

4527

LOEBENSTEIN

JOBBS

FIELD BOOK

No. 365F

MICROFILMED  
DEC 24 1964

ENGINEERING DEPARTMENT  
CITY OF SAN DIEGO.  
CALIFORNIA.

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
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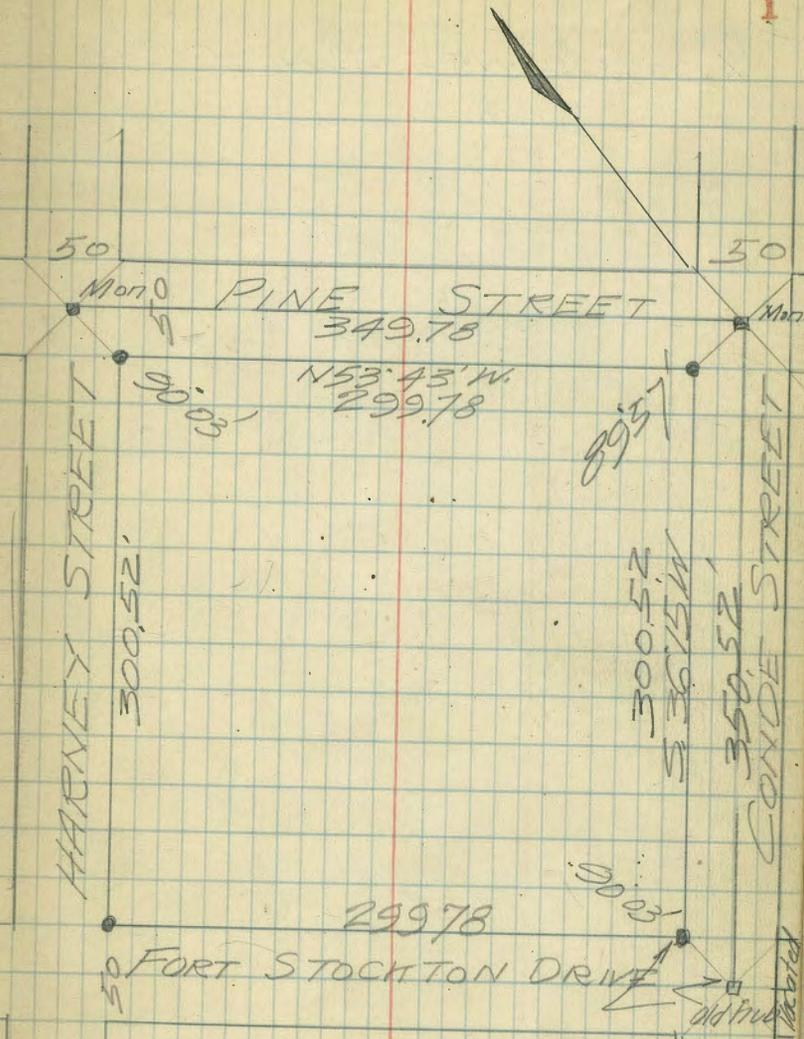
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**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
IRVING PARK STATION  
CHICAGO, ILL.

BLOCK 474 Old San Diego  
Ralph Hurlbert.

Dec. 7/1933

Indexed  
c. S. K.



Note - set  $1\frac{1}{2}$ " iron pipes at  
corners of block.

indexed  
C.S.K.

# X Sects CONDE PLACE

⊕ Pine St

W 30'

2

040

045

045

1400

1200

1450

175

2100

245

R 50

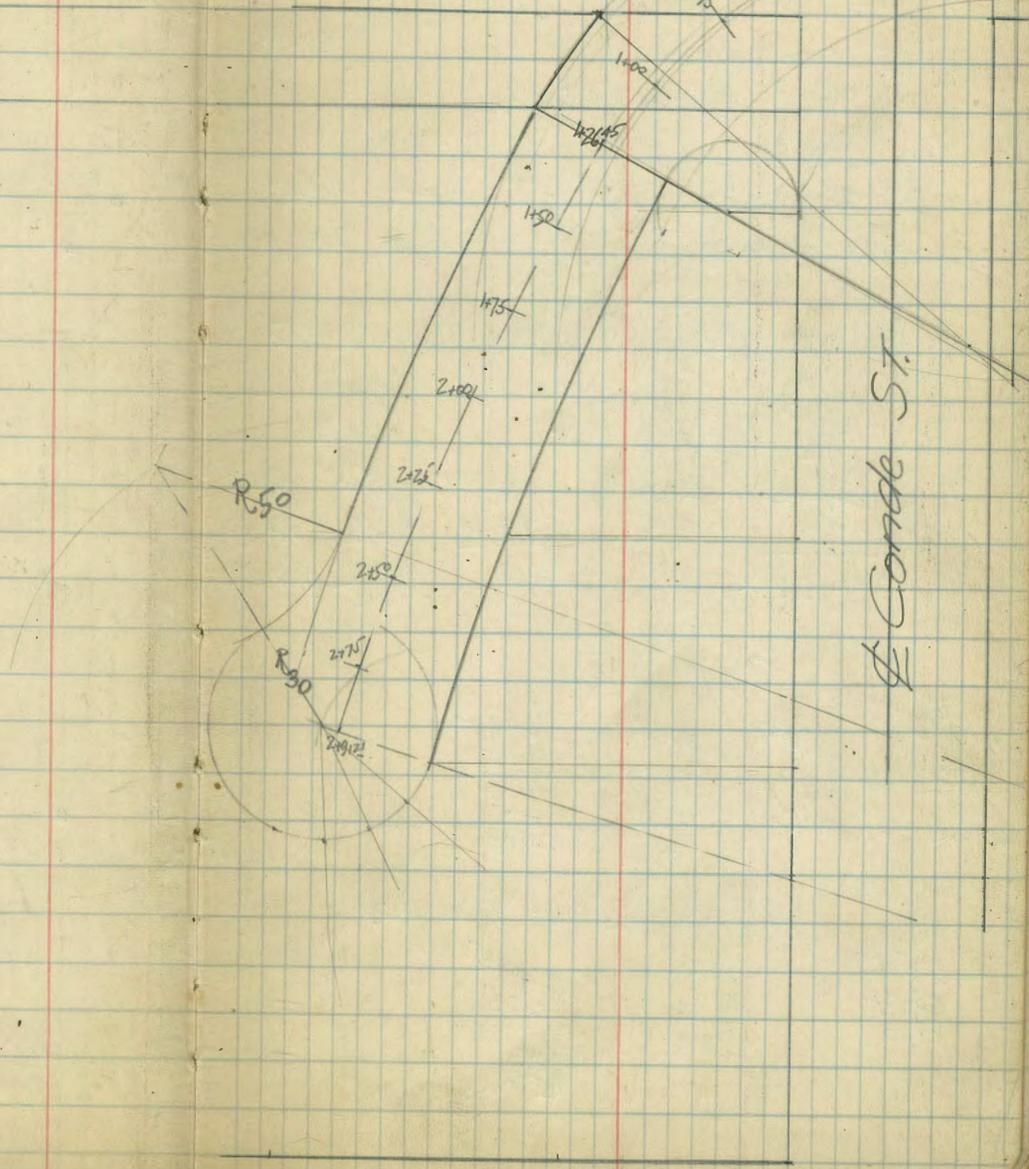
245

R 90

275

290

⊕ Conde St



March 31/1934

C.T. SE. Cor Pine & Arista

see Bk 100-page 40

5.06 251.04

245.98

Cor. Mon & Conde  
& Pine

4.24 246.80

Top wall at end.

0.0 251.04

251.04

37 1/2 W

244.8  
6.24  
0.0  
\$ Pine

246.05  
5.00  
25¢

247.7  
3.32  
50K  
12 Pine

Interjection Pine & Conde Sts

≡ Conde St

247.42	247.80	247.20	247.66	248.60
3.62	3.25	3.84	3.38	2.14
0.0. \$ Pine	8N	14N	25K & C Pine	50N & C Pine

243.9  
7.3  
0.0  
\$ Pine

50 W - W Conde

244.7	246.2	246.5
6.26	4.81	4.51
25	50N 12 Pine	55N

17 1/2 W. of ≡

245.6	246.2	247.1	248.1
5.43	4.80	3.92	2.35
0.0 \$ Pine	10N	25N ♀	50N 12 Pine

25 W = ♀ Pine & Conde

245.2	246.8	248.5
3.84	4.12	2.53
0.0	25 ♀	50K 12 Pine

X SECTS CONDE ST.

✓✓ CONDE = 0

✓ Pine = 0

Cor. Mon of Conde & Pine 246.80  
 0.57 247.37

Line 0+0

243.8	245.2	247.4
<u>3.5</u>	<u>2.2</u>	<u>0.0</u>
✓✓	✓	✓

0+25

243.3	244.0	243.1	242.8	243.1	246.0	246.5
<u>4.10</u>	<u>3.4</u>	<u>4.7</u>	<u>4.6</u>	<u>4.3</u>	<u>1.4</u>	<u>0.9</u>
0	9	15	25	32	43	50

0+50

242.3	242.8	240.6	240.4	240.6	243.7	244.2
<u>5.1</u>	<u>4.6</u>	<u>6.8</u>	<u>7.0</u>	<u>6.75</u>	<u>3.65</u>	<u>3.2</u>
0	9	13	25	35	40	50

0+75

240.3	240.2	237.6	238.6	238.7	239.6	238.6
<u>7.1</u>	<u>7.1</u>	<u>9.8</u>	<u>8.8</u>	<u>8.7</u>	<u>7.8</u>	<u>8.8</u>
0	8	11	25	33	39	50

H.I

247.37

238.6	235.3
<u>8.8</u>	<u>12.1</u>
0+87	0+94
237.1	
<u>10.3</u>	
0+91	

✓✓ Conde

✓ Conde

Line 1+00

238.6	235.2	233.5	233.0
<u>11.3</u>	<u>12.2</u>	<u>13.9</u>	<u>1.4</u>
119	25	37	50
		(12.67)	23470
0.23	234.93		

Line 1+25

232.9	229.4	228.9	227.4
<u>1.95</u>	<u>5.5</u>	<u>8.0</u>	<u>7.5</u>
0	14	25	50

Line 1+50

225.6	225.8	224.2	222.5
<u>9.25</u>	<u>9.05</u>	<u>10.7</u>	<u>12.4</u>
0	3	25	50

1.79 224.26 (12.46) 222.47

H.I.  
224.26  
Line 1+75

222.3  
2.0  
0

220.0  
4.3  
25

219.1  
5.2  
50

Line 2+00

218.4  
59.0  
0

216.7  
7.55  
25

215.7  
8.6  
50

Line 2+25

215.0  
9.3  
0

214.1  
10.2  
25

213.4  
10.9  
50

(1233) 219.3  
0.62 212.55

Line 2+50

211.8  
9.8  
0

210.6  
19.5  
25

211.2  
14  
50

Line 2+75

207.9  
4.7  
0

207.0  
5.6  
25

205.8  
6.8  
50

212.55

¢ of Conde

206.4  
6.2  
2480

202.1  
9.5  
2+95

199.6  
13.0  
3+00

(1234) 200.71

0.46 200.67

198.3  
2.4  
3+02

195.5  
4.8  
3+10

194.0  
6.7  
3+20

190.7  
10.0  
3+25.5

¢ Fort Stockton -

188.7  
12.0  
3+35

(1209) 188.58

0.96 189.54

184.8  
4.7  
3+50

180.3  
9.2  
3+60

177.8  
11.7  
3+68

(1275) 176.79

1.02 177.80

172.7  
5.1  
3+72

175.3  
2.3  
3+75

171.5  
6.3  
3+83

169.4  
8.4  
3+90

166.9  
10.85  
3+98

167.4  
10.4  
4+00

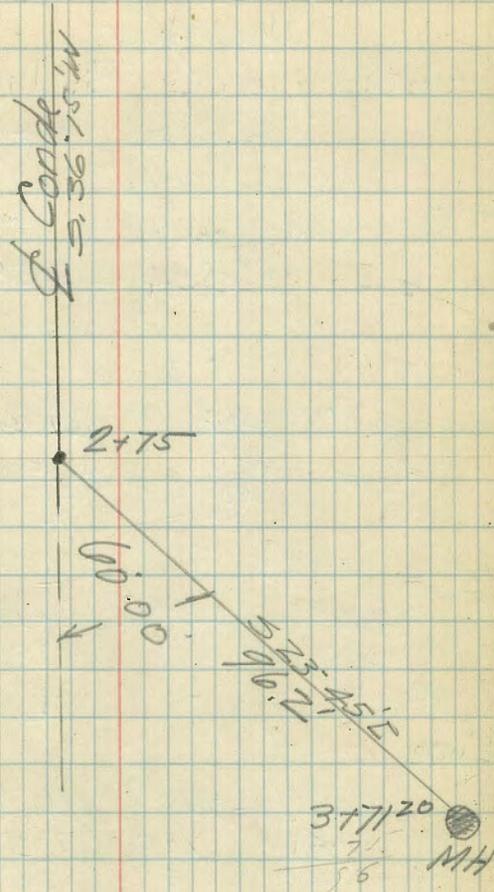
85.2  
19.28  
4+07.3 M.H. Cover

15.52  
162.28  
4+07.3 approx flow line

# Change of Line for Sewer

2+75  $\phi$  of Conde. to M.H.

Station	H.I.		
2+75	216	209.27	207.11
205.2	201.7		
4.1	8.54		
2+87	3+00	(13.01)	196.26
	3.80	200.06	
3+25		7.49	192.57
		(13.00)	187.06
	0.61	187.67	
3+50		11.14	176.53
		(12.40)	175.27
	2.83	178.10	
3+55		6.36	171.74
+61		9.30	168.80
+71.20 M.H. Cover		8.82	169.28



# X SECTY. CONDE PLACE

March 24/35

Stations on Ely line of  
Conde St = 0+0  
Ely line Conde Place = 0-

Top wall - (page 3) 251.04  
0.54 251.58

## Line 0+0

246.76	247.15	247.62	248.01	248.61
482	443	396	357	297
0	10	25	40	50
P	curb	£	curb	£

## Line 0+25

246.78	245.8	246.78	247.54	247.92
580	5.78	480	404	366
0	5	20	35	40
		£		

## Line 0+50

244.17	244.28	244.39	244.53	244.56
741	7.30	7.9	7.05	7.02
0	5	20	35	40
		£		

## Line 0+75

242.62	242.34	241.51	240.81	240.79
896	9.24	20.07	10.77	10.79
0	5	20	35	40
		£		

## Line 1+00

241.03	240.73	240.12	239.38
10.55	10.85	11.46	12.20
0	5	20	35

H.I 7  
251.58

(-11.89) 239.69

0.48 240.17

## Line 1+26.45

239.69	239.51	238.79	237.87	237.58
048	066	138	230	259
0	5	20	35	40

## Line 1+50

238.25	238.15	237.80	237.17	236.92
1.92	2.02	237	3.0	325
0	5	20	35	40

## Line 1+75

236.78	236.67	236.34	235.90	235.77
339	350	383	427	440
0	5	20	35	40

## Line 2+00

235.79	235.39	235.17	234.75	234.67
468	4.78	5.00	542	55
0	5	20	35	40

## Line 2+25

234.34	234.35	234.08	233.69	233.66
5.83	5.82	6.09	6.18	6.7
0	5	20	35	40

## Line 2+50

232.91	232.90	232.92	232.64	232.59
236	219	725	753	758
0	5	20	35	41

240.17

Line 2+75

23156	23173	23167	23179	23171
<u>861</u>	<u>844</u>	<u>850</u>	<u>838</u>	<u>846</u>
0	5	20	35	40

Line 2+91<sup>21</sup>

23080	23092	23125	23125	23123	23096
<u>937</u>	<u>925</u>	<u>892</u>	<u>892</u>	<u>894</u>	<u>921</u>
0	5	20	30	35	40

Can  
banjo

Around banjo.

Can  $\angle$  24<sup>30</sup> = Arc of 12.83 - R 30

Line 2+91<sup>21</sup>

23058	23092	23125
<u>937</u>	<u>925</u>	<u>892</u>
0	5	30

3+04<sup>04</sup>

23026	23033	23125
<u>991</u>	<u>984</u>	<u>892</u>
0	5	30

3+16<sup>87</sup>

23012	23037
<u>1085</u>	<u>980</u>
0	5

3+29<sup>70</sup>

23002	23033
<u>1015</u>	<u>984</u>
0	5

240.17

3+42 <sup>53</sup>	23011	23031	23125
	<u>1056</u>	<u>986</u>	<u>30</u>
	0	5	

3+55 <sup>36</sup>	23010	23027
	<u>1007</u>	<u>990</u>
	0	5

3+68 <sup>19</sup>	23028	23029
	<u>989</u>	<u>978</u>
	0	5

3+81 <sup>02</sup>	23060	23076
	<u>957</u>	<u>941</u>
	0	5

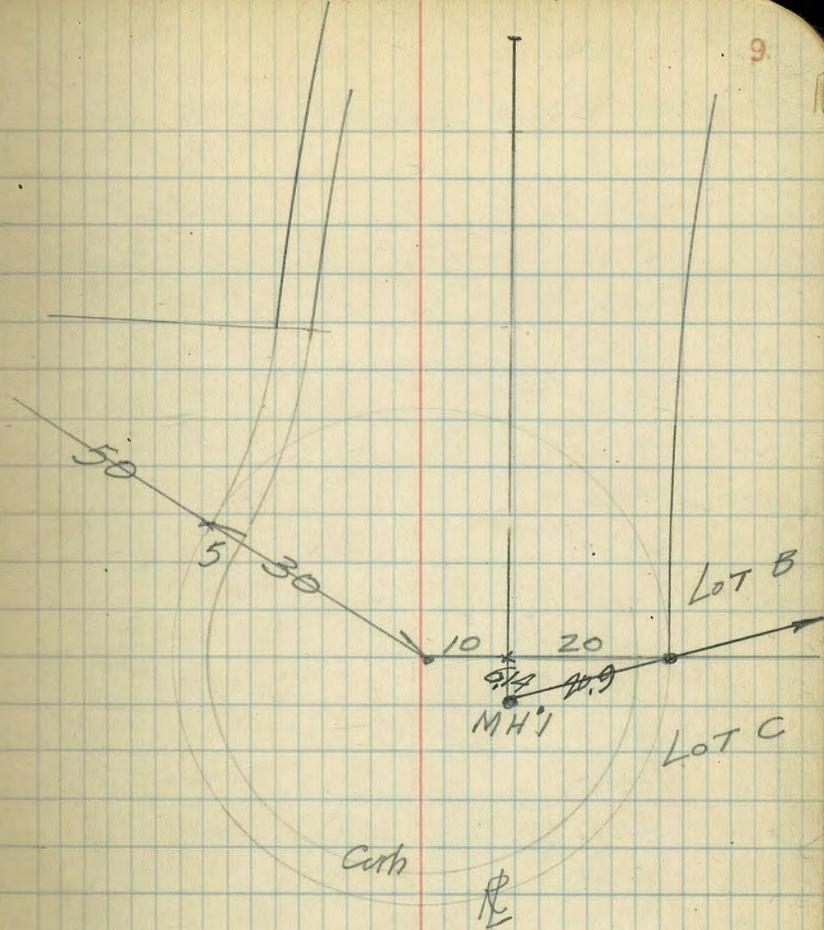
3+93 <sup>85</sup>	23113	23122
	<u>904</u>	<u>895</u>
	0	5

4+07 <sup>95</sup>	23171	23176
PRC.	<u>846</u>	<u>841</u>
	0	5

Sewer Line  
Danjo to Conde St.

P.R.C. = 4 + 0.7<sup>25</sup> page 8- 231.76  
4.16 235.92

MH #1 = 0	5.23	230.69
0 + 20 pipe Lot B	4.66	231.26
+ 50 Lot C	9.10	226.8
+ 75	12.40	223.5
	(12.88)	223.04
130	224.34	
+ 00	2.8	221.5
+ 10	3.9	220.4
+ 16	5.6	218.7
+ 41 = Conde St. MH #2	7.05	217.29



Check of  
Charles St. Grades

£ > below High side

EL. Carolina	N CB	£	S CB
0+00	—		267.25
+20	267.64		268.14
+40	268.61		269.11
+60	269.68		270.18
+80	270.85		271.35
1. P.V.C.	272.09		272.59
+50	275.33		275.83
2	278.56		279.06
+50	281.80		282.30
3	285.04		285.54
+50	288.28		288.78
3 + 80 P.C.	290.22		290.72
4 + 20	292.68		293.18
+60	294.87		295.37
5	296.80		297.30
+40	298.44		298.96
+80	299.85		300.35
6 + 10.50	300.75		301.25

271.02 spike in Pale 100' E on Charles  
Carolina

Check of  
Wilcox ST Grades

	N 66		S 66
00 EL Cat.			
0 +25 PC	259.83 ✓		260.33 ✓
+50	260.83 ✓		261.33 ✓
1	262.82 ✓	✓	263.32 ✓
+50	264.82 ✓		265.32 ✓
2	266.81 ✓	✓	267.31 ✓
+50	268.81 ✓		269.31 ✓
3	270.80 ✓	✓	271.30 ✓
+50	272.75 ✓		273.25 ✓
3 +90 PC	274.31 ✓	✓	274.81 ✓
4 +30	276.04 ✓		276.54 ✓
4 +70	278.11 ✓		278.61 ✓
5 +10	280.48 ✓		280.98 ✓
5 +50	283.14 ✓		283.64 ✓
5 +90	285.95 ✓		286.45 ✓
6 +10.50	287.24 ✓		287.74 ✓

271.02  
 3.00  
 274.02  
 0.42  
 274.20  
 12.09  
 286.29

check of  
Jennings St. Grades

12

	N 66			S 66	
00:EL CAT.					
0 + 25 P.C.	249.72	3L		250.00	2L
+50	250.35			250.85	
1	251.60	4H		252.10	3H
1 + 58.8V	252.95	3H	✓	253.45	✓
1 + 98.8V	253.88			254.38	
2 + 38.8V	254.6V	✓	3L	255.1V	3L
2 + 78.8V	255.7			255.67	
3 + 18.8V	255.54	✓ P.V.C.	2L	256.04	2L
3 + 50	255.74			256.24	
4	256.07.2V	2V		256.57	✓
+50	256.40			256.90	
5 + 00	256.75V	2L		257.25	2L
5 + 33.8V	256.97	P.V.C.	✓	257.47	
5 + 73.80	257.50	✓		258.0	3L
6 + 10.5	258.50			259.0	

245.59  
~~12.41~~  
 258.00  
~~1.65~~  
~~256.35~~  
~~4.88~~  
 261.23

B.M. spike fence Post

Cross Section Alley Block 6 Hartleys North Park  
And Block C McFadden & Buxton N.P.

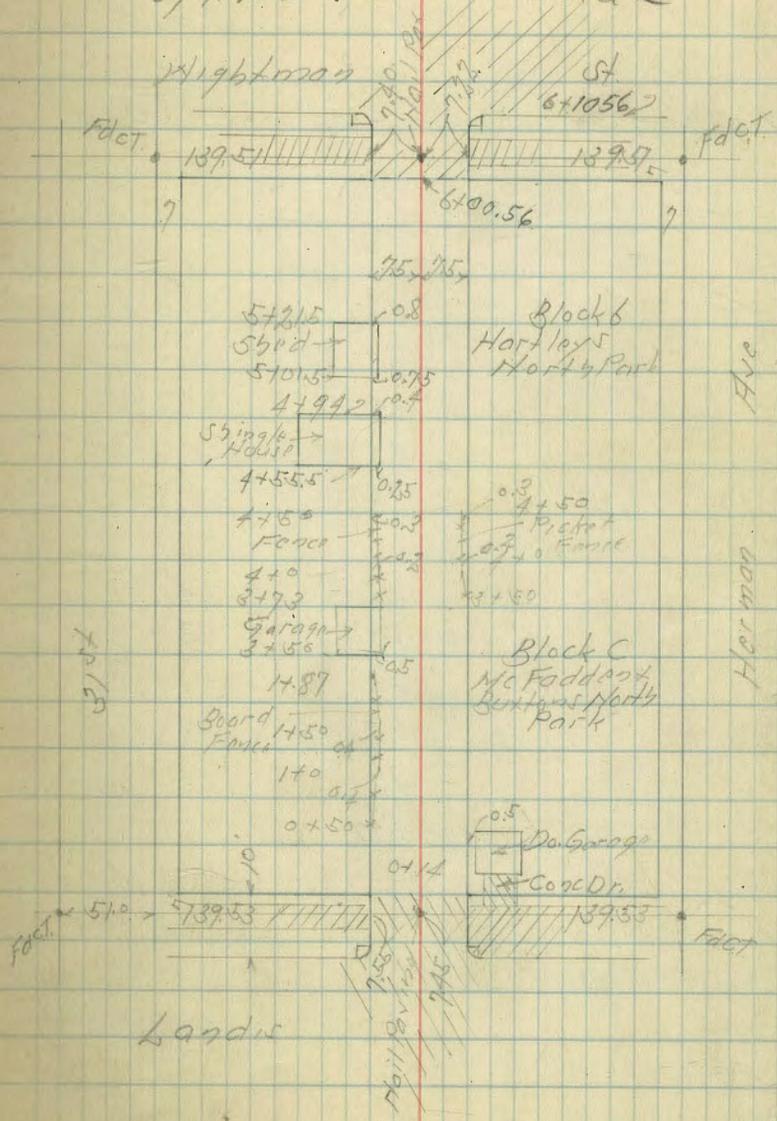
BM	953	351.41	341.88	S.E.P.P. Landis
		0-10 = N of Landis		
N of Pavng	8.46	342.95		
L " "	8.38	343.03		
F " "	8.32	343.09		
		0+10 = N.L. Landis		
F Topcb	7.61	343.80		
Gutter on Pavng	7.67	343.74		
L " "	8.02	343.39		
Gutter " "	7.93	343.48		
N Topcb	7.85	343.56		
		0+14		
N	5.4	346.0		
L	5.8	345.6		
F	5.6	345.8		
+2.7 = N of Conc Dr	5.21	346.20		
		0+30		
F	4.6	346.8		
L	4.7	346.7		
N	5.0	346.4		
+10	5.1	346.3		
		0+50		
-10	5.0	346.4		
N	4.6	346.8		
L	4.1	347.3		

Reduced & Plotted by H.M. Cole  
June 7, 1940 Profile 2833

INDEXED

EFB 141 by order  
of H.W. 9.0 on each side

June 5-40  
S. 1100  
Northern  
W Moore



Herman Ave

351.41

F		4.4	347.0
	0+64		
F-67	= 1/2 Garage Conc Floor 4.60		346.81
	0+69		
F+09	= Fly Box Pole		
	0+75		
-10		4.6	346.8
F		4.2	347.2
1/2		3.9	347.5
H		4.3	347.1
+10		4.6	346.8
	1+0		
-10		4.3	347.1
H		3.9	347.5
1/2		3.9	347.5
F		4.3	347.1
+10		4.4	347.0
TP	5.63	353.27	347.64
	1+21		
H	= 1/2 Conc Walk	5.25	348.02
	1+50		
-10		5.7	347.6
F		5.5	347.8
1/2		5.4	347.9
H		5.4	347.9

353.27

+10		5.8	347.5
	1+95		
F+0.7	= Fly Box Pole		
	1+0		
H		5.0	348.3
1/2		4.9	348.4
F		5.0	348.3
	2+23		
H	= 1/2 Conc H	4.81	348.46
	2+50		
-10		4.8	348.5
F		4.4	348.9
1/2		4.3	349.0
H		4.4	348.9
+10		4.2	349.1
	3+0		
-5	= 1/2 Oiled Drain	3.7	349.6
H		3.5	349.8
1/2		3.7	349.6
F	= Fly Box Pole	3.6	349.7
+10		4.0	349.3
	3+50		
-10		3.6	349.7
F		3.7	350.1
1/2		3.0	350.3

		353.27	
H		2.8	350.5
+10		5.0	350.3
		345.7	
H+0.5 = 1/2 Garage Dirt Floor	2.9		350.4
	4.0		
H	2.2		351.1
L	2.3		351.0
+7.3 = Fly Power Pole			
F	2.5		350.8
+10	2.8		350.5
TP	6.05	357.53	1.79
	4.50		351.48
-10	6.5		351.0
F	5.9		351.6
L	5.7		351.8
H	5.9		351.6
+10	6.0		351.5
		475	
H	5.4		352.1
+3	5.2		352.3
L	4.8		352.7
+6	5.0		352.5
F	5.4		352.1
+10	6.0		351.5

		357.53	
		4197	
F		5.2	352.3
+10 = Fly Power Pole			
+3		4.7	352.8
L		4.5	353.0
+4		4.8	352.7
+6		5.5	352.0
+7.1 = 1/2 18 Conc Walk		5.19	352.34
H		5.2	352.3
		4199	
F +10 = 1/2 2' Palm Tree			
		5425	
-10		4.9	352.6
H		4.4	353.1
L		4.3	353.2
F		4.8	352.7
		5450	
F		4.1	353.4
L		3.9	353.6
H		4.4	353.1
+10		4.5	353.0
TP	2.01	355.56	3.98
		5475	
-10 = 1/2 2.5 Door		2.50	353.06
H		2.3	353.3

355.56

L		2.1	353.5
E		2.5	353.1

5+93

-2.8	= NY Conc Dr	2.83	352.73
E	NY Conc Floor Garage	3.2	352.4
L		3.1	352.5
H		3.0	352.6
+2.2	= Fly Conc Drive	3.03	352.53

6+00.56 = 52 Nightman

H	TopCb	4.46	351.10
Gutter	on Paving	4.63	350.93
L	" "	5.07	350.49
Gutter	" "	4.95	350.61
E	TopCb	4.84	350.72

6+10.56 = 50 Nightman

E	on Paving	5.41	350.15
L	" "	5.35	350.21
H	" "	5.17	350.39
BM		3.06	352.50

NFBP  
4 BM  
352.50

Cross Section of Alley Block 323 Reed + Dalays  
 29th St to 30th St. Between Clay + Franklin

INDEXED  
 EFB

Sept. 6th 40  
 Sisson  
 Northern  
 W Moore

17

BM 8.06 86.11 78.05 SEBP Clay + 29th

0-10 = FC 29th St

H	Top Cb	4.38	81.73
'	Gutter or Grooved	4.8	81.3
d	" "	4.3	81.8
S	" "	4.2	81.9

0+0 = FL 29th St

S	Top Conc Wall	1.62	84.49
S		4.2	81.9
d		4.1	82.0
H		4.3	81.8
H	Top Cb	4.11	82.00

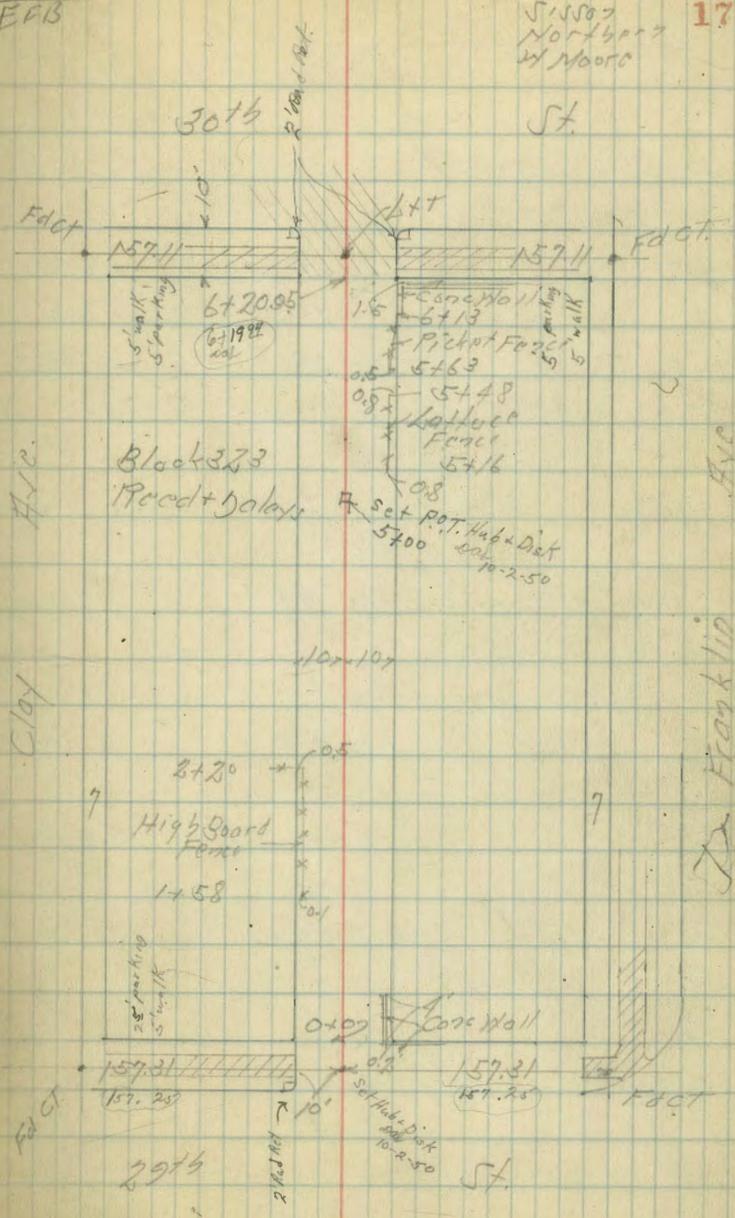
0+4

H		3.0	83.1
+2		3.7	82.4
d		3.9	82.2
+6		3.6	82.5
S		1.6	84.5

0+25

S		1.6	84.5
+6		3.2	82.9
d		3.3	82.8
+6		3.3	82.8
H		2.4	83.7

Reduced - Plotted by H.M. Cole  
 6/7/40



86.11

0+50

-10	3.9	82.2
N	3.5	82.6
+5	2.9	83.2
Z	2.9	83.2
+5	2.8	83.3
S	2.0	84.1

0+84

5+0.8 - Sky Power Pole

0+90

5+0.2 - Garage Dirt Floor 2.7

1+0

S - Garage Dirt Floor 2.8

Z	2.7	83.4
N	2.9	83.2
+8	3.5	82.6
+10	3.9	82.2

TP 4.40 87.52 ✓ 2.99 83.12

1+45

-10	5.0	82.5
N	4.3	83.2
Z	4.4	83.1
+9.8 - Garage Dirt Floor	4.4	83.1
S	4.4	83.1

87.52

1+75

S	4.3	83.2
Z	4.6	82.9
N	4.6	82.9

2+0

-10	5.9	82.1
N	4.7	82.8
Z	4.7	82.8

+9.4 - Sky Power Pole

S-

	4.5	83.0
+10	4.3	83.2

2+45

-10	4.9	82.6
S	4.6	82.9
Z	4.8	82.7
N on Ground	4.9	82.6
+0.5 - Garage Dirt Floor	5.6	81.9

Not Being Used

2+75

-10	6.3	81.2
N	5.0	82.5
Z	4.8	82.7
S	4.7	82.8

87.52

2+90

N-4.4 = ~~Garage~~ Dirt Floor 6.2  
Hot Being Closed 81.3

S+0.7 = Sky Power Pole

3+0.4

-8.8 = ~~Garage~~ Dirt Floor 5.2 82.3

S 5.0 82.5

S 5.0 82.5

H 5.0 82.5

+4.1 = ~~Garage~~ Dirt Floor 6.0 81.5

3+4.0

-10 6.3 81.2

H 4.6 82.9

S 4.4 83.1

S 4.6 82.9

3+6.0

S 3.6 83.9

S 3.8 83.7

H 3.7 83.8

+10 3.6 83.9

3+6.9

H = ~~Garage~~ Dirt Floor 3.4 84.1  
Hot Being Closed

TP 11.95 96.20 ✓ 32.7 84.25 ✓

3+9.0

S-6.7 = ~~Do. Garage~~ Dirt Floor 10.5 85.7

96.20 ✓

3+9.6

H = ~~Garage~~ Dirt Floor 11.2 85.0

4+0

H 11.1 85.1

S 10.4 85.8

+9 = Sky Power Pole

S 10.6 85.6

+5 10.6 85.6

4+1.3

-5.2 = ~~Garage~~ 11.7 Opening 8.7 87.5  
Dirt Floor

S 9.2 87.0

S 9.5 86.7

+7 9.6 86.6

H 8.7 87.5

+5 8.1 88.1

4+5.0

H 5.9 90.3

S 6.2 90.0

+6 6.2 90.0

S 5.3 90.9

4+7.5

S 7.8 93.4

+2 4.9 91.3

S 5.0 91.2

+7 4.8 91.4

	96.20		
N		4.1	92.1
	5+10		
N		4.4	91.8
+4		4.8	91.4
Z		4.7	91.5
+7		4.4	91.8
S		2.7	93.5
	5+0.7		
S-1.5 = Garage Dirt Floor		4.2	92.0
	5+2.0		
S+0.8 = Sky Power Pole			
	5+2.5		
S		3.2	93.0
+1		4.3	91.9
Z		5.0	91.2
+7		4.9	91.3
N		4.2	92.0
	5+3.2		
S+0.7 = Conc Walk		3.62	92.57
	5+5.0		
-10		6.4	89.8
N		5.9	90.3
+3		6.6	89.6
Z		6.6	89.6
+4		6.5	89.7

	96.20		
S		6.0	90.2
+10		5.8	90.4
	5+7.5		
S		7.8	88.4
+2		9.4	86.8
Z		9.9	86.3
+7		10.0	86.2
N		8.7	87.5
	6+0		
N		12.0	84.2
TP	0.35	84.35	12.20
+3		2.0	82.4
Z		2.2	82.2
+8		1.8	82.6
S		+1.4	85.8
	6+1.3		
S Top Conc Wall		0.56	83.79
S		2.0	82.4
+4		4.0	80.4
Z		4.4	80.0
+6		4.4	80.0
N		1.9	82.5
	6+20.05 = WL 20' H		
N Top Cb		5.90	78.45
Gutter on Parings		5.99	78.36

84.35

1/2	on Paving	6.13	78.22
	Gutter on Paving	5.59	78.76
S	Top of Cb	5.20	79.15
S	Top of concrete	1.10	83.25
	HCb 30' 45"		
S	on Paving	6.14	78.21
1/2	" "	6.50	77.85
1/2	" "	6.88	77.47
TP	8.51	92.33 ✓	0.53
For Check		4.38	83.82 ✓
			87.95

on Curb  
H. Footing  
N. H. O. Curb  
V. 10' 30" 13  
8/10/03  
88.03





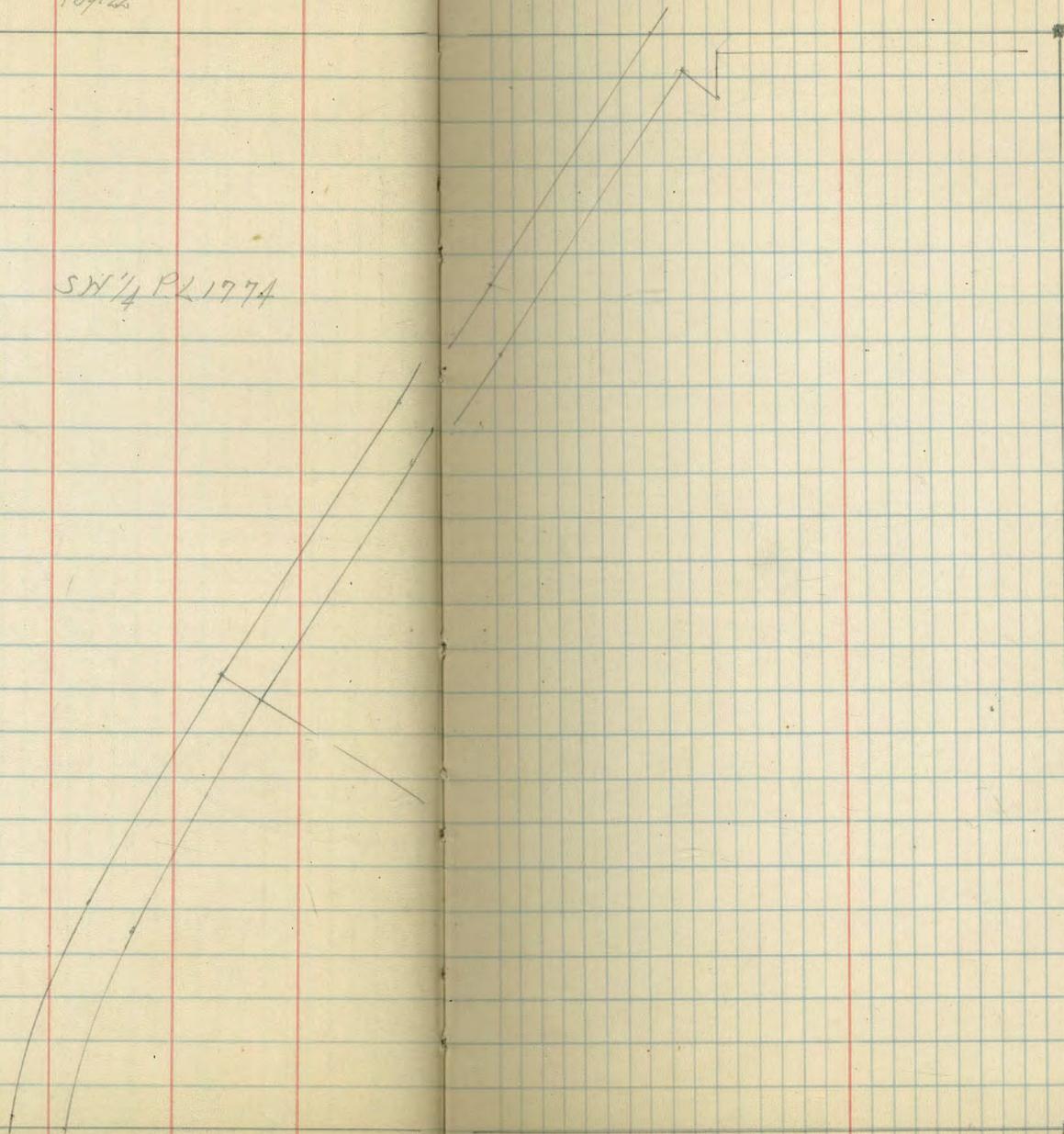
Page 23

1216917 No. 009

1418214 HT 8  
off

SW 1/4 PL 1774

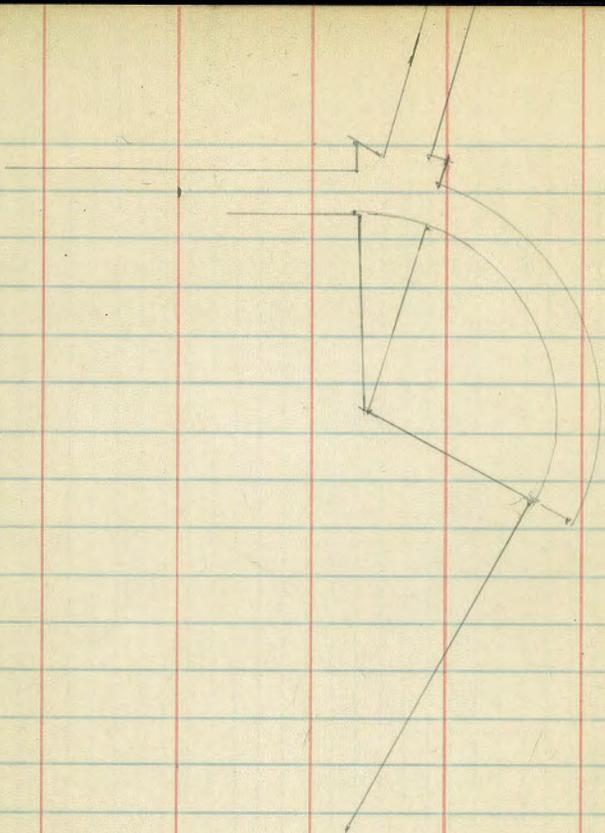
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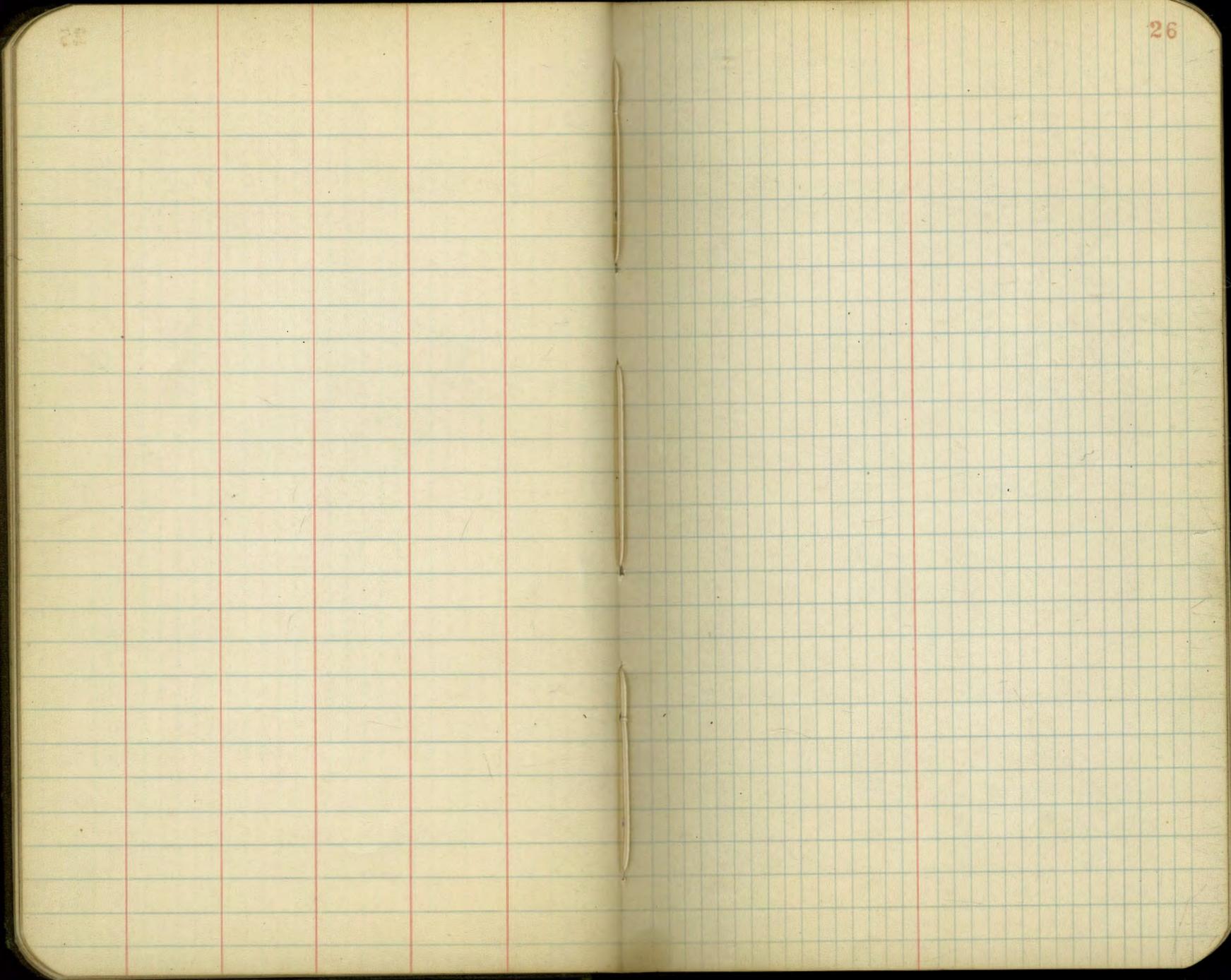


1371485

SFH 1774

26429.00









2+50

2+10

1+81

1+80 = Eucalyptus tree 38.8 ✓

1+75 = Jac. Tree 22.8 ✓

1+50

1+20

0+90

127.05

21

22

23

124.0	124.1	124.2	124.4	124.3	124.1
29.5	29.5	2.0	2.6	2.7	2.9
29.5	29.5	2.0	2.6	2.7	2.9

123.7	123.4	123.1	123.1	123.3	122.8
3.3	3.6	3.9	3.9	3.7	3.5
29.5	29.5	3.9	3.9	3.7	3.5

122.90

123.71	122.5	122.1	122.3	122.5	122.8	122.2	123.5
4.15	4.5	4.3	4.7	4.5	4.4	4.8	4.5
29.5	29.5	2.3	2.1	4.5	4.4	3.0	4.0

122.4	122.4	122.0	122.5	122.8	123.8	123.9	123.2
4.6	4.6	5.0	4.5	4.8	5.6	5.1	5.1
3.0	2.1	1.9	4.5	3.8	2.6	3.5	4.0

122.3	123.2	121.9	122.6	123.4	123.8	123.9	124.1	124.0
4.7	4.8	5.1	4.4	5.6	5.2	5.1	4.9	4.0
3.0	2.2	1.9	1.3	2.5	1.1	1.9	3.0	1.0

122.3	122.2	121.7	123.0	123.9	124.4	125.0	124.9	125.2
4.7	4.8	5.2	4.0	5.1	5.6	5.0	5.1	4.0
3.0	2.2	1.9	1.3	2.5	1.1	1.9	3.0	1.0

127.05

4+65 - Sky Power Pole 275 Ft.  
4+50

4+0

3+65

3+39.50 = E.L. Escudo

3+09.50 = Escudo 786 126.07

2+79.50 = W.L. Escudo - Sky Power Pole 275 Ft.

TP 9.09 133.93 2.21 124.84  
127.05

40.00	130.6	40.00	130.3	40.00	129.6	40.00	129.1	40.00	128.7	40.00	128.3
40.00	129.2	40.00	128.8	40.00	128.2	40.00	127.7	40.00	127.2	40.00	126.8
40.00	127.7	40.00	127.2	40.00	126.8	40.00	126.3	40.00	125.8	40.00	125.3
40.00	126.5	40.00	126.0	40.00	125.5	40.00	125.0	40.00	124.5	40.00	124.0
40.00	125.0	40.00	124.5	40.00	124.0	40.00	123.5	40.00	123.0	40.00	122.5
40.00	123.5	40.00	123.0	40.00	122.5	40.00	122.0	40.00	121.5	40.00	121.0
40.00	121.0	40.00	120.5	40.00	120.0	40.00	119.5	40.00	119.0	40.00	118.5
40.00	118.5	40.00	118.0	40.00	117.5	40.00	117.0	40.00	116.5	40.00	116.0
40.00	116.0	40.00	115.5	40.00	115.0	40.00	114.5	40.00	114.0	40.00	113.5
40.00	113.5	40.00	113.0	40.00	112.5	40.00	112.0	40.00	111.5	40.00	111.0
40.00	111.0	40.00	110.5	40.00	110.0	40.00	109.5	40.00	109.0	40.00	108.5
40.00	108.5	40.00	108.0	40.00	107.5	40.00	107.0	40.00	106.5	40.00	106.0
40.00	106.0	40.00	105.5	40.00	105.0	40.00	104.5	40.00	104.0	40.00	103.5
40.00	103.5	40.00	103.0	40.00	102.5	40.00	102.0	40.00	101.5	40.00	101.0
40.00	101.0	40.00	100.5	40.00	100.0	40.00	99.5	40.00	99.0	40.00	98.5
40.00	98.5	40.00	98.0	40.00	97.5	40.00	97.0	40.00	96.5	40.00	96.0
40.00	96.0	40.00	95.5	40.00	95.0	40.00	94.5	40.00	94.0	40.00	93.5
40.00	93.5	40.00	93.0	40.00	92.5	40.00	92.0	40.00	91.5	40.00	91.0
40.00	91.0	40.00	90.5	40.00	90.0	40.00	89.5	40.00	89.0	40.00	88.5
40.00	88.5	40.00	88.0	40.00	87.5	40.00	87.0	40.00	86.5	40.00	86.0
40.00	86.0	40.00	85.5	40.00	85.0	40.00	84.5	40.00	84.0	40.00	83.5
40.00	83.5	40.00	83.0	40.00	82.5	40.00	82.0	40.00	81.5	40.00	81.0
40.00	81.0	40.00	80.5	40.00	80.0	40.00	79.5	40.00	79.0	40.00	78.5
40.00	78.5	40.00	78.0	40.00	77.5	40.00	77.0	40.00	76.5	40.00	76.0
40.00	76.0	40.00	75.5	40.00	75.0	40.00	74.5	40.00	74.0	40.00	73.5
40.00	73.5	40.00	73.0	40.00	72.5	40.00	72.0	40.00	71.5	40.00	71.0
40.00	71.0	40.00	70.5	40.00	70.0	40.00	69.5	40.00	69.0	40.00	68.5
40.00	68.5	40.00	68.0	40.00	67.5	40.00	67.0	40.00	66.5	40.00	66.0
40.00	66.0	40.00	65.5	40.00	65.0	40.00	64.5	40.00	64.0	40.00	63.5
40.00	63.5	40.00	63.0	40.00	62.5	40.00	62.0	40.00	61.5	40.00	61.0
40.00	61.0	40.00	60.5	40.00	60.0	40.00	59.5	40.00	59.0	40.00	58.5
40.00	58.5	40.00	58.0	40.00	57.5	40.00	57.0	40.00	56.5	40.00	56.0
40.00	56.0	40.00	55.5	40.00	55.0	40.00	54.5	40.00	54.0	40.00	53.5
40.00	53.5	40.00	53.0	40.00	52.5	40.00	52.0	40.00	51.5	40.00	51.0
40.00	51.0	40.00	50.5	40.00	50.0	40.00	49.5	40.00	49.0	40.00	48.5
40.00	48.5	40.00	48.0	40.00	47.5	40.00	47.0	40.00	46.5	40.00	46.0
40.00	46.0	40.00	45.5	40.00	45.0	40.00	44.5	40.00	44.0	40.00	43.5
40.00	43.5	40.00	43.0	40.00	42.5	40.00	42.0	40.00	41.5	40.00	41.0
40.00	41.0	40.00	40.5	40.00	40.0	40.00	39.5	40.00	39.0	40.00	38.5
40.00	38.5	40.00	38.0	40.00	37.5	40.00	37.0	40.00	36.5	40.00	36.0
40.00	36.0	40.00	35.5	40.00	35.0	40.00	34.5	40.00	34.0	40.00	33.5
40.00	33.5	40.00	33.0	40.00	32.5	40.00	32.0	40.00	31.5	40.00	31.0
40.00	31.0	40.00	30.5	40.00	30.0	40.00	29.5	40.00	29.0	40.00	28.5
40.00	28.5	40.00	28.0	40.00	27.5	40.00	27.0	40.00	26.5	40.00	26.0
40.00	26.0	40.00	25.5	40.00	25.0	40.00	24.5	40.00	24.0	40.00	23.5
40.00	23.5	40.00	23.0	40.00	22.5	40.00	22.0	40.00	21.5	40.00	21.0
40.00	21.0	40.00	20.5	40.00	20.0	40.00	19.5	40.00	19.0	40.00	18.5
40.00	18.5	40.00	18.0	40.00	17.5	40.00	17.0	40.00	16.5	40.00	16.0
40.00	16.0	40.00	15.5	40.00	15.0	40.00	14.5	40.00	14.0	40.00	13.5
40.00	13.5	40.00	13.0	40.00	12.5	40.00	12.0	40.00	11.5	40.00	11.0
40.00	11.0	40.00	10.5	40.00	10.0	40.00	9.5	40.00	9.0	40.00	8.5
40.00	8.5	40.00	8.0	40.00	7.5	40.00	7.0	40.00	6.5	40.00	6.0
40.00	6.0	40.00	5.5	40.00	5.0	40.00	4.5	40.00	4.0	40.00	3.5
40.00	3.5	40.00	3.0	40.00	2.5	40.00	2.0	40.00	1.5	40.00	1.0
40.00	1.0	40.00	0.5	40.00	0.0	40.00	0.0	40.00	0.0	40.00	0.0

126.23

770

28.9

✓ 11/17/20  
11/17/20  
11/17/20  
11/17/20  
11/17/20

133.93

7+0

6+64.70 = EL 48<sup>135</sup>

6+34.70 = L 48<sup>16</sup>

TP 9.41 143.19 0.15 133.78

6+04.70 = NL 48<sup>155</sup>

6+02 = Sky Power Pole 22.4 Rh ✓

5+50

5+0

133.93

LT	L	PL
140.5 225 30	140.5 225 30	138.1 225 30
139.2 40 30	139.2 40 30	136.1 40 30
1382 5.0 10	1382 5.0 10	1361 5.0 10
1371 6.1 10	1371 6.1 10	1359 6.1 10
1361 7.1 10	1361 7.1 10	1351 7.1 10
1352 8.0 10	1352 8.0 10	1340 8.0 10
1351 8.1 10	1351 8.1 10	1335 8.1 10
1335 9.1 10	1335 9.1 10	1325 9.1 10
1327 10.1 10	1327 10.1 10	1311 10.1 10
1325 11.1 10	1325 11.1 10	1304 11.1 10
1322 12.1 10	1322 12.1 10	1300 12.1 10
1311 13.1 10	1311 13.1 10	1299 13.1 10
1308 14.1 10	1308 14.1 10	1291 14.1 10
1301 15.1 10	1301 15.1 10	1288 15.1 10
1298 16.1 10	1298 16.1 10	1278 16.1 10
1296 17.1 10	1296 17.1 10	1278 17.1 10
1285 18.1 10	1285 18.1 10	1278 18.1 10
1278 19.1 10	1278 19.1 10	1278 19.1 10
1278 20.1 10	1278 20.1 10	1278 20.1 10

22-Batt  
 Cobble  
 10K  
 22-Batt  
 Cobble  
 10K



11+25

11+0

10+75

10+50

TP 0.88 132.35 11.22 131.97

10+25

9+8977-FL Gloria

143.19

122.7	121.8	119.2	118.7	118.3	116.7	115.3
9.7	10.6	10.2	10.7	14.1	15.7	17.1
45	60	10		15	60	50

119.3	118.9	118.8	119.4	118.5	119.1	119.0
13.1	13.5	13.6	13.0	12.9	10.3	10.4
60	60	15		10	60	15

121.5	121.4	121.6	121.6	123.1	124.8	124.3	125.4
10.9	11.0	10.9	10.8	9.3	7.6	7.1	7.0
15	30	15		5	18	60	10

125.1	126.9	127.6	126.1	126.0	127.2	127.4	128.6	129.3	130.7	131.1	131.0
7.3	5.5	4.8	6.8	6.4	8.2	4.9	8.8	8.1	1.7	1.6	1.4
40	60	10	60	7	60		5	14	17	60	40

131.8	132.2	131.2	132.1	134.1	133.7	134.0
11.4	11.0	12.0	11.1	9.1	9.5	8.8
60	17	14		18	30	10

135.7	135.2	136.0	138.0	137.7	137.1
7.5	8.0	7.7	8.2	5.5	6.1
60	10	10	10	30	10

BM  
1370470: Wcb 49th St

7.64 12471

NET 1114  
Occasionally  
49th St

126.15 121.74 122.2 122.8 123.1 122.0 120.7 120.2

6.20 10.61 10.3 9.6 9.3 10.1 11.7 13.2  
50.00 28.8 30. 5. 10. 30. 10.

127.3 125.9 125.2 122.8 123.4 123.0 121.8 121.3  
5.1 6.5 7.7 9.6 9.0 9.4 10.6 11.1  
10 30 23 15 10 10 30 10

12195

12169.07 = Power or Pole 23.2 Rt

128.9 128.5 121.0 125.3 124.6 124.0 123.5  
3.5 3.9 5.1 7.1 7.8 8.1 8.9  
10 30 20 10 10 30 10

12130

129.9 129.7 128.8 127.5 126.2 125.3 124.7  
3.5 3.7 3.6 4.9 6.7 7.1 7.7  
10 30 10 10 10 30 10

1210

129.0 127.8 126.6 126.5 125.8 125.3  
3.1 4.6 5.8 5.9 6.6 7.1  
10 30 20 30 30 10

11775

128.5 127.3 123.7 123.4 123.8 123.2  
3.9 5.1 8.7 9.0 8.6 9.2  
10 30 15 30 30 10

11150

127.7 126.6 121.9 120.6 120.6 119.7 119.2  
4.7 5.8 10.5 11.8 11.8 13.7 13.7  
10 30 8 15 30 10

127.35

127.35

Cross Section Front 110  
47th St to 48th St

INDEXED  
EPB

Oct 23-40 35

St-N

St

pt-5

- 0+62
- 0+59 = 24" Pepper Tree 20.8 ft ✓
- 0+50 = 12" Olive Tree 21.2 ft ✓
- 0+31 = 3" Olive Tree 20.7 ft ✓
- 0+03'
- 0+02 = 5 1/2" Parrot Palm 22.2 ft of 2 ✓
- 0+0 = F 6 47th St
- 0-10 = F 6 47th St

Red. Plot. 10-31-40 C.B.H.  
Profile # 1896

						112.76	111.69
						3.30	3.27
						20.1	30.00
						2 1/2" Cap	30" Wall
						111.3	111.3 ✓
112.6	112.5	112.6	111.6	111.2	111.5	3.8	3.8
3.5	3.6	2.5	2.5	3.9	3.8	15	30
40	30	19	16	11			
112.0	111.9	112.0	110.9	110.9	110.9	111.2	111.3
3.1	3.2	3.1	4.2	4.2	4.2	3.9	3.8
40	30	19	18	18	18	30	30
111.2	111.2	110.1	110.2	109.3	109.3	109.2	110.9
3.9	3.9	5.0	4.9	5.8	5.8	5.9	4.7
40	30	25	17	13		18	20
109.7	109.51	109.03		109.05	108.67	108.92	109.18
5.4	5.55	6.03		6.01	6.39	6.08	5.88
30	19.7	19.7		30	19.8	19.8	30
		30=Cut			30	30	
109.51	108.95			108.78	108.49	108.92	
5.55	6.11			6.28	6.57	6.11	
30=Cut	30=Cut				30=Cut	30=Cut	
				115.06			

TP	5.93	115.06	8.44	109.13
BM	1.08	117.57		118.49

See R.P.  
Occupation  
47th St.

2+79.5 = W.L. Escuela

2+79 = Sky Power Pole 21.1 Rt ✓

2+50

2+0

TP 9.15 124.13 0.08 114.98

1+50

1+35 = Sky Power Pole 21.1 Rt of 2 ✓

1+23 = Garage on Rt

1+0

0+89 = 6" Olive Tree 21.1 Lt ✓

0+70 = 6" Olive Tree 21.7 Lt ✓

115.06

Lt L Rt

118.1	118.6	116.8	116.8	116.6	116.8	116.0
60	61	73	73	75	73	81
30	17	13		15	20	30

117.9	117.7	117.5	116.8	116.0	116.0	115.4	115.2
63	64	66	83	81	81	87	89
40	30	20	13		15	30	40

116.5	116.6	116.4	114.8	114.9	114.8	114.3	113.9
76	75	77	93	92	92	98	103
40	30	22	14		15	30	40

124.13

114.7	114.5	113.8	113.8	113.8	113.4	113.3
87	86	13	13	13	17	18
30	21	13		15	30	40

113.05 113.19

201  
207.5  
21 = W Gen  
Horse  
187  
307  
Horse  
8  
Cane  
Flour

113.91	113.59	113.4	112.1	112.3	112.3	112.5	112.4
115	117	12	20	28	28	26	27
30	29	25	15		15	23	30

215 Gen  
Stall  
25 Gen  
Walt

✓

115.06

TP 12.11 135.99 0.25 12388

4+75

4+63 - Sly Power Pole 216 Rt. ✓

4+50

4+0

3+60

3+39.50 - FL Escuela

3+09.50 - Escuela

124.13

4+ 2+ Pt

121.4	121.2	121.5	122.8	122.8	123.0	122.9	122.8
27 40	29 30	26 32	15 14	13	15	13 30	13 40

120.8	120.9	121.0	121.7	121.9	121.6	121.1	120.9	121.2
33 35	32 30	31 18	29 14	28	25 14	30 19	32 30	29 40

119.9	119.4	119.8	120.0	119.7	119.1	119.0	118.9
42 30	47 30	43 14	41	44 14	50 19	51 30	52 40

119.6	119.9	118.6	118.0	118.4	117.8	117.5	117.1
45 30	42 19	55 14	53	57 15	63 30	66 30	70 40

119.2	119.0	118.0	118.2	117.7	117.2	116.9
49 30	51 18	61 12	59	64 15	69 30	72 30

118.0	117.8	117.6	117.2	116.9
61 30	63 15	65 13	69 15	72 30

Franklin

BM

2.52

140.58

J2 Top of Hill  
Franklin  
+ 7875 ft

TP 8.93 143.10 1.82 134.17

6+08 - Sly Power Pole 20.8 ft of R ✓

6+047 - WL 48' 6" ST

5+75

5+50

5+25

5+0

135.99

LA

A

RT

38

131.4	132.1	131.8	131.5	132.3	133.8	134.0
4.6 30	5.9 30	4.2 7	4.5	3.7 13	2.3 18	2.0 30

128.9	129.8	130.5	129.0	128.8	129.0	131.8	131.5
7.1 40	6.2 30	5.5 18	7.0 14	7.7	7.0 13	4.2 17	4.5 30

127.0	126.8	127.7	127.2	127.2	127.4	129.2	129.5
9.0 40	9.2 30	8.3 18	8.8 13	8.8	8.6 14	6.8 18	6.5 30

124.9	125.4	126.3	125.7	125.6	125.9	127.2	127.4
11.1 40	10.6 30	9.7 17	10.3 13	10.4	10.1 15	8.8 19	8.3 30

123.8	124.8	125.2	124.4	124.2	124.4	125.2	125.4
12.2 40	11.2 30	10.8 30	11.6 16	11.8	11.6 15	10.8 30	10.6 40

135.99

Cross Section Escudo  
Ocean View Blvd to Imperial 17.10

INDEXED  
EPB

Oct 23 1939  
Surrey 39  
Markham  
Pt. Moore

2+50

119.71	117.6	117.6	117.2	117.7	118.5	118.5	119.2	119.6
857	10.7	10.7	11.1	10.6	9.8	9.8	9.1	8.7
30.7	30	27	25	23	23	8	18	30

Top Wall

2+0

120.90	119.0	119.0	118.7	119.2	119.9	120.1	120.8	121.5
746	9.3	9.3	9.6	9.1	8.4	8.2	7.5	6.8
30.7	30	27	25	23	23	7	20	30

Top Wall

1+50

122.29	120.7	120.7	120.3	120.8	121.4	121.7	122.8
599	7.6	7.6	8.0	7.5	6.9	6.6	5.5
30.7	30	27	25	23	15	15	30

Top Wall

1+0

123.62	122.4	122.5	121.9	122.6	123.1	123.6	124.6
466	5.9	5.8	6.4	5.7	5.2	4.9	3.7
30.7	30	27	25	23	15	15	30

Top Wall

0+50

124.95	123.8	123.9	123.4	124.0	124.6	125.0	126.1
3.23	4.5	4.4	4.9	4.5	3.7	3.3	2.7
30.7	30	27	25	23	23	30	30

Top Wall

0+0 = 174 Ocean View Blvd

124.8	125.7	126.7
3.5	2.6	1.6
30		30

BN 221 128.28

126.07

0+0 to 6  
Ocean View  
Escudo  
17.10

128.28

Red & Plot. 10-31-40 CBH.  
Profile 2726 & Leabenstein's

St. S Pt

4+50

114.5	114.8	115.3	114.5	114.9	115.9	115.9	116.1	117.1	117.7
75	73	67	75	71	61	61	59	49	43
40	30	26	27	23	13		14	17	30

4+0

114.1	115.1	114.5	115.0	115.1	116.0	116.0	116.1	116.7	116.4
76	69	75	70	69	60	60	59	53	46
40	30	26	24	18	13		9	16	30

3+50

115.4	114.5	115.6	116.3	116.0	116.2	116.3	117.1	117.6
74	66	75	64	57	60	58	57	49
40	30	26	24	15	12		8	16

TP

5.37 122.00 116.5 116.63

122.00

3+14

114.1	115.0	115.1	115.8	116.5	116.9	116.8	117.6	118.3
142	133	132	135	118	116	115	107	100
45	30	28	25	15		8	16	30

3+0

116.5	116.5	115.8	116.6	117.0	117.1	117.9	118.3
148	148	125	117	113	112	104	100
30	28	25	23		8	17	30

2198 = Hy Conc Wall on St

128.28

118.54

9.24  
30.7 = Top Wall  
21.5 = H

128.28

Escuela

47

7+55

120.62

1.38 ✓  
28.225  
67.000

7+50

119.2	119.3	119.4	118.7	119.1	119.4	120.0	120.5	121.0
2.8	2.7	2.6	3.3	2.9	2.6	2.0	1.5	1.0
40	30	18	13		14	30	30	40

7+35

120.62

1.38 ✓  
29.554  
67.000

7+0

118.7	118.8	118.8	118.7	118.7	119.0	120.1	120.2	120.7
3.3	3.2	3.2	3.8	3.3	3.0	1.9	1.8	1.3
40	30	20	13		14	17	30	40

6+0

115.5	115.7	116.1	116.9	116.5	116.7	119.0	117.4	116.8	116.5
6.5	6.3	5.9	5.1	5.5	5.3	5.0	4.6	5.2	5.5
40	30	18	14	13		8	10	15	30

5+50

114.4	114.7	115.2	116.2	115.9	116.2	116.5	116.9	116.3	116.9
7.6	7.3	6.8	5.8	5.1	5.8	5.5	5.1	5.2	5.1
40	30	16	13	11		10	11	13	30

5+0

114.3	114.6	114.9	116.9	116.0	116.2	117.0	117.7
7.7	7.4	7.1	6.1	6.0	5.8	5.0	4.3
40	30	18	13	12.5.00	15	18	30

122.00

TP 9.78 125.89 5.89 116.11

9+0

114.2 114.5 115.0 116.2 116.2 116.3 116.1 117.4 117.6  
 7.8 7.5 7.0 5.7 5.8 5.7 5.9 4.6 4.4  
 40 30 30 13 13 11 16 30 40

8+50

114.0 114.4 115.4 116.7 117.0 116.9 116.2 117.5 119.0  
 8.0 7.6 6.6 5.3 5.0 5.1 5.8 4.5 3.0  
 40 30 35 13 11 11 21 30 40

8+26

115.4 116.3 117.5 117.2 117.6  
 6.6 5.7 4.5 4.8 4.4  
 40 30 33 13 44

8+20

116.8 117.6 117.8 117.9 117.7 117.6 118.2 118.0 119.1  
 5.2 4.4 4.2 4.7 4.3 4.4 3.8 4.0 3.9  
 40 30 34 13 40 13 18 30 40

8+0

116.8 117.5 117.7 118.1 118.2 119.5 119.2 119.5  
 5.2 4.5 4.3 3.9 3.8 2.5 3.8 4.5  
 40 30 13 15 18 30 40

7+72

122.00

122.00

120.73

127.7  
 127.2 - 114.5  
 112.7

10+65

115.9	116.2	116.7	117.5	117.5	117.7	118.7	119.0	119.0
10.0	9.7	9.2	8.4	8.4	8.2	7.7	6.9	6.9
40	30	18	13		4	20	30	40

10+35

117.0	118.3	117.9	117.1	117.5	117.4	118.6	119.2	119.3
8.9	7.6	8.0	8.8	8.7	8.5	7.1	6.7	6.6
40	30	20	12		14	19	30	40

10+0

116.5	116.8	116.4	116.7	116.9	117.0	117.5	117.7	117.2
9.4	9.1	9.5	9.2	9.0	8.9	8.4	8.2	8.7
40	30	24	15		16	19	30	40

9+75

116.3	116.6	116.3	116.4	116.5	116.7	115.9	116.0	116.3
9.6	9.3	9.6	9.5	9.4	9.2	10.0	9.9	9.6
40	30	20	10		16	17	30	40

9+50

114.6	114.6	114.8	116.5	116.2	116.3	116.5	115.8	116.1	115.8
11.3	11.3	11.1	9.4	9.7	9.6	9.4	10.1	9.8	10.1
40	30	23	13	8		15	17	30	40

9+15 = 18' Corp. Culy in bad order

12589

11426

116.3

11.6

11418'

Corp. Culy

12589

11486

11.0

16.4

11418'

Corp. Culy

BM 1.45 124.44  
12+98.6 = S. Ede. Paving

on Lt & Imperial Escuela

12+7438 = S. L. Imperial

12+50

12+22 = My. Hocho. Pdr 22.8 Lt. ✓

12+0

11+50

11+0

12589

Lt L R

122.87 124.40 125.74  
3.02 1.49 0.15  
30.00 30.00 30.00

121.8 122.7 123.1 123.3 123.9 124.2 125.3 125.4  
1.1 0.3 2.8 2.6 3.0 1.7 0.6 0.5  
30. 30. 30. 30. 30. 30. 30. 30.

120.5 120.7 121.1 121.7 121.9 121.9 122.5 124.3 125.0 125.6  
5.1 5.2 4.8 4.3 4.0 4.0 3.1 1.6 0.9 0.3  
40. 30. 30. 30. 30. 30. 30. 30. 30. 30.

118.7 118.9 119.1 119.9 119.7 119.8 119.8 120.3 120.1 121.3 122.3  
7.7 7.0 6.8 6.0 6.2 6.1 6.1 5.6 5.8 4.6 3.6  
40 30 31 18 15 4 5 18 30 40

116.8 117.2 118.0 118.8 118.5 118.6 118.5 119.0 118.6 119.8 120.5 119.5  
9.1 8.7 7.9 7.1 7.4 7.3 7.4 6.9 7.2 6.4 5.4 6.4  
40 30 18 15 11 11 8 14 14 30 40

115.9 116.0 117.6 118.3 117.7 117.8 117.7 118.1 117.8 118.1 119.0  
10.6 9.9 8.3 7.6 8.2 8.1 8.2 7.8 8.1 7.5 6.9  
40 30 16 14 11 8 8 25 30 40

125.89

Cross Section 48th St.  
Ocean View Blvd. to Imperial Ave.

INDEXED  
EPB

Lt=111

2

Oct. 25/40  
Rt. E 45

1+60 = Sly Picket Fence 19.5 ft. ✓

1+50

134.6	134.9	135.3	136.4	136.8
6.5 30	6.3 15	5.8	4.7 9	4.3 30

1+30

135.9	135.1	135.6	137.0	138.9
5.2 30	6.0 15	5.5	4.1 15	2.2 30

1+0

136.4	136.1	135.7	136.0	137.7	139.4
4.7 30	5.0 30	5.4 15	5.1	3.4 15	1.7 30

0+50

136.1	136.7	136.2	136.7	137.5	139.5
5.0 30	4.4 18	4.9 14	4.4	3.6 18	1.6 30

0+30

136.0	136.8	136.2	136.6	138.9	139.57	139.68
5.1 30	4.3 21	4.9 14	4.5	2.2 23	1.53 27	1.15 30 on right

Conc. Wall ✓

0+0 = H. Ocean View Blvd.

134.9	134.2	139.1
6.2 30	4.9	2.0 30

B.M. 6.39 14110

134.71  
Hub  
Ocean View  
+ 48th St.

141.10

Red+ Plot. 11-1-40 CBH

4+84 = 54 Wire Fence 29.5 ft ✓

4+50

4+0

3+50

TP 7.31 143.07 5.34 125.76

3+0

2+50

2+0

1+90 = 14 Picket Fence 19.5 ft. ✓

141.10

Oct 28-49 46

1353	1359	137.0	136.6	137.0	138.4	140.7	141.7
7.8	7.2	6.1	6.5	6.1	4.7	3.4	1.4
40	30	16	14		10	30	40

1353	1362	1369	137.1	136.7	137.2	137.7	139.0	139.8	140.5	141.4
7.8	6.9	6.2	6.0	6.4	5.9	5.4	4.1	5.3	2.6	1.7
40	30	28	16	14	19	5.4	10	20	30	40

134.7	135.3	135.9	136.6	136.1	136.6	138.1	138.6	140.0	141.1
8.4	7.8	7.2	6.5	7.0	6.5	5.0	4.5	6.1	5.0
40	30	25	17	14		8	18	30	40

143.07

135.0	135.9	135.4	136.3	138.3	137.6	139.5
6.1	5.2	5.7	4.8	2.8	3.5	1.6
30	18	14		7	10	30

132.7	133.6	134.9	135.3	137.1	136.3	137.6
8.4	7.5	6.2	5.8	4.9	4.8	5.5
40	30	18		8	11	30

133.6	134.3	134.7	135.5	136.2
7.5	6.8	6.4	5.6	4.9
30	15		8	30

141.10

6+67.33 - N. L. Franklin

6+37.33 -  $\frac{1}{2}$  Franklin

BM

2.48

140.59

5 FT Top of  
Franklin  
48' 5"

6+07.33 - N. L. Franklin - Fict Hyd 220 Ft ✓

5775

5750

5+33 - N. L. Wire Fence 295 Ft

570

143.07

4

5

Rt

47

1314	1323	1323	1330	133.9	134.8
117	108	108	10.1	9.3	8.8
30	24	14		15	30

1315	1337	1346	1353	1379	1381
116	91	8.5	7.8	5.2	5.0
30	15		9	25	30

1348	1359	1353	1366	1378	1383	1397
8.8	7.7	7.8	6.5	5.3	4.8	5.7
30	19	15		7	19	30

1353	1359	1368	1364	1369	1372	1384	1409	1420
7.8	7.7	6.3	6.7	6.8	5.9	4.7	2.7	1.1
40	30	18	15	1		10	30	40

1355	1362	1371	1375	1369	1376	1380	1387	139.6	1418	1423
26	6.9	6.0	5.6	6.2	5.5	5.1	4.4	3.5	1.8	0.8
40	30	28	17	14		8	4	14	30	40

1356	1361	1369	1365	1374	1382	1395	1407	1417	1424
7.5	7.0	6.7	6.6	5.7	4.9	3.6	3.1	1.4	0.9
40	30	18	14		5	7	17	30	40

143.07

9+0

1253	1247	1248	1252	1250	1250	1250	1249
$\frac{76}{40}$	$\frac{82}{30}$	$\frac{81}{17}$	$\frac{77}{8}$	$\frac{79}{}$	$\frac{79}{10}$	$\frac{79}{30}$	$\frac{80}{40}$

8+70

1254	1252	1251	1255	1254	1256	1253	1252
$\frac{75}{40}$	$\frac{77}{30}$	$\frac{78}{13}$	$\frac{78}{9}$	$\frac{75}{}$	$\frac{72}{15}$	$\frac{76}{30}$	$\frac{77}{40}$

8+50

1262	1260	1256	1260	1256	1258	1261	1269	1274	1284	1286
$\frac{67}{40}$	$\frac{69}{30}$	$\frac{73}{30}$	$\frac{69}{12}$	$\frac{73}{10}$	$\frac{71}{}$	$\frac{68}{18}$	$\frac{60}{38}$	$\frac{55}{38}$	$\frac{15}{30}$	$\frac{13}{40}$

8+0

1270	1264	1263	1270	1266	1268	1273	1276	1280
$\frac{59}{40}$	$\frac{65}{30}$	$\frac{66}{17}$	$\frac{59}{15}$	$\frac{63}{12}$	$\frac{61}{}$	$\frac{56}{15}$	$\frac{53}{30}$	$\frac{49}{40}$

7+50

1271	1281	1286	1279	1281	1288	1297	1300
$\frac{58}{40}$	$\frac{18}{30}$	$\frac{43}{36}$	$\frac{50}{19}$	$\frac{48}{}$	$\frac{41}{15}$	$\frac{37}{30}$	$\frac{29}{40}$

TP

2.16

132.94

1239

130.78

132.94

7+0

1296	1297	1300	1307	1316	1321	1331	1329	1329
$\frac{136}{40}$	$\frac{124}{30}$	$\frac{131}{15}$	$\frac{124}{}$	$\frac{115}{4}$	$\frac{110}{15}$	$\frac{100}{20}$	$\frac{103}{30}$	$\frac{103}{40}$

143.07

143.07

12+0

1329	1333	1335	1337	1358	1378
$\frac{80}{30}$	$\frac{76}{15}$	$\frac{74}{15}$	$\frac{72}{15}$	$\frac{71}{30}$	$\frac{71}{10}$

11+63 = Fly Wire Fence 288 ft

11+50

1303	1304	1311	1313	1319	1317	1323	1367
$\frac{106}{10}$	$\frac{105}{30}$	$\frac{98}{25}$	$\frac{96}{15}$	$\frac{90}{15}$	$\frac{92}{18}$	$\frac{86}{30}$	$\frac{77}{10}$

TP 8.99 140.94 0.99 131.95

140.94

11+0

1293	1294	1297	1299	1298	1294	1301	1301	1333
$\frac{86}{10}$	$\frac{85}{30}$	$\frac{82}{15}$	$\frac{80}{15}$	$\frac{81}{15}$	$\frac{85}{18}$	$\frac{78}{21}$	$\frac{78}{30}$	$\frac{70}{10}$

10+64 = Fly Wire Fence 286 ft

10+50

1278	1275	1279	1277	1288	1308
$\frac{61}{30}$	$\frac{64}{8}$	$\frac{60}{15}$	$\frac{63}{15}$	$\frac{61}{30}$	$\frac{61}{10}$

10+0

1242	1254	1261	1265	1262	1262	1264	1270
$\frac{87}{10}$	$\frac{75}{30}$	$\frac{68}{25}$	$\frac{64}{15}$	$\frac{67}{15}$	$\frac{67}{15}$	$\frac{65}{10}$	$\frac{66}{30}$

9+50

1232	1243	1251	1256	1255	1257	1253	1258	1262
$\frac{97}{10}$	$\frac{86}{30}$	$\frac{78}{15}$	$\frac{78}{15}$	$\frac{74}{15}$	$\frac{72}{15}$	$\frac{76}{18}$	$\frac{76}{30}$	$\frac{67}{10}$

132.94

132.94

Lt

L

PA

BM

1305

13789

on Lt.  
Imperial +  
48 1/2

12+8993-5 Edge Paving

135.89 136.67 137.76 138.83 139.47

5.05 4.27 3.18 2.11 1.47  
5000 Pav 3000 Pav on Paving 3000 Pav 15000 Pav

12+6893-5 Imperial

1358 1359 1363 1369 1376

5.1 5.0 4.6 4.0 3.3  
30 18 1.6 30

12+50

1347 1350 1349 1354 1361 1362 1381

6.2 5.9 6.0 5.5 4.8 4.7 3.8  
40 30 15 12 30 20

140.94

140.94

Cross Section Glosio St  
Ocean View Blvd to Franklin

INDEXED  
E/FB

St-21

2

00728-10  
51  
P.F. No. 7  
22 17 001

2+50

1432	142.8	142.3	141.5	141.7	141.7	140.9	140.5	139.6	139.9
2.6	3.0	3.5	4.3	4.1	4.1	4.9	5.3	6.2	6.8
40	30	17	13	6	6	11	25	30	40

2+0

142.5	142.5	142.3	141.9	140.1	139.9	140.0	139.4	138.1	136.3
3.3	3.3	3.5	4.8	5.7	5.9	5.8	6.4	7.7	9.5
40	30	25	14	12	14	14	25	30	40

1+50

141.8	141.9	140.7	139.7	139.4	139.1	138.3	137.2	135.7
4.0	3.9	5.1	6.1	6.4	6.7	7.5	8.6	10.1
40	30	14	12	6	13	26	30	40

1+0

140.6	140.7	140.1	139.3	139.5	139.3	138.5	137.8	137.3	136.6
5.2	5.1	5.7	6.5	6.3	6.5	7.3	8.0	8.5	9.2
40	30	28	12	6	8	11	20	30	40

0+50

140.6	140.5	138.7	138.4	138.0	136.8	136.5
5.2	5.3	7.1	7.4	7.8	9.0	9.3
40	30	15	7	8	30	40

0+0 = 1/2 Ocean View Blvd

139.8	139.8	139.0	138.9	137.0	136.5	135.5
6.0	6.0	6.8	6.9	8.8	9.3	10.3
30	14	9	6	10	21	30

BM

7.90

145.84

137.94

Hub  
Ocean View  
+ 9/10/10  
Post 28

14 584

Red & Plot 11-1-40 C.B.H.

5+14 - W4 Power Pole 16.7 ✓

5+0

4+53 : 8' Tree 26' Rt. ✓

4+50

4+38

4+16 - W4 Anchor Pole 15.6 ✓

4+0

TP 7.10 152.15 0.79 145.05

3+50

3+0

145.84

147.6	147.7	147.5	145.9	145.3	144.7	144.5	144.2
4.6	4.5	4.7	6.3	6.9	7.5	7.7	8.0
40	30	14	9		15	30	40

147.8	147.8	146.4	146.2	145.5	145.5	145.9
4.4	4.4	5.8	6.0	6.7	6.7	7.3
40	30	13		15	30	40

145.23

6.92 ✓  
2.5.5  
2.25.5  
No. 590

146.7	146.7	146.7	146.1	145.6	145.6	144.7	144.4
5.5	5.5	5.5	6.1	6.6	6.6	7.5	7.8
40	30	16	11		13	30	40

152.15

145.4	145.4	145.8	144.8	144.6	144.5	144.0	144.4	144.1	143.7	142.7
0.4	0.4	0.0	1.0	1.8	1.3	1.8	1.4	1.7	2.1	3.1
40	36	14	12		7	10	14	25	30	40

144.0	143.6	143.0	142.9	142.8	142.1	142.7	142.5	141.8	141.3
1.8	2.2	2.8	2.9	3.0	3.7	3.1	3.3	4.0	4.5
40	30	15		8	10	13	25	30	40

145.84

BM			1.73	116.47
TP	8.37	118.20	9.90	109.83

SW BP  
050021107  
47755  
116.49

TP	2.18	119.73	11.75	116.55
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BM			3.88	124.42
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AVT 2  
Imperial  
Escuela  
124.44

TP	0.28	128.30	10.97	128.02
----	------	--------	-------	--------

BM			1.05	137.94
----	--	--	------	--------

AVT 2  
Imperial  
1379.44  
13789

TP	8.04	138.99	12.15	130.95
----	------	--------	-------	--------

TP	2.54	143.10	11.59	140.56
----	------	--------	-------	--------

SE Top H<sub>2</sub>O  
Franklin  
140.56

6+04.44 - S. L. Franklin

147.1	146.7	146.2	146.1	145.4	145.3
5.1	5.5	6.0	6.1	6.8	6.9
30	15	12		18	30

5+50

147.9	147.8	146.7	145.6	145.1	145.0	144.5	144.4
7.8	1.1	5.5	6.6	7.1	7.7	7.7	7.8
40	30	15	10		17	30	40

5+16

152.15

152.15

142.28

9.87

2.00  
Carc Floor

2 Levels T St. Escudela St 400' East  
 T St. Produced From the West  
 East of Escudela

BM	11.14	127.63	116.49	SWBP Occochee St
TP	10.50	137.51	0.62	127.01
0+0 = Ek Escudela		2.8		134.7
+30		2.1		135.4
+40		2.5		135.0
+70		7.8		129.7
TP	1.30	126.46	12.35	125.16
1+0		2.5		124.0
+25		8.0		118.5
TP	0.63	114.86	12.23	114.23
+50		2.8		112.1
+75		9.2		105.7
TP	2.08	104.75	12.19	102.67
2+0		4.5		100.3
+30 = bottom marsh		11.4		93.4
+60		4.8		100.0
+70		3.6		101.2
+90		4.0		100.8
3+0		2.6		102.2
TP	12.46	116.98	0.23	104.53
+25		10.7		106.3
+50		9.3		107.7
+75		6.6		110.4
4+0		5.4		111.6
+28 = opp. Fick Hyd		4.5		112.5

Rect. Plot  
 10-91-40  
 G.R.H.  
 on Koebenstem  
 Profile

INDEXED  
 E.F.G.

Oct 29-40  
 J. J. J.  
 Markham  
 W. Moore

54

116.98

BM

0.02

116.96

0.2700  
 Fick Hyd  
 33' Hyd  
 4+28

Cross Section Franklin Ave.  
48th St to 49th St.

INDEXED  
EPB

1+27 Sly Power Pole 208 ft  
1+25

1+0

0+75

0+50

0+25

0+0 = EA 48 1/2 St.

Notes Red Plot 11-14-40 CBH.

BM

9.53

150.11

14058

SE Top of  
Franklin  
48th St

11-14

2

RT-1

Nov 13-40  
S. S. 500 55  
Northway  
2d Mount

139.6	140.8	142.9	143.7	144.0	144.6	145.2
10.5	9.3	7.2	6.4	6.1	5.5	4.9
40	30	15		14	16	30

138.6	138.8	141.2	142.4	142.9	144.6
11.5	11.3	8.9	7.7	7.2	5.5
40	30	15		15	30

137.3	138.8	139.6	141.9	142.2	144.0
12.8	11.3	10.5	8.2	7.9	6.1
40	30	14		15	30

136.4	138.7	139.7	141.4	141.1	141.6	143.0
13.7	11.4	10.4	8.7	9.0	8.5	7.1
40	30	24		4	17	30

135.8	136.4	137.9	138.8	139.8	141.1
14.3	13.7	13.2	11.3	10.3	9.0
40	30	20		15	30

134.6	138.2	139.4
15.5	11.9	10.7
30		30

150.11

2+95 = 2 Gloria

2+65 = H L Gloria = Sky Power Pole 204 RT  
= H H Anchor Pole 180 Lt.

2+25

2+0

1+75

1+50

150.11

Lt

Z

Rt

56

891

1438	1450	1463	1458	1460	1460
6.3 40	5.1 30	3.8 15	4.3	4.1 15	4.1 30

1459	1459	1461	1463	1466	1473	1470
4.8 40	4.3 30	4.0 15	3.8	3.5 16	2.8 20	3.1 30

1442	1445	1438	1443	1462	1469	1476	1480
5.9 40	5.6 30	6.3 30	5.8 10	3.9	3.2 13	2.5 15	2.1 30

1444	1449	1449	1459	1462	1467	1473
5.7 40	5.2 30	5.2 15	4.2	3.9 13	3.4 15	2.8 20

1418	1419	1446	1451	1451	145.6	1466
8.3 40	8.3 30	5.5 9	5.0	5.9 14	4.5 16	3.5 30

1416	1409	1416	1441	1446	144.6	1452	1458
8.5 40	9.7 30	8.5 18	6.0 8	5.5	5.5 15	4.9 16	4.3 30

150.11

4+59 = Sly Power Pole 20.8 RT

4+50

4+25

TP 6.67 151.66 5.12 144.99

4+0

3+75

3+50

3+25 = FLG/or 10

150.11

Lt

R

RT

146.2	146.1	145.9	145.4	145.4	145.7
5.5	5.6	5.8	6.3	6.3	6.0
10	30	15		15	30

146.2	145.9	146.1	145.3	145.1	144.9	144.8
5.5	5.8	5.6	6.4	6.6	6.8	6.9
10	30	11	8		15	30

151.66

145.8	145.5	145.8	144.8	144.5	144.6
4.3	4.6	4.3	5.3	5.6	5.5
10	30	18		15	30

145.2	145.0	145.4	144.7	144.8	144.7
4.9	5.1	4.7	5.4	5.3	5.4
10	30	15		15	30

144.6	144.2	145.5	144.8	144.7	144.7
5.5	5.9	4.6	5.3	5.4	5.4
10	30	10		15	30

144.1	144.7	145.7	146.1	145.2	145.2	146.0	145.3
6.0	5.4	4.4	4.0	4.9	4.9	5.1	4.8
10	30	30	10	8		15	30

150.11

6431 = Sky Power Pole 230 ft

640

5775

5750

5725

570

4175

157.66

64

2

RT

58

148.0	147.4	146.5	146.3	146.0
3.7	4.3	5.2	5.4	5.7
30	15		15	30

148.4	148.0	147.9	147.6	147.2	146.7
3.3	3.7	3.8	4.1	4.5	5.0
40	30	15		15	30

150.3	149.9	148.3	147.6	147.5	148.0
1.4	1.8	3.4	4.1	4.3	3.7
40	30	15		15	30

147.0	147.2	148.1	148.2	147.7	147.0
4.7	4.5	3.6	3.5	4.0	4.7
40	30	15		15	30

146.8	146.4	146.8	147.0	146.9	147.2
4.9	5.3	4.9	4.7	4.8	4.5
40	30	15		15	30

146.6	147.3	147.7	147.2	146.2	145.4
5.1	4.4	4.0	4.5	5.5	6.3
40	30	15		15	30

157.66

St.

S

RA

BM

343

148.23

SE Top of Hyd  
Franklin  
49150

St 38 - W Curb Line 49 1/2 St

147.52	146.71	146.4	146.1	146.0	145.6	145.3	145.46	145.30
4.14	4.95	5.3	5.6	5.7	6.1	6.4	6.20	6.36
60-cb top	30-cb top	30	15		15	30	30-cb top	30-cb top

St 33 - W Curb Line 07 49 1/2 St

146.78	146.71	146.1	146.1	146.1	145.6	145.64	145.57
4.88	4.95	5.6	5.6	5.6	6.1	6.07	6.09
30-cb top	209	209	15		15	21.8-cb top	30-cb top

151.66

151.66



(2)  
 cb 4.04 2.40  
 Pav 4.68 1.76

(3)  
 cb 4.00 2.44  
 Pav 4.60 1.84

(4)  
 cb 3.94 2.50

(5) = E.C.  
 cb 4.09 2.35

cb 40' E of E.C. 4.04 2.40

### Pond N of Courts

Water level 7.30 - 0.86  
 Bottom 10.0 - 3.56

### Pond S of Courts

Water level 8.40 1.96  
 Bottom 9.0 2.56

Pond S of Courts  
 Under Stahlman Club House  
 Water level 7.60 - 1.16  
 Bottom 9.6 - 3.2  
 Conc. foundation acts as dam

### El-on Pav. E.L. Pacific

S cb line Courts 4.43 + 2.01  
 S 1/4 " " 4.11 2.33  
 E " " 4.03 2.41  
 N 1/4 " " 4.08 2.36  
 N cb line " 4.37 2.07

Top Hyd Pac. + Courts 2.65 3.79 ? New Hyd

<sup>at</sup>  
 E.L. Conc. Box drain Bend 9.43 - 2.99 30' E of Pac. EL  
 " inlet to Cut-Hole Box 8.93 - 2.49

T.P. 7.31 - 7.93 5.82 0.62

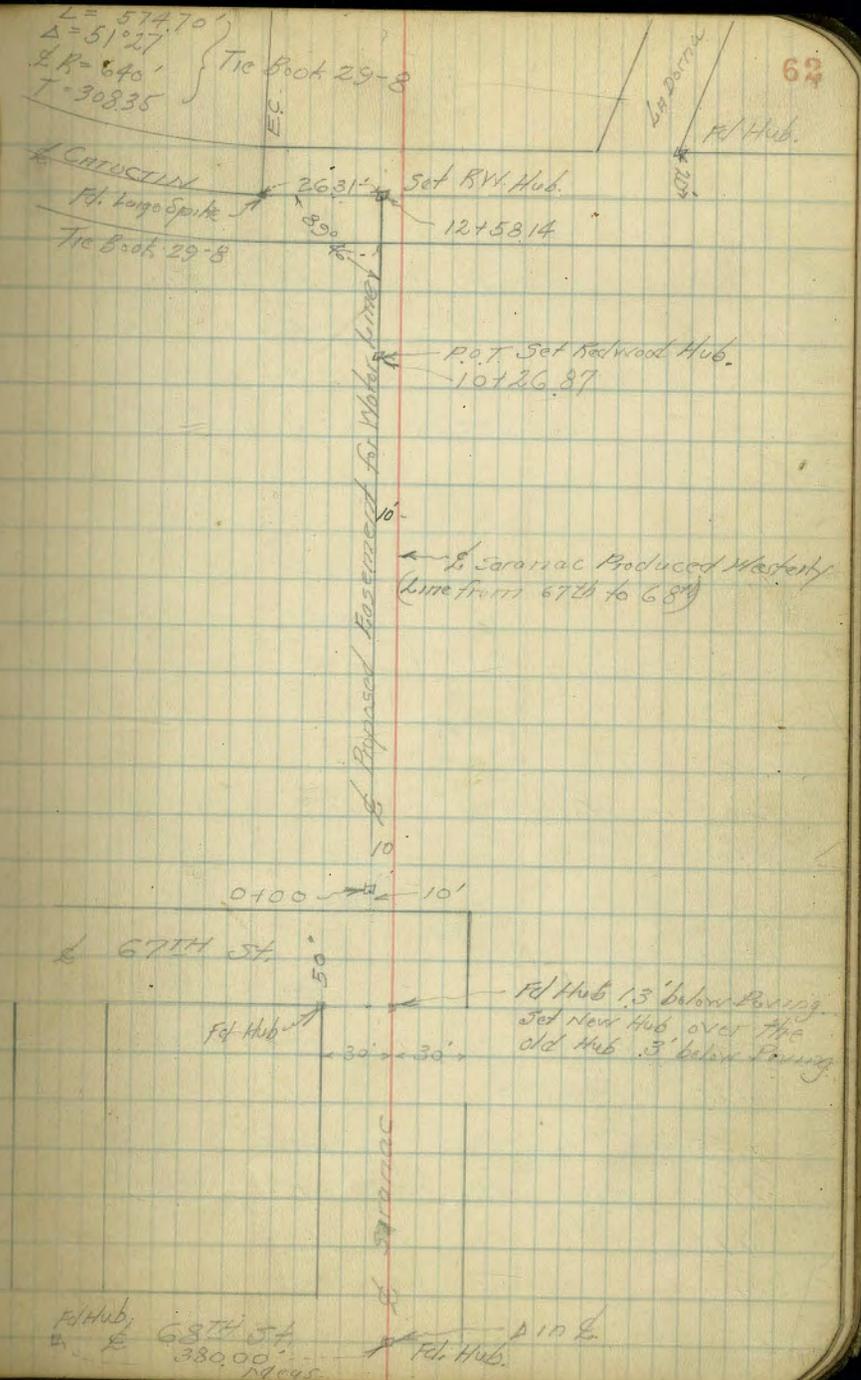
Clear out of Box drain at Kertz + Courts  
 on iron grate 5.01 2.92  
 E.L. Box 9.81 - 1.88

Walker  
Bliss  
Isbell  
3-5-41

Location for Easement  
in La Mesa Colony  
from 67th St. to Collectin Drive  
on a Prolongation of a line  
10' South of E. Saranac St.  
Hubs at E. 68th + 67th Streets used  
to Produce Line West.  
Line run on true & proposed easement.

	1.91	455.61		453.70	SV. 8P 67th St. Cap
T.P.	2.80	499.11	9.30	446.31	
W.L. 67th = 0+00 on Hub.			2.44		
+50			2.5		
1700			54		
+35			9.4		
+55			12.5		
T.P.	12.98	437.81	12.68	436.43	
2+00			8.4		
+25			11.5		
T.P.	0.40	425.15	13.06	424.75	
2+35			0.8		
+50			6.8		
+70 - Bottom of Wash			16.6		
3+00			12.3		
+50			7.4		
+50			7.3		
+80			4.6		
4+00			4.2		

Cont P. 63



4+25			4.5	
+50			6.4	
+65			7.5	
T.P.	0.72	413.47	12.40	412.75
5+100			2.4	
+125			3.3	
T.P.	0.80	401.38	12.89	400.58
5+50			3.8	
+65			8.3	
+77			14.4	
+93			17.1	
+98 = Bottom Wash			19.3	
6+05			16.3	
+35			15.2	
+45 in Wash			15.8	
+55			14.0	
+70			12.6	
+88			9.1	
7+00			3.3	
T.P.	12.72	413.81	0.29	401.09
+25			6.6	
+45			0.8	
T.P.	12.66	426.35	0.12	413.69
+75			7.1	
8+00			3.2	
T.P.	11.35	437.43	0.27	426.08

on Bolt  
8120

8+40			9.2	
+80			4.4	
9+00			1.6	
T.P.	12.20	449.60	0.03	437.40
+20			10.8	
+50			6.6	
9+85			1.7	
T.P.	10.26	459.04	0.82	448.78
10+26.87 on Hub.			7.46	
+50			6.1	
11+00			5.0	
+50			4.3	
12+00			4.2	
+35			4.4	
12+58.14 on Hub = Collection			4.83	
+58.14 on Ground			4.7	
T.P.	6.29	459.45	5.88	453.16
SE Top Hyd.			2.48	456.97
T.P.	3.67	456.83	6.29	453.16
T.P.	6.94	459.79	3.98	452.85
T.P.	6.45	464.37	1.87	457.92
T.P.	6.50	467.91	2.96	461.41
T.P.	5.61	469.26	4.26	463.65
T.P.	4.52	469.66	4.12	465.14
chk. N.W. 8P El Cuyos Collection			4.08	465.58
				465.66 = 8P
				0.08 Error

Cross Section Rosecrans St  
For Sidewalk on West Side  
Canon St to Rogers

Indexed  
LVI

May 19. 41  
Sisson  
North 4007  
Mount  
Albion 64

BM 117 32.08 ✓ 30.91  
TP 398 24.93 ✓ 11.13 20.95 ✓  
W.W. R.P.  
Canon St  
Locust

0+75.1 - Sky Solid Walk

W.L. 398 20.95

+10 = Wcb Top 4.50 20.43

0+85

W.L. 39 21.0

Wcb 10 Drive 49 20.0

+0

W.L. 3.4 21.5

+8 40 20.9

Wcb 42 20.7

+25

W.L. 29 22.0

+3 26 21.3

Wcb 394 20.99

+60

W.L. 23 22.7

+3 29 22.0

Wcb 348 21.45

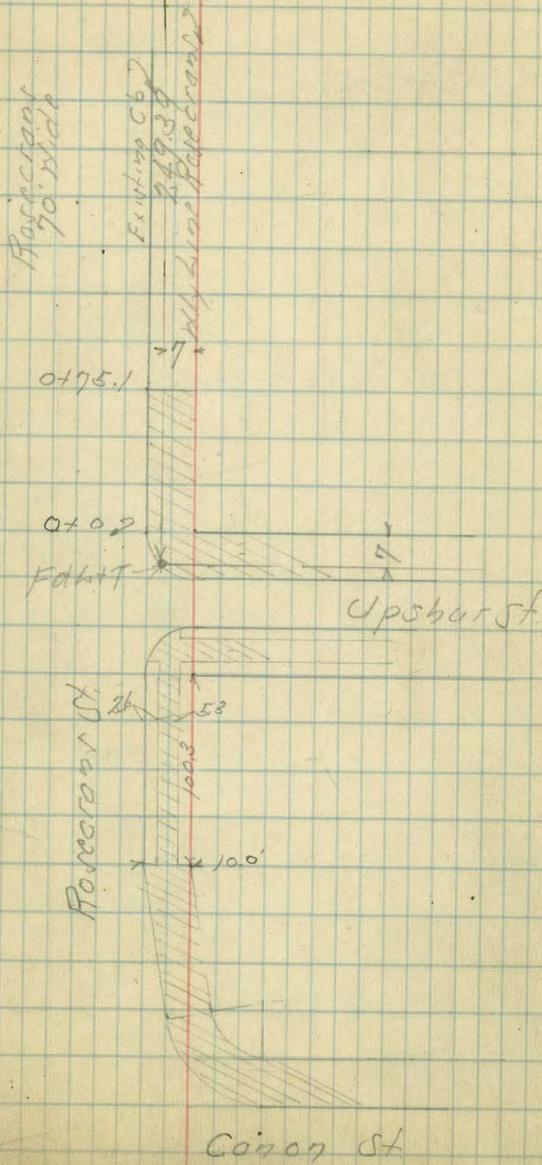
+75

W.L. 19 23.0

+8 28 22.1

+8 29 22.0

Wcb 327 21.66



24.93

2+0

H.L.	1.8	23.1
+3	2.3	22.6
H.Cb Top	2.88	22.05

2+25

H.L.	1.5	23.4
+3	2.0	22.9
H.Cb	2.61	22.32

2+37.5 C.B.C

H.L.	1.8	23.1
+2	2.3	22.6
H.Cb	2.46	22.47

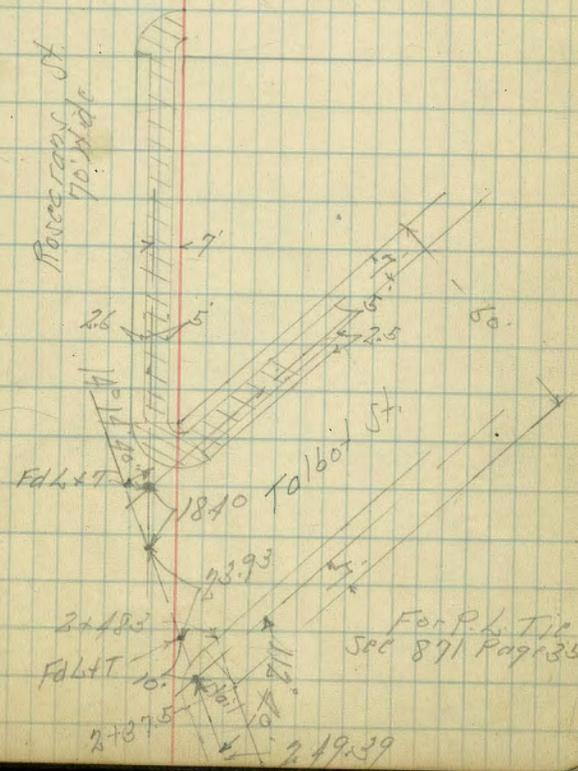
2+48.3

H.L. on Cb	2.34	22.59
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24.20

2+0

0+0.2





57.99

~~57.78~~

4175

W L	32	54.8
+26 = Top Granite Wall	4.6	53.4
+26 Base "	7.0	51.0
WCB	8.04	49.95

540

W L	21	55.4
+26 = Top Granite Wall	37	54.3
+26 Base " "	59	52.1
+8	67	51.3
WCB	7.15	50.84

5428

W L	22	55.8
+27 = Top Granite Wall	30	55.0
+27 Base " "	57	52.3
+7	61	51.9
WCB	6.43	51.56

5436

W L +78 = Wly Por Pol

5437 = Cb BC

W L	41.5	59.5
+4	26	55.4
+9	57	52.3
WCB	6.03	51.96

Sec A

Cb BC

521	52.68
-----	-------

67

57.99

~~57.78~~

5748

W L and Cb	3.63	54.36
TP	155	55.0
	<del>55.29</del>	3.95
	540.4	53.83

No. 1 Pol

So. Armada

0+0 = S.L. Armada

0+89.8 = Sly Conc Walk

W L	43.6	59.2
+27 Top Wall	43.2	58.8
+29 Base Wall	1.9	53.7
WCB Top	2.12	53.48

1425

W L	42.4	58.0
+28 = Top Wall	42.1	57.7
+29 Base "	2.3	53.3
WCB Top	2.83	52.77

1450 = Sly Conc Wall

W L	42.2	57.8
+28 = Top Wall	41.4	57.0
+29 Base "	3.0	52.6
WCB	3.75	51.85

1460

W L	0.5	55.1
+5	38	51.8
WCB	4.13	51.47

55.60  
~~55.39~~

1+70

HL	29	52.7
+7	4.7	50.9
WCB in Drive	5.23	50.37

1+80

HL	0.0	55.6
+3	4.2	51.4
WCB	4.98	50.68

2+0

HL	1.1	54.5
+3	5.2	50.3
WCB	5.72	49.87

2+25

HL	1.4	54.2
+3	6.5	49.1
WCB	6.73	48.87

2+50

HL	2.6	53.0
+5	7.2	48.4
WCB	7.73	47.87

2+75

HL	4.8	50.8
+3	8.2	47.4
WCB	8.72	46.88

55.60  
~~55.39~~

3+0

HL	5.0	50.6
+2.7 Top Wall	5.3	50.3
+2.7 Base "	9.3	46.3
WCB	9.69	45.91

3+25

HL	5.0	50.6
+2.7 Top Wall	5.3	50.3
+2.7 Base "	10.3	45.3
WCB	10.66	44.94

3+50

HL	6.9	48.7
+2.7 = Top Wall	6.8	48.8
+2.7 Base "	11.6	44.0
WCB	11.66	43.94
TP 0.67	<del>11.70</del>	43.64

4+0

HL	+4.0	48.3
+2.9 Top Wall	+2.8	48.1
+2.9 Base "	3.1	42.2
WCB	2.29	41.92

4+24.2 = W4 Conc Dr

HL	12.5	46.8
+2.9 Top Wall	12.5	46.8
+2.9 Base "	3.7	40.6
WCB	3.72	40.59

4431

~~4410~~

4746 - Sly Core Drive

XL	7.21	46.4
+2.9 = Top Wall	7.21	46.4
+2.9 = Base "	3.9	40.4
XCB	4.17	40.14

4455

XL	1.0	43.3
+5	3.8	40.5
XCB	4.55	39.76

4463

XL	2.8	41.5
+8	3.8	40.5
+9	4.9	39.4
XCB	4.88	39.43

4475

XL	0.9	43.4
+5	4.0	40.3
+8	4.6	39.7
XCB	5.37	38.94

540

XL	0.5	43.8
+4	4.4	39.9
+8	6.3	38.0
XCB	6.70	37.91

1580/47

69

Rogers

44647

4464

0 Fire Hyd  
24

4408 - Pole

24

3780

2764.5

2741.5

2735.1

1790.5 Pole

0788 Pole

18" Dia + 0.5

070

6716.80

2770.5

Pole

18" Dia

16.0

Black  
Paving

Fire Hydrant

Fire Hydrant

4431  
4410

5+25

XL	1.9	42.4
+4	4.8	39.5
+8	7.5	36.8
WCB	7.41	36.90

5+50

XL	3.2	41.1
+5	6.3	38.0
+8	8.2	36.1
WCB	8.32	35.98

5+75

XL	3.1	41.2
+4	7.4	36.9
+8	9.5	34.8
WCB	9.44	34.87

6+0

WCB	3.0	41.3
+4	7.7	36.6
+8	10.3	34.0
WCB	10.29	34.02

6+16.80 = Δ on ccb line

XL	3.8	40.5
+4	8.4	35.9
+8	10.6	33.7
WCB	10.76	33.55

4431  
4410

5947 ✓  
5786

TP 5.48 10.32

33.99

Hall Pole  
of 402W

33.78

0+10 = Δ in WCB

WCB	6.44	33.03
+2	6.37	33.10
+4	4.2	35.3
+10	1.0	38.5

0+30

WCB	7.01	32.46
+2	7.0	32.5
+4	4.9	34.6
+6	2.6	36.9
+10	1.4	38.1

0+65

WCB	7.18	32.29
+2	7.2	32.3
+4	5.2	34.3
+10	3.2	36.3

1+0

WCB	6.83	32.64
+2	6.8	32.7
+5	3.5	36.0
+10	0.9	38.6

39.47  
39.26

1+30

WCB	6.10	33.37
+2	6.1	33.4
+5	2.7	36.8
+10	0.6	38.9

1+40

WCB	5.77	33.70
+2	5.7	33.8
+5	4.8	35.2
+10	3.7	35.8

1+50

WCB	5.41	34.03
+2	5.4	34.1
+4	2.6	36.9
+10	1.7	37.8

1+70

WCB	4.73	34.74
+2	4.7	34.8
+4	2.6	36.9
+10	1.6	41.1

2+0

W	3.59	35.88
+2	3.5	36.0
+5	0.2	39.3
+10	2.8	43.3
+15	2.6	43.1

71

39.47  
39.26

2+20

WCB	2.77	36.70
+2	2.6	36.9
+5	+0.8	40.3
+8	+3.5	43.0
+15	+3.7	43.2

2+35.4 - Fly Conc Walk

WCB	2.16	37.31
+5.5 Fly Walk	2.02	37.45
+12	+3.2	42.7

2+41.5

WCB	1.93	37.51
+5.5	1.74	37.73
+12	0.5	39.0

TP 11.83 ~~50.25~~ 51.07 0.23 ~~39.03~~ 39.24

2+80 = Fly Conc Walk

WCB in Conc	8.68	42.39
+5.5 Fly Conc Walk	8.05	43.02
+10	7.8	43.8

4+0

WCB	7.43	43.64
+5	7.5	43.6
+10	6.2	44.9

Rosecrans St.

51.07  
50.86

4+08

Wcb	7.15	43.92
+4	6.9	44.2
+10	5.8	45.9

4+14

Wcb	6.90	44.17
+5	6.5	44.6
+8	4.2	46.9
+10	3.5	47.6

4+30

Wcb	6.21	44.86
+1	6.1	45.0
+3	4.3	46.8
+6	1.5	49.6
+10	0.9	50.2

4+64.7 - N.L. Rogers

Wcb - Sky End	4.74	46.33
+3	4.9	46.7
+6	0.0	51.1
+8	+1.4	52.5
+10	+2.5	53.6

51.07  
50.86

4+75

Wcb Ground	5.0	46.1
+1	5.0	46.1
+2	2.1	49.0
+7	+2.2	53.3
+10		54.1

TP 12.28 ~~63.01~~ 62.80 0.34 ~~50.52~~ 50.73

TP 5.90 ~~68.60~~ 68.39 0.11 ~~62.69~~ 62.90

BM

4.46

~~63.93~~ N.E.P.P.  
Rosecrans  
St. Perry  
64.14 → 64.15

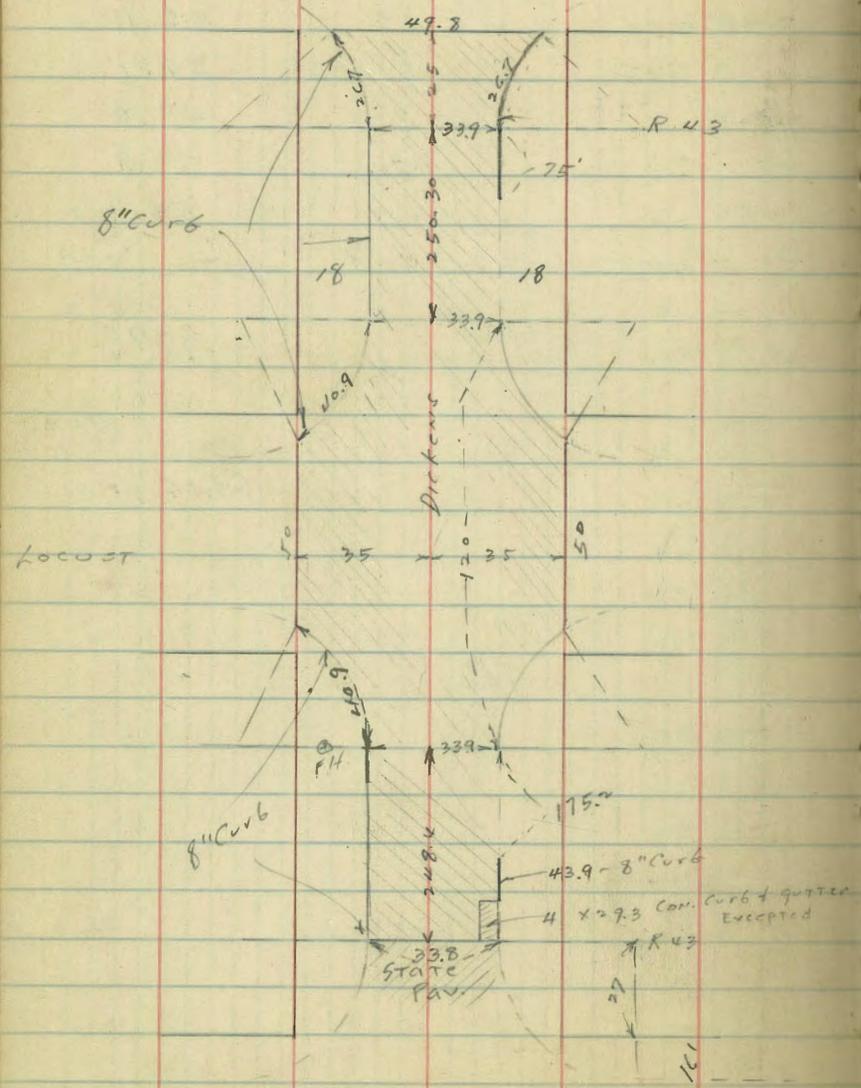
Final slope stage on  
Dickens St Hazard Const

Indexed  
LM

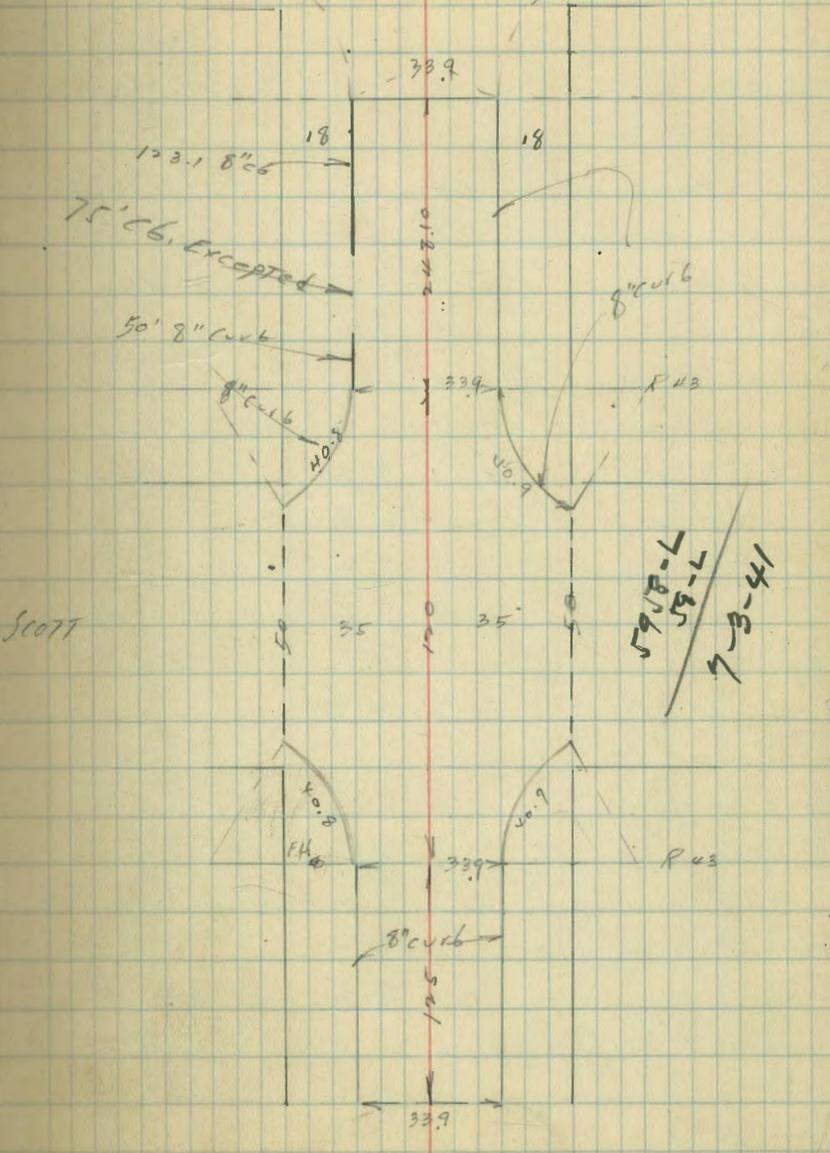
Rosecrans

Moore  
Osborn  
Covert 73  
7-2-41

Evergreen



Rosecrans



59.58-L  
58-L  
7-3-41

Moore & sec sidewalks on 18' curbs  
7-2-41 Dickens, Scott to 150' Ely

7.67

74

to show exceptions of Fall

0 + 66

SW 1/4 3' CT. R.P.	3.80	7.42	3.82	Dickens Scott			
				S		5.1	2.0
				+5		5.4	2.2
				+7		4.4	3.2
				S c6		4.4	3.2
0 + 00 = Ely Scott St							
S		4.4	3.2		0 + 68		
+ 10 c6		4.6	3.0	S		5.4	2.0
N		4.6	3.0	+13		4.9	2.7
+ 10 c6		4.9	2.7	S c6 in drive		4.8	2.8
0 + 25 c6. P.C.					0 + 75		
N		5.8	1.8	N		7.2	0.4
+ 5		5.8	1.8	+4		7.2	0.4
+ 8		4.7	2.9	+8		4.2	3.4
N c6		4.8	2.8	N c6		4.6	3.0
S		4.5	3.1		0 + 80		
S c6		4.5	3.1	S		6.2	1.4
0 + 50				+13		5.0	2.6
S		5.1	2.5	S c6 in drive		4.7	2.9
+ 2		5.1	2.5		0 + 83		
+ 7		4.2	3.4	S		7.0	0.6
S c6		4.4	3.2	+9		6.7	0.9
N		6.7	0.9	+13		4.2	3.4
+ 4		6.7	0.9	S c6		4.3	3.3
+ 7		4.5	3.1		1 + 0.0		
N c6		4.6	3.0	S		7.5	0.1
				+9		6.4	1.2

1700		
S + 13	4.3	3.3
S cb	4.2	3.4
N	7.4	00
+ 3	7.6	00
+ 9	4.1	3.5
N cb	4.4	3.2
1725		
N	7.9	- 0.3
+ 1	7.9	- 0.3
+ 9	4.0	3.6
N cb	4.3	3.3
S	8.1	- 0.5
+ 5	7.4	0.2
+ 14	4.1	3.5
S cb	4.0	3.6
eng curb 1 + 50 = + Pav.		
S	8.2	- 0.6
+ 8	8.1	- 0.5
+ 14	4.0	3.6
S cb	3.9	3.7
N	7.6	0.0
+ 5	7.4	0.2
+ 9	4.2	3.4
N cb	4.1	3.5

1755		
N	7.9	- 0.3
+ 6	7.7	- 0.1
+ 12	5.7	1.9
N cb	5.2	2.4
1/4	4.7	2.9
c	4.7	2.9
1/4	4.6	3.0
S cb	4.9	2.7
+ 5	6.0	1.6
+ 12	8.0	- 0.4
S	8.2	- 0.6
1785		
S	8.4	- 0.8
cb	7.7	- 0.1
1/4	6.9	0.7
c	6.1	1.5
1/4	5.8	1.8
cb	6.3	1.3
N	7.9	- 0.3

Final on Emerson  
Rosecrans to Scott.

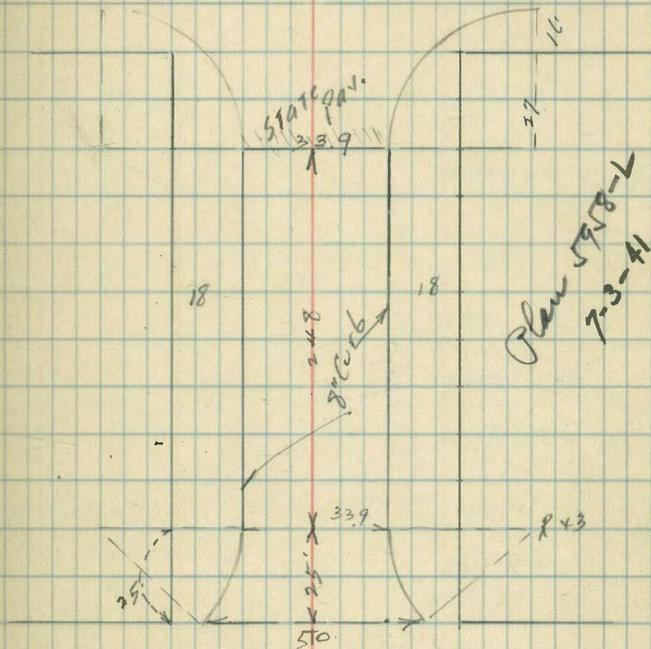
Indexed  
LM

Moore  
7-2-41.

76

Emerson

Rosecrans



Scott

Final Meas. of alley  
 Blk 190 S.D.L. + T. Co's add.

Meas  
 Osborne  
 Covert  
 01844  
 7-18-44

SAMPSON

ST 77

6+01.4	19.9		
			$19.95 \times 51.4 = 1025.43$
5+50	20		
5+00	20		
4+50	20		<del><math>20.00 \times 150 = 3000.00</math></del>
4+00	20		
3+50	19.8		$19.90 \times 50 = 995.00$
			$19.90 \times 49 = 975.10$
3+01	20		
3+00	18.9		$19.45 \times 1 = 19.45$
Corr. PUT IN by P.O.	10'		$18.90 \times 16 = 302.40$
2+84	18.9		$19.45 \times 1 = 19.45$
2+83	20		$20 \times 33 = 660.00$
+50	20		
2+00	19.7		$19.85 \times 50 = 992.50$
1+80	19.6		$19.65 \times 20 = 393.00$
1+50	20		$19.80 \times 30 = 594.00$
1+00	19.9		$19.95 \times 50 = 997.50$
0+50	19.6		$19.75 \times 50 = 987.50$
0+00	19.7		$19.65 \times 50 = 982.50$
			<b>GBN → 11,943.83</b>

FRANIS

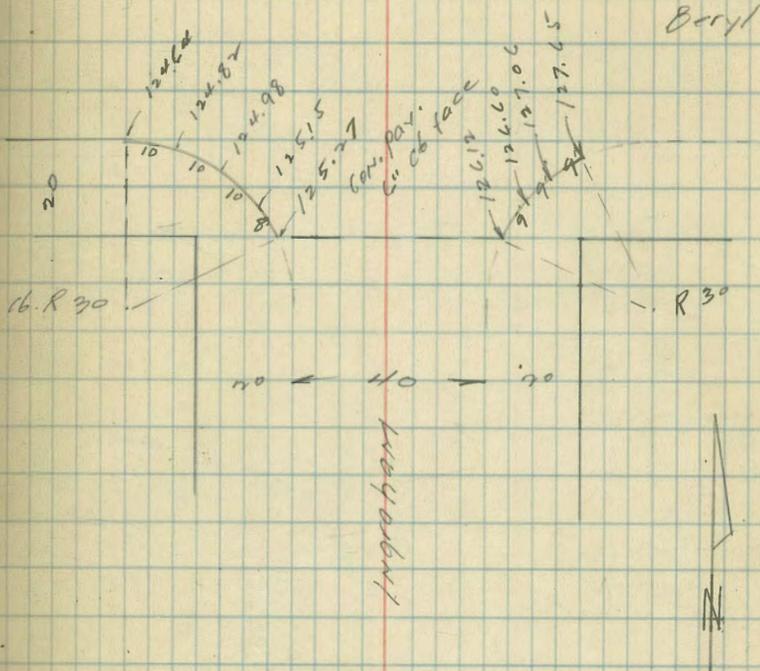
ST

B.22

Curb Elev: at  
Ingraham & Beryl

Moore

7-10-41.





DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder  
stake for any width roadway, slope 1 X to 1.  
If ground is nearly level, the cut or fill at side  
stake is located by the double copy method in  
left column and top row. The number in both

---

**IMPROVED TABLES**  
**AND**  
**INFORMATION**

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TABLE No. 2.

To find Tangent and External for curve of  
any other degree, divide by degree of curve and  
add constant found in column of constants.  
Degrees of curve with a given tangent found  
by dividing tangent (or external), opposite by  
given tangent (or external).  
The distance from a point on the tangent to  
the curve is very nearly the square of the tangent  
length divided by twice the radius.

## DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

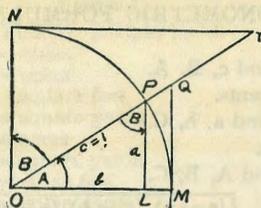
Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



46.7  
5.7  
2.5  
2.5  
559.4

TABLE II  
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin a}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

