

1518

1518

FIELD BOOK

No. 385 F

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CALIFORNIA
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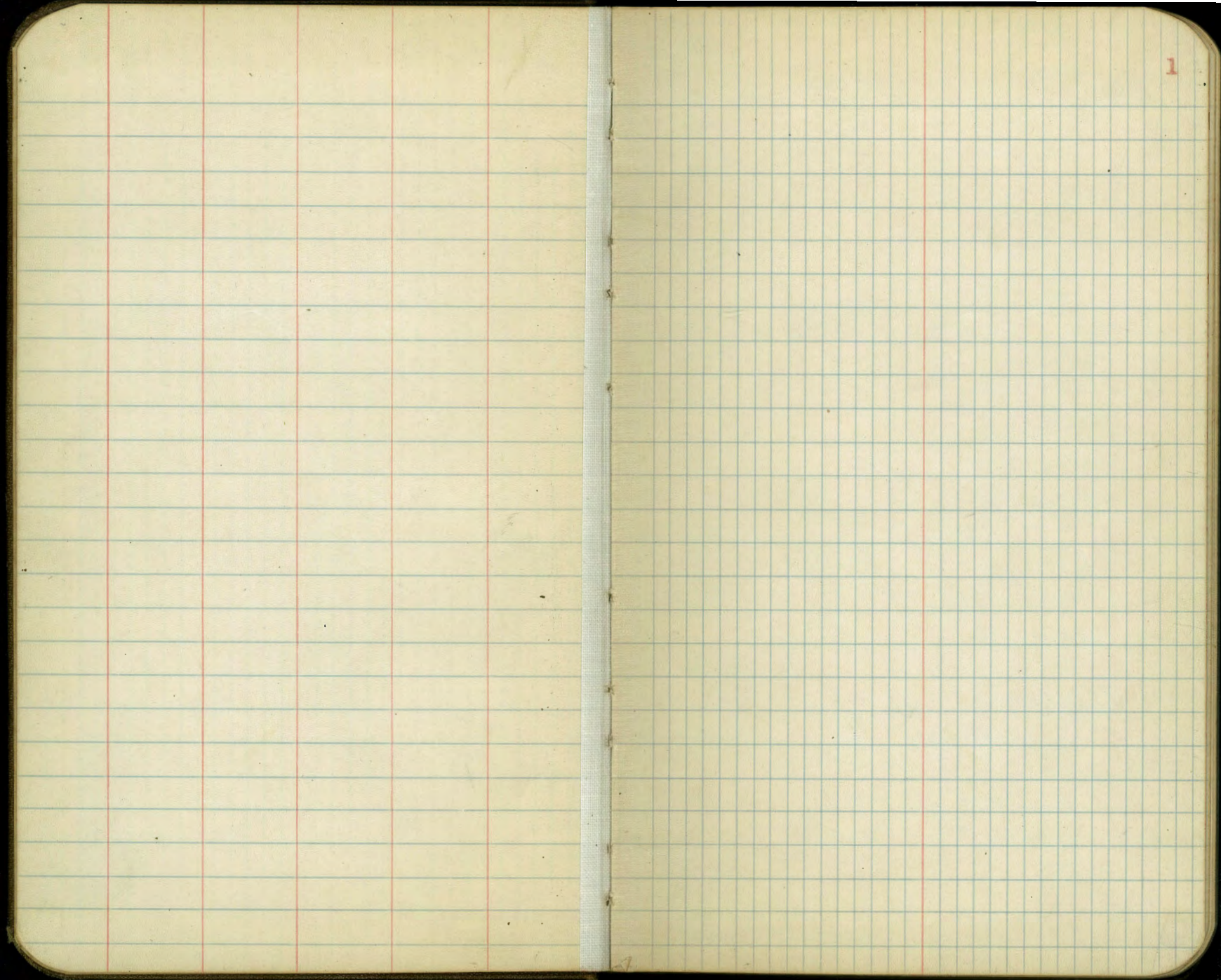
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THE FREDERICK POST CO.
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IRVING PARK STATION
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Indexed
C.S.R.

Ladden
Blow
Anderson.

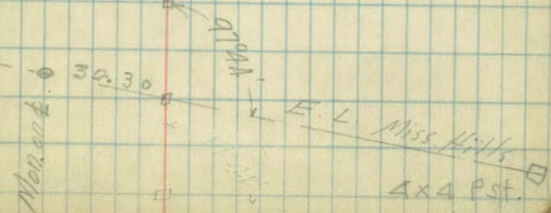
10-8-35

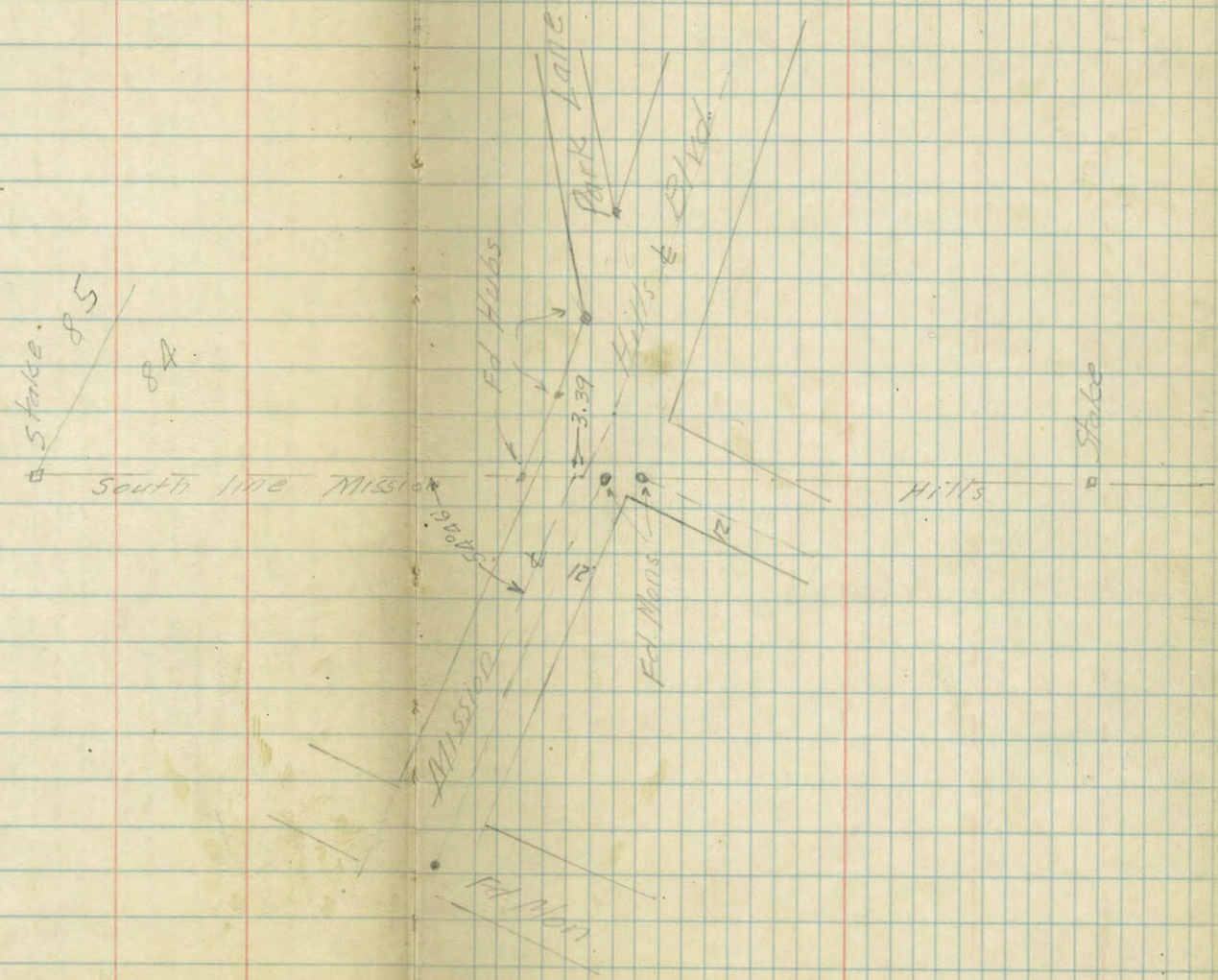
2

Westerly line of Mission Hills Blvd through Mission Hills
Map No 1115

Mission Hills
See next page

10	41.70		Fd. Hub.	
9	66.90	2°41'R	Fd. Hub	54
8	49.82		Fd. Hub	
7	343.10		Set hub	
6	253.50	3°49'L	Fd. Hub.	
5	105.11	10°37'L	Fd. Hub	
4	57.31	9°16'L	Fd. Hub.	
3	106.57	19°25'30"L	Set Hub	
2	169.54	6°00'L	Fd. Hub.	
1			Fd. Hub	30.30
0				





Indexed
C.S.R.

1-9-35
Lowden
Brown
Anderson

4

Center line of Mission Hills Blvd. From Kettner St. to
Washington St.

+50

4+00

+50

+41¹⁰

L 0°02' R

w'ly 19' line Union St.

3+00

+50

2+00

1+50

+28⁶

E'ly line Titus St.

+78⁶

w'ly line Titus St.

+50

0+00

94°12' ↙
E'ly line Kettner

+50

9+00

+50

+42¹⁰ L 0°04'R

w/ly 13' line

8+00

+50

7+00

+50

6+00

+91⁶⁰ L 0°06'L

w/ly 13' line

+50

5+00

14+00

+50⁰⁹ L 2°41'L

+28⁵⁹ L 51°57'L

+25²⁰ L 51°46'R

13+00

+50

12+00

+50

11+00

10+92⁵² L 0°07'R

+50

10+00

w/ly 13' line

20+00

+50

19+00

+50

+09⁵⁰ L 349' R

18+00

+50

17+00

+50

16+00

+50

15+00

14+50

2 - 09.60
31 - 09.95

29.60

24+00

+50

+10° L 6°00'R

23+00

+50

+09°60' L 19°25'30" R ✓

22+00

+59°25' L 9°16'R

+50

21+00

+59°60' L 10°37'R

20+50

28+50 7°00'56"

~~2729~~
~~2473~~
~~2067~~

28+00 4°09'03"

27+50 1°-17'-10"
Δ=25°10' R

R=500

+78°⁰⁰ B.C. T=111.61

L=219.62

27+00

26+50

26+00

25+50

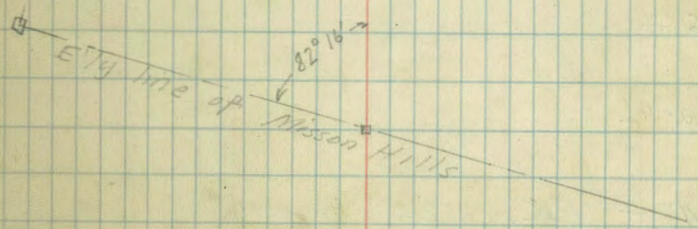
25+00

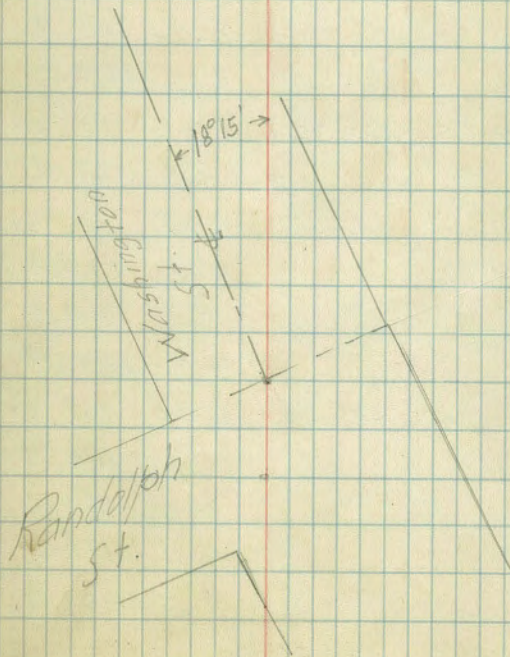
24+73⁸⁰

25+00

24+50

4x4 post marked N.E. Bk.



$$\begin{array}{r} 43.06 \\ 47.162 \\ \hline 15.44 \end{array}$$
 $30+61.36$
 $29+93.06$
 $+ 47.62 \text{ F.C. } 12^{\circ}35'$
 $29+00$
 $9^{\circ}52'52''$


Indexed
C.S.R.

Center line profile of Mission Hills Blvd
from Kettner* to Washington.

1-10-35

11

Laidon
Brown
Anderson.

B.M.	2.91	102.13		99.22
0+00			12.4	89.7
T.P.	12.68	109.56	5.25	96.88
0+50			11.0	98.56
0+78 ^e			9.43	100.13
1+03 ^e			7.41	102.15
1+28 ^e			6.51	103.05
1+50			5.7	103.9
T.P.	12.80	122.07	0.29	109.27
2+00			12.3	109.4
+50			8.2	113.9
3+00			1.5	120.6
T.P.	12.65	133.72	1.00	121.07
3+50			6.6	127.1
T.P.	12.60	145.27	1.05	132.67
4+00			11.0	134.3
4+50			10.6	134.7
+75			3.9	141.4
T.P.	12.84	157.65	0.46	144.87
5+00			11.4	146.2
+50			4.0	153.7
5+92			5.4	152.3
6+00			5.5	152.2
T.P.	13.05	170.66	0.04	157.61

BP top wall SE Kettner & Pringle

98.56
 1.5
 100.06

Pvt.
" E
"

		170.66		
6+50			10.9	159.8
7+00			6.7	164.0
+50			5.2	165.3
8+00		✓	1.6	169.1
T.P.	11.46	181.58	0.54	170.12
8+50			4.3	177.3
9+00		✓	3.1	178.5
T.P.	12.76	193.40	0.94	180.64
9+50			9.7	183.7
10+00			4.8	188.6
+50			5.1	188.3
11+00			2.5	190.9
11+05			3.00	193.40
+50			1.7	191.7
12+00		✓	0.4	193.0
T.P.	11.19	204.05	0.54	192.86
+25			9.8	194.2
+50			14.2	189.8
13+00			20.6	183.4
+25 ³			18.9	185.1
+50 ²⁹			15.0	189.0
14+00			8.5	195.5
+50			5.5	198.5
15+00			8.8	195.2

Top MH.

		204.05		
15+50			8.5	195.5
16+00			4.5	199.5
+50			2.0	202.0
T.P. 13.00	216.65		0.40	203.65
17+00			9.5	207.1
+50			5.6	211.0
18+09 ⁵			3.0	213.6
T.P. 11.97	225.60		3.02	213.63
+50			11.9	213.7
19+00			14.0	211.6
+33			15.4	210.2
+35			23.4	202.2
+37			15.5	210.1
+50			17.4	208.2
+75			27.3	198.3
20+00			17.2	208.4
+25			10.0	215.6
+50			5.9	219.7
+59 ⁶			6.11	219.49
21+00			4.9	220.7
+50			1.6	224.0
+59 ⁹⁵	11.03	235.03	1.60	224.00
22+00			8.0	227.0
+09 ⁶⁰			8.7	226.3

Hub 18+09⁵

on Hub

235.03

22+50			5.0	230.0
23+00			2.5	232.5
+10	10.44	242.44	3.03	232.00
+50			8.0	234.4
24+00			6.3	236.1
+50			4.2	238.2
+74			4.3	238.1
25+00			1.5	240.9
T.P.	12.91	254.21	1.14	241.30
+50			11.6	242.6
26+00			8.7	245.5
26+50			4.4	249.8
27+00			1.4	252.8
27+28	12.45	265.57	1.09	253.12
+50			8.9	256.7
28+00			5.4	260.2
28+50			4.6	261.0
29+00			1.5	264.1
T.P.	11.24	276.69	0.12	265.45
+47 ⁶³			10.3	266.4
+93 ⁰⁶			9.11	267.58
30+61 ³⁶			4.20	272.49
B.M.			6.39	270.30

on hub

P.V.H.

"

S.E. Washington and Lark 269.94 Rec.

(Plug pulled out)

Levels Atlantic St.
Barnett Ave. North
0400 to 1040

Indexed
a.s.k.

667

1-18-35
Moore 15

BM 6.85 6.67
0400

-6.18

Mon
Barnett
Hwy 10

F Gutter

545

1.22

Top Cb

487

1.80

0400

1450

N Top Cb

5.80

0.87

F Top Cb

437

2.30

Gutter

647

0.20

Gutter

474

1.93

2

5.56

1.11

2

506

1.61

F Gutter

5.88

0.79

N Gutter

609

0.58

0125.55 B.C. H

Top Cb

570

0.97

F Gutter

5.85

0.82

240

2

5.55

1.12

2

432

2.35

N Gutter

635

0.32

F Gutter

425

2.42

Top Cb

5.85

0.82

Top Cb

420

2.47

0450

2450

N Top Cb

5.83

0.84

F Top Cb

430

2.37

Gutter

627

0.40

Gutter

465

2.02

2

5.51

1.13

2

423

2.44

F Gutter

5.75

0.92

240

0158

N Top Cb

431

2.36

F Top Cb

5.00

1.67

Gutter

438

2.29

Gutter

5.77

0.90

2

434

2.33

2

5.50

1.17

F Gutter

508

1.59

N Gutter out

Top Cb

447

2.20

140

3421

N Top Cb

5.95

0.92

F Top Cb

457

2.13

Gutter

620

0.47

Gutter

517

1.50

2

5.40

1.27

2

446

2.21

667

W Gutter	4.50	2.17
TopCb	4.30	2.37
	3+50	
W TopCb	4.40	2.27
Gutter	4.90	1.77
⌊	4.60	2.07
E Gutter	5.25	1.42
TopCb	4.62	2.05
	4+0	
F TopCb	4.74	1.93
Gutter	5.43	1.24
⌊	4.80	1.87
W Gutter	5.30	1.37
TopCb	4.58	2.09
	4+51 = End of Ch on E	
W TopCb	4.67	2.00
Gutter	5.65	1.02
⌊	4.80	1.87
E Gutter	5.82	0.85
TopCb End	4.88	1.79
	5+0	
E Edge Pav	5.17	1.50
⌊	4.80	1.87
W Gutter	5.31	1.36
TopCb	4.65	2.02

667

16

	5+51 = End of Ch on W	
W TopCb End	4.66	2.01
Gutter	5.24	1.43
⌊	4.66	2.01
E Edge Pav	4.82	1.85
	6+0	
E Edge Pav	4.67	2.00
⌊	4.56	2.11
W Edge "	4.77	1.90
	6+50	
W Edge Pav	4.70	1.97
⌊	4.50	2.17
E Edge Pav	4.61	2.06
	7+0	
E Edge Pav	4.49	2.18
⌊	4.41	2.26
W " "	4.57	2.10
	7+50	
W Edge Pav	4.44	2.23
⌊	4.27	2.40
E " "	4.36	2.31
	8+0	
E Edge Pav	4.32	2.35
⌊	4.22	2.45
W " "	4.40	2.27

6.67

17

8:50

H Edge Pav. 4.42 2.25

L 4.23 2.44

F " " 4.34 2.33

9:10

F Edge Pav. 4.40 2.27

L 4.30 2.37

H " " 4.50 2.17

9:50

H Edge Pav. 4.60 2.07

L 4.40 2.27

F " " 4.40 2.17

10:10

F Edge Pav. 4.63 2.04

L 4.48 2.19

H " " 4.63 2.04

Levels Atlantic St.

3570 to 4670

BM #3	5.90	8.51	2.61
	3570		
W Edge Pav	4.27	4.24	
L	4.06	4.45	
F	4.19	4.32	
	35750		
F Edge Pav	4.05	4.46	
L	3.93	4.58	
H	4.17	4.34	
	3670		
W Edge Pav	4.02	4.49	
L	3.77	4.74	
F	3.87	4.64	
	36750		
F Edge Pav	3.72	4.79	
L	3.65	4.86	
H	3.92	4.59	
	3770		
W Edge Pav	3.76	4.75	
L	3.52	4.98	
F	3.63	4.88	
	37750		
F Edge Pav	3.52	4.99	
L	3.43	5.08	
H	3.65	4.86	

W of
Walnut
Moore

8.51

	3870		
W Edge Pav	3.52	4.99	
L	3.30	5.21	
F	3.38	5.13	
	38750		
F Edge Pav	3.27	5.24	
L	3.19	5.34	
H	3.41	5.10	
	3970		
W Edge Pav	3.25	5.26	
L	3.02	5.48	
F	3.12	5.38	
TP	3.38	8.67	3.22
	39750		
F Edge Pav	3.22	5.45	
L	3.12	5.55	
H	3.25	5.32	
	4070		
W Edge Pav	3.22	5.45	
L	3.04	5.63	
F	3.14	5.53	
	40750		
F Edge Pav	3.16	5.51	
L	3.07	5.60	
H	3.22	5.39	

867

41+0		
W Edge Pav	3.38	5.29
L	3.17	5.50
F " "	3.28	5.39

41+50		
E Edge Pav	3.47	5.20
L	3.38	5.29
W " "	3.57	5.10

42+0		
W Edge Pav	3.84	4.83
L	3.63	5.04
F " "	3.70	4.97

42+50 = 3' N of L Pavement to east		
E Edge Pav	4.01	4.66
L	3.93	4.74
W " "	4.12	4.55

43+0		
W Edge Pav	4.41	4.26
L	4.18	4.49
F " "	4.26	4.41

43+50		
E Edge Pav	4.48	4.19
L	4.40	4.27
W " "	4.60	4.07

867

44+0		
W Edge Pav	4.82	3.85
L	4.62	4.04
F " "	4.74	3.93

44+50		
E Edge Pav	5.00	3.67
L	4.89	3.78
W " "	5.06	3.61

45+0		
W Edge Pav	5.32	3.35
L	5.11	3.56
F " "	5.23	3.44

45+50		
E Edge Pav	5.47	3.20
L	5.38	3.29
W " "	5.61	3.06

46+0		
W Edge Pav	5.94	2.73
L	5.51	3.16
F " "	5.53	3.14 Super.

X Section Mission Hills Blvd-

Partridge
Walker
Bower
Weir

Indexed
C.S.R.

Sta		Elev. &	Grade
0+00	Int. E. P. Ketterer and E. Mission Hills Blvd.	89.7	
0+17		94.4	H.L.
0+50		98.56	
0+60		99.7	H.L.
0+78.6	S. Pavement Line Titus St.	100.13	
1+28.6	N. Pavement Line Titus St.	103.05	
1+50		103.9	
2+00		109.4	

(See pg 11 For
Elevations)

Sta	Left	Right	House
0+00	-1.4 50 88.3	-0.8 34.5 88.9	-0.3 16.4 89.4
0+17	-4.4 42 89.9	-2.4 18.7 87.3	-0.6 14 86.8
0+50	-2.5 50 91.1	-2.4 30 91.2	-0.6 19 88.0
0+60	-3.3 50 96.4	-1.7 22.4 98.0	
0+78.6	-0.6 18 99.53	-0.3 9 99.83	
1+28.6	-1.0 18 102.05	-0.4 9 102.65	
1+50	-9.3 24 94.6	-9.3 16 94.6	-7.1 16 96.8
2+00	-18.0 50 91.4	-15.3 17.8 94.1	-5.8 9.7 103.6

Sta	Left	Right	House
0+00	+0.7 3.5 90.4	+2.0 6.0 91.7	+6.1 19 97.8
0+17	+0.3 4 94.7	+2.0 8.5 96.4	+2.3 2.2 91.7
0+50	+1.7 13 100.3	+2.0 29 100.6	
0+60	+1.3 50 101.0	+3.4 22.5 103.1	
0+78.6	+0.2 9 100.15	+0.4 18 100.17	
1+28.6	+0.1 9 103.15	+0.1 18 103.15	
1+50	+4.9 13.8 108.8	+9.8 21.6 113.7	+10.5 24.8 114.4
2+00	+3.7 9 113.1	+4.9 15.5 114.3	+10.0 2.5 119.4

Sta	Elev. \pm	Grade	Bank W.W.	$\frac{L}{W}$	$\frac{L}{W}$	$\frac{L}{W}$	$\frac{L}{W}$	$\frac{L}{W}$	$\frac{L}{W}$	$\frac{L}{W}$	$\frac{L}{W}$
2+50	113.9		$\frac{-20.5}{76.5}$	$\frac{-20.3}{38.0}$	$\frac{-13.3}{31.5}$	$\frac{+7.0}{12}$	$\frac{+13}{33}$	$\frac{+19.7}{50}$			
			93.4	93.6	100.6	120.9	126.9	133.6			
2+75	115.0	H.L.	$\frac{-20.7}{65}$	$\frac{-21.6}{55}$	$\frac{-13}{36}$	$\frac{-6.0}{18}$	$\frac{+13.0}{25}$	$\frac{+21.5}{50}$			
			94.3	93.4	102.0	109.0	128.0	136.5			
3+00	120.6		$\frac{-27.4}{79}$	$\frac{-23.1}{55}$	$\frac{-13}{33}$	$\frac{-5.5}{17}$	$\frac{+10.2}{25}$	$\frac{+19.2}{50}$			
			93.2	97.5	107.6	115.1	130.8	139.8			
3+50	127.1		$\frac{-29.7}{91}$	$\frac{-26.8}{81.5}$	$\frac{-24.6}{70}$	$\frac{-16.4}{49}$	$\frac{-13}{35}$	$\frac{-7.3}{22.6}$	$\frac{+9.2}{24}$	$\frac{+12}{34}$	$\frac{+18.2}{50}$
			97.4	100.3	102.5	110.7	114.1	119.8	136.3	139.1	145.3
3+78	131.2	H.L.	$\frac{-31.0}{115}$	$\frac{-34.2}{88}$	$\frac{-34}{71}$	$\frac{-28}{59}$	$\frac{-19}{46}$	$\frac{-13.0}{34}$	$\frac{+12.4}{38}$	$\frac{+18.2}{50}$	
			100.2	97.0	97.2	103.2	112.2	118.2	143.6	149.4	
4+00	134.3		$\frac{-31.5}{103}$	$\frac{-35}{60}$	$\frac{-34.2}{55}$	$\frac{-13}{25}$	$\frac{-5.8}{13}$	$\frac{+6.7}{21}$	$\frac{+12.0}{33.5}$	$\frac{+17}{50}$	
			101.8	99.3	100.1	121.3	128.5	141.0	146.3	151.8	
4+50	134.7		$\frac{-29.1}{110}$	$\frac{-33}{92}$	$\frac{-33}{70}$	$\frac{-25}{60}$	$\frac{-12}{30}$	$\frac{+9.5}{14}$	$\frac{+12.7}{20}$	$\frac{+20.0}{40}$	$\frac{+22.5}{50}$
			105.6	101.7	101.7	109.7	122.7	144.2	147.4	154.7	157.2
5+00	146.2		$\frac{-36.5}{106}$	$\frac{-25}{69}$	$\frac{-13.0}{33}$	$\frac{+8.2}{21}$	$\frac{+18.4}{50}$				
			109.7	121.2	133.2	154.4	164.6				

Sta	Elev. & Grade	W.W.	L4	±	R4	
5+50	153.7	$\frac{-40}{130}$ $\frac{-43.5}{103}$ $\frac{-43.6}{89}$ $\frac{-34.2}{74}$ $\frac{-31.5}{47}$ $\frac{-12.0}{21}$		$\frac{+2.4}{12}$ $\frac{+7.2}{28}$ $\frac{+16.6}{50}$	113.7 110.2 110.1 119.5 132.2 141.7 156.1 160.9 170.3	
6+00	152.2	$\frac{-43.0}{119}$ $\frac{-38.4}{110}$ $\frac{-36.0}{85}$ $\frac{-24}{57}$ $\frac{-11.0}{27}$	Bank W.W.	$\frac{+12.0}{24}$ $\frac{+22.2}{50}$	109.2 113.8 116.2 128.2 141.2 164.2 174.4	
6+50	159.8	$\frac{-46}{115}$ $\frac{-38}{88}$ $\frac{-23}{55}$ $\frac{-13}{34}$ $\frac{-9.6}{20}$		$\frac{+7.1}{19}$ $\frac{+13.0}{34}$ $\frac{+19.7}{50}$	113.8 121.8 136.8 146.8 150.2 166.9 172.8 179.5	
7+00	164.0	$\frac{-43.3}{123}$ $\frac{-44.7}{95}$	W.W.	$\frac{-47.3}{93}$ $\frac{-48}{80}$ $\frac{-35}{73}$ $\frac{-26}{60}$ $\frac{-13}{30}$	$\frac{+9.0}{18}$ $\frac{+12}{28.5}$ $\frac{+22.5}{50}$	120.7 119.3 116.7 116.0 129.0 138.0 151.0 173.0 177.0 186.5
7+50	165.3 122.3 126.3 131.1	$\frac{-43.0}{123}$ $\frac{-39.0}{103}$ $\frac{-34.2}{83}$		$\frac{-26.0}{70}$ $\frac{-22}{60}$ $\frac{-13.0}{38}$ $\frac{-24}{30}$ $\frac{-5.2}{13}$	$\frac{+12.0}{25}$ $\frac{+25.0}{50}$	139.3 143.3 152.3 155.9 160.1 177.3 190.3
8+00	169.1		W.W.	$\frac{-45.7}{124}$ $\frac{-36.5}{98}$ $\frac{-18.0}{57}$ $\frac{-12.0}{39}$ $\frac{-4.7}{20}$	$\frac{+8.6}{23}$ $\frac{+13.0}{31}$ $\frac{+22.8}{50}$	123.9 132.6 151.1 157.1 164.4 177.7 182.1 191.9
8+50	177.3 128.3	$\frac{-49}{102}$		$\frac{-48.2}{92}$ $\frac{-38.0}{78}$ $\frac{-25.0}{59}$ $\frac{-12.0}{34}$ $\frac{-4.0}{15}$	$\frac{+6.0}{20}$ $\frac{+9.2}{35}$ $\frac{+14.7}{50}$	129.1 139.3 152.3 165.3 173.3 183.3 186.5 192.0
9+00	178.5		W.W.	$\frac{-49.1}{114}$ $\frac{-39.4}{79}$ $\frac{-17.9}{53}$ $\frac{-13.0}{38}$ $\frac{-4.7}{17}$	$\frac{+5.5}{13}$ $\frac{+10.7}{28}$ $\frac{+23.2}{50}$	129.4 149.1 160.6 165.5 173.8 184.0 189.2 201.7

Sta	Elev. \pm	Grade	Lt.	\pm	TR																				
9+50	183.7		W.W. -53.2 113	-42.5 97	-39 89	-26 67	-23.5 62	-8.5 28	+9.0 19	+21.2 50	130.5	141.2	144.7	157.7	160.2	175.2	192.7	204.9							
10+00	188.6			-52 120	-31.6 79	-26 67	-7.0 26	-3.6 9	+7.4 12	+13.0 28	+23.2 50	136.6	157.0	162.6	181.6	185.0	196.0	201.6	211.8						
10+50	188.3			W.W. -52.7 102	-33.4 73	-26 58	-20.5 47	-13.0 27	+13.0 25	+27.0 50	135.6	154.7	162.3	167.8	175.3	201.3	215.3								
11+00	190.0	H.L.		W.W. -50.3 96	-20.3 52	-18 27	0.0 7	+5.8 13	+25.0 50	139.7	169.7	179.0	190.0	195.8	215.0										
11+50	191.7			-50.5 124	-44 104	-39 74	-26.0 66	-13.0 34	+11.6 23	+24.0 50	141.2	147.7	152.7	165.7	178.7	203.8	215.7								
12+00	193.0			-46.7 108	-35 80	-26 66	-13.0 35	-4.8 16	+13.0 27	+23.8 50	146.3	161.0	167.0	180.0	188.2	206.0	216.8								
12+25	194.7			-44.6 96	-39 84	-32.6 74	-26 58	-17.1 39	-13 25	-2.1 7	+2.7 11	+2.6 24	+12 32	+20.2 50	149.6	155.2	161.6	168.2	177.1	181.2	192.1	196.9	202.8	206.2	214.4
12+50	199.8			W.W. -43.1 88	-36 80	-26 60	-13 30	+13 32	+20.7 50	146.7	153.8	163.8	176.8	202.8	210.5										

Sta	Elev. \pm	Grade	Lt.		\pm	Rt.			
13+00	183.4		$\frac{-35}{91}$	$\frac{-32.6}{81}$	$\frac{-26}{59}$	$\frac{-13}{31}$	$\frac{+8.7}{78}$	$\frac{+13}{30}$	$\frac{+21.6}{50}$
			148.4	150.8	157.4	170.4	192.1	196.4	205.0
13+50 ⁰⁹	189.0		$\frac{-38.4}{96}$	$\frac{-35.4}{91}$	$\frac{-26}{70}$	$\frac{-13.0}{39}$	$\frac{+10.4}{20}$	$\frac{+20.8}{50}$	
			150.6	153.6	163.0	176.0	199.4	209.8	
14+00	195.5		$\frac{-42.6}{98}$	$\frac{-26}{64}$	$\frac{-18.2}{50}$	$\frac{-13}{37}$	$\frac{+8.4}{16}$	$\frac{+12}{30}$	$\frac{+23.2}{50}$
			152.9	169.5	177.3	182.5	203.9	207.5	218.7
14+50	198.5		$\frac{-43.6}{85}$	$\frac{-38}{77}$	$\frac{-25}{56}$	$\frac{-9.8}{24}$	$\frac{+12.2}{30}$	$\frac{+22.6}{50}$	
			154.9	160.5	173.5	188.7	210.7	221.1	
15+00	195.2	$\frac{-37.8}{90}$	$\frac{-32.4}{82}$	$\frac{-26.0}{64}$	$\frac{-21.2}{56}$	$\frac{-13.0}{31}$	$\frac{-8.3}{22}$	$\frac{+13.0}{26}$	$\frac{+24.2}{50}$
		157.4	162.8	169.2	174.0	182.2	186.9	208.2	219.4
15+50	195.5		$\frac{-36}{109}$	$\frac{-34}{106}$	$\frac{-31.5}{86}$	$\frac{-23.6}{66}$	$\frac{-13.0}{33}$	$\frac{+10.0}{27}$	$\frac{+25.0}{50}$
			159.5	161.5	164.0	171.9	182.5	208.5	220.5
16+00	199.5		$\frac{-37.7}{88.5}$	$\frac{-27.0}{69}$	$\frac{-26.0}{60}$	$\frac{-13.0}{32}$	$\frac{+14.0}{19}$	$\frac{+23.4}{50}$	
			161.8	172.5	173.5	186.5	210.5	222.9	
16+50	202.0		$\frac{-38.7}{96}$	$\frac{-26}{56}$	$\frac{-13.0}{28}$	$\frac{+15.0}{26}$	$\frac{+23.8}{50}$		
			163.3	176.0	189.0	215.0	225.8		

Sta.	Ele. & Grade	W.W.	Lt.	±	Rt.			
17+00	207.1	$\frac{-41.4}{108}$	$\frac{-36.0}{83}$	$\frac{-26.0}{68}$	$\frac{-13.0}{38}$	$\frac{+13.0}{28}$	$\frac{+21.6}{50}$	
		165.7	171.1	181.1	194.1	220.1	228.7	
17+50	211.0	$\frac{-42.3}{109}$	$\frac{-38.0}{104}$	$\frac{-22.7}{54}$	$\frac{-13.0}{33}$	$\frac{+13.0}{27}$	$\frac{+20.5}{50}$	
		168.7	173.0	188.3	198.0	224.0	231.5	
18+09.5	213.6	$\frac{-42.6}{105}$	$\frac{-37.4}{74}$	$\frac{-26.0}{62}$	$\frac{-13.0}{34}$	$\frac{+13.0}{32}$	$\frac{+21.0}{50}$	
		171.0	176.2	187.6	200.6	226.6	234.6	
18+50	213.7	$\frac{-38.5}{95}$	$\frac{-32.0}{76}$	$\frac{-26.0}{60}$	$\frac{-13.0}{28}$	$\frac{+7.0}{20}$	$\frac{+13.0}{32}$	$\frac{+21.4}{50}$
		175.2	181.7	187.7	200.7	220.7	226.7	
19+00	211.6	$\frac{-35.2}{79}$	$\frac{-26.0}{60}$	$\frac{-13.0}{32}$	$\frac{+13.0}{30}$	$\frac{+20.7}{50}$		
		176.4	185.6	198.6	224.6	232.3		
19+50	208.2	$\frac{-30.0}{90}$	$\frac{-25}{74}$	$\frac{-19.7}{55}$	$\frac{-12.0}{34}$	$\frac{-4.7}{15}$	$\frac{+10.0}{24}$	$\frac{+17.0}{50}$
		178.2	183.2	188.5	196.2	203.5	218.2	
19+75	199.4							
20+00	208.7							

n' file

W.W.

H.L

H.L

Sta	Elev ξ	Grade	Lt	ξ	Rt.							
20+59.6	219.5		$\frac{-36.0}{87}$ 183.5	$\frac{-26.0}{59}$ 173.5	$\frac{-15.7}{35}$ 203.8	$\frac{-13.0}{26}$ 206.5	$\frac{+6.2}{12}$ 225.7	$\frac{+13.0}{34}$ 232.5	$\frac{+19.5}{50}$ 239.0			
21+00	220.7		$\frac{-34.3}{93}$ 186.4	$\frac{-29.0}{73}$ 191.7	$\frac{-25.0}{62}$ 195.7	$\frac{-12.0}{28}$ 208.7	$\frac{+12.0}{23}$ 232.7	$\frac{+21.4}{50}$ 242.1				
21+59.95	224.0		$\frac{-32.8}{96}$ 191.2	$\frac{-30.5}{78}$ 193.5	$\frac{-26.0}{68}$ 198.0	$\frac{-13.0}{33}$ 211.0	$\frac{+4.7}{9}$ 228.7	$\frac{+13.0}{29}$ 237.0	$\frac{+22.0}{50}$ 246.0			
22+09.6	226.3		$\frac{-29.6}{78}$ 196.7	$\frac{-24.0}{63}$ 202.3	$\frac{-12.0}{33}$ 214.3	$\frac{-3.8}{13}$ 22.5	$\frac{+13.0}{30}$ 239.3	$\frac{+16.7}{45}$ 243.0				
22+50	230.0	W.W. -81.1 86 1989	$\frac{-28.4}{75}$ 201.6	$\frac{-24.0}{59}$ 206.0	$\frac{-17.6}{44}$ 212.4	$\frac{-11.0}{27}$ 219.0	$\frac{-1.6}{9}$ 228.4	$\frac{+1.9}{10}$ 231.9	$\frac{+10.8}{30}$ 240.8	Top Wall Ground		
23+10	232.0	W.W.	$\frac{-29.2}{77.5}$ 202.8	$\frac{-24}{60}$ 208.0	$\frac{-14.4}{40}$ 217.6	$\frac{-12.0}{31}$ 220.0	$\frac{-0.8}{5}$ 229.2	$\frac{+3.7}{10.5}$ 235.7	$\frac{+6.8}{17}$ 238.8	$\frac{+11.3}{31}$ 243.3	F Wall.	
23+50	234.4	W.W.	$\frac{-30.4}{83}$ 204.0	$\frac{-16.3}{47}$ 218.1	$\frac{-16.0}{37}$ 218.4	$\frac{-12.0}{28}$ 222.4	$\frac{-9.5}{22}$ 224.9	$\frac{+2.5}{11}$ 236.9	$\frac{+6.0}{11.5}$ 240.4	$\frac{+10.6}{34}$ 245.0	Base Wall Top Wall Shed. ξ	
24+0.0	236.1	W.W.	$\frac{-28.4}{80}$ 207.7	$\frac{-26.0}{73}$ 210.1	$\frac{-21.8}{60}$ 214.3	$\frac{-13.0}{35}$ 223.1	$\frac{+1.8}{10}$ 237.9	$\frac{+5.2}{10.5}$ 241.3	$\frac{+8.0}{28}$ 244.1	$\frac{+10.0}{30}$ 246.1	$\frac{+11.2}{42}$ 247.3	Base Wall

Sta	Elev \pm Grade	Lt.	♀	R.L. Base of wall	Top of wall	Base of wall			
24+34	235.4 H.L.	$\frac{-27.2}{77}$	$\frac{-20.3}{58}$	$\frac{-13.0}{40}$	$\frac{+4.5}{9}$	$\frac{+6.4}{16}$	$\frac{+10.5}{31}$	$\frac{+13.0}{33}$	$\frac{+13.5}{42}$
		208.2	215.1	222.4	239.9	241.8	245.9	248.4	248.9
24+73.8	238.1	$\frac{-26.3}{69}$	$\frac{-17.5}{56}$	$\frac{-12.0}{35}$	$\frac{+6.8}{19}$	$\frac{+13.0}{39}$	$\frac{+15.9}{50}$		
		211.8	220.6	226.7	244.9	251.1	254.0		
25+00	240.9	$\frac{-26.6}{66}$	$\frac{19.3}{53}$	$\frac{-13.0}{35}$	$\frac{+8.0}{27}$	$\frac{+14.6}{50}$			
		214.3	221.6	227.9	248.9	255.5			
25+50	242.6	$\frac{-25.0}{71}$	$\frac{-17.6}{56}$	$\frac{-10.7}{31}$	$\frac{-7.6}{23}$	$\frac{+6.4}{18}$	$\frac{+11.8}{37}$	$\frac{+20.6}{50}$	
		217.6	225.0	231.9	235.0	249.0	254.4	263.2	
25+75	246.0 H.L.	$\frac{-25.5}{64}$	$\frac{-22.0}{55}$	$\frac{-13.0}{32}$	$\frac{-1.5}{6}$	$\frac{+1.7}{11}$	$\frac{+9.8}{35}$	$\frac{+17.2}{50}$	
		220.5	224.0	233.0	244.5	247.7	255.8	263.2	
26+00	245.5	$\frac{-24.0}{69}$	$\frac{-13.0}{40}$	$\frac{-10.2}{27}$	$\frac{-7.2}{20}$	$\frac{+4.5}{12}$	$\frac{+12.0}{35}$	$\frac{+17.5}{50}$	
		221.5	232.5	235.3	239.3	250.0	257.5	263.0	
26+50	249.8	$\frac{-25.4}{67}$	$\frac{-18.3}{48}$	$\frac{-13.0}{33}$	$\frac{+4.7}{12}$	$\frac{+8.8}{33}$	$\frac{+12.0}{50}$		
		224.4	231.5	236.8	254.5	258.6	261.8		
27+00	252.8	$\frac{-24.7}{72}$	$\frac{-21.4}{48.5}$	$\frac{-13.0}{35}$	$\frac{+5.0}{23}$	$\frac{+7.7}{38}$	$\frac{+9.0}{50}$		
		228.1	231.4	239.8	257.8	260.5	261.8		

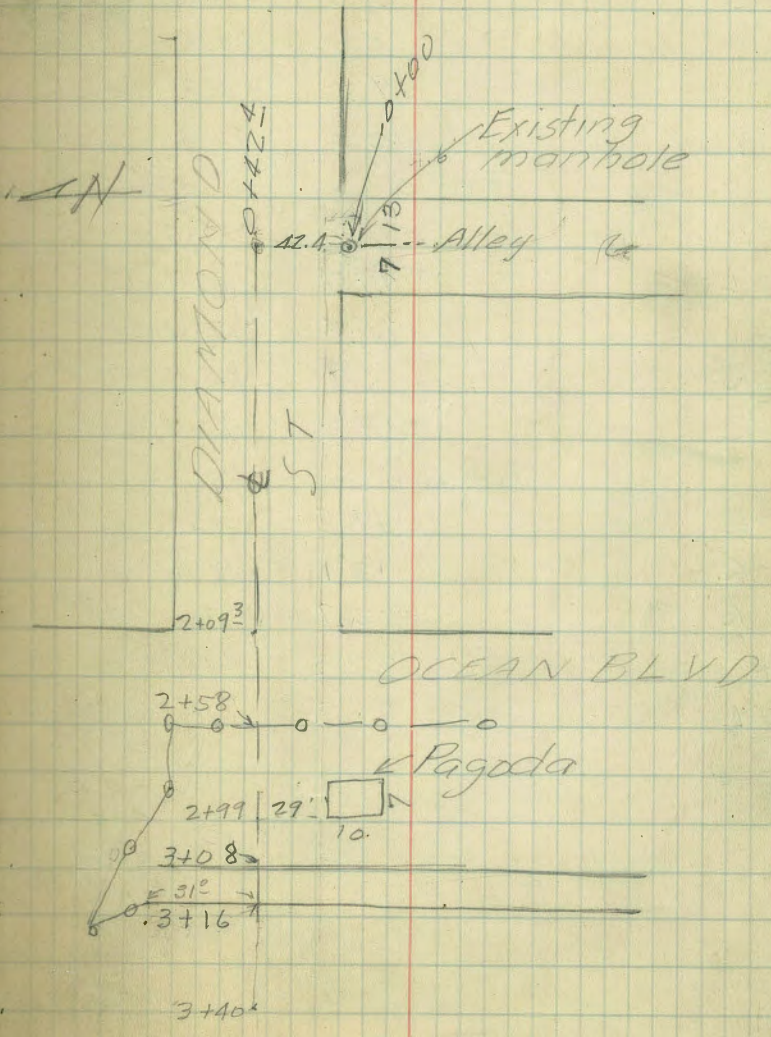
Sta	Elev. \pm	W.W.	LT.	\pm	RT.	N. Curb Washington
27+28 B.C.	253.12	$\frac{-22.6}{77}$	$\frac{-15.1}{58}$	$\frac{-13.0}{43}$ $\frac{-4.3}{16}$	$\frac{+3.0}{13}$ $\frac{+6.8}{33}$ $\frac{+8.5}{50}$ $\frac{+10.7}{60}$ $\frac{+18.9}{67.3}$	
		230.5	238.0	240.1 248.8	256.1 259.9	261.6 263.8 264.0
27+50	256.7	$\frac{-22.2}{85}$	$\frac{-18.2}{69}$	$\frac{-16.3}{59.6}$ $\frac{-13.0}{48}$ $\frac{-1.3}{11}$	$\frac{+2.6}{17.7}$ $\frac{+4.4}{32}$ $\frac{+5.1}{47}$ $\frac{+7.3}{55}$ $\frac{+7.7}{62.5}$	N. Curb Washington
		232.5	238.5	240.4 243.7 255.4	259.3 261.1 261.8	264.0 264.4
28+00	260.2	$\frac{-17.5}{71}$	$\frac{-9.5}{50}$	$\frac{-3.0}{28}$ $\frac{-1.8}{8.5}$	$\frac{+1.0}{22.6}$ $\frac{+3.2}{33.8}$ $\frac{+4.2}{42}$ $\frac{+4.3}{56.5}$	N. Curb
		242.7	250.7	257.2 258.4	261.2 263.4	264.4 264.5
28+50	261.0		$\frac{-1.4}{50}$	$\frac{-1.5}{8.7}$	$\frac{+1.8}{2.7}$ $\frac{+3.7}{3.7}$ $\frac{+4.0}{4.7}$	N. Curb
		259.6	259.5	259.2	257.3	257.0
29+00	264.1		$\frac{+0.7}{50}$	$\frac{0.0}{2.7}$	$\frac{+0.7}{1.2}$ $\frac{+1.3}{24.5}$ $\frac{+1.7}{35}$	N. Curb
		264.8	264.1	264.8	265.4	265.8
29+47.62 E.C.	266.4		$\frac{-0.6}{50}$	$\frac{-0.7}{26.3}$	$\frac{+0.6}{2.3}$	N. Curb
		265.8	265.7	265.8		

Notes for Comfort
station and sewer
line at Diamond St.

May 28-35
Louden
Graboski
another guy.

Indexed
C.S.K.

B.M.	4.32	36.72	32.40	NE Ocean Blvd. Diamond
0+00 M.H. FL		9.90	26.82	
0+00 M.H. Rim		7.10	29.62	
0+42 [±] & Diamond		6.50	30.22	
0+49 [±]		6.37	30.35	
1+00		5.50	31.22	
2+00		4.67	32.05	
2+09 ³ End Pav.		4.60	32.12	
2+58		4.0	32.7	
3+00		4.0	32.7	
3+08		8.0	28.7	
T.P.	4.28	33.35	7.65	29.07
		3+08		
50 R		+0.4	33.8	
31 R		0.7	32.7	
&		8.0	28.7	
50 L		10.7	22.7	
		3+16		
50 L		10.6	22.8	
&		4.1	29.3	
40 R		0.0	33.4	
50 R		0.0	33.4	



H1-33.35

37

3+20

50R	1.4	32.0
24R	3.2	30.2
4R	5.8	27.6
Φ	9.1	24.3
50L	12.0	21.4

3+30

50L	18.0	15.4
20L	17.7	15.7
Φ	15.5	17.9
32R	8.9	24.5
46R	13.0	20.4

3+40

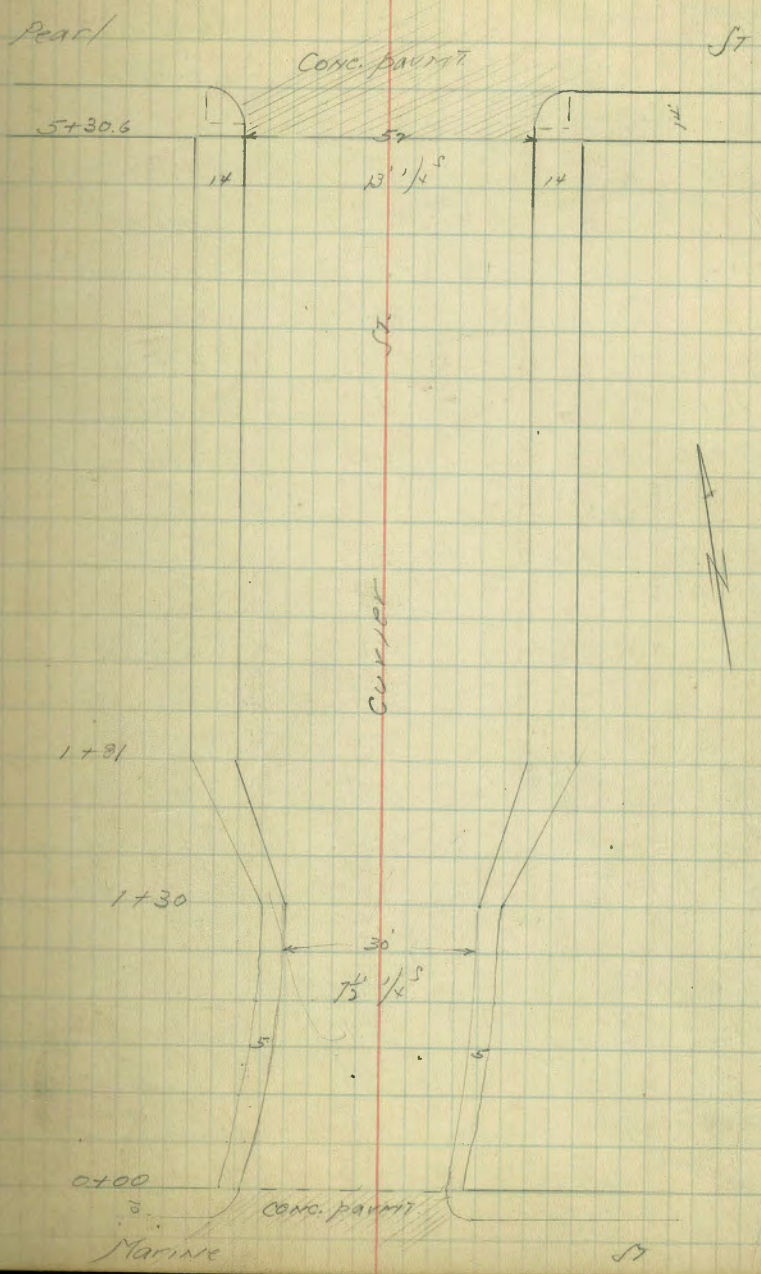
50R	17.5	15.9
35R	13.1	20.3
27R	12.9	20.5
Φ	22.3	11.1
50L	22.3	11.1

Moore
Lesson
4-6-34

XSec CURVER ST
Marine To Pearl

INDEXED
c.s.K.

NW8P	1289	77.9'		65.06	Pearl & LaSalle Blvd
T.P.	11.63	89.37	021	77.74	sdw NW Cor Pearl & Curver
00-10					
W	gut par.		375	85.52	
ob	" "		349	85.88	
1/4	" "		329	86.08	
C	" "		306	86.31	
1/4	" "		294	86.43	
ob	" "		285	86.52	
E	" "		270	86.67	
00-14 Marine					
E ob			223	87.14	
gut par			276	86.61	
1/4	" "		280	86.59	
C	" "		284	86.53	
1/4	" "		312	86.25	
gut	" "		342	85.95	
N ob			294	86.45	
0+20					
W ob			263	86.74	
gut			36	85.8	
1/4			32	86.2	
C			29	86.5	
1/4			28	86.6	



8937

8937

32

√ 1400

qut	2.8	86.66
E cb	1.77	87.60
√ 0700		
E cb	1.65	87.72
qut	2.9	86.5
1/4	2.9	86.5
c	2.5	86.6
1/4	3.3	86.1
qut	2.7	85.7
W cb	2.66	86.71
√ 0750		
W cb	2.78	86.59
qut	2.8	85.6
1/4	2.2	86.2
c	2.8	86.6
1/4	3.6	85.8
qut	2.9	86.5
E cb	1.62	87.75
√ 0775		
E cb	1.77	87.60
qut	2.9	86.5
1/4	2.9	86.5
c	2.9	86.5
1/4	3.5	85.9
qut	2.8	85.6
W cb	2.98	86.39

W cb	3.18	86.19
qut	4.0	85.4
1/4	3.6	85.8
c	3.1	86.3
1/4	2.8	86.5
qut	2.8	86.6
E cb	1.90	87.47
√ 1750		
E cb	2.04	87.33
qut	2.9	86.5
1/4	2.1	86.3
c	2.3	86.7
1/4	2.7	85.7
qut	4.2	85.2
W cb	3.52	85.85
√ 1781		
W cb	4.30	85.07
qut	5.1	84.5
1/4	4.4	85.0
c	3.7	85.7
1/4	3.7	85.7
qut	3.6	85.8
E cb	2.67	86.70
√ 2400		
E cb	3.04	86.33
qut	3.5	85.6

8937

1/2	4.0	85.4
c	4.1	85.3
1/4	4.8	84.6
gut	5.5	83.9
Wcb	4.65	84.69
✓ 2+50		
Wcb	5.46	83.91
gut	6.4	83.0
1/4	5.5	83.9
c	4.8	84.6
1/4	4.9	84.5
gut	5.0	84.4
Ecb	3.9	85.46
✓ 3+00		
Ecb	4.80	84.55
gut	5.8	83.6
1/4	5.7	83.7
c	5.9	83.5
1/4	6.5	82.9
gut	7.0	82.4
Wcb	6.25	83.12
✓ 3+50		
Wcb	7.07	82.30
gut	7.8	81.6
1/4	7.2	82.2
c	6.7	82.7

8937

33

1/4	6.6	82.8
gut	6.5	82.9
Ecb	5.54	83.83
✓ 4+00		
Ecb	6.30	83.07
gut	7.3	82.1
1/4	7.4	82.0
c	7.6	81.8
1/4	5.2	81.2
gut	8.7	80.7
Wcb	7.84	81.53
✓ 4+50		
Wcb	8.61	80.76
gut	9.5	79.9
1/4	8.9	80.5
c	8.2	81.2
1/4	8.0	81.4
gut	8.0	81.4
Ecb	7.68	82.29
✓ 5+00		
Ecb	7.89	81.48
gut	8.7	80.7
1/4	8.7	80.7
c	8.9	80.5
1/4	9.4	80.0
gut	10.2	79.2
Wcb	9.45	79.92

√ 430.60

Sly Pearl

W CB	987	79.50
QUIT pay	1034	79.02
1/4 "	976	79.61
C "	912	80.25
1/4 "	899	80.38
QUIT "	903	80.34
E CB	834	81.05

Sly CB Pearl - Valley Center

E.L. pay	898	80.39
CB "	921	80.16
1/4 "	953	79.84
C "	923	79.64
1/4 "	1014	79.23
CB "	1045	78.92
WL "	1073	78.64

TP OAF 78.9 1163 77.74

ch. to BM 1313 65.06 65.06

NWDP Pearl +
La Jolla Blvd

Indexed
C.S.R.

x sec alley 20' wide
DK & Lavola Park

Moore
6-15-35

Pearl

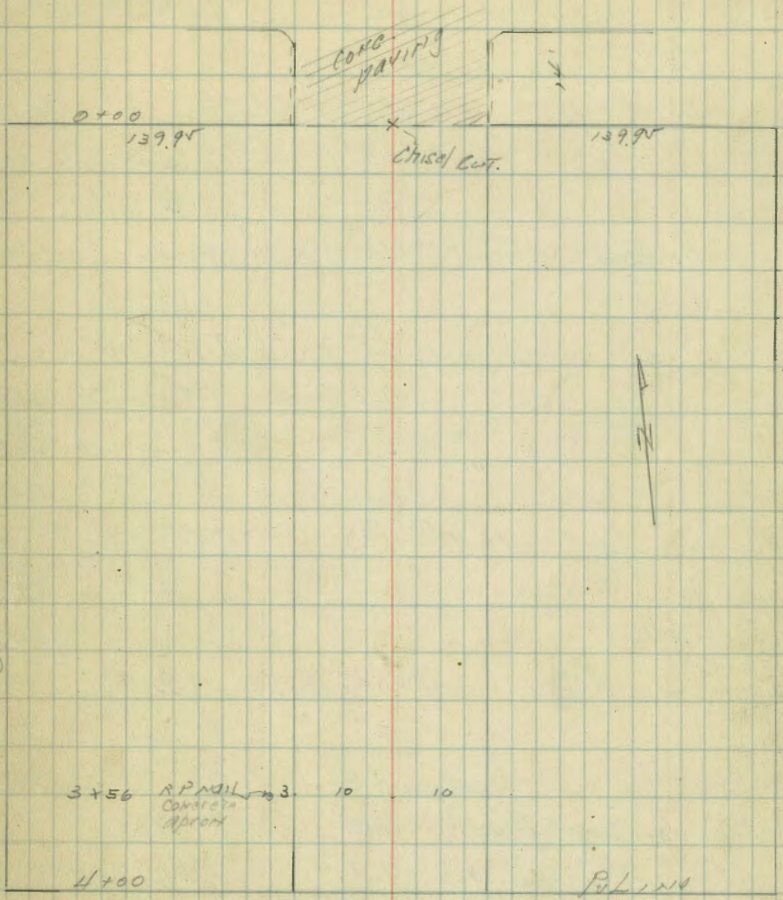
ST.

35

	12.66	90.40	77.74	T.P. 1021
0-14 = 5' cut Pearl				
W on pt.	5.95		84.55	
C " "	5.55		84.85	
E " "	5.21		85.19	
00				
E Top cb	4.40		86.00	
" pt	4.70		85.70	
C "	5.06		85.34	
W "	5.01		85.39	
" Top cb	4.97		85.43	
0+20 = 1/4 edge 3 car garage dirt floor				
W-3.8 dirt floor	4.7		85.7	
W	4.7		85.7	
C ✓	4.7		85.7-	
E	4.5		85.9	
0+48 1/4 edge 3 car gar. dirt floor				
E	4.0		86.4	
C ✓	3.9		86.5	
W	4.2		86.2	
+3.8 dirt floor	4.3		86.1	
0+59				
W	4.0		86.4	
C	3.7		86.7	
E	3.9		86.5	

ST.

Corner



ST.

Draper

0+59	90.40			
E +10 Sx gar. dirt floor	3.6	86.8		
0+93				
E	3.2	87.2		
C ✓	3.2	87.2		
W	3.2	87.2		
+5.8 Sx gar. dirt floor	3.2	87.2		
1+50				
W	2.1	88.3		
C ✓	2.0	88.4		
E	2.1	88.3		
T.P.	7.87	96.94	1.33	89.07
1+90				
E	7.7	89.2		
C ✓	7.7	89.2		
W	7.7	89.2		
+3.7 edge Conc. Apron	7.87	89.07		
+4.5 Sing. r floor gar	7.87	89.07		
2+09				
- 3.7 Sx gar Conc. floor	7.12	89.7		
- 2.0 edge " apron	7.14	89.80		
W	7.2	89.7		
C ✓	7.3	89.6		
E	7.2	89.7		

2+50				
E	6.1	90.8		
C ✓	6.2	90.7		
+9 S' Bd fence	6.1	90.8		nly end fence
2+73				
W 2' wide cement walk	5.71	91.23		1.5' walk
2+80 = Nly double gar + Sly end S' Bd fence				ON WEST
- 2' Conc floor garage	5.28	91.66		1.0' walk
W + 0.6 " apron	5.39	91.55		
W + 1.6 line Bd fence	5.4	91.5		
C ✓	5.4	91.5		
E	5.2	91.7		
2+45				
E-13 Sx gar. dirt floor	4.2	92.7		
3+00 Sly edge double garage on west				
E	4.7	92.2		
C ✓	4.9	92.0		
+9.4 Conc. apron	5.16	91.78		
W + 2 " floor garage	5.06	91.88		
3+26 = Nly double garage on west				
W-4 Conc floor	3.95	92.99		
W " apron	4.18	92.76		
C ✓	4.5	92.4		
E	4.3	92.6		

96.94

3746 Sly double gar on West

E		3.7	93.2
C	✓	4.0	92.9
W	Conc. Apron	3.89	93.05
+4	" floor garage	3.86	93.08

3756 Nly double gar on West

W	-4.7 Conc. floor	3.71	93.23
"	+1.7 " 91	3.74	93.20
W		3.7	93.2
C		3.7	93.2
E		3.5	93.4

3776 Sly double garage on West

E		3.0	93.9
C		3.1 ²	93.8
W		3.7	93.2
+1.7	Conc. Apron	3.86	93.08
+4.7	" floor garage	3.81	93.13

if 100 = Purple line

W		2.8	94.1
C		2.4	94.5
E		2.1	94.8

T.T. 0.34 93.34 3.92 93.02

Ch. top of on E side 6.00 87.34 87.33

Prior
at 1+30 p. 32

10-23-35

Survey Camino Del Rio.

Miller. Road. S. side Mission Valley.
Walker. from Old Town to 6th St. Extension.
Bliss.

5+00

See Book. 1528. - P. 1
for Complete Notes

1+16.95 Hub. E.C.

0+00 P.I. Hub ϕ Taylor St.

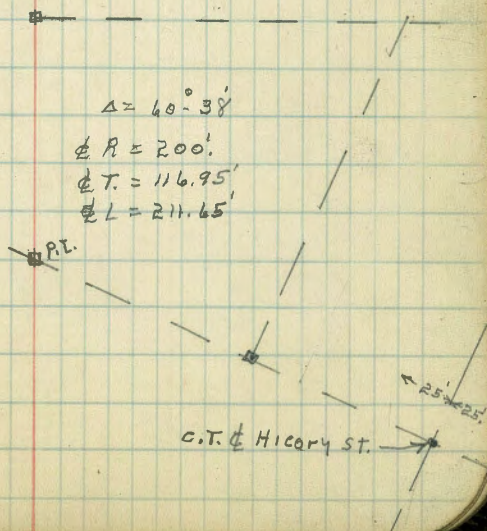
ϕ Taylor St.

$\Delta = 40^{\circ} 38'$
 $\phi R = 200'$
 $\phi T = 116.95'$
 $\phi L = 211.65'$

P.I.

C.T. ϕ Hicory St.

$\leftarrow 25^{\circ} 42'$



11+00

5+00

17+00

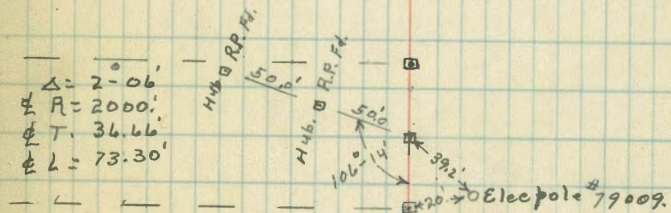
15+11.2L

Hub. E.C.

Hub. P.I.

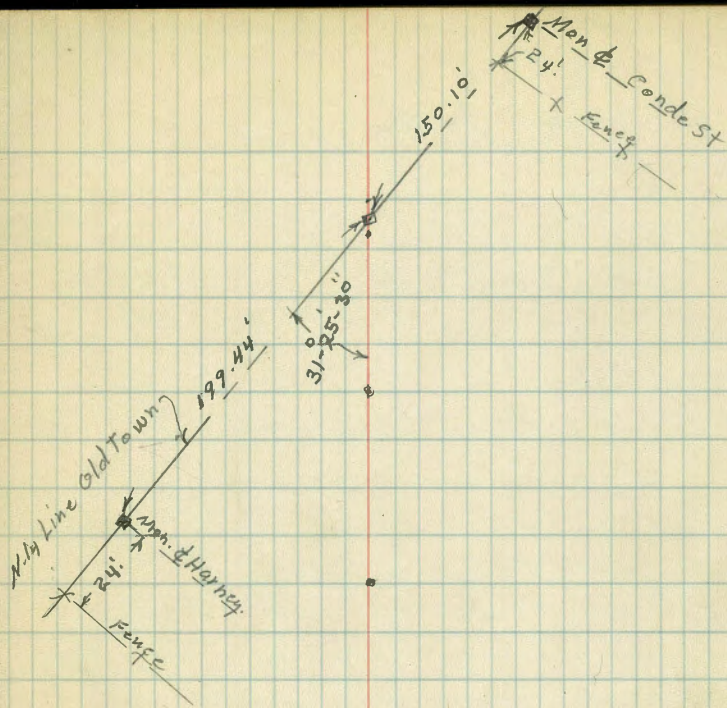
14+37.2L

Hub. B.C.

 $\Delta = 2^{\circ} 06'$
 $R = 2000'$
 $T = 36.66'$
 $L = 73.30'$


11+00

RR+82 22 Hub. P.O.T. Nly. line Old Town.



29+66.22

Hub.

P.O.T.

29+00

23+00

50.0' Hub. R.P. P.A.
37.0' Hub. R.P. P.A.

42

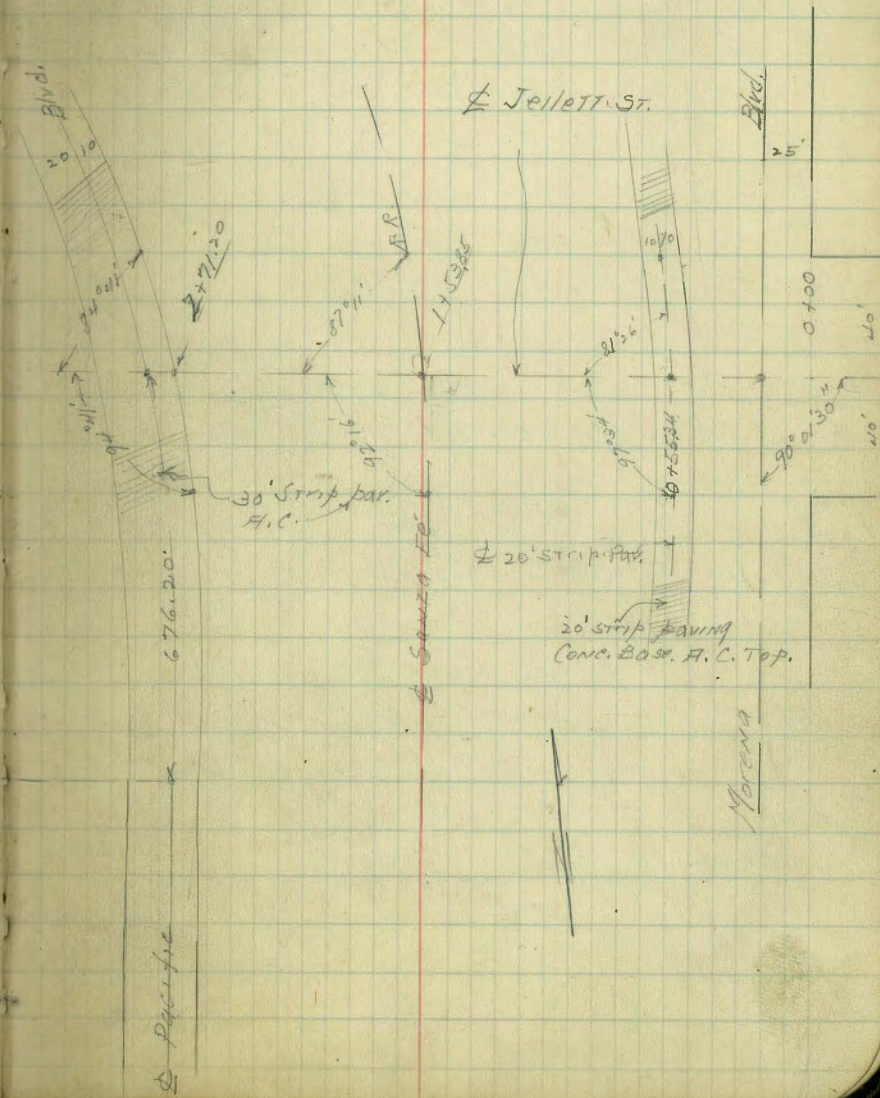
Moore
2-26-36

INDEXED
C.S.R.

43

Survey of Jellert St 50' wide Morena Blvd To Pacific Blvd

Levels p 44



1 + 12

1 + 06

1 + 03

0 + 85

0 + 65.4 W edge 20' Strip Pav.

0 + 55.34 E 20' Strip Pav

0 + 25

0 + 00 E Jellett St / Mon. Morning E Sta.

Mon. inside
Sw Cor. RR Row. 7.19 1852

1133

Mon. Morning
Jellett St

E Jellett St.

44

Pencil Guy
7.05
30

5/4

Nth 4.

INSIDE CITY V.S.C. #6
ROW RR 3M 30
ST

11.00	11.14		11.50	11.80	11.02		12.40
7.5	7.4	Cor. Row	6.0		6.5	Cor. Row	6.1
4.0	3.0	28	1.5	5.7	1.0	28	4.0

11.60	13.00	13.40	13.10	14.00	13.30
6.9	5.5	5.1	5.4	5.4	5.2
4.0	1.5	1.5	1.5	2.8	4.0

13.35	13.55	13.90
5.1	4.7	4.6
4.0		4.0

13.50	13.90	14.00
5.0	4.5	4.3
4.0		4.0

11.80	12.90	14.10	13.90	15.00
5.7	4.6	4.4	4.6	3.5
4.0	1.5	1.5	1.5	4.0

16.90	16.80	13.80	14.90	15.00	15.20	14.40
1.6	2.7	4.7	3.6	3.3	3.3	1.1
4.0	3.0	1.7	1.5	1.5	1.5	4.0

1852

J.P. 1.24 9.21 10.55 7.97

1+70

1+57

W rail RR. Top rail

E rail RR Top rail

1+50

1+38

1+25

18.52

Σ

45

$\frac{6.54}{12.0}$	$\frac{7.44}{25}$	$\frac{9.94}{15}$	$\frac{10.44}{8.3}$	$\frac{8.14}{10}$	$\frac{9.44}{10.3}$
$\frac{40}{40}$				$\frac{40}{40}$	$\frac{40}{40}$

$\frac{10.94}{7.6}$	$\frac{11.34}{7.2}$	$\frac{11.44}{7.1}$
$\frac{40}{40}$		$\frac{40}{40}$

$\frac{11.85}{7.07}$	$\frac{11.79}{6.73}$	$\frac{12.14}{6.40}$
$\frac{40}{40}$		$\frac{40}{40}$

$\frac{11.69}{6.23}$	$\frac{14.04}{6.50}$	$\frac{14.39}{6.13}$
$\frac{40}{40}$		$\frac{40}{40}$

$\frac{11.12}{7.4}$	$\frac{14.14}{6.4}$	$\frac{11.84}{6.7}$
$\frac{40}{40}$		$\frac{40}{40}$

RR Crossing
5.24
19

$\frac{10.74}{7.8}$	$\frac{10.74}{7.8}$	$\frac{12.14}{6.4}$	$\frac{12.24}{6.3}$	$\frac{10.84}{7.7}$	$\frac{10.84}{7.7}$
$\frac{40}{40}$	$\frac{30}{30}$	$\frac{40}{40}$		$\frac{40}{40}$	$\frac{40}{40}$

18.52
Σ

check to B.P. Max.		6.53	11.33	11.33
T.P.	9.89	17.86	12.4	7.97

E. edge pav. on Pae. Blvd.

2+50

$\frac{8.86}{\frac{5.25}{40}}$	$\frac{3.96}{\sqrt{25}}$	$\frac{4.06}{\frac{5.15}{40}}$
--------------------------------	--------------------------	--------------------------------

$\frac{3.81}{\frac{5.2}{40}}$	$\frac{3.91}{\frac{5.3}{15}}$	$\frac{4.21}{5.0}$	$\frac{4.01}{\frac{5.2}{15}}$	$\frac{4.01}{\frac{5.2}{40}}$
-------------------------------	-------------------------------	--------------------	-------------------------------	-------------------------------

2+35

$\frac{4.21}{\frac{5.0}{40}}$	$\frac{4.61}{\frac{4.6}{15}}$	$\frac{4.41}{4.8}$	$\frac{4.21}{\frac{5.0}{15}}$	$\frac{4.01}{\frac{5.2}{40}}$
-------------------------------	-------------------------------	--------------------	-------------------------------	-------------------------------

2+20

$\frac{5.21}{\frac{4.0}{40}}$	$\frac{5.61}{\frac{4.6}{20}}$	$\frac{5.81}{3.4}$	$\frac{6.01}{\frac{3.2}{15}}$	$\frac{7.01}{\frac{2.2}{40}}$
-------------------------------	-------------------------------	--------------------	-------------------------------	-------------------------------

2+05

$\frac{6.01}{\frac{3.2}{40}}$	$\frac{7.01}{\frac{2.2}{15}}$	$\frac{7.21}{17}$	$\frac{6.71}{\frac{2.5}{15}}$	$\frac{7.31}{\frac{1.9}{40}}$
-------------------------------	-------------------------------	-------------------	-------------------------------	-------------------------------

2+03

SURFACE ROW FENCE
29

N.W. COR ROW FENCE
28

921

921

11-17-36
Miller
Walker
Bliss.

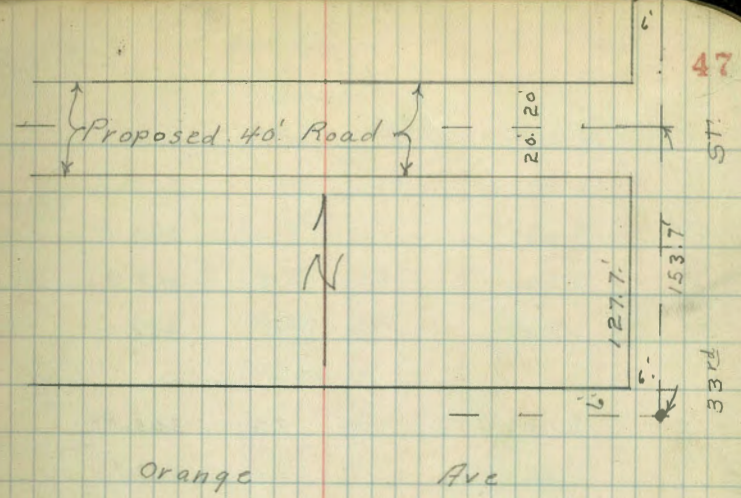
X Sec. 40' Road. N. of Orange Ave
W. of 33rd for Mrs. Bryant.
Thru lots 17 to 20, Teralta

Indexed
C.S.K.

B.M. B.P. 7.13 373.79 366.66 4 Orange. N.W. 33rd

14' E. of W. line = W. curb of 33rd St.

S-20	cmt. ch	5.80	367.99
S-20	gutter Pav	6.41	367.38
S	" "	6.08	367.71
S	cmt. ch	5.50	368.29
±	" "	5.35	368.44
±	Gutter Pav	5.92	367.82
N	" "	5.67	368.12
N	cmt. ch	5.10	368.69
N + 20	" "	4.76	368.03
N + 20	gutter Pav.	5.36	368.43
1.5' E. of W. line = W. edge 5.33 cmt. walk			
N-20		4.56	369.23
N		4.90	368.89
±		5.08	368.71
S		5.30	368.49
S + 20		5.63	368.16
0+00 = W. line 33 rd St.			
S		5.1	368.2
1/4		4.9	368.9
±		4.7	369.2
1/4		4.8	369.0
N		4.7	369.1



	373.79	
	0+03 W.	
1/4	3.9	369.9
1/4	4.3	369.5
±	4.1	369.7
1/4	4.2	369.6
S	4.6	369.2
	0+50 W.	
S	5.0	368.8
1/4	4.6	369.2
±	4.6	369.2
1/4	4.9	368.9
N	4.7	369.1

373.79

1+00 W.

N	5.4	368.4
1/4	5.5	368.3
1/2	5.5	368.3
3/4	5.4	368.4
S	5.8	368.0

1+50 W.

S	7.0	366.8
1/4	6.7	367.1
1/2	6.7	367.1
3/4	6.2	367.6
N	6.0	367.8

2+00 W.

N	6.8	367.0
1/4	7.1	366.7
1/2	7.0	366.8
3/4	7.0	366.8
S	7.5	366.3

2+50

S	8.0	365.8
1/4	7.8	366.0
1/2	7.7	366.1
3/4	7.4	366.4
N	7.1	366.7

T.P.	2.65	369.15	7.29	366.50
------	------	--------	------	--------

369.15

48

3+00 W.

N	3.0	366.2
1/4	3.0	366.2
1/2	3.4	365.8
3/4	3.3	365.9
S	3.8	365.4

3+50 W.

S	4.4	364.8
1/4	4.5	364.7
1/2	4.2	365.0
3/4	4.1	365.1
N	3.9	365.3

4+00 W.

N	4.6	364.6
1/4	5.1	364.1
1/2	5.6	363.6
3/4	5.5	363.7
S	5.4	363.8

4+50 W.

S	6.4	362.8
1/4	5.9	363.3
1/2	6.3	362.9
3/4	6.0	363.2
N	6.2	363.0

369.15

4+70 W.

N	5.7	363.5
1/4	6.1	363.1
1/2	6.2	363.0
3/4	6.2	363.0
S	6.1	363.1

4+80

S	6.0	363.2
1/4	5.1	364.1
1/2	4.8	364.4
3/4	4.3	364.9
N	3.9	365.3

4+94

N	4.0	365.2
1/4	4.1	365.1
1/2	4.0	365.2
3/4	4.7	364.5
S	5.0	364.2

5+00	1/2	6.0	363.2
5+12	1/2	10.7	358.5
5+16	1/2	11.8	357.4
5+24	1/2	10.3	358.9
5+40	1/2	8.0	361.2
5+53	1/2	6.3	360.9

N.S. Drainage
Ditch

369.15

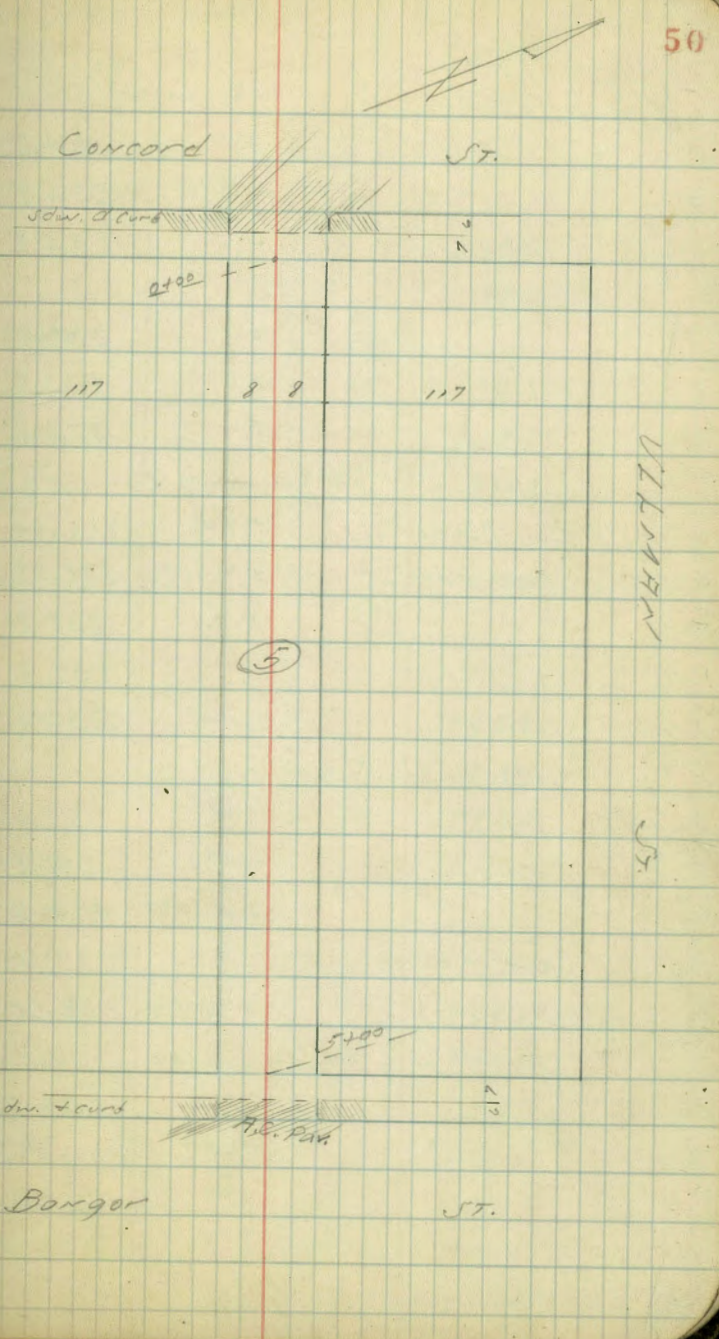
49

T.P.	8.80	369.56	8.39	360.76
chk Orig B.M.			2.90	366.66 ✓

X Sec of Alley 10' wide
 Bit of Roseville HTS
 Box Wilton + Trumbull
 Bangor + Concord

Indexed
 c.s.K.

NEED	Time	Concord	Trumbull
	8:10	229.58	230.48
00-13 = Ely curb Concord			
S par		9.43	229.15
C "		9.51	229.07
N "		9.57	229.01
00-07			
N cb		9.08	229.50
N par		9.42	229.16
C "		9.38	229.20
S "		9.31	229.27
S = b		8.96	229.62
0+00 = Ely Concord			
S		6.8	231.8
+W		8.0	230.6
C		7.7	230.9
+S		7.6	231.0
N		6.3	232.3
0+15			
N		5.0	233.6
C		5.3	233.3
S		5.2	233.4
0+30			
S		4.5	234.1
C		4.4	234.0
N		4.6	234.0



0 + 50

N	4.4	234.2
C	4.4	234.2
S	4.4	234.2
1 + 00		
S	5.1	233.5
C	5.3	233.3
N	5.2	233.4

1 + 13 = Wly ^{Double} gar on N S, do

- 13 = Cor. floor Cent.	5.94	232.64
- 1.5 = Cent apron	5.96	232.62
N	5.9	232.7
C	5.9	232.7
S	5.6	233.0

1 + 29 = Ely above

S	6.3	232.3
C	6.4	232.2
N	6.1	232.5
+ 1.5 Cent apron	5.98	232.60
+ 13 " floor	6.00	232.58

1 + 54 Wly Gar. on S S, do

N	7.7	230.9
C	7.9	230.7
S	8.0	230.6
+ 8 dirt floor	7.9	230.7

214
1 + 72 = above Gar.

- 8 dirt floor	8.1	230.5
S Fence in alley 0.4	8.5	230.1
C	8.6	230.0
N	8.9	230.3
2 + 00		
N	10.0	228.6
C	10.4	228.2
S 1.10 fence in alley	9.0	229.6

T.P. 1.27 227.11 ✓ 12.7 ✓ 225.84

2 + 30

S fence in alley 1.10	1.9	225.2
C	2.4	224.5
N	2.7	224.4

2 + 50

end of fence 1.0 in alley

2 + 60

N	5.0	222.1
C	4.6	222.5
S	4.0	223.1

3 + 00

S	6.3	220.8
C	7.0	220.1
N	7.5	219.6

3+50

N	8.1	219.0
C	7.4	219.7
S	6.3	220.8

4+00

S	9.8	217.3
C	9.9	217.2
N	10.2	216.9

4+50

N	12.7	214.4
C	12.9	214.2
S	12.5	214.6

T.P. 2.01 216.77 12.35 214.70

5+00 = wly Bangor

S	4.2	212.6
C	4.3	212.5
N	5.1	211.7

5+07

N cb	10.04	206.73
N pav	10.36	206.41
C "	9.85	206.92
S "	9.33	207.44
S ct	9.01	207.76

Please check this
To profile or
pav. plan

5+13 = wly curb of Bangor

S	pav.	9.54	207.23
C	"	10.01	206.76
N	"	10.52	206.25

Prop. Sensor on Voltage
E of Willow St.

Indexed
C.S.M.

Wood
2-2-47

53

SW30	3.32	169.49	166.17	Willow Whittier
0+00-ELY Willow		2.1	167.4	
+20		3.4	165.9	
+50		7.0	162.5	
+75		8.1	161.4	
T.P.	0.27	156.94	156.67	
+87		1.8	158.1	
1+00		5.5	151.4	
+10		9.2	147.5	
+20		13.5	143.4	
T.P.	0.27	144.99	144.12	
+28		3.7	140.7	
+33		2.6	141.8	
+60		8.9	135.5	
+75		15.8	128.6	
T.P.	0.90	132.81	131.91	
+85		7.3	125.5	
2+00		8.5	124.3	
+50		11.0	121.8	
2+84.5	ground	13.1	119.7	
"	P.M.M.H.	12.10	120.71	
"	E.L.S.M.H.	30.50	102.31	

Note - 00 to 1785 is on old fill.

Voltage

Willow

0+00

2+84.50 = Ex. S.M.H.

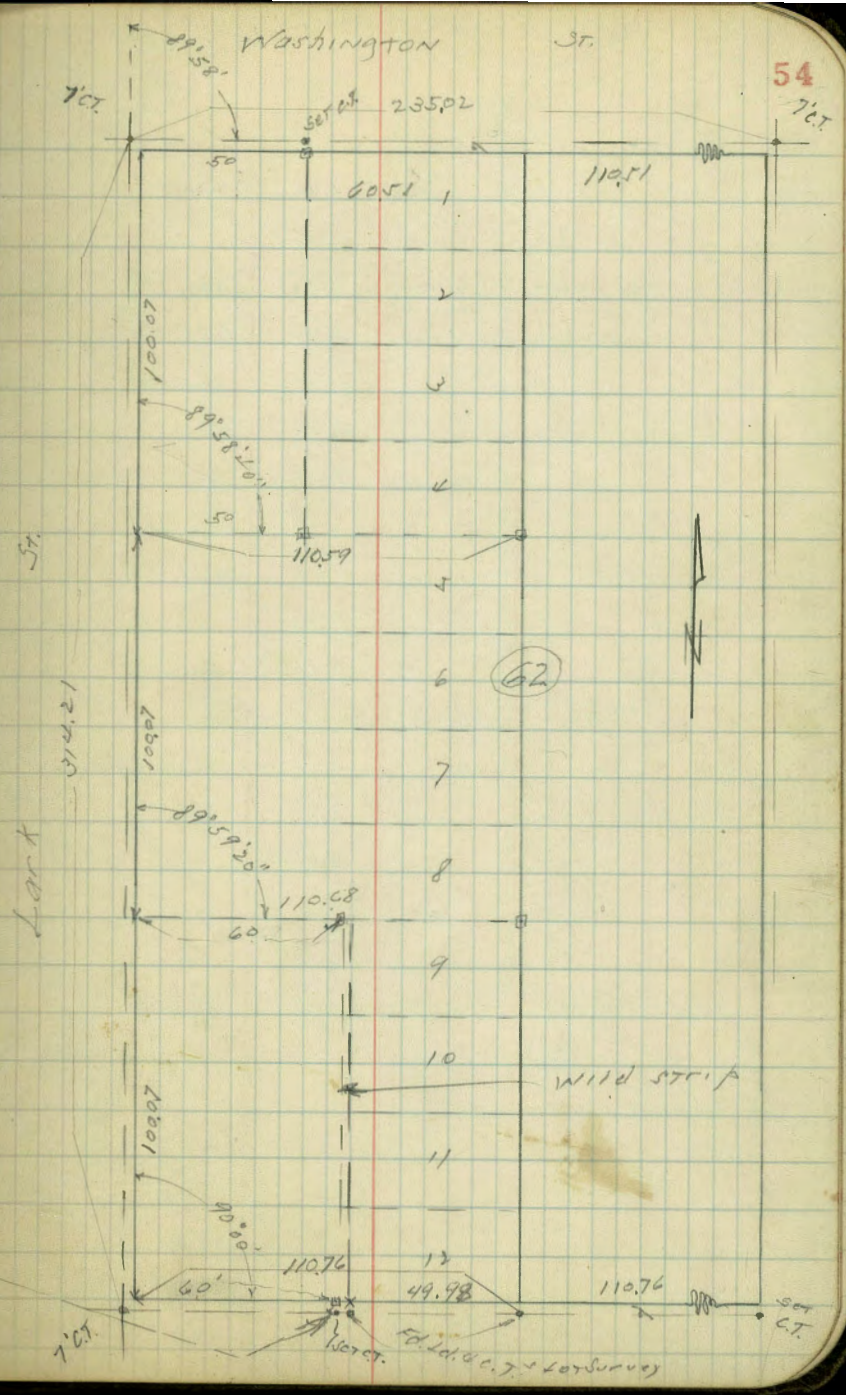
Indexed
C.S.K. Moore
4-10-37

Survey of portions of
Lots 1-12 Situated Arnold & Chaate's

To enlarge the Grant School Playgrounds

- = 2d. 4" C.T.
- = 2"x2" RW Hubs

Fd. chisel cut .39 W of C.T.
> diff. private Lot Surveys



471.09

	0+50 (cow)	
E. cl.	5.6	465.5
E	5.6	465.5
	1+00	
E	6.1	465.0
cl	6.2	464.9
1/4	6.0	465.1
♀	6.0	465.1
1/4	6.0	465.1
cl	6.1	465.0
W.	5.9	465.2
	1+50	
W	6.7	464.4
cl	7.1	464.0
1/4	6.9	464.2
♀	6.8	464.3
1/4	6.9	464.2
cl	7.1	464.0
E	6.7	464.4
	2+00	
E	8.3	462.8
cl	8.3	462.8
1/4	8.1	463.0
♀	8.1	463.0
1/4	8.3	462.8
cl	8.4	462.7
W	8.6	462.5

471.09

60.154

56

	2+50	
W	10.7	460.4
cl	10.5	460.6
1/4	10.3	460.8
♀	10.2	460.9
1/4	10.2	460.9
cl	9.9	461.2
E.	10.0	461.1
	3+00	
E	12.2	458.9
cl	12.6	458.5
1/4	12.8	458.3
♀	13.1	458.0
1/4	13.6	457.5
cl	14.2	456.9
W	15.2	455.9

— T.F. — 0.66 — 458.84 — 12.91 — 458.18 —

	3+25	
W	5.4	453.4
cl	5.2	453.6
1/4	4.5	454.3
♀	3.8	455.0
1/4	3.3	455.5
cl	2.5	456.3
E	2.7	456.1

45884

3+50

E	5.8	453.0
cl	6.1	452.7
1/4	6.2	452.6
⊕	6.8	452.0
1/4	7.3	451.5
d	7.5	451.3
w	7.8	451.0

3+75

w	10.2	448.6
d	9.8	449.0
1/4	9.7	449.1
⊕	9.5	449.3
1/4	9.2	449.6
cl	9.1	449.7
E	8.6	450.2

4+10

E	12.1	446.7
cl	12.6	446.2
1/4	12.5	446.3
⊕	12.4	446.4
1/4	12.6	446.2
cl	12.9	445.9
w	13.7	445.1

T.P.

0.63

446.82

12.65

446.19

446.82

60th 54

4+50

w	5.4	441.4
cl	5.0	441.8
1/4	4.9	441.9
⊕	5.0	441.8
1/4	5.0	441.8
cl	4.7	442.1
E	3.8	443.0

5+00

E	10.7	436.1
cl	11.2	435.6
1/4	11.2	435.6
⊕	11.3	435.5
1/4	11.3	435.5
cl	11.7	435.1
w	11.0	435.8

5+25

w	13.6	433.2
d	14.0	432.8
1/4	14.0	432.8
⊕	13.8	433.0
1/4	13.8	433.0
cl	13.5	433.3
E	12.8	434.0

5+50

E	14.8	432.0
---	------	-------

T.P.

0.30

434.52

12.60

434.22

57

5+50 (con)

c.d	3.2	431.3
"4	3.2	431.3
¢	3.2	431.3
"4	3.3	431.2
cl	3.3	431.2
w	2.7	431.8

6+00

w	6.4	428.1
cl	6.4	428.1
"4	6.6	427.9
¢	6.6	427.9
"4	7.0	427.5
cl	7.1	427.4
¢	6.8	427.7

6+50

¢	9.6	424.9
cl	9.7	424.8
"4	9.6	424.9
¢	9.5	425.0
"4	9.4	425.1
cl	9.4	425.1
w	8.9	425.6

7+15

w	11.6	422.9
cl	11.4	423.1
"4	11.8	422.7

¢	12.4	422.1
"4	12.7	421.8
cl	12.6	421.9
¢	12.8	421.7

T.P. — 2.85 — 424.71 — 12.66 — 421.86 —

7+39⁵ = N. Line Estelle st Map 1829

¢	4.1	420.6
cl	3.8	420.9
"4	3.9	420.8
¢	3.7	421.0
"4	3.6	421.1
cl	3.8	420.9
cl	4.0	420.7

7+63⁶ = Existing curb return

w. Top. ent. cl.	4.83	419.88
w+10 curb Line to S. Top. cl.	5.00	419.71

7+64⁵ S. Line Cileher Tract. = Hedge Pavmt.

2' w of cl. line = ent. cl.	5.01	419.70
" " gutter pay.	5.58	419.13
w. cl. Line	5.52	419.19
"4	5.34	419.37
¢	5.16	419.55
"4	5.04	419.67
cl	4.90	419.81
¢	4.70	420.01

424.71

Set. B.M. BP.

4.97

419.74

W. ch. 60th St

S. line Gilcher Tract

T.P.

12.35

436.76

0.30

424.41

T.P.

12.99

449.41

0.34

436.42

T.P.

13.03

462.25

0.19

449.22

T.P.

8.49

470.69

0.05

462.20

chk. B.M. BP.

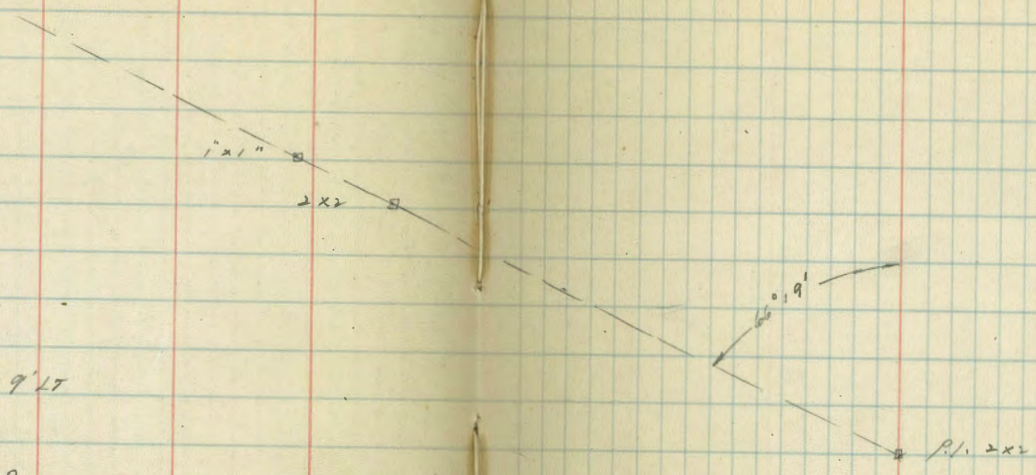
5.42

465.27

N.W. El Cajon

Gilcher

9+75.81 P.O.T.
9+43.01 = E.C.



$\Delta = 66.9' LT$
 $R = 300$
 $T = 196.0$
 $L = 3 \times 7.2$

7+91.78 = P.I.

5+95.78 = B.C. LT

5+79.98

4+65.78

3+46.15 = E.C.

±

2 x 2 B.C. LT.

2 x 2 P.O.T.

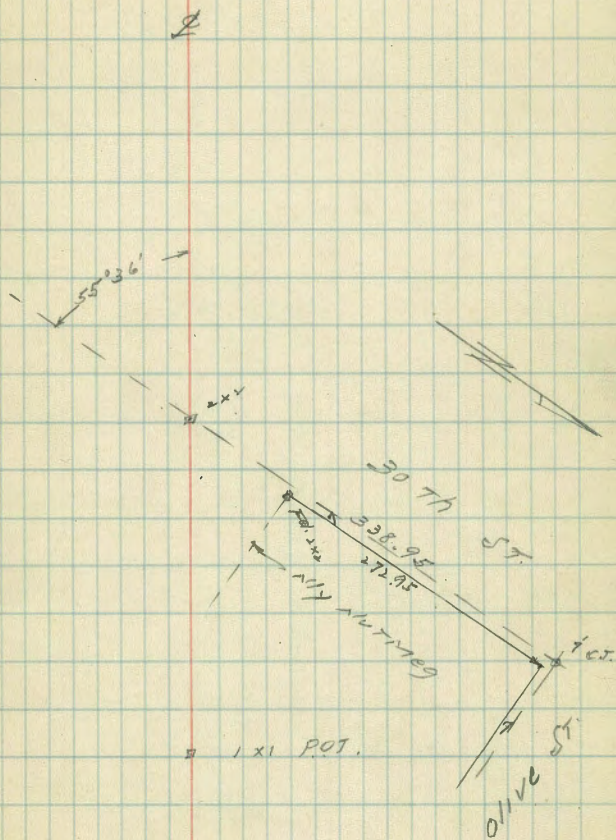
2 x 2 P.I.

2 x 2 E.C.

14 + 04.75 = Ely 7' Line of 30th from North

12 + 73.53

9 + 75.81



NUTMEG ST. EXT.
 & Levels on "B" Line

1 4° 20.8

+75

0+50 1° 57.0

0+30

0+08.95 B.C. RT

0+00 wly edge par.

0-10 = wly c6 32nd

SWBP 245 300.07

These Elevations seem to be 11.82L high
 Bench Mark should have been of San Marcos 285.795
 Checked by STS 11/5 Nov 21 - 38

32nd
 277.62 Kalmia
 285.795

292.1
 8.0

270.7
 9.4

291.7
 8.4

296.1
 4.0

297.1
 3.00 Hub

295.8
 2.5' par

295.4
 4.43 par

Change Elevations

300.07

4.750

4

3+4615 EL. 16° 06'

5 13° 58.8

TR. 5.10 295.44 9.71 290.36

2+50 11° 31.0

2+00 9° 07.3

1+50 6° 44.1

30007

2836
11.92063
9.72888
6.72443
4.2

29546

2887
6.42775
5.62934
5.7

30007

T.P. 3.12 261.36 12.83 258.24

5 + 95.78 B.C. LT

T.P. 0.37 271.07 12.31 270.70

5 + 79.98 P.O.T.

+ 57

+ 30

5

4 + 66

T.P. 0.14 283.01 12.59 282.87
295.46

~~R~~

268.07
3.00
+106

271.07

27531

970
Hub

274.7

8.3

270.9

12.1

268.1

14.9

284.8

1.2

283.01

+65 W edge creek

+45 E edge creek

+30

7 9°57.1

6+80 8°02.54

6+65

T.P. 1.95 250.76 12.55 248.81

6+36 3°50.44

261.36

234.08
10.2

234.76
10.0

237.56
13.2

236.76
14.8

237.96
12.8

239.06
11.7

250.76
249.86
11.5

261.36
2

outs on Right are hand level notes
apart of Elevation *all*

248.66
18.1

30 P
Creek

249.16
12.4

20.0	27.0	RR emb
41.4	71.3	
260.6	264.4	

+80

8 +50

24^o 10.6

T.P.

12.10

261.76

1.10

249.66

+28

+15

8

19^o 30.1

7 +94

7 +75

250.76

LT

261.76

232.96	233.06
17.8	17.7
5.5	1.2
Creek	
232.6	232.3

232.96	232.3
17.5	17.0
1.8	0.8
Creek	
232.6	232.3

232.96	232.3
16.8	11.7
1.5	
Creek	
232.6	232.3

232.96	232.3
16.6	7.5
1.4	
Creek	
232.6	232.3

232.96	232.3
12.6	8.2
1.2	
Creek	
232.6	232.3

60	170	350	480	RR Emb
781	173.1	124.5	120.5	
2472	2522	2636	262.6	

250.76

+37

11

T.P. 11.41 201.48 11.69 250.07

+50

10

+75

7 9 +43.01 EC 33° 09.5'

9 27° 03.10

201.76

22.0

237.38

$$\begin{array}{r} 400 \text{ below 2} \\ -39 \\ \hline 235.5 \end{array}$$

22.1

14.0	21.0	28.0 RR	40.0 RRomb
17.5	13.0	18.9	108
24.69	252.4	258.3	258.2

261.48

248.26

254.96

6.8

12.0 RR	22.0 RRomb
16.1	18.4
26.1	26.4

258.26

3.5

222.61

50.0
Creek

9.15

15.0 RR	22.0 RRomb
40.5 + 10.2	10.8
262.8	263.4

247.46

12.5

261.76

check back to BM			7.11	297.66	297.62
T.P.	819	304.77	0.39	296.58	<u>0.04</u>
T.P.	1215	296.97	0.01	284.84	
T.P.	1265	284.83	0.50	272.18	
T.P.	1280	272.48	1.80	259.68	

13+00

17 + 72.53 P.O.T. ON HUB

+50

+15

12

11+50

201.48

150.20
11.2

252.76
8.72

254.38
7.1

252.88
8.6

249.88
11.0

241.98
19.5

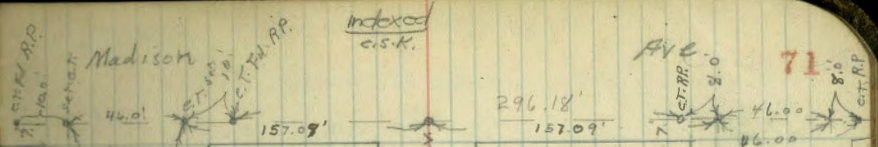
201.48

350	200	60	20
<u>-145</u>	<u>-81</u>	<u>+36</u>	<u>+20</u>
205	119	96	40

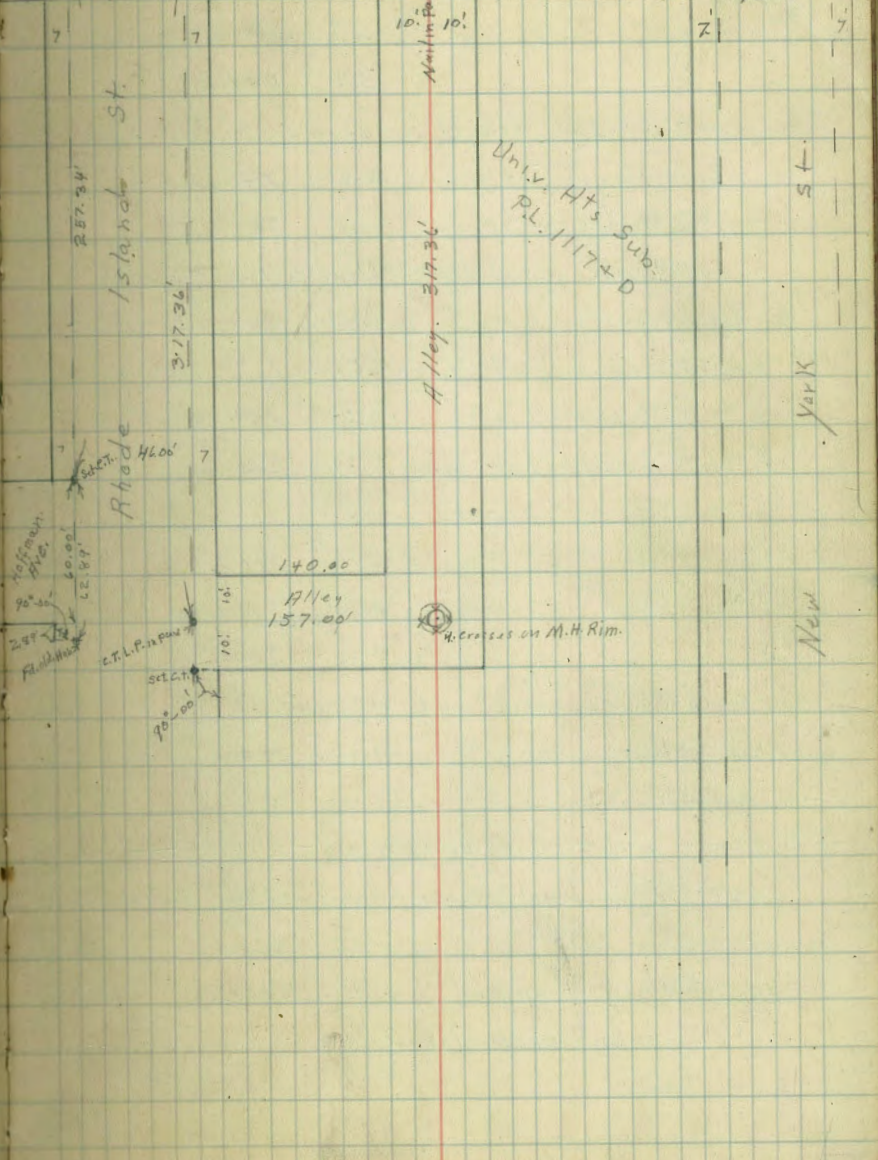
180	230	280	300
<u>-420</u>	<u>-215</u>	<u>+110</u>	<u>-170</u>
256.4	256.5	263.4	271.4

7-9-37
Miller
Walker
Bliss

X See Alley South of Madison Ave
Bet. New York St. + Rhode Island St
20' Wide.



B.M.	4.29	344.80	340.51	S.W. Madison + New York
14' N of S. line = S. ch. line Madison				
E-20	G. pav.	5.76	339.04	
E-20	Top. ch.	5.22	339.58	
E	" "	5.27	339.53	
E	G. pav	5.81	338.99	
Φ	" "	5.95	338.85	
W	" "	6.04	338.76	
W	Top. ch	5.43	339.37	
+20	" "	5.52	339.28	
+20	G. Pav	6.13	338.67	
0+00 = S. line Madison Ave				
W. curb + pav.		5.10	339.70	
Φ	"	5.31	339.49	
+ Pav	"	5.19	339.61	
E. on dirt. pav + ch. covered		3.5	341.30	
E. curb + pav. figured		4.98	339.82	
0+03.2				
E		3.5	341.30	
+2		3.9	340.9	
+5		5.0	339.8	
Φ		5.0	339.8	
+6		4.9	339.9	
+8		4.2	340.6	
W.				



344.80

0+25 S.

W	4.0	340.8
☿	3.7	341.1
♁	3.7	341.1

0+33 N. End double garage on E. ent. floor 3.0 Back

E - 3' = floor	3.70	341.10
E - 1.3 = W. edge ent. apron	3.85	340.95

0+44 ☿ garage on W. ent. floor 3.7 Back.

W - 3.7 = floor	3.87	340.93
-----------------	------	--------

0+49 = S. End. above garage on E.

E - 3' = floor	3.76	341.04
E - 1.3 = W. edge ent. apron	3.84	340.96

0+50

♁	3.7	341.1
☿	3.7	341.1
W	4.2	340.6

0+66 N. End ^{double} garage on E. ent. floor 3.0 Back.

0.4' in Alley = W. edge ent. apron	4.20	340.6
E - 3' = floor	3.85	340.95

T.P. — 4.76 — 345.26 — 4.30 — 340.50 —

0+77 = N. End. double garage on W. ent. floor 4.5' Back

W - 4.5 = floor	4.59	340.67
W - 3' = E. edge ent. apron	4.97	340.29

0+82 = S. End above garage on E

E - 3' = floor	4.64	340.62
0.4 in Alley = W. edge ent. apron	4.78	340.48

345.26

0+95 = S. End. above garage on W.

W - 4.5 = floor	4.63	340.63
W - 3' = E. edge ent. apron	4.95	340.31

1+00

W	5.4	339.9
☿	5.0	340.3
♁	4.8	340.5

1+25

♁	5.2	340.1
☿	5.1	340.2
W	5.5	339.8

1+50

W	6.1	339.2
☿	5.9	339.4
♁	6.0	339.3

1+75

♁	6.6	338.7
☿	6.3	339.0
W	7.1	338.2

2+00

W	7.9	337.4
☿	7.6	337.7
♁	7.6	337.7

2+20

♁	9.2	336.1
☿	9.2	336.1
W	9.0	336.3

72

T.P. 1.28 — 335.82 — 10.72 — 334.54

2+40

W	0.4	335.4
☉	0.7	335.1
E.	0.5	335.3

2+50

E	1.7	334.1
☉	1.5	334.3
W	2.0	333.8

2+75

W	3.2	332.6
☉	3.0	332.8
E	2.4	333.0

3+00³⁶ = N. Line E+W. Alley

E	4.8	331.0
☉	4.5	331.3
W	4.5	331.3

3+10³⁶ ☉ E+W. Alley

W	5.0	330.8
☉	Rim M.H.	4.97 330.85
E	5.4	330.4

3+20³⁶ = S. Line E+W. Alley

E	5.4	330.4
☉	5.4	330.4
W	5.4	330.4

E+W. Alley

0+00 = W. Line N+S. Alley

S.	5.4	330.4
☉	5.0	330.8
N	4.5	331.3

0+25 = W.

N	4.7	331.1
+4	4.7	331.1
☉	5.4	330.4
S	5.9	329.9

0+50 = W.

S	6.5	329.3
☉	5.9	329.9
N	5.4	330.4

0+75 = W

N	6.3	329.5
+5	6.3	329.5
☉	7.0	328.8

S	7.4	328.4
---	-----	-------

1+00 = W

S	8.4	327.4
☉	7.9	327.9
+7	7.3	328.5
N	6.4	329.4

1+20 W

N	7.7	328.1
E	8.7	327.1
S	9.1	326.7

1+40 W = E. Line Rhode Island St.

S. Top. cmt. at E. End	10.47	325.35
S. pav. E. edge	10.77	325.05
E " " "	10.52	325.30
N. " " "	9.80	326.02
N cmt. at " "	9.32	326.50

1+55 = E. of Line

N pav	10.09	325.73
E "	10.83	324.99
S "	11.47	324.35

T.P.	9.76	344.30	1.28	334.54
------	------	--------	------	--------

Orig B.M.		3.79	340.51
-----------	--	------	--------

Moore
10-1-37

Xsec of Hiley 20' wide
Blk 20 Ocean Beach
Bet. Coronado + Santa Cruz from Ebers to Froude

Indexed
C.R.K.

119.19

75

			MON. Santa Cruz + Ebers			
SW 7 CF				N	0+25	10.8 108.4
SW Mon	11.3	106.95	106.95	95.42	" "	+5 12.2 102.0
SE TOP FH				C		12.4 106.8
				+2		12.0 102.2
				+6		10.2 109.0
				S		9.9 109.3
					0+50	
				S		7.7 111.5
				+5		8.0 111.2
				+6		8.7 110.5
				C		8.8 110.2
				N		8.5 110.7
					0+62	
					-9.5 SW. 99. dirt floor	9.1 110.1 10' wide
				N		8.4 110.8
				C		7.6 111.6
				S		7.1 112.1
					1+00	
				S		5.0 114.2
				C		5.6 112.6
				N		5.4 113.8
					1+50	
				N		1.7 117.5
				C		1.6 117.6
				+8		1.0 118.2
				S		0.0 119.2
T.P.	12.64	119.19	0.40	106.58		

Buller

131.67

T.P.	13.08	131.67	0.60	118.59
	1+78			
- 10	W edge dls. gar. floor	10.40	121.27	
- 6	W " CONC. APRON	10.42	121.25	
S		11.0	120.7	
C		11.8	119.9	
N		12.7	119.0	

1+81

N E S, N. gar. dirt	10 wide	12.6	119.1	
	1+96			
N		10.8	120.9	
C		10.9	120.8	
S		10.4	121.3	
+ 6	Edge CONC APRON	10.44	121.23	
+ 10	" dls Gar floor	10.48	121.24	

2+25

S		8.9	122.8	
C		9.0	122.7	
N		9.9	121.8	

2+50

- S		7.9	123.8	
N		7.5	124.2	
C		6.5	125.2	
S		5.8	125.9	

2+75

S		0.6	131.1
C		2.5	129.2
N		3.5	128.2
+ 10		5.0	126.6
T.P.	12.75	144.00	0.42
			131.25

3+00

NORTH ENTRANCE DRIVE IN FROM SANTA CRUZ

- 10		10.1	130.9
N		11.5	132.5
C		11.1	132.9
+ 5		11.0	133.0
+ 4		10.7	133.8
N		9.5	134.5

3+25

S		4.0	141.0
+ 4		6.5	137.8
C		6.6	137.4
+ 5		5.7	138.3
N		7.5	136.5
+ 10		9.7	134.3

3+50

- 10		4.7	139.3
N		1.7	142.3
C		2.0	142.0

144.00

+6			1.2	142.8
S			0.1	143.9
T.P.	12.58	156.52	0.06	143.94
	3+90			
S			6.5	150.0
C			8.3	148.2
N			9.5	147.0
+10			11.6	144.9
	4+15			
-15	center wash		14.8	141.7
N			8.4	148.1
C			6.6	149.9
+2			6.0	149.9
S			3.9	152.6
	4+37			
-8			2.9	151.8
S			7.3	149.2
C			9.3	147.2
N			9.7	146.8
+10			10.4	146.1
	4+47			
-10			6.5	150.0
N			6.6	149.9
C			8.6	147.9
S	center wash		8.5	148.0
+10			5.9	150.6

156.52

77

				4+63
-8	center wash		7.2	149.3
S			4.5	152.0
C			4.1	152.4
+4			1.9	154.6
N			2.7	153.8
+10			2.7	153.8
T.P.	12.77	169.20	0.09	156.43
	4+75			
-5			12.4	156.8
N			11.4	157.8
+4			10.2	159.0
C			11.2	158.0
+2			11.1	158.1
S			15.5	153.7
+10			18.4	150.8
	5+00			
-10			14.0	155.2
S			8.8	160.4
+6			5.8	163.4
C			6.0	163.2
N			8.1	161.1
+5			9.2	160.0

170.69.2

5+25

- S	5.2	164.0
N	4.3	164.9
C	5.2	164.0
S	8.2	162.0
+ 10	10.0	159.2

5+50

- 10	6.5	162.7
S	4.1	163.1
C	4.1	165.1
N	2.5	166.7
+ 5	2.9	166.3

5+75

N	2.2	167.0
C	1.9	167.3
S	1.8	167.4

T.P.	5.30	173.24	1.26	167.94
------	------	--------	------	--------

5+99 W.L. Fraude

S	cb	3.49	169.75
S	par	4.13	169.11
C	"	5.22	168.02
N	"	5.94	167.30
N	cb	5.85	167.39

673.24

78

6+11 = W cb 1, NE Fraude

N	par	6.47	166.27
C	"	5.95	167.89
S	"	4.22	169.02

Note! No B.M. please check cb. Els. to profile

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 N to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in bold

IMPROVED TABLES
AND
INFORMATION

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of correction. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Tangents.

Given A, B, c; to find a, b, C.

Use Law of Sines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (E+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792
$\frac{13}{16}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844
$\frac{7}{8}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896
$\frac{15}{16}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.0000
	0	1	2	3	4	5	6	7	8	9	10	11

TABLE IV
USEFUL RELATIONS

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links
360°	= 21600'	= 1296000"
Radius	= arc of 57.2957790°	
Arc of 1° (radius = 1)	= .017453292	
Arc of 1' (radius = 1)	= .000290888	
Arc of 1" (radius = 1)	= .000004848	

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{\pi}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11½ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{\sum v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

Horizontal Distance = R - R sin² a + C cos a

Vertical Distance = R ½ sin 2 a + C sin a

R = Reading × $\frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

46
16
62

Randolph St Turn Lt
1875 5x Year

16.00
18.00

666
2.90
44.30
40.51
3.79

N 87-18 30 W
11 00-34 30
89 57 00

22 7
27.41
13.3

360
60
21600

13
21600
15 8
1020