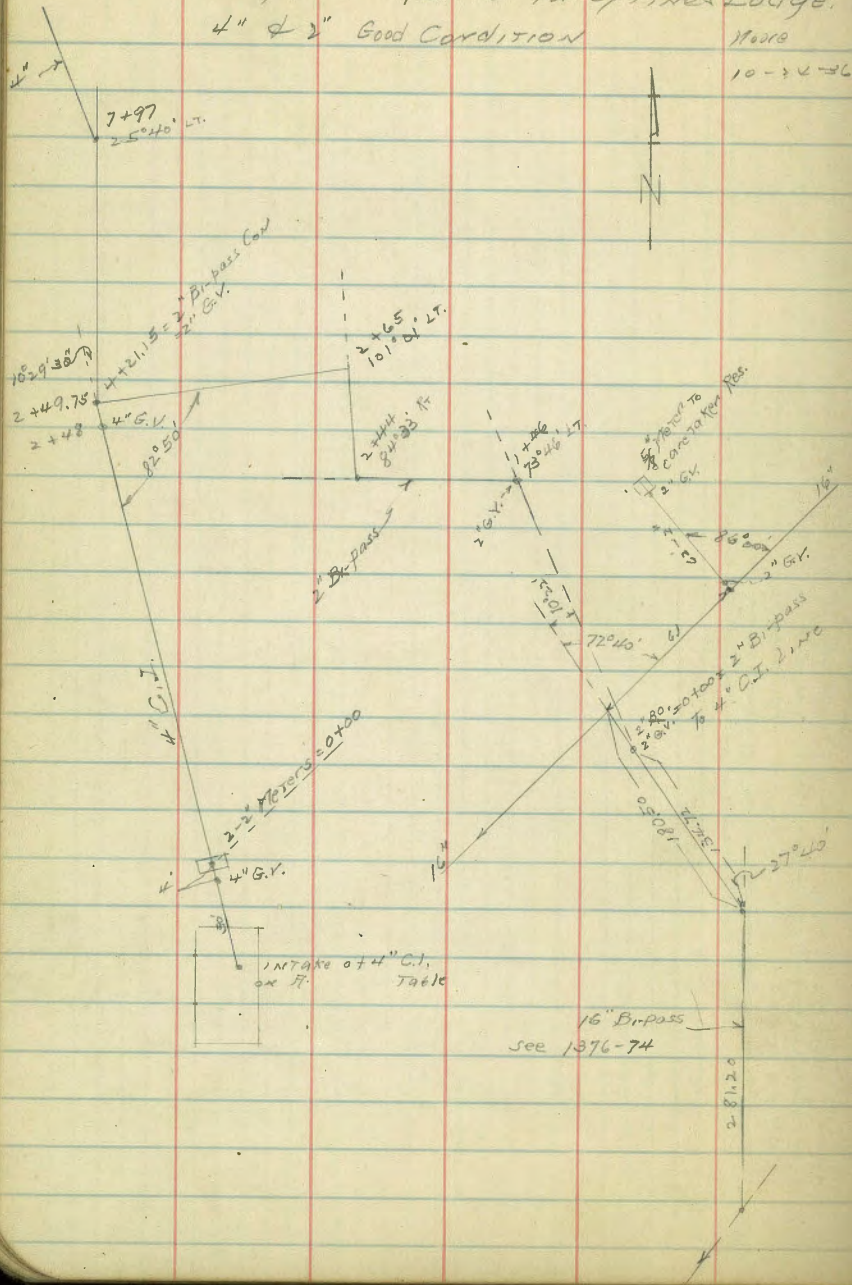
beg. of 3" w 2 screw pipe





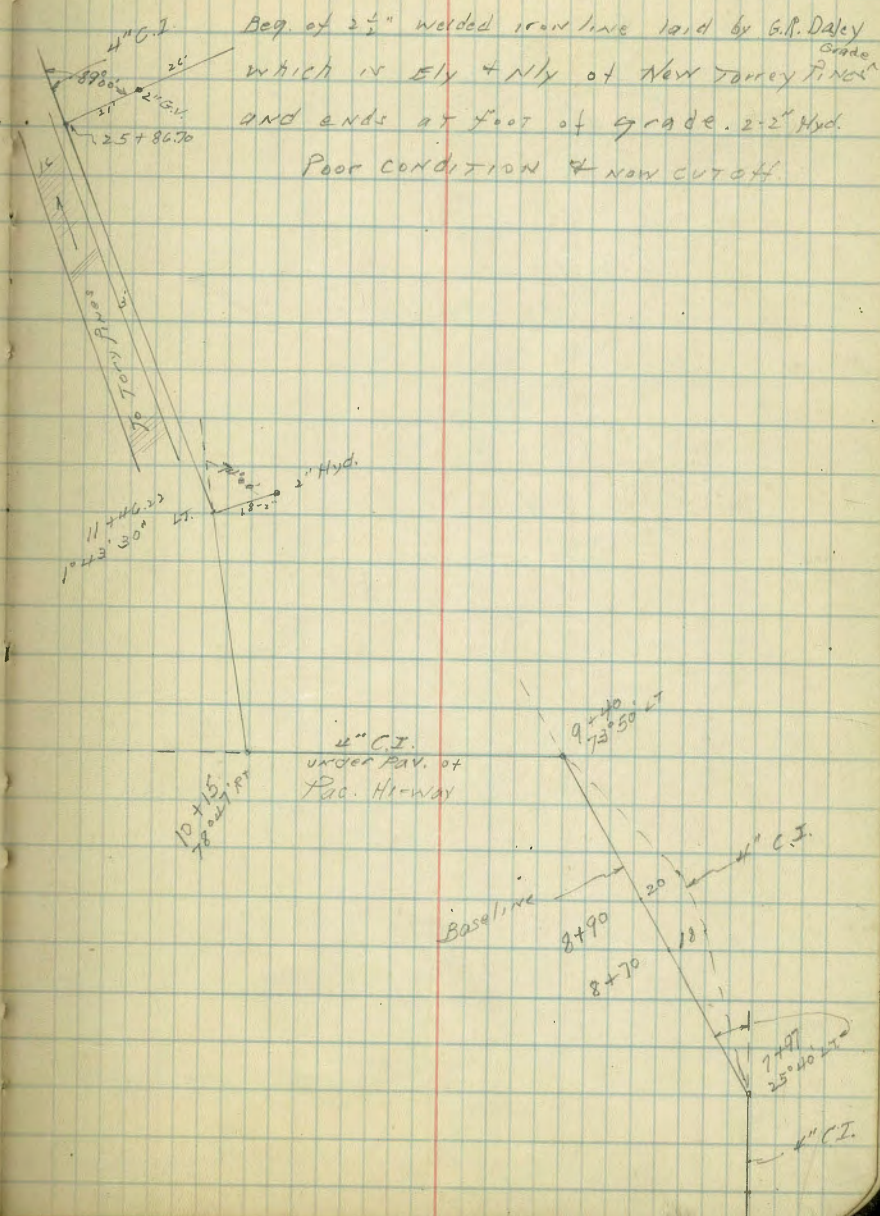
Location of 4" C.I. Water Main
Torrey Pines Res. to Torrey Pines Lodge.
4" & 2" Good Condition

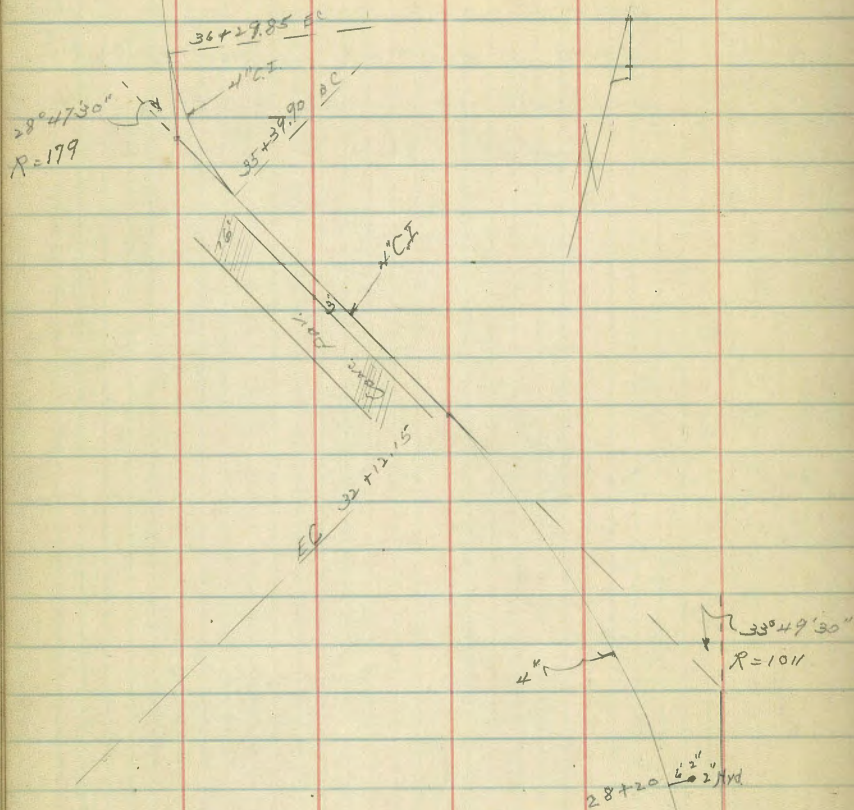
Moore
10-24-36



Indexed
c.s.k.

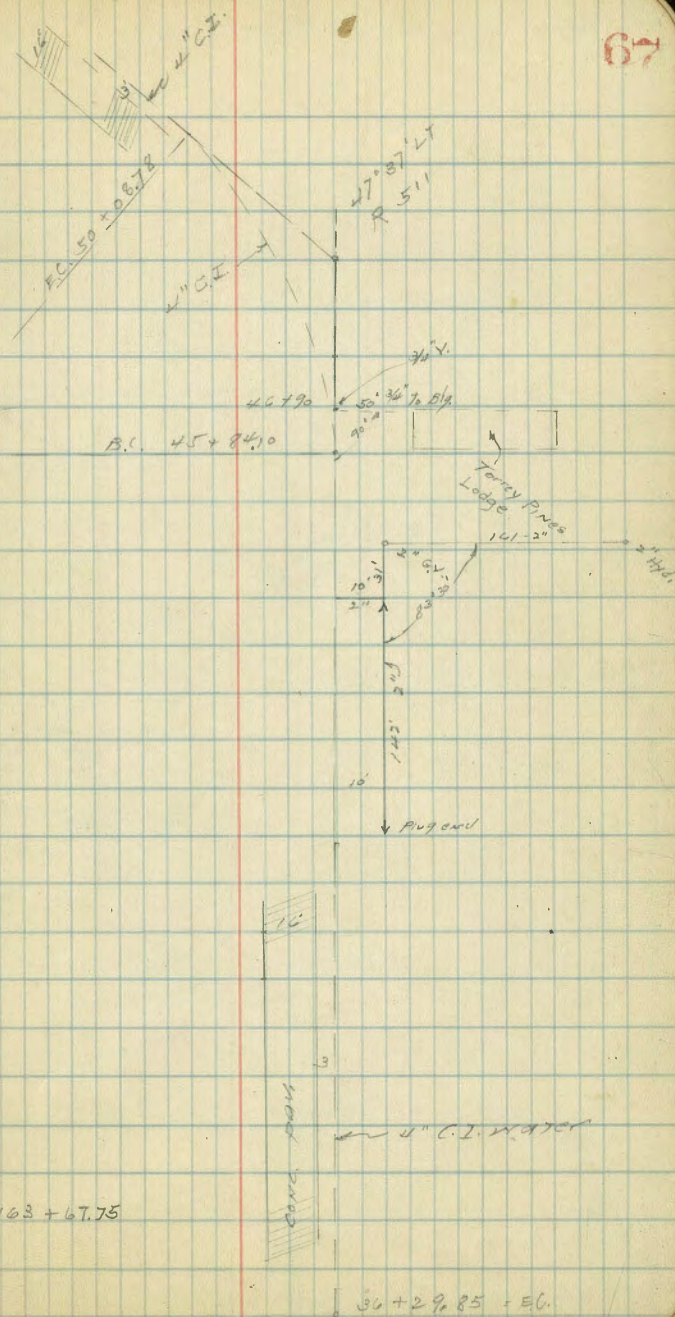
Req. of 2 1/2" welded iron line laid by G.P. Daley
Grade
which is Ely & Nly of New Torrey Pines
and ends at foot of grade. 2-2" Hyd.
Poor condition & new cutoff.





BC. 26+15.30 = B.G. of Pav. = STA. 163 + 67.75

25+86.70



30+29.85 = EC.

399.82
1+50

E	5.2	394.6
Φ	5.0	394.8
W	4.6	395.2

1+85

W	4.7	395.1
Φ	4.7	395.1
E	4.9	394.9

2+00

E	4.7	395.7
Φ	4.2	395.6
W	4.1	395.7

2+50

W	3.5	396.3
Φ	3.8	396.0
E	4.3	395.5

2+78 garage on W. dirt floor 1.4 Back

E	4.6	395.2
Φ	4.2	395.6
W	3.8	396.0
W+1.4=floor	3.6	396.2

2+96.9' see on Δ Biscelov

N	3.8	396.0
---	-----	-------

Φ	4.2	395.6
TR Φ stub 504 400.14	4.72	395.10
+1.7 M.H. Top Not. for yardage	5.53	394.61

2+96.2 Δ

E	4.2	395.9
---	-----	-------

400.14
3+25

70

E	4.5	395.6
Φ	4.7	395.4
W	4.3	395.8

3+50

W	4.6	395.5
Φ	4.6	395.5
E	4.6	395.5

3+75

E	4.4	395.7
Φ	4.5	395.6
W	4.5	395.6

4+00

W	4.1	396.0
Φ	4.2	395.9
E	4.1	396.0

4+13 garage on E. dirt floor 3' Back

E - 3 = floor	4.4	395.7
---------------	-----	-------

4+25

E	4.2	395.9
Φ	4.5	395.6
W	4.3	395.8

4+50

W	4.1	396.0
Φ	4.0	396.1
E	4.3	395.8

400.14

4+75

E 4.0 395.5

E 4.3 395.8

W 4 4.3 395.8

⑤ + 92 Garage on W. ent. floor 23. Back

W-5.5 E. End. ent. Apron 4.10 396.0

5+00

W 3.9 396.2

E 4.0 396.1

E 4.2 395.9

5+35

E 4.2 395.9

E 4.1 396.0

W 4.3 395.8

5+59 = S. Line Mt. View Dr. on E

W of E = S. End. ent. cl. 4.23 395.91

" " " = " " pav. 4.57 395.57

E " " " 4.81 395.33

" " " " 4.65 395.49

E. of E = " " ent 4.49 395.65

Sly. cb. of Mt. View Dr.

E. ent. cl. 4.89 395.25

E. pav 5.44 394.70

E " 5.40 394.74

W " 5.35 394.79

W ent. cl. 4.67 395.47

B.M. B.P. 4.69 395.45

S.W. 35"

+ Mt. View Dr.

= 395.42

71

Indexed
c.s.k.

X sec of Horton Ave. 50' wide
Hawk to Spruce

Moore
2-30-37
Sep 51

LT.

8
10
2

RT.

72

Note - Sec. taken at 90° with Horton

Wly Hawk
Wly Spruce to W 1.68 1.94.75 1.90.07 Top End cb

194.75 = T

00 = Wly Hawk on Conc. Pav.

191.5 191.0 190.50
2.3 0.8 4.65 = pav
2.5 1.5

0 + 13.90 = Sly Spruce to West

191.7 191.4 190.3 190.0
2.1 3.4 4.80
2.5 1.5 1.5 1.7 = pav

0 + 48.90 = F " " "

191.5 191.0 191.0 190.3 189.8
4.0 4.5 4.5 4.5 5.0
2.5 1.5 1.5 1.5 2.5

0 + 73.90 = Nly " " "

189.4 190.1 191.6 191.6 190.8
5.4 4.7 2.2 2.2 4.0
2.5 1.5 1.5 1.5 2.5

1 + 00

187.3 186.9 186.0 185.7 186.1 187.90
7.5 7.7 8.8 9.1 8.7 6.85
2.5 1.5 1.5 1.5 2.5 2.6 = 600 ft

1 + 30

175.6 177.4 179.0 181.4 183.4 184.8
19.2 17.6 15.8 13.4 11.4 10.0
2.5 2.5 1.5 1.5 1.5 2.5

1 + 39.84 = Sly Spruce 90° RT S Ely Cor Horton 4' 10' 10' 10'

175.2 177.6 179.3 181.8 183.9 184.8
19.0 12.2 15.5 13.0 10.9 10.0
2.5 2.5 1.5 1.5 1.5 2.5

1 + 58.09 = Sly Spruce to East (now closed)

175.4 178.3 180.5 184.1 186.7 187.7
19.0 16.5 14.3 10.7 8.0 7.6
2.5 2.5 1.5 1.5 1.5 2.5

Fronts on Hawk

194.75

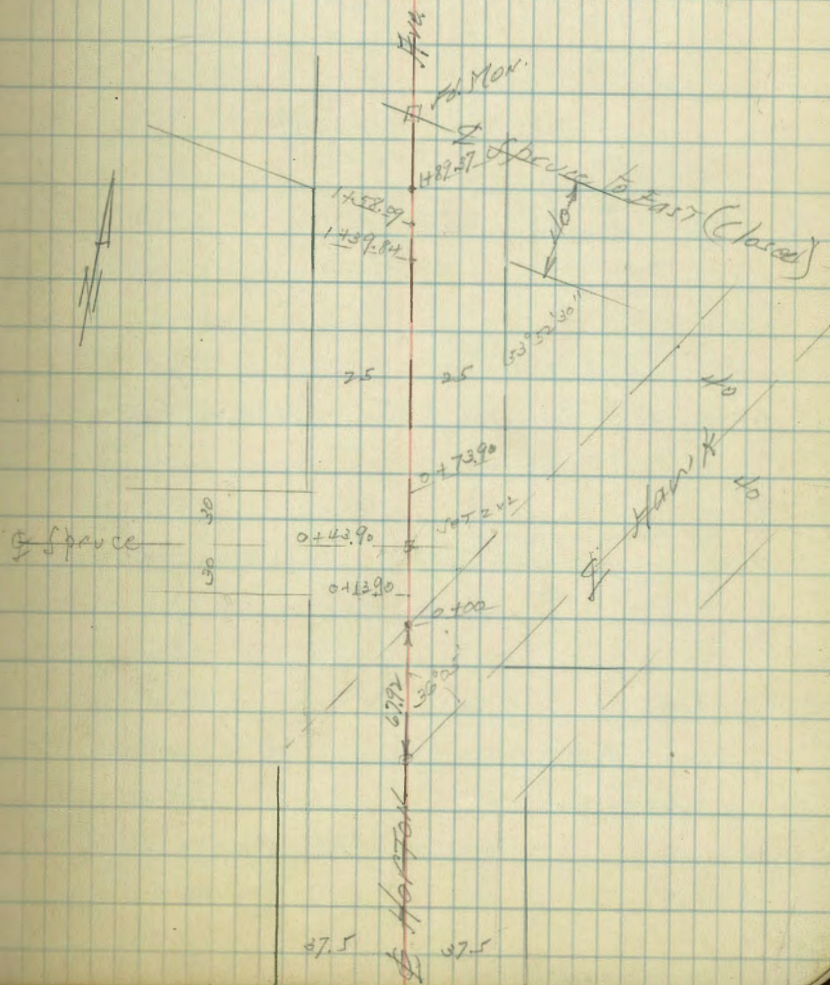
1 + 70 -

1 + 89.37 = AT RT. Δ WITH SWLY COR. Spruce + Horton

TO EAST

178.0	179.3	184.3	185.3	186.9	189.7	✓
$\frac{168}{50}$	$\frac{155}{25}$	$\frac{125}{15}$	9.5	$\frac{7.9}{15}$	$\frac{71}{25}$	

178.0	179.7	181.7	183.8	185.7	186.7	✓
$\frac{16.8}{50}$	$\frac{15.6}{25}$	$\frac{13.6}{15}$	11.0	$\frac{91}{15}$	$\frac{8.1}{25}$	



LT

RT

RT

73

194.75 = T

2-28-37
 Miller
 Walker
 Bliss

X Sec. Alley Blk 175 Land + Town

Evans to Sampson. bet Kearney + Logan.

B.M.B.P. 924 72.28 63.02 N.W. Evans + Logan

Evans Unpaved.

10' W. of E. line = E. ch. Evans St.

N. ent. ch.	4.87	67.41
N gutter	5.4	66.9
☒ "	5.9	66.4
S. "	6.2	66.1
S. ent. ch.	5.42	66.86

0+00 = E. Line Evans St.

10.55 S. of ☒ Top. ch. E. End	5.31	66.97
" " " ground	5.4	66.9
☒ " "	5.4	66.9
10.55 N. of ☒ " "	4.8	67.5
" " " " Top. ch. E. End.	4.63	67.65

0+14 Pepper Tree 24" Diam protrudes 0.5' in Alley

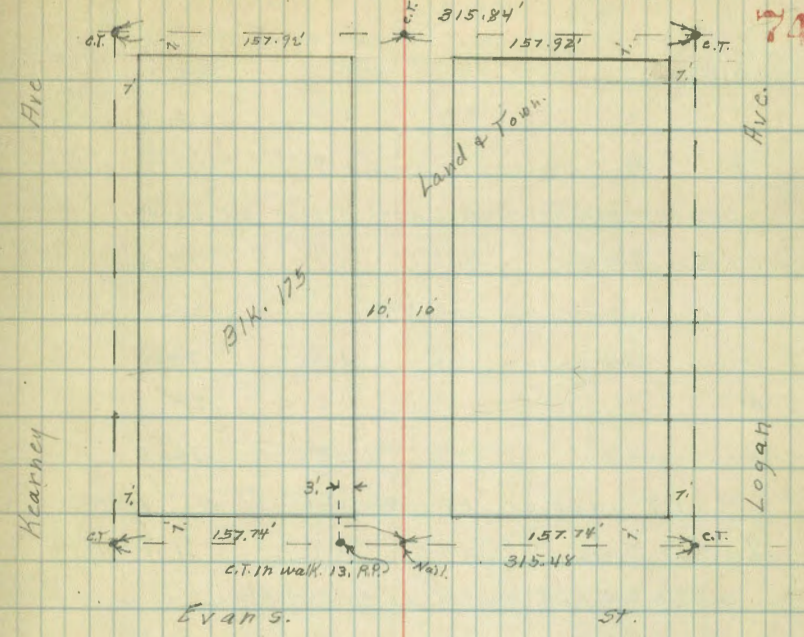
0+15

N	4.0	68.3
+3	4.7	67.6
☒	4.8	67.5
+7	4.7	67.6
S	4.0	68.3

0+55 = W. End 4 garages on S. dirt floors 6.0' Back

S-6. garage floor	3.7	68.6
S	3.7	68.6
☒	3.7	68.6
N	3.3	69.0

Sampson



Evans St.

0+94 = E. End. above 4. garages.

S-6. = floor 3.1 69.2

1+00 = W End. 3. garages on S. center garage Ctr. on Line

N	2.9	69.4
☒	3.1	69.2
S. = floor	3.1	69.2

1+14 = ☒ center garage 0.2 S. of S. line

S+0.2 = ent. floor 2.9 69.4

1+24 = E. End. above garages on S. 0.4' Back

W+0.4 = floor 3.0 69.3

72.28
1+50

S	2.6	69.7
4	2.4	69.9
N	2.3	70.0

1+58 = garage on N. dirt floor 2.5' Back
N+2.5 = floor 1.9 70.4

2+00

N	1.5	70.8
4	1.8	70.5
S	1.8	70.5

2+07 garage on N. dirt floor 9' Back

N+9' = floor 0.6 71.7

2+25 = W. End. garage on S. dirt floor 1.0' in Alley.

9'0 S. of 4. floor 1.6 70.7

2+37 = E. End. above garage on S. 0.3' in Alley

9.7 S. of 4. Floor

2+42 = W. End. dwelling on S. 0.4' in Alley.

2+50.

S+0.4 = floor of Dwelling 1.1 71.2

S+0.4 1.7 70.6

4 1.8 70.5

N. 1.8 70.5

at 2+63 Dwelling 15. on S. line

(W. End. Board. Fence 0.2' in Alley)

2+75 = (E. End dwelling on S. 0.2' Back.

72.28
3+00 { E. End. above Fence on S. 0.2' in Alley
W " 3. garages on S. 0.1' in Alley Dirt floors. 75

N.	1.8	70.5
----	-----	------

12	2.5	69.8
----	-----	------

4 M.H.	2.3	70.0
--------	-----	------

S. floor	2.5	69.8
----------	-----	------

3+25 = E. End above garages. on S. line

S = floor	3.3	69.0
-----------	-----	------

T.P.	3.21	72.11	3.38	68.90
------	------	-------	------	-------

3+50

S	4.0	68.1
---	-----	------

4	3.9	68.2
---	-----	------

N	3.9	68.2
---	-----	------

3+70 { garage on S. dirt floor 4' Back
garage on N " " on N. line

N floor	4.3	67.8
---------	-----	------

4	4.3	67.8
---	-----	------

S	4.3	67.8
---	-----	------

4+ = floor	4.3	67.8
------------	-----	------

4+00

S	4.7	67.4
---	-----	------

4	4.4	67.7
---	-----	------

N	4.5	67.6
---	-----	------

4+19 garage on N. cnt. floor 2.1 Back

N+0.9 = S. End cnt. apron	4.30	67.81
---------------------------	------	-------

N+2.1 = floor	4.20	67.91
---------------	------	-------

4+25 ctr. double garage on S. dirt floors. 1.5' Back
 S + 1.5 = floor. 4.6 67.5
 4+35 ctr. double garage on N. dirt floor 2.2' Back
 N + 2.2' = floor. 4.3 67.8

4+50

N 4.4 67.7
 E 4.5 67.6
 S 4.8 67.3

4+52 = W. End. 4. garages on S. dirt floors on line

S 5.3 66.8
 +2 4.8 67.3
 E 4.5 67.6
 N 4.4 67.7

4+89 = E. End above garages on S. line

N 4.5 67.6
 E 4.7 67.4
 +7 4.9 67.2
 S 5.3 66.8

5+00.

S 4.8 67.3
 E 4.6 67.5
 N 4.6 67.5

5+05 garage on S. dirt floor. 1.2' Back

4.8 67.3

5+50

N 4.4 67.7
 E 4.4 67.7
 S 4.8 67.3

5+97 Pepper tree 30" diam S. side on S. line
 Property Owner wants this removed.

6+007 = W. Line Sampson.

10.7 S of E = cont. d. w. End. 4.48 67.63
 " " " pav. W. " 4.52 67.59
 E " " " 4.69 67.42
 0.8' E of E M.H. Top. 4.69 67.42
 10.1' N of E = pav. W. End 4.30 67.81
 10.1 " " = cont. d. " 4.12 67.99

10' E. of W. line = W. ch. line - Sampson

N. cont. d. 4.18 67.93
 N. pav 4.86 67.25
 E " 5.10 67.01
 S + 0.7 pav 5.36 66.75
 S + 0.7 cont. d. 4.84 67.27

B.M. B.P.

T.P. 3.41 72.31 3.21 64.55 + Sampson
 64.49
 68.90

ch. Orig. B.M.

9.28 63.03 = 63.02

N.W. Logach

64.55 + Sampson

64.49

68.90

7-16-37
Miller
Walker
Bliss

X Sec. E. Side Kettner
Broad way to E.

Indexed
risks

14.20

2450

777

BM. B.P.	3.70	14.20	10.50	s. E. Kettner + Broadway
	0+00 = S. Line Broadway - N. End. Drive 1			
E. cl	3.75	10.45		
E. Gutter	4.30	9.90		
	0+16			
E. G. No. cl	4.34	9.84		
	0+32 = S. End. Drive 1			
E. cl	3.45	10.75		
E. G	4.50	9.70		
	0+69 = N. End. Drive 2			
E. cl	3.75	10.45		
E. G	4.74	9.46		
	0+97 = S. End. Drive 2			
E. cl	3.97	10.23		
E. G	4.96	9.25		
	1+25			
E. cl	4.18	10.02		
E. G	5.15	9.05		
	1+50			
E. cl	4.40	9.80		
E. G	5.39	8.81		
	2+00			
E. cl	4.80	9.40		
E. G	5.78	8.42		

E. cl	5.27	8.93		
E. G	6.14	8.06		
	3+00 = N. Line E St			
E. cl	5.65	8.55		
E. G	6.53	7.67		
T.P.	3.99	14.49	3.70	10.50
	0+00 = S. Line Broadway			
8.6 W. of E. cl	4.56	9.93		
15.6 W. of E. cl = E. Rail	4.45	10.04		
	0+16 S.			
17.2 W. of E. cl = E. Rail	4.55	9.94		
8.6 W. " " "	4.45	10.04		
	0+32			
8.6 W. of E. cl	4.72	9.77		
17.2 " " " = E. Rail	4.67	9.82		
	0+69			
17.2 W. of E. cl = E. Rail	4.89	9.60		
8.6 " " " "	4.86	9.63		
	0+97			
8.6 W. of E. cl	5.10	9.39		
17.2 " " " "	5.13	9.36		
	1+25			
17.2 W. of E. cl	5.33	9.16		
8.6 W. of E. cl	5.24	9.21		

14.49
1+50

8.6' W of E. d	5.49	9.00
17.2' " " " = E. Rail	5.51	8.98
2+00		
17.2' W of E. d	5.89	8.60
8.6' " " "	5.72	8.77
7.6' " " " Steam M.H. Cover	5.68	8.81
2+50 S		
8.6' W. of E. d	6.30	8.19
17.2' " " " "	6.23	8.26
3+00 = N Line E. St		
17.2' W of E. d = E. Rail	6.62	7.87
8.6' " " " "	6.67	7.82

2+94
6.5' W of E. d Steam M.H. Cover 6.50 7.99

BM 10.50	E Line Keel ex stake	S. on Rd cutb.	10.80	10.86	S Line Bdy.	Exit	78
5.42	4.92	5.12	4.99	10.15, 10.07, 9.94	0+00, 0+16, 0+32	0+69	9.65
<u>15.92</u>	<u>11.00</u>	<u>5.12</u>	<u>4.99</u>	<u>5.77</u>	<u>5.85</u>	<u>5.88</u>	<u>6.27</u>

1+00	1+25	1+50	1+75	2+00	2+25
7.40	9.20				
6.52					

2+50	2+75	N Line E.
		3+00
		7.80

15.92
6.46
New 7.46 B.M. B.P.S.W. Ketterer + Brood way

553

Rocky Ocean Beach { Maggie & New Post
Funds & Budget

4.00.14
395.42
4.72

822
73
760

UNIV 4157
NEBP 576.50

077

46 4.56

550
10
216

599.4
12
611.4