

1517



65166 75951

DIT 261.52  
45° 18' 30"  
49° 20'

95010  
770000  
769420  
98800  
95015  
850

MICROFILMED

DEC 24 1964

ENGINEERING DEPARTMENT  
SAN DIEGO  
CALIFORNIA

220578  
99165  
222713

22992  
75851

31.35  
28215  
22992  
65166

137892  
137892  
22982  
114916  
137892  
1498645012

MADE IN U.S.A.

210 38.10 1721 1376.8 15989 169.8201  
9766 19532  
99.6  
88.6  
78.6  
53.6  
27.2

**Our Leather Bound Engineers Note Books  
are carried in the following rulings:**

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19-12  
9 36  
4 48

11 84  
45 01  
9-48  
95-55  
831



Herschel + Wall SWP 105.72

" Prosper - SE " 98.96

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AMERICAN AND BRITISH BOOKS  
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100

101



Proposed Flying Cage  
San Diego Zoo

B.M	1.69	283.12		281.43	CT East End Pool
TP	1.30	273.09	1133.	271.79	
TP	1.78	262.16	1271	260.38	
B.M			4.13x	258.03	Cone Hill H. Gorilla Grate
TP	0.35	249.63	12.88	249.28	
TP	0.64	237.43	12.84	236.79	
TP	0.24	224.85	12.82	224.61	
TP	0.79	212.93	12.71	212.14	

Note - 8 to Beg of Batter 29.25

Top Elev. 224.00

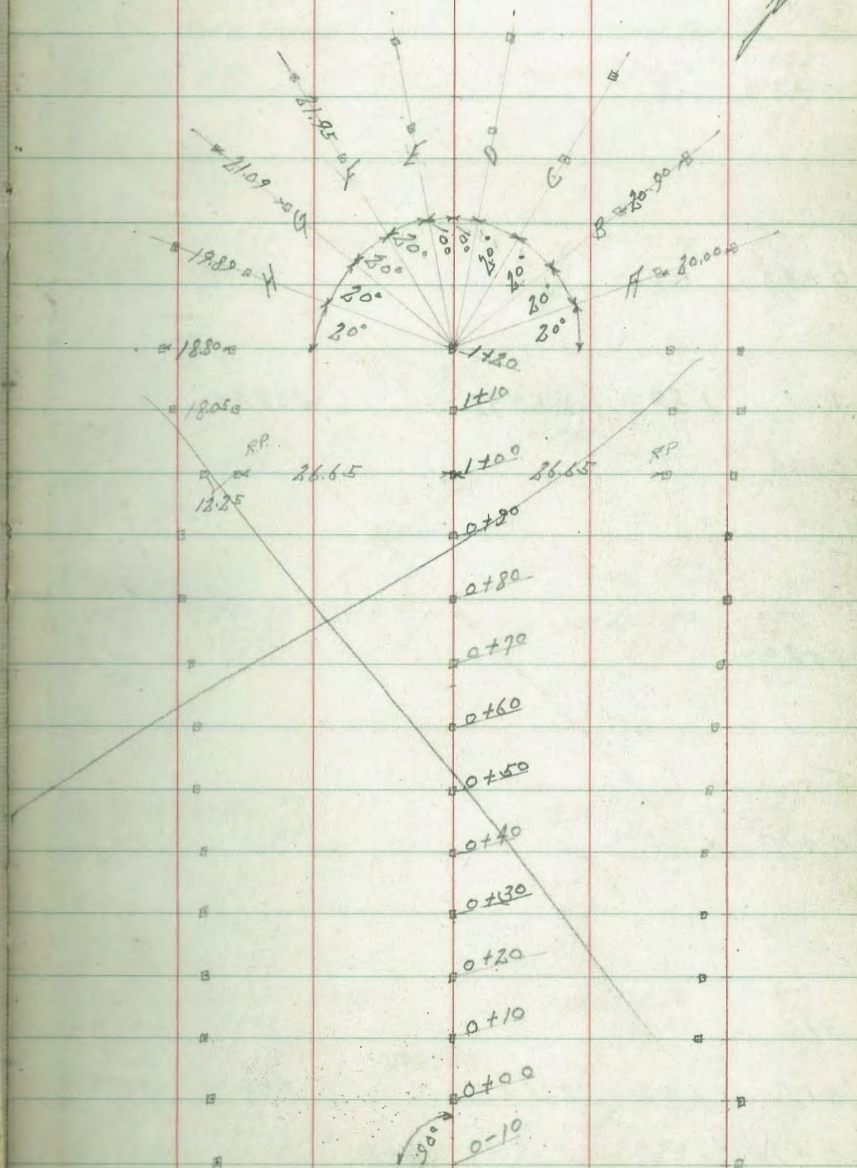
Elev. Beg of Batter 219.75

Batter 225 to 12 = 1875 Per ft

Indexed  
c.s.R.

Sheet 27

Dec 20-34  
Moore





See p 47

Lt=So  
Top of Footing

Rt=North  
Top of Footing

0+50

9.09	256.00	-13.75
7.23	32.53	
<u>01.86</u>		
7.0		

-16.05	253.20	6.72
	33.05	6.03
		<u>00.09</u>
		7.0

0+40

6.49	258.60	-11.15
6.54	32.04	
<u>00.05</u>		
7.0		

-14.05	255.70	4.22
	32.58	3.75
		<u>00.87</u>
		7.0

BM 1.89 259.92 258.03

0+20

4.99	260.10	-9.65
5.08	31.76	
<u>00.39</u>		
7.0		

BM 258.93  
7.06  
265.09

-10.65	259.10	5.17
	31.95	4.87
		<u>00.60</u>
		7.0

0+20

4.37	260.20	-9.55
3.67	31.74	
<u>00.70</u>		
7.0		

-9.95	259.80	4.77
	31.82	4.37
		<u>00.40</u>
		7.0

0+10

3.00	261.57	-8.18
3.84	31.48	
<u>00.74</u>		
7.0		

-8.25	261.50	3.07
	31.50	2.19
		<u>00.88</u>
		7.0

0+0

0.64	263.85	-5.80
1.02	31.04	
<u>00.40</u>		
7.0		

C.I. Conc  
No. 11  
0+258

-5.55	264.20	0.37
	30.99	11.96
		<u>02.36</u>
		7.0

BM 6.54 264.57 258.03

0-10

1.76	269.75	
4.04	29.95	
<u>2.28</u>		
7.0		

269.75	1.26
29.95	1.93
	<u>00.67</u>
	7.0

BM 12.98 271.01 258.03

Remaining wall  
271.01



See p 47

Lt  
Top of Footing

Z

Rt  
Top Footing

1+0

3.50  
3.33  
60.17  
7.0

232.70  
36.90 - 37.05

-37.95 231.80  
37.06

4.40  
4.18  
60.22  
7.0

TP 0.31 236.20 11.67 235.89

236.20

0+90

3.46  
3.82  
60.38  
7.0

237.40  
36.01 - 32.35

-34.05 235.70  
36.33

11.86  
60.19  
7.0

0+80

~~265.09  
12.98  
252.11  
0.35  
252.66  
12.64  
240.02  
240.87  
240.86~~

9.66  
10.05  
60.32  
7.0

242.00  
34.97 - 26.75

-30.05 239.70  
35.58

7.86  
6.76  
61.40  
7.0

0+70

4.76  
4.83  
60.07  
7.0

247.90  
34.05 - 21.85

-25.25 243.80  
34.81

3.76  
2.32  
61.44  
7.0

TP 0.28 247.56 12.64 247.28

247.56

0+60

13.09  
13.99  
60.10  
7.0

252.00  
33.28 - 17.75

-18.75 248.00  
34.03

11.92  
11.06  
60.92  
7.0

259.92

259.92



Lt

A

Rt

"F"

$$\begin{array}{r} 9.62 \\ 11.62 \\ \hline F 23.00 \\ 7.0 \end{array}$$

$$\begin{array}{r} -62.15 \\ 207.60 \\ \hline 41.60 \end{array}$$

"G"

$$\begin{array}{r} 5.03 \\ 6.23 \\ \hline F 11.26 \\ 7.0 \end{array}$$

$$\begin{array}{r} 212.20 \\ 40.74 \\ \hline -57.55 \end{array}$$

TP 1.21 217.22 12.00 215.91

~~217.22~~

"H"

$$\begin{array}{r} 10.31 \\ 11.73 \\ \hline F 22.04 \\ 7.0 \end{array}$$

$$\begin{array}{r} 218.60 \\ 39.54 \\ \hline -51.15 \end{array}$$

"A"

$$\begin{array}{r} -51.75 \\ 218.00 \\ \hline 39.65 \end{array}$$

$$\begin{array}{r} 10.91 \\ 12.55 \\ \hline F 164 \\ 7.0 \end{array}$$

1+20

$$\begin{array}{r} 4.51 \\ 5.00 \\ \hline F 9.51 \\ 7.0 \end{array}$$

$$\begin{array}{r} 224.40 \\ 38.45 \\ \hline -45.35 \end{array}$$

$$\begin{array}{r} -46.05 \\ 223.70 \\ \hline 38.58 \end{array}$$

$$\begin{array}{r} 5.21 \\ 5.37 \\ \hline F 10.16 \\ 7.0 \end{array}$$

TP 0.76 228.91 8.05 228.15

07 Stob  
3772+  
1+10

228.91

1+10

$$\begin{array}{r} 7.80 \\ 8.05 \\ \hline F 15.85 \\ 7.0 \end{array}$$

$$\begin{array}{r} 228.40 \\ 37.70 \\ \hline -41.35 \end{array}$$

$$\begin{array}{r} -43.15 \\ 226.60 \\ \hline 38.04 \end{array}$$

$$\begin{array}{r} 9.60 \\ 8.82 \\ \hline F 18.42 \\ 7.0 \end{array}$$

236.20

236.20



B.M.

2.42

204.67

Top Pipe Fence  
Past N/4 End  
Tiger Grotto

E

~~2.09  
2.80  
F 0.71  
7.0~~

~~206.00 - 63.75  
41.90~~

D

~~-68.25 201.50  
42.75~~

~~6.59  
7.81  
F 1.22  
7.0~~

C

~~-62.75 207.00  
41.71~~

~~1.09  
6.98  
F 5.89  
7.0~~

T

0.92

208.09

10.05

207.17

208.09

B

~~213.20 - 56.55 4.03  
40.55 6.80  
F 2.18  
7.0~~

217.22

217.22



Tied 7' Toward 2

Top of Inside Footing

Top of Inside Footing

"G"

1.02  
37  
60.91

214.20  
33.65

TP

0.23 215.22 18.02 214.99

215.22

"H"

9.41  
8.81  
60.80

218.60  
33.65

"H"

218.00  
33.65  
10.01  
10.50  
F0.49

+20

3.61  
2.01  
F0.40

227.40  
33.65

223.70  
33.65  
4.31  
6.36  
F2.05

+10

-0.39  
1.02  
F1.41

228.40  
33.65

226.60  
33.65  
1.41  
3.32  
F1.91

TP

0.07 228.01 18.92 227.94

228.01

140

8.16  
9.88  
F1.92

232.90  
33.65

231.80  
33.65  
3.06  
11.37  
F2.21

240.86

240.86



Sop p 47

7

Top of Inside Footing

Z

Top of Inside Footing

B"

$\frac{213.20}{33.65} \quad \frac{208}{178}$   
C 0.27

C"

$\frac{208.50}{33.65} \quad \frac{6.72}{6.09}$   
C 0.63

D"

$\frac{205.50}{33.65} \quad \frac{9.72}{9.44}$   
C 0.28

E"

$\frac{7.22}{5.72}$   
C 1.47

$\frac{208.00}{33.65}$

F"

$\frac{4.22}{3.50}$   
C 0.78

$\frac{211.00}{33.65}$

215.22

215.221



B

C

D

E

F

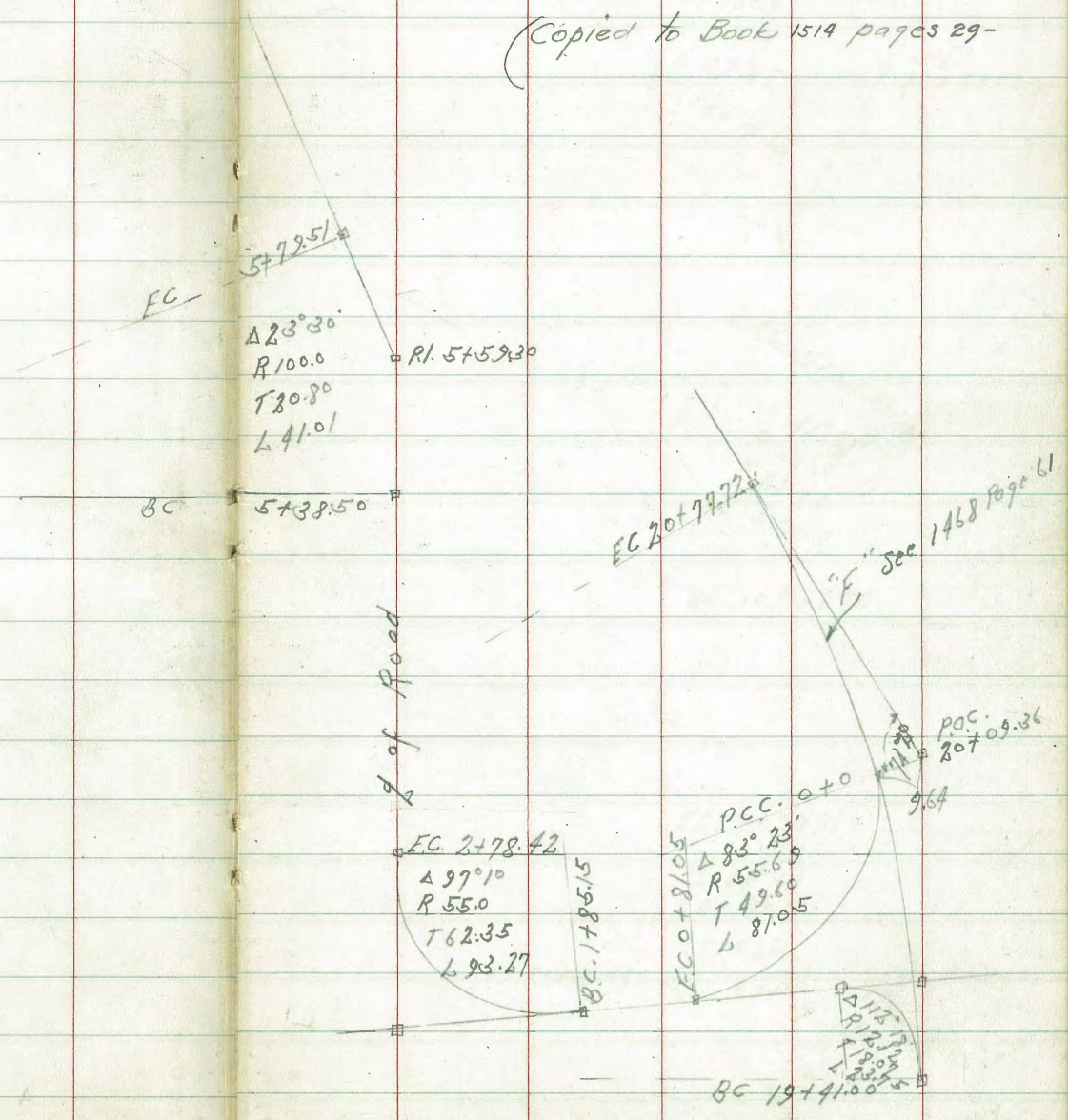


Alignment of Road west of Deer Point  
San Diego Co

INDEXED  
C.S.K.

Dec. 27-34  
Moore

(Copied to Book 1514 pages 29-





EC. 13+48.53

$\Delta 21^{\circ} 42'$

R 100.0

T 19.17

L 37.87

BC. 13+10.56

(91)  
13+29.83

EC. 11+03.96

$\Delta 31^{\circ} 32'$

R 100.0

T 28.23

L 55.04

PI. 10+77.15

BC. 10+48.92

EC. 7+79.01

$\Delta 44^{\circ} 04'$

R 130.0

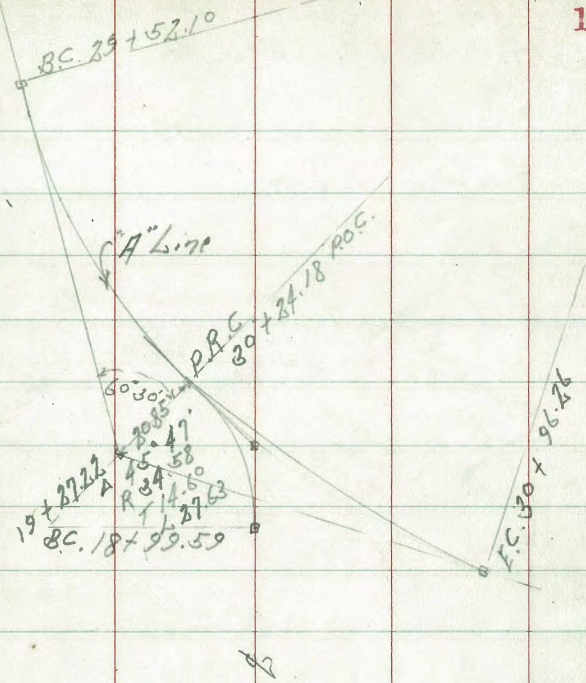
T 52.61

L 99.98

PI. 7+31.64

BC. 6+79.03





FC 17 + 59.01

A 73° 28'  
 R 100.0  
 T 74.63  
 L 128.22

PT. 17 + 05.42

BC 16 + 30.79



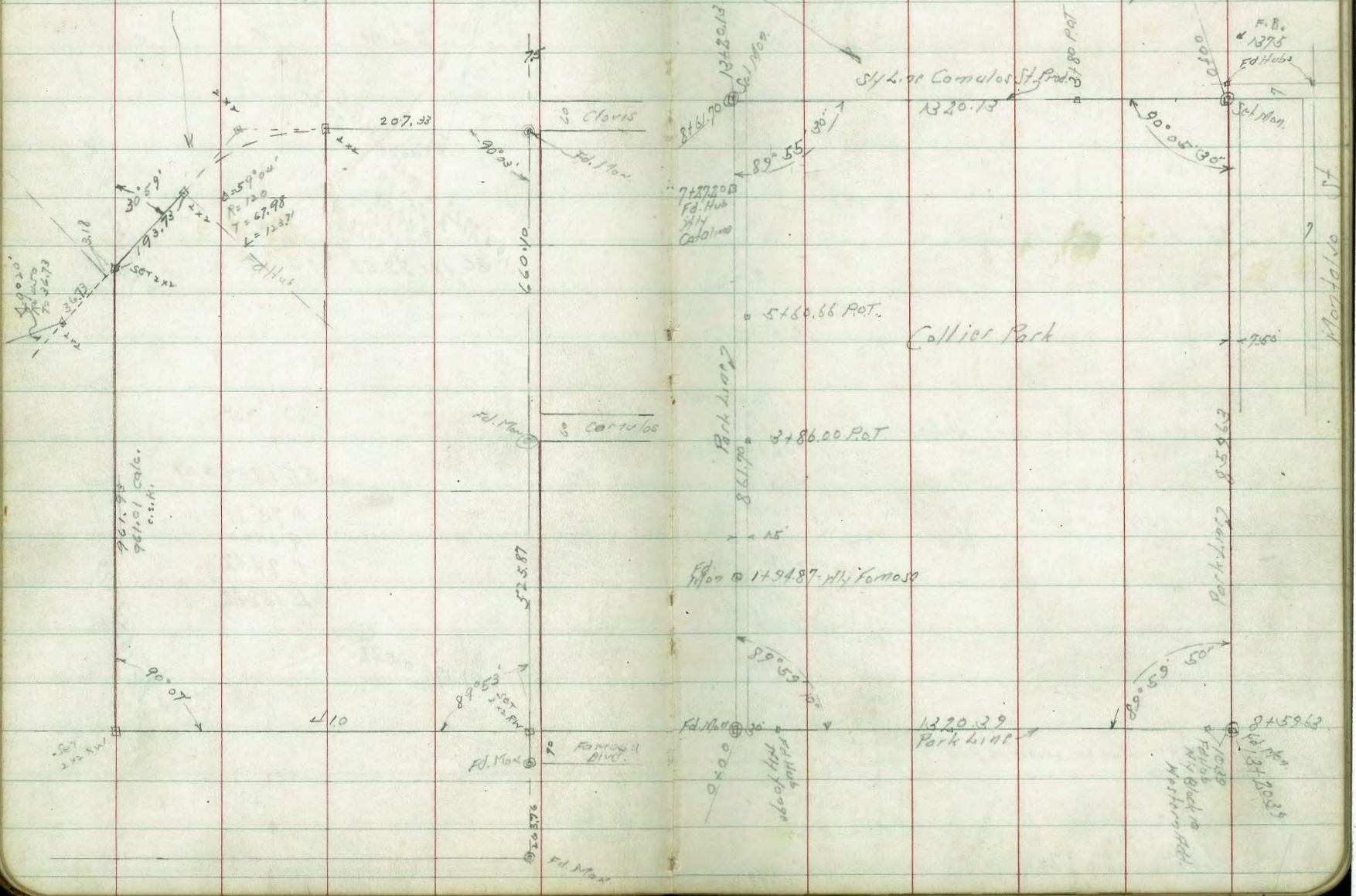
Proposed High School Site #1  
Collier Park 26.06 Ha.

Indexed  
C.S.K.

1-16-35  
Moore 12

Plotted 2103-B  
C.S.K.

Site #2 1-14-37





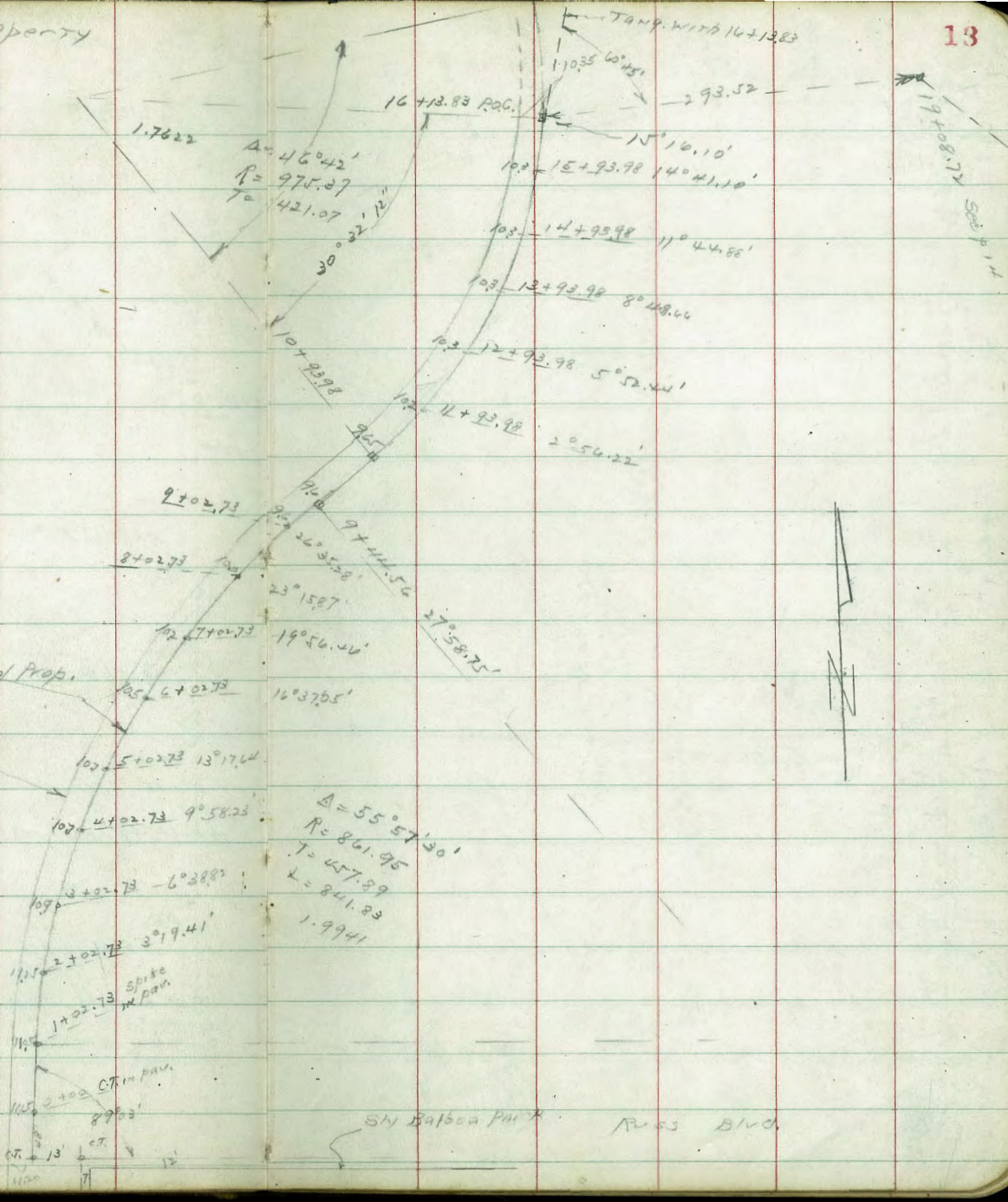
Moore  
12-21-36

S.D. High School Property  
- see p 14

16+13.83 POC. 2x2 RW hub

10+93.98 B.C. 2x2 RW hub

9+44.56 EC 2x2 RW "



Proposed Wly Line of School Prop.

Gauge of Ely rail of Ely Track

1+02.73 B.C. RT. on hd. spike in pav.

0+00 Wly of Russ Blvd. CT.

00-48 Sly 12' Line of Russ Blvd. CT

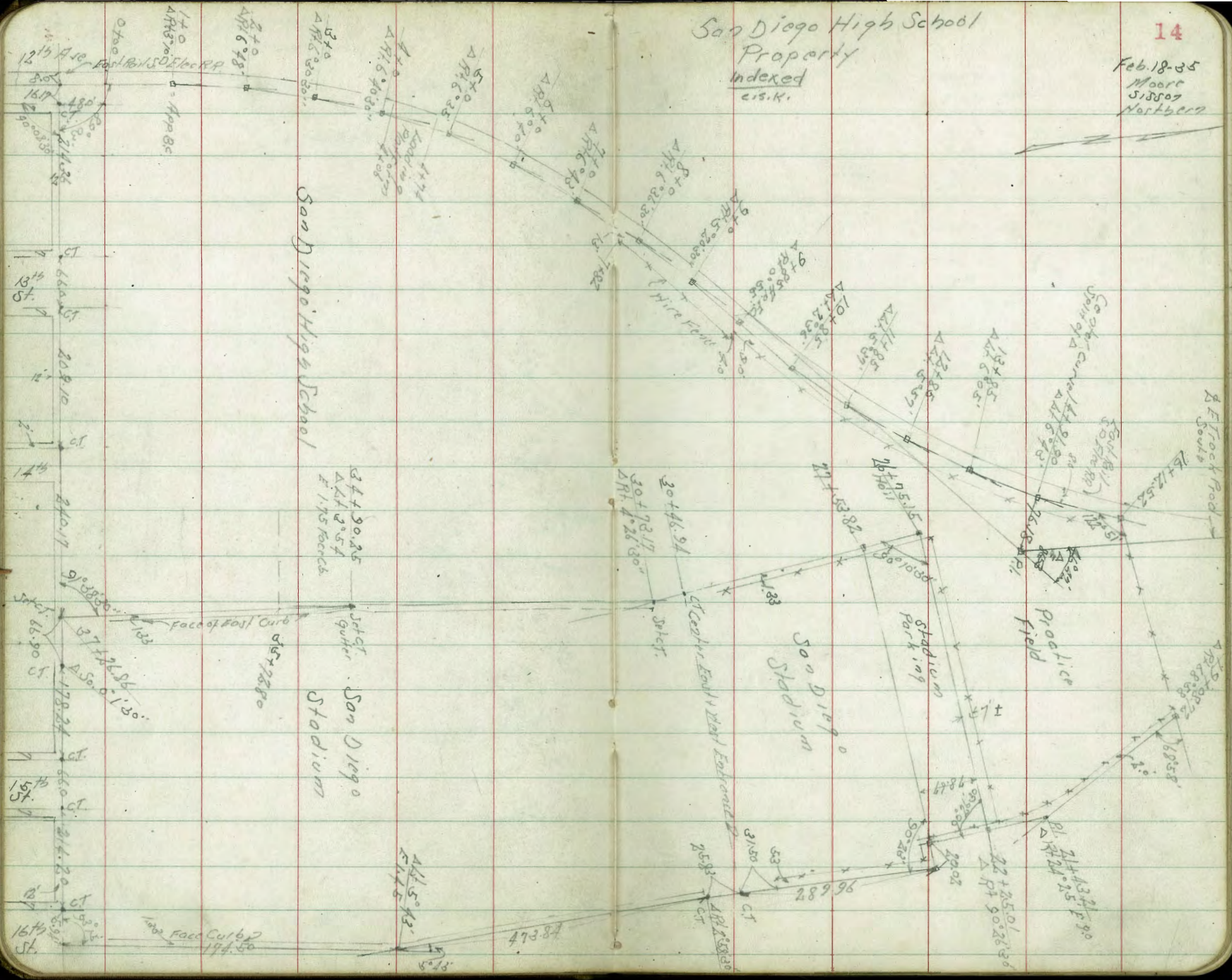
12 7 5 5'

SN Balboa Park Russ Blvd.



San Diego High School  
Property  
Indexed  
C.S.K.

Feb. 18-35  
Moore  
513807  
Northern



San Diego High School

Stadium  
Stadium  
Stadium  
Stadium

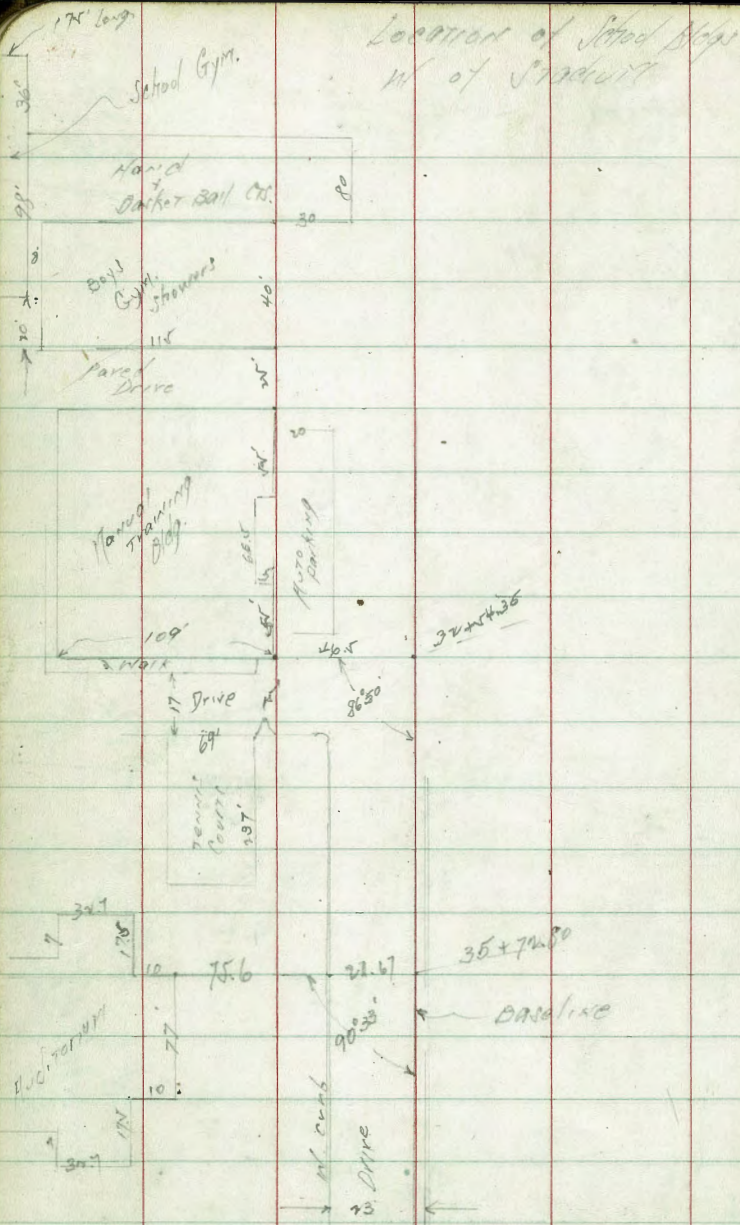
San Diego  
Stadium

Produce  
Field

A.E. Brock Road

140  
474370  
0700  
1215  
167  
186  
190  
192  
194  
196  
198  
200  
202  
204  
206  
208  
210  
212  
214  
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222  
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228  
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388  
390  
392  
394  
396  
398  
400





Location of Stood Steps  
W of Stadium

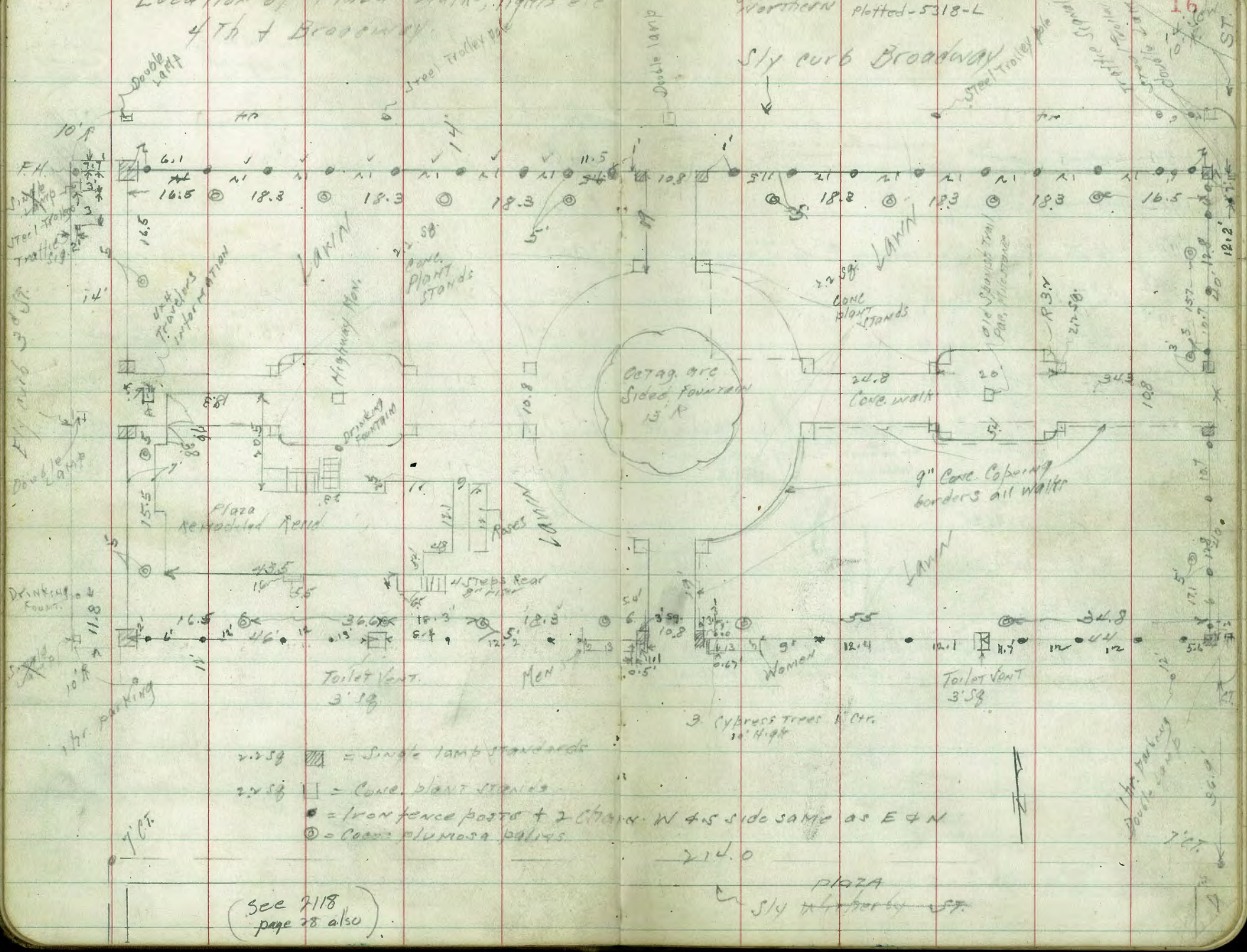
LOCATION OF  
PAVING

EMILET. TO W - W "	W mil W Tr. to to Edge pav.	width paving
0 + 42.5	21	27
0 + 90	21	30
1 + 00	21	20
7 + 00	21	30
9 + 00	21	30
12 + 85	21	30
13 + 85	21	30
14 + 91.9	21	30
16 + 12.5	21	30



Location of Plaza walks, lights etc  
4th + Broadway.

Moore 2-20-35 INDEXED  
Lisson Northern plotted-5318-L  
C.B.K.



(See 7118  
page 28 also)

214.0

PLAZA  
Sly curb Broadway ST.



36"

21-15-30

92849  
70

Bearing

~~10150~~ ~~Δ 2° 3" L~~

55.2

8+95<sup>E</sup> ~~Δ 0° 29'~~ 100.2

8+95<sup>E</sup> Δ Lt 3° 01' <sup>52'</sup> Line crown  $\Phi$  of Triggs

8+39<sup>E</sup> Δ Rt 1° 15' 200.2

6+39<sup>E</sup> Δ Lt 2° 27' 30" 178.2

4+80<sup>E</sup> Δ Rt 10° 05' 98.2

3+82<sup>E</sup> Δ Rt 19° 13' Line crown  $\Phi$  of Mason St  
at intersection of Monument  
Mason

3+20

> 2+00 Δ Lt 11° 46' 30"

Void

> 1+00 Δ Lt 12° 4' 30"

S 39° 07' 30" E

> 0+22<sup>25</sup>  $\Phi$  Line of Whitman 17<sup>th</sup> South 59° E

S 27° 03" E

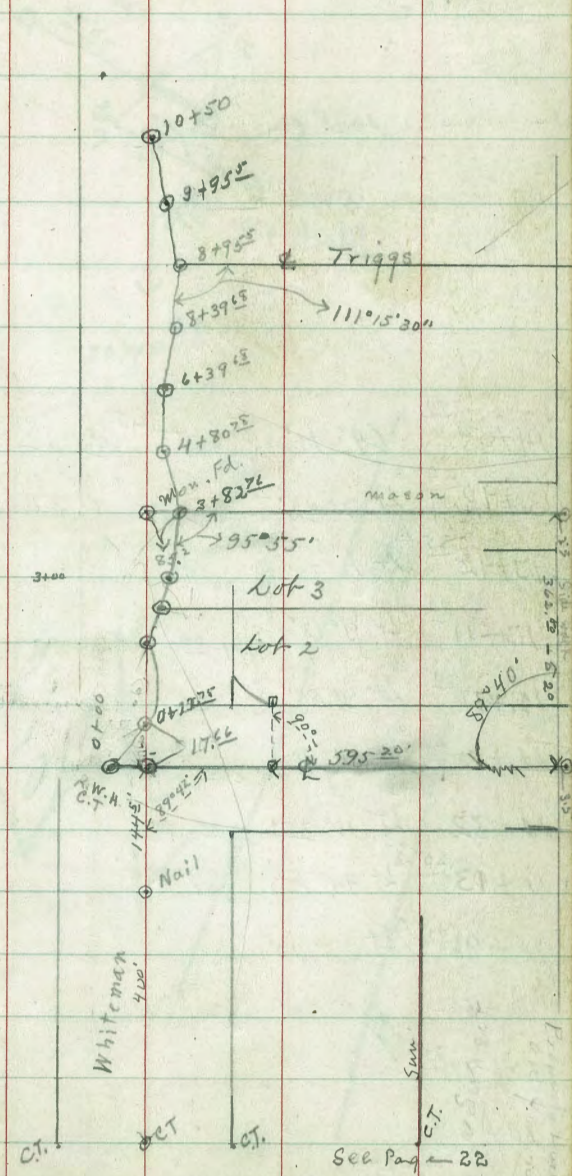
> 0+00 from intersection of Waller

S 50° 45" E

4+00 Trail

0+00 C. Tack

S 53° 45" E 5



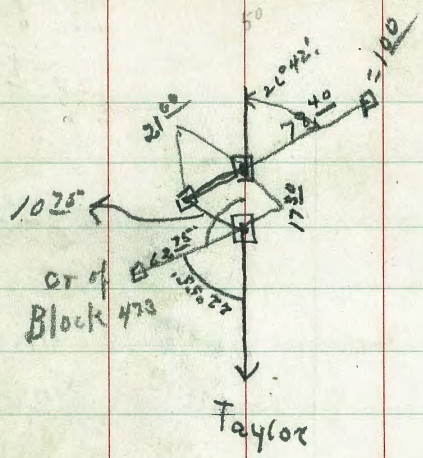
See Page 22



173  
132.3  
41

148.29  
32  
16

191.26  
173.76  
17.50

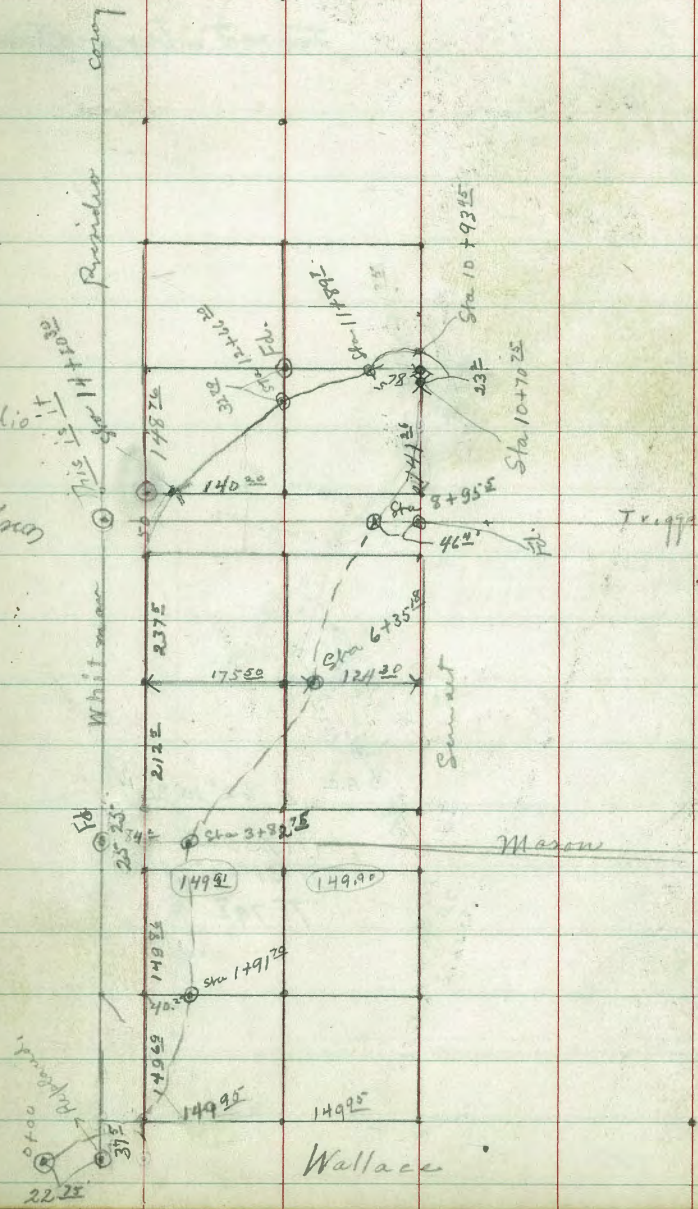


14+54	50	64° 11'	44.50
13+90	20	Lt 7° 32'	47.25
13+42	35	Lt 19° 35'	30.65
13+11	70	Lt 9° 13'	51.05
12+78	70	Lt 9° 05'	32.60
10+52	20	Lt 4° 20'	20.5
10+32	20	Lt 10° 35'	18.25
11+13	20	Lt 44° 12'	16.50
10+96	75	Lt 37° 40'	11.0
10+86			22.00
10+70	75		
10+60			
10+50		Δ Lt 6° 40'	

44.50 to c.T. E of corner of Presidio  
 (Drawings of Rest Room)

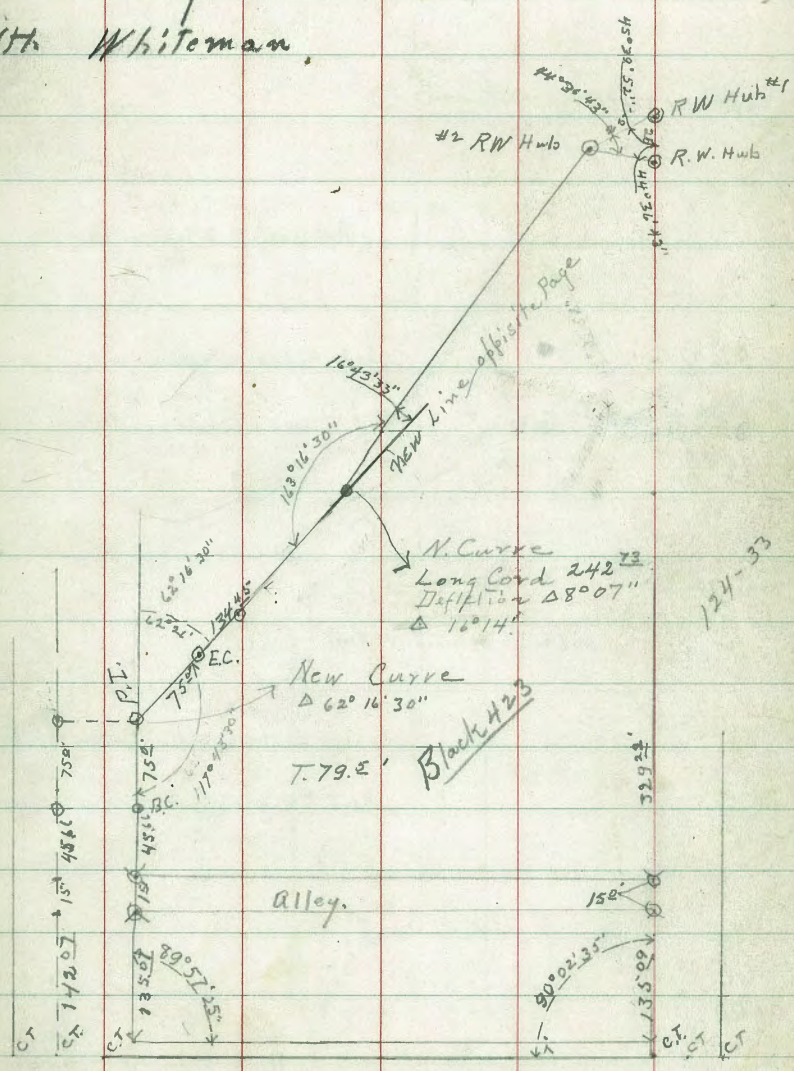
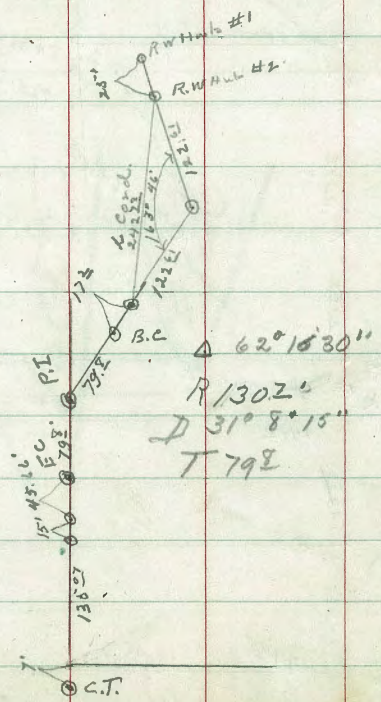
**Void**  
**Void**

2.37





Jackson St From Taylor  
To Intersection with Whiteman





Relocation of Lot Corners on North Line (N30°E) of Block 429+429 - (also Whitman) and tying in the NE Easterly Line of New Road to these corners. Also projection of Whitman Easterly to  $\phi$  of Twiggs St.

Sta Remarks

3771.01 + 3750 (2)

(Not Set)

5+8236

Set Redwood Hob.

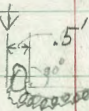
5+62.0 = 0+21.5 Page 17

$\phi$  Whitman Crosses E Side of Cobble Stone Drain on E Line of St

5+41.86

Note

Assumed NE Line



Cross Section Cobble Drain NE Line

Road Showing assumed NE Line

Road

0+00

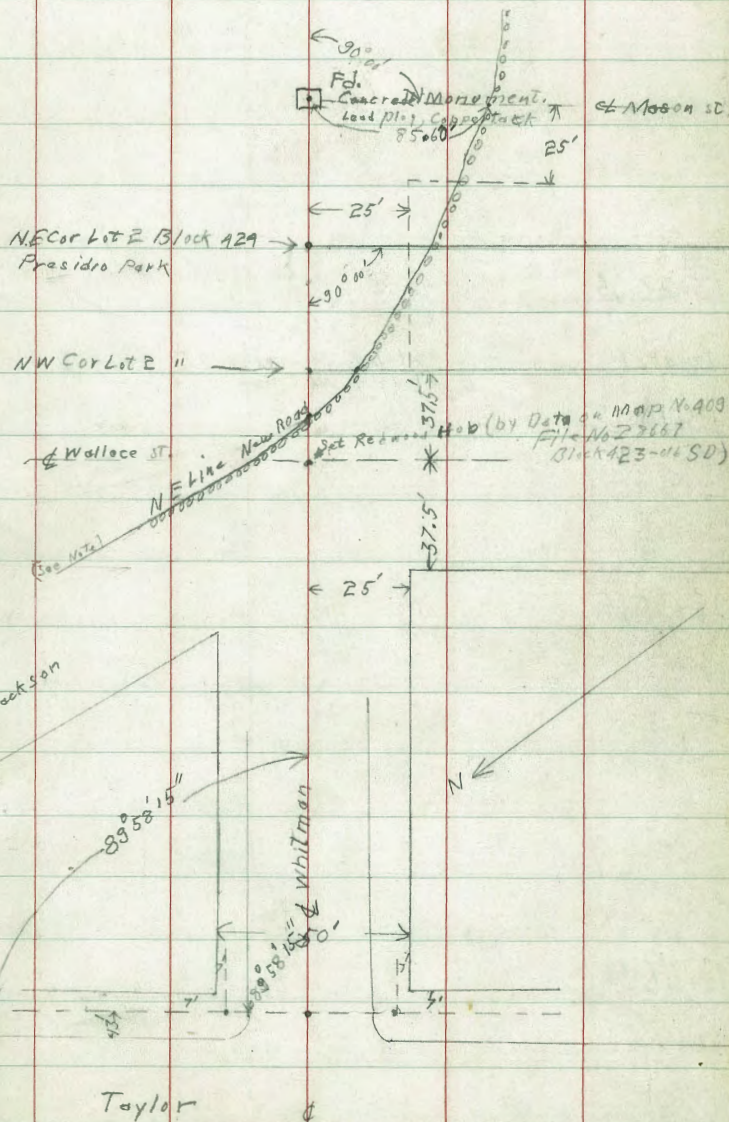
A.R. Essery  $\pi$  5/14/35 indated  
A.B. Goldwell  
Paul Losey

12.57  
14.55  
17.20

20

149.89  
17.92  
32.5  
362.05

Note (Ties to New Road not completed)





Sta                      Remarks

13+82.36

13+46.01  
69.51

13+13.45

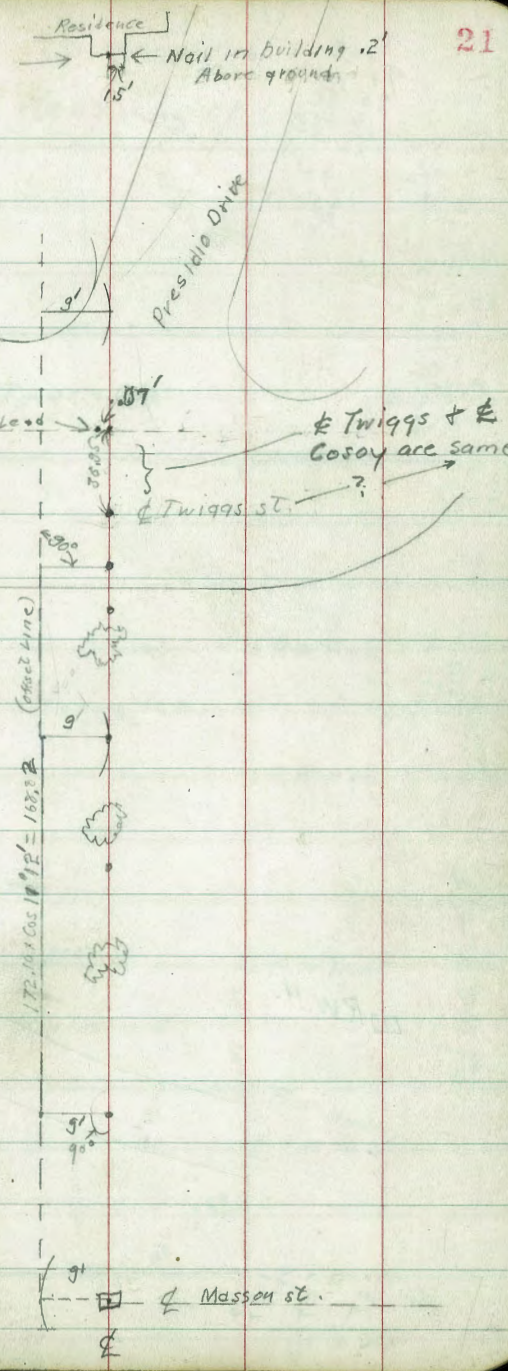
78.50  
12+35.15

11.65.87  
10+66.33

8+71.21

Set by chaining 475' from ♀ Mason St  
E along ♀ Whitman

AR. Essex  $\pi$  5/1955  
AB, Cold wall / Foresight  
Raul Losey





97.60  
 35.50  
 16.85  
 ---  
 521.35  
 149.15  
 25  
 ---  
 174.15

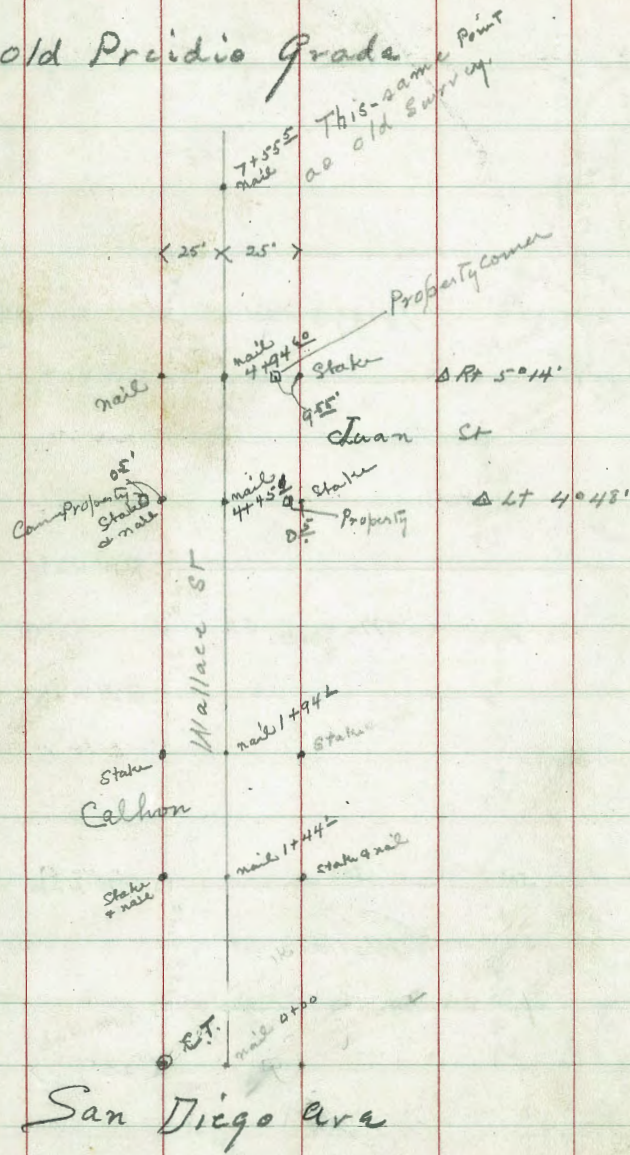
137.  
 97.  
 ---  
 40



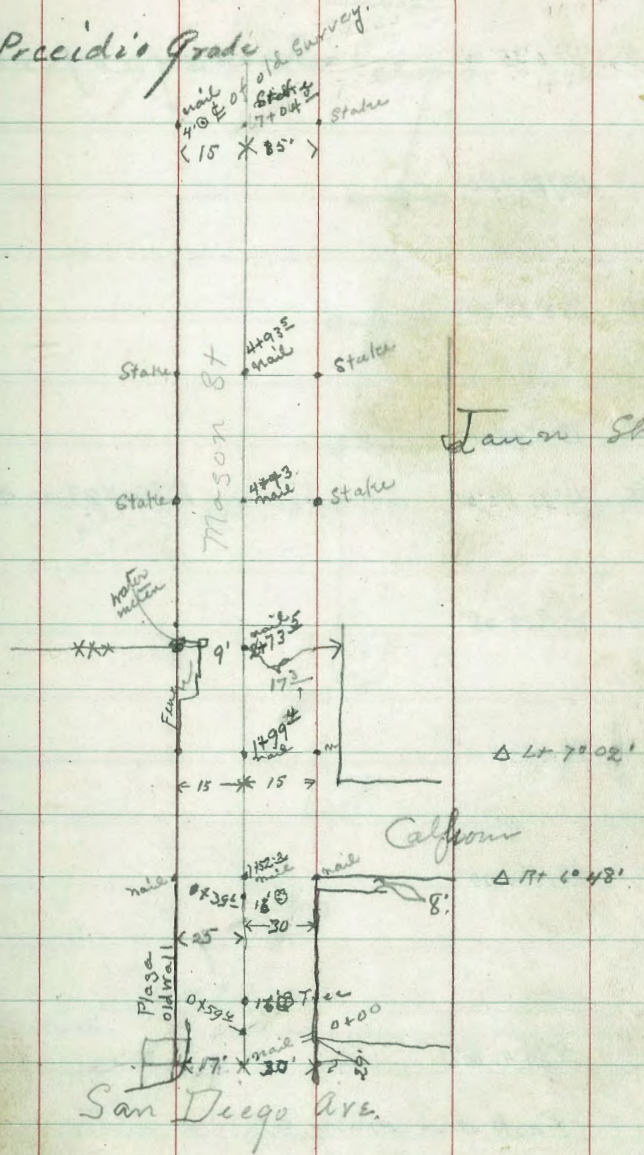
300  
 50  
 299.90  
 25  
 ---  
 674.70  
 300  
 ---  
 374.90  
 50  
 ---  
 324.90  
 842  
 ---  
 2402  
 30.2  
 ---  
 210.5  
 149.95  
 59.35  
 ---  
 90.70



# old Precidio Grade



# Old Precidio Grade





azimuth

Survey of Old Precidio grade Road

6+66 =  $19^{\circ} 0' 35'' 00''$

5+50  $19^{\circ} 10' 45'' 00''$

4+50.00  $19^{\circ} 3' 56'' 30''$

3+89.25  $19^{\circ} 6' 47'' 30''$

3+89.75  $14^{\circ} 9' 51'' 00''$  Line between Bets 424 & 449

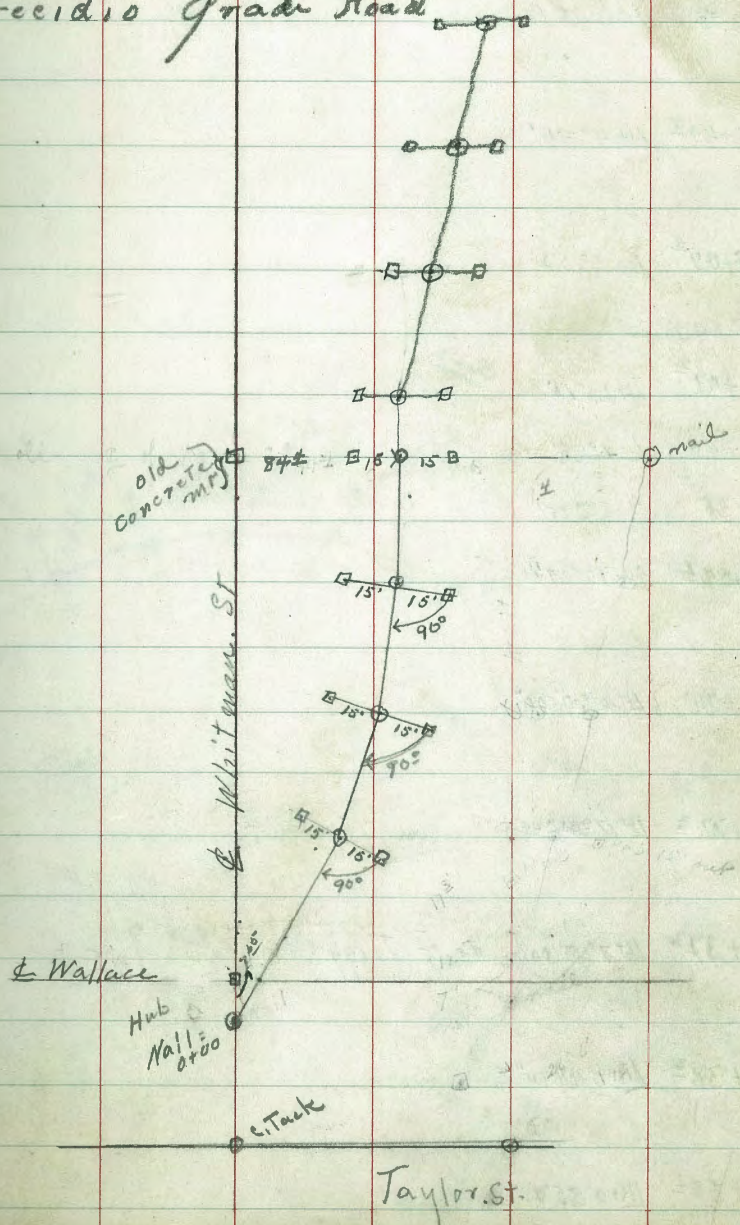
3+00  $14^{\circ} 1' 39'' 00''$

2+00  $14^{\circ} 10' 50'' 00''$

1+00  $14^{\circ} 12' 9'' 00''$

0+00  $15^{\circ} 29' 46'' 00''$

Each and every station noted  
on this survey is a P.I. of curve





13+83<sup>2</sup> next Page

13+49<sup>2</sup> Lt 4° 44'

13+09<sup>2</sup> Lt 3° 52'

12+49<sup>2</sup> Lt 3° 53'

12+07<sup>2</sup> Lt 10° 18' 00" check

11+51<sup>2</sup> Lt 8° 15' ✓ To Lot Center 44<sup>32</sup>

11+08<sup>2</sup> Lt 17° 27' 00" to Lot Center 15<sup>00</sup>

10+21<sup>2</sup> Lt 13° 45' 0"

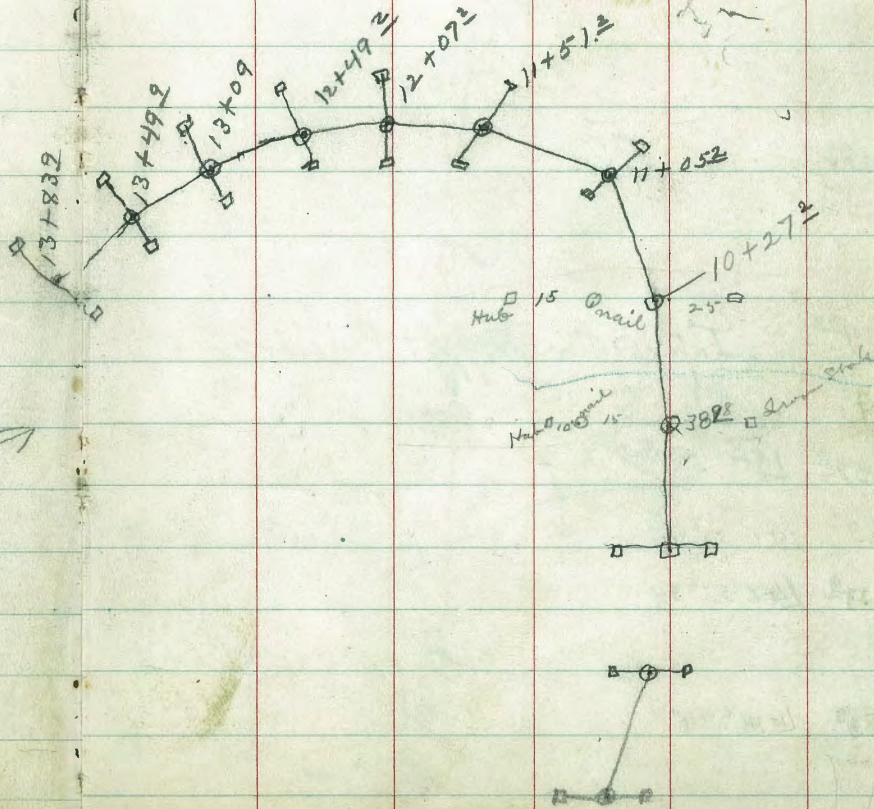
9+71<sup>2</sup> Lt 7° 50' 00"

9+27<sup>2</sup> Lt 7° 50' 00" E of Triggs St

6'

8+66<sup>2</sup> Lt 1° 43' 00"

7+66<sup>2</sup> Lt 0° 35' 00"





59.14  
23  
44.14

26  
17.91  
5.21

66.09

15734<sup>ex</sup>

Intersection Triggs & Precidia  
43E

14489<sup>2</sup>

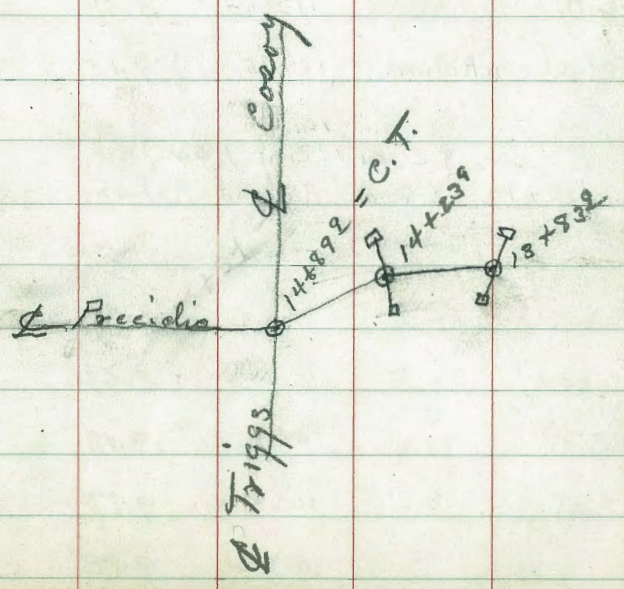
LST. check

14423<sup>2</sup>

L46°52'30"

13483<sup>2</sup>

L44°44'





8-20-35  
Miller  
Walker  
Bliss

Sassafras St. X See.  
Metzner to Pacific Hwy

80' wide  
14' chs.  
13' 1/2

indexed  
C.S.K.

19.90

27

Top B.M.F.H.	8.00	19.90	11.90	S.E. Pacific & Sassafras				
		00 = E Line Pacific			gutter		11.27	8.63
					s.d		10.63	9.27
S.		10.5	9.40		S		10.6	9.3
+ 10 = emt. ch. on Return		10.75	9.15				0 + 50	
Gutter pav.		11.33	8.57		S-10		10.6	9.3
S. ch line "		11.23	8.67		S		10.6	9.3
S. 1/4 "		10.84	9.06		ch		10.8	9.1
♀ "		10.71	9.19		1/4		10.5	9.4
N. 1/4 "		10.82	9.08		♀		10.2	9.7
N. ch line "		11.20	8.70		1/4		10.3	9.6
+ 4.0 gutter		11.32	8.58		ch		10.5	9.4
+ 4.0 emt. ch. on Return		10.75	9.15		N.		10.2	9.7
N.		10.6	9.30		+ 1 on pav		9.8	10.1
		E. End. Emt. Pav.			+ 10		9.8	10.1
		0 + 12 = E.C. 20' Rad. ch. Returns						
N.		10.7	9.2				0 + 88	
ch.		10.62	9.28		N-10 pav.		9.45	10.45
Gutter pav		11.23	8.67		- 1 "		9.40	10.50
1/4 "		10.77	9.13		- 0.5 Top 5" curb		8.45	11.25 W. End.
♀ "		10.63	9.27		N.		9.4	10.5
1/4 "		10.82	9.08					



19.90

	1+00		
N-10, pay	9.3	10.6	
N-1, u	9.3	10.6	
N-05 Top emf. el.	8.55	11.35	
N	9.1	10.8	
el	9.2	10.7	
"4	9.3	10.6	
±	9.4	10.5	
"4	9.4	10.5	
el	9.4	10.5	
S	10.0	9.9	
+10	10.4	9.5	

1+25

S-10	10.1	9.8	
S-5	7.1	12.8	
S	7.3	12.6	
el	7.5	12.4	
"4	8.0	11.9	
±	7.8	12.1	
"4	7.7	12.2	
el	7.9	12.0	

19.90

N		7.7	12.2	
+0.2 Top emf. el.		7.86	12.04	
+0.6 pay.		9.00	10.90	
+10. u		9.10	10.80	
	1+29.			
N. line Top emf. el.		7.81	12.09	Brk. Grade
	1+35 <sup>5</sup>			
N-10 pay at foot of wall		9.00	10.90	
N-0.6 pay at " " "		8.84	11.06	
N-0.2 Top emf. el.		6.76	13.14	
N				

1+36

N-10 Top Wall dirt. to E.		6.82	13.08	
N-0.6 " " " "		6.70	13.20	
N-0.2 " curb.		6.70	13.20	
N.				
	1+50			
N-10		4.8	15.10	
N-0.2		4.43	15.47	
N		4.6	15.30	

Sassafras St. 28



		19.90				30.32	
		1750 (con)					
N. el		4.8	15.10		+8	12.2	18.1
"4		5.0	14.90		N	14.1	16.2
Φ		4.5	15.40		+7	14.1	16.2
"4		3.8	16.10				
el		3.0	16.90		-10	13.4	16.9
S		3.0	16.90		N	13.4	16.9
+10		3.3	16.60		+2	13.3	17.0
T		1456			+4	11.1	19.2
N-0.2 Top ent curb		3.55	16.35	Brk grade	el	8.6	21.7
		1459			"4	8.3	22.0
N-0.2 East End Top ent wall		3.58	16.32		Φ	8.0	22.3
T.P.	11.27	30.32	0.85	19.05	"4	7.7	22.6
		1475			d	7.9	22.4
S-10		10.2	20.1		S	8.2	22.1
S		10.8	19.5		+10	9.0	21.3
el		10.8	19.5			2400	
"4		11.0	19.3		-10	8.6	21.7
Φ		11.3	19.0		S	8.5	21.8
"4		11.5	18.8		el	7.6	22.7
el		11.8	18.5		"4	7.5	22.8



30.32  
2+00 (cont)

ϕ	7.8	22.5
1/4	8.1	22.2
cl.	8.4	21.9
+10	10.3	20.0
N.	10.3	20.0
+10	10.2	20.1

2+10

-10	8.1	22.2
N	7.6	22.7
d	6.7	23.6
1/4	6.6	23.7
ϕ	4.5	23.8
1/4	6.5	23.8
d	6.4	23.9
S.	5.4	24.9
+10	5.3	25.0

2+40

-10	4.8	25.5
S	4.8	25.5
cl	4.8	25.5

30.32

1/4	4.7	25.6
ϕ	4.4	25.9
1/4	4.8	25.5
cl	4.9	25.4
N	5.3	25.0
+10	6.3	24.0

2+48<sup>L</sup> = W. Rail A.T.S.F.R.R.

N	4.34	25.98	26.00
ok ϕ	4.04	26.24	26.15
ok S.	3.85	26.47	26.34

2+52<sup>g</sup> = E Rail

S	3.84	26.48
ϕ	4.08	26.24
N	4.34	25.98

2+62 ϕ BIK signal

S. Line = N. side emb. foundation

Top emb. foundation	3.18	27.14
---------------------	------	-------



30.32  
2+66.

S-10	4.0	26.3
S	4.1	26.2
cl	4.7	25.6
"4	4.8	25.5
±	5.0	25.3
"4	5.1	25.2
cl	5.3	25.0
N	5.5	24.8
+10	5.8	24.5
	2+70	
N.	2.3	28.0
+7	3.7	26.6
cl	1.0	29.3
"4	0.6	29.7
±	0.9	29.4
+6	0.6	29.7
+9	4.0	26.3
"4	4.5	25.8
+5	4.3	26.0
+9	1.4	28.9

30.32

Sassafra. St.

31

cl		1.4	28.9
+2		2.7	27.6
S		4.4	25.9
T.P.	12.19	42.10	0.41
		2+78.	
S		14.0	28.1
cl		14.2	27.9
"4		14.7	27.4
±		14.2	27.9
"4		13.6	28.5
cl		14.0	28.1
N		15.4	26.7
		3+00	
N		12.4	29.7
cl		13.3	28.8
"4		13.5	28.6
±		12.3	29.8
"4		10.9	31.2
cl		12.6	29.5
S		13.0	29.1



42.10  
3+25

S	10.8	31.3
cl	10.5	31.6
1/4	10.5	31.6
±	11.2	30.9
1/4	11.7	30.4
cl	11.8	30.3
N	11.7	30.4

3+50

N	10.8	31.3
cl	11.0	31.1
1/4	10.4	31.7
±	10.5	31.6
1/4	9.8	32.3
cl	8.8	33.3
S	9.7	32.4
	10.3	31.8

3+75

-10	6.4	35.7
S	6.3	35.8
cl	6.6	35.5

42.10

Sassafras St. 32

+4	7.7	34.4
1/4	8.1	34.0
± ground	8.4	33.7
± Top M.H. Rim	7.98	34.12
1/4	8.6	33.5
cl	9.4	32.7
N	9.7	32.4
+10	9.8	32.3

4+00

N	6.7	35.4
cl	6.0	36.1
1/4	5.9	36.2
±	5.6	36.5
1/4	5.0	37.1
+2	4.8	37.3
+3	7.3	34.8
+11	7.0	35.1
cl	4.4	37.7
S	3.8	38.3



	42.10				51.39		Sassafras St. 33
	4+25						
5		1.2	40.9		+4 = S. E. Cor. Wooden steps	8.70	42.69 on emt. bottom step
+9		1.9	40.2		cl.	10.0	41.4
cl.		5.0	37.1		1/4	9.8	41.6
+7		6.2	35.9		1/4	9.8	41.6
+8		2.0	40.1		1/4	9.2	42.2
1/4		1.9	40.2		+10	9.4	42.0
1/4		2.5	39.6		+11	14.3	37.1
1/4		2.8	39.3		cl.	14.4	37.0
cl.		3.1	39.0		+8	12.2	39.2
+10 =	S. W. Cor. wooden Porch.	2.5	39.6	ground.	+9	9.8	41.6
+10 =	" " " "	+4.7	46.8	floor	S	9.5	41.9
N =	N. W. Cor. Wooden Porch.	2.5	39.6	ground	+10	9.0	42.4
	4+36						
N. W. Cor. Wooden stairs							
N. W. E. Cor. Wooden Porch		1.2	40.9	ground.	-10	8.4	43.0
S. E. " " stairs		1.2	40.9	" "	S	8.4	43.0
T.P.	9.92	51.39	-0.63	41.47	cl.	9.1	42.3
	4+43				1/4	8.8	42.6
N. = N. E. Cor. Wooden steps		8.70	42.69	on emt. bottom step	1/4	8.5	42.9
+11 = " " " "		9.3	42.1	ground	1/4	9.0	42.4
+4 = S. E. " " " "		9.7	41.7	" "	cl.	9.5	41.9
					N.	8.6	42.8



51.39  
4+68

N	6.4	45.0
cb	4.8	44.6
'4	6.3	45.1
¢	5.4	46.0
'4	6.1	45.3
cb	5.6	45.8
5	7.0	44.4
+10	6.8	44.6

4+75 = W Line Kettner

S-5	5.1	46.3
S = Cor. cont. Return	3.13	48.26
W. End. cont. cb. "	3.80	47.59
Gutter W. end. Pav.	4.53	46.86
'4 " " "	4.46	46.93
¢ " " "	4.58	46.81
'4 " " "	5.10	46.29
gutter " " "	5.81	45.58
W. End. cont. cb. Return	5.23	46.16
N. on cor. cont. "	4.65	46.74

Sassafras St 34

51.39  
12' E W  
of S. Line = W-  
s. ch. Line of Kettner

N. Line cont. cb.	5.85	45.54
N " gutter Pav	6.55	44.84
N. ch. Line "	5.04	46.35
'4 "	4.39	47.00
¢ "	4.08	47.31
'4 "	3.87	47.52
s. ch. line "	3.90	47.49
s. Line gutter "	4.03	47.36
s. " cont. cb	3.38	48.01
BM. B.P. S.E. Kettner + Sassafras.	2.34	49.65 = 49.01

See page 59 for  
Block India to Kettner



Soundings for Sunset Cliffs  
Prop. Pier A from T #1  
Sight on #2

Nov. 5-31  
Miller Rec.  
Walker T.

NOTE!  
See F.B. 1407-67-73  
for location A for Soundings

35

#1 ✓ 9:53 AM, 16°-48' RT.

#2 ✓ 8°-31' RT.

#3 ✓ 10°-45' RT.

#4 ✓ 12°-21' RT.

#5 ✓ 14°-32' RT.

#6 ✓ 17°-31' RT.

#7 ✓ 20°-05' RT.

#8 ✓ 22°-12' RT.

#9 ✓ 24°-37' RT.

#10 ✓ 10:02 AM, 25°-10' RT.



# 11	✓	25 From Baseline 27-36 Rt
# 12	✓	29°-20' Rt.
# 13	✓	31°-11' Rt.
# 14	✓	33°-36' Rt.
# 15	✓	35°-19' Rt.
# 16	✓	37°-31' Rt.
# 17	✓	39°-22' Rt.
# 18	✓	41°-15' Rt.
# 19	✓	42°-47' Rt.
# 20	✓	10:10 AM. 43°-40' Rt.



- |    |   |                       |
|----|---|-----------------------|
| 21 | ✓ | 45° 10' RT            |
| 22 | ✓ | 46° 20' RT            |
| 23 | ✓ | 47° 05' RT            |
| 24 | ✓ | 48° 08' RT            |
| 25 | ✓ | 49° 02' RT            |
| 26 | ✓ | 50° 24' RT            |
| 27 | ✓ | 51° 27' RT            |
| 28 | ✓ | 52° 43' RT            |
| 29 | ✓ | 53° 51' RT            |
| 30 | ✓ | 10:20 A.M. 54° 42' RT |



25. from Base  
Line
- # 31 ✓ 55-51 RT
- # 32 ✓ 56-45 RT
- # 33 ✓ 57-55 RT
- # 34 ✓ 58-33 RT
- # 35 ✓ 59-29 RT
- # 36 ✓ 60-28 RT
- # 37 ✓ 10:30 AM 62-05 RT
- # 38 ✓ 10:34 AM 58-15 RT
- # 39 ✓ 57-40 RT
- # 40 ✓ 10:37 A.M. 57-14 RT



# 41	✓	Δs. from Baseline 56°03' RT
# 42	✓	0' 54-41 RT
# 43	✓	53-28 RT
# 44	✓	52-23 RT
# 45	✓	50-40 RT
# 46	✓	49-31 RT
# 47	✓	48-01 RT
# 48	✓	46-33 RT
# 49	✓	44-14 RT
# 50	✓	10:48 A.M. 42-38 RT



#		
# 51	✓	Ls. from Base line 0' 40-32 Rt
# 52	✓	37°-29' Rt
# 53	✓	33°-56' Rt
# 54	✓	30°-14' Rt
# 55	✓	27°-57' Rt
# 56	✓	25°-02' Rt
# 57	✓	21°-43' Rt
# 58	✓	18°-47' Rt
# 59	✓	15°-10' Rt
# 60	✓	11.01 A.M. 12°-56' Rt



		25. from Baseline
# 61	✓	10°-06' Rt
# 62	✓	7°-34' Rt
# 63	✓	6°-08' Rt
# 64	✓	7°-56' Rt.
# 65	✓	9°-02' Rt.
# 66	✓	9°-36' Rt.
# 67	✓	12°-21' Rt.
# 68	✓	16°-24' Rt.
# 69	✓	20°-23' Rt
# 70	✓	11:11 A.M. 24°-49' Rt



Ls from  
Baseline

# 71	✓	28°-29' Rt
# 72	✓	31°-37' Rt
# 73	✓	36°-44' Rt
# 74	✓	41°-13' Rt
# 75	✓	44°-45' Rt
# 76	✓	47°-37' Rt
# 77	✓	50°-42' Rt
# 78	✓	54°-11' Rt
# 79	✓	56°-41' Rt
# 80	✓	11:20 A.M. 60°-10' Rt



25. from  
Baseline

# 81 ✓ 62° 43' RT.

# 82 ✓ 64° 50' RT.

# 83 ✓ 66° 43' RT.

# 84 ✓ 68° 30' RT.

# 85 ✓ 70° 16' RT.

# 86 ✓ 71° 00' RT.

# 87 ✓ 72° 11' RT.

# 88 ✓ 11:30 A.M. 72° 25' RT.

# 89

# 90 p 44 for soundings



Soundings for Prof.  
Pier at Sunset Cliffs

- 7.04 City Datum = El. water 11:48 P.M.

Nov. 5, 1925 - see 1407-69

#	✓	Sounding	Tide	U.S.C. & G. Elev.				Tide	U.S.C. & G. Elev.
#1	✓	taken on Baseline	7.3	+2.48	-4.82	#18	✓	16.5	+2.33
#2	✓		8.0	2.48	-5.52	#19	✓	17.0	2.32
#3	✓		8.5	2.47	-6.03	#20	✓	16.5	2.32
#4	✓		9.0	2.46	-6.54	#21	✓	20.0	2.31
#5	✓		9.0	2.45	-6.55	#22	✓	19.0	2.30
#6	✓		9.0	2.44	-6.56	#23	✓	18.5	2.29
#7	✓		11.0	2.43	-8.56	#24	✓	18.0	2.28
#8	✓		13.0	2.42	-10.58	#25	✓	18.5	2.27
#9	✓		14.5	2.41	-12.09	#26	✓	19.0	2.27
#10	✓		15.0	2.40	-12.6	#27	✓	20.5	2.26
#11	✓		14.5	2.39	-12.11	#28	✓	20.5	2.25
#12	✓		14.0	2.39	-11.61	#29	✓	22.0	2.24
#13	✓		16.0	2.38	-13.62	#30	✓	23.0	2.24
#14	✓		16.0	2.37	-13.63	#31	✓	24.0	2.23
#15	✓		17.0	2.36	-14.64	#32	✓	26.0	2.22
#16	✓		17.0	2.35	-14.65	#33	✓	26.5	2.20
#17	✓		17.0	2.34	-14.66	#34	✓	28.0	2.19
						#35	✓	28.0	2.17
						#36	✓	30.0	2.16
						#37	✓	31.5	2.14

#32 = Edge of beds

#37 end shot on Baseline



						45			
#	beginning of Sounding	Tide	U.S.C.B.G. Elev.	#	Tide	U.S.C.B.G. Elev.			
#38	beginning of Sounding Baseline	30.5	+2.13	-28.37	#58	10.5	+2.02	-8.48	
39	✓	28.5	2.11	-26.39	59	✓	9.5	2.02	-7.48
40	✓	28.0	2.10	-25.9	60	✓	8.5	2.02	-6.48
41	✓	28.0	2.10	-25.9	61	✓	7.5	2.01	-5.49
42	✓	27.0	2.09	-24.91	62	✓	6.0	2.01	-3.99
43	✓	26.5	2.09	-24.41	63	✓	8.5	2.01	-6.49
44	✓	26.0	2.08	-23.92	63	Approx. 65' from	8.5	2.01	Face Cliff
45	✓	24.5	2.08	-22.42	64	✓	7.5	2.01	-5.49
46	✓	23.5	2.08	-21.42	64	beg. Nly or RT.	7.5	2.01	of Sounding of Lead
47	✓	21.5	2.07	-19.43	65	✓	8.0	2.01	-5.99
48	✓	20.5	2.07	-18.43	66	✓	2.0	2.00	-0.0
49	✓	20.0	2.06	-17.94	66	Top of rock 10' diam.	2.0	2.00	-0.0
50	✓	20.5	2.06	-18.44	67	✓	8.0	2.00	-6.0
51	✓	20.5	2.05	-18.45	68	✓	10.0	2.00	-8.0
52	✓	18.0	2.05	-15.95	69	✓	11.0	2.00	-9.0
53	✓	17.5	2.04	-15.46	70	✓	13.0	2.00	-11.0
54	✓	17.0	2.04	-14.96	71	✓	10.0	2.00	-8.0
55	✓	16.5	2.04	-14.46	72	✓	11.0	2.00	-9.0
56	✓	14.5	2.03	-12.47	73	✓	13.0	2.00	-11.0
57	✓	12.0	2.03	-9.97	74	✓	12.5	2.00	-10.5
					75	✓	13.0	2.00	-11.0
					76	✓	13.0	2.00	-11.0
					77	✓	14.5	2.00	-12.5



			Tide	U.S.C. 46, Elev.
#78	✓	16.5	+2.00	-14.5
79	✓	18.5	2.00	-16.5
80	✓	17.5	2.00	-15.5
81	✓	18.5	2.00	-16.5
82	✓	21.0	2.00	-19.0
83	✓	22.5	2.00	-20.5
84	✓	23.5	2.00	-21.5
85	✓ Ely edge of pbeads	25.0	2.00	-23.0
86	✓	26.5	2.00	-24.5
87	✓	28.0	2.00	-26.0
88	✓	30.0	2.00	-28.0



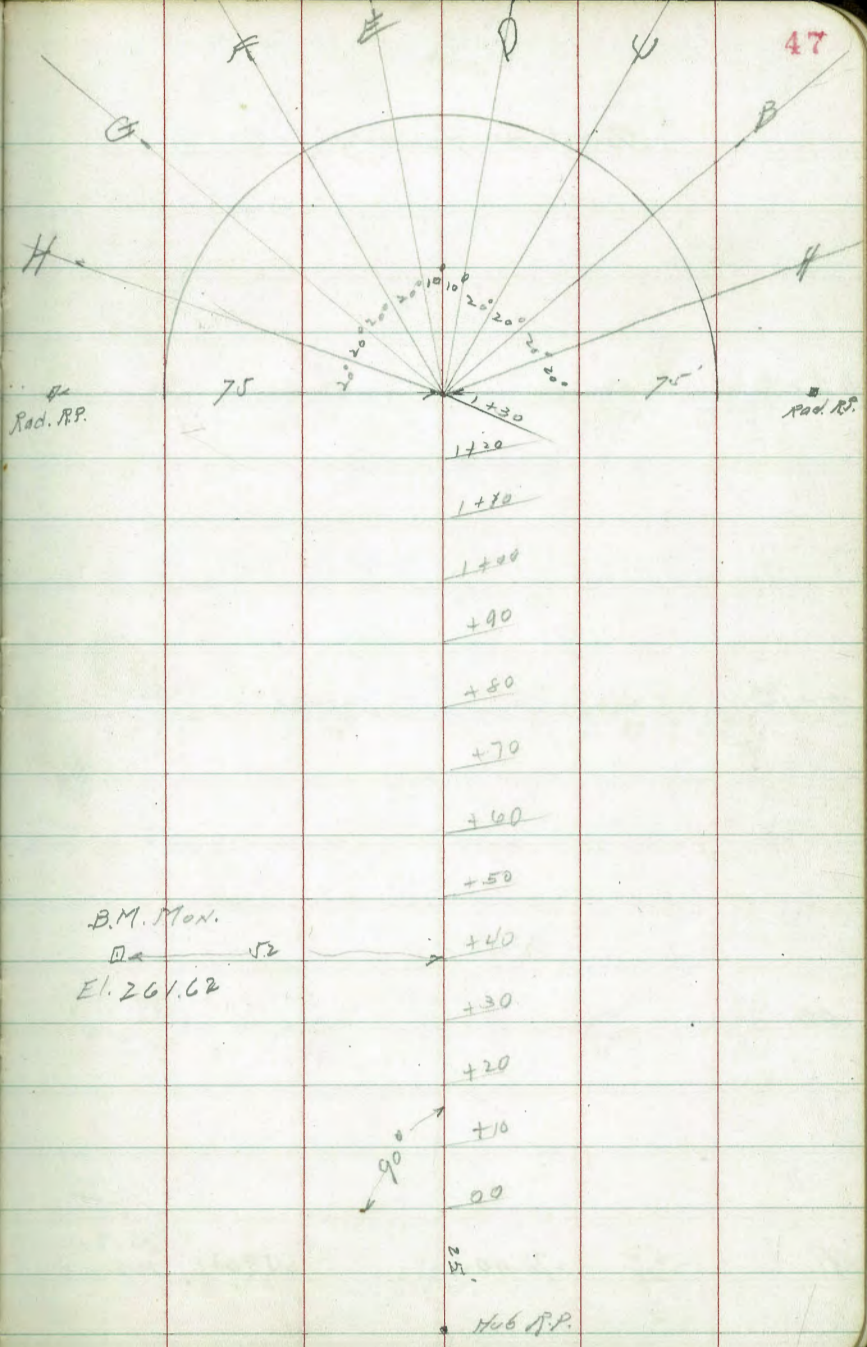
Prepared Flying Page  
San Diego Zoo Balboa Park

Moore  
Miller 1227.  
Sisson  
Bliss  
11-20-35

Note:

± to top of batter 299.5  
El. top of batter 269.75  
Batter = 2.25 to 12 ft. = 18% per ft.  
El. Top = 294.00  
El. pt. of batter for perp. inside footing = 250.00

B.M. 1/4 Cor. Mon	878	261.62	
C.T. B.M. 1237	270.40	25803	Conc. Wall W/ax Corrilla page





## Outside footings

0 + 20

$$\begin{array}{r} 8.90 \\ 2.84 \\ \hline C \quad 1.06 \\ 10 \end{array}$$

$$\begin{array}{r} 26.50 \\ \hline 31.50 \end{array}$$

$$\begin{array}{r} 26.50 \\ \hline 31.50 \end{array}$$

$$\begin{array}{r} 8.90 \\ 2.84 \\ \hline C \quad 1.50 \\ 10 \end{array}$$

0 + 10

$$\begin{array}{r} 6.20 \\ 4.03 \\ \hline C \quad 0.17 \\ 10 \end{array}$$

$$\begin{array}{r} 26.420 \\ \hline 30.99 \end{array}$$

$$\begin{array}{r} 26.420 \\ \hline 30.99 \end{array}$$

$$\begin{array}{r} 6.20 \\ 3.04 \\ \hline C \quad 0.36 \\ 12 \end{array}$$

00

$$\begin{array}{r} 0.65 \\ 0.96 \\ \hline C \quad 0.31 \\ 10 \end{array}$$

$$\begin{array}{r} 26.97 \\ \hline 29.94 \end{array}$$

$$\begin{array}{r} 26.97 \\ \hline 29.94 \end{array}$$

$$\begin{array}{r} 0.65 \\ 1.50 \\ \hline C \quad 0.73 \\ 10 \end{array}$$

371

1237

270.40

25803

 15 Conc.  
 1825 Wall

270.40

$$\begin{array}{r} 270.40 \\ \hline 11.1 \end{array}$$



Outside footing

Level #2  
on Lt.

270.40  
17.84  
258.56  
2.19  
260.75 X

0+50

$\frac{705}{547}$  258.70  
C  $\frac{4.53}{10}$  32.96

253.70  
32.96

$\frac{667}{271}$   
C  $\frac{5.91}{10}$

Level #1

T.P. on Rt.

021

260.34

10.29

260.11

0+40

$\frac{1130}{10.77}$  259.10  
C  $\frac{0.53}{10}$  31.95

259.10  
31.95

$\frac{1130}{10.46}$   
C  $\frac{0.34}{10}$

0+30

$\frac{1060}{8.93}$  259.80  
C  $\frac{1.07}{10}$  31.82

259.80  
31.82

$\frac{1060}{9.21}$   
C  $\frac{0.79}{10}$

270.40

270.40



Outside Footings

H.  
Level #1  
ON RT.

0+80

17.95  
3.44  
C 4.53  
10

242.80  
31.0

242.80  
35.0

5.65  
2.16  
C 3.49  
10

0+70

12.75  
8.51  
C 4.24  
10

248.0  
34.03

248.0  
34.03

12.32  
10.44  
C 1.88  
10

Level #2  
ON LT.

0+00

260.75  
13.42  
247.33 TP  
6.27  
247.60

8.55  
2.86  
C 5.69  
10

242.20  
32.4

242.20  
32.4

8.12  
6.28  
C 1.84  
10

TP      0.56      248.45      12.43      247.89  
260.34



Outside Footings

H1

Level #1 ft.

Σ

51

1410

$$\begin{array}{r} 451 \\ 228 \\ \hline C \ 2.43 \\ 10 \end{array}$$

$$\begin{array}{r} 23080 \\ \hline 37.25 \end{array}$$

$$\begin{array}{r} 230.80 \\ \hline 37.25 \end{array}$$

$$\begin{array}{r} 635 \\ 442 \\ \hline C \ 1.43 \end{array}$$

Level #2

or L1

1400

$$\begin{array}{r} 24760 T \\ 1287 \\ \hline 234.73 \\ 0.58 \\ \hline 235.31 \end{array}$$

$$\begin{array}{r} 1190 \\ 1047 \\ \hline C \ 1.43 \\ 10 \end{array}$$

$$\begin{array}{r} 235.70 \\ \hline 36.33 \end{array}$$

$$\begin{array}{r} 235.70 \\ 144 \\ 297 \\ \hline 36.33 \end{array}$$

$$\begin{array}{r} C \ 1.43 \\ 10 \end{array}$$

0490

237.15

$$\begin{array}{r} 9.40 \\ 5.74 \\ \hline C \ 5.66 \\ 10 \end{array}$$

$$\begin{array}{r} 238.20 \\ \hline 35.87 \end{array}$$

$$\begin{array}{r} 238.20 \\ \hline 35.87 \end{array}$$

$$\begin{array}{r} 1025 \\ 605 \\ \hline C \ 4.28 \\ 10 \end{array}$$

T.P.

027

237.03

11.64

236.81

248.45



# Outside Footings

2

52

Level #1  
on Rt

" 7 "

~~36.84~~  
~~10.75~~  
~~47.20~~

~~269.75~~  
~~234.60~~  
~~45.15~~  
~~18.75~~  
~~235.75~~  
~~210.05~~  
~~31.20~~  
~~32.15~~  
~~8.95~~  
~~29.75~~  
~~3~~

1730 - 8

~~1161~~  
~~11.13~~  
~~C 0.73~~  
~~10~~

~~223.70~~  
~~38.58~~

~~21650~~  
~~39.93~~

~~821~~  
~~766~~  
~~C 0.25~~  
~~10~~

Level #4  
on Lt.

1720

23(31) 7

T.P. 004 224.71 12.48 224.67

~~10.71~~  
~~0.66~~  
~~C 4.05~~  
~~10~~

~~224.60~~  
~~38.42~~

~~224.60~~  
~~38.42~~

~~12.55~~  
~~2.17~~  
~~C 3.43~~  
~~10~~

237.15 Correction

237.08



Outside footings

Q

D

201.50  
42.75

831  
953  
F 1.27  
10

C

207.0  
41.72

281  
952  
F 5.71  
10

T.P. 0.37 2098/ 10.31 209.44

B

T.P. 6.38 219.75 11.29 213.42  
224.71

213.20  
40.55

11.51  
14.66  
F 3.15  
10



Outside Footings  
Level #1

H

$$\begin{array}{r}
 52.5 \\
 2.60 \\
 \hline
 C \quad 55.1 \\
 10 \\
 \hline
 216.50 \\
 39.93 \\
 \hline
 \end{array}$$

G

$$\begin{array}{r}
 655 \\
 9.45 \\
 \hline
 F \quad 664.45 \\
 10 \\
 \hline
 213.20 \\
 40.55 \\
 \hline
 \end{array}$$

F

$$\begin{array}{r}
 12.75 \\
 14.23 \\
 \hline
 F \quad 27.98 \\
 10 \\
 \hline
 207.0 \\
 41.72 \\
 \hline
 \end{array}$$

E

1.P.      0.37      209.81      1031      209.44  
 219.75

$$\begin{array}{r}
 831 \\
 1047 \\
 \hline
 F \quad 1878 \\
 2.16 \\
 \hline
 10 \\
 \hline
 201.50 \\
 42.75 \\
 \hline
 \end{array}$$



Inside footing

Tied 7' towards L

level #1  
ON RT.

1+30 = R

$$\begin{array}{r} 1161 \\ .1135 \\ \hline 1026 \\ 7 \end{array}$$

$$\begin{array}{r} 223.70 \\ \hline 33.65 \end{array}$$

$$\begin{array}{r} 223.70 \\ \hline 33.65 \end{array}$$

$$\begin{array}{r} 101 \\ 3.08 \\ \hline 2.07 \\ 7 \end{array}$$

1+20

$$\begin{array}{r} 1971 \\ 836 \\ \hline 1135 \\ 7 \end{array}$$

$$\begin{array}{r} 224.60 \\ \hline 33.65 \end{array}$$

$$\begin{array}{r} 224.60 \\ \hline 33.65 \end{array}$$

$$\begin{array}{r} 1285 \\ 1243 \\ \hline 42 \\ 7 \end{array}$$

1+10

224.71

237.15 Correction

237.08

Level #2

235.31 T

$$\begin{array}{r} 451 \\ 486 \\ \hline 937 \\ 7 \end{array}$$

$$\begin{array}{r} 230.80 \\ \hline 33.65 \end{array}$$

$$\begin{array}{r} 230.80 \\ \hline 33.65 \end{array}$$

$$\begin{array}{r} 635 \\ 768 \\ \hline 133 \\ 7 \end{array}$$



INSIDE FOOTINGS  
Level #1

£

56

C

207.0      281  
33.65      070  
C 2.11  
7

B

213.20      1151  
33.65      11.29  
C 0.24  
7

T.P.      0.37      209.81      10.31      209.44

A

T.P.      6.33      219.75      11.29      213.47

ON B  
inside  
cut state

224.71

216.50      821  
33.65      721  
C 1.00  
7



inside footings  
level #1

Q

F

12.75	207.0
<u>8.95</u>	<u>33.65</u>
C 4.90	
7	

E

83	201.50
<u>0.37</u>	<u>33.65</u>
C 7.94	
7	

T.P. check  
on cut stake inside  
see p 7

037

209.24
<u>208</u>
1.44
<u>0.47</u>
0.93

D

201.50	831
<u>33.65</u>	<u>405</u>
	726
	7

T.P.	037	209.81	1031	209.24
		219.75		



INSIDE FOOTINGS

£

58

H

	322	216.50
	082	
C	<u>2.66</u>	<u>33.65</u>
	7	

G

219.75

	655	218.20
	487	
C	<u>1.68</u>	<u>33.65</u>
	7	



More  
S. 100 ft  
disc  
11-2-20

Cross Section of Sassafras St  
INDIA to KETTNER

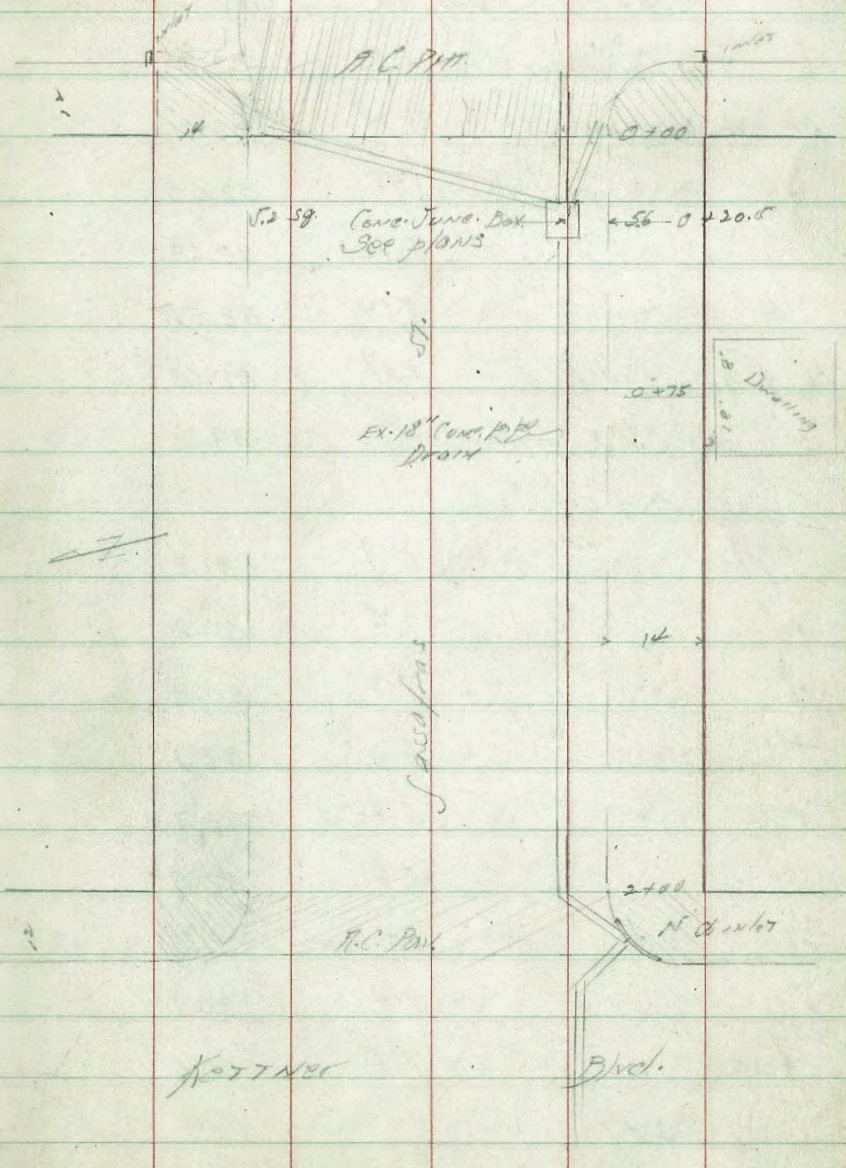
30' wide  
14' deep  
12' high

indexed  
c.s.K.

India

59

SECT	3.17	88.05	84.58	Secs. 4 India
	0-25			
S par.		4.00	83.45	
cb "		4.72	83.33	
1/2 "		4.60	83.45	
C "		4.30	83.75	
1/2 "		4.30	83.75	
cb "		4.36	83.69	
N "		4.31	83.74	
	0-12			
N cb		5.01	83.04	
N FL drain inlet		6.20	81.85	
cb par		5.11	82.94	
1/2 "		4.81	83.24	
C "		4.80	83.25	
1/2 "		4.99	83.06	
cb "		5.53	82.52	
S top of		5.03	82.97	
S FL drain inlet		6.24	81.81	





88.05

0+00 = W/ly India St

J	Top Cor Return	4.81	83.24
cb	4 gvt. pav	5.74	82.31
1/4	"	5.45	82.60
C	"	5.40	82.65
1/4	"	5.54	82.51
cb	+ gvt pav	5.37	82.68
N	top Cor Return	4.70	83.35

0+04

-10		6.9	81.2
N		7.5	80.6
cb		7.3	80.8
1/4		6.0	82.1
C		5.4	82.7
1/4		5.6	82.5
cb		6.3	81.8
J		8.0	80.1
+10		7.5	80.6

0+10

-12		11.5	76.6
-----	--	------	------

88.05

60

J		11.3	76.8
+10		11.5	76.6
cb		9.0	79.1
+5		6.7	81.4
1/4		7.3	80.8
C		8.6	79.5
1/4		8.5	79.6
cb		11.0	77.1
N		12.0	76.1
+10		11.0	77.1

0+20.5 <sup>Junc.</sup> <sub>Box</sub>

Top B.M. M.H.	12.92	75.13
F.L. 18" pipe	16.77	71.28
F.P. 0.10 H.22	12.93	75.12

0+25

0-20		6.3	68.9
N		5.7	69.5
cb		4.0	71.2
1/4		4.7	70.5
C		5.2	70.0



75.22

S 1/4	5.0	70.2
cb	7.0	71.2
S	3.1	72.1
+20	2.5	72.7
0+50		
-20	5.3	69.9
S	5.8	69.4
cb	6.5	68.7
+7	6.5	68.7
1/4	8.0	67.2
C	8.5	66.7
1/4	8.4	66.8
cb	8.1	67.1
✓	8.0	67.2
+20	8.3	66.9
0+75		
-20	10.2	64.8
✓	10.8	64.4
cb	11.5	63.7
+7	12.5	62.7

75.22

61

1/4	12.5	62.7
C	11.5	63.7
1/4	10.8	64.4
+95 Top 18" Cont. pipe	9.5	66.0
cb	9.3	65.9
S	8.4	66.8
+25	8.4	66.8
+3 Parat floor el.	7.0	68.2
1+00		
-20	11.1	64.1
S	11.1	64.1
cb	11.3	63.9
+3 Top Cont. pipe	12.55	62.67
1/4	12.4	62.8
C	13.7	61.5
1/4	14.5	60.7
+4	15.0	60.2
cb	14.4	60.8
✓	12.5	62.7
+20	11.8	63.4

Dundberg

not  
done



		75.22		
T.P	0.69	63.24	12.67	62.55
	1+03			
-20			14.5	48.7
✓			14.1	49.1
+1			1.9	61.3
cb			2.2	61.0
+8			3.1	60.1
1/4			2.6	60.6
C			2.4	60.8
C	Toprim S.M.H.		1.50	61.7
1/4			0.8	62.4
cb			+0.5	63.7
+13			+0.5	63.7
S			8.0	55.2
+20			11.0	52.2
	1+25			
-20			13.2	50.0
-2			12.5	50.7
-1			2.1	61.1

63.24

S		2.1	61.1
cb		2.6	60.6
1/4		3.2	60.0
C		3.8	59.4
+2		5.4	57.8
1/4		5.4	57.8
+5		6.2	57.0
+7		5.0	58.2
cb		5.0	58.2
N		5.6	57.6
+1		5.0	48.2
+20		5.3	47.9
	1+50		
-20		5.5	47.7
✓		5.0	48.2
+2		7.0	56.2
cb		6.4	56.8
+6		6.4	56.8
+9		7.5	55.7
1/4		7.6	55.6



6324

C		8.3	54.9
+2		5.7	57.5
1/4		4.5	58.7
+5		3.2	60.0
cb		4.2	59.0
S		4.3	58.9
+2		12.8	50.4
+20		13.3	49.9
	1+75		
-20		13.7	49.5
-2		12.7	50.5
S		6.3	56.9
cb		7.0	56.2
1/4		7.3	55.9
+10		9.0	54.2
C		11.5	51.7
1/4		11.4	51.8
+4		11.4	51.8
+5		9.4	53.8
+10		9.3	53.9

6324

63

cb		14.7	48.5
N		15.5	47.7
+20		15.5	47.7
	1+87		
-20		15.5	47.7
N		15.5	47.7
cb		15.0	47.9
+8		14.5	48.7
+11		11.4	51.8
+12		13.7	49.5
1/4		13.8	49.4
C		13.3	49.9
+3		11.1	52.1
1/4		9.5	53.7
cb		9.4	53.8
S		8.0	55.2
+2		12.6	50.6
+20		13.6	49.6
	1+92		
S -20		13.7	49.5



-2		12.7	50.5
S		10.0	53.2
cb		9.6	53.6
+3		9.5	53.7
1/4		11.1	52.1
+10		12.0	51.2
C		13.5	49.7
1/4		14.6	48.6
cb		15.5	47.7
N		15.5	47.7
+20		15.5	47.7
J.P.	4.03	12.9	50.3
	2 + 00 = Ely Kottner		
-20		6.8	47.6
N	corr Cor Top	6.85	47.80
cb	Top ob	6.45	47.87
gut	par	7.19	47.16
1/4	"	6.28	48.07
C	"	5.77	48.58
1/4	"	5.50	48.85

S	gut	5.57	48.78
S	cb Top ob	4.91	49.44
S	" Cor corr.	5.13	49.22
	2 + 14 = Ely cb of Kottner		
S	cb top	5.34	49.01
S	L gut	5.93	48.42
cb	par	5.80	48.55
1/4	"	5.84	48.51
C	"	6.11	48.24
1/4	"	6.50	47.85
cb	"	7.11	47.24
N	gut "	7.60	46.75
N	Top ob	6.85	47.50
	SEly cb. inlet KOTT + San.		
	Top grating	5.83	48.52
	FL	7.17	47.18
	Ch. to SE of Kottner		
	Sanitary	5.34	49.01

49.01  
 0.0  
 49.01 ✓







0+48.6			
W Lawn	3.1	271.1	
C cent Dr	3.06	271.16	
E " "	3.10	271.12	
0+88.4			
E cent dr.	4.94	269.28	
C " "	4.82	269.40	
W Lawn	5.0	269.2	
1+00 = end of 6.8 cent. drive = BC			
W ground	5.6	268.6	
C cent Dr	5.30	268.92	
E Strawberry	5.3	268.8	
1+14.72			
W	6.6	262.6	
7.5 Ely	6.5	262.7	
1+29.45			
W	7.4	266.8	
7.5 Ely	7.2	267.0	
TP	2.7	269.32	707
			267.15

1+44.17			
W - 1		2.63	266.69
W ground		2.7	266.6
7.5 Sly		3.2	266.1
1+58.90 = EC for N L alley			
W is N/L Garage & alley		3.4	265.8
7.5 Sly Stub		3.96	265.36
Sly 1/2 alley on widened Curve			
1+166.9 = Part #1			
S		1.6	267.7
7.5 N of SL		1.7	267.6
1+333.8			
S = gravel drive		2.5	266.8
7.5 N of SL		2.6	266.7
1+500.7			
S		3.4	265.9
7.5 N of SL		3.3	266.0



42.5 feet

1 + 66.76 = 1 + 6390 correct sta 146533

26932

= E.C. on S. Line alley 20' here

S 3.9 265.4

C 20' wide 4.2 265.1

N 3.7 265.6

1 + 69 = Ely edge of 30 Garage correct sta 1470.43

N + 0.20 cem floor 4.33 264.99

C 4.5 264.8

S 4.1 265.1

1 + 81.26 = P.C. of Banjo correct sta 1482.69

S 4.9 264.4

C 4.8 264.5

+ 9.8 = N cem gar floor 4.32 265.00

1 + 88.3 cor sta 1489.23

N Garage cem floor 4.31 265.01

C 5.0 264.3

+ 5 edge Cem. Apron 5.07 264.25

S " " " 5.01 264.31

1 + 91.8 = PRC correct sta 1491.35

S - 44 Car. Cem floor N.E. Cor. 7.46 261.86

S PRC. cem. 7.13 262.19

26932

S + 8 edge Apron 5.40 264.92

C 5.3 264.0

+ 9.8 = Sly edge Garage cem floor 4.31 265.01

N PRC in Garage on floor 4.30 265.02

2 + 06 corr sta 2105.55

N 4.6 264.7

C 6.2 263.1

+ 22 7.52 261.78

+ 26 = NW Cor Gar. cem floor 7.47 261.85

S in Car. on floor 7.46 261.86

2 + 15.90 = P. Banjo corr sta = 2112.33

S 9.0 260.3

+ 5 9.0 260.3

+ 6 Top 8" Cem. Wall 7.81 261.51

C 6.4 262.9

+ 10 6" Cem. Wall on line of 30 Garage 5.55 263.77 Rose Garden 20' alley

N on Lawn 4.6 264.7

2 + 28.90 = NW Lot 2 corr sta 2130.33

N + NW Lot 2 5.20 264.12 Top 6" Cem wall

C " " " 6.66 262.66



2+289

C on ground W/L Lot v 7.3 262.0

+N 7.8 261.5

+2v 9.6 259.7

S on Sky Prod. W/L Lot v 10.8 258.8

Strubbery 10 in alley Bargo

T.P. 710 274.25 217 267.15

check to B.M. 596 268.29 268.28  
0.01







0+05 = FRONT LINE STATION

00 = N/y Harschel

0-02 = N/y edge walk

0-07 = 7' Lane = S/y edge walk

0-14 = Top cb

0-14 = paved gutter

SWBP 5.89 111.62

10573 Harschel  
Wall

111.62

106.71	106.82	106.75	106.88	106.7	107.0
4.91	4.80	4.87	4.74	4.9	4.6
25	28	19	10	19	15
	Entrance				96 = dirt

106.66	106.56	106.87	106.7	106.9
4.96	5.06	4.75	4.9	4.7
25	19	10	15	15

106.57	106.98	106.88	106.93	107.13
5.5	5.4	4.74	4.69	4.59
25	19	10	15	15

106.32	106.32	106.79	106.87	107.03
5.30	5.30	4.83	4.75	4.59
25	19	10	15	15

105.97	106.15	106.75	106.80	107.00
5.42	5.47	4.81	4.82	4.68
25	16	14	15	15

105.97	106.15	106.17	106.24	106.36
5.42	5.47	5.25	5.33	5.16
25	16	14	15	15

111.62



1+43 alley not graded

1+40 = Sly alley

1+38

1+00

0+57

0+06 = drain

11162

27

106.7

4.9  
4.9  
—  
0

107.9

6.7  
6.7  
—  
0

107.4

4.2  
4.2  
—  
0

107.0

4.6  
4.6  
—  
0

107.2

4.4  
4.4  
—  
0

CON. WALK

FL. 4<sup>th</sup> drain

108.3

4.3  
4.3  
—  
0

108.7

2.9  
2.9  
—  
0

108.3

4.6  
4.6  
—  
0

107.5

4.1  
4.1  
—  
0

107.23

2.9  
2.9  
—  
0

106.10

1.5  
1.5  
—  
0

Baseline 2+80

6.4

108.8

2.8

108.2

6.4

107.9

4.3  
4.3  
—  
0

107.1

4.5  
4.5  
—  
0

28

108.3

6.4  
6.4  
—  
0

108.5

4.1  
4.1  
—  
0

108.1

6.4  
6.4  
—  
0

107.5

4.1  
4.1  
—  
0

107.1

4.5  
4.5  
—  
0

71

11162





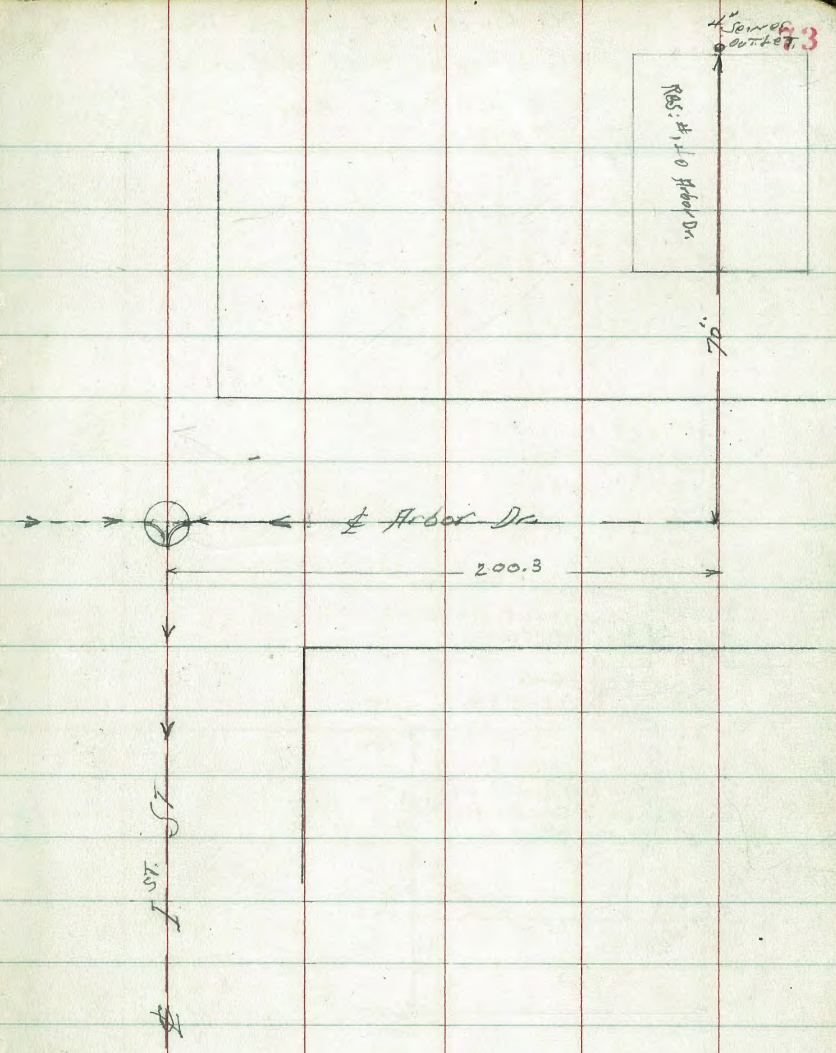


index of  
C.S.K

Sewer Levels  
at Res. # 140 Harbor Drive

Moore  
10-24-36

SE.A.P.	1.98	290.03	288.05	1st St. of Harbor Dr.
Rim S.M.H.	1st of Harbor	2.68	287.35	
FL.	" " front W.	5.96	284.07	
"	" " " E	5.84	284.19	
200.3 E	of M.H. on part.	0.66	283.37	
T.P.	4.97	287.62	7.38	282.65
Fl. of 4" C.I. Sewer outlet		2.17	285.45	
	in rear of Res. # 140 Harbor Dr.			



4" Sewer outlet  
3







11-17-36  
Miller  
Walker  
Bliss

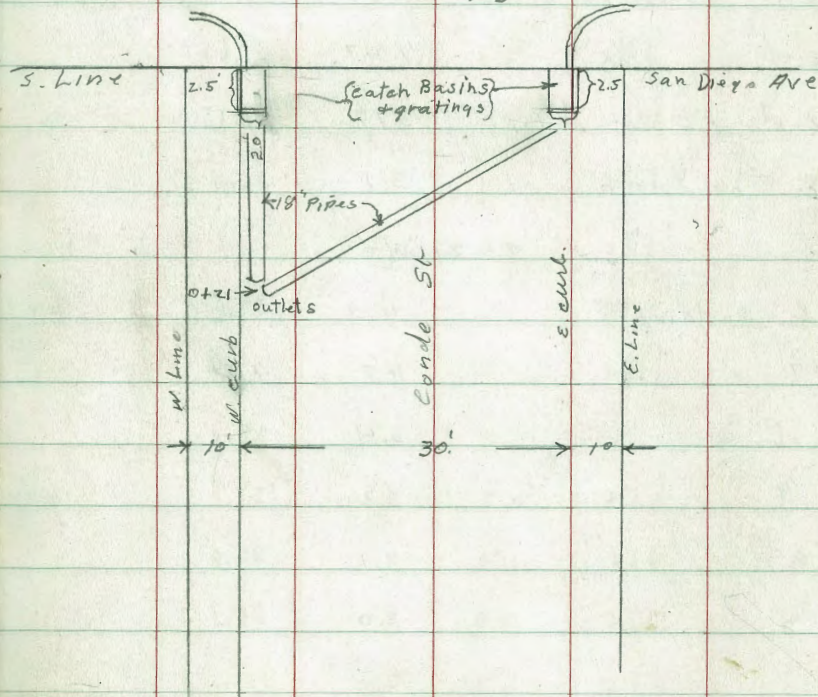
X Soc Conde St.  
San Diego Ave to Congress St.  
50' wide - 10' cbs. 7.5' 1/4s

Indexed  
C.S.K.

33.12

75

BM. B.P.	1.15	33.12	31.97	S.W. Conde + San Diego Ave
	12' N. of S. Line = S. Curb of San Diego Ave		33.12	
W-20	ent. cb	1.15	31.97	gutter N.W. Cor. catch basin
W	pay	1.51	31.61	ent. cl
cl	"	1.44	31.66	+2.5 E. edge S. End. ent. walk
"	"	1.38	31.74	+7.5 W " " " " "
E	"	1.34	31.78	N
"	"	1.38	31.74	
cl	"	1.51	31.61	
E	"	1.51	31.61	
E	ent. cl	0.95	32.17	
+15		1.51	31.61	
+40		1.41	31.71	
	0+00 = S. Line San Diego Ave			
E		1.4	31.7	
+2.5	E edge S. End. walk	1.24	31.86	
+7.5	W " " " "	1.29	31.83	
S. ent. cl		1.36	31.76	
gutter	N.E. Cor. catch basin	1.98	31.14	
"		1.87	31.25	





33.12

0+0.25 W-3

		33.12	
W	1.4	31.7	
+9.5 W. end. int. dr	1.67	31.45	
+9.5 S. W. cor. catch basin	2.04	31.04	
1/4	1.9	31.2	
1/4	2.0	31.1	
1/4	2.1	31.0	
E. dr on s.e. cor. grading	1.85	31.27	
E. dr	1.47	31.65	
E. dr FL. Outlet Pipe	3.77	29.35	
E. building	3.1	30.0	
	0+21 W-3		
E Building	4.7	28.4	
+7	4.7	28.4	
dr	3.4	29.7	
1/4	3.3	29.8	
1/4	3.1	30.0	
1/4	3.0	30.1	
+8 = Outlet Both 18" Pipes.	5.2	27.9	Not. for yardage
	2.7	30.4	

33.12

76

		33.1	
+8	3.5	29.6	
W	4.5	28.6	
+10	4.5	28.6	
	0+40 W. End Building on E.		
	0+41 W-5		
-10	5.5	27.6	
W	5.5	27.6	
dr	5.4	27.5	
1/4	4.5	28.6	
1/4	4.7	28.4	
1/4	4.8	28.3	
dr	5.0	28.1	
E	5.2	27.9	
+10	5.2	27.9	
	0+53 S		
E-10	5.5	27.6	
E	5.6	27.5	
dr	5.8	27.3	
1/4	5.8	27.3	
1/4	5.8	27.3	
1/4	6.1	27.0	



33.12

0+53 W

33.1

cl	6.2	26.9
W	5.7	27.4
+10	5.8	27.3
	0+72	
-10	6.0	27.1
W	6.1	27.0
cl	6.5	26.6
+3	7.0	26.1
1/4	6.6	26.5
⊕	6.5	26.6
1/4	6.5	26.6
cl	6.2	26.9
E	6.1	27.0
+0.5 = ⊕ Garage Dirt floor	6.1	27.0
	1+00	
-5	5.8	27.3
E-5	5.9	27.2
cl	6.3	26.8
1/4	6.5	26.6
+3	7.1	26.0
⊕	7.2	25.9

33.12

77

33.1

1/4	7.3	25.8
cl	7.5	25.6
+3	6.6	26.5
W	6.7	26.4
+10	6.7	26.4
	1+50	
W-10	7.8	25.3
W	7.9	25.2
+7	8.0	25.1
cl	8.9	24.2
1/4	8.6	24.5
T.P.	2.91	27.03
⊕	2.2	24.8
1/4	2.2	24.8
cl	1.9	25.1
E under church		
+11 = E side church	0.6	26.2
+25	0.9	26.1
+50	0.4	26.6
+75	0.7	26.3



27.03

2+00 W

		<u>27.0</u>
E-75	2.4	24.6
E-50	2.5	24.5
E-25	3.0	24.0
E	3.1	23.9
cl	3.3	23.7
1/4	3.6	23.4
ϕ	3.8	23.2
1/4	4.1	22.9
cl	4.9	22.1
+3	4.5	22.5
W	4.3	22.7
+5	4.2	22.8
	2+25	
W	5.5	21.5
cl	5.5	21.5
1/4	5.2	21.8
ϕ	5.0	22.0
1/4	4.7	22.3
cl	4.7	22.3
E	4.5	22.5

27.03

78

		<u>27.0</u>
E+25	3.7	23.3
E+50	3.2	23.8
E+75	2.8	24.2
	2+50	
E	5.0	22.0
cl	5.3	21.7
1/4	5.9	21.1
ϕ	6.1	20.9
1/4	6.1	20.9
cl	6.1	20.9
W	6.1	20.9
	2+95	
W	7.5	19.5
cl	7.5	19.5
1/4	7.7	19.3
ϕ	7.3	19.7
1/4	7.3	19.7
cl	6.0	21.0
E	5.8	21.2



27.03

300 = N. Line Congress St.

27.0

E 37.7 6.9 20.1

ch 7.3 19.7

1/4 7.6 19.4

4 7.7 19.3

1/4 7.8 19.2

eb 7.7 19.3

W. 8.0 19.0

T.P. 8.76 3.2.88 2.91 24.12

ehk. orig B.M. 0.91 31.97 ✓

IMPROVED TABLES

AND  
INFORMATION



27.5  
1

DIRECTIONS FOR USE OF TABLES

Distance of slope taken from side of shoulder  
table for any width roadway slope 1 1/2 to 1  
If ground is nearly level the top or bottom of  
slope is located by the double-sight method in  
left column and topography will be under the  
right column.

From this table to slope table. If ground is not

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**IMPROVED TABLES**  
**AND**  
**INFORMATION**

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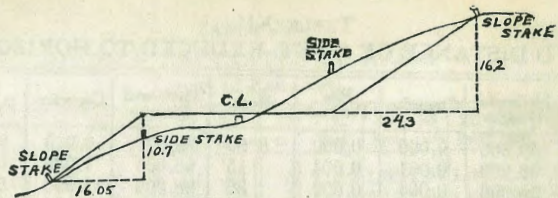
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To find station and lateral for curve of  
any other degree divide by length of curve and  
multiplication found in column of conversion.  
Degree of curve with a given length may be found  
by dividing length by conversion factor.  
The distance from a point on the tangent to  
the curve is very nearly the same as the distance  
but divided by cosine the radius.









DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

1+56. 3.55  
 End. 1+59 3.58  
 43  
 34.5  
 8.5  
 20  
 8.5  
 11.8

43.  
 32.5  
 9.5

