

1535

PLASTER

LEVEL BOOK

No. 310F

1535

MICROFILMED
DEC 24 1964

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO.
CALIFORNIA.

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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

Alley Cont from P. 80

1

| | 190 ¹⁶ | 300 | 187.14 |
|---------------------------------------|--------------------|-------|--------|
| 1+16 = L. steps to House on E on line | | | |
| 1+20 | Wall 1.1 in Alley. | | |
| E _o on top Wall | 2.0 | 188.2 | |
| +1.1 toe Wall | 3.6 | 186.6 | |
| L _o | 3.9 | 186.3 | |
| +5 | 3.7 | 186.5 | |
| W | 4.5 | 185.7 | |
| +10 | 7.1 | 183.1 | |
| 1+34 = End Wall on E 1" in Alley | | | |
| E _o on Wall | 1.5 | 188.7 | |
| +1.1 " Ground at Wall | 2.9 | 187.3 | |

Score
11-10-86

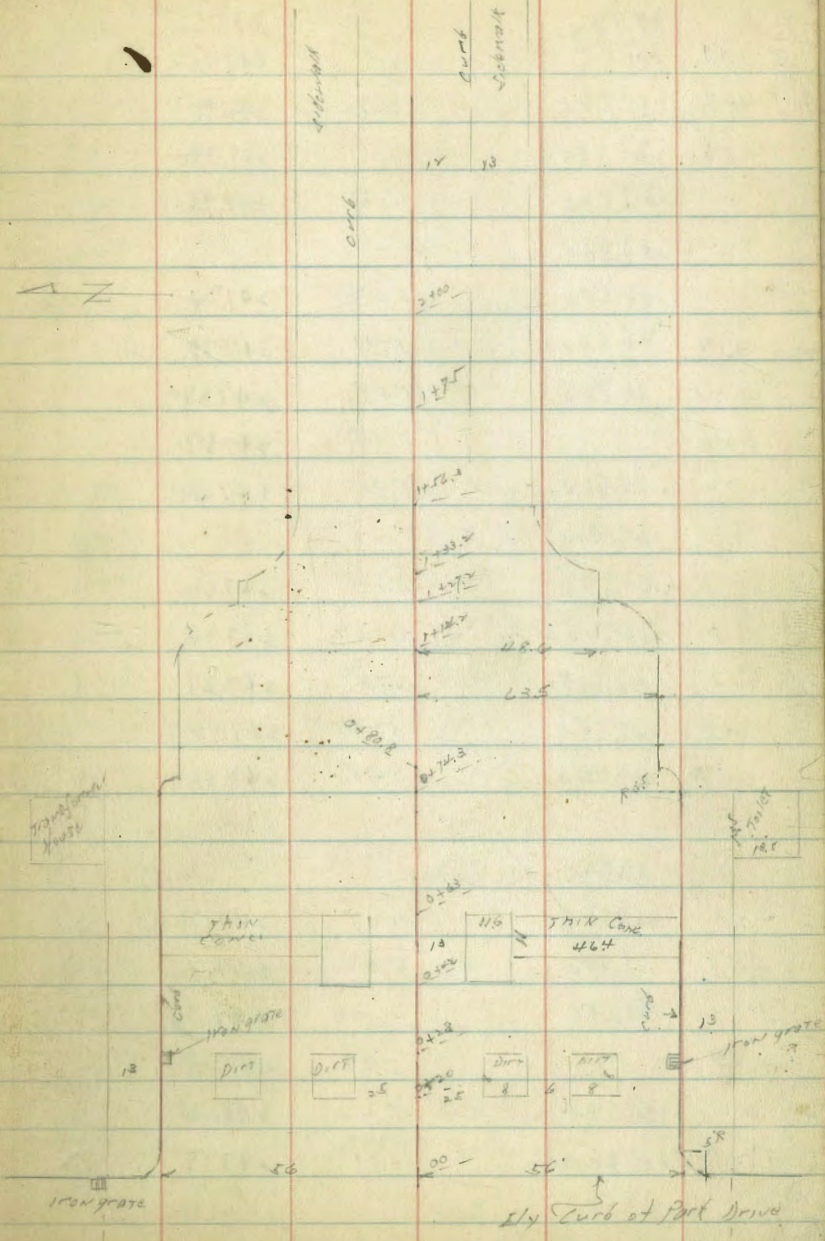
Indexed
c.s.R.

Laurel

El. of Ex. PAVING + curbs etc.

W. Laurel St. Entrance to Balboa Park

| | | | | |
|-----------|-------------------|--------|--------|-------------|
| N.W. B.P. | 1.83 | 253.76 | 251.93 | 6744 Laurel |
| | Sly $\frac{1}{2}$ | | 253.76 | |
| | 0+00 | | | |
| ± | par | 6.05 | 247.71 | |
| +20 | par | 6.10 | 247.66 | |
| +40 | " | 6.14 | 247.64 | |
| +50 | " | 6.13 | 247.63 | |
| +69 | " | 6.04 | 247.74 | |
| " | cb | 5.46 | 248.30 | |
| | 0+20 | | | |
| ± | par | 6.10 | 247.66 | |
| +14 | " | 6.05 | 247.71 | |
| +25 | " | 6.13 | 247.63 | |
| +34 | " | 6.18 | 247.58 | |
| +39 | " | 6.22 | 247.54 | |
| +47 | " | 6.26 | 247.50 | |
| +54 | " | 6.30 | 247.46 | |
| " | cb | 5.69 | 248.07 | |
| | 0+28 | | | |
| ± | par | 6.06 | 247.70 | |
| +12 | " | 6.05 | 247.71 | |
| +25 | " | 6.10 | 247.66 | |
| +33 | " | 6.12 | 247.64 | |



253.76

| | | | |
|-------|-----------------|------|--------|
| ♀ +39 | par | 6.14 | 247.64 |
| +47 | " | 6.20 | 247.56 |
| +56 | " | 6.37 | 247.39 |
| " | cb | 5.81 | 247.95 |
| | 0+36 | | |
| ♀ | | 6.04 | 247.72 |
| +12 | | 5.99 | 247.77 |
| +25 | | 5.89 | 247.87 |
| +40 | | 5.89 | 247.87 |
| +56 | par. top cb end | 5.90 | 247.86 |
| | 0+44 | | |
| ♀ | par | 6.10 | 247.66 |
| +12 | " top of old cb | 6.07 | 247.74 |
| +25 | par. | 5.87 | 247.89 |
| +40 | " | 5.84 | 247.92 |
| +56 | " | 5.95 | 247.81 |
| | N/4 1/2 0700 | | |
| ♀ +20 | par | 6.05 | 247.71 |
| +40 | " | 6.04 | 247.72 |
| +56 | " | 6.00 | 247.76 |
| +69 | " | 5.99 | 247.77 |
| " | cb | 5.42 | 248.34 |
| +74 | iron grate | 4.01 | 247.75 |

253.76

| | | | |
|-------|-----------------|------|--------|
| | 0+20 | | |
| ♀ +12 | par. | 5.99 | 247.77 |
| +25 | " | 6.11 | 247.65 |
| +33 | " | 6.14 | 247.64 |
| +39 | " | 6.14 | 247.62 |
| +47 | " | 6.21 | 247.55 |
| +56 | " | 6.27 | 247.49 |
| " | cb | 5.75 | 248.01 |
| | 0+28 | | |
| ♀ +12 | par. | 5.99 | 247.77 |
| +25 | " | 6.02 | 247.74 |
| +33 | " | 6.07 | 247.69 |
| +39 | " | 6.09 | 247.67 |
| +47 | " | 6.15 | 247.61 |
| +56 | par. iron grate | 6.40 | 247.36 |
| " | " | 5.84 | 247.92 |
| | 0+36 | | |
| ♀ +12 | par. | 5.91 | 247.85 |
| +25 | " | 5.83 | 247.93 |
| +40 | " | 5.91 | 247.85 |
| +56 | Top end ab | 5.93 | 247.83 |
| | 0+42 | | |
| ♀ +12 | par. | 5.99 | 247.77 |
| +25 | " | 5.85 | 247.91 |
| +40 | " | 5.91 | 247.85 |
| +56 | " | 5.97 | 247.84 |

| | | | | | |
|-------|--------|----------|------|--------|--|
| | | 250.76 | | | |
| JP | 413 | 251.87 | 0.02 | 247.74 | |
| | 0.503 | 5/14 1/2 | | 251.87 | |
| ♀ | par | | 4.62 | 247.25 | |
| +12 | " | | 4.55 | 247.32 | |
| +25 | " | | 4.43 | 247.44 | |
| +40 | " | | 4.42 | 247.45 | |
| +56 | " | | 4.41 | 247.46 | |
| +71 | " | | 4.36 | 247.51 | |
| | 0+74.3 | | | | |
| ♀ | par | | 4.80 | 247.07 | |
| +12 | " | | 4.72 | 247.15 | |
| +25 | " | | 4.57 | 247.30 | |
| +40 | " | | 4.57 | 247.30 | |
| +56 | " | | 4.57 | 247.30 | |
| +71 | " | | 4.55 | 247.32 | |
| | 0+80.8 | | | | |
| ♀ | | | 4.85 | 247.02 | |
| +12 | par | | 4.86 | 247.01 | |
| +25 | " | | 4.64 | 247.23 | |
| +40 | " | | 4.60 | 247.27 | |
| +56 | " | | 4.63 | 247.24 | |
| +63.5 | " | | 4.67 | 247.20 | |
| | 1+14.2 | | | | |
| ♀ | par | | 5.21 | 246.66 | |
| +12 | " | | 5.18 | 246.69 | |

| | | | | | |
|--|--|--------|--|--|--------|
| | | 257.87 | | | |
| | | | | | 251.87 |
| | | | | | 246.83 |
| | | | | | 246.84 |
| | | | | | 246.81 |
| | | | | | 246.77 |
| | | | | | |
| | | | | | 246.57 |
| | | | | | 246.57 |
| | | | | | 246.73 |
| | | | | | 246.70 |
| | | | | | 246.61 |
| | | | | | |
| | | | | | 246.50 |
| | | | | | 246.49 |
| | | | | | 246.69 |
| | | | | | 246.59 |
| | | | | | 246.52 |
| | | | | | |
| | | | | | 246.25 |
| | | | | | 246.28 |
| | | | | | 246.54 |
| | | | | | |
| | | | | | 246.03 |
| | | | | | 246.06 |
| | | | | | 246.29 |

251.87

251.87

| | | | | |
|---|------|-------------|------|--------|
| | 2+00 | on old pay. | | |
| ♀ | pay. | | 623 | 245.64 |
| | +12 | | 6.61 | 245.26 |
| | " | cb | 6.12 | 245.74 |
| | +25 | sdw | 5.83 | 246.04 |

N/4 1/2
0+63

| | | | | |
|---|-----|--|------|--------|
| ♀ | +12 | | 4.53 | 247.34 |
| | +25 | | 4.38 | 247.49 |
| | +40 | | 4.40 | 247.47 |
| | +56 | | 4.39 | 247.46 |
| | +71 | | 4.37 | 247.50 |

0+74.3

| | | | | |
|---|-----|--|------|--------|
| ♀ | +12 | | 4.71 | 247.16 |
| | +25 | | 4.55 | 247.32 |
| | +40 | | 4.53 | 247.34 |
| | +56 | | 4.53 | 247.34 |
| | +71 | | 4.47 | 247.40 |

0+80.8

| | | | | |
|---|-------|-----|------|--------|
| ♀ | +12 | pay | 4.83 | 247.04 |
| | +25 | " | 4.65 | 247.22 |
| | +40 | " | 4.62 | 247.25 |
| | +56 | " | 4.63 | 247.24 |
| | +62.5 | " | 4.65 | 247.22 |

251.87

251.87

| | | | | |
|---|--------|--|------|--------|
| | 1714.2 | | | |
| ♀ | +12 | | 5.21 | 246.66 |
| | +25 | | 5.04 | 246.83 |
| | +40 | | 5.01 | 246.86 |
| | +56 | | 5.02 | 246.85 |
| | +62.5 | | 5.01 | 246.86 |

1727.7

| | | | | |
|---|-------|-----|------|--------|
| ♀ | +12 | pay | 5.35 | 246.52 |
| | +25 | | 5.17 | 246.70 |
| | +40 | | 5.15 | 246.72 |
| | +48.6 | | 5.72 | 246.74 |

1730.2

| | | | | |
|---|-------|--|------|--------|
| ♀ | +12 | | 5.38 | 246.49 |
| | +25 | | 5.22 | 246.64 |
| | +40 | | 5.17 | 246.70 |
| | +48.6 | | 5.17 | 246.70 |

1756.3

| | | | | |
|---|-----|--|------|--------|
| ♀ | +12 | | 5.63 | 246.24 |
| | +25 | | 5.34 | 246.53 |

1775

| | | | | |
|---|-----|---------------|------|--------|
| ♀ | +12 | old cb 4 pay. | 5.77 | 246.10 |
| | +25 | | 5.59 | 246.30 |

2+00

| | | | | |
|---|-------|------|------|--------|
| ♀ | +12 | 9.27 | 6.60 | 245.27 |
| | " | cb | 6.17 | 245.75 |
| | +24.5 | sdw | 5.87 | 246.00 |

Indexed
C.S.K.

Moore
11-10-36

27.

AT.

6

Elev of Ex. Paving & Curbs
Plaza de Panama, Balboa Park.

3475
3461.7

Fill in with Base
Return 5'

Palace of Fine Arts

cem. steps
72

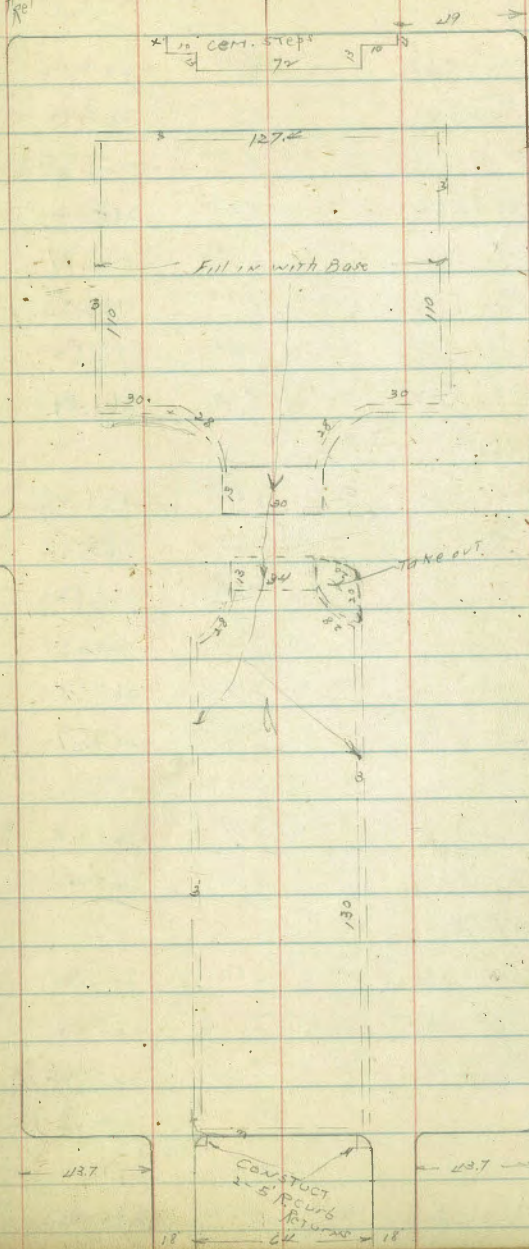
29

NECOR
Plaza de Panama

| | | | |
|-----------|-------|------------------|--------|
| Top. F.H. | 368 | 272.42 | 268.74 |
| | 00-20 | Wly Dr. to Organ | 272.42 |
| E cb | | 808 | 264.34 |
| gut | | 852 | 263.90 |
| C | | 852 | 263.90 |
| gut | | 871 | 263.71 |
| W cb | | 825 | 264.17 |
| | 00-20 | Fly Dr. to Organ | |
| W cb | | 725 | 265.17 |
| gut | | 700 | 264.78 |
| C | | 752 | 264.89 |
| gut | | 751 | 264.91 |
| E cb | | 700 | 265.38 |
| | 0700 | | |
| C cb | | 765 | 264.77 |
| C P | | 813 | 264.29 |
| 32 R cb | | 724 | 265.18 |
| " " P | | 771 | 264.71 |
| 50 R cb | | 696 | 265.46 |
| " " P | | 745 | 264.97 |
| 62 R P | | 736 | 265.06 |
| 927 R cb | | 647 | 265.95 |
| " " P | | 697 | 265.45 |

1489.4
Laurel
1437.0

0700



| | | | |
|--------|----|------|--------|
| 0+00 | | | |
| 52 L | cb | 7.98 | 264.44 |
| " " | P | 8.49 | 263.93 |
| 50 L | P | 8.77 | 263.65 |
| " " | cb | 8.30 | 264.12 |
| 62 L | cb | 8.45 | 263.97 |
| " " | P | 8.97 | 263.43 |
| 93.7 L | cb | 8.80 | 263.62 |
| " " | P | 9.25 | 263.19 |
| 0+25 | | | |
| C | P | 8.21 | 264.21 |
| 31 L | P | 8.53 | 263.89 |
| 62 L | P | 9.00 | 263.42 |
| 93.7 L | P | 9.20 | 263.22 |
| " " | cb | 8.73 | 263.69 |
| 31 R | P | 7.65 | 264.77 |
| 62 R | P | 7.31 | 265.11 |
| 93.7 R | P | 6.98 | 265.44 |
| " R | cb | 6.48 | 265.94 |
| 0+50 | | | |
| 93.7 R | cb | 6.52 | 265.90 |
| " " | P | 7.00 | 265.42 |
| 62 R | P | 7.28 | 265.14 |
| 31 R | " | 7.70 | 264.72 |
| C | " | 8.21 | 264.21 |
| 31 L | " | 8.56 | 263.86 |

| | | | |
|--------|----|------|--------|
| 62 L | P | 8.97 | 263.45 |
| 93.7 L | P | 9.25 | 263.17 |
| " " | cb | 8.74 | 263.68 |
| 0+75 | | | |
| 93.7 L | cb | 8.75 | 263.67 |
| " " | P | 9.25 | 263.08 |
| 62 L | P | 8.94 | 263.50 |
| 31 L | P | 8.53 | 263.89 |
| C | P | 8.22 | 264.20 |
| 31 R | P | 7.69 | 264.73 |
| 62 R | P | 7.30 | 265.12 |
| 93.7 R | P | 7.03 | 265.39 |
| " " | cb | 6.50 | 265.92 |
| 1+00 | | | |
| 93.7 R | cb | 6.49 | 265.93 |
| " R | P | 7.03 | 265.39 |
| 62 R | P | 7.32 | 265.08 |
| 31 R | P | 7.72 | 264.70 |
| C | P | 8.22 | 264.20 |
| 31 L | P | 8.55 | 263.87 |
| 62 L | P | 8.91 | 263.51 |
| 93.7 L | P | 9.34 | 263.08 |
| " " | cb | 8.79 | 263.63 |
| 1+28.7 | | | |
| 93.7 L | cb | 8.78 | 263.64 |
| " " | P | 9.31 | 263.11 |

Rod 9.45
 grate
 iron
 7 tied
 93.7 of

| | | | |
|------------|--------|--------|--------|
| | | | 272.42 |
| 62 L P | 8.81 | 263.61 | |
| 31 " P | 8.54 | 263.88 | |
| C P | 8.20 | 264.22 | |
| 31 P P | 7.77 | 264.65 | |
| 62 P P | 7.34 | 265.08 | |
| 93.7 P P | 6.98 | 265.44 | |
| " " cb | 6.52 | 265.90 | |
| | 1+57.4 | | |
| 113.7 P cb | 6.44 | 266.00 | |
| " P P | 6.90 | 265.52 | |
| 93.7 P cb | 6.44 | 265.98 | |
| " " P | 6.91 | 265.51 | |
| 62 P P | 7.31 | 265.11 | |
| 31 P P | 7.70 | 264.72 | |
| C P | 8.07 | 264.35 | |
| 31 L | 8.52 | 263.90 | |
| 62 L | 8.85 | 263.57 | |
| 93.7 L P | 9.27 | 263.15 | |
| " " cb | 8.75 | 263.67 | |
| 113.7 L P | 9.55 | 262.87 | |
| " " cb | 9.02 | 263.40 | |
| | 1+73.4 | | |
| 113.7 L P | 9.50 | 262.88 | |
| 93.7 " P | 9.28 | 263.14 | |
| 62 " " | 8.90 | 263.52 | |
| 31 " " | 8.55 | 263.87 | |

| | | | |
|------------|--------|--------|--------|
| | | | 272.42 |
| C Par | 8.15 | 264.27 | |
| 31 P " | 7.79 | 264.63 | |
| 62 P " | 7.30 | 265.12 | |
| 93.7 P " | 6.98 | 265.54 | |
| 113.7 P " | 6.75 | 265.67 | |
| | 1+89.4 | | |
| 113.7 P cb | 6.42 | 266.00 | |
| " P P | 6.90 | 265.52 | |
| 93.7 cb | 6.49 | 265.93 | |
| " P P | 6.85 | 265.57 | |
| 62 P P | 7.32 | 265.10 | |
| 31 P | 7.73 | 264.69 | |
| C | 8.12 | 264.30 | |
| 31 L P | 8.52 | 263.90 | |
| 62 L P | 8.94 | 263.48 | |
| 93.7 L | 9.30 | 263.12 | |
| " cb | 8.84 | 263.60 | |
| 103.7 L P | 9.25 | 262.97 | |
| " cb | 8.90 | 263.52 | |
| | 2+00 | | |
| 93.7 L cb | 8.82 | 263.60 | |
| " " P | 9.29 | 263.13 | |
| 62 L | 8.91 | 263.51 | |
| 31 | 8.50 | 263.92 | |
| C | 8.19 | 264.23 | |
| 31 P | 7.76 | 264.66 | |

| | | 272.42 | |
|----------|------|--------|--------|
| 62 P | | 7.30 | 265.12 |
| 93.7 P | | 7.01 | 265.41 |
| " " | | 6.51 | 265.91 |
| | 2+25 | | |
| 93.7 P | | 6.50 | 265.92 |
| " " | | 7.07 | 265.35 |
| 62 P | | 7.31 | 265.11 |
| 31 P | | 7.82 | 264.60 |
| C | | 8.21 | 264.21 |
| 31 L | | 8.60 | 263.82 |
| 62 L | | 8.98 | 263.44 |
| 93.7 L P | | 9.26 | 263.16 |
| " " | cb | 8.81 | 263.61 |
| | 2+50 | | |
| 93.7 L | cb | 8.81 | 263.61 |
| " " | P | 9.38 | 263.04 |
| 62 L | P | 8.94 | 263.48 |
| 31 L | | 8.56 | 263.86 |
| C | | 8.17 | 264.25 |
| 31 P | | 7.84 | 264.58 |
| 62 P | P | 7.37 | 265.05 |
| 93.7 P | P | 7.04 | 265.38 |
| " P | cb | 6.51 | 265.91 |
| | 2+75 | | |
| 93.7 P | cb | 6.50 | 265.92 |
| " " | P | 7.03 | 265.39 |

| | | 272.42 | |
|--------|------|--------|--------|
| 62 P | | 7.36 | 265.06 |
| 31 P | | 7.80 | 264.62 |
| C | | 8.24 | 264.18 |
| 31 L | | 8.60 | 263.82 |
| 62 L | | 8.98 | 263.49 |
| 93.7 L | | 9.27 | 263.00 |
| " " | cb | 8.85 | 263.57 |
| | 2+85 | | |
| 93.7 L | cb | 9.26 | 263.96 |
| | 3+00 | | |
| 93.7 | cb | 8.82 | 263.60 |
| " " | P | 9.40 | 263.02 |
| 62 L | | 8.97 | 263.45 |
| 31 L | | 8.60 | 263.82 |
| C | | 8.14 | 264.28 |
| 31 P | | 7.83 | 264.57 |
| 62 P | | 7.35 | 265.07 |
| 93.7 P | P | 7.04 | 265.38 |
| " " | cb | 6.52 | 265.90 |
| | 3+25 | | |
| 93.7 P | cb | 6.52 | 265.90 |
| " " | P | 7.05 | 265.37 |
| 62 P | | 7.32 | 265.10 |
| 31 P | | 7.79 | 264.63 |
| C | | 8.21 | 264.21 |
| 31 L | | 8.57 | 263.85 |

272.42

| | | | |
|--------|--------------------|--------|--------|
| 62 L | | 8.97 | 263.45 |
| 93.7 L | P | 9.28 | 263.14 |
| " " | cb | 8.80 | 263.62 |
| 93.7 L | cb | 8.78 | 263.64 |
| " " | Par | 9.50 | 263.12 |
| 02 L | " | 8.90 | 263.52 |
| 31 L | " | 8.48 | 263.94 |
| C | " | 8.16 | 264.26 |
| 01 P | " | 7.77 | 264.65 |
| 62 P | " | 7.36 | 265.06 |
| 93.7 P | P | 7.04 | 265.38 |
| " " | cb | 6.55 | 265.87 |
| | | 3+61.7 | |
| 93.7 P | cb | 6.55 | 265.87 |
| " " | P | 7.07 | 265.35 |
| 02 R | " | 7.38 | 265.04 |
| 31 P | Par. foot of steel | 7.85 | 264.57 |
| C | " | 8.21 | 264.21 |
| 31 L | " | 8.52 | 263.90 |
| 62 L | " | 8.91 | 263.51 |
| 93.7 L | 12" drain | 9.30 | 263.12 |
| " " | " | 8.79 | 263.63 |

272.42

| | | | |
|--------|-----------|------|--------|
| | | 3+75 | |
| 93.7 L | cb + Par. | 8.81 | 263.61 |
| 80 L | cb | 8.44 | 263.78 |
| " " | P | 9.10 | 263.32 |
| 62 L | P | 8.91 | 263.51 |
| 46 L | cb | 8.18 | 264.24 |
| " L | P | 8.78 | 263.64 |
| 44.5 P | of C Par. | 7.60 | 264.82 |
| " " | cb | 7.09 | 265.33 |
| 62 P | P | 7.36 | 265.06 |
| 93.7 P | P | 7.07 | 265.35 |
| " " | cb | 6.57 | 265.85 |

E. Laurel St Care to Park

| | | | | |
|--------|---------------|--------|--------|----------------|
| NWBP | 3.30 | 287.08 | 283.28 | Park Laurel |
| | 0+00 | | 287.08 | |
| 10 R | cb. | 4.74 | 282.34 | |
| " " | P | 5.23 | 281.85 | |
| C | P | 5.04 | 282.04 | |
| 10 L | P | 5.23 | 281.85 | |
| " " | cb | 4.76 | 282.32 | |
| | 0+10 | | | |
| C | P | 4.97 | 282.11 | |
| 10 L | P | 5.00 | 282.08 | |
| 42.5 L | P | 5.05 | 282.03 | |
| 52.5 L | P | 5.02 | 282.06 | |
| 87 L | P | 4.94 | 282.14 | |
| 16 R | P | 4.97 | 282.11 | |
| 42.5 R | P | 5.04 | 282.04 | |
| 52.5 R | P | 5.08 | 282.00 | |
| 60.5 R | on iron grate | 5.20 | 281.88 | |
| 97.6 R | P | 5.09 | 281.99 | |
| | 0+20 | | | |
| C | P | 4.75 | 282.33 | |
| 16 R | P | 4.84 | 282.24 | |
| 40 R | | 4.81 | 282.27 | |
| 60 R | | 4.84 | 282.25 | |
| 97.6 R | | 5.07 | 282.01 | |



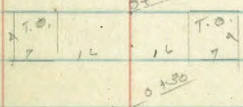
17.

17.

E Laurel

0+54.5

+76.0



do
ST
57.9
57.9

ST
57.9
57.9

2+10

0+20

10

15

← 25

10

20.5

16

14

27

10

42.0

→

287.08

| | | | |
|-------|---|------|--------|
| 16 Lt | P | 4.80 | 287.28 |
| 40 L | P | 4.79 | 287.29 |
| 60 L | P | 4.75 | 287.33 |
| 87 L | P | 4.82 | 287.26 |

| | | | | |
|----|------|--------|------|--------|
| TP | 5.11 | 287.58 | 4.61 | 287.47 |
|----|------|--------|------|--------|

287.58

| | | | |
|-------|---|------|--------|
| ± | P | 5.12 | 287.46 |
| 16 Lt | P | 5.21 | 287.37 |
| 40 L | P | 5.13 | 287.45 |
| 60 Lt | P | 5.14 | 287.44 |
| 87 Lt | P | 5.10 | 287.48 |
| 16 R | P | 5.19 | 287.39 |
| 40 R | P | 5.14 | 287.44 |
| 60 R | P | 5.11 | 287.47 |
| 87 R | P | 5.14 | 287.44 |

0+58.7

| | | | |
|-------|---|------|--------|
| C | P | 4.98 | 287.60 |
| 16 Rt | " | 4.96 | 287.62 |
| 40 R | " | 5.01 | 287.57 |
| 60 R | " | 5.03 | 287.55 |
| 97 R | " | 4.99 | 287.59 |
| 16 Lt | " | 4.99 | 287.59 |
| 40 L | " | 4.97 | 287.61 |
| 60 L | " | 4.96 | 287.62 |

287.58

| | | | |
|-------|---|------|--------|
| 97 Lt | P | 4.89 | 287.69 |
|-------|---|------|--------|

0+70.4

| | | | |
|---|---|------|--------|
| C | P | 4.78 | 287.80 |
|---|---|------|--------|

| | | | |
|------|---|------|--------|
| 16 L | " | 4.80 | 287.78 |
|------|---|------|--------|

| | | | |
|------|---|------|--------|
| 40 L | " | 4.80 | 287.78 |
|------|---|------|--------|

| | | | |
|------|---|------|--------|
| 60 L | " | 4.75 | 287.83 |
|------|---|------|--------|

| | | | |
|-------|---|------|--------|
| 97 Lt | " | 4.79 | 287.79 |
|-------|---|------|--------|

| | | | |
|-------|---|------|--------|
| 16 Rt | " | 4.80 | 287.78 |
|-------|---|------|--------|

| | | | |
|------|---|------|--------|
| 40 R | " | 4.81 | 287.77 |
|------|---|------|--------|

| | | | |
|------|---|------|--------|
| 60 R | " | 4.87 | 287.71 |
|------|---|------|--------|

| | | | |
|------|---|------|--------|
| 97 R | " | 4.81 | 287.77 |
|------|---|------|--------|

0+84.5 Edge of checker board = ^{why 26} _{20x20}

| | | | |
|------|---|------|--------|
| 97 R | " | 4.80 | 287.78 |
|------|---|------|--------|

| | | | |
|------|---|------|--------|
| 60 R | " | 4.84 | 287.74 |
|------|---|------|--------|

| | | | |
|------|---|------|--------|
| 40 R | " | 4.84 | 287.74 |
|------|---|------|--------|

| | | | |
|------|---|------|--------|
| 16 R | " | 4.83 | 287.75 |
|------|---|------|--------|

| | | | |
|---|---|------|--------|
| C | " | 4.82 | 287.76 |
|---|---|------|--------|

| | | | |
|-------|---|------|--------|
| 16 Lt | " | 4.78 | 287.80 |
|-------|---|------|--------|

| | | | |
|------|---|------|--------|
| 40 L | " | 4.76 | 287.82 |
|------|---|------|--------|

| | | | |
|------|---|------|--------|
| 60 L | " | 4.75 | 287.83 |
|------|---|------|--------|

| | | | |
|------|---|------|--------|
| 97 L | " | 4.76 | 287.82 |
|------|---|------|--------|

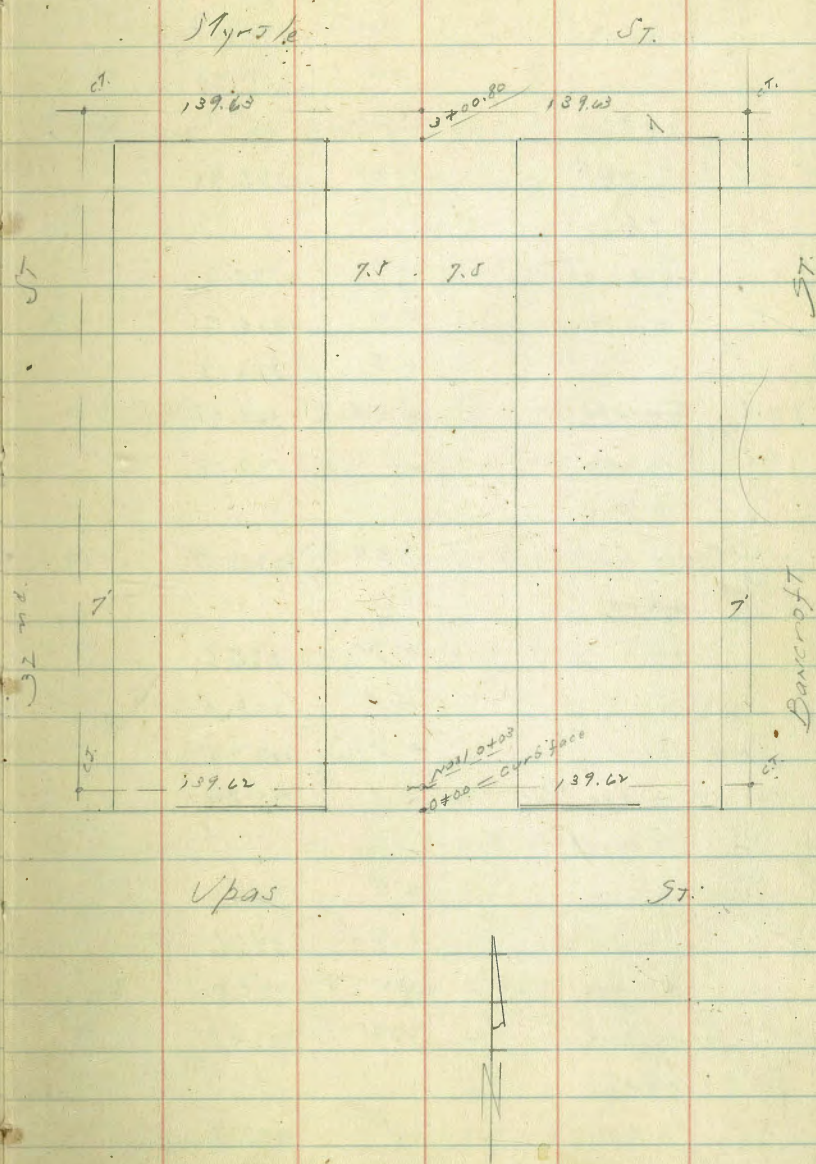
4.80 287.8

Xsec alley 15' wide
Blk 48 Park Villas
Upas + Myrtle, 32nd + Bancroft

SUN. EP 5.31 329.21 323.90 32nd + Upas

0+00 = Curb face N. side Upas

| | | | |
|------|----------|------|--------|
| W | cb | 5.49 | 323.72 |
| W | pav | 6.03 | 323.18 |
| C | | 6.05 | 323.16 |
| E | pav | 6.16 | 323.02 |
| E | cb | 5.65 | 323.56 |
| 0+10 | | | |
| E | Top walk | 2.17 | 325.05 |
| | + 0.5 | 4.8 | 324.4 |
| C | | 5.2 | 324.0 |
| | + 4 | 5.1 | 324.1 |
| W | | 4.3 | 324.9 |
| 0+20 | | | |
| W | | 4.2 | 325.0 |
| C | | 4.6 | 324.6 |
| | + 7 | 3.9 | 325.3 |
| E | Top walk | 3.40 | 325.81 |
| 0+49 | | | |
| E | | 2.17 | 327.04 |
| | + 0.5 | 3.0 | 326.2 |



329.21

| | | | |
|----------|---------------------------|------|--------|
| C | | 3.2 | 325.8 |
| W | | 3.3 | 325.9 |
| | 0+51 | | |
| W | E S' walk | 2.90 | 326.25 |
| | 0+61 | | |
| W | | 2.9 | 326.3 |
| C | | 3.2 | 326.0 |
| E | | 2.8 | 326.4 |
| | +0.8 Cem apron | 2.53 | 326.68 |
| | +4.5 Sin. Gar. cem. floor | 2.04 | 327.17 |
| | 0+74 | | |
| E - J. S | Sin Gar. " " | 1.96 | 327.25 |
| | 0+80 | | |
| E | | 2.6 | 326.6 |
| C | | 2.8 | 326.4 |
| W | Cem. Apron | 2.84 | 326.35 |
| | +16 Sin. Gar. cem. floor | 2.37 | 326.84 |
| | 1+00 | | |
| W | | 2.7 | 326.5 |
| C | | 2.6 | 326.6 |
| E | | 2.4 | 326.8 |
| | +5.3 Sin. Gar. Cem. floor | 1.73 | 327.48 |
| | 1+35 | | |
| E | | 2.1 | 327.1 |
| C | | 2.1 | 327.1 |
| W | | 2.2 | 327.0 |

329.21

14

| | | | |
|-------|----------------------|--------|--------|
| W +1 | Sin. Gar. dirt floor | 2.2 | 327.0 |
| | 1+48 | | |
| E - J | Sin. Gar. Cem. floor | 1.28 | 327.93 |
| | 1+60 | | |
| W | | 1.6 | 327.6 |
| C | | 1.9 | 327.3 |
| E | | 1.8 | 327.4 |
| | 1+83 | | |
| - 8.5 | Sin. Gar. Cem. floor | 0.43 | 328.28 |
| E | | 1.4 | 327.8 |
| C | | 1.3 | 327.9 |
| W | | 0.9 | 328.3 |
| T.P. | 7.05 | 334.88 | 1.38 |
| | 2+00 | | |
| W | | 6.7 | 328.2 |
| C | | 6.8 | 328.1 |
| E | | 6.7 | 328.2 |
| | 2+21 | | |
| - 9 | Sin. Gar. Cem. floor | 4.93 | 329.95 |
| E | | 6.1 | 328.8 |
| C | | 6.3 | 328.6 |
| W | | 6.2 | 328.9 |
| +2 | Cem Apron | 6.14 | 328.74 |
| +18 | Sin Gar Cem floor | 5.95 | 328.93 |

2+50

| | | | |
|---|--|-----|-------|
| W | | 5.7 | 329.2 |
| C | | 5.6 | 329.3 |
| E | | 5.4 | 329.5 |

2+82

| | | | |
|------|-------------------|------|--------|
| E-18 | SIN GAR. CEM Hour | 9.72 | 331.16 |
| -15 | CEM APRON | 3.88 | 331.00 |
| E | | 4.7 | 330.2 |
| C | | 4.8 | 330.1 |
| W | | 5.0 | 329.9 |

2+93

| | | | |
|-----|------------------------------|------|--------|
| W | | 4.9 | 330.0 |
| C | | 4.8 | 330.1 |
| E | | 4.8 | 330.1 |
| +15 | CEM apron | 4.09 | 330.79 |
| +18 | SIN GAR ^{CEM} floor | 4.09 | 330.79 |

3+00.8

| | | | |
|---|-----|------|--------|
| E | cb | 4.95 | 329.95 |
| E | pay | 4.98 | 329.90 |
| C | " | 5.19 | 329.69 |
| W | " | 5.04 | 329.84 |
| W | cb | 4.95 | 329.93 |

| | | | | |
|---------------|-----|--------|--------|--------|
| T.P. | 138 | 329.21 | 7.05 | 327.83 |
| check to B.P. | | 25.30 | 323.91 | 323.90 |

Indexed
C.S.M.

Moore
12-2-36

16

Proposed Sewer W 1/2 Blk 8 City Hts.

S.E. Ch. R. Hub
Boundary
Maple

2.84

298.64

295.80

B.M. Hub

00=St Maple

7.1

+ 50

7.6

+ 50

8.0

+ 50

8.6

+ 77.5 = N.L. Lot 11

9.1

289.5

FL. Ex. M.H. E Maple alley

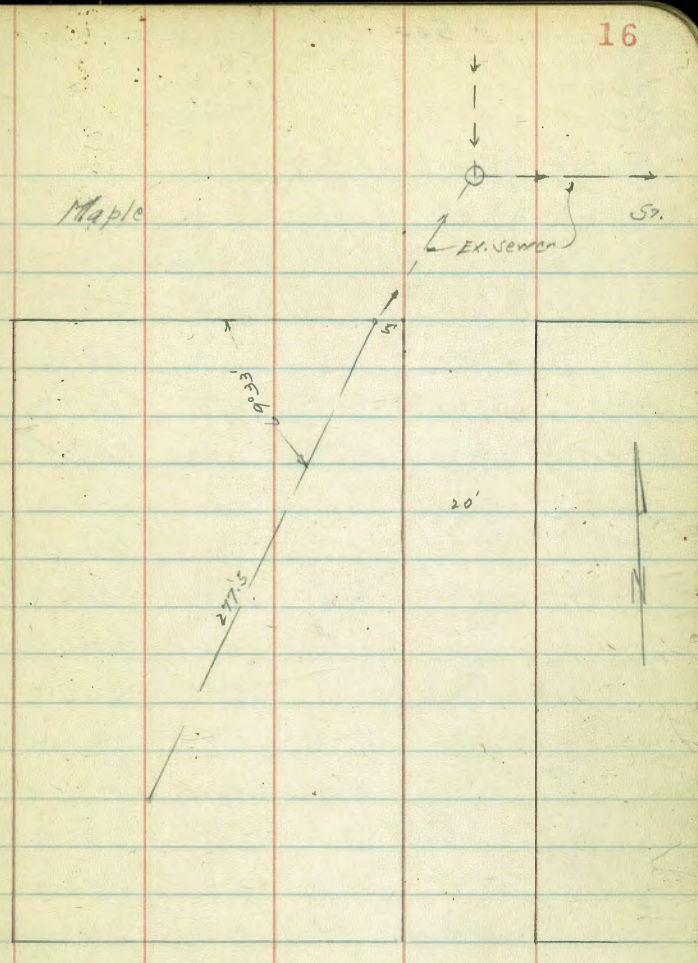
13.76

284.88

286.8
1.4
288.2
289.5
1.3

Maple

Boundary



2-13-37

X Sec. Euclid Ave El Cajon North

Indexed
c.s.k.

354.78

17

Miller
Walker
Bliss

| | | | | | | | |
|-----------------|------------------|---------------|----------------------------|-------------------------------------|----------------------------|------|--------|
| B.M. B.P. | 4.84 | 352.04 | 347.20 | S.W. 47 th & El Cajon | +45 | 7.0 | 347.8 |
| T.P. B.M. | 9.07 | 354.78 | 345.71 | S.W. Euclid & El Cajon | +56 | 7.7 | 347.1 |
| | | | | | | 1+00 | |
| | N. Line | El Cajon Blvd | on diagonal | | E +50 | 8.0 | 346.8 |
| E - | | 7.1 | 347.7 | | +42 | 6.6 | 348.2 |
| +2.5 E | Edge walk S. End | 6.99 | 347.79 | | +40 | 6.6 | 348.2 |
| +7.5 W | " " " " | 7.04 | 347.74 | | +30 | 6.6 | 348.2 |
| +10.2 = ch. | " " " " | 7.04 | 347.74 | | +20 | 6.7 | 348.1 |
| gutter | | 7.8 | 347.0 | | Gutter | 7.1 | 347.7 |
| +20.3 | | 8.0 | 346.8 | | E+10-E. ch | 6.58 | 348.20 |
| +30.4 | | 8.2 | 346.6 | | | 1+25 | |
| +40.6 = W. Line | | 8.0 | 346.8 | | E | 6.6 | 348.2 |
| +50.7 | | 7.8 | 347.0 | | +2.5 = E. Edge walk N. End | 6.28 | 348.50 |
| | 0+00 = N. Line | El Cajon | on E. at 90 ⁵⁰⁰ | | +7.5 = W " " " | 6.33 | 348.45 |
| E + 50 | | 7.8 | 347.0 | | +10 = ch | 6.37 | 348.41 |
| +40 = W. Line | | 8.0 | 346.8 | | G | 6.8 | 348.0 |
| +30 | | 7.8 | 347.0 | | +20 | 6.6 | 348.2 |
| +20 | | 7.8 | 347.0 | | +30 | 6.3 | 348.5 |
| gutter | | 7.8 | 347.0 | | +40 | 6.6 | 348.2 |
| E+10=ch. | | 7.03 | 347.75 | | +42 | 6.6 | 348.2 |
| | 0+50 | | | | +50 | 7.8 | 347.0 |
| E+10 = ch. | | 6.80 | 347.98 | | | 1+50 | |
| gutter | | 7.5 | 347.3 | | E+50 | 7.7 | 347.1 |
| +20 | | 7.3 | 347.5 | | +45 | 7.3 | 347.5 |
| +30 | | 6.8 | 348.0 | | +40 | 6.1 | 348.7 |
| +40 = W | | 7.0 | 347.8 | | +30 | 6.2 | 348.6 |

354.78

1+50 con

| | | |
|-----------------------------|------|--------|
| E+20 | 6.3 | 348.5 |
| G | 6.6 | 348.2 |
| +10=d | 6.26 | 348.52 |
| C | 6.3 | 348.5 |
| 1+73.10 | | |
| E | 6.0 | 348.8 |
| +2.5 = E edge walk. S. End | 5.98 | 348.80 |
| +7.5 = W " " " " | 6.08 | 348.70 |
| +10=d | 6.15 | 348.63 |
| G | 6.5 | 348.3 |
| +20 | 6.2 | 348.6 |
| +30 | 5.8 | 349.0 |
| +40 | 5.9 | 348.9 |
| +45 | 7.1 | 347.7 |
| +50 | 7.6 | 347.2 |
| 2+00 | | |
| C+50 | 7.0 | 347.8 |
| +45 | 6.6 | 348.2 |
| +40 | 5.3 | 349.5 |
| +30 | 5.8 | 349.0 |
| +20 | 5.8 | 349.0 |
| G | 6.1 | 348.7 |
| +10=d | 5.93 | 348.85 |
| 2+23 ⁵⁹ | | |
| E | 5.2 | 349.6 |
| +2.5 = E. Edge walk. N. End | 5.15 | 349.63 |
| +7.5 = W. " " " " | 5.21 | 349.57 |

354.78

Euclid

18

| | | |
|-----------------------------|------|--------|
| +10=d | 5.30 | 349.48 |
| G | 5.4 | 349.0 |
| +20 | 5.4 | 349.4 |
| +30 | 5.4 | 349.4 |
| +40 | 5.4 | 349.4 |
| +45 | 6.3 | 348.5 |
| +50 | 6.7 | 348.1 |
| 2+50 | | |
| E+52 doorway to Bldg | 4.75 | 350.03 |
| +50 ground- | 6.2 | 348.6 |
| +45 | 6.0 | 348.8 |
| +40 | 5.3 | 349.5 |
| +30 | 5.0 | 349.8 |
| +20 | 4.9 | 349.9 |
| G | 5.3 | 349.5 |
| +10=d | 4.51 | 350.27 |
| E | 4.6 | 350.2 |
| 2+77 ²⁰ | | |
| C | 3.7 | 351.1 |
| +2.5 = E. Edge walk. S. End | 3.63 | 351.15 |
| +7.5 = W " " S " | 3.70 | 351.08 |
| +10=d | 3.76 | 351.02 |
| G | 4.6 | 350.2 |
| +20 | 4.2 | 350.6 |
| +30 | 4.2 | 350.6 |
| +40 | 4.4 | 350.0 |

354.78

+45 5.5 349.3

+50 5.8 349.0

2+91

E+51 This Building Gone
Doorway to Lumber Co 4.10 350.68

E+51 grounds under platform 5.6 349.2

3+00

E+50 5.7 349.1

E+45 change 5.2 349.6

+40 4.0 350.8

+30 3.6 351.2

+20 3.5 351.3

G 4.1 350.7

+10=d 3.08 351.70

3+50+

E+10=d 1.67 353.11

G 2.3 352.5

+20 2.1 352.7

+30 2.1 352.7

✓ +30 S. End Fence station 3+53
 ✓ +40 = Fence S. End

2.5 352.3

+45 4.0 350.8

+50 4.7 350.1

T.P. 7.90 360.70 ✓ 1.98 352.80

✓ E+50 = Eucalyptus Tree 10" Diam
 3+77

3+87

✓ E+50 Eucalyptus Tree 12" Diam

Eucal Ave

19

360.70

4+00

+50 7.6 353.1

+44 6.0 354.7

+40 6.3 354.4

+30 6.7 354.0

+20 6.8 353.9

G 6.9 353.8

+10=d 6.16 354.54

4+28³⁰

E 4.4 356.3

+2.5 e edge walk N end 5.30 355.40

+7.5 w " " " " 5.37 355.33

+10=d 5.43 355.27

G 6.2 354.5

+20 6.2 354.5

+30 6.1 354.6

+40 = fence 5.3 355.4

+44 5.2 355.5

+50 7.3 353.4

4+50

+50 6.7 354.0

+40 = fence 5.2 355.5

+20 5.5 355.2

+10 5.7 355.0

G 5.7 355.0

+10=d 4.86 355.84

E 4.6 356.1

360.70

Carbon E. should be removed and vertical
Curve Replac The Brk in Grade

| | | | |
|-------------|--|------|--------|
| E | 4+78 | 3.8 | 356.9 |
| +10 = cl | | 3.93 | 356.77 |
| G | | 5.0 | 355.7 |
| +20 | | 5.0 | 355.7 |
| +30 | | 4.8 | 355.9 |
| +36 | | 4.7 | 356.0 |
| +40 = Fence | | 3.9 | 356.8 |
| +45 | | 5.4 | 355.3 |
| +50 | | 6.2 | 354.5 |
| | 5+00 | | |
| +50 | | 5.0 | 355.7 |
| +40 = Fence | | 4.0 | 356.7 |
| +36 | | 4.1 | 356.6 |
| +30 | | 4.6 | 356.1 |
| +20 | | 4.9 | 355.8 |
| G | | 4.9 | 355.8 |
| +10 | | 4.12 | 356.58 |
| E | | 4.0 | 356.7 |
| | 5+50 = Double Garage E+51 ^E | | |
| E | | 4.5 | 356.2 |
| +10 = cl | | 4.50 | 356.20 |
| G | | 5.2 | 355.5 |
| +20 | | 5.2 | 355.5 |
| +30 | | 4.8 | 355.9 |
| +40 = Fence | | 5.0 | 355.7 |
| +50 | | 5.4 | 355.3 |

360.70

Eucalid

20

| | | | |
|-----------------------------------|-------|------|------------------|
| ✓ E+38 Eucalyptus Tree 20" Diam. | 5+85 | | |
| ✓ E+47. Garage S. dirt floors | 6+02 | 6.2 | 354.5 dirt floor |
| +40 = Fence | | 5.8 | 354.9 |
| +35 | | 5.1 | 355.6 |
| +30 | | 5.3 | 355.4 |
| +20 | | 5.5 | 355.2 |
| G | | 5.7 | 355.0 |
| E+10 = cl | | 5.00 | 355.70 |
| E+7.5 = wedge walk S. End | | 4.90 | 355.80 |
| E+2.5 = E " " " | | 4.89 | 355.81 |
| E | | 4.5 | 356.2 |
| | 6+25 | | |
| ✓ E+38 Eucalyptus Tree 20" Diam | above | | |
| E+47. N. End garage dirt floor | 6+45 | 7.2 | 353.5 |
| E+38 Eucalyptus Tree 20" Diam | | | |
| E+67 = W End. Garage | | 4.3 | 352.4 |
| E+10 = cl | 6+50 | 5.40 | 355.30 |
| G | | 5.8 | 354.9 |
| +20 | | 5.8 | 354.9 |
| +30 | | 5.5 | 355.2 |
| +40 = Fence | | 5.6 | 355.1 |
| +47 | | 7.5 | 353.2 |
| +50 | | 7.5 | 353.2 |
| | 6+55 | | |
| E+38 Eucalyptus Tree 22" Diam | | | |
| | 6+64 | | |
| E+38 Eucalyptus Tree 20" Diam. | | | |
| | 6+76 | | |
| E+38 Eucalyptus Tree 20" in Diam. | | | |

7+00

| | | | |
|--------------------------------|---|------|--------|
| E+50 | | 7.7 | 353.0 |
| +40 Fence | | 6.6 | 354.1 |
| +38 | | 5.7 | 355.0 |
| +30 | | 6.0 | 354.7 |
| +20 | | 6.2 | 354.5 |
| G | | 6.2 | 354.5 |
| E+10=cl | | 5.86 | 354.84 |
| E+45 = Flowering Tree 12" Diam | 7+10 | | |
| E | 7+52 | 6.1 | 354.6 |
| +2.5 = E. edge walk N. End | | 5.98 | 354.72 |
| +7.5 = W " " " | | 6.06 | 354.64 |
| +10 = cl | | 6.17 | 354.53 |
| G | | 6.4 | 354.3 |
| +20 | | 6.5 | 354.2 |
| +30 | | 6.4 | 354.3 |
| +40 = Fence | | 6.7 | 354.0 |
| +42 | | 8.4 | 352.3 |
| +50 | | 8.7 | 352.0 |
| E+58 | 7+84 8+01.5 Pepper Tree 10" Diam. | | |
| +50 | | 8.0 | 352.7 |
| +42 | | 6.0 | 352.7 |
| +40 = fence | | 7.3 | 353.4 |
| +30 | | 6.8 | 353.9 |
| +20 | | 6.7 | 354.0 |
| G | | 6.4 | 354.3 |
| +10 = cl | | 6.39 | 354.31 |

| | | | | |
|---------------------------------|--------------------------------------|------|--------|---|
| E+75 = W. edge walk S. End | | 6.40 | 354.30 | $\overline{\text{X}360.70}$ $\quad 7.82$ $\quad 352.80$ $\quad \underline{0.62}$ $\quad 353.42$ $\quad \underline{6.22}$ $\quad 347.20$ $\quad \text{chk. B.M.}$ |
| E+2.5 = E " " " | | 6.31 | 354.39 | |
| E | | 6.1 | 354.6 | |
| | 8+50 | | | |
| E+10 = cl | | 6.75 | 353.95 | |
| G | | 7.0 | 353.7 | |
| +20 | | 7.0 | 353.7 | |
| +30 | | 7.0 | 353.7 | |
| +40 = Fence | | 7.3 | 353.4 | |
| +42 | | 8.3 | 352.4 | |
| +50 | | 8.3 | 352.4 | |
| | 9+01.92 = S. End. curb walk & paymt. | | | |
| E+86 = 10' out | | 10.0 | 350.7 | |
| E+76 = S.W. Cor. 10' walk to N. | | 7.98 | 352.72 | |
| E+66 = W. ent. cl & walk to N. | | 8.10 | 352.60 | |
| E+66 = W. gutter Pav S. End. | | 8.05 | 352.15 | |
| E+53 = " " " | | 7.97 | 352.73 | |
| E+40 Fence N. End | | 7.57 | 353.13 | |
| +30 | | 7.39 | 353.31 | |
| +20 | | 7.17 | 353.53 | |
| G | | 7.23 | 353.47 | |
| E+10 = cl | | 6.98 | 353.72 | |
| S. edge Alley Pav | | | | |
| +7.5 = W. edge walk N. End. | | 6.93 | 353.77 | |
| E+2.5 = S. Edge Alley Pav | | 6.78 | 353.92 | |
| E. Line = S " " " | | 6.75 | 353.95 | |
| Set B.M. on | | 6.84 | 353.86 | $\left\{ \begin{array}{l} \text{E. 5' line Euclid} \\ \text{3' S. of N. line} \\ \text{Belmont.} \end{array} \right.$ |

Indexed
C.S.K.

Additional Notes Euclid Ave N. of El Cajon Blvd.

356.86

Euclid

22

Widened

Copied from card by A.E.B.

6.39 352.10

345.71

N. Curb El Cajon Blvd

W.L. Euclid Top curb East end 5.59 346.51

Gutter Paring 5.94 346.16

7' North North Curb E/Cajon

W.L. Euclid sedge walk E. end 5.36 346.74

12' North North Curb El Cajon

W.L. Euclid N. edge walk E. end 5.18 346.92

No end of Pavement not very good

0.5 S of N.L. El Cajon W.L. Euclid 1 5.43 346.67

10 S " " " E.L. + 40 = N. W. cor Paring 5.55 346.55

15 S " " " E.L. + 20 5.21 346.89

2.0 S " " " E.L. + 10 5.08 347.02

4-15-38
walk
AM. 11.15 356.86 345.71
N. cb. El Cajon Ave

E+76 = Proposed W. Line - Top. eb. 10.18 346.68

E 76 = " " " Gutter par 10.96 345.90

4' W. of W. Line = E. End. 13' cb. inlet. 10.16 346.70 Top. eb.

" " " " " " 11.20 345.66 Gutter Pav.

7' N. of N. cb. = S. Edge cone walk

E+76 = Proposed W. Line 10.03 346.83

12' N. of N. cb. = N. Edge cone walk

E+76 = W. Line 9.93 346.93

N. Line El Cajon

E+66 9.8 347.1

E+76 = W. Line 9.8 347.1

0+00 = 20' 00" from W. Line on East

E+66 10.0 346.9

E+76 = W. Line 9.6 347.3

0+50

E+66 9.7 347.2

E+76 = W 9.7 347.2

1+00

E+66 9.5 347.4

E+76 = W 9.4 347.5

1+25

E+66 9.5 347.4

E+76 = W 9.3 347.6

1+50

E+66 10.2 346.7

E+76 = W. Line 9.4 347.5

1+73¹⁰

E+66 9.6 347.3

E+76 = W 10.0 346.9

2+00

E+66 9.5 347.4

E+76 = W 9.9 347.0

2+13

E+66 = S. E. Cor. Wooden Porch 9.7 347.4

E+74 = S. E. Cor. Frame House 9.7 347.2

E+98 = S. W. " " " 9.8 347.1

2+23⁵⁰

E+66 9.2 347.7

E+76 under House

356.86

2+24

E+68 N.E. Cor. Porch. 9.2 347.7

E+74 N.W. " " 9.2 347.7

2+33^E

E+84 = N.E. Cor. above House 9.2 347.7

E+98 = N.W. " " " 9.6 347.3

2+41

E+51^{1/2} = S.E. Cor. Stucco Office Bldg. 8.5 348.4

E+66 9.2 347.7

E+76 = W. Line 9.4 347.5

E+101^E = S.W. Cor. Stucco Office Bldg. 9.6 347.3

2+46

E+47.6 = S.E. Cor. ent. porch } ground 8.2 348.7
ent. porch 7.38 349.48E+51^{1/2} S.W. " " " ground. 8.2 348.72+55^EE+47^{1/2} = N.E. Cor. ent. porch. 8.2 348.7E+51^{1/2} = N.W. " " " 8.2 348.72+61^EE+51^{1/2} = N.E. Cor. Stucco Office Bldg. 8.2 348.7

E+66 9.0 347.9

E+76 = W. Line 9.4 347.5

E+101^E = N.W. " " " " 9.6 347.3

2+80

E+40 7.0 349.9

E+52 8.1 348.8

E+66 8.9 348.0

E+76 9.3 347.6

E+86 9.6 347.3

356.86

2+81

E+40 7.0 349.9

E+51^{1/2} Top. conc. wall S. End. 5.64 351.72

E+52 ground. to W. 8.1 348.8

E+66 8.9 348.0

E+76 9.3 347.6

E+86 9.6 347.3

3+00 changed from E+40 west

E+40 6.1 350.8

E+51^{1/2} Top. conc. wall 5.4 351.5

E+52 8.0 348.9

E+66 8.4 348.5

E+76 8.9 348.0

E+86 9.4 347.5

3+15

E+40 6.0 350.9

E+51^{1/2} Top. conc. wall N. End 5.15 351.71

E+52 7.4 349.5

E+66 8.4 348.5

E+76 8.8 348.1

E+86 9.2 347.7

3+16

E+40 6.0 350.9

E+52 7.4 349.5

E+66 8.4 348.5

E+76 8.8 348.1

E+86 9.2 347.7

Euclid

23

3+29

| | | |
|----------------------------|-------|----------|
| E+50 = S.E. Cor. shed. | 7.6 | 349.3 |
| E+66 | 8.3 | 348.6 |
| E+76 = W. | 8.8 | 348.1 |
| E+92 = S.W. Cor above shed | 9.4 | 347.5 |
| T.P. | 10.22 | 362.14 ✓ |
| | 4.94 | 351.92 |

3+50 N. End Lumber Cos. yard

| | | |
|---------------------|------|-------|
| E+50 - NE. Cor shed | 12.0 | 350.1 |
| E+66 | 12.5 | 349.6 |
| E+76 = W. | 13.6 | 348.5 |
| E+92 N.W. Cor. shed | 14.5 | 347.6 |

4+60

| | | |
|----------|------|-------|
| E+66 | 10.6 | 351.5 |
| E+76 = W | 11.6 | 350.5 |
| E+86 | 12.6 | 349.5 |

4+28 ³

| | | |
|----------|------|-------|
| E+66 | 9.7 | 352.4 |
| E+76 = W | 10.8 | 351.3 |
| E+86 | 11.8 | 350.3 |

4+50

| | | |
|----------|------|-------|
| E+66 | 9.6 | 352.5 |
| E+76 = W | 10.6 | 351.5 |
| E+86 | 11.4 | 350.7 |

4+78 Curb on E should be removed & a vertical curve
Replace the Brk. in Grade. There is no walk on E.

| | | |
|----------|------|-------|
| E+66 | 11.0 | 351.1 |
| E+76 = W | 9.7 | 352.4 |
| E+86 | 8.1 | 354.0 |

5+00

| | | |
|------|-----|-------|
| E+66 | 7.6 | 354.5 |
| E+76 | 8.5 | 353.6 |
| E+86 | 9.4 | 352.7 |

5+50

| | | | | |
|--------|--------------------------|-----|-------|--------------|
| E+51.5 | E. side of Double garage | 6.8 | 355.3 | wooden floor |
|--------|--------------------------|-----|-------|--------------|

5+60 ⁶ N. side of Garage

| | | |
|------------------------|------|-------|
| E+50 | 6.8 | 355.3 |
| E+66 | 9.0 | 353.1 |
| E+78 = N.W. Cor Garage | 10.0 | 352.1 |
| E+86 | 10.4 | 351.7 |

5+63

| | | |
|------|------|-------|
| E+50 | 7.5 | 354.6 |
| E+66 | 9.0 | 353.1 |
| E+76 | 10.0 | 352.1 |
| E+86 | 10.4 | 351.7 |

no original
see
cont

6+00 S. side of garage

| | | |
|----------------------------------|-----|-------|
| E+47 S.E. cor. garage dirt floor | 7.6 | 354.5 |
| E+66 | 8.6 | 353.5 |
| E+76 | 9.2 | 352.9 |
| E+86 | 9.4 | 352.7 |

| | | | | |
|------|------|----------|------|--------|
| T.P. | 8.80 | 360.42 ✓ | 7.52 | 354.62 |
|------|------|----------|------|--------|

6+50

| | | |
|------|-----|-------|
| E+66 | 8.0 | 352.4 |
| E+76 | 8.5 | 351.9 |
| E+86 | 9.0 | 351.4 |

Continued F.B. 1551 - P. 5

"A" LINE

Moore
4-13-27

Indexed
C.S.K.

Silvergate Ave. EXT. Thru P.L. 183
to Intersection of Canyon + Talbot St.

3+44.4

3+22.44 POT. Top of Chicken House

3+07

2+85.94 = E.C. = 2x2 Hub

$$\Delta = 16^{\circ}23'LT.$$

$$R = 1000$$

$$T = 143.95$$

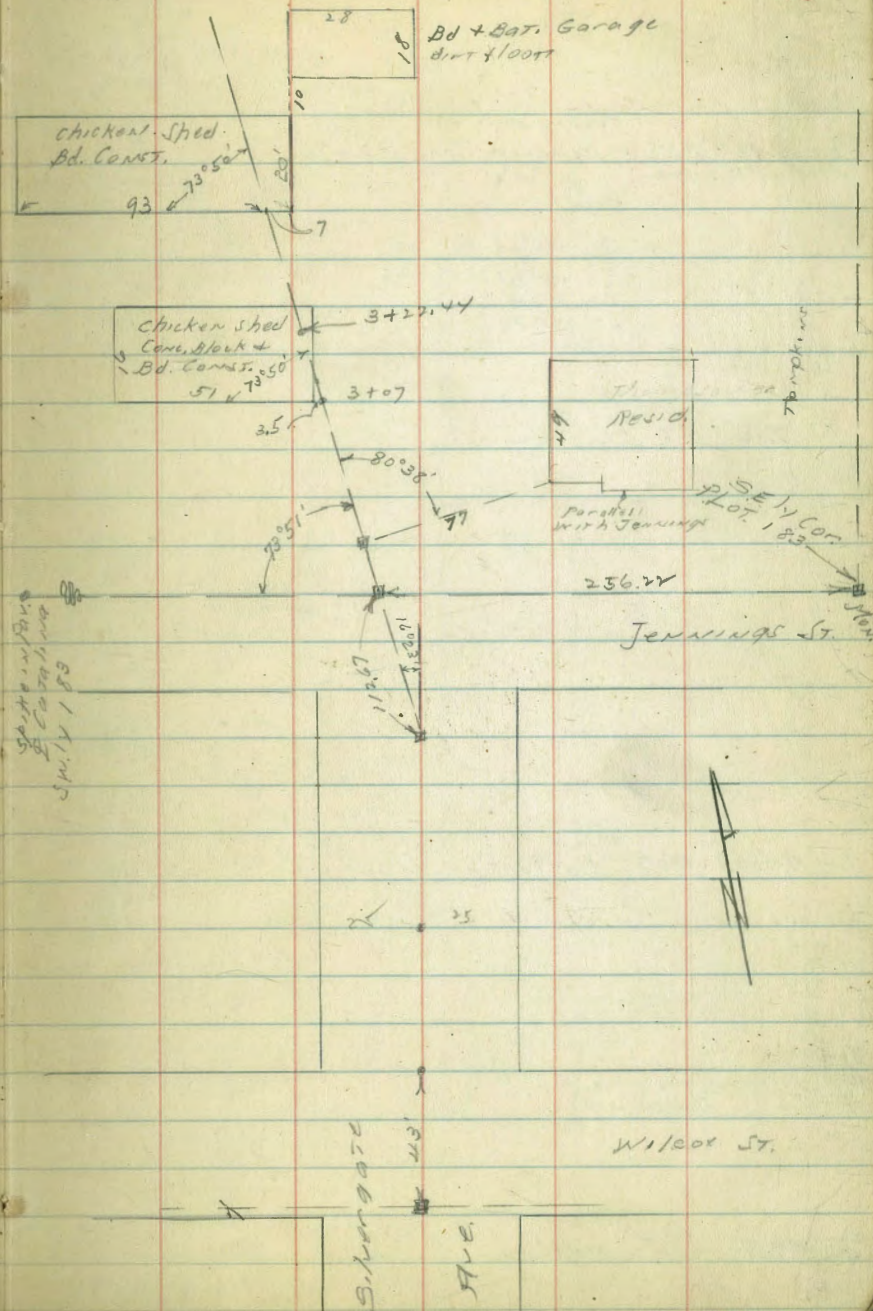
$$L = 285.94$$

$$1.7188 = 1'$$

1+43.95 = P.I. 2x2 Hub

0+00 = nail = B.C. "A" LINE

0+00 - 52.72 = nail = Nly Wilcox St.



Catalina Blvd
 13+32.98 = PRC = Cañon St Sta. 58+70
 END of "A" LINE

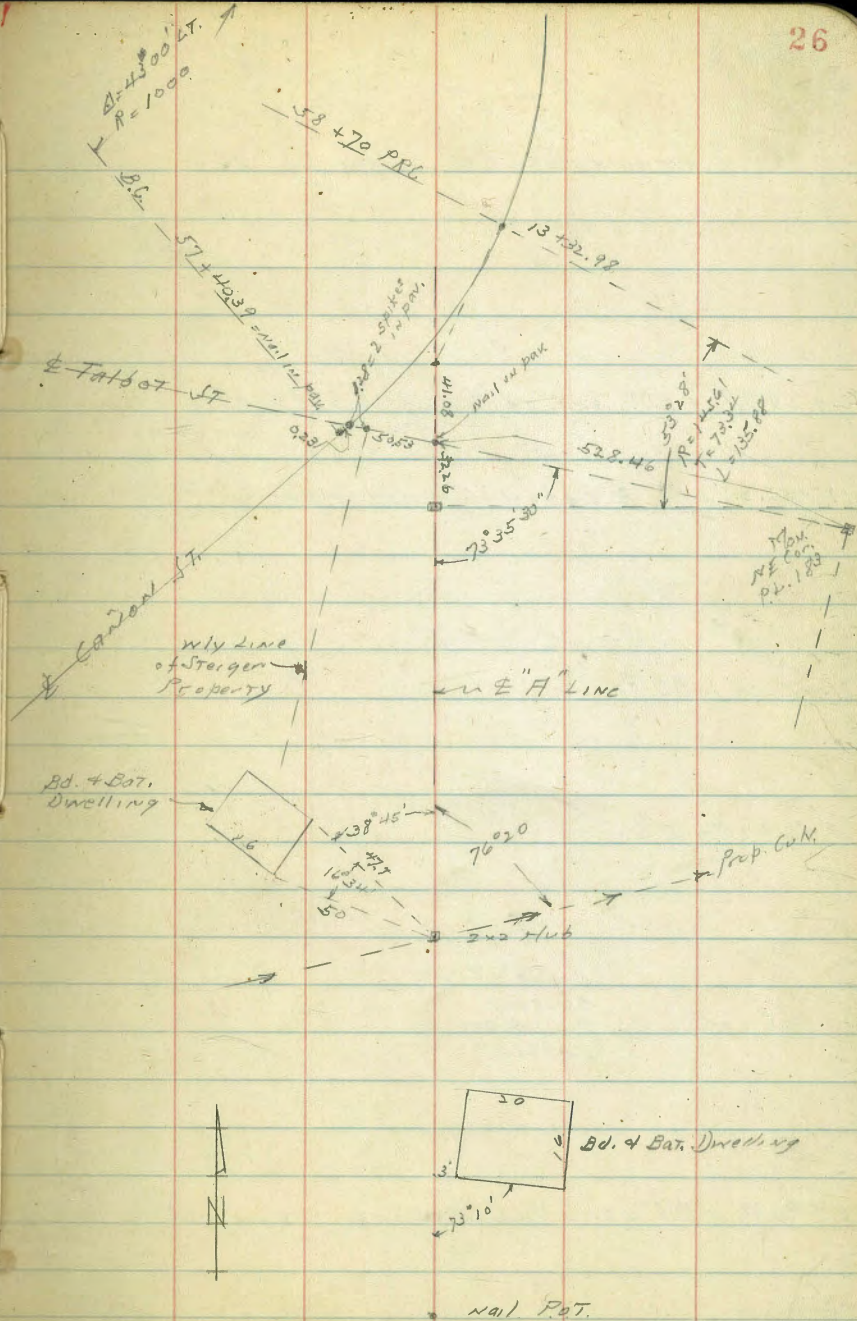
$A = 53^{\circ}28' RT$
 $R = 145.61$
 $T = 72.34$
 $L = 134.88$
 $11.80' = 1'$

11+97.10 B.C. RT. $\times \times$ Hub

7+94.30 P.O.T. Bottom of draw = Culv. $\times \times$ Hub

7+52 Dwelling

7+09.90 P.O.T. nail



"B" Line

Silvergate Ave. EXT. thro PL 183

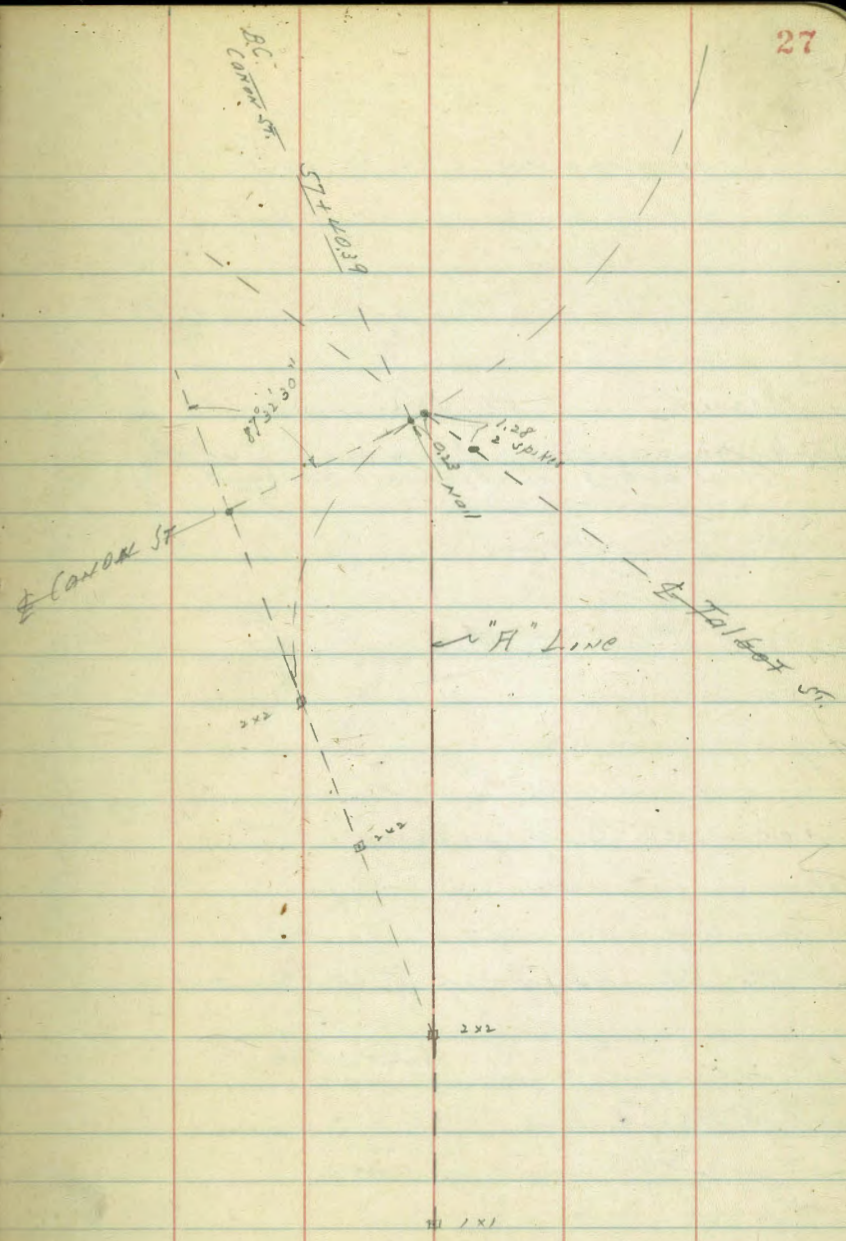
CANON ST. STA.
 12+69.79 = P.P.C. end of "B" Line = 57+40.39
 $\Delta = 87^{\circ}32'30''$ RT.
 $R = 60.68$
 12+35.21 = P.I. @ CANON ST. = nail in pav.
 $T = 58.13$
 $L = 92.71$

11+77.08 = B.C. PT

11+29.15 = E.C.

$\Delta = 26^{\circ}39' LT$
 $R = 500$
 $T = 118.42$
 $L = 232.57$
 10+15 = P.I.

8+96.58 = B.C. LT = Beg. "B" Line



"C" Line

Silvergate Ave EXT. thru Pl 183

58+29.72 Ed. spike in pav = EC Carver St.
 "C" Line
 10+23.96 = End of "C" Line = on Curve
 Meas. and A on forward Tangent

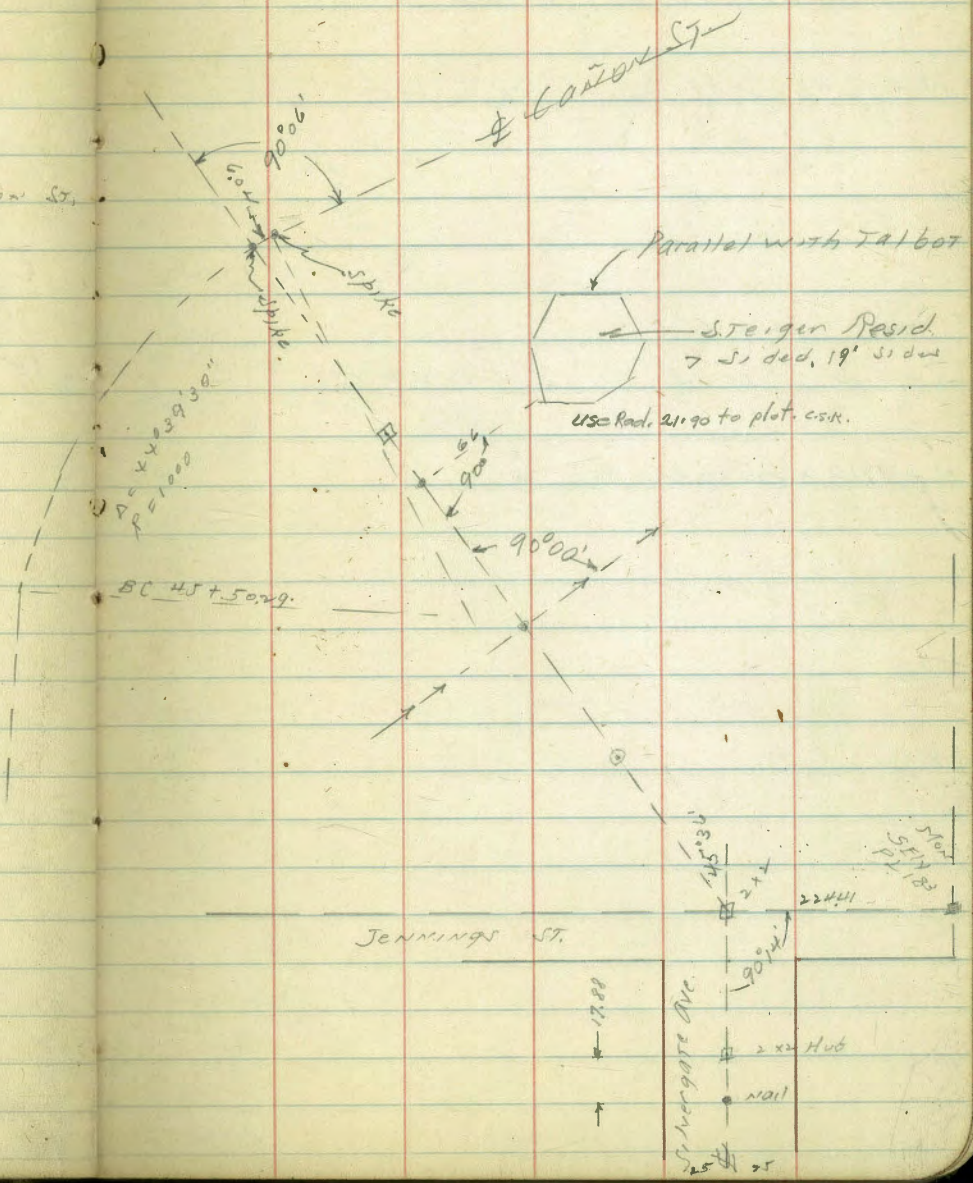
7+97.04 P.O.T. 2x2 Hub
 7+50

6+00 36" Culu. proposed

2+38.76 E.C. nail in roof of chicken house

$\Delta = 45^\circ 36' 17''$
 $R = 300$
 $T = 126.11$
 $L = 238.76$
 $S = 72.96$

0+17.88 = P.I. "A" Line 1+43.95
 0+00 = nail = BC LT.

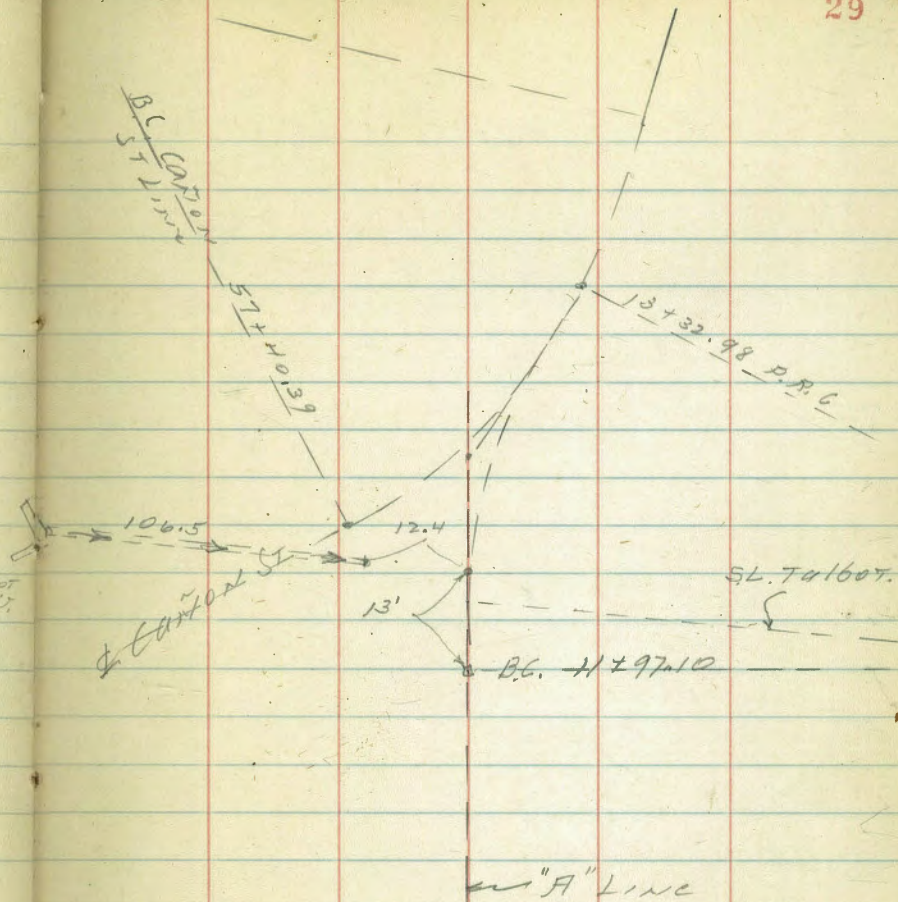


Location of Ex. 18" Corr. I.P. Culv.
at Canyon + Talbot.

13+32.98 = P.R.C. with Canyon St.

12+10.10 106.5' Ex. 18" Corr. I.P. Culv.
parallel with Talbot St.

11+97.10 = \gg = B.G. RT.



April
4-3-37

Cross Sec. of Rosecrans

Ingraham to Seville

To be graded 40' wide
and " " " full 80' width in cuts
for dirt

+50

see 1469-8 to 80

30

+50

29

+50

28

+50

27+00

26+77.45 on pave - zero section

SWBP

341

0.97

0.50

Rosecrans
Ingraham

see other book for pav. fl.

Indexed
C.S.K.

L.T.

P.T.

31

-0.2

+0.2

-0.3

+0.2

-0.7

-0.4

-0.7

-0.1

+0.2

-0.3

+0.2

-0.5

-0.4

-0.4

+0.3

+0.3

-0.3

+0.3

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+0.1

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+0.4

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+0.1

+0.1

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+0.5

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+0.4

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+0.1

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+0.4

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+0.5

+0.2

-0.3

+0.4

-0.2

+0.5

4
197

3/

+50

292

+50

293

+50

294

+50

297

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297

41 CONST. 18" CUM AT 90° WITH F

+50

40

39 +6106 EC 4° 29.60

+50 4° 13.78

39 3° 02.16

+50 1° 50.54

38 0° 38.92

384

27

| | | | | | | | | | | | | | | | | |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|--------------------|
| $\frac{5.5}{20}$ | $\frac{4.8}{25}$ | $\frac{4.1}{30}$ | $\frac{3.4}{35}$ | $\frac{2.7}{40}$ | $\frac{2.0}{45}$ | $\frac{1.3}{50}$ | $\frac{0.6}{55}$ | $\frac{0.0}{60}$ | $\frac{0.7}{65}$ | $\frac{1.4}{70}$ | $\frac{2.1}{75}$ | $\frac{2.8}{80}$ | $\frac{3.5}{85}$ | $\frac{4.2}{90}$ | $\frac{4.9}{95}$ | $\frac{5.6}{100}$ |
| -1.2 | -1.0 | -0.8 | -0.6 | -0.4 | -0.2 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 | 2.0 |
| $\frac{4.5}{20}$ | $\frac{3.9}{25}$ | $\frac{3.3}{30}$ | $\frac{2.7}{35}$ | $\frac{2.1}{40}$ | $\frac{1.5}{45}$ | $\frac{0.9}{50}$ | $\frac{0.3}{55}$ | $\frac{-0.3}{60}$ | $\frac{-0.9}{65}$ | $\frac{-1.5}{70}$ | $\frac{-2.1}{75}$ | $\frac{-2.7}{80}$ | $\frac{-3.3}{85}$ | $\frac{-3.9}{90}$ | $\frac{-4.5}{95}$ | $\frac{-5.1}{100}$ |
| -1.2 | -1.0 | -0.8 | -0.6 | -0.4 | -0.2 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 | 2.0 |
| $\frac{4.5}{20}$ | $\frac{3.9}{25}$ | $\frac{3.3}{30}$ | $\frac{2.7}{35}$ | $\frac{2.1}{40}$ | $\frac{1.5}{45}$ | $\frac{0.9}{50}$ | $\frac{0.3}{55}$ | $\frac{-0.3}{60}$ | $\frac{-0.9}{65}$ | $\frac{-1.5}{70}$ | $\frac{-2.1}{75}$ | $\frac{-2.7}{80}$ | $\frac{-3.3}{85}$ | $\frac{-3.9}{90}$ | $\frac{-4.5}{95}$ | $\frac{-5.1}{100}$ |
| -1.2 | -1.0 | -0.8 | -0.6 | -0.4 | -0.2 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 | 2.0 |
| $\frac{4.5}{20}$ | $\frac{3.9}{25}$ | $\frac{3.3}{30}$ | $\frac{2.7}{35}$ | $\frac{2.1}{40}$ | $\frac{1.5}{45}$ | $\frac{0.9}{50}$ | $\frac{0.3}{55}$ | $\frac{-0.3}{60}$ | $\frac{-0.9}{65}$ | $\frac{-1.5}{70}$ | $\frac{-2.1}{75}$ | $\frac{-2.7}{80}$ | $\frac{-3.3}{85}$ | $\frac{-3.9}{90}$ | $\frac{-4.5}{95}$ | $\frac{-5.1}{100}$ |
| -1.2 | -1.0 | -0.8 | -0.6 | -0.4 | -0.2 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 | 2.0 |

34

384

41 + 50

42

TP

12.07 13.28 2.40 1.41

+50

43

+50

44

+50

$\frac{5}{3} \begin{array}{r} -1.4 \\ 0 \end{array}$
 $\frac{2}{5} \begin{array}{r} -1.2 \\ 0 \end{array}$
 $\frac{1}{9} \begin{array}{r} +0.7 \\ 0 \end{array}$
 $\frac{6}{0} \begin{array}{r} +0.8 \\ 0 \end{array}$
 $\frac{3}{7} \begin{array}{r} +0.7 \\ 0 \end{array}$
 $\frac{2}{4} \begin{array}{r} -0.7 \\ 0 \end{array}$
 $\frac{1}{0} \begin{array}{r} -0.6 \\ 0 \end{array}$

$\frac{5}{5} \begin{array}{r} -1.3 \\ 0 \end{array}$
 $\frac{2}{5} \begin{array}{r} -0.8 \\ 0 \end{array}$
 $\frac{2}{9} \begin{array}{r} +1.2 \\ 0 \end{array}$
 $\frac{2}{2} \begin{array}{r} +1.3 \\ 0 \end{array}$
 $\frac{1}{7} \begin{array}{r} +1.6 \\ 0 \end{array}$
 $\frac{1}{0} \begin{array}{r} 0.0 \\ 0 \end{array}$
 $\frac{5}{5} \begin{array}{r} -0.4 \\ 0 \end{array}$

$\frac{5}{0} \begin{array}{r} -1.2 \\ 0 \end{array}$
 $\frac{2}{5} \begin{array}{r} -0.9 \\ 0 \end{array}$
 $\frac{2}{19} \begin{array}{r} +2.0 \\ 0 \end{array}$
 $\frac{1}{3} \begin{array}{r} +2.2 \\ 0 \end{array}$
 $\frac{1}{7} \begin{array}{r} +2.0 \\ 0 \end{array}$
 $\frac{2}{5} \begin{array}{r} +0.5 \\ 0 \end{array}$
 $\frac{5}{0} \begin{array}{r} +0.4 \\ 0 \end{array}$

$\frac{5}{0} \begin{array}{r} -0.8 \\ 0 \end{array}$
 $\frac{2}{5} \begin{array}{r} -0.3 \\ 0 \end{array}$
 $\frac{10}{19} \begin{array}{r} +3.2 \\ 0 \end{array}$
 $\frac{10}{0} \begin{array}{r} +3.5 \\ 0 \end{array}$
 $\frac{10}{17} \begin{array}{r} +3.5 \\ 0 \end{array}$
 $\frac{12}{21} \begin{array}{r} +1.5 \\ 0 \end{array}$
 $\frac{11}{0} \begin{array}{r} +2.5 \\ 0 \end{array}$

$\frac{5}{0} \begin{array}{r} +2.8 \\ 0 \end{array}$
 $\frac{2}{4} \begin{array}{r} +3.2 \\ 0 \end{array}$
 $\frac{2}{7} \begin{array}{r} +5.1 \\ 0 \end{array}$
 $\frac{8}{0} \begin{array}{r} +5.5 \\ 0 \end{array}$
 $\frac{4}{4} \begin{array}{r} +5.0 \\ 0 \end{array}$
 $\frac{5}{4} \begin{array}{r} +5.4 \\ 0 \end{array}$
 $\frac{8}{0} \begin{array}{r} +6.1 \\ 0 \end{array}$
 $\frac{10}{0} \begin{array}{r} +6.6 \\ 0 \end{array}$

$\frac{5}{0} \begin{array}{r} +7.8 \\ 0 \end{array}$
 $\frac{2}{9} \begin{array}{r} +7.8 \\ 0 \end{array}$
 $\frac{5}{19} \begin{array}{r} +8.1 \\ 0 \end{array}$
 $\frac{5}{7} \begin{array}{r} +7.6 \\ 0 \end{array}$
 $\frac{5}{8} \begin{array}{r} +7.7 \\ 0 \end{array}$
 $\frac{5}{10} \begin{array}{r} +7.6 \\ 0 \end{array}$
 $\frac{5}{8} \begin{array}{r} +8.2 \\ 0 \end{array}$
 $\frac{2}{7} \begin{array}{r} +8.8 \\ 0 \end{array}$
 $\frac{5}{0} \begin{array}{r} +10.7 \\ 0 \end{array}$
 $\frac{10}{0} \begin{array}{r} +11.0 \\ 0 \end{array}$

$\frac{1}{40} \begin{array}{r} 12.4 \\ 0 \end{array}$
 $\frac{1}{41} \begin{array}{r} 12.5 \\ 0 \end{array}$
 $\frac{1}{40} \begin{array}{r} 10.7 \\ 0 \end{array}$
 $\frac{2}{20} \begin{array}{r} 10.6 \\ 0 \end{array}$
 $\frac{1}{18} \begin{array}{r} 9.8 \\ 0 \end{array}$
 $\frac{5}{4} \begin{array}{r} 10.1 \\ 0 \end{array}$
 $\frac{2}{17} \begin{array}{r} 9.6 \\ 0 \end{array}$
 $\frac{1}{18} \begin{array}{r} 10.4 \\ 0 \end{array}$
 $\frac{2}{17} \begin{array}{r} 10.7 \\ 0 \end{array}$
 $\frac{6}{0} \begin{array}{r} 13.1 \\ 0 \end{array}$
 $\frac{5}{0} \begin{array}{r} 13.4 \\ 0 \end{array}$

584

584

51 16° 43.15

T.P. 1208 58.92 0.51 2682

+50 13° 51.3

50 10° 59.4

+50 8° 07.5

49 5° 15.0

+50 2° 29.7

48+0830 B.C. RT

27.35

| | LT | RT | RT |
|------|------|------|------|
| 28.4 | 28.4 | 28.4 | 28.4 |
| 10.5 | 10.5 | 10.5 | 10.5 |
| 20 | 20 | 20 | 20 |
| 26.5 | 26.5 | 26.5 | 26.5 |
| 12.5 | 12.5 | 12.5 | 12.5 |
| 19 | 19 | 19 | 19 |
| 28.4 | 28.4 | 28.4 | 28.4 |
| 10.5 | 10.5 | 10.5 | 10.5 |
| 20 | 20 | 20 | 20 |
| 26.5 | 26.5 | 26.5 | 26.5 |
| 12.5 | 12.5 | 12.5 | 12.5 |
| 19 | 19 | 19 | 19 |
| 27.1 | 27.1 | 27.1 | 27.1 |
| 11.8 | 11.8 | 11.8 | 11.8 |
| 18 | 18 | 18 | 18 |
| 26.3 | 26.3 | 26.3 | 26.3 |
| 12.6 | 12.6 | 12.6 | 12.6 |
| 23 | 23 | 23 | 23 |
| 29.0 | 29.0 | 29.0 | 29.0 |
| 9.9 | 9.9 | 9.9 | 9.9 |
| 28 | 28 | 28 | 28 |
| 29.0 | 29.0 | 29.0 | 29.0 |
| 9.9 | 9.9 | 9.9 | 9.9 |
| 28 | 28 | 28 | 28 |
| 31.5 | 31.5 | 31.5 | 31.5 |
| 7.2 | 7.2 | 7.2 | 7.2 |
| 40 | 40 | 40 | 40 |

| | | | |
|------|------|------|------|
| 24.9 | 24.9 | 24.9 | 24.9 |
| 4.0 | 4.0 | 4.0 | 4.0 |
| 25.1 | 25.1 | 25.1 | 25.1 |
| 1.6 | 1.6 | 1.6 | 1.6 |
| 21.9 | 21.9 | 21.9 | 21.9 |
| 15.5 | 15.5 | 15.5 | 15.5 |
| 20 | 20 | 20 | 20 |
| 21.9 | 21.9 | 21.9 | 21.9 |
| 15.5 | 15.5 | 15.5 | 15.5 |
| 20 | 20 | 20 | 20 |
| 25.9 | 25.9 | 25.9 | 25.9 |
| 1.6 | 1.6 | 1.6 | 1.6 |
| 20 | 20 | 20 | 20 |
| 18.9 | 18.9 | 18.9 | 18.9 |
| 5.0 | 5.0 | 5.0 | 5.0 |
| 19.6 | 19.6 | 19.6 | 19.6 |
| 7.8 | 7.8 | 7.8 | 7.8 |
| 16 | 16 | 16 | 16 |
| 20.2 | 20.2 | 20.2 | 20.2 |
| 18 | 18 | 18 | 18 |
| 19.9 | 19.9 | 19.9 | 19.9 |
| 1.0 | 1.0 | 1.0 | 1.0 |
| 17.8 | 17.8 | 17.8 | 17.8 |
| 9.0 | 9.0 | 9.0 | 9.0 |
| 17 | 17 | 17 | 17 |
| 18.9 | 18.9 | 18.9 | 18.9 |
| 8.5 | 8.5 | 8.5 | 8.5 |
| 17.7 | 17.7 | 17.7 | 17.7 |
| 15 | 15 | 15 | 15 |
| 16.1 | 16.1 | 16.1 | 16.1 |
| 11.2 | 11.2 | 11.2 | 11.2 |
| 15 | 15 | 15 | 15 |
| 17.0 | 17.0 | 17.0 | 17.0 |
| 10.4 | 10.4 | 10.4 | 10.4 |
| 20 | 20 | 20 | 20 |
| 15.1 | 15.1 | 15.1 | 15.1 |
| 12.3 | 12.3 | 12.3 | 12.3 |
| 20 | 20 | 20 | 20 |
| 15.6 | 15.6 | 15.6 | 15.6 |
| 11.8 | 11.8 | 11.8 | 11.8 |
| 20 | 20 | 20 | 20 |
| 16.1 | 16.1 | 16.1 | 16.1 |
| 11.2 | 11.2 | 11.2 | 11.2 |
| 15 | 15 | 15 | 15 |
| 15.7 | 15.7 | 15.7 | 15.7 |
| 11.7 | 11.7 | 11.7 | 11.7 |
| 17 | 17 | 17 | 17 |
| 15.3 | 15.3 | 15.3 | 15.3 |
| 14.1 | 14.1 | 14.1 | 14.1 |
| 17 | 17 | 17 | 17 |
| 16.1 | 16.1 | 16.1 | 16.1 |
| 11.3 | 11.3 | 11.3 | 11.3 |
| 19 | 19 | 19 | 19 |
| 16.6 | 16.6 | 16.6 | 16.6 |
| 10.8 | 10.8 | 10.8 | 10.8 |
| 20 | 20 | 20 | 20 |
| 14.7 | 14.7 | 14.7 | 14.7 |
| 17 | 17 | 17 | 17 |
| 15.2 | 15.2 | 15.2 | 15.2 |
| 12.2 | 12.2 | 12.2 | 12.2 |
| 19 | 19 | 19 | 19 |
| 15.7 | 15.7 | 15.7 | 15.7 |
| 11.7 | 11.7 | 11.7 | 11.7 |
| 20 | 20 | 20 | 20 |

27.35

LT

R

RT

check to 811 BP SW Rosser Rd
 6117 807 408 41.58 41.59
 F.P. 7.98 45.66 119 37.73

54 + 59.42 = 20¢ spike in pay. See. Taxes on edge of pay.

54 + 15.47 EL 20 20.

54 22 24.9

51 + 50 19 45.64

3894

3892

| | | | | | | | | | | | |
|-----|------|-----|------|-----|------|-----|------|-----|------|-----|------|
| 40 | 35.5 | 40 | 34.8 | 40 | 31.8 | 40 | 31.5 | 40 | 30.7 | 40 | 30.7 |
| 29 | 35.9 | 29 | 35.2 | 29 | 31.8 | 29 | 31.5 | 29 | 32.8 | 29 | 32.8 |
| 26 | 32.9 | 26 | 35.2 | 26 | 29.3 | 26 | 29.3 | 26 | 32.7 | 26 | 32.7 |
| 20 | 32.7 | 20 | 31.4 | 20 | 29.4 | 20 | 29.4 | 20 | 31.7 | 20 | 31.7 |
| 19 | 34.1 | 19 | 33.5 | 19 | 31.5 | 19 | 31.5 | 19 | 31.5 | 19 | 31.5 |
| 6 | 35.0 | 6 | 34.3 | 6 | 31.5 | 6 | 31.5 | 6 | 33.8 | 6 | 33.8 |
| 2.6 | 35.4 | 2.6 | 32.9 | 2.6 | 30.7 | 2.6 | 30.7 | 2.6 | 31.8 | 2.6 | 31.8 |
| 2.7 | 34.9 | 2.7 | 35.7 | 2.7 | 32.8 | 2.7 | 32.8 | 2.7 | 32.7 | 2.7 | 32.7 |
| 40 | 36.5 | 40 | 35.1 | 40 | 32.7 | 40 | 32.7 | 40 | 31.8 | 40 | 31.8 |
| 40 | 36.2 | 40 | 36.5 | 40 | 34.4 | 40 | 34.4 | 40 | 32.7 | 40 | 32.7 |
| 2.1 | 36.7 | 2.1 | 36.2 | 2.1 | 34.4 | 2.1 | 34.4 | 2.1 | 32.7 | 2.1 | 32.7 |
| 2.1 | 36.7 | 2.1 | 36.2 | 2.1 | 34.4 | 2.1 | 34.4 | 2.1 | 32.7 | 2.1 | 32.7 |
| 2.1 | 36.7 | 2.1 | 36.2 | 2.1 | 34.4 | 2.1 | 34.4 | 2.1 | 32.7 | 2.1 | 32.7 |

5-19-37

Muller
Walker
Bliss

X Sec. Alleys Bk. 64 E. W. Morse
Bet. C + Broadway - 28th + 29th

Indexed
C.S.R.

39

— BM BP — 11.61 — 187.66 — 176.05 —
— T.P. — 11.93 — 198.17 — 142 — 186.24 —

N + S. Alley.

14' N. of S. line = s. d. line of C. St.

| | | |
|-------------|-------|--------|
| W. cont. d. | 9.82 | 188.35 |
| N. pav. | 10.30 | 187.87 |
| ☐ " | 9.74 | 188.43 |
| E. " | 9.21 | 188.96 |
| E. cont. d. | 8.80 | 189.37 |

0+00 - 9 Line C. St.

| | | |
|--|------|--------|
| E. cont. d. s. End | 8.54 | 189.63 |
| E. pav. " " | 9.00 | 189.17 |
| ☐ " " " | 9.50 | 188.67 |
| W. " " " | 9.44 | 188.73 |
| W. cont. d. " " } N.E. Cor. Garage N. Front | 9.31 | 188.86 |

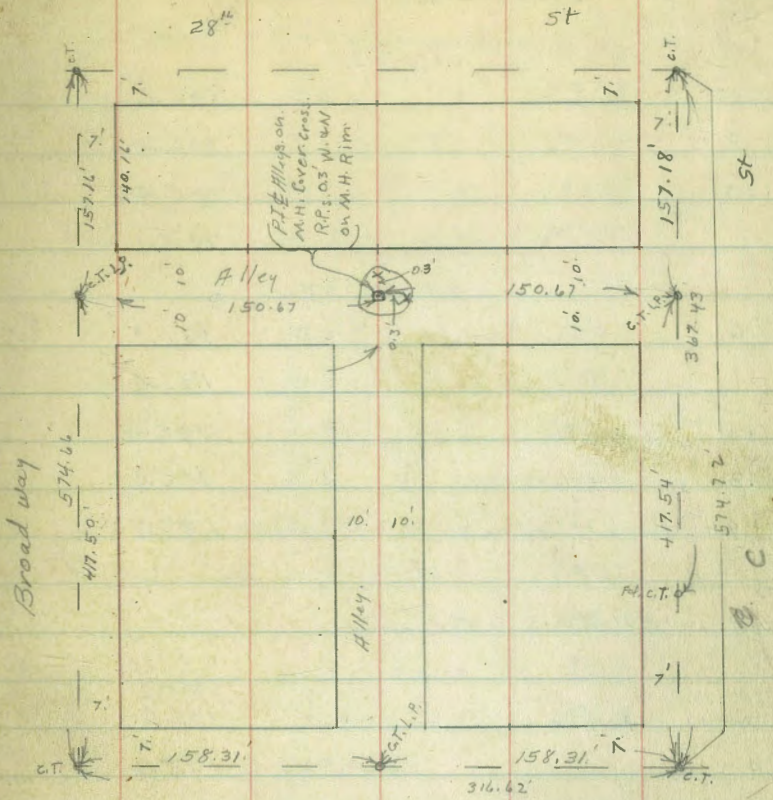
0+00²⁰ S.

| | | |
|---------------------|------|--------|
| W. = E. side garage | 7.8 | 190.4 |
| ☐ | 6.7 | 191.8 |
| E. | 6.7 | 191.5 |
| E. Top. wall | 4.88 | 193.29 |

0+03

| | | |
|-----------------|-----|-------|
| E | 4.9 | 193.3 |
| ☐ | 5.4 | 192.8 |
| W E Side Garage | 6.8 | 191.4 |

— T.P. — 5.28 — 200.09 — 3.36 — 194.81 — Top. Gas. Pipe



200.09

0+05 S.

| | | |
|-----------------------|-----|-------|
| W+05 = E. side garage | 3.5 | 196.6 |
| ± | 3.2 | 196.9 |
| +5 | 3.7 | 196.4 |
| E | 5.0 | 195.1 |

0+10

| | | |
|-----------------------|-----|-------|
| E | 2.8 | 197.3 |
| ± | 2.3 | 197.8 |
| +4 | 3.2 | 196.9 |
| +9.3 = E. side Garage | 3.5 | 196.6 |
| +9.4 Roof of Garage | 2.4 | 197.7 |

0+18 = S. End. Garage on W.

0.9 in Alley = S. E. car Garage

0+50

| | | |
|----------------|-----|-------|
| W | 4.9 | 195.2 |
| W+07 = Fence | 4.9 | 195.2 |
| ± | 4.8 | 195.3 |
| E. 9.5 = Fence | 4.6 | 195.5 |

0+81

| | | |
|-------------|-----|-------|
| E. Fence OK | 6.8 | 193.3 |
| ± | 6.9 | 193.2 |
| W. Fence OK | 6.7 | 193.4 |

0+84 = N. End. double garage on W. line cmt. floor

| | | |
|---------------------------|------|--------|
| W. = floor | 8.24 | 191.85 |
| +1.5 = E. Edge cmt. apron | 8.32 | 191.77 |
| ± | 7.1 | 193.0 |
| E | 6.8 | 193.3 |

200.09

40

0+99 = S. End. above garage on W. line

| | | |
|---------------------------|------|--------|
| E | 7.6 | 192.5 |
| ± | 8.2 | 191.9 |
| +8.5 = E. Edge cmt. apron | 8.37 | 191.72 |
| W = floor | 8.26 | 191.83 |

1+30

| | | |
|----|------|-------|
| W | 11.0 | 189.1 |
| ± | 11.0 | 189.1 |
| +4 | 10.7 | 189.4 |
| E | 9.3 | 190.8 |

1+40 [±] = N. line E. & W. Alley

| | | |
|----|------|-------|
| E. | 9.7 | 190.4 |
| +3 | 11.4 | 188.7 |
| ± | 11.7 | 188.4 |
| W | 12.2 | 187.9 |

1+50 [±] = ± E & W Alley

| | | |
|--------------------|-------|--------|
| W - 15 | 14.5 | 185.6 |
| W | 13.3 | 186.8 |
| W + 5 | 12.4 | 187.7 |
| ± Top. sewer M. H. | 12.18 | 187.91 |
| E | 11.7 | 188.4 |

1+60 [±] = S. Line E & W Alley

| | | |
|----|------|-------|
| E | 11.6 | 188.5 |
| ± | 12.8 | 187.3 |
| +7 | 12.9 | 187.2 |
| W. | 14.0 | 186.1 |

2+00

| | | |
|----|------|-------|
| W | 16.5 | 183.6 |
| +3 | 14.5 | 185.6 |
| £ | 14.5 | 185.6 |
| E | 14.0 | 186.1 |

T.P. 0.59 188.48 12.20 187.89

2+20

| | | |
|----|-----|-------|
| E | 2.9 | 185.6 |
| £ | 3.0 | 185.5 |
| +4 | 3.5 | 185.0 |
| W | 5.7 | 182.8 |
| +5 | 6.9 | 181.6 |

2+50

| | | |
|-----|-----|-------|
| W-5 | 5.4 | 183.1 |
| W | 4.8 | 183.7 |
| £ | 3.4 | 185.1 |
| +9 | 3.9 | 185.4 |
| E | 2.4 | 186.1 |

2+60

| | | |
|----|-----|-------|
| E | 1.7 | 186.8 |
| +3 | 3.0 | 185.5 |
| £ | 3.7 | 184.8 |
| +8 | 3.7 | 184.8 |
| W | 4.2 | 184.3 |

2+72

| | | |
|----|-----|-------|
| W | 3.6 | 184.9 |
| +3 | 3.6 | 184.9 |
| +5 | 5.5 | 183.0 |
| +V | 6.5 | 182.0 |
| £ | 6.6 | 181.9 |
| +5 | 5.6 | 182.9 |
| E | 1.4 | 187.1 |

2+92

| | | |
|----|------|-------|
| E | 6.6 | 181.9 |
| £ | 11.2 | 177.3 |
| +3 | 10.8 | 178.0 |
| +5 | 7.5 | 181.0 |
| +7 | 3.4 | 185.1 |
| W | 3.4 | 185.1 |

2+97

| | | |
|----|------|-------|
| W | 4.0 | 184.5 |
| +9 | 8.5 | 180.0 |
| +5 | 13.6 | 174.9 |
| £ | 13.0 | 175.5 |
| +7 | 12.6 | 175.9 |
| E | 9.5 | 179.0 |

T.P. 2.75 178.22 13.01 175.47

3+0134 = N. Line Broadway curb + Pav. deep.

| | | | |
|----|--------|-----|-------|
| E | ground | 2.9 | 175.3 |
| +5 | " | 4.1 | 174.1 |
| ± | " | 4.2 | 174.0 |
| W | " | 4.2 | 174.0 |

4' S. of N. Line

| | | | |
|----|----------|------|--------|
| W. | ent. cl. | 5.80 | 172.42 |
| W. | pav. | 6.06 | 172.16 |
| ± | " | 5.60 | 172.62 |
| E. | " | 4.74 | 173.48 |
| E. | ent. cl. | 4.18 | 174.04 |

9' S. of N. Line

| | | | |
|----|----------|------|--------|
| E. | ent. cl. | 4.74 | 174.04 |
| E. | pav. | 4.76 | 173.46 |
| ± | " | 5.66 | 172.56 |
| W. | " | 6.27 | 171.95 |
| W | ent. cl. | 5.84 | 172.38 |

14' S. of N. line = N. cl. Line Broadway

| | | | |
|----|----------|------|--------|
| W. | ent. cl. | 5.93 | 172.29 |
| W | pav. | 6.56 | 171.66 |
| ± | " | 5.75 | 172.47 |
| E | " | 4.93 | 173.29 |
| E. | ent. cl. | 4.20 | 174.02 |

T.P. — 1207 — 199.93 — 187.49 —

Top. M.H.
Page 41

0+00 = E. Line N & S. Alley

| | | | |
|-----|---------------------------|------|-------|
| N | Board Fence 0.3' in Alley | 9.5 | 190.4 |
| + 4 | " | 11.3 | 188.6 |
| ± | " | 11.5 | 188.4 |
| S | " | 11.4 | 188.5 |

0+25

| | | | |
|----|------------|-----|-------|
| S | " | 9.4 | 190.5 |
| ± | " | 9.1 | 190.8 |
| N. | Fence 0.5' | 8.4 | 191.5 |

0+44 garage on N. dirt floor 0.5 Back

| | | |
|-----------------|-----|-------|
| N - 0.5 = floor | 7.2 | 192.7 |
|-----------------|-----|-------|

0+50

| | | | |
|---|---|-----|-------|
| N | " | 6.3 | 193.6 |
| ± | " | 7.1 | 192.8 |
| S | " | | |

0+61 ± double garage on N. ent. floor 6' Back

| | | |
|------------------|------|--------|
| N - 6.0' = floor | 5.36 | 194.57 |
|------------------|------|--------|

1+00

| | | | |
|----|---|-----|-------|
| S. | " | 4.6 | 195.3 |
| ± | " | 4.5 | 195.4 |
| N | " | 4.2 | 195.7 |

1+30 = W. End ^{double} garage on N. dirt floor 0.6 Back
 N-0.6' floor 3.8 196.1

1+48 = E. End above garage
 N-0.6' = floor 3.7 196.2

1+50

N 3.7 196.2

⊕ 3.7 196.2

S 4.0 195.9

1+86 = W. End double garage on N dirt floor 3.0 Back
 N-3.0' = floor 3.0 196.9

1+97 = E. End above garage
 N-3.0' = floor 3.0 196.9

2+0.0

S 3.4 196.5

⊕ 3.1 196.8

N. 2.6 197.3

2+07 garage on N. cnt. floor 3' Back

N-1.6' = S. End. cnt. apron. 2.13 197.80

N-3.0' = floor 2.78 198.15

2+15 = W. End double garage on N cnt. floor 1.0 Back

N. = S. End. cnt. apron 2.00 197.93

N-1.0' = floor 1.80 198.13

2+31 = E. End above garage

N-1.0' = floor 1.92 198.01

N = S. End. cnt. apron. 2.03 197.90

⊕ 2.6 197.3

S 2.7 197.2

2+50

S 2.8 197.1

⊕ 2.7 197.2

N 2.6 197.3

2+56 garage on S. dirt floor 0.9 Back

S-0.9' = floor 2.9 197.0

2+75

N. 2.9 197.0

⊕ 3.0 196.9

S. 3.0 196.9

3+00

S 3.6 196.3

⊕ 3.6 196.3

N. 3.2 196.7

Y.P. — 1.71 — 198.05 — 3.59 — 196.34 —

3+05 = W. End double garage on S. cnt. floor 2.3 Back

S-2.3' floor 1.81 196.24

S-0.8' = N. End. cnt. apron 1.97 196.08

3+19 = E. End above garage 3.3' Back Not. parallel

S-3.3' = floor 1.88 196.17

S-0.8' = N. End. cnt. apron 2.05 196.00

3+50

N 3.4 194.7

⊕ 3.1 195.0

S 2.8 195.3

198.05.

3+54 garage on N. dirt floor 1.3' Back

N-1.3 = floor 3.3 194.8

3+63 garage on N. Wooden floor 0.7' Back

N-0.7 = floor. 3.3 194.8

3+65

S 3.2 194.9

+8.5 = Top of M.H. 3.37 194.68

ϕ 3.6 194.5

N 3.6 194.5

3+85

N 4.5 193.6

+4. 4.7 193.4

+6. 6.4 191.7

ϕ 6.8 191.3

+4 6.8 191.3

+7 6.2 191.9

+8 4.6 193.5

S. 4.6 193.5

3+95

S 4.9 193.2

+3 8.3 189.8

ϕ 8.9 189.2

+4 8.2 189.9

N. 5.1 193.0

198.05

400.5

3+95 E = W. Line 29th St.

N. cont. d. 10.00 188.05

N. pav 10.10 187.95

ϕ " 10.12 187.93

S " 9.69 188.36

S. cont. d. 9.37 188.68

10' E. of W. Line = W. d. Line of 29th St

S. cont. d. 9.53 188.52

S. pav 10.17 187.88

ϕ " 10.53 187.52

S. " 10.82 187.23

S. cont. d. 10.14 187.91

T.P. 3.47 193.67 4.85 193.20

T.P. 3.37 184.24 12.80 180.87

chk: orig BM 8.19 176.05

44

30. Roadway
7.50 1/4s.

Boundary St. X See

Thorn St. South
curbed + walks. in

7-6-37
Miller
Walker
Bliss

Indexed
c. 500

294.07

45

B.M. B.P. — 0.96 — 304.65 — — 303.69 — N.E. Thorn + Nite

T.P. Top Hydt — 0.13 — 294.07 — 10.71 — 293.94 —

0+00 = N. line Redwood on E. 60' wide 10' closed

20' N. of S. End Pav = { 6+22 North on W. curb } diagonal
 { 6+35.5 North on E. curb }

E. ch. line = pav 3.86 290.21

1/4 " 3.92 290.15

1/4 " 3.89 290.18

1/4 " 3.87 290.20

W. ch. Line " 3.73 290.34

10' N. of S. edge Pav { 6+12' N. on W. curb } on diagonal
 { 6+25.5 " " E. " }

W. ch. line = pav 4.41 289.66

1/4 " 4.44 289.63

1/4 " 4.46 289.61

1/4 " 4.51 289.56

E. ch. line " 4.63 289.44

6+19.2 = S. line Thorn St. to E.

E. curb. 4.29 289.98

gutter pav. 4.92 289.15

S. Edge Ex. Pav. = { 6+02' N. on W. ch. } on diagonal
 { 6+15.5 " " E. " }

E. ch. 4.48 289.59

gutter pav. 5.12 288.95

1/4 " 5.09 288.92 sunk

1/4 " 5.12 288.95 sunk

1/4 " 4.90 289.17

G. " 5.07 289.00

" " + 4.4 = gutter 5.27 288.80 on ch. Return

" " + 4.4 = ch. ch. 4.67 289.40

6+00 Nat. Rt. 4s.

W. ch. line 5.3 288.8

1/4 " 5.4 288.7

1/4 " 5.5 288.6

1/4 " 5.6 288.5

G 6.2 288.9

E. ch. 5.23 289.84

5+90 P. C. Curb R. turn on W.

W. ch. 5.18 288.89

5+77.5

E. ch. sunk. Break 6.52 289.55

5+75

E. ch. 6.64 287.43

G 7.4 286.7

1/4 " 6.8 287.3

1/4 " 6.4 287.2

1/4 " 6.7 287.4

G 6.5 287.6

W. ch. 5.79 288.28

5+62 N.

1/4 Top M.H. 6.80 287.27

5+50 North

| | | |
|------|------|--------|
| W. d | 6.82 | 287.25 |
| G | 7.5 | 286.6 |
| 1/4 | 7.6 | 286.5 |
| ⊕ | 7.5 | 286.6 |
| 1/4 | 7.8 | 286.3 |
| G | 8.2 | 285.9 |
| E. d | 7.46 | 286.61 |

5+25 N

| | | |
|------|------|--------|
| E. d | 8.39 | 285.68 |
| G | 9.0 | 285.1 |
| 1/4 | 8.8 | 285.3 |
| ⊕ | 8.3 | 285.8 |
| 1/4 | 8.4 | 285.7 |
| G | 8.3 | 285.8 |
| W. d | 7.57 | 286.50 |

5+00 N

| | | |
|------|------|--------|
| W. d | 8.50 | 285.57 |
| G | 9.1 | 285.0 |
| 1/4 | 9.1 | 285.0 |
| ⊕ | 9.0 | 285.1 |
| 1/4 | 9.4 | 284.7 |
| G | 10.0 | 284.1 |
| E. d | 9.38 | 284.69 |

4+75 N.

| | | |
|------|-------|--------|
| E. d | 10.13 | 283.94 |
| G | 10.7 | 283.7 |
| 1/4 | 10.1 | 284.0 |
| ⊕ | 9.9 | 284.2 |
| 1/4 | 9.9 | 284.2 |
| G | 9.9 | 284.2 |
| W. d | 9.23 | 284.84 |

4+50 N

| | | |
|------|-------|--------|
| W. d | 9.71 | 284.36 |
| G | 10.6 | 283.5 |
| 1/4 | 10.3 | 283.8 |
| ⊕ | 10.5 | 283.6 |
| 1/4 | 10.9 | 283.2 |
| G | 11.3 | 282.8 |
| E. d | 10.92 | 283.25 |

4+25

| | | |
|------|-------|--------|
| E. d | 11.27 | 282.80 |
| G | 11.8 | 282.2 |
| 1/4 | 11.4 | 282.7 |
| ⊕ | 10.9 | 283.2 |
| 1/4 | 10.7 | 283.4 |
| G | 10.9 | 283.2 |
| W. d | 10.09 | 283.98 |

294.07
4+12 N. = N. End. 20' ch. inlets on E+W.

| | | |
|------------------|-------|--------|
| W. ch | 10.09 | 283.98 |
| G = F.L. opening | 11.12 | 282.95 |
| " | 10.8 | 283.3 |
| ♀ | 10.9 | 283.2 |
| " | 11.4 | 282.7 |
| G = F.L. opening | 12.30 | 281.77 |
| E. ch | 11.30 | 282.77 |

4+02 = ♀ inlets

| | | |
|----------------------------|-------|--------|
| E. ch | 11.31 | 282.76 |
| Gutter = ch. inlet grating | 12.29 | 281.78 |
| + 2.5 = " " " | 12.23 | 281.84 |
| " | 11.3 | 282.8 |
| ♀ | 10.7 | 283.4 |
| " | 10.7 | 283.4 |
| + 5.0 = ch. inlet grating | 11.11 | 282.96 |
| G = " " " | 11.13 | 282.94 |
| W. ch | 10.09 | 283.98 |

3+92 = S. End. ch. inlets

| | | |
|------------------|-------|--------|
| W. ch | 10.03 | 284.04 |
| G = F.L. opening | 11.00 | 283.02 |
| " | 10.6 | 283.5 |
| ♀ | 10.8 | 283.3 |
| " | 11.4 | 282.7 |
| G = F.L. opening | 12.31 | 281.76 |
| E. ch | 11.27 | 282.80 |

294.07 Boundary St 47

3+70 N

| | | |
|-------|-------|--------|
| E. ch | 10.85 | 283.22 |
| G. | 11.7 | 282.4 |
| " | 11.2 | 282.9 |
| ♀ | 10.7 | 283.4 |
| " | 10.5 | 283.6 |
| G. | 10.4 | 282.2 |
| W. ch | 9.89 | 284.25 |

3+69

| | | |
|----------------------------------|-------|--------|
| W. ch. dipped for drive = N. End | 10.38 | 283.69 |
|----------------------------------|-------|--------|

3+56

| | | |
|--------------------------------|-------|--------|
| W. ch. dipped for drive S. End | 10.30 | 283.27 |
|--------------------------------|-------|--------|

3+50

| | | |
|-------|-------|--------|
| W. ch | 9.50 | 284.57 |
| G | 10.2 | 283.9 |
| " | 10.3 | 283.8 |
| ♀ | 10.3 | 283.8 |
| " | 10.7 | 283.4 |
| G | 11.1 | 283.0 |
| E. ch | 10.59 | 283.48 |

3+00

| | | |
|-------|------|--------|
| E. ch | 9.67 | 284.4 |
| G | 10.2 | 283.9 |
| " | 9.8 | 284.3 |
| ♀ | 9.3 | 284.8 |
| " | 9.2 | 284.9 |
| G | 9.8 | 284.3 |
| W. ch | 8.60 | 285.47 |

294.07

2+98 N

W. d. dipped for drive N End 9.15 284.92

2+87 N

W. d. dipped for drive S. End 8.95 285.12

2+50 N

W. d. 7.66 286.41

G 8.7 285.4

1/4 8.4 285.7

1/4 8.6 285.5

1/4 9.0 285.1

G 9.3 284.5

E. d. 8.74 285.33

T.P. 10.53 295.88 8.72 285.35

2+20. Brk. E. d.

E. d. 10.01 285.87

2+10.3 Brk. E. d.

E. d. to N. 9.93 285.95

2+10.6 N Brk. E. d. sunk

E. d. to S. 9.97 285.91

2+00 N.

E. d. 9.88 286.00

G 10.2 285.7

1/4 9.9 286.0

1/4 9.4 286.5

1/4 9.4 286.5

295.88

Boundary St

48

G 9.6 286.3

W. d. 8.62 287.26

1+85. Brk. E. d. sunk

E. d. 9.66 286.22

1+50 N

W. d. 7.70 288.18

G 8.7 287.2

1/4 8.5 287.4

1/4 8.5 287.4

1/4 9.0 286.9

G 9.3 286.6

E. d. 8.77 287.11

1+00 N

E. d. 7.71 288.17

G 8.3 287.6

1/4 7.9 288.0

1/4 7.6 288.3

1/4 7.7 288.1

G 7.9 288.0

W. d. 6.76 289.12

0+50 N.

W. d. 5.82 290.06

G 6.7 289.2

1/4 6.7 289.2

1/4 6.7 289.2

1/4 7.1 288.8

295.88

0+50 N con

295.88

Boundary St

49

| | | | | | |
|---|------|--------|--------|-------|--------|
| G | 7.4 | 288.5 | ♀ | 5.7 | 290.2 |
| E. cl | 6.89 | 288.99 | 1/4 | 5.5 | 290.4 |
| 0+00 = N. line Redwood to E 60' wide 10' cl - 10' 1/2 | | | | | |
| E. cl | 6.11 | 289.22 | G | 5.4 | 290.5 |
| G | 6.8 | 289.1 | w. cl | 4.75 | 291.13 |
| 1/4 | 6.3 | 289.6 | ♀ | 5.05 | 290.83 |
| ♀ | 5.9 | 290.0 | w. cl | 5.05 | 290.83 |
| 1/4 | 5.8 | 290.1 | G | 5.05 | 290.83 |
| G | 5.9 | 290.0 | 1/4 | 5.3 | 290.6 |
| w. cl | 4.93 | 290.95 | ♀ | 5.6 | 290.3 |
| 10' S = N. cl | | | | | |
| w. cl | 4.84 | 291.04 | 1/4 | 6.0 | 289.9 |
| G | 5.6 | 290.3 | cl | 6.0 | 289.9 |
| 1/4 | 5.7 | 290.2 | E | 6.1 | 289.0 |
| ♀ | 5.8 | 290.1 | | | |
| 1/4 | 6.2 | 289.7 | | | |
| G ≈ E. cl line | 6.5 | 289.4 | | | |
| | | | | 5.1/4 | |
| +7 ground | 6.1 | 289.8 | E | 5.8 | 290.1 |
| +10 = E. line ground | 4.5 | 291.4 | cl | 6.0 | 289.9 |
| +10 = E. " cl. E. end ref. | 6.14 | 289.24 | 1/4 | 5.8 | 290.1 |
| | | | ♀ | 5.5 | 290.4 |
| | | | 1/4 | 5.3 | 290.6 |
| | | | G | 5.0 | 290.9 |
| | | | w. cl. | 4.60 | 291.26 |
| E | 5.1 | 290.8 | | | |
| +3 | 5.9 | 290.0 | | | |
| cl | 6.3 | 289.6 | | | |
| 1/4 | 6.0 | 289.9 | | | |

295.88

S. d. Lin-

295.88

1700 S.

| | | |
|-----------------------------|------|--------|
| W. d. | 4.79 | 291.39 |
| G | 5.2 | 290.7 |
| " | 5.3 | 290.6 |
| + | 5.4 | 290.5 |
| " | 5.7 | 290.2 |
| d | 5.8 | 290.1 |
| | 5.5 | |
| E | 5.5 | 290.4 |
| E. d. E End. Return | 5.56 | 290.32 |
| 0+00 = S. Line Redwood on E | | |
| E d | 5.37 | 290.51 |
| G | 5.8 | 290.1 |
| " | 5.6 | 290.3 |
| + | 5.3 | 290.6 |
| " | 5.3 | 290.6 |
| G | 5.1 | 290.8 |
| W. d. | 4.44 | 291.44 |
| 0+50 S. | | |
| W d | 4.12 | 291.76 |
| G | 4.8 | 291.1 |
| " | 4.9 | 291.0 |
| + | 4.9 | 291.0 |
| " | 5.3 | 290.6 |
| G | 5.5 | 290.4 |
| E d | 5.13 | 290.75 |

| | | |
|--|------|--------|
| E. d | 4.79 | 291.09 |
| G | 5.1 | 290.8 |
| " | 5.0 | 290.9 |
| + | 4.7 | 291.2 |
| " | 4.6 | 291.3 |
| G | 4.6 | 291.3 |
| W. d | 3.82 | 292.06 |
| 1450 S | | |
| W. d | 3.53 | 292.35 |
| G | 4.12 | 291.76 |
| " | 4.2 | 291.7 |
| + | 4.6 | 291.3 |
| " | 4.8 | 291.1 |
| G | 4.9 | 291.0 |
| E. d | 4.44 | 291.44 |
| 1460 S = N. End. Redwood W | | |
| E. d. | 4.42 | 291.46 |
| W. d. | 3.44 | 292.44 |
| (1+71.20 S. on E. d.) Nudge Part 1 + 632 S. " W. d. } on diagonal | | |
| E. d. | 4.59 | 291.29 |
| G. p. v. | 5.20 | 290.68 |
| " | 4.70 | 291.18 |
| + | 4.33 | 291.55 |
| " | 4.19 | 291.69 |
| G | 4.15 | 291.73 |
| W. d. | 3.44 | 292.44 |

295.88 indexed c.s.R.

Boundary St 51

T.P. 11.96 304.40 3.44 292.44

T.P. 10.70 315.06 0.04 304.36

B.M. B.P. 2.05 313.01 313.01 + Redwood

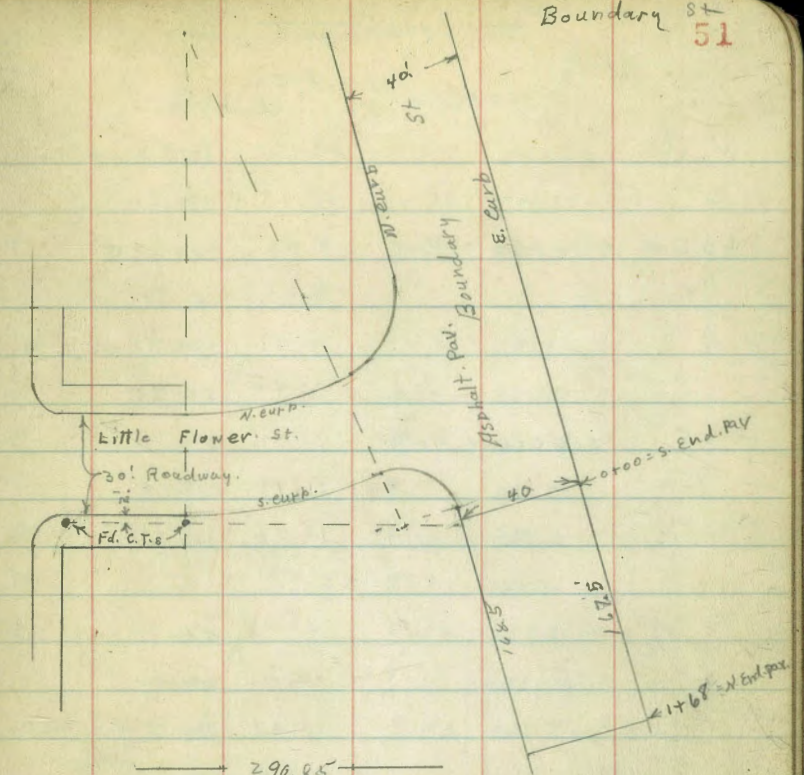
X See Boundary, S. of Little Flower St.

40' Roadway - 10' 1/4s.

T.P. 11.18 293.62 292.44 Top of Pav.

B.M. B.P. 0.07 293.55 + Redwood

T.P. 10.63 290.85 12.80 280.82



30' N. of 0+00

| | | |
|---|-------|--------|
| E.d | 9.97 | 280.88 |
| G Pav | 10.72 | 280.13 |
| 1/4 " | 9.99 | 280.86 |
| ϕ " | 9.56 | 281.29 |
| 1/4 " | 9.46 | 281.39 |
| w.d. line " | 9.54 | 281.29 |
| 15' N. of 0+00 = N. End. d. inlets on E&W | | |
| w.d. = F.L. opening | 8.83 | 282.02 |
| w.d. line pav. | 9.93 | 280.92 |
| G " | 9.93 | 280.92 |
| 1/4 " | 9.95 | 280.90 |
| ϕ " | 9.97 | 280.88 |

290.85

| | | |
|-----------------------------|-------|--------|
| 1/4 pav | 10.45 | 280.40 |
| G " | 11.17 | 299.68 |
| E.d | 10.01 | 280.84 |
| 8' N. of 0+00 = ϕ d. inlets | | |
| E.d | 10.01 | 280.84 |
| G. on grating | 11.17 | 299.68 |
| 1/4 | 10.59 | 280.26 |
| ϕ | 10.08 | 280.77 |
| 1/4 | 9.98 | 280.87 |
| w.d. line on grating | 10.25 | 280.60 |
| + 0.2. W. d. | 9.04 | 281.81 |

290.85

0+00 = { S. End Pav.
S. " ch. inlets.

| | | |
|-------------------------|---------|----------|
| W. ch | 7.12 | 281.73 |
| G | 10.25 | 280.60 |
| +3.5 = edge conc gutter | 9.84 | 280.97 ✓ |
| " | 9.91 | 280.94 |
| ⊕ | 10.07 | 280.78 ✓ |
| " | 10.49 | 280.35 |
| +6.5 = edge conc gutter | 10.94 | 279.91 ✓ |
| G | 11.17 | 279.68 |
| E. ch. | 10.03 | 280.82 |
| | 0+20 S. | |
| E. ch | 10.08 | 280.77 |
| G | 10.81 | 280.04 |
| +3.5 = WG | 10.67 | 280.18 ✓ |
| " | 10.2 | 280.7 |
| ⊕ | 10.1 | 280.8 |
| " | 9.4 | 281.1 |
| +6.5 = EG | 9.63 | 281.22 ✓ |
| G | 9.80 | 281.05 |
| W. ch | 9.06 | 281.29 |
| | 0+40 S. | |
| W. ch | 8.76 | 282.09 |
| G | 9.47 | 281.38 |
| +3.5 E.C | 9.31 | 281.54 ✓ |
| " | 9.2 | 281.7 |
| ⊕ | 9.2 | 281.7 |
| " | 9.7 | 281.2 |

290.85

Boundary St

52

| | | |
|-------------|---------|----------|
| +6.5 = WG | 10.25 | 280.60 ✓ |
| G | 10.34 | 280.51 |
| E ch | 9.67 | 281.18 |
| | 0+60 S. | |
| E. ch | 9.03 | 281.82 |
| G | 9.80 | 281.05 |
| +3.5 = W.G. | 9.59 | 281.26 ✓ |
| " | 9.1 | 281.85 |
| ⊕ | 8.6 | 282.3 |
| " | 8.3 | 282.6 |
| +6.5 = E.C | 8.54 | 282.31 ✓ |
| G | 8.73 | 282.12 |
| W. ch | 8.03 | 282.82 |
| | 0+80 S. | |
| W. ch | 7.12 | 283.73 |
| G | 7.85 | 283.00 |
| +3.5 = E.C | 7.67 | 283.18 ✓ |
| " | 7.4 | 283.5 |
| ⊕ | 7.7 | 283.2 |
| " | 8.2 | 282.7 |
| +6.5 = WG | 8.65 | 282.20 ✓ |
| G | 8.84 | 282.04 |
| E. ch. | 8.14 | 282.71 |

290.85

1+00 S.

| | | |
|-------------|------|----------|
| E. cl | 6.87 | 283.98 |
| G | 7.62 | 283.23 |
| +3.5 = W.G. | 7.43 | 283.42 ✓ |
| 1/4 | 7.1 | 283.8 |
| 1/2 | 6.6 | 284.3 |
| 1/4 | 6.4 | 284.5 |
| +6.5 = W.G. | 6.64 | 284.21 ✓ |
| G | 6.82 | 284.03 |
| W. cl. | 6.08 | 284.79 |

1+40 S.

| | | |
|-------------|------|----------|
| W. cl | 3.43 | 282.42 |
| G | 4.18 | 286.67 |
| +3.5 = E.G. | 4.03 | 286.72 ✓ |
| 1/4 | 4.0 | 286.9 |
| 1/2 | 4.1 | 286.8 |
| 1/4 | 4.3 | 286.6 |
| +6.5 = W.G. | 4.77 | 286.08 ✓ |
| G | 4.93 | 285.92 |
| E. cl | 4.21 | 286.74 |

1+68 South.

| | | |
|-------------|------|----------|
| E. cl | 2.35 | 288.50 |
| G | 3.07 | 287.78 |
| +3.5 = W.G. | 2.87 | 287.98 ✓ |
| 1/4 | 2.50 | 288.35 |
| 1/2 | 2.11 | 288.74 ✓ |
| 1/4 | 2.07 | 288.78 |

290.95

Boundary St.

53

| | | | |
|-------------|------|------|----------|
| +6.5 = E.C. | Pay. | 2.01 | 288.84 ✓ |
| G | " | 2.17 | 288.68 |
| W. cl. | | 1.35 | 289.50 |
| 1+78 S. | | | |
| W. cl. Line | pay | 1.52 | 289.33 |
| 1/4 | " | 1.52 | 289.33 |
| 1/2 | " | 1.55 | 289.30 |
| 1/4 | " | 1.94 | 288.91 |
| G | " | 2.44 | 288.41 |
| E. cl. | " | 1.77 | 289.08 |

1+88 S.

| | | | |
|-------------|-----|------|--------|
| E. cl. Line | pay | 2.01 | 288.84 |
| 1/4 | " | 1.43 | 289.42 |
| 1/2 | " | 1.15 | 289.70 |
| 1/4 | " | 1.09 | 289.76 |
| W. cl. Line | " | 1.05 | 289.50 |

chk. E.G. pay. 1+71²⁰ Page 50 0.17 290.64 ✓

N. End. Pay B.C. Curve W. cl.

7-22-37

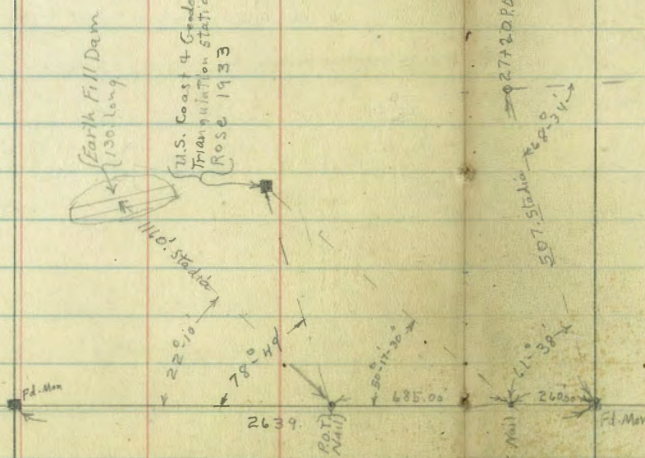
Survey P.L.s 1276-1277

Indexed
C.S.K.

Miller
Walker
Bliss

P.L. 1278

Earth Fill Dam
(150' long)
U.S. Coast & Geodetic
Triangulation Station Mon.
Rose 1933
P.L. 1277



P.L. 1272

P.L. 1273

027+20 RAT Nail
507.52
24.34

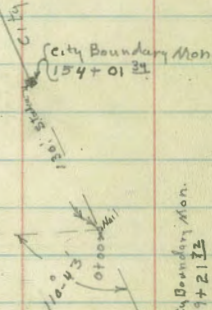
030+46 POT Nail

Random Like to locate
S.E. + S.W. cor. of
P.L. 1277
Stadia measurements

P.L. 1276

104659 POT Nail

91100 POT Nail



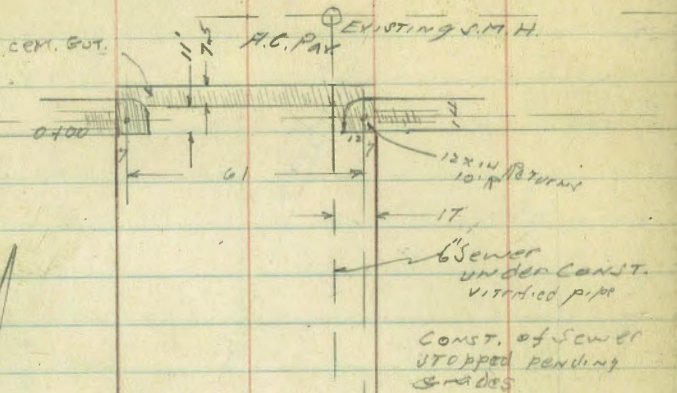
P.L. 1274

P.L. 1275

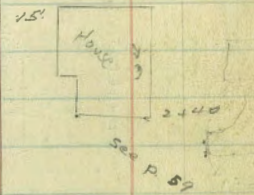
104706.80 Int City Boundary
(4N) Line P.L. 1274 Produced

Swamp

Xsec of State & Columbia
 Chalmers to Walnut.
 Walnut, State to 100' SWly of Columbia

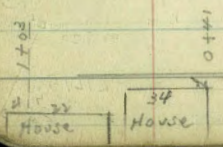


Columbia



Walnut

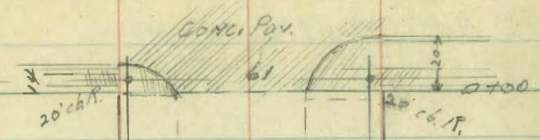
Walnut State St



Indexed
 C.S.K.

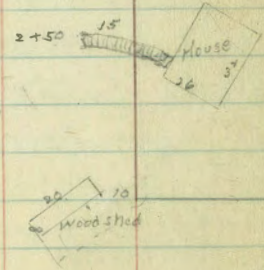
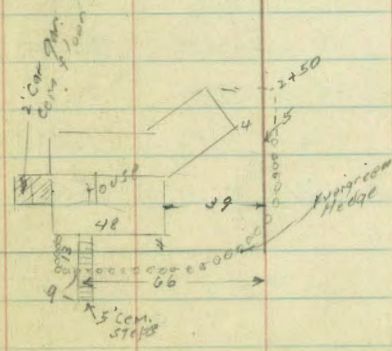
Chalmers St

274.40

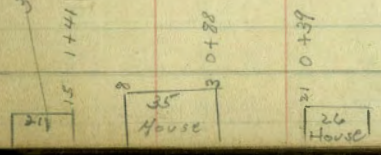


20 30 25

STATE



Scange



Mon.

07 07

75' wide
W cb = 20'
E cb = 25'
80' wide
14' cbs

X sec of
STATE + Columbia, Chalmers to Walnut
→ WALNUT, STATE to 12' W of Columbia

Moore
85-27
106.46

| | | | | | | | |
|----------|---|--------|-------|----------------------|-------------|--------------|--------------|
| | | | | Chalmers Columbia | cb + 5 W | 11.4 12.1 | 95.1 94.4 |
| S.E.B.P. | 9.35 | 106.46 | 97.11 | | +10 | 12.8 | 93.7 |
| | COLUMBIA ST. Cent. 00-11 = Sly edge gut | | | | | 0 + 5.3 | |
| E | cont. | 9.4 | 97.1 | | -10 | 13.1 | 93.4 |
| + 9 | Top cb | 9.55 | 96.91 | | W | 11.5 | 95.0 |
| + 9.1 | gut | 10.08 | 96.38 | | + 8 | 8.3 | 98.2 |
| C | | 11.61 | 94.85 | | cb | 8.0 | 98.5 |
| cb + 3 | gut | 13.20 | 93.26 | | 1/2 | 7.0 | 99.5 |
| " + 3.1 | Top cb | 12.67 | 93.79 | | C | 6.8 | 99.7 |
| W | | 12.7 | 93.8 | | 1/2 | 5.9 | 100.6 |
| | 0 + 00 = Sly Chalmers | | | | cb | 4.8 | 101.7 |
| W | Cent = WL Columbia | 12.14 | 93.9 | | + 7 | 1.3 | 105.2 |
| cb | Top cb | 12.68 | 93.78 | | E | Top bank | + 3.3 |
| 1/2 | | 11.7 | 94.8 | | | 0 + 7.3 | 109.8 |
| C | | 10.5 | 96.0 | | E | Top bank. | + 6.9 |
| 1/2 | | 9.8 | 96.7 | | + 2 | + 6.9 | 113.4 |
| cb | " " | 9.53 | 96.93 | | cb | 1.8 | 104.7 |
| E | Cent = E.L. Columbia | 9.21 | 97.25 | | 1/2 | 2.7 | 103.8 |
| | 0 + 37 | | | | C | 4.0 | 102.5 |
| E | | 5.2 | 101.3 | | 1/2 | 4.6 | 101.9 |
| cb | | 5.8 | 100.7 | | cb | 5.3 | 101.2 |
| 1/2 | | 7.4 | 99.1 | | W | 3.1 | 103.4 |
| C | | 8.7 | 97.8 | | + 3 | 11.2 | 95.3 |
| 1/2 | | 9.0 | 97.5 | | + 10 | 11.6 | 94.9 |
| cb | | 9.1 | 97.4 | T.P. | 12.94 | 118.91 | 0.49 |
| | | | | | | | 105.97 |

118.91

1+00

| | | |
|-----------------------|------|-------|
| - 15 | 24.6 | 94.3 |
| - 4 | 23.6 | 95.3 |
| - 2 | 12.2 | 106.7 |
| W | 12.1 | 106.8 |
| cb | 13.5 | 105.4 |
| 1/4 | 13.5 | 105.4 |
| C | 12.1 | 106.8 |
| 1/4 | 11.4 | 107.5 |
| +7.7 Bot. sewer ditch | 15.0 | 103.9 |
| cb | 8.4 | 110.3 |
| +10 | +1.5 | 120.4 |
| E top bank | +1.5 | 120.4 |
| 1+35 | | |
| E top bank | +7.0 | 125.9 |
| cb | 1.7 | 117.2 |
| 1/4 | 5.4 | 113.5 |
| C | 6.7 | 112.2 |
| 1/4 | 8.0 | 110.9 |
| cb | 3.7 | 111.2 |
| W | 6.6 | 112.3 |
| +2 | 18.7 | 100.2 |
| +10 | 23.7 | 95.2 |
| +25 | 25.1 | 93.8 |
| 1+45 | | |
| W - 25 | 22.4 | 96.5 |
| - 8 | 19.6 | 99.3 |

118.91

Columbia

57

| | | |
|--------------|-------|--------|
| W - 6 | 2.5 | 116.4 |
| W | 4.5 | 114.4 |
| +5 | 5.8 | 113.1 |
| cb | 5.8 | 113.1 |
| 1+47 | | |
| W - 25 | 5.3 | 113.6 |
| - 4 | 2.2 | 116.7 |
| W | 3.7 | 115.2 |
| +5 | 5.5 | 113.4 |
| cb | 5.5 | 113.4 |
| 1/4 | 5.2 | 113.7 |
| C | 5.0 | 113.9 |
| 1/4 | 2.5 | 116.4 |
| cb | 0.4 | 118.5 |
| E top bank | +8.8 | 127.7 |
| T.P. | 12.68 | 131.09 |
| 0.50 | | 118.41 |
| - 5 top bank | 0.0 | 131.1 |
| E | 1.3 | 129.8 |
| cb | 8.1 | 123.0 |
| 1/4 | 10.6 | 120.5 |
| C | 12.8 | 118.3 |
| +5 | 13.4 | 117.7 |
| +7 | 15.0 | 116.1 |
| 1/4 | 15.0 | 116.1 |

131.09

| | | | |
|-------|-------------------------------|------|-------|
| cb | | 14.9 | 116.2 |
| +0 | | 13.5 | 117.6 |
| W | | 12.9 | 118.2 |
| +10 | | 13.3 | 117.8 |
| | 2+00 | | |
| -10 | | 9.5 | 121.6 |
| W | | 8.3 | 122.8 |
| +2 | | 9.5 | 121.6 |
| cb | | 9.7 | 121.4 |
| 1/4 | | 9.6 | 121.5 |
| +5 | | 9.7 | 121.4 |
| +7 | | 8.4 | 122.5 |
| 0 | | 8.6 | 122.5 |
| 1/4 | | 6.2 | 124.9 |
| +7.7 | bot. sewer ditch | 10.2 | 120.9 |
| cb | | 3.5 | 127.6 |
| +10 | | +1.6 | 132.7 |
| E | | +3.6 | 134.7 |
| +1 | TOP BANK | +4.5 | 135.6 |
| | 2+25 | | |
| E -15 | House CONST. ^{under} | | |
| E | | +7.0 | 138.1 |
| +1 | | +5.7 | 136.8 |
| cb | | +1.5 | 132.6 |
| 1/4 | | 1.8 | 129.3 |
| c | | 2.0 | 127.1 |

131.09

Columbia

58

| | | | |
|------|--------------|------|--------|
| C +0 | | 4.3 | 126.8 |
| +8 | | 6.3 | 124.8 |
| 1/4 | | 6.3 | 124.8 |
| cb | | 6.4 | 124.7 |
| W | | 5.9 | 125.2 |
| +10 | | 7.3 | 123.8 |
| | 2+50 | | |
| -10 | | 5.5 | 125.6 |
| W | | 3.5 | 127.6 |
| cb | | 3.3 | 127.8 |
| 1/4 | | 3.4 | 127.7 |
| +5 | | 3.6 | 127.5 |
| +7 | | 1.5 | 129.6 |
| T.P. | 12.74 142.29 | 1.54 | 129.55 |
| c | | 11.7 | 130.6 |
| 1/4 | | 9.0 | 133.3 |
| cb | | 5.9 | 136.4 |
| E | on iron pin | 2.3 | 140.0 |
| +1 | TOP BANK | 1.4 | 140.9 |
| | 2+75 | | |
| -1 | TOP BANK | +0.5 | 142.8 |
| E | | 0.9 | 141.4 |
| cb | | 3.3 | 139.0 |
| 1/4 | | 6.7 | 135.6 |
| C | | 8.4 | 133.9 |
| +7 | | 9.5 | 132.8 |

S. edge prop.
= auto Dr.
Told owner to
delay pouring
concr. pending
grade

| | | |
|------------|------|-------|
| +9 | 11.9 | 130.4 |
| 1/4 | 12.1 | 130.2 |
| cb | 11.9 | 130.4 |
| +5 | 11.5 | 130.8 |
| W | 12.8 | 129.5 |
| +10 | 15.2 | 127.1 |
| 3700 = Nly | | |
| -10 | 14.3 | 128.0 |
| W | 12.4 | 129.9 |
| +8 | 9.8 | 132.5 |
| cb | 10.0 | 132.3 |
| 1/4 | 10.1 | 132.2 |
| +3 | 10.2 | 132.1 |
| +6 | 7.5 | 134.8 |
| C | 6.2 | 136.1 |
| 1/4 | 4.2 | 138.1 |
| cb | 1.9 | 140.4 |
| E | 0.0 | 142.3 |
| +2 | +1.3 | 143.6 |

T.P. Φ hub Columbia
Walnut 7.68 134.61

Garage levels
E side Columbia St
bet Walnut &
Chalmers

Sly Chalmers = 0400

S.F.P. 13.20 110

T.P. 13.21 120

1406 5' E of E.L. 110

" 8" " 90

1421 " S edge 120

T.P. 11.85 130

T.P. 8.37 140

1495 E.L. E' dms 110

" " # 34 " 100

" " " Top 100

" 55.5 E dms 100

" " Top Cen 100

" 80' dble gar 100

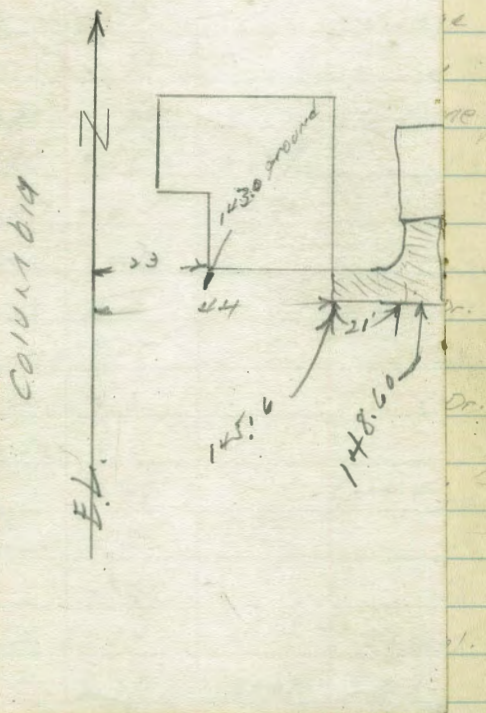
+44 E.L. N edge 100

" " 10' E of E.L. 100

+48.7 N edge S ribb 100

134.61 = Φ Hub
12.75
147.36
2.30
145.16
7.84
153.00

44 220
145.16



Cor.
Walnut

| | | |
|-------------------------------|------|--------|
| 29 | 11.9 | 130.4 |
| 1/4 | 12.1 | 130.2 |
| 26 | 11.9 | 130.4 |
| +5 | 11.5 | 130.8 |
| W | 12.8 | 129.5 |
| +10 | 15.2 | 127.1 |
| 3700 = N/4 | | |
| -10 | 14.3 | 128.0 |
| W | 12.4 | 129.9 |
| +8 | 9.8 | 132.5 |
| 26 | 10.0 | 132.3 |
| 1/4 | 10.1 | 132.2 |
| +9 | 10.2 | 132.1 |
| +6 | 7.5 | 134.8 |
| C | 6.2 | 136.1 |
| 1/4 | 4.2 | 138.1 |
| 26 | 1.9 | 140.4 |
| E | 0.0 | 142.3 |
| +2 | +1.3 | 143.6 |
| T.P. E hub Columbia Walnut | 7.68 | 134.61 |

Garage Levels
E side Columbia St
bet Walnut &
Chalmers

Sly Chalmers = 0400

| | | | | | |
|--------|-----------------|-----------------|------|--------|---------------------------|
| SEBP | 13.20 | 110.31 | | 97.11 | Col. Chalmers |
| T.P. | 13.21 | 123.44 | 0.08 | 110.23 | |
| 1406 | 5' E of EL | Apron | 2.54 | | N edge |
| " | 8 " | " gar. | 3.98 | | " " |
| 1421 | S edge apron | gar. | | | EL SAME |
| T.P. | 11.85 | 134.94 | 0.35 | 123.09 | |
| T.P. | 8.37 | 143.27 | 0.04 | 134.90 | |
| 1495 | EL | E dirt Dr. | 10.0 | | |
| " | " | #34 " | 5.8 | | E dirt Dr. |
| " | " | " Top step | 5.25 | | |
| " | 55.5 | E dirt Dr. | 2.8 | | E dirt Dr. |
| " | " | " Top Cent step | 2.0 | | |
| " | 80 | double gar. | 0.28 | | Cent Fl. |
| 2+44 | EL | N edge ribbon | 4.34 | | |
| " | " | 10' E of EL | 2.90 | | |
| 2+48.7 | N edge S ribbon | | 4.34 | | EL. Col. |
| | | | 8.66 | 134.61 | E Hub Col. + Walnut |

Note!
 £ of improvement
 is not £ on STATE ST.

120.94

60

| State St. Xsec | | 75' wide | | | | | |
|-------------------------|---------------------|----------|--------|----------------------|--------|--------|--------|
| Chalmers to Walnut | | | | | C + 5 | + 0.6 | 121.5 |
| | | | | | cb | + 2.5 | 123.4 |
| | | | | | E | + 9.1 | 130.0 |
| S.E.B.P. | 12.14 | 109.25 | 97.11 | Columbia Chalmers | 0 + 20 | | |
| T.P. | 12.45 | 120.94 | 076 | | E | + 13.0 | 133.9 |
| | 00 - 14 = | | | | cb | + 7.5 | 128.4 |
| W Top cb | | 11.95 | 108.99 | | C | + 3.8 | 124.7 |
| W gut | | 12.45 | 108.49 | | + 11 | + 1.0 | 121.9 |
| cb on pav | | 10.60 | 110.28 | | + 13 | 5.8 | 115.1 |
| C " " | | 9.43 | 111.51 | | cb | 6.1 | 114.8 |
| cb " " | | 7.21 | 113.13 | | + 8 | 5.7 | 115.2 |
| + 6 gut | | 6.86 | 114.08 | | W | 4.3 | 116.6 |
| + 6 Top curb | | 6.35 | 114.59 | | + 5 | 5.0 | 115.9 |
| | 0 + 00 Sly Chalmers | | | | 0 + 40 | | |
| E | | 1.8 | 119.1 | | - 10 | 4.0 | 116.9 |
| cb Top cb | | 7.70 | 113.24 | | W | 0.9 | 120.0 |
| gut pav | | 8.16 | 112.78 | | + 17 | 1.7 | 119.2 |
| C = + 15 " £ of roadway | | 8.55 | 112.39 | | | | |
| cb of STATE on pav | | 8.93 | 112.01 | | T.P. | 12.49 | 132.95 |
| + 0.8 gut | | 8.94 | 112.00 | | + 18 | 9.8 | 123.1 |
| + 0.98 Top cb | | 8.42 | 112.52 | | cb | 9.1 | 123.8 |
| W | | 8.3 | 112.6 | | C | 5.2 | 127.7 |
| | 0 + 02 | | | | cb | 1.3 | 131.6 |
| W cb + 11 | | 8.0 | 112.9 | | E | + 5.2 | 138.1 |
| + 13 | | 3.5 | 117.4 | | 0 + 60 | | |
| C | | 2.0 | 118.9 | | E | + 7.2 | 140.1 |

1981
11.8.7
C

11.8.25
11.3.25
11.3.24
11.3.23
11.3.22
11.3.21
11.3.20
11.3.19
11.3.18
11.3.17
11.3.16
11.3.15
11.3.14
11.3.13
11.3.12
11.3.11
11.3.10
11.3.9
11.3.8
11.3.7
11.3.6
11.3.5
11.3.4
11.3.3
11.3.2
11.3.1

| | | |
|-------|-------|-------|
| E +20 | +3.8 | 136.7 |
| cb | +1.8 | 134.7 |
| c | 3.5 | 129.4 |
| cb | 7.5 | 125.4 |
| +1 | 9.8 | 123.1 |
| W | 10.5 | 122.4 |
| +3 | 12.3 | 120.6 |
| +15 | 14.4 | 118.5 |
| | 0+80 | |
| -10 | 10.3 | 122.6 |
| W | 8.1 | 124.8 |
| +5 | 6.7 | 126.2 |
| cb | 5.9 | 127.0 |
| +8 | 5.4 | 127.5 |
| +9 | 2.8 | 130.1 |
| C | 1.0 | 131.9 |
| cb | +4.2 | 137.1 |
| +7 | +6.0 | 138.9 |
| E | +8.8 | 141.7 |
| | 1+00 | |
| E | +10.5 | 143.4 |
| +17 | +6.6 | 139.5 |
| cb | +4.8 | 137.7 |
| +5 | +3.6 | 136.5 |
| +8 | +0.5 | 133.4 |
| C | 0.0 | 132.9 |

132.95

STATE 61

| | | |
|------|------|--------|
| cb | 2.5 | 130.4 |
| +4 | 3.3 | 129.6 |
| +6 | 2.1 | 130.8 |
| W | 4.1 | 129.8 |
| +10 | 3.4 | 129.5 |
| TP | 1242 | 145.03 |
| | 1+18 | 0.34 |
| | | 132.61 |
| | | |
| E cb | 6.0 | 139.0 |
| +15 | 4.1 | 140.9 |
| +20 | 1.0 | 144.0 |
| E | 0.0 | 145.0 |
| | 1+20 | |
| -10 | 8.1 | 136.7 |
| W | 8.4 | 136.6 |
| cb | 8.5 | 136.5 |
| +5 | 7.8 | 137.2 |
| +6 | 9.7 | 135.3 |
| C | 8.2 | 136.8 |
| cb | 5.5 | 139.5 |
| E | 1.6 | 143.4 |
| | 1+40 | |
| E | +1.7 | 146.7 |
| +10 | 0.0 | 145.0 |
| cb | 1.9 | 143.1 |
| C | 3.7 | 141.3 |

| | | | | | | |
|--------|---------|------|------|-------|------|------|
| 139.0 | 6.0 | 1+18 | | 18.5 | 1.4 | 15 |
| 132.61 | 1.45.03 | 12.4 | T.P. | 120.6 | 12.3 | +3 |
| | | | | 12.4 | 10.5 | M |
| 129.5 | 3.4 | +10 | | 123.1 | 9.8 | +1 |
| 129.8 | 0.1 | M | | 125.4 | 7.5 | c6 |
| 130.8 | 2.1 | +6 | | 129.4 | 3.5 | c |
| 129.6 | 5.3 | +4 | | 134.7 | +4.8 | c6 |
| 130.4 | 2.5 | c6 | | 136.7 | +3.8 | E+20 |

504.70
 Easton -233
 112.50
 -6 -33
 111.5
 -11 -42
 110.6
 -16 -49.5
 109.83
 -21 -5.55
 109.25
 -26 -5.90
 108.80
 56.25
 113.25
 113.25
 113.80
 114.25
 115.85
 116.90
 118.11
 56.811
 5 ENQ -66
 99-66
 8-66-6.6
 -116-6.05
 -166-5.1
 -216-4.0
 -266-2.95
 31.6-1.8
 326-0.9
 119.84
 112.57
 23
 114.8
 Returns State &
 Chalmers

145.03

| | | | | |
|-----------------|--------|--------|-------|--------|
| C + 1 | | 1.9 | 143.1 | |
| cb | | 1.7 | 143.3 | |
| W | | 2.6 | 142.4 | |
| + 10 | | 2.7 | 142.3 | |
| T.P. | 12.27 | 156.90 | 0.40 | 144.63 |
| | 1 + 54 | | | |
| - 10 | | 11.5 | 145.4 | |
| W. | | 11.4 | 145.5 | |
| cb | | 11.2 | 145.7 | |
| + 2 | | 11.0 | 145.9 | |
| + 4 | | 12.0 | 144.6 | |
| C | | 11.4 | 145.5 | |
| + 8 | | 10.6 | 146.3 | |
| + 15 | | 8.6 | 148.3 | |
| E | | 8.0 | 148.9 | |
| floor el. House | 1 + 80 | 2.6 | 154.3 | |
| E | | 5.0 | 151.9 | |
| cb | | 6.1 | 150.8 | |
| C | | 6.5 | 150.4 | |
| cb | | 6.4 | 150.5 | |
| W | | 5.8 | 151.1 | |
| | 2 + 15 | | | |
| W | | 1.0 | 155.9 | |
| cb | | 1.7 | 155.2 | |
| C | | 2.4 | 154.5 | |

156.90

State 62

| | | | | |
|--------|---------------|--------|-------|-----------|
| C + 12 | | 1.4 | 155.5 | |
| cb | | 0.5 | 156.4 | |
| + 3 | | 1.1 | 155.8 | |
| E | | 1.3 | 155.6 | |
| T.P. | 560 | 162.12 | 0.38 | 156.52 |
| | 2 + 50 | | | |
| E | | 5.5 | 156.6 | |
| cb | | 4.6 | 157.5 | |
| C | | 3.7 | 158.4 | |
| cb | | 3.3 | 158.8 | |
| W | | 2.4 | 159.7 | |
| | 2 + 75 | | | |
| W | | 1.5 | 160.6 | |
| + 7 | | 1.9 | 160.2 | |
| + 9 | | 2.6 | 159.5 | |
| cb | | 2.5 | 159.6 | |
| C | | 3.5 | 158.6 | |
| cb | | 5.6 | 156.5 | |
| E | | 7.9 | 154.2 | |
| + 7 | SW. Cor House | 7.0 | 155.1 | floor el. |
| | 2 + 90 | | | |
| E | | 10.9 | 151.2 | |
| + 15 | | 7.7 | 154.4 | |
| cb | | 7.1 | 155.0 | |
| C | | 5.3 | 156.8 | |
| cb | | 3.6 | 158.5 | |

162.12

+13 3.5 158.6
 +15 2.3 159.8
 W 1.9 160.2

3400 N 1/2 Walnut

W 2.2 159.9
 +5 2.4 159.7
 +4 4.4 157.7
 cb 4.8 157.3
 C 6.9 155.2
 +12 8.0 154.1
 cb 13.0 149.1
 E 12.4 149.7
 +10 13.0 149.1

N cb

-10 16.9 145.2
 E 13.8 148.3
 cb 12.8 149.3
 C 9.5 152.6
 +7 7.8 154.3
 cb 7.8 154.3
 +8 7.5 154.6
 +13 6.5 155.6
 W 6.0 156.1

N 1/2

W 8.0 154.1
 cb 10.0 152.1

162.12

STATE

63

C 11.5 150.6
 cb 12.7 149.4
 +18 19.7 142.4
 E 18.2 143.9

+10 25.5 136.6
 +20 27.8 134.3

80' wide \$ WALNUT
 E+20 TOP CUT 19.8 142.3

cb 18.8 143.3

C 16.3 145.8

cb 12.7 149.4

W ON 2 x 2 Hub 10.91 151.21 B.M.

T.P. 0.86 152.07 10.91 151.21

S 1/4

W 5.4 146.7

cb 8.2 143.9

C 10.0 142.1

+9 TOP CUT 12.4 139.5

S cb

W 6.8 145.3

+4 8.9 143.2

cb 12.1 140.0

+11 TOP CUT 13.8 138.3

T.P. 1.61 141.18 12.50 139.57

141.18

SL WALNUT

| | | | |
|------|---------|------|-------|
| W | | 3.8 | 137.4 |
| +18 | TOP CUT | 4.9 | 136.3 |
| W CB | | 16.9 | 124.3 |
| | +15 | | |
| W | | 10.4 | 130.8 |
| +9 | | 10.0 | 131.2 |
| CB | | 20.1 | 121.1 |

T.P. 0.05 128.61 12.42 128.56

E WALNUT

| | | | |
|----------|------------------------------|-------|--------|
| E CB +18 | bot. cut | 7.4 | 121.0 |
| E | TOP CB N side Glenwood Pa | 8.07 | 120.54 |
| | S 1/4 | | |
| E CB | bot. cut | 7.6 | 121.0 |
| +10 | TOP CB | 9.21 | 119.40 |
| +10 | gut | 10.07 | 118.54 |
| E | par. | 9.75 | 118.86 |
| | S CB | | |
| E +5 | | 10.2 | 118.4 |
| +11 | TOP CB | 10.45 | 118.16 |
| +11 | | 11.30 | 117.31 |
| E CB | | 11.27 | 117.34 |

128.61

STATE

64

SL WALNUT

| | | | |
|----------|-----------|-------|--------|
| W CB +11 | bot. bank | 11.7 | 116.9 |
| C | TOP CB | 11.45 | 117.16 |
| | +15 | | |
| W CB +10 | TOP CB | 12.45 | 116.16 |
| +10 | gut | 13.3 | 115.3 |
| C | par | 13.2 | 115.2 |

X sec of Walnut

80' wide
14' cb
12' 1/2

164.20

65

| | | | | |
|-------------------------|-------|--------|--------|--|
| B.M. 200 | 12.99 | 164.20 | 151.21 | |
| 00 = W.L. STATE | | | | |
| 39' W of STATE | | | | |
| - 21 N edge House track | 33.1 | 131.1 | | |
| S | 24.0 | 140.2 | | |
| cb | 18.0 | 145.6 | | |
| 1/4 | 14.1 | 150.1 | | |
| C | 10.0 | 154.2 | | |
| 1/2 | 9.1 | 155.1 | | |
| +11 | 7.7 | 156.5 | | |
| cb | 6.4 | 157.8 | | |
| +4 | 4.9 | 159.3 | | |
| N Lamin | 4.2 | 160.0 | | |
| 0+66 | | | | |
| N-4 floor el. House | 1.02 | 163.18 | | |
| N | 3.9 | 160.3 | | |
| +9 Top of Steps | 4.0 | 160.2 | | |
| cb | 6.0 | 158.2 | | |
| +3 bot " | 7.0 | 157.2 | | |
| 1/2 | 9.1 | 155.1 | | |
| C | 11.0 | 153.2 | | |
| 0+88 | | | | |
| N | 8.8 | 155.4 | | |
| cb | 8.9 | 155.3 | | |
| 1/2 | 10.0 | 153.8 | | |

W.L. STATE
E Walnut

| | | | | |
|---|------|--------|------|-----------------|
| 0 | 11.8 | 152.4 | | |
| 1/4 | 12.6 | 151.6 | | |
| cb | 15.6 | 148.6 | | |
| +10 | 18.4 | 145.8 | | |
| S N edge walk | 21.4 | 142.8 | | |
| +3 N.E. ^{cor} edge house | 20.5 | 143.7 | | floor el. |
| T.P. | 0.26 | 158.32 | 6.74 | 157.46 |
| 0+94 | | | | |
| N-31 E double gar. ^{corr.} floor | 3.30 | 155.02 | | |
| N | 3.3 | 155.0 | | |
| cb | 3.4 | 154.9 | | |
| 1+23 | | | | |
| S-8 NW cor house | 14.8 | 143.5 | | corr. on street |
| S | 13.4 | 144.9 | | |
| cb | 10.7 | 147.6 | | |
| 1/2 | 9.3 | 149.0 | | |
| 0 | 8.2 | 150.1 | | |
| 1/4 | 7.0 | 151.3 | | |
| cb | 6.2 | 152.1 | | |
| N | 5.3 | 153.0 | | |
| 1+41 | | | | |
| S | 14.9 | 143.4 | | |
| 15' Bot Edge plan gar. | 16.8 | 141.5 | | floor el. |

158.32

| | | | | |
|------|---------------------|--------|--------------------|--------|
| | 1765 | | | |
| n' | | 10.5 | 147.8 | |
| cb | | 10.6 | 147.7 | |
| 1/4 | | 11.5 | 146.8 | |
| c | | 12.3 | 146.0 | |
| 1/4 | | 13.5 | 144.8 | |
| cb | | 15.0 | 143.3 ^a | |
| 5 | | 16.3 | 142.0 | |
| +15 | wedge 3 car gar. | 16.8 | 141.5 | |
| T.P. | 0.70 | 146.22 | 12.80 | 145.52 |
| | 179 ^v | | | |
| -15 | | 9.4 | 136.8 | |
| 5 | | 6.5 | 139.7 | |
| cb | | 6.2 | 140.0 | |
| +8 | | 5.7 | 140.5 | |
| 1/4 | | 3.9 | 142.3 | |
| c | | 2.9 | 143.3 | |
| 1/4 | | 2.5 | 143.7 | |
| cb | | 1.8 | 144.4 | |
| n' | | 1.7 | 144.5 | |
| | 2+00 = Ely Columbia | | | |
| n' | on iron pin | 3.94 | 142.28 | |
| cb | | 4.0 | 142.2 | |
| 1/4 | | 4.4 | 141.8 | |
| c | | 5.0 | 141.2 | |

146.22

Walnut

66

| | | | |
|-----|-------|------|-------|
| 1/4 | | 6.7 | 139.5 |
| cb | | 7.1 | 139.1 |
| 5 | | 8.0 | 138.2 |
| +15 | | 10.5 | 135.7 |
| | E cb | | |
| -15 | | 11.7 | 134.5 |
| 5 | | 9.5 | 136.7 |
| cb | | 8.5 | 137.7 |
| 1/4 | | 8.3 | 137.9 |
| c | | 7.5 | 138.7 |
| 1/4 | | 6.5 | 139.7 |
| cb | | 6.0 | 140.2 |
| n' | | 5.8 | 140.4 |
| | E 1/4 | | |
| n' | | 8.1 | 138.1 |
| cb | | 7.4 | 138.6 |
| 1/4 | | 8.2 | 138.0 |
| c | | 9.8 | 136.4 |
| 1/4 | | 9.9 | 136.3 |
| cb | | 10.1 | 136.1 |
| 5 | | 11.4 | 134.8 |
| +15 | | 13.8 | 132.4 |
| | ⊕ | | |
| -15 | | 75.2 | 131.0 |
| 5 | | 12.8 | 133.4 |
| cb | | 11.4 | 134.8 |

146.22

| | | | | |
|-----|--------------|-------|--------|--------|
| 1/2 | | 11.3 | 134.9 | |
| c | ON E VxV HUB | 11.59 | 134.63 | 134.61 |
| 1/4 | | 11.4 | 134.6 | |
| +6 | | 12.0 | 134.2 | |
| cb | | 9.9 | 136.3 | |
| N | | 10.3 | 135.9 | |

Wt

| | | | | |
|-----|--|------|-------|--|
| N | | 14.4 | 131.8 | |
| cb | | 13.3 | 132.9 | |
| 1/4 | | 12.5 | 133.7 | |
| c | | 12.5 | 133.7 | |
| 1/2 | | 12.6 | 133.6 | |
| cb | | 12.9 | 133.3 | |
| S | | 15.0 | 131.2 | |
| +15 | | 16.8 | 129.4 | |

Wt cb

| | | | | |
|-----|--|------|-------|--|
| -15 | | 18.3 | 127.9 | |
| S | | 17.0 | 129.2 | |
| cb | | 15.4 | 130.8 | |
| 1/4 | | 14.5 | 131.7 | |
| c | | 14.1 | 132.1 | |
| 1/2 | | 14.0 | 132.2 | |
| cb | | 13.4 | 132.8 | |
| N | | 13.9 | 132.3 | |

| | | | | | |
|------|------|--------|-------|--------|-----------|
| T.P. | 1.36 | 135.99 | 11.59 | 134.63 | E 2x2 HUB |
|------|------|--------|-------|--------|-----------|

135.99

WALNUT 67

Wt Columbia c 0+00

| | | | | |
|-----|--|------|-------|--|
| N | | 6.2 | 129.8 | |
| cb | | 6.0 | 130.0 | |
| 1/4 | | 5.9 | 130.1 | |
| c | | 6.4 | 129.6 | |
| 1/2 | | 6.9 | 129.1 | |
| cb | | 7.8 | 128.2 | |
| S | | 8.7 | 127.3 | |
| +15 | | 10.4 | 125.6 | |

0+25

| | | | | |
|-----|--|------|-------|--|
| -15 | | 10.1 | 121.9 | |
| S | | 12.9 | 123.1 | |
| cb | | 12.1 | 123.9 | |
| 1/4 | | 11.5 | 124.5 | |
| c | | 11.4 | 124.6 | |
| 1/2 | | 10.7 | 125.3 | |
| cb | | 10.5 | 125.5 | |
| N | | 10.9 | 125.1 | |

| | | | | |
|------|------|--------|-------|--------|
| T.P. | 0.68 | 123.94 | 12.73 | 123.26 |
|------|------|--------|-------|--------|

0+41

| | | | | |
|-----|--|-----|-------|--|
| N | | 2.1 | 121.8 | |
| cb | | 1.7 | 122.2 | |
| 1/2 | | 2.0 | 121.9 | |
| c | | 2.4 | 121.5 | |

| | | | | | | | |
|------------------------------|--|------|-------|----------------|------------|------|-----------------|
| 1/2 | | 2.3 | 121.6 | | cb | 2.1 | 107.6 |
| cb | | 3.1 | 120.8 | | S | 5.7 | 106.5 |
| S | | 4.0 | 119.9 | | +17 house | 4.5 | 107.2 on ground |
| +V NWCOR house | | 4.1 | 119.8 | | 1 + 25 | | |
| 0 + 75 | | | | | - | 10.5 | 101.2 |
| - 2 NWCOR house | | 3.1 | 120.8 | Main floor (l) | S | 9.5 | 102.2 |
| - V TOP LOWER STEP ON STAIRS | | 9.5 | 114.4 | Lower floor | +8 | 9.2 | 102.5 |
| S ON CORR. | | 9.8 | 114.1 | | +11 | 10.7 | 101.0 |
| cb | | 9.6 | 114.3 | | cb | 11.5 | 100.2 |
| 1/2 | | 9.6 | 114.3 | | 1/2 | 11.7 | 100.0 |
| c | | 9.4 | 114.3 | | | | |
| 1/2 | | 10.2 | 113.7 | | c | 11.1 | 100.6 |
| cb | | 10.0 | 113.9 | | 1/2 | 11.9 | 99.8 |
| N | | 10.2 | 113.7 | | cb | 10.9 | 100.8 |
| 0 + 97 | | | | | N | 9.2 | 102.5 |
| N | | 14.3 | 109.6 | | +1 TOP CUT | 9.2 | 102.5 |
| +15 TOP CUT | | 14.0 | 109.9 | | +3 BOT. " | 34.5 | 77.2 |

T.P. 044 111.73 1247 111.27

1403

| | | | |
|-----|----------|------|-------|
| N-3 | BOT. CUT | 30.8 | 80.9 |
| N-1 | TOP " | 3.6 | 108.1 |
| N | | 3.6 | 108.1 |
| cb | | 4.1 | 107.6 |
| 1/2 | | 4.3 | 107.4 |
| c | | 4.3 | 107.4 |
| 1/2 | | 4.1 | 107.6 |

Moore
12/3/37

Xsec of Puterbaugh 50' wide
12' curbs
Pringle to Mission Hills Blvd.

EM. 13' CT. 5.53 230.82 225.29 Pringle
Puterbaugh

0+0-10 = Nly curb Pringle

| | | |
|-------------------|------|--------|
| W cb W.L. Top cb. | 4.47 | 226.35 |
| W gut pav. | 5.38 | 225.44 |
| W cb " | 4.87 | 225.95 |
| C " | 3.92 | 226.90 |
| E cb " | 3.04 | 227.78 |
| E cb E.L. Top cb. | 1.84 | 228.98 |
| " gut pav. | 2.56 | 228.26 |

0+00 = Nly Pringle

| | | |
|------------|------|--------|
| E | 1.7 | 229.1 |
| cb Top | 1.79 | 229.03 |
| " gut pav. | 2.60 | 228.22 |
| C " | 3.33 | 227.49 |
| cb " " | 5.05 | 225.77 |
| cb Top cb. | 4.52 | 226.30 |
| W | 4.2 | 226.6 |

0+30

| | | |
|------------------------|------|--------|
| W | 3.6 | 227.2 |
| +10 | 3.1 | 227.7 |
| cb | 3.6 | 227.2 |
| C | 2.6 | 228.2 |
| gut | 2.2 | 228.6 |
| cb Top | 1.34 | 229.48 |
| +5.67 inside edge work | 1.12 | 229.70 |

Indexed
C.S.K.

69

Mission Hills Blvd.

12' curb
Pringle

12' E 1+96

9' x 9' curb
Pringle

1+47

1+31

Puterbaugh

2+20

12' curb
Pringle

2+30

12'

0+00

conc. pav.

R/10

Pringle

12' curb
Pringle
EM. 225.29

| | | | |
|----------|-----------|------|--------|
| | 0+69 | | |
| E + 6.33 | edge walk | 0.68 | 229.94 |
| cb | | 0.97 | 229.85 |
| gut | | 1.6 | 229.2 |
| c | | 2.2 | 228.6 |
| cb | | 2.5 | 228.3 |
| +3 | | 2.2 | 228.6 |
| W | | 2.7 | 228.1 |
| | 0+70 | | |
| W | | 2.4 | 228.2 |
| +9 | | 2.1 | 228.7 |
| cb | | 2.5 | 228.3 |
| c | | 2.1 | 228.7 |
| gut | | 1.7 | 229.1 |
| cb top | | 0.89 | 229.93 |
| + 5.67 | edge walk | 0.79 | 230.03 |
| | 0+80 | | |
| E + 6.33 | edge walk | 0.89 | 229.93 |
| | | 1.02 | 229.80 |
| gut | | 1.9 | 228.9 |
| c | | 2.2 | 228.6 |
| cb | | 2.4 | 228.2 |
| +3 | | 2.2 | 228.6 |
| W | | 2.7 | 228.1 |
| | 1+18 | | |
| W | on lawn | 3.3 | 227.5 |

| | | | |
|------------------------------|-----------|------|--------|
| cb | | 3.4 | 227.4 |
| +4 | | 3.8 | 227.0 |
| a | | 3.2 | 227.6 |
| gut | | 3.1 | 227.7 |
| cb top cons. | | 1.90 | 228.92 |
| + 5.67 | edge walk | 1.75 | 229.17 |
| | 1+28 | | |
| E + 6.33 | edge walk | 2.06 | 228.76 |
| cb top cons. | | 2.17 | 228.65 |
| gut | | 4.8 | 227.0 |
| c | | 3.8 | 227.0 |
| +10 | | 4.6 | 226.2 |
| cb | | 3.8 | 227.0 |
| W | | 3.6 | 227.2 |
| | 1+31 | | |
| W - 4 = 5/8 line double gar. | | 3.62 | 227.20 |
| W | | 3.9 | 226.9 |
| | 1+38 | | |
| W | | 4.1 | 226.7 |
| cb | | 4.5 | 226.3 |
| +4 | | 5.1 | 225.7 |
| c | | 4.5 | 226.3 |
| gut | | 4.3 | 226.5 |
| cb top | | 3.20 | 227.62 |
| + 5.67 | edge walk | 3.03 | 227.79 |

cem. floor

1+47

| | | | |
|-----------------------------|------|--------|-------------|
| W - 4 N.Y. line double gar. | 8.74 | 227.08 | cert. floor |
| W | 4.9 | 225.9 | |

| | | | | |
|------|------|--------|-------|--------|
| T.P. | 2.17 | 218.06 | 12.93 | 217.89 |
| T.P. | 1.42 | 206.75 | 12.73 | 205.22 |

1+80

| | | | |
|------------------|------|--------|--|
| W | 9.2 | 221.6 | |
| cb | 8.8 | 222.0 | |
| C | 8.5 | 222.3 | |
| gut | 8.0 | 222.8 | |
| cb TOP | 7.52 | 223.30 | |
| + 5.47 edge walk | 7.34 | 223.48 | |

2+70

| | | |
|----|------|-------|
| W | 10.5 | 196.2 |
| cb | 10.5 | 196.2 |
| C | 10.2 | 196.5 |
| +7 | 10.2 | 196.5 |
| cb | 8.2 | 198.5 |
| E | 5.5 | 201.2 |

1+96

| | | | |
|------------------------------|------|-------|---------|
| W | 11.0 | 219.8 | |
| +18 E 5 in. gar. dirt floor | 13.9 | 216.9 | 8' wide |
| 2+20 = end cb + walk on cart | | | |

2+85

| | | |
|----|------|-------|
| E | 12.2 | 194.5 |
| cb | 15.3 | 191.4 |
| C | 17.4 | 189.1 |
| cb | 18.9 | 187.8 |
| W | 19.2 | 187.5 |

| | | |
|------------------|-------|--------|
| gut + TOP cb. | 11.64 | 219.14 |
| + 5.87 edge walk | 11.52 | 219.30 |

3+00 = Sly Mission Hills Blvd.

| | | |
|----|------|-------|
| W | 24.0 | 182.7 |
| cb | 22.5 | 184.2 |
| C | 21.4 | 185.3 |
| cb | 20.5 | 186.2 |
| E | 19.0 | 187.7 |

2+40

| | | |
|----|------|-------|
| E | 10.6 | 220.2 |
| cb | 13.5 | 217.3 |
| C | 14.6 | 216.2 |
| cb | 15.3 | 215.5 |
| +6 | 17.2 | 213.6 |
| W | 16.6 | 214.2 |

Please check
to Mission Hills Blvd. Profile

X sec alley 20' wide
 BIK 166 U.H.

Moore
 1-19-88

Indexed
 c.s.k.

72

S.E.P.P. 6.60 369.54 362.94 Lincoln
 Utah

0+00 = N1/4 Lincoln

| | | | |
|---|-----|------|--------|
| W | cb | 5.59 | 363.95 |
| W | Par | 5.72 | 363.82 |
| C | " | 6.09 | 363.48 |
| E | " | 5.89 | 363.65 |
| E | cb | 5.72 | 363.82 |

0+05

| | | | |
|---|--|-----|-------|
| E | | 4.5 | 365.0 |
| C | | 5.2 | 364.3 |
| W | | 4.5 | 365.0 |

0+25

| | | | |
|---|--|-----|-------|
| W | | 4.4 | 365.1 |
| C | | 4.9 | 364.6 |
| E | | 4.7 | 364.8 |

0+43

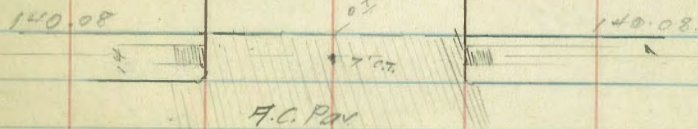
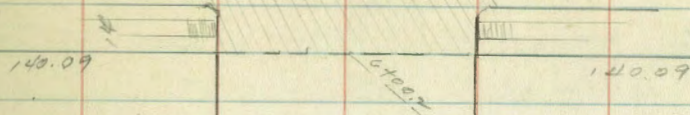
| | | | |
|---|-----------|------|--------|
| E | E 2' MARK | 4.25 | 365.29 |
| C | | 4.7 | 364.8 |

| | | | |
|---|--|-----|-------|
| W | | 4.4 | 365.1 |
|---|--|-----|-------|

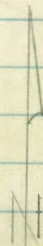
0+52

| | | | |
|---|--|-----|-------|
| W | | 4.8 | 364.7 |
| C | | 4.6 | 364.9 |
| E | | 4.3 | 365.2 |

+5 S. edge triple gate dirt 4.2 365.3



⊙ 0+82 focal tree
 should be removed.
 Roots stop up sewer
 line in alley



LINCOLN

369.54

0+57

W Sin. gar. dirt 2.6 364.9

0+82

-5 N edge triple gar. dirt 2.1 365.4

-1 E. Foot. tree 30" diam. should be removed

E 3.9 365.6

C 2.1 365.4

W 3.8 365.7

0+89

W 2 mark 3.58 365.96

1+00

W 3.9 365.6

C 4.0 365.5

E 3.9 365.6

1. +43

-3.5 Sin. gar. dirt 3.4 366.1

E 3.5 366.0

C 3.5 366.0

W 3.1 366.4

1+57

W 3.3 366.2

C 3.4 366.1

E 3.5 366.0

+6 Sin. gar. dirt 3.4 366.1

369.54

2+08

E 3.1 366.4

C 3.1 366.4

W Sin. gar. dirt 2.7 366.8

2+50

W 3.0 366.5

C 2.7 366.8

E 3.8 366.7

2+78

E 2.0 367.5

C 2.3 367.3

W 2.1 367.4

+1 E 4' mark 1.92 367.62

2+00

W 2.3 367.2

C 2.3 367.2

E 2.1 367.4

T.P. 6.48 374.03 1.99 367.55

3+08

E 6.6 367.4

C 6.7 367.3

W 6.6 367.4

+1 E approx com. 6.56 367.47

+3.5 gar. com.

WEST
ENTRANCE

374.03

| | | |
|---------------------|------|--------|
| 2+59 | | |
| - 2 S.W. gar. corr. | 5.90 | 368.13 |
| W | 6.0 | 368.0 |
| C | 6.7 | 367.8 |
| E | 6.3 | 367.7 |

4+00

| | | |
|----------------------|-----|-------|
| E Fence 0.4 in alley | 6.0 | 368.0 |
| C | 6.1 | 367.9 |
| W | 6.0 | 368.0 |

4+33

| | | |
|-------------------|------|--------|
| W | 5.7 | 368.3 |
| C | 5.7 | 368.3 |
| E 2' walk on line | 5.59 | 368.44 |

4+50

| | | |
|---|-----|-------|
| E Nudge 10' shot of ⁱⁿ alley | 5.2 | 368.8 |
| C | 5.2 | 368.8 |
| W | 5.0 | 368.0 |

4+57

| | | |
|--------------------|------|--------|
| - 1.7 E gar. corr. | 4.77 | 369.26 |
| W | 4.8 | 369.2 |

4+80

| | | |
|-------------|------|--------|
| E E 3' walk | 4.45 | 369.58 |
|-------------|------|--------|

4+87

| | | |
|---|-----|-------|
| W | 4.8 | 369.2 |
| E | 4.8 | 369.2 |

374.03

74

| | | |
|------------------|-----|-------|
| E S.W. gar. corr | 4.6 | 369.4 |
|------------------|-----|-------|

5+03

| | | |
|-----------------------------|------|--------|
| - 1 Sedge triple gar. corr. | 4.38 | 369.65 |
|-----------------------------|------|--------|

| | | |
|---------------|------|-------|
| E corr. apron | 4.43 | 369.6 |
|---------------|------|-------|

| | | |
|---|-----|-------|
| C | 4.5 | 369.5 |
|---|-----|-------|

| | | |
|---|-----|-------|
| W | 4.7 | 369.3 |
|---|-----|-------|

5+02

| | | |
|---|-----|-------|
| W | 4.3 | 369.7 |
|---|-----|-------|

| | | |
|---|-----|-------|
| C | 4.3 | 369.7 |
|---|-----|-------|

| | | |
|--------------|------|--------|
| E corr apron | 4.46 | 369.57 |
|--------------|------|--------|

| | | |
|------------------------------|------|--------|
| + 1 N edge triple gar. corr. | 4.37 | 369.66 |
|------------------------------|------|--------|

5+42

| | | |
|---------------------|------|--------|
| - 1 S.W. gar. corr. | 4.27 | 369.76 |
|---------------------|------|--------|

| | | |
|-----------|------|--------|
| E apron " | 4.26 | 369.67 |
|-----------|------|--------|

| | | |
|---|-----|-------|
| C | 4.2 | 369.8 |
|---|-----|-------|

| | | |
|---|-----|-------|
| W | 4.2 | 369.8 |
|---|-----|-------|

5+49

| | | |
|-----------|------|--------|
| E 2' walk | 4.24 | 369.79 |
|-----------|------|--------|

5+75

| | | |
|---|-----|-------|
| W | 4.4 | 369.6 |
|---|-----|-------|

| | | |
|---|-----|-------|
| C | 4.3 | 369.7 |
|---|-----|-------|

| | | |
|---|-----|-------|
| E | 4.7 | 369.3 |
|---|-----|-------|

5+90

| | | |
|---|-----|-------|
| E | 4.8 | 369.2 |
|---|-----|-------|

| | | |
|---|-----|-------|
| C | 4.6 | 369.4 |
|---|-----|-------|

| | | |
|---|-----|-------|
| W | 4.6 | 369.4 |
|---|-----|-------|

| | | | | |
|-----------------------|--------|--------|--------|--|
| 6400.4 SE PAIK | 374.03 | | | |
| W Top cb | 5.28 | 368.75 | | |
| W paik. | 5.40 | 368.63 | | |
| O " | 5.47 | 368.56 | | |
| E " | 5.82 | 368.91 | | |
| E Top cb | 5.14 | 368.89 | | |
| T.P. 448 | 373.27 | 5.24 | 368.79 | |
| S.E. B.P. Paik-1 date | 3.27 | 370.00 | 369.96 | |

Columbia Street

To Eckenrode for study 8-6-57

X sec alley "Blue Bird Lane" 20' wide
 BIK 45 La Jolla Park

Moore
 3-31-38.

| | | | | | |
|-------------|-------|--------|------|--------|--------------|
| SE. 7' C.T. | 12.92 | 165.08 | | 152.16 | Torrey Rd. |
| | | | | 152.25 | Prospect Pl. |
| T.R. | 7.64 | 172.49 | 0.23 | 164.85 | |

0-14 = N 26 Prospect

| | | | | | |
|-------|--|------|--|--------|--|
| W pav | | 5.75 | | 166.74 | |
| C " | | 4.62 | | 167.85 | |
| E " | | 3.17 | | 169.32 | |

0-7

| | | | | | |
|--------------|--|------|--|--------|-----|
| E pav. | | 2.55 | | 169.94 | |
| C " Ld. C.T. | | 4.21 | | 168.28 | BIK |
| +5 " | | 4.89 | | 167.60 | |
| W " | | 5.08 | | 167.46 | |

0+00 = N 2 Prospect Pl

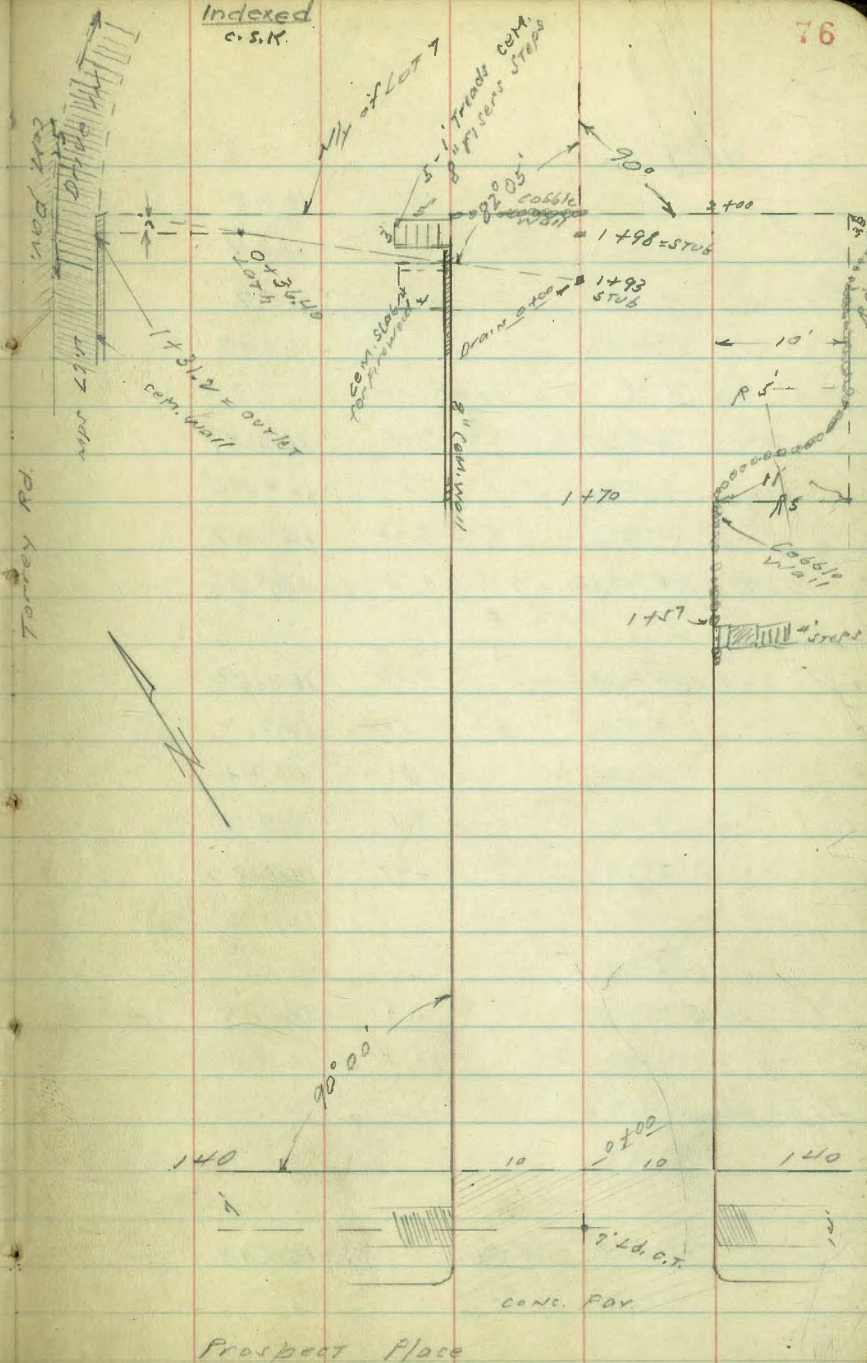
| | | | | | |
|--------------------------|--|------|--|--------|--|
| W pav | | 4.96 | | 167.53 | |
| +5 " | | 4.81 | | 167.68 | |
| C " | | 4.04 | | 168.45 | |
| E " | | 2.50 | | 169.99 | |
| E Top and beg. Cem. wall | | 2.85 | | 170.14 | |

0+09

| | | | | | |
|------------|--|------|--|--------|--|
| E Top Wall | | 3.72 | | 168.77 | |
| E | | 5.4 | | 166.9 | |
| C | | 6.4 | | 166.1 | |
| +5 | | 6.6 | | 165.9 | |
| W | | 6.1 | | 166.4 | |

Indexed
 c. S. K.

76



172.49

| | | |
|-------------------------------|------|--------|
| W | 7.7 | 164.8 |
| C | 7.6 | 164.9 |
| E | 6.8 | 165.7 |
| E TOP wall | 4.40 | 167.09 |
| 0+58 E of 2' cent. cross wall | | |
| E Bot. 2' cent. step | 7.18 | 165.31 |
| E cur | 7.54 | 164.95 |
| C | 8.22 | 164.27 |
| W TOP wall + Bot. wall | 8.13 | 164.36 |
| 1+00 | | |
| W TOP end cent. wall | 9.20 | 163.19 |
| W | 10.2 | 162.1 |
| C | 10.2 | 162.1 |
| E | 9.7 | 162.8 |
| E " " " " | 6.47 | 166.02 |

1+25

| | | |
|-------------|------|-------|
| E Hedge | 11.3 | 161.2 |
| C | 11.7 | 160.8 |
| W Bd. Fence | 11.6 | 160.9 |

T.P. 0.75 160.61 12.63 159.86

160.61

77

1+55

| | | |
|---------------------------|------|--------|
| W | 2.1 | 158.5 |
| C | 2.2 | 158.4 |
| E | 2.0 | 158.6 |
| E 2' 4" cent. step & wall | 1.11 | 159.50 |
| 1+70 | | |
| E | 3.1 | 157.5 |
| C | 3.3 | 157.3 |
| W | 3.2 | 157.4 |
| W 609.7 Top Cent. wall | 1.80 | 158.81 |
| 1+75 | | |
| W TOP | 2.12 | 158.49 |
| W | 3.6 | 157.0 |
| C | 3.7 | 156.9 |
| E | 3.7 | 156.9 |
| E + 5 | 3.4 | 157.2 |

6+9.04
Cobble wall
on east
and end
of hedge

on west

1+80

| | | |
|--------|------|--------|
| W | 3.7 | 156.9 |
| E | 3.8 | 156.8 |
| C | 4.1 | 156.5 |
| W | 4.1 | 156.5 |
| W wall | 2.42 | 158.19 |

1+90

| | | |
|--------|------|--------|
| W wall | 3.05 | 157.58 |
| W | 4.7 | 155.9 |
| C | 4.7 | 155.9 |

| | | |
|----------------------|------|--------|
| E | 4.7 | 155.9 |
| +10 | 4.1 | 156.5 |
| 2+00 | | |
| -10 | 4.3 | 156.3 |
| E | 4.8 | 155.8 |
| C | 4.9 | 155.7 |
| C Top cobble wall | 4.3 | 156.3 |
| W " of 3' corr. step | 5.03 | 155.58 |

Levels for drain

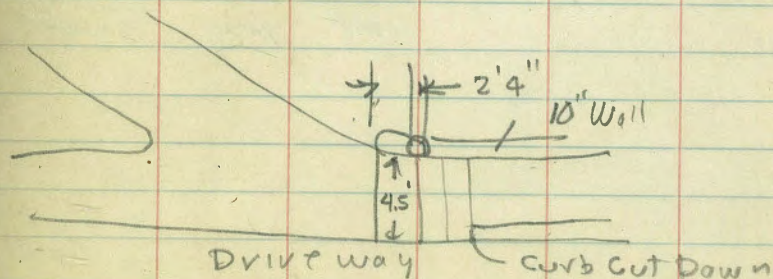
| | | | |
|--|------|--------|------------------|
| 1+93 2 alleys 0+00 stub for drain | 4.57 | 156.04 | |
| 0+10 ground | 4.7 | 155.9 | |
| 0+10.3 Top wall | 3.01 | 157.60 | |
| 0+11 bot " also corr. 4x4 slab | 7.92 | 152.69 | |
| 0+18 beg. + sly edge brick wall | 8.61 | 152.00 | Replace Brick |
| 0+29 end + 1/4 " | 9.3 | 151.3 | |
| 0+36.4 Δ STUB | 9.72 | 150.89 | |
| 0+50 2' 4" N edge 15' Pine " Torrey | 12.2 | 148.4 | |

| | | | | |
|------|------|--------|-------|--------|
| T.P. | 1.58 | 149.75 | 12.44 | 148.17 |
| 0+80 | | | 5.9 | 143.9 |
| 1+10 | | | 10.8 | 139.0 |

149.75

| | | | | |
|--|------|--------|-------|-------------------|
| T.P. | 1.37 | 138.69 | 12.43 | 137.32 |
| 1+31.2 Top 10" corr wall | 2.42 | 135.27 | | |
| 1+31.2 Top inside edge of 4.67 wide sidewalk = F.L. of drain Drive will be spillw | 4.45 | 134.24 | | |
| +4.67 Top curb drive | 4.94 | 133.75 | | = Ely c6. |
| " gut. corr. par. | 5.05 | 133.64 | | of Torrey Road |

| | | | | |
|--------------------|-------|--------|------|--------|
| T.P. | 12.66 | 151.06 | 0.29 | 138.40 |
| T.P. | 6.33 | 156.99 | 0.40 | 150.66 |
| check to B.M. C.T. | | | 4.84 | 152.15 |

152.16
~~152.65~~

La Jolla
check levels

Moore
21-1-38.

| | | | | | | |
|---------------------|-------|--------|------|-----------|----------------------------|---------------|
| S. Cor. B.P. | 13.00 | 145.08 | | 132.08 | Prospect Pl. Park Row | Bench Bk. El. |
| T.P. | 10.30 | 155.26 | 0.12 | 144.96 | | |
| SE. 7' C.T. | | | 2.72 | 152.54 | Jorrey Rd. Prospect Pl. | 152.65 ✓ |
| | | | | <u>38</u> | | |
| Top curb NW Cor. | | | 5.83 | 149.43 | " " | 149.98 |

| | | | | | | |
|--------------|-------|---------|-------|---------|--------------------------|--------|
| S. Cor. B.P. | 1.66 | 133.74 | | 132.08 | Prospect Pl. Park Row | |
| T.P. | 0.505 | 124.075 | 10.17 | 123.57 | | |
| N. Cor. B.P. | 1.49 | 114.975 | 10.59 | 113.485 | Prospect Cave | 113.11 |
| T.P. | 2.98 | 108.91 | 9.045 | 105.93 | | |
| T.P. | 1.54 | 105.74 | 4.71 | 104.20 | | |
| T.P. | 1.29 | 98.89 | 9.14 | 96.60 | | |
| SW B.P. | | | 4.44 | 94.45 | Prospect Cave | 94.07 |

Walker. Additional Levels North-South Alley.
 18bell Alley, 64 - E.W. Morse Add.
 8-1-40 Det. Broadway & C - St.
 " 28th & 29

145067 P. 40
 BM. Rim
 Sewer NH

| | | | | |
|---|------------|--|--------|--------|
| S | - | 2.25 | 190.16 | 187.91 |
| T | | 0+60 = 60' N.H.L. Broadway | | |
| | -10 | | 7.9 | 182.3 |
| S | W | | 6.4 | 183.8 |
| | +3 | | 5.8 | 184.4 |
| T | L | | 5.3 | 184.9 |
| | E | | 4.4 | 185.8 |
| | +5 | | 2.9 | 182.3 |
| | | 0+70 | | |
| | E | | 4.6 | 185.6 |
| S | L | | 5.1 | 185.1 |
| T | +5 | | 5.3 | 184.9 |
| M | W | | 6.8 | 183.4 |
| T | +10 | | 8.7 | 181.5 |
| T | | 0+85 - Beginning Fence & Cobble Wall on East | | |
| T | | Wall is 0.6' in Alley Fence on West | | |
| | -10 | | 8.8 | 181.4 |
| S | W | | 7.2 | 183.0 |
| | +5 | | 5.2 | 185.0 |
| | L | | 4.7 | 185.8 |
| | +9.4 = toe | Loose wall | 4.4 | 185.5 |
| | E on | " " | 2.9 | 187.8 |

Cert P-1

Alley.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.
 Distance of slope stake from side or shoulder
 stake for any width roadway, slope 1 to 1.
 If ground is nearly level, the cut or fill at side
 stake is located by the double entry method in
 left column and top row. The number in body

IMPROVED TABLES
 AND
 INFORMATION

Note. Cobble wall is built on
 better (No Cement)

Redwood & Felton NW. BP 313.01

41.59

500
585
215

860.
215
1075

574.72
157.18
417.54

1.90 \pm 8' cont 20' 2A

1.27

131

cont 5 back

Part 10610

12-25