

1521



FIELD BOOK

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JAN 21 1965

Imperial Ave X Sec 32<sup>nd</sup> St. Fly - 1-24

Alley Blk-5 City Hts Annex No 2 <sup>44<sup>th</sup> & Fairmount</sup> Dwight & Myrtle 25-27

✓ ✓ 104 ✓ ✓ — <sup>48 - Van Dyke</sup> Myrtle & Thorn 28 to 31

✓ ✓ 6 Chester Park <sup>47 - Euclid</sup> Orange & El Cajon 32-35

✓ ✓ 65 W.P. Herberts <sup>39-40</sup> Meade & Monroe 36-38

Gamma St 38<sup>th</sup> to 43<sup>rd</sup> 39-50

Narragansett <sup>chatsworth to plum</sup> 55-63

Curb levels Lowell Westerly from plum 64-

Golden Gate Dr. 65

Alley Blk 13 <sup>39<sup>th</sup> & 40<sup>th</sup> orange</sup> Resub 20<sup>th</sup> Blk N Teralta <sup>dark</sup> 66

Drainage SE Cor. Mission & Mississippi 69

Ocean View Gardens Survey 70

Valle Citos Storm Drain La Jolla Shores 71-74

Alley Blk-F. McFadden & Duxford, 33 Park Villas 75

Pacific Highway 77

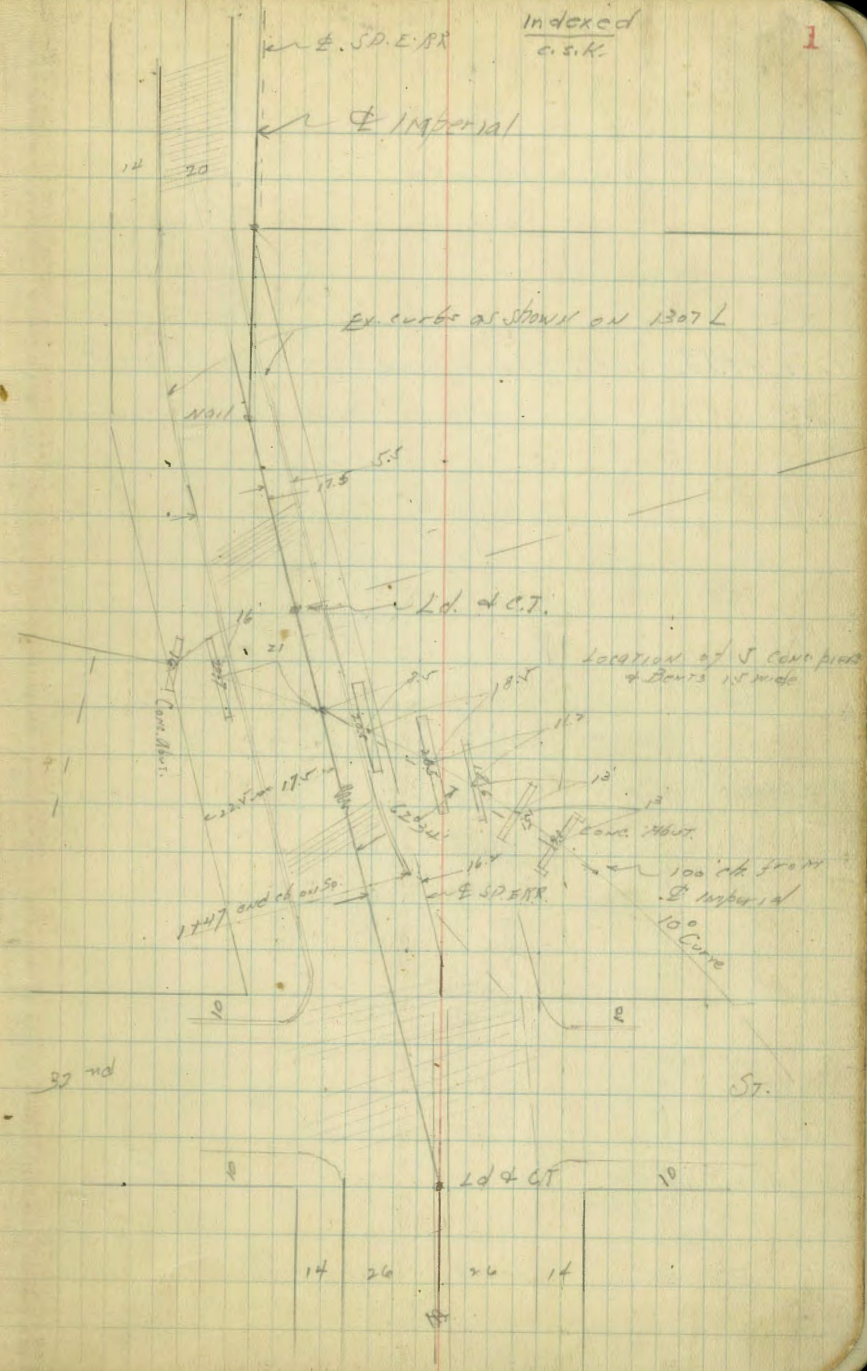
Imperial Ave. Cross Section  
 P.W. Est. Estimate.

Note: Ex. curbs paving etc 95 on 1307 L

5 + 26.03	EC	7° 40'	Nail
5		6° 25.32	$\Delta = N^{\circ} 20' RT$
+ 75		5° 13.70	$R = 600$
+ 50		4° 07.08	$T = 80.77$
+ 25		2° 50.46	$L = 160.57$
4		1° 38.84	2.8648
1		0° 27.27	

3 + 65.46 B.C. RT.  
 3 + 64.77 Int. of  $\Phi$  of Cuyamaca RR. xing  
 Ströl span over paving strip  
 overhead

0 + 00 14° 24' LT Wly of 32nd St.

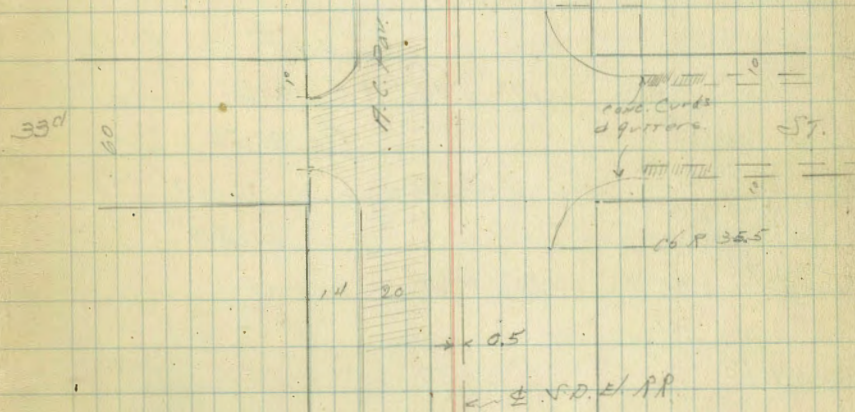


13 + 26.34 Ely edge bridge

17 + 49.59 Wly edge bridge & end SDEPR track

8 + 38.60 Wly of 33d S N

15 + 26.03 EC. nail



15 + 71.43 E.C. 23° 33.50

+50 20° 38.09

+25 17° 13.46

15 13° 48.83

+75 10° 24.20

+50 6° 59.57

14 + 25 3° 34.94

13 + 98.74 B.C. RT.

13 + 81.7

2 story Bldg in ST.

$A = 47^{\circ} 07' RT$

$ER = 210$

$T = 91.56$

$L = 172.69$

8.1851

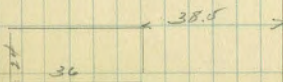
2497

Mon.

Note!

Part not widened as shown on plans.

Wall



20.4 RT.

19+87.26 EC 16° 36' 30"

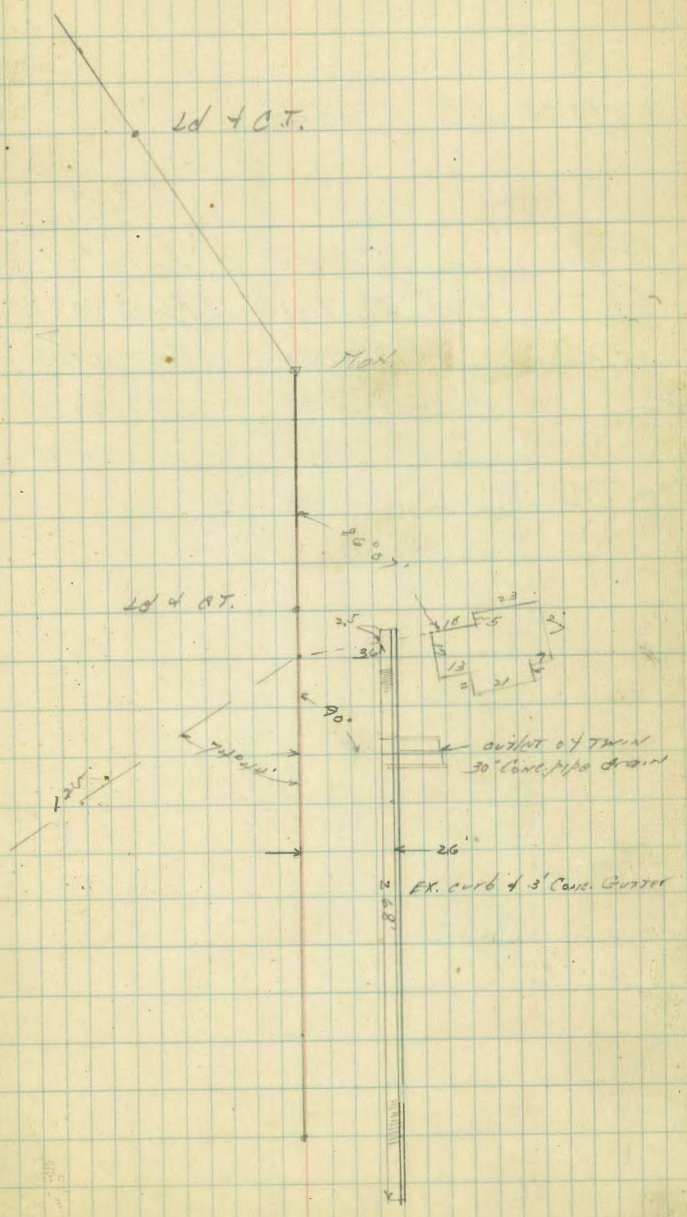
+75	15° 26.24	L = 33° 13' LT
+50	13° 03.00	R = 300
+25	10° 39.76	T = 89.48
19	8° 16.54	L = 173.94
+75	5° 53.28	V. 72.96
+50	3° 30.04	
+25	1° 06.80	

18+13.34 BC  
18+09.36 9/4 edge resistance in ST

17+69 ± outlet of drain

Net of twin 30" Conc. pipe drain  
See plans of Francis St.

15+71.43 EC



22+80.02 E.C.  $7^{\circ}00'40''$

+75  $6^{\circ}43.40$   $A=14^{\circ}01'20''$  LT.

+50  $5^{\circ}17.46$   $R=500$

+25  $3^{\circ}51.52$   $T=61.49$

22  $2^{\circ}25.58$   $L=122.37$

+75  $0^{\circ}59.64$   $3.4377$

21+57.65 B.C. LT.

40. + C.T.

2d + C.T.

19+87.26 E.C.



26 + 35.42 EC. 29° 19' 30"

+ 25 27° 09.24 Δ = 58° 39' RT

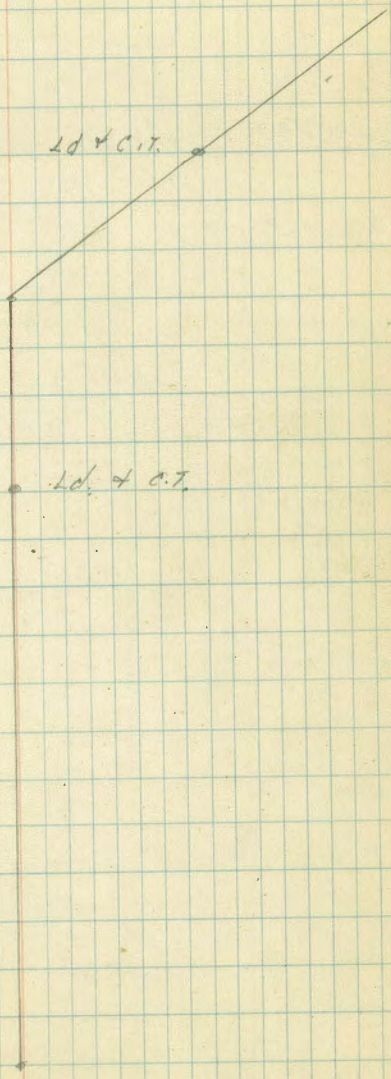
26 21° 56.75 QR = 137.52

+ 75 16° 44.28 T = 77.25

+ 50 11° 31.81 L = 142.77

25 + 25 6° 19.34 12.499

24 + 94.65 BC RT. ch = 496



22 + 8002 EC.

29+89.75 Wly Jewish Cem.

29+67.25 EC.

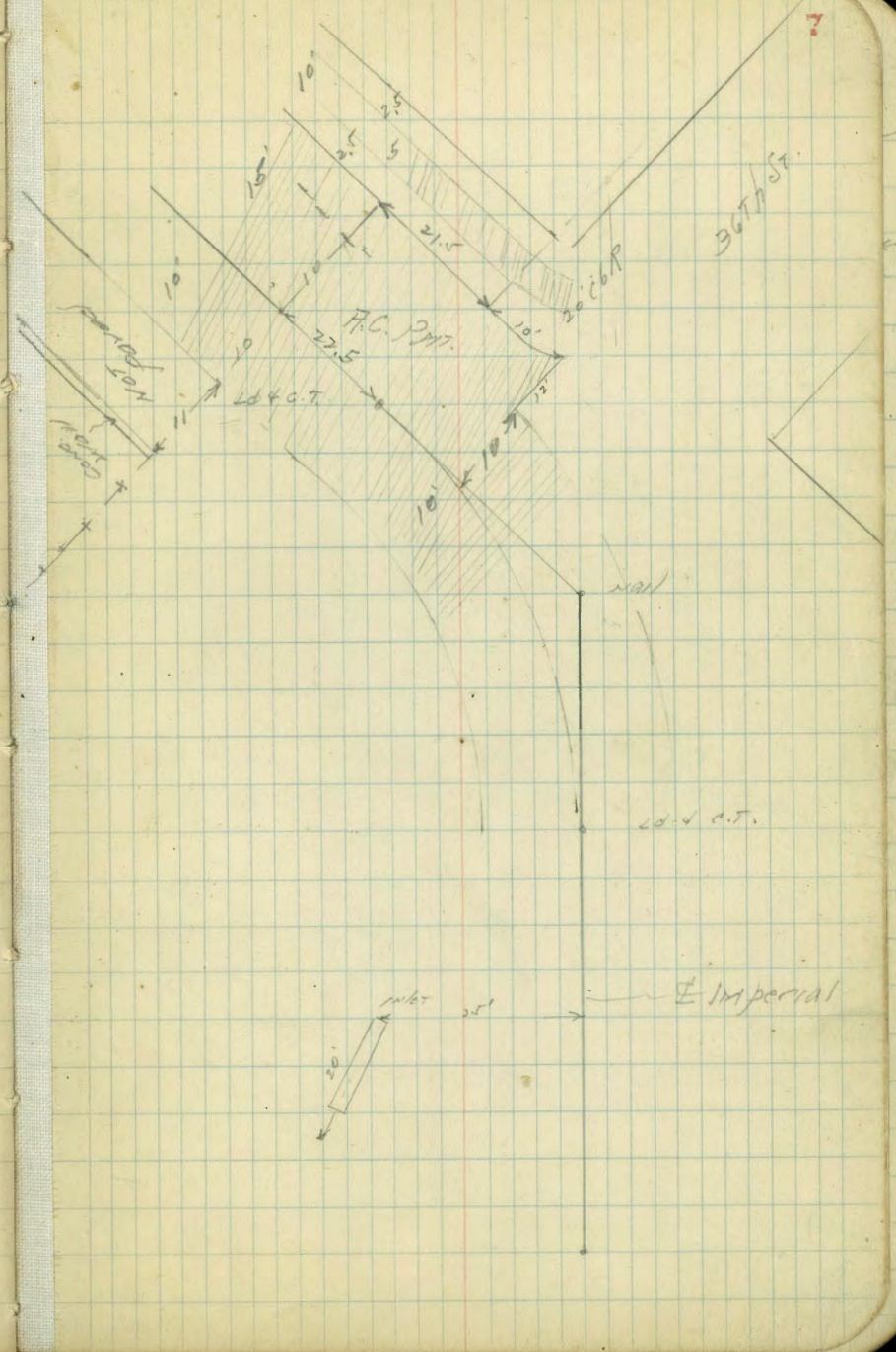
$R 59^{\circ} 03' LT.$   
 $\Delta P 123.24$   
 $T 69.91$   
 $L 127.11$

Jewish Cem.

28+40.14 B.C. LT.

27+50 24" I.P. drain by St. Dept.

26+35.42 ES.



Imperial Fire  
Cross Sections  
32nd to 36th

✓ +47 deg. of or 50.

700.

0+62

0+61.95 = Ely line 32nd

0+51.62 = Ely of 32nd

0+30.97 = E 32nd

0+00 = NWly 32nd St

Note:  
Section to 0+13  
Taken parallel to 32nd

NW/3P 3.30 70.33

07.03 1146.4  
32nd

67.23	66.78	67.01	66.88	67.01	66.88	67.23	66.78	67.01	66.88	67.23	66.78	67.01	66.88
65.33	66.37	66.31	66.48	66.31	66.48	65.33	66.37	66.31	66.48	65.33	66.37	66.31	66.48
64.33	66.17	66.17	66.48	66.17	66.48	64.33	66.17	66.17	66.48	64.33	66.17	66.17	66.48
63.53	65.82	66.78	66.44	66.78	66.44	63.53	65.82	66.78	66.44	63.53	65.82	66.78	66.44
63.10	65.76	67.03	66.46	67.03	66.46	63.10	65.76	67.03	66.46	63.10	65.76	67.03	66.46
62.58	65.77	66.91	66.52	66.91	66.52	62.58	65.77	66.91	66.52	62.58	65.77	66.91	66.52
62.70	65.38	66.37	66.60	66.37	66.60	62.70	65.38	66.37	66.60	62.70	65.38	66.37	66.60
59.07	65.89	66.91	66.60	66.91	66.60	59.07	65.89	66.91	66.60	59.07	65.89	66.91	66.60
58.47	65.03	66.03	66.63	66.03	66.63	58.47	65.03	66.03	66.63	58.47	65.03	66.03	66.63
58.81	65.43	66.91	66.63	66.91	66.63	58.81	65.43	66.91	66.63	58.81	65.43	66.91	66.63
59.03	65.03	66.91	66.60	66.91	66.60	59.03	65.03	66.91	66.60	59.03	65.03	66.91	66.60
58.68	65.03	66.91	66.60	66.91	66.60	58.68	65.03	66.91	66.60	58.68	65.03	66.91	66.60
58.73	65.03	66.91	66.60	66.91	66.60	58.73	65.03	66.91	66.60	58.73	65.03	66.91	66.60
59.33	65.03	66.91	66.60	66.91	66.60	59.33	65.03	66.91	66.60	59.33	65.03	66.91	66.60
68.33	65.03	66.91	66.60	66.91	66.60	68.33	65.03	66.91	66.60	68.33	65.03	66.91	66.60

3 +64.77 Taken on 2 of Overhead

+50

+25

2+00

T.P. 286 4971 1214 46.85

+50

2+00

T.P. 0.87 59.01 1219 58.14  
70.33

62.81	58.41	53.71	44.01	44.18	43.57	44.01	43.86	44.14	44.06	42.61	42.51	43.01	57.41
+13.1 40	+9.5 33	00 31	7.0 24	7.0 24	7.5 24	7.5 24	7.5 24	7.5 24	7.5 24	7.5 24	7.5 24	7.5 24	7.5 24
57.23	57.23	57.23	57.23	57.23	57.23	57.23	57.23	57.23	57.23	57.23	57.23	57.23	57.23
+7.87													

60.41	59.71	50.31	50.11	49.57	49.31	49.71	50.08	50.01	50.01	58.21	73.11
+1.4 40	+0.7 31	8.7 23	8.90 17.5 65	9.2 17.5 65	9.7 17.5 65	9.7 17.5 65	9.7 17.5 65	9.7 17.5 65	9.7 17.5 65	9.7 17.5 65	9.7 17.5 65
58.01	58.01	54.61	54.46	53.91	54.18	54.05	54.39	54.84	54.81	59.91	60.44
1.0 40	1.0 31	2.4 23	2.4 17.5 65	5.10 17.5 65	4.83 17.5 65	4.96 17.5 65	4.64 17.5 65	4.27 17.5 65	4.24 17.5 65	4.24 17.5 65	4.24 17.5 65

√+26.03 EC end cb on So.

√+00

1.71 39.70 11.7x 37.99

27.40	28.00	37.50	37.60	37.85	37.40	36.90	37.30	37.10	37.29	37.00	39.30	40.30
14.5	5	28	29	32.5	32.5	32.8	32.3	32.5	32.6	1.7	0.9	
5	20	36	36	36	36	36	36	36	36	36	40	
				9ut	9ut	9ut	9ut	9ut	9ut	9ut		
				cb	cb	cb	cb	cb	cb	cb		

27.51	37.31	38.11	38.31	37.81	37.77	38.71	37.91	38.95	32.91	40.71	41.51	
22.2	12.4	11.6	11.40	11.90	11.94	11.60	11.8	11.66	11.5	9.0	8.2	
60	40	38	38	38	38	38	38	38	38	38	40	
			9ut	9ut	9ut	9ut	9ut	9ut	9ut	9ut	9ut	
			cb	cb	cb	cb	cb	cb	cb	cb	cb	
33.61	36.51	39.41	39.18	38.49	38.78	39.11	39.00	39.11	41.31	40.71		
16.1	13.2	10.3	10.53	11.27	10.93	10.60	10.71	10.71	10.2	9.0		
50	40	38	38	38	38	38	38	38	38	38		
			9ut	9ut	9ut	9ut	9ut	9ut	9ut	9ut		
			cb	cb	cb	cb	cb	cb	cb	cb		
43.11	42.21	40.11	39.93	39.21	39.65	39.61	39.91	39.71	39.71	43.91	44.51	
66	27	26	26.576	26.576	26.576	26.576	26.576	26.576	26.576	26.576	26.576	
			9ut	9ut	9ut	9ut	9ut	9ut	9ut	9ut	9ut	
			cb	cb	cb	cb	cb	cb	cb	cb	cb	
53.71	55.31	47.11	40.71	40.68	40.17	40.49	40.35	40.64	40.58	40.61	46.11	46.41
4.0	5.6	2.6	9.0	9.03	9.14	9.24	9.36	9.07	9.12	9.1	5.6	5.6
40	34	31	38	38	38	38	38	38	38	38	40	40
				9ut	9ut	9ut	9ut	9ut	9ut	9ut	9ut	9ut
				cb	cb	cb	cb	cb	cb	cb	cb	cb
42.51	61.41	42.41	41.94	41.41	41.76	41.58	41.74	41.87	41.71	50.71		
12.8	11.7	7.3	7.77	8.30	8.30	8.30	8.30	8.30	8.30	8.30	8.30	
40	33	27	33	33	33	33	33	33	33	33	40	
			9ut	9ut	9ut	9ut	9ut	9ut	9ut	9ut	9ut	
			cb	cb	cb	cb	cb	cb	cb	cb	cb	

+√

+√0

+2√

√+00

3+65.46 BC

49.71

49.71

T.P. 1.99 31.06 10.63 29.07

8

W0

7+00

6+50

+95

+75

5+50

15.6	15.6	24.10	24.10	24.10	24.10
15.4	15.4	24.40	24.30	24.30	27.50
15.2	15.2	31.50	30.10	30.10	29.10
15.1	15.1	31.90	30.45	30.45	29.04
15.0	15.0	31.46	30.00	30.00	28.63
14.9	14.9	31.65	30.25	30.25	28.80
14.8	14.8	31.50	30.15	30.15	28.77
14.7	14.7	31.10	29.80	29.80	28.60
14.6	14.6	31.60	30.00	30.00	28.60
14.5	14.5	31.70	30.10	30.10	28.80
14.4	14.4	23.20	23.10	23.10	24.80
14.3	14.3	23.20	23.10	23.10	24.20
14.2	14.2	22.90	23.10	23.10	24.00
14.1	14.1	23.40	23.40	23.40	
14.0	14.0	23.40	23.40	23.40	
13.9	13.9	32.25	32.25	32.25	
13.8	13.8	32.75	32.75	32.75	
13.7	13.7	32.75	32.75	32.75	
13.6	13.6	32.50	32.50	32.50	
13.5	13.5	32.60	32.60	32.60	
13.4	13.4	33.30	33.30	33.30	
13.3	13.3	24.40	24.40	24.40	
13.2	13.2	23.60	23.60	23.60	
13.1	13.1	23.40	23.40	23.40	
13.0	13.0	23.40	23.40	23.40	
12.9	12.9	26.50	26.50	26.50	
12.8	12.8	25.90	25.90	25.90	
12.7	12.7	24.70	24.70	24.70	
12.6	12.6				
12.5	12.5				
12.4	12.4				
12.3	12.3				
12.2	12.2				
12.1	12.1				
12.0	12.0				

39.70

39.70



check to BP  
N side  
Bridge

T.P.	3.50	32.38	2.77	29.61	29.57
			2.18	28.88	

IX

+50

X

+50

+39

9 +50

31.06

4.7	26.36	4.7	25.96	4.7	25.96	4.7	24.26	4.7	23.86
4.8	26.75	4.8	26.22	4.8	26.22	4.8	25.46	4.8	24.26
4.8	26.25	4.8	26.45	4.8	26.45	4.8	26.56	4.8	27.66
4.8	26.51	4.8	25.91	4.8	25.91	4.8	26.85	4.8	27.96
4.8	26.61	4.8	26.36	4.8	26.36	4.8	26.39	4.8	27.51
4.8	26.55	4.8	26.36	4.8	26.36	4.8	26.84	4.8	27.94
4.8	26.56	4.8	26.26	4.8	26.26	4.8	26.86	4.8	27.85
4.8	26.46	4.8	25.86	4.8	25.86	4.8	26.46	4.8	27.76
4.8	27.96	4.8	26.26	4.8	26.26	4.8	26.86	4.8	27.56
4.8	28.36	4.8	25.06	4.8	25.06	4.8	26.06	4.8	23.76
4.8	23.36	4.8	23.76	4.8	23.76	4.8	24.46	4.8	23.06
4.8	23.36	4.8	23.56	4.8	23.56	4.8	24.46	4.8	23.06

31.06

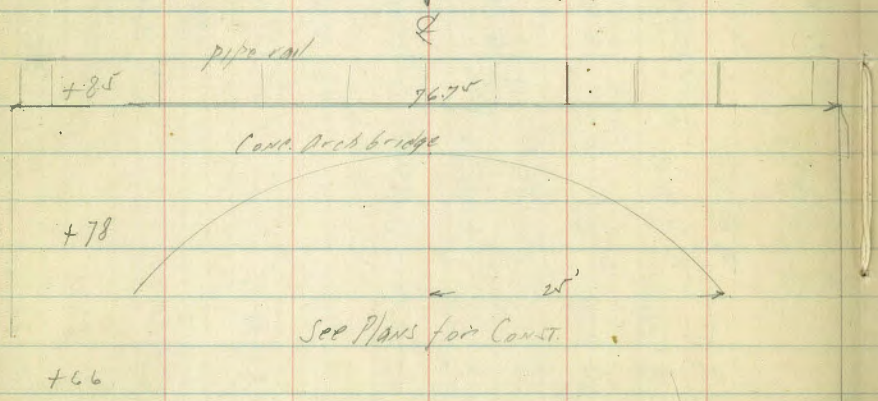


13 + 26.34 Fly and Conc. Arch bridge

+14

13 + 40.5

+88.96 Bridge Conc. Arch



12 + 49.59 Fly and bridge

37.38

8.3	24.08
4.2	
2.0	22.38
Total Conc. Wall	

41.70	25.38	41.70	22.98
37.2	29.76	37.2	23.98
30.2	28.88	31	26.08
26.75	28.63	30	27.58
23.25	28.55	27	28.68
20.0	28.50	26	28.72
16.75	28.55	25	28.67
13.5	28.68	24	28.58
10.25	28.68	23	29.58
7.0	29.78	22	25.58
3.75	25.08	21	21.08
0.5	22.38	20	20.08
0.0	22.38	19	19.88
0.0	21.58	18	19.88

15

+75

+50

14 + 25

13 + 98.74 BC

+50

T.P. of bridge 327

13 x 27

*this curve not indicated as Max Shores*

32.88 2.77 29.61

32.38

21/50	25.78	26.08	26.98	27.48	27.48	26.68	29.68
70/40	25.88	26.98	27.95	27.55	27.18	27.48	27.48
65/50	26.78	27.33	27.33	26.78	26.31	27.18	27.36
59/40	26.68	27.18	27.18	26.68	26.28	26.45	26.78
49/50	26.38	27.58	27.58	25.98	25.98	26.36	26.45
45/40	23.48	22.88	22.88	24.18	24.18	26.18	26.38
40/50	22.88	22.08	22.08	22.88	23.38	25.48	25.98
38/50	23.38	22.78	22.78	23.38	23.38	25.48	25.98
38/50	24.98	27.08	28.58	28.58	28.58	27.18	27.18
38/50	28.58	28.58	28.18	28.18	28.18	26.45	26.78
32/50	32.58	32.58	28.08	21.78	21.78	26.18	26.38
32/50	32.38	32.38	20.68	20.68	20.68	25.48	25.98

+22

17

+50

16

N. + 7143 EC Pay 20 wide + end from here on

+50

+44

N + 25

37.88

32.88

34.18	35.98	35.88	35.28	34.48	30.18	25.08
1.3	1.3	1.0	1.4	1.6	1.7	1.8
40	40	40	40	40	40	40
27.88	28.47	28.28	28.08	28.28	28.68	25.08
1.0	1.6	1.8	1.8	1.6	1.4	1.8
40	40	40	40	40	40	40
27.43	27.48	27.53	27.59	27.78	28.11	29.38
1.45	1.35	1.39	1.39	1.20	1.27	1.5
40	40	40	40	40	40	40
27.08	27.37	27.48	27.65	27.91	28.22	
1.80	1.40	1.46	1.45	1.47	1.66	
40	40	40	40	40	40	
26.78	27.05	27.18	27.45	27.86	28.11	
1.10	1.70	1.40	1.45	1.67	1.27	
40	40	40	40	40	40	
26.58	26.87	26.93	27.11	27.47	27.83	
1.10	1.60	1.57	1.60	1.41	1.05	
40	40	40	40	40	40	
26.68	27.23	27.42	27.62	27.88	27.73	
1.10	1.26	1.26	1.26	1.56	1.14	
40	40	40	40	40	40	
	27.68	27.78	27.18	26.88	28.38	
	1.10	1.10	1.10	1.10	1.10	
	40	40	40	40	40	
	26.68	26.78	26.88	26.98	27.08	
	1.10	1.10	1.10	1.10	1.10	
	40	40	40	40	40	
	26.18	26.28	26.38	26.48	26.58	
	1.10	1.10	1.10	1.10	1.10	
	40	40	40	40	40	

1.70 NW end curb on West

Driveway 70' x 10' 50'



20

+ 87.36 EC

+ 75

+ 50

+ 25

19

+ 75

18 + 50

42.00

42.00

10.2	9.8	9.3	8.5	6.70	6.2	6.35	6.1	5.1	4.3
40	40	40	40	10	10	10	10	10	10
31.80	32.20	32.70	35.50	35.30	35.58	35.68	35.60	40.30	41.70
Nudge road									
10.2	9.8	9.3	8.5	6.70	6.2	6.35	6.1	5.1	4.3
40	40	40	40	10	10	10	10	10	10
31.80	32.20	32.70	35.50	35.30	35.58	35.68	35.60	40.30	41.70
Nudge road									
9.9	9.1	8.3	7.4	7.2	7.1	7.7	7.7	7.7	7.7
40	40	40	40	10	10	10	10	10	10
31.40	32.00	32.15	32.77	32.98	33.60	33.00	33.20	33.20	32.60
Nudge road front of Granite Co.									
10.4	10.0	9.4	8.2	9.2	9.2	9.2	9.2	9.2	9.2
40	40	40	40	10	10	10	10	10	10
31.00	31.00	30.97	31.58	31.82	31.82	31.82	31.82	31.82	31.30
11.0	11.0	11.03	10.42	10.18	10.2	10.2	10.2	10.2	10.2
40	40	40	40	10	10	10	10	10	10
30.10	31.00	30.97	30.56	30.80	31.40	28.80	28.90	28.50	28.50
11.4	11.4	11.41	11.20	11.30	11.30	11.30	11.30	11.30	11.30
40	40	40	40	10	10	10	10	10	10
29.50	29.50	29.25	29.84	30.20	30.70	27.60	27.40	27.40	27.40
12.5	12.5	12.5	12.16	12.50	11.3	10.2	12.6	14.6	14.6
40	40	40	40	10	10	10	10	10	10
29.60	29.10	28.78	29.40	29.67	30.00	26.90	25.90	25.50	25.50
13.2	13.2	13.2	13.60	13.2	13.2	15.1	16.1	15.6	15.6
40	40	40	40	10	10	10	10	10	10
29.60	29.10	28.78	29.40	29.67	30.00	26.90	25.90	25.50	25.50

+25

22

+75

+57.65 BC

+20

21

T.P.

12.20

53.67

053

41.47

20+50

42.00

31.40	30.27	29.47	29.67	30.17
10.6 50	23.2 50	24.2 44	24.0 72	23.5 75
31.40	30.47	29.47	29.37	29.67
10.6 50	23.2 50	24.2 46	24.0 72	23.5 75
31.60	30.47	32.87	46.67	33.37
10.6 50	23.2 50	24.2 40	24.0 72	23.5 75
38.30	41.47	45.77	47.49	48.67
37 24	12.2 20	17 21	17.0 20	15.0 20
38.58	41.57	46.01	47.84	48.92
34.4 10	12.10 10	7.66 10	6.18 10	4.2 10
38.67	41.81	46.36	47.84	49.39
3.33	11.86	7.31	7.33	4.38
38.66	41.69	46.39	47.99	49.49
33.2 10	11.98 10	2.38 10	5.63 10	11.8 10
38.20	41.87	45.77	47.67	49.37
3.8 20	11.3 20	7.9 12	6.0 10	4.5 10
38.30	55.27	59.87	56.17	63.27
3.7 32	16 40	14.2 28	12.2 28	9.6 20
42.60	61.07	60.87	62.57	68.97
10.6 40	27 40	17.2 40	18.7 40	19.6 40

20' edge  
20' road

20' edge  
20' road

20' edge  
20' road

20' edge  
20' road

20' edge  
20' road

42.00

J.P. 12.79 78.15 0.57 6536

+50

22

+50

22

J.P. 12.79 65.93 0.53 5314

+80.0v EC.

22 +50

53.67

39.73	39.28	52.83	63.13	62.96	62.91	62.65	61.93	72.43	77.93
$\frac{26.2}{78}$	$\frac{24.3}{60}$	$\frac{13.1}{45}$	$\frac{21.8}{18}$	$\frac{2.97}{10}$	30v	$\frac{52.8}{10}$	$\frac{4.0}{21}$	$\frac{4.65}{31}$	$\frac{+12.0}{40}$
N. edge 1000									
37.23	37.43	48.63	59.63	59.75	59.82	59.66	59.23	75.13	77.93
$\frac{28.7}{75}$	$\frac{28.5}{54}$	$\frac{23.3}{48}$	$\frac{6.3}{17}$	$\frac{6.8}{10}$	6.1	$\frac{62.7}{10}$	$\frac{6.7}{18}$	$\frac{19.2}{36}$	$\frac{+12.0}{40}$
N. edge 1000									
34.43	34.53	37.43	55.43	56.62	56.75	56.60	56.03	74.63	
$\frac{31.5}{75}$	$\frac{31.4}{54}$	$\frac{28.5}{48}$	$\frac{10.5}{20}$	$\frac{11.1}{10}$	9.18	$\frac{9.32}{10}$	$\frac{9.9}{17}$	$\frac{+8.7}{40}$	
N. edge 1000									
32.73	32.93	34.73	52.93	53.54	53.79	53.81	53.53	63.73	70.13
$\frac{33.2}{75}$	$\frac{33.0}{54}$	$\frac{31.2}{48}$	$\frac{18.0}{20}$	$\frac{12.9}{10}$	12.14	$\frac{12.2}{10}$	$\frac{12.4}{18}$	$\frac{12.2}{36}$	$\frac{+4.0}{40}$
N. edge 1000									

31.87	30.37	32.97	51.87	52.46	52.43	52.62	52.67	62.67	68.07
$\frac{21.8}{75}$	$\frac{22.6}{53}$	$\frac{20.7}{46}$	$\frac{11.6}{10}$	$\frac{11.1}{10}$	10	$\frac{10.5}{10}$	$\frac{11.0}{20}$	$\frac{+9.0}{30}$	$\frac{+14.4}{40}$
N. edge 1000									
30.77	30.37	35.27	50.07	50.55	50.88	51.00	50.97	65.97	
$\frac{22.9}{75}$	$\frac{23.6}{53}$	$\frac{18.4}{46}$	$\frac{6.6}{20}$	$\frac{3.12}{10}$	2.9	$\frac{2.67}{10}$	$\frac{2.1}{20}$	$\frac{+12.3}{40}$	
N. edge 1000									

53.67

+50

+35. 1/2 EC

+25

26

+75

+50

25 + 25 Curve widened on inside

25 + 94.65 BC

78.15

78.15

37.0	41.15	51.55	55.95	58.15	58.15
80	41.05	58.65	60.85	56.55	20.0
29.0	50.15	68.65	67.15	65.75	13.0
50	54.05	71.95	74.05	74.55	13.0
41	66.45	73.15	73.95	74.45	2.90
40	66.13	72.75	73.87	74.40	2.90
1020	65.98	72.50	73.18	73.81	75.25
10.20	65.43	71.72	72.85	73.35	74.82
10.90	64.35	71.25	72.85	73.35	74.25
11.1	60.15	87.35	84.25	83.35	80.95
11.1	86.15	87.45	85.85	86.15	86.95
10.20	81.85	87.45	85.85	86.15	86.95



T.P. 953 9964 032 90.11

+75

+50 Curve widened out inside

+40.4 BC.

28

+50

1.7	87.53	86.13	76.23	72.43	18.0	60	72.43	1.7	87.53	86.13	76.23	72.43	18.0	60
4.0					17.4	40	73.03	1.5	87.23	86.93	76.83	73.03	17.4	40
1.7					9.5	30	80.93	1.2	86.23	87.03	84.23	80.93	9.5	30
1.5					11.5	21	78.93	1.1	85.33	85.33	83.23	78.93	11.5	21
1.2					9.7	21	80.73	1.1	86.26	86.26	84.06	80.73	9.7	21
1.0					9.33	10.3	81.10	1.1	87.03	87.03	84.38	81.10	9.33	10.3
1.0					9.1	9.1	81.29	1.1	87.28	87.28	84.32	81.29	9.1	9.1
1.0					9.25	9.7	81.18	1.1	87.66	87.66	84.13	81.18	9.25	9.7
1.0					9.5	16	80.93	1.1	87.63	87.63	84.13	80.93	9.5	16
1.0					6.4	25	87.03	1.1	82.03	82.03	88.43	87.03	6.4	25
1.0					10.2	40	90.63	1.1	94.93	94.93	95.13	90.63	10.2	40
1.0					8.7	40	94.43	1.1	94.43	94.43	95.43	94.43	8.7	40

4.0 of 1.000 drain

T.P. 12.70 90.43 042 77.73

29

78.15

1.6	65.55	78.10	77.98	77.15	85.15	86.85	12.6	65	65.55	78.10	77.98	77.15	85.15	86.85	12.6	65
1.6							9.6	44	68.55	78.10	77.98	77.15	85.15	86.85	12.6	65
1.6							9.2	27	77.95	78.10	77.98	77.15	85.15	86.85	12.6	65
1.6							10.4	10.4	78.10	78.10	77.98	77.15	85.15	86.85	12.6	65
1.6							0.0	0.0	78.15	78.15	77.98	77.15	85.15	86.85	12.6	65
1.6							0.7	9.7	77.98	78.15	77.98	77.15	85.15	86.85	12.6	65
1.6							1.0	16	77.15	78.15	77.98	77.15	85.15	86.85	12.6	65
1.6							7.0	30	85.15	78.15	77.98	77.15	85.15	86.85	12.6	65
1.6							8.7	40	86.85	78.15	77.98	77.15	85.15	86.85	12.6	65

78.15

Chart SEBP  
Imp. + Sour. 4/100k

1.09 97.95 97.91  
0.04 error

29 + 89.75 = Wly Int Jewish Cemetery

+ 67.25 EC

+ 50

+ 41.5

+ 25

29

99.64

10.2 40	89.44	91.84	7.2 40	92.44	2.46 21	95.18
9.25 40	90.14	92.74	6.1 40	93.54	5.1 21	94.54
10.2 40	89.34	92.14	6.2 40	93.04	4.96 21	94.68
9.25 40	89.70	92.74	5.38 40	93.76	4.56 21	95.08
9.06 40	90.58	93.17	5.25 40	94.09		
9.25 40	90.87	93.27	5.26 40	94.08		
9.1 40	91.54	93.64	5.42 40	94.22		
9.06 40	93.64	94.14	5.70 40	94.14		
			5.95 40			
			6.00 40			
			6.37 40			
			6.57 40			
			6.90 40			
			7.15 40			
			7.25 40			
			7.5 40			
			7.8 40			

Top Comp  
Wol

OUT IN BRIND IN  
TO ALL STR

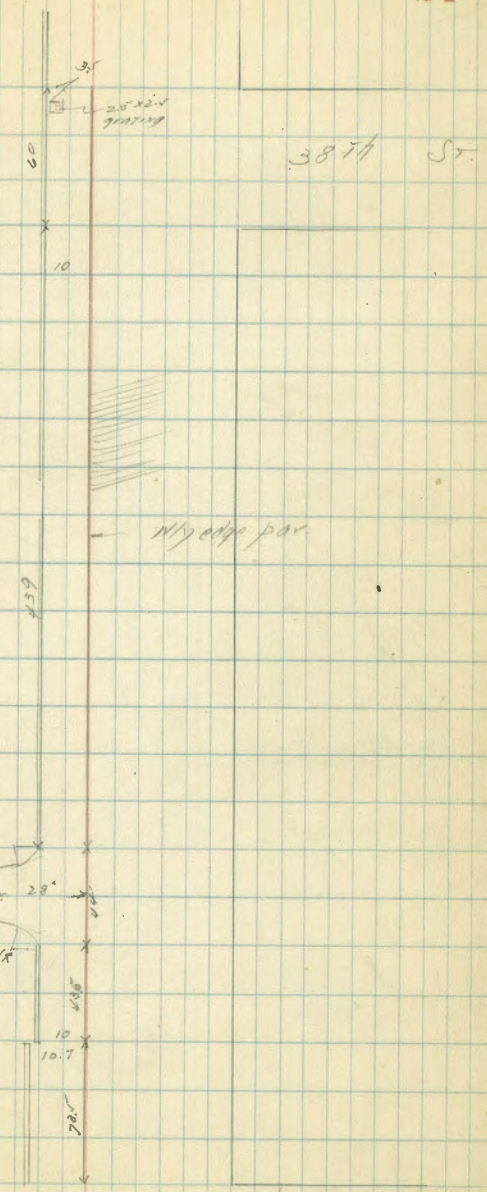
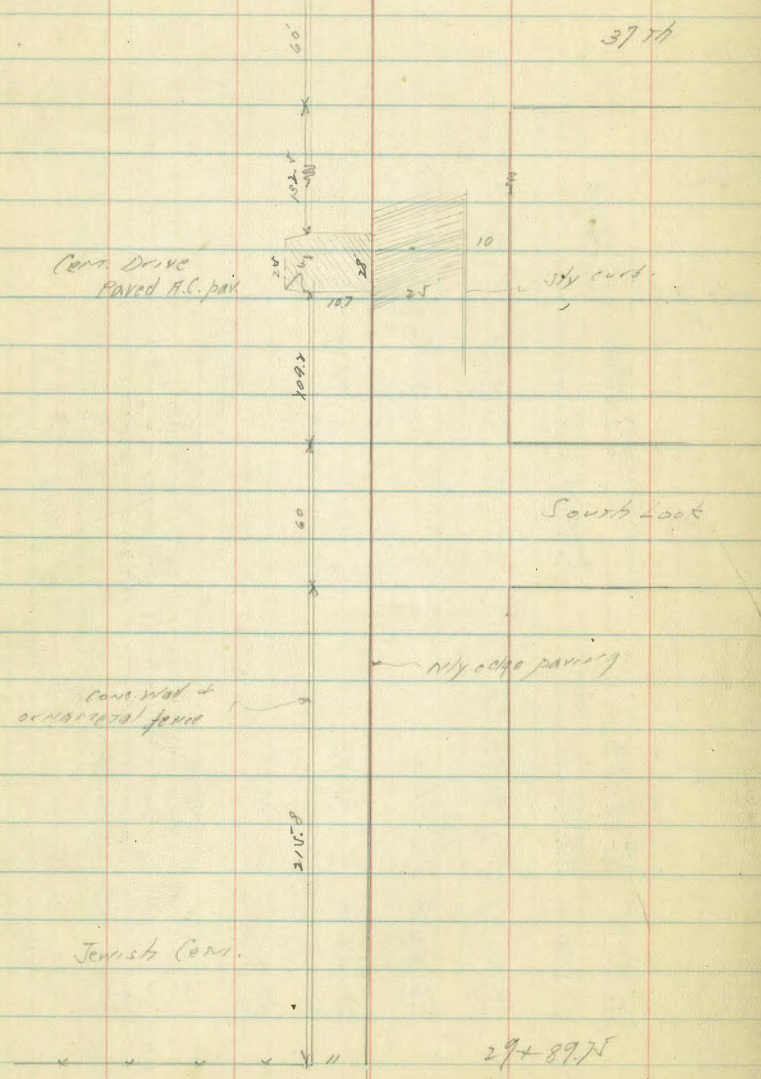
Top curb

End of  
return

99.64

Proposed paving of  
 strip between Curatory Wall &  
 Nly edge of Ex. paving on  
 Imperial Ave. 36<sup>th</sup> Ely.

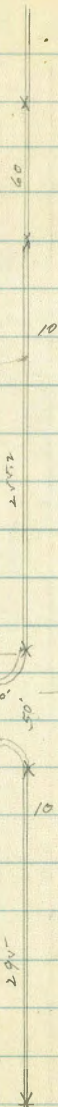
Indexed  
 c-S.K.



37th St.

39th

Conc. wall  
wire fence



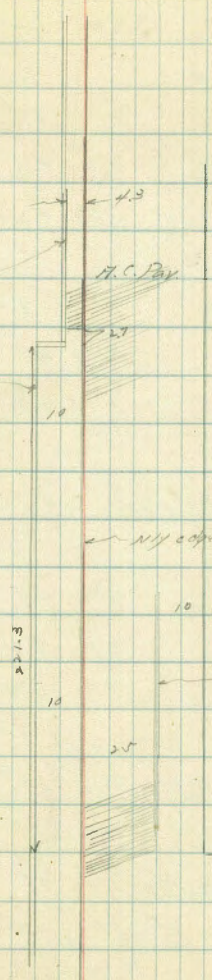
Mt. Hope Entrance



My edge paving

38th St.

Concrete wall



My edge paving

sidewalk

39th St

Moore  
1-27-36

X SEC alley 20' wide  
bet. Dwyer & Fairmont. and  
Dwyer & Myrtle. = NOT paved.  
BIR-5 C.Hts. Annex Ho. 2

Indexed  
C.S.K.

346.22

26

NWBP 533 346.22 340.89 Dwight Fairmont

SL Dwight = 00

W Top cb 4.45 341.77

C 4.4 341.8

E 4.20 342.02

0+10

E 3.5 342.7

C 4.1 342.1

W 3.8 342.4

0+19

E - 1<sup>st</sup> Sin. gar. corr floor 3.70 342.52

0+50

W 4.8 341.4

C 4.4 341.8

E 4.2 342.0

0+65

W - 9 Sin. gar corr floor 4.79 341.43

0+80

W - 8 Sin. gar. Floor (corr) 4.95 341.27

W - 9<sup>th</sup> Sin. gar. corr floor 4.72 341.50

1+00

E 4.8 341.4

C 4.7 341.5

W 5.1 341.1

1+26

W ONLINE Sin. gar. corr floor 4.67 341.55

1+50

W 5.0 341.2

C 5.1 341.1

E 5.1 341.1

2+00

E 5.0 341.2

C 5.4 340.8

W 5.3 340.9

2+44

E - 1<sup>st</sup> Sin. gar. corr floor 5.7 340.5

2+50

W 6.0 340.2

C 6.0 340.2

E 5.9 340.3

3+00

E 6.5 339.7

C 6.4 339.8

W 6.5 339.7

3+54

W - 1<sup>st</sup> door to cabinet shop Wood floor 7.08 338.4

W 7.3 338.9

C 7.2 339.0

E 7.2 339.0

T.P. 055 339.61 7.16 339.06

339.61

4+00

E	1.0	338.6
C	1.2	338.4
W	1.1	338.5

4+43

W-3	SIN. GAR. dirt floor	1.6	338.0
-----	----------------------	-----	-------

4+50

W	1.7	337.9
C	1.8	337.8
E	1.7	337.9

4+84

E-6.4	SIN. GAR. CORR. floor	2.25	337.36
-------	-----------------------	------	--------

5+12

E-9	SIN. GAR. CORR. floor	2.54	337.09
E	2.80	336.81	
C	2.7	336.9	
W	2.7	336.9	

5+42

W	3.5	336.1	
C	3.7	335.9	
E	3.6	336.0	
+15	SIN. GAR. CORR. floor	3.37	336.24

5+90

E	5.2	334.4
C	5.9	333.7
W	5.3	334.3

339.61

6+01' = NW Myrtle

Myrtle NOT paved 27

W	TOP of also ground 6+6	333.15
C	6.5	333.1
E	" " " " 6.20	333.41

T.P.	1.81	333.13	8.29	331.32
------	------	--------	------	--------

T.P.	10.14	330.11	13.16	319.97
------	-------	--------	-------	--------

ch. to NW BP	NON DIRT Myrtle	4.03	326.08	326.11
				0.03

Moore  
1-28-36

X sec alley 20' wide  
bet. Van Dyke + 43d and Myrtle <sup>cs.K.</sup> NOT paved  
Myrtle + Thorx Thorn " graded  
B/K. 104. City Heights.

331.96

Van Dyke Myrtle	5.85	331.96	326.11	NW 50	E	5.8	326.2		
00-30					C	6.1	325.9		
S'E of alley	7.4	324.8			W	6.1	325.9		
0-12									
S'E of EL alley = Ex. FH. Topog	7.40	324.56			W	SIN. Cot. dirt floor	6.5	325.5	on line
0+00 = SL Myrtle									
E Top ob	7.18	324.78			W		6.9	325.1	
E ground	6.6	325.4			C		7.0	325.0	
C "	6.6	325.4			E		6.9	325.1	
W "	6.1	325.9							
W Top ob	6.70	325.26			E		7.8	324.2	
0+04					C		8.4	323.6	
W	3.9	328.1			W		8.2	323.8	
+5	5.8	326.2							
C	6.1	325.9			W		9.6	322.4	
+4	6.0	326.0			C		9.5	322.5	
E	4.5	327.5			E		9.4	322.6	
0+15									
E	4.4	327.6			E		10.8	321.2	
C	4.9	327.1			C		11.1	320.9	
W	4.2	327.8			W		11.0	321.0	
0+45									
W	4.5	327.5			T.P.	0.56	320.92	11.60	320.36
C	4.8	327.2							
E SIN. gm. dirt floor	4.7	327.3	on line		W		0.9	320.0	

C		1.1	319.8
E		1.2	319.7
+15		5.1	315.8
	3 + 50		
- 20	Bag. of Lot Excav. on E.	11.2	309.7
E		3.5	317.4
+3		2.2	318.7
C		2.5	318.4
W		2.3	318.6
	4 + 00		
W		5.2	315.7
C		4.9	316.0
+8		4.5	316.4
E		5.2	315.7
+18		11.8	309.1
	4 + 50		
- 20	End of Excav. on E side alley	12.1	308.8
E		8.0	312.9
C		8.9	312.0
W		10.1	310.8
+10		13.0	307.9
T.P.	086	308.87	12.91
	5 + 00		
- 15		11.5	297.4
W		6.8	302.7
C		4.9	304.0

E		2.1	306.8
+15		0.0	308.9
	5 + 30		
- 10		6.5	302.4
E		8.1	300.8
C		10.7	298.2
W		12.0	296.9
+10		13.7	295.2
T.P.	421	300.90	12.18
	5 + 60		
- 10		10.1	290.8
W		8.4	292.5
C		7.1	293.8
E		5.4	295.5
+10		3.8	297.1
	5 + 97.8 = NLT horn		
- 10		8.5	292.4
E		10.6	290.3
C		13.0	287.9
W		13.7	287.2
+5		13.8	287.1
+15		10.5	284.4
	6 + 00 Conc. Wall across alley		
	5 E of # alley	13.4	287.5
		7.7	293.2

5077017

Top wall



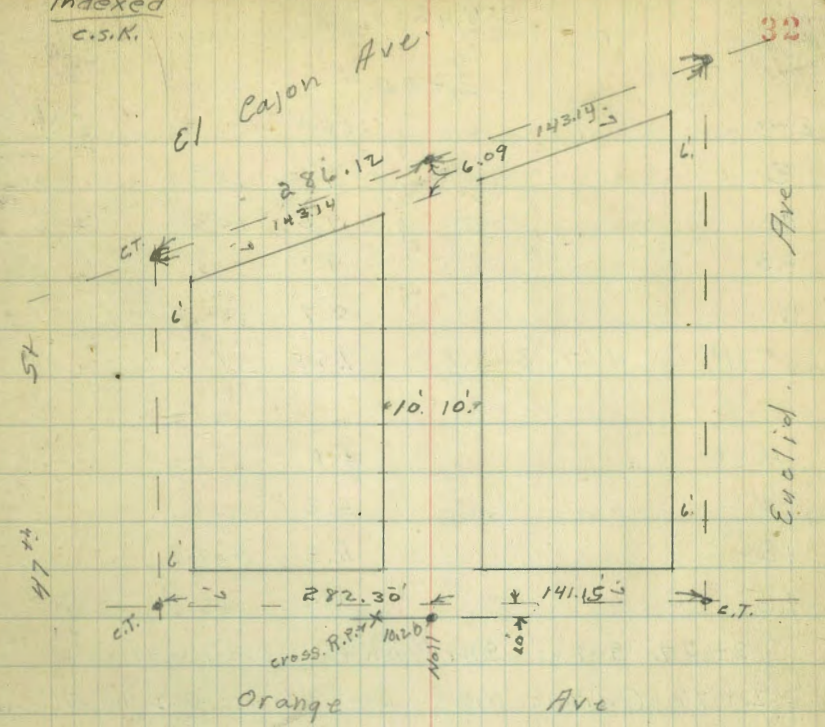
6 + 10				
5' E of 2nd alley	14.2	286.7		
6 + 25				
5' E of 2nd alley	11.7	289.2		
6 + 47.8 = 10' S of 2nd alley				
5' E of 2nd alley	13.9	287.0		
T.P.	12.47	312.76	0.61	300.29
T.P.	11.62	323.74	0.63	312.13
T.P.	7.50		0.72	323.03
ch to BM		24.2	326.11	326.11



2-19-36 X Sec. Alley BIK 6. Chesler Park  
 Miller, Walker, Bliss  
 Orange to El Cajon. Bet. 47<sup>th</sup> + Euclid

B.M. B.P.	7.77	358.46		350.69	N.W. Orange
B.M. B.P.			3.86	354.60	+ Euclid N.W. 47 <sup>th</sup> + Orange
15' S. of N. Line = N. ch. Line of Orange Ave					
W - 20	emt. ch.		3.74	354.72	
W	" "		3.85	354.61	
E	4 "		4.38	354.08	
+ 20	" "		4.96	353.50	
0+00 = N. Line Orange Ave					
E	emt. ch.		4.22	354.24	
E	ground.		4.2	354.3	
±	"		4.5	354.0	
W	"		4.0	354.5	
W	emt. ch.		3.72	354.74	
0+50					
W			4.2	354.3	
±			4.4	354.1	
E			4.6	353.9	
0+64 double garage on W. emt. floor 8.1' Back					
W - 8.1'	floor		3.96	354.50	
0+90 garage on E. emt. floor 22' Back					
E - 22'	floor		6.8	351.7	
1+00					
E			6.3	352.2	
±			6.0	352.5	
W			5.2	353.3	

Indexed  
 C.S.K.



Σ 358.46

1+07 garage on W. dirt floor		
W - 6.7		353.29
1+50		
W		351.7
+7		350.9
±		351.0
+9		350.7
E		350.1
+5		349.8

2+00

E-5	10.0	348.5
E	9.6	348.9
⊕	9.5	348.0
+3	9.5	349.0
W	8.7	349.8
T.P.	4.67	353.58
	9.55	348.91

2+50

W-5	5.0	348.6
W	5.3	348.3
+E	5.3	348.3
+5	5.9	347.7

2+52 S. End Shed on E. 0.2 in Alley

2+76 Garage on E. cmt. floor 0.2 in Alley

0.2 in Alley = floor 5.52 348.06

2+94 Garage on W. cmt. floor. 3.6' Back

W-3.6' floor 4.94 348.64

3+00 = N End. above Shed. on E. Line

E 5.6 348.0

⊕ 5.2 348.4

W 4.9 348.7

+5 4.9 348.7

3+11 double garage on E. cmt. floor 0.3 in Alley

E. on floor 5.60 347.98

3+41 double garage on E. cmt. floor { garage doors } 0.3 in Alley

E. on floor 5.37 348.21

3+50

W-5	4.7	348.9
W	4.7	348.9
⊕	5.2	348.4
E	5.4	348.2
E+5	5.6	348.0

4+00

E-5	5.6	348.0
E	5.4	348.2
⊕	5.6	348.0
W	4.6	349.0
W+5	4.4	349.2

4+06 garage on W. cmt. floor 5.5' Back.

W-5.5' floor 3.86 349.72

4+43 garage on W. cmt. floor 5.5' Back

W-5.5' = floor 4.20 349.38

4+50

W-5	4.6	349.0
W	5.0	348.6
⊕	5.5	348.1
E	5.9	347.7
+5	6.1	347.5

4+68 garage on E. cmt. floor 3.3' Back

E-3.3' floor 5.75 347.83

4+91 garage on E. cmt. floor 2.8' Back.

E-2.8' floor 5.93 347.65

353.58

5+00

E-5	6.3	347.3
E	6.2	347.4
☿	5.7	347.9
W	5.6	348.0
+5	5.4	348.2

5+42 garage on E. dirt floor 2.7' Back

E-2.7 floor	6.3	347.3
-------------	-----	-------

5+50

W-5	5.9	347.7
W	6.1	347.5
☿	6.3	347.3
E	6.5	347.1
E+5	6.6	347.0

5+59 garage on W. cmt. floor 6.0' Back

W-6.0' floor	5.57	348.01
--------------	------	--------

5+91 garage on W. cmt. floor 6.0' Back

W-6.0 floor	5.50	348.08
-------------	------	--------

6+00

E+5.	7.0	346.6
E	6.7	346.9
☿	6.6	347.0
W	6.3	347.3
W-5	6.5	347.1

6+12 double garage on E. cmt. floor 2.1' Back

E-2.1 = floor	6.80	346.68
---------------	------	--------

353.58

34

6+39 double garage on E. cmt. floor 2.1' Back

E-2.1 floor	6.90	346.68
-------------	------	--------

6+50

W-5'	6.6	347.0
W	6.6	347.0
☿	6.8	346.8
E.	7.2	346.4
+5'	7.4	346.2

6+61 garage on W. cmt. floor 7.0' Back.

W-7.0 floor.	5.38	348.20
--------------	------	--------

T.P. 4.53	351.26	6.85	346.73
-----------	--------	------	--------

6+90 garage on W. cmt. floor 7.0' Back.

W-7.0' = floor	3.8	347.5
----------------	-----	-------

7+00

E-5	5.2	346.1
E	5.2	346.1
☿	5.0	346.3
W	4.4	346.7
+5	4.2	347.1

7+02 = S. end Board Fence on W. 1/3' in Alley

7+0.9 garage on E. cmt. floor 5.2' Back.

E-5.2' floor	5.07	346.19
--------------	------	--------

7+42 garage on E. cmt. floor 5.3' Back  
E-5.3 floor 5.35 345.91

7+50

W-5 5.3 346.0

W 5.2 346.1

+1.3 Board Fence 5.2 346.1

Φ 5.2 346.1

E 5.5 345.8

+5 5.7 345.6

7+92 Board Fence on W. 1.3' in Alley

8+00 Fence on W. 0.8 in Alley

E = W. side shed. 4.7 346.6

Φ 4.9 346.4

+9.2 Board Fence 5.2 346.1

W 5.4 345.9

8+02 N. of shed. on E

W 5.2 346.0

Φ 5.0 346.3

+5 4.7 346.6

E 5.5 345.8

+5 5.7 345.6

8+50

-5 5.8 345.5

E 5.6 345.7

+5 5.0 346.3

Φ 5.0 346.3

W 5.4 345.9

+5 5.3 346.0

9+00

W-5 5.0 346.3

W 5.3 346.0

Φ 5.0 346.3

E 4.8 346.5

E 5.4 345.9

+5 5.6 345.7

9+50<sup>5</sup> Φ = S. Line El Cajon Ave on diagonal

9+52 Φ = S. End. Pav. on diagonal

E on S. End. curb 3. N. of S. Line 5.23 346.03

E S. End. Pav 5.47 345.79

Φ Pav 5.73 345.53

W. " 5.22 346.04

W cmt. ch. 4.90 346.36

16' N. of S. Line = S. ch. line of El Cajon Ave.

W-20 ch. 5.00 346.26

W-20 pav 5.40 345.86

W " 5.44 345.78

W ch 5.04 346.22

Φ Pav 5.60 345.66

E ch 5.30 345.96

E Pav 5.61 345.65

E +10 " 5.66 345.60

E +10 ch 5.31 345.95

chk B.M. B.P. S.W. 47<sup>th</sup> El Cajon Ave 4.10 347.16 = 347.20

Moore  
+1-36

Hilley Sec 15' wide  
DIX 65 W.P. Herberts add.

index  
c.s.k.

NW/SE	Dist	3775 + Moore
	NL Moore=00	
W CB	5.29	369.99
W DAV	5.41	369.84
C "	5.63	369.62
E "	5.50	369.75
E CB	5.28	369.97
	0+10	
E	5.1	370.2
C	5.1	370.2
W	5.1	369.80
	0+58	
-8	5.88	370.37
W	4.8	370.5
C	4.7	370.6
E	4.9	370.4
	1+00	
E	4.3	371.0
C	4.2	371.1
W	4.3	371.0
	1+50	
W	3.1	372.2
C	2.2	372.1
E	3.2	372.1

MONROE  
A.C. DIST.

Fire

6+00.75

Sewer M.H. Flushing Tank  
4" DIAM. 5+83.5

5+90

5+85

5+76

Paves. area to be  
1.5' wide to be  
excepted

2" CEMENT WALK  
0.5' back

Garage  
4" CEMENT APRON  
on LINE

5+50.70  
6" CORRUGATED  
3' HIGH METAL WIRE  
FENCE  
5+53.40

020

5  
4  
3

2+50

2+00

0+58  
0+58  
8' back

0+50  
Stucco  
laundry  
Stucco  
Paved.

0+100

A.C. DIST.

Moore

Fire

376.25

2+00

E	2.7	372.6
C	2.6	372.7
W	2.7	372.6

+25

W	2.2	373.1
C	2.4	372.9
E	2.8	372.5

+50

E	2.5	372.8
C	2.3	373.0
W	2.4	372.9

3+00 = low spot to be drained

W	2.8	372.5
C	2.7	372.6
E	2.8	372.5

+50

E	2.4	372.9
C	2.3	373.0
W	2.5	372.8

T.P. 2.9 376.07 1.37 373.88

4+00

W	3.3	372.8
C	3.3	372.8
E	3.1	373.0

376.07

37

4+50

E	3.2	372.9
C	3.2	372.9
W	3.2	372.9

5+00

W	3.2	372.9
C	3.1	373.0
E	3.4	372.7

5+13.4 beg. of pav.

E	3.2	372.7	
C	3.0	373.1	
W	ground	3.3	372.8

W Top of wall 2.83 373.24

5+29

W - 0.2 E W Cem. Walk +  
wide gate 3.04 373.09

5+50.8

W	Top of wall	2.83	373.30
W	ground	2.8	373.3
C		3.0	373.1
E	Cem apron on line	3.38	372.75
+4	Cem floor	2.87	373.26

5+56 &amp; Corage

-4	Cor. Cem floor	2.87	373.26
E	v apron	3.38	372.75

5+65

E-0.5 Top 2.5 wide Cem. Walk 3.10 373.03



Top alley curb  
St. Monroe on  
E.L. alley

5+65

E	3.1	373.0
C	3.2	372.9
W	3.1	373.0

T.P. for CONST. paving

410

371.97

5+80

W	3.3	372.8
C - S edge flush tank	3.30	372.83
E	3.3	372.8
+ 0.5 Top curb walk	3.2	372.9

5+85

E - 0.5 walk	3.30	372.9
E	3.5	372.6
C - S edge flush tank	3.3	372.81
W	3.5	372.6

5+95

W	4.1	372.0
C	4.1	372.0
E	4.1	372.0
+ 0.5 curb walk	3.81	372.32

6+00.75 St. Monroe

E Top ob	4.10	371.97
E pav	4.39	371.68
C "	4.65	371.41
W "	4.65	371.42
W cb	4.23	371.64

T.P. 1.43 375.31

219

373.88

check to starting B.M.

5.55

369.76

369.75  
0.01

Please report this flush tank for  
grade if possible. Mr. Greer of  
Sewer Dept. says lower grade would  
be quite expensive.

Sta. 5+13.4 to 6+00.75 - Sect. to be paved  
See p 36 for area to be excepted by  
wish of Prop. owner & Mr. Broades.



4-17-30  
Miller  
Walker  
Bliss

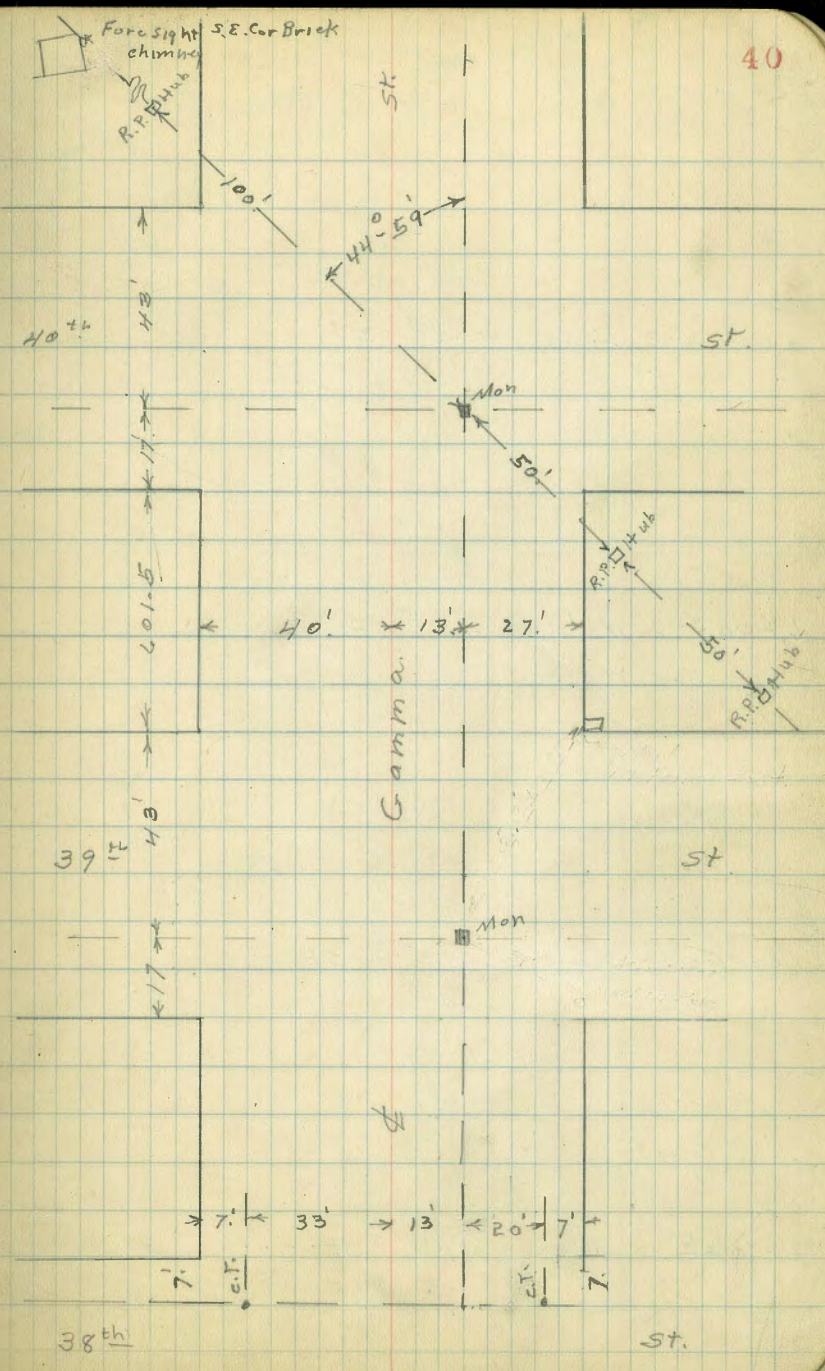
Gamma St. X. See  
39<sup>th</sup> St. to (Highland Ave) 43<sup>rd</sup> St.  
(frame changed.)

INDEXED  
C.S.N.

0+00 = E. Line 40<sup>th</sup> St.

1+01.5 W. Line 40<sup>th</sup> St.

0+00 = E. Line 39<sup>th</sup> St

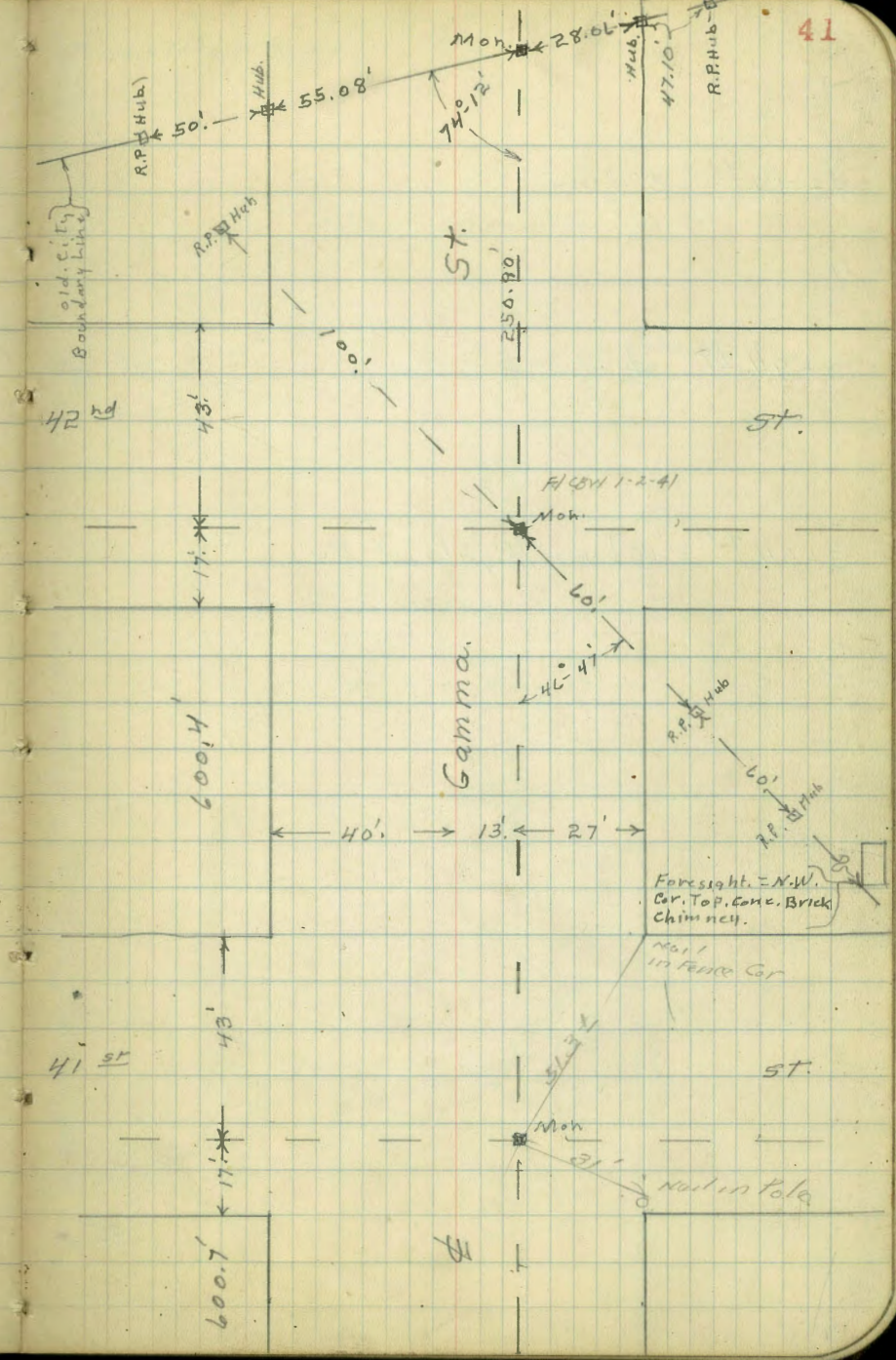


0+00 = E. Line 42<sup>nd</sup> St.

6+00 = W. Line 42<sup>nd</sup> St.

0+00 = E. Line 41<sup>st</sup> St.

6+06 = W. Line 41<sup>st</sup> St.



4+34<sup>49</sup> E. Line

4

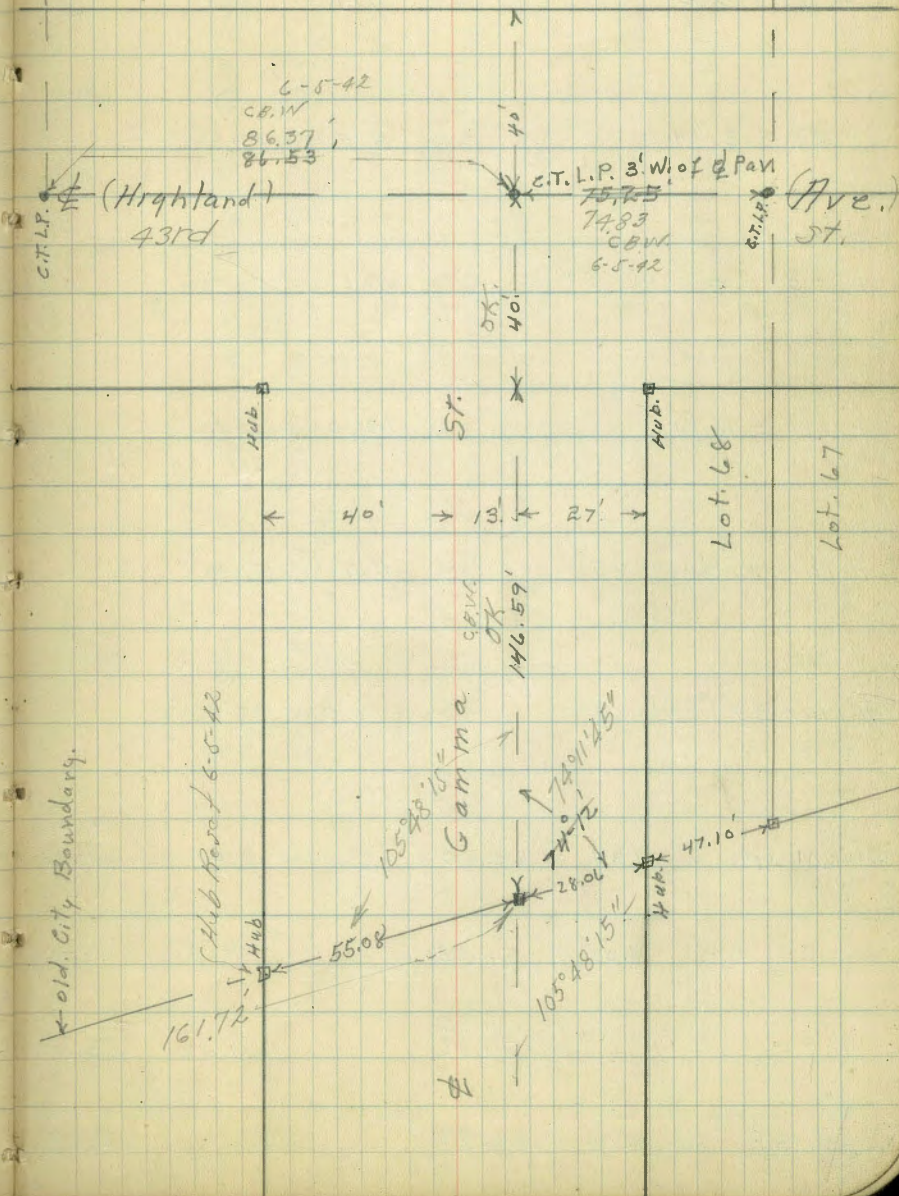
3+94.49  $\neq$

3+54<sup>49</sup> = W. Line Highland Ave

← S. Line Palm Hills Sub.

Lot 64

Lot 67



Gamma St.

E Rod

+ 48 = E ch.

11.1 52.0

+ 39 = E. 44

11.5 51.6

+ 30 = E 39<sup>th</sup> St

11.6 51.5

+ 21 = W. 44

12.0 51.10

+ 12 = W. ch.

11.8 51.3

W. line 39<sup>th</sup> St.

12.0 51.1

Set. B.M. s.p.k.

11.34

63.10

2.27

51.76

Elec Pole S. E. Cor 39<sup>th</sup> + Gamma.

Set. B.M. B.P.

8.02

54.03

8.35

46.01

S. E. Cor 39<sup>th</sup> + Delta St.

T.P.

1.76

54.36

11.39

52.60

B.M. B.P.

0.70

63.99

63.29

N.W. Cor 40<sup>th</sup> + Delta Sts

Lt.

53.5

52.8

52.0

52.0

51.5

51.2

51.0

9.6  
40  
N10.3  
26  
ch11.1  
13  
14

11.1

11.6  
13  
1411.9  
26  
ch12.1  
40  
5

52.8

52.4

51.9

51.6

51.4

51.0

50.7

10.3  
40  
N10.7  
2611.2  
13

11.5

11.7  
1312.1  
2612.4  
40  
5

52.3

52.0

51.6

51.5

51.1

50.8

50.8

10.8  
40  
N11.1  
2611.5  
1311.6  
sewer  
W.H12.0  
1312.3  
2612.3  
40  
5

52.1

51.8

51.4

51.1

50.9

50.6

50.5

11.0  
40  
N11.3  
2611.7  
13

12.0

12.4  
1312.5  
2612.6  
40  
5

52.4

51.7

51.5

51.3

50.8

50.6

50.5

10.7  
40  
N11.4  
2611.6  
13

11.8

12.3  
1312.5  
2612.6  
40  
5

52.10

51.5

51.2

51.1

50.6

50.4

50.4

11.0  
40  
N11.6  
26  
ch11.9  
13  
14

12.0

12.5  
13  
1412.7  
26  
ch12.7  
40  
5

63.10

63.10

Gamma St  
 E. Rod.

3 9.6 64.7  
 T.P. 12.47 74.25 1.32 61.78

+50 1.3 61.8

2 4.3 58.8

+50 6.3 56.8

1 8.2 54.9

+50 9.8 53.3

$W + \frac{60}{50} = 0 + 0 = E. \text{ Line } 39^{\text{th}} \text{ St}$   
 63.10 11.1 52.0

Lt.

62.9 63.2 63.5 63.7 64.7  
 11.9 11.1 10.8 10.6 9.6  
 50 40 26 13 4  
 N cl cl

Rt.

44  
 Rt

64.9 64.8 65.5  
 9.4 9.5 8.8  
 13 26 40  
 4 cl 5

74.25

60.7	60.9	61.1	61.8	62.0	61.8	62.8	63.4
2.4	2.2	2.0	1.3	1.1	1.3	0.3	1.03
40	26	13		13	26	27	40
58.3	58.3	58.3	58.8	58.9	58.6	59.2	59.3
4.8	4.8	4.8	4.3	4.2	4.5	3.9	3.8
40	26	13		13	26	27	40
56.5	56.7	56.8	56.8	56.6	56.4	57.1	57.5
6.1	6.4	6.3	6.3	6.5	6.7	6.0	5.6
40	26	13		13	26	27	40
54.9	54.9	55.0	54.9	54.8	54.7	55.4	55.3
8.2	8.2	8.1	8.2	8.3	8.4	7.7	7.8
40	26	13		18	26	27	40
53.8	53.7	53.3	53.3	53.3	52.9		52.7
9.3	9.4	9.8	9.8	9.8	10.2		10.4
40	26	13		13	26		40
53.7	53.0	52.3	52.0	51.5	51.6	51.1	
9.4	10.1	10.8	11.1	11.6	11.5	12.0	
40	26	13		13	26	40	
N	cl	1/4	63.10	1/4	cl	5	

♀

T.P. 8.01 94.82 0.21 86.81

+50 2.3 84.7

5 4.1 82.9

+75 5.2 81.8

+50 8.4 78.6

T.P. 12.85 87.02 0.08 74.17

4 1.9 72.4

+50 6.7 67.6

74.25

	74.0	75.3	77.9	79.2	84.7	84.8	85.0	88.6	88.9	90.4
	13.0	11.7	9.1	7.8	2.3	2.2	2.0	+1.6	+1.9	+3.4
	50	40	26	13	5	13	26	29	37	40
	74.1	75.8	78.6	80.4	81.7	82.9	82.7	83.1	86.0	86.2
	12.9	11.2	8.4	6.6	5.3	4.1	4.3	3.9	1.0	0.8
	50	40	26	13	5	13	26	29	38	40
	74.1	75.9	78.6	79.3	81.2	81.8	81.4	81.5	83.5	83.0
	12.9	11.1	8.4	7.7	5.8	5.2	5.6	5.5	3.5	4.0
	50	40	26	19	13	13	26	28	40	40
	73.0	74.4	76.2	76.5	78.4	78.6	78.5	78.1	79.0	78.9
	14.0	12.6	10.8	10.5	8.6	8.4	8.5	8.9	8.0	8.1
	50	40	26	19	13	13	13	26	27	40

87.02

	67.3	69.8	70.5	71.0	72.6	72.4	72.4	72.1	72.9	72.7
	5.0	4.5	3.8	3.3	1.7	1.9	1.9	2.2	1.4	1.6
	50	40	26	13	2	13	13	26	27	40
	66.2	66.0	66.6	66.7	67.6	67.6	67.6	67.5	68.2	68.3
	8.1	8.3	7.7	7.6	6.7	6.7	6.7	6.8	6.1	6.0
	50	40	26	13	14	13	14	26	27	40
		N								5

74.25



## Gamma St

± Rod

Set. B.M. 50' S.W. R. P. Hub.

2.27 92.55

+ 61<sup>5</sup> = E. Line 40<sup>th</sup> St. = 0+00 6.1 88.7+ 51<sup>5</sup> = E. cl. 6.7 88.1+ 41<sup>5</sup> = E. 4<sup>th</sup> 7.6 87.2+ 31<sup>5</sup> = E. 7.8 87.0+ 21<sup>5</sup> = W. 1<sup>st</sup> 7.8 87.0+ 11<sup>5</sup> = W. cl. 7.5 87.36+01<sup>5</sup> = W. Line 40<sup>th</sup> St. 7.8 87.0

94.82

Lt.

±

Rt. 16

40<sup>th</sup> + Gamma.

78.0	79.7	81.4	84.1	88.7	89.4	91.1	93.6
16.8	15.1	13.4	10.7	6.1	5.4	3.7	1.2
50	40	26	13		13	26	40
	N	cl	14		14	26	5.
78.6	79.6	81.3	83.9	88.1	88.9	89.5	91.3
16.2	15.2	13.5	10.9	6.7	5.9	5.3	3.5
50	40	24	13		3	13	26
77.2	78.4	80.5	83.7	87.2	88.5	89.5	90.9
17.6	16.4	14.3	11.1	7.6	6.3	5.3	3.9
50	40	26	13		3	13	26
77.2	77.8	80.2	82.8	87.0	88.3	89.2	90.5
17.6	17.0	14.6	12.0	7.9	6.5	5.6	4.3
50	40	26	13		4	13	26
75.8	78.5	79.8	81.4	87.0	88.3	88.8	89.9
19.0	16.3	15.0	13.4	7.8	6.5	6.0	4.9
50	40	26	13		2	13	26
75.6	78.2	80.0	81.2	87.5	88.2	89.2	91.2
19.2	14.6	14.8	13.6	7.5	6.6	5.6	3.6
50	40	26	13		13	26	29
75.4	77.8	80.1	80.8	83.2	87.0	87.6	88.1
19.4	17.0	14.7	14.9	11.6	7.8	7.2	6.7
50	40	26	13	2		13	24
	N	cl	14			14	cl
							29
							37
							40
							5.

94.82  
±

Gamma St.  
 E Rod

T.P. 1.50 88.18 8.14 86.68

3 8.2 86.6

+50 5.8 89.0

2 6.0 88.8

+50 7.1 87.7

1 7.4 87.4

+50 6.6 88.2

0+00 = E. Line 40<sup>th</sup> St.

94.82

Lt.

⊘

Rt. 47

80.4	81.0	82.3	84.2	86.5	86.6	86.6	88.4	89.7	91.1
14.4	13.8	12.5	10.6	8.3	8.2	8.2	6.4	5.1	3.7
50	40	26	13	6	6	13	16	26	40
83.3	84.0	85.4	87.3	89.0	89.0	88.5	90.1	90.7	92.1
11.5	10.8	9.4	7.5	5.8	5.8	6.3	4.7	4.1	2.7
50	40	26	13	8	8	13	14	26	40
83.8	84.5	85.3	86.8	87.1	88.8	88.4	87.6	90.9	91.8
11.0	10.3	9.5	8.0	5.7	6.0	6.4	5.2	3.9	3.0
50	40	26	13	8	10	13	24	26	40
81.0	82.0	83.7	85.0	85.5	87.5	87.7	87.6	87.1	90.0
13.8	12.8	11.1	9.8	9.3	7.3	7.1	7.2	5.7	4.8
50	40	26	13	10	4	4	13	24	26
80.1	81.9	82.8	84.8	87.2	87.4	87.3	87.3	88.2	89.4
14.7	12.9	11.0	10.0	7.6	7.4	7.5	7.5	6.6	5.4
50	40	26	13	3	3	13	16	20	26
80.0	81.7	82.5	85.2	88.0	88.2	88.3	88.3	87.2	90.9
14.8	13.1	12.3	9.6	6.8	6.6	6.5	6.5	5.6	3.9
50	40	26	13	2	2	13	11	18	26
			14			17		22	26
									40
									5

94.82

⊘

Gamma St

± Rod

6400<sup>±</sup> = W. line 41<sup>st</sup> st. → 5.5 75.1

Lt.										Rt.	
72.4	72.8	73.1	73.6	74.4	75.1	74.7	74.3	75.1			48
8.2	7.8	7.5	7.0	6.2	5.5	5.9	6.3	5.5			
50	40	26	13	9		13	26	40			
	N	dc	4								

B.M. Nail 4.99 80.56 12.61 75.57

Elec Pole S.W. Gamma + 41<sup>st</sup> sts

80.56

+50

12.7

72.2	72.9	73.7	74.4	75.5	75.5	75.5	76.0	76.9
16.0	15.3	14.5	13.8	12.7	12.7	12.7	12.2	11.3
50	40	26	13	7		13	26	40

5

10.3

74.1	74.9	76.2	77.0	78.2	77.9	77.7	79.3	79.6	81.1
14.1	13.3	12.0	11.2	10.0	10.3	10.5	8.9	8.6	7.1
50	40	26	13	8		13	16	26	40

+50

6.9

76.5	78.1	79.3	80.6	81.4	81.3	80.9	82.0	82.5	83.7
11.7	10.1	8.9	7.6	6.8	6.9	7.3	6.2	5.7	4.5
50	40	26	13	16		13	16	26	40

4

5.4

79.4	80.2	80.3	81.2	82.7	82.8	83.2	85.3	85.7	86.4
8.8	8.0	7.9	7.0	5.5	5.4	5.0	2.9	2.5	1.8
50	40	26	13	7		13	16	26	40

+50

3.8

77.9	79.6	81.4	83.0	84.1	84.4	84.4	87.1	87.9	88.8
10.3	8.6	6.8	5.2	4.1	3.8	3.8	1.1	0.3	0.6
50	40	26	13	8		13	18	26	40
	N	dc	4			11		dc	5

88.18

88.18

## Gamma St

± Rod

1 5.0 75.6

+50 5.4 75.2

0  
+60<sup>k</sup> = E line H1<sup>st</sup> = 0+00 5.9 74.7+50<sup>v</sup> = E. cl 6.0 74.6+40<sup>k</sup> = E. ly 6.1 74.5+30<sup>k</sup> = cl 6.17 74.39+20<sup>k</sup> = W. ly 6.0 74.6+10<sup>k</sup> = W. ch. 5.7 74.9

80.56

Lt

73.9	74.3	74.7	74.8	75.6	75.5	<del>75.6</del>	75.2	75.8	76.6
6.7	6.3	5.9	5.8	5.0	5.1	5.0	5.3	4.8	4.0
50	40	24	23	20	13		13	26	40
	X	cl	cl				14	cl	5
73.6	73.8	74.2		75.1	75.2	75.2	75.2	75.2	75.6
70	6.8	6.4		5.5	5.4	5.4	5.4	5.4	5.0
50	40	24		13		13	13	26	40
72.8	73.2	73.6	74.4	74.7	74.6	74.8	75.3		
7.8	7.4	7.0	6.2	5.9	6.0	5.8	5.3		
50	40	26	13		13	26	40		
72.6	73.0	73.6	74.1	74.6	74.6	74.6	75.2		
8.0	7.6	7.0	6.5	6.0	6.0	6.0	5.4		
50	40	26	13		13	26	40		
72.0	72.3	72.8	73.8	74.5	74.6	74.7	75.0		
8.5	8.3	7.8	6.8	6.1	6.0	5.9	5.6		
50	40	26	13		13	26	40		
71.9	72.3	72.9	73.8	74.39	74.6	74.7	75.0		
8.7	8.3	7.7	6.8	6.17	6.0	5.9	5.6		
50	40	26	13	M.H. rim.	13	26	40		
71.9	72.5	72.8	73.7	74.6	74.5	74.6	74.9		
8.7	8.1	7.8	6.9	6.0	6.1	6.0	5.7		
50	40	26	13		13	26	40		
72.3	72.5	72.9	73.8	74.9	74.6	74.6	75.0		
8.3	8.1	7.7	6.8	5.7	6.0	6.0	5.6		
50	40	24	13		13	26	40		
	X	cl	14		14	26	40		

80.56



Gamma St.

± Rod

+50 5.1 78.3

78.3	78.3	78.3	76.9	76.8	78.1	78.3	78.4	78.4	77.3	77.1	77.1	77.0
5.1	5.1	5.1	6.5	6.6	5.3	5.1	5.0	5.0	6.1	6.3	6.3	6.4
50	40	35	33	26	13	13	13	17	20	26	40	50
					34		14			26	9	

T.P. 5.65 83.41 2.80 77.76

83.41

4 2.7 77.9

77.4	77.0	76.5	77.4	77.9	78.0	77.4	77.4	77.9
3.0	3.6	4.1	3.2	2.7	2.6	3.0	3.2	3.3
50	40	26	13		13	26	40	50

+50 3.3 77.3

75.5	75.3	76.1	77.2	77.3	77.3	75.5	75.5	76.5	77.5
5.1	5.3	4.5	3.4	3.3	3.3	5.1	5.1	4.1	3.1
50	40	26	13		13	22	26	40	50

3 3.8 76.8

74.6	74.6	74.6	76.7	76.8	76.8	76.1	77.1	76.2	76.1
6.0	6.0	6.0	3.9	3.8	3.8	4.5	3.5	4.4	4.5
50	40	26	13		13	18	26	40	50

+50 4.1 76.5

73.7	72.9	73.1	76.0	76.1	76.5	76.5	75.2	75.2	76.0	76.3
6.7	7.7	7.5	4.6	4.5	4.1	4.1	5.4	5.4	4.6	4.3
50	40	26	16	13		13	19	26	40	50

2 4.3 76.3

72.6	73.0	73.7	74.1	75.6	76.0	76.3	76.2	75.3	75.6	76.4
8.0	7.6	6.9	6.5	5.0	4.6	4.3	4.4	5.3	5.0	4.2
50	40	26	22	17	13		13	19	26	40

+50 4.7 75.9

73.5	73.9	74.4	74.7	75.9	75.9	75.9	76.1	75.9	77.0
7.1	6.7	6.2	5.9	4.7	4.7	4.7	4.5	4.7	3.6
50	40	26	21	18	13		13	14	40
		26	14						5

80.56

80.56

±

Gamma St

+50 <sup>H</sup>	E. d	4.5	78.9
+40 <sup>H</sup>	E 1/4	4.4	79.0
+30 <sup>H</sup>	±	4.6	78.8
+20 <sup>H</sup>	W. 1/4	4.6	78.9
+10 <sup>H</sup>	W. d	4.7	78.7
6 + 00 <sup>H</sup>	W. Line 1/2 <sup>59</sup> St.	4.7	78.7
+50		4.9	78.5
5		5.0	78.4

83.41

<u>83.7</u>	<u>82.8</u>	<u>82.8</u>	<u>78.4</u>	<u>78.7</u>	<u>78.9</u>	<u>78.5</u>	<u>77.9</u>	<u>79.0</u>	<u>78.0</u>	<u>77.0</u>	<u>76.4</u>
40.3	0.6	0.6	5.0	4.7	4.5	4.9	5.5	4.4	5.4	6.4	7.0
40	26	21	18	13	13	13	20	22	26	40	50
<u>83.0</u>	<u>82.7</u>	<u>82.7</u>	<u>78.5</u>	<u>78.5</u>	<u>79.0</u>	<u>78.5</u>	<u>78.6</u>	<u>79.4</u>	<u>78.3</u>	<u>77.1</u>	<u>76.3</u>
0.4	0.7	0.7	4.9	4.9	4.4	4.9	4.8	4.0	5.1	6.3	7.1
40	26	21	18	13	13	13	19	20	26	40	50
<u>82.5</u>	<u>82.5</u>	<u>82.8</u>	<u>78.6</u>	<u>78.6</u>	<u>78.8</u>	<u>78.9</u>	<u>79.7</u>	<u>79.2</u>	<u>78.0</u>	<u>77.0</u>	
0.9	0.9	0.6	4.8	4.8	4.6	5.0	3.7	4.2	5.4	6.4	
40	26	21	18	13	M.H. 13	13	19	21	26	40	50
					Rim.						
		<u>80.8</u>	<u>80.0</u>	<u>78.6</u>	<u>78.6</u>	<u>78.9</u>	<u>78.3</u>	<u>78.2</u>	<u>77.2</u>	<u>76.4</u>	
		2.6	3.4	4.8	4.8	4.5	5.1	5.2	6.2	7.0	
		40	26	18	13	13	13	26	40	50	
		<u>80.8</u>	<u>79.4</u>	<u>78.5</u>	<u>78.7</u>		<u>78.2</u>	<u>77.9</u>	<u>76.8</u>	<u>75.9</u>	
		2.6	4.0	4.9	4.7		5.2	5.5	6.6	7.5	
		40	26	13	13		13	26	40	50	
		<u>81.0</u>	<u>79.6</u>	<u>78.6</u>	<u>78.7</u>	<u>78.2</u>	<u>78.2</u>	<u>77.1</u>	<u>75.9</u>		
		2.4	3.8	4.4	4.7	5.2	5.2	6.3	7.5		
		40	26	13	13	13	26	40	50		
		<u>78.6</u>	<u>79.0</u>	<u>78.6</u>	<u>78.8</u>	<u>78.5</u>	<u>77.3</u>	<u>74.8</u>	<u>74.6</u>	<u>73.4</u>	<u>72.4</u>
		4.8	4.4	4.8	4.6	4.9	5.1	6.1	8.6	8.8	10.0
		50	40	26	13	13	13	18	22	26	40
		<u>77.5</u>	<u>77.5</u>	<u>77.0</u>	<u>78.4</u>	<u>78.4</u>	<u>78.3</u>	<u>77.9</u>	<u>76.2</u>	<u>75.6</u>	<u>74.8</u>
		5.9	5.9	6.4	5.0	5.0	5.1	5.5	7.2	7.8	8.6
		50	40	26	13	13	13	18	21	26	40

83.41

≡  
≡  
≡  
≡  
≡

Gamma St

± Rod

3 5.9 78.0

+50 4.9 79.0

Lt	81.9	81.2	80.9	77.4	77.6	78.0	77.2	76.3	78.7	RT	78.7	78.0
	2.0	2.7	3.0	6.5	6.3	5.9	6.7	7.6	5.2	5.2	5.2	5.9
	40	26	21	18	13	13	13	20	22	26	40	40
	80.8	80.1	79.6	78.2	78.6	79.0		78.3	76.5	75.6	74.8	
	3.1	3.8	4.3	5.7	5.3	4.9		5.6	7.4	8.3	9.1	
	40	26	23	21	13			13	26	40	50	

B.M. Hub 9.33 83.85 8.89 74.52

S. line Gamma St  
old. City Boundary

83.85

2 3.9 79.5

+50 3.9 79.5

	82.2	81.7	81.7	78.8	79.3	79.5	79.0	78.4	76.4	75.1	74.4
	1.2	1.7	1.7	4.6	4.1	3.9	4.4	5.0	7.0	8.3	9.0
	40	26	24	23	13	3.9	13	20	24	40	50
	82.1	81.1	81.0	78.9	79.3	79.5	78.9	77.2	75.8	75.1	
	1.3	2.3	2.4	4.5	4.1	3.9	4.5	6.2	7.6	8.3	
	40	26	24	23	13	3.9	13	26	40	50	
	83.8	82.9	82.8	78.4	78.8	79.3	78.8	78.3	76.7	75.8	
	+0.4	0.5	0.6	5.0	4.6	4.1	4.6	5.1	6.7	7.6	
	40	26	23	21	13		13	26	46	50	
	84.3	83.5	83.1	78.4	78.7	79.2	78.6	78.0	77.2	78.7	77.8
	+0.9	+0.1	0.3	5.0	4.7	4.2	4.8	5.4	4.2	4.7	5.6
	40	26	28	28	13		13	21	22	26	40
	84.3	83.1	83.1	78.5	78.7	78.9	78.4	78.4	79.4	78.0	76.9
	+0.9	0.3	0.3	4.9	4.7	4.5	5.0	5.0	4.0	5.4	6.5
	40	26	22	19	13		13	19	26	26	40
	N	N			14		14			26	50

1 4.1 79.3

+50 4.2 79.2

0+00 +60<sup>4</sup> = 8. line = 42<sup>hd</sup> = 0+00 4.5 78.9

83.41

83.41

± Rod

T.P. 10.60 75.52 2.62 64.92

B.M. B.P. 10.94 67.54 4.26 56.60

Top con + Head wall N.W. Cor. Delta + (Highland) 43<sup>m</sup>

T.P. 1.35 60.86 13.00 59.51

T.P. 1.04 72.51 12.38 71.47

+88<sup>47</sup> = M. Edge ent. Pav. 9.39

76.81	76.00	75.23	74.46	73.66	72.90	72.05
7.04	7.85	8.62	9.39	10.19	10.95	11.80
40	26	13		13	26	40

+81 9.4

76.1	75.7	74.9	74.5	73.6	72.5	71.3
7.8	8.2	9.0	9.4	10.3	11.4	12.6
40	26	13		13	26	40

+79 9.2

81.4	80.5	79.2	75.9	74.9	74.7	73.7	73.1	72.0	71.3
2.5	3.4	4.7	8.5	9.0	9.2	10.2	10.8	7.9	6.6
40	26	23	18	13		13	26	29	40

+65 8.8

81.2	81.2	80.9	75.9	75.4	75.1	74.3	74.7	73.8	73.1
2.3	2.7	3.0	8.5	8.5	8.8	9.6	9.2	5.1	5.8
40	26	22	17	13		13	22	26	40

+54<sup>49</sup> = W. Line Highland. 8.1

83.6	82.9	82.5	75.7	75.7	75.8	75.1	74.9	74.5	74.2
0.3	1.0	1.4	8.2	8.2	8.1	8.8	9.0	4.4	4.7
40	26	22	16	13	13	13	22	26	40
N	d			44				d	5

3

83.85

83.85

±



B.M. B.P.			5.21	10.55 =1054	N.W. Cor Main & Woden.
T.P.	3.62	15.86	9.54	12.24	
Set. B.M. B.P.	1.13	21.78	12.43	20.65	Wly Cor Woden & Cotton wood.
T.P.	0.26	33.08	10.19	32.82	
Set. B.M. B.P.	0.95	43.01	7.99	42.06	S.W. 39 <sup>th</sup> & Epsilon. ✓
T.P.	50.05		9.29	47.63	
B.M. B.P.	3.86	56.92	11.39	53.06	N.W. 40 <sup>th</sup> & Epsilon ✓
B.M. B.P.	1.16	64.45	12.80	63.29	N.W. 40 <sup>th</sup> & Delta. ✓
T.P. B.M.	2.38	76.09	1.81	73.71	S.W. 13 <sup>th</sup> Mon 41 <sup>st</sup> & Delta ✓
		75.52			

Prop. Ext. of Narragansett  
 Chatsworth to Plum  
 at Lowell

Steve  
 Sisson  
 Northern  
 9-26-86

Indexed  
 C.S.K.

6+12.40 INT. of Nly of Lot 1 PL. 200

E.C. 4+93.13

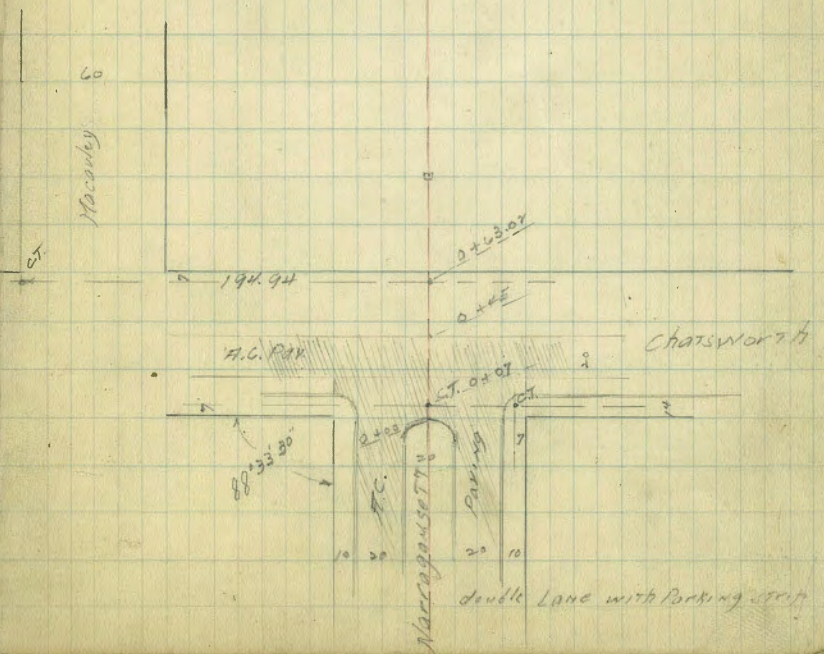
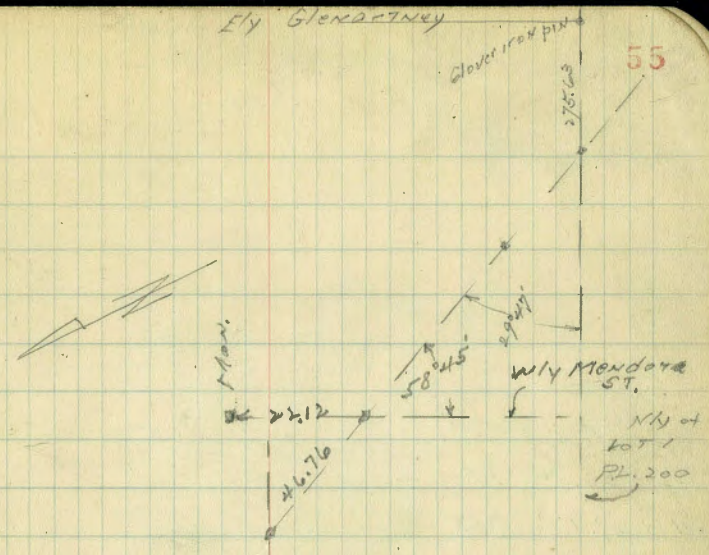
2+90 = P.I.

$\Delta = 29^{\circ}47' R$   
 $R = 800$   
 $T = 212.72$   
 $L = 415.85$

0+77.28 B.C. Pt.

0+00 = Wly Chatsworth Blvd.

Fly Glenarney



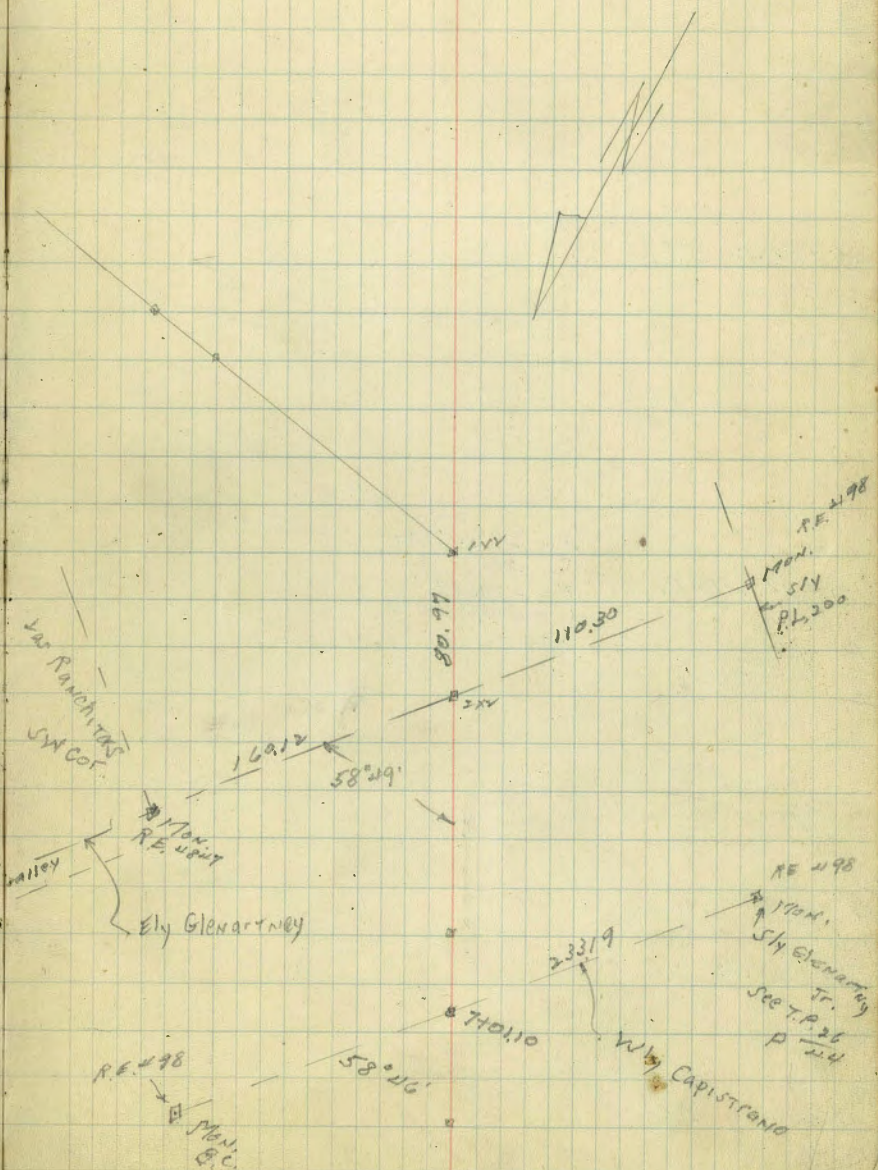
12 + 06.84 F.C.

11 + 69.58 P.O.T.

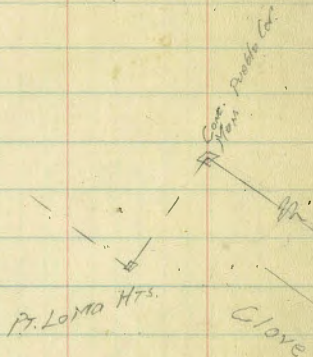
10 + 15.39 - P.I.  
 Δ = 61° 32' 27"  
 R = 400  
 T = 238.13  
 L = 429.58

7 + 77.26 B.C. 27

6 + 12.40



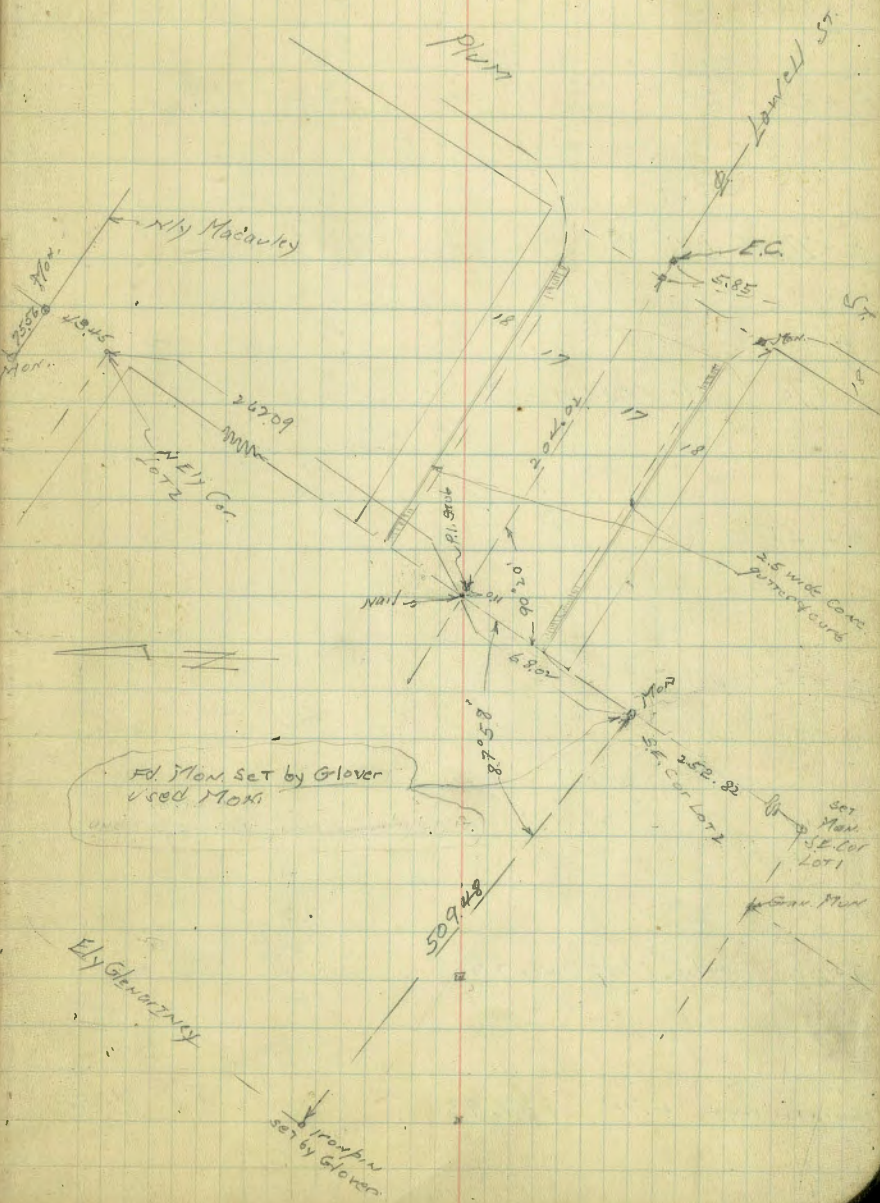
16+78.9x E.C.



$A = 29^{\circ} 24' RT$   
 $EP = 800$   
 $T = 209.87$   
 $L = 110.50$

12+68.42 O.C. RT

12+06.84 E.C.



YSEC of EXT. of Narragansett  
 Chatsworth to Plum and Lowell

+50  
 +100  
 0+77.28 BC Rt  
 0+70 fly Chatsworth  
 0+65  
 0+35  
 0+14  
 0+00 = wly Chatsworth  
 Chatsworth  
 Narragansett 4.74 137.93

	LT.		PT.
10	127.6	129.5	133.2
70	130.2	131.8	135.0
40	132.0	133.3	135.4
50	131.8	133.7	135.8
20	134.1	134.2	136.1
10	132.88	134.62	136.43
30	132.73	134.64	136.66
40	132.20	134.60	135.75
50	133.20	134.60	135.75
60	134.03	134.97	135.53
70	133.39	134.19	136.10
80	134.03	134.19	136.10
90	133.39	134.19	136.10
100	134.03	134.19	136.10

137.93

4 + 93.13 EC

J.P. 7.8 135.49 9.62 128.31

+50

4

+50

3

+50

2+00

137.93

127.0	127.5	126.26	125.1	125.2
6.4	8.0	9.3	10.4	10.3
40	20	20	20	40

130.6	128.8	127.6	126.9	126.7
10.3	10.3	10.3	11.0	11.2
40	20	20	20	40
131.4	130.6	129.3	128.6	127.3
8.6	8.6	8.6	8.6	8.6
40	20	20	20	40
130.0	129.4	129.3	129.6	129.9
11.0	11.0	11.0	11.0	11.0
40	20	20	20	40
128.9	129.3	130.0	130.9	131.5
9.0	9.0	9.0	9.0	9.0
40	20	20	20	40
127.0	127.7	128.1	128.8	130.4
10.9	10.9	10.9	10.9	10.9
40	20	20	20	40
126.7	127.3	128.3	129.8	130.4
11.2	11.0	11.0	11.0	11.0
40	20	20	20	40

137.93

T.P. 7.39 142.80 0.08 135.41

7+77.26 D.C. LT.

+50

7

+50

6

+50

+100

135.49

17.

18

19

60

6.9 40	128.6	9.7 40	125.8	7.8 40	127.7	11.4 40	128.9	4.4 40	131.1	4.5 40	133.0	0.3 40	135.2
5.3 40	127.3	10.8 40	124.7	10.0 40	124.9	8.4 40	127.1	11.2 40	128.0	9.3 40	130.2	4.2 40	131.3
9.6 40	125.9	11.5 40	124.0	11.5 40	124.0	10.9 40	124.6	9.7 40	125.8	8.4 40	127.1	7.67 40	127.82
10.6 40	124.9	11.9 40	123.6	12.0 40	123.5	11.7 40	123.8	11.4 40	124.1	10.2 40	125.3	9.8 40	125.7
10.5 40	125.0	11.3 40	124.2	12.1 40	123.4	12.9 40	124.6	12.4 40	123.1	11.3 40	124.2	10.7 40	124.8

135.49

11

10 + 50

T.P.

6.31

146.72

2.39

140.41

10

+ 50

9

+ 50

8 + 00

142.80

$$\begin{array}{r} 143.9 \\ 4.8 \\ \hline 148.7 \\ 4.0 \\ \hline 152.7 \end{array}$$

$$\begin{array}{r} 142.4 \\ 4.8 \\ \hline 147.2 \\ 4.8 \\ \hline 152.0 \end{array}$$

$$\begin{array}{r} 142.5 \\ 4.2 \\ \hline 146.7 \\ 2.1 \\ \hline 148.8 \end{array}$$

$$\begin{array}{r} 141.8 \\ 4.9 \\ \hline 146.7 \\ 5.2 \\ \hline 151.9 \end{array}$$

$$\begin{array}{r} 139.9 \\ 4.8 \\ \hline 144.7 \\ 4.7 \\ \hline 149.4 \end{array}$$

$$\begin{array}{r} 137.6 \\ 4.1 \\ \hline 141.7 \\ 4.1 \\ \hline 145.8 \end{array}$$

$$\begin{array}{r} 136.4 \\ 4.1 \\ \hline 140.5 \\ 4.1 \\ \hline 144.6 \end{array}$$

$$\begin{array}{r} 133.7 \\ 4.1 \\ \hline 137.8 \\ 4.1 \\ \hline 141.9 \end{array}$$

$$\begin{array}{r} 130.2 \\ 4.1 \\ \hline 134.3 \\ 4.1 \\ \hline 138.4 \end{array}$$

$$\begin{array}{r} 126.7 \\ 4.1 \\ \hline 130.8 \\ 4.1 \\ \hline 134.9 \end{array}$$

$$\begin{array}{r} 135.8 \\ 4.9 \\ \hline 140.7 \\ 4.0 \\ \hline 144.7 \end{array}$$

$$\begin{array}{r} 132.4 \\ 4.9 \\ \hline 137.3 \\ 4.0 \\ \hline 141.3 \end{array}$$

$$\begin{array}{r} 128.1 \\ 4.9 \\ \hline 133.0 \\ 4.0 \\ \hline 137.0 \end{array}$$

$$\begin{array}{r} 126.3 \\ 4.9 \\ \hline 131.2 \\ 4.0 \\ \hline 135.2 \end{array}$$

$$\begin{array}{r} 124.8 \\ 4.9 \\ \hline 129.7 \\ 4.0 \\ \hline 133.7 \end{array}$$

142.80



+50

13

12 + 68.42 BC RT

T.P. 050 134.24 12.98 133.74

+50

12 + 00.84 EC

14

11 + 50

146.72

17

17

17

132.5	127.0
7.7	7.2
20	20
134.7	134.7
4.5	4.5
20	20
130.2	130.2
4.0	4.0
20	20
132.2	132.2
5.1	5.1
20	20
129.1	129.1
8.2	8.2
20	20
128.2	128.2
6.0	6.0
20	20
131.2	131.2
5.0	5.0
20	20
130.8	130.8
6.0	6.0
20	20
127.9	127.9
1.9	1.9
20	20
125.2	125.2

130.2	126.3
4.0	7.9
20	20
132.9	132.9
4.0	4.0
20	20
133.7	133.7
5.1	5.1
20	20
129.1	126.0
8.2	8.2
20	20
128.2	128.2
6.0	6.0
20	20
131.2	131.2
5.0	5.0
20	20
130.8	130.8
6.0	6.0
20	20
127.9	127.9
1.9	1.9
20	20
125.2	125.2

129.1	126.0
8.2	8.2
20	20
128.2	128.2
6.0	6.0
20	20
131.2	131.2
5.0	5.0
20	20
130.8	130.8
6.0	6.0
20	20
127.9	127.9
1.9	1.9
20	20
125.2	125.2

128.2	125.2
6.0	6.0
20	20
131.2	131.2
5.0	5.0
20	20
130.8	130.8
6.0	6.0
20	20
127.9	127.9
1.9	1.9
20	20
125.2	125.2

143.8	138.7	136.4
8.0	10.3	10.3
20	20	20
138.7	138.7	136.4
8.0	8.0	8.0
20	20	20
138.7	138.7	136.4
8.0	8.0	8.0
20	20	20
143.6	138.3	135.4
8.2	9.1	9.1
20	20	20
138.3	138.3	135.4
8.2	8.2	8.2
20	20	20
143.7	138.1	135.4
8.2	9.7	9.7
20	20	20
138.1	138.1	135.4
8.2	8.2	8.2
20	20	20
143.9	138.7	132.1
8.0	9.1	9.1
20	20	20
138.7	138.7	132.1
8.0	8.0	8.0
20	20	20
144.0	139.1	132.0
7.0	9.1	9.1
20	20	20
139.1	139.1	132.0
7.0	7.0	7.0
20	20	20

134.24

146.72

16

T.P. 0.60 97.30 12.94 96.70

+50

$\begin{array}{r} 2.4 \\ 97.30 \\ \hline 94.80 \end{array}$	$\begin{array}{r} 2.01 \\ 94.69 \\ \hline 92.68 \end{array}$	$\begin{array}{r} 3.20 \\ 93.90 \\ \hline 90.70 \end{array}$	$\begin{array}{r} 9.2 \\ 94.10 \\ \hline 84.90 \end{array}$	$\begin{array}{r} 4.05 \\ 93.25 \\ \hline 89.20 \end{array}$	$\begin{array}{r} 4.14 \\ 94.16 \\ \hline 90.02 \end{array}$	$\begin{array}{r} 4.0 \\ 93.30 \\ \hline 89.30 \end{array}$	$\begin{array}{r} 4.33 \\ 97.60 \\ \hline 93.27 \end{array}$	$\begin{array}{r} 4.0 \\ 100.00 \\ \hline 96.00 \end{array}$
---	--	--	---	--	--	---	--	--

T.P. 0.25 109.62 12.86 109.87

15

+50

$\begin{array}{r} 13.21 \\ 108.96 \\ \hline 95.75 \end{array}$	$\begin{array}{r} 14.07 \\ 108.16 \\ \hline 94.09 \end{array}$	$\begin{array}{r} 14.0 \\ 108.23 \\ \hline 94.23 \end{array}$	$\begin{array}{r} 15.01 \\ 107.22 \\ \hline 92.21 \end{array}$	$\begin{array}{r} 14.21 \\ 108.02 \\ \hline 93.81 \end{array}$	$\begin{array}{r} 14.6 \\ 109.62 \\ \hline 95.02 \end{array}$	$\begin{array}{r} 15.2 \\ 107.03 \\ \hline 91.83 \end{array}$	$\begin{array}{r} 12.0 \\ 110.23 \\ \hline 98.23 \end{array}$	$\begin{array}{r} 11.9 \\ 110.33 \\ \hline 98.43 \end{array}$
--	--	---	--	--	---	---	---	---

T.P. 104 122.23 130.3 121.21

14

134.24

$\begin{array}{r} 12.3 \\ 121.9 \\ \hline 109.6 \end{array}$	$\begin{array}{r} 12.0 \\ 122.2 \\ \hline 110.2 \end{array}$	$\begin{array}{r} 11.6 \\ 122.23 \\ \hline 110.63 \end{array}$	$\begin{array}{r} 11.4 \\ 123.0 \\ \hline 111.6 \end{array}$	$\begin{array}{r} 11.5 \\ 121.7 \\ \hline 110.2 \end{array}$
--	--	--	--	--

134.24

SE. Cor  
Lot 7  
P.K. 200

Curve Levels on Lowell  
 Plum Wly To " Pl.

119.05

SWBP	7.77	94.99	87.22	Lowell Plum	N CB	6.91	113.04
0+00 = W/L PLUM					" 9UT	6.26	112.69
S Top CB		10.12	84.87		2+24.55 RP		
N " "		10.17	84.82		N CB	3.87	115.18
0+25 = CB P.C.					" 9UT	4.18	114.87
N CB		7.49	82.60		2+50		
S "		7.35	82.64		N CB	2.46	116.59
T.P.	12.66	107.27	0.38	94.61	" 9UT	2.79	116.26
	12.05	119.05	0.27	107.00	T.P.	11.98	130.14
2+04.08 = Ely Ranch 172					3+00		
N CB		6.85	112.20		N CB	6.46	121.70
9UT		7.24	111.61		" 9UT	8.77	121.37
C Pav. E.M.H.		7.28	111.77		5+50		
9UT		7.48	111.57		N CB	3.22	127.94
S CB. Prod. from East		6.27	112.38		" 9UT	3.56	126.58

2+14.42 = PC							

check to SWBP Lowell Plum  
 1002 87.28 87.22  
 006

Contd. p 65

10+78.9W = E.C.  
 5.85

10+48.07 = PC. Curb Return end gutter

97.30

91.10	88.30	87.70	86.95	87.30	86.96	87.72	87.90	93.90	94.90
6.2	9.0	9.40	10.25	10.0	10.2	9.8	9.4	10.1	10.4
10	10	17.5	17.5		10.2	10.7	9.4	10.2	10.4
					9.4	9.8	9.4	10.1	10.4

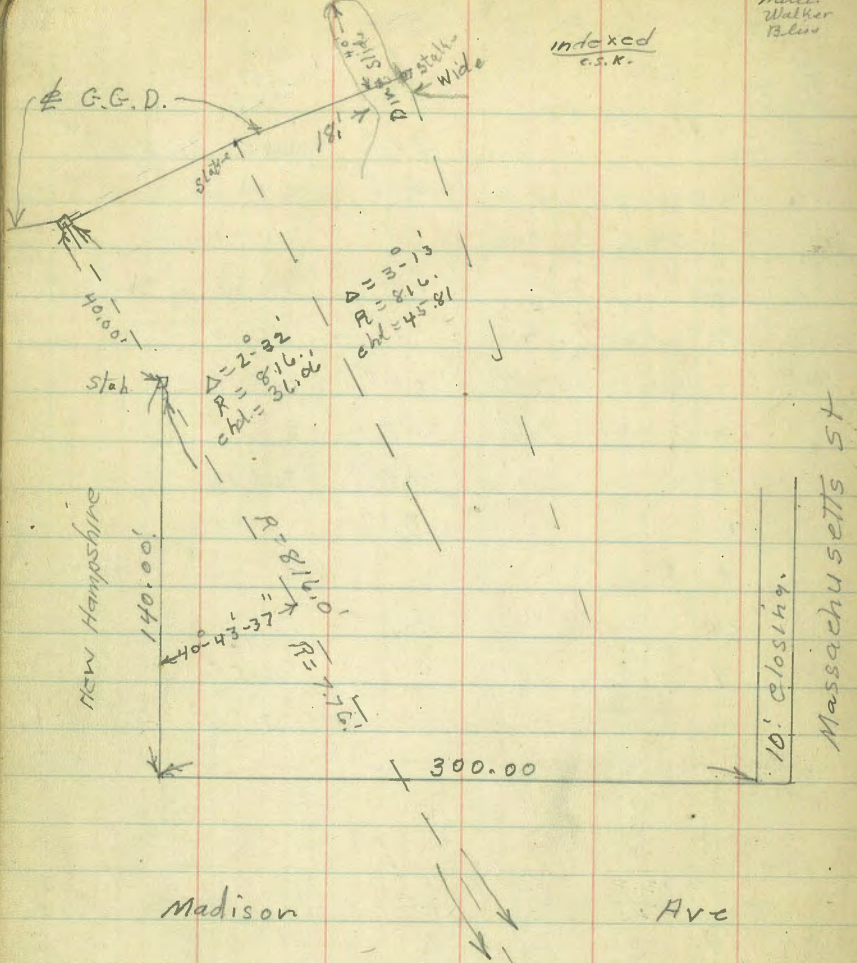
97.30

Survey of Golden Gate Drive

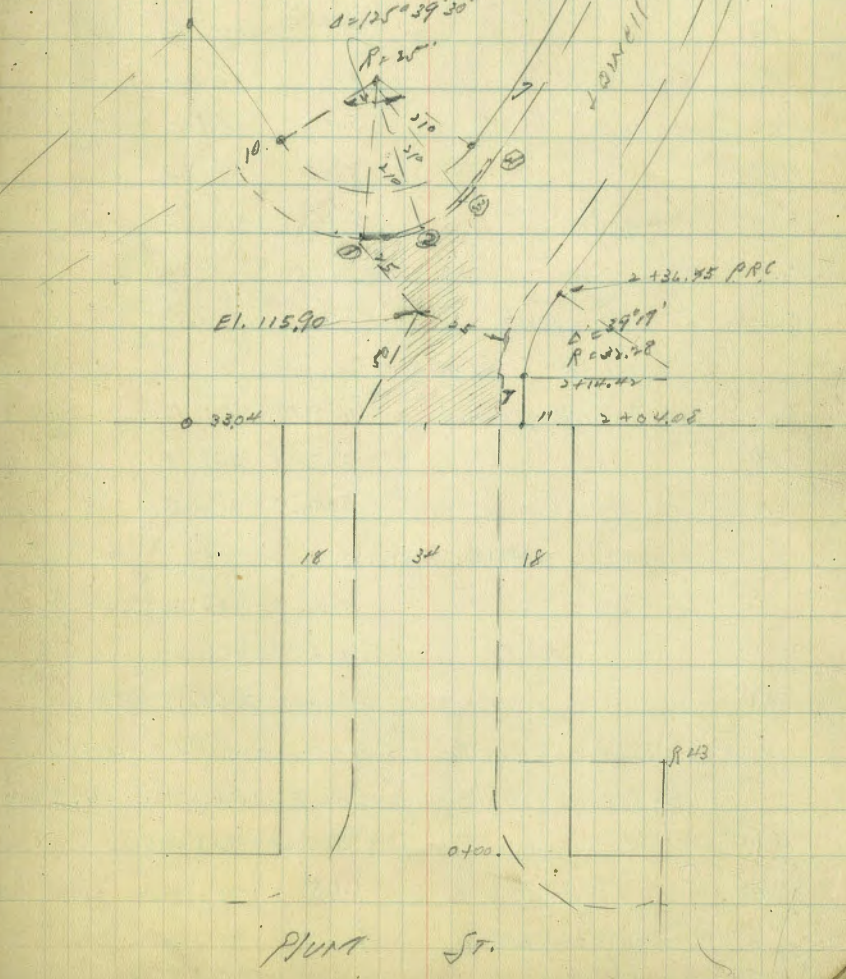
11-6-34  
Miller  
Walker  
Blair

130.12

indexed  
C.S.K.



① Top end of	11.01	119.13
gut	11.25	118.79
② cb	11.34	118.82
gut	11.54	118.49
③ cb	11.01	119.13
gut	11.34	118.79
④ = P.C.C. cb	10.08	120.06
gut	10.29	119.75
50' W. P.C.C. cb	4.26	124.88
25' " " "	0.17	125.97



11-6-36  
Miles  
Walker  
Bliss

X See Alley B.K. 13. Sub. Lots 20 to 59, Blk N  
Teralta. Orange to Polk. bet. 39<sup>th</sup> + 40<sup>th</sup> Sts

indexed  
c.s.k.

Orange

Ave

66

B.M. B.P. 4.26 370.03 365.77 n.w. 39<sup>th</sup> + orange

14' N. of S. Line = S. Curb Line Orange

E. - 25	dirt gutter	5.9	364.1
E. - 25	ent. curb.	5.35	364.68
E.	" "	5.32	364.71
E.	dirt gutter	5.8	364.2
E.	" "	5.7	364.3
W.	" "	5.7	364.3
W.	ent. curb.	5.11	364.92
+25	" "	5.03	365.00
+25	dirt gutter	5.5	364.5

1.5 N. of S. Line = S. Side ent. Walk.

E. = S. End. Alley Curb. 5.21 364.82

0+00 = S. Line Orange

W. S. End. Curb. + ground.	4.87	365.16
±	5.3	364.7
E.	5.2	364.8

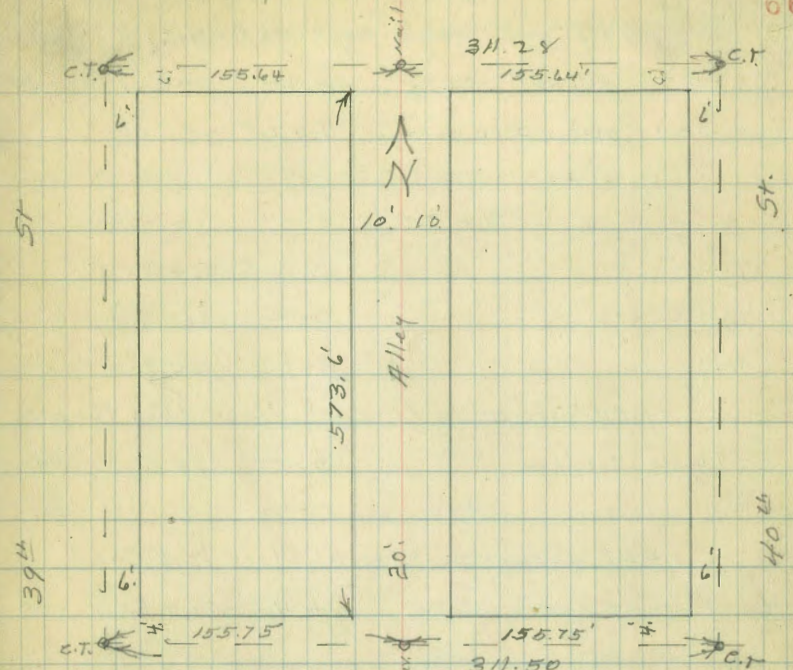
0+15. South.

E	4.5	365.5
±	4.7	365.3
W	4.5	365.5

0+22 = S. End. Cypress. Hedge on W. 1.0' in Alley

0+62 = N. End. double garage on E. ent. floor 4.8' back

W	5.0	365.0	
±	4.8	365.2	
E + 1	w. edge ent. apron.	4.77	365.26
E + 4.8	floor	4.67	365.36



Polk

Ave

370.03

0+77 = S. End. above garages. on E

E - 4.8'	= floor	4.77	365.26	✓
E - 1.0'	= w. edge ent. apron.	4.83	365.20	

0+81 N. End. double garage on E. ent. floor 4.7' back

E - 4.7'	floor	4.60	365.43	✓
E - 0.7'	w. edge ent. apron.	4.88	365.15	

0+90 garage on W

W - 3.1'	= floor.	4.65	365.38	✓
W - 1.1'	= E. edge ent. apron	4.80	365.23	

370.03

0+99 S. End double garage on E. 4.7' Back  
 E-4.7 floor 4.80 ✓ 365.23 ✓  
 E-0.7 cmt. apron w. edge 5.02 ✓ 365.01

1+00.

E. 5.2 ✓ 364.8  
 ♀ 5.2 ✓ 364.8  
 W. 5.1 ✓ 364.9

1+09 garage on E. cmt. floor 12.5 Back  
 E-12.5 = floor 5.0 ✓ 365.0 ✓

1+41 garage on E. cmt. floor 12.5 Back  
 E-12.5 floor 5.4 ✓ 364.6 ✓

1+50

W 5.6 ✓ 364.4  
 ♀ 5.4 ✓ 364.6  
 E. 5.0 ✓ 365.0

1+65 garage on W. cmt. floor 1.1 Back  
 W-1.1 = floor. 5.3 ✓ 364.7 ✓

1+82 garage on W. cmt. floor 1.2 Back  
 5.72 ✓ 364.31 ✓

2+00

E 5.9 ✓ 364.1  
 ♀ 5.9 ✓ 364.1  
 W 5.7 ✓ 364.3

370.03

2+0.5 = N. End double garage on W. cmt. floor 1.5 Back 67  
 W-1.5 = floor 5.80 ✓ 364.23 ✓

2+25 = S. End. above garages on W. ✓  
 W-1.5 5.83 ✓ 364.20

2+33 garage on E. cmt. floor 0.5 Back  
 E-0.5 6.25 ✓ 363.78 ✓

2+50

W 6.3 ✓ 363.7  
 ♀ 6.5 ✓ 363.5  
 E 6.6 ✓ 363.4

2+81 garage on E. cmt. floor 2.0 Back  
 E-2 = floor 6.60 ✓ 363.43 ✓

E 6.6 ✓ 363.4  
 ♀ 6.7 ✓ 363.3  
 W. 6.8 ✓ 363.2

2+97 garage on W. cmt. floor 5.0 Back.  
 W-5.1 = floor 6.35 ✓ 363.68 ✓

T.P. 3.52 366.89 - 6.66 ✓ 363.37

Sta 3+30 see next page.

3+54 { garage on W. cmt. floor 3.3 Back  
 N. End double garage on E. cmt. floor 2.0 Back

E-2 = floor 3.84 ✓ 363.05 ✓

E 3.9 ✓ 363.0  
 ♀ 3.8 ✓ 363.1  
 W 4.0 ✓ 362.9

+33 = floor 3.84 ✓ 363.03 ✓

366.89.

3+30

W.	3.6 ✓	363.3
φ.	3.6 ✓	363.3
E.	3.5 ✓	363.4

3+70 { garage on W. cmt. floor 3.2' Back  
 S. end. above garages on E. 2.5' Back

W-3.2' = floor	4.05 ✓	362.84	✓
E-2.5' = " Not parallel to fly	3.90 ✓	362.99	✓

4+00

E	4.1 ✓	362.8
φ	4.3 ✓	362.6
W	4.3 ✓	362.6

4+32 garage on W. dirt floor 5.1' Back

W-5.1' floor	5.1 ✓	361.8	✓
--------------	-------	-------	---

4+50

W	5.0 ✓	361.9
φ	4.9 ✓	362.0
E	4.6 ✓	362.3

5+00

E	5.1 ✓	361.8
φ	5.4 ✓	361.5
W	5.3 ✓	361.6

366.89

5+30

W	5.6 ✓	361.3
φ	5.8 ✓	361.1
E	5.7 ✓	361.2

5+60

E	6.5 ✓	360.4
φ	7.0 ✓	359.9
W.	4.6 ✓	360.3

5+70

W	6.8 ✓	360.1
+5	7.6 ✓	359.3
φ	7.7 ✓	359.2
+5	7.5 ✓	359.4
E.	6.7 ✓	360.2

5+73 1/2 = N. Line Polk Ave.

E. cmt. cl.	7.54 ✓	359.38
E. pav. N. end.	7.65 ✓	359.24
φ " " "	7.82 ✓	359.07
W " " "	7.63 ✓	359.26
W. cmt. cl.	7.48 ✓	359.41

6.5' S. of N. Line = N. cl. line

W. cmt. cl.	7.58 ✓	359.31
W gutter	8.06 ✓	358.83
φ " "	8.13 ✓	358.76
E. " "	8.14 ✓	358.75
E cmt. cl.	7.66 ✓	359.23

58

BM chk

366.89
TP. 2.73
563.76
6.36
370.82
4.54
365.78

Indexed  
c.s.K.

Drainage S. E. Cor. Mission +  
Mississippi Sts.

11-6-36  
Walter  
Blum

B.M. B.P. 1.54. 341.60

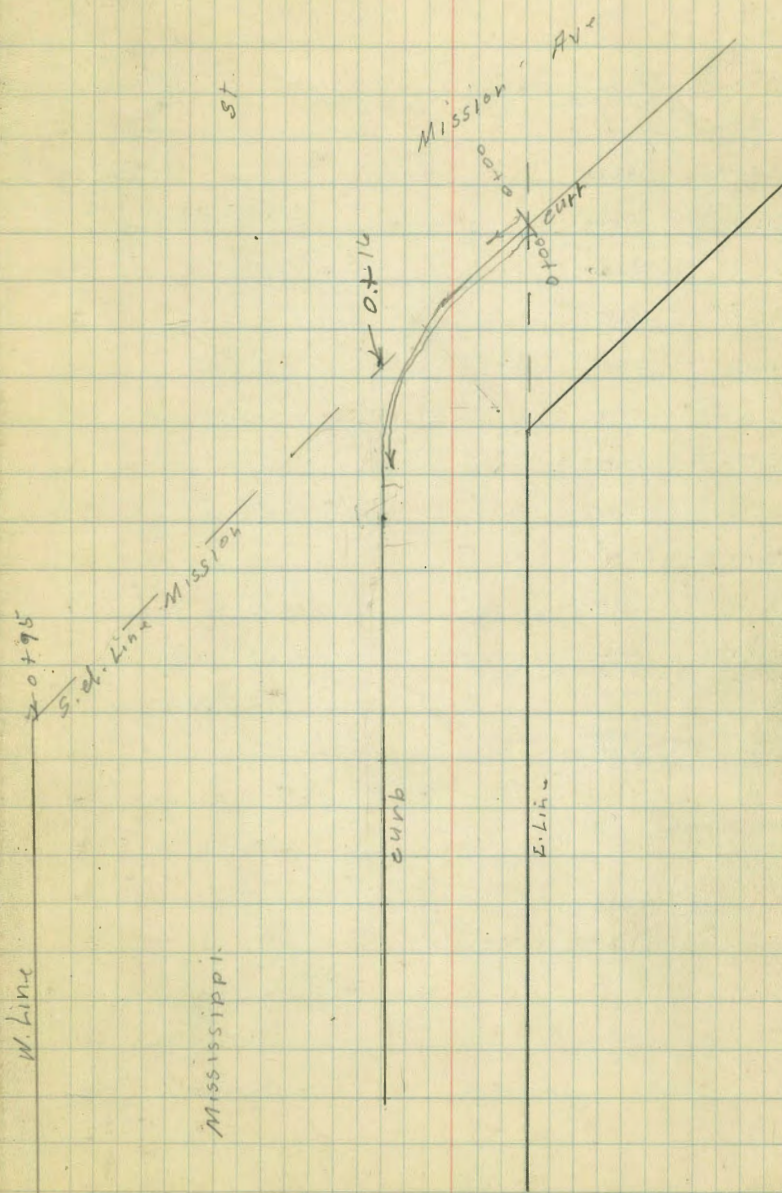
34006 S. E. Madison  
+ Mississippi

S. of Line Mission

0+00 = E. Line Mississippi	4.29
0+17 W. E. ch.	4.33
0+35 "	4.49
0+50 "	4.59
0+70 "	4.67
0+79 W. ch. MISSISSIPPI	4.71
0+95 " Line "	4.99

E. gutter Line MISSISSIPPI

0+60 = E. Line MISSISSIPPI	4.29
0+10 S	4.35
0+20 "	4.41
0+30 "	4.46
0+40 "	4.53
0+50 "	4.53
0+65 "	4.50
0+85 "	4.63
1+00	4.60
1+40	4.70





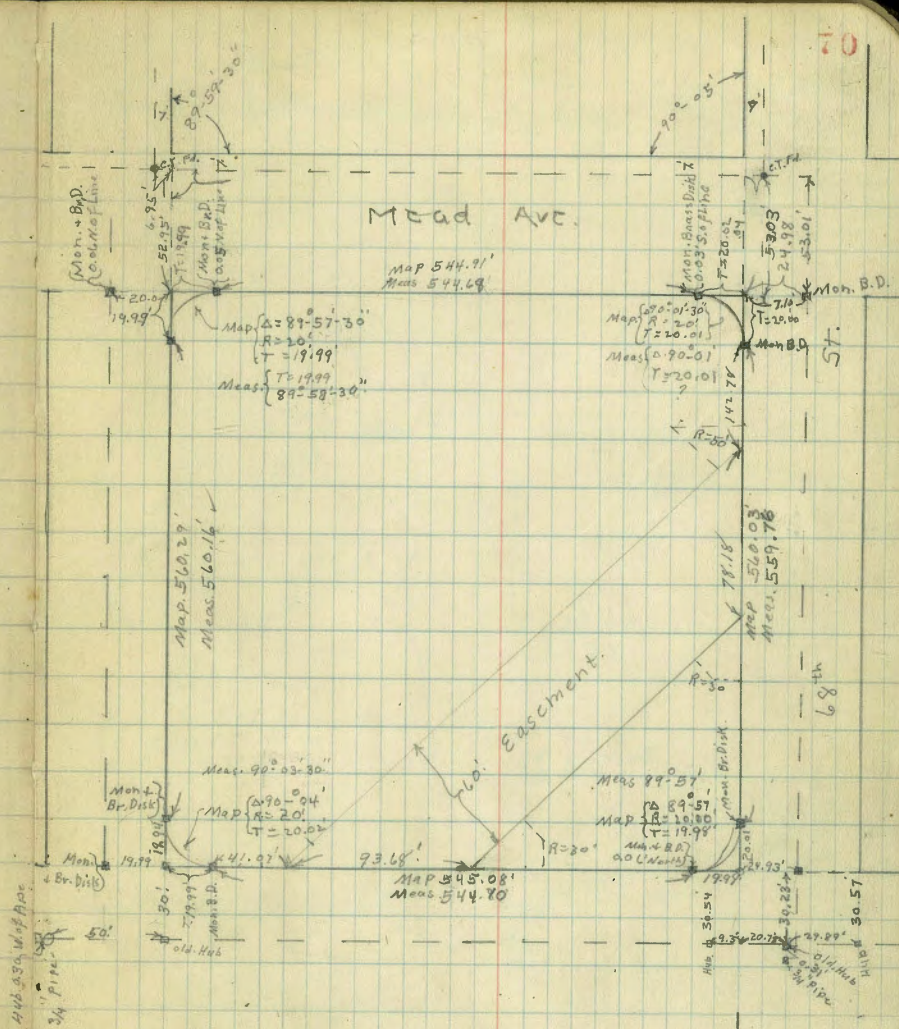
1-7-37  
Mellen  
Walker  
Bloss

Ocean View Gardens.  
chh. of Subdivision Map.

Indexed  
C.S.K.

Measurements on Lots  
N. Line to Regan Rd

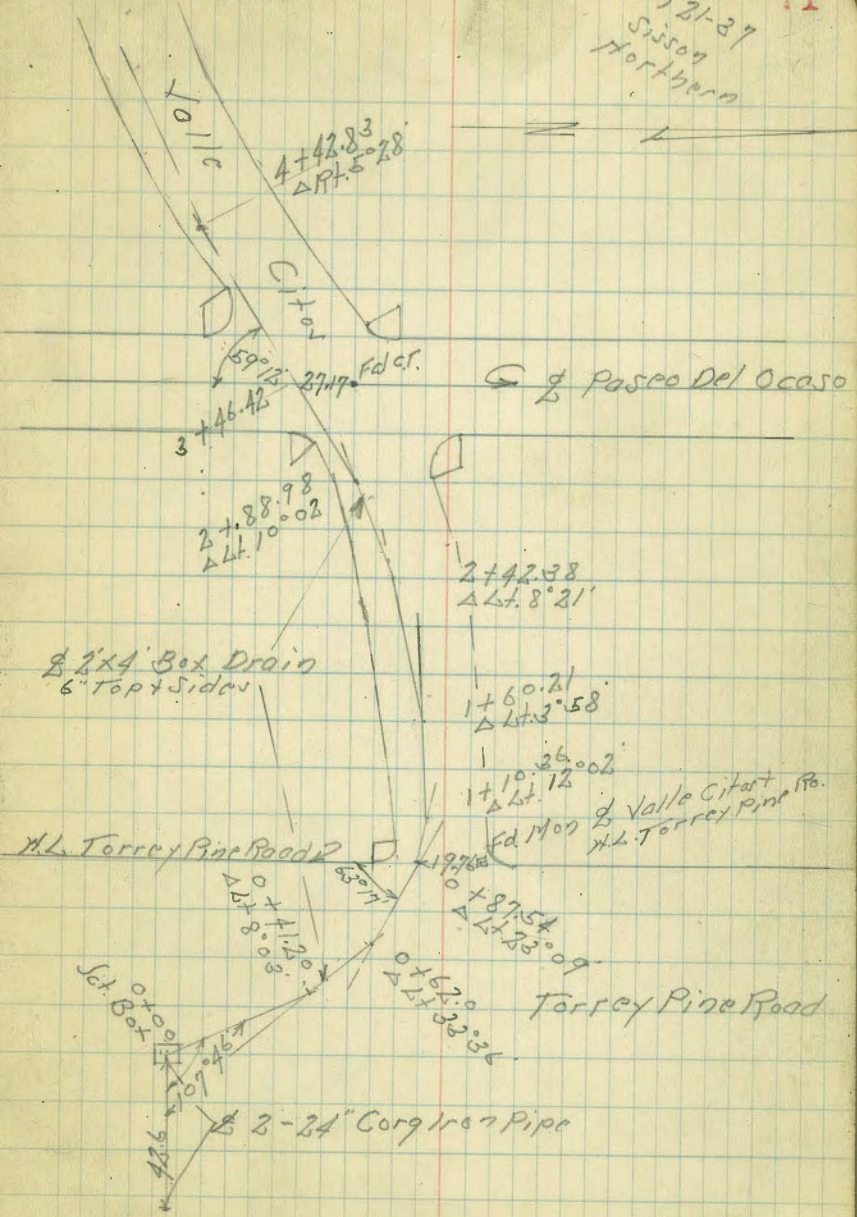
	N. Line Meas.	S.E. nd.
Lot 1	32.97'	33.00'
" 2	52.94'	53.00'
" 3	52.97'	53.00'
" 4	52.97'	52.90'
" 5	52.94'	53.05'
" 6	52.98'	52.97'
" 7	52.99'	52.97'
" 8	52.98'	52.97'
" 9	53.00'	52.93'
" 10	53.00'	52.97'
" 11	34.80'	35.12'
	544.62'	544.88'
	19.99	19.99
	20.02	19.98
	584.63	584.85

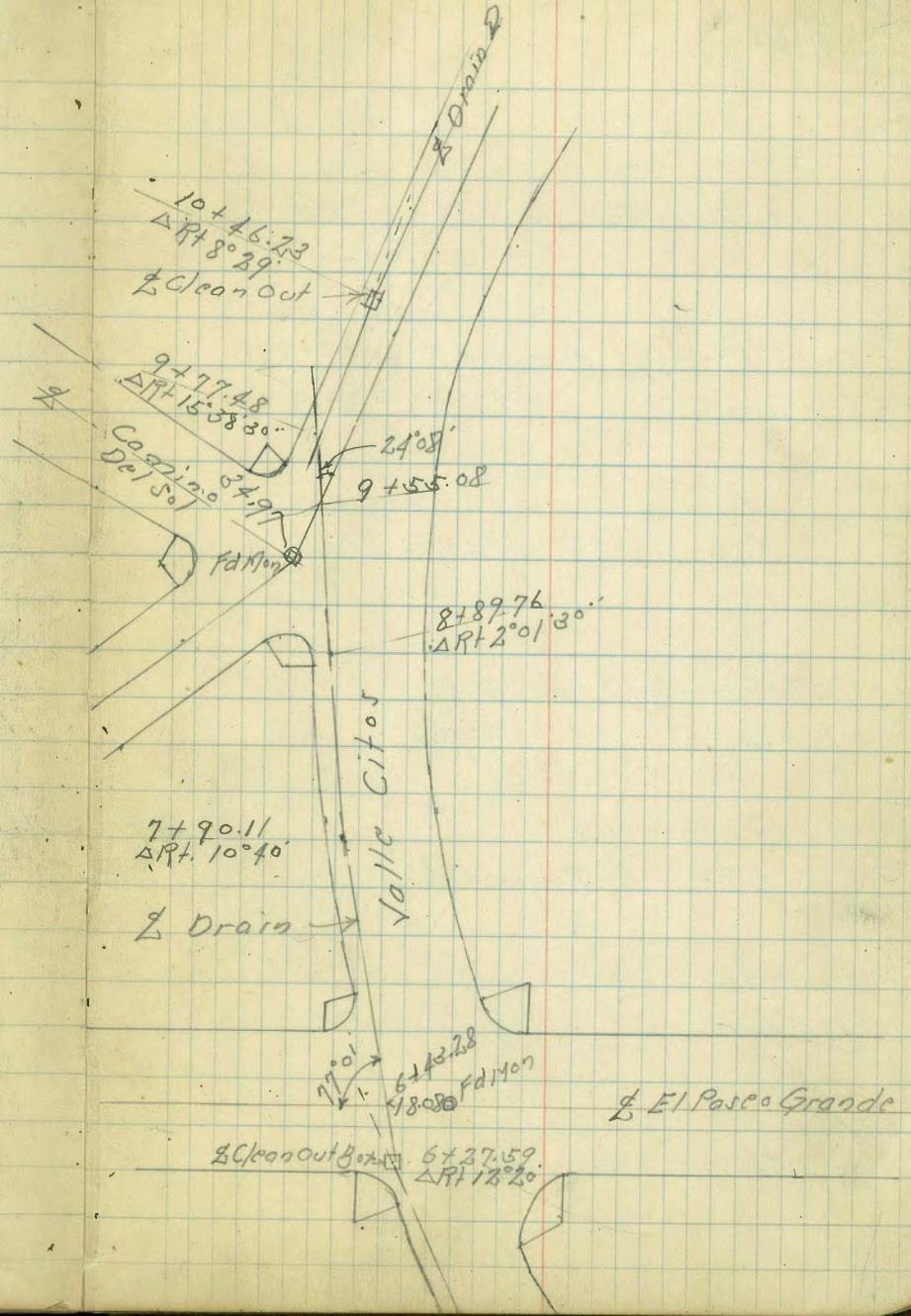


Valle Citar  
 Location of Existing 2'x4 Conc.  
 Storm Drain La Jolla Shores Pt. Ocaso

INDEXED  
 C.S.K.

Jan 21-37  
 Sisson  
 Hartburn  
 71





Levels Valle Citoz Drain

	FS	H.I.	BS	Elev	BP Spotted Ayudie De Laplaya
BM	4.28	8.09		3.81	

14+05.73 - Outlet F.L. 9.28 - 1.19

10+46.23 - Clean Out Rim 4.45 3.64  
 Floor Line 8.63 - 0.54

TP 8.74 12.38 4.45 3.64

6+27.59 - Clean Out Rim 5.37 7.01  
 Floor Line 10.30 2.08

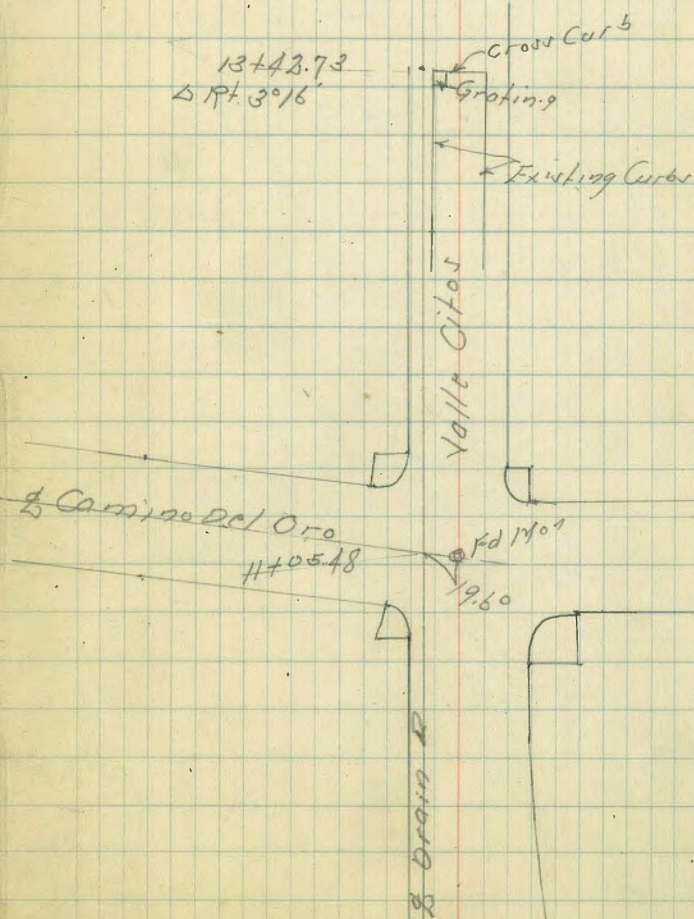
TP 6.93 16.25 3.06 9.32

0+0 - Set Box Rim 3.05 13.20  
 Floor Line 6.82 9.43

42.6 E of Set Box -  
 Inlet 2-24" Pipe F.L. 5.47 10.75

14+05.73 =  
 Out let of  
 2'x4' Drain

13+42.73  
 Δ Pt 30/6'



LOCATION of Drain  
at La Jolla Shores  
N of Paso Del Ocaso,  
and Camino del Oro

Moore  
Sisson  
Northon  
3-1-47  
Indexed  
C.S.K.

Rec p 70	12.36	25.50		10.20	P.M. JCT. BOX
T.P.	9.73	36.26	1.03	26.53	

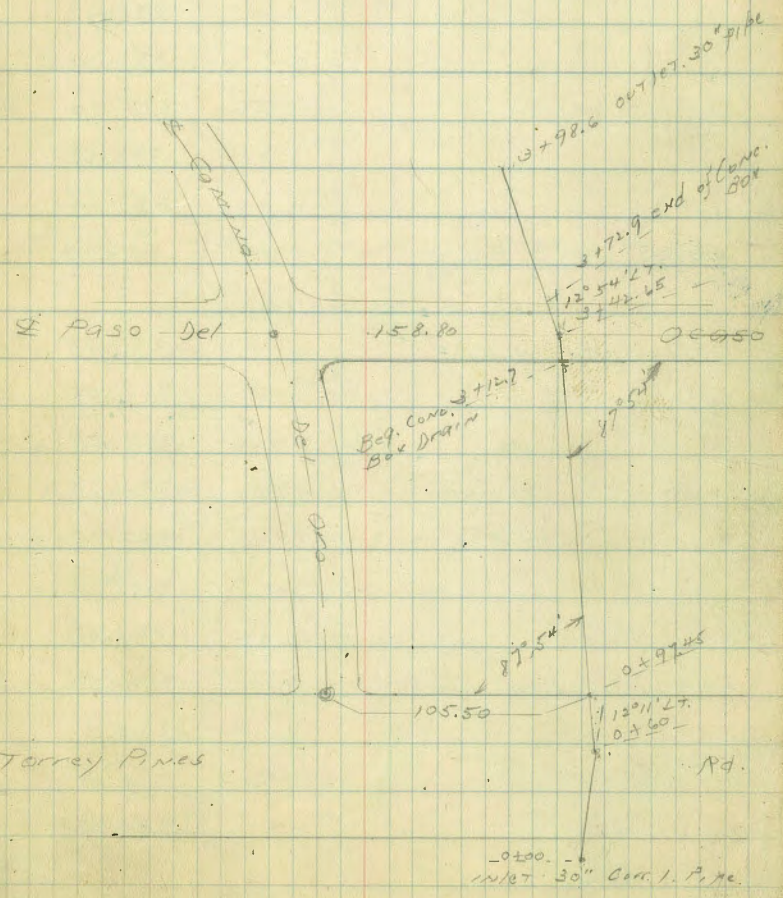
F.L.  
0+00 = inlet of 30" Corr. I.P. 12.03 22.23

T.P. 0.87 22.52 12.56 21.70

3 + 12.7 Box. Conc. Box 9.0 13.52

3 + 98.0 outlet 30" pipe 13.6 8.92

Conc. Box drain  
at Paso Del Ocaso



Torrey Pines

0+00 -  
inlet 30" Corr. I.P. etc.

2-3-37 X Sec. Alley BIK F. M. Fadden + Buxtons  
 " " " " 33 Park Villas  
 Dwight to Landis bet. 31st + Herman.

B.M.B.P	6.01	338.47		332.46
old B.M. Cond				
Set B.M.B.P. X	5.70	338.52	5.65	332.82

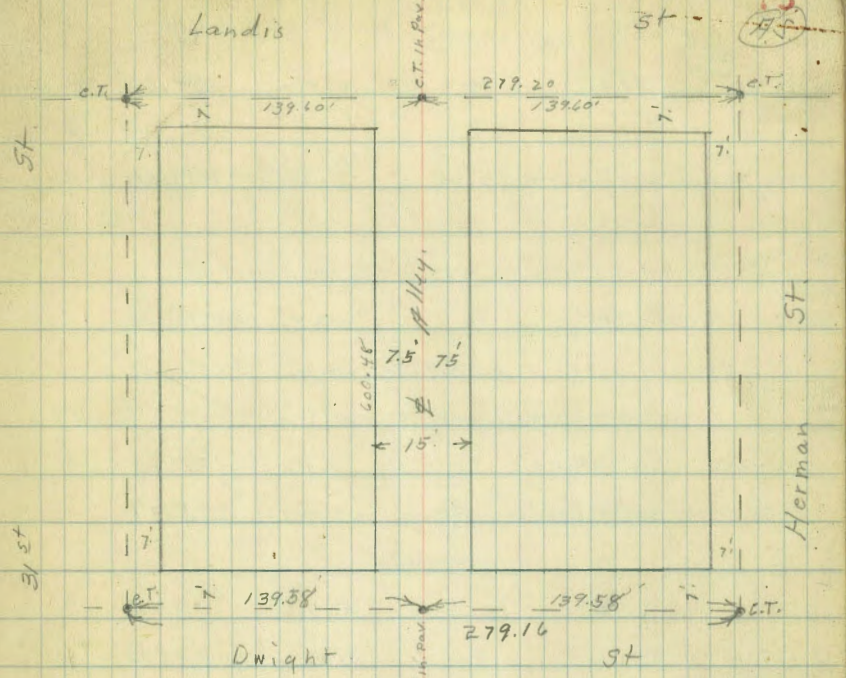
N.E. Ray  
 + Dwight Sls  
 N.E. 21st  
 + Dwight

00-10 = N. ch Line Dwight St.

W. - 25	gutter pav	5.70	332.82
W. - 25	ent. ch	5.15	333.37
W.	" "	5.00	333.48
N.	gutter Pav.	5.60	332.92
±	" "	5.52	333.00
E.	" "	5.43	333.09
E.	ent. ch.	5.00	333.52
E + 25	" "	4.88	333.64
E + 25	gutter Pav	5.39	333.13

0+00 = N. Line Dwight.

E. ent. d. N. End.	4.77	333.75
E. pav	4.94	333.58
±	5.04	333.48
W.	4.90	333.62
W ent d	4.80	333.72
0+38 garage on W. ent floor	1.8' Back	
W - 1.8 floor	4.00	334.52
W - 0.2 E. End. ent. Apron	4.12	334.40
W	4.1	334.4
±	4.2	334.3
E.	4.2	334.3



	338.52	
0+59 garage on E. ent floor	4' Back	
E - 4.0' = floor	3.85	334.67
0+70 garage on E. ent floor	4' Back	
E - 4.0 floor	3.76	334.76
E	3.9	334.6
±	3.8	334.7
W	3.4	335.1
	1+00	
W	3.5	335.0
±	3.6	334.9
E	3.5	335.0

338.52

1+07 5 garage on E. cnt. floor 3.6 Back  
E-3.6 floor 2.90 335.62

7.3 E. of  $\phi$  = W. Edge cnt. apron 3.12 335.40

0+77 = S. End. Fence on E. 0.4 in Alley

1+00 = N " " " 0.4 in Alley

T.P. 8.71 344.07 3.16 335.36

1+46 garage on E. cnt. floor 3.8 Back

E-3.8 = cnt. floor 7.88 336.19

7.2 E. of  $\phi$  = W. Edge cnt. Apron 8.09 335.97

1+50

E 8.0 336.1

$\phi$  8.2 335.9

W 8.2 335.9

+0.2 =  $\phi$ , E. End. 30" cnt. walls 7.96 336.12

1+75 = S. End. lattice fence on E. 0.5 in Alley

2+00

W 7.1 337.0

$\phi$  7.1 337.0

E. 7.0 337.1

2+25 = N. End. above Fence 0.2 in Alley.

2+50

E 6.4 337.7

$\phi$  6.1 338.0

W 6.1 338.0

344.07

3+00

W 4.8 339.3

$\phi$  4.9 339.2

$\phi$  Sewer M.H. Top. 4.98 339.09

W?E 4.7 339.4

3+46

E-0.6 = W. End. 36" cnt. walk. 3.36 340.71

3+50

W 2.9 341.2

$\phi$  2.9 341.2

E 3.2 340.9

4+00

E 2.3 341.8

$\phi$  2.3 341.8

W 2.5 341.6

4+50

W 1.3 342.8

$\phi$  1.3 342.8

E 1.3 342.8

T.P. 5.42 348.37 1.12 342.95

5+00

E 4.8 343.6

$\phi$  4.5 343.9

W 4.3 344.1

348.37

5+50

W	4.0	344.4
±	4.0	344.4
E	4.1	344.3

5+70

C	3.7	344.7
±	3.6	344.8
W	3.5	344.9

5+90

W	3.8	344.6
±	4.2	344.2
E	4.0	344.4

6+00<sup>48</sup> = S. Line - Landis St

E. cnt. db	S. End.	5.11	343.26
E. Pav	" "	5.26	343.11
±	" "	5.45	342.92
W	" "	5.20	343.17
W. cnt. db	" "	5.12	343.25

6+16<sup>48</sup> = S. db. Line of Landis St

W-25	cnt db	5.51	342.86
W-25	pav	5.97	342.40
W	"	5.79	342.58
W	cnt. db	5.27	343.10
±	pav	5.74	342.63
E	"	5.72	342.65
E	cnt. db	5.28	343.09
E+25	cnt. db	5.01	343.36
E+25	pav	5.53	342.84

348.37

77

S.E. 31<sup>51</sup>

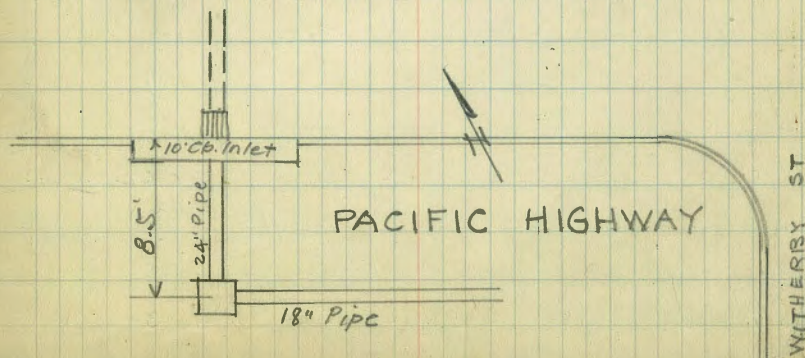
T.P.B.M.B.P.	0.05	342.01	6.41	341.96	± Landis St
T.P.B.M.B.P.	5.79	338.61	7.19	332.82	± 41.88
chk. orig. B.M.			6.15	332.46	± 4.8 31 <sup>51</sup> ± 2 night

Drainage at Pacific Highway, Witherby and Subway Sts  
Copied from Book 1503, p 77.

B.M.	6.11	7.24	1.13	NE Witherby + Pacific
Sec A' at 90° to Pacific at Point A (Sec 15-21/78)				
N Gutter at "A"	pav	6.72	0.52	
+15.25 S = N 1/4	"	6.38	0.86	
+30.5 S = ± Pac. Hwy.		6.04	1.20	
+45.75 S = S 1/4		6.18	1.06	
+61 S = S gutter in driveway		6.75	0.49	

Copied from Grade Book - 186

B.M.	4.70	5.83	1.13	NE Witherby and Subway Sts.
Top of sewer 10' W of Sec A'	8.30	-2.47		
Paving ± Pacific	4.70	1.13		
F.L. 24' Pipe Outlet 10' Cb Inlet.	8.02	-2.19		
Top of Water Main (10' S of ± Pacific)	10.00	-4.17		





10-29-37  
Miller  
Bliss

Drainage at Pacific Ave  
& Subway St.

Indexed  
C.S.K.

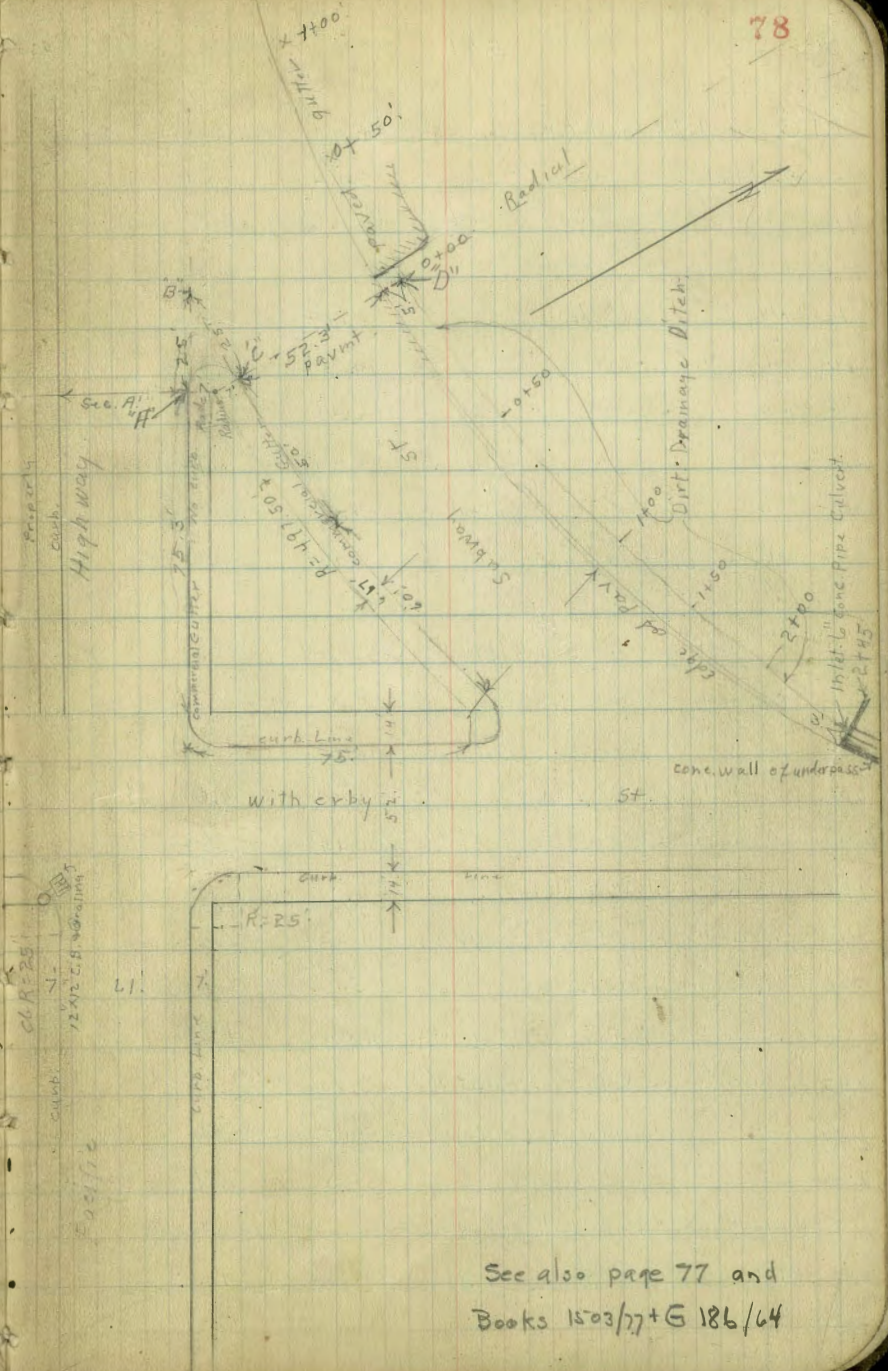
				Indexed C.S.K.
B.M. Slyarb	0.32	28.05	27.73	Witherby & Moore STs
T.P.	0.24	15.26	13.03	15.02
T.P.	1.83	6.27	10.82	4.44
N. Gutter of Pacific				6.27
200' E of E. line Witherby gutter			5.42	.85
160.0 " " " " " " "			5.50	.77
100.0 " " " " " " "			5.44	.79
50.0 " " " " " " "			5.61	.66
11.0 " " " " " " "			5.57	.70
Set B.M. B.P.			5.14	1.13
E. Line Witherby			5.55	.72
114' W = E. d. = P.I. Curbs.			5.57	.70
25' N of d. P.E. in E. gutter Witherby			5.60	.67
50' " " " " " " " " "			5.49	.78
75' " " " " " " " " "			5.06	1.21
40' W of E. Line = E. Witherby			5.64	.63
66' W of E. = N. d. = P.I. Curbs.			5.67	.60
25' N of above d. P.I. in W. gutter Witherby			5.68	.59
50' " " " " " " " " "			5.61	.66
75' " " " " " " " " "			5.19	1.08
W. Line Witherby N. gutter Pac.			5.70	.57
+25' W			5.68	.59
+50' W			5.72	.55
+75.3' W		" at A"	5.75	0.52
1+00 <sup>3</sup>		" " B"	5.77	.50
1+10		" " "	5.62	.65
T.P. on 7' Radius	4.78	5.81	5.24	1.03

P.C. Curb Return  
N. E Pacific  
& Witherby

P.C. d. Ret.

P.C. 7' Rad  
Curb. Return

opposite  
Point "A"



See also page 77 and  
Books 1503/77 + G 186/64

P.T.C. opposite 7 <sup>th</sup> Rad. in Sly Gutter subway st	5.21	.60	
50' Ely of Pt C	5.14	.67	
110 " " " " " " " "	4.66	1.15	
13' Nly from "C" on Radial Line	4.79	1.02	
26.2 " " " " " " " "	4.32	1.49	
39.3 " " " " " " " "	4.54	1.25	
52.4 " " " " " " " " = Edge Pav	5.09	.72	
57.2 " " " " " " " " = "D" = dirt gutter	5.9	-0.1	
50' Wly of "D" paved gutter	5.77	.04	
100. " " " " " " " "	5.66	.15	
4' " " " " " " " " Ely End	5.80	.01	
50' Ely of "D" dirt ditch	5.9	-0.1	
" " " " " " " " Edge Pav 5' S of ditch	4.92	.89	
100 " " " " " " " " dirt ditch	5.8	0.0	
" " " " " " " " edge Pav 6' S of ditch	4.49	1.32	
150 " " " " " " " " dirt ditch	6.1	-0.3	
" " " " " " " " Edge Pav 6' S of ditch	4.53	1.28	
200 " " " " " " " " dirt ditch	5.8	0.0	
" " " " " " " " edge Pav 6' S of ditch	4.53	1.28	
245 " " " " " " " " inlet 6' conc. culvert	5.80	.01	
" " " " " " " " Edge pav. 3' S of culvert	5.15	.66	
" " " " " " " " Top zone wall	3.30	2.51	B.P. BM.
Stations continued on next Page.			
T.P.	5.95	6.98	4.78 1.03
T.P.	11.87	18.35	0.50 6.48

T.P.	12.70	29.59	1.46	16.89
Orig. BM.			1.87	27.72 = 27.72
Stations N.Wly side subway, pav. con. from preceding Page				
B.P. BM.	3.26	5.77	2.51	Top. conc. wall Preceding Page
2+65 Nly edge pav. base of wall		5.83	-0.06	
2+65 " " " " " " " " Top " " "		3.26	+2.51	
2+82.5 edge pav base " " " " " " " " " " " "		6.61	-0.84	
2+82.5 F.L. Outlet 6' Culvert		6.54	-0.81	
2+82.5 Top wall .18' Thick		3.30	+2.47	{ 24x30 Cleanout Back of wall with Grating at Top of wall
3+25 Nly edge pav base of wall		8.83	-3.06	
3+25 " " " " " " " " Top " " "		3.30	+2.47	
3+54 Nly edge pav base " " " " " " " " " " " "		9.70	-3.93	
3+54 " " " " " " " " Top " " "		3.36	+2.41	

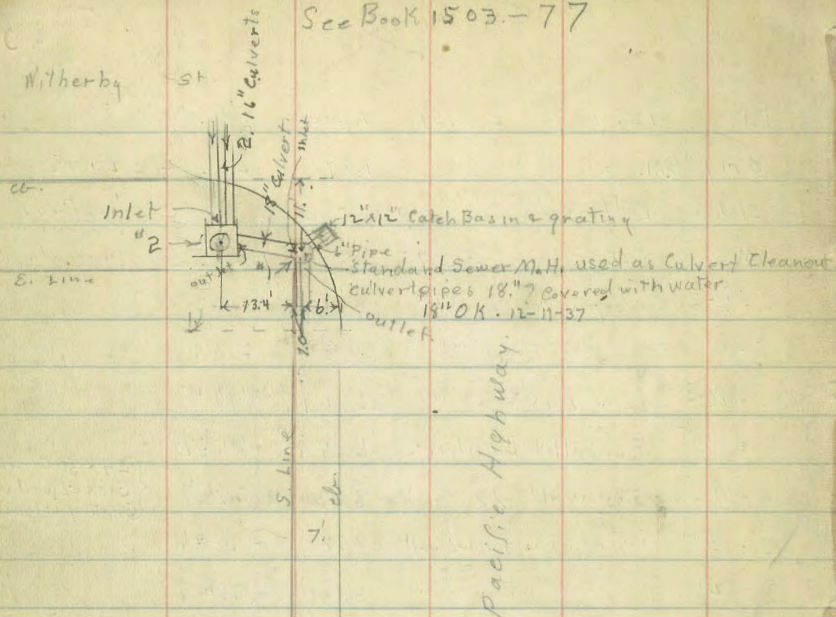
Levels Sly side Pacific Highway at Witherby  
N. E. Witherby  
+ Pacific Highway

B.M.B.P.	5.47	6.60	1.13	
Grating of 12x12 C.B. S.S. Cont. Pacific + Witherby = gutter - Top of cl. at C.B.		5.71	0.83	
		5.03	+1.57	
4 Witherby St		5.75	0.85	
W. Line Witherby cl.		5.24	1.36	
" " " " " " " " gutter		5.99	0.61	
1+00 W. Top cl. (Gutter covered)		5.55	1.05	
2+00 W " " " " " " " "		5.78	0.82	
2+94 E. End 15' cl. inlet Gutter =		7.01	-0.41	cl. inlet filled with cold patch paving.
3+01.5 " " " " " " " "		7.12	-0.52	
3+01.5 " " " " " " " " cl.		6.00	0.60	

Con. Page 80

See Book 1503-77

Wetherby St



Pacific Highway

X - 6.60

F.L. Culverts in Sewer M.H. Cleanout, # 9.50 - 2.90

Additional Notes. 12-11-37.

B.M.	6.4	7.24	1.13	N.E. Wetherby & Pacific
F.L. 18" Culvert in Cleanout #	10.14	- 2.90		2 ft. above
F.L. 18" Culvert outlet in	11.2	10.04	- 2.80	
F.L. 12" " outlet "	11.2	9.84	- 2.60	

Book 1503-77

5.50	5.50	5.50
4.64	4.54	4.34
1.14	10.04	9.84
2.90		

## IMPROVED TABLES AND INFORMATION

← SEE 4408 & 6057

2201 B.

G.B. 186 - 64

1503-77



16 24.5 137.50 279.20  
39.58 14 137.04 137.60

348.87 341.88  
338.47  
9.90  
9.83  
4.51  
.86

74.02 = 41.5+

4.58  
4.75  
9.50

177 60  
92 02  
87 58

8.46 42 = 47 W to 3.985 4.65  
9.23 42 mil

NWBP Mode 4 39th 369.75  
SWBP Monnet 3874 374.50  
S. Lin + Epsilon Prod. 0.51h pav 52.30

3.12  
2.2  
1.90

SL Lowell PLANT W 205.2  
205.5

582.93  
K { 17.97  
18.36  
L { 19.44  
19.87  
196 20.99

242.01  
332.82  
119  
32.44  
6.15  
X 3  
7.5  
158.

40.45 PL Cor To NL etc  
NL etc Lowell To PL 203.62

PLUM  
Lowell = SW 87.22