

1519

FIELD BOOK

No. 385 F

MICROFILMED

DEC 24 1964

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

868
9909

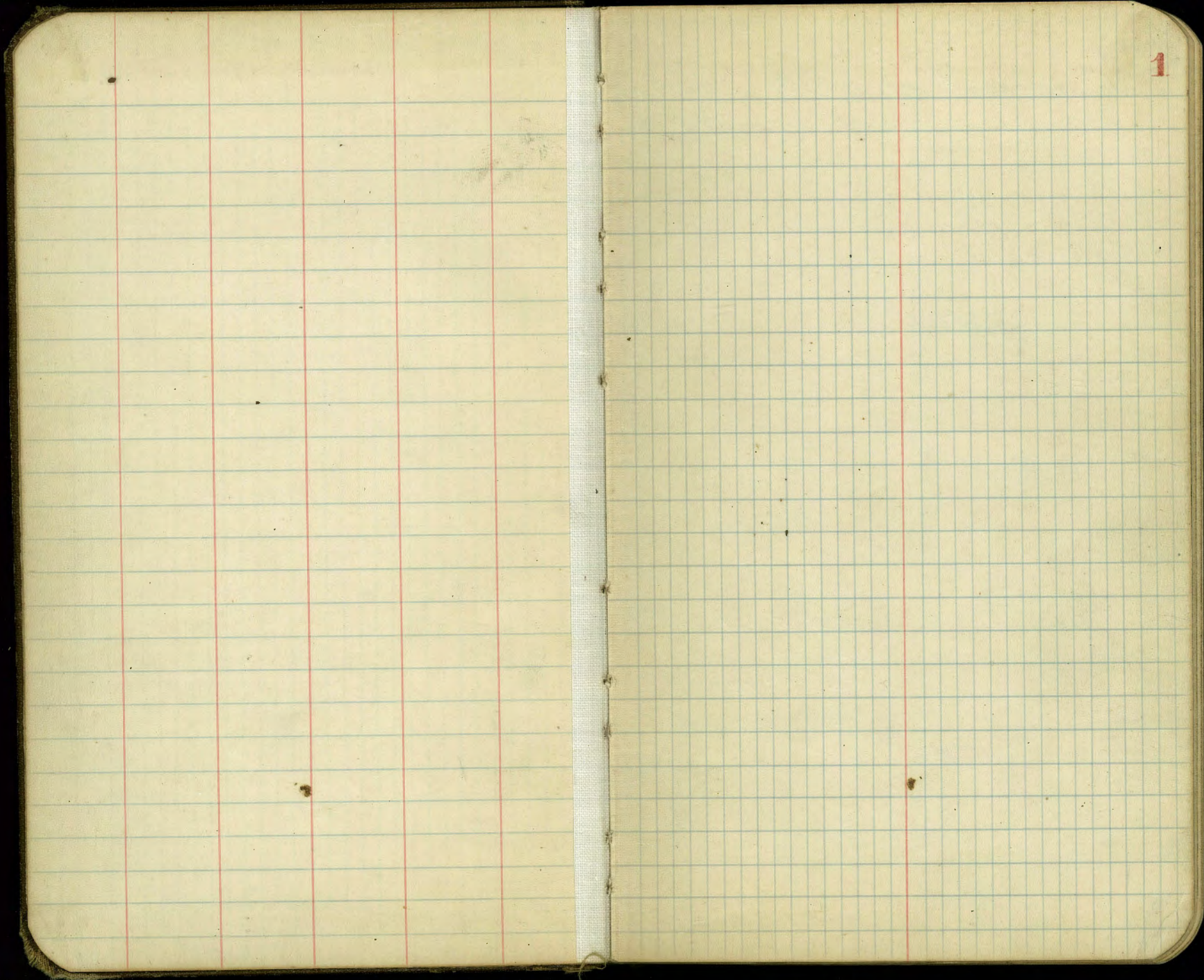
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1

S85°37'30"E ✓

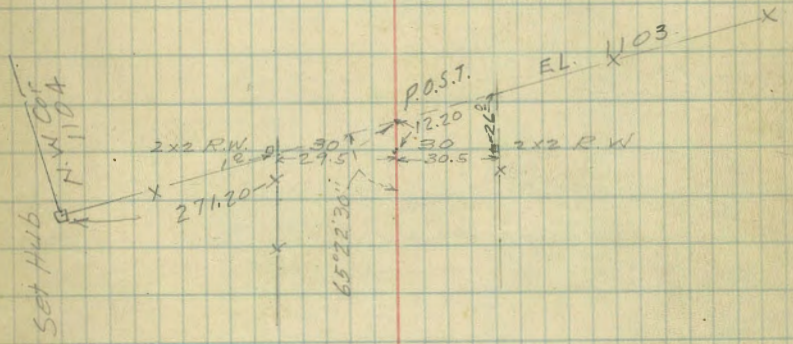
16+04⁸¹ E.C.

15+36¹⁴ Road corner (West line of 1103 & East line of 1104)

15+15²⁴ B.C.

$\Delta = 5^{\circ}05'30''$ Lt.
 $R = 1000$
 $T = 44.46$ ✓
 $L = 88.87$

212 R.W. of 30' 30' 212 R.W.
 EC



26+00

25+00

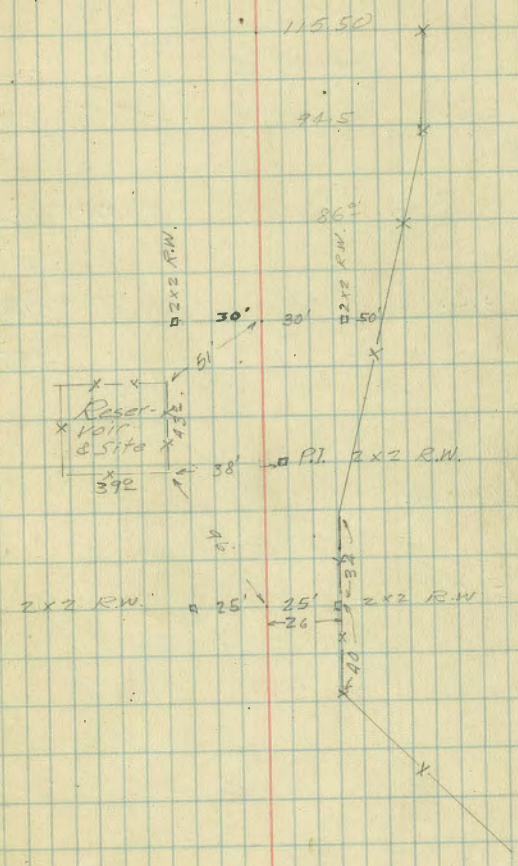
24+00

N80°57'30"E ✓

23+79.79 E.C.

22+15.99 B.C.

$\Delta = 13^\circ 25'$ L*
 $R = 700$
 $T = 82.33$ ✓
 $L = 163.91$



34+00

33+00

N72°12'E ✓

32+91⁸⁵ E.C.

2x2 R.W. 25' x 25' x 25'

32+00

Δ 15° 25' Rt.

R 500

31+57²⁵ B.C.

T 67.68 ✓

2x2 R.W. 38' x 28' x 17' to Fence

L 134.55

31+00

30+00

N56°47'E ✓

29+20⁶⁴ E.C.

2x2 R.W. 30' x 25' x 58' E.C.

29+00

28+00

27+09⁶⁸ B.C.

Δ = 74° 10' 30" Lt.

R = 500

T = 107.07 ✓

L = 210.96

2x2 R.W. 25' x 25' x 2x2 R.W. B.C.

52+00

51+00

50+00

49+00

48+00

47+00

46+00

45+26.03 E.C.

45+00

44+01.75 B.C

44+

43+

42+25.83

41+

40+

39+

38+00

37+00

36+00

35+00

N64°58'E ✓

Δ 7°14' Lt.

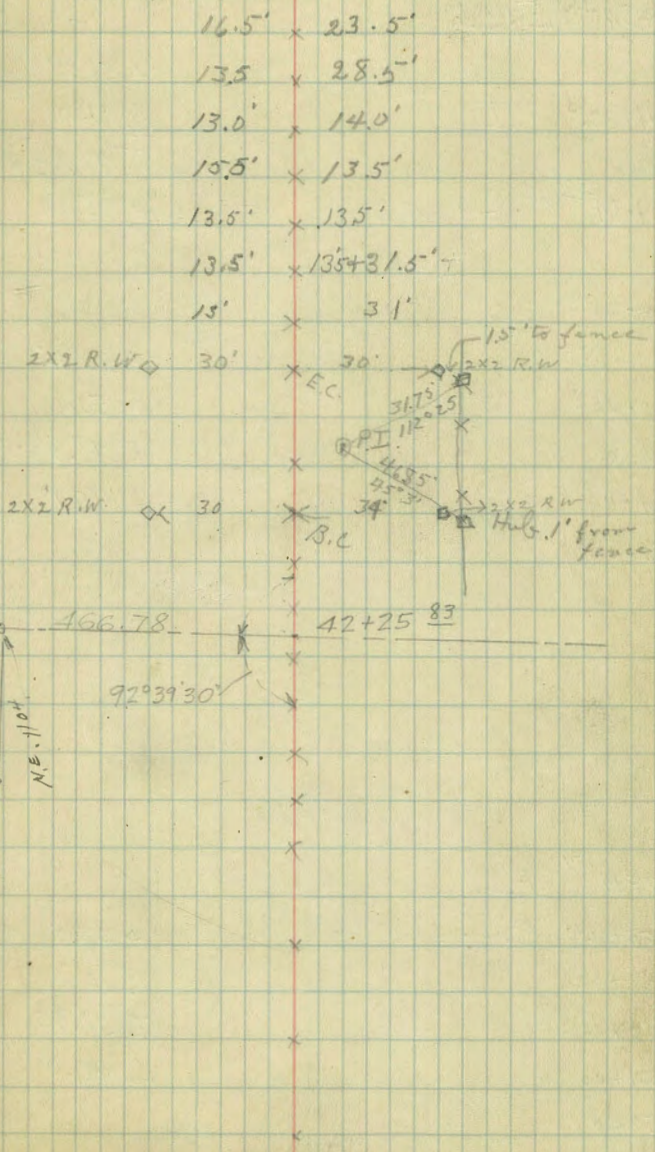
R. 1000

T. 6321 ✓

L 124.25

{ Road crosses East line 1104
+ West line 1105 }

NE 1104 Rd 4x4 in st. rd.



16.5' x 23.5'

13.5' x 28.5'

13.0' x 14.0'

10.5' x 13.5'

13.5' x 13.5'

13.5' x 135+31.5'

15' x 31'

2x2 R.W. 30'

E.C.

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

2x2 R.W. 30'

x

B.C.

x

x

x

x

x

x

x

x

x

x

x

x

466.78

42+25.83

92°39'30'

15' to fence

Hub 1' from fence

NE 1104

64+97²⁶ Road crosses line between lot 2 of Archie Norman
 64+80²⁴ E.C. & land of Earl Victor Rubin

64+32⁷³ P.I.

$\Delta 5^{\circ}30'$ Lt.

R 1000

T 48.03 ✓

63+84⁸⁰ B.C.

L 95.99

58917'E ✓

62+20⁷⁷ E.C.

11.7³⁰

61+25

$\Delta 22^{\circ}15'$ Rt.

60+26⁶⁶ B.C.

R 500.

T 98.34 ✓

60+00

L 194.17

59+00

58+00

N 68°28'E ✓

57+21⁵⁴ E.C. + 71.54

56+61⁴⁵ B.C. + 69.45

$\Delta 3^{\circ}30'$ Rt.

R 1000

T 30.55 ✓

56+00

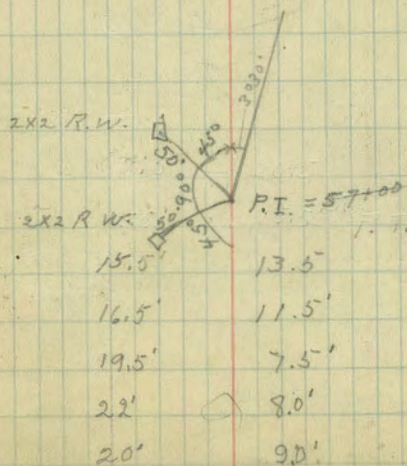
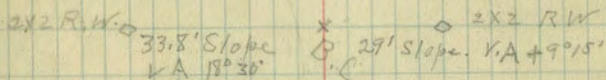
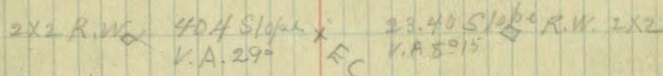
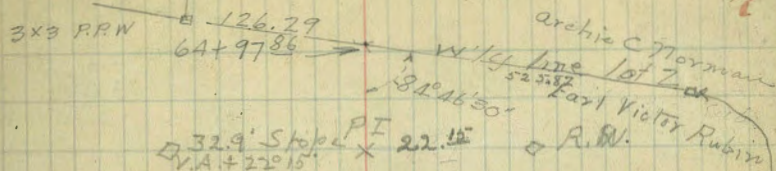
L 60.09

55+00

54+00

53+00

52+65



77+90⁵¹ Fence line on West Lot 3
See page 29 no Corada notes possible

77+00

76+00

75+00

74+00

73+00

72+58⁴⁵ Line between Lots 3+4 of E.W. Morse's
Page 34 Coordinates

72+00

S87°36'30"E ✓

71+23³⁴ E.C.

70+60⁸⁰ P.I.

Δ 790'30" R+

R. 1000

69+98¹¹ B.C.

T = 62.69 ✓

69+20³⁰

L = 125.23

69+00

68+00

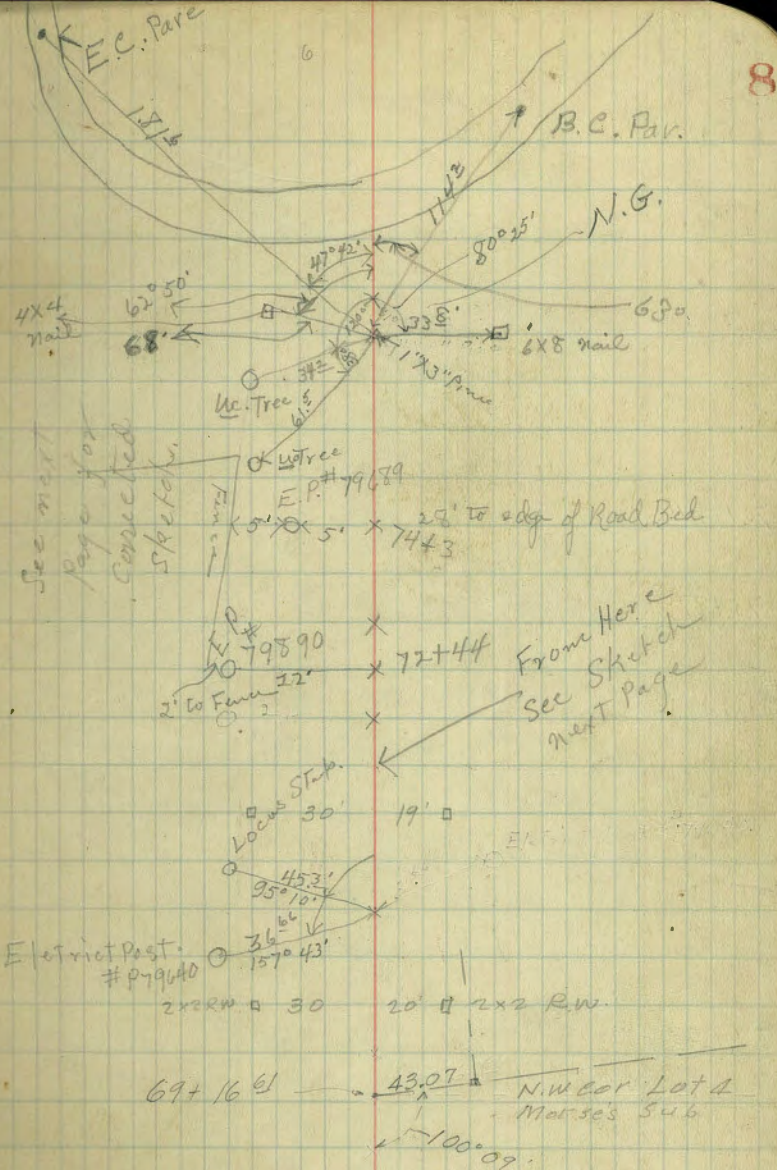
Line between Lot 4 + Morrison's Lot 2
for Coordinates see page 30 Plan page 23

67+00

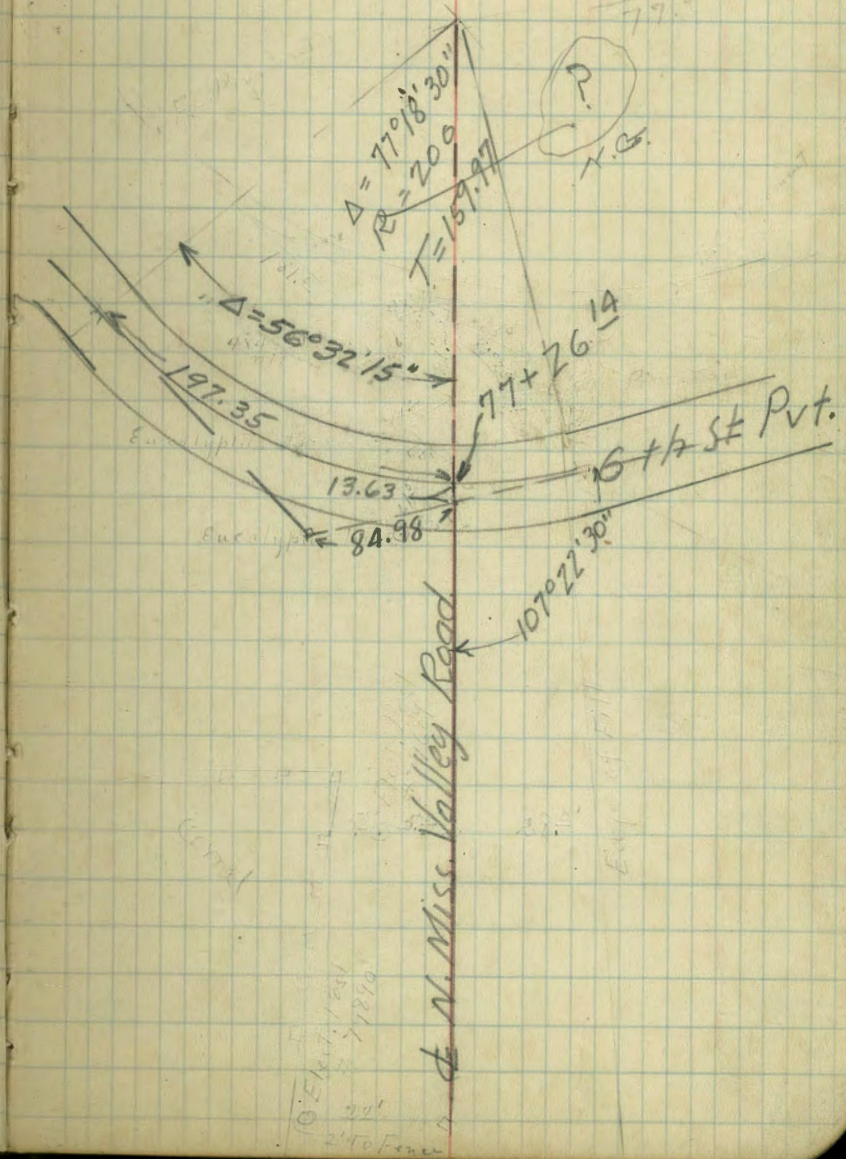
66+00

65+00

N85°13'E ✓



77.2611
 13.63
 $\hline 77.1251$
 68
 $\hline 77.5057$



O.E.K. 7/1/201
 7/18/10
 240 Feet

86+97⁸¹ L.

$$\Delta = 60^{\circ}29'45'' \text{ Rt.}$$

85+71³⁰ E.C.

$$\Delta = 36' 25'' \square 2 \times 2 \text{ R.W.}$$

$$\Delta = 32^{\circ}11'30'' \text{ Lt.}$$

$$R = 600$$

$$T = 173.14$$

$$L = 337.11$$

82+34²⁵ P.C.

$$2 \times 2 \text{ R.W.} \square 60 \quad 25 \quad \square 2 \times 2 \text{ R.W.}$$

82+00

81+06⁵⁶ line between Scripps + E.W. Mowen
Sub. Crown road

81+00

80+84⁰⁸ line between lots 34 + E.W. Mowen
Sub + Scripps

80+00

79+23⁴⁹ E.C.

79+00 (See P. 9) $\Delta = 56^{\circ}32'15'' \text{ Rt.}$

$$R = 200$$

78+00

$$L = 197.35$$

77+26¹⁴ P.O.C.

Lt. & Curve Rt.

98+00

97+00

$$\Delta = 63^{\circ}04'30'' \text{ Lt.}$$

$$R = 500$$

$$T = 306.85$$

$$L = 550.44$$

96+00

95+19.75 BC

95+00

94+00

93+00

92+00

91+00

90+00

89+00

88+00

87+00

PI. 2x2 R.W.

50 25' 2x2 R.W.

$$\begin{array}{r}
 95 + 19.75 \\
 - 306.85 \\
 \hline
 9832.60
 \end{array}$$

109+00

108+00

107+00

+31° L

 $\Delta = 6^{\circ} 26' \text{ Rt.}$

New Fence

+90°

23' 2x2 R.W.

106+00

105+00

 $6^{\circ} 26' \text{ Rt.}$

104+00

103+00

102+00

101+00

100+70⁹ E.C.100+00⁵⁰

100+06

{ Road crosses into Alfa Grants
from Haggards Land

99+00

$$\begin{array}{r} 100 \text{ } ^{21} \\ 100 \text{ } ^{70} \\ \hline 101 \end{array}$$

45°40'

30' 25' 2x2 R.W.

an continues through to Sta 129+70²⁶
Coordinates Page

$$\Delta = 22^{\circ}53' \text{ Rt}$$

$$R = 700$$

118+40²³ B.C.

$$T = 141.67$$

118

$$L = 279.87$$

117

116

115

114+16¹³ E.C.

11

114

113

2x2 R.W

P.I. \rightarrow \square

or bank in ditch

112

$$\Delta = 57^{\circ}44'30'' \text{ Rt}$$

111

$$R = 350$$

$$T = 192.98$$

110+63⁴¹ B.C.

$$L = 352.72$$

110+00

128

127+28¹⁶ E.C.

127

126

125

$$\Delta = 38^{\circ}45'30'' \text{ Lt.}$$

124

$$R = 500$$

$$T = 175.87$$

123+89⁹³ B.C.

$$L = 338.23$$

123

122

121+20¹⁰ E.C.

12

121

2x2 R.W. P.I. □

120

119

140

139

138

137

136+48⁴⁰ L.

$\Delta = 1^{\circ}56''$ Lt.

136

135

134

133

132

131

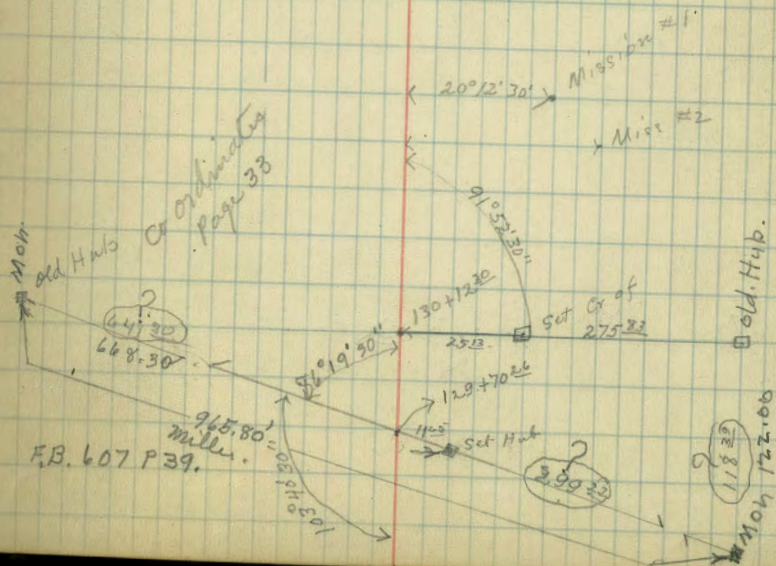
130+12³⁰

130

129+70²⁶

129

Crossed line between {
 alpha grant + mable
 Eckhart center line
 # 1173



CH 130
 299.20
 940.52
 965.50
 55.28

149+90¹⁵ E.C.

149 $\Delta = 8^{\circ}30'30''$ RT

$R = 1000$

148+41⁶⁵ B.C.

$T = 74.38$

147+37²²

$L = 148.50$

148

147

146

145+02⁵⁷ E.C.

145

144
143+50⁹

143

$\Delta = 27^{\circ}17'15''$ Lt.

142

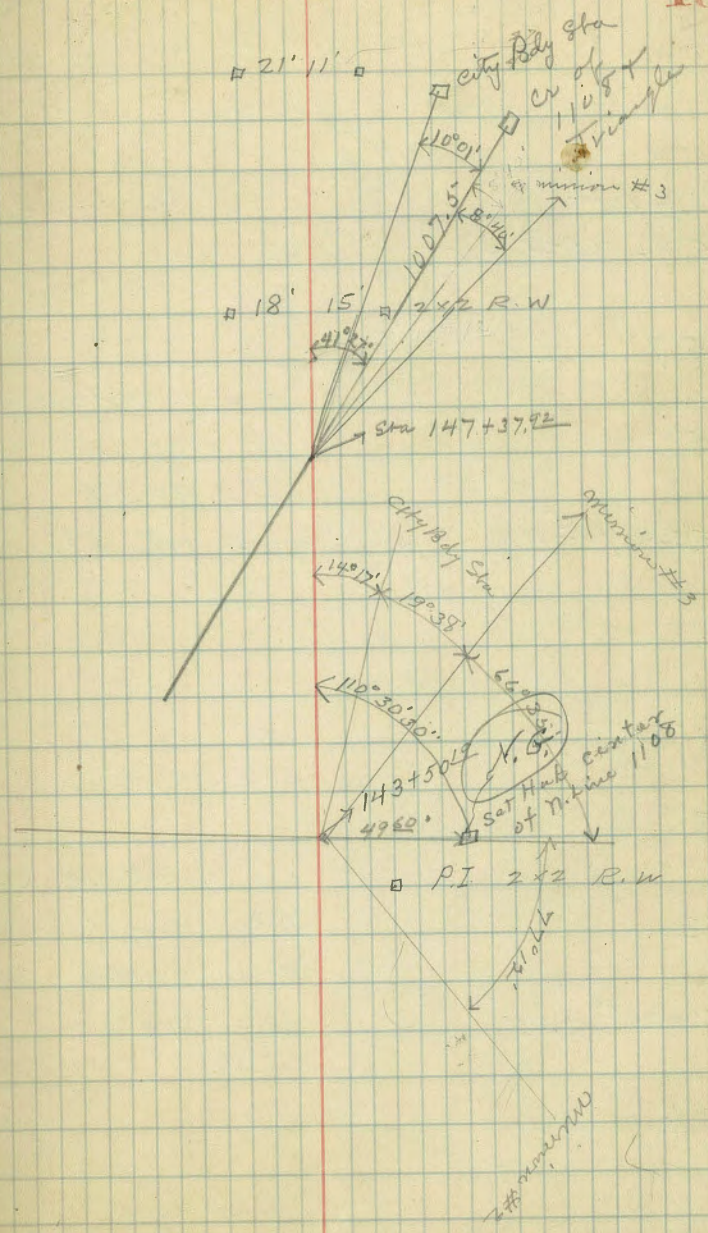
$R = 700$

$T = 169.95$

141+69²¹ B.C.

$L = 333.38$

141



169

168

167

166

165

164+23⁴⁰ E.C.

164

$$\Delta = 9^{\circ}40'45'' \text{ Rt}$$

163

$$R = 1000$$

$$T = 84.66$$

162+54⁴¹ B.C.

$$L = 168.93$$

162

161

160

159+94⁹⁶ L.

$$\Delta = 5^{\circ}53'30'' \text{ Rt}$$

□ 14' 16' □

□ 15 15 □ 2x2

2x2 □ 155
□ 157

177+04⁹² E.C.

177

176

$$\Delta = 27^{\circ} 11' \text{ Lt.}$$

$$R = 500$$

175

$$T = 170.85$$

$$L = 237.23$$

174+67⁶⁹ B.C.

174

173

172

171+34⁹⁶ E.C.

171

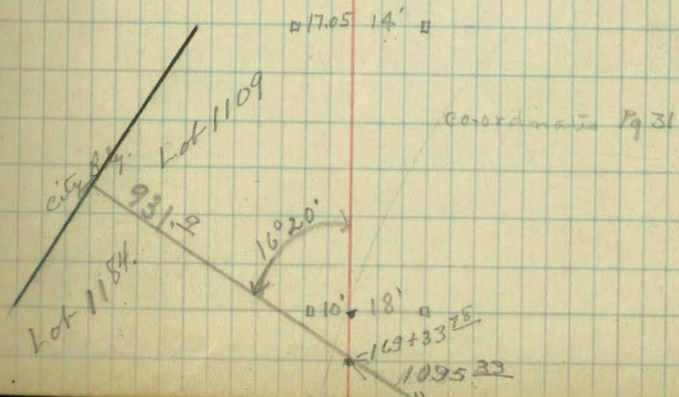
$$\Delta = 7^{\circ} 56' 45'' \text{ Lt.}$$

$$R = 1000$$

170

$$T = 69.44$$

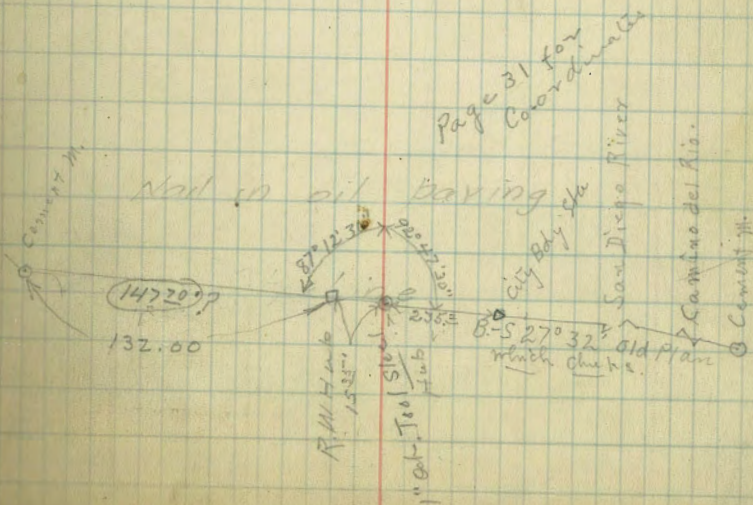
$$L = 138.68$$

169+96²⁸ B.C.169+33²⁸

17849.26

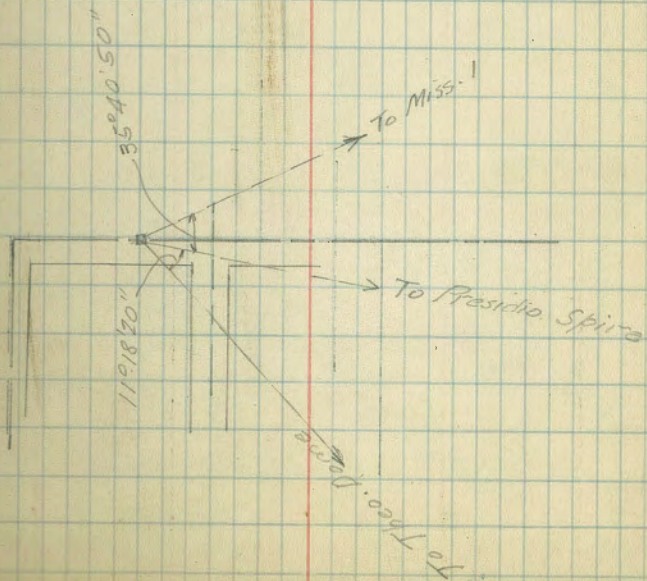
17774.44

City Line

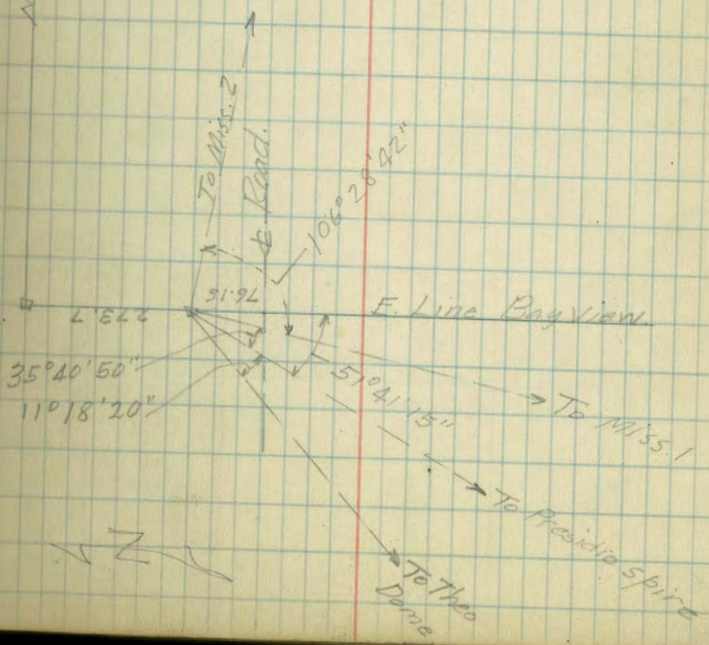
17849.26
17774.44
74.821 x 7.70 132
15.35
147.35

76 15
273 7
349 85

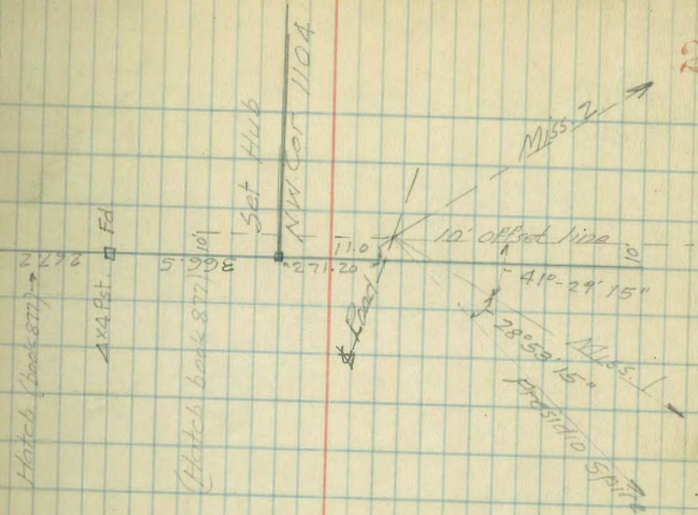
51-41-15

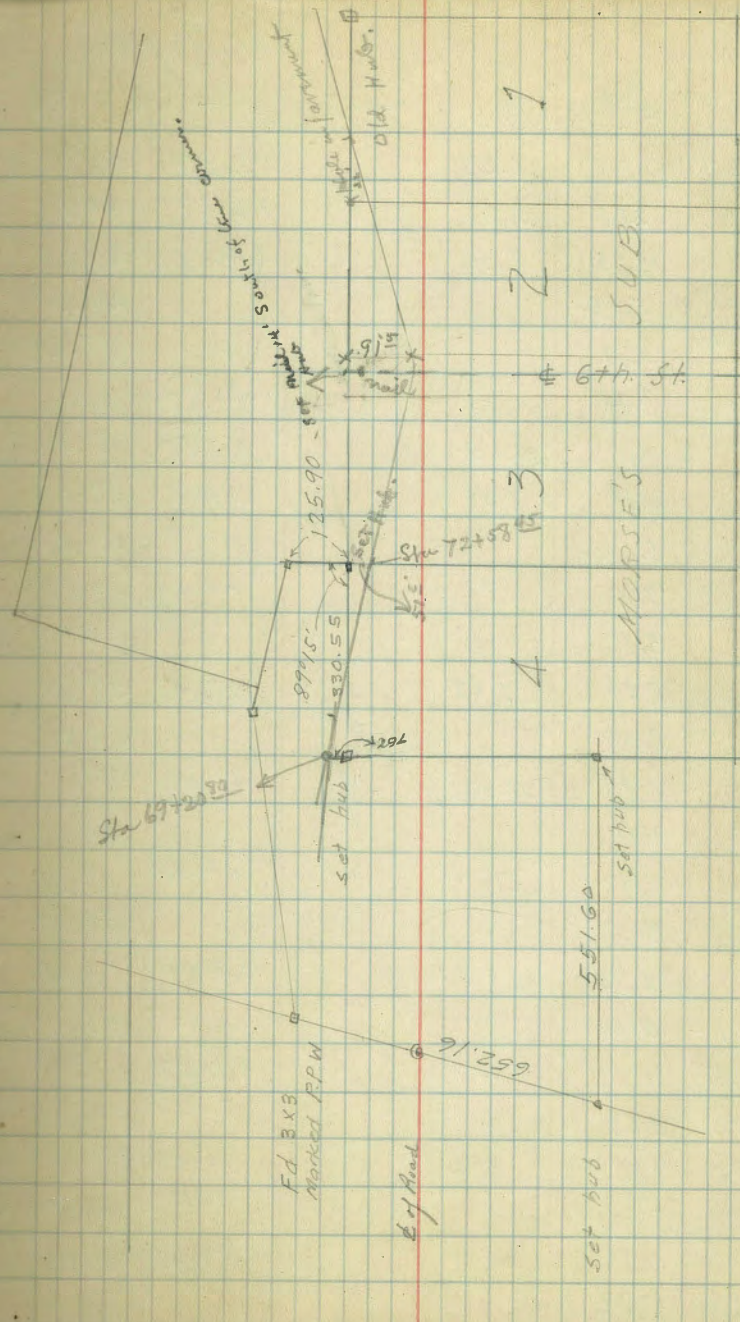
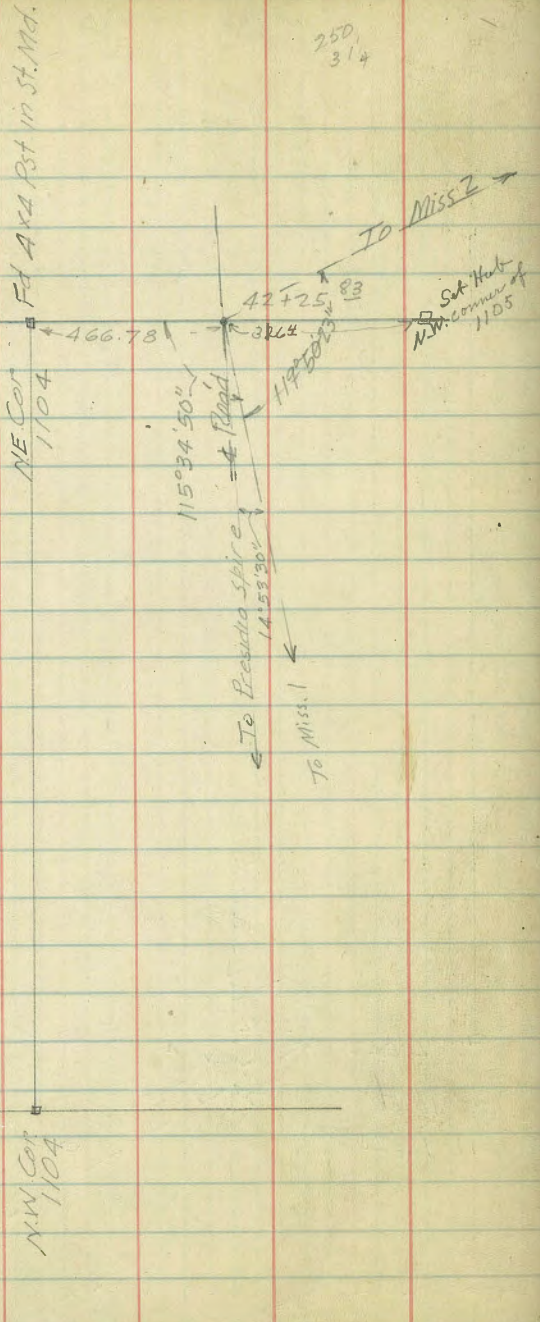


NL PL 1103



NE Cor 1103





Sta.	F.S.	B.S.	Diff.	H.I.	Elv.
B.M. = EC		0.23		52.47	52.24
B.C.	12.98	2.88		42.37	39.49
P.T.	12.93	2.56		32.00	29.44
77+12 ⁵¹	5.65				26.35
76+87+1	4.71				27.29
67+50	3.21	11.95		40.84	28.79
64+97 ⁵⁸	1.01	13.65		53.48	39.83
64+90	0.10	8.31		61.62	53.39
64+34	5.02				55.67
57+16	7.92	6.73		60.50	53.77
54+06	5.16				55.34
48+96	5.91	7.88		62.47	54.59
45+26 ⁰³	5.07				57.40
39+25	11.88	10.43		61.02	50.59
34+35	5.11				55.91
32+91 ⁸⁵	0.03	3.06		64.05	60.99
28+30	5.08				59.97
26+60	12.76	1.80		53.09	51.29
23+79.2	5.08				48.01
18+95	11.36	0.94		42.67	41.73
15+90	5.29				36.38
10+80	9.46	6.72		39.93	33.21
6+80	5.07				34.88
5+30	0.18	10.71		50.46	39.75
3+30	5.06				45.40

x E.C. on Camp/Heazley Road
 x B.C. " "

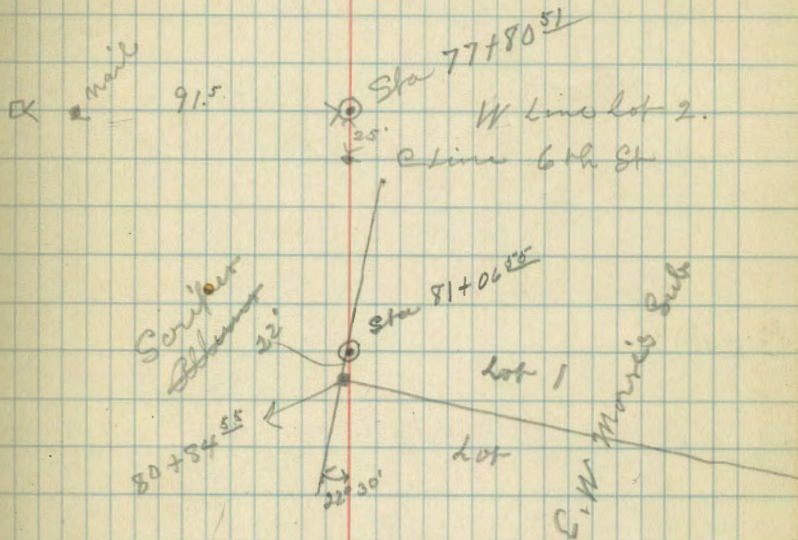
Sta	F.S.	B.S.	Diff	H.I.	Elv.
3+30	5.06			50.46	45.40
1+30	0.42	7.44		57.48	50.04
0+00	5.27				52.21
B.M.	1.01				56.47
B.M.	1.08				56.40
B.M.	0.0	0.01		52.25	52.24
86+97E	13.31	0.55		39.49	38.94
89+25	5.10				34.39
96+50	0.42	13.21		52.28	39.07
100+40	5.02				47.26
102+05	0.03	4.55		56.80	52.25
105+35	5.04	6.45		58.70	51.76
108+45	6.05	3.05		55.70	52.65
111+51	3.05	5.05		57.70	52.65
114+70	5.05	6.07		58.72	52.65
117+80	6.07	4.30		56.95	52.65
119+00	1.75	6.07		61.27	55.20
120+90	4.58	7.94		64.73	56.79
124+97	5.02				59.71
126+47	9.70	4.50		59.53	55.03
134+47	5.02				54.51
144+17	9.35	3.15		58.33	50.18

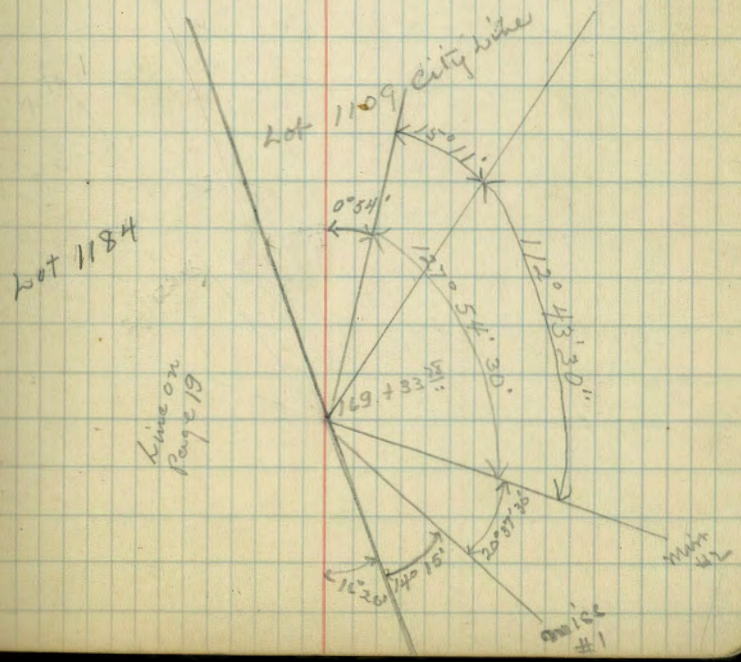
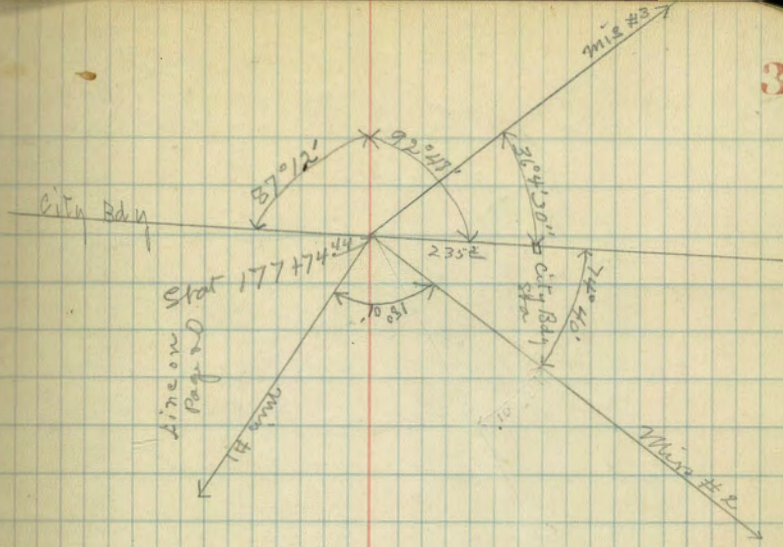
R. Wood Hub 25' to Right of $\frac{1}{2}$ of Road at 0+00
 Highest point on Water Meter box 5' R. of
 above R. Wood Hub.

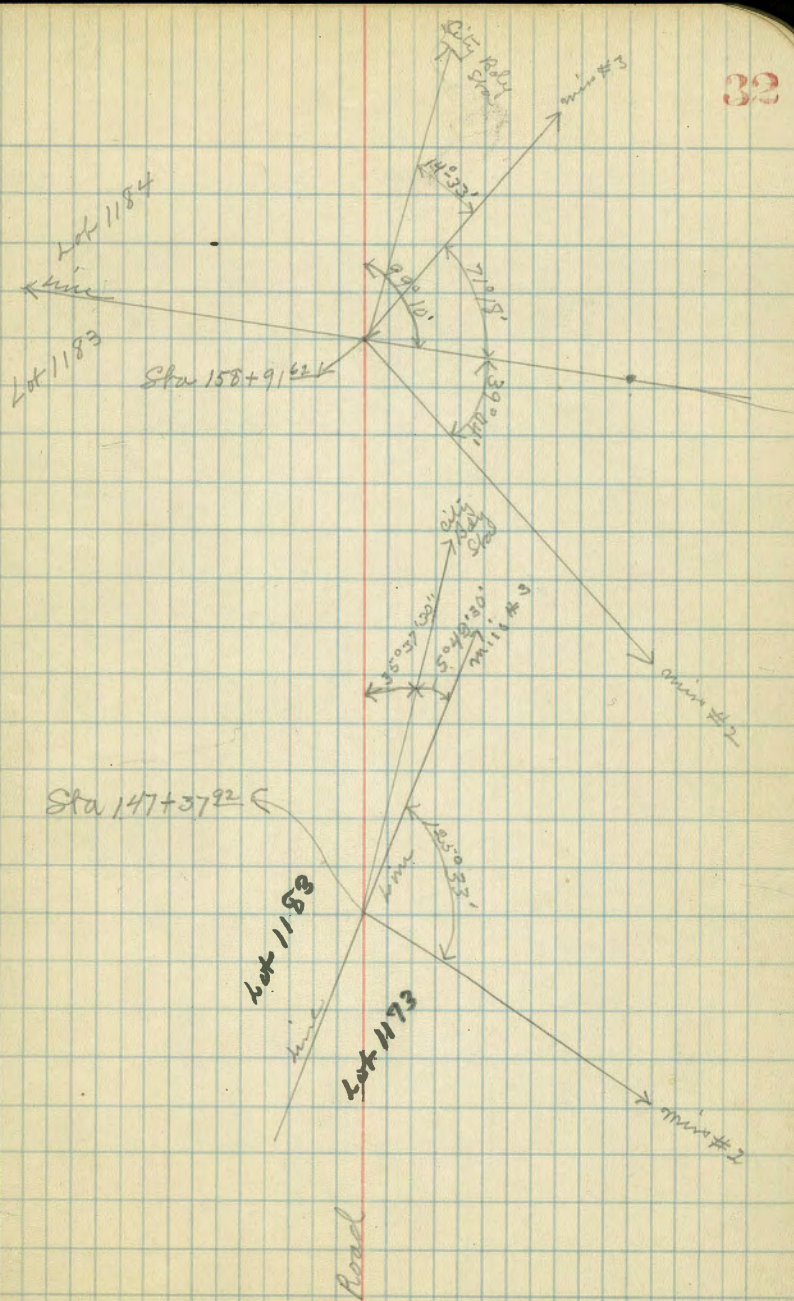
Lead plug on $\frac{1}{2}$ at E.C. on
 Caprip heading road. Just beyond
 Murphy's cartway Road

Sta	F.S	B.S	Diff	HI	Elv
144+17	9.35	3.15		53.33	50.18
148+41 ⁶⁵	5.06				48.27
160+87	0.07	5.53		58.79	53.26
164+23 ⁴	5.01				53.78
167+45	0.06	11.03		69.76	58.73
169+55	4.98				64.78
171+05	0.01	9.97		79.72	69.75
175+40	5.12				74.60
176+50	0.45	6.17		85.44	79.27
177+45	5.06				80.39
177+74 ⁴⁴	4.44				81.00
B.M.	2.24				83.20

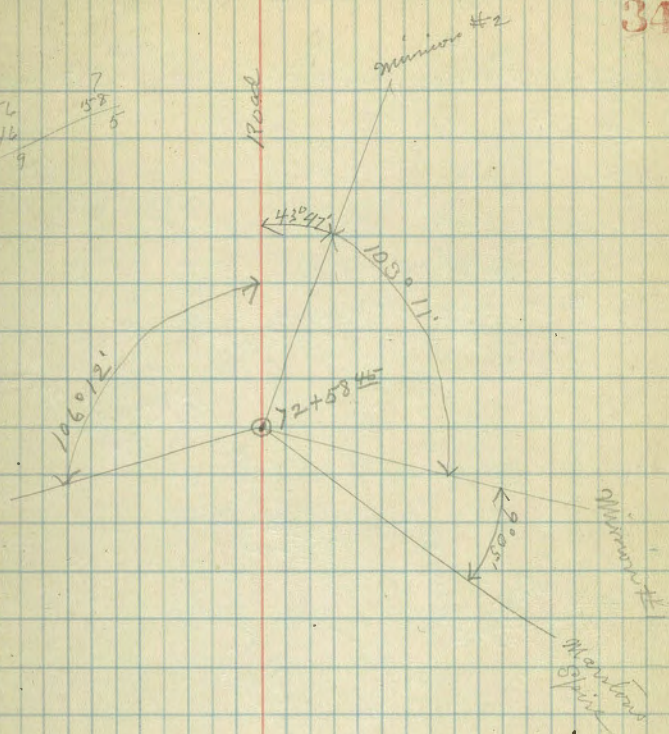
Cr of Fence to the right
on stone end of ditch with Black mark







$$\begin{array}{r} 156 \\ 146 \\ \hline 9 \end{array} \quad \begin{array}{r} 7 \\ 58 \\ \hline 5 \end{array}$$

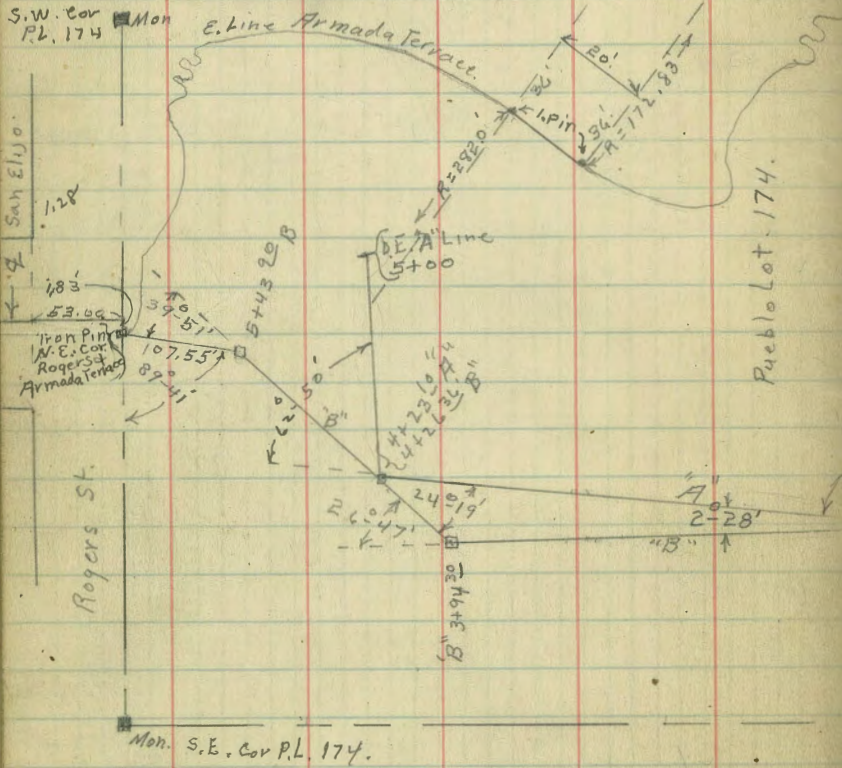


Indexed
c.s.K.

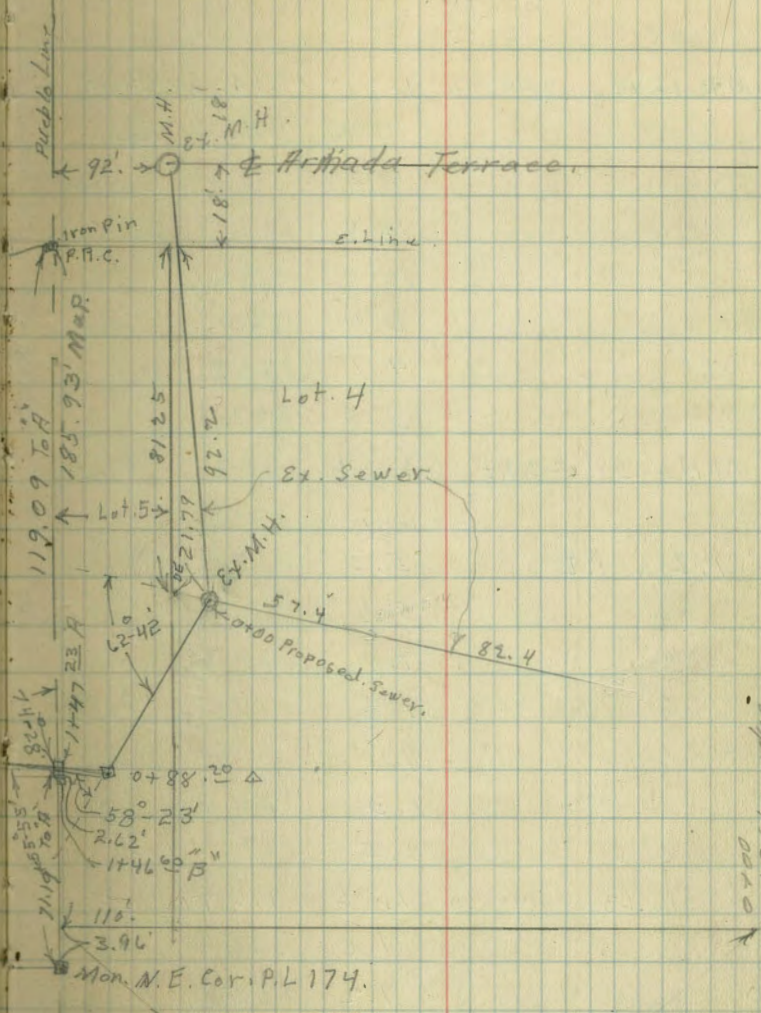
In. P.L.s. 175 & 174.

Survey Proposed Sewer 6-13-35
Miller,
Walker,
Bliss.

B.M. R.P. Hab. S. Line Rogers. St. 40' W.				
of W. Line San Elijo. St.	157.63			Grade Book 121. S. E. Roseman Equal to
B.M. B.P.	216	63.96	61.80	
T.P.	1.39	52.75	12.60	51.36
T.P. N.E. Cor. ch. Inlet W. ch.	5.31	47.24		Rogers. St



Mon. N.W. Cor. P.L. 174
E. 75.00 18° 20'
W. 100 13° 57' +22.04'



"11"
A. line Levels on Proposed Sewer
in Pueblo Lot 174.

0+00	8.17	13.80	128.63	114.83	Fl. MH
0+00				9.55	119.08 Top 44
0+00				9.8	118.8 Ground
0+04				12.4	116.2 "
0+18				10.0	118.6 "
+43				6.1	122.5
+50				4.7	123.9
0+75				5.9	122.7
0+88 ²⁰	M.H. $\angle 58^{\circ} 23' RT$			8.24	120.39 Hub.
1+00				6.8	121.8
1+47 ²³	P. Line P.I.			5.3	123.3
1+75				5.6	123.0
2+00				2.8	120.8
2+15				9.6	119.0
2+33				9.8	118.8
2+50				8.3	120.3
2+80				1.5	127.1
T.P.	13.23	140.00	1.86	126.77	
3+00				11.6	128.4
3+20				9.2	130.8
3+50				8.8	131.2
3+79 ²⁴				10.17	129.83 sTub
4+00				12.1	127.9
4+23 ¹⁰	= 4+24 ³⁶ "	$\beta 262-56' RT$	16.8	123.2	
4+50				128.0	
4+75				131.2	
5+00	D.E. Bottom gully			123.0	

B. line
128.63

36

0+88 ²⁰	M.H. $\angle 55-55' RT$			8.24	120.39	Hub.
1+00				7.0	121.6	
1+46 ⁶⁰	P. line P.I.			6.0	122.6	
1+75				6.8	121.8	
2+00				9.5	119.1	
2+15				11.0	117.6	
2+33				11.6	117.0	
2+50				10.7	117.9	
2+80				3.9	124.7	
T.P.	13.23	140.00	1.86	126.77		
3+00				13.8	126.2	
3+28 ²⁰	P.O.T.			11.57	128.43	Hub
3+35				11.3	128.7	
3+72				13.7	126.3	
3+94 ³⁰	M.H. $\angle 26-47' RT$			17.0	123.0	
4+26 ³⁶	= 4+23 ¹⁰ " A			16.8	123.2	
T.P.	4.33	131.84	12.49	127.51		
4+60				13.0	118.8	
4+72				19.5	113.3	
4+82				24.0	107.8	
5+07				1.8	130.0	
T.P.	12.71	143.77	0.78	131.06		
5+19				7.0	136.8	
5+43 ²⁰	L			2.06	135.71	Hub.
T.P.	13.01	156.67	0.17	143.60		
T.P.	6.55	159.65	3.51	153.10		

over.

159.65

37

B.M. R.P. Hub. S. Side Rogers. ✓
40' W. of W. Line San Elijo. 2.02 157.63 G.B. K121

S. Line Rogers. N. of San Elijo 3.86 / 155.79

S. " " E. " " " 4.90 / 154.75

T.P. 0.08 146.98 12.75 146.90

T.P. 0.27 134.65 12.60 134.38

Top. M.H. 0+00 15.57 119.08 ✓

Xsec of Talbot St.
Leroy to Bangor

Moore
Sisson
Northrup
9/4/35

indexed
c.s.K.

Pueblo line

page 40 for levels

1+00

$\frac{79.3}{9.0}$	$\frac{80.1}{8.2}$	$\frac{82.1}{6.2}$	$\frac{80.1}{8.2}$	$\frac{78.5}{1.2}$	$\frac{81.6}{1.6}$	$\frac{82.0}{2.5}$
26.4	5	1	8.2	1.2	1.6	2.5

0+75

$\frac{80.2}{8.1}$	$\frac{78.2}{9.6}$	$\frac{78.2}{9.1}$	$\frac{84.2}{8.1}$	$\frac{77.8}{10.5}$	$\frac{80.3}{5.0}$	$\frac{76.6}{11.7}$
26.4	20	10	8.1	1.2	1.7	2.4

0+50

$\frac{78.1}{10.2}$	$\frac{78.2}{10.1}$	$\frac{77.3}{11.0}$	$\frac{78.0}{9.3}$	$\frac{76.9}{11.4}$	$\frac{78.3}{10.0}$
26.4	20	10	9.3	1.2	2.4

0+25

$\frac{77.3}{11.0}$	$\frac{76.4}{11.9}$	$\frac{76.9}{11.4}$	$\frac{77.3}{11.0}$	$\frac{76.1}{12.2}$
26.4	11.9	10	1.5	2.4

T.P. 11.77 8831 0.18 76.54

$\frac{88.31}{7}$

0+00 end of paving on 701607

$\frac{76.5}{0.20}$	$\frac{75.81}{1.21}$	$\frac{74.75}{1.97}$	$\frac{74.65}{2.07}$	$\frac{75.32}{1.40}$	$\frac{75.39}{1.33}$
25 curb	25 gut. pav.	25 pav.	15 gut	15 cb.	25 Top Com. hand wall

0-35 = w/ cb line Leroy St.

$\frac{74.13}{2.59}$	$\frac{73.21}{3.51}$	$\frac{72.61}{2.11}$	$\frac{73.45}{2.27}$
25 curb	25 gutter pav.	25 pav.	25 pav.

T.P. 12.19 76.72 0.27 64.53

$\frac{76.72}{7}$

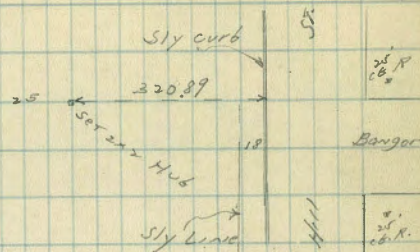
xxw/BP 1303 64.80 57.77 Evergreen 701607

Talbot St.
Leroy to Bangor

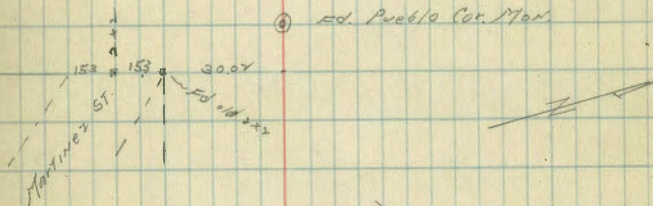
Pueblo Line

39

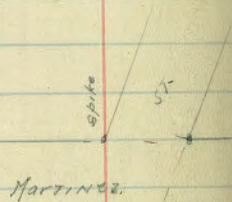
11+48.14 Wly Bangor in Roseville Hrs.



10+50.84
10+20.84 Fly Bangor in Golden Park



5+09.11
4+71.20
Martinez

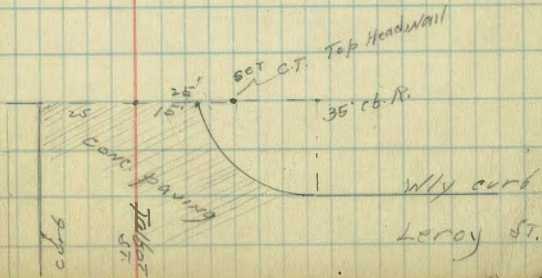


Ed. Pueblo Cor. Mon.
113.25
Ed. old spike
26.4
25
Set 1021
W'1
Set RP 200
Line for Cur
1/2" 1 P. 20

1+29.60

Pueblo for Mon. OUT 70 25' SET 1" STUB

0+00



2+50

$\frac{91.8}{4.0}$	$\frac{91.8}{4.6}$	$\frac{88.6}{7.4}$	$\frac{88.1}{7.7}$	$\frac{89.1}{6.7}$	$\frac{85.8}{10.0}$	$\frac{85.7}{10.1}$	$\frac{88.0}{7.8}$	$\frac{85.7}{10.1}$	$\frac{88.8}{7.0}$
$\frac{22.4}{18}$	$\frac{18}{18}$	$\frac{18}{18}$	$\frac{18}{18}$	$\frac{18}{9}$	$\frac{18}{10}$	$\frac{18}{15}$	$\frac{18}{24}$	$\frac{18}{28}$	$\frac{18}{29}$

2+25

$\frac{91.5}{4.3}$	$\frac{90.2}{5.1}$	$\frac{89.2}{8.6}$	$\frac{85.5}{10.0}$	$\frac{86.2}{9.6}$	$\frac{84.5}{11.3}$	$\frac{84.1}{11.7}$	$\frac{84.7}{11.1}$	$\frac{87.8}{8.0}$
$\frac{26.4}{21}$	$\frac{23}{21}$	$\frac{21}{21}$	$\frac{21}{21}$	$\frac{21}{10}$	$\frac{21}{15}$	$\frac{21}{24}$	$\frac{21}{25}$	$\frac{21}{30}$

2+17

12" Conv. pipe draw over Ft. ^{0.625} Rod
 from Runway made Rod
 -17%

2+00

$\frac{84.4}{9.4}$	$\frac{84.5}{11.3}$	$\frac{84.3}{11.5}$	$\frac{83.9}{11.9}$	$\frac{84.2}{11.6}$	$\frac{86.8}{9.0}$
$\frac{26.4}{15}$	$\frac{15}{15}$	$\frac{15}{15}$	$\frac{15}{15}$	$\frac{15}{24}$	$\frac{15}{24}$

1+75

$\frac{84.7}{11.6}$	$\frac{83.8}{12.0}$	$\frac{83.3}{12.5}$	$\frac{82.7}{13.1}$	$\frac{82.2}{12.1}$	$\frac{85.7}{10.1}$	$\frac{86.8}{10.0}$
$\frac{26.4}{18}$	$\frac{18}{18}$	$\frac{18}{18}$	$\frac{18}{15}$	$\frac{18}{22}$	$\frac{18}{23}$	$\frac{18}{25}$

1+50

$\frac{82.0}{13.8}$	$\frac{82.6}{13.2}$	$\frac{82.5}{13.0}$	$\frac{81.1}{14.7}$	$\frac{82.4}{13.4}$
$\frac{26.4}{15}$	$\frac{15}{15}$	$\frac{15}{15}$	$\frac{15}{24}$	$\frac{15}{25}$

J.P. ^{Hub 26} 1+29.60 12.66 95.81 5.16 83.15

95.81

1+29.60 = Pueblo line to South

$\frac{89.2}{9.1}$	$\frac{81.5}{6.8}$	$\frac{81.3}{7.0}$	$\frac{81.9}{6.4}$	$\frac{80.3}{8.0}$	$\frac{80.8}{7.5}$	$\frac{83.15}{5.16}$
$\frac{26.4}{10}$	$\frac{10}{10}$	$\frac{10}{10}$	$\frac{10}{7}$	$\frac{10}{10}$	$\frac{10}{13}$	$\frac{15}{15}$

88.31

88.31

3+75

$\frac{105.2}{2.7}$	$\frac{100.3}{7.5}$	$\frac{95.4}{10.4}$	$\frac{92.2}{11.4}$	$\frac{91.4}{17.0}$	$\frac{90.9}{17.5}$	$\frac{96.2}{11.7}$
$\frac{26.4}{15}$	$\frac{13.4}{15}$		$\frac{25}{25}$	$\frac{30}{30}$	$\frac{38}{38}$	$\frac{43}{43}$

3+60

$\frac{102.9}{15.5}$	$\frac{97.5}{10.9}$	$\frac{96.2}{11.7}$	$\frac{96.8}{12.1}$	$\frac{92.4}{16.0}$	$\frac{89.3}{19.1}$	$\frac{96.8}{17.4}$
$\frac{26.4}{15}$	$\frac{10}{10}$		$\frac{25}{25}$	$\frac{27}{27}$	$\frac{40}{40}$	$\frac{44}{44}$

3+50

$\frac{104.6}{6.8}$	$\frac{97.0}{11.4}$	$\frac{96.0}{12.4}$	$\frac{95.6}{12.8}$	$\frac{90.8}{18.4}$	$\frac{88.8}{19.5}$	$\frac{94.4}{14.0}$
$\frac{14.4}{15}$	$\frac{15}{15}$		$\frac{22}{22}$	$\frac{25}{25}$	$\frac{32}{32}$	$\frac{42}{42}$

3+25

$\frac{97.8}{10.6}$	$\frac{95.3}{13.1}$	$\frac{94.1}{14.3}$	$\frac{94.3}{14.1}$	$\frac{87.8}{20.6}$	$\frac{82.8}{22.6}$	$\frac{82.5}{20.6}$	$\frac{73.2}{14.7}$
$\frac{26.4}{15}$	$\frac{15}{15}$		$\frac{19}{19}$	$\frac{21}{21}$	$\frac{25}{25}$	$\frac{38}{38}$	$\frac{42}{42}$

3+00

$\frac{96.2}{12.3}$	$\frac{92.9}{15.5}$	$\frac{92.5}{15.6}$	$\frac{90.3}{18.1}$	$\frac{89.5}{18.6}$	$\frac{82.3}{21.1}$	$\frac{92.3}{16.1}$
$\frac{26.4}{15}$		$\frac{15}{15}$	$\frac{17}{17}$	$\frac{25}{25}$	$\frac{37}{37}$	$\frac{38}{38}$

T.P.

12.84 108.41 0.24 95.57

$\frac{108.41}{3}$

2+75

$\frac{933}{2.5}$
 $\frac{26.4}{15}$

$\frac{92.0}{3.8}$	$\frac{90.2}{5.1}$	$\frac{88.5}{7.0}$	$\frac{87.3}{7.5}$	$\frac{86.4}{9.4}$	$\frac{91.6}{11.2}$
	$\frac{14}{14}$	$\frac{17}{17}$	$\frac{25}{25}$	$\frac{37}{37}$	$\frac{38}{38}$

2+53

86.29

12 0 Sewer M.H. N.M.
9.72 feet

$\frac{95.81}{3}$

√+50

$$\begin{array}{r} 133.4 \\ 8.5 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 125.5 \\ 20.1 \\ \hline 20.1 \end{array} \quad \begin{array}{r} 108.2 \\ 37.7 \\ \hline 5 \end{array} \quad \begin{array}{r} 108.5 \\ 36.4 \\ \hline 15 \end{array} \quad \begin{array}{r} 108.4 \\ 37.9 \\ \hline 55 \end{array} \quad \begin{array}{r} 108.5 \\ 37.4 \\ \hline 20 \end{array}$$

√+25

$$\begin{array}{r} 136.9 \\ 9.0 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 122.1 \\ 23.8 \\ \hline 23.8 \end{array} \quad \begin{array}{r} 107.6 \\ 38.3 \\ \hline 5 \end{array} \quad \begin{array}{r} 110.5 \\ 35.4 \\ \hline 15 \end{array} \quad \begin{array}{r} 106.8 \\ 39.1 \\ \hline 25 \end{array} \quad \begin{array}{r} 106.5 \\ 39.2 \\ \hline 40 \end{array}$$

√+00

$$\begin{array}{r} 135.0 \\ 10.9 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 122.2 \\ 23.7 \\ \hline 23.7 \end{array} \quad \begin{array}{r} 108.5 \\ 36.0 \\ \hline 4 \end{array} \quad \begin{array}{r} 106.8 \\ 39.1 \\ \hline 15 \end{array} \quad \begin{array}{r} 105.8 \\ 40.1 \\ \hline 25 \end{array} \quad \begin{array}{r} 105.3 \\ 40.6 \\ \hline 40 \end{array}$$

T.P.	13.17	144.94	0.31	132.77
T.P.	12.64	133.08	0.24	120.44
T.P.	12.53	120.68	0.26	108.15

145.94
3

√+75

$$\begin{array}{r} 131.3 \\ + 22.9 \\ \hline 26.4 \end{array} \quad \begin{array}{r} 125.4 \\ + 17.0 \\ \hline 15 \end{array} \quad + 9.0 \quad \begin{array}{r} 105.0 \\ 34 \\ \hline 3 \end{array} \quad \begin{array}{r} 105.3 \\ 32.1 \\ \hline 25 \end{array} \quad \begin{array}{r} 104.6 \\ 3.8 \\ \hline 35 \end{array} \quad \begin{array}{r} 102.4 \\ 6.0 \\ \hline 50 \end{array}$$

√+50

$$\begin{array}{r} 124.9 \\ + 16.5 \\ \hline 26.4 \end{array} \quad \begin{array}{r} 128.5 \\ + 10.5 \\ \hline 15 \end{array} \quad \begin{array}{r} 111.1 \\ + 2.7 \\ \hline 1 \end{array} \quad 1.3 \quad \begin{array}{r} 103.8 \\ 4.6 \\ \hline 1 \end{array} \quad \begin{array}{r} 103.6 \\ 2.8 \\ \hline 18 \end{array} \quad \begin{array}{r} 102.4 \\ 6.0 \\ \hline 25 \end{array} \quad \begin{array}{r} 101.8 \\ 6.6 \\ \hline 30 \end{array} \quad \begin{array}{r} 98.7 \\ 9.7 \\ \hline 36 \end{array} \quad \begin{array}{r} 98.0 \\ 9.4 \\ \hline 45 \end{array} \quad \begin{array}{r} 101.1 \\ 6.6 \\ \hline 50 \end{array}$$

√+25

$$\begin{array}{r} 112.4 \\ + 9.0 \\ \hline 26.4 \end{array} \quad \begin{array}{r} 112.2 \\ + 3.8 \\ \hline 15 \end{array} \quad \begin{array}{r} 105.0 \\ 34 \\ \hline 15 \end{array} \quad \begin{array}{r} 102.9 \\ 15.5 \\ \hline 12 \end{array} \quad \begin{array}{r} 100.1 \\ 9.2 \\ \hline 21 \end{array} \quad \begin{array}{r} 99.8 \\ 8.6 \\ \hline 21 \end{array} \quad \begin{array}{r} 93.0 \\ 15.4 \\ \hline 25 \end{array} \quad \begin{array}{r} 92.4 \\ 16.0 \\ \hline 40 \end{array} \quad \begin{array}{r} 99.5 \\ 8.9 \\ \hline 50 \end{array}$$

√+00

$$\begin{array}{r} 109.7 \\ + 13 \\ \hline 26.4 \end{array} \quad \begin{array}{r} 105.1 \\ 3.3 \\ \hline 15 \end{array} \quad \begin{array}{r} 100.8 \\ 7.6 \\ \hline 10 \end{array} \quad \begin{array}{r} 98.2 \\ 9.7 \\ \hline 10 \end{array} \quad \begin{array}{r} 98.8 \\ 10.5 \\ \hline 20 \end{array} \quad \begin{array}{r} 96.2 \\ 15.2 \\ \hline 25 \end{array} \quad \begin{array}{r} 90.1 \\ 18.3 \\ \hline 30 \end{array} \quad \begin{array}{r} 90.1 \\ 18.3 \\ \hline 40 \end{array} \quad \begin{array}{r} 97.5 \\ 10.6 \\ \hline 43 \end{array}$$

108.41
3

7+00

$\frac{137.1}{10.8}$
26.4

$\frac{126.3}{21.6}$
4

$\frac{123.9}{24.0}$

$\frac{119.5}{28.4}$
10

$\frac{116.5}{31.4}$
25

$\frac{116.5}{36.0}$
28

$\frac{112.5}{35.4}$
40

$\frac{118.0}{29.9}$
41

6+75

$\frac{136.0}{11.5}$
26.4

$\frac{123.3}{24.6}$
10

$\frac{119.8}{28.1}$
18

$\frac{118.2}{32.5}$
25

$\frac{115.4}{32.5}$
30

$\frac{115.4}{33.0}$
35

$\frac{115}{36.4}$
42

$\frac{115.5}{32.1}$
45

6+50

$\frac{142.5}{5.4}$
26.4

$\frac{129.8}{18.1}$

$\frac{126.1}{21.8}$
2

$\frac{114.4}{33.5}$
18

$\frac{113.6}{34.3}$
25

$\frac{114.0}{33.9}$
40

6+45

$\frac{143.0}{4.9}$
26.4

$\frac{130.4}{17.5}$

$\frac{118.4}{29.5}$
4

$\frac{114.3}{28.6}$
15

$\frac{113.2}{34.6}$
25

$\frac{114.2}{33.7}$
40

6+25

$\frac{145.5}{2.4}$
26.4

$\frac{140.4}{7.5}$
15

$\frac{131.9}{16.0}$

$\frac{112.5}{30.1}$
4

$\frac{112.2}{31.7}$
10

$\frac{114.5}{33.4}$
25

$\frac{111.8}{36.1}$
40

T.P.

383 147.85 1.92 144.02

$\frac{147.85}{5}$

6+00

$\frac{148.0}{2.9}$
26.4

$\frac{129.2}{16.7}$

$\frac{113.5}{32.4}$
5

$\frac{113.1}{32.8}$
10

$\frac{110.4}{35.5}$
15

$\frac{110.3}{35.6}$
25

$\frac{110.8}{37.1}$
40

5+75

$\frac{139.3}{4.6}$
26.4

$\frac{134.5}{11.4}$
15

$\frac{127.6}{18.3}$

$\frac{116}{34.3}$
5

$\frac{112.3}{33.6}$
10

$\frac{109.5}{36.4}$
15

$\frac{109.3}{36.0}$
25

$\frac{108.2}{36.7}$
40

$\frac{145.92}{5}$

T.P. mail in pole 6.59 157.01 3.43 144.47

7.9+00

$\frac{192.3}{5.6}$	$\frac{138.7}{9.2}$	$\frac{154.9}{16.0}$	$\frac{120.2}{6}$	$\frac{122.9}{10}$	$\frac{127.5}{2.1}$	$\frac{122}{2.7}$	$\frac{118.6}{29.3}$	$\frac{120.2}{19.9}$
26.4	15				24	25	33	35

6.8+75

$\frac{138.9}{2.0}$	$\frac{121.1}{1.69}$	$\frac{127.7}{20.2}$	$\frac{126.6}{21.3}$	$\frac{127.4}{30.5}$	$\frac{118.1}{28.0}$	$\frac{121}{20.8}$
26.4	15		23	24	32	38

6.8+50

$\frac{136.9}{11.0}$	$\frac{127.2}{20.7}$	$\frac{126.0}{21.9}$	$\frac{124.8}{23.1}$	$\frac{124.8}{24.4}$	$\frac{114.5}{24.5}$	$\frac{125.0}{22.9}$
26.4		10	23	25	33	35

6.8+25

$\frac{134.9}{13.0}$	$\frac{125.0}{22.9}$	$\frac{123.2}{24.7}$	$\frac{116.0}{21.9}$	$\frac{118.9}{29.0}$	$\frac{123.5}{24.1}$
26.4		20	25	34	35

6.8+00

$\frac{132.1}{10.8}$	$\frac{132.5}{15.1}$	$\frac{124.7}{23.2}$	$\frac{122.4}{24.5}$	$\frac{116.0}{31.9}$	$\frac{115.2}{32.7}$	$\frac{122.7}{24.7}$
26.4	15		15	25	32	34

7.7+75

$\frac{138.5}{9.1}$	$\frac{135.5}{12.4}$	$\frac{131.5}{16.1}$	$\frac{127.3}{20.6}$	$\frac{122}{24.7}$	$\frac{120.2}{27.7}$	$\frac{116.3}{32.6}$	$\frac{114.5}{33.1}$	$\frac{121.2}{26.7}$
26.4	15	5		10	20	28	35	36

6.7+50

$\frac{139.7}{8.2}$	$\frac{135.7}{12.2}$	$\frac{130.6}{17.3}$	$\frac{126.5}{21.1}$	$\frac{123.5}{24.4}$	$\frac{121.2}{26.2}$	$\frac{119.5}{28.1}$	$\frac{114.0}{33.9}$	$\frac{114.6}{33.9}$	$\frac{119.9}{28.0}$
26.4	15		3	8	15	21	25	30	35

7+25

$\frac{139.5}{8.1}$	$\frac{127.7}{20.4}$	$\frac{127.9}{15}$	$\frac{120.9}{20}$	$\frac{117.5}{17.5}$	$\frac{118.7}{19.2}$	$\frac{112.5}{34.7}$	$\frac{113.2}{34.7}$	$\frac{118.4}{29.5}$
26.4				23	23	25	32	35

147.85

147.85

10+75

$\frac{138.7}{11.9}$	$\frac{138.1}{12.2}$	$\frac{133.7}{11.9}$	$\frac{133.2}{12.9}$	$\frac{138.0}{12.6}$	$\frac{132.5}{12.8}$
$\frac{26.4}{21}$	$\frac{18}{18}$	$\frac{12.9}{12}$	$\frac{12.6}{8}$		

$\frac{137.9}{12.7}$	$\frac{140.5}{9.8}$
$\frac{25}{25}$	$\frac{25}{25}$

T.P

11.94 150.58 12.35 138.00

$\frac{150.58}{3}$

10+50

$\frac{147.3}{7.7}$	$\frac{132.0}{14.0}$	$\frac{131.3}{12.7}$	$\frac{136.3}{14.7}$
$\frac{26.4}{7}$	$\frac{13}{13}$	$\frac{7}{7}$	$\frac{14.7}{14.7}$

$\frac{135.2}{15.3}$	$\frac{136.2}{14.3}$
$\frac{25}{25}$	$\frac{25}{25}$

10+25

$\frac{145.2}{5.3}$	$\frac{141.4}{9.6}$	$\frac{137.4}{12.6}$	$\frac{129.9}{21.1}$
$\frac{26.4}{26.4}$	$\frac{15}{15}$	$\frac{7}{7}$	

$\frac{134.4}{16.6}$	$\frac{134.4}{14.6}$	$\frac{134.8}{16.7}$	$\frac{135.9}{15.0}$
$\frac{25}{25}$	$\frac{25}{25}$	$\frac{25}{25}$	$\frac{25}{25}$

10+00

$\frac{146.0}{5.0}$	$\frac{142.1}{8.9}$	$\frac{138.5}{12.5}$	$\frac{135.6}{15.4}$
$\frac{26.4}{26.4}$	$\frac{15}{15}$	$\frac{10}{10}$	$\frac{15.4}{15.4}$

$\frac{128.8}{22.1}$	$\frac{130.8}{20.2}$	$\frac{133.4}{17.6}$	$\frac{133.5}{17.5}$	$\frac{133.1}{17.9}$
$\frac{4}{4}$	$\frac{12}{12}$	$\frac{15}{15}$	$\frac{25}{25}$	$\frac{25}{25}$

9+75

$\frac{146.3}{4.7}$	$\frac{141.8}{9.2}$	$\frac{138.6}{12.4}$	$\frac{136.0}{15.0}$
$\frac{26.4}{26.4}$	$\frac{15}{15}$	$\frac{10}{10}$	$\frac{15.0}{15.0}$

$\frac{145.2}{23.8}$	$\frac{131.9}{19.1}$	$\frac{132.0}{19.0}$	$\frac{132.0}{19.0}$
$\frac{25}{25}$	$\frac{20}{20}$	$\frac{25}{25}$	$\frac{25}{25}$

9+50

$\frac{146.9}{4.1}$	$\frac{142.9}{8.1}$	$\frac{138.2}{14.3}$	$\frac{130.9}{20.1}$
$\frac{26.4}{26.4}$	$\frac{15}{15}$	$\frac{10}{10}$	$\frac{10}{10}$

$\frac{136.4}{22.6}$	$\frac{123.4}{27.6}$	$\frac{131.0}{20.0}$
$\frac{15}{15}$	$\frac{25}{25}$	$\frac{40}{40}$

9+25

$\frac{146.0}{6.0}$	$\frac{141.8}{9.2}$	$\frac{135.5}{17.2}$	$\frac{130.5}{20.5}$
$\frac{26.4}{26.4}$	$\frac{13}{13}$	$\frac{10}{10}$	$\frac{10}{10}$

$\frac{124.9}{26.1}$	$\frac{124.4}{26.6}$	$\frac{119.8}{31.3}$	$\frac{122.5}{28.5}$	$\frac{130.0}{21.0}$
$\frac{20}{20}$	$\frac{25}{25}$	$\frac{20}{20}$	$\frac{40}{40}$	$\frac{41}{41}$

17.01

$\frac{157.01}{3}$

13 + 48.14 = Miller last section 3400
150x/56

167.6 = 167.5

12 + 98.14

T.P. 11.45 172.02 0.91 160.57

12 + 50

12 + 00

11 + 75

T.P. 11.14 161.48 0.24 150.34

11 + 50

11 + 25

11 + 00

150.58

137.9
12.7
NS
ditch
from Bow Ave

139.9 139.7 136.0
10.7 16.9 14.4
20 35 26.4
11.2 11.7 10.2
22 16 7
140.7
10.7
10.7

150.58

160.0 161.4 161.8 161.8 163.8 165.0 165.9
12.0 10.6 10.2 10.2 8.2 7.0 6.1
35 26.4 15 15 15 20 35

170.07

155.8 156.5 156.2 156.3 156.4 157.2 159.1 160.9 160.4
5.7 5.0 4.8 5.2 5.1 4.3 2.4 1.5 1.1
35 26.4 15 15 15 13 15 20 35

149.6 150.5 151.3 150.8 151.2 153.2 154.1 154.1
11.9 11.0 10.4 10.7 10.3 8.3 7.4 7.4
35 26.4 15 15 15 18 20 35

146.3 147.4 148.4 148.3 148.5 151.5 151.8
14.2 14.1 12.1 13.2 13.0 9.7 9.7
35 26.4 15 15 17 25 25 35

33
12.2
Red #100190

145.1 145.5 146.4 146.6 148.4 148.6
4.5 5.1 4.5 4.5 2.2 2.0
35 26.2 15 20 25 35

144.1 143.7 142 138.9 142.5 143.4 144.4 145.4
6.5 6.7 6.4 11.7 8.1 7.2 6.2 5.2
38 22 11 8 6 7.2 25 35

140.9 142.9
9.7 7.7
25 35

80' wide
14' elev.
13' ups.

38th St. X sec.

Thorn to Redwood.

5-11-36
Miller
Walker
Blas

309.12

indexed
c.s.k.

47

B.M. B.P.	0.45	318.63		318.18	N. W. 40 th + Myrtle
T.P.	0.88	306.67	12.84	305.79	
T.P. B.M. B.P.	9.92	309.91	6.68	299.99	N.W. 40 th + Thorn.
T.P. Nail Pole	7.68	309.12	8.47	301.44	S.W. 38 th + Thorn.

N. Line Thorn St

W			13.1	296.0	
cl			11.9	297.2	
1/4			11.2	297.9	
cl			10.4	298.7	
1/4			9.0	300.1	
cl			8.0	301.1	
E			7.0	302.1	
E	N. cl.		6.6	302.5	
cl			7.2	301.9	
1/4			7.9	301.2	
cl			9.2	299.9	
1/4			10.6	298.5	
cl			11.4	297.7	
W			12.0	297.1	
W	N. 1/4		11.0	298.1	
cl			10.3	298.8	
1/4			9.6	299.5	
cl			8.5	300.6	

1/4	7.3	301.8
cl	6.1	302.5
E.	6.1	303.0
cl	5.7	303.4
cl	6.3	302.8
1/4	7.0	302.1
cl	7.8	301.3
1/4	8.7	300.4
cl	9.6	299.5
W.	10.5	298.6
W	9.7	299.4
cl	8.9	300.2
1/4	8.0	301.1
cl	7.1	302.0
1/4	6.5	302.6
cl	6.0	303.1
E	5.4	303.7
E	5.3	303.8
cl	5.7	303.4
1/4	6.4	302.7
cl	6.4	302.5
1/4	7.4	301.7
cl	8.1	301.0
W	8.7	300.4

309.12

0+00 = S. Line Thorh.

W	8.1	301.0
cb	7.5	301.6
1/4	6.9	302.2
♀	6.3	302.8
1/4	6.0	303.1
cb	5.3	303.8
E	4.8	304.3

0+50

E	4.3	304.8
cb	4.7	304.4
1/4	4.8	304.3
♀	4.7	304.4
1/4	5.6	303.5
cb	5.9	303.2
W	6.2	302.9

1+00

W	5.4	303.7
cb	5.3	303.8
1/4	5.0	304.1
♀	4.9	304.2
1/4	4.6	304.5
cb	4.6	304.5
E	4.2	304.9

309.12

1+50

E	4.0	305.1
cb	4.6	304.5
1/4	4.9	304.2
♀	5.1	304.0
1/4	5.0	304.1
cb	5.1	304.0
W	5.3	303.8

2+00

W	5.9	303.2
cb	5.7	303.4
1/4	5.5	303.6
♀	5.4	303.7
1/4	5.2	303.9
d	5.0	304.1
E	4.9	304.2

2+50

E	5.3	303.8
cb	5.5	303.6
1/4	5.7	303.4
♀	5.9	303.2
1/4	6.2	302.9
cb	6.3	302.8
W	4.3	302.8

38th

48

309.12

3+00

W.	7.6	301.5
cl	7.3	301.8
¹ / ₄	7.2	301.9
♀	7.1	302.0
¹ / ₄	7.0	302.1
cl	6.7	302.4
E.	6.6	302.5

3+50

E	7.9	301.2
cl	8.2	300.9
¹ / ₄	8.3	300.8
♀	8.5	300.6
¹ / ₄	8.6	300.5
cl	8.6	300.5
W.	8.8	300.3

4+00

W	10.8	298.3
cl	10.6	298.5
¹ / ₄	10.4	298.7
♀	10.3	298.8
¹ / ₄	10.3	298.8
cl	10.3	298.8
E	10.0	299.1

309.12

38th

4+50

49

E	10.8	298.3
cl	11.5	297.6
¹ / ₄	12.0	297.1
♀	12.4	296.7
¹ / ₄	12.7	296.4
cl	13.6	295.5
W.	14.4	294.7

T.P. 0.44 297.70 11.86 297.26

5+00

W.	4.9	292.8
cl	4.0	293.7
¹ / ₄	3.7	294.0
♀	2.9	294.8
¹ / ₄	2.3	295.4
cl	1.7	296.0
E	1.3	296.4

5+50

E	5.6	292.1
cl	6.3	291.4
¹ / ₄	7.0	290.7
♀	7.9	289.8
¹ / ₄	7.3	290.4
cl	7.0	290.7
W	7.0	290.7

297.70

5+75

W	9.8	287.9
cb.	9.0	288.7
1/4	10.2	287.5
±	9.9	287.8
1/4	9.3	288.4
cb.	8.0	289.7
E	7.4	290.3

5+98.5 = N Line Redwood.

E	9.1	288.6
cb.	9.9	287.8
1/4	11.6	286.1
±	13.7	284.0
1/4	13.6	284.1
cb.	11.0	286.7
W.	10.5	287.2

T.P.	10.94	306.27	2.37	295.33
------	-------	--------	------	--------

chk. BMBP N.W. 40 th + Redwood.	3.30	302.97
--	------	--------

B.M. Nail Pole	4.61	301.66	S.W. 39 th + Redwood.
----------------	------	--------	----------------------------------

38th

50

80. Wide
14. ch.
13. 1/4s

39th St. X Sec
Redwood. South

7 PLOTTED 5-11-36

306.50
£

Indexed
c.s.k.

51

BM Nail Pole

4.84 306.50

301.66 S.W. 39th
+ Redwood

E

3.7

302.8

ch

4.0

302.5

1/4

4.3

302.2

£

4.6

301.9

1/4

4.8

301.7

ch

5.0

301.5

W

5.3

301.2

S. 1/4

W

5.8

300.7

ch

5.3

301.2

1/4

4.9

301.6

£

4.7

301.8

1/4

4.1

302.4

ch

3.8

302.7

E

3.5

303.0

S. ch.

E

3.5

303.0

ch

4.1

302.4

1/4

4.4

302.1

£

4.8

301.7

1/4

5.0

301.5

ch

5.3

301.2

W

5.7

300.8

N. Line Redwood

W

3.7

302.8

ch

3.8

302.7

1/4

3.7

302.8

£

3.6

302.9

1/4

3.4

303.1

ch

3.3

303.2

E

2.9

303.6

N. ch.

E

3.2

303.3

ch

3.6

302.9

1/4

3.8

302.7

£

4.0

302.5

1/4

4.1

302.4

ch

4.3

302.2

W

4.5

302.0

N 1/4

W

4.9

301.6

ch

4.5

302.0

1/4

4.3

302.2

£

4.3

302.2

1/4

4.0

302.5

ch

3.8

302.7

E

3.5

303.0

306.50
0+00 = S. Line Redwood St.

N	5.3	301.2
cl	4.6	301.9
1/4	4.8	301.7
⊕	4.8	301.7
1/4	4.5	302.0
cl	4.3	302.2
E	4.0	302.5

0+50

E	4.0	302.5
cl	4.4	302.1
1/4	5.0	301.5
⊕	5.1	301.4
1/4	5.1	301.4
cl	5.4	301.1
N	5.6	300.9

1+00

N	5.8	300.7
cl	5.6	300.9
1/4	5.3	301.2
⊕	5.2	301.3
1/4	5.2	301.3
cl	5.1	301.4
E	4.9	301.6

306.50
1+50

E	5.6	300.9
cl	5.4	301.1
1/4	5.6	300.9
⊕	5.9	300.6
1/4	5.9	300.6
cl	5.9	300.6
W	6.1	300.4

2+00

N	7.7	298.8
cl	7.0	299.5
1/4	7.5	299.0
⊕	7.2	299.3
1/4	7.0	299.5
cl	6.9	299.6
E	7.2	299.3

2+50

E	8.4	298.1
cl	8.6	297.9
1/4	8.7	297.8
⊕	9.3	297.2
1/4	9.5	297.0
cl	9.6	296.9
W	9.1	297.4

39th St.

52

306.50

3400

W	12.0	294.5
cl	11.6	294.9
1/4	11.5	295.0
1/2	11.3	295.2
1/4	11.0	295.5
cl	10.3	296.2
E	10.0	296.5

3750

E	11.4	295.1
cl	11.4	294.7
1/4	12.2	294.3
1/2	13.0	293.5
1/4	13.5	293.0
cl	13.8	292.7
W	15.6	290.9

T.P.	0.00	293.90	12.60	293.90
------	------	--------	-------	--------

4400

W.	3.8	290.1
cl	3.0	290.9
1/4	2.4	291.5
1/2	1.9	292.0
1/4	1.0	292.9
cl	0.5	293.4
E	+0.4	294.3

29390

4750

E	1.5	292.4
cl	2.0	291.9
1/4	3.1	290.8
1/2	4.0	289.9
1/4	4.4	289.5
cl	5.5	288.4
W	6.5	287.4
+10.	7.3	286.6

5700

-10	10.6	283.3
W	9.7	284.2
cl	8.8	285.1
1/4	7.4	286.5
1/2	6.8	287.1
+9	6.0	287.9
+10	5.1	288.8
1/4	4.8	289.1
cl	4.5	289.4
E	3.3	290.6

5750

E.	4.5	289.4
cl	5.6	288.3
1/4	7.0	286.9
1/2	8.0	285.9
1/4	9.2	284.7
cl	9.8	284.1
W	11.0	282.9

39th St

53

29390
5+98 20 2 N. Line Quince st

W	11.9	282.0
cb	10.5	283.4
1/4	9.5	284.4
ϕ	8.5	285.4
1/4	7.6	286.3
cb	6.8	287.1
E	6.4	287.5

N. cb

E	7.1	286.8
cb	7.2	286.7
1/4	7.8	286.1
ϕ	8.9	285.0
1/4	9.6	284.3
cb	10.3	283.6
W	11.7	282.2

N. 1/4

W	11.8	282.1
cb	10.5	283.4
1/4	9.9	284.0
ϕ	9.4	284.5
1/4	8.2	285.7
cb	8.0	285.9
E	7.9	286.0

293.90
ϕ Quince 39 26 st

54

E	8.8	285.1
cb	9.3	284.6
1/4	9.3	284.6
ϕ	10.1	283.8
1/4	10.4	283.5
cb	11.0	282.9
W	11.8	282.1

S. 1/4

W	12.0	281.9
cb	11.4	282.5
1/4	11.1	282.2
ϕ	10.8	283.1
1/4	10.3	283.6
cb	10.3	283.6
E	10.0	283.9

S. cb

E	10.8	283.1
cb	11.6	282.3
1/4	11.2	282.7
ϕ	11.7	282.2
1/4	11.9	282.0
cb	12.0	281.9
W	12.4	281.5

293.90

0+00 = S. line Quince

W	13.5	280.4
cb	13.0	280.9
1/4	13.2	280.7
1/4	12.8	281.1
1/4	12.2	281.7
cb	12.5	281.4
E	12.2	281.7

T.P. 0.48 281.56 12.82 281.08

0+50

E	1.8	279.8
cb	2.7	278.9
1/4	4.0	277.6
1/4	4.3	277.3
1/4	4.8	276.8
cb	5.3	276.3
W	6.2	275.4

1+00

W	8.5	273.1
cb	8.4	273.2
1/4	7.9	273.7
+10	7.4	274.2
1/4	6.3	275.3
1/4	5.2	276.4
cb	4.2	277.4
E	2.9	278.7

281.56

39th St.

1+50

55

E	5.0	276.6
cb	6.0	275.6
1/4	7.2	274.4
1/4	8.1	273.5
1/4	9.1	272.5
cb	9.8	271.8
W	10.4	271.2

B.M. Nail Pole

9.59 271.97

D19203-T.
3' E. of W line
at sta 1+50

2+00

W	12.9	268.7
cb	12.4	269.2
1/4	11.5	270.1
1/4	10.9	270.7
1/4	10.5	271.1
cb	9.7	271.9
E	8.5	273.1

2+50

E	10.9	270.7
cb	11.8	269.8
1/4	12.2	269.4
1/4	13.0	268.6
1/4	13.7	267.9
cb	14.0	267.6
W	14.4	267.2

281.56

T.P. 3,20 272.45 12.31 269.25

3+00

W	6.2	266.3
cb	5.7	266.8
1/4	5.4	267.1
±	4.7	267.8
1/4	4.4	268.1
cb	4.0	268.5
E	3.2	269.3

3+50

E	4.4	268.1
cb	4.8	267.7
1/4	5.4	267.1
±	5.9	266.6
1/4	6.2	266.3
cb	6.8	265.7
W	7.1	265.4

4+00

W	8.2	264.3
cb	7.9	264.6
1/4	7.2	265.3
±	6.9	265.6
1/4	6.7	265.8
cb	6.7	265.8
E	7.0	265.5

272.45
4+5039th St

56

E	11.8	260.7
cb	10.7	261.8
1/4	10.3	262.2
±	9.9	262.6
1/4	10.0	262.5
cb	10.2	262.3
W	10.5	262.0

5+00

W	13.5	259.0
cb	14.0	258.5
1/4	15.0	257.5
±	15.5	257.0
1/4	16.5	256.0
cb	17.0	255.5
E	18.0	254.5
+10	22.0	250.5

T.P. 12.51 284.81 0.15 272.30

T.P. 12.47 297.02 0.26 284.55

T.P. 10.28 306.80 0.50 296.52

B.M. Nail in Pole 5.14 301.66 S.W. 39th St
+Redwood

277.2³

NW Return of 350' Highview Dr

N 1/2 of NE of Highview P.C. return	6.86	270.37	Top cb
" " " " " gut pav.	7.50	269.73	
#1 cb	7.52	269.71	
" gut	8.12	269.11	
#2 cb	7.92	269.30	
" gut	8.50	268.73	
#3 cb	7.98	269.25	
" gut	8.53	268.70	
#4 cb end WL 350'	7.82	269.41	
" gut " "	8.41	268.82	
E Highview & WL 350'	8.38	268.85	on pav

SW Return

Top cb } WL 350' to N	8.30	268.93	
gut }	8.82	268.41	
25' E - P.C. of 300' Return	9.36	267.87	Top cb
" " gut	9.86	267.37	
#1 cb	9.88	267.35	
" gut	10.36	266.87	
#2 cb	10.48	266.75	
" gut	10.92	266.30	
#3 cb	10.96	266.27	
" gut	11.49	265.74	
#4 cb - EC cb return	11.26	265.77	
" gut	11.97	265.26	

374.23

1+30

E	4.0	370.2
♀	3.9	370.3
W	3.8	370.4

1+45

W	3.3	370.9
♀	3.1	371.1
+5	3.7	370.5
E	3.7	370.5

1+60

E	3.6	370.6
♀	4.0	370.2
W	3.8	370.4

From 1+50 to 1+90. Wooden Fence on W. 0.3' in Alley

From 1+90 to 2+00 Shed on W. 0.3' in Alley

2+00

W	3.6	370.6
♀	3.8	370.4
E	3.5	370.7

374.23

Alley BIK 1534.H

60

2+25

E	3.9	370.3
♀	4.1	370.1
W	3.9	370.3

2+50

W	3.2	371.0
♀	3.1	371.1
E	3.7	370.5

2+80

E	3.7	370.5
♀	3.9	370.3
W	3.8	370.4

3+00

W	3.8	370.4
♀	3.8	370.4
E	3.4	370.8

T.P. 5.90 376.42 3.71 370.52

3+50

E	5.6	370.8
♀	5.7	370.7
W	5.8	370.6

376.42

4+00

W	5.4	371.0
⊕	5.4	371.0
E	5.7	370.7

4+50

E	5.3	371.1
⊕	5.3	371.1
W	5.3	371.1

4+77 S. End. 6 garages on W. conc. floor 4.8' Back

W-4.8 floor	4.57	371.85
W	4.6	371.8
⊕	5.0	371.4
E	5.0	371.4

5+29 = N. End above Garages - 4.7 Back

E	5.1	371.3
⊕	5.0	371.4
W	5.0	371.4
W+ = floor	4.83	371.59

5+31 garage on E dirt floor 5.0 Back

E-5 = floor	5.00	371.4
W+ ⊕ 36" ent. walk	4.72	371.7

376.42

5+48

W-2.6 ⊕ 3' ent. walk	4.46	371.96
----------------------	------	--------

5+50

W	4.6	371.8
⊕	4.7	371.7
E	5.1	371.3

5+70

E	5.0	371.4
⊕	4.7	371.7
W	4.4	372.0

5+95

W	4.3	372.1
⊕	4.9	371.5
WE	4.8	371.6

6+00 = S. Line Howard Ave

E. ent. el. S. 2nd.	4.50	371.92
E. pav. " "	4.95	371.47
⊕ " " "	4.92	371.50
W " " "	4.74	371.68
W. ent. el. " "	4.37	372.05

6+14 = S. 6th. Line

W-30 pav	4.63	371.79
W-30 ent. el.	4.25	372.17
W " "	4.52	371.90
W. Pav.	4.97	371.45

Alley BIK 153. UH.

61

376.42

Alley Blk 153 U.H.

62

S. ch. line Howard.

4	pay.	4.97	371.45
E.	"	5.08	371.34
2	cmt. el	4.62	371.80
+30	" "	4.79	371.63
+30	pay.	5.30	371.12

B.M. Nail Pole 5.03 377.43 4.02 372.40
 W. Alley
 S. ch. Howard

B.M. B.P. S.E. Idaho & Howard. 4.44 372.99 = 373.01

Grades.

Howard.

6+00	371.64	371.47
------	--------	--------

6+70	369.56	369.36
6+50	369.43	369.25
6+30	369.21	369.09
6+00	368.80	368.81

Polk Ave

Re. X See Alley Bk 197 U.H
see F.B. 1381-57.

for Culvert see Page 69.

9-17-36
miles
Walker
Bliss

S.E. Lincoln
& Louisiana

S. of Lincoln
E. Line Alley

Indexed
c.s.K.

287.30

B.M. B.P.	1.07	301.07	300.00
T.P.	5.20	293.62	12.65 288.42

Set. B.M. Nail Pole		6.45	287.17
---------------------	--	------	--------

5+56 Garage on W. cmt. floor 19.0' Back **63**
W-19.0' = floor 3.20 284.1

5+42 Garage on E. cmt. floor 4.8' Back

W. 283.0

± 283.2

+6.8 cmt. apron 3.89 283.41

E " " 3.54 283.74

+6.8 " " + floor. 3.25 284.05

6+05⁵ = 6' N. of S. Line Lincoln = S. End Pav & cmt. apron

E-0.3 cmt. ch	6.70	286.92
---------------	------	--------

E-0.3 pav	6.87	286.75
-----------	------	--------

± "	6.91	286.71
-----	------	--------

+9.6 "	6.59	287.03
--------	------	--------

+9.6' cmt. ch	6.37	287.25
---------------	------	--------

5+27 ± Double garage on W. Dirt floor 6' Back

W-6 = floor 5.7 281.6

W	6.6	287.07
---	-----	--------

±	6.8	286.87
---	-----	--------

E	7.0	286.67
---	-----	--------

5+13 Double garage on E cmt. floor 7.7' Back

E-7.7 = floor 3.83 283.47

E 5.0 282.3

± 5.8 281.5

W 5.8 281.5

+10 6.5 280.8

From sta 5+93 to 6+05⁵ Nice Cypress
Hedge on E. 1.0' in alley could be saved
by excepting strip 12.5' Long by 1.0' Wide

5+21

5+00

E	8.9	284.7
---	-----	-------

±	8.9	284.7
---	-----	-------

W	8.6	285.0
---	-----	-------

W-10	6.4	280.9
------	-----	-------

W	6.5	280.8
---	-----	-------

±	6.5	280.8
---	-----	-------

E	6.3	281.0
---	-----	-------

+10	5.2	282.1
-----	-----	-------

T.P.	2.41	297.30	8.73	284.89
------	------	--------	------	--------

287.30

4+70

E- 10	6.0	281.3
E	6.4	280.9
+3	7.0	280.3
☿	7.1	280.2
W	7.2	280.1
+10	7.2	280.1

4+45 garage on e. cmt. floor 2.5 Buck

- 10	7.6	279.7
W	7.4	279.9
☿	7.2	280.1
E	7.0	280.3
+ 2.5 = floor	6.61	280.69

4+30

- 10	7.0	280.3
E	7.5	279.8
E+4	7.1	280.2
☿	7.0	280.3
W	7.1	280.2
+10	7.7	279.6

4+00

W.	5.6	281.7 ✓
☿	5.8	281.5 ✓
E	5.7	281.6 ✓

From 4+00 South. No change.

BM. B.P. 0.02 282.01

281.99

S. E. Univ
4 11.55

64

T.P. 8.45 283.98 6.48 275.53

From 1+77 to 2+22 5 New Garages on W.
cmt. floors 2.2' Back

1+81.5 ☿ ^{#1} = floor	4.57	279.41
1+90.5 ☿ ^{#2} = "	4.24	279.74
1+99.5 ☿ ^{#3} = "	4.27	279.71
2+08.5 ☿ ^{#4} = "	3.76	280.22
2+17.5 ☿ ^{#5} = "	3.76	280.22

X Sec. Alley BIK. K. U.H. Sub. PL 1113
Suncrest to Copley East of Kansas.

12-22-36
Miller
Walker.

Indexed
C.S.K.

65

B.M. B.P 3.90 392.94 ✓ 389.04

S.E. 30th
+ Adams.

14' S of N. Line = N. End. Line Suncrest Dr

W-25	Top. cl.	4.96	387.98
W-25	gutter pav	5.56	387.38
W	" "	5.60	387.34
W.	Top. cl.	5.07	387.87
±	pavmt.	5.67	387.27
±	" "	5.78	387.16
±	Top. cl.	5.17	387.77
+25	" "	5.21	387.73
+25	gutter pav	5.94	387.00

T.P. Nails in Pole 3.87 392.41 ✓ 4.40 388.54

S. Curb Suncrest
W. Line Alley E.
of Kansas

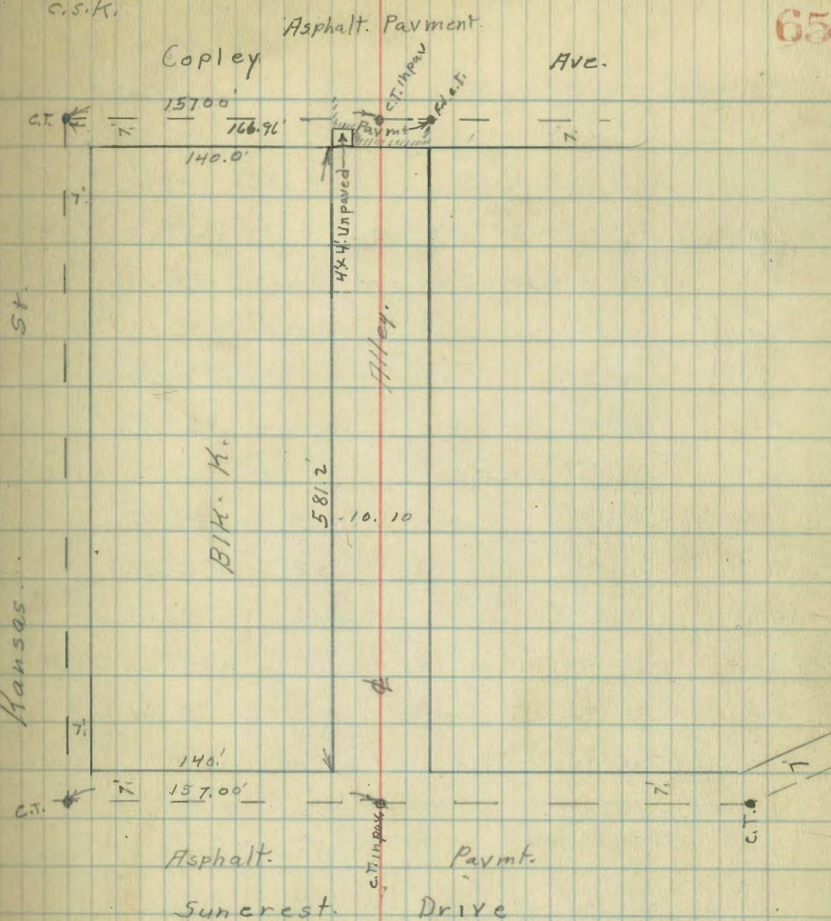
0+00 = N. Line Suncrest. = N. End. cmt. cl. + Pavmt.

E.	cmt. cl.	4.29	388.12
E.	pavmt.	4.50	387.91
±	" "	4.72	387.69
W	" "	4.55	387.86
W.	cmt. cl.	4.38	388.03

0+10 N.

W.		4.2	388.2
±		4.6	387.8
±		4.7	387.7

From 0+00 to 0+70 Wire fence on E. 1.3' in Alley



392.41
0+50N

E - 5		5.8	386.6
E		5.4	387.0
±		5.6	386.8
W		5.1	387.3
+93. garage on W. ent. floor 13.5 Back			
W-4.6	ent. apron	5.72	386.69
W-8	" "	5.41	387.00
W-13.5	floor	5.3	387.1
1100			
W-5		6.0	386.4
W		6.3	386.1
±		6.6	385.8
E		6.8	385.6
+5		7.3	385.1
1+19 garage on E dirt floor 1.7 Back			
E - 1.7	= floor	7.2	385.2
E		7.2	385.2
±		6.9	385.5
W		6.2	386.2

1+03. Proposed Drain

E. = 0+00		6.8	385.6
0+23		8.2	384.2
0+43		10.2	382.2
0+45		11.7	180.7
0+50		13.2	379.2

392.41
1+50

W - 5		6.0	386.4
W		6.2	386.2
±		6.8	385.6
E		7.2	385.2
+5		7.3	385.1
2+00			
-5		6.8	385.6
E		6.8	385.6
±		6.6	385.8
W		6.0	386.4
+5		5.8	386.6
2+50			
-5		5.6	386.8
W		5.6	386.8
±		6.1	386.3
E		6.4	386.0
+5		6.5	385.9
2+81			
± Top. M.H.		5.21	387.20
3+00			
-5		5.2	387.2
E		5.2	387.2
±		4.9	387.5
W		4.2	388.2
T.P.	5.88	393.94	4.35
			388.06

393.94

3+50

W.	5.8	388.1
±	5.8	388.1
E	6.2	387.7

3+57

W. - 0.3 = E. End. 24" cmt. walk	5.4	388.30
----------------------------------	-----	--------

4+00

E	5.5	388.4
±	5.5	388.4
W.	5.4	388.5

4+50

W	5.3	388.6
±	5.4	388.5
E	5.6	388.3

4+[?] garage on W. cmt Floor 4.3' Back

W - 4.3 = floor.	4.18	389.76
------------------	------	--------

5+00

E	5.0	388.9
±	4.9	389.0
W	4.8	389.1

5+30 garage on W. 0.6 Back.

W - 0.6 = floor	4.3	389.6
-----------------	-----	-------

5+37. S. End. cmt. walk on W.

9' W. of ± = walk	4.04	389.90
-------------------	------	--------

5+44 S. End. Dwelling on W. 0.6 Back

393.94

5+52.6 = S. End. cmt step on W.

67

W. walk to S.	4.05	389.89
+1.0 " " E. edge.	4.15	389.79
+2.5 S.E. cor cmt. step	4.15	389.79
±	4.3	389.6
+8	4.0	389.9
E.	4.8	389.1

5+55 = S. End. cmt. porch

7.5 W. of ± N.E. cor step.	4.15	389.79
7.5 " " S.E. " porch.	3.25	390.69
5+59 ± N. End. cmt. porch.		
7.5 W. of ± = N.E. Cor. porch.	3.25	390.69

5+72.7 = N. End. Dwelling on W. 0.6 Back

E	4.8	389.1
±	4.7	389.2
W.	4.2	389.7
+0.6 = N.E. Cor Dwelling	4.2	389.7

5+81.2 = S. line Copley Ave

W. S. End. cmt. cl. + dirt.	4.51	389.43
+4. pavmt.	5.14	388.80
± " "	5.40	388.54
E. " "	5.30	388.64

5+85.7

E = S. End. cmt. cl.	4.94	389.00
E. pavmt.	5.37	388.57
± " "	5.53	388.41
+6 " "	5.31	388.63

393.94

5+85² (con)

W. Line pav 5.04 388.86

W " ent. ch 4.68 369.26

5+95² = S. ch. line = Copley.

W. ent. ch 5.06 388.88

W. pav. 5.64 388.30

E " 5.80 388.14

E " 5.82 388.12

E. ent. ch 5.10 388.84

E + 5' pav. 5.90 388.04

T.P. 3.25 390.38 6.81 387.13

Spk. Pole S. ch. Suncrest W. Alley 1.84 388.54 ✓

" " 3.75 392.29 388.50

Orig B.M. 3.25 389.04 ✓

68

4-18-37
Miller
Walker
Bliss

Alley BIK. 197. U.H.
See Page 70

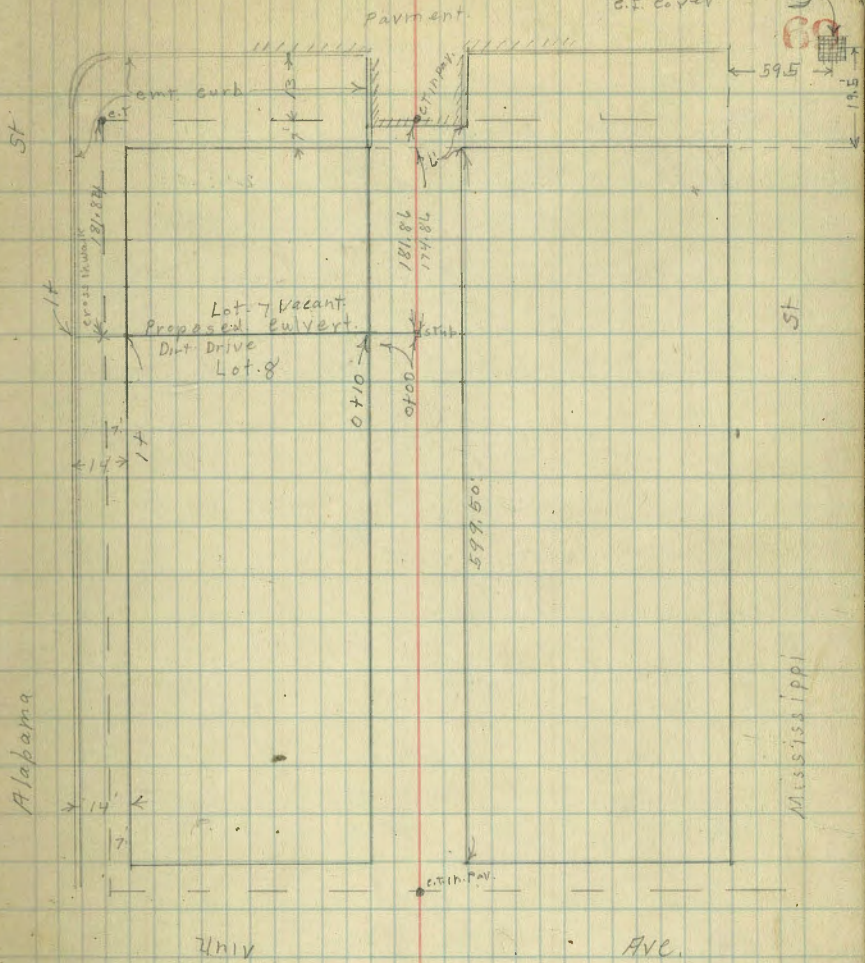
Lincoln

Ave

24"x24" Square Cleanout
Over Existing Culvert
G.I. Cover

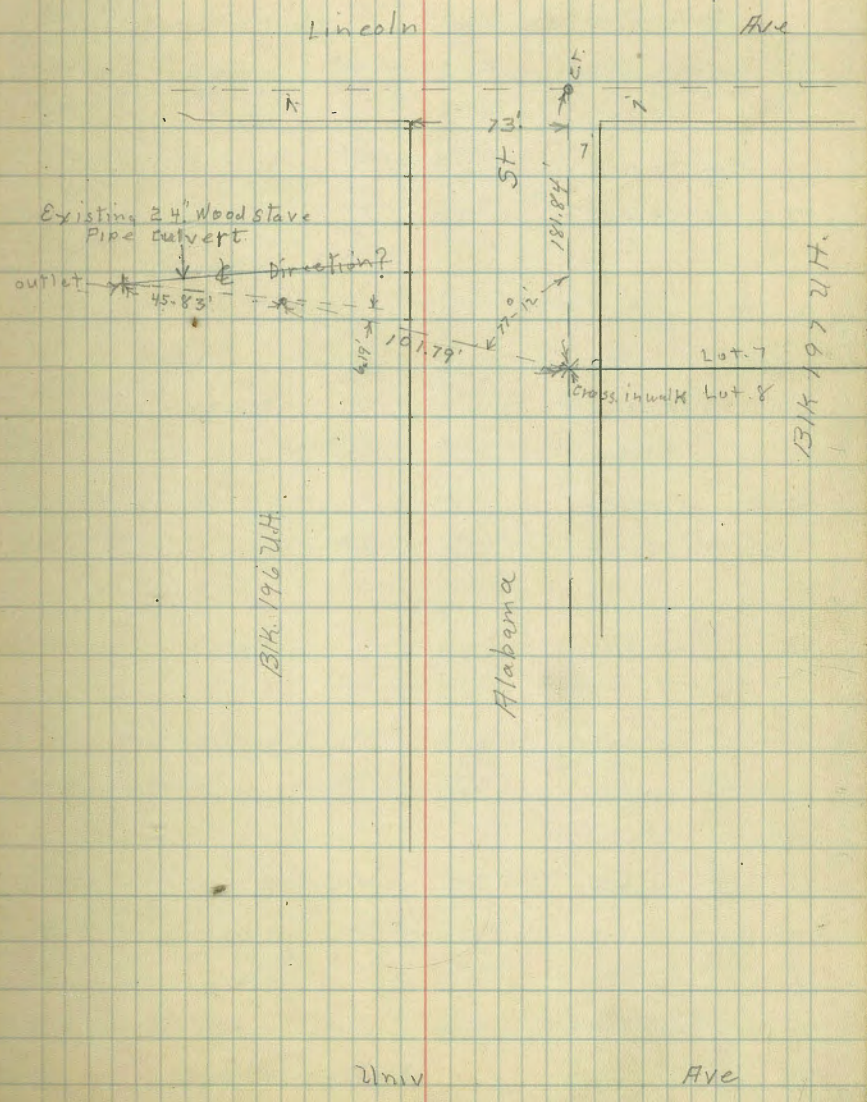
60

— B.M. Nails pole —	1.63	— 288.80 —	— 287.17 —
— T. P. —	2.64	— 283.08 —	— 8.36 — 286.44 —
0+00 = stub	on Line bet. Lots 7 & 8, Alley 17486 S. of S. Line Lincoln		2.64 280.44
0+10 = W. Line Alley		2.1	281.0
0+10.50 = 1' N. of N.E. Cor Garage		2.2	280.9
0+27.6 = 1' N. of N.W. "		3.4	279.7
0+50		3.7	279.4
1+00		3.9	279.2
1+25		4.1	279.0
1+49.95	Line Bet. Lots 7 & 8, E. Line Alabama		4.7 278.4
1+56.95	on cross. e. 7' Line		4.91 278.17
1+64 = E. curb line Top of		5.13	277.95
1+64 = E. " " gutter pav.		5.75	277.33
	S. on E. Curb line of Alabama.		
2+00 gutter		6.10	
2+50 "		6.76	
3+00 "		7.40	
3+48 "		8.13	
3+48 Top of ch. at apparent Brk.		7.27	275.81
— T. P. —	1.79	— 273.11 —	— 11.76 — 271.32 —
— ch. B.M. B.P. N. W. Univ + Alabama —	7.21	— 265.90 —	— 265.96 —



Location of Outlet. 24" Culvert
 In BIK. 196 Univ. Hts.
 See Page 69.

BM.				
Top of curb	3.21	281.16	277.95	sta. 1 + 64 Page 69
Outlet End. 24" Wood stave Pipe	20.16	261.00		



Moore
12-10-37.

XSCA Alley 20' wide
BIR 12 City Hts. Quarry #1
Bet. Highland + 45th
Dwight to Landis

Indexed
C-S.H.

353.31

71

NW 8P	4.94	353.31	348.37	Dwight 45th
0-14 N.C. Dwight				
curb NW Dwight	4.99	348.32	347.82	Top of
par. " " "	5.47	347.82	348.10	
E. Alley	5.31	348.10		
W.L. "	5.38	347.93		
Top of NE. 60'	Dwight Highland	5.77	347.54	
par. "	6.14	342.17		

W	2.9	350.4
0+66		
-7 SW gar cent. fl.	2.63	350.68
W	2.4	350.7
C	2.4	350.7
E	2.4	350.9
T.P.	5.72	350.66
2.37		350.94

0+00 NW Dwight		
W Top of	5.07	348.24
C	5.1	348.0
E ground	4.6	348.7
E Top of	5.08	348.23
0+10		
E	3.8	349.5
C	4.4	348.9
+6	4.3	349.0
W	3.8	349.5

0+82		
E-S S edge dble gar	5.57	351.09 cent fl.
E " Apron	5.77	350.89
C	5.5	351.2
W	5.4	351.3
0+98		
W	5.3	351.4
C	5.2	351.5
E Apron	5.52	351.14
E S edge gar.	5.51	351.15

0+30		
W	3.2	350.1
C	3.4	349.9
E	2.9	350.4
0+50		
E	2.9	350.4
C	3.0	350.3

1+08		
E-S SW gar cent.	5.51	351.15
E	5.4	351.3
C	5.3	351.4
W	5.1	351.6

356.66

1+50

W		5.2	351.8
C		4.8	351.9
E		5.1	351.6

1+60

E	-5 Singar cem.	4.85	351.81
E	apron "	5.13	351.53
C		4.9	351.8
W		5.2	351.5

1+90

-2	S.W. gar dirt	5.1	351.6
W		5.1	351.6
C		4.9	351.8
E		5.0	351.7

2+15

E		4.4	352.3
C		4.7	352.0
W		4.9	351.8

2+42

W	S edge gar cem	4.87	351.99
-4		4.72	351.84

3+60

-4	N edge gar, cem	4.60	352.06
W	apron "	4.69	351.92
C		4.8	351.9
E	S.W. gar cem	4.88	351.98

7 in. only

356.66

2+70

E	S.W. gar. dirt	4.70	351.96
---	----------------	------	--------

3+00

E		4.5	352.2
C		4.7	352.0
W		4.7	352.0

3+50

W		5.0	351.7
C		4.4	352.3
E		4.5	352.2

3+62

E		4.7	352.0
C		4.4	352.3
W		4.5	352.2

+4	S.W. gar. Cem	4.45	352.21
----	---------------	------	--------

4+00

W		4.1	352.6
C		4.9	351.7
E		5.2	351.5

4+20

E		4.8	351.9
C		4.9	351.8
W		4.6	352.1

+15	apron cem.	4.60	352.06
-----	------------	------	--------

+4	S.W. gar "	4.41	352.25
----	------------	------	--------

72

356.66

4+44

- 4	S. n. gar. cem.	4.44	352.22
W		4.9	351.8
C		4.9	351.9
E		5.0	351.2

4+93

E		5.0	351.1
C		5.4	351.2
W	apron cem.	4.68	351.98
+ 3	S. n. gar "	4.33	352.33

T.P. 3.10 354.25 5.51 351.15

5+56

- 35	S. n. gar. cem.		
W	E cem. ribbon	3.11	351.13
C		3.4	350.9
E		3.5	350.8
E + 4	E m	3.53	350.2

+ 35 S. n. gar. cem.

5+80

E		4.0	350.3
C		3.9	350.4
W		3.3	351.0

354.25

73

5+90

W		4.2	351.1
+ 6		4.5	349.8
C		4.6	349.7
E		4.3	350.0

4+00 = 5L Landis

E	cb top	6.43	347.82
C		5.0	348.7
W	cb "	5.57	348.68

6+14 5 cb 1, 2c Landis

W	^{9/10} top cb	5.84	348.41
E	" "	6.72	347.53 EST. Gr.
W	45. " "	11.33	342.92 343.0
"	" Pav.	11.75	342.50
E	L Highland cb.	1.44	352.83 352.90
"	" Pav.	1.98	352.27

Senior Levels
 PL 174-175
 P.35

MOORE
 1-17-38

74

106.32

	1.26	120.34	119.98	P.M.M.H.	54.50	14.7	91.6
T.P.	0:30	108.43	12.21	108.13	+75	15.9	90.4
					6	15.0	91.3
0+00	ground	1.2	107.2		T.P.	307	94.44
						12.95	93.37
+50		2.6	105.8				
1		4.2	104.2		6+30	7.8	88.6
+50		5.2	103.2		+60	13.2	83.2
2		6.9	101.5		+70	18.2	78.2
+25		11.2	97.2		+90	26.8	69.6
+76		20.6	87.8	?	+93	26.7	69.7
+65	bot. ravine	27.1	81.3		7+07	11.5	84.9
+80		20.5	87.9		+15	7.0	88.8
3		16.0	92.4		+30	4.9	91.5
+25		6.4	102.0		+50	4.6	91.8
+50		4.0	103.8		+75	11.9	84.5
					+85	14.1	82.3
T.P.	1.82	106.32	3.93	104.50	8	16.5	79.9
					+23	18.3	78.1
4+00		2.7	103.6		+42	4.0	92.4
+15	on pipe	4.31	102.01				
"	" Max. 437 E of pipe	5.37	100.95				
+50	on P.L.	8.5	97.8				
5+00	"	12.6	93.7				
+30	"	16.1	90.2				

Inst at Linda 1

Adm Tr - Theo Dome (1)	43°32' (12)	522°22'	43°31'50"
Theo Dome - Soledad	102°40'30" (12)	1232°05'15"	102°40'26"
U.H. Tank - Adm Tr (1)	71°55' (10)	719°11'45"	71°55'10"

Inst at Mission 1

Linda 2 - Linda 3 (1)	24°18' (6)	145°50'15"	24°18'22"
Linda 1 - Spire Old Miss (1)	96°43' (6)	580°16'	96°42'40"
Linda 2 - Ventilator Red Barn	43°37' (4)	174°29'	43°37'15"

Inst at Point on City line

Mission 1 - Linda 3	11°27'30" (6)	68°43'	11°27'10"
Linda 3 - Ventilator on red barn			143°36'30"

Inst at Mission 2

Mission 1 - Linda 2 (1)	26°08' (6)	156°47'30"	26°07'55"
Linda 2 - Linda 3 (1)	15°47' (6)	91°48'	15°47'10"
Linda 3 - Pt on City line	105°54' (6)	635°21'	105°53'30"
Linda 3 - Ventilator on Red barn	105°34' (A)	422°14'30"	105°33'38"

Inst at Mission 2

Mission 1 - Linda 1	(1)	21°57'30"	(6)	131°47'20"	21°57'53"
Linda 1 - Linda 2	(1)	4°10'30"	(6)	25°00'45"	4°10'07.5"
Linda 2 - Soledad	(1)	26°20'45"	(6)	158°04'	26°40'40"
Soledad - Chesterton Tank	(1)	50°14'	(6)	301°22'45"	50°13'47.5"
Chesterton Tank - Mission 3	(1)	64°54'	(6)	389°9'30"	64°53'15"
Linda 2 - ^{Spire} old Miss.	(1)	134°39'30"	(6)	807°56'45"	134°39'27.5"

Inst at Mission 3

Mission 1 - ^{Marston} Spire	(1)	2°43'20"	(6)	16°19'	2°43'10"
^{Marston} Spire - Soledad	(1)	44°08'40"	(6)	264°50'50"	44°08'28"
Soledad - ^{Chesterton} Tank	(1)	17°42'30"	(6)	106°14'50"	17°42'28"

Inst at Linda 2

Mission 1 - Mission 2	(1)	94°48'30"	(6)	568°50'	94°48'20"
Mission 1 - Linda 1	(1)	72°00'	(6)	431°57'50"	71°59'38"
^{Marston} Spire - Linda 1	(1)	48°17'	(6)	289°41'40"	48°16'56"
Mission 2 - ^{Old Mission} Spire	(1)	21°31'30"	(6)	129°08'	21°31'20"

Inst at Linda 1

Linda 2 - Miss. 1	(1)	58°05'	(6)	348°30'15"	58°05'02.5"
Chest. Water Tank - Linda 2	(1)	46°08'45"	(6)	276°53'50"	46°08'58"
M.B. Stack - Linda 2	(1)	90°53'30"	(4)	363°33'45"	90°53'26"

Inst at Linda 1

Adm Tr - Old Trc	(1)	22°53'10"	(16)	22°53'12.5"
Old Tr - Ben Mon	(1)	5°56'	(12)	5°56'27.5"
Ben Mon - "Mid"	(1)	6°48'40"	(12)	6°48'29.2"
Mid - Soledad	(1)	110°33'40"	(12)	110°33'07.5"
Adm Tr - Soledad	(1)	146°12'	(12)	146°12'05"

Inst at Linda 2

Old Tr - Ben Mon	(1)	6°30'30"	(12)	6°30'35"
Ben Mon - Theo. D.	(1)	15°06'	(12)	15°06'10"
Theo. D - Soledad	(1)	91°10'20"	(12)	91°10'37"
Old Tr - Soledad	(1)	112°47'20"	(12)	112°47'27"
Old Tr - ^{SPine} Marston M.	(1)	18°35'	(6)	18°35"
Old Tr - U.H. Tank	(1)	96°57'4"	(16)	96°57'11"
Old Tr - ^{Normal} Soledad	(1)	91°06'40"	(6)	91°06'15"
Old Tr - Linda 1	(1)	66°51'30"	(10)	66°51'42"

Inst at Mission 2

Linda 1 - Linda 2	(1)	49°56'	(6)	49°55'25"
Linda 2 - Mission 2	(1)	56°37'15"	(6)	56°37'03"
Linda 2 - Mission 3	(1)	52°32'	(6)	52°03'48"
Linda 1 - ^{Marston} spire	(1)	44°58'15"	(6)	44°58'08"
Soledad - Linda 1	(1)	6°02'50"	(6)	6°02'48"

Inst at Mission 2

93.50
187.00

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry marked in left column and top row. The number in body

IMPROVED TABLES

AND

INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add connection found in column of expansion. Degree of curve with a given length is found by dividing tangent (or external), opposite 1 by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg.	
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43	
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42	
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41	
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40	
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39	
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38	
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37	
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36	
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35	
55	192	.4231	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34	
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33	
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32	
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31	
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30	
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29	
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28	
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27	
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26	
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25	
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24	
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23	
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22	
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21	
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20	
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19	
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18	
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17	
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16	
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15	
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14	
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13	
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12	
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11	
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10	
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9	
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8	
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7	
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6	
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5	
85	962	11.4300	964	11.826	967	12.250	969	12.706	971	13.187	974	13.727	4	
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3	
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2	
88	994	28.636	9995	31.242	9996	34.368	997	38.189	997	42.964	9998	49.104	1	
89	9998	57.290	9999	68.760	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0	
60'	cos	50'	cos	50'	cos	40'	cos	30'	cos	20'	cos	10'	cos	deg.

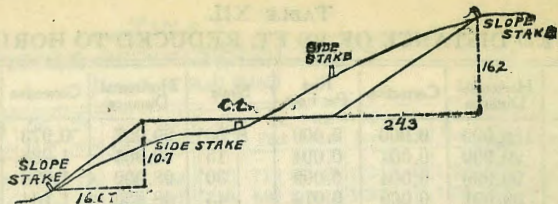
TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20

665.50
11.65
643.85



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

376.42
 50.00
 371.42

4.28
 58
 .11

392.29
387.04
326

20-37-30

332.0
319.
651.0

146.8

392.4
20.4

70+68⁸⁰
1+97⁶⁵
73+20⁹⁹
7258⁴⁵

296.2
20.2
326.4
390.38
384.54

283.98
281.44
2.54

27.6-1

N 7445
IV 1510
89.55
5882
7
581.2

7-10-30
5.35
440
6.7

Bill McCarthy

77+12.

555.
559.6

214-45
107-22-30

581.2
6.5
572.7

7712.51
13.63

7726.14
197.35

7923.49 E.C.

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4.

21
4
17

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7123.34

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77-48-30
38-39-15
79984

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47.10406

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425
13.80

54.23
2.28
55.55

43.3
28.7
72.0

94.30
32.06
626.36
26-47⁸⁰
2 24507⁴⁴
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24-19

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146.60

1030.5
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784.8
245.70
198.58
47.12

122
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14
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20.6
59.4
80.0