

1525



NATIONAL GEOGRAPHIC

NOTEBOOK

MICROF

DEC 24 1964

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*ENGINEERING and DRAFTING SUPPLIES*  
IRVING PARK STATION  
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ENGINEERING DEPARTMENT  
CITY OF SAN DIEGO,  
CALIFORNIA.

Xsec Rosecrans  
Cont'd from F.B. 1573

Indexed  
C.S.K.

765

1

T.P. 446 765 319 BK. 1523 p. 77

Nly Stearne +50

W	4.2	3.45
+14	5.0	2.65
cb	5.3	2.35
+7 par	4.9	2.74
1/4 "	4.95	2.70
+10 "	5.21	2.44
C	5.5	2.15
+3	6.3	1.35
rail	5.70	2.35
+8	5.3	2.35
+14	6.4	1.25
1/4	5.4	2.25
cb	6.7	0.95
E	7.2	0.45
+100		
E	7.4	0.25
cb	6.7	0.95
+10	6.6	1.05
1/4	5.7	1.95
+3	6.0	1.65
+9	5.2	2.45
rail	5.05	2.60

414	6.1	1.55
C	5.1	2.55
+7 par	4.97	2.68
1/4 "	4.70	2.95
+10 "	4.62	3.03
cb	4.9	2.75
+2	4.5	3.15
W	3.8	3.85
+150		
W	3.8	3.85
+14	4.0	3.65
cb	4.5	3.15
+7 par.	4.27	3.38
1/4 "	4.25	3.30
+10 "	4.00	3.05
C	4.7	2.95
+3	5.6	2.05
rail	4.00	3.05
+8	4.7	2.95
+14	5.6	2.05
1/4	4.9	2.75
+7	6.3	1.35
cb	6.9	0.75
E	7.4	0.25
2+00 Sly Tenneyson		
E	7.0	0.65

rb	6.8	0.85
+6	1.4	1.25
1/4	5.1	2.55
+9	4.1	3.55
rail	4.13	3.52
+14	5.1	2.55
C	4.0	3.65
+7 pay	4.00	3.65
1/4 "	3.92	3.73
+10 "	4.01	3.64
cb	3.9	3.75
+3	3.7	3.95
W	3.3	4.35
W 1/4 cb		
W	2.7	4.95
cb	3.6	4.05
+7 pay.	3.84	3.81
1/4 "	3.74	3.91
+10 "	3.87	3.78
C	3.9	3.75
+3	5.0	2.65
rail	3.97	3.68
+9	4.0	3.65
1/4	4.9	2.75
+7	5.8	1.85
cb	6.5	1.15

E	7.0	0.65
E TOHAYJOK		
E	6.2	1.45
cb	5.9	1.75
+10	4.9	2.75
1/4	4.7	2.95
+9	3.9	3.75
rail	3.74	3.89
+14	4.7	2.95
C	4.4	4.25
+7 pay	3.71	3.94
1/4 "	3.62	4.03
+10 "	3.68	3.97
cb	3.4	4.25
+11	3.5	4.15
W	2.3	5.35
W 1/4 cb		
W	2.6	5.05
+4	3.6	4.05
cb	3.5	4.15
+7 pay	3.55	4.10
1/4 "	3.48	4.17
+10 "	3.58	4.07
C	3.4	4.25
+3	4.4	3.25
rail	3.50	4.15

765

+9	3.6	4.05
1/4	4.6	3.05
+8	4.7	2.95
CB	6.0	1.65
E	6.3	1.35

N/Temp/Corr = 00

E	6.2	1.35
CB	6.1	1.55
+5	5.5	2.15
1/4	4.3	3.35
+9	3.3	4.35
rail	3.8	4.47
+14	4.2	3.45
C	3.2	4.45
+7 pav	3.3	4.31
1/4 "	3.3	4.35
+10 "	3.4	4.25
CB	3.4	4.25
+3	3.1	4.55
+12	4.4	4.25
W	2.1	5.55

0 + 50

W	0.8	6.85
+3	1.8	5.85
+14	1.7	5.95
CB	2.5	5.15

765

3

+7 pav	2.4	5.24
1/4 "	2.3	5.32
+10 "	2.4	5.22
C	2.4	5.25
+3	3.2	4.45
rail	2.11	5.54
+8	2.2	5.45
+14	3.2	4.45
1/4	2.6	5.05
+7	3.7	3.95
CB	4.1	3.55
E	4.3	3.35

T.P. 11.40 1708<sup>v</sup> 197 568

1700

E	12.2	4.88
CB	12.4	4.88
+9	11.8	5.28
1/4	11.1	5.98
+9	10.4	6.68
rail	10.25	6.83
+14	11.3	5.78
C	10.6	6.48
+7 pav	10.25	6.73
1/4 "	10.14	6.94
+10 "	10.22	6.86
CB	10.4	6.68

1708

K <sup>2</sup>	9.6	7.48
W	8.6	8.48
	1+50	
W	7.1	9.98
+14	8.1	8.98
cb	8.6	8.48
+7 bar	8.65	8.43
1/4 "	8.5	8.56
+10 "	8.63	8.45
C	9.2	7.88
+3	9.9	7.18
rail	8.85	8.23
+8	9.0	8.08
1/4	9.5	7.58
cb	10.3	6.78
E	10.3	6.78
	2+00 Sly VDal	
F	8.8	8.28
cb	9.2	7.88
+9	8.8	8.28
1/4	8.1	8.98
+9	7.4	9.68
rail	7.40	9.68
+14	8.4	8.68
C	7.4	9.68
+7 bar	6.91	10.17

1708

4

1/4 bar	6.84	10.24
+10 "	6.95	10.10
cb	7.0	10.08
+2	5.8	11.28
W	4.9	12.18
	Sly cb	
W	4.1	12.98
+13	5.4	11.68
cb	6.4	10.68
+7 bar	6.36	10.72
1/4 "	6.18	10.90
+10 "	6.21	10.87
C	6.3	10.78
+3	7.9	9.18
rail	6.90	10.18
+8	7.0	10.08
1/4	7.4	9.68
cb	8.5	8.58
E	8.7	8.38
	E VDal	
F	7.8	9.28
cb	8.2	8.88
+12	7.2	9.88
1/4	7.0	10.08
+9	6.5	10.58
rail	6.42	10.66

17.08

+14	7.5	9.58
C	5.8	11.28
+7 pav	5.58	11.50
1/4 "	5.59	11.49
+10 "	5.78	11.30
cb sly drive	6.09	10.99
w	4.32	12.76
N/y cb		
w - 16 top com cb	6.09	16.99
w	3.6	13.48
cb	5.7	11.38
+7 pav	5.43	11.65
1/4 "	5.22	11.86
+10 "	5.24	11.84
A	5.5	11.58
+3	6.9	10.18
rail	5.95	11.13
+8	6.0	11.08
1/4	6.8	10.28
cb	7.7	9.38
E	7.6	9.48
N/y vdat = 00		
E	6.6	10.48
cb	7.1	9.98
1/4	6.6	10.48
+9	5.6	11.48

17.08

5

rail	5.25	11.53
+14	6.25	10.58
C	4.9	12.18
+7 pav	4.87	12.21
1/4 "	4.86	12.22
+10 "	5.08	12.00
cb	4.9	12.18
+8.5 gut dirt	2.2	13.88
" top cb	2.60	14.48
w sdu	2.25	14.83
0+25		
w cb top PC. return	3.23	13.85
0+50		
w	0.9	16.18
+3	2.1	14.98
cb top com	2.92	14.16
gut dirt	4.5	12.58
+7 pav	4.46	12.62
1/4 "	4.24	12.82
+10 "	4.27	12.81
C	4.4	12.68
+3	5.9	11.18
rail	5.00	12.08
+8	5.0	12.08
1/4	5.1	11.98
cb	6.1	10.98
E	5.2	11.88



8+7

W/CP +7 pav	4.02	13.06
1/4 "	3.93	13.15
+10 "	4.05	13.03
/700		
E	4.7	12.38
cb	5.5	11.58
+10	5.0	12.08
1/4	4.0	13.08
+3	5.6	11.48
+9	4.8	12.28
rail	4.73	12.35
+14	5.7	11.38
C	3.8	13.28
+7 pav	3.85	13.23
1/4 "	3.75	13.33
+10 "	3.93	13.25
cb	4.0	13.08
+3	2.0	15.08
W	0.6	16.48
/150		
W	0.4	16.68
+3	1.8	15.28
+13	1.4	15.68
cb	4.3	12.78
+7 pav	4.19	12.89
1/4 "	4.04	13.04

+10 pav	4.06	13.02
C	2.7	13.38
+3	5.5	11.58
rail	4.53	12.55
+8	4.7	12.38
+14	5.6	11.48
1/4	2.4	14.48
+8	5.2	11.88
cb	5.3	11.78
E	4.7	12.38
2700 = Sly Voltare		
E	5.5	11.58
cb	5.6	11.48
+8	5.4	11.68
1/4	2.9	14.18
+3	5.8	11.28
+9	4.7	12.38
rail	4.72	12.36
+14	5.6	11.48
C	4.1	12.98
+7 pav	4.37	12.71
1/4 "	4.23	12.75
+10 "	4.40	12.68
cb	4.6	12.48
+3	2.3	14.78
+11	1.3	15.78
W	0.0	17.08

1708

T.P	5.43	17.87	4.64	12.44
	5/4. ob.			
w		1.4		16.47
+13		2.3		15.57
cb		5.25		12.37
+7 pav		5.31		12.56
1/4 "		5.19		12.68
+10 "		5.25		12.62
c		5.3		12.57
+3		6.5		11.37
rail		5.62		12.25
+8		5.6		12.27
+14		6.6		11.27
1/4		3.6		14.27
+8		6.1		11.77
cb		6.7		11.17
E		6.8		11.07
	E Voltare			
E		7.2		10.67
cb		7.1		10.77
+9		6.5		11.37
1/4		3.7		14.17
+3		6.7		11.17
+9		5.7		12.17
rail		5.71		12.16
+14		6.7		11.17

1787

7

c		5.1		12.77
+7 pav		5.40		12.47
1/4 "		5.3		12.54
+10 "		5.41		12.46
cb		5.5		12.37
+3		3.0		14.87
w		0.8		17.07
	N/y ob			
w		1.8		16.07
+13		4.3		13.57
cb		5.5		12.37
+7 pav		5.57		12.30
1/4 "		5.45		12.42
+10 "		5.56		12.31
c		5.3		12.57
+3		6.9		10.97
rail		5.82		12.04
+8		5.9		11.97
+14		6.8		11.07
1/4		3.6		14.27
+8		6.3		11.57
cb		7.5		10.37
E		7.7		10.17
	N/y Voltare = 0.0			
E		7.3		10.57
cb		7.4		10.67

1787

+v	6.9	10.97
1/4	4.2	13.67
+w	7.0	10.87
+9	6.0	11.87
rail	5.94	11.93
+14	7.0	10.87
C	5.3	12.57
+7 pay	5.67	12.20
1/4 "	5.53	12.34
+10 "	5.56	12.31
cb	5.8	12.07
+2	4.2	13.67
w	3.2	14.67

0+50

w	3.5	14.37
+14	4.4	13.47
cb	5.9	11.97
+7 pay	5.91	11.96
1/4 "	5.84	12.03
+10 "	5.92	11.95
C	5.8	12.07
+3	7.3	10.57
rail	6.27	11.60
+8	6.3	11.57
+14	7.3	10.57
1/4	5.8	14.07

1787

8

+8	6.2	11.67
cb	6.7	11.17
E	7.4	10.47
	1+00	
E	7.5	10.37
cb	6.8	11.07
+9	6.2	11.67
1/4	4.5	14.37
+3	7.4	10.47
+9	6.5	11.37
rail	6.48	11.44
+14	7.3	10.57
C	5.8	12.07
+7 pay	6.01	11.86
1/4 "	6.03	11.84
+10 "	6.17	11.70
cb	5.8	12.07
+2	5.0	12.87
w	4.5	13.37
	1+50	
w	4.6	13.27
+14	5.1	12.77
cb	6.6	11.27
+7 pay	6.33	11.54
1/4 "	6.21	11.66
+10 "	6.22	11.65

1787-

C	6.1	11.77
+3	2.4	10.47
rail	6.59	11.28
+8	6.7	11.17
+14	7.5	10.37
1/4	4.5	13.37
+8	6.4	11.47
CB	7.1	10.77
E	8.7	9.17
1+7N		
W CB	5.5N	12.35
gut pav	6.30	11.57
1+79N		
W CB +7 pav	6.5N	11.32
W 1/4 "	6.57	11.50
+10 "	6.27	11.50
1+94		
C +7 pav	6.7N	11.15
W 1/4 "	6.67	11.20
+10 "	6.56	11.31
↓ +00 Sly Whirner		
E	9.9	7.97
+6	8.1	9.77
CB	7.2	10.67
1/4	5.7	12.17
+3	7.8	10.07

1787

9

+9	6.6	11.27		
rail	6.56	11.31		
+14	7.7	10.17		
C	6.1	11.77		
+7 pav	6.66	11.21		
1/4 "	6.61	11.26		
+10 "	6.50	11.37		
CB "	6.26	11.51		
+7 <sup>N</sup> gut "	5.86	12.01		
+7 <sup>S</sup> Top CB	5.26	12.61		
W	4.5	13.37		
T.P. 43N	16.57	5.68	12.19	
NW.B.P. 106	5.79	18.57	3.73	12.78
SL + 04				
C + 11		7.9		10.67
E 1/4		9.4		9.17
+4		6.5		12.07
+12		7.5		11.07
CB		10.2		8.17
E		10.5		8.07
+15		14.2		4.37
SL + 10				
- 15		10.5		8.07
E bot. ditch		14.9		3.67
CB		13.5		5.07
1/4		12.7		5.87

 BM #6  
 NW 1/4 Sec  
 Rosocraux

1/4 +2	7.9	10.67
+9	7.4	11.17
rail	7.7	10.87
C	7.5	11.07
+7 pav	7.09	11.48
1/4 "	7.02	11.55
+10 "	7.1	11.46
cb "	6.91	11.66
W+1 " gut	5.77	12.80
" Tot of	5.20	13.37
Sly of whittier		
w pav	5.59	12.98
cb "	6.31	11.76
+7 pav	7.04	11.53
1/4 "	6.95	11.62
+10 "	6.99	11.58
C	7.7	10.87
rail	7.08	11.49
+8	7.3	11.27
+15	8.4	10.17
1/4	11.0	7.57
+4	12.5	6.07
cb	13.6	4.97
E	13.8	4.77
+5	10.5	8.07

Sly of +5		
E	10.2	8.37
+10	14.4	4.17
cb	14.1	4.47
1/4	12.7	5.87
+2.7 FL 36" outlet 1. pipe	11.12	7.45 PA Culy.
+3	8.0	10.57
+9	7.3	11.27
rail	7.03	11.54
+12.7	7.7	10.87
" FL. inlet 36" pipe	10.66	7.91
C	7.5	11.07
E whittier		
w pav	5.44	13.13
cb "	6.77	11.80
+7 "	6.75	11.82
1/4 "	6.64	11.93
+10 "	6.68	11.89
C	6.6	11.97
+3	7.8	10.77
rail	6.93	11.64
+8	7.1	11.47
+12	8.2	10.37
1/4	11.5	7.07
+6	7.5	10.77
+14	8.2	10.37

cb	13.2	5.37
+11	13.5	5.07
E	8.6	9.97
♀ +5		
F	7.5	11.07
+5	6.8	11.77
+7	12.0	6.57
cb	13.2	5.37
+3	9.0	9.57
1/4	7.3	11.27
+3	8.1	10.47
+9	7.0	11.57
rail	6.88	11.69
+14	7.8	10.77
C	6.9	11.67
N/y cb. W/Whittier		
E	8.9	9.67
+10	7.2	11.37
cb	10.4	8.17
+8	7.3	11.27
1/4	7.0	11.57
+3	7.7	10.87
+9	6.9	11.67
W rail	6.74	11.83
+14	7.7	10.87
C	6.4	12.17

+7 pav	6.48	12.09
1/4 "	6.41	12.16
+10 "	6.52	12.05
cb "	6.72	11.85
W "	5.51	13.06
N/L Whittier = 00		
W	5.30	13.27
+8 top cb	5.70	12.87
" gut	6.28	12.29
cb pav.	6.52	12.05
+7 pav	6.27	12.30
1/4 "	6.19	12.38
+10 "	6.26	12.31
C	6.3	12.27
+13	7.2	11.17
rail	6.40	12.17
+8	6.6	11.97
+14	7.2	11.27
1/4	6.0	12.57
+8	6.8	11.77
+14	9.2	9.27
cb	9.4	9.17
+4	6.9	11.67
E	8.7	9.87
+5	9.0	9.57

0+45.7 18.57

C + T pav	5.60	12.97
W 1/2 "	5.54	13.03
+10 "	5.65	12.92
+14 "	5.84	12.73
+N.V.	6.00	12.57
W CUT	6.03	12.54
W cb	5.16	13.41

0+50

-5	8.0	10.57
E	7.7	10.87
+12	6.2	12.37
cb	7.6	10.97
+2	8.4	10.17
+10	6.0	12.57
1/4	5.5	13.07
+3	6.6	11.97
+9	5.6	12.97
rail	5.57	13.00
+14	6.9	11.67
C	5.9	12.67
+7 pav	5.56	13.01
1/4 "	5.49	13.08
+10 "	5.79	12.78
+14 "	5.96	12.61
+15.5	5.96	12.61
CUT	5.95	12.62
cb	5.05	13.52

1+00 18.57

W cb top	5.59	14.98
cut	4.62	13.95
+1.5	4.67	13.90
+3	4.35	14.22
1/4 pav	4.11	14.46
+10 "	4.23	14.34
C	4.3	14.27
+3	5.3	13.27
rail	4.21	14.36
+8	4.3	14.27
+14	5.2	13.37
1/4	4.0	14.57
+8	4.6	13.97
cb	8.3	10.27
+6	5.2	13.37
E	6.2	12.37

1+50

E	4.1	14.47
+10	4.4	14.17
cb	6.4	12.17
+4	6.4	12.17
+10	3.6	14.97
1/4	3.1	15.47
+3	3.9	14.67
+9	3.0	15.57
W rail	2.86	15.71

18.57

HI in this  
column for  
E. rail only

18.57

13

+14	4.3	14.27
C	2.7	15.87
+7 pav	2.80	15.77
1/4 "	2.70	15.87
+14	3.00	15.57
+15.5	3.30	15.27
gut	3.7	14.87
w cb Top	2.06	16.51
+93		
w cb r	0.67	17.90
gut	1.79	16.78
+15	1.98	16.59
+3	1.63	16.94
1/4	1.47	17.10
2 too S/y Xenophon		
w Top cb	0.42	18.15
gut	1.56	17.01
+3	1.80	16.77
+7 pav	1.29	17.28
1/4 "	1.25	17.32
+10 "	1.35	17.02
C	1.0	17.57
+3	2.5	16.07
w rail	1.49	17.08
+8	1.6	16.97
+14	2.6	15.97

1/4	2.0	16.57
+7	2.7	15.87
+10	4.2	14.37
cb	5.0	13.57
+3	1.7	16.87
E	3.1	15.47
T.P	9.50	27.66
S/y cb	0.41	18.16
E	12.1	15.56
+11	10.7	16.96
+12	12.9	14.76
cb	13.0	14.66
+10	10.2	17.46
1/4	10.3	17.36
+3	11.0	16.66
+9	10.2	17.46
rail	10.10	17.56
+14	11.0	16.66
C	9.9	17.76
+7 pav	9.97	17.69
1/4 "	9.87	17.79
+10 "	9.87	17.79
cb	9.78	17.88
w gut	8.82	18.84
" Top cb PC	8.70	18.96

BM #7

S.W.S.P. 66  
Xenophon  
Reservoirs



♀ Xenophon

27.66

27.66

27.78 <sup>14</sup> x

w pav	8.06	19.60
cb "	9.36	18.30
+7 "	9.47	18.19
1/4 "	9.41	18.25
+10 "	9.41	18.15
C	9.6	18.06
+3	10.6	17.06
w rail	9.7	17.95
+8	9.7	17.96
+14	10.9	16.76
1/4	10.2	17.46
cb	11.1	16.56
+6	12.4	15.26
+8	10.6	17.06
E	10.3	17.36
N/y cb		
E cb Top	9.34	18.32
" gut	10.34	17.32
+4 edge cem gut	10.16	17.50
1/4	10.1	17.56
+3	10.5	17.16
+9	9.4	18.26
rail	9.31	18.35
+14	10.2	17.46
C	9.2	18.46
+7 pav	9.0	18.66

18.16  
9.62  
17.78

E rail  
9.41  
17.37

1/4 pav	8.94	18.72
+10 "	9.04	18.62
cb	8.96	18.70
w gut	7.81	19.85
" Top cb PC	7.27	20.39
N/y Xenophon = 00		
w S/y edge Lavin	5.4	22.26
+10	7.9	19.76
cb Top cem	8.04	19.62
gut	8.63	19.03
+7 pav	8.53	19.13
1/4 "	8.41	19.25
+10 "	8.48	19.18
C	8.9	18.76
+3	9.9	17.76
rail	8.94	18.72
+8	9.0	18.66
+14	10.1	17.56
1/4	9.2	18.46
+13 edge gut	9.79	17.87
gut	9.97	17.69
E cb	8.95	18.71
O+50		
E cb	7.96	19.70
gut	8.97	18.69
+4 edge gut	8.81	18.85

9.04  
18.79

27.66

27.78

27.66

15  
27.78

1/4	8.2	19.46
+3	8.9	18.76
+9	7.9	19.76
rail	7.90	19.76
+14	9.3	18.36
C	7.8	19.86
+7 bay	7.52	20.14
1/4 "	7.42	20.23
+10 "	7.52	20.14
cb	7.6	20.06
+3	6.9	20.76
+8	6.4	21.26
W lawn	4.0	23.66
+100		
W	3.7	23.96
+8	5.3	22.36
+13	5.8	21.86
cb	6.5	21.16
+7 bay	6.56	21.10
1/4 "	6.42	21.24
+10 "	6.42	21.21
C	6.5	21.16
+3	7.9	19.76
rail	6.98	20.68
+8	7.0	20.66
+14	8.3	19.36

8.01  
19.777.06  
20.72

1/4	7.5	20.16
+13 edge gut	7.83	19.83
gut	7.94	19.70
E cb	6.96	20.70
+150		
E cb	5.86	21.80
gut	6.88	20.78
+4	6.72	20.94
1/4	6.1	21.56
+3	7.2	20.46
+9	6.0	21.66
rail	6.02	21.64
+14	7.4	20.26
C	5.6	22.06
+7 bay	5.51	22.15
1/4 "	5.44	22.22
+10 "	5.55	22.11
cb	5.6	22.06
+3	4.8	22.86
W	4.2	23.46
+100 Sly Jange		
W	3.3	24.36
cb	4.7	22.96
+7 bay	4.58	23.08
1/4 "	4.46	23.20
+10 "	4.56	23.10

C=8  
21.70

27.66

27.78

S.L. + 13.5 =  
Culvert

27.66

716  
2778

C	4.8	22.86
+3	6.5	21.16
rail	5.06	22.60
+8	5.2	22.46
+14	6.1	21.56
1/4	5.4	22.26
+13	5.05	21.81
gut	5.98	21.68
E cb	4.98	22.68
5/4 cb Yonge		
E cb	4.83	22.83
gut	5.84	21.84
+4 edge gut	5.65	22.01
1/4	5.3	22.36
+3	5.9	21.76
+9	5.0	22.66
rail	4.90	22.76
+14	5.9	21.76
C	4.4	23.26
+7 pav	4.36	23.30
1/4 "	4.33	23.33
+10 "	4.48	23.18
cb	4.4	23.26
W	2.0	25.06

517  
22.61

W Top conc Lip	5.54	24.12
+34 FL pipe	5.04	22.62
5/4 Yonge		
W	5.7	24.96
+13	3.4	24.26
cb	4.7	22.96
+7 pav	4.34	23.32
1/4 "	4.20	23.46
+10 "	4.23	23.43
C	4.3	23.36
+3	5.7	21.96
W rail	4.73	22.93
+8	4.9	22.76
+14	5.7	21.96
1/4	4.9	22.76
+13 edge gut	5.56	22.10
gut	5.66	22.00
E cb Top	4.65	23.01
5/4 cb		
E cb	4.51	23.15
gut	5.51	22.15
+4	5.42	22.24
1/4	4.8	22.86
+3	5.6	22.06
+9	4.6	23.06
rail	4.59	23.07

4.83  
22.95

	27.66		27.78
+14	5.6	22.06	
C	4.0	23.66	
+7 pav	4.18	23.48	
1/4 "	4.3	23.53	
+10 "	4.29	23.37	
cb	4.6	23.06	
+3	3.0	24.66	
W	1.8	25.86	
W/y Young = 00			
W	2.2	25.46	
+13	2.1	24.56	
cb	4.2	23.26	
+7 pav	4.19	23.47	
1/4 "	4.05	23.61	
+10 "	4.11	23.55	
C	4.1	23.56	
+3	5.4	22.26	
rail	4.45	23.21	4.48
+8	4.6	23.06	23.30
+14	5.5	22.16	
1/4	4.6	23.06	
+13 edge gut	5.28	22.38	
gut	5.38	22.28	
E cb top	4.39	23.27	

	0 + 50	27.66	27.78
E cb	4.04	23.62	
gut	5.02	22.64	
+4	4.82	22.84	
1/4	4.2	23.46	
+3	4.9	22.76	
+9	4.1	23.56	
rail	4.00	23.66	4.07
+14	5.1	22.56	23.71
C	3.5	24.16	
+7 pav	3.66	24.00	
1/4 "	3.59	24.07	
+10 "	3.70	23.96	
cb	3.9	23.76	
+2	3.0	24.66	
W	1.6	26.06	
W 1+00			
W	2.3	25.36	
cb corr top	2.40	25.26	
gut dirt	2.2	24.26	
+7 pav	3.27	24.39	
1/4 "	3.16	24.50	
+10 "	3.22	24.44	
C	3.2	24.46	
+3	4.8	22.86	
rail	3.59	24.07	3.47
+8	3.7	23.96	24.11
+14	4.5	23.16	

27.66

2778

1/4	3.5	24.16
+13 edge gut	4.43	23.23
gut	4.54	23.12
E cb	3.54	24.12
1750		
E cb	3.20	24.46
gut	4.17	23.49
+4	3.94	23.72
1/4	3.2	24.26
+3	4.1	23.56
+9	3.2	24.46
rail	3.11	24.55
+14	4.2	23.46
C	2.7	24.96
+7 pav	2.75	24.91
1/4 "	2.70	24.96
+10 "	2.78	24.88
gut dirt	2.1	24.56
W Top cb	1.98	25.68
W	1.8	25.86
2+.00 = Sly Zola		
W	1.2	26.46
+8 cb	1.43	26.23
gut pav	2.13	25.53
cb "	2.26	25.40
+7 "	2.34	25.32

3.18  
24.60

27.66

\*  
27.78<sup>18</sup>

1/4 pav	2.25	25.41
+10 "	2.28	25.38
C	2.2	25.46
+3	3.5	24.16
rail	2.57	25.09
+8	2.7	24.96
+14	2.6	24.06
1/4	2.8	24.86
+13 edge gut	3.59	24.07
gut	3.75	23.91
E cb	2.79	24.87
T.P. 7.97 33.36	2.27	25.39
Sly cb Zola		
E Top cb	8.43	24.93
gut	9.40	23.96
+4 edge gut	9.25	24.11
1/4	8.3	25.06
+3	9.1	24.26
+9	8.1	25.26
rail	8.16	25.20
+14	9.1	24.26
C	8.2	25.16
+7 pav	7.95	25.41
1/4 "	7.91	25.45
+10 "	8.02	25.34
cb "	7.91	25.45

2.65  
25.01

3336

2778 \*

w	6.9v	26.44	
E Zola			
w pav.	66v	26.72	
cb	77x	25.62	
+7	801	25.35	
1/4	79v	25.44	
+10	798	25.38	
C	7.7	25.66	
+3	89	24.46	
w rail	798	25.38	2.44
+8	8.1	25.26	25.34
+14	9.0	24.36	
1/4	8v	25.16	
+13 edge gut	9.25	24.11	
gut	9.07	23.99	
E cb	8.39	24.97	
Nly curb Zola			
E cb	8.33	25.03	
gut	9.32	24.04	
+4	9.25	24.11	
1/4	7.8	25.56	
+3	8.8	24.56	
+9	7.9	25.46	
rail	7.90	25.46	
+14	8.7	24.66	
C	8.1	25.26	

23,36

19

27.78 \*

C + 7	pav	8.00	25.36	
1/4	"	7.95	25.41	
+10	"	8.05	25.28	
cb	"	7.94	25.42	
w		7.08	26.28	
	Nly Zola=00			
w		7.1	26.26	
+8	Top	7.49	25.87	
"	gut grade	8.31	25.05	cb inlet
"	FL inlet Box	10.65	22.68	
cb		8.7	25.19	
+7	pav	8.03	25.33	
1/4	"	7.94	25.42	
+10	"	7.98	25.38	
C		7.6	25.76	
+3		8.5	24.86	
	rail	7.74	25.62	2.16
+8		7.8	25.56	25.62
+14		8.6	24.76	
1/4		7.8	25.56	
+13		9.14	24.24	T.P. 2.56
	gut	9.56	23.80	25.22
E cb		8.22	25.14	9.82
	O+50			35.04
E cb		7.64	25.72	
gut		8.64	24.72	
+4	gut edge	8.50	24.86	

2336

T  
95.04

1/4	7.1	26.26	
+2	8.2	25.16	
+9	7.4	25.96	
rail	7.38	25.96	9.04
+1X	8.0	25.36	26.00
C	7.1	26.26	
+7 pay	7.23	26.13	
1/4 "	7.16	26.20	
+10 "	7.32	26.04	
gut pad	7.6	26.20	
cb top cork	6.49	26.87	
1+00			
W of Top	5.62	27.74	
gut pad	6.25	27.11	
+7 "	6.54	26.82	
1/4 "	6.42	26.94	
+10 "	6.48	26.88	
C	6.4	26.96	
+3	7.5	25.86	
rail	6.79	26.57	8.44
+9	6.9	26.46	26.60
+14	7.7	25.66	
1/4	6.9	26.46	
+13 edge gut	7.72	25.64	
gut	7.81	25.55	
E cb	6.82	26.54	

1+50

33.36

T  
33.36

E cb	6.05	27.31	
gut	7.03	26.03	
+4 edge gut	6.86	26.50	
1/4	6.2	27.16	
+3	6.9	26.46	
+9	5.9	27.46	
rail	5.89	27.47	7.58
+14	6.6	26.76	27.46
C	5.4	27.96	
+7 pay	5.70	27.66	
1/4 "	5.62	27.74	
+10 "	5.75	27.61	
gut "	5.42	27.94	
x1 Top cb	4.79	28.57	
2+00 S/y Alcor			
W	2.8	30.56	
+8 Top cb	3.92	30.04	
" gut	3.98	29.38	
cb pad	4.48	28.88	
+7 "	4.91	28.45	
1/4 "	4.78	28.58	
+10 "	4.81	28.55	
C	4.7	28.66	
+3	6.0	27.36	
rail	4.88	28.48	6.58
+8	4.8	28.56	28.46

3336

π  
35.04

C + 14	6.4	27.16
1/4	5.3	28.06
+ 13	5.97	27.39
gut	6.10	27.26
E cb	5.10	28.26
S/y cb H/corr		
E cb	4.67	28.69
gut	5.69	27.67
+ 4	5.56	27.80
1/4	4.6	28.76
+ 3	5.5	27.86
+ 9	4.6	28.76
rail	4.54	28.82
+ 14	5.6	27.76
C	4.0	29.36
+ 7 pav.	4.45	28.91
1/4 "	4.33	29.03
+ 10 "	4.45	28.88
cb "	4.05	29.28
W "	3.00	30.36
E Meott		
W pav.	2.49	30.87
cb "	3.69	29.67
+ 7 "	3.97	29.39
1/4 "	3.91	29.45
+ 10 "	3.97	29.39

3336

21  
35.04

C	3.9	29.46
+ 3	5.3	28.06
rail	4.6	29.20
+ 8	4.1	29.26
+ 14	5.4	28.16
1/4	4.5	28.86
+ 13	5.15	28.18
gut	5.34	28.02
E cb	4.53	29.03
1/4 cb		
E cb	3.99	29.37
gut	4.97	28.39
+ 4	4.52	28.54
1/4	3.7	29.66
+ 3	4.9	28.46
+ 9	3.8	29.56
rail	3.80	29.56
+ 14	5.1	28.26
C	3.4	29.96
+ 7 pav.	3.50	29.86
1/4 "	3.45	29.91
+ 10 "	3.54	29.82
cb "	3.29	30.07
W "	2.11	31.25
W 1/4 Meott + 00		
W	1.6	31.76

5.86  
29.18~~5.4~~  
~~29.92~~



3336

350x

W+8 Top cb	1.91	31.45
" gut pav	2.49	30.87
cb "	2.93	30.43
+7 "	3.09	30.27
1/4 "	2.99	30.37
+10 "	3.0v	30.34
c	3.1	30.26
+3	4.6	28.76
rail	3.41	29.95
+8	3.4	29.96
+1x	4.5	28.86
1/4	3.7	29.66
+13 edge gut	4.4v	28.94
gut	4.46	28.80
E cb	3.58	29.78
	0x50	
E cb	2.5v	30.84
gut	3.51	29.85
+4	3.29	30.07
1/4	2.8	30.56
+3	3.4	29.96
+9	2.2	31.16
rail	2.17	31.19
+14	3.2	30.06
c	1.5	31.86
+7 pav	2.09	31.27

$$\frac{51}{2992}$$

$$\frac{4.05}{30.99}$$

3336

350x<sup>22</sup>

1/4 pav	1.97	31.39
+10 "	2.06	31.30
cb gut	2.07	31.29
XI cb Top	1.86	32.00
	1400	
XI cb	0.33	33.03
gut pav	0.9v	32.44
+7 "	1.09	32.27
1/4 "	0.90	32.46
+10 "	0.95	32.41
c	1.2	32.16
+3	2.4	30.96
rail	1.18	32.18
+8	1.2	32.16
+14	2.3	31.06
1/4	1.2	32.16
T.P	11.4v 4330	1.48 31.88
+13	1.248	31.02
gut	1.242	30.88
E cb	11.44	31.86
	1450	
E cb	10.43	32.87
gut	11.41	31.89
+4	11.25	32.05
1/4	10.7	32.60
+3	11.1	32.20

$$\frac{293}{32.11}$$

4/330

95.04

+9		10.1	33.20	
rail		9.98	33.32	1.79
+14		11.3	32.00	33.25
C		9.8	33.50	
+7 pav		9.80	33.50	
1/4 "		9.81	33.49	
+10 "		9.97	33.33	
gut "		10.06	33.24	
W cb		9.30	34.00	
2 too Shy Browning				
W		7.0	36.30	
+8	Top cb	7.56	35.74	
"	gut	8.14	35.16	
cb	pav	8.83	34.47	
+7	"	8.90	34.40	
1/4	"	8.76	34.54	
+10	"	8.80	34.50	
C		8.6	34.70	
+3		10.0	33.30	
rail		8.8w	34.48	0.59
+8		9.1	34.20	34.45
+14		10.0	33.30	
1/4		9.5	33.80	T.P. 0.86
+13		10.17	33.13	34.18
gut		10.39	32.91	12.15
E cb		9.39	33.91	46.33

Shy cb

4/330

23  
46.33

E cb		8.93	34.37	
gut		9.90	33.40	
+4		9.73	33.57	
1/4		9.0	34.30	
+3		9.5	33.80	
+9		8.4	34.90	
rail		8.41	34.89	
+14		9.6	33.70	
C		8.2	35.10	
+7 pav		8.41	34.89	
1/4 "		8.51	34.99	
+10 "		8.44	34.86	
cb "		8.28	35.02	
W "		6.88	36.42	
♀ Browning				
W pav		6.34	36.96	
cb "		7.85	35.45	
+7 "		7.98	35.32	
1/4 "		7.82	35.48	
+10 "		7.88	35.42	
C		7.9	35.40	
+3		9.5	33.80	
rail		8.05	35.25	11.01
+8		8.0	35.30	35.32
+9		9.0	34.30	
1/4		8.7	34.60	

4330

46.83

1/4 + 1/2	9.28	34.02
qut	9.42	33.87
E cb	8.45	34.85
N/y cb Browning		
E cb	7.93	35.37
qut	8.91	34.39
+4	8.26	34.54
1/4	8.2	35.30
+3	8.6	34.70
+9	7.7	35.60
rail	7.13	35.77
+14	8.7	34.60
C	7.2	36.10
+7 pav	7.36	35.94
1/4 "	7.25	35.95
+10 "	7.03	35.77
cb "	7.45	35.85
A/ "	5.82	37.48
N/y Browning		
w	5.3	38.00
+8 top cb	5.69	37.61
" qut	6.57	36.73
cb pav	7.05	36.25
Set BM	5.81	37.49
+7 "	7.02	36.28
1/4 "	6.86	36.44

B.M. #8  
NW 3P CB  
Browning  
Resection

+10 pav	6.91	36.39
C	6.9	36.40
+3	8.2	35.10
rail	7.09	36.21
+8	7.2	36.10
+14	8.1	35.20
1/4	7.7	35.60
+13	8.28	35.02
qut	8.40	34.90
E cb	7.43	35.87
D + 50		
E cb	6.10	37.20
qut	7.11	36.20
+4	6.98	36.32
1/4	6.2	37.10
+3	6.9	36.40
+9	5.8	37.50
rail	5.88	37.42
+14	7.3	36.00
C	5.5	37.80
+7 pav	5.73	37.57
1/4 "	5.67	37.63
+10 "	5.79	37.51
cb	5.9	37.40
+3	4.8	38.50
w	3.6	39.70

46.83 <sup>24</sup>

10.16  
36.12

8.93  
37.40

4330

W	2.1	41.20	
+13	3.3	40.00	
cb	4.7	38.60	
+7 par	4.59	38.71	
1/4 "	4.45	38.85	
+10 "	4.50	38.80	
C	4.5	38.80	
+3	5.9	37.40	
rail	4.74	38.58	7.70
+8	4.7	38.60	38.57
+14	5.7	37.60	
1/4	4.8	38.50	
+13	5.73	37.57	
gut	5.85	37.48	
E cb	4.84	38.46	
/ +50			
E cb	3.52	39.78	
gut	4.51	38.79	
+4	4.39	38.91	
1/4	3.9	39.40	
+3	4.8	38.50	
+9	3.6	39.70	
rail	3.52	39.78	6.57
+14	4.7	38.60	39.76
C	3.3	40.00	
+7 par	3.25	40.08	

46.33

4330

1/4 par	3.17	40.13	
410 "	3.23	39.97	
cb	3.4	39.90	
+3	3.5	40.80	
W	0.7	42.60	
2+00 Sky Curve			
W	1.3	42.00	
+8 Top cb	1.30	41.98	
" gut	1.99	41.31	
cb par	2.03	41.27	
+7 "	2.05	41.25	
1/4 "	1.92	41.38	
+10 "	1.96	41.34	
C	1.9	41.40	
+3	2.6	39.70	
rail	2.25	40.95	5.38
+8	2.4	40.90	40.95
+14	2.4	39.90	
1/4	2.9	40.40	
+13	3.27	40.03	
gut	3.25	39.95	
E cb	2.36	40.94	
Sky cb			
E cb	2.00	41.30	
gut	3.02	40.28	
+4	2.90	40.40	

25  
46.33

4330

4033

4330

4033<sup>26</sup>

1/4	2.5	40.80
+2	2.1	40.10
+9	2.1	41.20
rail	2.00	41.30
+14	2.1	40.10
C	1.8	41.50
+7 pav	1.69	41.61
1/4 "	1.65	41.65
+10 "	1.77	41.53
cb "	1.75	41.55
w "	1.17	42.13
Curtis		
w pav	0.81	42.49
cb "	1.79	41.81
+7 "	1.75	41.75
1/4 "	1.42	41.88
+10	1.48	41.82
C	1.6	41.70
+2	2.8	40.50
rail	1.72	41.57
+8	1.8	41.50
+14	2.9	40.40
1/4	1.9	41.40
+12	2.70	40.60
gut	2.84	40.48
E cb	1.82	41.48

4.75  
41.58

N/y cb		
E cb	1.57	41.73
gut	2.75	40.75
+4	2.42	40.88
1/4	1.5	41.80
+2	2.5	40.80
+9	1.5	41.80
rail	1.38	41.92
+14	2.2	41.10
C	1.1	42.20
+7 pav	1.43	42.07
1/4 "	1.17	42.13
+10 "	1.28	42.02
cb "	1.33	41.97
w "	0.76	42.54
Curtis		
N/y	0.0	43.30
+8 Top cb	0.17	43.13
" gut	0.83	42.47
cb pav	1.11	42.19
+7 "	1.01	42.29
1/4 "	0.91	42.39
+10	0.96	42.34
C	0.9	42.40
+3	2.0	41.30
rail	1.08	42.22

4.15  
42.18

4330

44.33

50.97

27  
46.33

+8		1.1	42.20	
+14		2.2	41.10	
1/4		1.5	41.80	
+4		2.17	41.13	
gut		2.25	41.05	
F cb		1.28	42.02	
T.P	894	50.97	1.27	42.03
	0 +50			
F cb		8.01	42.96	
gut		8.98	41.99	
+4		8.84	42.13	
1/4		8.2	42.77	
+3		8.8	42.17	
+9		7.9	43.07	
rail		7.83	43.14	
+14		8.9	42.07	
C		7.6	43.37	
+7 pav		7.62	43.35	
1/4 "		7.57	43.40	
+10		7.67	43.30	
gut		7.60	43.37	
cb		6.93	44.04	
w/		6.3	44.67	
	+00			
w/		5.6	45.37	
cb		6.6	44.37	

+7 pav	6.45	44.42		
1/4 "	6.56	44.41		
+10 "	6.61	44.36		
C	6.5	44.47		
+3	8.0	42.97		
rail	6.92	44.05		
+8	6.9	44.07		
+14	8.0	42.97		
1/4	7.2	43.77		
+13	7.88	43.09		
gut	8.01	42.96		
F cb	7.05	43.92		
	1 +50			
F cb	6.00	44.97		
gut	6.98	43.99		
+4	6.83	44.14		
1/4	6.4	44.57		
+3	7.2	43.77		
+9	6.0	44.97		
rail	5.89	45.08		
+14	7.0	43.97		
C	5.6	45.37		
+7 pav	5.75	45.22		
1/4 "	5.71	45.26		
+10 "	5.85	45.12		
cb	5.8	45.17		
+3	5.2	45.77		

2.29  
44.04

1.34  
44.99

50.97

$\begin{array}{r} 46.33 \\ 1.34 \\ \hline 47.67 \\ 10.32 \\ \hline 57.99 \end{array}$

w	47	46.27
1+7 <sup>3</sup>		
w gut grate	5.67	45.30
FL Box	10.63	40.34
1+7 <sup>4</sup>		
w cb top P.C.	4.49	46.48
" gut	5.81	45.66
2+00 Sly Dumas		
w	4.0	46.97
+8 cb top	4.23	46.74
" gut grate	5.39	45.58
" FL Box	9.69	41.28
cb pat	5.07	45.90
+7 "	4.77	46.20
1/4 "	4.66	46.31
+10 "	4.70	46.27
c	4.6	46.37
+3	5.8	45.17
rail	4.92	46.05
+8	5.0	45.97
+14	6.0	44.97
1/4	5.0	45.97
+13	5.88	45.09
gut	6.07	44.90
E cb	5.06	45.91

50.97

54.99<sup>28</sup>

Sly cb

Ec	4.8	46.29
gut	5.70	45.27
+1	5.52	45.45
1/4	5.0	45.97
+3	5.6	45.37
+9	4.8	46.17
rail	4.57	46.40
+14	5.7	45.27
c	4.3	46.67
+7 pat	4.28	46.69
1/4 "	4.28	46.69
+10 "	4.48	46.49
cb "	4.61	46.36
w "	4.45	46.52
2 Dumas		
w pat	4.07	46.90
cb "	4.12	46.85
+7 "	4.13	46.84
1/4 "	4.00	46.97
+10 "	4.00	46.97
c	4.0	46.97
+3	5.3	45.67
rail	4.27	46.70
+8	4.3	46.67
+14	5.3	45.67
1/4	4.5	46.47

9.00

45.99

$\begin{array}{r} 831 \\ \hline 46.68 \end{array}$

50.97

54.99

50.97

29  
54.99

1/4 + 13	5.20	45.77
gut	5.32	45.65
F cb	4.34	46.63
N/y cb		
F cb	4.03	46.94
gut	4.99	45.98
+4	4.85	46.12
1/4	4.2	46.77
+3	4.9	46.07
+9	4.0	46.97
+ rail	3.96	47.01
+ 14	5.0	45.97
C	3.9	47.07
+ 7 pav	3.72	47.25
1/4 "	3.67	47.30
+ 10 "	3.50	47.17
cb "	3.93	47.04
N/	3.67	47.30
N/y Dumas-00		
N/	2.6	48.37
+ 8 Top cb	2.74	48.23
" gut	3.64	47.33
cb pav	3.59	47.38
+ 7 "	3.49	47.48
1/4 "	3.35	47.59
+ 10 "	3.42	47.55

C	3.5	47.47
+ 3	4.7	46.27
rail	3.67	47.30
+ 8	3.8	47.17
+ 14	4.7	46.27
1/4	3.9	47.07
+ 13	4.21	46.46
gut	4.61	46.36
F cb	3.63	47.34
0 + 50		
F cb	2.88	48.09
gut	3.87	47.10
+ 4	3.70	47.27
1/4	3.3	47.67
+ 3	4.1	46.87
+ 9	3.1	47.87
rail	2.99	47.98
+ 14	4.1	46.87
C	2.9	48.07
+ 7 pav	2.73	48.24
1/4 "	2.63	48.34
+ 10 "	2.72	48.25
cb " gut	3.11	47.86
N cb	2.12	48.85
1 + 00		
N cb	1.36	49.61
gut	2.35	48.62

7.74  
47.257.04  
47.93



50.97

54.99

+7 pav	2.01	48.96	
1/4 "	1.89	49.08	
+10 "	1.97	49.00	
C	1.9	49.07	
+3	3.3	47.67	
rail	2.31	48.62	6.41
+8	2.5	48.47	48.58
+14	5.4	47.57	
1/4	2.6	48.37	
+13	2.96	48.01	
qut	2.13	47.84	
E cb	2.15	48.82	
/ +50			
E cb	1.30	49.67	
qut	2.26	48.71	
+4	2.19	48.78	
1/4	1.8	49.17	
+3	—		
+9	1.7	49.27	
rail	1.62	49.35	5.69
+14	—		49.30
C	1.3	49.67	
+7 Pav	1.27	49.70	
1/4 "	1.19	49.78	
+10 "	1.28	49.69	
qut	1.58	49.39	
w cb	0.63	50.34	

54.99<sup>30</sup>

50.97			
T.P. 2.27	53.12	0.12	50.85
2 + 00 Sly Elliott			
w	1.8		51.32
+8 Top cb	1.98		51.14
" qut	2.90		50.22
cb pav	2.76		50.36
+7 "	2.78		50.34
1/4 "	2.71		50.41
+10 "	2.83		50.29
C	2.7		50.42
rail	3.06		50.06
1/4	3.1		50.02
+13	3.68		49.44
qut	3.86		49.26
E cb	2.89		50.23
Sly cb			
E cb	2.76		50.36
qut	3.72		49.40
+4	3.56		49.56
1/4	2.9		50.22
rail	3.02		50.10
C	2.7		50.42
+7 pav	2.66		50.46
1/4 "	2.56		50.56

5.03  
49.96

531V

52.99

+10 pav	2.65	50.47
cb "	2.60	50.52
w "	2.28	50.84
♀ Elliott		
w pav	2.15	50.97
cb "	2.52	50.59
+7 "	2.60	50.52
1/4 "	2.52	50.60
+10 "	2.58	50.54
C	2.6	50.52
rail	2.99	50.13
1/4	2.8	50.32
+13	3.50	49.62
gut	3.66	49.46
E cb	2.68	50.44
Nly of		
E dt	2.62	50.50
gut	2.61	49.51
+4	3.46	49.66
1/4	2.7	50.42
rail	3.00	50.12
C	2.9	50.22
+7 pav	2.65	50.47
1/4 "	2.58	50.54
+10 "	2.65	50.47
cb "	2.56	50.56
w "	2.30	50.82

4.92  
50.07

531V

52.99<sup>31</sup>

Nly Elliott		
w	1.8	51.32
+8 cb	1.95	51.17
" gut	2.83	50.29
cb pav	2.72	50.40
+7 pav	2.73	50.39
1/4 "	2.65	50.47
+10 "	2.70	50.42
C	2.9	50.22
rail	2.97	50.15
1/4	2.6	50.52
+13	3.52	49.60
gut	3.70	49.42
E cb	2.71	50.41
O+50		
E cb	2.93	50.19
gut	3.92	49.20
+4	3.76	49.36
1/4	3.2	49.92
+12 Eval switch	3.15	49.97
w rail main	3.17	49.95
C	3.1	50.02
+7 pav	2.89	50.23
1/4 "	2.84	50.28
+10 "	2.96	50.16
cb gut	3.30	49.82
" Top	2.32	50.80

4.89  
50.165.06  
49.93  
5.08 Eval  
49.91 Mark

1+00

53.12

54.99

2+00 Sly Freerail

53.12

54.99

W cb	2.56	50.56
gut	W. 45	49.57
+7 pav	3.21	49.91
1/4 "	3.13	49.99
+10 "	3.21	49.91
C	3.3	49.82
rail	3.48	49.64
1/x	3.6	49.52
+3.5 E rail switch	3.48	49.64
+13	4.09	49.03
gut	4.20	48.92
E cb	3.05	50.07

5.49  
49.50

3.88  
4.0

W	2.8	50.32
+8 Top	2.95	50.17
" gut	3.55	49.57
cb pav	3.73	49.39
+7 "	3.55	49.27
1/4 "	3.75	49.37
+10 "	3.83	49.29
C	3.5	49.62
rail	3.88	49.24
1/4	4.0	49.12
+3.5 E rail switch	3.98	49.14
+13	4.91	48.21
gut	5.10	48.02
E cb	4.11	49.01

5.75  
49.24

5.85  
49.14

1+50

E cb	3.59	49.53
gut	4.19	48.53
+4	4.40	48.72
+13.5 E rail switch	3.70	49.42
1/4	3.7	49.42
W rail	3.62	49.50
C	3.4	49.72
+7 pav	3.45	49.67
1/4 "	3.38	49.74
+10 "	3.47	49.65
gut	3.70	49.42
W cb	2.85	50.27

5.57  
49.42

5.52  
49.45

Sly cb		
E cb	4.29	48.83
gut	5.25	47.87
+4	5.08	48.04
+13.5 rail	4.10	49.02
1/4	4.2	48.92
W rail	4.03	49.09
C	3.9	49.22
+7 pav	3.98	49.14
1/4 "	3.89	49.23
+10 "	4.00	49.12
cb "	3.88	49.24
W "	3.33	49.79

Freeman

5312

54.99

W pav	388	49.74	
cb "	410	49.02	
+7 "	419	48.93	
1/4 "	406	49.06	
+10 "	411	49.01	
C	4.1	49.02	
rail	4.22	48.90	6.08
1/4	4.4	48.72	48.91
+13.5 E rail switch	433	48.79	6.20
+13	426	47.86	48.79
gut	5.42	47.70	
E cb	444	48.68	
N/y cb			
E cb	465	48.47	
gut	5.65	47.47	
+4	5.50	47.62	
+13.5 E rail switch	453	48.59	
1/4	4.6	48.52	
rail	4.36	48.76	
C	4.4	48.72	
+7 pav	428	48.84	
1/4 "	4.22	48.87	
+10 "	4.35	48.77	
cb "	430	48.82	
W	384	49.28	

N/y Freeman 00

5312

33  
54.99

W	3.7	49.42	
+8 Top cb	3.92	49.20	
" gut	4.51	48.61	
cb pav	4.45	48.67	
+7 "	4.53	48.59	
1/4 "	4.42	48.70	
+10 "	4.49	48.63	
C	4.6	48.52	
rail	4.54	48.58	6.39
1/4	4.8	48.32	48.60
+13.5 E rail switch	472	48.40	6.61
+13	5.67	47.45	48.38
gut	5.84	47.28	
E cb	4.85	48.27	
O 4.50			
E cb	5.38	47.74	
gut	6.38	46.74	
+4	6.24	46.88	
+13.8 E rail switch	5.13	47.99	7.04
1/4	5.2	47.92	47.95
W rail	4.92	48.17	6.88
C	5.0	48.12	48.11
+7 pav	5.05	48.07	
1/4 "	4.97	48.15	
+10 "	5.04	48.08	
gut	5.39	47.73	
cb Top	4.56	48.56	

53.12

54.99

531Y

54.84

1+00			
w cb	4.99	48.13	
qut	5.97	47.15	
+7 pav	5.62	47.50	
1/4 "	5.50	47.62	
+10 "	5.57	47.55	
C	5.5	47.62	
rail maid	5.42	47.70	7.27
1/4	5.8	47.32	47.72
+13	6.80	46.32	
qut	6.94	46.19	
E cb	5.95	47.17	
1+50			
E cb	6.02	47.10	
qut	7.17	45.95	
+4	7.03	46.09	
1/4	6.3	46.82	
rail maid	5.86	47.26	7.76
C	5.8	47.32	47.23
+7 pav	6.14	46.98	
1/4 "	6.07	47.05	
+10 "	6.15	46.97	J.P. 7.90
qut	6.46	46.66	27.09
w cb	5.45	47.67	54.82 x
2+00 Sly Goldsmith			
w	5.4	47.72	
+8 cb	5.67	47.45	
" qut	6.80	46.32	

cb	6.52	46.60	
+7 pav	6.27	46.85	
1/4 "	6.21	46.91	
+10 "	6.28	46.84	
C	6.3	46.82	
rail	6.24	46.89	7.97
1/4	6.6	46.52	46.85
+13	7.39	45.73	
qut	7.5	45.57	
E cb	6.14	46.98	
Sly ob			
E cb	6.08	47.04	
qut	7.55	45.57	
+4	7.40	45.72	
1/4	6.7	46.42	
rail	6.25	46.87	
C	6.3	46.82	
+7 pav	6.13	46.99	
1/4 "	6.08	47.04	
+10 "	6.18	46.94	
cb "	5.99	47.13	
w "	5.75	47.37	
Goldsmith			
w pav	5.50	47.62	
cb "	5.91	47.21	
+7 "	6.05	47.07	

1/4 pav	5.95	47.17	
+10 "	6.00	47.12	
C	6.1	47.02	
rail	6.23	46.89	8.02
1/4	6.5	46.82	46.80
+13 edge gut	7.43	45.69	Meet this
gut	Slab over inlet		
Ecb	6.13	46.99	
Nly cb Goldsmith			
Ecb	6.08	47.04	
gut	7.58	45.54	
+4	7.41	45.71	
1/4	6.7	46.42	
rail	6.16	46.96	
C	6.3	46.82	
+7 pav	6.12	47.00	
1/4 "	6.05	47.07	
+10 "	6.15	46.97	
cb "	5.99	47.13	
" "	5.80	47.32	
Nly Goldsmith = 00			
W	5.5	47.62	
+8 Top cb	5.61	47.51	
" gut	6.79	46.33	
cb pav	6.35	46.77	
+7 "	6.19	46.93	

W 1/4 pav	6.10	47.02	
+10 "	6.16	46.96	
C	6.1	47.02	
rail	6.07	47.05	7.85
1/4	6.4	46.72	46.97
+13	7.33	45.79	
gut	7.48	45.64	
Ecb	6.04	47.08	
T.P.	8.07	55.15	6.04
0.50			
Ecb	8.20	46.95	
gut	9.27	45.88	
+4	9.09	46.06	
1/4	8.2	46.95	
rail	7.59	47.56	7.31
C	7.8	47.35	47.51
+7 pav	7.95	47.20	
1/4 "	7.85	47.30	
+10 "	7.95	47.20	
gut	8.30	46.85	
W cb	7.30	47.85	
1.700			
Web	6.57	48.58	
gut pav	7.52	47.63	
+7 pav	7.18	47.97	
1/4 "	7.07	48.08	

J.V.N

1/4 + 10 pav	7.11	48.04	
C	6.8	48.35	
rail	6.91	48.24	6.68
1/4	7.3	47.85	48.14
+ 13	8.28	46.87	
quT	8.42	46.73	
E cb	7.42	47.73	
/ + 5.0			
E cb	6.53	48.62	
quT	7.50	47.65	
+ 4	7.33	47.82	
1/4	6.9	48.25	
rail	6.30	48.85	6.03
C	6.4	48.75	48.79
+ 7 pav	6.34	48.81	
1/4 "	6.27	48.88	
+ 10 "	6.39	48.76	
quT	6.58	48.57	
w cb	5.73	49.42	
2 too Sly Homer			
w	5.0	50.15	
+ 8 cb	5.20	49.95	
" quT	5.94	49.21	
cb pav	5.96	49.19	
+ 7 "	5.76	49.39	
1/4 "	5.62	49.53	

J.V.N

36  
5.2.82

+ 10 pav	5.65	49.50	
C	5.4	49.75	
rail	5.66	49.49	5.37
1/4	6.0	49.15	49.45
+ 13	6.45	48.70	
quT	6.59	48.56	
E cb	5.63	49.52	
Sly cb			
E cb	5.31	49.84	
quT	6.26	48.89	
+ 4	6.12	49.03	
1/4	5.7	49.45	
rail	5.41	49.72	
C	5.4	49.75	
+ 7 pav	5.44	49.71	
1/4 "	5.42	49.73	
+ 10 "	5.53	49.62	
cb "	5.71	49.44	
w "	5.20	49.95	
E			
w pav	4.62	50.53	
cb "	5.37	49.78	
+ 7 "	5.31	49.84	
1/4 "	5.4	50.00	
+ 10 "	5.20	49.95	
C	5.2	49.95	

rail 5.28 49.87 1.94  
 1/4 5.4 49.75 49.50  
 +13 5.84 49.33  
 gut 5.96 49.19  
 Ecb 4.99 50.16

Nly cb  
 Ecb 4.69 50.46  
 gut 5.64 49.51  
 +4 5.53 49.62  
 1/4 5.2 49.95  
 rail 5.03 50.12  
 c 5.1 50.05  
 +7 pav 5.00 50.15  
 1/4 " 4.91 50.24  
 +10 " 5.03 50.12  
 cb " 5.11 50.04  
 r " 4.48 50.67

Nly Hompr=00  
 w 3.9 51.25  
 +8 cb 4.07 51.08  
 " gut 5.02 50.12  
 cb pav 4.92 50.23  
 +7 " 4.95 50.40  
 1/4 4.66 50.49  
 +10 " 4.76 50.39  
 c 4.7 50.45

rail 4.79 50.36 1.44  
 1/4 4.8 50.35 50.35  
 +4 5.24 49.91  
 gut 5.37 49.78  
 Ecb 4.41 50.74

NWBR curb 3.65 57.50  
 O+25  
 wcb 3.71 51.44  
 gut 4.68 50.47  
 +3 edge gut 4.47 50.68  
 +7 bark 4.30 50.85  
 O+50

Ecb 3.35 51.80  
 gut 4.34 50.83  
 +4 4.18 50.97  
 1/4 4.0 51.15  
 rail 3.79 51.36  
 c 3.8 51.35  
 +7 pav 3.87 51.28  
 1/4 " 3.78 51.37  
 +10 " 3.94 51.23  
 1/4 +14 edge gut 4.05 51.10  
 gut 4.22 50.93  
 wcb 3.21 51.94

37  
 54.82  
 BM #19  
 Homer  
 R. records  
 3.34  
 51.28  
 51.50  
 51.82



54.8x

1400		54.8x
w cb	2.31	52.84
gut	3.32	51.83
+3	3.05	52.10
+7 pav	3.00	52.15
1/4 "	2.85	52.30
+10 "	2.91	52.24
C	2.9	52.25
rail	3.18	51.97
1/4	2.2	51.95
+13	3.19	51.66
gut	3.60	51.55
E cb	2.67	52.48

1450		52.8x
E cb	1.82	53.33
gut	2.71	52.44
+4	2.49	52.66
1/4	2.3	52.85
rail	2.29	52.86
C	1.8	53.35
+7 pav	1.96	53.19
1/4 "	1.89	53.26
+10 "	2.01	53.14
+14 edge gut	2.08	53.07
gut	2.39	52.76
w cb	1.38	53.77

54.8x

1475		54.8x
w cb	0.93	54.22
gut	1.93	53.22
+2 edge gut	1.62	53.53
+7 pav	1.56	53.59
2+00 Sly / base		
w	0.0	55.15
+8 cb	0.40	54.75
" gut	1.43	53.72
+11.5 edge gut	1.17	53.98
cb dirt	1.0	54.15
+7 pav	1.08	54.07
1/4 "	0.99	54.16
+10 "	1.10	54.05
C	1.0	54.15
rail	1.46	53.69
1/4	1.5	53.65
+13	1.44	53.49
gut	1.77	53.38
E cb	1.00	54.15
Sly cb		
E cb	0.71	54.44
gut	1.43	53.72
+4	1.31	53.84
1/4	1.2	53.95
rail	1.30	53.85
C	0.8	54.35

1.19  
53.65  
53.65  
1.19  
53.65  
55.67x

55.45

55.67

55.94

55.07<sup>39</sup>

+7 pav	0.78	54.37
1/4 "	0.71	54.44
+10 "	0.76	54.39
cb dirt	0.4	54.75
w "	0.4	54.75

T.P	105	55.94	0.26	54.89
-----	-----	-------	------	-------

E/break

w dirt	0.4	55.54
cb "	0.4	55.54
+7 pav	1.13	54.81
1/4 "	1.17	54.77
+10 "	1.20	54.74
C	1.5	54.44
rail	1.94	54.00
1/4	2.0	53.94
+13	1.81	54.13
gut	2.00	53.94
E cb	1.35	54.59
N/4 cb		
E cb	1.53	54.91
gut	2.18	53.76
+4	2.04	53.90
1/4	2.1	53.84
rail	1.82	54.12

C	1.5	54.44
+7 pav	1.52	54.42
1/4 "	1.33	54.61
+10 "	1.37	54.57
cb dirt	1.0	54.94
w "	1.2	54.74

NL/break = 00

w	0.6	55.34
+8 cb	0.99	54.95
" gut	1.99	53.95
+11.5 edge gut	1.70	54.24
cb dirt	1.6	54.34
+7 pav	1.65	54.29
1/4 "	1.60	54.34
+10 "	1.65	54.29
C	1.70	54.24
rail	1.85	54.09
1/4	2.0	53.94
+13	2.33	53.61
gut	2.24	53.50
E cb	1.79	54.15

O+25 P.C.

w top cb	1.48	54.46
gut	2.48	53.46
+3 edge gut	2.35	53.59
+7 pav	2.26	53.88

1.57
54.10

1.49
53.85

1.55
54.12

0 + 50 55.94 55.07

F cb	2.59	53.35	
gut	3.25	52.69	
+ 4	3.09	52.85	
1/4	2.9	53.04	
rail	2.74	53.20	2.44
C	2.6	53.34	53.23
+ 7 pav	2.55	53.39	
1/4 "	2.44	53.50	
+ 10 "	2.51	53.43	
+ 14 edge gut	2.65	53.29	
gut	2.91	53.03	
w cb	1.91	54.03	
/ + 00			
w cb	2.79	53.15	
gut	3.81	52.13	
+ w edge gut	3.59	52.35	
+ 7 pav	3.36	52.58	
1/4 "	3.30	52.64	
+ 10 "	3.40	52.54	
C	3.5	52.44	
rail	3.75	52.19	3.46
1/4	3.9	52.04	52.21
+ 15	3.96	51.98	
gut	4.10	51.84	
E cb	3.43	52.51	

1 + 50 55.94 40 55.07

F cb	4.25	51.69	
gut	4.92	51.02	
+ 4	4.72	51.22	
1/4	5.0	50.94	
rail	4.67	51.27	2.44
C	4.5	51.44	51.25
+ 7 pav	4.22	51.72	
1/4 "	4.14	51.80	
+ 10 "	4.26	51.68	
+ 14 edge	4.39	51.55	
gut	4.65	51.29	
w cb	3.64	52.30	
/ + 75			
w cb	4.07	51.87	
gut	4.89	51.05	
+ 3	4.80	51.14	
+ 7 pav	4.78	51.36	
2 + 00 Sly James			
w	4.2	51.64	
+ 8 cb	4.48	51.46	
" gut	5.05	50.89	
cb pav	5.21	50.73	
+ 7 "	5.25	50.59	
1/4 "	5.24	50.70	
+ 10 "	5.32	50.62	
C	5.3	50.64	

5594

5507

5594

41  
5507

rair	5.66	50.28	5.40
1/4	5.9	50.04	50.20
+4	6.16	49.78	
gut	6.20	49.74	
Ecb	5.50	50.44	
SL +7 - settled gut			
Ecb	5.74	50.20	
gut	6.56	49.38	
+4	6.46	49.48	
1/4 cb			
Ecb	5.90	50.02	
gut	6.54	49.40	
+4	6.41	49.53	
1/4	6.2	49.74	
rair	6.02	49.92	
C	5.8	50.14	
+7 pav	5.74	50.20	
1/4 "	5.70	50.24	
+10 "	5.83	50.11	
cb	5.65	50.29	
x/	5.32	50.62	
£			
w/ pav	5.80	50.14	
cb	6.14	49.54	
+7 "	6.26	49.68	
1/4 "	6.13	49.81	

+10 pav	6.20	49.74
C	6.5	49.64
rair	6.42	49.51
1/4	6.5	49.44
+13	6.98	48.96
gut	7.11	48.83
Ecb	6.32	49.62
N/4 cb		
Ecb	6.71	49.23
gut	7.45	48.49
+4	7.30	48.64
1/4	6.9	49.04
rair	6.85	49.09
C	6.7	49.24
+7 pav	6.63	49.31
1/4 "	6.60	49.34
+10 "	6.73	49.21
cb	6.63	49.31
w "	6.56	49.38
N/4 James = 00		
w.	6.4	49.54
+5 cb	6.62	49.32
cb gut	7.32	48.62
cb	7.22	48.72
+7 pav	7.15	48.79
1/4 "	7.03	48.91

6.17  
49.50

V.F. 94

V.F. 67

1400

V.F. 94

V.F. 67

42

+10 pav	7.11	48.83	
C	7.1	48.84	
rail	7.21	48.73	6.96
1/4	7.2	48.54	48.71
+13	7.68	48.26	
gut	7.87	48.07	
E cb	7.21	48.73	

0425 Rect

w cb	7.14	48.80	
gut	8.17	47.77	
+2	7.95	47.99	
+7 pav	7.83	48.11	

0+50

E cb	8.25	47.69	
gut	8.93	47.01	
+4	8.74	47.20	
1/4	8.5	47.44	
rail	8.48	47.66	8.05
C	8.1	47.84	47.62
+7 pav	8.19	47.75	
1/4 "	8.10	47.84	
+10 "	8.20	47.74	
+14 edge gut	8.57	47.37	
W cb	7.56	48.38	

BM #10

James  
Rosecrance

NW BP curb

7.14 48.80

w cb	8.75	47.19	
gut	9.75	46.19	
+3 edge gut	9.36	46.58	
+7 pav	9.27	46.67	
1/4 "	9.20	46.74	
+10 "	9.17	46.77	
E	9.0	46.94	
rail	9.27	46.67	9.05
1/4	9.5	46.44	46.64
+12 edge gut	9.73	46.21	
gut	9.91	46.03	
E cb	9.27	46.67	

1750

E cb	10.64	45.30	
gut	11.32	44.62	
+4 edge gut	11.12	44.82	
1/4	10.6	45.34	
rail	10.33	45.61	10.07
C	10.1	45.84	45.60
+7 pav	10.82	45.92	
1/4 "	10.02	45.92	
+10 "	10.15	45.79	
+14 edge gut	10.30	45.64	
gut	10.59	45.35	
W cb	9.60	46.34	

5594

55.07

4719

55.07 <sup>43</sup>1 + 7<sup>1/2</sup> PC.

w cb	9.87	46.07
gut	10.55	45.09
+ 3 edge gut	10.58	45.36
+ 7 pav.	10.43	45.51

T.P. 173 4719 10.48 45.46

2+00 - Sly Kingsley

W	1.5	45.69
+ 8 cb	1.65	45.54
" gut	2.15	45.04
cb	2.22	44.97
+ 7 pav	2.19	45.00
1/4 "	2.10	45.09
+ 10 "	2.16	45.03
C	2.2	44.99
rail	2.52	44.67
1/4	2.5	44.69
+ 13.	3.25	43.94
gut	3.40	43.79
E cb	2.72	44.47
Sly cb		
E cb	3.01	44.18
gut	2.69	43.50
+ 4	3.55	43.64
1/4	2.8	44.39

10.97  
44.70

rail	2.74	44.35
C	2.5	44.69
+ 7 pav	2.40	44.79
1/4 "	2.34	44.85
+ 10 "	2.46	44.73
cb "	2.53	44.66
W "	2.18	45.01

E Kingsley

W pav	2.71	44.78
cb "	2.84	44.35
+ 7 "	2.79	44.40
1/4 "	2.67	44.52
+ 10 "	2.75	44.44
C	2.7	44.49
rail	3.06	44.13
1/4	3.0	44.19
+ 13	3.92	43.27
gut	4.07	43.12
E <sup>cb</sup> in drive	4.08	43.11
Nly cb		
E cb	3.79	43.40
gut	4.44	42.65
+ 4	4.31	42.88
1/4	3.3	43.89
rail	3.32	43.87
C	2.9	44.29

11.54  
44.13

4719

55.67

L + 7 pav	2.99	44.20
1/4 "	3.91	44.28
+ 10 "	3.05	44.14
cb	3.05	44.14
w/ "	2.80	44.39
N/y Kungeloyoo		
w	3.15	44.69
+ 8 cb	2.77	44.42
" gut	3.42	43.77
cb pav	3.39	43.80
+ 7 "	3.98	43.81
1/4 "	3.25	43.94
+ 10 "	3.19	43.90
C	3.12	43.99
rail	3.60	43.59
1/4	3.8	43.39
+ 13	4.72	42.47
gut	4.84	42.35
F cb	4.17	43.02
O + 25 Kcb		
w ropet	3.22	43.97
gut	4.22	42.97
+ 2	4.00	43.19
+ 7	3.82	43.37

TP. 11209  
43.60  
+ 84  
46.44x

O + 50

4719

44  
46.64

Fcb	5.22	41.97
gut	5.78	41.41
+ 4	5.65	41.54
1/4	4.8	42.39
rail	4.40	42.79
C	4.2	42.99
+ 7 pav	4.14	43.05
1/4 "	4.10	43.09
+ 10 "	4.28	42.91
+ 14 edge gut	4.40	42.79
gut	4.57	42.62
x/cb	3.54	43.65
/ 100		
w cb	4.42	42.77
gut	5.22	41.77
+ 3	5.14	42.05
+ 7 pav	5.03	42.16
1/4 "	4.87	42.32
+ 10 "	4.92	42.27
C	4.9	42.29
rail	5.20	41.99
1/4	5.6	41.59
+ 15	6.70	40.49
gut	6.82	40.37
F cb	6.29	40.90

3.97  
42.77

4.58  
41.86

1750

4719

4044

E cb	7.4	40.05
gut	7.60	39.59
+4	7.49	39.70
1/4	6.6	40.59
rail	6.02	41.17
C	5.6	41.59
+7 pav	5.75	41.44
1/4 "	5.62	41.57
+10 "	5.78	41.41
+14 edge gut	5.79	41.40
gut	6.03	41.16
1/2 cb	5.03	42.16

5.43

41.01

1775

W cb	5.42	41.77
gut	6.34	40.85
+7 pav	6.13	41.06
1/4 "	5.95	41.24
+10 "	6.11	41.08
C	6.34	40.85
rail	6.23	40.86
3400 Sly Lyttro		5.85
W 7000	5.45	41.74
gut	6.52	40.67
cb pav	6.30	40.89
1/4 "	6.21	40.98
+10 "	6.40	40.79

40.59

4719

45

C pav	6.65	40.54
+10 rail	6.97	40.22
1/4 pav	7.34	39.85
+14 edge gut + pav	8.33	38.86
gut + pav	8.51	38.68
E cb	8.22	39.07

0.47

39.97

SWBP curb

5.42

41.77

BM #11

LYTTON

ROCCORANO

41.75

0.02 error

cb to #11

4.28

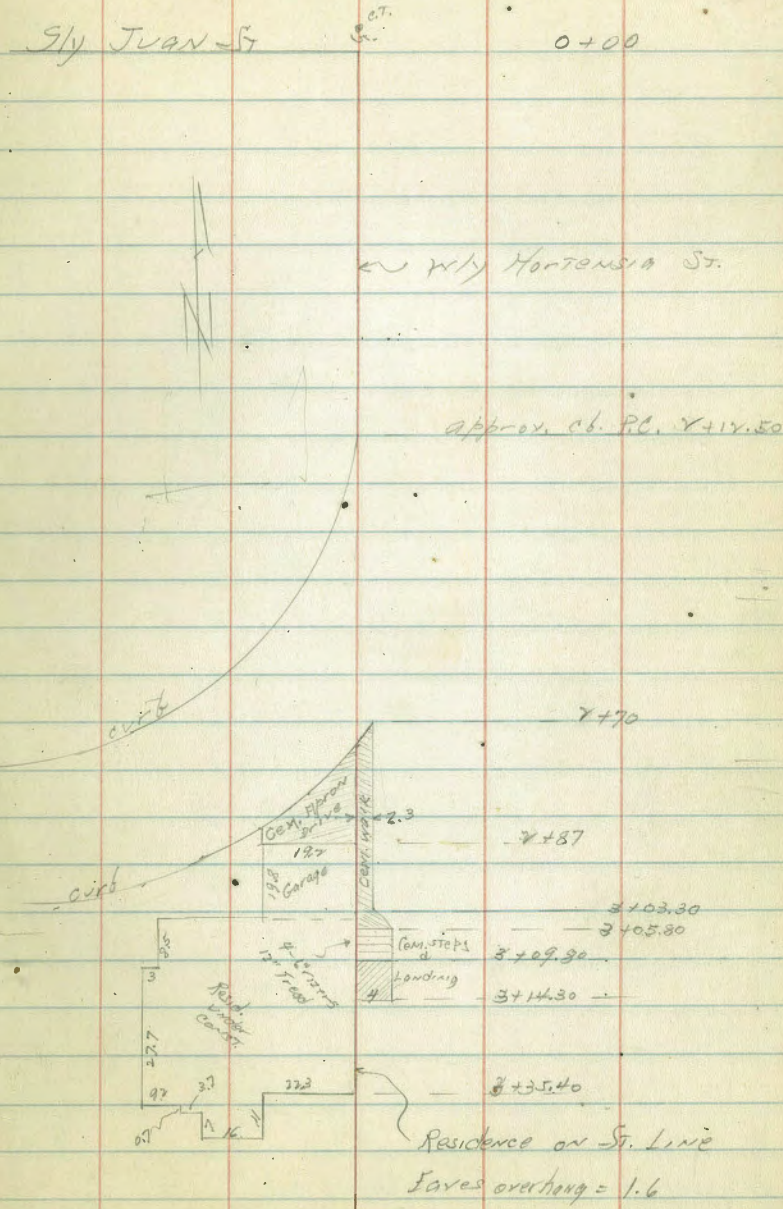
41.74

0.01



Location of Residence, under construction  
with regard to Hortensia St.  
337' Sly from Sly Juan St.

Moore  
Sisson  
Northland 9-19-58



Moore  
1-10-36

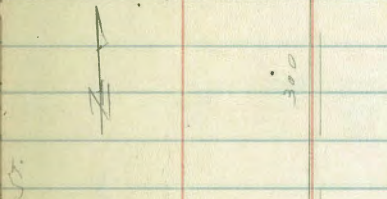
Contour Levels E of 6th St.  
Grape to Ivy for Prop. Archery Range

Indexed  
C.S.K.

47

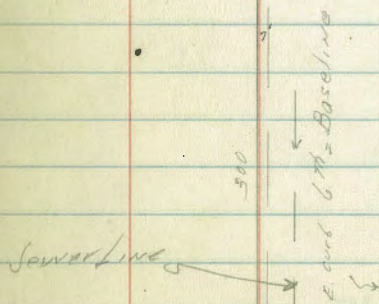
St Ivy

8+35



Hawthorn

2" Water Line 4+79



5th Ct. R Grape

0+84

0+10 CONST. TOILETS about here.



Contour Levels E of 67h

Grape to Ivy St. Taken at RT & from Baseline  
 Note! Ely slope of Gulch is shrub & tree covered.

E of 67h = Baseline

1715

$\frac{1816.2}{21.70}$	$\frac{P. Palm}{3}$	$\frac{P. Palm}{17.5}$	$\frac{182}{22.0}$	$\frac{182.1}{21.1}$	$\frac{180.2}{13.0}$	$\frac{193.2}{9.5}$
			$\frac{27}{27}$	$\frac{6.8}{6.8}$	$\frac{5.2}{5.2}$	$\frac{11.0}{11.0}$

wedge part

1713

$\frac{Eu. Tree}{25}$

T.P. 1310 203.17 134 190.07

203.17

0+98

$\frac{18018}{11.23}$	$\frac{18015}{10.9}$	$\frac{1810}{10.4}$	$\frac{182.3}{9.1}$	$\frac{184.3}{7.1}$	$\frac{191.2}{0.2}$
	$\frac{27}{27}$	$\frac{50}{50}$	$\frac{27}{27}$	$\frac{5.0}{5.0}$	$\frac{10.4}{10.4}$

Eu. Tree  
wedge part

0+94

$\frac{Eu. Tree}{93}$

0+75

$\frac{17826}{12.55}$	$\frac{1824}{10.0}$	$\frac{1844}{7.0}$	$\frac{Eu. Tree}{22}$	$\frac{1890}{94}$
	$\frac{60}{60}$	$\frac{75}{75}$	$\frac{82}{82}$	

0+60

$\frac{P. Palm}{3}$

+50

$\frac{177.61}{13.80}$	$\frac{1824}{12.0}$	$\frac{181.3}{10.1}$	$\frac{1874}{4.0}$
	$\frac{50}{50}$	$\frac{65}{65}$	$\frac{89}{89}$

wedge part

00 = 80 S of ST line of Grape St.

$\frac{175.16}{cb 16.25}$	$\frac{1764}{14.2}$	$\frac{1843}{7.0}$	$\frac{1824}{4.0}$
	$\frac{50}{50}$	$\frac{70}{70}$	$\frac{24}{24}$

wedge part

NWBP 12.90 191.41 178.51 5th of Grape

191.41

3 + 20

← E 16

	191.67		196.9	185.6	186.5	191.4	192.4	214.1	216.8
d sunk	38	P Palm	35.4	41.4	40.3	38.4	34.2	12.7	10.0
			72	50	70	120	140	180	196 edge
									227

T.P. 1246 226.77 0.68 214.21

226.77

3 + 00

	190.6	190.7	185.3	186.5	203.6	214.89
	24.3	24.2	29.6	28.4	11.3	0.2
		22	50	120	140	182

2 + 85

P Palm	P Palm
3	18

2 + 25

	18.77		182.7	184.6	189.4	185.9	197.4	202.5	210.9
	27.2	P. Palm	27.0	30.3	30.5	29.0	17.5	7.4	2.0
			22	45	70	85	125	150	162
									Palm

2 + 04

	285.6		185.8	184.3	184.4	191.2	198.4	207.0
	29.3	P. Palm	29.1	30.6	30.5	23.7	15.5	7.9
			22	40	80	100	125	128 edge
								Palm

T.P. 1225 214.89 0.58 202.64

214.89

1 + 70

	183.7	184.2	182.2	183.2	194.1	202.7
	19.3	19.0	20.0	19.4	9.1	0.5
		22	40	70	100	135

1 + 41

P.P. Tree
41

203.17

203.17

E.C.B.

J+78

J+45

	Pop. Tree	
	43	
P. Palm	P. Palm	
3	18	

T.P. nail part 4.80 230.60 0.19 225.78

230.60  
4

J+40

203.0	203.3	190.1	187.4	187.7	205.1	218.1	225.7
238	235	Pop. Tree 367	384	39.1	21.7	27	1.0
	30	47	50	71	738	170	200
							247 edge part

J+04

Pop. Tree  
51

J+95

P. Palm  
18

J+84

200.1	200.2	189.9	182.5	182.1	203.6	213.5	223.2	224.6
26.7	26.6	37.0	39.3	38.7	23.2	22.0	26	2.8
	30	55	70	77	180	200	225	247 part
		Pop. Tree						

J+45

198.0	P. Palm	M. Palm	188.0	187.5	186.6	187.3	20.2	203.3	212.5	221.5	223.5
28.8	3	18	25	40	60	39.1	39.7	23.5	140	150	3.3
						100	145	180	200	220	247
								Pop. Tree			part

J+06

185.9	195.7	187.0	186.8	187.2	189.8	211.6	221.9
20.9	31.1	37.8	40.0	39.0	37.0	5.8	4.0
	18	45	70	100	145	170	210
	Pop. Tree						200 edge part

J+65

193.9	194.0	186.4	186.3	188.8	211.8	217.8	220.2
32.9	32.8	40.4	40.5	38.0	15.0	7.0	6.6
	3	18	55	100	170	200	220
	P. Palm	P. Palm					edge part

226.77

226.77  
7

7+46

E C 6

$\frac{213.3}{17.0}$	$\frac{213.3}{17.3}$	$\frac{193.6}{37.0}$	$\frac{193.9}{32.7}$	$\frac{193.8}{36.2}$	$\frac{217.6}{13.0}$
		Pop 700			
		51	65	122	109
					190

7+27

$\frac{212.4}{18.2}$	$\frac{212.6}{18.0}$	$\frac{192.0}{33.6}$	$\frac{193.1}{37.0}$	$\frac{192.4}{38.2}$	$\frac{192.9}{37.7}$	$\frac{215.6}{14.0}$	$\frac{226.6}{2.0}$	$\frac{229.8}{0.8}$
		Pop 700	70	100	134	185	230	250
								edge fountain

7+06

H. Palmer  
 $\frac{3}{18}$

7+00

$\frac{211.0}{17.6}$	$\frac{214.2}{19.2}$	$\frac{192.4}{32.2}$	$\frac{190.3}{40.1}$	$\frac{191.2}{39.4}$	$\frac{191.5}{37.1}$	$\frac{208.6}{20.5}$
		48	63	100	115	100

6+83

$\frac{210.2}{20.4}$	$\frac{210.4}{20.2}$	$\frac{192.2}{33.2}$	$\frac{190.4}{40.2}$	$\frac{190.6}{40.0}$	$\frac{192.6}{38.0}$	$\frac{210.1}{20.2}$	$\frac{220.8}{9.8}$	$\frac{228.2}{1.7}$
		48	63	100	120	160	200	240
								edge fountain

6+06

H. Palmer  
 $\frac{3}{18}$

6+25

H. Palmer  
 $\frac{3}{18}$

6+00

$\frac{206.1}{24.5}$	$\frac{206.4}{24.2}$	$\frac{190.2}{40.2}$	$\frac{188.3}{41.3}$	$\frac{188.1}{41.5}$	$\frac{200.2}{30.2}$	$\frac{220.5}{10.1}$	$\frac{226.8}{3.8}$	Part
		65	100	134	160	200	230	241
								10' Drink fountain

5+85

H. Palmer  
 $\frac{3}{18}$

230.60

230.60  
2

Check to 11.35 214.96 215.00

T.P. 409 226.31 734 222.22

8+86 = Sly edge dirt path to

$\frac{220.4}{92}$      $\frac{220.7}{89}$      $\frac{221.2}{84}$      $\frac{226.2}{59}$   
 = Sly edge path So of Bird Cage

8+75

$\frac{219.8}{98}$      $\frac{11.1}{5}$      $\frac{11.7}{15}$      $\frac{220.2}{94}$      $\frac{217.7}{119}$      $\frac{224.6}{50}$      $\frac{225.5}{41}$   
 = Sly edge path to W

8+65

$\frac{225.2}{44}$   
 = Turn of path  
 150

8+50

$\frac{218.5}{111}$      $\frac{218.2}{114}$      $\frac{211.5}{181}$      $\frac{210.0}{176}$      $\frac{216.9}{127}$      $\frac{221.6}{80}$      $\frac{224.0}{108}$

8+25

$\frac{11.1}{3}$      $\frac{11.7}{15}$

T.P. 587 229.56 691 223.69

$\frac{229.56}{7}$

8+00

$\frac{216.0}{16}$      $\frac{216.0}{16}$      $\frac{197.3}{55}$      $\frac{197.6}{85}$      $\frac{214.2}{145}$      $\frac{213.2}{105}$      $\frac{224.1}{200}$     edge path

7+86

$\frac{11.1}{3}$

7+74 all struts & joists from here N.Y.

$\frac{214.6}{16.0}$      $\frac{214.5}{16.1}$      $\frac{194.6}{34.0}$      $\frac{194.6}{57}$      $\frac{194.0}{97}$      $\frac{194.0}{36.6}$      $\frac{203.6}{27.0}$      $\frac{201.4}{29.8}$      $\frac{221.4}{9.2}$      $\frac{227.1}{3.5}$   
 = 30' dist.    = 4' = Euc. tree 12' dist.    edge path

230.60

$\frac{230.60}{7}$

Moore  
1-24-26

X500 oily E 2W 20' wide  
119 U.H.

373.41  
373.74

SEBP.M	6.83	371.30	364.30	Howard
T.P.	4.05	373.24	368.76	Ohio

371.13  
373.24

364.30  
364.47

1+00

0+00 = Ely Kanisai

N Top ob		3.91	369.33	
N Pav		4.27	68.97	
C		4.25	68.99	
S		4.13	69.11	
S Top ob		3.89	69.35	

0+25

S		4.2	69.0	
C		3.9	69.3	
N		4.4	69.0	

0+50

N		4.1	69.1	
C		4.1	69.1	
S		4.2	69.0	

0+73

S		4.7	68.5	
C		4.5	68.7	
N		4.3	68.9	

0+82

-3	S.N. Gar. Cen. Hoar	4.44	68.80	
N	" Floor	4.57	68.67	

368.73  
368.73  
4.1  
4.6  
3.68  
3.68  
0.83  
0.10

N		4.6	68.6
C		4.7	68.5
S		4.9	68.3

1+28

-2.7	Q double Gar. Floor	4.87	68.37
S		4.9	68.3
C		4.7	68.5

1+40

N		4.6	68.6
C		4.7	68.5
S		5.0	68.2

1+60

S		4.6	68.6
C		4.6	68.6
N		4.5	68.7

+2.5 Double gar. dirt Hoar

2+00

N		4.8	68.4
C		4.6	68.6
S		4.6	68.6

2+25

S		5.4	68.0
C		5.4	67.8
N		5.2	67.8

368.23  
50.1  
4.7  
0.14  
hold grades  
set from  
Howard +  
Ohio B.M.



37341

N +38 double gate floor- 5.5 68.09  
 2+80

N 6.2 67.6

C 6.1 67.1

+7 6.0 67.2

J 4.4 68.8

2+99.5 W/Y 30th

S ob 7.3 67.11

S pr 7.38 66.86

c 7.4 65.82

N 7.43 65.81

N ob 7.30 65.94

#61

461

368.71

368.88

9.14

364.10

364.27

SE BP El Canyon 07/16

5.61

363.10

363.27

363.10

363.10 used on original notes to establish grade

paired on curb  
 369.34 = VS6S

363.10 City

363.27  
 363.10  
 0.03

Wood 36  
1-3-36

Xmas alley 17 wide  
61 N. H. St.

Indexed  
c.s.k.

392.49

55  
Additional Spec  
Page 57  
Oct 3-39  
F.S.

SE.BP.	4.00	389.80	385.80	32 <sup>d</sup> Adams	N
T.P.	7.14	392.49	385.35	Marked 2477 on 10166	1+72
E.W. alley 0.400 = Ely 33 <sup>d</sup> St.					corn. Flood
N	par.	6.31	386.18		N
C	"	6.61	385.88		C
S	"	6.46	386.03		S
	0+25				2+00
S		5.8	386.7		S
C		5.7	386.8		C
N		6.1	386.4		N
	0+50				2+40
N		5.5	387.0		N
C		5.4	387.1		C
S		5.5	387.0		S
	0+69				2+68
S		5.5	387.0		S
C		5.1	387.4		C
N		5.0	387.5		N
+18 + E drive to Bldg		4.87	387.62		2+83 = 2' E of W.L. Feiton
	1+00				N sdw
N		5.0	387.5		N par
C		5.1	387.4		C "
S		5.2	387.3		S "
	1+40.5				S sdw
S		4.6	387.9		
C		4.7	387.8		

	4.5	388.0			
	4.06	388.43			Level floor
	4.50	387.99			
	4.4	388.1			
	4.5	388.0			
	4.0	388.5			
	4.0	388.5			
	4.2	388.3			
	3.8	388.7			
	3.6	388.9			
	3.6	388.9			
	4.0	388.5			
	4.0	388.5			
	4.1	388.4			
	4.55	387.99			
	4.65	387.84			
	4.63	387.86			
	4.48	388.01			
	4.43	388.06			

Nt Salley  
15' wide

392.49

61 N. H.S.

392.49

56

0+00 SL of E+Walley

2+50

W	4.7	387.8
C	4.6	387.9
E	4.8	387.7

W	hurst 7 walley	5.4	387.1
C		5.4	387.1
E		5.4	387.3

0+50

F	5.1	387.4
C	5.4	387.3
W	4.9	387.6

T.P.	291	390.00	5.40	387.09
	3+00	390.00		

F		2.9	387.1
C		3.1	386.9
W		3.4	386.8

1+00

W	4.9	387.6
C	5.1	387.4
E	5.1	387.4

	3+50		
W	torvald in alley 8	3.3	386.7
C		3.3	386.7
E		3.1	386.9

1+50

F	5.0	387.5
C	4.8	387.7
W	4.8	387.7

	4+00		
F		4.0	386.0
C		4.0	386.0
W		4.0	386.0

2+00

W	4.7	387.8
C	4.4	388.1
E	4.3	388.2

	4+50		
W		4.3	385.7
C		4.3	385.7
E		4.1	385.9

2+10

F	4.2	388.3
C	4.4	388.1
W	5.0	387.5

	5+00		
F		4.7	385.3
C		4.7	385.3
W		4.7	385.3

+24 E double gate

	5.04	387.45
--	------	--------

level  
0.01  
7/100

390.00

J+09

E on line Sin gar. corr. floor 4.68 385.32

J+50

W 4.9 385.1

C 4.8 385.2

E 4.6 385.4

J+61

E-5 double gar. corr. floor 4.87 385.13

J+94

E-2 Sin gar. corr. floor 4.95 385.05

0+00

E 5.0 385.0

C 5.1 384.9

W 5.1 384.9

6+50 = N.L. Madison

W 6 5.65 384.35

W 7 5.70 384.30

C 5.85 384.15

E 5.62 384.38

E 6 5.57 384.43

T.P. 5.96 389.95 601 383.99

N to SE of Madison &amp; Feiton 378 386.17

S. 68° W dit marked  
3775 St.Oct 3-39 57  
51505

E + W Alley

4.93 392.54 387.62

0+25

0.7 H of S Edge 2' Cor. Walk 5.78 386.76 ✓

0+50

0.7 H of S Edge 2' Cor. Walk  
E End of Walk 5.20 387.84 ✓

0+86

1.8 H of N.L. 2' 3' Door Conc. 4.80 387.74 ✓

1+06

0.8 H of N.L. 2' 5' Door Conc. 4.76 387.78 ✓

1+45

0.3 H of N.L. 2' 5' Door Conc. 4.57 387.97 ✓

N+5

0+98

1.5 E of E.L. 2' 3' Cor. Walk 4.51 388.03 ✓

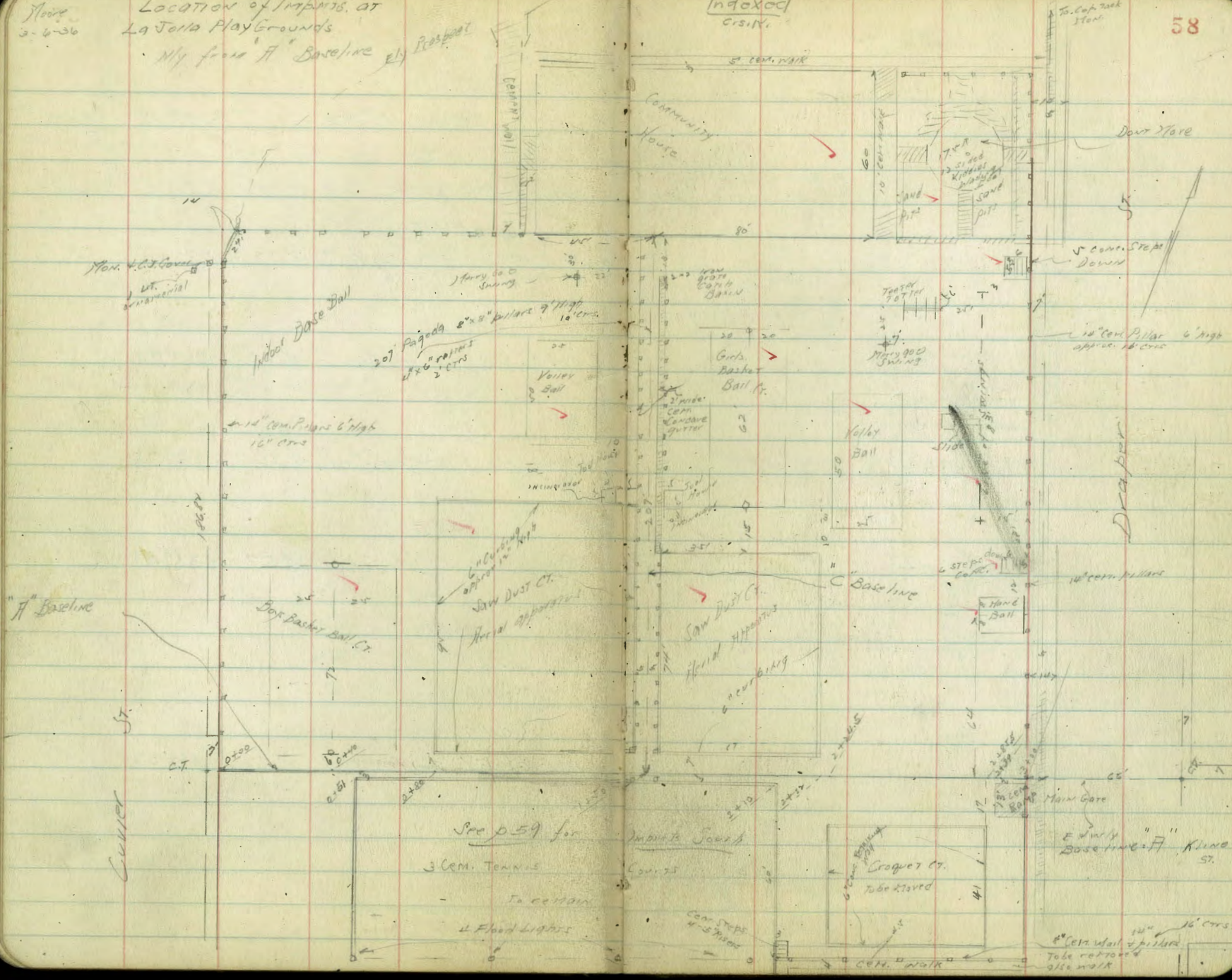
2 Drive  
1.8 H of N.L.  
0+89  
30925

Moore  
3-6-36

# Location of Impms. at La Jolla Playgrounds

My first "A" Baseline

Indexed  
CRISK.



See p. 59 for

INDEXED SOUTH

3 Cem. Tennis

COURTS

To cement

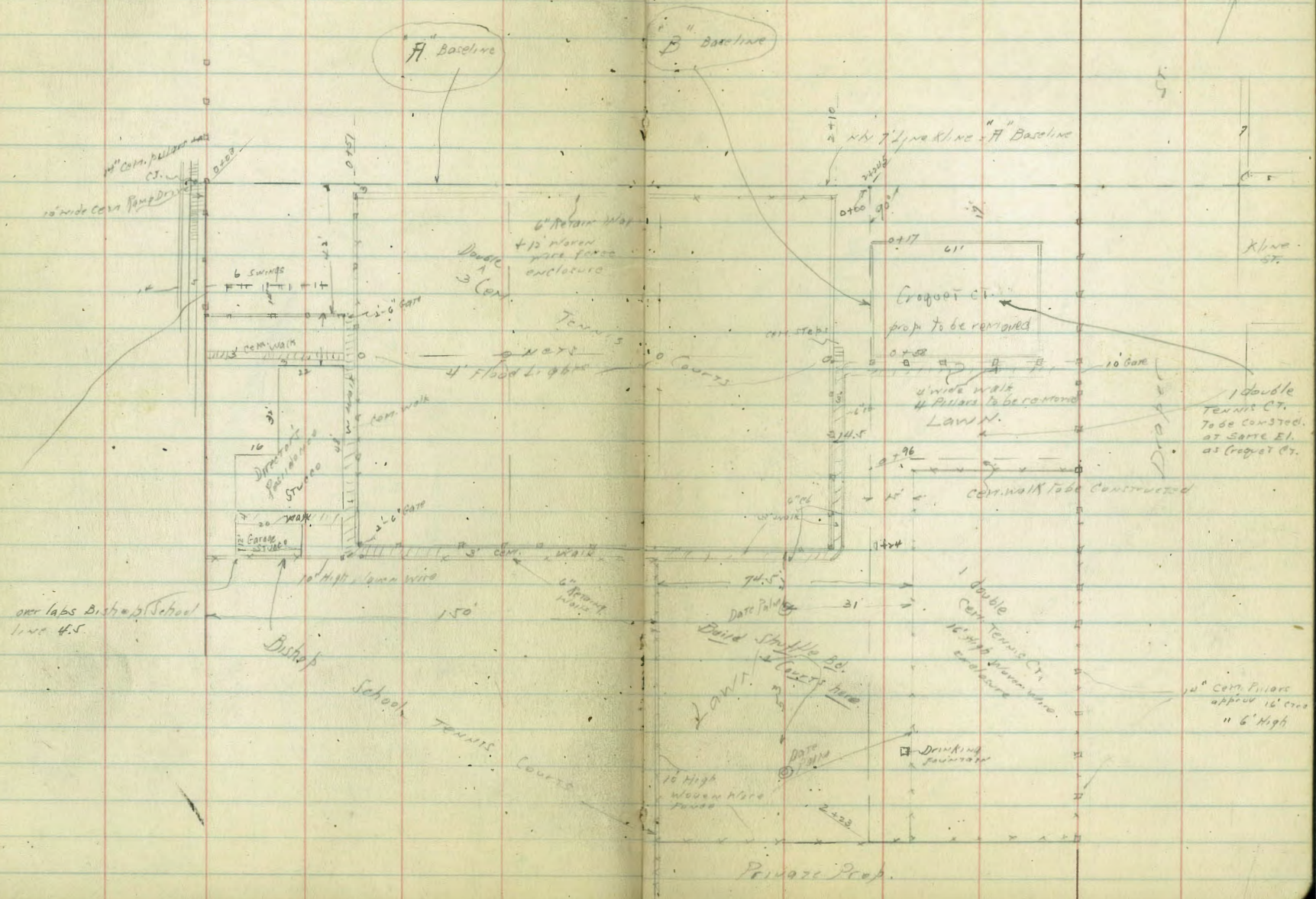
4 Flood Lights

Croquet Ct.  
to be moved

E. side of  
Baseline "A" 57.

8" Cem. Wall & Pillars  
To be removed  
also walk

La Jolla Play Grounds  
Site from "A" Baseline





La Jolla Play grounds  
Levels for contours  
of M + "A" to N  
of "A" Baseline

207 N of "A"

186.82 N of "A"

155 N of "A"

102' N of "A"

42' S of "A"

7' N of "A"

2.15' S of "A" = ground Base of Corn Tennis Cts.

3' S of "A" Baseline = Top Corn. Tennis Cts.

NEBP 7.56 84.05 76.49 Kline Currier Str

LT.

5.32 5.7 4.8  
100 136 gr 70 70 3.6 gr

9.12 8.7 5.36 5.7 4.8  
104 150 148 149 gr 70 gr 3.6 gr

5.29 6.0 4.6  
148 149 gr 70 gr 3.5 gr

5.78 5.8 4.6 3.7 3.5 3.5  
148 149 gr 70 gr 70 gr 3.5 gr

7.46 7.4 5.06 5.8 5.8 3.6  
148 150 148 149 gr 99.9 gr 99

7.52 7.4 5.07 5.7 5.0 4.6 3.6 3.6 3.6  
164 150 149 149 gr 99 70 gr 70 70 5 gr 3.5

5.0 4.6 3.5  
99 70 3.5

3.77 3.5 3.00  
99 70 Corn Tennis Cts.





La Jolla May grounds  
Area S of "A" Baseline

127.5 S of "A"

124' S of "A" = S edge of Triple Tennis Ct To West

96 S of "A" = NE of Ex. Tennis Ct

63.8 = Nedge 3' Cem. Walk - This 3' walk 46" cb. to be removed  
also ret. wall & 14" Pillars  
To Make room for prop. Tennis Ct.  
to serve same as Ex. Ct. South.

62.7 S of "A" = Top 8" wall

62.6 S of "A" = Nedge 8" Cem. Ret. wall

58' S of "A"

Center of Croquet Ct. =

6.0

82.37

Grade of Prop.  
Tennis Ct.

17' S of "A" Baseline

88.37

LF "B" RT. = Wly from "B" 63

Baseline

4.67  
75  
Tennis

5.0  
75  
Lawn

5.20  
75  
6'6"

6.48  
74.8  
6'6"

4.60  
75  
Tennis

4.63  
75  
Tennis

5.0  
75  
Lawn

5.37  
75  
Walk

6.45  
74.8  
Wall

6.74  
74.8  
Tennis Ct.

2.29  
75  
Top Wall

4.86  
75  
Cem. Ct.

4.86  
75  
Cem. of Tennis Ct.

4.9  
75  
Lawn

5.30  
75  
Cem. Wall

6.27  
74.8  
Top Wall

6.74  
74.8  
Tennis Ct.

3.8  
75  
Cem. Wall

4.7  
75  
Cem.

5.0  
75  
Cem. Walk  
E. Top Step

6.27  
74.8  
Top Wall

6.74  
74.8  
Tennis Ct.

2.90  
75  
Cem. Wall

4.08  
75  
Cem. Wall

4.27  
75  
Cem. Wall

5.7  
75  
gr.

6.8  
75  
gr.

6.8  
75  
gr. against  
Cem. Steps

5.7  
75  
gr.

5.9  
61  
gr.

5.26  
61  
cb.

5.66  
61  
cb.

6.7  
61  
0.1 gr.

6.71  
61  
Cem. Tennis Ct.

5.0  
75  
gr.

5.8  
61  
gr.

5.11  
61  
cb.

5.6  
61  
Topch.

6.6  
61  
0.1 gr.

6.74  
61  
Cem. Tennis Ct.

88.37

check to B.M.  
 T.P. 70<sup>u</sup> 8333 68<sup>x</sup> 76.49 76.49  
 12.08 76.29

223' S of A"

5.30 5.30 6.1 6.3 6.8 7.41 8.0 7.11  
 7.0 7.0 10 10 30 30 69 74.5 74.5  
 ← JENNIS ST ← LOWN LOWN LOWN LOWN LOWN

193' S of A"

5.06 5.6 5.3 7.0 7.9 7.10  
 7.0 7.0 30 69 74.5 74.5  
 ← JENNIS ST ← LOWN LOWN LOWN LOWN

160' S of A"

4.88 5.3 4.7 6.83 7.8 7.13  
 7.0 7.0 30 69 74.5 74.5  
 ← JENNIS ST ← LOWN LOWN LOWN LOWN

88.37

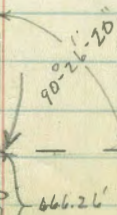
88.37



12-14-36 Survey Pueblo lots 1269-1272-1293  
 Miller Walker Blinn  
 1294 & E. 1/2 of 1295 City  
 Land for Leases.

Sta. 213+28<sup>13</sup> B.C.R. Fl. Cr.  
 F.B. 1325-P. 44  
 Rose Canyon Road

900.24 R.O.M. Sheet



Sta. 197+61.53 E.C.

4-20-37 X Sec. Chamouné Landis to Dwight  
 Miller Walker Blinn  
 60' wide - 12' chs. 9' 1/4 s

Index of  
 C. S. K. 66

N.W. Landis

BM. B.P. — 1.37 — 342.32 — — 341.00 — + Chamouné

0+00 - 32'

W.d	0.92	341.40
G. Pav	1.59	340.73
1/4 "	1.03	341.29
1/4 "	0.92	341.40
1/4 "	1.10	341.22
G "	1.65	340.67
E. d	1.02	341.30

0+00 - 20'

E. d	1.13	341.19
G. Pav	1.81	340.51
1/4 "	1.25	341.07
1/4 "	1.02	341.30
1/4 "	1.11	341.21
G "	1.66	340.66
W. d "	1.03	341.29

0+00 - 08'

W. emb. d	1.12	341.20
G Pav	1.85	340.47
1/4 "	1.17	341.15
1/4 "	1.08	341.24
1/4 "	1.33	340.99
G "	1.95	340.37
E. emb. d "	1.26	341.06



0+23 = N. ch. on W.

E	1.5	340.8
cl	1.6	340.7
"4	1.3	341.0
±	1.3	341.0
"4	1.6	340.7
cl	2.0	340.3
W G	2.1	340.2
W. Incl.	1.39	340.93

0+32 = ± to E.

W	2.2	340.1
cl	2.1	340.2
"4	1.7	340.6
± Top sewer M.H.	1.30	341.02
"4	1.4	340.9
cl	1.8	340.5
E.	1.4	340.9

0+49 = ± to W

E	2.1	340.2
cl	2.1	340.2
"4	1.8	340.5
±	1.7	340.6
"4	2.0	340.3
cl	2.1	340.2
W.	1.6	340.7

0+52 = S. ch. on E.

W	1.6	340.7
cl	2.1	340.2
"4	2.0	340.3
±	1.7	340.6
"4	1.8	340.5
cl	2.1	340.2
E. G.	2.1	340.2
E. Top ch.	1.83	340.49

0+64 = S. Line on E

E. ch	1.82	340.50
G	2.3	340.0
"4	2.1	340.2
cl	1.8	340.5
"4	2.1	340.2
cl	2.3	340.0
W.	2.0	340.3

0+75 = S. ch. Line to W.

W. = Top ch.	1.83	340.49
W. G.	2.6	339.7
cl	2.7	339.6
"4	2.2	340.1
±	2.0	340.3
"4	2.3	340.0
G	2.7	339.6
E. ch.	2.26	340.06

0+89 = s. Line Landis to West = 0+00

E. d.	2.74	339.58
G	3.1	339.2
"	2.7	339.6
⊥	2.3	340.0
"	2.4	339.9
G	2.5	339.8
W. d.	1.97	340.35
0+50 s.		
W. d.	3.79	338.53
G	4.2	338.1
"	4.1	338.2
⊥	3.9	338.4
"	4.3	338.0
G	4.7	337.6
E. d.	4.51	337.81
1+00		
E. d.	6.27	336.05
G	7.1	335.2
"	6.3	336.0
⊥	6.0	336.3
"	5.9	336.4
G	6.2	336.1
W. d.	5.65	336.67
1+50		
W. d.	7.61	334.71
G	8.2	334.1

"	7.9	334.4
⊥	7.7	334.6
"	8.3	334.0
G	8.8	333.5
E. d.	8.06	334.26
2+00		
E. d.	9.83	332.49
G	10.3	332.0
"	10.0	332.3
⊥	9.6	332.7
"	9.8	332.5
G	10.4	331.9
W. d.	9.52	332.80
2+50		
W. d.	11.42	330.90
G	12.2	330.1
"	11.5	330.8
⊥	11.3	331.0
"	11.7	330.6
G	12.3	330.0
E. d.	11.60	330.7
2+77		
E. d.	12.48	329.54
G	12.9	329.4
"	12.7	329.6
⊥	12.2	330.1



2+77 (con)

14			12.4	329.9
+5			12.5	329.8
G			13.5	328.8
w.d			12.43	329.89
T.P.	107	330.75	12.64	329.68

3+00

w.d			1.52	329.23
G			2.4	328.4
+4			1.5	329.3
14			1.4	329.4
±			1.2	329.6
14			1.6	329.2
G			2.1	328.7
E.d			1.58	329.17

3+50

E.d			2.79	327.96
G			3.2	327.6
14			2.8	328.0
±			2.7	328.1
14			2.5	328.3
G			2.9	327.9
+6			3.6	327.2
w.d			2.67	328.08

4+00

w.d			3.47	327.28
G			4.2	326.6

+4			3.8	327.0
14			3.7	327.1
±			3.6	327.2
+5			3.7	327.1
14			4.3	326.5
G			4.3	326.5
E.d			3.7	326.97

4+50

E.d			4.70	326.05
G			5.2	325.6
14			5.2	325.6
±			4.7	326.1
14			4.4	326.4
G			4.9	325.9
w.d			4.24	326.51

5+00

w.d			5.08	325.67
G			5.9	324.9
14			5.4	325.4
±			5.3	325.5
14			5.7	325.1
G			6.0	324.8
E.d			5.52	325.23

5450

E. d	6.30	324.45
G	6.9	323.9
14	6.4	324.4
⊕	6.1	324.7
14	6.3	324.5
G	6.4	324.4
W. d	6.00	324.75

T.P. B.M. = 4.27 328.27 6.73 324.02 = N.W. Dwight. + champagne 324.00.  
 5+75 = S. End cmt. walk + curb one e.

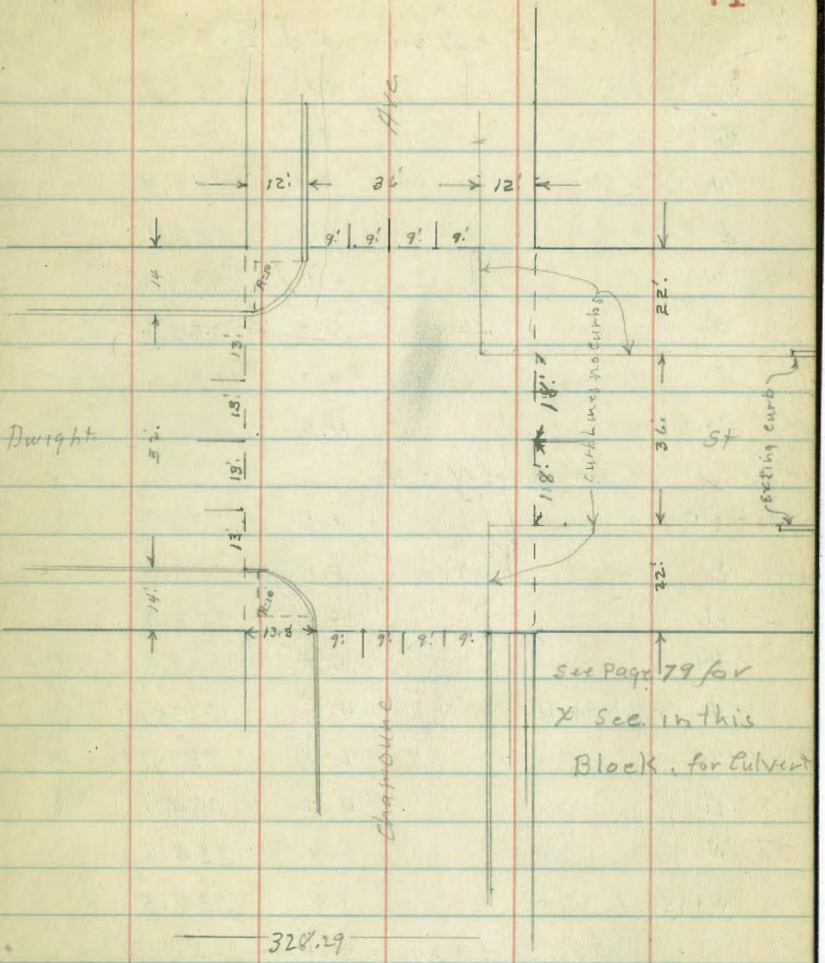
E. d	4.33	323.94
+ 5.67 E = W. edge cmt walk	4.18	324.09
+ 10.0 E = E. " " "	4.06	324.21

6+00 <sup>50</sup> = N. Line = Dwight = 00

W. d	4.30	323.97
G	4.6	323.7
14	4.3	324.0
⊕	4.3	324.0
14	4.4	323.9
G	4.7	323.6

ch. drvt.	4.3	324.0
E	4.0	324.3
14' S. of N. = N. ch. Line to W.		
E	4.1	324.2
+ 10.0	4.4	323.9
ch	4.9	323.4
14	4.5	323.8

E Dwight



N. d. Line (con)

⊕	4.5	323.8
14	4.4	323.9
d.	4.6	323.7
W. Line Top. d.	4.24	324.03
W. ground.	3.9	324.4
+ 15 "	3.6	324.7

22' S. of N. Line = N. of Line to E.

W	4.1	324.2
cl	4.5	323.8
114	4.5	323.8
±	4.6	323.7
114	4.6	323.7
cl	5.0	323.3
E	4.7	323.6
+25	4.5	323.8

40' S. of N = ±

-25	4.6	323.7
E	5.0	323.3
cl	5.0	323.3
114	5.0	323.3
± Top. M.H.	4.70	323.57
114	4.6	323.7
cl	4.2	324.1
W.	3.7	324.6
W+15	2.8	325.5

58' S. of N. Line = S. of Line to E.

W-15	3.6	324.7
W	4.0	324.3
cl	4.3	324.0
114	4.5	323.8
±	4.6	323.7
114	4.9	323.4
cl	5.3	323.0

E	5.6	322.7
+15	5.2	323.1
+20	4.5	323.8
+50	3.8	324.5

66' S. of N = S. of Line to W

E-50	3.7	324.6
E-20	4.5	323.8
E-15	5.9	322.4
E-10	5.8	322.5
E-8	4.8	323.5
E	4.9	323.4
cl	5.2	323.1
114	4.9	323.4
±	4.6	323.7
114	4.5	323.8
cl	4.4	323.9
W. ground	3.9	324.4
W. Top. cont. cl	4.28	324.01
+15 W. ground	3.6	324.7

80' S. of N. Line = S. Line Dwight = N. End walk to cl on E.

W. cl	4.35	323.94
G	4.4	323.9
114	4.6	323.7
±	4.5	323.8
114	4.7	323.6
G	5.0	323.3

S Line = 0+00

E. ch. N. End	5.30	322.99
+6.0 = W. edge walls N. End	5.12	323.17
+10.33 = E. " " N. End	5.04	323.25
E	4.7	323.6
+3	3.4	324.9
+14	3.8	324.5
+16	5.9	322.4
+29	5.9	322.4
+43	4.1	324.2
+50	3.9	324.4
3.6 S. of S. Line = S. edge = face ext. wall		
-50	3.8	324.5
-40	4.1	324.2
-35 = E. End cone wall E. 5' thick	5.9	322.4
-26	6.2	322.1
-16 = W. End cone wall	5.9	322.4
-12	3.0	325.3
-3	3.4	324.9
E.	4.8	323.5
3.7 S. of S. Line		
E	4.8	323.5
+3	3.4	324.9
+12	3.0	325.3
+16 base of wall	12.6	315.7
+26 " " "	12.6	315.7
+33 " " "	12.3	316.0

+35	5.9	322.4
+40	4.1	324.2
+50	3.8	324.5
16' S. of S. Line, Daight		
E-50	9.0	319.3
E-35	10.0	318.3
E-34 E. side wash bottom	12.5	315.8
E-21 W. " " "	13.4	314.9
E-19	7.0	321.3
E-10	2.6	325.7
E	4.1	324.2
E. d	4.7	323.51
G	4.9	323.4
H	4.6	323.7
I	4.2	324.1
J	4.3	324.0
G	4.1	324.2
W. d	3.8	324.41

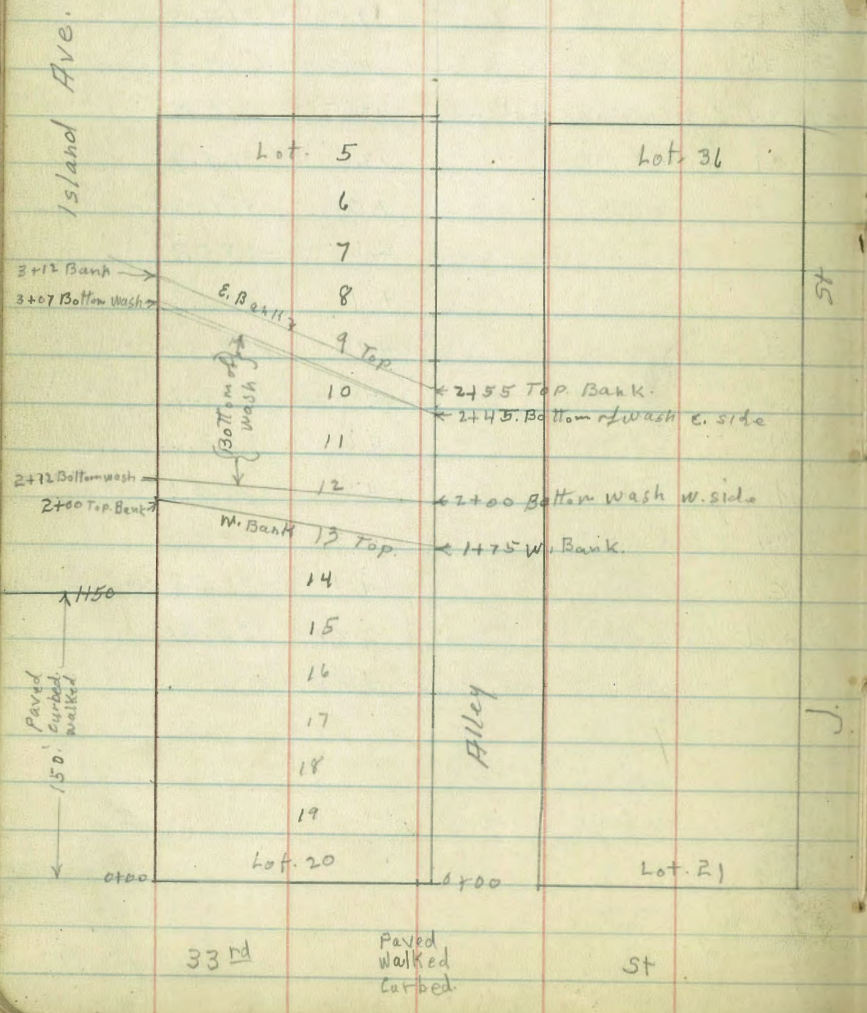
Continued on Page 79.

7-8-37  
Miller  
Walker  
Blair

Survey of Chollas Creek in  
Blk. 4. ME Larens. Add.  
F.M. #291.

200  
212  
307  
312

175  
2  
246  
258



X Sec. Area at former location  
of Palisades. Caffer for Park Dept.

12-18-36  
Miller  
Walker.

Indexed  
C.S.K.

1430N.  
P.C. CURB 75

B.M. Top. d. P.C. 8.22 108.22 100.0 ass. 0+00 E+W. 0+25 North.

0+25 N. gutter pavmt. 8.50  
0+25 N on curb at P.C. 8.22  
0+50 N " " 7.73  
0+75 N " " 7.30  
1+00 N " " 7.70  
1+25 N " " 6.22  
1+25 N gutter Pav 6.50  
1+50 N ground. 5.7  
1+50 N 0+2.7E. Top. eb. on curve 5.75

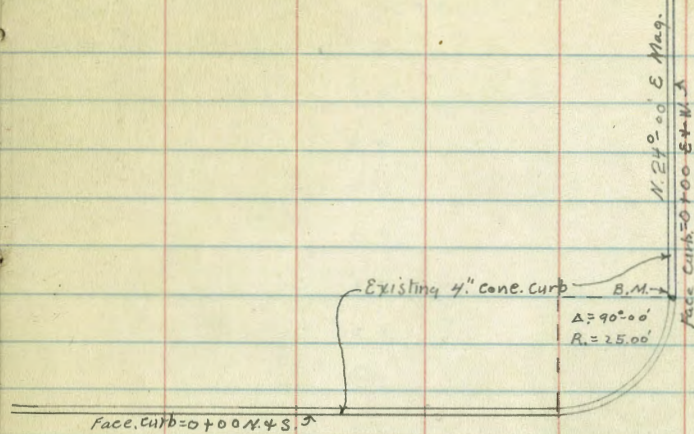
0+12<sup>E</sup> N.  
1+50' N. 4.4  
1+25' N. 5.0  
1+00 N 5.4  
0+75 N. 5.9  
0+50 N 6.0  
0+25 N 6.8

0+25 W.  
0+00 gutter pav 9.01  
0+00 N+S Top. eb. 8.70  
0+12<sup>E</sup> N. 7.0  
0+25 N. 5.4  
0+50 N. 5.1  
0+75 N. 5.0  
1+00 N 5.5  
1+25 N 4.7  
1+50 3.8

Grade.

Grade

Grade.



1+65	108.22	
1+50 N.	0+50 W. 2.8	Grade
	2.9	Grade.
1+35 N	4.7	
1+25 N	4.8	
1+00 N	4.9	
0+75 N	5.0	
0+50 N	5.2	
0+25 N	5.3	
0+14 N	5.4	
0+12.5 N	5.9	
0+09.5 N	7.2	
0+00 N+S = Curb.	8.54	
	0+75 W.	
0+00 N+S = Curb.	8.43	
0+11 N.	7.1	
0+12.5 N.	5.4	
0+25 N.	5.3	
0+50 N	5.2	
0+75 N.	4.8	
1+00 N.	4.8	
1+25 N.	4.5	
1+25 N.	1.7	Grade
1+50 N	1.2	Grade
	1+00 W.	
1+50 N.	0.2	Grade
1+25 N	0.7	Grade
1+11 N.	1.3	Grade

108.22

1+00' W. (con)

1+00 N.	3.4
0+90 N.	4.9
0+75 N.	4.8
0+50 N.	5.0
0+25 N.	5.3
0+12 <sup>5</sup> N	5.6
0+10 N.	6.8
0+00 N+S. = curb	8.30

1+35' W.

0+00 <sup>N+S</sup> gutter Pav	8.48	
0+00 N+S = curb	8.16	
0+12.5 N.	4.9	Grade
0+25 N.	3.7	Grade
0+25 N 1+29 W.	4.3	
0+25 N 1+27 W	5.4	
0+43 N 1+25 W	3.2	
0+43 N 1+22 W	4.8	
0+50 N 1+31 W.	2.6	
0+50 N 1+30 W.	4.9	
0+75 N. 1+27 W	4.9	
0+50 N. 1+35 W.	2.5	Grade
0+75 N 1+35 W.	2.0	Grade
1+00 N 1+35 W.	0.7	Grade
1+00 N 1+04 W	3.6	
1+00 N 1+12 W.	1.0	Grade
1+25 N 1+35 W	0.3	Grade

77



108.22

1450 W.

78

1425 N	0.0	108.2	Grade
1400 N	0.8	107.4	Grade
0475 N	1.8		Grade
0450 N	2.5		Grade
0425 N	3.6		Grade
0412 <sup>E</sup>	4.4		Grade

7-19-37 X. Sec. Chamounie & Dwight  
 Miller  
 Wal. Ke. Continued from Page 73  
 Bliss

B.M.	220	326.20		324.00
T.P.	3.51	320.16	9.55	316.65
		24' S. of S. Line Dwight		320.16
40' E. of E. Line Chamounie		3.5		316.7
33 " " " "			3.4	316.4
31 " " " " Wash		11.0		309.2
28 " " " " " "			11.0	309.2
25 " " " " " "			1.2	319.0
		29' S. of S. Line Dwight		
29' E. of E. Line Chamounie		2.8		317.4
31 " " " " " " Wash			11.2	309.0
35 " " " " " " " "			11.4	308.8
34.9 " " " " " " " "			4.6	315.6
40 " " " " " " " "			3.6	316.6
46 " " " " " " " "			4.4	315.8
47 " " " " " " Wash		19.8		308.4
57 " " " " " " " "			10.5	309.7
		31' S. of S. of Dwight		
65 E. of Chamounie		10.0		310.2
57 " " " " " " N.E. edge wash		13.0		307.2
33 " " " " " " " "			11.7	308.5
32.9 " " " " " " " "			3.3	316.9
		43' S. of Dwight		
37.9 E. of Chamounie		3.7		316.5
38.0 " " " " " " S.W. edge wash		12.0		308.2
70 " " " " " " E " " "			13.0	307.2
75 " " " " " " " "			11.0	309.2

N.W. Chamounie  
 & Dwight

				47' S. of Dwight	320.2
				75' E. of Chamounie	11.4
				70 " " " " E. edge wash	13.5
				52 " " " " " " " "	13.5
				51 " " " " " " " "	11.5
				44 " " " " " " " "	8.5
				38 " " " " " " " "	4.5
				55' S. of Dwight	
				40' E. of Chamounie	6.3
				62 " " " " " " " "	11.7
				65 " " " " " " Wedge wash	14.6
				69 " " " " " " E " " "	14.4
				75 " " " " " " " "	13.0
				70' S. of Dwight	
				40' E. of Chamounie	8.2
				60 " " " " " " " "	14.0
				67 " " " " " " Wedge wash	15.0
				72 " " " " " " E " " "	15.6
				75 " " " " " " " "	12.4
				85' S. of Dwight	
				42' E. of Chamounie	11.7
				55 " " " " " " " "	15.0
				61 " " " " " " Wedge wash	15.7
				67 " " " " " " E " " "	15.8
				68 " " " " " " " "	13.5

42.

46  
34.80  
24.80  
70.

~~46~~  
~~34.8~~  
~~11.2~~

45  
~~34.8~~  
1.2

150.82  
267  
189.82

24  
11.2  
10  
244  
78.0

3480

126  
81  
207

4.10  
4.02  
39V 41~