

1530

1530

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ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

Our Leather Bound Engineers Note Books are carried in the following rulings:

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- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

INDEXED

to page # 74
except pages 27 & 28

Handwritten notes and calculations at the top of the right page, including numbers like 14/4, 3 1/2, 7 1/2, 12 1/2, 60, 160, 170, 60, 10000, 7 1/2, 2 1/2, 46.

Camino Del Rio
Continued from Book 1528

INDEXED
C.S.K.

INDEXED

107

for Ties + Monuments
on Mission Valley Road
= CAMINO DEL RIO

+50

See F.B. 1588

106

+88⁸⁷

P.O.T. C.T. & Ex. Pav.

62+92.74 B.C.L.T. Pavmt
Book G 154 - P 4.

LS = 89-58-30

LR = 121.56

LT = 121.51

LL = 190.89

+50

INDEXED

105

+50

104

+50

103

+50

→ Don't use this station ←

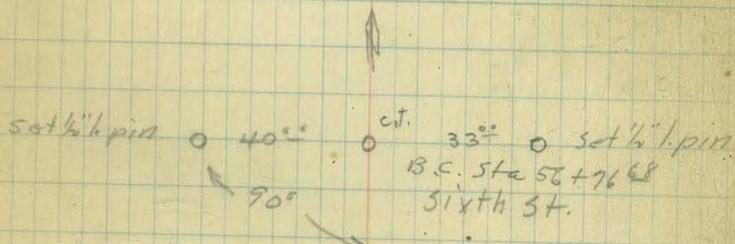
102+05⁰⁶ E.C. = Improvement: Plats

102+07⁶³ E.C. = C.T. & Ex Pav. at: } 59+11.38 E.C. Pavmt
Book G 154 - P 4

o.k.

1

♀ = Pueblo Line



113

+50

112

+50

111

+50

110

+50

109

+50

108

+50

z Pueblo Line

z

124

+50

123

+50

122

+50

121

+50

120

+50

119

+50

+45

118

See Page 26

original. $\$$ = Final $\$$

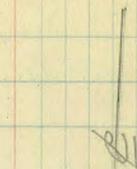
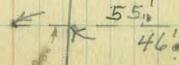
Abandoned
Line
Pueblo

North

55'
46'

According to Property
owner this is an artesian
Well - 14" casing
Casing covered with water

pond



~~See Page 26 for Change~~

+50

+25⁰⁷ E.C.

Def. Ls
Hub. 7-17.75

(+24³⁵ Plans)

Set 1/2" l. pin. 50° 50° set 1/2" l. pin

129

6-35

+50

5-09

$\Delta = 14^{\circ} 35' 30''$ Lt.
 $R = 1000'$
 $T = 128.03'$
 $L = 254.67'$

128

3-43

+50

2-17

127

0-51

+70⁴⁰ B.C.Lt. Hub.

(+69⁴⁵ Plans)

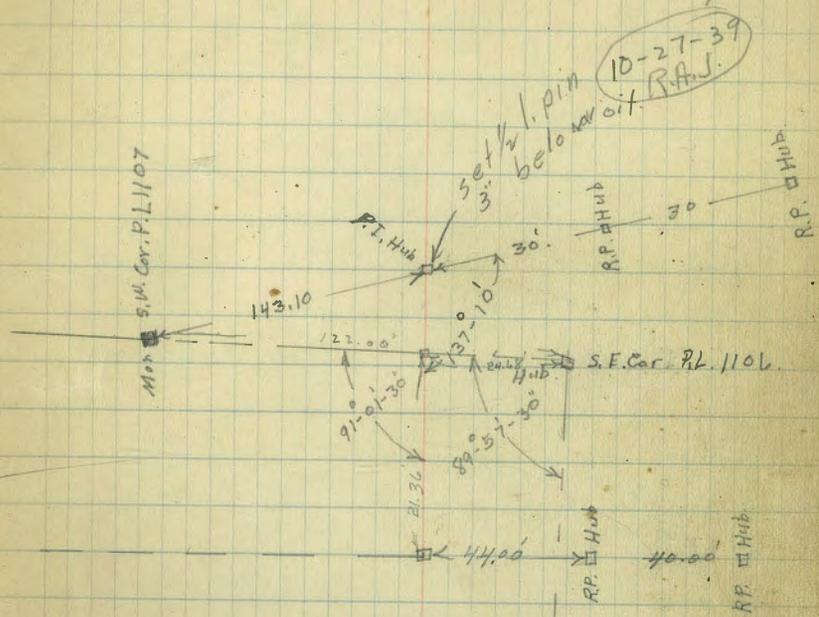
+50

126

+50

125

+50



See Page 26

Orig. & Final &

Abandoned Picta Line

Pueblo Lot. Ties:

~~Abandoned. See Page 26~~

Original Δ = Final Δ

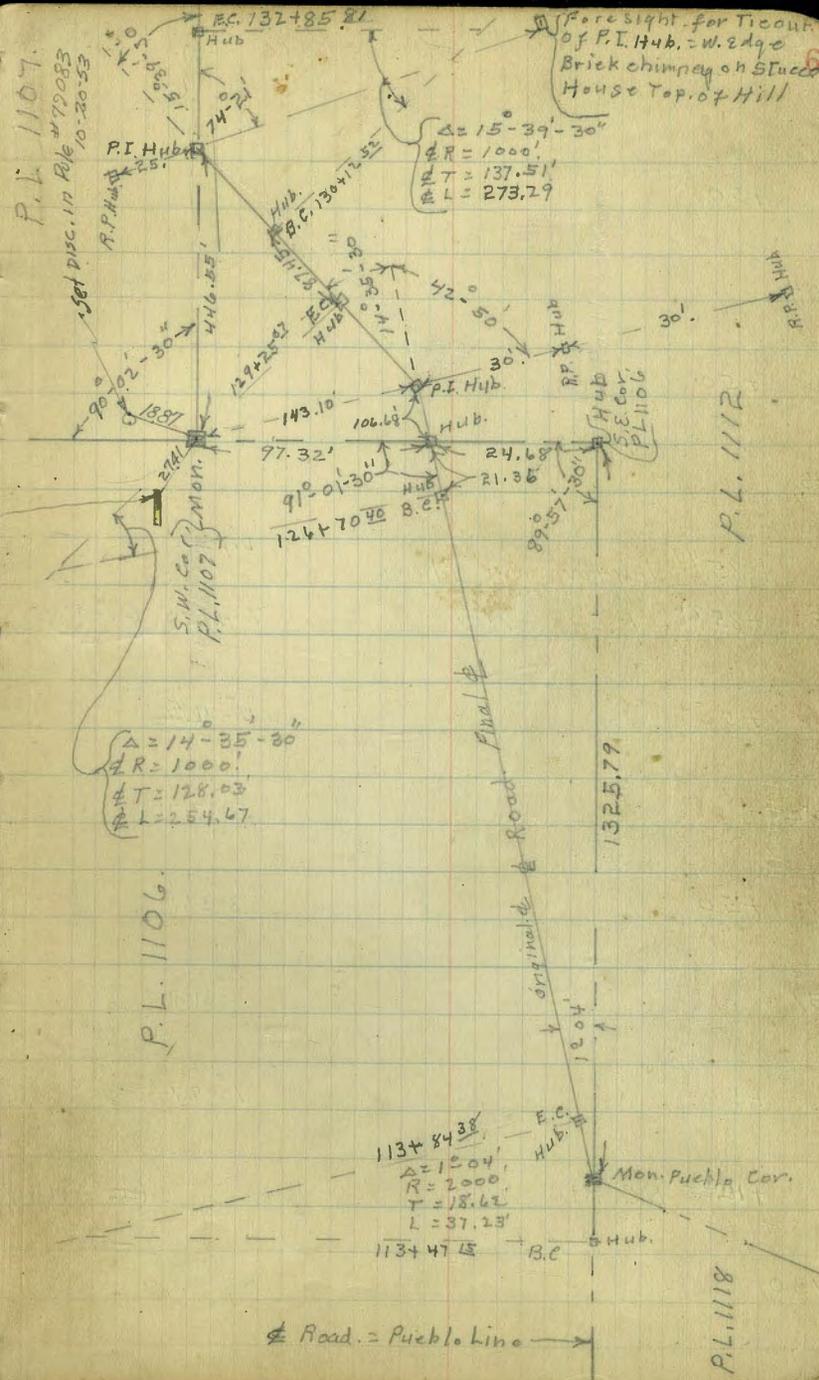
97.32
 24.44
 122.00
 72.00
 $14-35-30$
 $1-04$
 $15-39-30$

130.125
 137.5
 3150.0

000043
 056000

Mon. N.W. Cor. P.L. 1107.

Set chisled
 Cross in Conc. Hl.
 Wall
 10-20-53
 C.B. Walker



P.L. 1107.

P.L. 1106.

P.L. 1112

Page 79

Δ Road = Pueblo Line

Abandoned. See Page 26.

+50

134

+50

133

Def. L₀.

+85⁵¹ E.C. Hub

7-49.75 (+85⁴³ Plang)

+50

6-48.4

132

+50

5-22.4

131

+50

2-30.4

+12⁵² B.C. Rt. Hub.

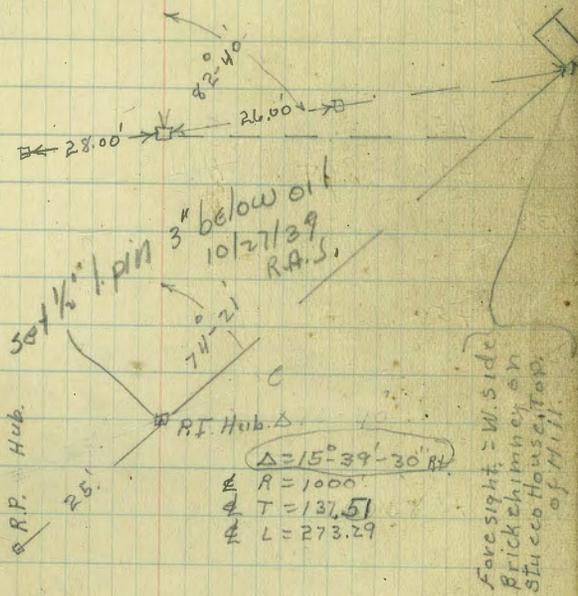
(+12⁰⁶ Plang)

130

32.0
287
33

7

Pueblo Line = ϕ



Hub Δ 50⁰⁰ \square 50⁰⁰ \square set 1/2" pin

ϕ

141

+50

140

+50

139

+50

+20 P.O.T Hub

138

+50

137

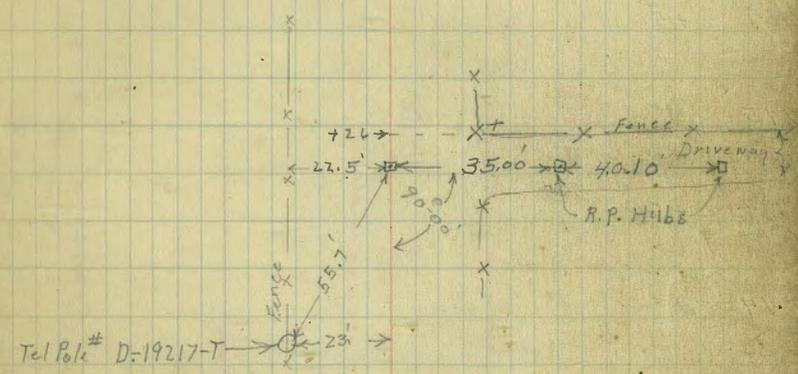
+50

136

+50

135

Pueblo Line = ~~4~~



~~4~~

+50

147

+50

+06²⁵ P.O.T. Hub

146

+50

145

+50

144

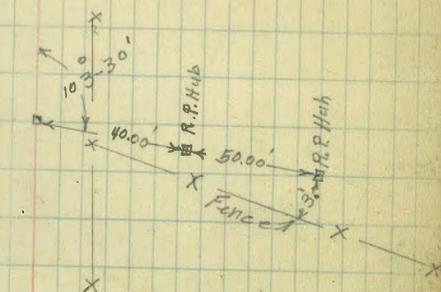
+50

143

+50

142

+50



Pueblo Line =

±

+45⁵⁰ P.O.T. Hub. over Mon S.E. Cor P.L. 1107

153

+50

152

+50

151

+50

150

+50

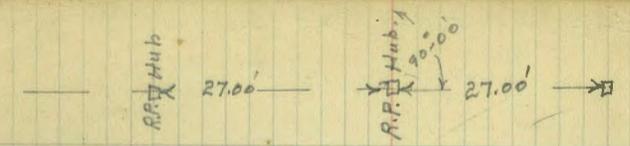
149

+50

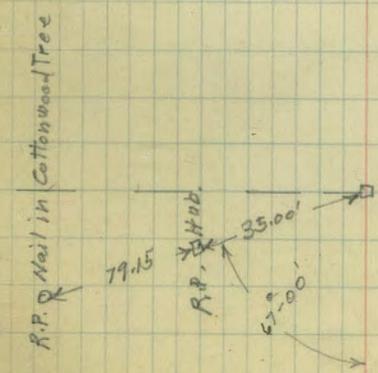
148

Pueblo Lot. Line = £

	Def. C.	
+18 ⁵⁹ E.C. Hub	12-36-35"	(+18 ¹⁹ plan)
159	12-04	
+50	10-38'	
138	9-13	
+50	7-47'	
157	6-21	
+50	4-55'	
156	3-29	
+50	2-03	
155 + 00 (21.57)	0-37'	
+78 ⁴³ B.C. Lt. Hub		(+78 ⁰³ plan)
+50		
154		



$\angle = 25^{\circ}13' - 10''$
 $\phi R = 1000$
 $\phi T = 223.70$
 $\phi L = 440.16'$
 □ P.T. Hub



153 + 45⁵⁰
 Hub over
 P.O.T. MoVi S.E. P.L. 1107
 continued from page 10

+68⁸⁵ E.C. Hub. 12³⁵ 35' (^{D.P.L.}+68⁸⁷ plan)

+50 12⁰⁰ 03'

165 10⁰⁰ 37'

+50 9⁰⁰ 11'

164 7⁰⁰ 45'

+50 6⁰⁰ 10'

163 4⁰⁰ 54'

+50 3⁰⁰ 28'

162 2⁰⁰ 02'

+50 0⁰⁰ 36'

+29¹² B.C. Rt Hub. (+28⁶⁴ plan)

161
+50

160
+50

35.00' 75.00'

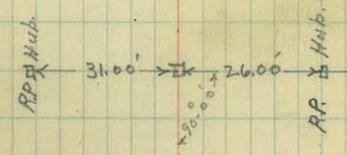
Parab. Line

R.P. Hub.

R.P. Hub. 13
Radial Line

P.I. Hub.

$\Delta = 25^{\circ} 11' 40''$
 $\phi R = 1000'$
 $\phi T = 223.48'$
 $\phi L = 439.73'$



172 P.O.T. Hub.

+50

171

+50

170

+50

169

+50

168

+50

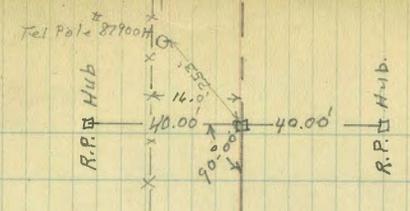
167

+50

166

+97⁵³ Fd Moh. N.E. Cor Lot "A" Licensed Survey # 167

0.10 Lth of ϕ .



P.L. 1110.

Line

Backlo

P.L. 1111

Lot 4

Lot A.

178

+50

177

+50

176

+50

175

+50

174

+50

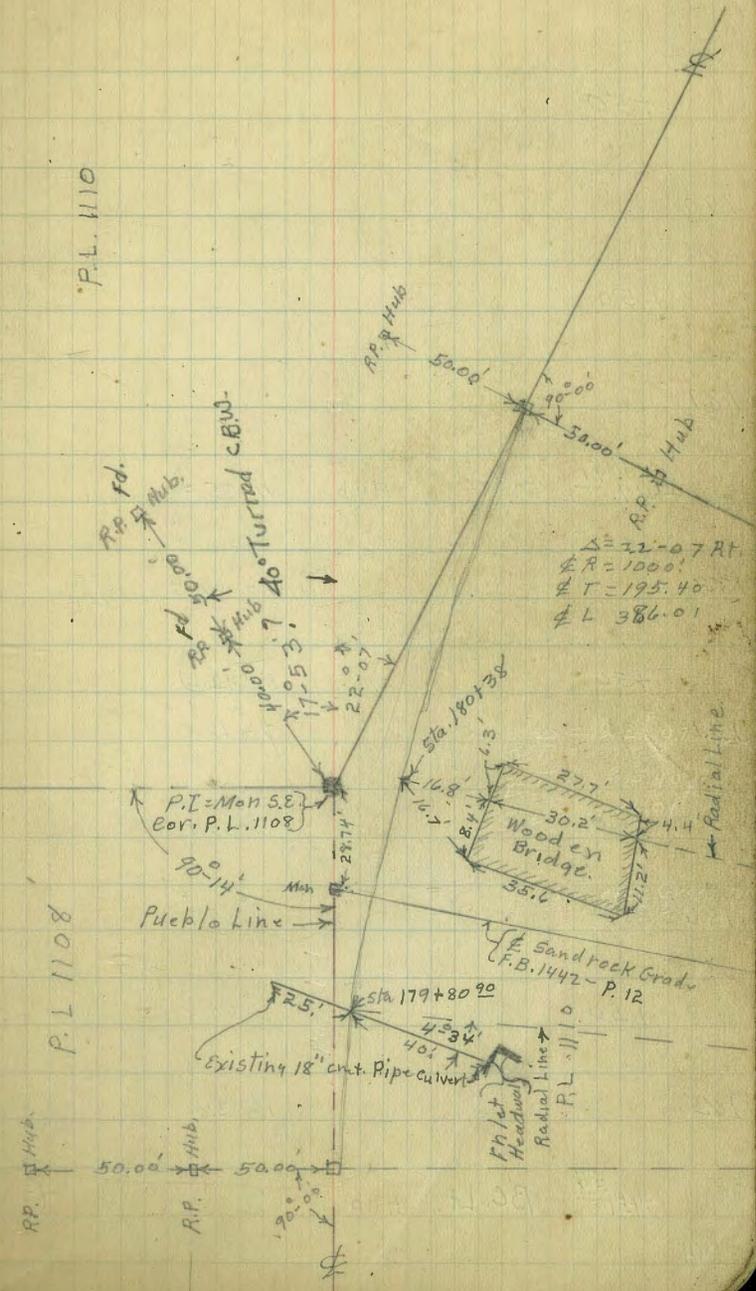
173

+50

Pueblo Line

184		213.33'	
	+50		
183			
	+32 ⁰⁵	E.C. Hub.	Def Ls., 11-03.5 (= +31 ²⁴ plan)
182			
	+50		10-04.5
	+50		8-42.5
181			
	+75		7-16.5
	+50		6-33.5
	+38		5-50.5
	+25		5-30.1
			5-07.5
180			
	+80.9		4-24.5
	+75		3-51.7
			3-41.6
	+50		2-58.6
179			
			1-32.7
	+46 ⁰⁴	B.C. Rt Hub	= +45 ²³ plan

1 to 4 1/4" Plug in 4" Pipe
NE Cor. P.L. 1108.



184+45.38
 182+32.05

 2-13.33

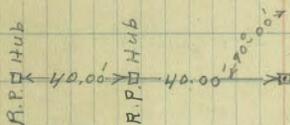
+50

190

+50

189

+49⁹¹ E.C. Hub 11°-35.3' (= +49¹⁰ plan)



188

10°-09.5'

+50

8°-43.6'

187

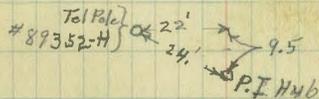
7°-17.6'

Δ = 23°-10'-40" Lt.

QR = 10000

QT = 205.07'

QL = 404.53'



+50

5°-51.7'

186

4°-25.7'

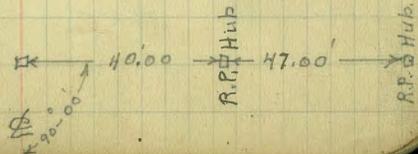
+50

2°-59.8'

185

1°-33.8'

+45³⁸ B.C. Lt. Hub. (= 44⁵⁷ plan)



184

197

+50

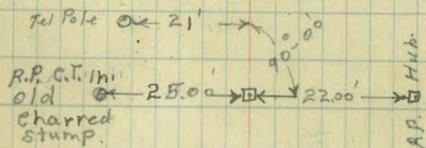
196

+50

195

+85 Tel Pole * 89355 - H 21' LH

+50 P.O.T. Hub



194

+50

193

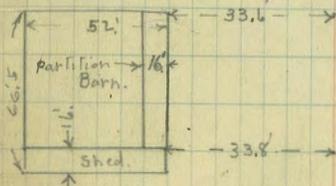
+50

+41.50 E. Side Barn

192

+91. w. side Barn

+50



191

203
 +55.24 P.I. Lot Line Bet. Lots 7 + 8.
 33.92
 +21.32 E.C. Hub Ref Ls. 1
 3-09.25 (E 203420 4 Pln)

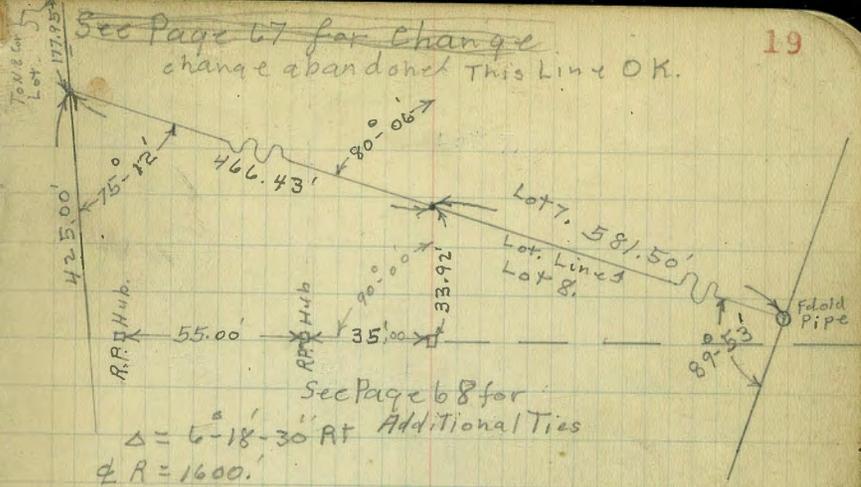
202
 +50
 2-46.3
 1-52.6

201
 +50
 0-58.9
 745.16 B.E. Pt. Hub (-244 42 Pln)

200
 +50

199
 +50

198
 +50



See T.P. Book # 9 P 34-36
 " Page 68 for Ties.

Camino Del Rio
old City Line East. 3/10/36

See Page 69. for New Alignment at Boundary.

Additional Ties Monuments set etc.
See F.B. 1588
County Survey from Station at 205+35.44
See County Book 727

+59⁹⁸ Hub. ϕ on City Boundary Line (Plan: 204+58⁶⁷)
+53⁷⁹ Hub. on City Boundary 20' Lt of ϕ
+50

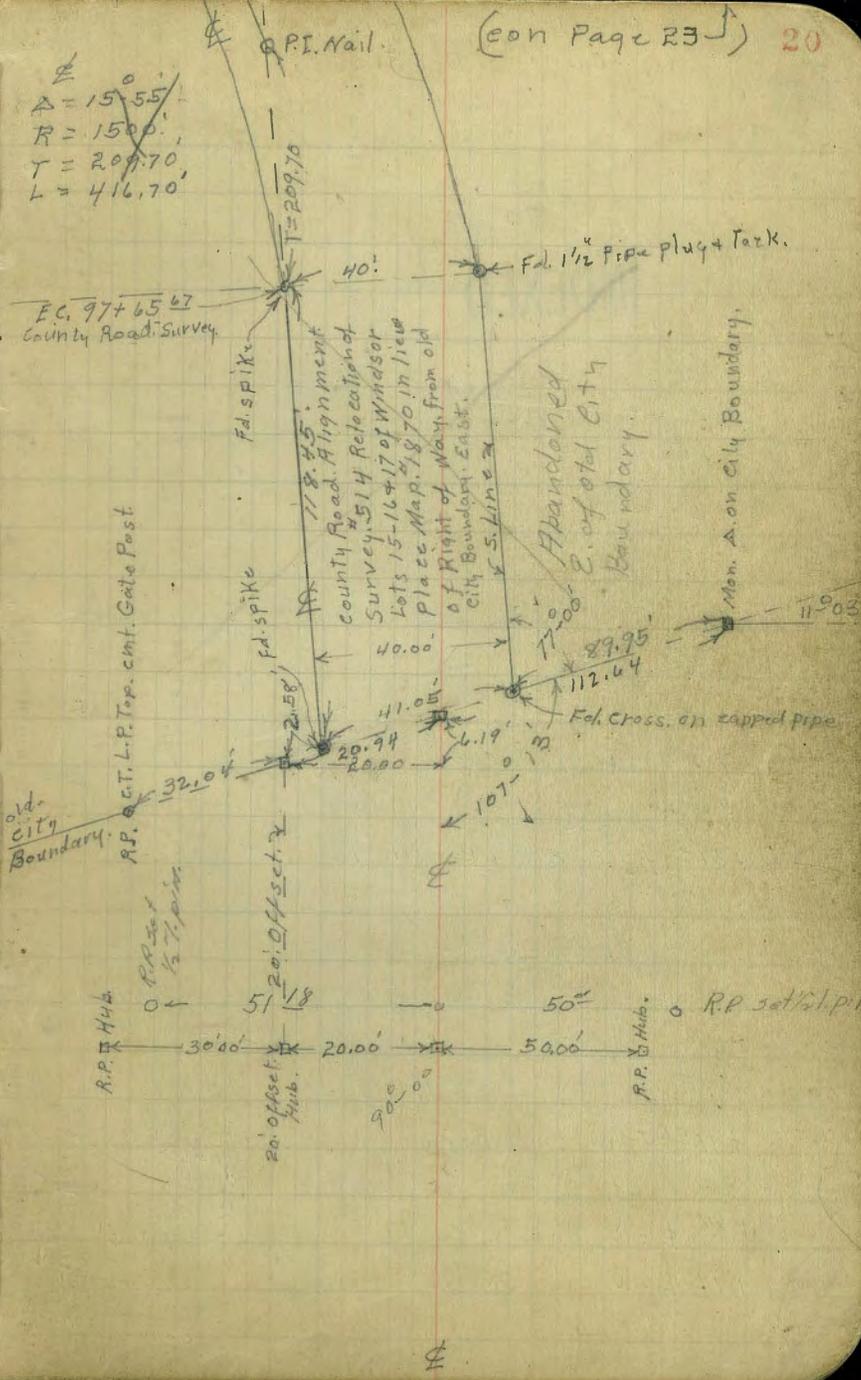
206

+50
+35⁵¹ R.C.Rt. Curve to Join County Station 72+99.22 see P. 73.
+08⁴⁸ P.O.T. Hub.

205

+50

204



(con Page 23) 20

205+74. 9' Lt of d ($d = S.T.$) = { N.W. cor shed. see Page 21
E. End. Fence

+51 18' Lt of d ($d = S.T.$) = Elec Pole 79707

+50 13' " " " ($d = S.T.$) = Fence S. side Ex. Road

+48.5
+35.5 BC. Lt. curve to Meet County $\#$ see Page 73.
+34.2

+22.2

205

+95 10' $\#$ = Cross fence 10.5 s. of Gate Post

+76 10' $\#$ Cross. Fence 10. s. of Gate Post

+56.2

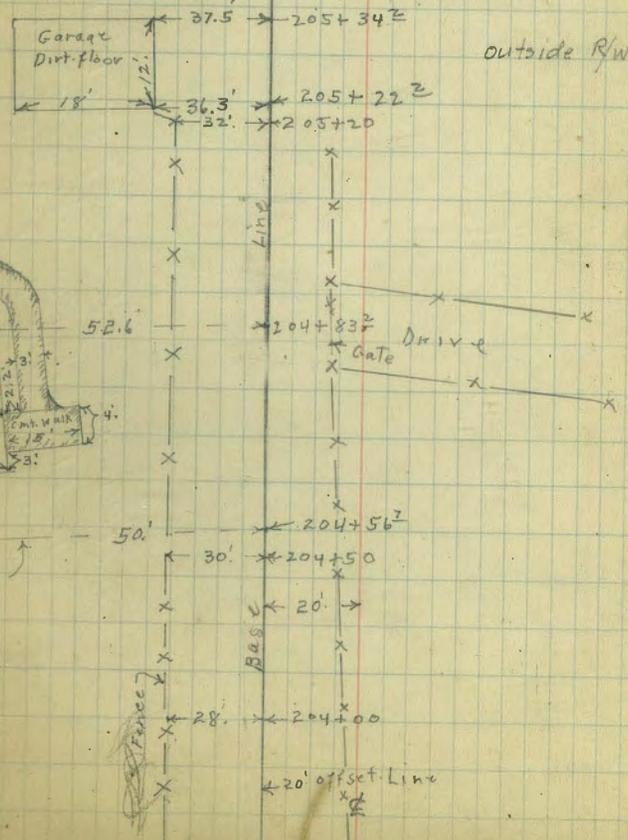
+34 48.7 Lt = Tel Pole D-192 59-T

204

See Page 21 →

From sta 205+35.5 B.C. Lt
East Base Line is a Line parallel to a
420' N. of semi Tangent

← 36.6 → sta 205+48.5 = W. End. Cmt wall



Camino Del Rio 3/10/36

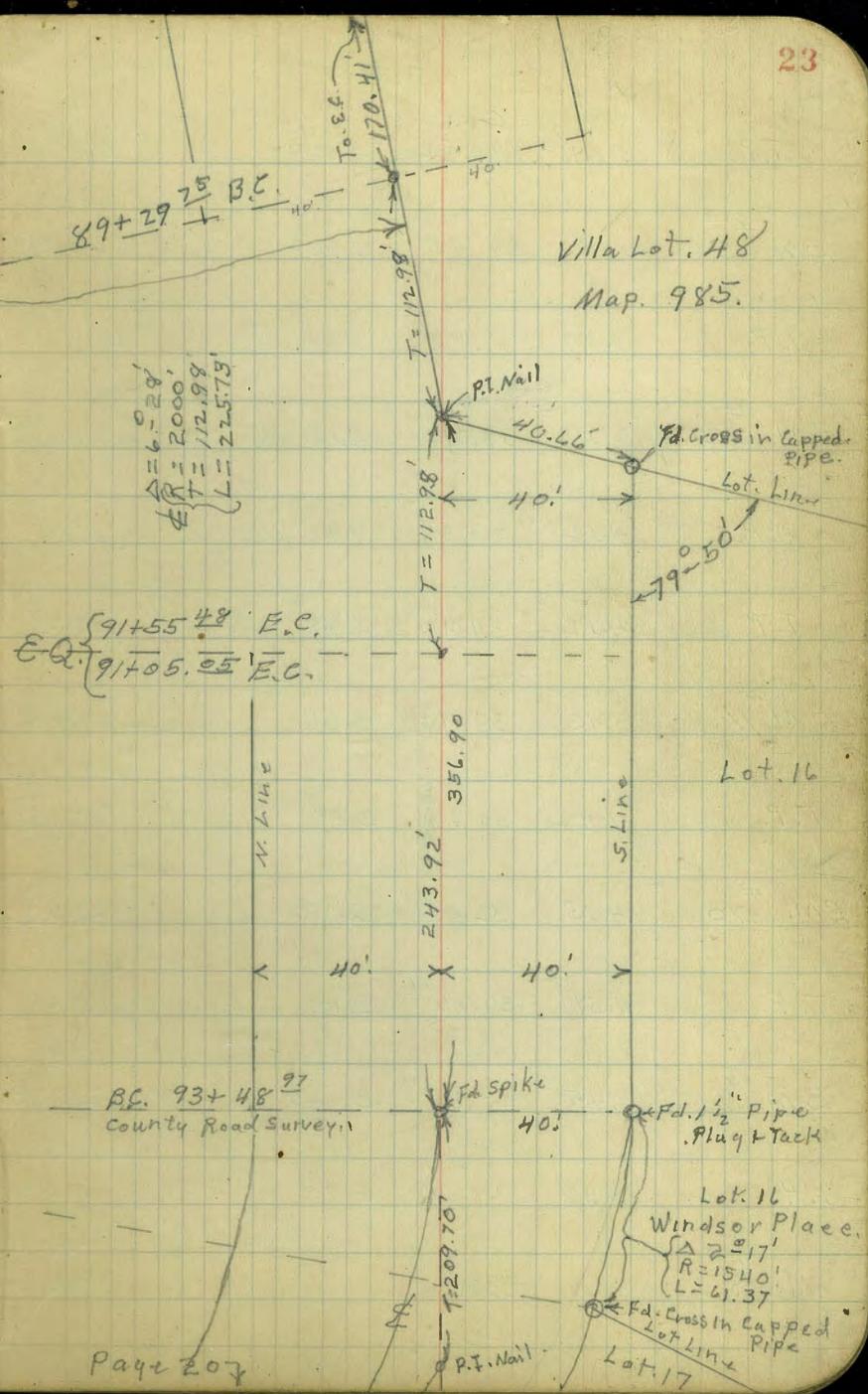
County Road Survey 514
80' R. of Way. Replacing old
R. of Way Maps 1870-1985 & 875

See T.P. Book 18 - Page 25-26 & 27 for
Alignment From station 89+29.75 to Sta. 74+86.30
point where City Boundary Line Leaves the Road.

See Page 69 for New Alignment.

Abandoned from 93+48.97 B.C.
To Old City Boundary New stationing
from 93+48.22 East. see page 69

Continued from Page 20



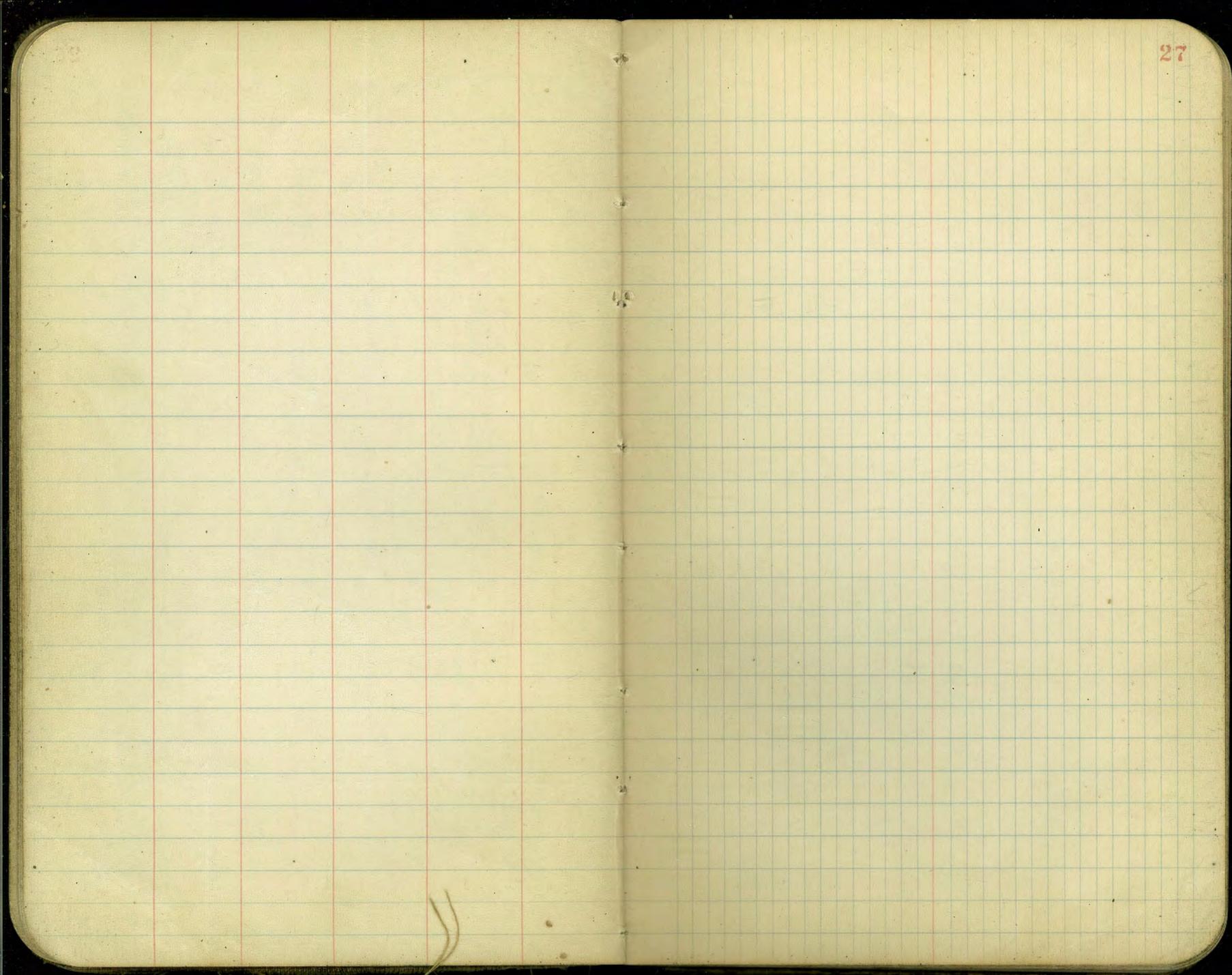
Page 207

Bench Marks

24

T.P.	5.01	40.62	4.24	35.61	Nail Tel Pole 87899 H	15' Lt. Sta 169+19.
B.M. #13	2.48	39.85	1.42	37.37	3 Nails in Elec Pole #79132	28.5' Rt. of Sta 164+21
T.P.	7.77	38.79	5.90	31.62		
B.M. #12	6.14	37.52	4.16	31.38 ✓ =	31.37 City B.M. B.P. Cmt. Mon ^{out.}	26.5' Lt. of Sta. 154+22
T.P.	4.12	35.54 ✓	2.98	31.42 ✓	Nail in Tel. Pole #87894-H	24' Lt. of Sta. 151+32
T.P.	4.12	34.40 ✓	2.88	30.28 ✓	Nail in Elec Pole #79119	23' Rt. of Sta 145+21
B.M. #11	3.43	33.16 ✓	3.66	29.73 ✓	2 Nails Tel. Pole D-19217-T	23' Lt. of Sta. 137+69
T.P.	4.92	33.39 ✓	3.58	28.47 ✓	Nail in Tel Pole #89546-H.	32' Lt. of Sta. 131+64
B.M. #10	4.15	32.05 ✓	2.86	27.90 ✓	3 Nails in Elec Pole #79082	46' Rt of Sta 126+50
T.P.	4.51	30.76 ✓	2.13	26.25 ✓	Nail in Elec Pole #79079	32' Rt. of Sta. 119+25
B.M. #9	3.45	28.38 ✓	3.25	24.93 ✓	3 Nails in Cypress Tree	26' Rt. of Sta. 113+70
T.P.	5.45	28.18 ✓	5.27	22.73 ✓		
B.M. #8	4.64 ✓	28.00 ✓		23.36 ✓	B.P. Sly End Existing 48" X 18" Culvert	64' Rt. Sta 100+67 ⁵³

B.M. #17		2.34		44.38	Cross N. side Iron Rim Water Dept. Man Hole 53.3' Lt. Sta 206+37
B.M. #16	11.94	66.72	1.74	54.78	R.P. Hub. 35' Lt of Sta 202+21 ³² E.C.
T.P.	11.40	56.52	5.48	45.12	Nail Tel. Pole # 306148 - H. 22' Lt. of Sta 198+29
B.M. #15	8.50	50.60	1.68	42.10	3 Nails in Tel. Pole # 89354 21.5' Lt. of Sta 191+13
T.P.	2.35	43.78	8.32	41.43	Nail in Elec Pole # 79143
B.M. #14	2.07	49.76	2.71	47.69	{ 3 Nails in Large Cypress Tree 55' Rt. of Sta 180+50 E. line Sand Rock Gravel
T.P.	12.10	50.40	2.32	38.30	Nail Tel Pole # 305605 H 16' Lt. of Sta 173+75
		40.62			



Camino Del Rio X. See
Continued from FB. 1528

INDEXED

						LT		RT
+ 39.			4.84	23.14		22.60 5.4 50	22.30 5.7 40	22.60 5.40 M.PAV
+ 05.			5.08	22.92			22.60 5.4 50	22.70 5.3 20
106	27.23	4.30					22.60 5.4 50	22.70 5.3 20
+ 88 ⁸⁷	B.C. Existing 20' Strip Paymt.	5.14	22.86			22.60 5.4 50	22.30 5.4 23	22.60 5.5 20
+ 50	27.28	4.26	4.98	23.02	F43 29.0	22.20 5.8 50	22.20 5.8 28	23.00 5.0 23
105	27.29	4.16	4.87	23.13	F46 29.6	22.30 5.7 50	22.90 5.1 28	23.50 4.5 23
+ 50	27.26	4.04	4.78	23.22	F47 29.6	22.10 5.9 50	22.10 5.9 28	23.50 4.5 23
104	27.18	3.86	4.68	23.32	F47 29.0	23.10 4.9 50	23.20 4.8 30	23.20 5.1 24
+ 50	27.05	3.66	4.61	23.39	F51 29.3	23.20 4.8 50	23.20 4.8 30	23.50 4.5 24
103	26.92					23.10 4.9 50	23.20 4.8 30	23.20 4.8 24
B.M. # 8.	4.64	28.00	23.36			23.10 4.9 50	23.20 4.8 30	23.20 4.8 24

F49
29.3

F43
29.0

F46
29.6

F47
29.6

F47
29.0

F51
29.3

28.00

B.P. Sly End. Headwall Existing 48" x 18" Culvert. 64' At Sta 100+67.50

29

F43
29.0

B.M. #9 3.45 28.38 3.45 24.93

T.P. 5.28 28.38 5.08 23.10

+84³⁸ EC. 26.12 3.04 5.1 23.08
+50
+47¹⁵ BC. Lt.

113 26.02 3.14 5.3 22.88

+50 25.95 3.07 5.3 22.88

112 25.94 -3.06 5.3 22.88

+50 25.95 -2.77 5.0 23.18

111 26.02 -3.04 5.2 22.98

+50 26.12 -3.04 5.1 23.08

28.18

3 Nails in Cypress Tree 26' Rt. of Sta 113+70

F40	5.2	5.2	4.3	4.8	5.1	5.1	5.1	5.1	5.1	5.0	4.1	4.0	F28
27.2	50	27	24	20	15	15	15	15	15	20	24	50	27.2
	22.58	22.58	23.48	23.18	22.98	22.88	22.88	22.88	22.88	22.18	23.18	23.88	24.18
F40	5.6	5.6	4.7	5.0	5.2	5.3	5.0	5.0	5.0	5.0	4.3	4.7	F28
27.2	50	27	24	20	15	15	15	15	15	20	24	30	27.2
	22.38	22.38	23.28	23.18	22.98	22.88	22.88	22.88	22.88	22.18	23.18	23.88	23.48
F45	5.8	5.8	4.9	5.0	5.2	5.3	5.0	5.0	5.0	5.2	3.8	4.6	F26
28.1	50	27	24	20	15	15	15	15	15	20	17	30	27.2
	22.48	22.48	22.98	22.88	22.88	22.88	22.88	22.88	22.88	22.98	23.98	23.58	23.58
F40	5.7	5.7	5.2	5.3	5.3	5.3	5.0	5.0	5.0	5.2	4.2	5.0	F31
27.8	50	27	24	20	15	15	15	15	15	20	27	30	27.6
	22.48	22.48	22.88	22.88	22.88	22.88	23.18	23.18	23.18	23.18	24.18	23.18	23.18
F38	5.7	5.7	5.3	5.3	5.3	5.0	5.0	5.0	5.0	5.0	4.0	5.0	F25
27.5	50	27	24	20	15	15	15	15	15	20	20	30	27.2
	22.48	22.48	22.88	22.88	22.88	23.18	23.18	23.18	23.18	23.18	24.18	23.18	23.18
F37	5.6	5.6	5.1	5.3	5.2	5.2	5.0	5.0	5.0	5.6	4.5	5.1	F30
27.5	50	27	24	20	15	15	15	15	15	20	27	30	27.5
	22.58	22.58	23.08	22.88	22.98	22.98	23.18	23.18	23.18	22.58	23.68	23.08	23.08
F35	5.6	5.6	5.1	5.3	5.3	5.1	5.0	5.5	4.5	5.1	5.1	5.1	F30
27.2	50	27	24	18	15	15	15	20	27	30	30	50	28.1
	22.58	22.58	23.08	21.78	22.88	22.88	23.08	23.18	22.68	23.68	23.08	23.08	23.08
							28.18						

118 +22 Tel Pole # D:19204-T 2.5' Lt.
 27.25 3.07 4.2 24.18

+50 27.12 3.14 4.4 23.98

117 27.00 3.32 4.7 23.68

+67 Tel Pole* D:19203-T 1.6' Lt
 +50 26.87 3.29 4.8 23.58

116 26.75 3.27 4.9 23.48

+50 26.62 3.04 4.8 23.58

115 26.50 3.02 4.9 23.48

+50 26.38 2.90 4.9 23.48

114 26.25 3.27 5.4 22.98
 28.38

Lt. 23.88 23.88 25.08 24.18 24.28 24.38 24.98 25.28 22
 F4.0 4.5 4.5 3.3 4.2 4.1 4.0 3.4 3.1 F2.5
 29.0 50 20 15 15 15 20 30 50 47.5 (20)

F36 28.7 23.78 23.78 25.28 23.18 23.68 23.88 23.98 24.38 25.58 24.98 24.98
 4.5 4.4 3.0 4.4 4.4 4.3 4.1 4.0 2.8 3.4 3.4 F2.0
 50 20 15 12 15 20 30 28 30 35 50 22.8 (3)

F38 28.7 23.78 23.78 25.28 23.18 23.68 23.88 23.98 24.38 25.28 24.68 24.68
 4.6 4.6 3.1 3.1 5.2 4.7 4.5 4.4 4.3 3.1 3.7 3.7 F2.3
 50 20 17 15 11 15 15 20 28 30 35 50 30.4 (7)

F42 29.3 23.78 23.78 24.18 23.58 23.58 23.88 23.98 24.08 25.28 24.58 24.58
 4.6 4.6 4.2 4.8 4.8 4.5 4.4 4.3 3.1 3.8 3.8 F2.6
 50 23 20 15 15 15 20 21 32 35 50 28.4

F44 29.6 23.58 23.58 24.78 24.48 23.48 23.78 23.98 23.98 24.98 24.78 24.78
 4.8 4.8 3.6 3.9 4.9 4.6 4.4 4.4 3.4 3.6 3.6 F2.4
 27 23 20 15 15 15 20 25 30 50 28.7

F42 26.0 23.38 23.38 24.98 24.88 23.58 23.78 23.88 23.98 24.88 24.68 24.68
 5.0 5.0 3.4 3.5 4.5 4.8 4.6 4.5 4.4 3.5 3.7 3.7 F2.2
 50 23 20 15 12 15 20 24 28 28 50 28.4

F42 26.6 23.28 23.28 24.78 24.28 23.48 23.68 23.78 24.58 24.68 24.68 24.68
 5.1 5.1 3.6 4.1 4.9 4.7 4.6 3.8 3.7 3.7 3.7 F2.4
 50 24 20 15 15 15 20 24 24 50 26.7 (3)

F45 27.2 22.98 22.98 24.58 24.58 23.48 23.68 23.78 24.58 24.68 24.68 24.68
 5.4 5.4 3.8 3.8 4.4 5.3 4.9 5.0 4.8 3.7 3.7 3.7 F2.6
 50 25 22 20 15 9 15 15 20 24 50 26.1 (3)

F43 28.1 22.98 22.98 23.28 23.28 22.98 23.28 23.28 24.68 24.28 24.28 24.28
 5.4 5.4 4.5 5.1 5.1 5.4 5.1 5.1 3.7 4.1 4.1 F3.0
 50 47 24 20 15 15 15 20 27 50 28.0

+20 Tel Pole 4.5' Lt.
 122 28.25 F40 6.5 24.26

+50 28.12 3.66 6.3 24.46

+18 Tel Pole 7' Lt.
 121 28.00 3.84 6.6 24.16

+50 27.87 3.11 6.0 24.76

120 27.75 3.19 6.2 24.56

T.P. 4.51 30.76 2.13 26.25

+71 Tel Pole #8952-H 10' Lt.
 +50 27.62 3.54 4.13 24.08

119 27.50 3.22 4.1 24.28

+50 27.37 3.09 4.1 24.28
 28.38

Lt
 24.66
 F37
 28.4
 6.1 6.1 6.0 6.0 5.1 6.5 6.7 5.4 5.4 5.2 5.3 4.2 5.2
 50 20 15 11 8 5 7 15 20 40 42 50
 24.56 24.56 24.56 24.76 25.86 24.46 24.06 25.06 25.96 25.56 25.46 26.56 25.56

F40
 28.4
 6.2 6.2 6.2 6.0 4.9 6.3 6.7 5.7 5.5 5.4 4.4 4.4 5.2
 50 20 15 11 8 5 15 20 39 40 50

F37
 28.4
 6.2 6.3 6.2 6.2 5.0 6.6 5.7 5.6 5.7 4.8 5.1 4.6
 50 20 15 12 9 15 20 38 39 50

F41
 28.7
 6.2 6.3 6.3 6.0 4.7 6.0 5.9 5.8 5.9 4.9 4.8 4.8
 50 20 15 12 9 15 20 37 38 50

F36
 28.4
 50 6.3 6.4 4.8 6.2 6.1 5.9 6.0 5.0 5.0 5.0
 20 15 10 15 20 35 36 50

30.76

Nail in Elec Pole #79079 32' Rt. of Sta 119445

F42
 29.3
 4.0 3.9 4.0 2.4 4.3 3.5 3.5 3.5 2.4 2.4 2.4
 50 20 15 13 13 20 33 35 50

F40
 29.0
 4.2 4.2 3.4 2.9 4.0 4.1 3.7 3.6 3.6 2.3 2.3 2.3
 50 20 15 12 5 15 20 32 33 50

F39
 29.0
 4.3 4.3 4.3 3.8 4.2 4.1 3.7 3.7 3.7 2.4 2.4 2.4
 50 20 15 13 5 15 20 31 35 50

28.38

F30
 40.8

F33
 40.6

F30
 42.2

F25
 37.1

F18
 35.8

F28
 32.6

F14
 33.5

B.M. # 10 4.15 32.05 2.86 27.90

3. Nails in Elec Pole # 79082 46' Rt. of sta. 126 + 50

126 1/2 S = 0.3 29.25 3.00 4.5 26.26

F38 29.0 6.0 5.8 5.1 4.5 4.0 4.2 4.0 4.7 F37 47.9 (26)

+53 Tel Pole 3' Rt. 29.12 2.16 3.8 26.96

F43 30.0 6.1 6.1 6.0 5.8 3.8 4.7 5.4 4.2 4.4 4.5 5.0

125 29.00 3.24 5.0 25.76

F43 29.3 6.2 6.2 6.1 6.0 4.6 5.0 6.0 5.6 4.6 4.7 4.5 4.9

+50 28.87 2.71 4.6 26.16

F41 29.3 6.2 6.2 6.1 6.1 4.0 4.6 5.8 5.0 5.0 4.3 3.7 4.6

+13 = Tel Pole 2' Lt. 28.75 3.09 5.1 25.66

F44 29.6 6.3 6.2 6.2 6.2 4.7 5.1 6.2 5.7 4.9 4.7 3.8 5.1 4.3

+50 28.62 3.26 5.4 25.36

F43 29.0 6.4 6.3 6.0 6.0 4.4 5.4 6.5 5.3 5.1 4.9 3.8 4 4.1

123 28.50 3.34 5.6 25.16

F38 29.7 6.0 6.0 6.0 6.2 4.7 5.6 6.3 5.5 5.4 5.1 5.2 4.4 4.1 5.2

+50 28.37 3.71 6.1 24.66 30.76

F36 28.4 6.0 6.0 6.0 5.8 4.5 5.1 6.2 5.2 5.2 5.2 5.4 4.1 4.1 5.1

(20)

+50 $\frac{1}{2}S=1.4$ 30.38 3.83 5.5 26.55

+12⁵² B.C. RT

130 $\frac{1}{2}S=0.8$ 30.25 4.0 5.8 26.25

+50 $\frac{1}{2}S=0.7$ 30.12 3.57 5.5 26.55

+25⁰⁷ EC

129 $\frac{1}{2}S=1.2$ 30.00 3.05 5.1 26.95

+50 $\frac{1}{2}S=1.4$ 29.87 2.62 4.8 27.25

+49 Elec Pole #79088 10' RT.

128 $\frac{1}{2}S=1H$ 29.75 2.40 4.7 27.35

+50 $\frac{1}{2}S=1H$ 29.62 2.57 5.0 27.05

+0.2 Tel Pole 3' Lt

127 $\frac{1}{2}S=1.2$ 29.50 3.45 6.0 26.05

+70⁴⁰ B.C. Lt.

+50 $\frac{1}{2}S=1.7$ 29.37 5.22 7.9 24.15
32.05

LT	27.55	26.85	26.35	26.35	26.95	26.55	26.35	26.15	26.55	RT
F50	4.5	5.2	5.7	5.7	5.1	5.5	5.7	5.9	5.5	F30
508	50	45	20	15	13		15	20	50	27.2
26.75	27.25	26.75	26.35	26.35	27.05	26.25	26.25	26.25	26.45	
F38	5.3	4.8	5.3	5.7	5.7	5.0	5.8	5.8	5.4	F31
460	50	45	43	20	16	15	15	20	50	27.15
27.55	27.55	26.85	26.75	26.65	26.55	26.55	26.55	26.05	26.15	
F21	4.5	4.5	5.2	5.3	5.4	5.5	5.5	6.0	5.9	F47
412	50	42	40	20	15		4	5	15	30.2
27.95	26.95	26.95	26.95	26.95	26.95	26.75	26.05	26.25	26.35	
F23	4.7	5.1	5.1	5.1	5.1	5.3	6.0	5.8	5.7	F34
382	50	38	20	15	15	6	10	15	20	31.1
27.55	27.35	27.25	27.25	27.25	27.25	27.25	26.95	26.05	26.55	
F08	4.5	4.7	4.8	4.8	4.1	5.7	6.0	5.5	5.5	F51
32.5	50	20	15		10	15	20	50	50	30.8
27.15	26.85	27.05	27.35	27.35	26.95	27.25	26.05	25.95	26.35	
F16	4.9	5.2	5.0	4.7	5.1	4.8	5.0	5.1	5.1	F55
25.7	50	20	15		15	20	20	50	50	31.1
26.95	26.85	27.05	27.05	27.35	27.35	27.25	27.15	26.35	26.35	
F17	5.1	5.2	5.4	5.0	4.7	4.7	4.9	5.1	5.1	F45
25.4	50	20	15		15	10	00	50	50	29.6
26.85	26.55	26.55	26.05	26.05	26.05	27.35	27.55	27.55	27.55	
F20	5.2	5.5	5.5	6.0	5.0	4.7	4.5	4.5	4.5	F30
26.0	50	20	15		4	15	10	50	50	38.5
24.75	24.75	26.05	25.05	24.15	24.35	26.65	26.55	26.85	26.85	
F38	7.8	7.3	6.0	7.0	7.9	7.7	5.4	5.5	5.2	F33
28.7	50	30	20	15	5	7	15	20	50	46.9
					32	0				25

Grado Fill

+50 30.30 3.1 6.2 27.19

F17 26.3 6.0 50 27.19 6.0 50 27.39 4.8 27 29.09 5.4 20 28.39 5.7 15 28.29 6.3 13 27.19 6.2 15 26.79 5.7 20 26.79 5.1 14 28.29 5.8 36 27.59 6.7 40 26.69 6.6 F2.0 50 26.0

134 - 30.34 3.1 6.2 27.19

F14 26.6 6.2 50 27.19 6.0 30 27.49 4.3 28 28.79 5.0 20 27.79 5.1 15 27.79 6.2 13 27.29 4.2 15 26.59 6.6 20 26.79 4.4 23 28.89 5.3 33 28.09 6.8 34 26.59 6.6 F2.0 26.3

+50 1/2 S = 0.4 30.43 3.34 6.3 27.09

F24 27.2 6.2 50 27.19 5.9 31 27.49 4.6 28 28.79 5.6 20 27.79 5.6 15 27.29 6.1 13 27.09 6.3 15 26.59 4.8 20 28.89 4.5 24 28.89 6.0 30 27.39 6.7 F2.5 50 26.9

133 1/2 S = 8 30.52 3.63 6.5 26.89

+85 81 E.C.

F35 28.4 6.3 50 27.09 6.2 31 27.19 5.0 28 28.39 5.5 20 27.89 5.8 15 27.59 6.5 13 26.89 6.5 15 26.89 5.5 20 28.39 6.6 30 26.79 6.6 50 26.79 6.6 F2.0 26.5

+50 1/2 S = 1.4 30.57 3.68 6.5 26.89

4P 28.4 6.2 50 27.09 6.2 31 27.19 4.7 27 28.69 4.4 20 28.59 6.5 15 26.89 6.5 15 26.89 5.7 15 27.69 4.8 20 28.59 6.7 30 26.69 6.4 50 26.79 6.4 F1.1 24.5

132 1/2 S = 1.4 30.59 3.80 6.6 26.79

+76 El. & Pole 15' RT.

F38 28.6 6.4 50 26.79 6.5 35 26.89 5.4 30 27.99 5.5 21 27.89 6.2 20 27.19 6.5 15 26.89 6.6 9 26.79 5.5 11 27.89 5.3 15 28.09 5.6 20 27.79 6.3 25 27.09 4.3 F2.5 50 26.4

+50 1/2 S = 1.4 30.55 3.96 6.8 26.59

F5 30.8 6.6 50 26.79 6.6 40 26.79 5.3 36 28.09 5.1 28 27.79 6.3 27 27.09 6.5 20 26.89 6.6 15 26.79 6.8 4 26.59 5.0 5 27.39 5.5 13 27.89 6.0 15 27.39 6.8 20 26.59 6.8 F2.5 50 27.0

T.P. 4.92 33.39 3.58 28.47

33.39
Nail Tol. Pole # 89546-H 32' Lt. of Sta. 131+64

131 1/2 S = 1.4 30.48 3.03 4.6 27.45

32.05

F48 26.85 5.2 50 26.85 4.0 43 28.05 5.0 33 27.05 5.7 20 26.85 5.7 15 26.35 4.7 5 27.35 4.0 32 27.45 4.2 7 27.85 5.5 15 26.55 5.5 20 26.55 5.5 50 26.45 6.8 F2.6 27.2

Grade Fill

B.M. # 12 6.36 37.74 4.16

31.38 B.P. Mon. 26.5' Lt. of Sta. 154 + 22
31.37 City

+78¹³ B.C. Lt.

+50 1/2 S = 0.7 33.50 2.2

F12
25.1

30.94	31.54	31.34	31.34	31.34	30.94	31.54	31.54	31.54	31.54
4.4	4.0	4.2	4.2	4.2	4.6	4.0	4.0	4.0	4.0
50	25	20	15	15	15	17	20	50	50

F21
26.3

154 33.37 2.5

F24
26.3

31.04	30.64	31.04	30.94	30.94	31.14	30.14	30.14	30.94	31.54	31.54
4.5	4.9	4.5	4.6	4.6	4.4	5.4	5.4	4.6	4.0	4.0
50	25	20	15	15	13	15	17	20	21	50

F20
26.3

+50 33.25 2.3

F20
24.1 (4)

31.54	31.54	31.34	30.94	30.64	29.84	29.74	31.04	31.04	31.04
4.0	4.0	4.2	4.6	4.9	5.7	5.8	4.5	4.5	4.5
50	20	15	15	15	17	20	25	50	270

F16
27.0

153 33.12 2.3

F15
26.3 (6)

31.54	31.54	31.24	30.84	30.64	29.24	29.24	29.34	31.34	31.34
4.0	4.0	4.3	4.7	4.9	6.3	6.3	6.2	4.2	4.2
50	20	15	15	15	18	20	22	25	50

F13
27.7

+50 33.00 2.4

F22
49.7 (29)

31.54	31.44	30.94	30.64	30.54	30.54	29.14	29.14	31.44	31.44
4.0	4.1	4.6	4.9	5.0	5.0	6.4	6.4	4.1	4.1
50	20	15	15	15	17	20	23	26	50

F12
28.9

152 32.87 2.4

F17
26.6

31.34	31.14	30.74	30.54	30.34	30.04	29.44	29.44	31.44	31.44
4.2	4.4	4.8	5.0	5.2	5.5	6.1	6.1	4.1	4.1
50	20	15	15	15	19	20	23	25	50

F10
28.6

35.54

T.P. 4.12 35.54 2.98

31.42 Nail Tel Pole # 87894-H. 24' Lt. of Sta 151 + 82

34.40

+18⁵⁹ E.C. £ £
 159 $\frac{1}{2}S=1.0$ 34.62 F1.9
 +50 $\frac{1}{2}S=1.4$ 34.50 F1.9
 158 $\frac{1}{2}S=1.4$ 34.37 F1.7
 +67 Tel Guy Pole # 301485-H. 21' RT
 +67 Tel Pole # D-19230-T. 12.5 Lt.
 +50 $\frac{1}{2}S=1.4$ 34.25 F1.5
 +28 Elae Pole # 79128 21' RT
 157 $\frac{1}{2}S=1.4$ 34.12 F1.4
 +50 $\frac{1}{2}S=1.4$ 34.00 F1.6
 156 $\frac{1}{2}S=1.4$ 33.87 F1.6
 +50 $\frac{1}{2}S=1.4$ 33.75 F1.5
 155 $\frac{1}{2}S=1.0$ 33.62 F1.8

FL3 24.5	6.8 50	30.94 30	6.8 30	30.94 20	5.8 15	32.74 15	5.0 15	32.74 15	4.9 20	32.84 20	4.9 50	32.84 50	F2.2 24.9 (3)
F1.2 24.2	6.6 50	31.14 30	6.7 30	31.04 20	5.9 15	31.84 15	5.1 15	32.34 15	4.9 20	32.84 20	4.6 50	33.14 50	F2.5 26.2 (4)
F1.5 23.3	6.5 50	31.24 25	6.4 25	31.34 20	5.3 15	32.44 15	5.0 15	32.74 15	4.8 20	32.94 20	5.0 50	32.74 50	F2.5 27.2
F1.7 25.0	6.6 50	31.14 20	6.6 20	31.14 15	4.6 11	33.14 11	5.0 15	32.74 15	4.9 20	32.84 20	5.0 50	32.74 50	F2.4 27.0
Gr 23.3	6.6 50	31.14 20	6.5 20	31.24 15	4.8 15	32.94 15	5.3 15	32.44 15	5.0 15	32.74 15	5.0 20	32.74 20	5.3 26.0
F0.7 28.9 (10)	6.8 50	30.94 30	6.8 30	30.94 20	5.8 15	31.94 15	5.6 15	32.24 15	5.3 15	32.64 15	5.1 20	32.64 20	F2.7 27.2
Gr 28.8 (10)	6.8 50	30.94 30	6.6 30	31.14 20	5.2 15	32.54 15	5.7 15	32.04 15	5.5 15	32.24 15	5.5 20	32.24 20	F3.0 27.2
C03 33.0 (10)	6.8 50	30.94 40	6.7 40	31.04 30	5.4 20	32.34 20	5.7 15	32.04 15	5.5 15	32.24 15	5.7 20	32.24 20	F2.6 27.0
C03 29.0 (10)	6.9 50	30.84 30	6.8 30	31.04 20	5.6 15	32.34 15	5.7 15	32.04 15	5.5 11	32.24 11	5.7 20	32.04 20	F2.5 26.9

37.74

37.74

163
 +67 Elec Pole #79181 19' Rt
 +66 Tel Pole #82317-M. 19' Lt
 +50 $\frac{1}{2}S=1.4$ 35.62 F2.0

	30.37	30.47	31.87	32.67	33.07	33.57	33.37	33.57	35.17	34.67	34.57	43
F52	7.5	7.4	6.5	5.2	4.8	4.3	4.5	4.3	2.7	3.2	3.3	65
309	50	40	25	20	15	15	15	20	22	30	50	236
	30.37	30.87	32.87	31.67	31.77	32.97	33.07	33.07	33.07	34.07		
F48	7.5	7.0	5.0	6.2	6.1	4.9	4.8	4.8	3.8	3.8		604
381	50	35	23	20	15	12	15	17	20	50		214
(12)												

162
 +50 $\frac{1}{2}S=1.4$ 35.37 F2.5
 +29¹² B.C. Rt. $\frac{1}{2}S=1.0$ 35.25 F2.6

	30.27	30.27	32.57	32.57	32.07	32.87	32.87	32.97	34.07	33.47	33.27	
F55	7.6	7.6	5.3	5.3	5.8	4.8	5.0	5.0	4.9	3.8	4.4	65
293	50	40	24	20	15	13	15	15	20	23	29	50
	30.37	30.37	31.97	31.97	32.77	32.67	32.77	32.77	33.37	33.07	33.07	
F45	7.5	7.5	5.9	5.9	5.1	5.2	5.1	5.1	4.5	4.8	4.8	60
290	50	35	20	15	13	13	15	20	22	26	50	244

161
 $\frac{1}{2}S=0.7$ 35.12 F2.5

	30.77	30.77	32.37	32.37	32.67	32.67	32.67	32.67	32.67	33.27	33.07	
F34	7.1	7.1	5.5	5.5	5.2	5.2	5.2	5.2	5.2	4.6	4.8	60
275	50	35	25	20	15	15	15	20	25	28	50	241
						37.87						

T.P 4.02 37.87 3.89 33.85

Wall Elec. Pole 24.5 Rt. of sta. 160+26

+50 0.2 35.00 F2.6

	30.64	30.64	32.24	32.34	32.24	32.44	32.44	32.74	33.04	33.04	F16	
F28	7.1	7.1	5.5	5.4	5.1	5.3	5.3	5.0	4.7	4.7	24.0	
269	50	35	25	20	15	15	15	20	25	50	(3)	
	30.74	30.74	31.64	32.34	32.34	32.34	32.34	32.54	33.14	33.14		

160 $\frac{1}{2}S=0.2$ 34.87 F2.5

	30.74	30.74	31.64	32.64	32.64	32.44	32.64	32.74	32.74	32.74	F18	
F25	7.0	7.0	6.1	5.4	5.4	5.4	5.4	5.2	4.6	4.6	24.6	
152	50	35	28	20	15	15	15	20	25	50	(2)	

+50 $\frac{1}{2}S=0.7$ 34.75 F2.3
 37.74

	30.74	30.74	31.54	32.64	32.64	32.44	32.64	32.74	32.74	32.74	F27	
F18	7.0	7.0	6.2	5.1	5.1	5.3	5.1	5.0	5.0	5.0	24.8	(3)
354	50	35	30	20	15	15	15	20	50	50		
						37.74						

167 Grade
36.62 F1.6

+50 $\frac{1}{2}S=0.2$ 36.50 F1.0

166 $\frac{1}{2}S=0.7$ 36.37 6r

+73 Tel Pole 5' Lt.

+68^{vs} E.C.

+50 $\frac{1}{2}S=0.9$ 36.25 C0.5

165 $\frac{1}{2}S=1.4$ 36.12 C0.5

+50 $\frac{1}{2}S=1.4$ 36.00 C0.2

B.M. #13. 3.47 40.84 0.50 37.37

+22 Tel Pole 8' Lt.

164 $\frac{1}{2}S=1.4$ 35.87 F1.2

+50 $\frac{1}{2}S=1.4$ 35.75 F1.7

37.87

Lt. 32.54
F31 41.0 50 8.3 7.1 5.7 5.8 5.7 5.3
31.84 34.54 34.54 35.34 36.34 35.64 35.54 35.14 35.54

F27 26.7 9.0 6.3 6.3 5.5 4.5 5.2 5.3 5.2 5.0 4.2 3.5
50 20 15 11 8 7 15 20 30 50
31.54 33.64 34.34 34.74 36.34 36.34 36.44 37.74 38.34

F30 27.0 9.3 7.2 6.5 6.1 4.5 4.5 4.5 4.4 3.1 2.5
50 30 20 15 7 15 20 30 50
30.94 34.44 34.74 35.84 36.74 36.54 36.54 36.84 37.94

F32 27.0 9.9 6.4 6.1 5.0 4.1 4.3 4.3 4.0 2.9 1.6
50 20 15 7 15 20 28 30 50
30.84 31.14 34.44 34.84 35.54 36.64 36.54 36.64 38.04 39.34

F38 28.4 10.0 9.7 6.4 6.0 5.3 4.2 4.3 4.3 4.2 2.8 1.5
50 40 20 15 11 15 20 23 24 50
31.04 31.04 33.64 33.64 36.14 35.84 35.74 35.74 37.24 38.54

F12 25.0 9.8 9.8 7.2 7.2 4.7 5.0 5.1 5.1 5.1 3.6 2.3
50 30 20 15 4 15 20 23 24 50
30.57 30.57 32.37 33.47 34.67 34.67 34.67 34.77 36.47 37.27 37.47
30.57 30.57 31.57 32.97 33.87 34.07 34.07 34.07 34.87 36.07 35.77 35.77

Rt. 36.24 36.84 44
4.6 4.0 F1.0
30 50 25.1

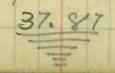
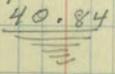
C03 29.0 37.34 38.34
30 50 10

C23 34.0 37.24 39.24
30 50 10

C16 29.4 37.24 38.54
30 50 10

C47 22.6 37.24 38.54
30 50 10

2/0 21.0 35.77 37.87
30 50 25.0



3' Nails Elce Pole # 791322 28.586 of Sta. 1647.21

171 F214 37.62 ✓ 5.4 35.48

+75 Tel Pole 16' Lt.

+50 F212 37.50 5.7 35.38

170 F229 37.37 6.0 35.08

+50 F217 37.25 6.0 35.00

T.P. 5:47 41.08 5:23 35.61

169 F238 37.12 ✓ 6.1 34.74

+50 F236 37.00 6.2 34.64

168 F253 36.87 6.5 34.34

+81 Tel Pole 15' Lt.

+50 F231 36.75 6.4 34.44

40.84

2+ 34.48
6.6 6.2 5.5 5.6 5.6 5.6 7.8 7.8 F1.9
50 20 15 15 20 32 33 50 26.3

F32 34.88
7.0 6.2 5.2 5.7 5.8 5.8 5.7 8.3 8.4 F1.6
50 20 15 15 20 30 33 50 26.3

F36 35.88
8.5 7.1 5.6 6.0 6.0 6.0 5.9 7.7 7.9 F2.0
50 20 15 15 20 29 33 50 26.3

F28 35.08
8.9 8.4 7.1 6.6 6.1 6.0 6.0 6.0 8.6 8.7 F1.7
50 40 35 20 15 15 20 27 33 50 26.3

41.08

Nail Tel Pole # 87899-H, 15' Lt. of Sta 169+19

F34 32.94
7.7 7.4 6.2 6.2 6.1 5.9 5.9 5.6 8.6 8.6 F1.8
50 25 20 15 15 20 27 31 50 26.3

F35 32.64
8.2 8.2 6.8 6.2 6.2 6.0 6.0 6.0 8.5 8.5 F1.9
50 35 20 15 15 20 28 33 50 26.3

F33 33.74
7.1 7.3 7.0 6.5 6.1 6.1 6.2 F2.4
50 20 15 15 20 50 26.6

F32 33.84
8.1 7.0 6.9 6.4 6.4 6.1 6.1 5.3 F1.8
50 40 20 15 15 20 50 26.0

40.84

175
 C1.02 41.65 7.5 42.67
 Grade 4

TP 11.87 50.17 2.78 38.30

+50 C0.6 40.92 0.1 40.98

174 F0.91 40.19 1.8 39.28

+75 Tel Pole 16' Lt.

+50 F1.73 39.51 3.3 37.78

173 F2.05 38.93 4.2 36.88

+50 F1.87 38.45 4.5 36.58

+20 Tel. Pole 15.5' Lt.

172 F2.10 38.08 5.1 35.98

+50 F2.12 37.80 5.4 35.68
 41.04

LT. 39.37 41.07 41.97 42.17 42.77 42.77 44.17 45.87 Rt.
 F02 10.8 9.1 8.2 8.0 7.4 7.4 6.0 4.3
 23.7 50 25 20 15 15 20 21 30 41 22.8
 50.17 24.2

Nail Tel Pole # 305 605 H. 16' Lt of sta 173+75

F08 38.08 39.18 40.28 40.28 40.98 41.28 41.28 41.28 42.48 43.38 43.48
 3.0 1.9 0.8 0.8 0.1 +0.2 +0.2 +0.2 +1.4 +2.3 +2.4
 23.8 50 25 20 15 15 20 21 23 30 30 50 50
 37.18 37.48 38.28 38.48 39.28 39.58 39.58 40.18 40.78 40.88 42.7

F26 39 3.1 2.8 2.1 1.8 1.7 1.7 0.9 0.3 0.2 0.2
 25.4 50 25 20 15 15 15 20 26 36 50 50 50

F34 35.58 36.38 36.88 37.78 37.98 38.08 38.08 38.38 38.28 38.28
 5.5 4.7 4.2 3.3 3.1 3.0 3.0 2.7 2.8 F1.8
 27.8 50 20 15 15 15 20 26 50 50 25.4

F32 35.58 35.78 36.08 36.88 37.08 37.08 37.08 37.58 37.58 37.58
 5.5 5.3 5.0 4.2 4.0 4.0 4.0 3.5 3.5 F2.0
 27.8 50 20 15 15 15 20 26 36 50 27.3

F2.9 35.48 35.88 35.98 36.58 36.58 36.58 36.58 37.08 37.08 37.08
 5.6 5.2 5.1 4.5 4.5 4.5 4.5 4.0 4.1 F1.6
 27.2 50 20 15 15 15 20 24 30 50 26.0

F26 35.08 35.58 36.08 35.98 36.18 36.18 36.18 36.88 36.88 36.88
 6.0 5.5 5.0 5.1 4.9 4.9 4.9 4.2 4.2 F2.2
 27.0 50 20 15 15 20 20 26 32 50 26.0

F2.7 34.78 35.28 35.88 35.68 35.68 35.68 35.68 34.28 34.28 34.28
 6.3 5.8 5.2 5.4 5.4 5.4 5.4 6.8 6.8 F2.1
 27.0 50 20 15 15 20 20 33 50 26.3

183 $\frac{1}{2}S=0.2$ 44.86 F744 11.6 37.42

F86
35.3

24
36.02
13.0 50
36.02
12.2 20
36.82
12.0 15
37.42
11.6
37.42
11.0 15
38.02
11.6 20
38.02
11.6 26
40.22
8.8
40.22
5.4 50
43.62
F62
33.0

+50 $\frac{1}{2}S=.7$ 45.55 F813 11.6 37.42

F98
37.4

36.02
13.0 50
36.62
12.4 20
36.82
12.2 15
37.42
11.6
37.42
11.4 15
37.62
11.2 20
37.82
9.4 39
39.62
4.7 47
44.32
4.7 50
44.32
F60
33.0

+32⁰⁵ E.C.

182 $\frac{1}{2}S=1.2$ 46.24 F822 11.0 38.02

F110
39.0

36.02
13.0 50
37.02
12.0 20
37.22
11.8 15
38.02
11.0
38.02
10.8 15
38.22
10.1 20
38.42
8.3 35
40.72
4.3 42
44.72
4.3 50
45.82
F58
31.4

+50 $\frac{1}{2}S=1.4$ 46.93 F891 11.0 38.02

F118
40.4

36.02
13.0 50
36.92
12.1 20
37.32
11.7 15
38.02
11.0
39.02
10.0 15
39.52
9.5 20
40.42
8.6 26
45.72
3.3 37
45.82
3.2 50
F24
30.5

49.02
||
||

BM #14. 1.33 49.02 4.63 47.69

3 Nails 1h. Large Cypress Tree 55' Rt. of Sta 180+55

181 $\frac{1}{2}S=1.4$ 47.50 F868 13.5 38.82

F114
40.1

36.42
15.4 50
37.52
14.8 20
37.72
14.4 15
38.82
13.5
40.32
12.0 15
41.72
10.6 20
46.62
5.7 29
46.82
5.5 50
GF
28.4

+75 12.7 39.62

+62 Tel Pole 13' Rt.

38.52
14.5 50
38.62
13.8 20
40.52
13.6 15
42.82
12.7
43.82
11.7 10
46.92
8.0 15
48.02
5.8 20
48.02
4.9 23
47.22
5.1 50

+50 $\frac{1}{2}S=1.4$ 47.84 F5.0 9.5 42.82

38.52
13.8 50
38.62
13.7 35
40.52
11.8
41.2
11.2 15
42.82
9.5 7
43.82
8.5 15
46.92
5.4 15
48.02
4.3 20
48.02
4.3 16
47.22
5.0 50

+46 10.0 42.32

52.82

38.32
14.0 50
41.22
11.1 20
41.52
10.8 15
42.32
10.0 12
42.32
10.0 15
43.12
4.2 15
48.12
4.2 20
48.02
4.3 16
47.32
5.0 50

52.32
||
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187	$\frac{1}{2}S=1.4$	40.58	F1.61	5.1	38.97	$\frac{28}{F14}$ 25.1	57.67 6.4 50	58.07 6.0 20	38.47 5.6 15	38.97 5.1	39.27 4.8 15	39.27 4.8 20	39.37 4.7 26	40.17 3.9 30	41.93 2.1 36	42.07 2.0 50
+54	Tel Pole	3. Lt.					37.47	37.77	37.87	38.67	39.07	39.27	39.27	39.57	40.47	42.07
+50	$\frac{1}{2}S=1.4$	40.71	F2.04	5.4	38.67	$\frac{F22 F28}{26.3}$	6.6 50	6.3 20	6.2 15	5.4	5.0 7	4.8 15	4.8 20	4.5 36	3.6 39	2.0 50
186	$\frac{1}{2}S=1.4$	41.01	F2.84	5.9	38.17	$\frac{24}{F18}$ 25.7	6.7 50	6.4 20	6.4 15	5.9	4.7 18	4.7 20	4.4 45	3.8 50	F1.6 47.3 36	2.3
+50	$\frac{1}{2}S=1.4$	41.42	F3.59	6.2	37.87	$\frac{F25}{26.6}$	6.8 50	6.4 20	6.3 15	6.2	5.6 15	5.0 20	4.6 27	4.2 50	F2.7 25.3	
							44.07									

T.P. 2.63 44.07 7.58 41.44 Nail in Elec Pole # 79143.

185	$\frac{1}{2}S=1.4$	42.07	F4.35	11.3	37.72	$\frac{F33}{27.8}$	37.22 11.8 50	37.52 11.5 20	37.52 11.5 15	37.72 11.3	37.92 11.1 15	37.92 11.1 20	38.62 10.4 26	40.02 9.0 50	F3.8 30.8	
+50	$\frac{1}{2}S=1.0$	42.79	F4.77	11.0	38.02	$\frac{F46}{31.4}$	36.92 12.1 50	37.22 11.8 20	37.32 11.7 15	38.02 11.0	38.32 10.7 15	38.42 10.6 20	39.62 9.4 40	41.02 8.0 50	F4.0 30.2	
+45 ³⁸	B.C. Lt.						36.52	37.22	37.22	37.82	38.12	38.12	40.12	41.02		
184	$\frac{1}{2}S=0.5$	43.48	F5.66	11.2	37.82	$\frac{F63}{32.0}$	36.52 12.5 50	37.12 11.8 20	37.32 11.8 15	37.72 11.2	38.02 10.9 15	38.02 10.9 20	39.52 8.9 48	42.02 8.0 50	F5.6 31.7	
+50	00	44.17	F6.45	11.3	37.72	$\frac{F7.6}{33.8}$	36.52 12.5 50	37.12 11.9 20	37.32 11.7 15	37.72 11.3	38.02 11.0 15	38.02 11.0 20	39.52 9.5 45	42.02 7.0 50	F4.5 30.0	
							49.02									

199 46.87 F1.62 10.0 45.25

42.05	42.55	44.15	44.35	44.65	45.05	45.25	45.55	45.95	46.85	47.75	48.65	53
F2.8	12.7	11.1	10.9	10.6	10.2	10.0	9.7	9.3	8.4	7.5	6.6	C10
13.2	24	25	20	15	13	15	15	18	20	24	50	24.2
50												
42.15	42.53	43.65	43.65	44.25	44.95	45.15	45.55	46.15	47.15	48.75	49.25	

+50 46.33 F1.18 10.1 45.15

42.15	42.53	43.65	43.65	44.25	44.95	45.15	45.55	46.15	47.15	48.75	49.25	
F2.5	12.7	11.6	11.6	11.0	10.3	10.1	9.7	9.1	8.1	6.5	6.0	C15
13.1	26	23	20	15	13	15	15	18	20	24	50	23.0
50												

45.12 ? 55.25 ask.

T.P. 10.13 55.25 7.61

45.12 Nail Tel. Pole #306144-H. 22' Lt. of Sta 198+29

+33 Elce Pole 22.5RT,

+29 Tel Pole 22' Lt.

198 45.97 F0.44 7.2 45.53

41.43	42.43	43.33	43.73	44.13	44.93	45.53	45.73	46.13	47.73	49.93	50.53	C33
F2.4	11.3	10.3	9.4	9.0	8.6	7.8	7.2	7.0	6.6	5.0	2.8	22
26.0	50	32	27	20	15	13	15	15	19	20	24	50

+50 45.72 C0.11 6.9 45.83

41.33	42.33	43.43	44.23	44.43	45.53	45.83	46.13	46.13	47.83	49.73	50.43	C36
F1.6	11.4	10.4	9.3	8.5	8.3	7.2	6.9	6.6	6.6	4.9	3.0	2.3
24.5	50	31	26	20	15	13	15	15	19	20	24	50

197 45.46 C0.47 6.8 45.93

41.43	42.33	43.73	44.53	44.53	45.53	45.93	45.93	45.93	47.53	49.33	50.13	C15
F1.0	11.3	10.4	9.0	8.2	8.2	7.2	6.8	6.8	6.8	5.2	3.4	2.6
24.2	50	31	26	20	15	13	15	15	19	20	24	50

+76 Tel. Pole 21.5 Lt.

+50 45.20 C0.53 7.0 45.73

41.43	42.33	43.63	44.13	44.53	45.43	45.73	45.83	45.83	47.33	49.33	49.93	C40
F1.4	11.3	10.4	9.1	8.6	8.2	7.3	7.0	6.9	6.9	5.7	3.4	2.8
23.9	50	31	26	20	15	13	15	15	18	20	24	50

196 44.94 C0.79 7.0 45.73

41.33	42.43	43.73	44.43	44.53	45.33	45.73	45.73	47.43	49.33	49.93	50.43	C44
F0.5	11.4	10.3	9.0	8.3	8.2	7.4	7.0	7.0	5.3	3.4	2.8	2.4
23.0	50	31	26	20	15	13	15	15	20	24	50	25.9

+50 44.68 C1.45 6.6 46.18

41.43	42.73	44.73	45.43	45.73	46.18	45.83	47.43	48.23	49.73	50.33	50.33	C13
C0.3	11.3	10.0	8.0	7.3	7.0	6.6	6.9	5.3	4.5	3.0	2.4	2.4
20.9	50	30	25	20	15	15	15	17	20	24	50	21.3

52.73

52.73

203 $\frac{1}{2}S=0.1$ 56.59 C 3.05 7.0

56.94	57.84	58.24	58.64	58.84	58.14	58.14	57.84	58.94	58.64	59.64	61.84	61.64	61.84	63.04
9.7	8.0	8.8	8.5	8.5	8.8	7.7	8.0	7.0	4.4	5.0	4.8	3.6		
36.0	38	32	32	20	15	6	5	1	5	15	20	50		

rd. 34
40 wide
C 5.6
30.4

+50 $\frac{1}{2}S=0.3$ 55.19 C 0.65 10.8 55.84

56.04	56.34	55.44	55.44	55.54	55.84	56.64	58.54	59.24	59.94	60.54
10.6	10.3	11.2	11.2	11.1	10.8	10.0	8.1	7.4	6.7	6.1
50	26	25	20	15	10	7	10	15	20	50

C 0.6
28.6 (10)
66.64
C 5.1
29.8

BM # 16 11.86 66.64 0.47

54.78 R.P. Hub 35' Lt. of 202 + 21 32 EC.

+21 32 EC

202 $\frac{1}{2}S=0.5$ 53.77 F 0.82 2.3 52.95

F14	52.15	53.25	53.35	52.65	52.85	52.95	53.05	55.25	56.35	56.35	56.75
3.1	2.0	1.9	2.6	2.4	2.3	2.2	2.0	1.1	1.1	1.1	1.5
25.7	50	32	21	20	15	11	15	17	20	50	27.5

+50 $\frac{1}{2}S=0.6$ 52.37 F 1.92 4.8 50.45

F22	48.05	49.35	50.85	50.15	50.85	50.85	50.85	50.25	50.25	50.25	52.45	53.45	54.05
7.2	5.9	4.4	5.1	4.4	5.0	4.8	4.4	5.0	5.0	5.0	2.8	1.8	1.2
26.1	50	33	28	20	16	15	10	13	15	16	20	22	50

201 $\frac{1}{2}S=0.6$ 50.97 F 2.72 7.0 48.25

F40	45.45	46.65	47.75	47.45	48.25	48.25	48.85	48.05	47.95	49.35	50.55	51.25	51.25
9.8	8.6	7.5	7.8	7.0	7.0	6.4	7.2	7.3	5.9	4.7	4.0	4.0	4.0
26.1	50	30	25	20	15	13	15	18	20	24	50	24.5	C 0.3

+50 $\frac{1}{2}S=0.4$ 49.66 F 2.91 8.5 46.75

+46 16 B.C. RT

F5P	44.25	44.65	45.55	45.75	46.65	46.75	47.45	47.45	47.45	48.55	49.25	51.25	51.25
11.0	10.6	9.7	9.5	8.6	8.5	7.8	7.4	7.4	6.7	6.0	6.0	6.0	6.0
26.3	50	28	25	20	15	15	20	22	25	50	25.7	25.7	F 0.2

200 $\frac{1}{2}S=0.2$ 48.54 F 2.24 9.0 46.25

F40	43.35	44.05	45.15	45.55	45.95	46.25	46.65	46.75	47.65	48.05	48.05	48.05	48.05
11.9	11.2	10.1	9.7	9.3	9.0	8.6	8.5	8.5	7.6	7.2	7.2	7.2	7.2
26.1	50	28	25	20	15	15	15	20	24	50	24.8	24.8	F 0.5

+50 $\frac{1}{2}S=0$ 47.61 F 2.06 9.7 45.55

55.25

F36	42.45	43.05	44.25	44.45	44.95	45.55	45.55	45.75	46.55	47.45	48.15	48.15	48.15
12.8	12.2	11.0	10.8	10.3	9.7	9.7	9.5	9.5	8.7	7.8	7.1	7.1	7.1
25.5	50	28	25	20	15	13	15	15	20	24	50	23.2	23.2

55.25
F 0.6
23.2
(4)

206 63.94 3.3 68.50

+51 Elee Pole 18' Lt.
+50 1/2 S = 0.2 63.0 3.3 68.50
+35 BC

205 1/2 S = 0.1 62.0 C 5.8 4.0 67.80

+50 1/2 S = 0.1 60.8 C 4.8 4.2 65.60

T.P 7.04 71.80 1.88 64.76

+35
204 59.4 C 5.34 1.9 64.74

+11 E. Pole of Transformer station 6.5 Lt. of d

204 +95 W. Pole of Transformer station 5' Lt. of d

+50 58.00 C 5.64 3.0 63.64
46.64

Lt.

65.20
4.6 5.0 5.6 4.6 3.3 2.1 2.0 0.3
50 20 10 15 15 20 50

65.70 66.20 67.30 68.50 68.90 69.10 70.70
6.1 5.6 4.5 3.3 2.9 2.7 1.1
50 20 15 15 15 20 50

64.20 66.00 66.40 67.80 67.80 68.10 68.50 69.80
6.4 5.8 5.4 4.0 4.0 3.7 3.3 2.0
50 20 17 15 15 15 20 50

C 3.6
49.6 (26)

64.20 64.20 65.20 65.60 66.70 66.80 68.40
7.6 7.6 6.6 6.2 5.1 5.0 3.4
50 20 15 15 15 20 50 C 6.9
31.7

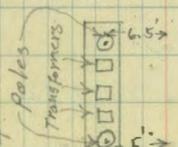
71.80

Nail Tel Pole D-19259-T 46. Lt of Sta 204+35

61.34 61.94 61.84 62.24 62.34 64.24 64.74 65.44 65.84 67.84
C 2.7 5.3 4.7 4.8 4.4 4.3 2.4 1.9 1.2 0.8 + 1.2 C 7.1
21.49 50 47 39 20 15 7 15 20 50 31.8
(22)

C 2.5
40.474
50 46 44 20 15 12 7 5 3.0 2.6 2.0 1.0
(18)

59.24 59.94 60.34 60.54 60.44 59.94 60.94 62.44 63.64 63.84 64.04 65.64
66.64



Sta	+ H.I.	- Elev
B.M.	8.51 72.89	64.38
205	$\frac{1}{2} s = 0.1$	62.0 C5.8
+50	$\frac{1}{2} s = 0.2$	63.0 C5.3
206	$\frac{1}{2} s = 0.2$	63.94 C3.6
+50	$\frac{1}{2} s = 0.2$	64.7 C2.3
71 + 50	county $\frac{1}{2} s = 0.2$	65.2 C0.6
71		65.7 65.9
70 + 50		66.1

$\frac{1219}{7}$

Lt.	L	RT
$\frac{C41}{57.2} (27)$	27.8 5.1	$\frac{C27}{49.8} (23)$
$\frac{C33}{50.5} (27)$	68.3 46	$\frac{E7.6}{49.6} (23)$
$\frac{C1.8}{49.2} (27)$	67.5 54	$\frac{C6.5}{50.4} (25)$
$\frac{Gr}{47.4} (27)$	67.0 59	$\frac{C4.6}{49.0} (26)$
$\frac{F1.2}{38.3} (20)$	65.8 7.1	$\frac{C2.6}{26.4} (4)$
$\frac{C0.7}{23.0} (2)$		$\frac{F1.2}{33.3} (12)$

B.M. #17	7.42	64.38
206 + 50	5.0	66.80
	71.80	

{ cross. N. side iron Rim of Water Dept. Man Hole
53.3' ht of Sta 206 + 37

$\frac{64.20}{7.6}$	$\frac{64.90}{6.9}$	$\frac{65.30}{6.5}$	$\frac{66.80}{5.0}$	$\frac{67.80}{4.0}$	$\frac{67.80}{4.0}$	$\frac{70.30}{1.5}$
50	20	15	15	20	20	50.

Moore
 30330N
 30330N
 2-9-37

El. of High Water Marks on
 CAMINO DEL RIO, Flood of Feb. 6, 1937
 Old Town to City Boundary

INDEXED

5+50	10.04	14.29	2.4	13.64
8+50			1.8	14.74
14+50			1.4	14.64
20+50			1.0	15.04
27+50			0.7	15.34
TP. Pole #7900	2.90	22.54		19.64
56+00			1.4	18.14
TP. Pole #7904	4.09	22.75		18.66
66+00			3.0	19.75
TP. Pole #7905	1.80	21.07		19.27
80+00			1.70	19.37
BM #1	5.10	24.17		19.07
87+38	Country DETENTION GATE	2.3		21.87
BM #8	5.20	28.76		23.36
100+70			3.4	25.16
BM #9	3.90	28.83		24.93
112+50			3.3	25.53

Indexed

c.s.k.

57

TP. Pole #8950	5.00	33.47		28.47
181+50			4.50	28.97
TP. Pole #8994-A	4.30	35.77		31.47
151+00			3.80	31.97
BM #13	3.10	40.27		27.87
162+00			5.00	34.87
TP. Pole #8999-A	4.80	40.47		35.67
170+00			5.0	35.41
El. Pole #79128	3.40	45.07		41.40
185+50			5.00	39.43
BM #15				42.10
#8935	3.50	45.60		42.10
191+00			6.10	39.50

2-7-36

Culvert Profiles #16
Station 126+90
on Radial Lin-

58

100' Lt.	6.7	25.9
70' Lt.	6.0	26.6
35' Lt.	6.0	26.6
31' Lt.	4.9	27.7
13' Lt.	5.7	26.9
7' Lt.	6.7	25.9
φ	5.8	26.8
16' Rt.	4.2	28.4
35' Rt.	3.9	28.7
40' Rt.	4.6	28.0
60' Rt.	5.1	27.5
100' Rt. of φ	3.8	28.8

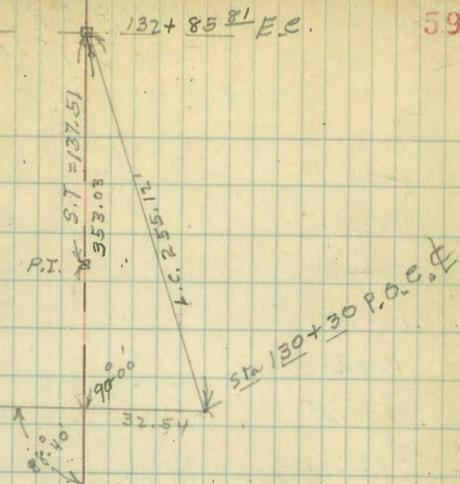
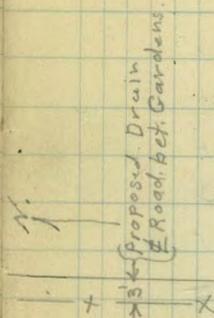
B.M. 10	4.68	32.58
---------	------	-------

27.90

Gullvert Profiles #17
Sta 130+30i

13+00			5.8	26.5
12+70			6.3	26.0
12+30			6.8	25.5
12+00			7.8	24.5
11+50			8.0	24.3
11+25			7.0	25.0
11+00			5.1	27.2
F.P.	6.0	32.3	5.50	26.30
10+00			5.5	26.3
9+00			5.4	26.4
8+00			5.2	26.6
7+00			5.2	26.6
6+00			4.8	27.0
5+00			5.0	26.8
T.P.	4.80	31.80	4.80	27.00
400' Lt.			4.4	27.0
300' Lt.			4.9	26.9
200' Lt.			5.4	26.4
100' Lt.			5.2	26.6
50' Lt.			5.1	26.7
8' Lt.			4.6	27.2
£			5.5	26.3
50' Rt.			5.4	26.4
100' Rt. of £			5.2	26.6
B.M. Nail Pole	3.33	31.80	28.47	

Page 36



17+20 bottom sand Pit.	11.2	19.9	S. of River
17+00	7.6	23.5	
16+85	4.6	26.5	
16+00	5.3	25.8	
15+00	4.9	26.7	
14+00	4.1	27.0	
T.P.	4.60	31.10	5.80 26.50
		32.30	

Sta 140 + 30. ϕ v #19
 289-58' from E, to N, from ϕ
 Line 4.2, and Parallel to Fence.

1400' Lt			6.1	28.1	
1330' Lt			5.0	27.2	
1300' Lt			5.1	27.1	
12400' Lt			4.9	27.3	
1100' Lt			4.7	27.5	
1000' Lt			4.7	29.5	
900' Lt			4.5	29.7	
800' Lt			4.7	27.5	
700' Lt			5.0	27.2	
T.P.	5.20	34.20	4.46		29.00
600' Lt			4.4	29.0	
500' Lt			4.0	27.4	
400' Lt			4.2	27.2	
300' Lt			4.2	27.2	
200' Lt			4.4	27.0	
100' Lt			4.8	28.6	
25' Lt of ϕ			5.2	28.2	
ϕ			5.4	28.0	
15' Rt of ϕ			6.0	27.4	
25' Rt			5.3	28.1	
50' Rt			6.0	27.4	
100' Rt			5.5	27.9	
BM. #11	3.67	33.40		29.73	

60

1800' Lt	In River	11.7	27.2	
1755' Lt	S. Side River	11.3	27.6	
1747' Lt	S. Bank River	9.5	24.4	
1700' Lt		6.0	27.9	
1685' Lt		5.0	28.9	
1650' Lt		4.8	29.1	
T.P.	6.50	33.90	5.80	27.40
1600' Lt		5.8	27.4	
1540' Lt		5.5	27.7	
1517' Lt		7.5	25.7	
1500' Lt		7.5	25.7	
1490' Lt		9.7	23.5	
7' to W. of 1475' Lt		11.0	24.2	in sump. Not a channel
1475' Lt		7.6	25.6	
1452' Lt		7.0	26.2	
T.P.	5.60	33.20	6.60	27.60
1448' Lt		6.6	27.6	
				34.20

Sta 153+50 ϕ #21
 5.50' E. of S.E. cor P.L. 1107
 \angle 89°-58' E. to N. from ϕ
 Parallel to Puerto Lin.

61

T.P. 4.50 33.50 6.10 29.00

1500 Lt 5.0 30.1

1400 Lt 3.7 31.4

1300 Lt 4.7 30.4

1200 Lt 3.6 31.5

1100 Lt 3.5 31.6

1000 Lt 3.0 32.1

T.P. 2.80 35.10 3.50 32.30

900 Lt 3.5 32.3

800 Lt 3.2 32.6

700 Lt 3.1 32.7

600 Lt 3.5 32.3

500 Lt 3.5 32.3

400 Lt 4.1 31.7

300 Lt 5.0 30.8

200 Lt 5.9 29.9

150 Lt 5.8 30.0

100 Lt 4.5 31.3

25 Lt of ϕ 4.5 31.3

ϕ 4.8 31.0

15 Rt 4.8 31.0

25 Rt 4.3 31.5

100 Rt of ϕ 4.6 31.2

B.M. #12 4.42 35.80 31.38

1900 Lt 7.0 26.5

1885 Lt 9.5 24.0

1822 Lt S. Edge Channel 9.7 23.8

1812 Lt 7.2 26.3

1800 Lt 7.2 26.3

1706 Lt 7.0 26.5

1615 Lt 7.2 26.3

1611 Lt 4.3 29.2

1600 Lt 4.5 29.0

33.50

Sta 162 + 41. ✓ 622
 Sta 162 + 39 P.Q.E.
 culvert. Profile E. 2.
 of Fence. + Parallel to it,
 at Rt. Ls to S. line of Pueblo Lot 1108.

1000 Lt		5.0	32.8	
935 Lt		5.3	32.5	
920 Lt		6.3	31.5	
900 Lt		6.2	31.6	
800 Lt		4.6	33.2	
700 Lt		4.8	33.0	
600 Lt		4.4	33.4	
T.P.	4.8	37.8	4.96	33.00
500 Lt		5.0	33.0	
437 Lt		4.7	32.3	
420 Lt		6.0	32.0	
400 Lt		5.7	32.3	
300 Lt		5.0	33.0	
200 Lt		5.2	32.8	
100 Lt		7.2	30.8	
38 Lt		7.9	30.1	
11 Lt of ♀		5.2	32.8	
♀		4.9	33.1	
18 Rt		4.9	33.1	
25 Rt		3.7	34.3	
45 Rt		4.5	33.5	
100 Rt of ♀		4.8	33.2	
B.M. #13	0.59	37.96		37.37

1175	S. side River	10.0	27.8
1162	S. Bank "	5.3	32.5
1100		5.3	32.5
1087		6.3	31.5

37.8

Sta 180 + 37.14
Box Culvert - 2.9 sec #4

51.43
43.67
- 7.76

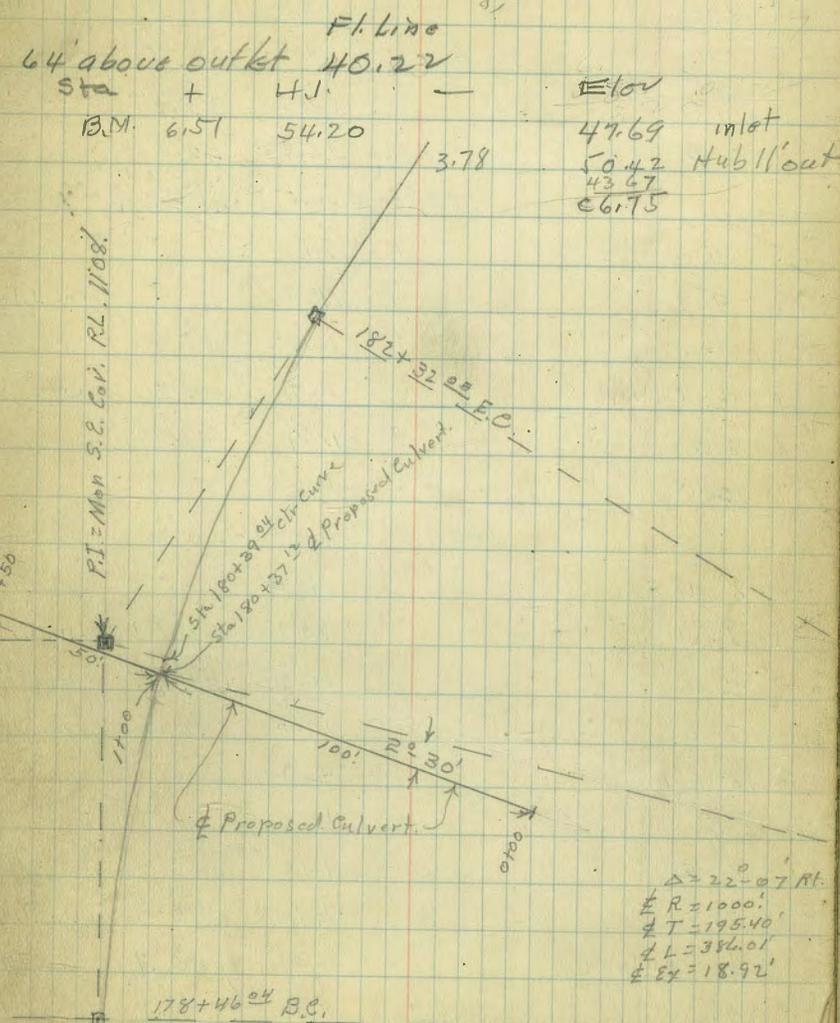
Station	Dist	Elev	Notes
B.M. 14	3.64	53.33	
Intak			
outlet	1.90	51.43	Fl. Grader
11. E	10.22	43.11	37.5
9. E	6.0	46.0	
♀ Culvert	8.1	43.9	in. Ditch
9. W	8.7	43.3	
10. W	8.0	44.0	" "
	4.0	48.0	E. Line Sand Rock Road
13. W	4.0	48.0	E. Line Sand Rock Road
10. W	6.9	45.1	in. ditch
♀ Culvert	7.5	44.5	" "
6. E	7.3	44.7	" "
10. E	4.2	47.8	" "
12. W	2.0	50.0	E. Line Sand Rock Road
10. W	5.1	46.9	in. ditch
♀ Culvert	5.1	46.9	" "
4. E	6.0	46.0	" "
9. E	2.5	49.5	" "

0+45

0+25

100' Rt. of ♀ = 0+00

B.M. #14 4.30 51.99 47.69



Δ = 222.07 Rt.
R = 1000'
T = 195.40'
L = 386.01'
Sx = 18.92'

Station 180+39 ^L
 Culvert levels

64

20' W	9.6	44.4	
11' W	13.3	38.7	1 st Ditch
	13.5	38.5	" "
7' E	13.9	38.1	" "
8' E	11.7	40.3	" "

1+50 = X line R. of W.

11' E	9.1		
9' E	10.9		1 st Ditch
	10.8	41.2	" "
4' Culvert	11.7	40.3	" "
8' W	10.9	41.1	" "
12' W	5.6	40.4	" "

1+00 = 4' R. of W.

8' W	4.2		
7' W	10.1	41.9	1 st Ditch
4'	10.3	41.7	" "
7' E	10.5	41.5	" "
8' E	4.2		" "

0+84

8' E	4.0		
7' E	7.7	44.3	1 st Ditch
4' culvert	8.3	43.7	" "
7' W	8.7	43.3	" "
8' W	9.0	48.0	E. Line Sand Rock Road

0+52

51.99

Culvert Profile #28
Sta. 206+32.85 ✓

4+00	5.6	63.6
3+75 Δ	4.1	65.1
3+41	3.5	65.7
3+40	2.5	66.7
3+26 = N side Barn	1.7	67.5
T.P. 1.59	49.21 ✓	12.57
2+91 S. side Barn	10.2	70.0
2+50	8.3	71.9
2+00	4.4	75.8
T.P. 0.13	80.19 ✓	12.86
1+50	12.7	80.7
1+00	9.5	83.4
0+50	6.0	86.9
0+12 E. Bank of wash	3.0	89.9
0+00 in wash	4.7	89.7

Proposed Culvert

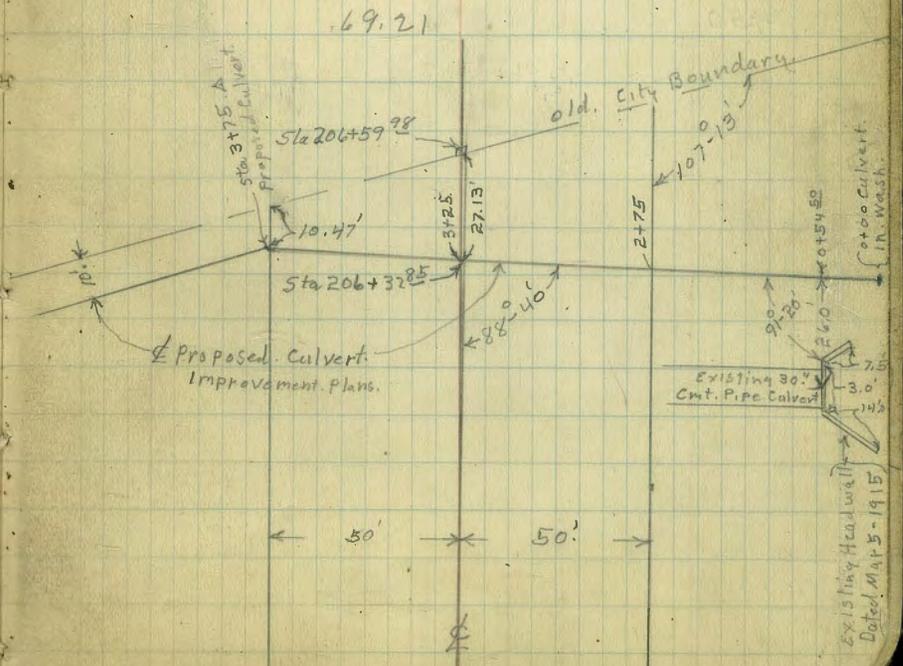
Inlet Existing 30" Culvert	26.0' W. of Sta. 206+54.50	10.50	87.4	F.L. Pipe
Top Head wall over pipe		6.50	86.4	
Top S.W. End Wing wall		5.15	87.7	
W S.W. " " "		4.00	86.9	

Existing Culvert

T.P.	10.13	92.92 ✓	0.72	82.79
T.R.	12.20	83.51	1.14	71.31
B.M. #17	8.07	72.45		64.38

BM #11			3.07	64.38
T.P. 11.10	47.45	0.19		56.35
T.R. 12.86	56.54	2.83		43.68
7+46 In River		11.0		35.5
7+15 S. Bank of River		6.1		40.4
T.P. 2.83	46.51 ✓	12.87		43.68
6+50		13.8		49.8
22 Ft. of 6" 20 Outlet Culvert		15.40		41.7
16 Ft. of 6" 05 Top 30" Pipe at 2		11.55		45.0
4+05		11.1		45.5
17' To Lt. of 5+82		9.35		47.7
5+82		9.8		46.8
T.P. 0.20	56.55 ✓	12.86		56.35
5+00		13.0		56.7
4+50		8.8		60.4

Pipe Does Not Run Straight from Inlet to Outlet
Floor of Pump House



+50

199

+50

198

+50

197

Camino Del Rio
change in Alignment, from
Sta. 200+44.47

203

~~Abandoned~~

+50

202

201+50.88 E.C. Nail.

+44.47 B.C. Rt Hub.

200

Nail • P.O.T.

$\Delta = 3^{\circ}48'40''$
 $R = 1600'$
 $T = 53.23$
 $L = 106.41$

75.00

Tres to Lot lines in Pueblo Lot. 1113

Indexed
C.S.K.

P.L. 1109.

425.00
425. Map

Fd. old Pipe + 4x4
N.W. Cr P.L. 1113.

N.E. Cor P.L. 1110

104-40-30

463.00

Sta 198+31 1/2

73-55

Lot 8, F.M. 875

Sta. 200+45.4 BC
C=187.0
R=1100
T=90.16
L=170.16

Sta 202+21.2 IC

33.91

Sta 202+55.4

581.50

89-53

405.86
408.69

409. Map.

P.L. 1113.

Flod. Fix.

P.L. 1110

old Ferris on P.L. Line

2.83

Fd. Pipe

20-4-30

803.30
To Mon see
UTR Bank 9-P. 34

68

177.95

165. Map.

4x4 N.E. Cor
P.L. 1113

Fd. old Hub S.W. Cor. City Property
in Lot 32 Rancho Mission S.D.
Replaced with 1 1/2" Pipe Wooden Plug + C.T.

112.60
395.27
507.93

Curve to Join County

105+35 51.8 C.L. Curve to Join County
72+99.6 Curve
from East

404.74

107.18

395.29

112.60

Hub
Camino Del Rio
Sta 206+59.98
Page 20

Mon. on old
City Boundary

Lot 7, F.M. 875.

11.03

573.86

Fdx Top. Capped
2" Pipe County
Rel Survey 514
S. line Windsor
place

133.96

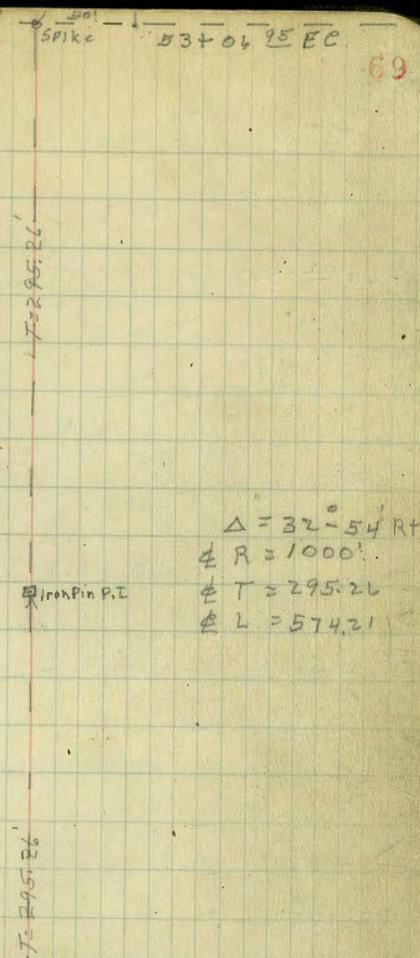
11-14-36

Muller
Walker
Blair

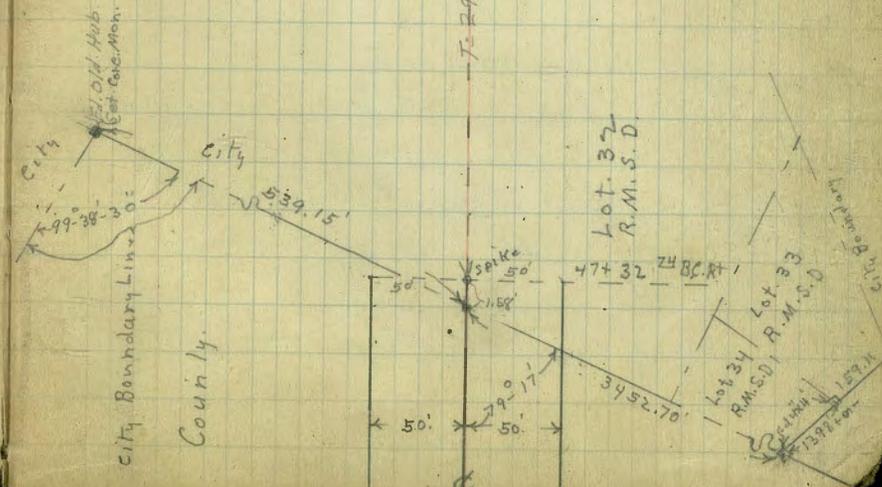
Camino Del Rio New Alignment.
San Diego Road Survey, No 720 Termini Map.
Being a Relocation of Road Survey 514 Det. L.

+50	Fence 5' Lt. of ϕ	14°-49'
52	Fence 1.0 Rt. of ϕ	13°-23.2'
+50	Fence 3.0 Rt. of ϕ	11°-57.3'
51	Fence 4.0 Rt. of ϕ	10°-31.3'
+50	Fence 1.0 Rt. of ϕ	9°-05.4'
50	Fence 1.0 Lt. of ϕ	7°-39.4'
+50	Fence 3.0 Lt. of ϕ	6°-13.5'
49	Fence 7.0 Lt. of ϕ	4°-47.5'
+50	Fence 14' Lt. of ϕ	3°-21.6'
48	old Fence 25' Lt. of ϕ	1°-55.6'
+50	old Fence 39' Lt. of ϕ	
47+3274	BC Rt. old Fence 43' Lt. of ϕ	
47+31	1/16 P.I. & Rd + E. Line Lot 32, R.M.S.D.	

50' Spike 53+06.95 EC 69



$\Delta = 32^{\circ} 54' RT$
 $\phi R = 1000'$
 $\phi T = 295.26$
 $\phi L = 574.21$



Lot 32
R.M.S.D.
 47+32 24 BC Rt.
 Lot 33
R.M.S.D.
 Lot 34
R.M.S.D.
 1897
 1898

57+60⁰² B.C. Lt. Fence 8' Lt. of ϕ
+50 Fence 7' Lt. of ϕ

57 Fence 7' Lt. of ϕ

+50
5760.02
5306.95
453.07

+50 Fence 15' Lt. of ϕ

56 Fence 11' Lt. of ϕ

+50 Fence 15' Lt. of ϕ

55 Fence 16' Lt. of ϕ

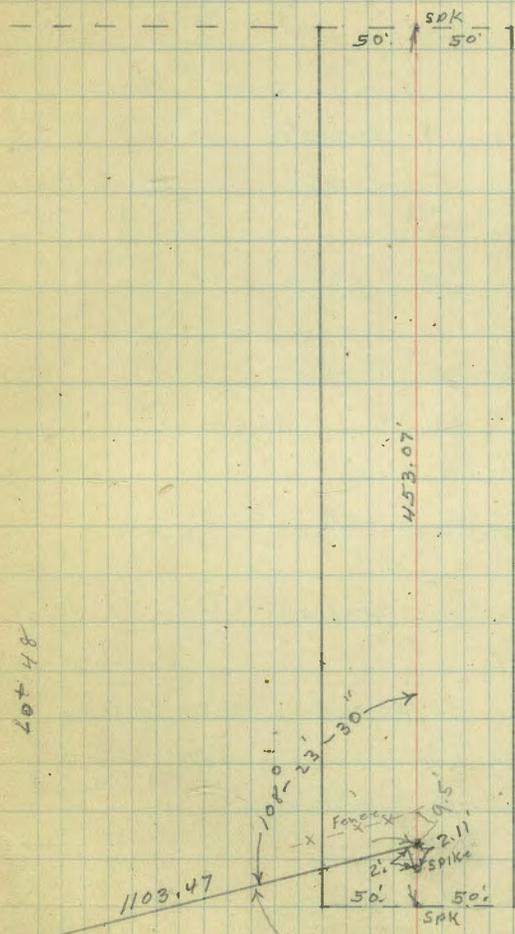
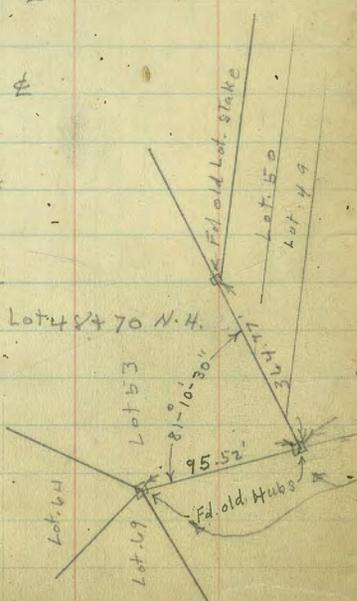
+50 Fence 19.0 Lt. of ϕ

54 Fence 17.0 Lt. of ϕ

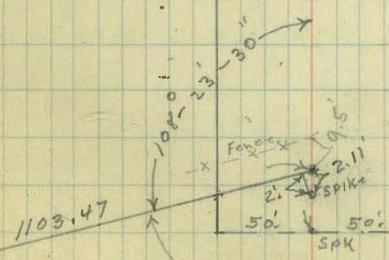
+50 Fence 17.0 Lt. of ϕ

+18.70
+16.52 spike ϕ
53+06⁹⁵ E.C.
P.I. ϕ + Lot Line Bot Lot 4 & 70 N.H.

53 Fence 13.0 Lt. of ϕ



Lot 48



This Line Produced from these Two Hubs

Lot 70

64+00³⁶ E.C.

63. Fence 13' Lt. of ϕ

+50 Fence 14' Lt. of ϕ

62 Fence 16' Lt. of ϕ

61+74⁶³ B.C. RT. Fence 19' Lt. of ϕ

+50 Fence 19' Lt. of ϕ

61 Fence 15' Lt. of ϕ

+50 Fence 11' Lt. of ϕ

60+04²³ E.C. Fence 9' Lt. of ϕ

60

+50 Fence 12' Lt. of ϕ

59 Fence 7' Lt. of ϕ

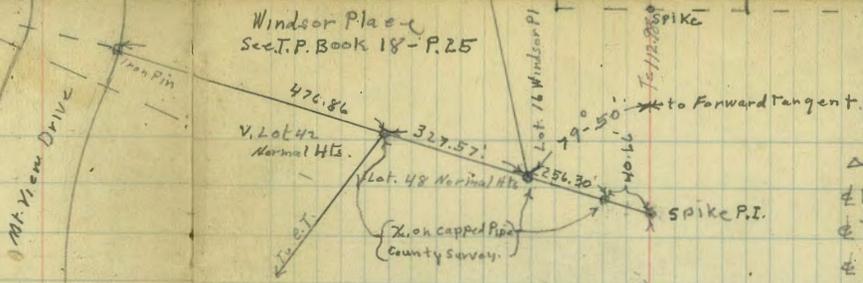
+82.73

+50 Fence 7' Lt. of ϕ

58 Fence 9' Lt. of ϕ

57+60⁰² B.C. Lt.

Windsor Place
See T.P. Book 18-P.25



71

$\Delta = 6-28$
 $\phi R = 2000'$
 $\phi T = 112.98'$
 $\phi L = 225.73'$

50' Spike 50'

170.41'

50' Spike 50'

T = 122.71'

Spike P.I.

To 122.71'

Spike

453.07'

$\Delta = 13-59-30$ Lt

$\phi R = 1000'$
 $\phi T = 122.71'$
 $\phi L = 244.20'$

+7194 Ctr curve Def L 5°-02'

+50 Fence 9' Lt of ϕ = 96+54.70 4-41.9'

69 Fence 14' Lt of ϕ = 96+04.70 3-55.8'

+50 Fence 22' Lt of ϕ = 95+54.70 3-09.7'

68 Fence 19' Lt of ϕ = 95+04.70 2-23.6'

+50 Fence 16' Lt of ϕ = 94+54.7 1-37.5'

67 Fence 15' Lt of ϕ = 94+04.69 0-51.4'

66+44 ²⁸ B.C. Rt. Fence 73' Lt of ϕ = 93+48.21

66 Fence 13' Lt of ϕ

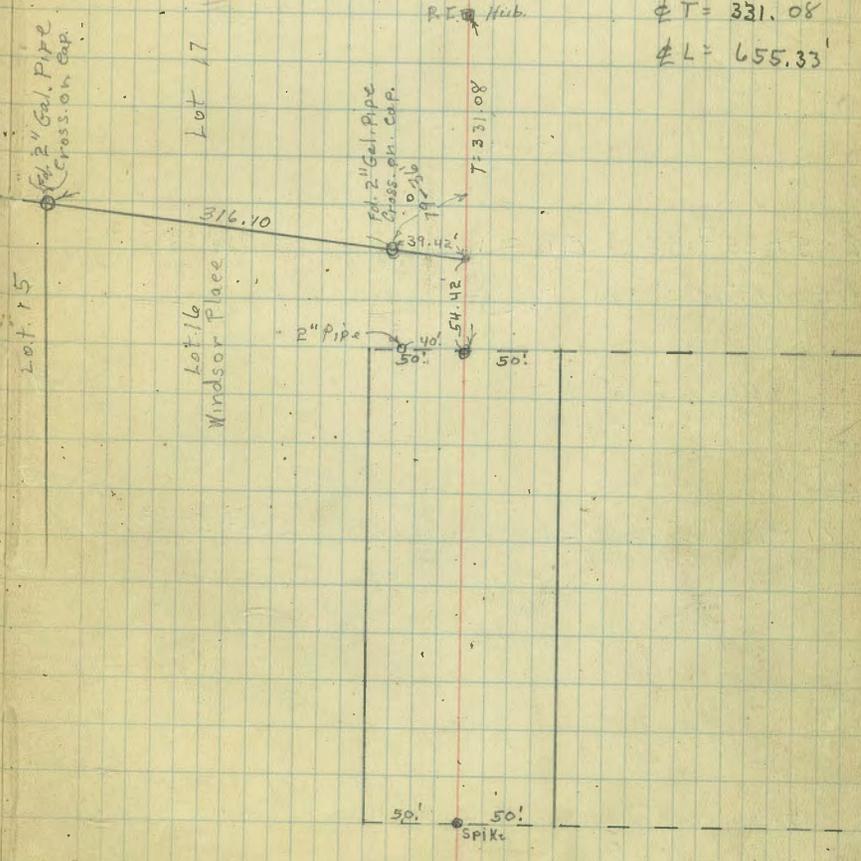
+50 Fence 12' Lt of ϕ

65 Fence 11' Lt of ϕ

+50 Fence 11' Lt of ϕ

64+00 ³¹ E.C. Fence 10' Lt of ϕ

+50 Fence 16' Lt of ϕ

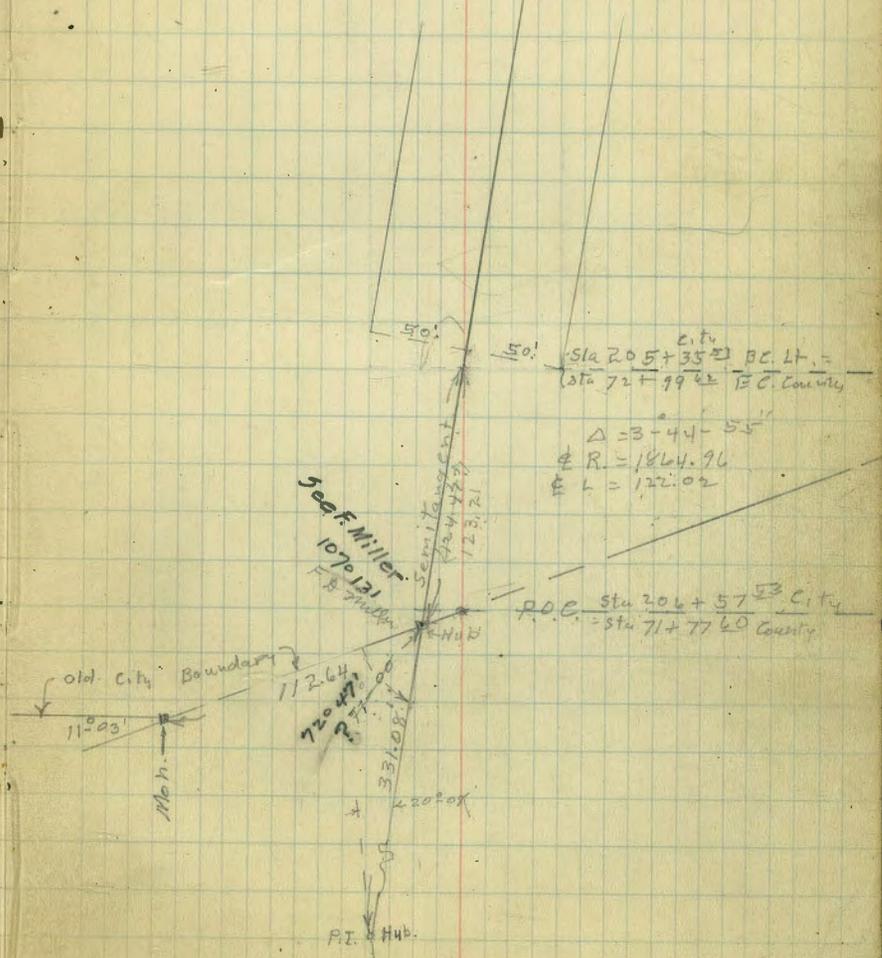


$\Delta 70-08'$
 $\phi R = 1844.96$
 $\phi T = 331.08$
 $\phi L = 655.33$

331.08
 122.5
 206.5

Additional Ties FB 1588 = Ties Monuments set.
 County Road Survey
 FB 727-9
 from old town

	Def L
205+35 ⁵¹ B.C. Lt. City } 72+99 ⁴² EC = County }	10-04
+50	9-18.7
72	8-32.8
71+77 ⁴⁰ Roc. Old City Boundary. County = 206+57 ⁵³ City	7-46.2
+50	
71	7-00
+50	6-14
+48 W end Fence 14' Lt of dc = 97+46.70	
70 Fence 6' Lt of dc = 97+04.70	5-29



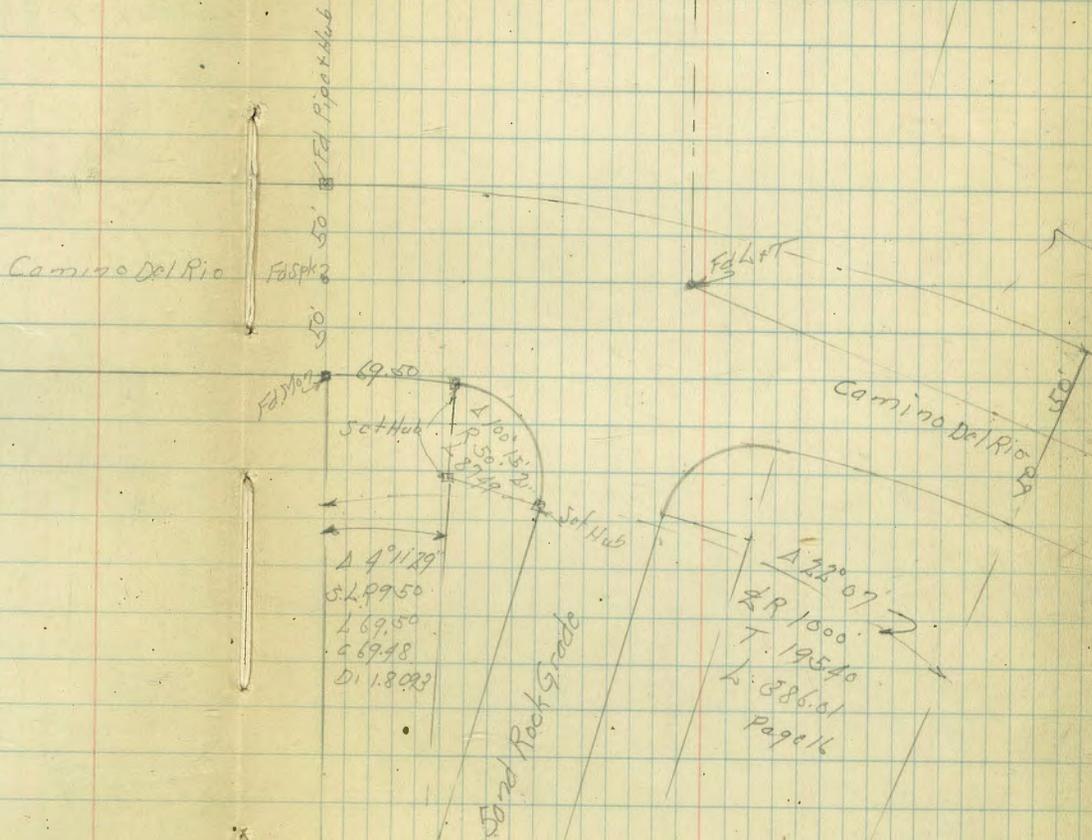
50' Sta 205+35⁵¹ B.C. Lt. =
 Sta 72+99⁴² EC County
 $\Delta = 3-44-55''$
 $\phi R = 1864.96$
 $E L = 122.02$

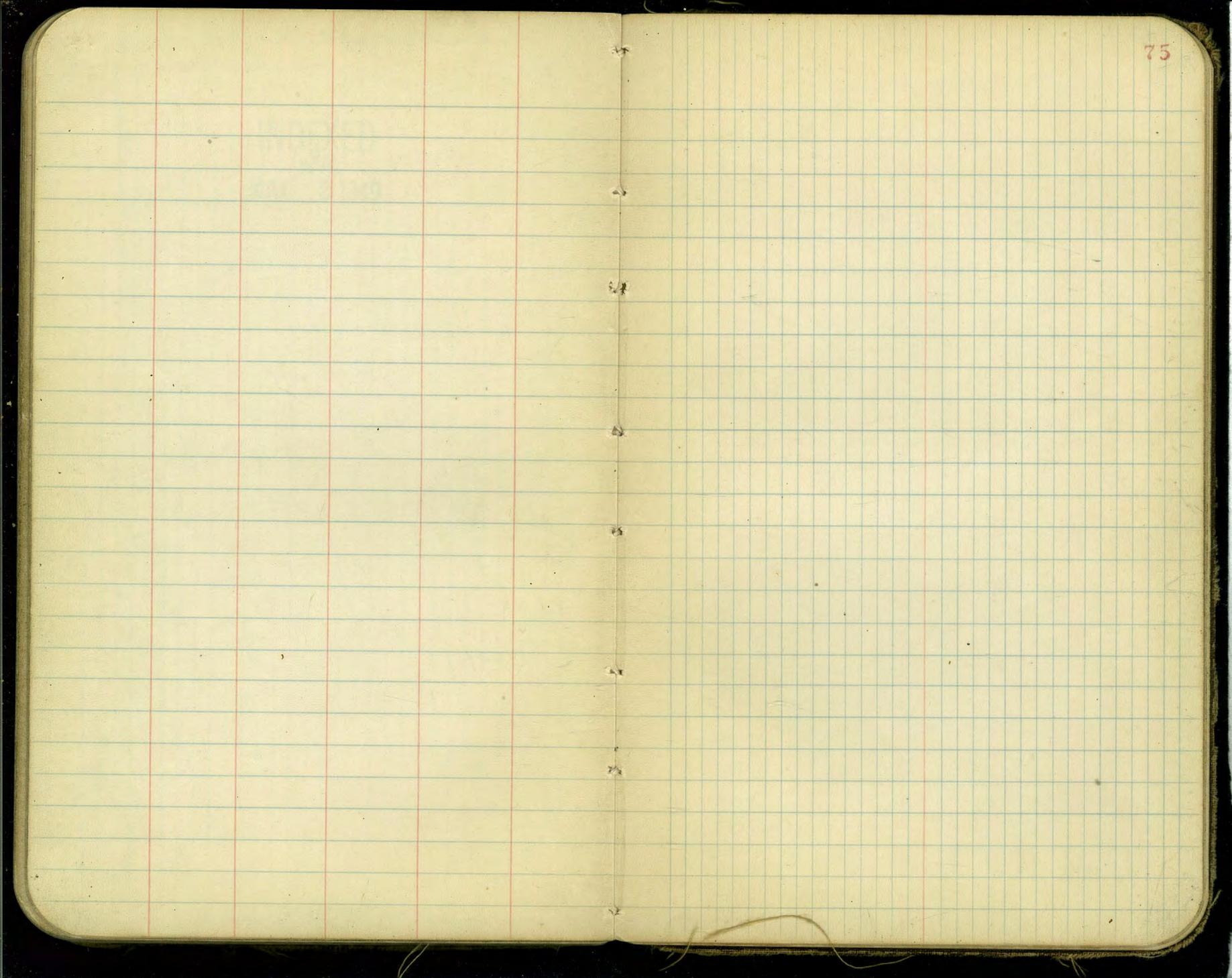
R.O.C. Sta 206+57⁵³ City
 = Sta 71+77⁴⁰ County

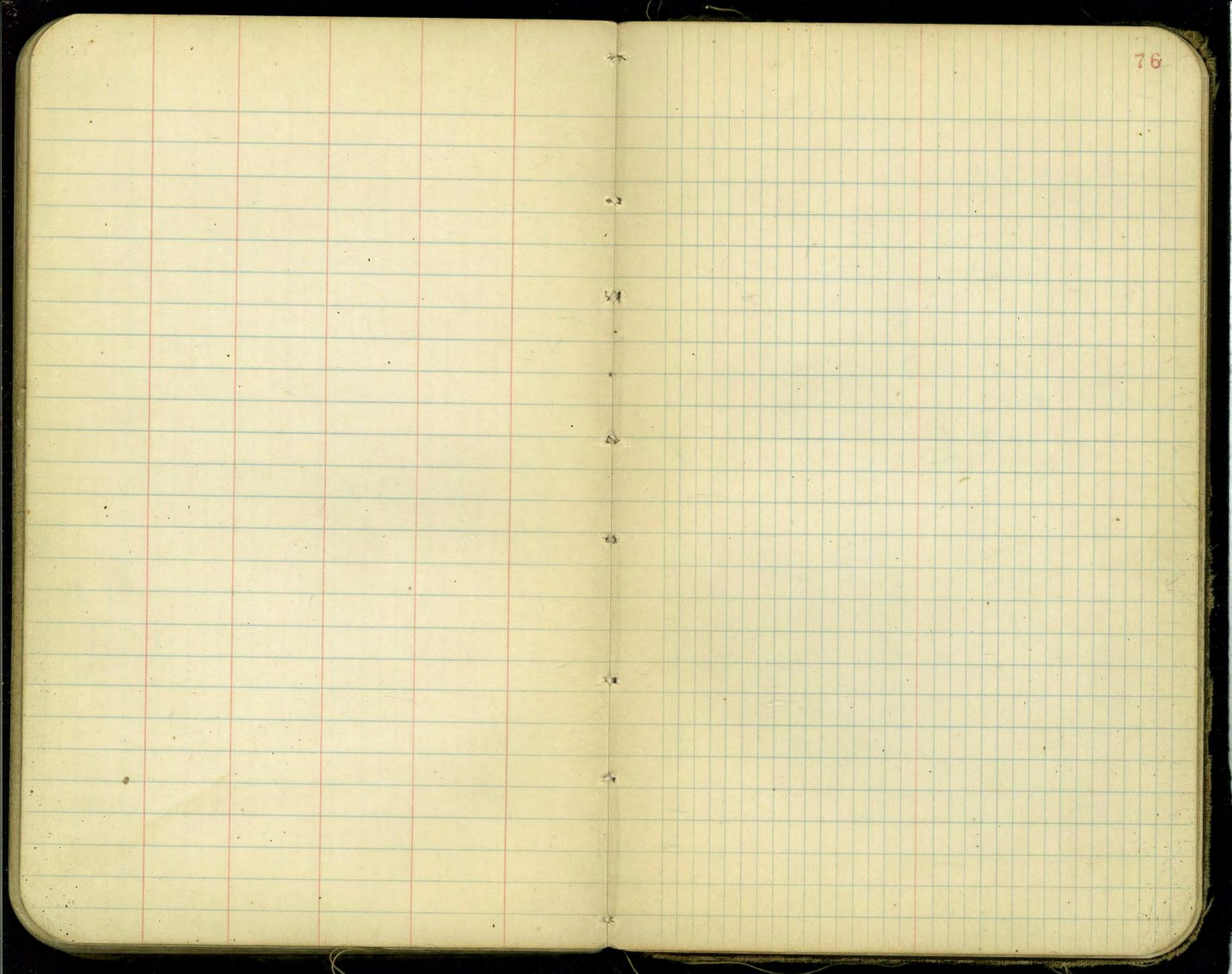
Camino Del Rio + Sand Rock Grade
 South West Corner

INDEXED
 WK
 MAY 2 1949

April 25 49 74
 A. Sisson
 D. Smith
 W. Berger
 No. 60135



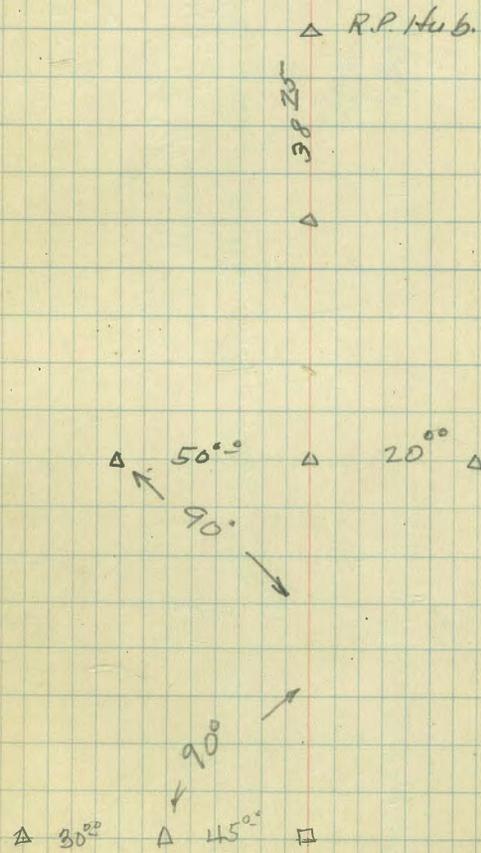




2+88⁰⁰ End

2+50

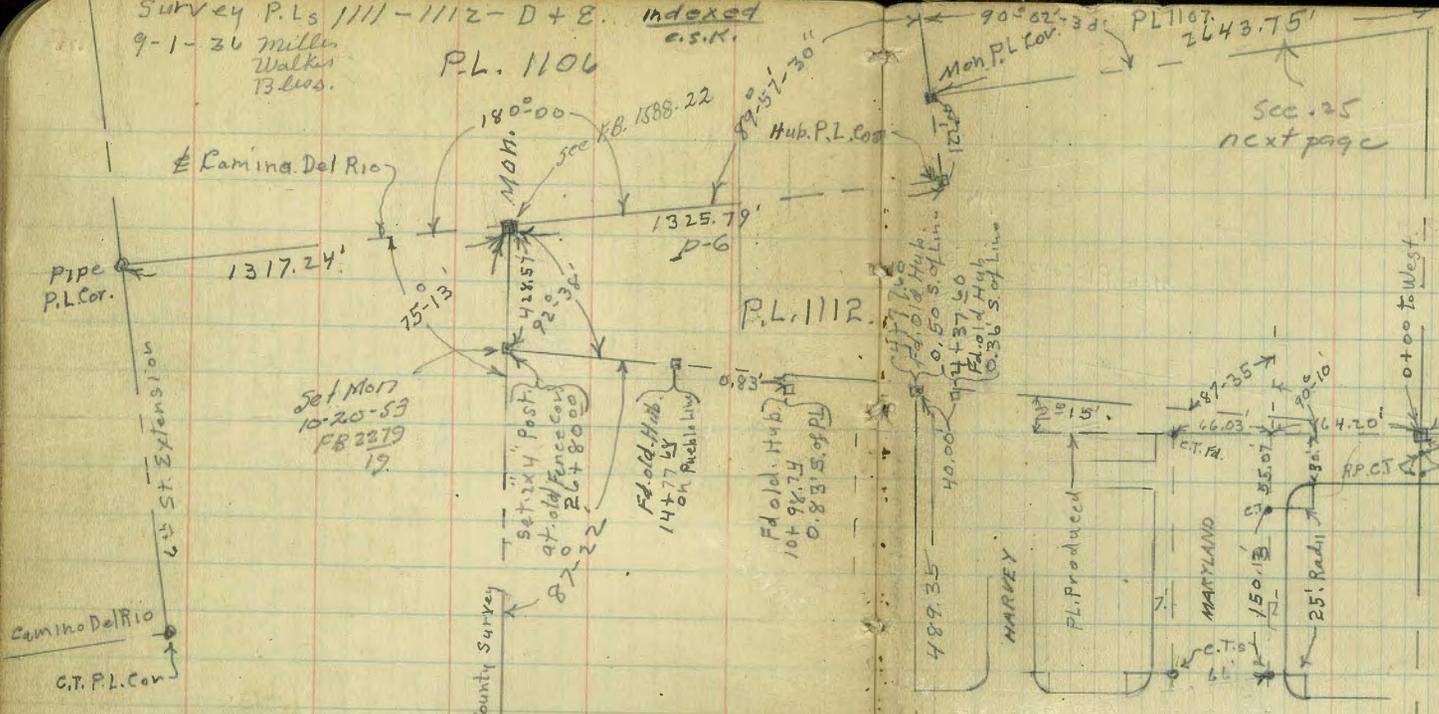
0+50



Survey P.Ls 1111-1112-D+E. Indexed
 9-1-36 Miller
 Walker
 13 Lvs.

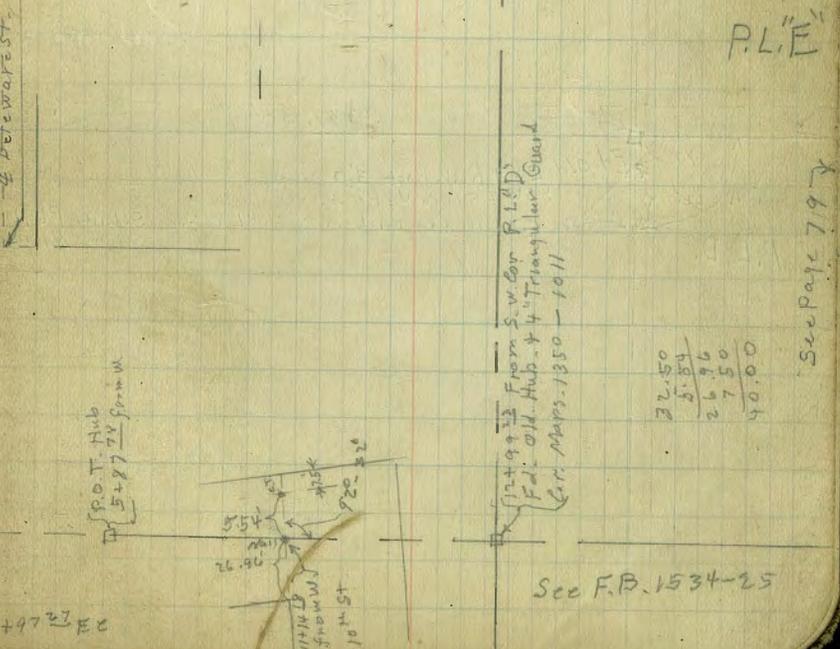
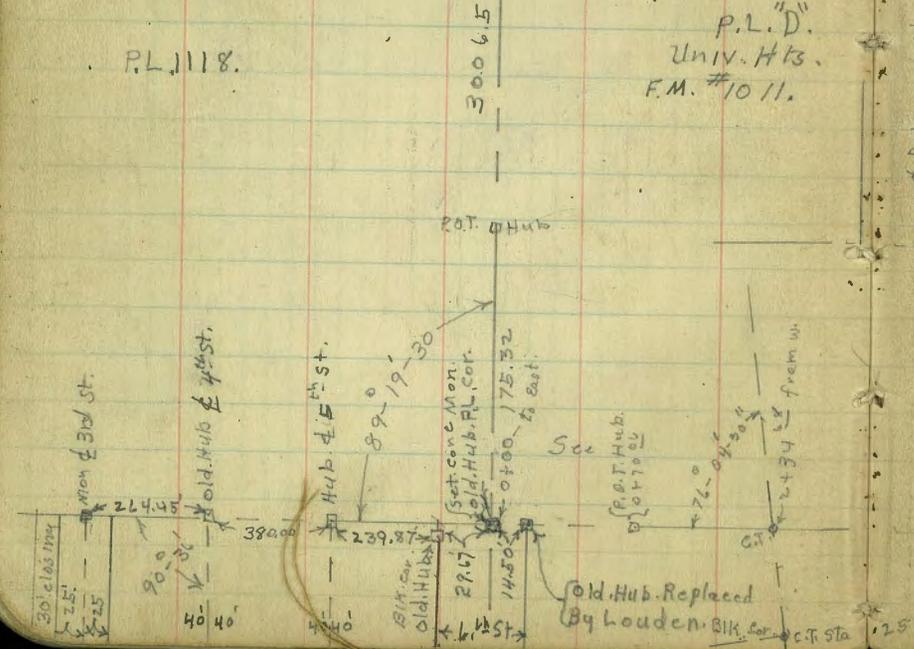
P.L. 1106

Indexed
 e.s.k.



See 25
 next page

P.L. 1111,
 This Post checks P.L.
 Cor. F.M. 1565
 + F.M. 1565.
 2'x4' page 79



32.50
5.84
26.66
7.50
40.00

See F.B. 1534-25

See Page 79

PL 1107

SEC. 75 previous page

Mons. P.L. Cors

279.86

To Mon S.W. cor PL 1107
121
2643.25

PL 1112

S.W. cor PL 1111

587.00'

274.80'

90° 00' 42"
22.0'
F. 0.01 2x3 R.W. Post 3'0" Deep
Set 2x4 R.W. Post over

P.L. D.

Set C.T.s in N.W. curbs. R.P.s to P.L. Cor
S. Line PL 1111
S. " Adams

PL 1108.

79

PL 1111

Mon N.W. cor

Mon S.W. Cor

St. Line of Adams

85.93' 313.83' 5.96' 313.91' 66.00' 323.90' 45.96' 324.17'

North Ave.

Park Blvd

Georgia St

S. Line Adams Ave

Florida St

Alabama St

P.L. E.

See Page 78

See Page 78

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1 1/2 to 1.
If ground is nearly level, the cut or fill at side
stake is located by the double entry method in
left column and top row. The number in body

IMPROVED TABLES
AND
INFORMATION

To find Tangent and Elevation for curve of
any other degree, divide by degree of curve and
add constant found in column of constants.
Degree of curve with a given T may be found
by dividing tangent for constant degree by
given tangent for constant.
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

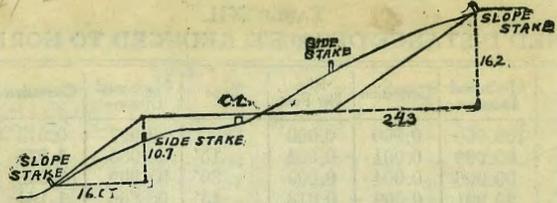
I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10'	58.34	.297	5° C.	10'	560.11	27.313	5° C.	10'	1070.6	99.155	5° C.
20'	66.67	.388	T	20'	568.53	28.137	T	20'	1079.2	100.75	T
30'	75.01	.491	.03	30'	576.95	28.974	.06	30'	1087.8	102.35	.10
40'	83.34	.606	E	40'	585.36	29.824	E	40'	1096.4	103.97	.13
50'	91.68	.733	.001	50'	593.79	30.686	.006	50'	1105.1	105.60	.013
2°	100.01	.873	10° C.	12°	602.21	31.561	10° C.	22°	1113.7	107.24	10° C.
10'	108.35	1.024	T	10'	610.64	32.447	T	10'	1122.4	108.90	T
20'	116.68	1.188	.06	20'	619.07	33.347	.13	20'	1131.0	110.57	.19
30'	125.02	1.364	E	30'	627.50	34.259	E	30'	1139.7	112.25	.26
40'	133.36	1.552	.003	40'	635.93	35.183	.011	40'	1148.4	113.95	.34
50'	141.70	1.752	T	50'	644.37	36.120	T	50'	1157.0	115.66	.42
3°	150.04	1.964	15° C.	13°	652.81	37.070	15° C.	23°	1165.7	117.38	15° C.
10'	158.38	2.188	T	10'	661.25	38.031	T	10'	1174.4	119.12	T
20'	166.72	2.425	.06	20'	669.70	39.006	.13	20'	1183.1	120.87	.19
30'	175.06	2.674	E	30'	678.15	39.993	E	30'	1191.8	122.63	.26
40'	183.40	2.934	.003	40'	686.60	40.992	.011	40'	1200.5	124.41	.34
50'	191.74	3.207	T	50'	695.06	42.004	T	50'	1209.2	126.20	.42
4°	200.08	3.492	20° C.	14°	703.51	43.029	20° C.	24°	1217.9	128.00	20° C.
10'	208.43	3.790	T	10'	711.97	44.066	T	10'	1226.6	129.82	T
20'	216.77	4.099	.06	20'	720.44	45.116	.13	20'	1235.3	131.65	.19
30'	225.12	4.421	E	30'	728.90	46.178	E	30'	1244.0	133.50	.26
40'	233.47	4.755	.003	40'	737.37	47.253	.011	40'	1252.8	135.35	.34
50'	241.81	5.100	T	50'	745.85	48.341	T	50'	1261.5	137.23	.42
5°	250.16	5.459	15° C.	15°	754.32	49.441	15° C.	25°	1270.2	139.11	15° C.
10'	258.51	5.829	T	10'	762.80	50.554	T	10'	1279.0	141.01	T
20'	266.86	6.211	.06	20'	771.29	51.679	.13	20'	1287.7	142.93	.19
30'	275.21	6.606	E	30'	779.77	52.818	E	30'	1296.5	144.85	.26
40'	283.57	7.013	.003	40'	788.26	53.969	.011	40'	1305.3	146.79	.34
50'	291.92	7.432	T	50'	796.75	55.132	T	50'	1314.0	148.75	.42
6°	300.28	7.863	20° C.	16°	805.25	56.309	20° C.	26°	1322.8	150.71	20° C.
10'	308.64	8.307	T	10'	813.75	57.498	T	10'	1331.6	152.69	T
20'	316.99	8.762	.06	20'	822.25	58.699	.13	20'	1340.4	154.69	.19
30'	325.35	9.230	E	30'	830.76	59.914	E	30'	1349.2	156.70	.26
40'	333.71	9.710	.003	40'	839.27	61.141	.011	40'	1358.0	158.72	.34
50'	342.08	10.202	T	50'	847.78	62.381	T	50'	1366.8	160.76	.42
7°	350.44	10.707	15° C.	17°	856.30	63.634	15° C.	27°	1375.6	162.81	15° C.
10'	358.81	11.224	T	10'	864.82	64.900	T	10'	1384.4	164.86	T
20'	367.17	11.753	.06	20'	873.35	66.178	.13	20'	1393.2	166.95	.19
30'	375.54	12.294	E	30'	881.88	67.470	E	30'	1402.0	169.04	.26
40'	383.91	12.847	.003	40'	890.41	68.774	.011	40'	1410.9	171.15	.34
50'	392.28	13.413	T	50'	898.95	70.091	T	50'	1419.7	173.27	.42
8°	400.66	13.991	20° C.	18°	907.49	71.421	20° C.	28°	1428.6	175.41	20° C.
10'	409.03	14.582	T	10'	916.03	72.764	T	10'	1437.4	177.55	T
20'	417.41	15.184	.06	20'	924.58	74.119	.13	20'	1446.3	179.72	.19
30'	425.79	15.799	E	30'	933.13	75.488	E	30'	1455.1	181.89	.26
40'	434.17	16.426	.003	40'	941.69	76.869	.011	40'	1464.0	184.08	.34
50'	442.55	17.065	T	50'	950.25	78.264	T	50'	1472.9	186.29	.42
9°	450.93	17.717	15° C.	19°	958.81	79.671	15° C.	29°	1481.8	188.51	15° C.
10'	459.32	18.381	T	10'	967.38	81.092	T	10'	1490.7	190.74	T
20'	467.71	19.058	.06	20'	975.96	82.525	.13	20'	1499.6	192.99	.19
30'	476.10	19.746	E	30'	984.53	83.972	E	30'	1508.5	195.25	.26
40'	484.49	20.447	.003	40'	993.12	85.431	.011	40'	1517.4	197.53	.34
50'	492.88	21.161	T	50'	1001.7	86.904	T	50'	1526.3	199.82	.42
10°	501.28	21.887	20° C.	20°	1010.3	88.389	20° C.	30°	1535.3	202.12	20° C.
10'	509.68	22.624	T	10'	1018.9	89.888	T	10'	1544.2	204.44	T
20'	518.08	23.375	.06	20'	1027.5	91.399	.13	20'	1553.1	206.77	.19
30'	526.48	24.138	E	30'	1036.1	92.924	E	30'	1562.1	209.12	.26
40'	534.89	24.913	.003	40'	1044.7	94.462	.011	40'	1571.0	211.48	.34
50'	543.29	25.700	T	50'	1053.3	96.013	T	50'	1580.0	213.86	.42

T = R tan ½ I E = R exsec ½ I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10'	1598.0	218.7	5° C.	10'	2151.7	390.7	5° C.	10'	2743.1	622.8	5° C.
20'	1606.9	221.1	T	20'	2161.2	394.1	T	20'	2753.4	627.2	T
30'	1615.9	223.5	.13	30'	2170.8	397.4	.17	30'	2763.7	631.7	.21
40'	1624.9	226.0	E	40'	2180.3	400.8	E	40'	2773.9	636.2	E
50'	1633.9	228.4	.023	50'	2189.9	404.2	.037	50'	2784.2	640.7	.056
32°	1643.0	230.9	10° C.	42°	2199.4	407.6	10° C.	52°	2794.0	645.2	10° C.
10'	1652.0	233.4	T	10'	2209.0	411.1	T	10'	2804.9	649.7	T
20'	1661.0	235.9	.06	20'	2218.6	414.5	.10	20'	2815.2	654.3	.14
30'	1670.0	238.4	E	30'	2228.1	418.0	E	30'	2825.6	658.8	E
40'	1679.1	241.0	.013	40'	2237.7	421.4	.017	40'	2835.9	663.4	.021
50'	1688.1	243.5	T	50'	2247.3	425.0	T	50'	2846.3	668.0	T
33°	1697.2	246.1	10° C.	43°	2257.0	428.5	10° C.	53°	2856.7	672.7	10° C.
10'	1706.3	248.7	T	10'	2266.6	432.0	T	10'	2867.1	677.3	T
20'	1715.3	251.3	.06	20'	2276.2	435.6	.10	20'	2877.5	682.0	.14
30'	1724.4	253.9	E	30'	2285.9	439.2	E	30'	2888.0	686.7	E
40'	1733.5	256.5	.013	40'	2295.6	442.8	.017	40'	2898.4	691.4	.017
50'	1742.6	259.1	T	50'	2305.2	446.4	T	50'	2908.9	696.1	T
34°	1751.7	261.8	15° C.	44°	2314.9	450.0	15° C.	54°	2919.4	700.9	15° C.
10'	1760.8	264.5	T	10'	2324.6	453.6	T	10'	2929.9	705.7	T
20'	1770.0	267.2	.06	20'	2334.3	457.3	.10	20'	2940.4	710.5	.14
30'	1779.1	269.9	E	30'	2344.1	461.0	E	30'	2951.0	715.3	E
40'	1788.2	272.6	.013	40'	2353.8	464.6	.017	40'	2961.5	720.1	.017
50'	1797.4	275.3	T	50'	2363.5	468.4	T	50'	2972.1	725.0	T
35°	1806.6	278.1	10° C.	45°	2373.3	472.1	10° C.	55°	2982.7	729.9	10° C.
10'	1815.7	280.8	T	10'	2383.1	475.8	T	10'	2993.3	734.8	T
20'	1824.9	283.6	.06	20'	2392.8	479.6	.10	20'	3003.9	739.7	.14
30'	1834.1	286.4	E	30'	2402.6	483.4	E	30'	3014.5	744.6	E
40'	1843.3	289.2	.013	40'	2412.4	487.2	.017	40'	3025.2	749.6	.017
50'	1852.5	292.0	T	50'	2422.3	491.0	T	50'	3035.8	754.6	T
36°	1861.7	294.9	15° C.	46°	2432.1	494.8	15° C.	56°	3046.5	759.6	15° C.
10'	1870.9	297.7	T	10'	2441.9	498.7	T	10'	3057.2	764.6	T
20'	1880.1	300.6	.06	20'	2451.8	502.5	.10	20'	3067.9	769.7	.14
30'	1889.4	303.5	E	30'	2461.7	506.4	E	30'	3078.7	774.7	E
40'	1898.6	306.4	.013	40'	2471.5	510.3	.017	40'	3089.4	779.8	.017
50'	1907.9	309.3	T	50'	2481.4	514.3	T	50'	3100.2	784.9	T
37°	1917.1	312.2	10° C.	47°	2491.3	518.2	10° C.	57°	3110.9	790.1	10° C.
10'	1926.4	315.2	T	10'	2501.2	522.2	T	10'	3121.7	795.2	T
20'	1935.7	318.1	.06	20'	2511.2	526.1	.10	20'	3132.6	800.4	.14
30'	1945.0	321.1	E	30'	2521.1	530.1	E	30'	3143.4	805.6	E
40'	1954.3	324.1	.013	40'	2531.1	534.2	.017	40'	3154.2	810.9	.017
50'	1963.6	327.1	T	50'	2541.0	538.2	T	50'	3165.1	816.1	T
38°	1972.9	330.2	15° C.	48°	2551.0	542.2	15° C.	58°	3176.0	821.4	15° C.
10'	1982.2	333.2	T	10'	2561.0	546.3	T	10'	3186.9	826.7	T
20'	1991.5	336.3	.06	20'	2571.0	550.4	.10	20'	3197.8	832.0	.14
30'	2000.9	339.3	E	30'	2581.0	554.5					

23° 10' 40"
46° 21' 20"



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

8.9
1.4
10.3

50
15.50
34x50

103.13
60
43

27.5
46
73.5

112.64
100 ST
90112
56320
653312
11264
00145
56320
45056
11264
1633280

9.0
3.8
5.2
4.8
1.8
6.1

17
15
31
1.4
7
21

56320
45056
11264

130 15.14

124 38.13
1176.62
130.14.75
.39

18232
180162
170

16
4.1
78
3-10

206 + 60
206.72

138
69

46.93 + 50
69

46.24 = 18.2
69

45.55 + 50
69

44.86 = 183
69

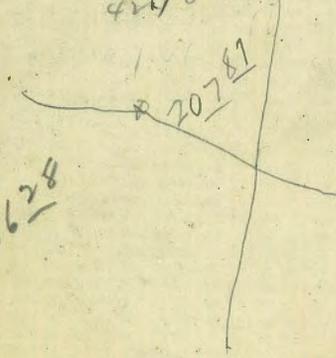
44.17 + 50
69

43.48 = 184
69

42.79
69

42.10 = 185

047628



84
48
237
185
655

ct. - 8.21 J.P. 79886
ct - 3 2' Hyd.

206.60
65

206.43.5

206 + 35

206 + 40

185 + 50

181 + 50

4.50

1.38

5.32

46.93

5.52

41.41

69

42.10

331.08
207.87
123.21

B.M. Man A Line & End School Prop.

31.37

234.63
201.74

19.3
40.5

2874
2065
8.09

436.4
218.2

259.8
29.9

195.40
4874
166.66

200 452
19427.

20221.3
201491.4

178 + 46.04
172.00

646.04

24.68
97.32

122.1

53.8
08.5
45.3

42
1.55

35.6

78 70
16
54

5 19000
4

1.4
2
3

33.6

295.26
4732.74
5028.00

15-

14.35-30
1.84
15.39-20

107.13
52758-30 2
79-14-30 W
52-37-30
26-37-00

82-30
9.54
92-26

59-06 30 W
44.48-30

x 20-27 W
82 30
102.57

206.2
32
32
64
96
19.24
16.4

1136565
1325.79
12691.94
137.58
12553.86
11.46
12565.32
64.89
69