

1526



FIELD BOOK

No. 385F

MICROFILMED

DEC 24 1964

1/2 - 1101
2-1101
1-30/178
1339/178

467
336
137

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

114
1146
1193
11411
11411

Topog in Park Swimm
Pool Area

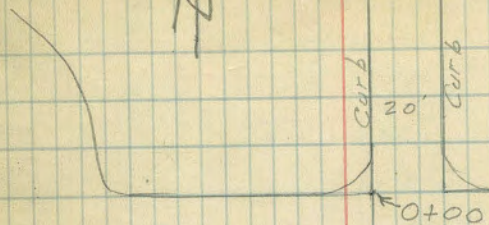
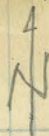
June 25-35

Louden

Caldwell

Grabowski

indexed
c.s.K.



SWIMMING
POOL
AREA

Base line for Baseball
and Volley ball areas.

6+00

B.M	1.84	281.36		279.52
T.P.*	5.29	278.82	7.83	273.53
		0+00		
15 R	End Curve return	6.10		272.72
		0+20		
±		5.7		273.1
25 R		7.0		271.8
50 R		8.2		270.6
75 R		9.1		269.7
		0+50		
75 R		9.6		269.2
54 R		8.3		270.5
50 R		7.9		270.9
25 R		6.8		272.0
±		5.7		273.1
		1+00		
±		4.9		273.9
25 R		6.2		272.6
56 R		7.8		271.0
60 R		9.0		269.8
75 R		9.9		268.9

N.W. Cor.
Base Peg pole

278.82

1+50

100 R		10.6		268.2
83 R		9.7		269.1
73 R		8.9		269.9
50 R		6.8		272.0
25 R		5.0		273.8
±		3.6		275.2
		0+00		
15 L	end curve ret.	4.63		274.19
		0+20		
20 L		5.3		273.5
50 L		4.7		274.1
75 L		3.8		275.0
		0+50		
75 L		3.7		275.1
50 L		4.3		274.5
20 L		5.4		273.4
		1+00		
20 L		4.3		274.5
50 L		3.8		275.0
75 L		3.1		275.7
		1+50		
75 L		2.7		276.1
50 L		2.9		275.9
20 L		3.1		275.7

278.82

2+00

100L	1.6	277.2
75L	1.9	276.9
50L	2.3	276.5
25L	2.4	276.4
Φ	3.8	275.0
25R	5.0	273.8
50R	7.1	271.7
66R	8.3	270.5
100R	10.2	268.6
124R	11.7	267.1
135R	12.0	266.8

2+50

181R	13.6	265.2
164R	13.3	265.5
151R	14.4	264.4
127R	13.8	265.0
100R	10.6	268.2
75R	9.5	269.3
50R	7.8	271.0
25R	5.6	273.2
Φ	4.1	274.7
25L	2.7	276.1
50L	2.0	276.8
75L	1.4	277.4
100L	1.2	277.6

278.82

TP 2.03

278.74 2.11 276.71

3+00

100L	2.0	276.7
75L	2.7	276.0
50L	2.7	276.0
25L	3.5	275.2
Φ	4.6	274.1
25R	6.2	272.5
50R	7.9	270.8
75R	9.1	269.6
100R	9.9	268.8
162R	12.5	266.2
185R	13.6	265.1
200R	14.8	263.9

3+50

200R	12.5	266.2
175R	11.2	267.5
150R	9.7	269.0
147R	9.0	269.7
125R	7.7	271.0
100R	6.9	271.8
75R	6.6	272.1
50R	7.0	271.7
25R	6.1	272.6
Φ	4.8	273.9

278.74

3+50

25L	4.1	274.6
50L	3.3	275.4
75L	2.9	275.8
100L	2.4	276.3

3+55

100L	3.0	275.7
75L	3.2	275.5
50L	3.5	275.2
25L	3.8	274.9
⊕	4.0	274.7
25R	4.6	274.1
33R	6.3	272.4
50R	6.9	271.8
75R	6.4	272.3
100R	6.7	272.0
146R	9.2	269.5
152R	9.9	268.8
182R	11.7	267.0
200R	12.6	266.1

278.74

3+60

200R	12.6	266.1
175R	10.7	268.0
153R	10.2	268.5
152R	9.2	269.5
123R	7.2	271.5
100R	6.7	272.0
92R	6.3	272.4
83R	5.3	273.4
50R	4.6	274.1
25R	4.5	274.2
⊕	4.1	274.6
25L	4.0	274.7
50L	3.6	275.1
75L	3.2	275.5
100L	2.9	275.8

3+65

100L	3.0	275.7
75L	3.0	275.7
50L	3.5	275.2
25L	3.9	274.8
⊕	4.2	274.5
50R	4.6	274.1
100R	5.1	273.6

3+65

278.74

124R	5.7	273.0
159R	10.3	268.4
200R	12.5	266.2

3+70

200R	12.4	266.3
175R	10.9	267.8
157R	10.4	268.3
145R	5.7	273.0
125R	5.4	273.3
100R	4.9	273.8
50R	4.6	274.1
⊕	4.2	274.5
25L	4.0	274.7
50L	3.3	275.4
75L	3.0	275.7
100L	2.8	275.9

4+00

100L	3.1	275.6
50L	3.2	275.5
⊕	4.1	274.6
50R	4.6	274.1
100R	5.0	273.7
150R	5.6	273.1
179R	6.2	272.5
193R	10.8	267.9
200R	10.8	267.9

5

278.74

4+50

200R	8.4	270.3
186R	8.0	270.7
182R	6.6	272.1
150R	6.4	272.3
100R	5.9	272.8
50R	5.2	273.5
⊕	4.5	274.2
50L	3.5	275.2
100L	3.6	275.1

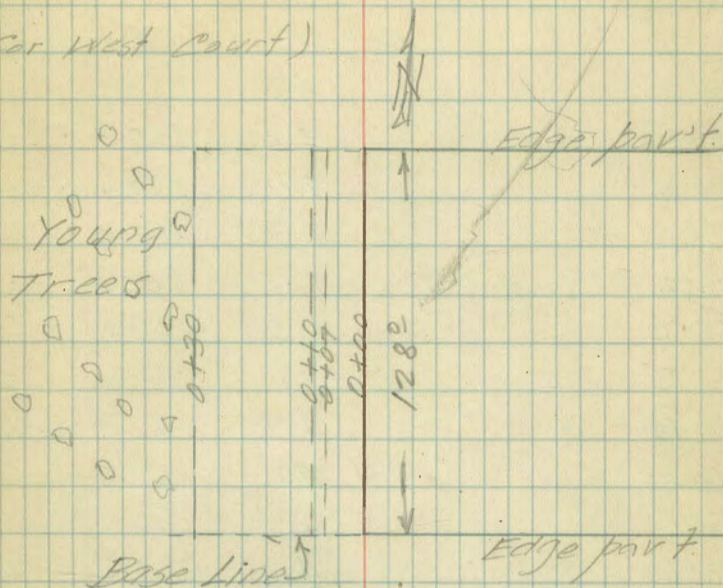
5+00

100L	4.4	274.3
50L	4.3	274.4
⊕	4.8	273.9
50R	5.5	273.2
100R	6.2	272.5
150R	6.6	272.1
200R	7.5	271.2
T.P.*	5.30	273.44

Indexed
C.S.K.

Topog at West end of
Tennis Courts 6

B.M.	3.00	272.74	269.74	Top pav. (S.W. Cor West Court)
		0+00		
10 L		4.1	268.6	
6 L		3.7	269.0	
4	on Pav	3.00	269.7	
50 R	" "	2.59	270.15	
100 R	" "	2.23	270.51	
128 R	" " Nodge	2.00	270.7	
133 R		2.2	270.5	
138 R		4.1	268.6	
		0+07		
10 L		4.5	268.2	
6 L		3.4	269.3	
B.L.		3.1	269.6	
50 R		2.8	269.9	
100 R		2.3	270.4	
128 R		2.1	270.6	
134 R		2.6	270.1	
138 R		4.1	268.6	



0+10

138R	4.3	268.4
128R	3.4	269.3
100R	4.0	268.7
50R	4.3	268.4
B.L.	4.6	268.1
10.L	4.6	268.1

0+11

10L	4.9	267.8
B.L.	4.9	267.8
50R	4.4	268.3
100R	4.4	268.3
128R	4.1	268.6
138R	4.3	268.4

0+30

138R	5.1	267.6
128R	5.0	267.7
100R	5.2	267.5
50R	5.4	267.3
B.L.	4.9	267.8
7L	5.3	267.4
12L	6.6	266.1

B.M.	1.39	280.91		279.52
T.P.*	3.16	276.59	7.48	273.43
T.P.	1.36	272.74	5.21	271.38
B.M.			3.00	269.74

← Top par. SW. Cor West Court

Topog at roque
 Courts. indexed
 C. S. R.

TP*	10.36	283.79	273.43	
T.P.	1.75	273.17	12.37	271.42
Top curb east roque of.	5.67	267.50		
	4.66	272.16	267.50	
	0+01			

11L		4.8	267.4
BL		4.7	267.5
4R	conc	4.68	267.48
30R	"	4.68	267.48
56R	"	4.66	267.50
60R		4.7	267.5
70R		4.8	267.4

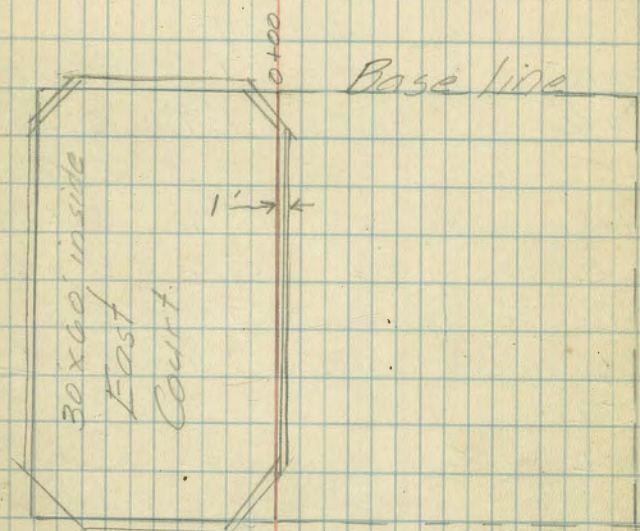
0+11.

70R		5.1	267.1
60R		4.8	267.4
30R		4.5	267.7
BL		4.9	267.3
10L		4.8	267.4

0+16

10L		5.2	267.0
3L		5.4	266.8
3L		6.2	265.8
BL		6.6	265.6
30R		6.8	265.4

A
 N



0+16

50R	6.6	265.6
60R	5.9	266.3
70R	5.7	266.5

0+30

70R	6.8	265.4
64R	5.7	266.5
60R	7.0	265.2
30R	7.1	265.1
6R	7.4	264.8
B.L.	7.1	265.1
1L	7.0	265.2
1.5L	5.8	266.4
10L	5.4	266.8

0+50

10L	6.1	266.1
13L	6.6	265.6
1L	7.0	265.2
B.L.	7.1	265.1
30R	7.2	265.0
49R	7.4	264.8
52R	6.9	265.3
60R	7.5	264.7
65R	6.0	266.2
70R	7.6	264.6

0+70

70R	7.5	264.7
60R	7.2	265.0
54R	6.6	265.6
48R	7.6	264.6
44R	6.1	266.1
37R	7.7	264.5
8R	7.4	264.8
B.L.	7.1	265.1
3L	6.8	265.4
10L	7.0	265.2

0+76

10L	7.2	265.0
1L	6.9	265.3
B.L.	7.3	264.9
16R	7.0	265.2
37R	7.5	264.7
50R	7.7	264.5
54R	6.9	265.3
60R	7.6	264.6
70R	7.7	264.5

0+80

70R	7.7	264.5
60R	7.4	264.8
56R	6.9	265.3
53R	7.9	264.3
48R	6.9	265.3
41R	7.1	265.1
38R	6.6	265.6
18R	6.9	265.3
8R	7.3	264.9
B.L.	7.0	265.2
5L	7.4	264.8
10L	7.9	264.3

0+90

10L	10.3	261.9
8L	8.3	263.9
B.L.	7.8	264.4
16R	7.3	264.9
25R	8.2	264.0
37R	8.5	263.7
60R	8.4	263.8
70R	8.6	263.6

Moore
7-8-35

Xsec of Girard St 10' curbs
Rear to Center
100' wide 17 1/2'
To 7+00 then
10' curb on west
To Center St.

indexed
C.S.K.

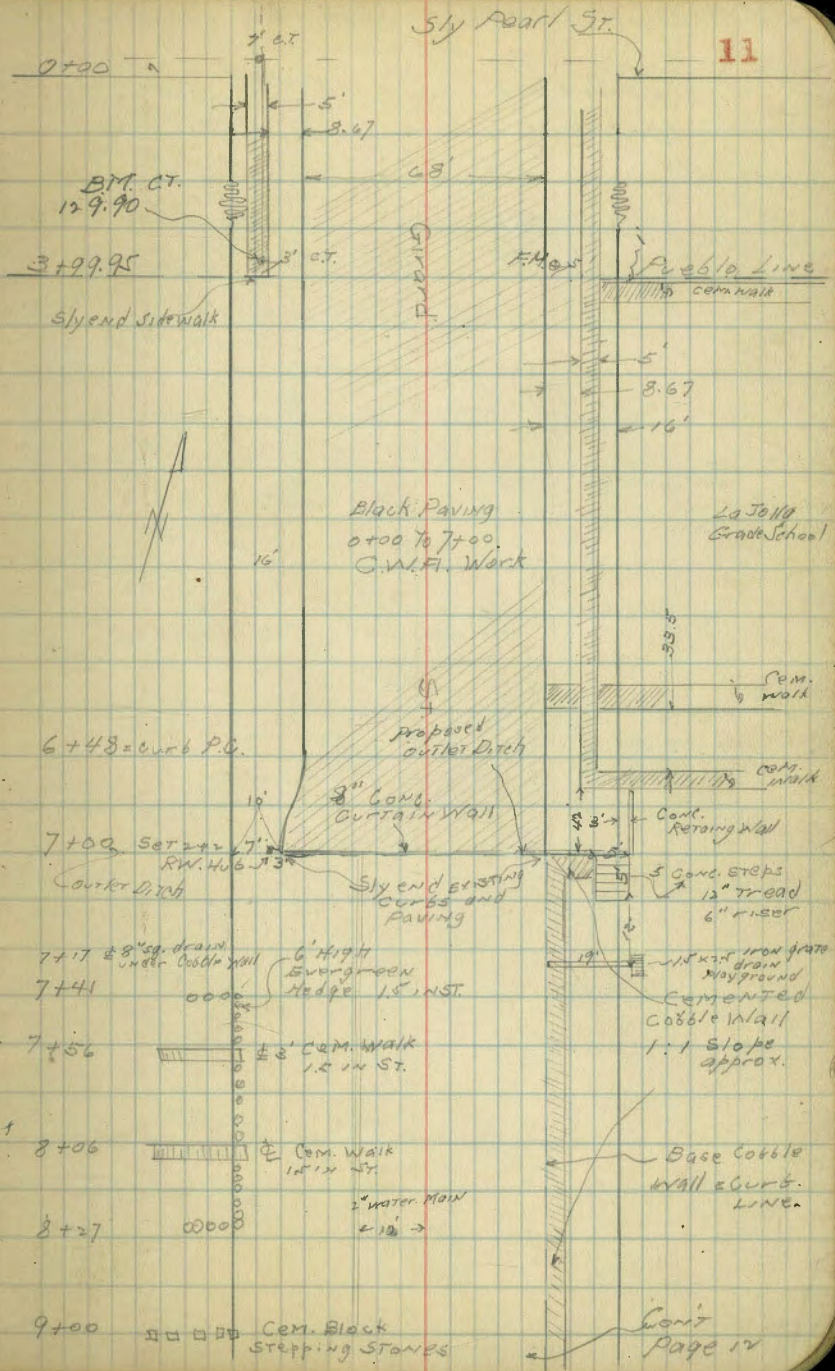
SW BP Rined Girard	128	105.25	103.97
T.P.	1299	107.94	103.0
T.P.	130x	120.81	0.17
SW J.C.			774.20

Sly Pearl = 00

Web		6.77	114.04
gut pav		7.22	113.59
1/4 "		6.71	114.10
C "		6.23	114.58
1/4 "		6.26	114.55
gut "		6.46	114.35
Ect		5.74	115.07
1+00			
Fcb		2.05	118.76
gut pav		2.78	118.03
1/4 "		2.80	118.01
C "		2.86	117.95
1/4 "		3.14	117.67
gut "		3.59	116.22
Web		2.80	118.01
T.P.			
	1224	132.57	0.48
	2+00		120.33
Web			
		10.53	122.04

CONT'D p 13

5 water meters
to be taken care of.
Lafayette Ave. Den
North
Box



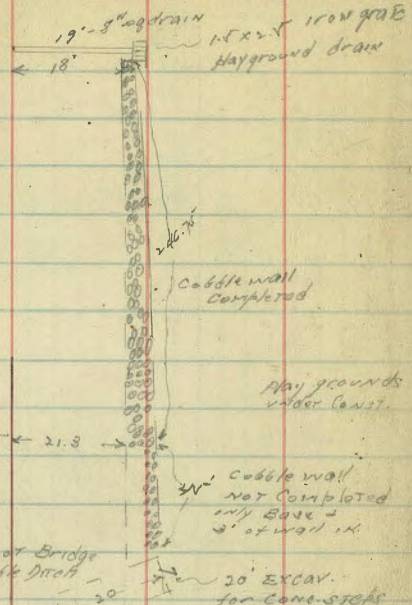
Location of Cobble Wall on School Playground

+ Foot Bridge over Storm Ditch

7+17 = grating + drain

7+18.25 = nly completed wall on school prop.

S.E.A. Project #38-811-386
School Ground Improv.

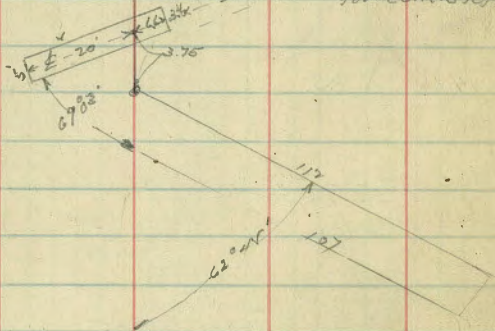


dry Cobble slope wall on school prop.

Ely curb

1 span wooden foot bridge over Cobble Ditch

10+27 = A wall & Ely curb



9+00 from papell

Ely curb line

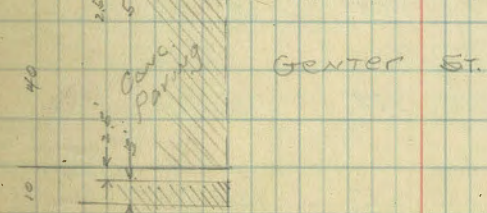
School Play grounds under construction

10+27.0 = A of curb line and Ely Barr of Slope Cobble wall

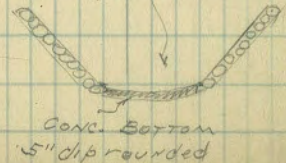
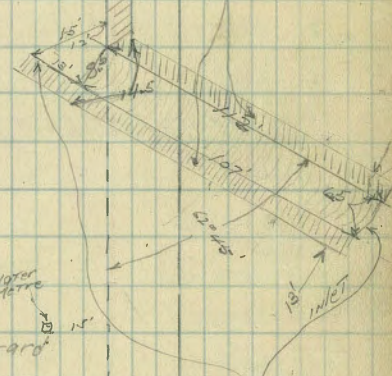
10+53 = 3' Brick walk

10+7460 = NLY GENTER ST.

7' CT. WL Girard



GENTER ST.



CONC. BOTTOM 5" dip rounded

1400

132.57

W	quT	par	11.23	121.34
1/4	"	"	10.94	121.63
C	"	"	10.65	121.92
1/4	"	"	10.65	121.92
quT	"	"	10.70	121.87
E ob	"	"	10.00	122.55

3+00

E ob	"	"	6.36	126.21
quT	par	"	7.15	125.42
1/4	"	"	6.95	125.62
C	"	"	6.88	125.69
1/4	"	"	7.02	125.55
quT	"	"	7.31	125.26
W ob	"	"	6.55	126.02

3 + 99.94 = pseudo line

W ob	"	"	2.63	129.94
quT	par	"	3.04	129.13
1/4	"	"	3.10	129.47
C	"	"	2.99	129.58
1/4	"	"	3.08	129.49
quT	"	"	3.40	129.17
E ob	"	"	2.59	129.98

Set BM.
3' of W7

2.67 129.90

Girard
3' of PL.
on W7 line

T.P. 13.17 145.36 0.38 132.19

145.36

√700

13

E ob	"	"	11.26	134.10
quT	par	"	12.07	133.29
1/4	"	"	11.81	133.55
C	"	"	11.65	133.71
1/4	"	"	11.74	133.62
quT	"	"	12.06	133.30
W ob	"	"	11.25	134.11

6+00

W ob	"	"	7.13	138.23
quT	par	"	7.83	137.53
1/4	"	"	7.62	137.74
C	"	"	7.45	137.91
1/4	"	"	7.50	137.86
quT	"	"	7.74	137.62
E ob	"	"	6.97	138.39

6+48

E ob	"	"	4.98	140.38
quT	par	"	5.71	139.65
1/4	"	"	5.56	139.80
C	"	"	5.42	139.94
1/4	"	"	5.57	139.85
quT	"	"	5.88	139.48
W ob	"	"	5.04	140.32

WL	7+00 end paving	2.9	142.46
W ob	end = WL + 10	2.83	142.53
quT	par	3.57	141.79

7+00

WCB +6	part of Top	CURTAIN Well	3.57	141.79
1/4	"		3.64	141.72
C	"		3.76	141.80
1/4	"		3.79	141.77
gut	"		3.72	141.61
E of end			2.92	142.44
EL			2.6	142.76

T.P. 836 153.39 0.33 145.03

7+05

EL Top	CONC Steps		7.94	145.45
+2	ELY Cobble Top		7.7	145.69
+2V	WLY " "		7.9	145.49
E of	borrow coldwater		11.2	142.19

7+17 3' E of EL ^{Top stone} growing 8.12 145.27

7+50

EL -4	bottom well		8.7	144.7
-3	top "		6.6	146.8
EL			6.3	147.1
+12	" "		6.5	146.9
E of	Bot		10.9	142.5
1/4			10.6	142.8
C			10.8	142.6
+10			9.2	144.2
1/4			9.2	144.2
C			8.6	144.8

CB +6		8.6	144.8
WL		8.2	145.0
7+56			
W Top	CONC walk	8.01	145.38
7+7			
W		7.3	146.1
+10	= NEW CT LINE	7.4	146.0
CB		7.2	146.2
+10		7.5	145.9
1/4		9.0	144.4
+4		9.9	143.5
C		9.8	143.6
1/4		10.5	142.9
CB	bot wall	10.6	142.8
+5	Top "	6.0	147.4
EL		5.7	147.7
+3	Top "	6.0	147.4
+4	Bot "	5.1	145.3
8+00			
E -5	bot wall	7.9	145.5
-3	Top "	5.3	148.1
EL		5.0	148.4
+11	" "	5.2	148.2
CB	Bot "	9.8	143.6
1/4		9.6	143.8
C		9.8	143.6

w 1/4		9.5	143.9
+10		6.7	146.7
cb		6.7	146.7
+6	New cb line	6.4	147.0
w		6.7	146.7
8+25			
w		5.5	147.9
+10	New cb line	5.7	147.7
cb		6.0	147.4
1/4		8.8	144.6
+9		8.5	144.9
+10	old creek bot	10.4	143.0
+15	" " "	10.7	142.7
C		8.0	145.4
1/4		8.3	145.1
cb	bot wall	9.4	144.2
+5	Top "	4.4	149.0
E.L.		4.2	149.2
+3	" "	4.6	148.8
+6	Bot "	8.4	145.2
8+50			
E-7	bot wall	7.8	145.6
-3	Top "	3.7	149.7
E.L.		3.4	150.0
+11	" "	3.6	149.8
cb	Bot "	8.0	145.4

cb +5		7.2	146.2
+10		8.8	144.6
1/4		7.7	145.7
+13		7.1	146.3
C		9.7	143.7
+5	old creek	10.0	143.4
+6		7.8	145.6
1/4		7.2	146.2
+10		6.4	147.0
cb		5.0	148.4
+6	new cb line	4.8	148.6
w		4.5	148.9
T.P.	6.90 156.30	3.99	149.40
8+75			
w		5.9	150.4
+10	new cb line	6.3	150.0
cb		6.0	150.3
+10		7.2	149.1
1/4		8.7	147.6
C		9.3	147.0
+15		10.0	146.3
1/4	old creek	11.5	144.8
+4		11.4	144.9
+9		9.3	147.0

15630

cb bot wall	10.0	146.3
+5 Top "	5.7	150.6
EL	5.6	150.7
+3 " "	5.9	150.4
+8 bot "	10.2	145.9
9+00		
R-8 bot wall	10.1	146.2
-3 Top "	4.9	151.4
EL	4.7	151.6
+11 " "	4.9	151.4
cb bot "	8.9	147.4
+6	8.2	148.1
+11	10.4	145.9
1/4 old creek	10.9	145.4
+4 " "	10.9	145.4
+5	8.5	147.8
C	8.6	147.7
+7	7.6	148.7
1/4	4.7	151.6
cb	4.6	151.7
+6 New ob line	4.8	151.5
W	2.7	151.6
9+25		
W	3.4	152.8
+10 New ob line	3.4	152.9
cb	3.1	153.2

15630

16

1/4	4.0	152.3
+12	8.5	147.8
C	9.0	147.3
+12 old creek	10.3	146.0
1/4	7.5	148.8
+15	6.7	149.6
cb bot wall	8.1	148.2
+5 Top "	4.2	152.1
EL	3.8	152.5
+3 " "	4.4	152.1
+9 bot "	10.5	145.8
9+50		
EL -10 bot wall	10.4	145.9
-4 Top "	3.4	152.9
EL	3.2	153.1
+11 " "	3.6	152.7
cb bot "	7.8	148.5
+2	6.3	150.0
1/4	6.4	149.9
+5	6.7	149.6
+8 old creek	9.5	146.8
C	9.0	147.3
+10	7.8	148.5
1/4	4.6	151.7
+5	2.6	153.7
cb old ob line	2.5	153.8

156.30

CB + 10 = new cb line	2.5	153.8
W	2.3	154.0
TP	6.84	160.10
	3.02	153.28
9.75		
W	5.7	154.9
+10 new cb line	5.5	154.6
cb old "	5.8	154.3
+6	6.0	154.1
1/4	10.6	149.5
+7	12.9	147.2
+12	12.3	147.8
C	8.4	151.7
1/4	9.1	151.0
+16	8.0	152.1
cb bot wall	10.4	149.7
+5 Top "	6.5	153.6
EL	5.4	154.9
+4 Top wall not finished	7.1	153.0
+12 bot wall	14.2	145.9
10+00		
EL - 12 bot wall	14.1	146.0
-5	6.6	153.5
EL	4.6	155.5
+11 Top wall	5.8	154.3

160.10

17

cb bot wall	9.5	150.6
+1	7.2	152.9
+10	7.3	152.8
1/4	8.3	151.8
+10	12.1	148.0
C	8.4	151.7
+10	7.4	152.7
1/4	5.4	154.7
+5	3.8	156.3
cb	4.3	155.8
+6 New cb line	4.8	155.3
W	4.8	155.3
10+27 = 8' in deep wall		
W	3.1	157.0
+10 new cb line	3.1	157.0
cb	3.0	157.1
+14	2.7	157.4
1/4	3.9	156.2
+5	6.5	153.6
C	7.0	153.1
1/4 Top Wly wall	5.6	154.5
+5 bot " "	9.8	150.3
cb = A bot wall	9.7	150.4
+5 Top "	5.4	154.7
E	4.7	155.4
+7	4.7	155.4

10+57

160.10

Levels on foot bridge + Excav. for steps
To playground

18

E +14 bot wall playground 12.8 147.3

10+52

E -27 wall not finished 12.0 148.1

-18 4.4 155.9

E L Top wall 48 155.3

+4 bot " 9.1 151.0

+12 " " wly side 9.1 151.0

cb Top " " 4.9 155.2

1/4 4.8 155.3

C 3.0 157.1

1/4 1.8 158.3

cb 1.8 158.3

+6 New cb line 1.8 158.3

W 7.2 157.9

T.P. 7.0 165.03 2.7 157.93

10+74.60 = Nly Center

W 6.3 158.7

+10 New cb line 6.5 158.5

cb 6.1 158.9

1/4 5.5 159.5

C 5.4 159.6

1/4 5.4 159.6

cb 7.3 157.7

160.10

00 = Wly end bridge deck 5.3 155.07

+26.6 Ely " " 5.6 154.94

+30 Top dirt excav. = 7' wide 5.2 154.90

+50 bot " " " 12.4 146.90

165.03

→ 10+74.60 Nly Center

cb +11 Top Wly wall 9.2 155.8

E bot ditch 13.5 151.5

+8 " " 13.5 151.5

+13 Top wall 9.0 156.0

Ncb Center -

E -15 bot ditch on Ely 13.4 151.6

-7 " " " Wly 13.4 151.6

-2 Top wall " 8.9 156.1

E 8.4 156.6

cb 6.7 158.3

1/4 5.0 160.0

C 5.3 159.7

1/4 5.6 159.4

cb 6.1 158.9

+6 New cb line 6.4 158.5

W gut pav. 4.97 158.06

W Top cb 6.28 New check page 19

165.03

Sly Center			
W	box	6.07	158.96
+10	new cb line	6.0	159.0
cb		5.8	159.2
1/4		5.0	160.0
c		4.7	160.3
1/4		4.1	160.9
cb		5.1	159.9
E		6.3	158.7
+12	Top w/ly wall ditch	8.3	156.7

Sly cb Center

E		4.6	160.4
cb		3.0	162.0
1/4		3.4	161.6
c		4.0	161.0
1/4		4.5	160.5
cb		5.25	159.5
+6	new cb line	5.7	159.3
W	gut pav.	5.93	159.10
ul	Top cb	5.30	159.73

Sly Center

W		5.4	159.6
+10		5.4	159.6
cb		5.3	159.7
1/4		4.4	160.6
C		3.8	161.2

Sly Center

165.03

19

1/4	3.2	161.8
cb	2.4	162.6
E	2.2	162.8

E ditch or cem bot. 1/4 let 12.50

E " opposite B cem. bot. 14.82

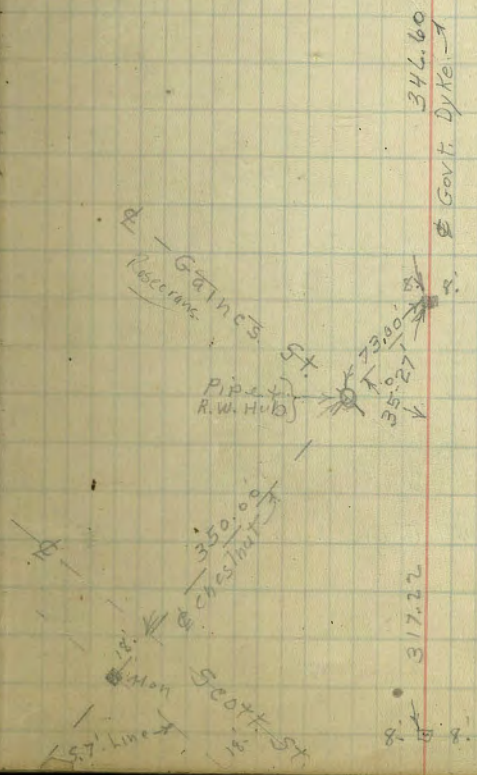
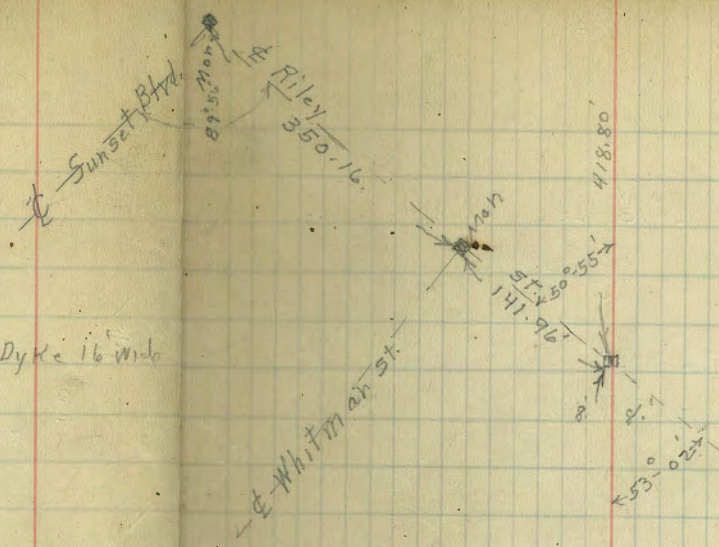
check levels

	12.06	118.38		106.84	office B.M.
TP	13.14	131.16	0.36	118.04	SWSP
T.P.	12.00	142.59	0.7	130.59	Draper
T.P.	12.98	155.32	0.25	142.34	Center
T.P.	9.66	164.63	0.35	154.97	
Top cb NW	Center		5.89	158.74	158.75
	ward				error 0.01
Set B.M. B.P.	new Cor curb		5.88	158.75	
	Center & ward				

11+80²⁰ Hub. of Riley St. \angle 2°-07' Lt. Dyke 16 wide

8+33⁶⁰ Hub. of Chestnut St. \angle 1°-27' Lt. Dyke 16 wide

5+16³⁸ Hub \angle 2°-10' Lt. Dyke 16 wide

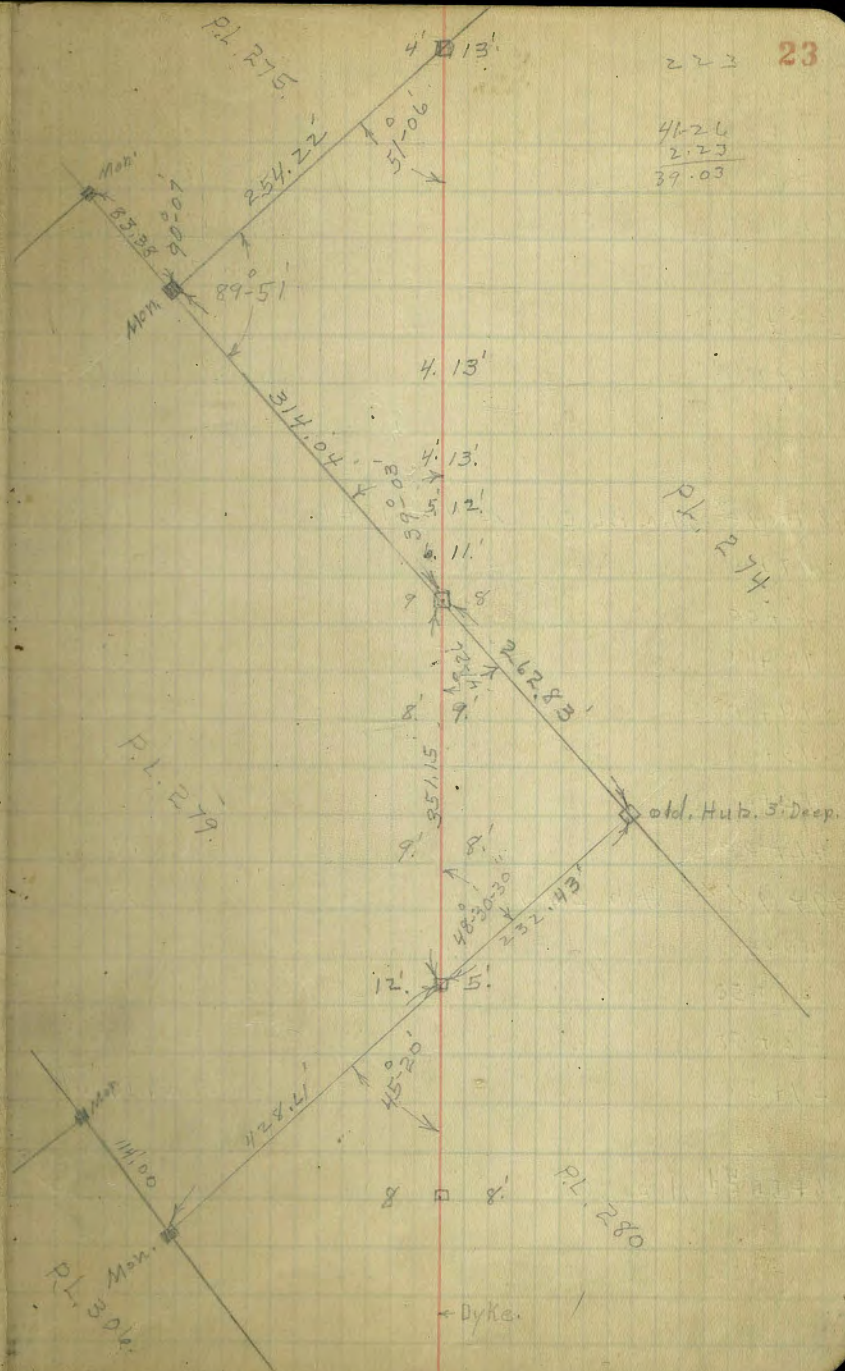


36+55.54 Hub. P.O.T.

Dyke 17' wide

223 23

41.26
2.23
39.03



36+50 " 17 "

35+50 " 17 "

34+50 " 17 "

33+50 " 17 "

32+5) ²⁶ Hub. $\angle 2^{\circ} 23' Lt.$ Dyke 17' wide

31+00 Dyke 17' wide

30+00 Dyke 17' wide

29+00 ⁸¹ Hub. $\angle 3^{\circ} 10' - 30' Lt.$ Dyke 17' wide

(N.B. from 27+65 Dyke on Curve to Lt.)

27+65 ⁴⁰ Hub. P.O.T. Dyke 16' wide

57+00
 56+00
 55+00
 54+00
 53+00
 52+00
 51+00
 50+00
 49+00

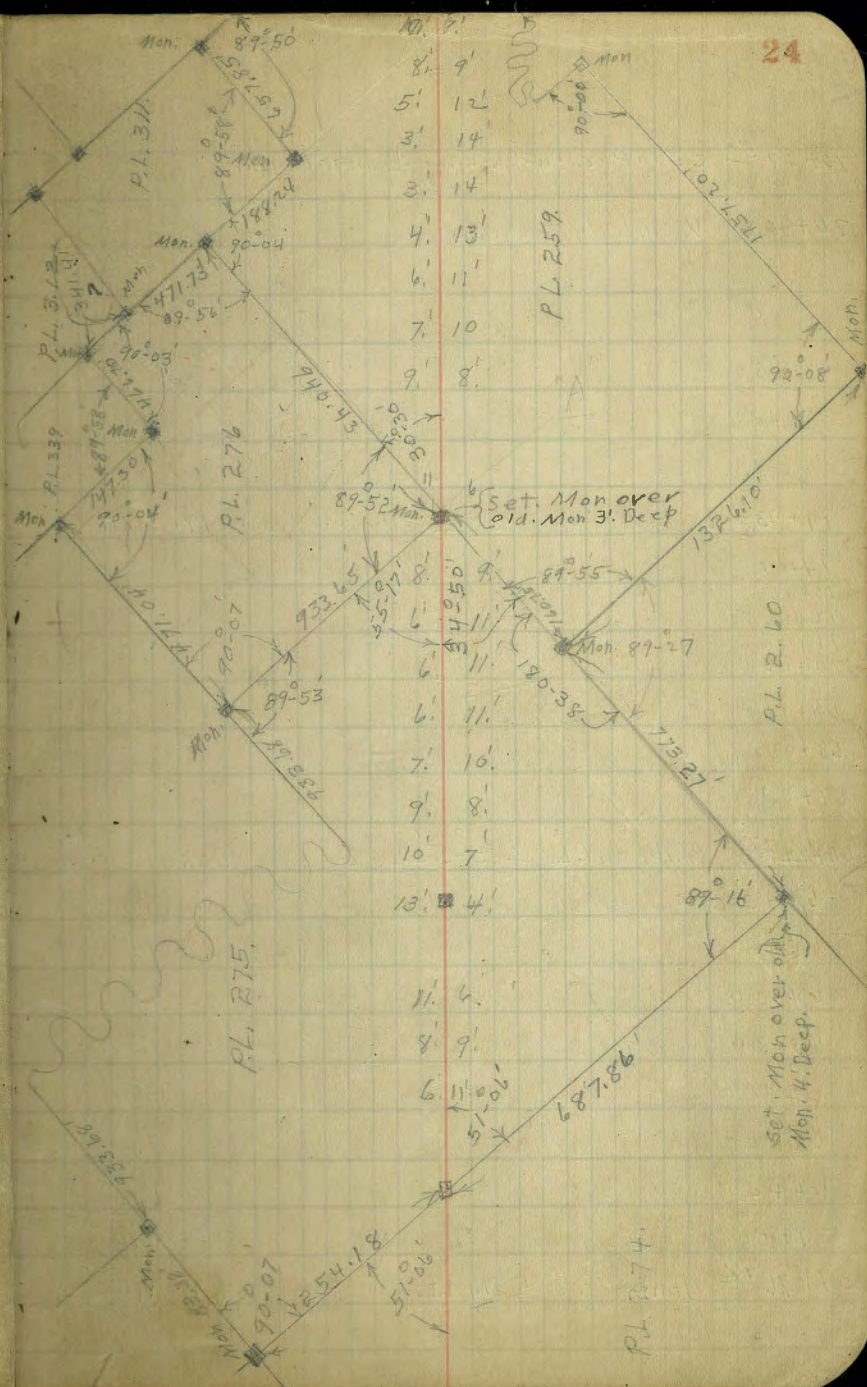
48+09⁸² Mon. P.L. Cor. $\angle 4-21$ Lt. 11' Lt. 6' Rt.

47+00 Dyke 17' wide
 46+00 " 17'
 45+00 " 17'
 44+00 " 17'
 43+00 " 17'
 42+00 " 17'
 41+00 " 17'

39+98²² Hub. $\angle 4-10$ Lt. 17'

39+50 " 17'
 38+50 " 17'
 37+50 Dyke 17' wide

36+55⁵⁴ Hub. P.O.T.



9-12-35 Location Improvements bet Curb.
Miller Walker Bliss
W. Walk. on Imperial Ave. 28th to 32nd Sts

N. Side Imperial Ave.

3+25 to 3+29 cmt. walk.
3+04 to 3+12 cmt. Drive.
2+81 to 2+86 cmt. walk.
2+77 Meter Box.
2+73 Trolley Guy Pole
2+53 to 2+63 cmt. Drive
2+38 to 2+42 cmt. walk
2+34 Meter Box
2+13, B. Acacia 8" Diam
1+91 to 1+95 cmt. walk.
1+81 Meter Box.
1+64 B. Acacia 5" Diam.
1+61 Trolley Guy Pole
1+59 Meter Box
1+43 to 1+55 cmt. Drive
1+21 B. Acacia 12" Diam
1+12 to 1+17 cmt. walk
1+09 Meter Box
0+74 to 0+79 cmt. walk.
0+68 Meter Box
0+64 B. Acacia 10" Diam
0+50 to 0+58 cmt. Drive
0+48 Trolley Wire Guy Pole
0+35 Meter Box
0+00 E. Line 28th St.

Indexed
C.S.K.

26

S. Side Imperial Ave.

2+22 Meter Box
2+15 B. Acacia 12" Diam
1+91 Hibiscus 3' Tall
1+81 Meter Box
1+76 to 1+80 cmt. walk
1+68 B. Acacia 12" Diam at base
1+66 Elec Power Pole
1+54 Hibiscus 3' High.
1+47 Bushy Tree 2" Diam at base 7' High
1+35 Hibiscus 2.5' High.
1+27 to 1+31 cmt. walk
1+23 Hibiscus 4' High.
1+15 B. Acacia 14" Diam
0+98 to 1+02 cmt. walk.
0+97 Meter Box
0+93 Silver Pine 2.5' High
0+83 " " 2.5' High
0+65 B. Acacia 4" Diam
0+59 Meter Box
0+50 to 0+55 cmt. walk
0+40 Elec Power Pole
0+35 Meter Box.
0+21 to 0+25 cmt. walk
0+15 B. Acacia 6" Diam at Base.
0+03 Fire Hydr.
0+00 = E. Line 28th St.

N. Side Imperial Ave.

- 0+91 B. Acacia 7" Diam
 0+60 To 0+75 cmt. Walk & Drive
 0+60 Meter Box
 0+54 B. Acacia 12" Diam.
 0+48 Trolley Guy Pole
 0+43 B. Acacia 6" Diam
 0+33 B. Acacia 4" Diam.
 0+23 To 0+27 cmt. Walk
 0+22 Meter Box
 0+19 B. Acacia 12" Diam.
 0+00 = E. Line 29th St.

 4+89 = W. Line 29th St. 60' wide.
 4+86 Trolley Guy Pole
 4+66 Meter Box
 4+37 To 4+89 cmt. walk
 4+30 To 4+37 cmt. Drive
 4+21 B. Acacia 7" Diam.
 4+06 to 4+10 cmt. walk
 4+00 Meter Box
 3+82 Trolley Guy Pole
 3+73 To 3+77 cmt. walk
 3+66 Meter Box
 3+60 B. Acacia 12" Diam.
 3+43 to 3+51 cmt. Drive
 3+38 Meter Box

S. Side Imperial

27

- 0+83 to 0+91 cmt. Drive
 0+79 Meter Box
 0+50 Elec. Power Pole
 0+37 to 0+48 Dirt. Driveway
 0+32 Meter Box
 0+24 to 0+28 cmt. walk.
 0+20 B. Acacia Tree 9" Diam
 0+02 Five Hydt. Poles
 0+00 = E. Line 29th St.
 4+86 Elec Power Pole
 4+89 = W. Line 29th St. 60' wide
 4+65 to 4+89 = cmt. walk
 4+64 Meter Box
 4+20 B. Acacia 6" Diam
 4+11 to 4+17 cmt. walk
 4+08 Meter Box
 3+90 to 3+98 cmt. Drive
 3+87 Elec Power Pole
 3+69 to 3+76 cmt. Drive
 3+65 Meter Box
 3+61 B. Acacia 14" Diam
 3+55 to 3+58 cmt. walk
 3+15 B. Acacia 4" Diam
 2+89 Elec Power Pole
 2+65 B. Acacia 10" Diam
 2+24 to 2+27 cmt. walk.

N. Side Imperial Ave

- 4+66 Meter Box.
 4+51 Pepper Tree 10" Diam.
 4+30 Pepper Tree 16" Diam.
 4+09 Pepper Tree 12" Diam.
 4+01 B. Acacia 8" Diam.
 3+99 Trolley Guy Pole
 3+86 Tree 2" Diam 5' High
 3+61 Tree 2" Diam 7' High
 3+38 Hibiscus 2' High.
 3+35 Meter Box
 3+28 B. Acacia 6" Diam
 3+22 to 3+25 cmt. walk.
 3+13 Hibiscus 2' High.
 2+79 Trolley Guy Pole
 2+74 Meter Box
 2+68 to 2+73 cmt. walk.
 2+52 Gas Service
 2+06 Meter Box
 1+99 B. Acacia 12" Diam
 1+75 Trolley Guy Pole.
 1+51 B. Acacia 10" Diam.
 1+45 to 1+48 cmt. walk.
 1+36 Meter Box.
 1+12 to 1+24 cmt. Drive
 0+98 to 1+02 cmt. Walk.
 0+96 Meter Box

S. Side Imperial Ave

28

- 4+10 Elec Power Pole
 4+07 Large Pepper Tree 24" Diam
 3+95 to 3+98 cmt. walk
 3+84 Meter Box
 3+70 to 3+75 cmt. walk
 3+49 B. Acacia 7" Diam
 3+35 to 3+38 cmt. walk
 3+33 Meter Box
 3+02 Elec Power Pole
 2+87 Dead B. Acacia 12" Diam
 2+72 to 2+76 cmt. walk
 2+71 Meter Box
 2+49 B. Acacia 12" Diam
 2+36 to 2+40 cmt. walk.
 2+34 Meter Box
 1+95 B. Acacia 14" Diam.
 1+87 Meter Box.
 1+83 to 1+87 cmt. walk.
 1+74 B. Acacia 8" Diam
 1+62 Elec Power Pole
 1+58 B. Acacia 10" Diam
 1+50 Meter Box
 1+44 to 1+50 cmt. walk
 1+36 B. Acacia 12" Diam
 0+94 to 1+24 lawn sprinkler system.
 0+94 Meter Box

N. side Imperial Ave

- 1+53 Meter Box
 1+51 Trolley Pole
 1+28 B. Acacia 10" Diam.
 1+13 Meter Box
 0+95 Meter Box
 0+49 Trolley Pole
 0+00 to 2+00 solid cmt. walk
 0+00 = E. line 30th St.
 7+24⁵ = W. line 30th St 60' wide
 7+22 Trolley Pole
 6+56 Gasoline Pump
 6+52 Meter Box
 6+25 to 6+33 stand pipes to Gasoline Tank.
 6+18 to 7+24⁵ solid cmt. walk.
 6+09 Trolley Pole
 5+96 Meter Box
 5+63 to 5+74 cmt. Drive
 5+46 Meter Box,
 5+36 to 5+40 cmt. walk
 5+31 Pepper Tree 24" Diam.
 5+18 Pepper Tree 24" Diam.
 5+05 Pepper Tree 24" Diam.
 4+98 Trolley Guy Pole
 4+82 Pepper Tree 12" Diam.
 4+73 to 4+77 cmt. walk.

S. side Imperial Ave

29

- 0+20 to 0+50 cmt. Drive
 0+13-0+15+0+18' Stand Pipes to Gasoline Tank
 0+10 Flag Pole
 0+03 Fire Hydt.
 0+00 = E. line 30th St
 7+24⁵ = W. line 30th St. 60' wide
 7+23 Elec Power Pole
 6+74 to 7+24⁵ cmt. walk.
 6+50 Meter Box
 6+22 Meter Box
 6+10 Elec Power Pole
 5+79 Cocos Palm 14" Diam.
 5+62 to 6+04 cmt. walk
 5+49 B. Acacia badly out of Plumb.
 5+15 to 5+25 cmt. Drive
 5+02 Elec Power Pole
 4+99 Eucalyptus 24" Diam
 4+88 Meter Box
 4+83 Eucalyptus 26" Diam
 4+66 Eucalyptus 20" Diam
 4+62 to 4+66 cmt. walk
 4+50 Eucalyptus 24" Diam
 4+35 Meter Box
 4+30 large Pepper Tree 24" Diam.
 4+17 to 4+20 cmt. walk

N. Side Imperial Ave

- 5+15 Cocos Palm 12" Diam.
 5+03 to 5+12 cmt. Drive
 4+91 Meter Box
 4+87 Trolley Pole
 4+79 to 4+83. cmt. walk
 4+75 B. Acacia 10" Diam.
 4+50 to 4+61 cmt. Drive
 4+49 Oleander bush 2' High
 4+27 to 4+31 cmt. walk.
 4+25 B. Acacia 8" Diam.
 4+18 Meter Box
 4+13 oleander bush 2.5' High.
 4+00 to 4+12 cmt. drive
 3+80 Trolley Pole.
 3+74 B. Acacia 10" Diam.
 3+53 Meter Box.
 3+45 Fig Tree 8" Diam.
 3+27 to 3+72 solid cmt. walk.
 3+25 B. Acacia 14" Diam.
 3+12 Meter Box.
 2+75 B. Acacia 12" Diam.
 2+72 Meter Box
 2+62 to 2+66 cmt. walk.
 2+50 Trolley Pole
 2+25 B. Acacia 6" Diam.
 2+01 Meter Box

S. Side Imperial Ave.

30

- 5+21 to 5+24 cmt. walk
 5+00 Elec Power Pole
 4+75 B. Acacia 6" Diam.
 4+36 Date Palm 1' High
 4+25 B. Acacia 6" Diam.
 3+77 Elec Power Pole
 3+75 B. Acacia 6" Diam.
 3+51 Meter Box
 3+29 B. Acacia 7" Diam.
²⁺⁹⁰
 2+75 to ^{Meter Box} 3+74 cmt. walk solid
 2+74 Elec Power Pole
 2+51 Gas. Service
 2+24 B. Acacia 12" Diam.
 1+94 to 2+07 cmt. Drive
 1+81 Meter Box
 1+72 B. Acacia 10" Diam.
 1+54 Elec Power Pole
 1+35 to 1+39 cmt. walk
 1+27 Meter Box
 1+22 B. Acacia 16" Diam.
 1+01 to 1+12 cmt. Drive
 0+93 Date Palm 24" Diam.
 0+83 to 0+87 cmt. walk
 0+78 Meter Box
 0+67 Date Palm 24" Diam.
 0+53 Elec Power Pole

N. Side Imperial Ave

- 1748 Meter Box.
 1744 Pepper Tree 18" Diam
 1734 to 1738 cmt. walk.
 1729 Pepper Tree 10" Diam
 1713 Gas Service
 0796 Pepper Tree 24" Diam.
 0781 Meter Box
 0777 Pepper Tree 22" Diam.
 0764 Meter Box
 0756 Pepper Tree 18" Diam.
 0750 Gas Service
 0747 Trolley Pole
 0740 Meter Box
 0735 Pepper Tree 24" Diam leans overwalk
 0700 to 0727 cmt. walk
 0700 = E. Line 31st St.

6700^g = W. Line 31st St. 60' wide

6700 Meter Box
 5798 Trolley Pole

- 5793 Cocos Palm 16" Diam
 5776 to 5784 cmt. walk
 5769 Cocos Palm
 5750 to 5763 cmt. Drive
 5740 Cocos Palm 12" Diam.
 5732 Meter Box
 5726 to 5731 cmt. walk

S. Side Imperial Ave.

31

- 2767 Elec Power Pole
 2745 Meter Box
 2729 B. Acacia 10" Diam
 2723 to 2727 cmt. walk
 1775 B. Acacia 12" Diam
 1761 to 1774 cmt. Drive
 1759 Elec Power Pole
 1734 Meter Box
 1725 B. Acacia 10" Diam
 0775 B. Acacia 8" Diam
 0762 Meter Box
 0744 Elec Power Pole
 0727 to 0759 cmt. Drive
 0726 stand pipe to Gasoline Tank
 0713 Meter Box
 0711 stand pipe to Gasoline Tank
 0701 = Fire Hydrant
 0700 = E. Line 31st St

6700^g = W. Line 31st St 60' Wide

6700 Elec Power Pole

5793 Meter Box

5783 Gas Service

5773 Cocos Palm 14" Diam.

5748 Meter Box

5726 B. Acacia 12" Diam

N. side Imperial Ave

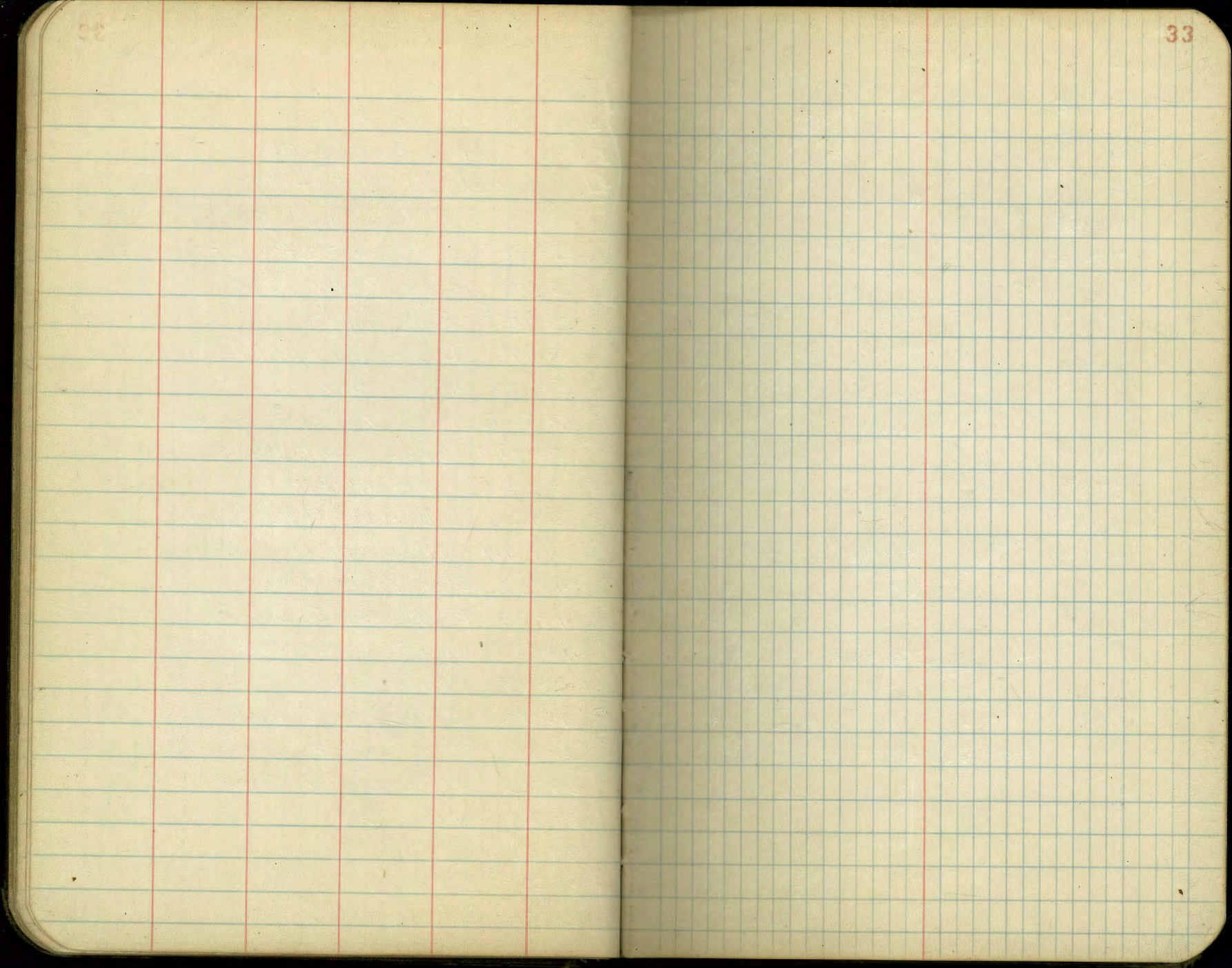
- 5+65 Meter Box
 5+45 Meter Box
 5+35 to 5+40 cmt. walk
 5+25 B. Acacia 4" Diam.
 4+87 Trolley Pole
 4+75 B. Acacia 5" Diam.
 4+54 Meter Box
 4+48 to 4+52 cmt. walk
 4+25 B. Acacia 5" Diam.
 4+16 Meter Box
 3+77 Trolley Pole
 3+72 B. Acacia 5" Diam.
 3+43 to 3+47 cmt. walk
 3+38 Meter Box
 2+78 B. Acacia 8" Diam.
 2+65 Meter Box
 2+59 to 2+63 cmt. walk
 2+49 Trolley Pole
 2+30 Meter Box
 2+25 B. Acacia 8" Diam.
 2+17 to 2+21 cmt. walk
 1+86 to 1+90 cmt. walk.
 1+75 B. Acacia 3" Diam.
 1+68 Meter Box
 1+64 Gas
 1+55 Trolley Pole.

N. side Imperial Ave

32

- 6+00⁴ = W. Line 32nd St.
 5+99 Trolley Pole
 5+79 to 5+86 cmt. walk.
 5+75 B. Acacia 5" Diam.

- S. side Imperial Ave
 6+00⁴ W. Line 32nd St.
 5+99 Elec Power Pole
 5+94⁵ Fire Hydr.
 5+75 B. Acacia 6" Diam.
 5+64 Meter Box
 5+50 to No cmt. side walk
 5+34 to 5+38 cmt. walk.
 5+29 Meter Box
 5+26 B. Acacia 12" Diam.
 4+94 Meter Box
 4+83 Elec Power Pole
 4+75 B. Acacia 5" Diam.
 4+51 to 4+55 cmt. walk.
 4+48 Meter Box
 4+25 B. Acacia 6" Diam.
 3+81 Elec Power Pole
 3+72 B. Acacia 8" Diam.
 3+41 Meter Box
 3+36 " "
 3+25 B. Acacia 3" Diam.
 2+75 B. Acacia 6" Diam.



75' wide
12' cbs
12.75' 1/4s.

X. Sec. Columbia St. Plat Page 34
Market St. South

9.26 35

BM. B.P.	4.35	9.26	4.91
	0+00 =	S. End. curb on E. S. Line Market. S. End. Pav. mt.	S. W. Market + Columbia
3' w. of W. ch. at Bldg	4.30	4.96	
W. emt. ch	4.38	4.88	
gutter Pav	4.94	4.32	
1/4 "	4.42	4.84	
ϕ "	4.04	5.20	
1/4 "	3.80	5.46	
+1' S. Rail of siding = pav.	3.74	5.52	
+9.5' = N. Rail of siding = pav.	3.65	5.61	
+12.6' S. " " Main S.D.A. RR	3.68	5.58	
#12.75 = E. ch. line = pav.	3.68	5.58	
ch + 8.35 = N. Rail Main Line	3.73	5.53	
E' ch + 12 = emt. Ret. + ground.	3.55	5.71	
	0+05.4	South	
E = N. Rail Main Line	3.81	5.45	
ch. on pav	3.71	5.55	
+3.8' S. Rail siding	3.72	5.54	
1/4 "	4.3	4.96	
ϕ "	4.2	5.06	
1/4 "	4.6	4.66	
gutter	5.0	4.26	
ch	4.48	4.78	
+3.	4.26	5.00	

W. ch - 3' - on walk	4.57	4.69
W. ch at N. side Entrance	4.72	4.54
gutter	5.2	4.06
1/4 "	4.6	4.66
ϕ "	4.5	4.76
1/4 "	4.5	4.76
ch	3.5	5.76
+5	3.5	5.76
E. = S. Rail siding	3.80	5.46
	0+33	South
E	3.5	5.76
ch	3.8	5.46
+9	4.7	4.56
1/4 "	4.7	4.36
ϕ "	4.7	4.56
1/4 "	5.0	4.26
gutter	5.5	3.76
ch	5.09	4.17
+3' = S. side Entrance.	5.06	4.20
T. P.	4.50 + 7.83	5.93 3.33
	0+47.3	
W. = S. side Building	5.6	2.23
	0+73.7	
W.	6.0	1.83
+9 Cor. Building	4.9	2.93
+12 Ground	5.0	2.83
S. End. emt. ch	4.55	3.28
Gutter	5.2	2.63

7.83.

0+73^z con.

w d + 6	4.6	3.23
w. 1/4	4.4	3.43
4	4.3	3.53
E. 1/4	4.2	3.63
el.	3.3	4.53
E.	2.15	5.33

0+78

4 Top. Sewer M.H.

1+00

E	3.0	4.83
el	3.5	4.33
1/4	5.0	2.83
4	5.6	2.23
1/4	5.7	2.13
el	6.1	1.73
w.	6.0	1.83

1+08

w	5.9	1.93
el	5.9	1.93
1/4	5.7	2.13
4	5.6	2.23
1/4	5.7	2.13
el	4.7	3.13
E	3.7	4.13

Columbia St 36

7.8.3

Levels on A.T.S.F. Rails.

W. Line Columbia

0+75 ⁵ South = N. Rail siding	5.49	2.34
0+81 ³ " = S. " "	5.52	2.31
0+91 ² " = N. " "	5.68	2.15
0+96 ⁴ " = S. " "	5.64	2.19
1+07 ⁴ " = N. " Main	5.39	2.44
1+13 ³ " = S. " "	5.33	2.50
1+16 ⁴ " = N. " siding	5.30	2.53
1+21 ⁸ " = S. " "	5.25	2.58

4 Columbia

1+01 ² = N. Rail siding	5.57	2.26
1+06 ⁹ = S. " "	5.59	2.24
1+12 ² = N. " "	5.78	2.05
1+17 ⁴ = S. " "	5.60	2.23
1+34 ² = N. " Main line	5.39	2.44
1+37 = N. " siding	5.35	2.48
1+40 = S. " Main line	5.37	2.46
1+42 ⁵ = S. " siding	5.32	2.51

E. Line Columbia

1+25 ² = N. Rail siding	5.43	2.40
1+31 ³ = Frog Pt.	5.39	2.44
1+36 ⁵ = S. Rail siding	5.31	2.52
1+60 ¹ = N. " Main line	5.49	2.34
1+65 ² = S. " " "	5.48	2.35

7.83

1+15

E	6.0	1.8
el	6.1	1.7
¹ / ₄	5.7	2.1
⊕	5.7	2.1
¹ / ₄	5.7	2.1
el	5.9	1.9
W	5.9	1.9

1+50

W	6.1	1.7
el	6.0	1.8
¹ / ₄	5.5	2.3
⊕	5.4	2.4
¹ / ₄	5.7	2.1
el	6.0	1.8
E	5.9	1.9

2+00

E	6.0	1.8
el	5.8	2.0
¹ / ₄	5.8	2.0
⊕	5.5	2.3
¹ / ₄	5.7	2.1
el	5.6	2.2
W	5.8	2.0

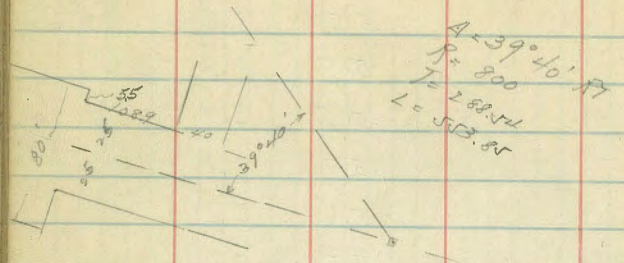
7.83

Columbia St 37

2+32.5 on W. } = W. End. Wooden platform.
 2+47.3 S. 4 E.

E	5.5	2.3
el	5.5	2.3
¹ / ₄	5.5	2.3
⊕	5.7	2.1
¹ / ₄	5.6	2.2
el	5.5	2.3
W	5.8	2.0
Original B.M.	2.92	4.91 = 4.91

8+37.20 E.C.

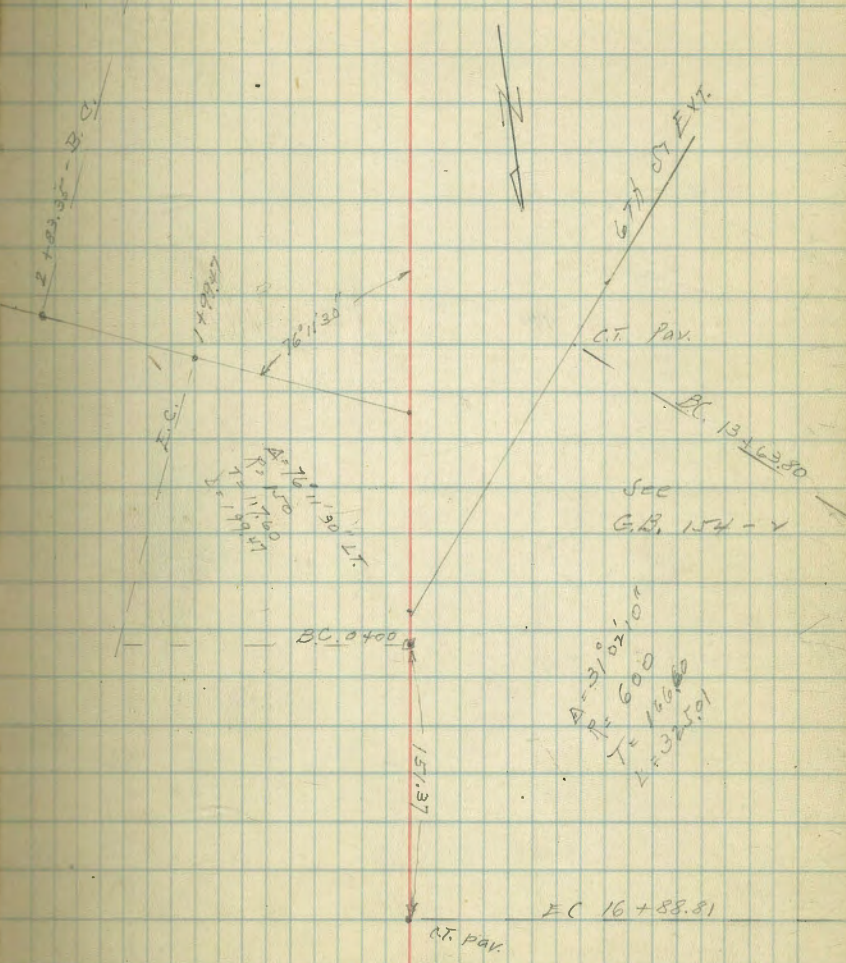


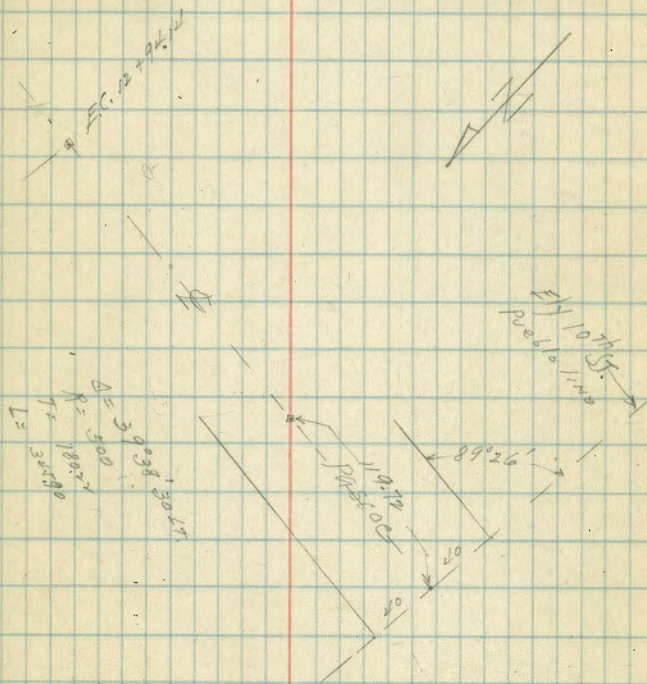
E Lincoln
Thru D.B. Williams Sub

#1 Proposed Road bet 6th + Richmond
via Lincoln + Pascoe Sts
on Nly side of cañon.

Moore
Gibson
Northrup
1-1936

Indexed
c.s. N.



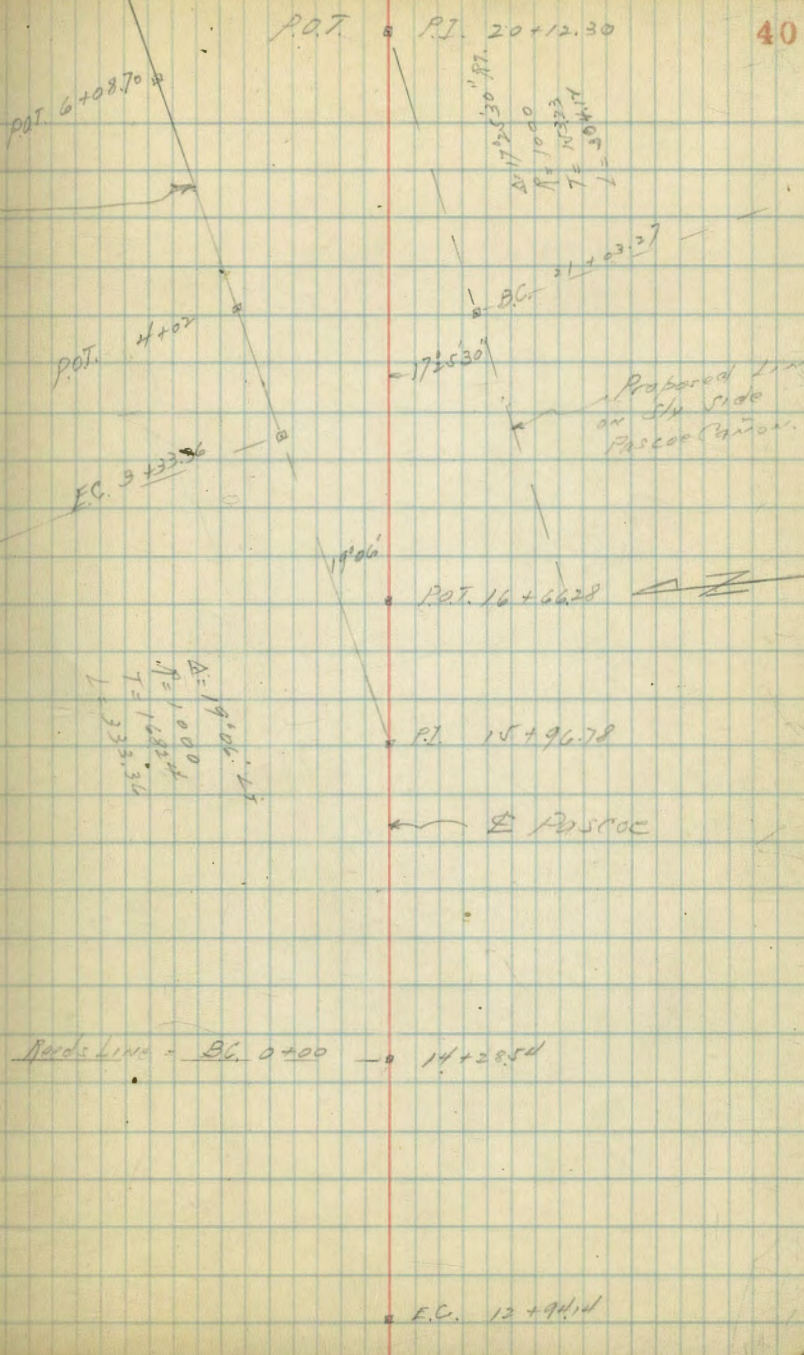


B.C. 9448.24

P.C. 8137.20

Line proposed by Mr Reed

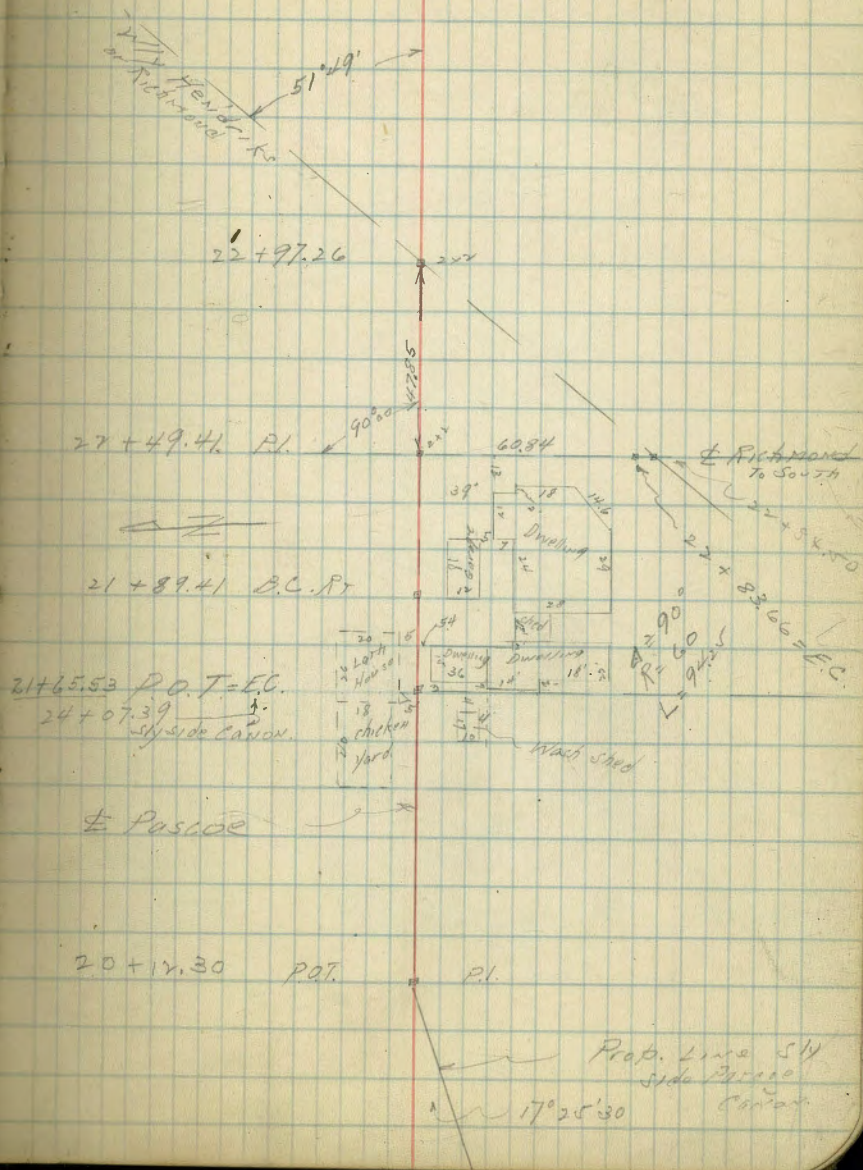
Curve on SW side Pastoc Canyon
PT 10+74
A = 57° 57' 47"
R = 600
T = 382.24
L = 206.84



Reed's Line - B.C. 0+00 - 14+28.54

E.C. 13+94.14

21 + 89.41 B.C. PT
 $\Delta = 90^\circ$ RT
 $R = 60$
 $L = 94.25$



21 + 65.53 P.O.T. = E.C.
 24 + 07.39
 side Canon

± Pascoe

20 + 14.30 POT. P.I.

Prop. Line S/N
 side Pyrene
 Canon
 17° 35' 30"

Line proposed by Mr Reed
from $\frac{0+00}{14+28.54}$ to $11+56.41$
ending at intersection Lincoln + Hendricks
or Fishpond

p 40

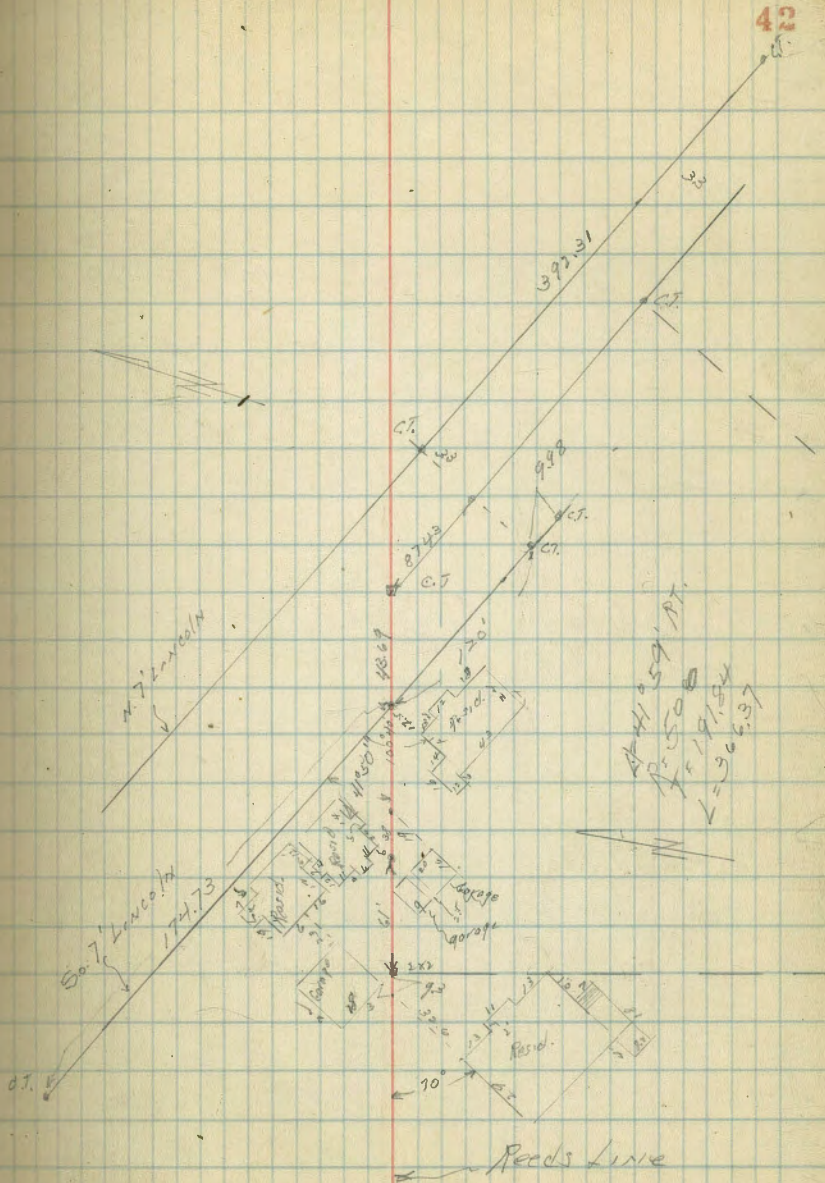
E.C. $11+56.41$ C.T.

P.I. C.T. $\Delta 41^{\circ}59'$ RT

B.L. $7+90.04$ RT

Proposed by Mr Reed p 40

$6+08.70$ P.O.T.



£ Levels Prop. road
 via Pasco + Lincoln
 bet. 67th + Richmond. Hendricks

£

+50

$\frac{189.6}{3.2}$

+25

$\frac{187.1}{1.7}$

0 + 00 Hhd = B.C. 17.

$\frac{186.33}{6.44}$ Hhd

-50

$\frac{183.67}{9.10}$ DAY

-100

$\frac{180.47}{12.30}$ DAY

0 - 157.37 = 16 + 8881 EC. 67th STREET on C. Track BM 177.01

$\frac{177.01}{15.76}$ DAY

T.P.	8.33	192.77	1257	184.44	
T.P.	0.01	197.01	1312	197.00	192.77
T.P.	0.63	210.14	1281	209.49	
T.P.	0.12	222.30	1267	222.18	
BM. COPT. EC.	0.45	234.85		234.40	7 + 86.37
67th ST. INT.					63.154 - 53

+50

$$\frac{160.0}{22.0}$$

+45

$$\frac{155.9}{26.1}$$

+30

Bottom 6th St Canyon 60" C.V.

$$\frac{153.5}{28.5}$$

+17

$$\frac{156.7}{25.3}$$

+100

$$\frac{162.0}{20.0}$$

O.T.P

137

181.95

12.19

180.58

$$\frac{181.95}{3}$$

O + 75

$$\frac{177.2}{21.6}$$

O + 57

$$\frac{189.2}{3.6}$$

192.77

$$\frac{192.77}{3}$$

+50 Bottom Paseo Cañon 60° C. V.

$\frac{154.0}{20.8}$

+25.

$\frac{153.6}{21.2}$

3

$\frac{158.2}{16.6}$

2 + 83.35 = BC RT

$\frac{161.5}{13.3}$

2 + 50

$\frac{169.8}{5.0}$

T.P. 2.44 174.78 901 172.34

$\frac{174.78}{3}$

1 + 99.47 E.C

$\frac{176.8}{5.2}$

1 + 75

$\frac{170.6}{11.4}$

181.95

$\frac{181.95}{3}$

+20 Bot wash from North 24" C.V.

$$\frac{173.3}{11.4}$$

+05

$$\frac{173.3}{11.4}$$

6

$$\frac{175.4}{9.3}$$

+50

$$\frac{174.7}{12.0}$$

T.P. 13.08 184.73 313 171.65

$$\frac{184.73}{3}$$

5

$$\frac{171.0}{3.8}$$

+50

$$\frac{161.1}{13.7}$$

4

$$\frac{156.3}{18.5}$$

174.78

$$\frac{174.78}{3}$$

8 + 37.20 E.C. Hyd.

$\frac{214.18}{5.26}$

T.P. 12.33 219.44 0.41 207.11

$\frac{219.44}{8}$

8 607 Mach from North 72" Culv

$\frac{199.5}{8.0}$

+50

$\frac{205.8}{1.7}$

T.P. 12.38 207.52 0.35 195.14

$\frac{207.52}{8}$

7

$\frac{198.0}{+2.5}$

T.P. 1163 195.49 0.87 183.86

$\frac{195.49}{8}$

6 +50

$\frac{176.4}{8.3}$

184.73

$\frac{184.73}{8}$

+50

$$\frac{250.7}{5.6}$$

+20

$$\frac{248.2}{8.1}$$

/0

$$\frac{251.6}{4.7}$$

9 + 4824 BC LT.

$$\frac{259.1}{+ 2.8}$$

9 + 30

$$\frac{257.3}{+ 1.0}$$

8 + 90

$$\frac{245.8}{10.5}$$

T.P. 13.09 256.30 0.33 243.21

$$\frac{256.30}{}$$

T.P. 17.13 243.54 0.32 231.41

8 + 50

$$\frac{222.6}{9.1}$$

T.P. 12.94 231.73 0.65 218.79

$$\frac{231.73}{}$$

219.44

T.P. 1324 258.34 0.20 245.10

+30

$$\begin{array}{r} 242.3 \\ \underline{3.0} \end{array}$$

17

$$\begin{array}{r} 223.7 \\ \underline{21.6} \end{array}$$

+93 Bot. wash from North 16" Cole.

$$\begin{array}{r} 219.8 \\ \underline{25.5} \end{array}$$

+60

$$\begin{array}{r} 239.8 \\ \underline{5.5} \end{array}$$

// +50

$$\begin{array}{r} 243.6 \\ \underline{1.7} \end{array}$$

T.P. 1.62 245.30 12.62 243.68

245.30

10 + 88

$$\begin{array}{r} 252.7 \\ \underline{3.6} \end{array}$$

256.30

$$\begin{array}{r} 256.30 \\ \underline{\quad} \end{array}$$

T.P. on Rock 097 258.65 1303 257.68

+50

14 +28.5+ BC LT = 0+00 Reed's Line on Hub. E/ = 266.6

14 +00

+50

13 +25

T.P 1271 270.71 034 258.00

12 +94.4 E.C. Hub

17 +50

258.34

263.0
7.7

266.61
4.10

269.6
1.1

256.9
13.8

262.3
8.4

270.71

255.54
280

249.1
22

258.34

16

$$\begin{array}{r} 240.3 \\ \underline{18.4} \end{array}$$

+55

$$\begin{array}{r} 239.9 \\ \underline{18.8} \end{array}$$

+65 Bot. draw from North 16" C.V.
Drainage from Vermont & Lincoln
Highways here

$$\begin{array}{r} 237.7 \\ \underline{21.0} \end{array}$$

+50

$$\begin{array}{r} 245.3 \\ \underline{13.4} \end{array}$$

+43 approx. 20-foot bridge on Vermont St.

+40

$$\begin{array}{r} 248.9 \\ \underline{9.8} \end{array}$$

15

$$\begin{array}{r} 249.6 \\ \underline{9.1} \end{array}$$

14+80

$$\begin{array}{r} 250.1 \\ \underline{8.6} \end{array}$$

258.65

$$\begin{array}{r} 258.65 \\ \underline{2} \end{array}$$

+50

25' LT 6' Lower
= bot. Cañon from NE
 $\frac{244.8}{6.5}$

18 + 25

$\frac{239.8}{11.5}$

+95

bot. Cañon from NE 36° C.M.

$\frac{235.1}{16.4}$

+50

Draw from So. Hills in base
24" C.M.

Also Draw from North
needed 24" C.M.

10' RT 3' Lower
bot. Cañon

T.P

5.48 251.27 12.86 245.79

$\frac{251.27}{}$

17

$\frac{243.2}{15.5}$

+65

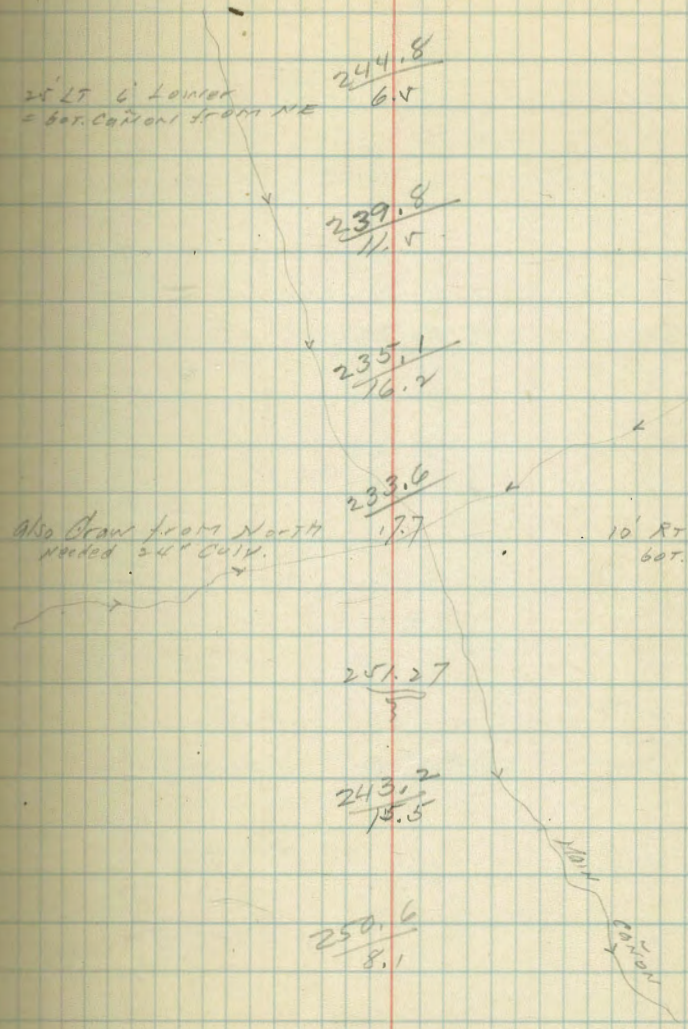
$\frac{250.6}{8.1}$

16 + 50

$\frac{247.7}{11.0}$

258.65

$\frac{258.65}{}$



+75

$$\frac{284.2}{2.3}$$

+50

$$\frac{279.5}{7.0}$$

T.P. 1306 286.54 0.81 273.48

$$\frac{286.54}{8}$$

20

$$\frac{272.1}{2.2}$$

+50

$$\frac{263.4}{10.9}$$

T.P. 1212 274.29 1.24 262.17

$$\frac{274.29}{8}$$

19

$$\frac{256.7}{6.7}$$

18+75

$$\frac{251.7}{11.7}$$

T.P. 1246 263.41 0.37 250.95
251.27

$$\frac{263.41}{8}$$

22 + 83.66 = EC.

+75

+50

22

21 + 89.41 BC. RT

21 + 65.53 ^{pot Hub} = EC. from Line on Sly side Pascoe Cañon

+50

21

TP	10.68	297.07	0.15	286.39
		286.54		

$$\frac{296.3}{0.8}$$

$$\frac{296.1}{1.0}$$

$$\frac{293.3}{3.8}$$

$$\frac{291.9}{5.2}$$

$$\frac{291.5}{5.6}$$

$$\frac{291.72}{5.35}$$

$$\frac{291.9}{5.2}$$

$$\frac{287.9}{9.2}$$

$$\frac{297.07}{8}$$

check to S.M.P.

Pascoe + Hendricks Svt. Cor. db. 304 294.03 293.74

23 + 14.26 Top of Wly Hendricks on E Pascoe

$$\begin{array}{r} 291.65 \\ \underline{5.42} \end{array}$$

$$\begin{array}{r} 291.17 \\ \underline{5.88} = \text{qtr. pay.} \end{array}$$

22 + 97.26 Hub on Wly Hendricks " " "

$$\begin{array}{r} 292.52 \\ \underline{4.55} \end{array}$$

+80

$$\begin{array}{r} 285.5 \\ \underline{11.6} \end{array}$$

22 + 49.41 Pt. on Hub

$$\begin{array}{r} 291.08 \\ \underline{5.99} \end{array}$$

23 + 40 pay. on E Robinson to South

$$\begin{array}{r} 297.1 \\ \underline{0.0} \end{array}$$

23 + 07.50 quarter pay

$$\begin{array}{r} 295.27 \\ \underline{1.80} \end{array}$$

23 + 07.50 top curb Hendricks

$$\begin{array}{r} 295.75 \\ \underline{1.34} \end{array}$$

22 + 84.50 = Wly Hendricks + E Robinson to So.

$$\begin{array}{r} 296.22 \\ \underline{0.85} \end{array}$$

297.07

$$\begin{array}{r} 297.07 \\ \underline{\quad} \end{array}$$

Reed's Proposed Line
 14+28.54 = 0+00 B.C. To 11+56.41 E.L.
 INTERSECTION OF LINCOLN & HANOVER STS

+30

$$\frac{260.9}{17.6}$$

$$\frac{252.7}{13.8}$$

+50

$$\frac{243.5}{23.0}$$

+37

Det. draw from North
 Drainage from
 pav. on Vermont

$$\frac{239.9}{16.6}$$

+15

Approx. 2 Foot Bridge on Vermont St.

$$\frac{249.7}{16.8}$$

$$\frac{257.7}{14.8}$$

0+50

$$\frac{250.8}{15.7}$$

14+28.54 = 0+00 Reed's proposed line

T.P. p. 50 8.77
 Rock

206.45

257.68

$$\frac{266.45}{2}$$

4 + 02 POT

$$\frac{273.25}{4.45}$$

T.P. 11.74 277.70 0.49 265.96

$$\frac{277.70}{7}$$

+50

$$\frac{257.2}{93}$$

3 + 33.36 EC

$$\frac{245.4}{21.1}$$

+27 Bot. draw from North

$$\frac{242.4}{24.1}$$

3

$$\frac{253.2}{133}$$

+70

$$\frac{261.9}{4.6}$$

2 + 50

$$\frac{262.1}{4.4}$$

266.45

$$\frac{266.45}{8}$$

+70

+50

6

+50

5

T.P.

12.11

289.36

0.45

277.25

+55

4+40

277.70

$\frac{286.6}{2.8}$

$\frac{286.6}{2.8}$

$\frac{284.9}{4.5}$

$\frac{282.0}{7.4}$

$\frac{280.1}{9.3}$

$\frac{289.36}{7}$

$\frac{266.4}{11.3}$

$\frac{271.8}{5.9}$

$\frac{277.70}{5}$

9

$$\frac{298.8}{7.2}$$

T.P. 862 306.00 299 297.38

$$\frac{30600}{4}$$

+50

$$\frac{297.3}{3.1}$$

8

$$\frac{296.0}{4.4}$$

7 + 90.04 BC ST.

$$\frac{295.64}{4.73}$$

+75.7 NLY edge alley pair

$$\frac{295.13}{5.24}$$

+14.4 SLY edge alley pairing

$$\frac{293.86}{6.51}$$

7+05

$$\frac{293.9}{6.5}$$

T.P. 1307 300.37 2.06 287.30
289.36

$$\frac{300.37}{2}$$

check to ^{BIT} Paccop + Handrake		4.06	293.98	293.94
T.P.	058	298.04	5.54	297.46

11 +56.41 E.C. pay.

$$\begin{array}{r} 301.47 \\ \hline 4.02 \\ \hline \end{array}$$

11

$$\begin{array}{r} 300.55 \\ \hline 5.45 \\ \hline \end{array}$$

+50 pay.

$$\begin{array}{r} 299.79 \\ \hline 6.21 \\ \hline \end{array}$$

+10 S/y Top of Lincoln w/ of

$$\begin{array}{r} 299.12 \\ \hline 6.88 \\ \hline \end{array}$$

pay 905 = 7.31

10

$$\begin{array}{r} 299.1 \\ \hline 6.9 \\ \hline \end{array}$$

9 +50

$$\begin{array}{r} 299.3 \\ \hline 6.7 \\ \hline \end{array}$$

306.00

$$\begin{array}{r} 306.00 \\ \hline 6 \\ \hline \end{array}$$

#2 Proposed Road on Sly Side
of Pascoe St. Cañon.
bet. 6th St. Ext. + Richmond.

POT. 7+23.96

EC = 2+48.65

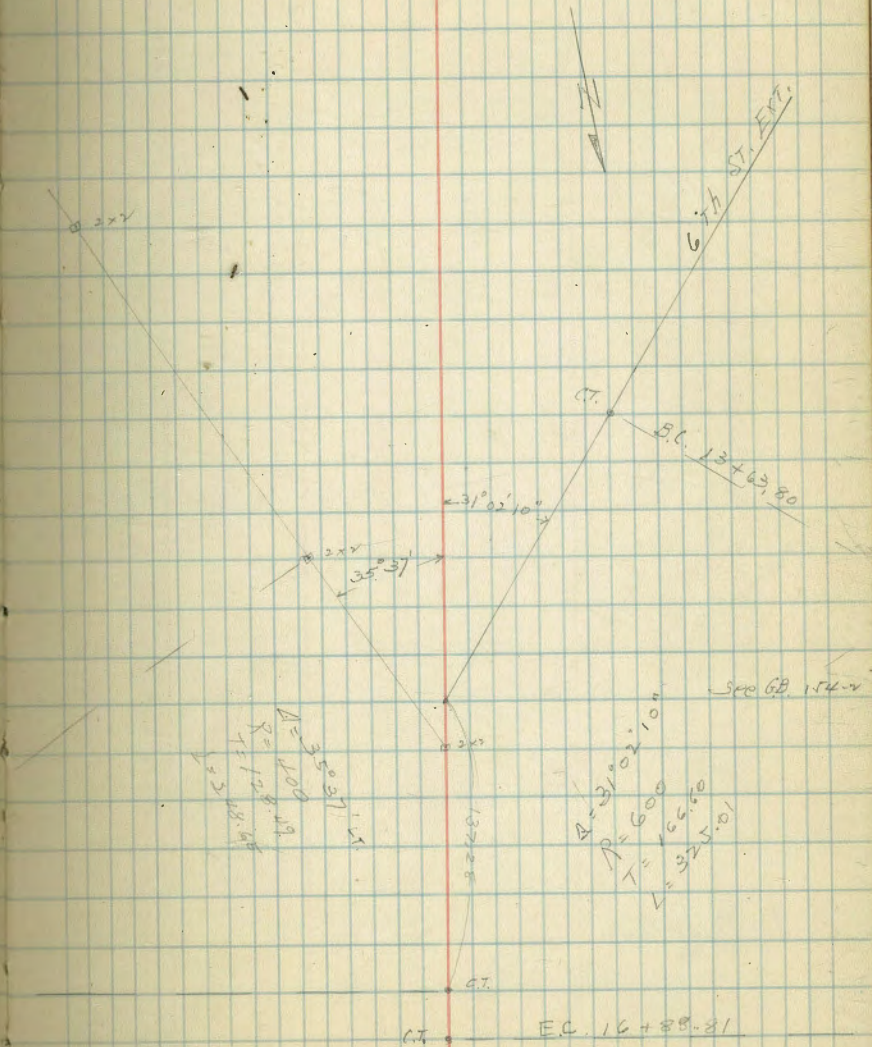
P1 222 35°37' LT.

0+00 = B.C. LT.

0-29.32

Indexed
C.S.N.

61

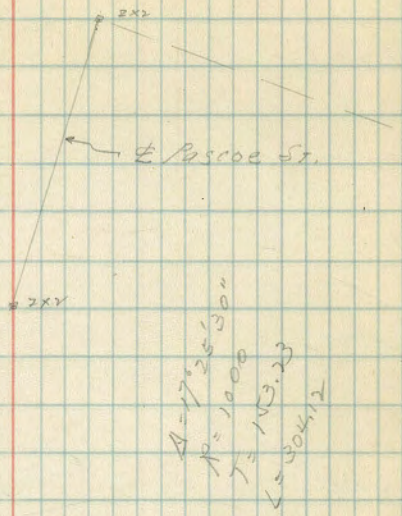


EC. = 24+07.39 = POT. sta 21+65.53 p 41

PI 17°25'30" R

BC 21+0327

EC 15+89.51



2x1

2x2

± Levels. of Prop. Rd.
Sly Side Pascoe St Canon.
6th to Richmond.

+20

$\frac{155.9}{34.7}$

2

$\frac{165.0}{24.1}$

+58

$\frac{188.2}{1.9}$

+50

$\frac{188.0}{2.1}$

+20

$\frac{185.8}{4.3}$

1

$\frac{184.9}{5.2}$

+50

bal.

$\frac{182.28}{7.7}$

0+00 = B.C.

bal.

$\frac{178.97}{11.08}$

B.M. 6th St Evr.

16+88.81

1204

190.05

177.01

EC. Cap track

$\frac{190.05}{7}$

+25

$\frac{197.0}{5.0}$

+

$\frac{199.7}{2.3}$

+75

$\frac{200.5}{1.5}$

+50

$\frac{198.3}{3.7}$

T.P.
3 +19 Rock 1223 2020 024 189.81

$\frac{20204}{9}$

3

$\frac{180.9}{9.1}$

+53

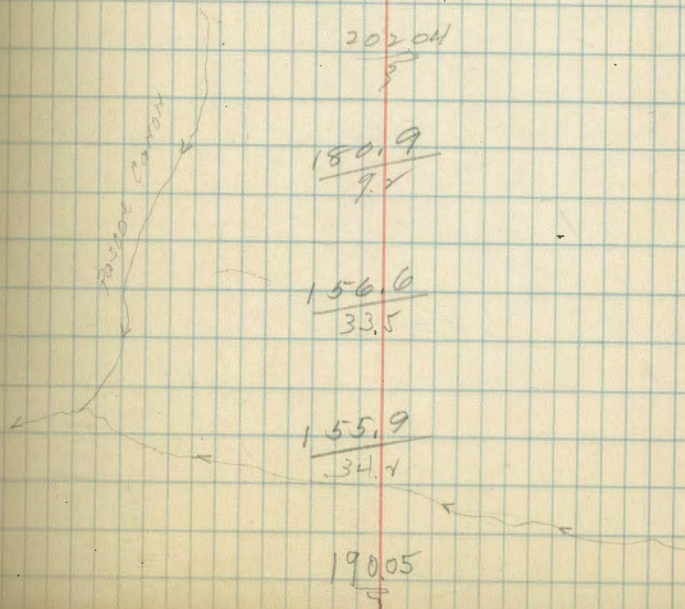
$\frac{156.6}{33.5}$

2 +48W = EC
Canyon drainage from 6th + 4th
60" Culv.

$\frac{155.9}{34.4}$

19005

$\frac{19005}{9}$



T.P. 1293 226.19 0.26 213.26

+15

$$\begin{array}{r} 210.5 \\ \hline 3.0 \end{array}$$

6

$$\begin{array}{r} 209.3 \\ \hline 4.2 \end{array}$$

+50

$$\begin{array}{r} 205.5 \\ \hline 8.0 \end{array}$$

+25

$$\begin{array}{r} 208.6 \\ \hline 4.9 \end{array}$$

5

$$\begin{array}{r} 205.8 \\ \hline 7.7 \end{array}$$

T.P. 11.76 213.52 0.28 201.76

$$\begin{array}{r} 213.52 \\ \hline 7 \end{array}$$

4 + 50

$$\begin{array}{r} 197.9 \\ \hline 4.1 \end{array}$$

202.04

202.04

T.P. 156 222.31 13.12 220.75

+80

$\frac{223.7}{102}$

+50

$\frac{228.1}{5.8}$

+25

$\frac{231.8}{2.1}$

$\frac{229.0}{4.9}$

+50

$\frac{226.7}{7.2}$

T.P. 8.25 233.87 057 225.62

6 + 30

226.19

$\frac{233.87}{8}$

$\frac{218.0}{8.4}$

$\frac{226.19}{3}$

+50

$$\begin{array}{r} 216.0 \\ \hline 6.9 \end{array}$$

+25

$$\begin{array}{r} 224.8 \\ \hline + 1.9 \end{array}$$

11

$$\begin{array}{r} 225.9 \\ \hline + 3.0 \end{array}$$

+75

$$\begin{array}{r} 224.3 \\ \hline + 1.4 \end{array}$$

+50

$$\begin{array}{r} 218.9 \\ \hline 4.0 \end{array}$$

+25

$$\begin{array}{r} 211.9 \\ \hline 11.0 \end{array}$$

10

$$\begin{array}{r} 208.6 \\ \hline 14.3 \end{array}$$

9482.66 B.C. LT.

$$\begin{array}{r} 207.6 \\ \hline 15.3 \end{array}$$

222.93

$$\begin{array}{r} 222.93 \\ \hline 3 \end{array}$$

+50

$$\begin{array}{r} 249.3 \\ \underline{9.8} \end{array}$$

+30

$$\begin{array}{r} 253.4 \\ \underline{5.2} \end{array}$$

13

$$\begin{array}{r} 249.9 \\ \underline{8.7} \end{array}$$

T.P.	12.01	258.63	0.90	246.62
------	-------	--------	------	--------

$$\begin{array}{r} 250.63 \\ \underline{7} \end{array}$$

T.P.	13.19	247.52	0.56	234.33
------	-------	--------	------	--------

+50

$$\begin{array}{r} 228.6 \\ \underline{6.3} \end{array}$$

T.P.	12.29	234.89	0.43	222.50
------	-------	--------	------	--------

$$\begin{array}{r} 234.89 \\ \underline{7} \end{array}$$

12	Drainage from So.	24" Culv.		
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$$\begin{array}{r} 200.4 \\ \underline{22.5} \end{array}$$

from 10th d. wash.

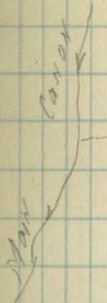
11+70

$$\begin{array}{r} 203.6 \\ \underline{19.3} \end{array}$$

222.93

$$\begin{array}{r} 222.93 \\ \underline{7} \end{array}$$

+14 drainage from So. 24" Culu.



214.0
33.7

+05

215.0
32.7

15

217.9
29.8

+50

241.0
6.7

T.P. 208 247.68 1303 245.60

247.68
7

+25

252.5
6.1

14

257.1
1.5

13 +70

250.2
8.4

258.63

258.63
2

T.P. 1321 260.58 03/ 247.37

17

$$\frac{247.1}{0.6}$$

+50

$$\frac{237.5}{10.2}$$

+20

$$\frac{239.7}{8.0}$$

16

$$\frac{241.1}{6.6}$$

N+89.51 EC

$$\frac{241.79}{5.89}$$

+X

$$\frac{240.6}{7.1}$$

N+50

$$\frac{231.5}{16.2}$$

247.68

$$\frac{247.68}{2}$$

79

$$\frac{256.5}{4.1}$$

+80

$$\frac{258.1}{2.5}$$

+50

$$\frac{254.0}{6.6}$$

+25

$$\frac{244.9}{15.7}$$

18

$$\frac{243.8}{16.8}$$

+64

approx. \pm Foot Bridge at Vermont St

+50

$$\frac{248.1}{12.5}$$

17 + 25

$$\frac{251.1}{9.5}$$

260.58

$$\frac{260.58}{7}$$

21 + 03.27 - B.C. ^{HT} Hub

+85

T.P. 1320 272.89 0.89 259.69

+42 Drainage from So. 24" Culi.

20

+70

+50

19+25

260.58

266.04
6.85

261.1
11.8

272.89
7

240.9
19.7

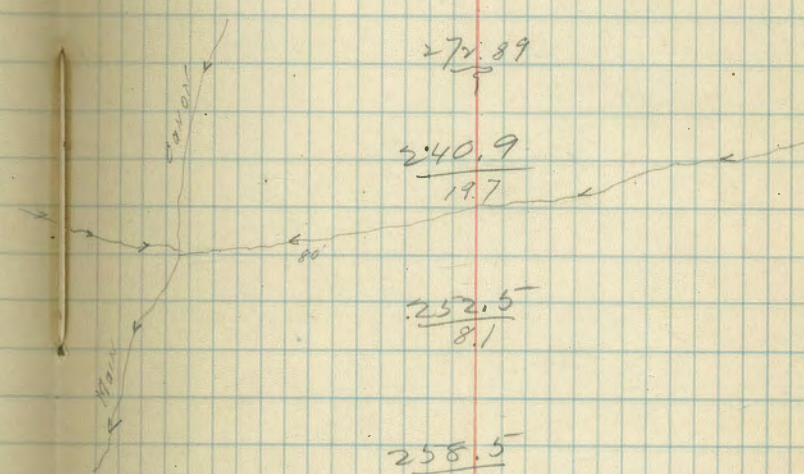
252.5
8.1

258.5
2.1

257.3
3.3

254.8
5.8

260.58
8



24. $+07.39 = EC = 879.21 + 65.53$ Pascoe L. wa.
 p. 54

314

291.61

291.72

 $\frac{0.11}{\text{error}}$

291.4

 $\frac{3.14}{3}$

24

 $\frac{291.8}{3.0}$

+50

 $\frac{289.0}{5.8}$

T.P.

10.86

294.75

135

283.89

 $\frac{294.75}{3}$

23

 $\frac{283.0}{2.2}$

+50

 $\frac{279.4}{5.8}$

22

 $\frac{274.7}{10.5}$

T.P.

12.76

285.24

0.41

272.48

 $\frac{285.24}{3}$

21 +50

 $\frac{272.4}{0.5}$

272.89

 $\frac{272.89}{3}$

± Levels on 9th St.
Robinson to Pascoe St.

+80

T.P. 12.95 288.04 0.11 275.10

+45

T.P. 11.95 275.21 0.61 263.26

+1939 EG.

2

T.P. 13.14 263.87 0.31 250.75

+50

+23 N by gut + 26.

+50 pav.

0+10 PC pav.

014 251.06

244.94 Grade curb on 9th
Pk. N of
approx. 200 ft of Robinson

±

77

277.9
10.1

288.04
12.95

266.3
8.9

275.21
0.61

262.48
1.39

255.1
1.8

263.87
0.31

249.4
1.7

246.78
428 = gut cb = 250

249.26

245.89
5.7

244.50
6.54

243.22
7.84

251.06
3

£

9		<u>284.66</u>		
		464		
	489	289.30	361	284.41
8+00		<u>284.51</u>		
		357		
7+00		<u>284.25</u>		
		377		
6+00		<u>283.87</u>		
		415		
5+30.4	pat. = NL Div. Div.	<u>283.38</u>		
		464		
5	PAY.	<u>283.17</u>		
		485		
+58		<u>282.69</u>		
		5.33		
+40		<u>283.1</u>		
		2.9		
4		<u>281.9</u>		
		6.1		
+50		<u>280.5</u>		
		7.5		
3+00		<u>279.0</u>		
		9.0		

288.04

13+37

Σ
231.0
181

T.P. 0.47 249.12 12.81 248.65

249.3
12.8

12+94

T.P. 0.41 261.46 12.36 261.05

264.7
8.7

+70

265.4
8.0

+60

T.P. 0.40 273.41 13.15 273.01

T.P. 4.45 286.16 7.59 281.71

280.0
9.3

+45

282.2
7.1

14

+45.5 gutter in drive
N 16. Washington

282.68
4.62

283.67
5.63

11

284.60
4.70

10

289.30

Σ

79

p 67
check ground Sta 7+00

229.0
20.1

229.0

229.0

16+59.01

227.7
21.4

16

235.1
14.0

+50

232.8
16.3

15

230.3
18.8

+75

237.2
11.9

+50

238.0
11.1

+30

232.6
16.5

14+03.19 B.C. LT

224.0
25.1

+73

218.1
31.0

13+20

220.1
29.1

249.12

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1 1/2 to 1.
If ground is nearly level, the cut or fill of side
stake is located by the double entry method in
left column and top row. The number in both

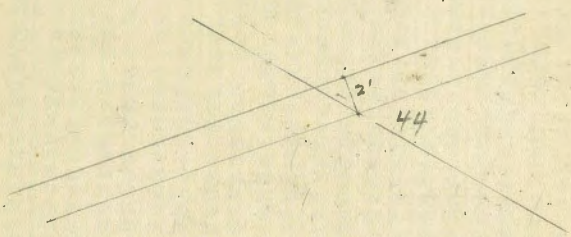
IMPROVED TABLES
AND
INFORMATION

TABLE No. 2.

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add position found in column of constants.
Degree of curve with given L may be found
by dividing tangent (or external) opposite L by
given tangent (or external).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

60967 $\overline{) 2,000,000}$ 3.28
 182901
 170990
 121934
 490560.
 487736

1.79.60
 79.15
 1.01.45



400.93
 367 - 66 70000
 4.0
 395 E Side FH

7 31.5
 7
 7.245

2.77

.7214 $\overline{) 2,000,000}$
 14428
 55120
 50498
 52220
 50498

3.28

60947 $\overline{) 2,000,000}$
 182844
 179590
 121894
 496960
 487576