

1531

1955

FIELD BOOK

No. 385F

1531

MICROFILMED

DEL 24 1964

ENGINEERING DEPARTMENT
CITY OF
CALIFORNIA.
SAN DIEGO, CALIF.

B.M. 17 = X. N. side Water Dept. M.H.
53.3 Lt. of Sta 206 + 37 El. 64.38.

(70)

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THE FREDERICK POST CO.
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1-20-36

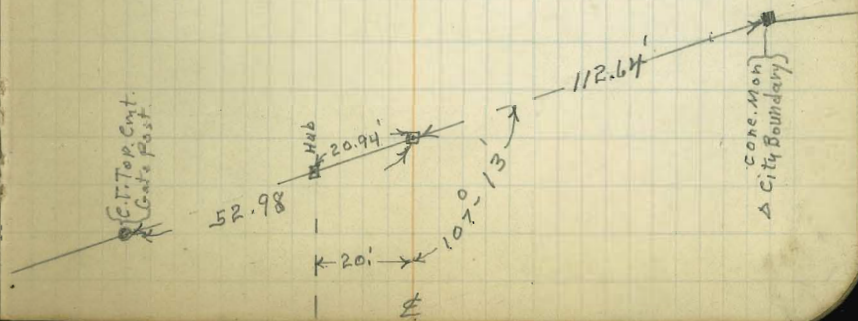
Camino Del Rio
Continued from F.B. 1530

E

1

+59⁹⁸ - P.O.T. Hub - P.I. City Boundary + E
 +53⁷⁹ Hub, P.I. City Boundary 20' Lt. of E

206



Levels for proposed Borrow Pit
 betw sta 54+00 and 63+27.43
 La Jolla Cañon Drive
 on Wly side of paving

Moore
 S. 5304
 Northward
 J-23-36

indexed
 c.s.K.

P.L. 1299

FB 1317-68
 GB 130-21

2

Man.

1046.09

92° 15'

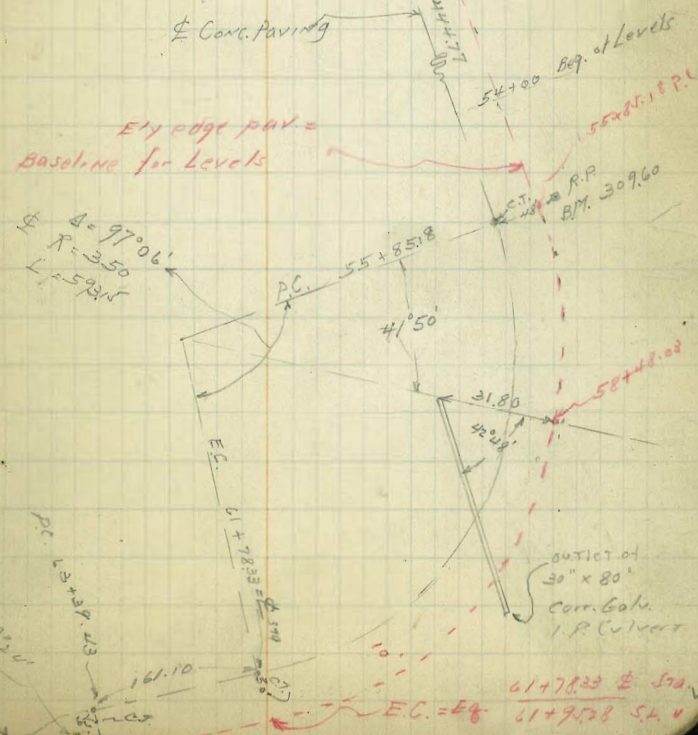
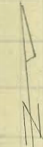
65.01

188.19

61.87

61.87

$\Delta = 6^{\circ}00'$
 $R = 2200$
 $L = 230.38$



Ely edge pave =
 Baseline for Levels

$\Delta = 97^{\circ}06'$
 $R = 3350$
 $L = 592.17$

PC

55+85.18

R.P.
 B.M. 309.60

41°50'

31.80

42.21

58+42.03

outlet of
 30" x 80"
 Corr. Gate
 1 P. Culvert

61+72.33 ± Sta
 EC = 61+72.33 Sta

PC 63+27.43
 $\Delta = 99^{\circ}21'$
 $R = 1000$
 $L = 101.60$
 C.T. 63+27.43

161.10

Borrow Pit Levels

56 +00

304.27

304.87

306.75

49.78

+85.18 P.C. Ely edge pav.

306.75

+50

T.P. 11.57 306.13 2.92 344.56

308.49

38.99

311.04

36.44

313.49

54+00 Note/ Sect. taken Radial

3399

T.P. 12.74 347.48 0.39 334.74

T.P. 13.11 335.13 0.84 322.02

B.M. 13.26 322.86 309.60

242 P.M.

R.P. Hub
48 Ely it
55485.18

304.27
E. edge of
Paving

52.92	52.26	50.47	308.42	59.06	307.3	59.1	308.4	58.6.13
303.18	303.87	305.66	304.9	304.9	306.0	316.7	316.9	316.9
46	46	46	46	46	46	46	46	46
302.5	303.5	304.9	307.3	307.3	307.3	316.9	322.4	316.9
46	46	46	46	46	46	46	46	46
304.6	305.3	306.0	308.4	308.4	308.4	316.9	322.4	316.9
46	46	46	46	46	46	46	46	46
320.3	321.6	316.7	316.7	316.7	316.7	316.7	322.4	316.9
46	46	46	46	46	46	46	46	46
330.0	329.7	324.9	324.9	324.9	324.9	324.9	322.4	322.4
46	46	46	46	46	46	46	46	46
340.4	339.8	331.9	331.9	331.9	331.9	331.9	334.8	331.9
46	46	46	46	46	46	46	46	46
346.4	346.5	346.3	346.3	346.3	346.3	346.3	343.3	346.3
46	46	46	46	46	46	46	46	46
352.1	352.0	351.7	351.7	351.7	351.7	351.7	343.3	343.3
46	46	46	46	46	46	46	46	46
363.3	363.3	351.7	351.7	351.7	351.7	351.7	347.1	347.1
46	46	46	46	46	46	46	46	46

59

Baseline
E edge
PAV
291.54

52.00
294.60
51.94
294.66
57.88

58+50

58 + 4803 = Culv. = 30" Culv. Corr. 1/P/R

T.P. NAIL
ford pan
out

2.93 346.54 12.52 3 vs. 01

120 ft. of 50"
57+60

296.44
57.69
298.37
57.76
300.42
55.71
302.37
53.76

58

+50

57

+75

56+50

356.13

55.16	291.38
20	
293.30	
55.16	290.9
20	
298.57	
55.16	296.6
20	
298.5	
55.16	313.1
20	
298.3	
55.16	329.1
20	
298.5	
55.16	337.6
20	
298.3	
55.16	344.7
20	
298.5	

50.93	295.20
20	
297.26	
61.7	299.4
40	
295.6	
58.8	297.8
50	
296.6	
55.8	302.3
55	
307.5	
51.5	304.6
60	
310.4	
57.4	316.9
35	
321.0	
51.9	324.2
100	
326.8	
26.9	329.2
110	
331.2	
58.4	302.3
53	
307.5	
45.7	304.6
60	
310.4	
35.1	316.9
35	
321.0	
29.2	324.2
100	
326.8	
24.9	329.2
110	
331.2	
58.7	302.3
38.1	
50	
307.5	
32.1	304.6
60	
310.4	
20.8	316.9
80	
321.0	
14.0	324.2
110	
326.8	
24.9	329.2
110	
331.2	
322.6	346.5
33.5	
48	
299.6	
318.7	
37.4	327.0
46	
327.0	
27.1	342.5
60	
342.5	
13.6	347.5
90	
347.5	
80	
347.5	
110	

356.13

E. edge
 Pav.
 Baseline

61+50

289.99
 3883

20.04
 20

60.8
 60

PT.
32.4
 41

24.6
 60

9.0
 90

+1.5
 110

T.P. Rock 126 321.82 10.02 320.56 100' PT. 04
 61+35
 T.P. 3.54 330.58 8.68 327.04
 T.P. Rock 232 335.72 13.14 333.40

321.82

61

285.01
 61.53

22.80
 20

6.31
 60

5.1
 40

47.7
 60

32.8
 85

19.0
 110

+50

287.08
 59.46

60.77
 20

60.5
 60

29.53
 51.2
 40

30.17
 44.8
 60

31.7
 29.8
 90

32.7
 18.8
 110

60

288.77
 57.77

287.71
 58.23
 20

287.4
 59.1
 27

288.4
 58.1
 49

304.0
 42.5
 41

311.2
 45.3
 20

320.4
 20.1
 85

331.3
 15.2
 110

+50

290.76
 55.78

289.45
 57.09
 20

288.9
 57.6
 29

316.2
 30.3
 40

325.9
 20.6
 60

340.2
 6.3
 90

343.9
 2.6
 110

59+35

291.66
 54.88

290.44
 41.0
 20

290.0
 40.5
 27

318.8
 27.7
 40

327.9
 16.6
 60

340.8
 5.7
 90

344.6
 1.9
 110

346.54

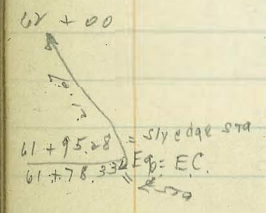
346.54

Sly edge
pav. + base + ...

check to BM. Tie nub. 90 S of 21772.23	2.73	281.40	281.41	0.01 error
T.P. 031	284.13	11.54	283.82	
T.P. 632	295.34	12.49	289.01	
T.P. 128	301.50	12.87	300.22	

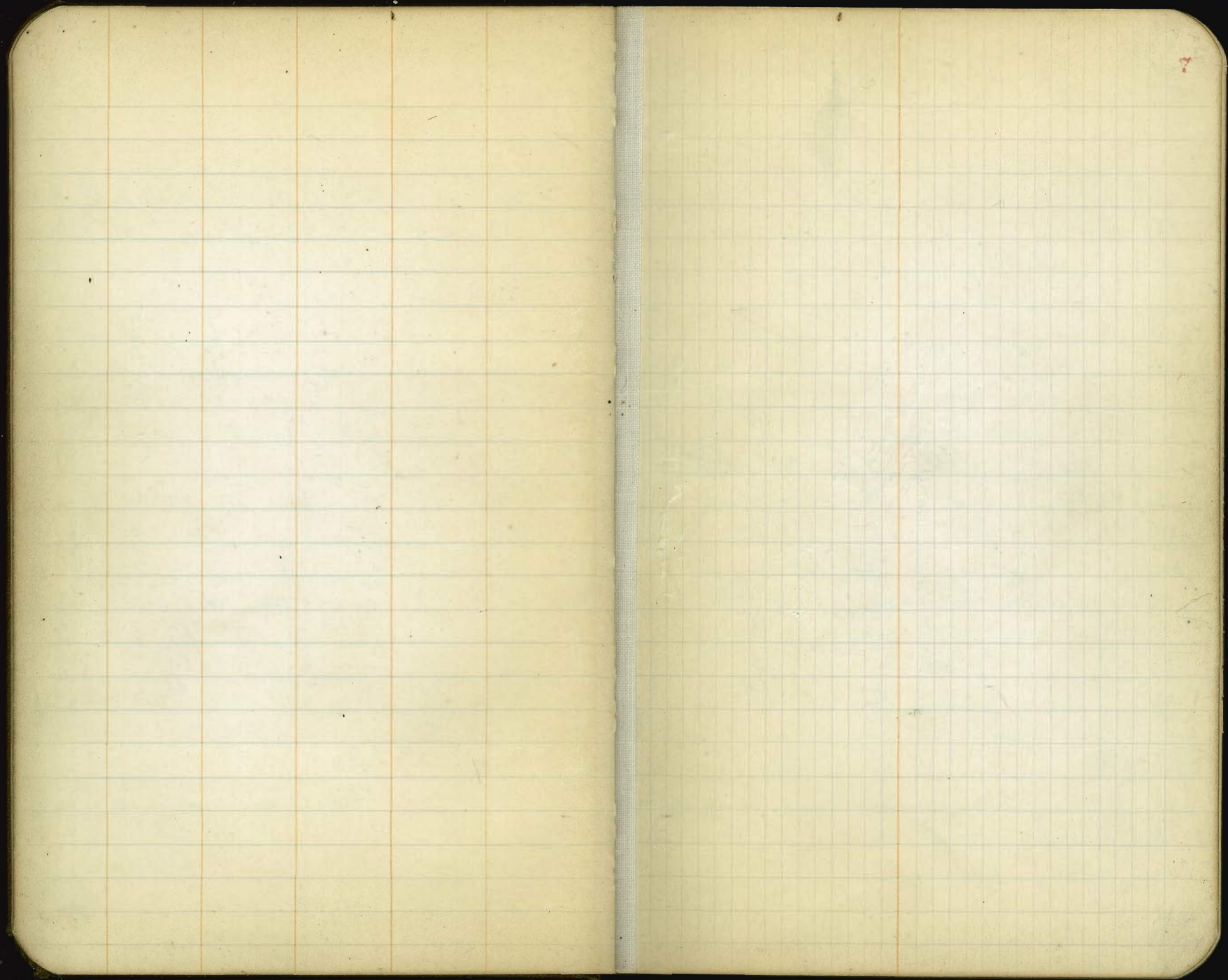
63 + 39.43 = PC of Lt. Curve	4137	271.72		
63	39.13	273.96		
+ 50	34.32	276.77		
64 + 00	33.73	279.86		
61 + 95.28 = Sly edge - ... 61 + 78.332 = Eq. = EC.	31.89	281.20		

T.P. 417	313.09	12.90	308.92	
	321.82			



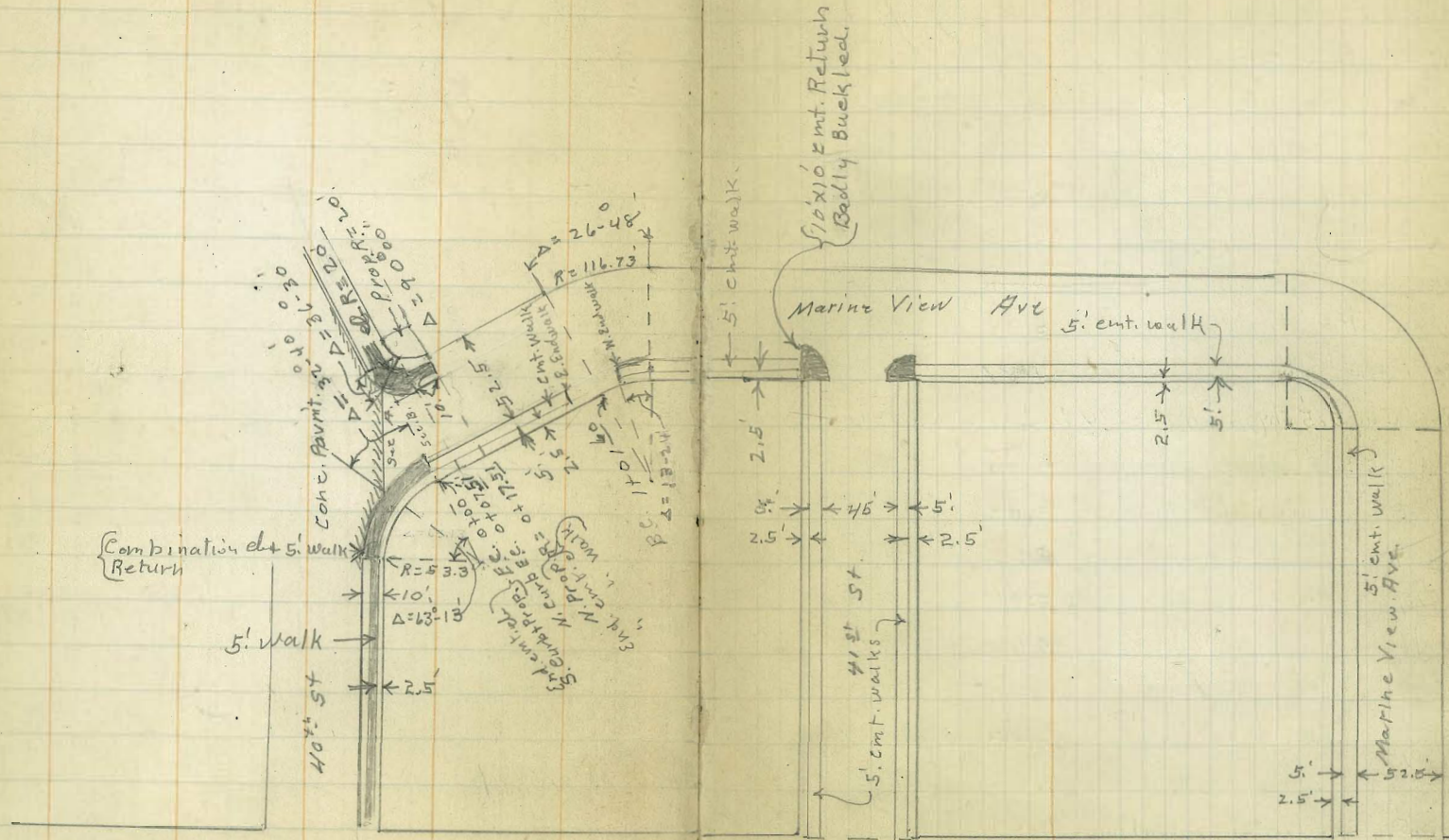
20.28	20	272.81		
4.97	38	273.4		
31.1	45	282.0		
25.5	60	287.9		
16.6	80	296.5		
2.8	110	308.3		
38.37	20	274.72		
49.0	30	274.1		
28.2	43	284.9		
18.3	60	294.8		
7.2	80	305.8		
1.8	110	319.1		
36.36	20	276.73		
47.1	27	276.0		
27.2	41	285.9		
16.3	60	292.7		
6.1	80	302.0		
1.5	110	316.1		
34.30	20	278.79		
35.6	29	277.5		
26.3	48	286.8		
16.0	60	290.1		
6.2	80	296.7		
1.8	110	304.3		
27.85	20	279.85		
41.5	30	278.2		
24.5	49	288.6		
10.2	60	292.9		
3.5	80	299.6		
0.5	110	313.6		

313.09



5.8-31 X See Marine View Ave
 Miller 40th St. to Division St. also
 Walker
 Bliss 41st St. Division to Marine View.

Indexed
 crsk.



Division

St. (paved)

60. wide 41st ST. X Sec. 5-8-36
 10' elev Division to Marine View Ave
 10' 1/4s

BM, BP 6.82 64.16 57.34 N.W. 41
 + Division

14' s. of N. Line = N. ch. Line of Division

W. emt. ch 6.82 57.34
 W Gutter pav 7.50 56.66
 ch " 7.05 57.11
 1/4 " " 6.69 57.47
 ± " " 6.29 57.87
 1/4 " " 6.03 58.13
 ch " 5.72 58.44
 E. Gutter " 5.39 58.77
 E. emt. ch 4.87 59.29

Roadway 0.5' shy 100 = N 1/4 Line Division

E + 7.5 = W. edge emt. Walk 4.90 59.26
 E + 10.2 =
 ch N. End. emt. ch d. 0.2 in st. 5.05 59.11
 Gutter N. End. pav. 5.73 58.43
 1/4 " " " 5.78 58.38
 ± " " " 5.93 58.23
 1/4 " " " 6.33 57.83
 + 9.7 =
 gutter " " " 6.83 57.33
 1/4 + 9.7 ch = N. End. emt. ch in st. ^{ch. 15 0.3} 6.22 57.94
 + 2.5 = E. edge emt. walk. 6.22 57.94

0750 N.

W + 7.5 = E. edge emt walk 5.57 58.58
 ch. 6.0 58.2
 1/4 5.7 58.5

6416

9

± 5.1 59.1
 1/4 5.1 59.1
 + 8 5.0 59.2
 ch 4.4 59.8
 + 2.5 = W. side emt. walk. 4.20 59.96
 1400
 E + 7.5 = W. edge emt. walk. 3.69 60.47
 ch. 3.7 60.5
 + 3 4.4 59.8
 1/4 4.4 59.8
 ± 4.2 60.0
 1/4 5.0 59.2
 ch 5.3 58.9
 + 2.5 = E. edge emt. walk 4.94 59.22
 T.P. 4.96 64.96 4.16 60.00

14023

108 W. of E. Line = Black Acacia Tree 8" Diam

14188

108 W. of E. Line Black Acacia Tree 8" Diam

14314

106 W. of E. Line Black Acacia Tree 6" Diam

14475

11 W. of E. Line Black Acacia Tree 4" Diam

A. 10' curb. would take them out.

64.96

1750

W + 7.5 = E. edge cmt. walk 4.95 60.01

cb 5.2 59.8

+3 5.7 59.3

1/4 4.9 60.1

ϕ 4.1 60.9

1/4 4.3 60.7

+5 4.4 60.6

+7 3.4 61.6

cb 3.4 61.6

+ 2.5 = W. edge cmt. walk 3.46 61.50

2+00

E + 7.5 = W. edge cmt. walk 2.78 62.18

cb 2.9 62.1

+2 2.9 62.1

+3 3.6 61.4

1/4 3.4 61.6

ϕ 3.4 61.6

1/4 4.2 60.8

+8 5.0 60.0

cb 4.3 60.7

+ 2.5 = E. edge cmt. walk 4.27 60.69

2+50 = S. Line Marine View, Ave

W + 7.5 = E. edge cmt. walk 3.59 61.37

cb. S. End 3.64 61.30

gutter 3.9 61.1

1/4 3.6 61.4

64.96

41st St.

10

ϕ 3.0 62.0

1/4 2.6 62.4

+8 2.7 62.3

gutter 2.1 62.9

cmt. cb. S. End 1.98 62.98

+ 2.5 = W. edge cmt. walk 1.92 63.04

T.P. 0.09 52.26 12.79 32.17

50' wide X See Main View Ave
 16' chs
 10' 1/4s 40th to Division St.
 5' cmt. walks.
 2.5' from Lin

52.26 = π Pay 10

Sec. A. E. Edge Pav. See Plal.

S. cmt. ch = 10.65 of ch. Produced from E.	9.35	42.91
Gutter Pav. = 10.6 " " " " " "	10.00	42.26
6.5 W. of above = N+S. Gutter & side Hd th SF	10.08	42.18
S. ch. line produced from E.	9.93	42.33
7.0 W. of above = N+S. Gutter	10.20	42.06
S. 1/4 Produced from E.	9.84	42.42
7.6' W. of above = N+S. Gutter	10.32	41.94
$\frac{1}{2}$ Produced from E.	9.84	42.42
8.2' W. of above = N+S. Gutter	10.50	41.76
N 1/4 Produced from E.	9.96	42.30
8.8' W. of above = N+S. Gutter	10.57	41.69
N. ch Produced from E.	10.27	41.99
9.4' W. of above = N+S. Gutter	10.77	41.49
9' N. ch. line Produced from E. = Gutter	10.56	41.70
9' N. of " " " " = cmt. ch.	9.96	42.30
9.9 W. of above = N+S. Gutter.	10.97	41.29

Sec. B = 0x00 = E.C. S. prop line + S. ch. line

1.3' N. of N. ch. produced from E. N. cmt. ch	9.36	42.90
1.3' N. = gutter	9.8	42.5
N. ch. Produced from E.	10.0	42.3
1/4	9.4	42.9
$\frac{1}{2}$	8.8	43.5
1/4	8.4	43.9

52.26

11

Gutter	8.3	44.0
S. ch = E. End cmt. ch	7.28	44.98
+ 2.5' = N. edge cmt. ch.	7.18	45.08

0 + 07 = E.C. Cmt. ch. on N

N. Gutter	9.8	42.50
N. cmt. ch	9.11	43.15

0 + 17.5' E.C. Prop. line on N = E. End cmt. ch + walk

N. ch of 4' cmt. walk to N	8.62	43.64
+ 2.5' N.E. Cor cmt. walk	8.65	43.61
+ 7.5' S. E " " "	8.67	43.59
ch. E. end cmt. ch	8.74	43.52
gutter	9.4	42.9
1/4	8.5	43.8
$\frac{1}{2}$	7.6	44.7
1/4	7.2	45.1
+ 9	7.0	45.3
ch	6.0	46.3
+ 2.5' = N. edge cmt. walk	5.92	46.34

0 + 59.56

5 + 7.5' = N. edge cmt. walk	2.81	49.45
ch	3.6	48.7
+ 2	4.2	48.1

52.26

0+59.56 (con)

1/4	4.2	48.1
ϕ	4.7	47.6
1/4	5.2	47.1
+5	5.6	46.7
ϕ	5.4	46.9
N	5.6	46.7
+5	6.4	45.9

0+91 E. End. of Good Walk on S.

7.5' N. of S. Line = N. edge ent. walk. 0.46 51.86

1+01.57 B.C.

N-5	3.5	48.8
N	2.7	49.6
ϕ	2.3	50.0
+5	2.6	49.7
1/4	2.0	50.3
ϕ	1.2	51.1
1/4	1.0	51.3
+8	0.6	51.7
ϕ	0.1	52.2
T.P.	12.84	65.05
0.09	52.17	
+2.5 = Walk N.G.	12.4	52.45

Ctn. Curve

7.5' N. of S. Line = N. edge walk 11.45 53.60

Walk N.G. to W
" O.K. 18

65.05

Marine View Ave

12

0+00 = E. C.

S. + 7.5' = N. edge ent. walk.	10.45	54.60
ϕ	11.3	53.8
1/4	11.0	54.1
ϕ	10.8	54.3
1/4	11.5	53.6
ϕ	11.5	53.6
N	11.2	53.9
+5	11.2	53.9

0+25 5 ϕ 3' Walk to N

N. = S. End. Walk 8.72 56.33

0+35 = ϕ 8' ent. Drive to N

N = S. End. Drive	7.94	57.11
ϕ	8.6	56.5
1/4	8.2	56.9
ϕ	7.7	57.4
1/4	8.3	56.8
+8	8.7	56.4
ϕ	7.6	57.5
+2.5 = N. edge ent. walk	7.55	57.50

65.05

0+84.42 = W. line - 41st ST.

ch - 2.5' = N. Edge cont. walk	3.79	61.26
ch. W. End N.G.	3.84	61.17
gutter	4.5	60.6
1/4	4.8	60.3
ϕ	4.6	60.5
1/4	5.4	59.7
+7	5.8	59.3
1 ch.	5.2	59.9
N.	5.0	60.1
W. ch. Line		
N	4.5	60.6
ch	4.8	60.3
+4	5.3	59.8
1/4	4.7	60.4
ϕ	4.0	61.1
1/4	4.1	61.0
ch	4.1	61.0
S. gutter	4.0	61.1
S. cont. ch	3.72	61.33
W. 1/4		
S	3.6	61.5
ch.	3.6	61.5
1/4	3.6	61.5
ϕ	3.4	61.7
1/4	4.1	61.0
+6	4.7	60.4

65.05

Marine View Ave

13

ch	4.2	60.9
N.	3.6	61.5
E 41 st ST		
N	3.2	61.9
ch	3.5	61.6
+7	3.9	61.2
1/4	3.5	61.6
ϕ	2.8	62.3
1/4	3.1	62.0
ch	3.1	62.0
S	3.0	62.1
E. 1/4		
S.	2.8	62.3
ch	2.9	62.2
1/4	2.8	62.3
ϕ	2.5	62.6
1/4	3.1	62.0
+3	3.5	61.6
ch	3.0	62.1
+5	1.6	63.5
N	1.6	63.5
E. ch.		
N.	1.2	63.9
+5	1.2	63.9
ch	2.4	62.7
+5	2.9	62.2

65.05

1/4	2.6	62.5
ϕ	2.1	63.0
1/4	2.6	62.5
el	2.3	62.8
S. cnt. el	2.05	63.00
S. gutter	2.1	63.0
0+00 = E. Line 41 st. St.		
S+7.5 = N. edge cnt. walk	1.84	63.2
cnt. el E. End.	1.95	63.10
gutter	2.0	63.1
+5	2.5	62.6
1/4	2.3	62.8
ϕ	1.8	63.3
1/4	2.3	62.8
+4	2.7	62.9
el	2.2	62.9
+3	2.0	63.1
+5	1.1	64.0
N	1.1	64.0
T.P.	9.49	73.90
	0+50	
N.	8.5	65.4
el	9.1	64.8
+2	9.5	64.4
1/4	8.9	65.0
ϕ	8.3	65.6

73.90

Marine View Ave. 14

1/4	9.1	64.8
+5	9.5	64.4
el	8.7	65.2
+2.5 = N. edge cnt. walk	8.51	65.39
0+75		
S+7.5 = N. edge cnt. walk	7.41	66.49
el	7.5	66.4
+5	8.4	65.5
1/4	8.0	65.9
ϕ	7.5	66.4
1/4	8.1	65.8
+7	8.6	65.3
el	8.0	65.9
N	7.9	66.0
1+00		
N	7.2	66.7
el	7.2	66.7
1/4	7.1	66.8
ϕ	6.6	67.3
1/4	7.1	66.8
+5	7.5	66.4
el	6.7	67.2
+2.5 = N. edge cnt. walk	6.66	67.24

73.90

1+50

S+7.5' = N. edge emt. walk	5.42	68.48
cl	5.8	68.1
+4	6.5	67.4
1/4	6.2	67.7
⊕	6.0	67.9
1/4	6.3	67.6
cl	6.5	67.4
N	7.6	66.3
+10	9.0	64.9

2+10 = B.C. 90°-00' RT.

-10	11.0	62.9
N	9.0	64.9
cl	6.3	67.6
1/4	5.7	68.2
⊕	5.6	68.3
1/4	5.7	68.2
+9	5.6	68.3
cl	4.9	69.0

+2.5' = N. edge emt. walk 4.54 69.36

Curve Divided into 4 Parts.

#1 Δ = 22°-30'

S+7.5' = N. edge emt. walk	4.43	69.47
cl	4.7	69.2
+1	5.5	68.4
1/4	5.6	68.3
⊕	5.4	68.5

73.90

Marine View Ave
15

+7	5.5	68.4
1/4	5.2	68.7
cl.	6.3	67.6
+2	6.4	67.5
N	9.4	64.5
+20	15.3	58.6

#2. Δ = 45°-00' ct. of curve

-20	17.7	56.2
N	10.4	63.5
cl.	6.6	67.3
1/4	5.0	68.9
⊕	5.2	68.7
1/4	5.3	68.6
+9	5.3	68.6
cl	4.5	69.4

+2.5' = N. edge of walk 4.26 69.64

#3' Δ = 67°-30'

S+7.5' = E. edge emt. walk	4.14	69.76
+9	4.4	69.5
cl	5.1	68.8
1/4	5.1	68.8
⊕	5.1	68.8
1/4	5.3	68.6
cl	8.0	65.9
E. ly. line	9.3	64.6
+5	10.0	63.9

#3 (con)

elg. +10	12.2	61.7
elg. +25	19.4	54.5
#4 $\Delta = 90^{\circ} - 00' = 0 + 00$		
E - 20	11.2	62.7
E.	8.7	65.2
el	6.7	67.2
$\frac{1}{4}$	5.1	68.8
$\frac{1}{2}$	4.9	69.0
$\frac{3}{4}$	4.9	69.0
el	4.8	69.1
+1	4.2	69.7
+2.5 = E. edge cmt. walk.	4.00	69.9

0 + 40

W + 7.5 = E. edge cmt. walk.	3.47	70.43
el	3.6	70.3
+2	4.4	69.5
$\frac{1}{4}$	4.1	69.8
$\frac{1}{2}$	4.1	69.8
$\frac{3}{4}$	4.5	69.4
el	4.7	69.2
E	4.7	69.2

1 + 00

E	3.8	70.1
el	3.8	70.1
$\frac{1}{4}$	3.4	70.5
$\frac{1}{2}$	3.0	70.9

$\frac{1}{4}$	3.2	70.7
+7	3.4	70.5
el	2.4	71.5
+2.5 = E. edge cmt. walk.	2.45	71.45
T.F. 5.81 77.47	2.24	71.66
1 + 50		
W + 7.5 = E. edge cmt. walk.	5.22	72.25
el	5.5	72.0
+2	6.4	71.1
$\frac{1}{4}$	6.1	71.4
$\frac{1}{2}$	5.9	71.6
$\frac{3}{4}$	6.0	71.5
el	6.3	71.2
E	5.8	71.7

2 + 00

E	4.3	73.2
el	5.3	72.2
$\frac{1}{4}$	5.1	72.4
$\frac{1}{2}$	4.9	72.6
$\frac{3}{4}$	4.8	72.7
+8	5.1	72.4
el	4.0	73.5
+2.5 = E. edge cmt. walk.	4.32	73.15

77.47

2+30 = N. Line Division St.

W + 7.5 = E. edge curwalk	3.60	73.9
emt. cl. N. End	3.72	73.75
gutter N. end. Pav.	4.37	73.10
1/4 " " "	4.14	73.33
1/4 " " "	4.01	73.46
1/4 " " "	4.10	73.37
gutter " " "	4.32	73.15
emt. cl. N. End	3.78	73.69
+ 2.0 = ^{W. edge} N. End. } emt. Walk	3.73	73.74
+ 7.0 = ^{E. edge} N. End. } emt. Walk	3.91	73.56
E.	4.0	73.97

14' S. of N. Line = N. cl. Line of Division

E. cl. Pav.	3.89	73.58
1/4 "	3.61	73.86
1/4 "	3.58	73.89
1/4 "	3.71	73.76
cl "	3.95	73.52
W "	4.27	73.20
W, emt. cl.	3.71	73.76
B.M. B.P.	3.71	73.76 = N.W. Division 73.75 + Marine View

Marine View Ave.

17

6-24-36

Camino Del Rio

Miller
Walker
Bliss

X Sec. change in Alignment from
Sta 14+37.21 BC to Sta 50+70.75 New E.C.

Book 1528 - P. 79 for change

17

14 Alignment & Ties

+50

16

+50

15

14+99.00 E.C.

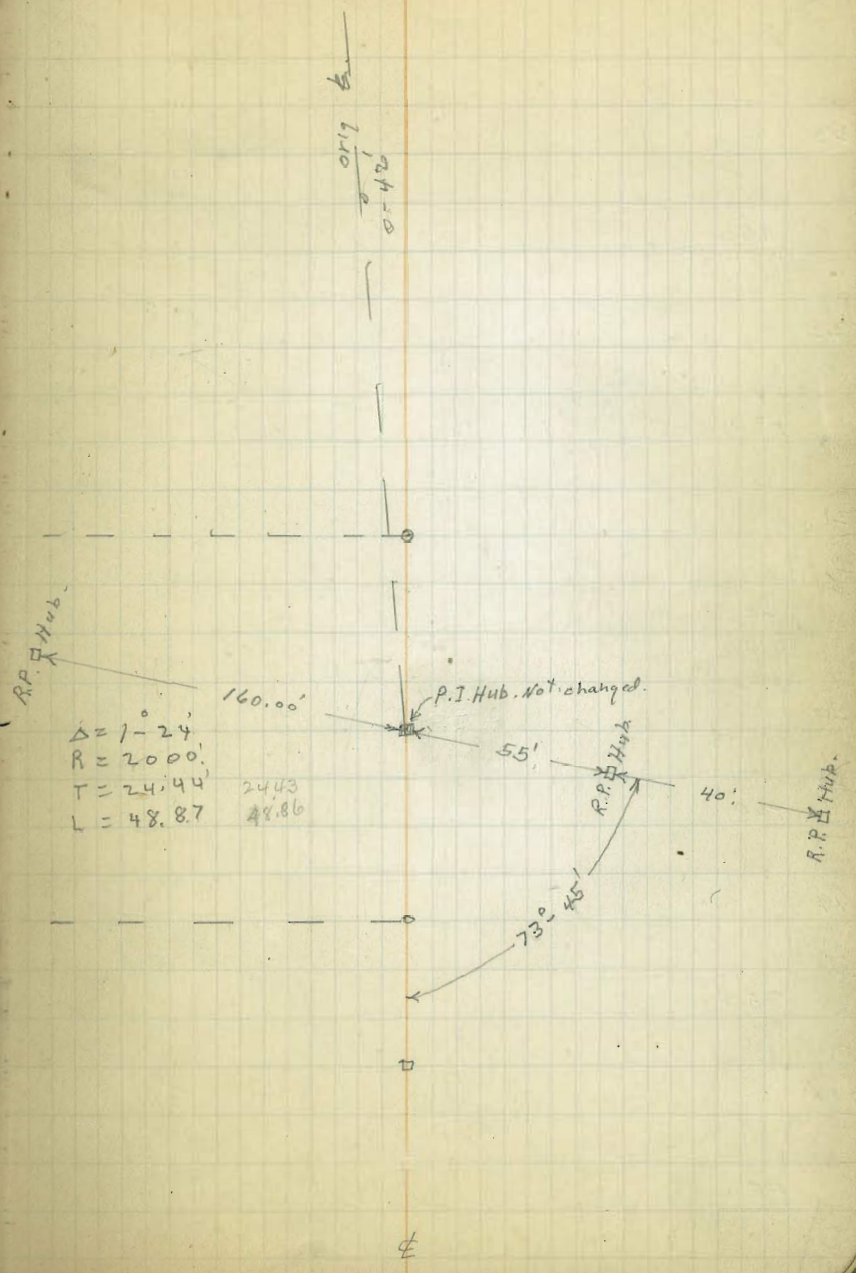
Abandoned 12-14-36
See F.B. 1528-80
Cross sections from 14+50
to 30+00 O.K. For "D" line
Final F.B. 1528-80.

14+50.13 New B.C. Lt.

14+37.21 P.O.T. Hub. change

14+37.21 B.C. Lt. Hub original line

Indexed
0.11X1



6-
mi
wa
B

+50

17

23

+50

16

22

+50

15

21

+50

20

+50

14

19

+50

13

18

+50

£

20

£

£

+50

30

+50

29

+50

28

+50

27

+50

26

+50

25

+50

24

£

2

22

37

+50

36

35 +50

+50

34

+50

33

+50

32

+50

31

2

42

+50

41

+50

40

+50

+10.99 E.C.

39

+50

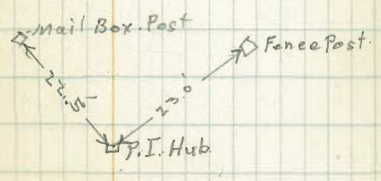
38

+50

+39.66 B.C. Lt.

37

$\Delta 4^{\circ} 54' 30''$
 $R = 2000'$
 $T = 85.70'$
 $L = 171.33'$



£

48

+50

47

+50

46

+50

45

+50

44

+50

43

+50

£

51

+70⁹⁵ New. F.C. = 50+69²⁸ old. sta

+50

50

+50

49

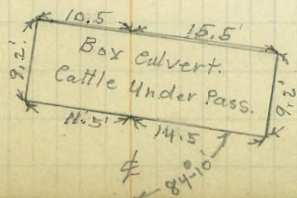
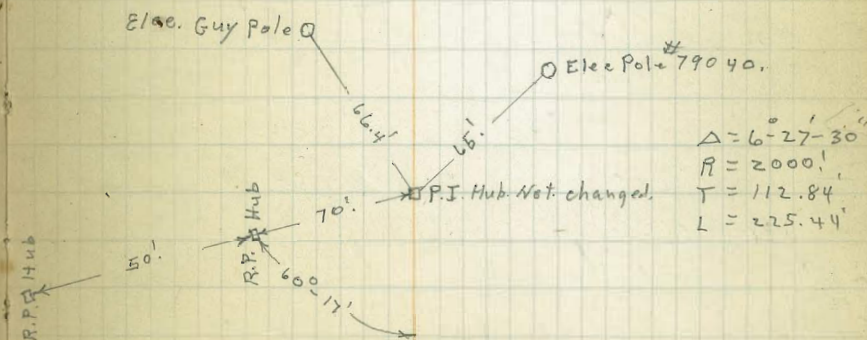
+45⁵¹ B.C. RT.

+36⁸ e. side Box Culvert. at ϕ

48

+27⁵ w. side Box Culvert. at ϕ

48



±

+50 5.0

+41 Elec Pole 14 RT.

17 5.3

+50 5.5

16 5.6

+50 5.8

15 5.8

+99 E.C.

14+50 5.9

B.M. T.P. 2.96 16.36 13.40

These x sec. O.K. from 14+50
to 30+00 for "D" Line F.B. 15 28-80.

10.4
6.0 6.0 8.3 8.5 5.5 5.3 5.0 4.8 4.4 6.0 6.5 9.9
50 27 26 20 16 15 15 17 20 50

10.2
6.2 6.4 6.2 8.6 8.5 8.4 5.7 5.3 5.1 5.1 6.8 6.3 10.1
50 30 27 25 20 18 15 15 15 18 20 50

10.2
6.2 6.0 8.8 9.0 8.2 5.6 5.5 5.5 6.6 7.3 9.4 7.0
50 28 26 20 18 15 15 20 20 50

10.4
6.0 6.2 8.3 8.3 5.5 5.6 5.3 5.7 7.0 7.6 8.8
50 33 29 20 15 15 15 20 30 50

10.1
6.3 6.3 9.3 9.6 6.9 5.7 5.8 5.5 5.2 6.0 7.5 7.5 8.9
50 29 23 20 15 13 15 15 18 20 28 50

10.5
5.9 5.9 9.4 9.4 6.3 5.8 5.7 5.7 7.8 8.4 8.0
50 28 20 15 12 15 15 20 23 24

11.5
4.9 6.0 10.0 9.4 4.2 5.9 5.7 5.6 8.1 8.9 7.5
50 25 20 15 10 15 20 30 50

16.36

Nails in Elec Pole #79010

±

21

6.2

+53 Elec Pole 12.5' Rt.

+50

5.1

T.P.

4.72

17.56

3.52

12.84

+07 Elec Guy Pole 13' Rt

20

4.7

+50

4.5

19.

4.4

+50

4.4

18

4.7

16.36

Lt

±

Rt

27

10.5

7.1
508.8
338.7
286.7
246.2
206.2
156.2
155.9
158.1
158.8
208.8
50

10.8

6.8
507.2
339.0
258.1
206.1
186.0
155.1
155.8
127.3
158.0
209.2
309.2
50

17.56

10.9

5.5
505.3
308.0
267.5
205.0
184.8
154.7
154.5
156.6
208.7
359.0
50

10.8

5.6
505.4
287.7
257.7
204.8
184.6
154.5
154.4
154.4
176.0
207.0
307.6
50

10.6

5.8
505.7
325.7
288.0
257.8
204.9
184.7
154.4
154.3
154.5
175.6
205.8
266.7
277.7
27

10.4

6.0
505.7
278.0
257.8
204.4
174.8
154.6
154.5
154.5
185.7
206.6
306.8
50

10.4

6.0
505.9
278.1
258.2
205.0
165.0
154.7
154.7
154.7
185.7
206.2
50

16.36

25

♀

4.0

111.8
 5.8 5.1 5.5 8.0 7.6 4.6 4.6 4.3 4.0 4.1 5.9 6.3 6.2 4.0
 50 36 32 28 25 21 20 15 15 12 15 20 35 50

+50

4.3

111.5 fence
 6.1 5.3 8.0 8.0 4.7 4.7 4.4 4.3 4.5 6.1 6.1 6.6 6.2
 50 32 28 26 21 20 15 15 11 13 15 20 50

24

4.4

111.2
 6.4 5.4 8.0 8.3 4.9 4.7 4.4 4.4 4.6 6.1 6.1 6.6 7.2
 50 31 29 26 20 15 15 11 13 15 20 50

+50 W. End. Eucalyptus grove on Rt.

4.6

10.8
 6.8 5.6 8.0 8.1 5.0 4.9 4.6 4.4 6.3 6.3 6.7 7.0 6.8
 50 33 30 25 20 15 15 10 13 15 20 35 50

+40 Elce Pole 10' Rt

23

5.0

10.0
 7.6 4.2 8.1 8.1 5.4 5.2 5.0 5.2 6.5 6.7 6.9 7.0
 50 32 28 23 20 15 15 13 15 17 20 50

+50 W. End. Eucalyptus grove on Lt.

5.4

9.3
 8.3 7.1 9.0 8.5 5.7 5.6 5.4 5.6 7.1 7.5 7.3
 50 31 27 23 20 15 15 13 15 20 50

+40 Elce Pole 10' Lt.

22

5.9

10.3
 7.3 8.1 9.1 9.0 6.4 6.0 5.9 5.8 6.7 7.7 7.7
 50 34 27 23 20 15 15 12 15 20 50

+50 W. End. Eucalyptus grove on Lt.

2.1

11.6
 6.1 7.6 8.7 7.0 6.2 6.1 6.1 6.4 7.7 8.4
 50 32 27 20 18 15 15 15 20 50

17.56

17.56

£

28

8.0

+70 Store Bldg 53' Lt.
+65 Ice Pole 4.5 Rt.
+65 Gas. pump. Island 40' Lt

+50

7.9

T.P. 7.97 22.01 3.52 14.04

27

+92 Cottage 53' Lt.

+90

3.7

+50

+42 Ice Pole 6' Rt.

26

3.7

+50

3.8

17.56

Lt

£

Rt.

29

11.7
9.3 8.8 7.7 7.7 7.8 8.0 7.8 9.7 9.7 9.7 8.0
50 31 23 20 15 7 15 20 28 50

11.4
9.6 9.1 8.0 8.0 8.0 7.9 7.7 9.9 9.9 10.0 10.8 9.0
50 30 23 20 15 6 16 15 20 35 50

22.01

12.3
5.3 5.3 3.6 3.6 3.6 3.7 3.5 6.0 6.0 5.8
50 37 24 20 15 7 15 20 50
House
Pump

12.3
5.3 5.3 6.8 6.8 3.7 3.6 3.6 3.7 3.5 6.0 6.0 5.8
50 35 32 29 24 20 15 7 15 20 50

12.6
5.0 5.0 6.8 6.8 3.9 3.9 3.9 3.6 3.6 5.2 6.0 5.4 6.4
50 35 32 27 23 20 15 6 10 15 20 50

12.3
5.3 5.6 7.3 7.4 4.1 4.1 3.9 3.7 3.8 5.8 5.8 5.8 6.7
50 36 33 28 23 20 15 9 13 15 20 50

12.2
5.4 5.4 7.6 7.5 4.3 4.2 4.1 3.8 3.9 5.9 6.5 6.5
50 34 31 24 23 20 15 10 15 20 50

117.56

£

T.P. 11.44 33.28 0.17 21.84

31 2.0

+50 3.3

30 4.5

+80 Fence 40' Lt.

+50 5.5

CHK BM WALE Pole 79014 4.49 17.52 ✓

+45 " " " 2' Rt.

29 6.5

+80 E. end. grove of small Eucalyptus trees on Rt.

+50 7.6

22.01

Lt.

£

Rt.

30

18.8			19.8	20.0				28.5		34.5
3.2	1.7	2.2	2.7	2.0	+3.3	+5.0	+6.5	+7.6	+12.5	
50	30	20	15	3	7	15	20	50		

15.1			18.5	18.7				21.0		32.0
6.3	3.3	3.4	3.5	3.3	0.5	+1.0	+4.0	+5.0	+10.0	
50	38	20	15	4	10	15	20	50		

14.0			17.3	17.5				21.3		29.2
8.0	7.0	4.5	4.7	4.7	4.5	2.1	0.7	0.2	+3.5	+7.2
50	40	36	20	15	6	15	20	27	50	

14.0				16.1	16.5			16.9		23.0
8.0	7.6	8.5	5.6	5.8	5.9	5.5	4.8	5.1	4.3	2.1
50	40	34	28	20	15	2	15	20	28	50

14.8				15.1	15.5			14.6		16.9
9.2	8.5	9.3	9.0	6.8	6.9	6.9	6.5	6.2	7.5	7.4
50	39	35	30	27	20	15	5	8	15	20

Fence

12.5				14.5	14.4			11.6		14.0
9.5	8.5	9.5	9.5	7.0	7.3	7.5	7.6	7.0	9.4	9.4
50	36	34	31	26	20	15	6	10	15	20

22.01

±

- +72 Tree stump 20" Diam 35' Lt.
 +69 Tel Pole 44' Lt.
 +64 Cypress Tree 8" Diam. 17' Rt.
 +58 Cypress Tree 24" Diam 13' Rt.
 +54 Fan Palm 35' Lt + Fan Palm 1' Rt.

- +50 4.7
 +50 Cypress Tree 10" Diam. 13' Rt.
 +47 cypress. Tree 14" Diam 13' Rt
 +42 Olive Tree 10" Diam 17' Rt.
 +38 Acacia Tree 14" Diam 35' Lt

33

- +95 Fan Palm 2' Rt.
 +84 Duq well 4" Diam 42' Rt.

- +50 8.5
 +41 Elce Pole 3' Lt.
 +40 E. End. New. Rail Fence 30' Rt.
 +35 Dead Palm Stump
 +03, Palm 3' Rt.

32

Use FB 1552 PA3
Sta 32 to 40

- +50 7.2

33.28

31+20 = W. end, New. Rail Fence 30' Rt.

Lt.

±

Rt.

31

8.8 8.4 6.0 5.5 5.5 5.5 4.7 4.7 4.2 2.2 1.0 +1.1 +2.7
 50 37 35 20 15 5 4 10 15 20 40 50

13.7 13.0 7.8 7.5 7.5 7.2 6.0 5.7 4.7 0.2
 50 40 34 20 15 7.5 15 20 50

15.0 14.4 9.4 9.3 9.2 8.5 7.8 7.1 1.8
 50 41 33 20 15 15 20 150

14.0 12.2 10.4 10.6 10.6 10.3 8.0 7.6 6.3 5.7 1.9
 50 40 35 20 15 3 2 15 20 50

14.1 11.7 12.1 12.1 11.8 7.2 5.3 4.9 3.1 2.1 0.3
 50 35 20 15 2 2 10 15 20 50

33.28

+76 Tel Pole 45.6 Lt.
 +68 Cypress Tree 16" Diam 13 Rt
 +67 Tree stump 18" Diam 36 Lt
 +63 Cypress Tree 6" Diam 13 Rt.
 +56 Cypress Tree 16" Diam 13 Rt
 +57. M H 34' Rt
 +55 N.E. Cor shed 21' Rt.

+50 8.2

T.P. 10.08 42.69 0.47 32.61

+50 Fan Palm 1' Rt
 +41 N.W. Cor shed, 21' Rt
 +38 Cypress 10" Diam 13. Rt
 +34 Tree stump 25" Diam 35' Lt.
 +34 Cypress 14" Diam 13 Rt.
 +19 Fan Palm 36' Lt.
 +13 olive Tree 17' Rt.
 +03 Tree stump 35' Lt.

34 1.1

+89 Elec Pole 4' Lt. + olive Tree 6" Diam 17' Rt.
 +86 Fan Palm 35' Lt.
 +78 Cypress Tree 18" Diam 13' Rt.
 +73 Cypress Tree 8" Diam 12' Rt.

33.28

10.6 10.0 10.2 10.2 10.2 9.8 8.2 7.5 6.0 5.6 4.0
 50 36 20 15 7 6 10 15 20 44 50

4.2 3.7 3.1 3.1 3.1 1.1 1.1 0.4 +1.3 +1.8 +3.1 +4.9
 50 35 20 15 6 5 10 15 20 41 50

33.28

£

36

3.1

- +92 M.H. 8.5 Lt.
 +75 Large Fan Palm on £
 +75 Large Fan Palm 37 Lt.
 +71 Large Date Palm Boxed. 6'. Rt.
 +67 Elec Pole 6.5 Lts
 +58 Tree stump 20" Diam 36' Lt.
 +53 small Date Palm 38' Rt.
 +51 small Date Palm 44' Rt.

+50

4.5

- +47 small Date Palm 26' Rt.
 +47 small Date Palm 35' Rt.
 +46 small Date Palm 32' Rt.
 +43 Fan Palm 27' Lt.
 +42 Fan Palm on £
 +41 small Date Palm 24' Rt.
 +26 small Date Palm 24' Rt.
 +09 olive Tree 43' Rt.
 +09 Olive Tree 33' Rt.

35

7.4

42.69

LT.

£

RT.

33

6.0	5.4	5.1	5.1	5.1	3.1	3.1	2.0	1.6	0.4
50	35	20	15	7	5	5	15	20	50

7.2	6.7	7.0	6.9	6.8	5.4	4.5	3.6	2.6	2.3	0.0
50	35	20	15	9	8	8	10	15	20	50

8.8	8.0	8.3	8.3	4.2	7.7	7.4	5.7	5.3	2.1
50	35	20	15	6	5	5	15	20	50

42.69

€

T.P. 5.36 46.40 1.65 41.04

- +63 Large Fan Palm 38' Lt.
- +01. Large Fan Palm 3' Lt

37 1.3

- +70 Large Fan Palm 38' Lt.
- +76 Large Fan Palm 2' Lt.
- +54 Tree stump 16" Diam 37.5 Lt.

750 2.2

- +45 Small Date Palm 7' Rt. Boxed.
- +34 Large Fan Palm 37.5' Lt.
- +38 Large Fan Palm 1' Lt.
- +23 Tel Pole Lt.
- +22 Tree stump 18" Diam 37' Lt
- +18 Small Date Palm 5' Rt
- +14 Large Date Palm 5' Rt
- +11 small Date Palm 5' Rt.
- +05. Large Fan Palm 37 Lt
- +05. Large Fan Palm on €

42.69

36

Lt

€

Rt.

34

Nails in Elec Pole #79031 Sta 3722

38	3.3	3.0	3.0	3.2	7.8	1.3	0.8	0.5	+1.3
50	36	20	16	8	5		15	20	50.

4.6	4.1	4.0	4.0	4.2	2.4	2.2	1.4	1.1	+0.9
50	36	20	15	7	5		15	20	50

42.69

L

LT

R

RT

36

T.P. 0.63 43.02 4.01 42.39

Nail Pole

+19 Elec Pole 5' RT.

43 5.7

7.4 6.3 6.7 6.7 6.7 5.7 5.8 5.4 4.4
50 36 20 15 2 15 20 50

+50 5.3

7.1 6.3 6.2 6.2 6.1 5.3 5.0 4.9 4.4 3.8
50 37 20 15 2 8.5 15 20 50
fence fence

42 5.2

6.5 6.0 5.8 5.8 5.8 5.2 4.4 4.4 3.4
50 38 20 15 2 15 20 50

+50 4.6

6.3 5.6 5.4 5.4 5.4 4.6 3.6 3.6 2.8
50 38 20 15 3 15 20 50

41. 4.7

6.2 5.6 5.3 5.3 5.3 4.7 3.9 3.8 3.6
56 39 20 15 3 15 20 50

+50 4.8

3.7 5.3 5.0 5.0 5.3 4.8 4.6 4.2 4.2 4.0
50 40 20 15 3 5 15 20 50
fence fence

+20 Elec Pole 2.5 RT.

40 4.6

5.6 5.6 5.3 5.0 5.0 5.0 4.4 4.6 4.0 4.0 3.4
50 42 40 20 15 4 3 15 20 50

46.40

46.40

E

46

13.0

9.5	9.5	12.0	13.0	13.0	13.0	13.0	13.0	13.0	13.5	
50	28	26	20	15				15	20	50

+85

12.2

5.5	6.1	11.5	12.1	12.1	12.2	11.4	8.2	8.7	7.5
40	28	26	20	15		11	15	20	50

+70

11.5

5.3	5.8	11.2	11.3	11.3	11.5	10.8	5.5	5.5	5.6
50	31	27	20	15		12	15	20	50

+50

10.4

5.1	5.6	10.3	10.2	10.2	10.4	10.4	9.7	5.3	5.3	5.3	5.4
50	31	24	20	15		6	9	14	25	20	50

fence

45

7.9

4.5	5.0	8.0	7.7	7.7	7.9	6.8	3.8	4.0	4.0	4.0
50	32	30	20	15		9	12	15	20	50

+50

5.5

4.6	4.3	5.5	5.5	5.5	5.5	5.2	3.4	3.5	3.5	3.6
50	31	30	20	15		9	13	15	20	50

44

4.6

4.0	4.0	4.4	4.4	4.4	4.6	4.6	3.4	3.3	2.5
50	33	32	20	15		8	15	20	50

+50

3.2

3.9	4.0	3.5	3.5	3.2	3.2	2.7	2.1
50	36	20	15		15	20	50

fence

43.02

43.02

±

Lt.

±

Rt

38

+75

4.7

12.3	11.3	5.0	4.7	4.7	4.3	5.6	9.2	10.5	10.0	4.2
50	30	20	15		13	15	20	23	40	50

+70

4.7

10.3	7.4	5.0	4.7	4.7	4.3	5.6	9.2	10.5	10.0	5.5
50	30	20	15		13	15	20	23	42	50

+55

4.6

5.0	7.5	5.2	4.7	4.6	4.5	6.2	9.0	10.3	7.8
9.7	33	20	15		13	15	20	25	50

+50

4.6

13.0	7.5	5.2	4.7	4.6	4.5	6.2	9.0	10.3	9.8
50	33	20	15		13	15	20	25	50

47.

4.1

13.3	11.7	4.2	4.2	4.1	3.8	7.1	9.5	9.2
50	31	20	15		11	15	20	50

+76 Eucalyptus Tree 30" Diam 46' Lt.

+50

2.8

7.0	8.4	2.8	2.8	2.8	2.8	2.5	6.0	8.5	7.0
50	32	22	20	15		10	15	20	50

+30 Eucalyptus Tree 36" Diam 31' Lt.

+25

1.9

0.4	1.5	1.7	2.0	1.9	1.8	5.2	7.3	8.6
50	35	20	15		10	15	20	50

T.P. 0.65 30.89 12.78 30.24

+08 Eucalyptus Tree 20" Diam 32' Lt

+03. Elk Pole 16' Rt.

43.02

30.89

fence

£

Lt.

£

Rt.

39

•TP. 3.47 29.92 4.44 26.45

+67 Elec Guy Pole 28' Lt.

+64 Elec Pole 22' Rt

+50

13.2	12.5	10.2	7.5	4.5	4.5	4.4	4.2	7.3	7.3	2.8
50	24	20	15	11		15	20	23	30	50
							Fence			

+37² E. side Culvert. see Page 25 4.4
section at 84° 10' to £

13.0	12.5	12.0	4.4	4.4	4.4	4.4	11.4	9.4	2.4
50	20	15	10.5		15	15.5	20	25	50

+36⁶ E. side culvert. 12.0
section at 84° 10' to £

13.0	12.5	12.4	12.4	12.0	12.0	12.0	11.4	10.0	2.4
50	20	15	10.5		15	15.5	20	25	50

+27.8 W. side Culvert. 12.0
section at 84° 10' to £

12.8	12.3	12.0	12.0	12.0	12.0	12.0	11.2	7.5	2.4
50	20	15	11.5		15	20	28	31	50

+27.4 W. side Culvert. 4.4
section at 84° 10' to £

12.8	12.3	9.0	4.4	4.4	4.4	12.0	11.2	7.5	2.4
50	20	15	11.5		15	20	28	31	50

48. 4.6

13.0	12.6	9.0	4.7	4.6	4.1	5.0	11.0	11.0	4.7	2.0
50	24	20	15		13	15	20	31	40	50
							Fence			

+96 Tree stump 30" Diam 8' High 47' Lt

+89 Tree stump 24" Diam 12' High 42' Lt

+77 Tree stump 36" Diam 10' High 47' Lt

30.89

30.89

L

LT

L

RT

40

T.P. Nails in Elec Pole

4.60

25.32

19' Lt. of sta 50+21

+50

5.12

15.8	12.0	9.7	5.6	5.2	5.6	5.6	5.1	+0.8	+6.6	+9.2
30.	25	20	15		15	20	28	38	42	50

+20 Elec Guy Pole 19' Lt.

+13 Elec Pole 32' RT.

50

4.5

9.7	5.7	5.4	5.1	4.5	4.7	4.5	4.4	0.7	+7.3	+8.0
50.	40.	20.	15.		15.	20.	24.	29.	31.	50.

+50

4.0

7.8	7.5	6.6	4.0	4.0	4.1	3.7	0.4	0.0	+5.6	+5.8
50	20	15	11		15	20	27	34	35	50

49.

3.9

10.5	10.5	7.2	4.3	4.7	4.1	3.2	3.9	3.7	3.5	+1.5	+1.0
50	43	40	30	20	15	13		15	20	26	50

29.92

29.92

xsec Girard St.
 Center N/4 To edge of Ex. paving.
 See 1520-14 xsec for 60' St. 10' ch
 W side Girard = West 10' 1/2"

Moore 8-7-36

Indexed
 C.S.K.

154.11

Top cb 7+00	11.58	154.11	142.53	W side Girard
7+00 - S/4 end of Ex. pav. See 1520-14				
W ground	11.7		142.4	
cb top	11.58		142.53	
90° par.	12.34		141.77	
1/4 "	12.25		141.86	
" "	12.25		141.76	
1/2 "	12.37		141.74	
cb "	12.29		141.82	
E = 50' of W side pav	12.34		141.77	
+24 90° pav	12.34		141.77	
+24 cb top	11.53		142.58	
7+50				
-24 bot Cobble wall	11.0		143.1	
-10 "	10.7		143.4	
E	10.3		143.8	
cb	10.2		143.9	
1/2	9.8		144.3	
"	9.5		144.6	
1/4	9.6		144.5	
cb	9.5		144.6	
W	9.3		144.8	
7+75				
W	8.3		145.8	

cb	8.2	145.9
1/4	8.1	146.0
"	8.2	145.7
1/2	8.9	145.2
cb	9.3	144.8
E	9.4	144.7
+8	9.4	144.7
+10	10.2	143.8
+24	11.0	143.1
8+00		
-24	10.8	143.3
-12	10.1	144.0
-8	8.2	145.7
E	8.3	145.8
cb	8.2	145.9
1/4	8.0	146.1
"	7.4	146.5
1/2	7.3	146.8
cb	7.2	146.9
W	7.3	146.8
8+25		
W	6.3	147.8
cb	6.5	147.6
1/2	6.8	147.3
"	6.8	147.3
1/4	7.0	147.1

cb	7.4	146.9
E	7.4	146.9
+9	7.6	146.7
+14	9.2	144.9
+24	10.8	143.3
8+50		
-24	9.5	144.6
-20	8.1	146.0
-10	9.3	144.8
-7	6.6	147.5
E	6.2	147.8
cb	6.3	147.8
1/4	5.8	148.3
c	5.7	148.2
1/4	5.8	148.3
cb	5.6	148.5
W-	5.2	148.9
8+75		
W	3.8	150.3
cb	4.3	149.8
1/4	4.1	150.0
c	4.2	149.9
1/4	4.4	149.7
cb	4.4	149.5
E	5.4	148.7
+6	5.8	148.3

E +9	9.5	144.6
+24	8.0	146.1
9+00		
-24	7.5	146.6
-5	8.4	145.7
-2	4.1	150.0
E	4.0	150.1
cb	3.0	151.1
1/4	2.7	151.4
c	2.4	151.5
1/4	2.4	151.7
cb	2.7	151.4
W	2.6	151.5
9+25		
W	1.2	152.9
cb	1.5	152.6
1/4	1.0	153.1
c	1.1	153.0
1/4	1.4	152.7
cb	2.2	151.9
E	3.6	150.5
+5	4.2	149.9
+9	8.0	146.1
F24	7.1	147.0
TP	10.41	163.6
	1.36	152.75

	9+50		
-24		15.3	147.9
-12		16.4	146.8
-9		11.5	151.7
E		10.6	152.6
cb		10.2	153.0
1/2		9.8	153.4
C		9.4	153.8
1/2		9.3	153.9
cb		9.2	153.8
W		9.2	154.0
	9+75		
W		8.8	154.4
cb		8.4	154.6
1/2		8.7	154.5
C		8.5	154.7
1/2		8.3	154.9
cb		8.8	154.4
E		9.3	153.9
+6		9.8	153.4
+10		13.7	149.5
+16		14.2	149.0
+20		12.0	151.2
+24		13.2	150.0
	10+00		
E - 24		13.0	150.2

E - 11		13.2	149.6
- 5		8.8	154.4
E		8.4	154.8
cb		7.3	155.9
1/2		7.1	156.1
e		7.2	156.0
1/2		7.5	155.7
cb		7.8	155.4
W		8.0	155.2
	10+27		
W		6.2	157.0
cb		6.2	157.0
1/2		5.9	157.3
C		5.9	157.3
1/2		5.7	157.5
cb		5.4	157.8
E		9.0	156.2
	10+52		
	10 Top cobble wall	8.2	154.6 at 2' in Cobble d. 1/2"
	10+52		
E		5.0	158.2
cb		4.2	159.0
1/2		4.7	158.5
e		4.9	158.3
1/2		5.0	158.2
cb		5.0	158.2
W		5.2	158.0

10+74.6

W	4.4	158.6
cb	4.6	158.6
1/2	4.2	159.0
"	4.0	159.2
1/4	3.6	159.6
cb	3.3	159.9
E	3.5	159.7

See 1524 for levels on intersection
of Center + Girard. wch

ch. to DP L.H. 158.75 158.75
Girard + Center

Note! Construct cobble slope wall &
cut bottom from 7.00 to 10.27 to complete
cobble storm ditch.

Levels on BIKs 18+19

New San Diego

B.M. U.S. Coast. + Geodetic Datum.

New Harbor Dept. B.M.

B.M. RR spike 4.30 15.10

W. Line Kettner

S. curb. Market } = W. End. Ret. 4.79

" " " " " " 5.33

S. Line Market

W. curb. Kettner } = S. End. Ret. 5.16

" " " " " " 5.57

T.P. 5.33 15.80

S. E. Cor BIK. 18 =

N. W. " Kettner + Belt. Sts. 4.8

N. Line Belt. & Calif. 4.0

T.P. 5.57 17.34

S. W. Cor. BIK. 19 =

N. E. " Belt + Pacific 3.9

E. Line Pacific S. E. Market 5.47

" " " " " " 5.84

T.P. 3.12

chk. B.M. B.R. S. E. Market } ~~3.09~~

W. Line Cal. S. E. Market } = W. End. Ret. 5.39

" " " " " " 5.89

10-10-36

Miller

Walker

Bliss

Eug. Fols

S. E. Market

+ California

Top. ch

gutter

Top. ch

gutter

ground

"

Top. curb

gutter

Top. ch

Gutters

Top. E. B

Grating

14.99

47

S. Line Market. W. ch

Calif. = S. End. Ret } 5.43

" " " " " " } 5.73

S. Line Market. E. ch

Calif. = S. End. Ret } 5.36

" " " " " " } 5.44

S. curb. Market. E. Line

Calif. = E. End. Ret } 5.26

" " " " " " } 5.81

P.I. E. curb. Calif. &

S. E. Market = S. E. } 6.06

Cor. Catch Basin Grating } 8.93

chk. Orig. B.M.

4.19

10.80

N.B. The grade of Belt. St. is to be about 2.0' above the grade of Market. St.

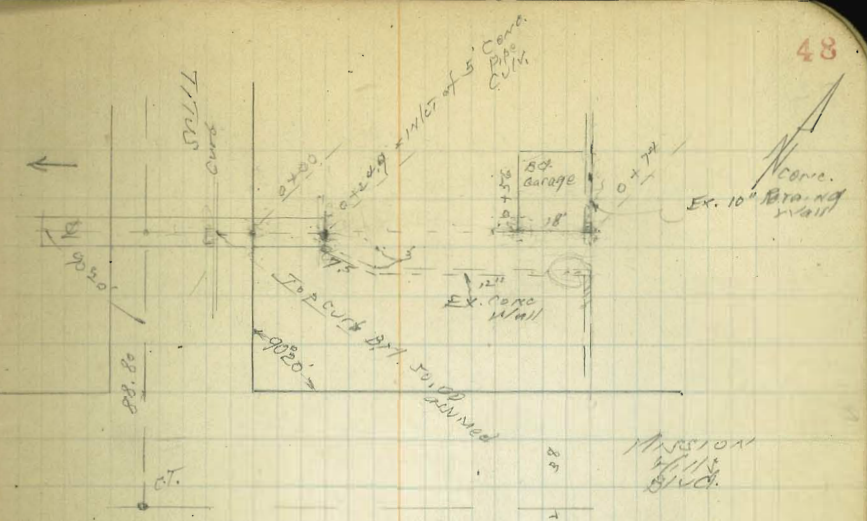
acc. to H. Bub.

$$\frac{3.12}{\cancel{3.12}} + \frac{9.01}{\cancel{9.01}} = 12.20 \quad \text{diff.} = 0.295$$

Moore
1-18-37

Indexed
C.S.K.

Levels for Prop. Retaining Wall
on Titus rly from Mission Hill Blvd



0+74

12	38	46.7	46.7	42.3	42.7	47.4
		$\frac{7.1}{4}$	$\frac{7.1}{4}$	$\frac{11.5}{0.5}$	$\frac{11.1}{5}$	$\frac{6.4}{5}$
		48.4	47.2	45.8	41.8	41.6
		$\frac{5.2}{5}$	$\frac{6.4}{5}$	$\frac{8.0}{2}$	$\frac{12.0}{5}$	$\frac{12.2}{5.7}$
						$\frac{9.0}{5.7}$

0+50

0+25

47.2	44.3	43.0	40.5	40.5	44.5	44.9
$\frac{6.0}{3}$	$\frac{9.5}{2}$	10.8	$\frac{13.3}{3}$	$\frac{12.3}{5.7}$	$\frac{9.3}{5.7}$	$\frac{8.9}{6}$

0+97

47.5	45.0	44.3	40.1	40.1	44.3	46.1
$\frac{6.3}{4}$	$\frac{8.3}{5}$	$\frac{9.5}{7}$	13.7	$\frac{13.7}{2.7}$	$\frac{9.5}{4.7}$	$\frac{7.7}{6}$

90° = 1/2 INLET of 5" Conc. Pipe

47.7	44.8	39.8	39.4	44.5	47.5
$\frac{6.1}{5}$	$\frac{9.0}{5}$	$\frac{14.0}{5}$	14.4	$\frac{9.3}{2.5}$	$\frac{6.3}{4}$

00-1

47.7	44.8	44.9	44.8	47.5
$\frac{6.1}{5}$	$\frac{9.0}{4}$	8.9	$\frac{9.0}{2}$	$\frac{6.3}{4}$

075

1375

50.00

assumed 2' face of ex. 10' wall

2 Cols.

1/2 INLET

53.75

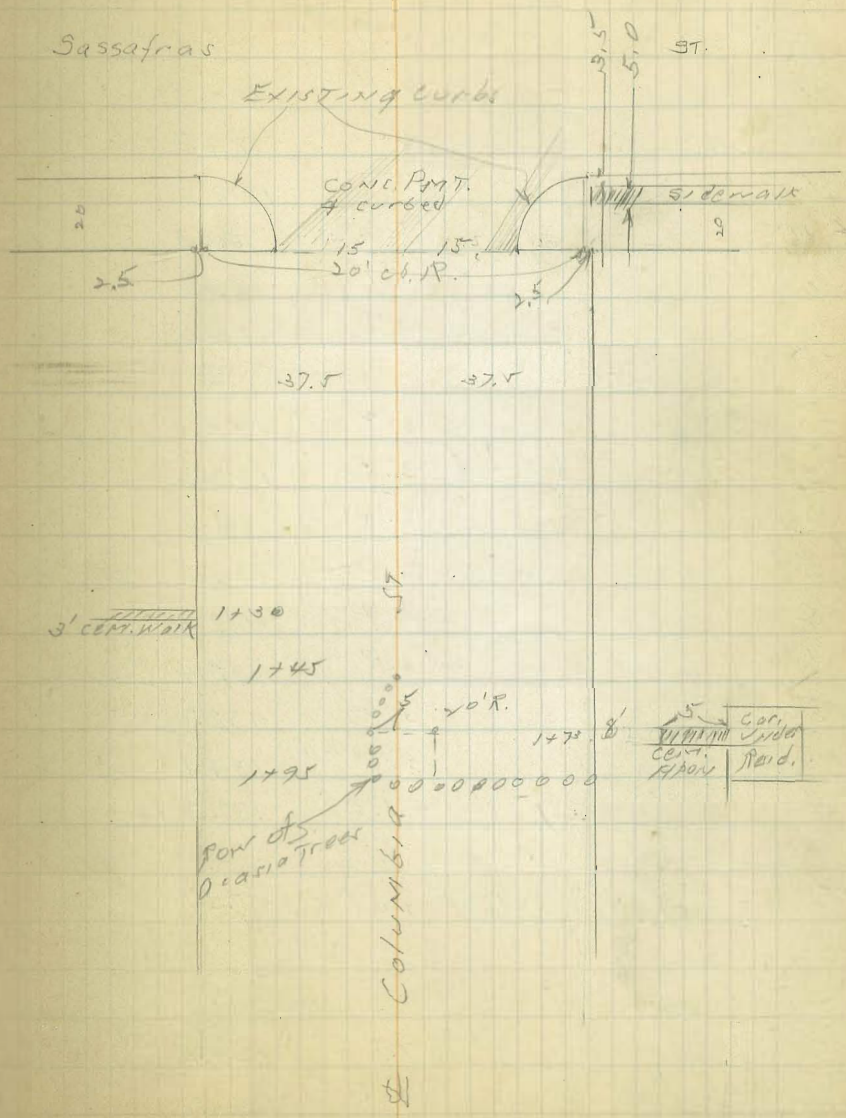
xsec of Columbia St. 75' wide
 22.5 cbr
 7.5 1/4"
 Sassafras Sy to Spruce

MWBSP	0.75	167.07		166.32	STATE Sassafras
T.P.	0.40	154.27	13.20	153.87	
T.P.	0.57	142.40	12.44	141.83	
T.P.	5.00	136.26	11.14	131.26	

0-10					
E cb TOP		9.47		126.79	
" 90T pav		9.93		126.33	
C "		10.53		125.73	
W 90T "		11.73		124.53	
W cb TOP		11.23		125.03	
00 = SL Sassafras St.					
W		13.2		123.1	
+10		11.0		125.3	
W cb TOP		10.22		126.04	
90T pav.		10.75		125.51	
1/2 "		10.35		125.91	
" "		10.09		126.17	
1/4 "		9.87		126.39	
90T "		9.71		126.55	
E cb TOP		9.29		126.97	
+18		6.2		130.1	
E		4.4		131.9	

Moore
 S. 2500
 North
 2-5-37
Raining like Hell

Indexed
 C.S.K.



0425

E	3.2	133.1
+u	4.9	131.4
cb	6.4	129.9
1/4	6.6	129.7
C	7.1	129.2
1/4	5.0	131.3
cb	4.1	132.2
W	9.7	126.6

0450

W	6.2	130.1
+17	2.5	133.8
cb	1.8	134.5
1/4	2.0	134.3
E	2.9	132.4
1/4	3.9	132.4
cb	3.0	132.7
+17	2.2	134.1
E	+1.0	137.3

TP 10.04 145.61 0.69 135.57

0475

E	7.5	138.1
+u	9.5	136.1
cb	10.7	134.9

1/4	11.2	134.4
C	11.4	134.2
1/4	9.9	135.7
cb	9.6	136.0
W	12.5	133.1
+5	13.5	132.1

1400

-5	13.1	132.5
W	12.1	133.5
cb	9.7	135.9
1/4	9.1	136.5
C	9.1	136.5
1/4	9.0	136.6
cb	8.5	137.1
+18	7.5	138.1
E	5.4	140.2

1425

E	2.1	143.5
+5	4.8	140.8
cb	5.9	139.7
1/4	5.9	139.7
C	6.4	139.2
1/4	7.5	138.1
cb	8.7	136.9
W	12.0	133.6
+5	12.8	132.8

1450

W	± of 5' cent. walk	12.9	133.42
1450			
W		12.8	132.8
W		11.8	133.8
cb		8.6	137.0
1/4		7.8	137.8
C		3.7	141.9
1/4		3.5	142.1
cb		2.5	142.1
+14		1.7	143.9
T.P.	3.22 147.32 ✓	1.51	144.10
+17		1.3	146.0
E		0.4	146.9

1473

-13	± Gar. floor cent.	0.61	146.71
-8	edge cent. apron	1.30	146.02
E		2.0	145.3
cb		4.5	142.8
1/4		4.6	142.7
C		4.8	142.5
1/4		4.5	142.8
cb		10.3	137.0
W		14.2	133.1
+1		12.4	132.9
+3	40' drop		

2400 Drop off of approx. 35'

-4		12.4	132.9
-2		14.2	133.1
W			
+5		11.5	135.8
cb		9.5	137.8
1/4		8.8	138.5
C		4.8	142.5
1/4		4.2	143.1
cb		4.6	142.7
+13		4.0	143.3
E		0.8	146.5
T.P.	1.52 144.58 ✓	4.26	143.06

2408

E		2.4	142.2
cb		4.5	140.1
1/4		5.6	139.0
C		6.7	137.9
1/4		7.2	137.4
cb		8.0	136.6
W		12.5	132.1
+2		12.8	131.8

2430

-4	Drop off		
W		13.5	131.1

cb	10.6	134.0
1/2	9.3	135.3
c	8.2	136.4
1/2	7.3	137.3
cb	5.5	139.1
E	3.5	141.1

2+70

E	7.0	135.6
cb	11.0	133.6
1/2	11.8	132.8
c	12.7	131.9
1/2	13.3	131.1
cb	15.9	128.7
W	16.3	128.3
+>	16.8	127.8

4 < drop off
3+00 = Top of Cut

- <	20.4	124.2
W	20.1	124.5
cb	18.2	126.4
1/2	17.3	127.5
c	16.2	128.4
1/2	15.8	128.8
cb	14.9	129.7
E	13.3	131.3

3+10

Drop off to NW - Spruce see Grades
of Spruce
Profile

TP	3.02	146.09	1.52	143.06
TP	0.47	136.05	10.51	135.58
ch to Ecb	SL	126.97	9.08	126.97

4+00			
S		4.3	64.7
+J		4.6	64.4
C		4.7	64.3
N		4.6	64.4
4+01			
N	-2 Sin. gar. dist floor	2.80	66.22
N		2.8	66.2
C		3.1	65.9
S		3.1	65.9
4+01			
S		2.4	66.4
C		2.5	66.5
N		2.4	66.6
	+1 Sin. gar. dist floor	2.4	66.6
4+79			
N		1.2	67.8
C		1.2	67.8
S		1.1	67.9
	+30 Sin. gar.	0.1	68.9
T.P.	11.00 79.56 0.46		68.56
4+00			
S		11.0	68.6
C		11.0	68.6
N		10.9	68.7

4+50			
-9	W edge Car.	9.0	70.3 door coated
N		9.0	70.6
C		9.1	70.5
S		9.1	70.5
4+84			
S		7.7	71.9
C		8.0	71.6
N		8.2	71.4
	+9 Ely edge dwelling	8.5	71.1
4+00			
N		7.5	72.1
C		7.4	72.2
+6		7.4	72.2
S		6.7	72.9
4+50			
S		5.4	74.2
C		5.6	74.0
N		5.8	73.8
4+90			
N		3.9	75.7
C		3.7	75.9
S		3.7	75.9
	6+04.20 Wly La Jolla Blvd		
306		2.61	76.95
S par		2.82	76.74

c par.	1.03	76.53
N "	2.22	76.84
1/2 ob ob	2.51	77.05

6 + 24.3 = W 907. L. J. Blvd.

N par	2.28	76.28
c "	2.01	76.25
s "	2.28	76.18

check to B.M.	1.08	78.48	78.48
			000

Charles ST 50' wide
Level
Catalina to Silvergateindexed
C.S.K.

286.07

57

BM #	VAIRO IN POB	I.02	276.04	271.02	Catalina char.
					00-30 = Fly edge pav. Catalina
N	par.		10.20	265.84	
C	"		9.88	266.16	
S	"		9.40	266.64	
					0+00 = Ely Catalina
S			8.5	267.8	
C			9.5	266.5	
N			10.1	265.9	
					0+50
N			7.2	268.8	
C			7.5	268.5	
S			6.3	269.7	
					1+00
S			3.6	272.4	
C			4.3	271.7	
N			4.5	271.5	
T.P.		11.23	286.07	1.40	274.67
					1+45
					3' W. CORN. WALK ON S. S' W ST.
			9.84	276.23	
					1+50
S			9.9	276.2	
C			10.9	275.2	

N			11.2	274.8	
					2+00
N			7.5	278.6	
C			7.4	278.8	
S			4.1	280.0	
					2+50
S			2.6	283.5	
C			4.0	282.1	
N			4.5	281.6	
					3+00
N			1.2	284.9	
C			0.9	285.2	
S			+0.4	286.5	
T.P.	1280	298.38	0.49	285.58	
					4+50
S			9.0	288.4	
C			10.1	288.3	
N			10.2	288.0	
					2+00
N			7.0	291.4	
C			7.0	291.4	
S			5.5	292.9	
					4+50
S			2.2	296.2	

C			4.4	294.0
N			4.1	294.3
	5+00			
N			1.7	296.7
C			1.9	296.5
S			0.2	298.2
T.P.	8.94	306.24	1.06	297.32
	5+50			
S			5.9	300.4
C			7.4	298.7
N			7.5	298.8
	6+00			
N			6.0	300.3
C			5.9	300.4
S			4.0	302.3
	6+50			
S			2.7	303.6
C			4.7	301.8
N			4.6	301.2
	6+75			
N			4.7	301.6
C			2.5	301.8
S			2.6	303.7

	6+99			
	cent. 1' in st.			
	2' wide walk		5.12	301.14
	7+00			
S			2.9	303.4
C			4.7	301.6
N			5.1	301.2
	7+26			
N			5.2	301.0
C			5.0	301.0
	+15 Top of Top step		4.31	301.95
	+18 " of Top step		3.42	302.84
S	on cent walk		5.23	303.03
	7+50			
S			4.1	302.2
C			6.2	300.1
N			6.2	300.1
	8+00			
N			8.0	298.3
C			8.4	299.9
S			6.2	300.1
	8+42			
S			8.2	298.1
C			10.4	295.9
N			10.8	295.5
	8+46			
N			11.5	294.8

2' wide
cent
steps
walk

C		10.6	295.9	
S		11.0	295.3	
	8 + 07.45 = wly Silvergate			
S		11.7	294.6	
C		12.0	294.3	
N		13.5	292.8	

FP 3.03 297.84 11.45 294.81

E Silvergate to 50.

N		6.4	291.2	
C		5.8	292.0	
S		5.1	292.7	

C + 19 = 6" curb on Ely Silvergate

S	top cb	4.85	293.02	
C	on S.P. end cb	5.11	292.73	292.70
N		6.4	291.4	

Wilcox St Level 50' wide
Silvergate wly 256.10

B.M. B.P. 4.37 299.10 294.73

00 - 25 = 2 Silvergate

S	13.8	283.3
C	14.5	282.6
N	15.1	282.0

0 + 00 = wly Silvergate

N	13.0	284.1
C	12.5	284.6
S	11.3	285.8

0 + 50

S	8.4	288.7
C	10.3	286.8
N	10.1	287.0

1 + 00

N	7.0	289.5
C	8.2	288.9
S	6.0	291.1

1 + 50

S	4.9	292.2
C	6.8	290.3
N	6.9	290.2

2 + 00

N	7.4	289.5
C	6.7	290.4

Indexed 297.10
C.S.K.

60

S	4.0	292.5		
J	5.8	291.3 ✓		
C	7.3	289.7		
N	10.4	286.7		
T.P.	0.54	285.47	2.17	284.93

Jennings St. Levels 50' wide
 Silvergate Wly 255.10

Indexed
 c.s.k. 273.82

285.47

00-25 = I Silvergate

S	9.4	276.1
C	9.6	275.9
N	11.1	274.7

1750

N	11.0	262.8
C	8.7	265.1
S	6.7	267.1

00 = Wly Silvergate

N	14.4	271.1
C	12.4	273.1
S	11.7	273.8

2400

S	10.9	262.9
C	11.8	262.0
N	14.5	259.3

T.P. 1.51 273.82 13.10 274.31

255.1

N	16.8	257.0
C	15.0	258.8
S	12.3	260.5

0+35

S	4.7	269.1
C	3.7	270.1
N	4.7	269.1

check to BM. 2x3 Hub
 of JOSEPHSTEIN

13.45	260.37	260.33
		0.06

0+75

N	6.8	267.0
C	5.2	268.6
S	5.7	268.1

1+00

S	4.7	269.1
C	6.1	267.7
N	8.0	265.8

Levels on Ex. Pav. on Curve

Indexed
c.s.K.

10' LT

±

10' RT

0+00
45+50.29
Intersection of
Catalina + Canon St.
Moore 3-27-37

+50 7° 09.78'

4 5° 49.78'

D = 440° 39' 30" RT.
± P = 1000
T = 4107.2
L = 779.43
def 1' = 1.7185

+50 4° 17.83'

1 2° 51.89'

0+50 1° 25.94 RT

BC = 00 = 45+50.29

00-50

BM #7
SPIRE FENCE
POST
40 27.04
48 4.00
7.43 253.02 245.59

$\frac{48.01}{5.01}$ $\frac{42.56}{5.44}$ $\frac{41.10}{5.92}$ 46

$\frac{48.21}{4.81}$ $\frac{42.79}{5.23}$ $\frac{41.28}{5.74}$ 51

$\frac{48.67}{4.25}$ $\frac{48.25}{4.79}$ $\frac{47.74}{5.28}$ 51

$\frac{49.19}{4.83}$ $\frac{48.89}{4.13}$ $\frac{48.40}{4.62}$ 49

$\frac{50.03}{2.99}$ $\frac{49.72}{3.30}$ $\frac{49.26}{3.76}$ 46

$\frac{50.99}{2.03}$ $\frac{50.79}{2.23}$ $\frac{50.42}{2.48}$ 37

$\frac{52.02}{1.0}$ $\frac{52.07}{0.95}$ $\frac{51.84}{1.18}$ 73

253.02
7

0 17° 11.33°

51.92
1.05

51.68
1.34

51.25
1.77

.43

+50 15° 45.38

51.39
1.63

51.05
1.97

50.64
2.38

.41

5 14° 19.44'

50.51
2.51

50.16
2.86

49.72
3.30

.447

+50 12° 53.49'

49.51
3.51

49.18
3.84

48.75
4.27

.43

4 11° 37.55'

48.76
4.26

48.44
4.58

48.06
4.96

.35

+50 10° 01.61'

48.21
4.81

47.88
5.14

47.47
5.55

.41

3 + 15

48.05
4.97

47.72
5.30

47.23
5.79

.45

3 8° 35.66'

48.07
4.95

47.62
5.30

47.16
5.86

.48

1 253.02

253.02
2

Levels on Ex. Pav. on
Catalina Blvd. Sly Production
of " " rily to Talbot.

Indexed
e.s.k.

10' LT

2

10' RT

64

+50

$\frac{48.38}{4.64}$

$\frac{48.55}{4.49}$

$\frac{48.36}{4.66}$

+16.5

$\frac{48.37}{4.65}$

$\frac{48.60}{4.52}$

$\frac{48.40}{4.62}$

$\frac{48.35}{4.67}$

$\frac{48.48}{4.58}$

$\frac{48.42}{4.60}$

+49.5 x 36" Corr. I.P.C.V. 90°

$\frac{44.24}{4.78}$
25

$\frac{47.92}{5.10}$
25 Handrail

$\frac{48.35}{4.67}$

$\frac{48.48}{4.62}$

$\frac{48.33}{4.69}$

$\frac{40.87}{12.15}$
65 FL

$\frac{48.42}{4.60}$

$\frac{48.44}{4.58}$

$\frac{48.20}{4.82}$

+50

$\frac{48.91}{4.11}$

$\frac{48.71}{4.31}$

$\frac{48.28}{4.74}$

$\frac{49.38}{3.64}$

$\frac{49.09}{3.95}$

$\frac{48.64}{4.38}$

$\frac{50.06}{2.96}$

$\frac{49.72}{3.25}$

$\frac{49.30}{3.72}$

0+50

B.C. = 00

253.02

253.02

5 + 89 = end of Pav.

+ 50

5

+ 50

4

3 + 71.8

Note! Some of this paving
 will have to come out and
 be raised - c.s.j.t.
 only serves as a ramp to
 meet paving on Curve
 on Canyon St and Catalina.

18" Corr. 1. P. Cutv. Note! Cutv. on A

Please figure A

253.02

49.35
3.27

49.40
3.27

49.35
3.27

48.52
4.50

48.68
4.34

48.58
4.42

48.39
4.28

48.50
4.50

48.40
4.42

48.39
4.63

48.53
4.49

48.42
4.40

48.39
4.63

48.55
4.47

48.39
4.63

FL. 44.67
8.35
31

45.17
7.85

47.44
5.58

23 = FL

23 = Headwall

253.02
253

Catalina Blvd. + Canyon St
 Layout of Alig. of Ex (Morse)
 State Paving

Indexed
 C.S.R.

Talbot St.

66

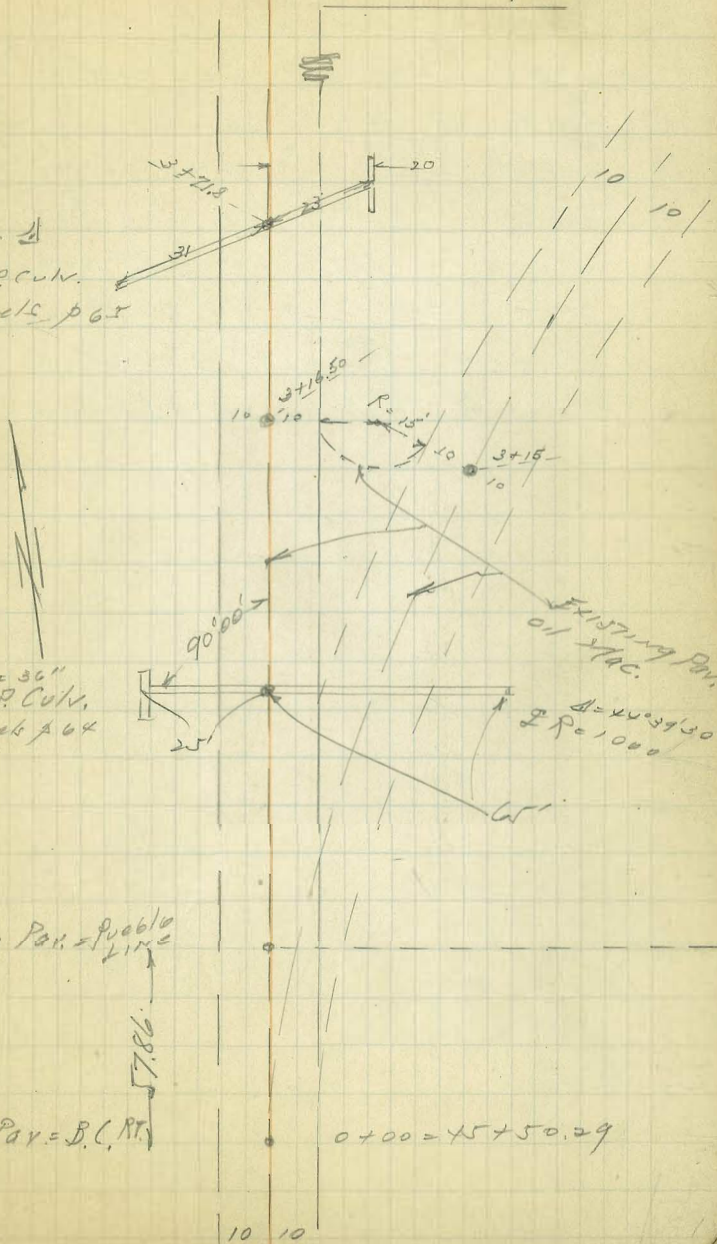
Please fig. 2

18" Corr. I.P. Culv.
 See levels p 65

2 + 49.5 = 36"
 Corr. I.P. Culv.
 See levels p 64

Splice in Pav. = Pueblo
 Line

Splice in Pav. = B.C. RT.



10 10

Moore
3-27-27

Location of 8" curb
and Pav. on Ely side of
Locust St. Southly of
Zola St. Private Contract

Note! Meas. of 9.85 meets
end of Existing 4" curb on
Sly line of Zola St. and is
parallel to Ely line of Locust St.

Indexed
C.S.K.

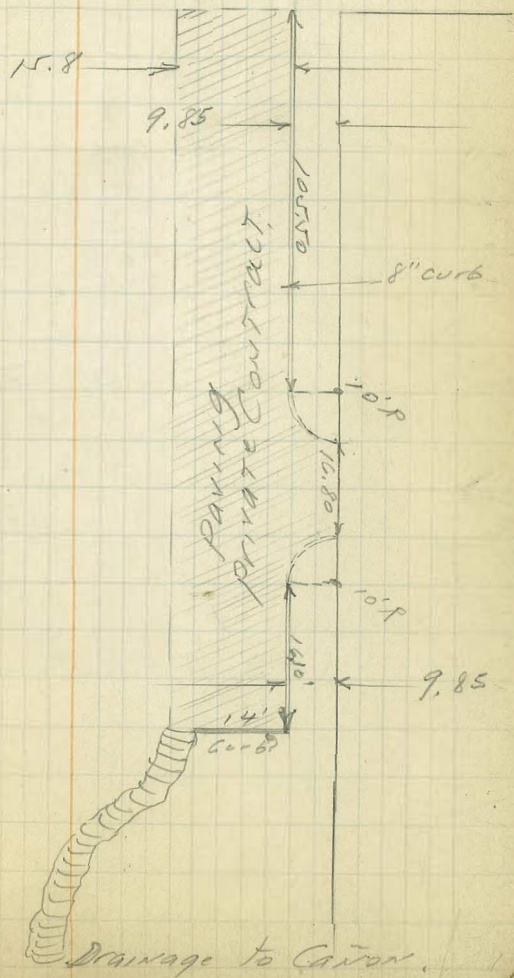
67



Locust St.

Ely of
Locust
St.

Zola St.



Locust St Levels Indexed
 S of Zola Block Pav. c.s.kr

NWBP	11.91	38.38		26.47	Restaurants Zola
TP	12.36	50.15	0.59	37.79	
TP	14.05	62.25	0.55	49.60	
T.P.	12.52	74.21	0.56	61.69	
T.P.	6.91	80.79	0.33	73.88	

1/4 Zola=00

E Top cb		3.71		77.08	
E gut pav		4.31			
+15.8 "		3.12			
0+05					
E cb		3.38			
gut pav		3.87			
+15.8		3.13			
0+10					
E cb		3.18		77.61	
gut		3.79			
+15.8		3.32			
0+15					
E cb		3.17			
gut		3.77			
+15.8		3.47			
0+20					
E cb		3.28		77.51	

80.79

E gut	3.84	
+15.8	3.57	
0+20		
E cb	4.65	
gut	4.23	
+15.8	4.05	
0+60		
E cb	4.05	76.74
" gut	4.54	
+15.8	4.54	
0+80		
E	4.60	76.19
gut	5.18	
+15.8	5.05	
1+00		
E cb	5.12	75.67
gut	5.81	
+15.8	5.67	
1+05.5 RC cb		
E cb	5.48	75.1
gut	6.03	
+15.8	5.99	
1+15.5		
E.L. cb	6.09	
" gut	6.67	
E cb pav	6.54	
+15.8	6.72	

1+42.3

E L cb	6.58
" gut	6.84
E cb par	7.46
+15.8 "	7.59

1+42.3 cb p.c.

E cb	7.74
" gut	8.17
+15.8	8.20

1+58.4 * end par

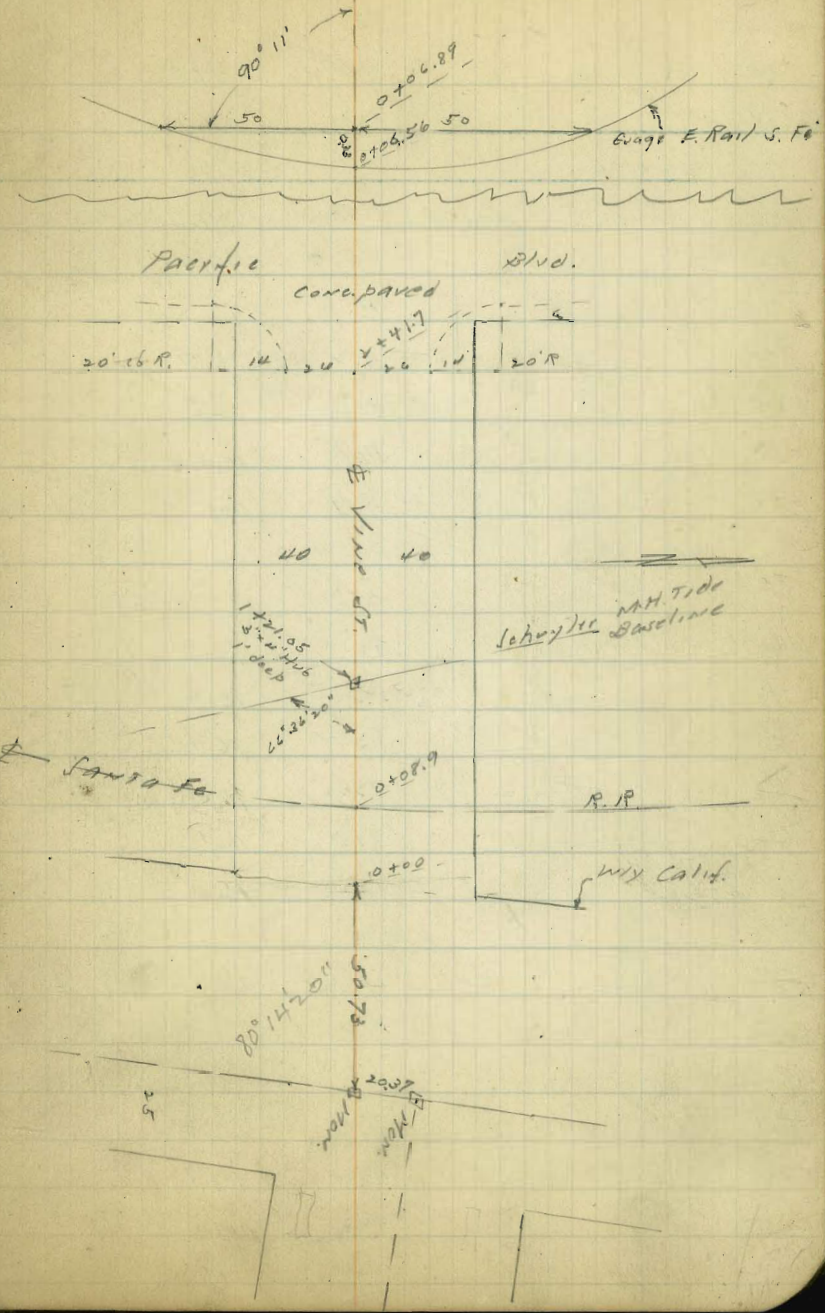
E cb	8.67	72.14
gut	9.00	
+14 top cb end	8.77	
+15.8 par	9.15	

Moore X sec of Vine St 80' wide Indexed
 19-37 Calif. to Pacific 12' cbs 10' / 1/2 csk.

S.E. BP. 0.73 20.31 39.58 Vine
 Kettner
 T.P. 0.49 28.28 12.72 27.59

0+100 = Wly Calif.

N.	4.9	21.4
cb	6.8	21.5
1/4	6.8	21.5
c	6.8	21.5
1/2	6.6	21.7
cb	6.6	21.7
S	6.9	21.4
0+06.56 = E Rail S. F. RR.		
S	5.14	23.14
c	5.17	23.11
N	5.20	23.08
0+11.88 = W Rail		
N	5.39	22.89
c	5.33	22.95
S	5.31	22.97
0+19		
S	6.8	21.5
cb	6.7	21.6
1/4	6.8	21.5
1/2	7.1	21.2
1/4	7.7	21.1



cb			7.3	21.0
N			7.1	21.2
	0+40			
N			10.7	17.6
cb			10.9	17.4
1/2			11.0	17.3
c			11.4	16.7
1/2			11.7	16.6
cb			11.8	16.5
S			11.9	16.4
	0+55			
S			12.6	15.7
cb			12.4	15.9
1/2			12.3	16.0
c			12.2	16.1
1/2			12.1	16.2
cb			12.2	16.1
N			12.3	16.0
T.P	2.33	1841	12.20	16.08
	1+00			
N			4.4	13.5
cb			4.6	13.5
1/2			4.6	13.8
c			4.4	13.5

1/2			4.5	13.9
cb			4.5	13.9
S			4.5	13.9
	1+21.05 = Schuyler Baseline			
S			6.4	12.0
cb			6.5	11.9
1/2			6.0	12.4
c			5.6	12.8
1/2			5.1	13.3
cb			5.0	13.4
N			5.3	13.1
	1+50			
N			7.8	10.6
cb			8.0	10.4
1/2			8.1	10.3
c			8.2	10.2
1/2			8.3	10.1
cb			8.5	9.9
S			8.4	9.0
	2+00			
S			8.8	9.6
cb			8.6	9.5
1/2			8.7	9.7
c			8.6	9.8
1/2			8.6	9.8
cb			8.5	9.9
N			8.5	9.9

2+41.7 = end of returns

N		8.2	10.1
cb	Top corr cb.	7.72	10.67
gut	ground	8.4	10.0
1/4	"	8.9	10.1
c	"	8.2	10.0
1/4	"	8.8	9.6
gut	"	8.7	9.7
cb	Top corr cb.	7.79	10.62
N		8.6	9.8

2+42 = edge of Conc. Pav.

N		8.6	9.8
cb	Top cb	7.80	10.61
gut	ON CONC PAV	8.42	9.99
1/4	" " "	8.10	10.31
c	" " "	7.90	10.4.8
1/4	" " "	8.14	10.27
gut	" " "	8.41	10.00
cb	Top cb.	7.75	10.64
N		8.3	10.1

2+41.7 = Ely curb of Pacific

N	TOP cb	8.22	10.19
N	gut ON PAV.	8.84	9.57
cb	ON "	8.73	9.68
1/4	" "	8.64	9.77
c	" "	8.53	9.75

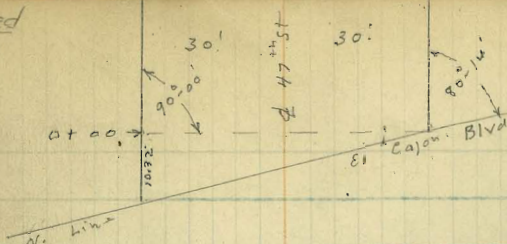
1/4	ON PAV	8.70	9.71
cb	" "	8.85	9.56
N	" " gut	8.99	9.42
N	ON CURB	8.40	10.01

6-4-37
Miller
Walker
Bliss

47th St. X See: El Cajon North

60' wide
12' elev.
9' 1/4 S.

Indexed
C.S.K.



73

6+44
How Walk
on X cut
page 76
OK
R.S.

B.M. B.P. 5.92 353.12 347.20 S.W. El Cajon + 47th St

N Line El Cajon = N. End. conc. Returns & pavnt.

w.	conc. Walk	5.15	347.97
cl	N. end. conc. cl.	5.51	347.61
gutter	pay	6.49	346.63
1/4	"	5.95	347.17
φ	"	5.85	347.27
1/4	"	6.21	346.91
gutter	"	6.27	346.85
E. conc. cl.		5.90	347.22 ✓
E. on conc. Return		5.58	347.54
0+00 = 90°-00' from N.E. Cor.			
E.		5.5	347.6
cl		5.7	347.4
+1		4.0	347.1
1/4		5.8	347.3
φ		5.7	347.4
1/4		5.7	347.4
+8		5.9	347.2
cl		5.4	347.7
w.		5.1	348.0
0+25			
w		4.9	348.2
d		5.0	348.1
+1		5.4	347.7

↑ 353.12

12' S. of N. Line of El Cajon Blvd. = E + W gutter

20.6 W. of φ Produced South =	5.48	347.64
W. cmt. cl. Return		
20.6 W. of φ = gutter {grating of curb inlet}	6.48	346.64
10.3 " " "	6.21	346.91
φ 47 th St. produced South	6.25	346.87
11.7 E. of φ	6.32	346.80
23.4 E. of φ = gutter	6.41	346.71
23.4 E. of φ = E. cmt. cl. Return	5.91	347.21
75 E. of φ N. gutter El Cajon	6.61	346.51

353.12

0+25 (con)

1/4	5.4	347.7
1/2	5.4	347.7
3/4	5.4	347.7
cl	5.4	347.7
E	5.1	348.0

0+50

E	5.3	347.8
W	5.3	347.8
1/4	5.1	348.0
1/2	5.1	348.0
3/4	5.2	347.9
1+6	5.5	347.6
cl	4.8	348.3
W	4.7	348.4

1+00

W	4.7	348.4
cl	4.7	348.4
1/4	4.7	348.4
1/2	4.5	348.6
3/4	4.6	348.5
cl	4.9	348.2
E	4.9	348.2

1+50

E	5.0	348.1
cl	4.8	348.3
1/4	4.7	348.4

353.12

47th

74

E	4.4	348.7
1/4	4.5	348.6
cl	4.6	348.5
W	4.5	348.6

1+60

W = E. End. cnt. walk 3' wide	4.67	348.45
-------------------------------	------	--------

1+98.5

W-1.0 = E. End. cnt. walk 3' wide	4.25	348.87
-----------------------------------	------	--------

2+00

W	4.3	348.8
cl	4.4	348.7
1/4	4.3	348.8
1/2	4.4	348.7
3/4	4.9	348.2
cl	4.9	348.2
E	5.1	348.0

2+38.5

W-1.0 = E. End. 3' walk.	3.85	349.27
--------------------------	------	--------

2+50

E	5.2	347.5
cl	5.2	347.9
1/4	5.0	348.1
1/2	4.7	348.4
3/4	4.7	348.4
cl	4.4	348.7
W	4.1	349.0

2+75

W = E. End. 3' walk	3.81	349.31
3+01.2 = S. Line Meade St		
W	4.1	349.0
el	4.6	348.5
1/4	4.6	348.5
el	4.7	348.4
1/4	4.8	348.3
el	5.0	348.1
E	4.9	348.2

3+40.2 = N. Line Meade St

E	5.3	347.8
el	5.0	348.1
1/4	5.0	348.1
el	4.9	348.2
1/4	4.9	348.2
el	4.8	348.3
W	4.4	348.7

T.P. 2.20 350.36 4.96 348.16

3+52

W = E. End. 4.5' cont. walk 1.48 348.88

3+70

W	1.8	348.6
el	2.3	348.1
+5	2.6	347.8
1/4	2.4	348.0

el	2.5	347.9
1/4	2.8	347.6
el	2.8	347.6
E	2.8	347.6

4+00

+3.	3.8	346.6
E.	4.5	345.9
+8	4.5	345.9
+10	3.6	346.8
el	3.6	346.8
1/4	3.5	346.9
el	3.1	347.3
1/4	3.0	347.4
el	2.7	347.7
W	2.3	348.1

4+34.5

W-0.3 = E. End. cont walk 3.13 347.23

4+50

W	3.8	346.6
el	4.4	346.0
1/4	4.5	345.9
el	4.6	345.8
1/4	5.0	345.4
el	5.0	345.4
E	5.1	345.3
+3	5.0	345.4

350.36

4+55

W-10 of E. End 2 strip ent. drive 3.78 346.58

5+00

E-3. 5.7 344.7

E. 5.7 344.7

cl 5.8 344.6

+2 6.2 344.2

1/4 6.1 344.3

E 6.1 344.3

1/4 5.8 344.6

cl 5.2 345.2

W 5.1 345.3

5+50

W 5.7 344.7

cl 5.9 344.5

1/4 6.5 343.9

E 6.6 343.8

1/4 6.9 343.5

cl 6.9 343.5

E 6.7 343.7

+3 6.7 343.7

5+66

1' W of E. = W. End. 3' ent. walk 6.80 343.56

5+35

24' E. of E = Pepper Tree 24" Diam

5+56

23.5' E of E = Pepper Tree 20" Diam

out. of position

47

76

350.36

6+00

E-3. 7.6 342.8

E 7.1 343.3

+9 7.1 343.3

cl 7.6 342.8

1/4 7.6 342.8

E 7.4 343.0

1/4 7.3 343.1

cl 7.1 343.3

W 6.5 343.9

6+50

W 7.7 342.7

cl 7.7 342.7

1/4 7.6 342.8

E 7.7 342.7

1/4 8.0 342.4

cl 7.8 342.6

E 7.9 342.5

+3 7.9 342.5

6+70. - 24' W of E - E side Base of Large double Pepper Tree (leans to East. Over wall)

T.P. 7.39 350.01 7.68 342.68

6+85

W. gutter Line = S. End. cl. in let. 7.72 342.35

W. cl. " " " " Top cl. 6.68 343.39

6+96

W. gutter Line = N. End. Curb. Inlet 7.70 342.37

W. cl. Line = N. End. cl. Inlet. Top cl. 6.58 343.49

6+85
025E75
342.35
2.08
346.43
4.41
341.99
6+44 =
Conc. Walk 35'
Side
1' E of W. End.
Elev. 341.99

350.07

7+00

E-3	6.0	344.1
E	6.5	343.6
cl	7.3	342.8
1/4	7.5	342.6
ϕ	7.6	342.5
1/4	7.3	342.8
+8	7.4	342.7
cl	6.7	343.4
+6	6.7	343.4
W	7.8	342.3
+10	9.0	341.1

7+50

-10	8.2	341.9
W	7.8	342.3
+4	7.4	342.7
+6	6.3	343.8
+11	6.3	343.8
cl	7.0	343.1
1/4	6.6	343.5
ϕ	6.5	343.6
1/4	6.4	343.7
cl	6.1	344.0
E	5.1	345.0

8+00

E	4.0	346.1
cl	4.8	345.3

350.67

47th

77

1/4	5.0	345.1
ϕ	4.9	345.2
1/4	5.2	344.9
cl	5.6	344.5
W	4.6	344.1
+10	6.5	343.6

8+50

-10	5.3	344.8
W	5.1	345.0
cl	4.8	345.3
1/4	4.3	345.8
ϕ	4.2	345.9
1/4	4.3	345.8
cl	4.2	345.9
E	4.0	346.1

8+95

E	4.8	345.3
cl	5.5	344.6
1/4	5.7	344.4
ϕ = E. Edge Sewer Flush Tank	4.53	345.54
+5.5 = W	4.53	345.54
1/4	5.0	345.1
cl	5.7	344.4
W	5.8	344.3

350.07

9+25

W	7.2	342.9
el	7.8	342.3
+4	8.3	341.8
1/4	8.4	341.7
el	8.5	341.6
1/4	8.4	341.7
el	8.5	341.6
+4	8.0	342.1
+10	5.5	344.6
E.	5.5	344.6

9+40

E.	5.8	344.3
+2	5.8	344.3
+8	9.4	340.7
el	9.8	340.3
1/4	10.1	340.0
el	10.3	339.8
1/4	10.4	339.7
el	10.4	339.7
+3	9.7	340.4
W	9.0	341.1

9+43³ = S. End curb, walk + Pav.

W.	10.2	339.8
+2 = W. edge ent. walk	10.31	339.76
+7. = E. " " "	10.40	339.67
+11. = ent. el.	10.55	339.52 = 339.52

F.B. 1185-P.40

350.07

47th St

78

gutter pav.	11.15	338.92
W + 21 = W. 1/4 of pav.	10.84	339.23
W + 31 = el	10.64	339.39
W + 41 = E. 1/4 of "	10.58	339.49
E. gutter	10.67	339.40
W + 51 = E. curb.	10.14	339.93
W + 55 = W. edge of walk	10.04	339.99
W + 60 = W. " " "	9.84	340.19
W + 61 = dirt.	9.1	340.97

25' N. of S. End of Pav.

E. ent. el.	11.32	338.75
E. gutter	11.76	338.31
+10 = 1/4	11.87	338.20
+20 = el	11.97	338.10
+30 = 1/4	12.30	337.77
+40 = gutter	12.75	337.32
+40 = E. ent. el.	12.28	337.79

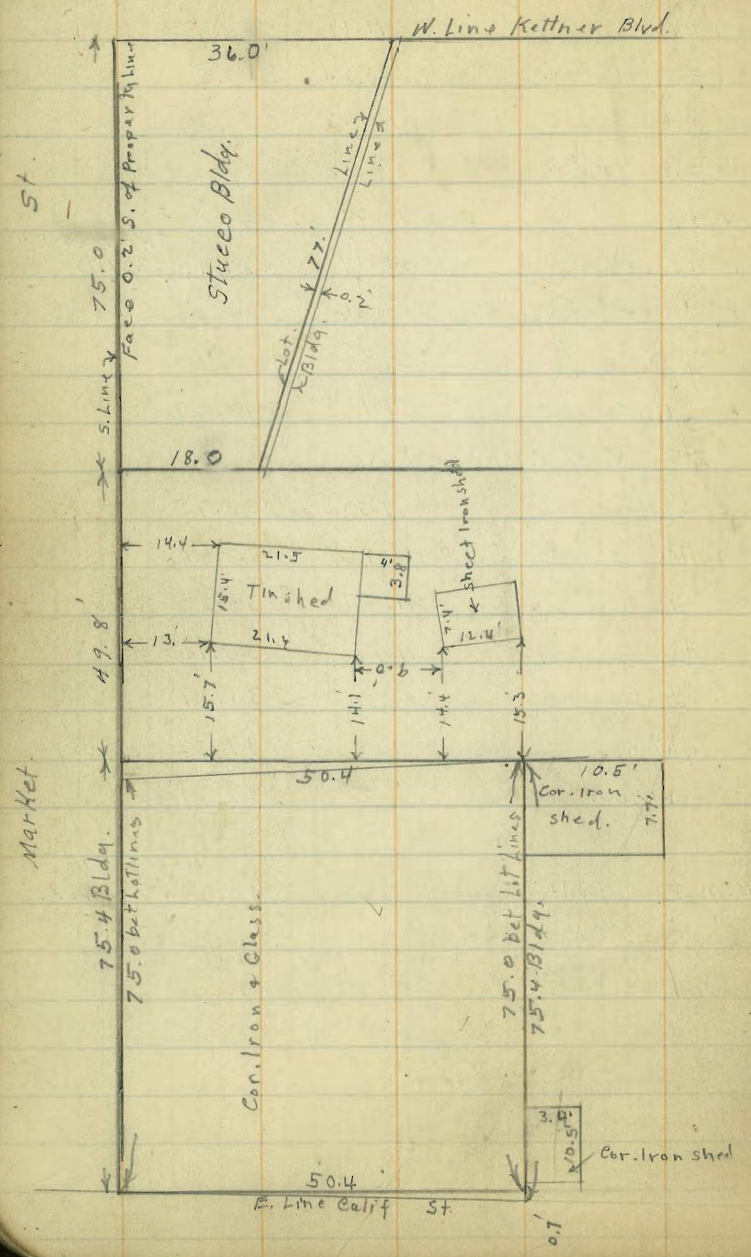
set. B.M. Top. Hgdt.

9.69 340.38 + Monroe.

S. E. 47th St

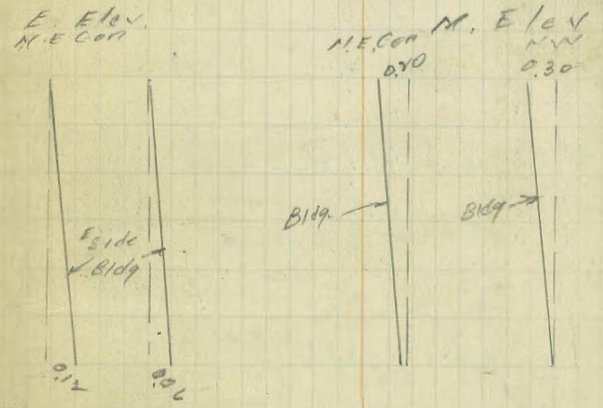
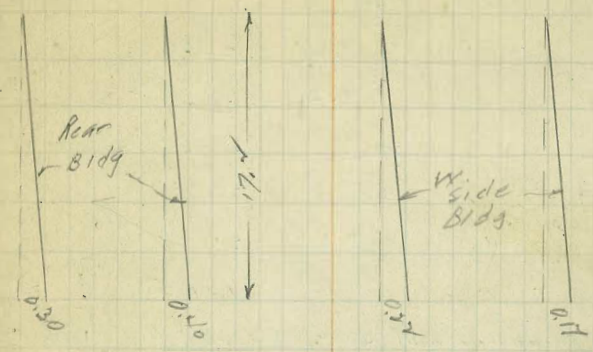
4-13-39
Miller
Walker
Bldg.

Survey of Bldgs. Blk-18
New San Diego.



Tile - Stucco Bldg
S.W. Cor
Calif. &
Market
S. Elev
SE Cor SW Cor
W. Elev
Rear Front

79



Elev. 5 1/2 of 2000 Bldg
SW cor Calif. & Market Moore
Sisson
Northern

	3.27	14.41	11.14	15046		
T.P.	4.95	15.00	4.36	10.05		
NW Cor 305, LANT 1			+ 7.15	22.15	} FRONT or N Elev	
Col. #1			+ 7.29	22.29		
" #2			+ 7.38	22.38		
" #3			+ 7.30	22.30		
" #4			+ 7.30	22.30		
NE Cor			+ 7.29	22.29		
T.P.	4.16	14.21	4.95	10.05		
SW Cor 20700	TOP	Parapet wall	+ 12.46	26.67	See 81.09	
+ 15	"	"	+ 12.59	26.80	" "	
+ 30	"	"	+ 12.64	26.83	" "	
+ 45	"	"	+ 12.58	26.79	" "	
+ 60	"	"	+ 12.53	26.74	" "	
+ 77	SE Cor	Bldg	"	+ 12.50	26.71	" "
T.P.	5.16	15.21	4.16	10.05		
NE Cor	TOP	Parapet	+ 11.77	26.98	} = E side	
Center	"	"	+ 11.59	26.80		

U-17-39.

Brass Disc. N.E. Cor. 200 & Market

TABLE No. 1

Distance of slope stake from side of shoulder
stake for any width roadway, slope 1 to 1.
If ground is nearly level, the cut or fill at side
stake is located by the double entry method in
left column and top row. The number in body
of table is same row and column gives distance
from side stake to slope stake. If ground is not
level amount to be added to amount
to cut or fill and find in table. Set up
rod at this point, and line of sight should cut
target.

IMPROVED TABLES
AND
INFORMATION

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Degree of curve with a given L may be found
by dividing tangent (or external), opposite L by
given tangent (or external).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

75.4
48.8
75.1
200.3

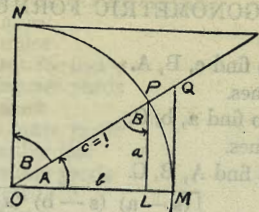


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Sines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$

56
 76
 640 4.20
 66° 46' 20
 11.14

26.67

17.52
 4.17

255

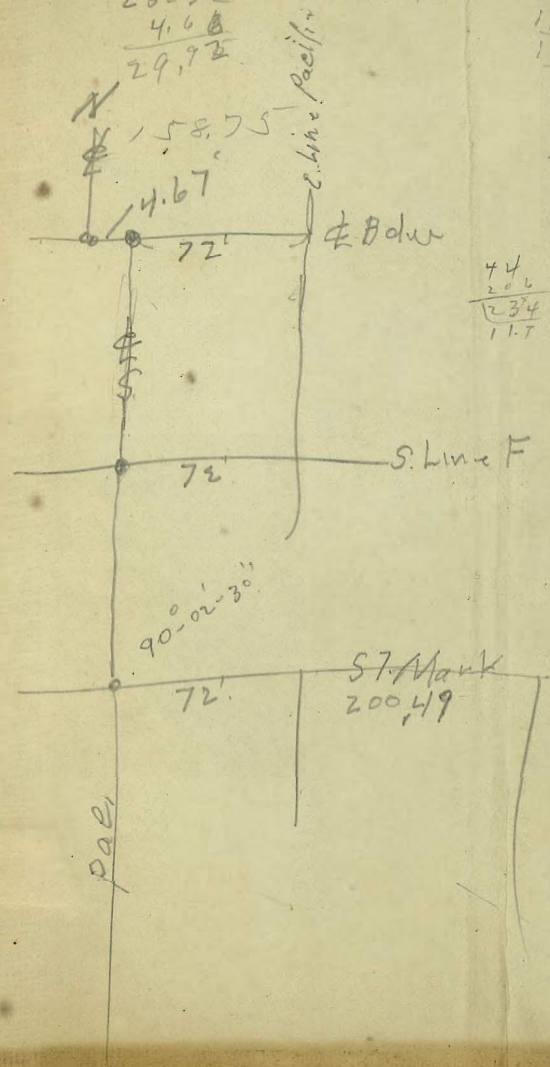
50
 17
 36
 18
 14
 3.2+00

11294
 109
 3344
 4614

35.6
 68
 77
 75.7

25.32
 4.68
 29.92

1128
 1.21.5
 1128
 87
 255
 87
 368
 9.2
 276



44
 206
 234
 117

214.26
 61.
 214.49
 489.75
 65
 12
 1300
 65
 7.800

200.26