

1528

1528

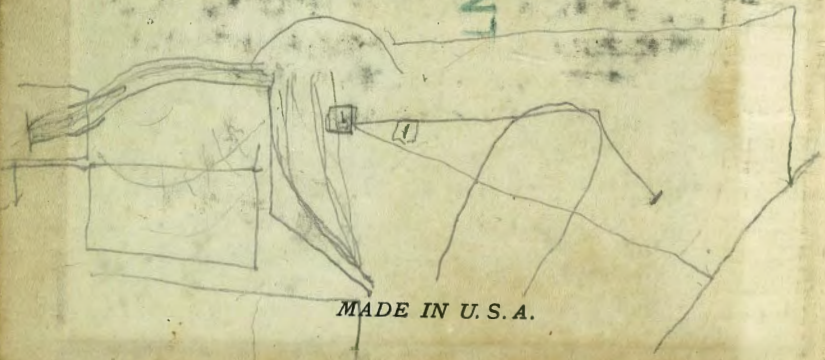
26.62  
L  
26.47

MICROFILMED

DEC 24 1964

ENGINEERING DEPARTMENT  
CITY OF  
SAN DIEGO,  
CALIFORNIA.

111  
25  
31



MADE IN U.S.A.

207  
2.2  
1.8  
101  
74  
27  
7000  
3500  
14000

Our Leather Bound Engineers Note Books 217 are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4x4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
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**THE FREDERICK POST CO.**  
ENGINEERING and DRAFTING SUPPLIES  
IRVING PARK STATION  
CHICAGO, ILL.

48764.92  
92.42  
49457.34

10-23-35  
Miller  
Walker  
Bliss

Survey Camino Del Rio  
Road. S. Side Mission Valley  
from Old Town to 6<sup>th</sup> St. Extension

4+00

3+47 Ex. Sewer M.H. 1.3' to Rt. of  $\phi$

1+39 Elec Pole #79002. 39' Rt.

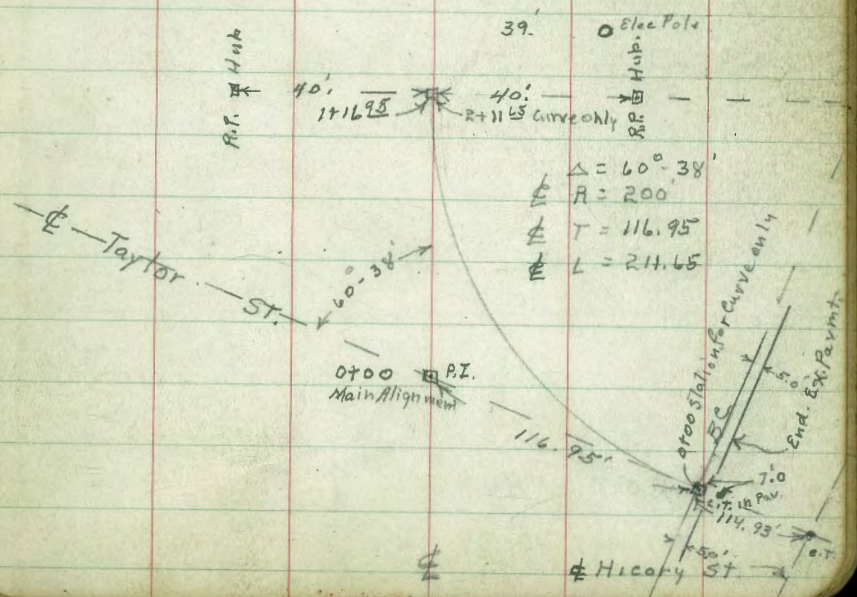
Station	Description	Hub	Curve =	Sta	Def. A.
1+16.95	E. P.	HUB	curve =	2+11.65	30° 19'
				1+75	25° 04'
				1+50	21° 29'
				1+25	17° 54'
				1+00	14° 19.5'
				0+75	10° 44.5'
				0+50	7° 10'
				0+25	3° 34'
0+00	P.I. Hub	$\phi$ Taylor ST			
				BC 0+00	

stations for Curve

Indexed  
e.s.m.

1

See Book 1552 P 6



9+00

+14 LL P.I. & Wly kin. P.L. 1102. Produced 514.

8+00

7

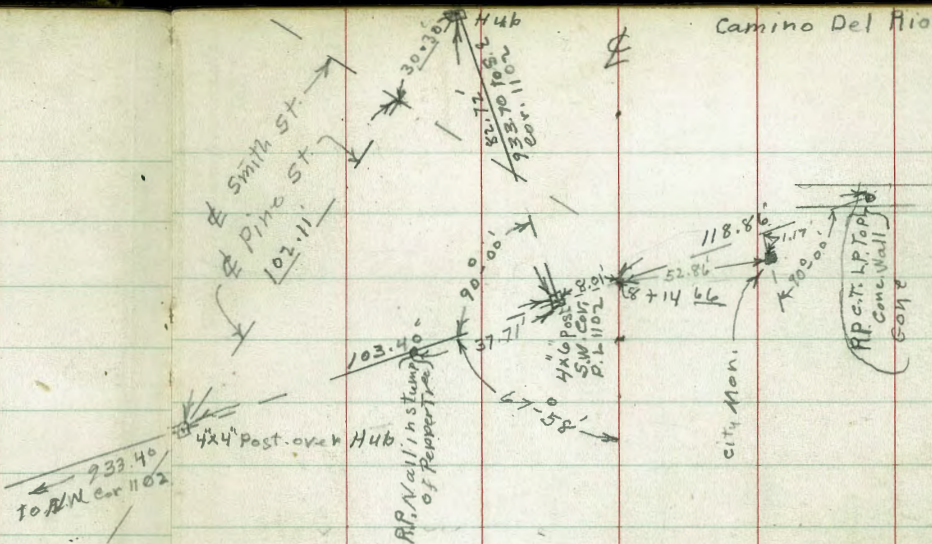
6

5

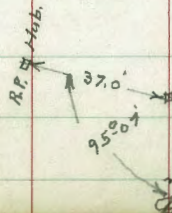
4+35

P.O.T. HUB.

4+00



Fore sight  
W. Side. Butt. of Lone  
Eucalyptus Tree.  
on Horizon.



14700

9+00

⊕

18+00

15+11 <sup>21</sup> E.C. Hub

Def L  
1+03

14+74 <sup>56</sup> Cr. Curve P.I.

0+31+5

+41 Elec Pole 20' Rt.

14+37 <sup>91</sup> B.C. Hub

14+00

$\Delta R = 06.44$   
 $\phi R = 2000'$   
 $\phi T = 36.66$   
 $\phi L = 73.30$

36.99  
73.24



These R.P.s. Plowed Out.  
See Page 72. for New R.P.s

See Page 72 for change in Alignment

"  
" 79 "  
" 19 "  
" L. Sec "

FB 1531

← 10-42

camino Del Rio

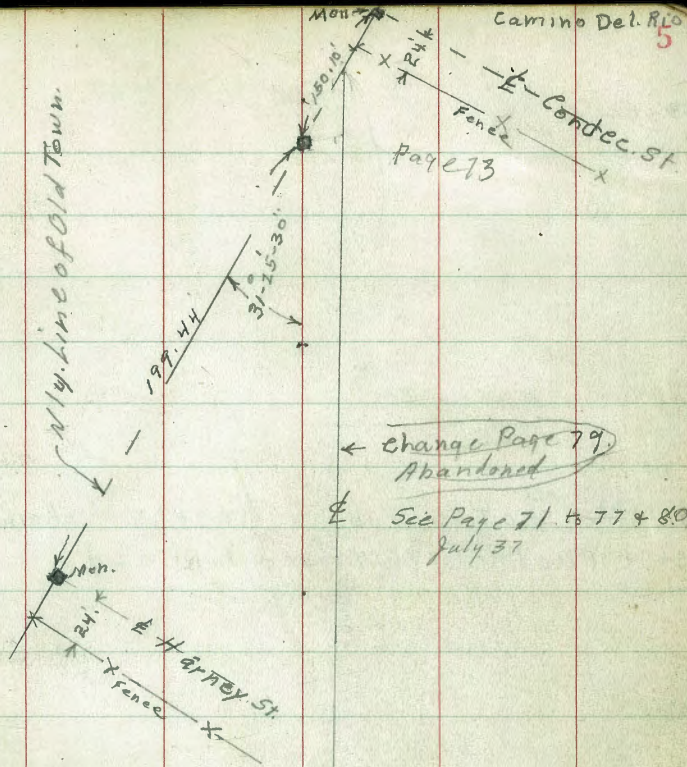
4

← change Page 79  
Abandoned.

See Page 71. to 77 & 80  
July '37.

23+00

22+82<sup>22</sup> Imp. Map. = (22+82<sup>21</sup> chained.)



14+00.

33+00

See Page 71-77 + 80

29+66<sup>22</sup> - MAP P.O.T. Hub. (29+65<sup>47</sup> chained)29+44 Elec Pole #19014. 20.0' to Rt. of  $\Phi$ 

28

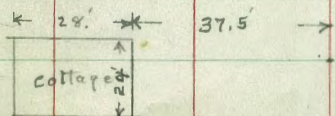
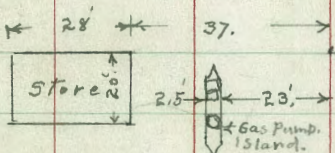
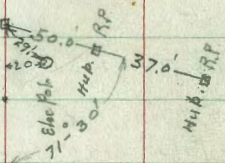
27 + 81.5 E. End. Store Bldg.  
 + 70. E. End. Gas. Pump Island.  
 + 61.5 W. End. Store Bldg.  
 + 60. W. End. Gas. pump. Island

404 Ely End. cottage

27

26+80 Wly End. cottage

23+00

See Page 71 to 77 + 80  
July '37



42+00

39+81<sup>22</sup> Imp. Map. F.C. = (39+81<sup>12</sup> chained)

39+29<sup>12</sup> ctr Curve

38+76.2<sup>5</sup> Imp. Map. B.C. Hub Lt. = (38+75<sup>35</sup> Measured.)

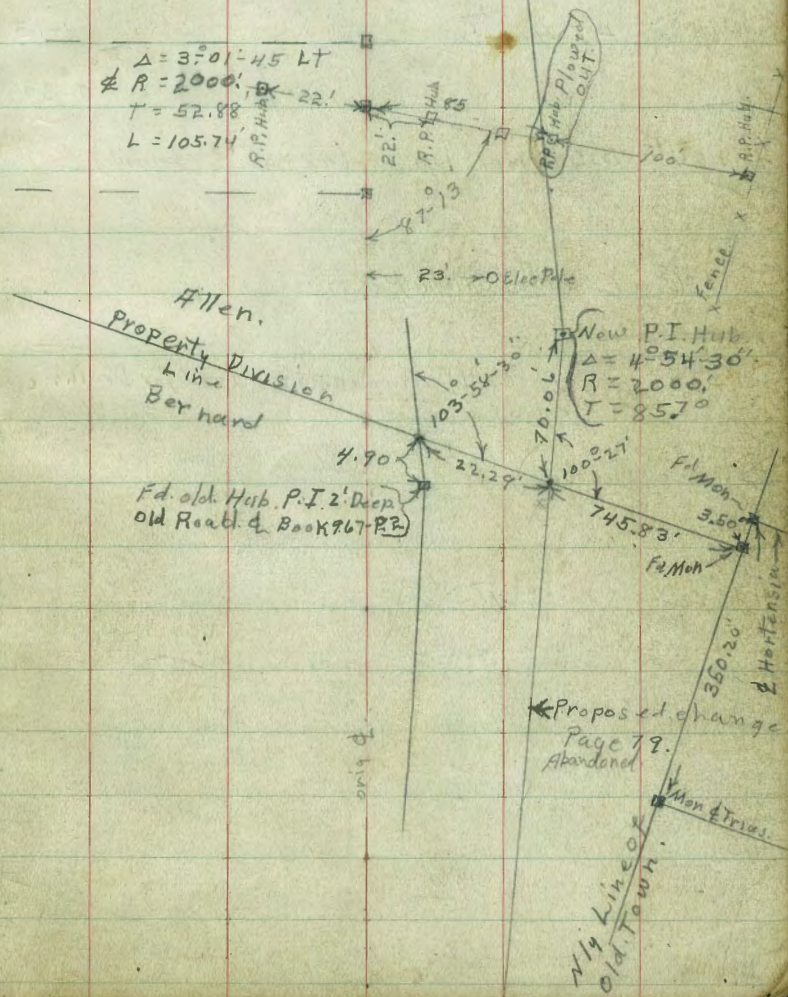
+68 Elec Pole # 79035 23' RT.

83+00

This line Abandoned →

See Page 71 to 77 & 80.

July 37.



42+00 52+00

50+49.3 E.C Imp Plan. = 50+48 1/2 chained. 2-34-45

50 1-56

39+81 +50 P.I. Hub. 1-13

39+249 0-30

48+64.2 B.C Imp Plan. (48+64 1/2 chained)

38+76

+68 +36.5 E. side Cattle Pass.

+27 W. side Cattle Underpass used for Drainage

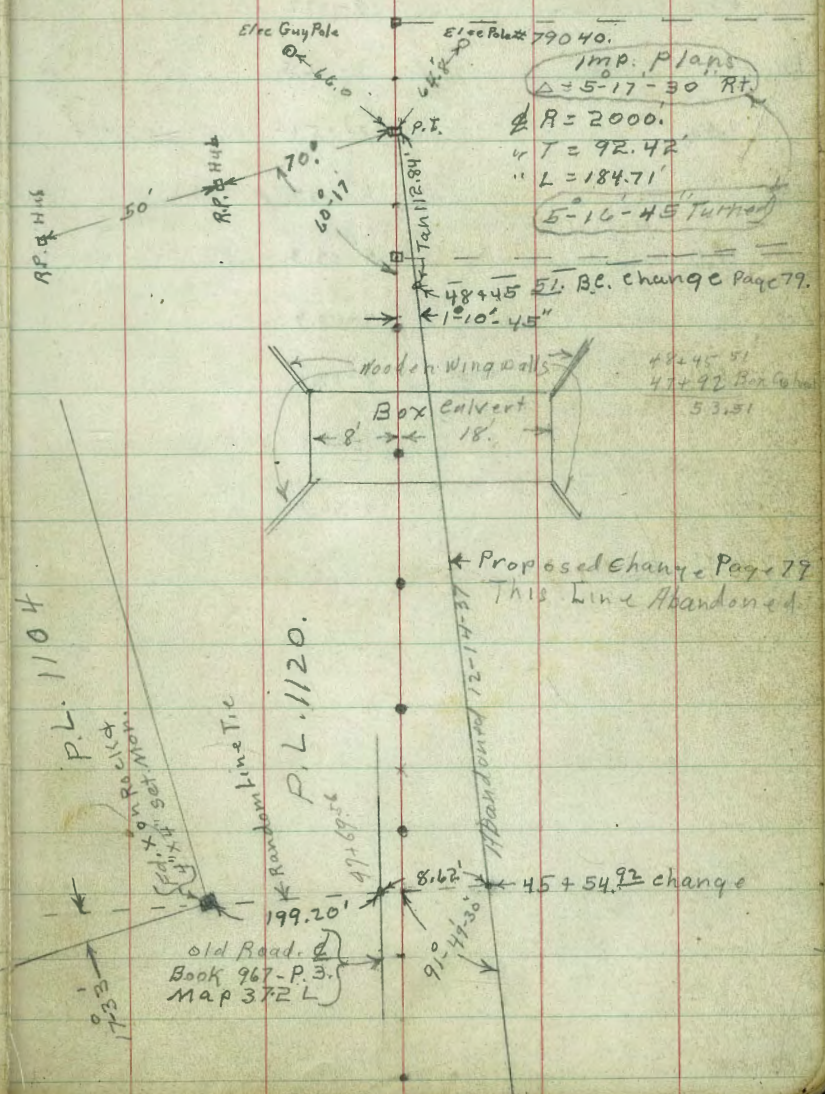
48

47

46

45

53+0



62+00

Def L.

61+37.08 E.G. Hub.

10-54.75

61

10-09.3

+50

9-07.9

60

8-06.5

+50

7-05.1

59

6-03.7

+50

P.I. Hub

5-02.3

58

4-00.9

+50

2-59.5

57

1-51.8

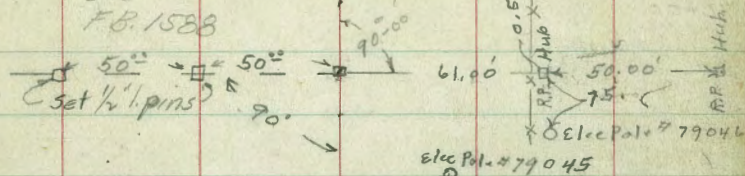
+50

0-56.7

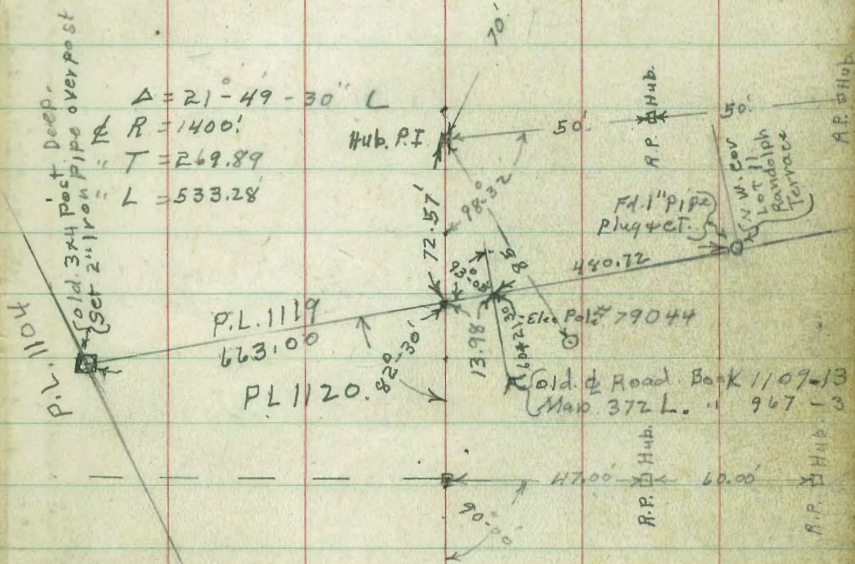
56+03.80

B.C. Hub.

52+00

54+03.8  
54+50  
153.8See  
F.B. 1588

old 3x4 post. Deep.  
Set 2" iron pipe over post

 $\Delta = 21-49-30'' L$ 
 $R = 1400'$ 
 $T = 269.89$ 
 $L = 533.28$ 


72+00

69+00 White Cliffs 84+00

62+00

camino del Rio

10

82+00

Camino del Rio

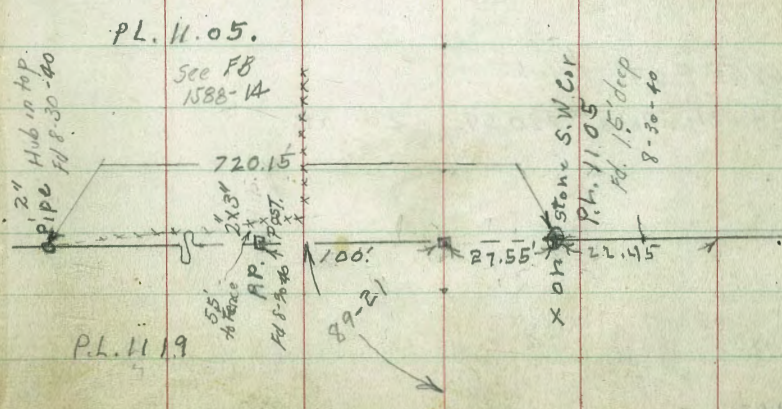
11

79+25 Culvert. 10 Hub.

P.L. 1119

73+39<sup>4</sup> P.O.T. Hub on P.L. Line

72+00



3+77<sup>28</sup> P.O.T. Fd. Hub.

2+50<sup>10</sup> P.I. Hub Main Line

(con. Page 14. Main Line)

+66<sup>89</sup> B.C. Hub. = 0+00 P.O.T. South Branch

89



P.L. 1105

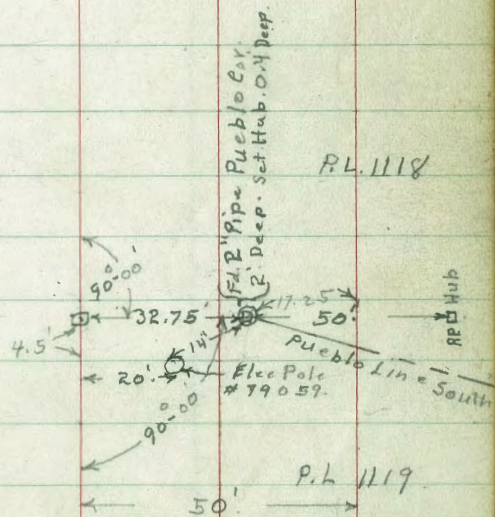
P.L. 1118

17.25
32.75
50.00

+68.55 P.O.T. Hub.

+64 Elec Pole #79059. 20' RT.

84



82+00

C.T.B. E.L.T. = 1057 88 27 Camino Del Rio.

391.25'

C.T. EC = 102407 42

Camino Del Rio

6<sup>th</sup> St Ext. 1  
Δ = 89-39-10"  
R = 150.  
T = 149.09  
L = 230.71

P.I. Lin.  
P.I. Hub

101.00

P.I. Hub

27.00

89.00

90.00

88.21

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

211.03'

39.57'

6.96'

C.T. Hub Cor.

6<sup>th</sup> St

Double Box Concrete Culvert

12' Wide 2.5' High

opening

13.4'

9+81

9+86

Camino Del Rio

South Branch

10+21 63 P.I. # 6<sup>th</sup> St Ext.

9+86 W. Edge Pav on S. End = E Side Culvert

9+81 W. Edge Pavmt on End. SW "

Pump House  
Concrete Sump  
10' x 12'

17' x 17' Rucklo Line

Fence

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

Proposed Culvert

Culvert

34.49

9

8

7

6

5

4

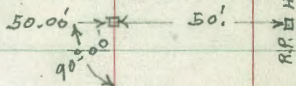
3+77 98 Fd. Hub P.O.T. South Branch.

111.53  
Cul 93

99

+24<sup>04</sup> B.C. Rt. Hub.

Shed of Nail  
RP. W. side Eucalyptus  
Tree



97

96

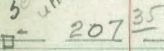
267

95

+57<sup>04</sup> E.C. Hub.

Def 4s.  
14<sup>0</sup>-02.5

Set 1/2 iron pin  
under fence



94

+50

12<sup>0</sup>-24.5

See FB 1588-17

93

+50

$\Delta = 28^{\circ} 05' Lt$   
 $R = 1000.$   
 $T = 250.10'$   
 $L = 490.15$

9<sup>0</sup>-32.6

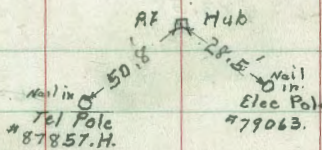
8<sup>0</sup>-06.6

92

+50

6<sup>0</sup>-40.7

5<sup>0</sup>-14.7



91

+50

3<sup>0</sup>-48.8

2<sup>0</sup>-22.8

90

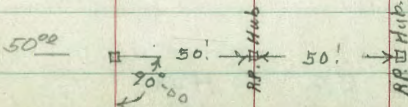
+66<sup>89</sup>

B.C. Lt. Hub.

0<sup>0</sup>-56.9

89+64<sup>33</sup> plan

Set 1/2 pin  
at fence



89

Con. from. Page 12.



Camino Del Rio

Set 1/2 h. pin.

22<sup>85</sup>

at in par. sta 64+83.32  
6th St Exten

23<sup>15</sup>

Set 1/2 h. pin

c.t. in Ex Pav.

continued in FB 1530

+88 27 c.t. Ex Pav. B.C. LF.

97 274.04  
94 + 57.04  
2 + 67.60

105

381.25'

104

103

+07 27 E.C.

{ c.t. Ex Pav.  
E.C. Ex 150 Radius.  
Curve

Def Ls.  
13° - 51.2'  
13° - 38.1'

c.t. Ex Pavmt E.C.

102

+50

12° - 12.2'

101

A = 27° 42' - 30" RT

10° - 46.2'

R = 1000'

9° - 20.3'

T = 246.6'

+50

L = 483.58

7° - 54.3'

100

+50

6° - 28.4'

P.I. = H46

99

5° - 02.4'

+50

3° - 36.5'

98

2° - 10.5'

+50

0° - 44.6'

+24 24 B.C.

Hub

97

EXISTING  
Box Culvert  
See Page 16.

Continued in F.B. 1530

102+07<sup>62</sup> E.C.

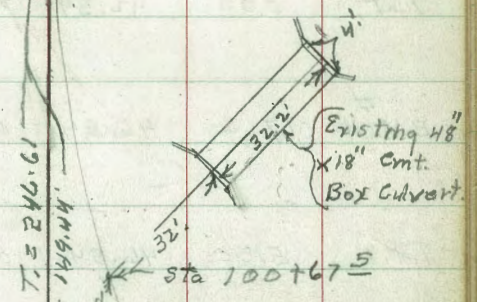
97+24<sup>04</sup> B.C.

102+07<sup>62</sup> E.C.

$$\begin{array}{r}
 15+30-56 \\
 12 \quad 11 \quad 24 \\
 \hline
 27-42-25
 \end{array}$$

C.T. & Ex. Par. E.C. 1<sup>st</sup> Ave Ext.

149.44  
 44° 54'



∠ 27° 42' 50"  
 R = 1000.00  
 T = 246.61  
 L = 1483.58'

P.L. Hub

sta 97+24<sup>04</sup> B.C. →

Bench Levels  
Camino Del Rio

indexed  
c.s.R.

17

T.P.	0.00	42.39	4.15	42.39	Nail in Elec Pole # 79037
B.M. # 4	0.67	46.54	0.67	45.87	3 Nails in 8" x 8" Fence Post. 84' Rt. of Sta 37+64
T.P.	5.50	46.54	0.34	41.04	Nail in Elec Pole # 79031 20.5 Rt. of Sta 37+24
T.P.	11.40	41.38	0.39	29.98	Nail in Tel Pole # B. 1919T.
T.P.	11.46	30.37	0.12	18.91	
B.M. # 3	7.55	19.03	4.65	11.48	Mon. & Condo St. + Wly Line Old Town. 78' Rt. of Sta 24+11
T.P.	2.73	16.13	2.68	13.40	Nail Elec Pole # 79010
B.M. # 2	1.77	16.08	3.67	14.31	B.P. cmt. wall 48' Rt. of Sta 8+58 <small>This B.M. to be destroyed</small>
B.M. # 2	3.83	18.14		14.31	B.P. cmt. Wall 48' Rt. of Sta. 8+58
B.M. # 2 A New.			4.33	14.81	Top City Mon. 49 <sup>5</sup> Rt. of Sta 8+35.
T.P.	3.41	17.98	6.08	14.57	
B.M. # 1	0.58	20.45		20.07	Wly curb Sly End. Old Town Highway Bridge

B.M. #6	5.78	24.84	3.74	19.06	{ U.S. Coast & Geodetic B.M. # T.321 - 1935 19.5 Rt. of Sta 87+71 <sup>50</sup>
T.P.	3.92	22.80	3.43	18.88	Nail Elec Pole #79059 20' Rt. of Sta 84+65
T.P.	3.03	22.31	2.90	19.28	Nail Elec Pole #79055 21' Rt. of Sta 79+67
T.P.	3.31	22.18	3.66	18.87	Nail Elec Pole 23' Rt. of Sta 73+71
T.P.	3.87	22.53	5.72	18.66	Nail Elec Pole #79049 26' Rt. of Sta 66+24
B.M. #5	2.98	24.88	0.64	21.40	3. Nails Elec Pole #79040 V Rt. of Sta 59+65
T.P.	2.42	22.04	8.02	19.62	Nail Elec Pole #79043
T.P.	2.32	27.64	6.27	25.32	Nail in Elec Pole 19' Lt. of Sta 50+21
TP	1.66	31.59	12.46	29.93	

42.39

BM #		5.10		23.36	B.P. Sly Head wall Ex 48" X 18' Culvert 64' Rt. 100+67 <sup>5</sup>
------	--	------	--	-------	---

BM #	4.49	28.46	0.72	23.97	B.P. Sly End. Ex Culvert. } W. side 6 <sup>th</sup> St. Extension S. Fork, Camino Del Rio.
------	------	-------	------	-------	---

T.P.	5.35	24.69	5.50	19.34	
------	------	-------	------	-------	--

		24.84			
--	--	-------	--	--	--

Camino Del Rio  
X. Sec.

Curve only  
1+50 \$ 8.0 14.78

1+00 7.6 15.18

0+53 Elec Pole 29 Rt.

0+50 6.5 16.28

Curve Only  
0+00 B.C. 5.2 17.28

0+00 B.C. - 5' Nly End Taylor St. Pav 5.21 17.57

BM. #  
B.M.B.P. 2.71 22.78 2.71 20.07

U.S. Coast + Geodetic  
B.M. # U. 321 - 1935. 4.21 17.41

BM. # 1 1.55 21.62 20.07

Indexed  
C.S.R. 2+

12.08	15.18	17.88	14.88	14.78	14.48	14.38	14.98	21.08
10.7	7.6	7.9	7.9	8.0	8.3	8.4	7.8	7.7
50	41	20	15	15	15	20	30	50

15.28	15.08	15.18	15.18	14.78	14.88	15.68	18.48	25.18
7.5	7.7	7.6	7.6	8.0	7.9	7.1	4.3	7.4
50	20	15	15	15	20	30	40	50

16.98	14.58	16.48	14.28	15.98	14.18	14.78	20.05	28.48
5.8	6.2	6.3	6.5	6.8	6.6	6.0	2.7	7.57
50	20	15	15	15	20	30	13	50

17.38	17.58	17.58	17.58	17.28	16.98	16.78	17.78	24.28
5.4	5.2	5.2	5.2	5.5	5.8	6.0	5.0	4.5
50	20	15	15	15	20	30	38	50

17.41	17.66	17.72	17.57	17.26	17.68	16.55	17.18	24.15
5.27	5.12	5.06	5.21	5.52	5.70	6.23	5.00	4.14
50	20	15	15	15	20	30	30	50
Pav	Pav	Pav	Pav	Pav	Pav	Pav	cl	

22.78

Wdy. Curb Sly. End Old Town. Highway Bridge

1.0 E. of E. cmt. Curb of Taylor St. 80' N. of N. Line  
Hicory St. = 5' S. of N. End ext. cmt. curb.

+37 Elev Pole 14' Rt  
 3 5.5 14.10

+50 5.5 14.10

T.P. 5.51 19.60 8.69 14.09

2 8.7 14.08

1+50 8.6 14.18

1+39 Elev Pole 39' Rt.

Curve only  
 2+11.65 = 1+16.25 E.C.  
 8.4 14.38

Curve only  
 1+75 8.1 14.68

22.78

2t. 8.10 19.60 x 13.30 13.40 x 14.10 14.10 21.80 RT. 28.60 51.60  
 11.5 6.0 4.3 6.2 5.5 5.5 +2.2 +2.0 +32.0  
 50. 37. 20. 15. 50. 35. 15. 20. 50

7.20 12.20 x 13.70 13.70 14.10 14.80 18.60 21.00 48.60  
 12.4 7.4 5.9 5.9 5.5 4.8 1.0 +1.4 +29.0  
 50 35 20. 15. 10 15 20 50

19.60

10.48 14.38 x 14.38 14.18 x 14.08 x 14.08 14.08 34.78 42.78 x  
 12.3 8.4 8.4 8.6 8.7 8.7 8.1 +12.0 +20.0  
 50. 31. 20. 15. 15 15 20 45 50

10.78 14.08 14.28 14.38 14.18 14.28 14.38 14.38 31.18 37.78  
 12.0 8.7 8.5 8.4 8.6 8.5 8.4 7.9 +8.4 +15.0  
 50 35 20 15 15 20. 25. 45. 50.

6.18 12.18 15.08 14.78 14.48 14.38 14.28 15.58 17.28  
 16.6 10.6 7.7 8.0 8.3 8.4 8.4 7.2 3.5  
 50. 43. 28. 20. 15. 15 15 34 50

8.28 14.38 14.98 14.68 14.68 14.28 14.28 14.78 21.78  
 14.5 8.4 7.8 8.1 8.1 8.5 8.5 8.0 1.0  
 50 30 20 15 15 20. 36. 50

22.78

+63 Elec Pole 7' Rt.

+50

4.5 13.54

3.34

3.94

12.44

12.24

12.34

12.44

13.54

17.34

18.74

19.54

20.14

42.74

14.7  
50

14.1  
45.

5.6  
38.

5.8  
20.

5.7  
15.

5.1  
5.

4.5

0.7  
5.

+0.7  
15

+1.5  
20

+2.1  
25

+24.7  
50

2 Hub

F.P. 4+35

3.29

18.04

4.85

14.75

18.04

5

4.6 13.00

3.60

12.70

12.90

12.30

13.00

16.50

18.60

19.10

27.90

35.60

36.60

16.0  
50

6.9  
40

7.3  
20

7.3  
15

6.6

3.1  
5

1.0  
15

0.5  
20

+8.3  
29

+16.0  
40

+17.8  
50

5.10

12.70

12.70

12.80

12.80

14.50

14.80

17.60

18.30

21.00

32.80

+50

5.1 14.50

14.5  
50

6.9  
39

6.9  
20

6.8  
16

6.8  
12

5.1

4.8  
6

2.0  
8

1.3  
15

+1.4  
20

+13.2  
50

6.40

13.20

13.00

13.00

13.80

19.60

21.70

29.80

13.0  
50

6.4  
38.

6.5  
20.

6.6  
15.

5.8

0.0  
15

+1.5  
20

+10.2  
50

2.60

13.20

13.70

13.10

14.10

21.60

23.60

39.10

54.60

+50

5.5 14.10

17.0  
50

6.4  
38.

6.5  
20.

6.5  
15.

5.5

+2.0  
15.

+4.0  
20.

+19.5  
40.

+35.0  
50.

+47 Ex. M.H. 1.3 Rt.

3

19.60

19.60  
1.3  
Rim

L.T.

R

R.T.

22



+77 Large Date Palm 11.0 Lt.  $\frac{1}{2}$

+52 Large Date Palm 11.5' Lt.

+50 15.91 4.3 12.10

+49 Tel. Pole 3.5 Lt.

~~BM. 2 2.11 16.40 3.75~~ 14.31  
 This B.M. Destroyed

BM. 2A New. 14.29  
 (14.31)  
 14.81

8 This B.M.  $\rightarrow$   
 Should be 13.81 according  
 to Johnson W.E.B.  
 15.79 4.7 13.34

+68 Elec Pole 22' Rt.

+50 15.56 5.6 12.44

+32 Tel. Pole 16.5 Lt.

+24 Ex M.H. 35' Rt.

7 5.7 12.34

+50 5.7 12.34

6 5.0 13.04

18.04

LT  $\frac{1}{2}$  RT.

7.90 10.20 10.80 x  
 9.0 6.2 5.6 4.3 4.3 4.1 3.5  
 50. 20. 15. 16. 16. 20. 50.

16.40

B.P. Top cmt. Wall 48' Rt. of Sta 8+58

49<sup>5</sup> Rt. of sta 8+35 Top of City Mon

9.04 13.24 13.24 x  
 9.0 4.8 4.8 4.7 5.7 5.7 5.6 5.8  
 50 20 15. 2. 15. 20. 50.

11.04 12.54 x  
 7.0 5.5 5.7 5.6 5.6 5.5 5.3 3.3 +3.5  
 50 43 20. 15. 15. 20. 38. 50

7.54 10.24 12.24 x  
 10.5 7.8 5.8 5.8 5.7 5.3 4.5 +2.5 +4.5 +10.0  
 50. 44. 20. 15 15. 20. 34. 48. 50.

3.54 9.44 12.34 x  
 14.5 8.6 5.7 5.9 5.9 5.7 5.1 4.5 0.0 +3.8 +15.0 +41.5  
 50. 42. 32. 20. 15. 15. 18. 20. 36. 48 50 50

3.44 9.04 11.84 12.24 x  
 14.6 9.0 6.2 5.8 5.9 5.5 5.0 5.0 0.9 0.5 +0.6 +2.8 +16.0 x  
 50. 44. 37. 20. 15 1. 5.0 9. 12. 15. 20. 30 43

18.04

	£		
12	5.2	11.20	
+50	4.9	11.50	
+47 Elec Pole 30' Rt.			
11.	7.4	9.00	
+50	8.0	8.40	
10.	8.1	8.30	
+50	7.0	9.40	16.16
+47 Large Fan Palm 20' Lt.			
+40 Elec Pole 39' Rt.			
9	5.5	10.90	16.40

	Lt.		Rt.
8.40	8.80	8.80	8.80
8.0	7.6	8.0	8.0
5.0	2.0	5.0	5.0
10.0	10.0	10.0	10.0
6.40	6.40	6.40	6.40
6.60 x	6.60 x	6.60 x	6.60 x
8.40	8.40	8.40	8.40
5.2	5.2	5.2	5.2
11.20	11.20	11.20	11.20
11.40	11.40	11.40	11.40
11.40	11.40	11.40	11.40
11.60	11.60	11.60	11.60
8.80	8.80	8.80	8.80
8.80	8.80	8.80	8.80
8.2	8.4	8.4	8.4
7.70	8.60	8.60	8.60
8.7	7.8	8.1	8.1
5.0	2.0	5.0	5.0
15.0	15.0	15.0	15.0
11.50	11.50	11.50	11.50
11.40	11.40	11.40	11.40
11.40	11.40	11.40	11.40
11.60	11.60	11.60	11.60
8.90	8.90	8.90	8.90
8.7	8.7	8.7	8.7
8.1	8.1	8.1	8.1
7.70	8.20	8.30	8.30
8.5	8.2	8.1	8.1
5.0	2.0	5.0	5.0
12.0	12.0	12.0	12.0
7.20 x	7.20 x	7.20 x	7.20 x
7.40	7.40	7.40	7.40
9.00	9.00	9.00	9.00
11.50	11.50	11.50	11.50
11.50	11.50	11.50	11.50
11.60	11.60	11.60	11.60
8.90	8.90	8.90	8.90
8.30	8.30	8.30	8.30
7.90	7.90	7.90	7.90
8.10	8.60	8.70	8.70
8.3	7.8	7.7	7.7
5.0	2.0	5.0	5.0
9.30 x	9.30 x	9.30 x	9.30 x
8.40	8.40	8.40	8.40
11.30	11.30	11.30	11.30
1.40	1.40	1.40	1.40
11.40	11.40	11.40	11.40
11.40	11.40	11.40	11.40
11.80	11.80	11.80	11.80
9.50	9.50	9.50	9.50
9.80	9.80	9.80	9.80
8.20	8.60	9.10	9.10
8.2	7.8	7.3	7.3
5.0	2.0	5.0	5.0
9.70	9.70	9.70	9.70
8.30	8.30	8.30	8.30
11.30	11.30	11.30	11.30
1.40	1.40	1.40	1.40
11.60	11.60	11.60	11.60
11.70	11.70	11.70	11.70
12.20	12.20	12.20	12.20
8.50	10.60	11.10	11.10
7.9	5.8	5.3	5.3
5.0	2.0	5.0	5.0
9.40	9.40	9.40	9.40
11.60	11.60	11.60	11.60
11.60	11.60	11.60	11.60
11.70	11.70	11.70	11.70
12.20	12.20	12.20	12.20
9.70	11.40	11.10	11.10
9.70	11.40	11.10	11.10
5.3	5.0	5.5	5.5
5.0	5.0	5.5	5.5
12.20	12.20	12.20	12.20
12.10	12.10	12.10	12.10
12.30	12.30	12.30	12.30
13.40	13.40	13.40	13.40
16.46			

15.44  
17.34  
13

+74<sup>52</sup> Ctr Curve

5.1 10.42

11.52	11.02	6.32	6.52	10.42	10.42	10.72	10.92	8.32	8.32
4.0	4.5	9.2	9.0	5.1	5.1	4.4	4.6	7.2	7.2
50	26	20	15	10	15	15	20	27	50

+41 Elec Pole 20. Rt

+37<sup>21</sup> B.C. Lt 5.0 10.52

11.12	11.02	6.12	6.12	7.02	10.42	10.52	10.62	10.72	9.22	7.72	7.22
4.4	4.5	9.4	9.4	8.5	5.1	5.0	4.9	4.8	6.3	7.8	8.3
50	28	23	20	15	10	10	15	20	25	34	50

14 5.1 10.42

10.22	9.52	6.22	6.22	10.32	10.42	10.52	10.52	10.52	5.92	5.82
5.3	4.0	9.3	9.3	5.2	5.1	5.0	5.0	5.0	9.6	9.7
50	22	20	15	8	15	20	20	26	39	50

+50 5.1 10.42

9.72	9.52	5.72	5.72	6.42	10.52	10.42	10.42	10.52	6.42	6.12
5.6	6.0	9.6	9.6	9.1	5.0	5.1	5.1	5.1	9.1	9.4
50	20	18	15	12	5	15	20	21	38	50

13 4.9 10.62

9.52	9.22	5.92	6.32	10.52	10.62	10.82	10.82	10.82	8.02	6.02
5.0	6.3	9.6	9.2	5.0	4.9	4.7	4.7	4.7	7.5	9.5
50	20	15	10	3	15	20	28	32	50	

+50 4.5 11.02

9.02	9.12	6.22	6.52	10.92	11.02	11.02	11.02	11.02	8.82	6.62
6.5	6.4	9.3	9.0	4.6	4.5	4.5	4.5	4.3	6.7	8.9
50	20	15	8	2	15	20	29	33	50	

T.P. 2.77 15.52 3.65 12.75

15.52

16.40

4

18

3.8

11.72

10.42	10.42	8.12	8.12	11.32	11.72	11.42	11.42	10.52	10.02
5.1	5.1	7.4	7.4	4.2	3.8	4.1	4.1	5.0	5.5
	23	20	15	12		15	20	23	

+50

4.2

11.32

10.12	10.32	7.82	7.82	11.12	11.32	11.52	11.52	10.32	9.82
5.4	5.4	7.7	7.7	4.4	4.2	4.0	4.0	5.2	5.7
	50	23	20	15	12	15	20	23	50

+41 Elec Pole 19.5' Rt.

17

4.5

11.02

10.32	10.42	7.72	8.12	10.72	11.02	11.22	11.12	11.12	9.52	10.52
5.2	5.1	7.8	7.4	4.8	4.5	4.3	4.4	4.4	6.0	5.0
	50	24	20	15	11	15	20	24	25	50

+50

4.7

10.82

10.12	10.32	7.42	8.02	10.82	10.82	11.02	10.82	9.72	9.12
5.4	5.2	8.1	7.5	4.7	4.7	4.5	4.7	5.8	6.4
	50	26	26	15	11	15	20	26	50

16.

4.7

10.82

10.52	10.22	7.52	7.52	10.82	10.82	11.02	11.02	9.42	8.72
5.0	5.3	8.0	8.0	4.7	4.7	4.5	4.5	6.1	6.8
	50	26	20	15	12	15	20	28	50

+50

4.9

10.62

10.52	10.02	7.12	7.12	10.72	10.62	10.82	10.92	9.22	8.72
5.0	5.5	8.4	8.4	4.8	4.9	4.7	4.6	5.3	6.2
	50	25	20	15	12	15	20	26	50

15 + 11<sup>21</sup> E.C.

4.9

10.62

10.92	9.92	6.72	6.82	7.32	10.32	10.62	10.72	10.92	8.62	8.52
4.6	5.4	8.8	8.7	8.2	5.2	4.9	4.8	4.6	6.9	7.0
	50	26	24	20	15	10	15	20	26	50

15.52

15.52

21

5.1 11.25

5.8	10.55	4
5.9	10.45	24
7.4	8.55	20
7.6	8.75	15
5.1	11.25	11
5.1	11.25	11
4.8	11.55	15
4.8	11.55	20
4.8	11.55	22
6.4	9.95	25
7.3	9.05	30
7.3	9.05	50

+54 Elec Pole 20' Pt.

+50 4.7 11.65

5.7	10.65	5.7	10.65
5.7	10.65	7.6	8.75
7.4	8.95	7.4	8.95
4.9	11.45	4.9	11.45
4.7	11.65	4.7	11.65
4.9	11.45	4.9	11.45
4.7	11.65	4.7	11.65
6.2	10.15	6.2	10.15
8.0	8.35	8.0	8.35
8.0	8.35	8.0	8.35

20

4.7 11.65

5.2	11.15	5.3	11.05
5.3	11.05	7.3	9.05
7.3	9.05	7.3	9.05
7.8	8.35	7.8	8.35
4.8	11.55	4.8	11.55
4.7	11.65	4.7	11.65
4.5	11.85	4.5	11.85
4.3	12.05	4.3	12.05
6.0	10.35	6.0	10.35
8.0	7.75	8.0	7.75

+50 4.5 11.85

5.8	10.55	5.3	11.05
5.3	11.05	8.1	8.25
8.1	8.25	7.6	8.75
4.6	11.75	4.6	11.75
4.5	11.85	4.5	11.85
4.3	12.05	4.3	12.05
4.3	12.05	4.3	12.05
6.0	10.35	6.0	10.35
7.7	8.65	7.7	8.65

19

4.5 11.85

5.7	10.65	5.8	10.55
5.8	10.55	8.0	8.35
8.0	8.35	8.0	8.35
4.7	11.65	4.7	11.65
4.5	11.85	4.5	11.85
4.3	12.05	4.3	12.05
4.3	12.05	4.3	12.05
5.8	10.55	5.8	10.55
7.7	8.65	7.7	8.65

+50 4.7 11.65

5.5	10.85	5.5	10.85
5.5	10.85	8.0	8.95
8.0	8.95	8.0	8.95
4.9	11.45	4.9	11.45
4.7	11.65	4.7	11.65
4.3	12.05	4.3	12.05
4.5	11.85	4.5	11.85
4.6	11.75	4.6	11.75
5.7	10.65	5.7	10.65
7.2	9.15	7.2	9.15

T.P. Nail 2.96 16.35 2.13

13.39  
= 13.40

16.35

15.52

24 5.4 12.92

7.2	6.6	7.6	8.8	7.1	8.4	5.4	5.1	5.2	5.2	7.0	8.0
50	22	20	18	15	12	9	15	20	22	25	50
11.12	11.72	10.72	9.52	9.22	9.92	12.72	12.92	13.22	13.12	13.12	11.72
RT.											

+50 5.5 12.82

7.7	6.4	8.4	9.1	5.7	5.5	5.3	5.4	7.2	7.5
50	22	20	15	10	15	20	23	50	
10.62	11.92	9.92	9.22	12.62	12.82	13.02	12.92	11.12	10.82

B.M. 3 6.84 18.32 6.84 11.48  
= 11.48

78' Rt. of Sta 2411 Mon. of Conde. St + Nly. Line Old Town.

+40 Elec Pole Rl. Rt.

Tip Nail 3.81 18.32 1.84 14.51  
Elec Pole #79012

23 4.0 12.35

9.85	10.85	8.85	8.85	12.35	12.35	12.55	12.65	12.65	11.05	10.65
6.5	5.5	7.5	7.5	4.0	4.0	3.8	3.7	3.7	5.3	5.7
50	21	20	15	10	10	15	20	22	25	50

+50 4.3 12.05

9.15	10.55	9.55	8.55	11.85	12.05	12.15	12.15	11.95	10.35	10.55
7.2	5.8	6.8	7.8	4.5	4.3	4.2	4.2	4.4	6.0	5.8
50	22	20	15	10	10	15	20	22	24	50

22 4.7 11.65

10.75	9.85	8.35	8.55	11.55	11.65	11.75	11.85	10.75	9.75
8.6	6.5	8.0	7.8	4.8	4.7	4.6	4.5	5.6	6.6
50	24	20	15	11	10	15	20	24	50

+50 4.9 11.45

11.85	10.25	8.75	8.95	11.35	11.45	11.45	11.35	11.25	10.05	9.15
4.5	6.1	7.6	7.4	5.0	4.9	4.9	5.0	5.1	6.3	7.2
50	24	20	15	10	10	15	20	23	25	50

16.35

16.35

10.32 28

+54 Elec Pole 20.5 RT

+50 4.4 13.92

27 4.5 13.82

+90 4.6 13.72

+50 4.6 13.72

+42 Elec Pole 21 RT

26 4.7 13.62

+50 4.8 13.52

25 4.9 13.42

+50 5.1 13.22

18.32

±

LT	RT
12.42	12.72
5.9	5.6
50	20
12.52	12.32
5.8	6.0
50	20
12.52	12.52
5.8	4.0
50	20
12.42	12.52
5.9	5.8
50	20
11.82	12.12
6.5	6.2
50	20
12.02	12.12
6.3	5.2
50	20
11.72	12.02
6.6	5.3
50	20
11.32	12.32
7.0	5.0
50	20

18.32

29

+87 Tel Pole 21' Lt

+50

11.7

18.66

Lt.

13.56

14.36

18.56

18.86

18.66

18.76

18.96

21.36

28.26

30

16.8  
50.

16.0  
40.

11.8  
20.

11.5  
15.

11.7  
15.

11.6  
15.

11.4  
20.

9.0  
23.

2.1  
50.

13.36  
17.0  
50

13.56  
16.8  
32

15.26  
15.1  
20

16.16  
14.2  
15

17.36  
13.0  
12.

17.36  
13.0  
15.

17.56  
12.8  
15.

17.76  
12.6  
20.

20.16  
10.2  
23.

26.46  
3.9  
50.

30

13.0

17.36

Mail Pole #79014

T. P.

12.84

30.36

0.80

17.52

30.36

+58 Tel. Pole 20' Lt.

+50

2.1

16.22

13.32  
5.0  
50

14.52  
3.8  
20

13.62  
4.7  
15

16.32  
2.0  
10

16.22  
2.1  
15

16.42  
1.9  
15

16.72  
1.6  
20

16.72  
1.6  
25

17.12  
1.2  
44.

20.32  
4.0  
50

+45 Elec Pole 20.5' Rt.

29

3.1

15.22

12.72  
5.6  
50

13.52  
4.8  
20

12.32  
4.0  
15

15.22  
3.1  
10

15.22  
3.1  
15

15.52  
2.8  
15

15.72  
2.6  
20

15.92  
2.4  
23

14.32  
4.0  
26

14.02  
4.3  
50

+69 Eucalyptus Tree 19' Lt.

+63 Tel Pole 20' Lt

+50

3.9

14.42

12.72  
5.6  
50

13.32  
5.0  
20

12.02  
6.3  
15

14.52  
3.8  
10

14.42  
3.9  
15

14.52  
3.8  
20

14.72  
3.5  
20

14.72  
3.6  
21

12.82  
5.5  
24

13.92  
5.4  
50

+40

3.9

14.42

12.62  
5.7  
50

13.32  
5.0  
20

13.92  
4.4  
16

14.42  
3.9  
10

14.42  
3.9  
15

14.52  
3.8  
20

14.52  
3.8  
21

14.72  
3.8  
25

12.72  
5.6  
50

13.92  
5.4  
50

28

4.2

14.12

12.42  
5.9  
50

13.02  
5.3  
20

13.82  
5.0  
15

14.22  
4.1  
8

14.12  
4.2  
15

14.02  
4.3  
20

14.12  
4.2  
21

14.12  
4.2  
24

12.12  
5.7  
50

13.02  
5.3  
50

18.32

18.32



¢

+86 Large Fan Palm 12' Lt  
 +73 Tree stump 20" Diam 12' Lt  
 +69 Tel Pole 20' Lt

+58 Large Fan Palm 12' Lt

+50 2.7 27.66

+38 Acacia Tree 14" Diam 12' Lt

33 4.8 25.56

SEE FB 1552 PAGE 2

+50 6.3 24.06

+40.5 Elae Pole 20' RT.

+21 Tel Pole 21' Lt

32 4.7 22.66

+50 9.1 21.26

31 10.5 19.86

30.36

31

RT

¢

RT

25.36	24.76	24.96	27.56	27.66	28.06	28.16	28.96	30.36	32.96
5.0	5.1	5.4	2.8	2.7	2.3	2.2	1.4	3.0	12.6
50	20	15	10	15	15	20	30	50	50

20.86	20.36	19.36	19.66	23.56	25.86	25.56	26.16	26.56	27.66	29.96
9.5	10.0	11.0	10.7	6.8	4.5	4.8	4.2	3.8	2.7	3.0
50	40	38	20	15	12	8	15	20	36	50

17.36	18.86	20.96	24.36	24.06	24.46	24.76	25.36	27.06
13.0	11.5	9.4	6.0	6.3	5.9	5.6	5.0	3.8
50	20	15	10	10	15	20	38	50

16.66	20.66	21.36	22.76	22.66	23.06	23.26	25.56	28.36
13.7	9.7	9.0	7.6	7.7	7.3	7.1	4.8	2.0
50	20	15	12	15	15	20	21	50

17.06	20.56	21.46	21.26	21.56	21.76	26.16	28.06	30.26	32.06
13.3	9.8	8.7	9.1	8.8	8.6	4.2	2.3	0.1	1.7
50	20	15	15	15	20	13	34	56	50

14.36	19.96	20.26	19.86	20.06	20.26	25.66	29.96
16.0	10.4	10.1	10.5	10.3	10.1	4.7	0.4
50	20	15	15	15	20	23	50

30.36

36

4  
3.7 37.60

LT. RT.  
36.60 36.80 37.00 37.60 37.60 37.90 39.60 40.70 41.20  
4.7 4.5 4.3 3.7 3.7 3.4 1.7 0.6 50.1  
50 20 15 15 15 20 22 40 50

+92<sup>6</sup> M.H. 16<sup>5</sup> Rt.

+75 Large Fan Palm 18' Lt.

+67 Elec Pole 19' Rt.

+59 Tree Stump 20" Diam 11' Lt.

+50 5.5 35.80

37.70  
36.0  
16.5  
TOP.M.H.  
35.30 35.50 35.80 35.80 35.90 35.90 37.20 40.20 40.70  
6.0 5.8 5.5 5.5 5.4 5.4 4.1 1.1 0.6  
50 20 15 15 15 17 20 40 50

+43 Large Fan Palm 11' Lt

35. 34.40

33.10 34.10 34.40 34.80 34.40 34.50 35.20 36.80 38.80  
8.2 7.2 6.9 6.5 6.9 6.8 6.1 4.5 2.5  
50 20 15 10 15 15 20 26 50

+76 Tel Pole 21' Lt.

+54<sup>67</sup> Tree Stump 18" Diam 12' Lt.

+50 8.7 32.60

32.10 32.60 32.60 32.90 32.60 32.60 32.70 34.00 35.40 38.30  
9.2 8.7 8.7 8.4 8.7 8.7 8.6 7.3 5.9 3.0  
50 20 15 9 15 18 20 25 50

+35 Tree Stump 20" Diam 12' Lt.

Tel. Pole 8.19.19.7

T.P. Nail } 11.31 41.30 0.37

29.99 ✓

(27.98)

+19 Large Fan Palm 12' Lt.

+03 Tree Stump 18" Diam 12' Lt.

34. 0.3 30.06

29.00 29.16 29.56 30.06 30.36 30.36 31.96 33.36 34.66 35.76  
1.3 1.2 0.8 0.5 0.0 0.0 +1.6 +3.0 +4.3 +5.4  
50 20 15 16 18 20 33 36 50

30.06

+89 Elec Pole 20' Rt.

30.36

38. 5.0 41.55

3 Nails in  
8' x 8' Fence Post  
8 ft. Rt. Sh. 37164

BM. 4 } 0.68 46.55 0.68 45.87

+51 Tree stump 16" Diam 10' Lt.

50 5.7

Nails Elec  
Pole # 79021

T.P. 5.51 46.55 0.26 41.04  
= 41.04

+35 Large Fan Palm 11' Lt.

+24 Elec Pole 20.5 Ft.

+19 Tree stump. 14" Diam 10' Lt.

+04 Large Fan Palm 10' Lt.

37 1.5 39.80

+70 Large Fan Palm 10.5 Lt.

+55 Tree stump. 11' Lt.

+50 2.5 38.80

+39 Large Fan Palm 11' Lt.

+24 Tel Pole 20' Lt

+23 Tree stump 18" Diam 11' Lt.

+06 Large Fan Palm 11' Lt

34 41.30

38.25	Lt.	38.25	39.05	39.55	41.55	41.55	41.95	42.05	42.65
8.3		8.3	7.5	7.0	5.0	5.0	4.6	4.5	3.9
50		50	20	15	9	15	15	20	50

38.55	38.55	39.85	40.35	41.05	40.85	41.05	41.45	42.15	44.05
8.0	8.0	6.7	6.2	5.5	5.7	5.5	5.1	4.4	2.5
50	30	20	15	10	15	15	20	30	50

38.20	38.80	39.00	39.80	39.80	39.80	41.00	41.50	42.80
3.1	2.5	2.3	1.5	1.5	1.5	0.3	0.2	1.5
50	20	15	15	15	20	23	30	50

37.30	38.20	38.40	38.80	38.80	38.80	40.50	41.70	42.50
4.0	3.1	2.9	2.5	2.5	2.5	0.8	0.6	1.2
50	20	15	25	15	20	23	30	50

41.30

41  
 40.24 1.2  
~~39.0~~ C 2.15 5.4 41.15

21.  
 C 0.7  
~~C 1.7~~  
 25.8  
 38.75  
 7.8  
 50  
 5.5  
 20  
 5.4  
 15  
 5.4  
 15  
 5.4  
 15  
 4.9  
 20  
 3.8  
 20  
 4.2  
 50  
 Rt.  
 42.75  
 42.35  
 34  
 C 2.3  
~~C 2.3~~  
 25.7

+50  
 40.63 (5) 0.9  
~~39.75~~ C 2.30 5.1 41.45

C 0.9  
~~C 2.3~~  
 25.2  
 39.75  
 6.9  
 50  
 5.5  
 30  
 5.4  
 20  
 5.3  
 15  
 5.1  
 15  
 4.45  
 15  
 4.55  
 20  
 4.5  
 50  
 1.2  
 C 2.0  
 25.9

+12 Elec Pole 22. Rt.  
 40.81 C 0.6  
~~39.20~~ C 2.25 5.1 41.45

0.8  
~~C 2.4~~  
 25.5  
 39.55  
 7.0  
 50  
 5.5  
 20  
 5.3  
 15  
 5.1  
 15  
 4.45  
 15  
 4.5  
 20  
 4.4  
 50  
 C 1.5  
~~C 3.2~~  
 25.7

+81<sup>99</sup> E.C. 5.1 41.45

39.55  
 7.0  
 50  
 39.85  
 6.7  
 40  
 41.25  
 5.3  
 20  
 41.25  
 5.3  
 15  
 41.45  
 5.1  
 15  
 41.45  
 4.4  
 20  
 42.55  
 4.0  
 50

+29<sup>12</sup> Ctr. of Curve. 5.0 41.55

38.55  
 8.0  
 50  
 39.25  
 7.3  
 35  
 40.25  
 6.3  
 20  
 41.25  
 5.3  
 15  
 41.55  
 5.0  
 15  
 41.85  
 4.7  
 20  
 42.55  
 4.0  
 50

39  
 +76<sup>25</sup> B.C. 4.9 41.65

38.35  
 8.1  
 50  
 38.45  
 8.1  
 40  
 40.55  
 6.0  
 20  
 41.55  
 5.0  
 15  
 41.65  
 4.9  
 15  
 42.05  
 4.3  
 15  
 42.35  
 4.2  
 20  
 43.05  
 3.5  
 50

+68 Elec Pole 23. Rt.  
 +50 4.8 41.75

39.05  
 7.5  
 50  
 39.95  
 5.6  
 20  
 40.85  
 5.4  
 16  
 41.75  
 4.8  
 11  
 41.75  
 4.8  
 15  
 42.25  
 4.3  
 15  
 42.55  
 4.0  
 20  
 43.05  
 3.5  
 50  
 46.55

46.55

44. 34.55 C 4.0 3.9 38.56

C 44  
26.5 (4)

38.46  
40 3.4 3.6 3.8 3.9 3.8 4.2 3.0  
50 40 20 15 30 15 20 24  
38.46  
39.06  
38.86  
38.66  
38.56  
38.66  
38.16  
39.46  
39.66  
39.26  
40.46  
39.66  
2.8 C 5.2  
50 18.0

+50 38.65 C 3.8.1 3.0 39.46

C 40  
24.2 (2)

38.46  
40 3.0 2.8 3.0  
50 20 15 20  
38.46  
39.46  
39.66  
39.46  
39.66  
39.26  
40.46  
39.66  
2.8 C 5.8  
50 27.0

+17 Elec Pole 22. RT.

43. 36.75 C 3.06 2.7 39.76

C 33  
27.0

38.56  
39.76  
39.86  
39.86  
39.76  
39.86  
40.66  
40.66  
40.36  
40.96  
40.96  
3.9 3.7 2.6 2.6 2.7 2.6 1.8 1.8 2.1 1.5 1.5  
50 40 20 15 20 12 13 15 20 30 30  
C 44  
26.8

New Elec Pole # 79037  
T.P. 0.68 43.08  
0.04 42.46 4.15

42.40  
542.39

42.46

+50 37.85 2.4 C 3.75 6.3 40.25

23  
C 26  
26.4

38.95  
39.75  
40.05  
40.25  
40.25  
40.85  
41.95  
41.95  
41.95  
41.95  
41.95  
7.6 6.8 6.5 6.3 6.3 5.7 4.6 4.6 4.6  
50 20 15 15 15 20 30 50  
C 44  
26.8

42 38.84 1.8 C 2.50 5.9 40.65

17  
C 24  
26.4

39.25  
40.55  
40.65  
40.65  
40.85  
41.85  
42.25  
42.25  
42.25  
42.25  
42.25  
7.3 6.8 5.9 5.9 5.7 5.2 4.3 4.3 4.3  
50 20 15 15 15 20 30 50  
C 44  
26.5

+50 39.64 1.45 C 2.15 5.5 41.05

15  
C 20  
26.3

39.65  
40.95  
40.95  
41.05  
41.05  
41.95  
42.95  
42.95  
42.95  
42.95  
42.95  
6.9 5.4 5.6 5.5 5.5 4.6 3.6 3.6 3.6  
50 20 15 15 15 20 30 50  
C 44  
26.6

46.55

46.55

T.P. 1.54 3 1,37 12.63 29.43

+25

13.7 28.76

	30.06								
	12.4	13.0	13.0	13.7	13.0	13.3	18.1	20.0	
	50.	20	15		15.	20	24	50	
	29.46	29.46	29.46	28.76	29.46	29.16	24.36	22.46	

+04 Elec Pole RR Rt.

46

30.15 C 0.2 13.1 30.0 12.5 29.96

C 3.8	32.56	33.46	30.96	30.26	29.96	30.56	30.96	30.16	
26.5	9.9	9.0	11.5	12.2	12.5	11.9	11.5	12.3	C 1.0
	50.	20.	14.	15.		15.	20.	50.	23.8

+75

11.2 31.26

	32.56	33.46	30.96	30.26	29.96	30.56	30.96	30.16	
	9.7	9.2	10.0	11.0	11.2	10.8	10.8	5.6	
	50	23	20	15		15	18	20	50
	32.46	31.46	31.26	31.66	31.66	31.66	34.86	36.86	

+50

31.25 Gr. 11.8 31.3 10.0 32.46

C 6.1	32.86	37.46	32.96	32.56	32.46	32.86	33.76	37.86	37.46
27.8 (3)	4.6	5.0	9.5	9.9	10.0	9.6	8.7	4.6	5.0
	50	23	20	15		15	14	20	50
	32.46	37.46	32.96	32.56	32.46	32.86	33.76	37.86	37.46

45

32.35 C 0.4 11.1 32.0 7.3 35.16

C 6.9	38.16	38.06	35.06	35.16	35.16	35.46	35.66	39.06	38.66
29.0 (4)	4.3	4.4	7.4	7.3	7.3	7.0	6.8	3.4	3.9
	50	23	20	15		15	20	23	50
	38.16	38.06	35.06	35.16	35.16	35.46	35.66	39.06	38.66

+50

33.45 C 1.2 8.8 34.9 5.0 37.46

C 5.4	38.16	38.66	37.16	37.36	37.46	37.46	37.56	37.16	
28.7	4.3	3.8	5.3	5.1	5.0	5.0	4.9	3.3	3.3
	50	23	20	15		15	20	24	50
	38.16	38.66	37.16	37.36	37.46	37.46	37.56	37.16	

42.46

C 6.4 29.7

48 1/25 = 0.1 26.62 F0.45 5.2 26.17

F88 17.67  
35.6 50 13.7 17.87  
24 20 13.5 11.3 14.07  
15 12 5.3 26.07  
5.2 26.17  
4.6 26.77  
15

Rt.  
20.67 19.87 26.67 27.97  
10.7 11.5 4.7 3.4  
20 32 43 50  
351 37

+72 5.2 26.17

17.87 18.67 24.67 26.37 26.17 26.57 22.87 20.27 20.87 24.77  
13.5 12.7 6.7 5.0 5.2 4.8 8.5 11.1 10.5 6.6  
50 30 20 15 15 15 20 26 43 50

+65 Boy Super 5.2 26.17

20.17 25.37 26.07 26.17 26.57 23.97 20.27 20.97  
11.2 6.0 5.3 5.2 4.8 7.4 11.1 10.4  
50 20 15 15 15 20 28 50

+50 27.37 F1.2 5.2 26.17

F44 20.87 25.07 26.07 26.17 26.57 22.57 26.57 20.97  
30.8 50 6.3 5.3 5.2 4.8 8.8 10.8 10.4 F66  
20 15 15 15 15 20 28 50 32.6

+40 5.1 26.27

17.37 18.37 24.27 26.17 26.27 26.57 23.67 20.77 21.37  
14.0 13.0 7.1 5.2 5.1 4.8 7.7 10.6 10.0  
50 33 20 15 15 15 20 27 50

47 28.15 F1.4 4.6 26.77

F95 17.77 19.67 22.97 26.87 26.77 26.97 24.77 21.47 21.67 F66  
36.5 50 11.7 8.4 4.5 4.6 4.4 5.6 9.9 9.7 33.8  
25 20 15 15 15 20 26 50

+50 29.07 F1.0 3.2 28.07

F74 22.57 21.07 21.07 25.57 28.27 28.07 28.37 25.47 22.57 21.77  
34.4 50 10.3 10.3 5.8 3.1 3.8 3.0 5.9 8.8 9.6 F70  
35 26 20 15 15 15 20 16 50 32.6

31.37

31.37

4

+49<sup>63</sup>  $\frac{1}{2}S=0.2$  E.C. 22.87  $\approx 2.2$  6.3 25.07

+21 Guy Pole 19' Lt.

+14 Elec Pole 32' Rt.

50  $\frac{1}{2}S=0.3$  23.62  $\approx 1.8$  6.0 25.37

+50  $\frac{1}{2}S=0.3$  24.37  $\approx 1.6$  5.4 25.97

49.  $\frac{1}{2}S=0.3$  25.12  $\approx 1.0$  5.3 26.07

+66 Guy Pole 26' Lt.

+64<sup>92</sup> B.C. Rt. 5.1 26.27

+63 Elec Pole 24' Rt.

+50  $\frac{1}{2}S=0.2$  25.87 C.O.S 5.0 26.37

+32 12.7 18.67

31.37

LT

RT

14.37

17.67

19.37

22.27

24.17

25.07

24.37

24.37

24.57

30.77

36.57

38.17

F46 17.0 13.7 12.0 9.1 7.2 6.3 7.0 7.0 6.8 0.6 +52 +68

29.0 50 25 20 15 12 15 20 28 36 42 40 50

20.37

24.07

24.57

24.77

25.37

25.27

25.27

25.37

28.57

37.37

37.97

C09 11.0 7.3 6.8 6.6 6.0 6.1 6.1 6.0 2.8 +6.0 +6.6

24.1 50 41 20 15 15 20 24 29 31 31 50

22.77

21.97

23.27

26.17

25.97

25.87

26.17

26.17

24.67

29.67

35.67

35.37

F25 9.2 9.4 8.1 5.2 5.4 5.5 5.2 5.2 1.7 1.7 +43 +40

26.5 50 20 15 10 15 20 23 30 36 37 50

18.87

25.77

25.07

25.37

26.17

26.07

26.17

26.97

24.97

31.07

31.07

C07 12.5 5.6 6.3 6.0 5.2 5.3 5.2 4.4 4.4 0.3 0.3 C40

23.0 50 28 20 15 11 15 20 23 27 50 24.2

17.37

17.77

19.77

21.97

26.27

26.27

26.27

26.37

26.17

24.17

24.77

27.07

14.0 13.6 11.6 9.4 5.1 5.1 5.1 5.0 5.2 7.2 6.6 4.3

50 26 20 15 9 15 20 24 27 41 50

17.67

18.17

22.27

26.27

26.37

24.37

24.57

23.67

23.77

26.97

F82 13.7 13.2 9.1 5.1 5.0 5.0 4.8 2.9 7.6 4.4 C04

35.0 50 20 15 9 15 20 26 35 50 21.4

17.87

18.07

18.17

18.67

18.87

18.97

19.67

22.57

26.87

13.5 13.3 13.2 12.7 12.5 12.4 11.7 8.8 4.5

50 20 15 15 15 20 30 33 50

Under Press  
No Yardage

31.37

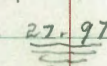


Grade	$\epsilon$	Grad	$\epsilon$	Grad	Sum	lt	lt	lt	lt	lt	lt	lt	lt	lt	lt
53	19.83	F5.86	14.0	13.97	$\frac{F6.3}{33.2}$	$\frac{12.97}{15.0}$ 50	$\frac{13.97}{14.0}$ 20	$\frac{13.97}{14.0}$ 15	$\frac{13.97}{14.0}$ 15	$\frac{13.97}{14.0}$ 15	$\frac{13.97}{14.0}$ 20	$\frac{13.97}{14.0}$ 20	$\frac{13.97}{14.0}$ 24	$\frac{18.37}{9.6}$ 29	$\frac{18.87}{9.1}$ 50
+50	20.23	F6.56	14.3	13.67	$\frac{F7.3}{33.8}$	$\frac{13.07}{14.9}$ 50	$\frac{13.77}{14.2}$ 20	$\frac{13.77}{14.2}$ 15	$\frac{13.67}{14.3}$ 15	$\frac{13.67}{14.3}$ 18	$\frac{13.67}{14.3}$ 20	$\frac{15.27}{12.7}$ 27	$\frac{15.27}{12.7}$ 27	$\frac{19.57}{8.4}$ 50	$\frac{19.97}{8.0}$ 50
52.	20.75	F7.38	14.4	13.37	$\frac{F7.3}{33.8}$	$\frac{13.57}{14.4}$ 50	$\frac{13.57}{14.4}$ 20	$\frac{13.47}{14.5}$ 15	$\frac{13.37}{14.4}$ 15	$\frac{14.47}{13.5}$ 12	$\frac{15.97}{12.0}$ 15	$\frac{15.97}{12.0}$ 20	$\frac{20.67}{7.3}$ 20	$\frac{21.27}{6.7}$ 47	$\frac{24.17}{3.8}$ 50
+50	21.38	F7.0	13.6	14.37	$\frac{F8.0}{35.0}$	$\frac{13.47}{14.5}$ 50	$\frac{13.47}{14.5}$ 20	$\frac{13.47}{14.5}$ 15	$\frac{14.37}{13.6}$ 15	$\frac{16.97}{11.0}$ 6	$\frac{22.27}{5.7}$ 13	$\frac{22.27}{5.7}$ 15	$\frac{22.27}{5.7}$ 20	$\frac{22.47}{5.5}$ 41	$\frac{38.17}{9.5}$ 47
51	22.0.6	22.12	C1.75	4.1	23.87	$\frac{F8.5}{35.9}$	$\frac{13.67}{14.3}$ 50	$\frac{13.97}{14.0}$ 25	$\frac{16.47}{11.5}$ 20	$\frac{17.97}{10.0}$ 15	$\frac{23.77}{4.2}$ 5	$\frac{23.87}{4.1}$ 5	$\frac{23.27}{4.7}$ 15	$\frac{23.27}{4.7}$ 20	$\frac{23.37}{4.6}$ 33
+75			4.0	23.97		$\frac{13.77}{14.2}$ 50	$\frac{13.87}{14.1}$ 35	$\frac{24.37}{8.2}$ 20	$\frac{19.77}{8.2}$ 15	$\frac{24.97}{7.0}$ 6	$\frac{23.97}{4.0}$ 4	$\frac{23.97}{4.0}$ 4	$\frac{23.97}{4.0}$ 20	$\frac{24.07}{3.9}$ 33	$\frac{33.97}{4.0}$ 43
Nail Pole 18	2.64	27.97	6.04	25.33											
lt. of Sta 50+21 T.P.				25.33											
				25.32											
				12.55											
				9.49											
				18.23											
				21.33											
				31.37											

30 49.7

23 41.2

35 50 32.0



		$\frac{1}{2}S = 0.86$		$\frac{1}{2}S = 0.6$	Grade	$\frac{1}{2}S = 0.3$	18.97	F 4.1	5.1	14.9	F 5.4	12.73	13.73	13.23	13.43	14.23	14.93	15.33	18.03	18.43	F 0.4
56		18.76	3.6	4.8	15.2	7.7	14.33	F 5.5	11.8	10.23	10.33	13.53	13.73	14.33	14.93	17.13	17.13	18.03	18.03	F 2.1	
				4.8	15.2	7.7	14.33	20.8	50	35	20	18	15	18	20	50	50.6			(29)	
+50		18.84	F 3.6	4.8	15.2	7.7	14.33	F 5.2	11.5	10.53	13.03	13.23	14.33	14.43	17.63	17.63	18.13	18.13	F 1.0		
				4.8	15.2	7.7	14.33	30.5	30	35	20	18	15	19	20	50	55.0			(34)	
55		18.97	F 4.1	5.1	14.9	7.8	14.23	F 5.4	9.3	12.73	13.73	13.43	14.23	14.93	15.33	18.03	18.03	18.43	18.43	F 0.4	
				5.1	14.9	7.8	14.23	31.1	50	40	20	15	18	20	25	50	52.0			(37)	
TP. Nail Pole	2.41	22.03	8.35		19.62																
#79043	0.34	19.96			21942																
+50		19.17	F 4.30	5.2	14.8	13.1	14.87	F 4.8	13.47	13.47	13.97	13.37	14.87	15.87	15.87	16.17	18.27	18.27	18.47	18.47	9.5
				5.2	14.8	13.1	14.87	31.4	50	20	15	15	21	25	30	50	62.2			(40)	
54		19.3	F 4.9	13.6	14.37			F 5.7	13.47	13.47	13.47	14.37	14.67	14.87	14.87	14.87	17.87	17.87	18.37	18.37	8.5
				13.6	14.37			31.7	50	20	15	15	20	26	34	50	62.1			(42)	
+50		19.52	F 5.25	13.7	14.27			F 6.0	13.37	12.97	12.97	14.27	14.27	14.27	15.27	17.97	17.97	18.37	18.37	2.6	
				13.7	14.27			32.0	50	20	15	15	20	27	33	50	65.0			(43)	
		27.97																			

22.03

27.97

65.0

+50  $\frac{1}{2}S=0.9$  19.37 F 5.34

£

8.0 14.03

F50  
30.5

Lt.

12.83  
9.2  
50

13.83  
8.2  
20

13.93  
8.1  
15

14.03  
8.0

14.63  
7.4  
15

15.33  
6.7  
20

17.23  
4.8  
26

18.33  
3.7  
50

41

C.0.2  
631  
(40)

59  $\frac{1}{2}S=0.9$  19.75 F 5.32

8.1 13.93

F55  
30.8

13.03  
9.0  
50

13.63  
8.4  
20

13.93  
8.1  
15

13.93  
8.1

14.83  
7.2  
15

15.63  
6.4  
20

16.73  
5.3  
27

17.43  
4.6  
50

F22  
60.3  
(36)

$\Delta$  +50  $\frac{1}{2}S=0.9$  19.13 F 4.90

7.8 14.23

F48  
30.2

12.93  
9.1  
50

13.63  
8.4  
20

13.63  
8.4  
15

14.23  
7.8

14.23  
7.8  
15

16.53  
5.5  
20

17.03  
5.0  
50

F34  
54.0 (30)

58  $\frac{1}{2}S=0.9$  19.00 F 5.37

8.4 13.63

F44  
29.6

12.03  
10.0  
50

13.43  
8.6  
40

14.03  
8.0  
20

14.83  
7.2  
15

13.63  
8.4

14.03  
8.0  
13

15.63  
5.4  
15

16.83  
5.2  
17

16.83  
5.2  
20

17.33  
4.7  
48

15.15  
6.9  
50

F33  
49.4  
(28)

+50  $\frac{1}{2}S=0.9$  18.88 F 5.45

8.6 13.43

F46  
29.6

11.53  
10.5  
50

13.63  
8.4  
35

14.53  
7.5  
20

13.83  
8.2  
15

13.43  
8.4

13.83  
8.2  
11

16.83  
5.2  
15

16.83  
5.2  
20

17.93  
4.1  
46

14.43  
7.6  
50

F26  
47.1  
(24)

57  $\frac{1}{2}S=0.9$  18.78 F 4.95

6.1 13.9  
8.2 13.83

F57  
30.8

11.33  
10.7  
50

12.43  
9.6  
35

13.23  
8.8  
20

13.63  
8.4  
15

13.83  
8.2

13.83  
8.2  
11

16.83  
5.2  
15

16.93  
5.1  
20

17.43  
4.6  
46

14.53  
7.5  
50

F25  
46.2  
(24)

+50  $\frac{1}{2}S=0.9$  18.73 F 3.14

4.7 15.3  
8.3 13.73

F48  
29.3

10.03  
12.0  
50

10.03  
12.0  
40

12.03  
10.0  
35

12.33  
9.7  
20

13.13  
8.9  
15

13.73  
8.3

14.73  
7.3  
13

16.63  
5.4  
15

16.93  
5.1  
20

17.53  
4.5  
48

15.03  
7.0  
50

F22  
47.7  
(24)

22.03

		Grade		\$	
+50	20.12	1.95	5.7	18.17	

F47  
29.6

14.37	15.87	16.57	18.17	18.77	19.87	19.87	19.87	21.07	42
9.5	8.0	7.3	5.7	5.1	4.0	4.0	4.0	2.8	
50	20	15		6	13	15	20	50	

23.87

T.P. BM #5	2.47	23.87	0.63		21.40
					= 21.40

3. Nails in Elec. Pole # 79046 Rt. of Sta 59+65

62	1/2 S = 0.1	20.0	2.37	4.4	17.63
----	-------------	------	------	-----	-------

F50  
30.2

14.03	15.23	15.93	17.63	18.83	20.03	20.03	20.73
8.0	6.8	6.1	4.4	3.2	2.0	2.0	1.3
50	20	15		13	15	20	50

# +50	1/2 S = 0.5	19.87	3.44	5.6	16.43
-------	-------------	-------	------	-----	-------

F51  
30.5

14.03	14.73	15.43	16.43	18.73	19.13	19.93	20.53
8.0	7.3	6.6	5.6	3.3	2.9	2.1	1.5
50	20	15		15	20	23	50

+37.08 E.C.

61	1/2 S = 0.7	19.76	4.72	7.0	15.03
----	-------------	-------	------	-----	-------

F47  
30.0

14.23	14.03	14.23	15.03	16.53	17.03	17.03	18.23	20.03
7.8	8.0	7.8	7.0	5.5	5.0	5.0	3.8	2.0
50	20	15		15	20	21	15	50

+50	1/2 S = 0.9	19.62	5.29	7.7	14.33
-----	-------------	-------	------	-----	-------

F47  
30.2

13.63	14.23	14.23	14.33	15.23	16.43	18.33	19.73
8.4	7.8	7.8	7.7	6.8	5.6	3.7	2.3
50	20	15		15	20	26	50

60.	1/2 S = 0.9	19.50	5.87	8.4	13.63
-----	-------------	-------	------	-----	-------

F6.2  
31.7

13.53	14.23	14.43	13.63	14.63	15.23	16.23	17.53	18.83
8.5	7.8	7.6	8.4	7.4	6.8	5.8	4.5	3.2
50	20	15		15	20	26	29	50

22.03

22.03

F15  
62.0  
37.0

¢

66 21.0 F 3.13 6.0 17.87

F55	9.0	9.0	9.1	5.6	6.0	6.0	5.9	5.9	9.3	10.0	F33
33	50	20	15	6		15	20	25	30	50	251
	14.87	14.87	14.77	18.27	17.87	17.87	17.97	17.97	14.57	13.87	43

+50 20.87 F 3.30 6.3 17.57

F66	8.5	9.7	9.5	8.5	6.1	6.3	6.0	6.0	5.6	9.0	8.7	F34
32.9	50	30	20	15	7		15	20	26	29	50	281
	15.37	14.17	14.37	15.37	17.77	17.57	17.87	17.87	18.27	14.87	15.17	

65 20.75 F 2.58 5.7 18.17

F73	9.1	11.4	9.6	9.5	9.0	5.5	5.7	5.8	5.8	5.6	8.1	8.2
34.50	30	20	15	8	2			15	20	27	30	50
	14.77	12.47	14.27	14.37	14.87	18.37	18.17	18.07	18.07	18.27	15.77	15.67

+50 20.62 F 2.55 5.8 18.07

F60	10.5	9.2	9.0	8.3	5.8	5.7	5.7	5.7	5.0	7.2	7.3
31.0	50	20	15	5	5			15	20	43	50
	13.37	14.67	14.87	15.57	18.07	18.17	18.17	18.87	18.87	16.67	16.57

64 20.50 F 2.13 5.5 18.37

F49	9.7	8.5	8.3	7.7	5.5	5.3	5.3	4.8	4.2	4.2	5.2
30.0	50	20	15	5		15	20	33	34	46	50
	14.17	15.37	15.57	16.17	18.37	18.57	18.57	19.07	19.67	19.67	18.67

+50 20.37 F 2.10 5.6 18.27

F50	9.6	8.3	8.0	6.6	5.6	4.8	4.7	4.6	4.3	3.4	3.1
30.2	50	20	15	2		3	15	20	36	37	50
	14.27	15.57	15.87	17.27	18.27	19.07	19.17	19.27	19.57	20.47	20.77

63 20.25 F 2.38 6.0 17.87

F48	2.5	3.7	9.6	7.7	2.5	6.0	5.7	4.1	4.1	4.0	
29.6	50	45	50	20	15		4	9	15	20	
	21.37	20.17	14.27	16.17	16.37	17.87	18.17	19.77	19.77	19.87	

23.87

C 11  
43.6  
25

23.87

69	Grade		C																	
	21.70	3.71	4.9	17.99	F51	5.4	6.3	6.7	4.9	4.9	4.7	4.7	4.6	6.5	6.5					
					30.1	50	20	15	11	11	15	20	23	20	5.0					
						17.29	16.59	16.19	17.99	17.99	18.19	18.19	18.29	16.39	16.39					

+50	21.61	3.72	5.0	17.89	F50	6.6	6.2	7.1	5.2	5.0	5.1	5.1	5.1	6.5	7.0					
					30.2	50	20	15	12	5.0	15	20	23	26	5.0					
						16.29	14.69	15.79	17.69	17.89	17.79	17.79	17.79	16.39	15.89					

68	21.50	3.81	5.2	17.69	F54	7.0	6.8	6.7	5.2	5.2	5.1	5.1	5.1	6.5	7.1	F46				
					30.5	50	20	15	12	12	15	20	23	27	30	29.3				
						15.89	16.09	16.19	17.69	17.69	17.79	17.79	17.79	16.39	15.79					

+50	21.37	3.68	5.2	17.69	F57	7.3	6.7	6.8	5.3	5.2	5.2	5.2	5.1	6.5	7.5	F53				
					31.4	50	30	20	15	12	15	20	23	25	30	29.3				
						15.59	15.89	16.19	16.09	17.59	17.69	17.69	17.69	16.39	15.39					

67	21.25	F3.66	5.3	17.59	F52	7.6	7.2	6.6	7.1	5.0	5.3	5.3	5.2	7.0	7.6	F54				
					30.2	50	30	20	15	11	15	20	23	27	30	29.3				
						15.29	15.69	16.29	15.79	17.89	17.59	17.59	17.59	15.89	15.29					

+50	21.12	F3.53	5.3	17.59	F54	7.3	7.5	7.0	7.5	5.3	5.3	5.1	5.1	5.2	7.7	8.7	F54			
					30.2	50	30	20	15	10	15	20	24	30	30	28.7				
						15.59	15.39	15.89	15.39	17.59	17.59	17.79	17.79	17.69	15.19	14.19				

T.P. 4.23 22.89 5.21 18.66

23.87

22.89

Naal Elec Pole #79049 26' Rt. of sta 66+24

23.87

+50  
Grade 21.50 F 3.41 4.8 18.09

F42  
28.4

5.8	5.2	6.1	5.1	4.8	4.8	4.8	4.5	7.8	7.5	6.7	6.8
50	25	20	15	4	15	20	21	21	33	36	32
											50
											16.89

72  
21.60 F 3.41 4.7 18.19

F45  
29.3

6.0	5.9	6.5	5.1	4.7	4.8	4.8	4.8	8.0	8.0	6.3	7.2
50	30	20	15	4	15	20	21	27	32	35	50
											50
											16.89

+50  
21.69 F 3.30 4.5 18.39

F43  
29.7

6.1	5.3	6.0	5.0	4.5	4.9	4.9	5.0	7.8	7.8	6.7	7.2
50	20	15	13	4	15	20	22	27	32	35	50
											50
											16.89

71  
21.75 F 3.56 4.7 18.19

F47  
30.0

6.0	5.7	6.5	5.0	4.7	4.9	4.9	5.2	8.0	8.0	6.7	6.7
50	20	15	13	4	15	20	22	27	32	35	50
											50
											16.89

+72 Elec Pole 25' At.

+50  
21.77 F 3.68 4.8 18.09

F47  
30.0

6.0	5.6	6.3	5.1	4.8	5.0	5.0	5.1	8.0	8.0	6.9	7.2
50	20	15	12	4	15	20	23	28	32	38	50
											50
											16.89

70.  
21.80 F 3.91 5.0 17.89

F52  
30.5

6.3	6.2	7.0	5.3	5.0	5.0	5.2	5.2	8.2	8.2	6.5	6.5
50	20	15	11	5	15	20	23	32	32	40	50
											50
											16.89

+50  
21.75 F 3.86 5.0 17.89

F45  
30.0

6.0	5.6	6.5	4.7	5.0	4.8	4.8	4.5	5.9	5.6	5.6	5.6
50	21	15	10	5	15	20	23	24	50	50	50
											50
											16.89

22.89

22.89





+67 Elec Pole 21' RT.

79 20.22 F 2.08 4.3 18.14

$\frac{F32}{27.0}$	$\frac{16.24}{6.2}$	$\frac{16.84}{5.6}$	$\frac{17.74}{4.7}$	$\frac{17.84}{4.6}$	$\frac{18.14}{4.3}$	$\frac{18.04}{4.4}$	$\frac{18.34}{4.1}$	$\frac{18.34}{4.1}$	$\frac{F20}{25.1}$
	$\frac{50}{50}$	$\frac{25}{25}$	$\frac{20}{20}$	$\frac{15}{15}$		$\frac{15}{15}$	$\frac{20}{20}$	$\frac{50}{50}$	

+50 20.30 F 2.16 4.3 18.14

$\frac{F35}{27.8}$	$\frac{16.34}{6.1}$	$\frac{16.34}{6.1}$	$\frac{17.54}{4.9}$	$\frac{17.84}{4.6}$	$\frac{18.14}{4.3}$	$\frac{17.99}{4.5}$	$\frac{17.99}{4.5}$	$\frac{17.44}{5.0}$	$\frac{F22}{25.7}$
	$\frac{50}{50}$	$\frac{25}{25}$	$\frac{20}{20}$	$\frac{15}{15}$		$\frac{15}{15}$	$\frac{20}{20}$	$\frac{50}{50}$	

78 20.40 F 2.31 4.4 18.04

$\frac{F40}{27.0}$	$\frac{16.44}{6.0}$	$\frac{16.44}{6.0}$	$\frac{17.14}{5.3}$	$\frac{17.84}{4.6}$	$\frac{18.04}{4.4}$	$\frac{17.84}{4.6}$	$\frac{17.84}{4.6}$	$\frac{17.04}{5.4}$	$\frac{17.04}{5.4}$
	$\frac{50}{50}$	$\frac{25}{25}$	$\frac{20}{20}$	$\frac{15}{15}$		$\frac{15}{15}$	$\frac{20}{20}$	$\frac{29}{29}$	$\frac{31}{31}$

+50 20.50 F 2.36 4.3 18.14

$\frac{F40}{27.2}$	$\frac{16.34}{6.1}$	$\frac{16.24}{6.2}$	$\frac{17.84}{4.6}$	$\frac{17.84}{4.6}$	$\frac{18.14}{4.3}$	$\frac{17.94}{4.5}$	$\frac{17.64}{4.8}$	$\frac{18.44}{4.0}$	$\frac{17.04}{5.4}$
	$\frac{50}{50}$	$\frac{20}{20}$	$\frac{18}{18}$	$\frac{15}{15}$		$\frac{15}{15}$	$\frac{20}{20}$	$\frac{4}{4}$	$\frac{24}{24}$

77 20.60 F 2.66 4.5 17.94

$\frac{F40}{29.3}$	$\frac{15.84}{6.6}$	$\frac{15.84}{6.6}$	$\frac{16.44}{6.0}$	$\frac{17.44}{5.0}$	$\frac{17.44}{5.0}$	$\frac{17.94}{4.5}$	$\frac{17.64}{4.8}$	$\frac{17.54}{4.9}$	$\frac{16.44}{6.0}$
	$\frac{50}{50}$	$\frac{30}{30}$	$\frac{20}{20}$	$\frac{18}{18}$	$\frac{15}{15}$		$\frac{15}{15}$	$\frac{20}{20}$	$\frac{26}{26}$

+72 Elec Pole 23' RT.

+50 20.70 3.06 4.8 17.64

$\frac{F44}{29.0}$	$\frac{15.54}{6.9}$	$\frac{15.74}{6.7}$	$\frac{16.44}{6.0}$	$\frac{17.24}{5.2}$	$\frac{17.64}{4.8}$	$\frac{17.84}{4.6}$	$\frac{17.84}{4.6}$	$\frac{16.44}{6.0}$	$\frac{16.04}{6.4}$
	$\frac{50}{50}$	$\frac{30}{30}$	$\frac{20}{20}$	$\frac{15}{15}$		$\frac{15}{15}$	$\frac{20}{20}$	$\frac{24}{24}$	$\frac{29}{29}$

76 20.80 F 3.46 5.1 17.34

$\frac{F53}{30.2}$	$\frac{15.44}{7.0}$	$\frac{15.84}{6.6}$	$\frac{17.04}{5.4}$	$\frac{17.34}{5.1}$	$\frac{17.54}{4.9}$	$\frac{17.64}{4.8}$	$\frac{15.84}{6.6}$	$\frac{15.84}{6.6}$	$\frac{16.94}{5.5}$
	$\frac{50}{50}$	$\frac{26}{26}$	$\frac{15}{15}$		$\frac{15}{15}$	$\frac{20}{20}$	$\frac{24}{24}$	$\frac{30}{30}$	$\frac{34}{34}$

22.44

22.44

$\frac{F46}{29.8}$



85 21.50 F 3.56 5.0 17.94

17.44  
 5.5 5.5 5.0 4.7 4.0 3.5 5.1 5.0 5.0 5.0 5.1 6.8 4.1 F5.4  
 50 32 27 23 20 17 15 18 26 24 26 50 29.6  
 F4.4  
 29.6  
 22.94

T.P. 4.05 22.94 3.29 18.89  
 = 18.84

Nails in Elec. Pole # 79059 20' Rt. of Sta 84+65

+44 Elec Pole 20' Rt.

+50 21.35 F 3.57 4.4 17.78

17.18 17.48 18.18 16.88 18.18 19.18 17.78 17.78 18.08 17.88 16.08 16.58 16.78  
 F3.8 5.0 4.7 4.0 5.3 4.0 3.0 4.4 4.4 4.1 4.3 6.1 5.6 5.4 F5.5  
 29.0 50 32 27 23 20 17 15 15 18 20 26 40 50 30.8

84 21.20 F 3.22 4.2 17.98

17.28 17.88 16.88 17.98 19.38 17.68 17.98 17.98 18.18 17.78 15.88 16.98 16.98  
 F3.8 4.9 4.3 5.3 4.2 2.8 4.5 4.2 4.2 4.0 4.4 6.3 5.2 5.2  
 28.7 50 27 23 20 17 15 15 15 20 24 26 36 50  
 F4.8  
 30.5

+50 21.05 F 3.37 4.5 17.68

17.48 17.68 16.58 18.38 17.68 17.68 17.98 17.88 17.98 17.98 15.98 17.18 17.18  
 F4.2 4.7 4.5 5.6 3.8 4.5 4.5 4.2 4.3 4.2 6.2 5.0 5.0  
 29.0 50 27 23 20 15 15 15 20 24 26 39 50 50  
 F5.0  
 30.4  
 30.5

83 20.90 3.32 4.6 17.58

17.38 17.78 16.78 17.98 18.98 17.38 17.58 17.88 17.98 17.98 15.88 16.58 17.18  
 F3.6 4.8 4.4 5.4 4.2 3.2 4.8 4.6 4.3 4.2 4.2 6.3 5.6 5.0  
 28.1 50 26 23 20 16 15 15 15 20 24 26 33 50 50  
 F5.0  
 30.5

+63 Elec Pole 20' Rt.

+50 20.75 F 3.27 4.7 17.48

17.58 17.58 18.18 17.18 18.58 17.48 17.48 17.58 18.18 18.18 16.08 16.98 17.08  
 F3.0 4.6 4.6 4.0 5.0 3.6 4.7 4.7 4.6 4.0 4.0 6.1 5.7 5.7  
 27.2 50 40 30 25 20 15 15 18 20 20 36 50 50  
 F4.5  
 27.5  
 22.18

♀

Lt.

♀

Rt

# B.M. 6 5.47 24.54 3.87 19.07  
219.06

19.5' Rt. of Sta 87 + 71.5  
{ U.S. Coast. & Geodetic B.M. # 321-1935.

88. 22.40 F 3.56 4.1 18.84

18.74 18.74 19.44 18.14 20.44 18.84 18.84 18.94 18.74 19.74  
F36 4.2 4.2 3.5 4.4 2.5 4.1 4.1 4.0 4.2 3.2 F3.8  
284 50 32 27 23 20 15 15 20 50 290

+70 Tel Pole 26.5 Lt.

+53 Elec Pole 19.5 Rt.

+50 22.25 F 3.61 4.3 18.64

18.44 18.44 19.44 17.74 20.44 18.54 18.64 18.84 18.84 19.34  
F38 4.5 4.5 3.5 5.2 2.5 4.4 4.3 4.1 4.1 3.6 F3.0  
278 50 32 27 23 20 15 15 20 50 27.8

+38 Gate to Detention Home

87 22.10 F 3.76 4.6 18.34

17.94 18.24 18.94 17.24 19.54 18.24 18.34 18.54 18.54 19.34 19.24  
F34 5.0 4.7 4.0 5.7 3.4 4.7 4.6 4.4 4.4 3.6 3.7 F3.2  
243 50 32 27 23 20 15 15 20 22 50 27.8

+50 21.95 F 3.81 4.8 18.14

17.74 17.94 18.44 16.94 19.34 18.04 18.14 18.24 18.24 19.24 19.14  
F38 5.2 5.0 4.5 6.0 3.6 4.9 4.8 4.7 4.7 3.7 3.8 F3.0  
300 50 32 27 23 20 15 15 20 22 50 27.5

+27 Tel Pole 26' Lt.

+25 Elec Pole # 79060 20. Rt.

86. 21.80 F 3.86 5.0 17.94

17.64 17.74 18.34 16.94 19.54 18.04 17.94 18.74 18.74 18.24 17.94  
F42 5.3 5.2 4.6 6.0 3.4 4.9 5.0 4.2 4.2 4.7 5.0 F3.3  
300 50 32 27 23 20 15 15 20 26 50 28.1

+50 21.65 F 3.61 4.9 18.04

17.44 17.44 18.14 16.84 19.54 17.94 18.04 18.24 17.94 17.94 16.44 17.14  
F37 5.5 5.5 4.8 6.1 3.4 5.0 4.9 4.7 5.0 4.4 6.5 5.8  
284 50 32 27 23 20 15 15 20 44 26 50 30.8

22.94

22.94

F5.2

30.8

+75 3' Lt. Tel Pole  
Grade

+50  $\frac{1}{2}S=1.04$  23.45 3.11 4.2 20.34

	19.74	19.74	19.84	20.44	19.04	19.04	20.34	21.34	19.84	20.14	20.14	20.34	19.14	5.1
F16	4.8	4.8	4.7	4.1	5.5	5.5	4.2	3.2	4.7	4.4	4.4	4.2	5.4	5.4
254	50	20	15	9	7	3		2	4	15	20	40	43	50

91  $\frac{1}{2}S=1.04$  23.30 F 3.56 4.8 19.74

	19.64	19.74	20.14	19.14	21.14	19.84	19.74	19.84	20.04	20.74	19.34	18.94		
F25	4.9	4.8	4.4	5.4	3.4	4.7	4.8	4.7	4.5	3.8	5.2	5.6		
256	50	20	15	11	7	5		15	20	30	36	50		

+50  $\frac{1}{2}S=1.04$  23.15 F 3.61 5.0 19.54

	19.54	19.44	19.94	18.84	20.84	19.44	19.54	19.74	19.84	19.04	18.94			
F23	5.0	5.1	4.6	5.7	3.7	5.1	5.0	4.8	4.7	5.5	5.6	5.2		
253	50	30	25	20	15	11		15	20	28	50	29.0		

+05 25.5 Lt. Tel Pole

90  $\frac{1}{2}S=1.0$  23.00 F 3.52 5.1 19.44

	19.44	19.24	19.64	18.54	21.04	19.34	19.44	19.54	19.54	18.54				
F22	5.1	5.3	4.9	6.0	3.5	5.2	5.1	5.0	5.0	6.0	5.4			
252	50	33	26	20	17	15		15	20	50	31.1			

+66 BC. Lt.

+50  $\frac{1}{2}S=0.4$  22.85 F 3.61 5.3 19.24

	19.14	19.14	20.04	18.54	20.14	20.54	19.14	19.24	19.24	19.44	18.64			
F23	5.4	5.4	4.5	6.0	4.4	4.0	5.4	5.3	5.3	5.1	5.9	4.8		
253	50	32	27	23	20	17	15		15	20	50	30.2		

+05 Elec Pole 19' Rt.

89  $\frac{1}{2}S=0.2$  22.70 F 3.56 5.4 19.14

	19.24	19.24	20.14	18.34	21.04	19.04	19.14	19.04	19.04	18.94				
F22	5.3	5.3	4.4	6.2	3.5	5.5	5.4	5.5	5.5	5.6	4.2			
250	50	32	27	23	20	15		15	20	50	29.3			

+50 22.55 F 3.61 5.6 18.94

	18.74	18.74	19.74	18.34	20.54	18.84	18.94	19.14	18.74	19.14				
F21	5.8	5.8	4.8	6.2	4.0	5.7	5.6	5.4	5.8	5.4	3.9			
258	50	32	24	23	20	15		15	20	50	29.3			

24.54

24.54

24 35  
19 20  
5 15

Grado  
+50 1/2 S = 1.0 24.35 F 4.26 6.7 19.09

94 1/2 S = 1.4 24.20 F 4.61 6.2 19.59

+50 1/2 S = 1.4 24.05 F 4.56 6.3 19.49

T.P. 6.44 25.79 5.19 19.35  
6.67 26.02  
6.0 20.0  
4.8 21.2  
6.3 19.7

93 1/2 S = 1.4 23.90 F 4.56 5.2 19.34

+50 1/2 S = 1.4 23.75 F 4.01 4.8 19.74

92 1/2 S = 1.4 23.60 F 3.16 4.1 20.44  
24.54

LT.  
19.49  
6.3 50  
6.7 20  
6.7 15  
6.7 15  
6.3 15  
6.2 20  
6.0 50  
F 57  
31.7

19.29  
6.5 50  
6.5 20  
6.6 15  
6.2 15  
6.1 15  
6.1 20  
5.1 50  
F 58  
31.4

20.29  
5.5 50  
6.1 20  
6.3 15  
6.3 15  
6.3 15  
6.2 20  
6.2 50  
F 61  
32.3

2579

R.P. Hab 50' Lt. of 94 + 57 04 F.C.

19.94  
4.6 50  
4.5 20  
4.4 15  
5.2 15  
5.3 20  
5.3 26  
5.3 20  
5.3 35  
2.7 40  
20.64  
19.24  
21.84  
20.14  
20.04  
F 55  
31.7

19.84  
4.7 50  
4.7 20  
4.7 15  
4.8 13  
4.8 15  
5.2 20  
3.0 25  
4.6 30  
19.74  
19.74  
20.74  
19.34  
21.54  
19.94  
20.24  
4.3 50  
4.5 50  
F 56  
31.7

19.64  
4.9 50  
4.8 20  
4.8 15  
4.6 2  
5.1 4  
4.1 4  
5.0 6  
5.0 10  
2.7 13  
4.8 15  
19.44  
20.44  
19.54  
19.54  
21.84  
20.04  
20.04  
20.44  
4.5 20  
4.1 50  
F 45  
30.25

2454

98  $\frac{1}{2}S=1.4$  25.40 F 4.91 5.3 20.49 F57  
31.7

+50  $\frac{1}{2}S=1.0$  25.25 F 4.46 5.0 20.79 F56  
31.1

97  $\frac{1}{2}S=0.7$  25.10 F 4.61 5.3 20.49 F50  
30.5

+50  $\frac{1}{2}S=0.3$  24.95 F 5.26 6.1 19.69 F53  
31.4

+25  $\frac{1}{2}S=0.0$

96  $\frac{1}{2}S=0.0$  24.80 F 5.61 6.6 19.19 F55  
31.4

+50  $\frac{1}{2}S=0.0$  24.65 F 5.76 6.9 18.89 F54  
31.4

95  $\frac{1}{2}S=0.5$  24.50 F 5.31 6.6 19.19 F48  
30.2  
25.79

41  
 $\frac{21.09}{4.7}$   
50  
20.79  
 $\frac{20.49}{5.3}$   
15  
 $\frac{20.49}{5.3}$   
20.49  
 $\frac{21.09}{4.7}$   
15  
 $\frac{20.79}{5.0}$   
20  
 $\frac{20.79}{5.0}$   
50  
F31  
27.8

$\frac{21.29}{4.5}$   
50  
20.69  
 $\frac{20.99}{4.8}$   
15  
 $\frac{20.79}{5.0}$   
20  
 $\frac{20.79}{5.0}$   
20  
 $\frac{20.39}{5.4}$   
50  
F38  
28.4

$\frac{21.19}{4.6}$   
50  
20.79  
 $\frac{20.79}{5.0}$   
15  
 $\frac{20.49}{5.3}$   
20  
 $\frac{20.39}{5.4}$   
15  
 $\frac{20.39}{5.4}$   
20  
 $\frac{19.39}{6.4}$   
50  
F39  
28.7

$\frac{20.69}{5.1}$   
50  
19.99  
 $\frac{19.89}{5.9}$   
15  
 $\frac{19.69}{6.1}$   
20  
 $\frac{19.29}{6.5}$   
15  
 $\frac{19.29}{6.5}$   
50  
F55  
31.1

$\frac{19.79}{6.0}$   
50  
19.39  
 $\frac{19.29}{6.5}$   
15  
 $\frac{19.19}{6.6}$   
20  
 $\frac{19.09}{6.7}$   
15  
 $\frac{19.09}{6.7}$   
20  
 $\frac{18.99}{6.8}$   
50  
F56  
31.4

$\frac{19.09}{6.7}$   
50  
18.99  
 $\frac{18.99}{6.8}$   
15  
 $\frac{18.89}{6.9}$   
20  
 $\frac{18.19}{6.6}$   
15  
 $\frac{18.29}{6.5}$   
20  
 $\frac{18.19}{6.6}$   
50  
F57  
31.4

$\frac{19.09}{6.7}$   
50  
19.29  
 $\frac{19.29}{6.5}$   
20  
 $\frac{19.19}{6.6}$   
15  
 $\frac{19.19}{6.6}$   
20  
 $\frac{19.19}{6.6}$   
20  
 $\frac{19.59}{6.7}$   
50  
F58  
31.7

25.79





$\frac{1}{2}$

Station	Grade	Dist	Area	Perim	Area	Perim	Area	Perim	Area	Perim	Area	Perim	
+50 $\frac{1}{2}S=0.5$	26.77	3.08	5.02	23.69	F57 30.2	21.61	21.71	22.91	23.81	23.69	23.69	23.49	
					71 50	70 30	51.8 20	41.9 15	50.2 10 N.Edge Pav	50.2	51.2 10 S.Edge Pav	23.49	
+07 $\frac{1}{2}$ EE			4.89	23.82		21.41	21.51	23.31	24.21	24.08	23.82	23.45	
						23 50	71.2 30	51.4 20	41.5 15	46.5 10 N.Edge Pav	4.89	51.2 10 S.Edge Pav	23.45
+05 $\frac{1}{2}$ Elec Pole 25' RT,													
102 $\frac{1}{2}S=1.00$	26.62	F V 8	23.8		F70 31.1	21.21	21.21	23.01	24.21	24.19	24.05	23.50	
						71.5 50	71.5 30	51.7 20	41.5 15	45.2 71 N.Edge Pav	4.66	51.2 10 S.Edge Pav	23.50
+75			4.66	24.05									
+48 $\frac{1}{2}S=1.14$	26.47	F 2.16	4.40	24.31	F64 32.0	21.11	20.91	22.71	23.41	24.41	24.31	23.71	
						71.6 50	71.4 30	61.0 20	51.3 15	41.3 7 N.Edge Pav	4.40	51.0 15	23.71
Nail at toe													
+25			4.5	24.21		20.91		21.51	21.91	22.11	24.21	24.18	
						28 50		71.2 20	61.8 15	61.6 7	4.5	4.53 9.40 N.Edge Pav	24.18
101 $\frac{1}{2}S=1.4$	26.30		8.0	20.71	F62 32.3	21.01			20.71	20.71	22.01	24.21	
						71.7 50			81.0 20	81.0 15	81.0	61.7 8	41.5 15
100 + 75			8.1	20.61		20.91			20.61	20.61	21.11	21.31	
						71.8 50			81.1 20	81.5 15	81.1	71.6 15	71.4 20

RT.

6.6  
5.9  
19.0

F32  
28.1

22.11

F22  
30.710

23.41

4.70  
5.0  
19.0

28.71

old.  
B.M. Mon.

7.39

21.325

37' E. + 18.3' N. of Pueblo Cor. Ct. in pav.

= 21.34

original Elev.

= 21.04

6<sup>th</sup> St. Extension Notes

Grade Book 154 P. 4

P.L. 1118

P.L. 1105

56  
P.L. 1118  
P.L. 1118  
1118

B.M. # 7

4.74

23.97

B. P. Sty. End Culvert. W. side 6<sup>th</sup> St. Extension

= 23.70

6<sup>th</sup> St Extension Notes

Camino Del Rio South Fork.

100 + 67<sup>5</sup>  $\phi$  = Production of  $\phi$  Existing Culvert.

See Page 16.

20.71  
8.0

20.83  
7.84

21.02  
7.69

22.11  
6.6

22.11  
6.6

F.L. W. side  
Ex. Culvert

F.L. S.W. side  
Ex. Culvert

continued in FB 1580 P. 29

103

1/2 = 0.0

26.92

3.38

5.17

28.71

F5L  
299

7.0

7.0

6.0

5.3

5.24

5.17

5.14

5.4

5.4

7.0

5.6

4.7

6.8

F44  
28.7

28.71

Lt.

$\phi$

Rt.

X See Camino Del Rio  
 South Fork  
 See Page 13.

+50		4.5	20.09
2		4.5	20.09
+50		4.7	19.89
1	50	5.0	19.59
+50		5.1	19.49
0+00	South Fork = 89766 <sup>29</sup>	5.3	17.29

T.P. Page 52 5.24 24.59

19.35

4.8 50	19.79	4.6 30	19.99	4.0 25	20.59	5.1 20	19.49	3.0 15	21.59	4.6 13	19.99	4.5	20.09	4.2 20	20.39	4.8 30	19.79	5.2 50	19.39						
4.8 50	19.79	4.7 33	19.89	4.2 27	20.39	5.4 23	19.19	4.1 20	20.49	3.2 17	21.39	4.6 15	19.99	4.5	20.09	4.3 15	20.29	4.0 20	20.59	3.5 15	21.09	5.0 30	19.59	5.3 50	18.79
4.9 50	19.69	4.8 33	19.79	4.5 27	20.09	5.5 23	19.09	4.3 20	20.29	3.3 17	21.29	4.8 15	19.79	4.7	19.89	4.5 15	20.09	4.1 20	20.49	5.1 30	19.49	5.4 50	19.19		
5.0 50	19.59	5.0 33	19.59	4.5 27	20.09	5.6 23	18.99	4.3 20	20.29	3.6 18	20.99	5.0 15	19.59	5.0	19.59	4.6 15	19.99	4.5 20	20.09	5.1 30	19.49	5.6 50	18.99		
5.1 50	19.49	5.3 33	19.29	4.5 27	20.09	6.0 23	18.59	4.6 20	19.99	3.6 18	20.99	5.1 15	19.49	5.1	19.49	5.1 15	19.49	5.0 20	19.59	5.9 50	18.69				
5.4 50	19.19	5.4 32	19.19	4.5 27	20.09	6.0 23	18.59	4.8 20	19.79	4.0 17	20.59	5.3 15	19.29	5.3	19.29	5.2 15	19.39	5.1 20	19.49	5.9 50	18.69				

24.59

R.P. Hub 50' Lt Sta 94+57.24 F.C.

6

3.6 20.99

47	19.89
50	50
43	20.29
24	24
33	21.29
22	22
41	19.99
20	20
47	19.89
16	16
26	21.99
15	15
38	20.79
12	12
31	20.99
16	16

+50

3.9 20.69

47	19.89
50	50
43	20.29
24	24
34	21.19
22	22
45	20.09
20	20
30	21.59
15	15
40	20.59
12	12
3	20.69
9	9

+23 Elce Pole 24 RT

+21 Tel Pole 24.5 Lt.

5

4.1 20.49

49	19.69
50	50
46	19.99
26	26
34	21.19
23	23
47	19.89
20	20
47	19.89
17	17
33	21.29
15	15
42	20.39
12	12
41	20.49
9	9

+50

4.3 20.29

49	19.69
50	50
45	20.09
27	27
34	21.19
24	24
48	19.79
22	22
48	19.79
20	20
48	19.79
17	17
32	21.39
15	15
43	20.29
12	12
43	20.29
9	9

4

4.5 20.09

50	19.59
50	50
38	19.59
28	28
38	20.79
24	24
51	19.49
20	20
51	19.49
17	17
31	21.49
15	15
43	20.29
12	12
45	20.09
9	9

+50

4.5 20.09

43	20.29
50	50
41	20.49
24	24
52	19.39
20	20
29	21.69
15	15
45	20.09
12	12
45	20.09
9	9

3

4.4 20.19

48	19.79
50	50
48	19.79
30	30
30	20.99
25	25
51	19.39
20	20
38	21.79
15	15
41	19.99
12	12
44	20.19
9	9

24.59

24.59

58

+50					6.0	20.60	5.5	21.10	4.2	22.40	5.4	21.20	5.4	21.20	4.0	22.60	5.1	21.50	4.6	22.00	4.7	21.90	4.7	21.90	4.3	22.30	5.4	21.20	6.0	24.60	59		
					50	24	22	20	15	13	12	18	12	15	20	21	28	28	20	21	28	28	21	28	28	28	28	28	28	28			
+20	Tel Pole	22.1	Lt.	4.6	22.00																												
+12	Ele Pole	20.5	Rt.			6.0	20.60	5.9	20.70	4.3	22.30	5.9	20.70	5.7	20.90	4.2	22.40	5.2	21.40	4.8	21.80	5.0	21.60	4.9	21.70	4.0	22.60	5.6	21.00	4.1	20.50		
				4.8	21.80	50	24	22	20	15	18	12	15	20	21	28	28	20	21	28	28	21	28	28	21	28	28	28	28	28	28		
+50				5.0	21.60	6.2	20.40	5.7	20.90	4.3	22.30	6.1	20.50	5.1	20.50	4.0	22.60	5.3	21.30	5.0	21.60	4.9	21.70	4.4	22.20	6.2	20.40	6.4	20.20				
						50	24	22	20	11	15	13	15	20	21	28	28	20	21	28	28	21	28	28	21	28	28	28	28	28	28		
7				5.3	21.30	6.3	20.30	6.0	20.60	4.1	22.50	6.0	20.60	5.9	20.70	5.0	21.60	5.5	21.10	5.3	21.30	5.2	21.40	5.2	21.40	4.5	22.10	6.2	20.40	5.5	20.10		
						50	24	22	20	16	15	12	16	15	12	15	12	12	12	13	15	15	15	20	20	21	28	28	28	28	28	28	
+50				5.5	21.10	6.5	20.10	6.2	20.40	5.1	21.50	6.4	20.20	6.4	20.20	4.5	22.10	5.7	20.90	5.5	21.10	5.4	21.20	5.5	21.10	4.5	22.10	6.1	20.50	6.4	20.20		
						50	22	23	20	16	15	12	16	15	12	15	12	12	12	13	15	15	20	20	21	28	28	28	28	28	28	28	28

26.60

T.P. 4.00 26.60 1.99 22.60 Nails Tel Pole 22.5 Lt. Sta. 6 + 20  
24.59

4

2+

2

R+

+85

2.61 23.99

3.1  
50 23.50

3.0  
20 23.60

2.85  
15 23.75

2.61  
50 23.99

2.55  
50 24.07

2.50  
20 24.10

1.9  
50 24.70

+95

2.70 23.90

4.4  
50 22.20

3.0  
20 23.60

3.0  
15 23.60

3.82  
7 22.78

2.70  
20 23.90

2.58  
15 24.02

2.55  
20 24.05

2.58  
20 24.02

4.9  
27 21.70

4.5  
50 22.10

+86

2.63 23.95

4.7  
50 21.90

6.0  
20 20.60

6.0  
15 20.60

4.8  
11 21.80

2.90  
10 N. PV 23.80

2.65  
20 PV 23.95

2.60  
15 PV 24.00

2.60  
20 24.00

2.60  
20 S. PV 24.00

0.6  
30 24.00

5.0  
50 26.00

+81 Elec Pole 23.5 Rt.

4.7  
50 21.90

4.5  
20 22.10

4.5  
15 22.10

4.0  
10 22.60

2.80  
10 N. PV 23.80

2.8  
20 PV 23.80

2.7  
15 23.90

2.7  
20 23.90

3.5  
28 23.10

4.0  
50 22.60

+81

2.8 23.80

4.8  
50 21.80

4.5  
20 22.10

4.3  
15 22.30

3.0  
13 23.60

3.9  
11 22.70

3.6  
15 23.00

3.6  
15 23.00

3.8  
20 22.80

3.2  
22 22.40

4.3  
30 22.90

4.8  
50 21.80

+50

3.6 23.00

5.5  
50 21.10

5.1  
25 21.50

3.5  
22 23.10

5.4  
20 21.20

5.4  
15 21.20

3.5  
12 23.10

4.8  
11 21.80

4.5  
11 22.10

4.5  
15 22.10

4.6  
20 22.00

4.1  
21 22.50

4.7  
28 21.90

5.0  
50 21.60

26.60

10

9

26.60

BM #9

2.62

23.98 =  
= 23.97

10 + 1/2" = W. Edge 6' Ex. 20' Pav. Strip 2.60 24.00

26.60

$$\begin{array}{r} 23.67 \\ 2.33 \\ \hline 25.00 \end{array}$$

$$\begin{array}{r} 23.92 \\ 2.08 \\ \hline 26.00 \end{array}$$

$$\begin{array}{r} 23.97 \\ 2.15 \\ \hline 26.12 \end{array}$$

$$\begin{array}{r} 24.00 \\ 2.00 \\ \hline 26.00 \end{array}$$

$$\begin{array}{r} 24.17 \\ 2.15 \\ \hline 26.32 \end{array}$$

$$\begin{array}{r} 24.20 \\ 2.00 \\ \hline 26.20 \end{array}$$

$$\begin{array}{r} 24.34 \\ 2.04 \\ \hline 26.38 \end{array}$$

$$\begin{array}{r} 24.50 \\ 2.00 \\ \hline 26.50 \end{array}$$

2-6-36

Camino Del Rio  
Culvert Profiles

Station 4+15 Culvert #7  
at Rt. L. to  $\phi$ .

Move to Sta 4+40 @ Request of EAS  
For New Profile Perchs for Culverts See

F.B. 1552-P. 1.

Abandoned  
2-7-38

100' Lt. of $\phi$	15.0	3.8	
56' Lt. of $\phi$	15.5	3.3	
39' Lt. of $\phi$	5.5	13.3	
9' Lt. of $\phi$	5.7	13.1	
8' Lt. of $\phi$	5.0	13.8	
$\phi$	4.3	14.5	
6' Rt. of $\phi$	4.3	14.5	
T.P. 4.0	<u>18.75</u>	21.0	14.75
11' Rt. of $\phi$	17.5	18.2	
50' Rt. of $\phi$	7.7	28.0	
B.M. $\phi$ Hub 4+35	21.0	<u>35.75</u>	14.75

Sta 12+65 ✓ Culvert - 3

X at Rt. L. to  $\phi$ . X  
 $\Delta$  changed.

62

18' Lt	6.3	9.2	
15' Lt	9.6	5.9	
9' Lt	9.4	6.1	
2' Lt	4.5	11.0	
$\phi$	4.5	11.0	
28' Rt	4.3	11.2	
36' Rt. of $\phi$	7.8	7.7	
85' Rt. of Sta. 13+20.	12.8	2.7	Low Point to be Drained
75' Rt. of $\phi$ 12+65	11.6	3.9	in Wash
B.M. T.P. Page 25	2.77	15.52	12.75
Sta 8+50 ✓			
at Rt. L. to $\phi$ . X			
200 Lt	11.7	4.7	
100 Lt	10.4	6.0	
50' Lt	9.0	7.4	
20' Lt. of $\phi$	6.2	10.2	
$\phi$	4.3	12.1	
20' Rt. of $\phi$	4.1	12.3	
50' Rt. of $\phi$	3.5	12.9	
B.M. #2	2.11	16.40	14.29

Abandoned  
2-7-38

Abandoned  
2-7-38

Culvert #2



Sta 12+651 Culvert 3

culvert 4

63

20+55 ✓  
 X at Rt. 2s to E. X  
 Δ change

				410		8.0	8.4
				390 Lt		9.4	7.0
				350 Lt		3.4	13.0
				300 Lt		5.1	11.3
				200 Lt		5.6	10.8
550' Lt		7.6	7.9	100' Lt		5.5	10.9
500' Lt		9.9	5.6	24 Lt		5.9	10.5
450 Lt		11.8	3.7	20 Lt		7.5	8.9
400 Lt		11.0	4.5	15 Lt		7.6	8.8
300 Lt		9.8	5.7	12 Lt of E		4.8	11.6
200' Lt		9.4	6.1	E		4.8	11.6
130' Lt		11.5	4.0	20' Rt of E		4.9	11.5
115' Lt		6.4	9.1	27' Rt		7.1	9.3
100' Lt		5.9	9.6	87' Rt Low Point		8.7	7.7

Abandoned  
 2-7-38

15.52

T.P. Page 27

3.01

16.40

13.39

Sta 54+50 ✓ Culvert #6  
at Rt 4s to ♀

OK. 2-7-38

100' Lt	13.3	9.9
70' Lt	13.2	10.0
52' Lt	9.9	13.3
10' Lt	9.8	13.4
♀	8.5	14.7
24 Rt	7.3	15.9
30' Rt	4.9	18.3
61 Rt	4.5	18.7
63 Rt	3.5	19.7
66 Rt	4.1	19.1
100' Rt	2.2	21.0
120' Rt of ♀	1.9	21.3

BM Nail (Page 40) 3.55 23.17

19.62

Sta 57+21 ✓  
Existing 36" emt. Pipe Culvert.

64

90' Lt	7.4	14.2
80' Lt	11.1	10.5
50' Lt	10.7	10.9
40' Lt	9.9	11.7
26' Lt of ♀	8.5	13.1
♀	8.0	13.6
17' N End. 8x36 Pipe	7.5	14.1 ground
17' " " " " "	8.83	12.76 F.L.
18	4.9	16.7
45' S	4.5	17.1
45.5' S S End. 8x36 Pipe	8.9	12.7 F.L.
45.5' S " " " " "	7.3	14.3 ground Drainage for
50' Rt = { Low Point South } { of Existing Road. }	7.3	14.3 E. & W.
75' Rt. of ♀	6.0	15.6

Page 40

BM Nail

1.97 21.59

19.62

Sta 58+50.1  
on Radial Line

Culvert 7

O.K. 2-7-38

Sta 65+00.1  
at RT L Sta 6

Culvert 8

65

O.K. 2-7-38

135' Lt	8.4	13.2	8.4	100' Lt	6.7	16.0
125' Lt	10.7	10.9	10.7	45' Lt	8.0	14.7
65' Lt	10.3	11.3	10.3	30' Lt	10.2	12.5
50' Lt	8.8	12.8	8.8	26' Lt	8.5	14.2
6	7.4	14.2	7.4	9' Lt	8.4	14.3
14' Rt	7.5	14.1	7.5	4' Lt	4.5	18.2
20' Rt	5.0	16.6	5.0	6	4.9	17.8
50' Rt	4.5	17.1	4.5	27' Rt	4.4	18.3
55' Rt	6.0	15.6	6.0	32' Rt	6.8	15.9
75' Rt	5.9	15.7	5.9	80' Rt	6.5	16.2
100' Rt	4.5	17.1	4.5	100' Rt of 6	4.7	18.0

Page 40

B.M. Nail

1.97

21.59

19.62

Page 44

B.M. Nail Pole

4.07

22.73

18.66

Sta 66+15 ✓ Culvert 9  
at Rt. 2s to  $\phi$

Sec F.B. 1552 - P. 1

100' Lt	7.6	15.1
50' Lt	8.2	14.5
23' Lt	7.3	15.4
17' Lt	8.4	14.3
7' Lt	4.9	17.8
$\phi$ } Ex. Road	4.9	17.8
24' Rt	4.9	17.8
28' Rt	8.2	14.5
40' Rt	9.0	13.7
75' Rt	9.2	13.5
90' Rt	9.1	13.6
95' Rt	7.6	15.1
100' Rt or $\phi$	7.6	15.1

X 22.73 Page 66

Sta 79+25 ✓ Culvert 10  
at Rt. 2s to  $\phi$

66

O.K. 2-7-38

5.5 Lt	5.5	17.5
62' Lt	5.9	17.1
42' Lt	7.0	16.0
21' Lt	6.5	16.5
17' Lt	5.0	18.0
$\phi$ } Ex. Road	4.8	18.2
19' Rt	4.8	18.2
20' Rt	4.2	18.8
25' Rt	5.0	18.0
50' Rt	4.8	18.2
100' Rt	4.4	18.6
BM: Nail Pole	3.68	22.95
		19.27

Station 89+00 ✓ - Culvert # 12

OK 2-7-'38

Station 100+0 ✓  
See Page 13 for location.

✓ #1

67

300' Lt		5.4	18.3
200' Lt	Natural Drainage	6.7	17.4
172' Lt		6.3	17.8
166' Lt		4.9	19.2
100' Lt		5.0	19.1
30' Lt		5.0	19.1
26' Lt		4.1	20.0
24' Lt		5.4	18.3
20' Lt		5.7	18.4
17' Lt		3.1	21.0
15' Lt		5.0	19.1
∅		5.0	19.1
30' Rt		5.0	19.1
100' Rt. of ∅		5.0	19.1
BM. # 6	5.05	24.12	19.07

7+84		4.4	22.6	
7+64		6.6	20.8	
4+70 <sup>4</sup>	N. End. Pump House	5.6	21.8	
4+68 <sup>4</sup>	S. End. Pump House	5.2	22.2	
6+00		5.6	21.8	
T.P.	5.65	27.40	5.02	21.75
5+00		5.2	21.6	
4+00N		6.0	20.8	
3+49N		6.0	20.8	
3+00N		5.4	21.0	
2+00N		6.2	20.6	
1+50N		6.2	20.6	
1+00N		5.3	21.5	
0+27N		4.6	22.2	
0+15N		6.1	20.7	
0+00	ground	5.4	21.4	
0+00				
(21' lt. of 9+86 <sup>4</sup> Camino Del Rio South Branch = N. end outlet Existing Double Box Culvert F.L.				
BM. # 7	2.80	26.77	23.97	

6.42 20.35 2.5x12'

5.24	78.60		23.36	
		8.1	20.5	
15+20	14 River	8.4	16.5	
15+07	S. Bank River	6.4	18.9	
13+50		5.1	20.2	
13+17		3.7	21.6	
12+00		3.3	22.0	
11+60		4.3	21.0	
11+25		4.5	20.8	
11+00		2.4	22.9	
T.P.	3.00	25.25	5.15	22.25
10+06		4.6	22.8	
9+45		6.0	21.4	
9+30		6.0	21.4	
9+06		4.7	22.7	

27.40

Culvert. Profile changed to  
 $\Delta 90^{\circ}-13-30^{\circ}$  E to N. from Sta. 29+66. 22' Culvert  
 #5

Row of Large Eucalyptus Trees

$\Delta 90^{\circ}-13-30^{\circ}$  E to N. at Sta. 29+71.17 500 1552/3

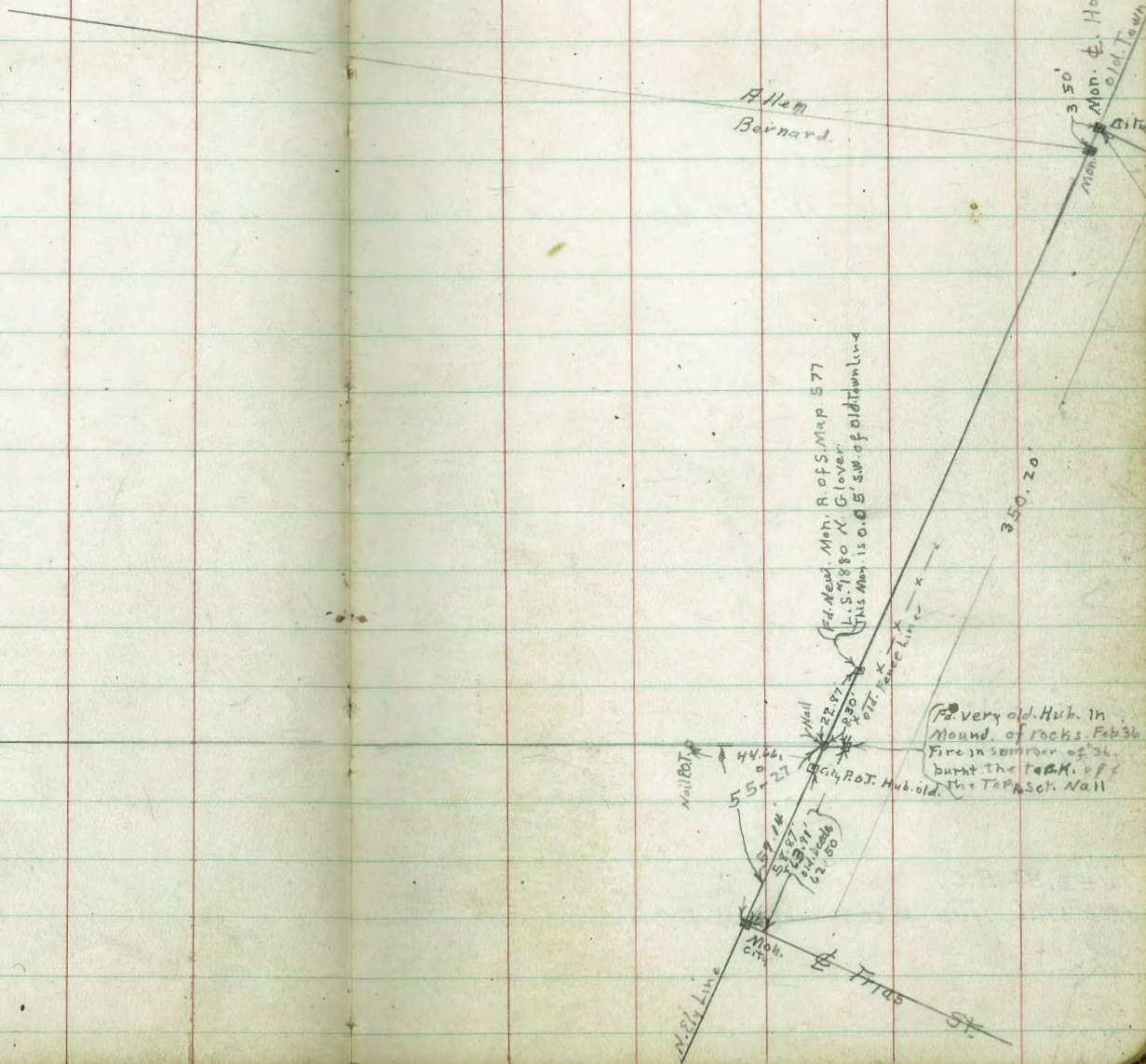
366' Rt of $\Phi$	11.0	10.5	
300' " " "	11.4	10.1	
285' " " "	9.8	11.70	
250' " " "	8.4	12.70	
200' " " "	8.8	12.70	
150' " " "	8.7	12.80	
100' " " "	9.0	12.50	
50' " " "	8.1	13.40	
22' " " "	7.4	14.10	
15' " " "	7.4	14.10	
18' Lt of $\Phi$	4.8	16.70	
$\Phi$	5.0	16.50	
22' Rt. of $\Phi$	4.8	16.70	
39' Rt. of $\Phi$	3.5	18.00	
50' Rt. of $\Phi$	4.6	23.10	
T.P. Page 30 3.98 21.50	17.52		Nail in Elec. # Pole 79014





6-29-37  
Walker  
Bliss

Camino Del Rio Ties "D" Line Page 80.



change in Alignment  
 from Station 14+37 2 B.C. to  
 Station 39+81 22 E.C.  
 See Page 80 for Detail.

6-29-37

Miller  
 Walker  
 Bliss

"D Line"

Camino Del Rio  
 See Page 80

72

18

+42.5 Blue Pole 16' Rt. of  $\phi$

17

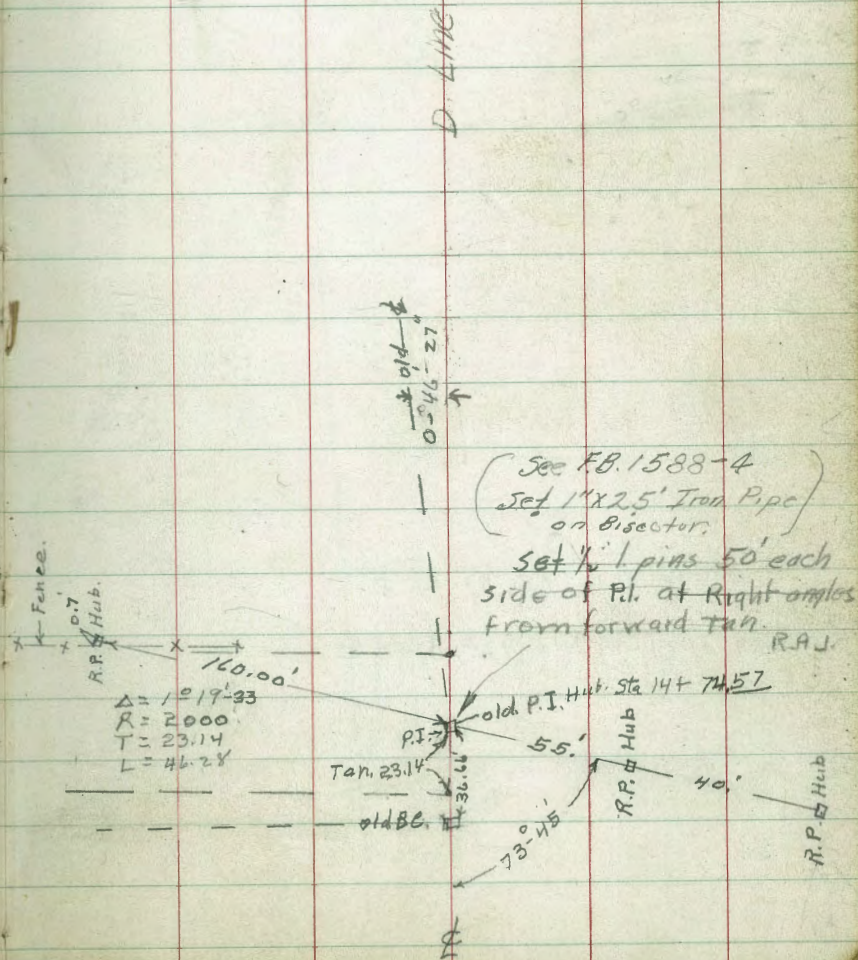
16

15

14+971 E.C.

14+513 B.C.

14+372 Hub. P.O.T. = (old B.C.)



+40 Elec Pole 9.3 RT of  $\phi$ 23+01 <sup>10</sup> Hub. Nly line Old Town

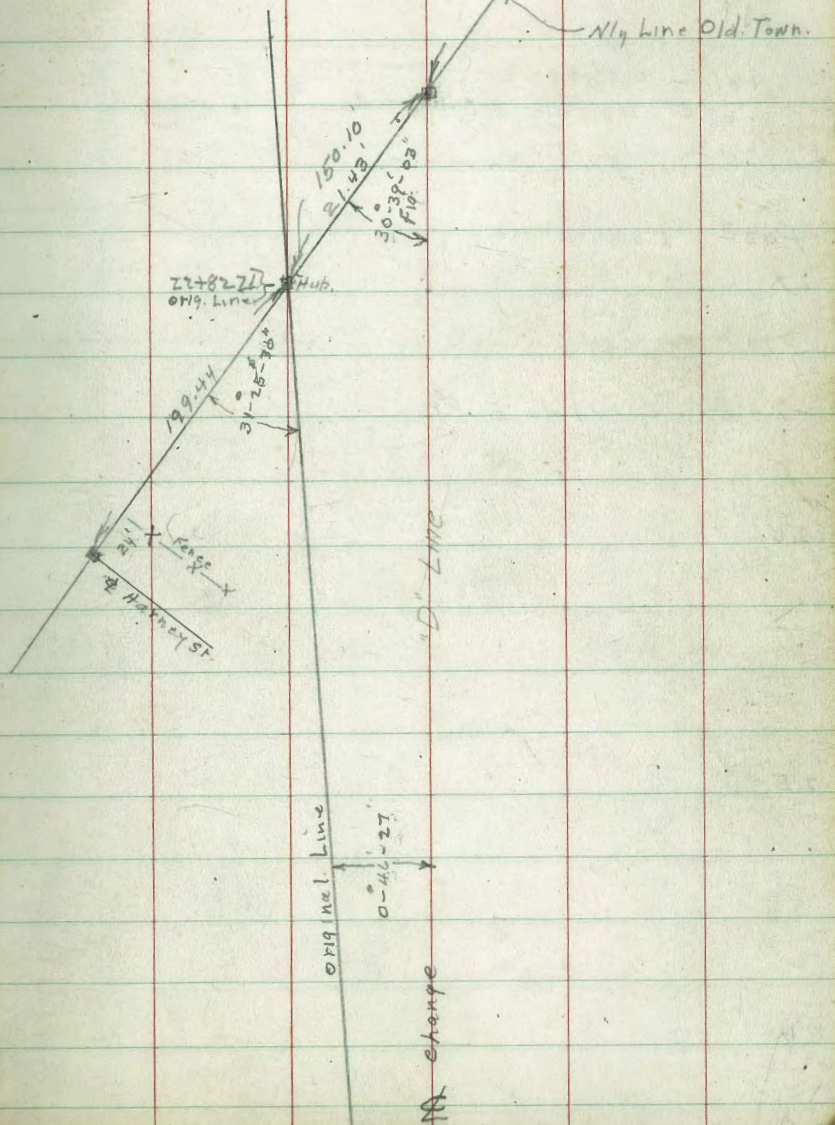
23

22

21

+54 Elec Pole 12i RT. of  $\phi$ +09 Elec Guy Pole 12<sup>1/2</sup> RT. of  $\phi$   
20

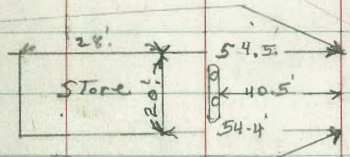
19



+60 39.66 Tel Pole D17152-T  
+40 40.64 Fence  
+13 50.44 Fence

28

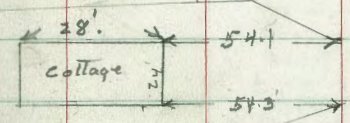
+81.5 e. edge stone  
+65.5 Elec Pole 3.0 RT of C  
+61.5 wedge stone



+03.4 e. edge collage

27

+79.4 wedge collage



+42.3 Elec Pole 5' RT

26

2703.4  
2677.4  
24

2761.5  
2677.4  
83.1

25

24

⊥

- +58 Cypress 18" Diam 10' RT
- +56 Fan Palm 30' Diam 2' Lt
- +55 Fan Palm 30' Diam 3' Lt
- +51 Cypress 12" Diam 10' RT
- +47 Cypress 16" Diam 10' RT
- +39 Acacia Tree 16" Diam 37' Lt

33

- +96 Fan Palm Tree 36" Diam on ☿
- +41 Elec Pole 4' Lt #79015
- +23 45' Lt = Tel Pole #D19199T
- +02 Fan Palm Tree 36" Diam 1' Rt. ☿

32

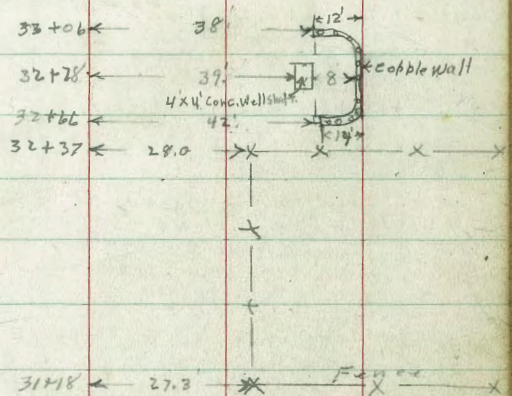
31

- +85 42' Lt. Tel Pole D-19200T

30

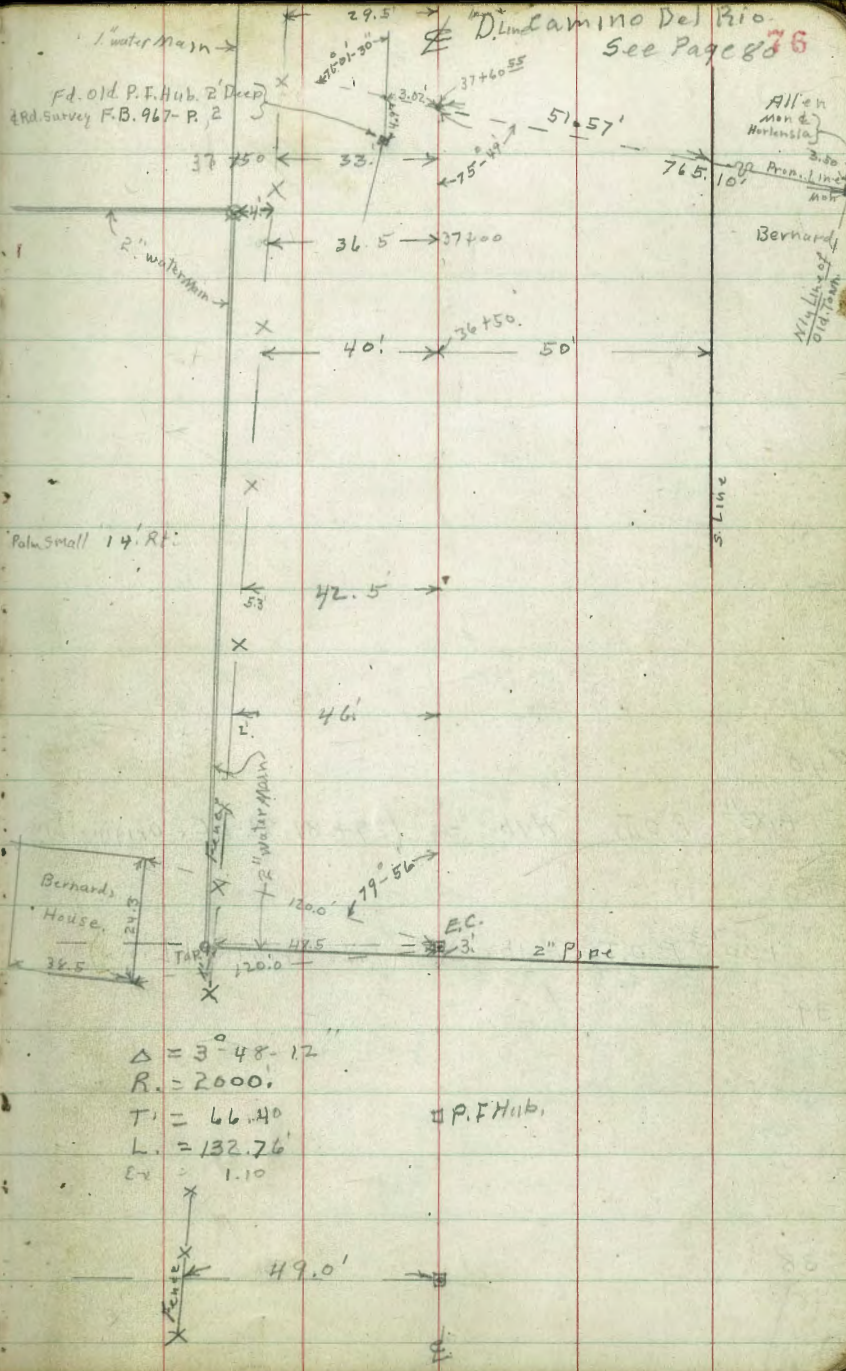
- +96 50' Lt B.W. Fence
- +77 42' Lt B.W. Fence
- +56 40' Lt Tel Pole D-17151-T
- +44 Elec Pole on ☿ #79014

29



31+18 ← 27.3 \* Fog → X

37+60 55 P.I. E + Division Line Bet. Allen & Bernhard



- +57 Tel Pole 28' Lt. # 307420H
- +37 Fan Palm 21' Lt.
- +24 Elec Pole 20' Rt. # 79031
- +04 Fan Palm 30" Diam 22' Lt
- 37+00 Fan Palm 30" Diam 3' Rt
- +72 Fan palm 30' Diam 24' Lt.
- +71 Fan Palm 30' Diam 22' Rt
- +56 stump 20' Diam 25' Lt.
- +44 Date Palm 18' High 19' Rt
- +40 Fan Palm 36" Diam 27' Lt. - Fan Palm 30' Diam 10' Rt
- +26 Tel Pole 36' Lt. # D19196T.
- +24 Stump 30" Diam 27' Lt.
- +20 Date Palm 16' High 15' Rt.
- +16 Date Palm 20' High 14' Rt.
- +13 Date Palm 20' High 14' Rt.
- +07 Fan Palm 36" Diam 28' Lt. - Date Palm 36" Diam 8' Rt. - Date Palm small 14' Rt.

- 36
- +76 Fan Palm 30" Diam 6' Rt - Fan Palm 36" Diam 30' Lt.
  - +72 Date Palm 12' Rt
  - +68 Elec Pole on E # 79030
  - +60 Stump 20' Diam 31' Lt.
  - +50 Date Palm 10' High
  - +49 " " 10' " "
  - +47 " " 10' " "
  - +45 Fan Palm 36" Diam 32' Rt Lt
  - +43 Fan Palm 32" Diam 5' Rt
  - +40 Date Palm 10' High 29' Rt
  - +23 Date Palm 8' High 28' Rt.
  - +07 olive Tree 70" Diam 36' Rt. + Olive Tree 14" Diam 46' Rt.

- 35
- +96 39 E.C. Hub.
  - +76 Tel Pole 45' Lt. # 307419H
  - +69 cypress 18" Diam 12' Rt
  - +60 " 8" " 12' Rt.
  - +55 cypress 20" Diam 12' Rt
  - +54 E. Side Barn 20'8" Rt 24' Long N to S.
  - +50 Fan Palm 15" Diam E
  - +40 W. Side old Barn 20' Rt. 24' Long N to S.
  - +38 cypress 14" Diam 11' Rt
  - +35 " " 11' Rt
  - 34 +18 Fan Palm 36" Diam 32' Lt
  - 34 +14 olive 15" Diam 15' Rt
  - 33 +89 Elec Pole 4' Lt # 9010
  - +87 Fan Palm 30' Diam 38' Lt. - olive Tree 8" Diam 14' Rt.
  - +77 cypress 18" Diam 10' Rt.
  - +71 Tel Pole 46' Lt. D-19198T

33+63 63 BE Lt Hub

$\Delta = 3^{\circ} 48' 12''$   
 $R = 2600.$   
 $T_1 = 66.40$       P.F. Hub.  
 $L = 132.76$   
 $E_v = 1.10$

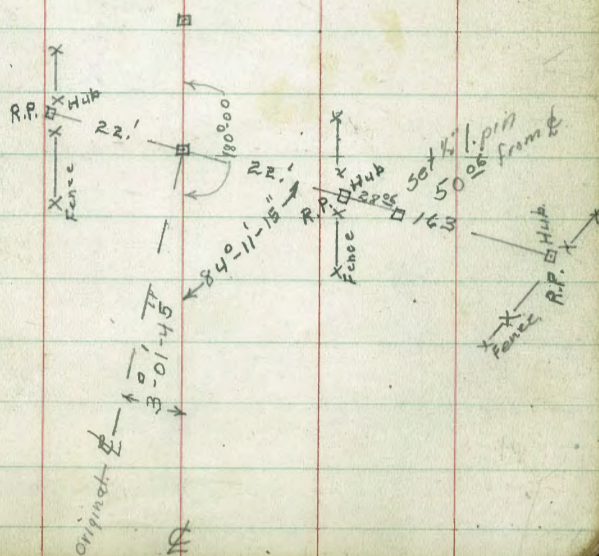
40.

+ 83<sup>11</sup> P.O.T. Hub. = (39 + 81.99 EC. original line)

+ 30<sup>23</sup> P.O.T. Hub. = (P.I. original line)

39

38



B Line Detail of Change 4-3-36

See Page 72.

Stations are Imp Plans  
for Actual Measurements.

See Pages 4 to 7.

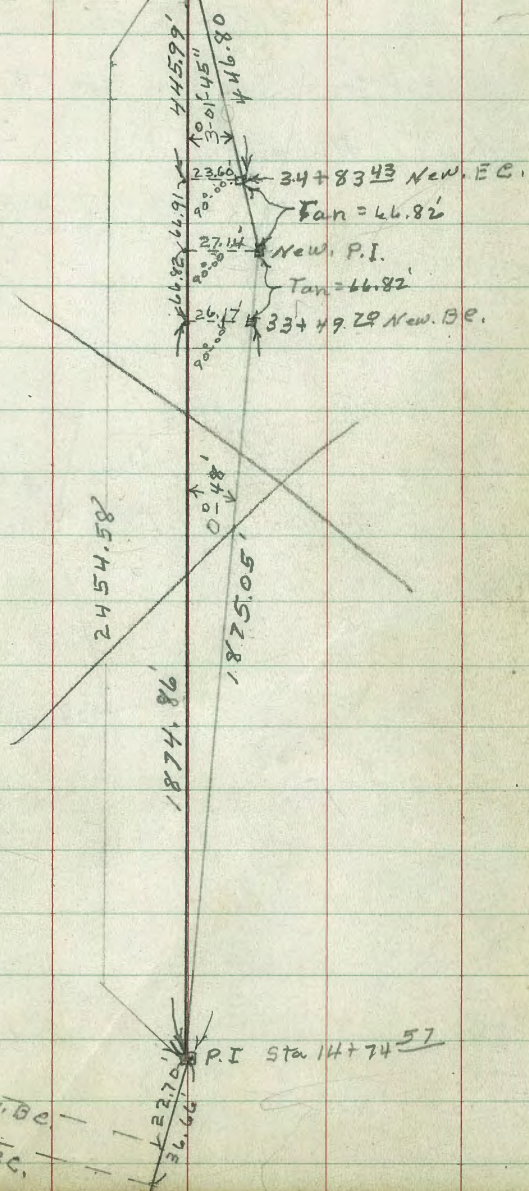
Abandoned 6-6-36.

See Page 80 & 71 to 77  
June 37

Camino Del Rio 78

original line  
39+81.29 E.C. -  
P.O.T. 39+83.11 New Line

P.I. orig line  
= 39+30.23 P.O.T. New Line



14+51.81 New B.C.  
14+37.21 Old B.C.



6-6-36 Change in Alignment "C" Line  
 Miller Camino Del Rio sta 14+37.1 BC  
 Walker TO 50+70.95 New E.C.  
 Blinn.

Indexed Stationing actual Measurements

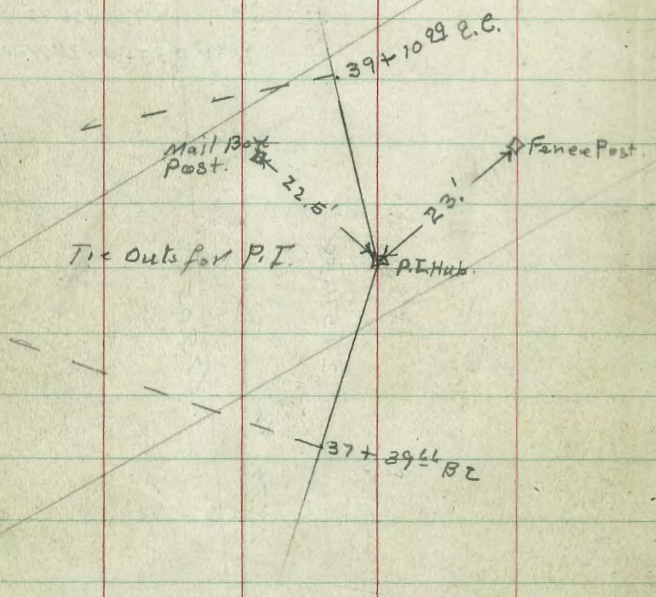
See Page 70.

For Cross Sections see FB. 1531-19

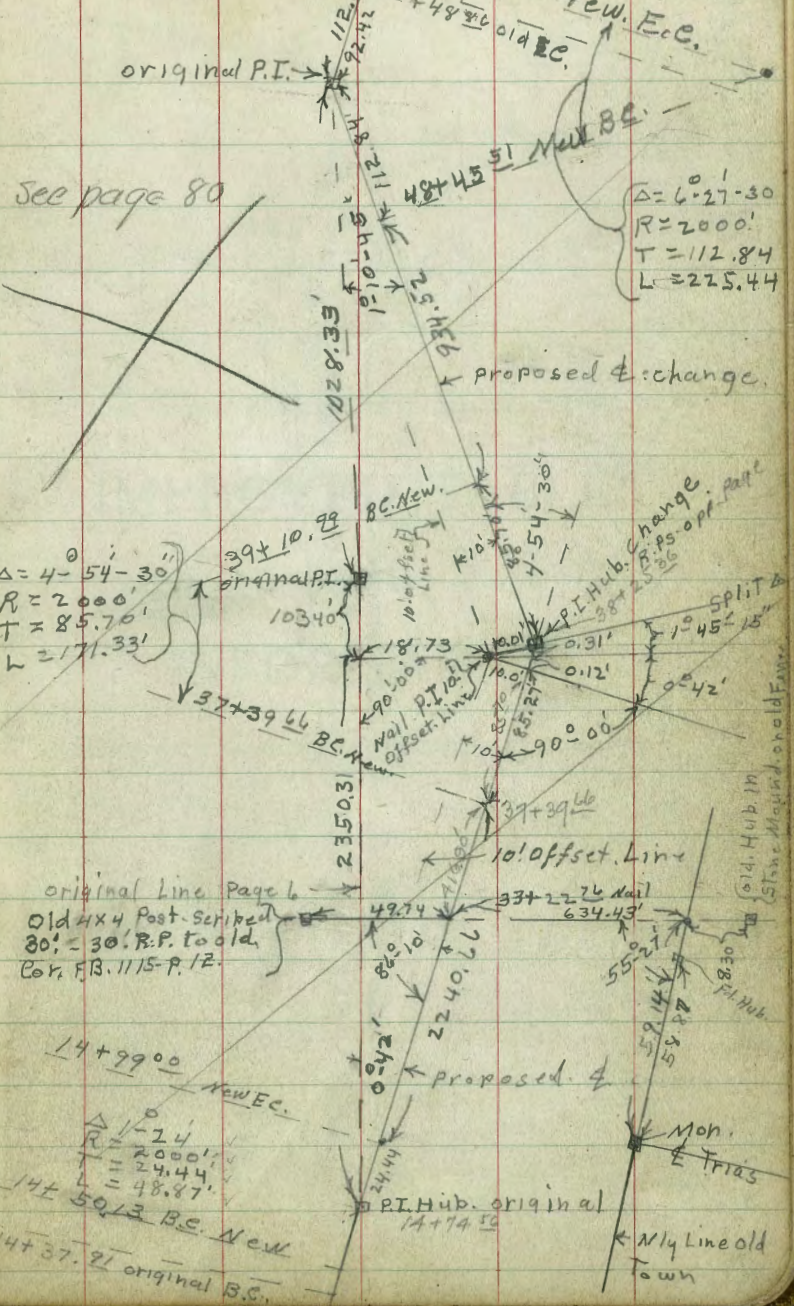
Abandoned 12-14-1936

See Page 80. 471 to 77

June 37.



Equation 50+69.28 old P.O.T. = 50+70.95 New E.C. 79



See page 80

$\Delta = 6^{\circ} 27' 30''$   
 $R = 2000'$   
 $T = 112.84$   
 $L = 225.44$

$\Delta = 4^{\circ} 54' 30''$   
 $R = 2000'$   
 $T = 85.76'$   
 $L = 171.33'$

original Line Page 6  
 Old 4x4 Post scribed  
 $30^{\circ} = 30'$  R.P. to old  
 Cor. FB. 1115-P. 12.

14+99.00 New E.C.  
 $\Delta = 1^{\circ} 24'$   
 $R = 2000'$   
 $T = 24.44'$   
 $L = 48.87'$   
 14+50.13 B.C. New  
 14+37.21 original B.C.

Old Hub in Stone Marking on old Fwy.

6  
7  
W  
B

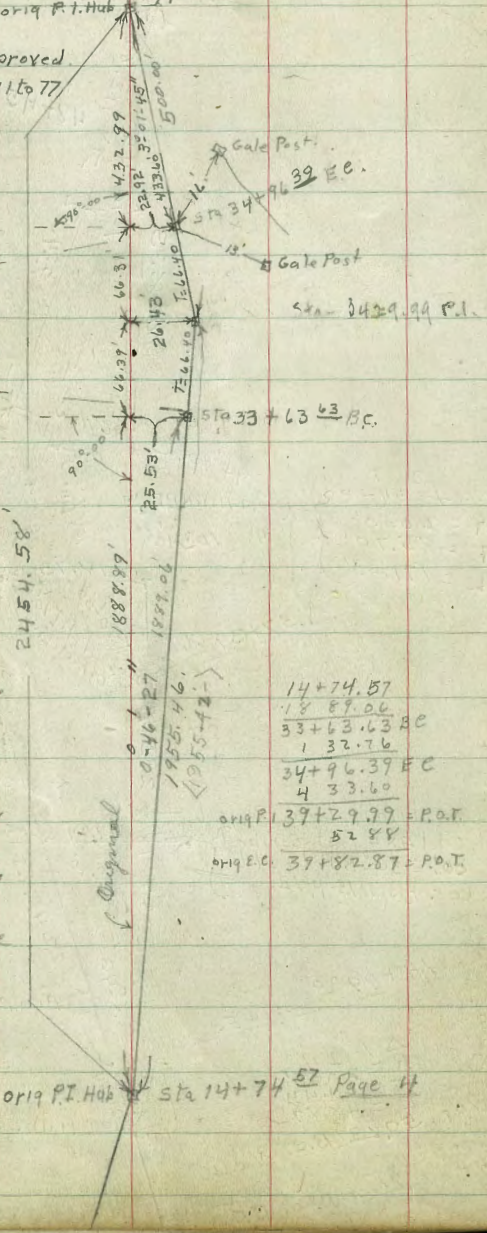
Camino Del Rio  
change 4-9-37  
Miller  
Walker  
Biles  
D Line  
orig P.I. Hub  
39+81.99 E.C.  
39+82.87 P.O.T.  
32+01+45  
39+29.99 P.O.T. Change.

This Alignment Approved  
June 37 See Pages 71 to 77  
for Ties.

$\Delta = 3-48-12''$   
A = 2000.  
T = 66.40  
L = 132.76  
64 = 7.10

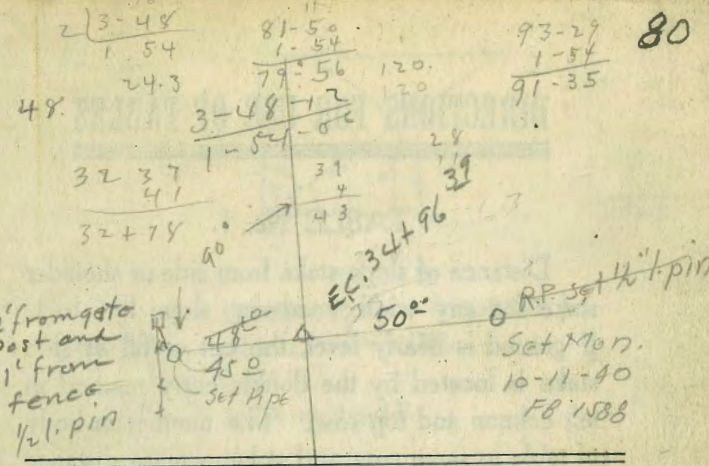
N. Line

38+50	23.3 N of Fence
38+00	20.5 N of Fence
37+50	17.0 N of Fence
37+00	13.5 N of Fence
36+50	10. N of Fence
36+00	7.50 N of Fence
35+50	4.0 N of Fence
35+63.5 EC	10 N of Fence

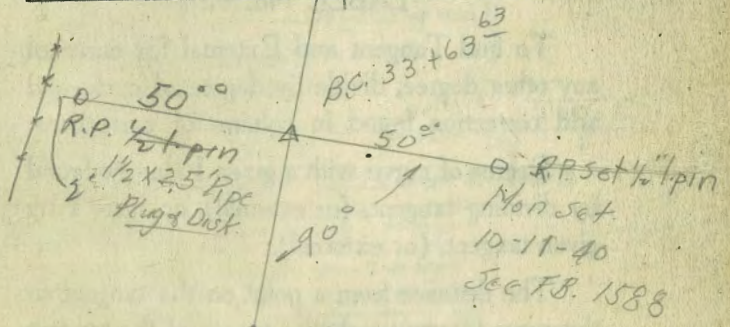


14+74.57  
1889.06  
53+63.63 B.C.  
132.76  
34+96.39 EC  
433.60  
orig P.I. 39+29.99 = P.O.T.  
52.84  
orig E.C. 39+82.87 = P.O.T.

$\Delta = 1-19-33''$  orig P.I. Hub sta 14+74.57 Page 4



## IMPROVED TABLES AND INFORMATION



Mon set  
10-11-40  
See FB. 1588

80

## DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

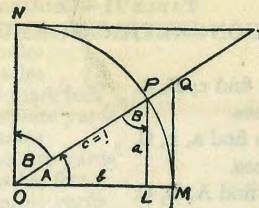
Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

20.5  
1.2  

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21.7



26.3  
21.7  

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4.6

29.7  
2.4  

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27.3

TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP$      $\angle B = \angle PON = \angle OPL$   
 $R = OB = c = 1$

$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$

$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$

$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$

$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$

$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$

$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$

$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$

$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$

$\text{exsec } A = PQ = \text{coexsec } B$   
 $\text{coexsec } A = PT = \text{exsec } B$

$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}}$      $\cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$

$\sin 2A = 2 \sin A \cos A$      $\cos 2A = \cos^2 A - \sin^2 A$

Law of Lines     $\frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$

Law of Cosines     $c^2 = a^2 + b^2 - 2ab \cos C$

Law of Tangents     $\frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$

349639  
993.60  
2999

97+24.04  
94+57.04  

---

2167.00

97+21.48  
94+54.88  

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266.60

266.80  
189  

---

77.80



TABLE X.  
MIDDLE ORDINATES OF RAILS  
Length of Rail (feet)

C o /	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C o	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.  
SHORT RADIUS CURVES

105 88 87  
102 67 62  
38125

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

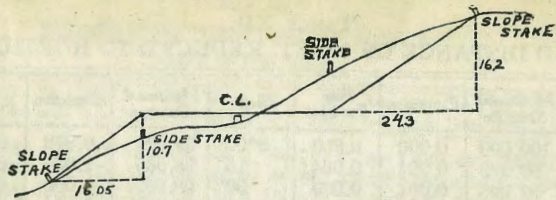
To find length of curve divide angle from P. C. to P. T. by central angle of chord,  
and multiply by length of chord.

TABLE XII.  
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.  
MINUTES IN DECIMALS OF A DEGREE.

0 30''	.00833	10' 30''	.17500	20' 30''	.34167	30' 10''	.50833	40' 30''	.67500	50' 10''	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	80	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	80	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	80	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	80	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	80	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	80	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 05	1 20	1 35	1 50	1 65	1 80	1 95	2 10	2 25	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
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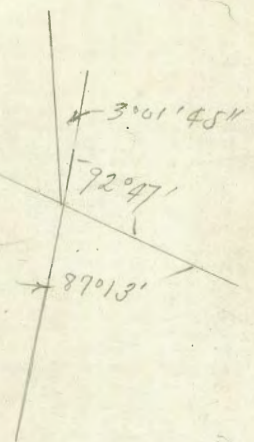
Computed by L. Leland Locke.

19.83  
13.97  
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3.11  
1.4  
1.7

60 017  
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560380  
509886  
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To find

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17.3  
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(11.14)

3.7 866. 4-5

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179-60  
106-15

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64  
350

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73-39  
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7339  
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8239.

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22.5  
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50.0

4+35 P.O.T.  
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2.87

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2.4  
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27.55  
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67  
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73-39  
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5.43-55

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18001-3  
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144  
172.8  
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9.12  
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12  
13.2

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21.2  
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(85  
1742)