

1536

FIELD BOOK

No. 5857

MICROFILMED

JUL 24 1964

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
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Indexed
ask.

Hand Level x sec
Prop. EXT. of 54th ST.
Sec 1402-67
for E.E.

Stone
Sisson
Newborn
11-19-34

+65

+50

+28

11

+50

+19.7 additive

10

9+50

$$\begin{array}{r} 318.0 \\ + 17.0 \\ \hline 335.0 \end{array}$$

$$\begin{array}{r} 308.9 \\ + 10.1 \\ \hline 319.0 \end{array}$$

$$\begin{array}{r} 298.4 \\ - 2.7 \\ \hline 295.7 \end{array}$$

$$\begin{array}{r} 390.2 \\ - 2.7 \\ \hline 387.5 \end{array}$$

$$\begin{array}{r} 284.7 \\ - 1.7 \\ \hline 283.0 \end{array}$$

$$\begin{array}{r} 322.9 \\ + 7.3 \\ \hline 330.2 \end{array}$$

$$\begin{array}{r} 316.9 \\ + 3.0 \\ \hline 319.9 \end{array}$$

$$\begin{array}{r} 303.4 \\ - 10.6 \\ \hline 292.8 \end{array}$$

$$\begin{array}{r} 293.0 \\ - 10.6 \\ \hline 282.4 \end{array}$$

$$\begin{array}{r} 288.9 \\ - 1.7 \\ \hline 287.2 \end{array}$$

$$\begin{array}{r} 329.9 \\ + 15.5 \\ \hline 345.4 \end{array}$$

$$\begin{array}{r} 324.0 \\ + 9.6 \\ \hline 333.6 \end{array}$$

$$\begin{array}{r} 314.4 \\ - 11.0 \\ \hline 303.4 \end{array}$$

$$\begin{array}{r} 303.4 \\ - 11.0 \\ \hline 292.4 \end{array}$$

$$\begin{array}{r} 295.5 \\ - 18.9 \\ \hline 276.6 \end{array}$$

$$\begin{array}{r} 334.0 \\ + 12.7 \\ \hline 346.7 \end{array}$$

$$\begin{array}{r} 331.3 \\ + 10.2 \\ \hline 341.5 \end{array}$$

$$\begin{array}{r} 321.1 \\ - 7.2 \\ \hline 313.9 \end{array}$$

$$\begin{array}{r} 311.9 \\ - 7.2 \\ \hline 304.7 \end{array}$$

$$\begin{array}{r} 303.4 \\ - 17.3 \\ \hline 286.1 \end{array}$$

$$\begin{array}{r} 350.9 \\ + 14.3 \\ \hline 365.2 \end{array}$$

$$\begin{array}{r} 345.3 \\ + 8.7 \\ \hline 354.0 \end{array}$$

$$\begin{array}{r} 336.6 \\ - 7.6 \\ \hline 329.0 \end{array}$$

$$\begin{array}{r} 329.0 \\ - 7.6 \\ \hline 321.4 \end{array}$$

$$\begin{array}{r} 322.4 \\ - 14.2 \\ \hline 308.2 \end{array}$$

$$\begin{array}{r} 357.2 \\ + 12.4 \\ \hline 369.6 \end{array}$$

$$\begin{array}{r} 351.0 \\ + 6.2 \\ \hline 357.2 \end{array}$$

$$\begin{array}{r} 344.5 \\ - 8.0 \\ \hline 336.5 \end{array}$$

$$\begin{array}{r} 336.8 \\ - 8.0 \\ \hline 328.8 \end{array}$$

$$\begin{array}{r} 329.7 \\ - 15.1 \\ \hline 314.6 \end{array}$$

$$\begin{array}{r} 361.2 \\ + 13.4 \\ \hline 374.6 \end{array}$$

$$\begin{array}{r} 353.3 \\ + 5.5 \\ \hline 358.8 \end{array}$$

$$\begin{array}{r} 347.5 \\ - 9.2 \\ \hline 338.3 \end{array}$$

$$\begin{array}{r} 338.6 \\ - 9.2 \\ \hline 329.4 \end{array}$$

$$\begin{array}{r} 332.1 \\ - 15.7 \\ \hline 316.4 \end{array}$$

$$\begin{array}{r} 366.5 \\ + 12.3 \\ \hline 378.8 \end{array}$$

$$\begin{array}{r} 359.0 \\ + 5.7 \\ \hline 364.7 \end{array}$$

$$\begin{array}{r} 353.3 \\ - 9.7 \\ \hline 343.6 \end{array}$$

$$\begin{array}{r} 343.6 \\ - 9.7 \\ \hline 333.9 \end{array}$$

$$\begin{array}{r} 336.2 \\ - 17.1 \\ \hline 319.1 \end{array}$$

+80

+75 OUTS SAME AS +80

+50

+45

13

+75

+50

+25

12

$\frac{274.3}{+9.7/100}$
 $\frac{268.6}{+40+1.7/75}$
 $\frac{266.3}{-0.6/50}$
 $\frac{264.0}{0.0/30}$
 $\frac{264.6}{-1.2/25}$
 $\frac{263.2}{+264.6/25}$
 $\frac{264.9}{+0.3/25}$
 $\frac{266.15}{+2.3/35}$
 $\frac{268.7}{+5.1/38}$
 $\frac{271.2}{+8.0/75}$
 $\frac{272.3}{+1.4/100}$

SAME EL. AS +45 MAX SAME OUTS

$\frac{282.8}{+17.7/90}$
 $\frac{272.0}{+6.7/60}$
 $\frac{266.8}{+1.5/20}$
 $\frac{264.3}{-1.0/30}$
 $\frac{265.6}{+0.3/38}$
 $\frac{266.3}{+1.0/50}$
 $\frac{268.5}{+3.5/100}$
 $\frac{273.3}{+8.0/115}$

$\frac{292.8}{+25.7/70}$
 $\frac{281.9}{+14.8/50}$
 $\frac{272.4}{+5.8/30}$
 $\frac{267.1}{0.0/15}$
 $\frac{264.8}{-2.3/8}$
 $\frac{267.1}{0.0/26}$
 $\frac{267.9}{20.8-2.2/20}$
 $\frac{264.9}{-0.6/45}$
 $\frac{268.5}{+0.6/50}$
 $\frac{268.1}{+1.0/75}$
 $\frac{269.1}{+2.0/115}$

$\frac{300.4}{+32.7/70}$
 $\frac{293.3}{+15.1/55}$
 $\frac{277.7}{+9.7/15}$
 $\frac{268.2}{-2.4/13}$
 $\frac{265.4}{-1.7/25}$
 $\frac{266.5}{0.0/50}$
 $\frac{268.2}{-1.5/60}$
 $\frac{266.7}{-0.6/115}$

$\frac{307.1}{+25.1/70}$
 $\frac{302.3}{+20.9/60}$
 $\frac{290.0}{+8.0/30}$
 $\frac{282.0}{-8.7/25}$
 $\frac{273.3}{-15.0/43}$
 $\frac{267.0}{-1.3/75}$
 $\frac{268.2}{-13.5/115}$

$\frac{312.5}{+20.5/70}$
 $\frac{301.4}{+15.1/50}$
 $\frac{293.9}{+5.0/25}$
 $\frac{288.3}{-7.3/30}$
 $\frac{281.0}{-16.1/70}$
 $\frac{272.2}{-18.2/100}$

$\frac{311.3}{+18.3/60}$
 $\frac{302.0}{+9.0/30}$
 $\frac{293.0}{-7.3/30}$
 $\frac{285.7}{-12.5/60}$
 $\frac{278.5}{-18.7/100}$

+50

$\frac{271.6}{-2.4}$	$\frac{276.4}{+2.8}$	$\frac{279.3}{+5.3}$	$\frac{270.0}{-1.0}$	$\frac{274.0}{+1.7}$	$\frac{275.7}{+5.7}$	$\frac{279.7}{+15.5}$	$\frac{289.5}{+21.5}$	$\frac{295.5}{+28.3}$
105	80	40	20	10	15	50	70	90

+34

$\frac{267.3}{-10.7}$	$\frac{273.5}{-4.5}$	$\frac{275.3}{-2.7}$	$\frac{267.7}{-10.3}$	$\frac{274.6}{-4.4}$	$\frac{280.6}{+2.6}$	$\frac{288.4}{+10.4}$	$\frac{293.4}{+15.4}$	$\frac{291.1}{+21.1}$
100	70	55	30	21	20	50	70	90

15

$\frac{261.1}{-14.5}$	$\frac{258.6}{-17.0}$	$\frac{260.4}{-15.2}$	$\frac{263.3}{-12.3}$	$\frac{274.6}{-1.0}$	$\frac{279.7}{+2.1}$	$\frac{287.1}{+11.5}$	$\frac{292.2}{+16.6}$	$\frac{292.2}{+29.2}$
115	95	65	97	6	25	50	70	90

+71.82 B.C. Pt.

$\frac{261.5}{-5.2}$	$\frac{262.0}{-5.0}$	$\frac{259.3}{-7.5}$	$\frac{260.6}{-6.5}$	$\frac{262.6}{-4.4}$	$\frac{261.2}{-5.7}$	$\frac{261.2}{-5.8}$	$\frac{262.7}{-4.9}$	$\frac{273.8}{+4.8}$	$\frac{284.2}{+17.2}$	$\frac{285.2}{+21.2}$
115	90	80	70	68	23	25	25	15	50	70

+50

$\frac{262.3}{-1.5}$	$\frac{262.4}{-1.4}$	$\frac{262.5}{-1.0}$	$\frac{262.5}{-2.9}$	$\frac{260.9}{-2.6}$	$\frac{261.2}{-0.2}$	$\frac{263.5}{-1.8}$	$\frac{262.0}{-0.2}$	$\frac{263.4}{-0.2}$	$\frac{263.5}{+8.4}$	$\frac{272.2}{+11.4}$	$\frac{275.2}{+24.7}$	$\frac{287.9}{+27.6}$
115	100	80	75	60	50	70	0	25	25	40	80	90

+40 Same El. on outs as +35

$\frac{262.4}{+0.3}$	$\frac{262.5}{+0.4}$	$\frac{262.5}{+0.7}$	$\frac{262.5}{-1.3}$	$\frac{260.5}{-0.8}$	$\frac{261.3}{-0.8}$	$\frac{262.1}{+1.7}$	$\frac{263.4}{+3.5}$	$\frac{265.6}{+11.7}$	$\frac{273.4}{+24.6}$
115	100	70	50	35	25	2	15	45	90

+35

$\frac{269.1}{+50}$	$\frac{268.9}{+31.85}$	$\frac{264.5}{+0.4}$	$\frac{263.7}{-0.1}$	$\frac{262.8}{-1.2}$	$\frac{262.7}{-1.2}$	$\frac{263.4}{+0.7}$	$\frac{272.0}{+7.9}$	$\frac{275.3}{+12.2}$	$\frac{285.3}{+22.1}$
100	80	60	50	55	15	20	50	70	100

14

+50

$\frac{349.7}{50}$	$\frac{346.1}{25}$	$\frac{341.4}{60}$	$\frac{335.6}{50}$	$\frac{329.5}{50}$	$\frac{317.1}{72}$	$\frac{320.2}{80}$
+8.1	+4.4	-4.4	-6.0	-3.1	-2.4	-1.2

18

$\frac{340.2}{50}$	$\frac{337.0}{25}$	$\frac{332.9}{50}$	$\frac{329.8}{50}$	$\frac{325.7}{50}$	$\frac{318.8}{70}$	$\frac{304.7}{80}$	$\frac{312.7}{90}$
+7.3	+2.7	-3.1	-3.1	-2.2	-2.4	-2.2	-2.0

+69.11 EC

$\frac{334.0}{50}$	$\frac{331.2}{25}$	$\frac{328.0}{50}$	$\frac{324.5}{25}$	$\frac{319.2}{50}$	$\frac{316.1}{60}$	$\frac{304.9}{80}$	$\frac{311.9}{90}$
+6.0	+4.2	-8.5	-8.8	-7.9	-2.1	-6.1	-6.1

+50

$\frac{329.5}{50}$	$\frac{327.2}{25}$	$\frac{324.5}{25}$	$\frac{320.4}{25}$	$\frac{315.0}{50}$	$\frac{306.4}{75}$	$\frac{302.4}{85}$	$\frac{306.5}{90}$
+4.0	+2.7	-2.1	-4.5	-9.5	-12.1	-12.1	-12.0

17

$\frac{318.3}{60}$	$\frac{318.4}{50}$	$\frac{318.4}{25}$	$\frac{317.3}{25}$	$\frac{313.3}{25}$	$\frac{306.8}{50}$	$\frac{300.0}{72}$	$\frac{297.0}{80}$	$\frac{300.3}{90}$
+1.0	+1.1	+1.1	-4.0	-10.5	-17.3	-20.3	-17.0	-17.0

+50

$\frac{306.7}{50}$	$\frac{310.0}{50}$	$\frac{311.0}{25}$	$\frac{310.4}{25}$	$\frac{305.1}{40}$	$\frac{296.8}{80}$	$\frac{290.7}{71}$	$\frac{294.8}{80}$	$\frac{300.4}{70}$
-3.7	-0.2	+0.6	-5.0	-13.6	-19.7	-15.6	-10.0	-10.0

+20

$\frac{295.7}{80}$	$\frac{300.3}{50}$	$\frac{304.5}{25}$	$\frac{304.0}{25}$	$\frac{298.5}{45}$	$\frac{292.3}{50}$	$\frac{287.5}{65}$	$\frac{294.5}{80}$
-8.3	-3.7	+0.5	-5.5	-1.7	-16.5	-12.5	-6.5

16

$\frac{285.1}{90}$	$\frac{287.0}{80}$	$\frac{291.4}{50}$	$\frac{294.7}{55}$	$\frac{295.1}{25}$	$\frac{291.1}{40}$	$\frac{280.7}{60}$	$\frac{285.1}{72}$	$\frac{294.1}{80}$	$\frac{294.1}{90}$
+10.0	-8.1	-3.7	+0.7	+4.0	-10.4	-10.0	+6.1	+6.1	

22

$\frac{403.3}{50}$	$\frac{398.3}{25}$	$\frac{391.9}{25}$	$\frac{390.1}{50}$
+ 7.7	+ 4.7	- 1.7	- 0.7

+50

$\frac{394.1}{50}$	$\frac{389.9}{25}$	$\frac{383.1}{25}$	$\frac{381.6}{50}$
+ 8.5	+ 4.3	- 1.7	- 1.2

+22.73 BC Pt.

$\frac{386.2}{50}$	$\frac{385.4}{25}$	$\frac{377.3}{25}$	$\frac{374.1}{60}$
+ 5.4	+ 4.0	- 1.7	- 4.7

21

$\frac{388.0}{50}$	$\frac{381.9}{25}$	$\frac{373.3}{25}$	$\frac{369.8}{60}$
+ 11.1	+ 5.0	- 3.6	- 7.1

+50

$\frac{381.7}{50}$	$\frac{375.9}{25}$	$\frac{365.3}{25}$	$\frac{360.1}{60}$
+ 11.2	+ 5.2	- 5.2	- 10.6

20

$\frac{374.6}{80}$	$\frac{368.9}{25}$	$\frac{357.8}{25}$	$\frac{351.8}{35}$	$\frac{346.4}{75}$	$\frac{341.7}{80}$
+ 11.7	+ 6.0	- 1.1	- 1.1	- 6.5	- 2.2

+50

$\frac{369.3}{50}$	$\frac{364.0}{25}$	$\frac{349.3}{25}$	$\frac{339.3}{58}$	$\frac{332.3}{70}$
+ 12.5	+ 7.2	- 7.7	- 17.5	- 24.5

19

$\frac{360.8}{50}$	$\frac{356.1}{25}$	$\frac{341.4}{25}$	$\frac{335.7}{26}$	$\frac{322.7}{65}$	$\frac{327.0}{75}$
+ 11.2	+ 6.7	- 8.2	- 13.9	- 22.9	- 22.6

+63.47 = E.C.

+50

24

+75

+50

+25

23

+50

$\frac{400.0}{-2.2}$	$\frac{404.7}{-4.7}$	$\frac{409.2}{+1.8}$	$\frac{411.0}{+1.8}$	$\frac{413.9}{+4.7}$
$\frac{400.7}{-2.2}$	$\frac{406.4}{-3.8}$	$\frac{410.2}{+1.2}$	$\frac{411.4}{+1.2}$	$\frac{413.2}{+4.0}$
$\frac{409.8}{-2.7}$	$\frac{411.5}{-1.8}$	$\frac{412.5}{+0.2}$	$\frac{413.2}{+0.2}$	$\frac{413.5}{+1.0}$
$\frac{412.1}{-2.0}$	$\frac{413.1}{-1.0}$	$\frac{414.1}{-0.7}$	$\frac{413.4}{-0.7}$	$\frac{414.1}{0.0}$
$\frac{415.0}{-2.2}$	$\frac{413.8}{+0.2}$	$\frac{413.5}{+0.2}$	$\frac{412.2}{-1.8}$	$\frac{411.2}{-2.0}$
$\frac{413.4}{+0.7}$	$\frac{412.0}{-0.7}$	$\frac{412.7}{+0.7}$	$\frac{410.3}{-2.4}$	$\frac{408.7}{-4.0}$
$\frac{411.6}{+2.0}$	$\frac{412.1}{+2.2}$	$\frac{409.6}{+1.3}$	$\frac{408.3}{-1.3}$	$\frac{407.3}{-2.8}$
$\frac{409.3}{+0.1}$	$\frac{407.2}{+2.0}$	$\frac{403.2}{+3.2}$	$\frac{399.5}{+3.7}$	$\frac{398.1}{-1.1}$

+75

+50

27 + 03 > 1 B.C. = C.V. ✓

B.M. 11.73 394.88 383.15 old Ac. Mod

+50

26

+50

25

370.6
18.9
60

373.1
21.8
40

378.6
16.3
25

387.6
7.0
70

391.9
3.0
25

395.7
+0.8
50

372.9
22.0
60

368.7
26.2
45

374.3
20.6
45

376.5
18.2
25

383.7
11.0
110

389.5
5.2
25

394.6
0.3
50

361.7
33.2
60

369.5
25.1
45

376.5
18.1
25

383.5
11.40
110

388.5
4.4
25

393.4
1.5
50

376.4
11.0
60

382.1
5.3
25

387.4
4.4
25

391.8
+10.2
60

380.4
10.7
60

386.1
5.0
25

391.1
4.5
25

395.6
+11.7
60

387.0
10.2
60

392.5
4.7
25

397.2
+2.0
25

401.2
+10.2
60

394.6
8.3
60

399.3
4.6
25

402.9
4.0
25

406.9
+10.5
60

407.4
407.4

413.4

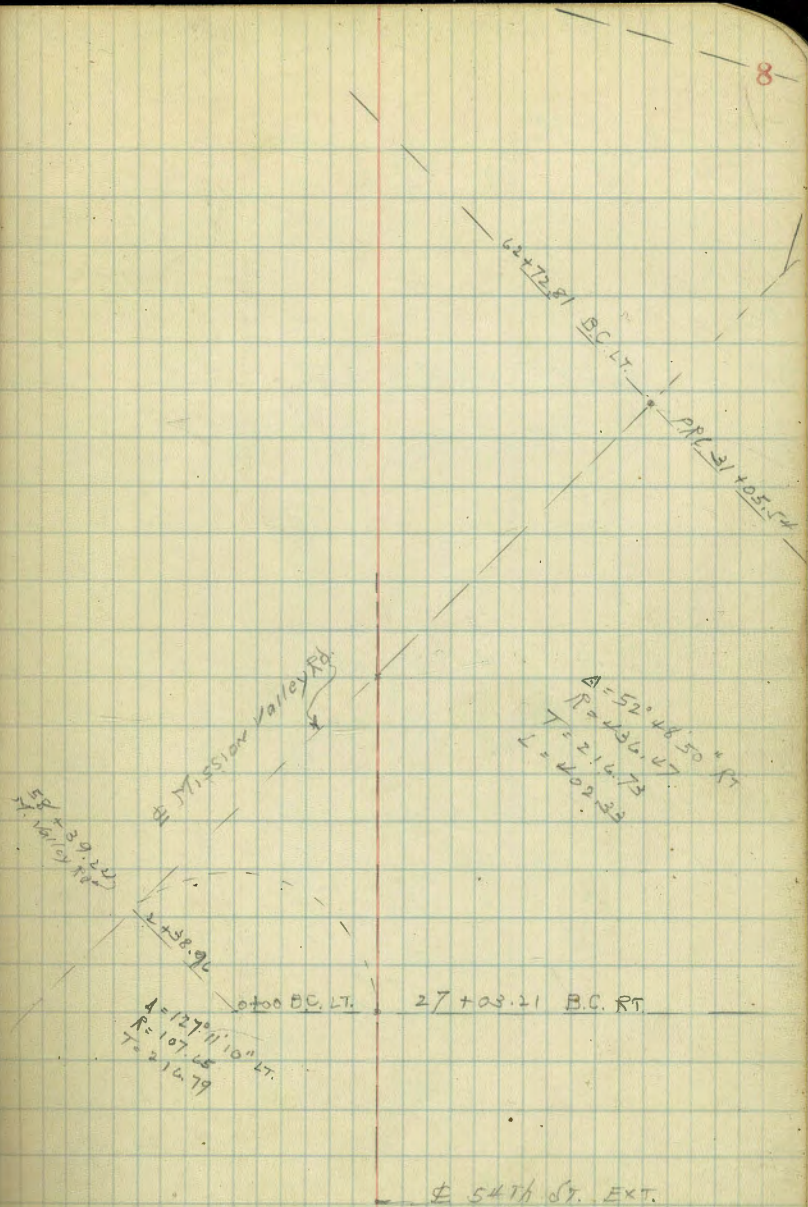
X

27

BM

26

25



+25

T.P. 12.50 430.07 0.69 417.51

29

T.P. 11.90 418.20 0.69 406.80

+75

+50

T.P. 12.71 406.99 0.00 394.28

28

394.88

$\frac{408.0}{22.1}$	$\frac{405.4}{24.4}$	$\frac{415.3}{148}$	$\frac{415.3}{11.8}$	$\frac{421.0}{9.1}$
$\frac{20}{20}$	$\frac{25}{25}$		$\frac{20}{20}$	$\frac{50}{50}$

$\frac{407.0}{11.2}$	$\frac{403.6}{14.6}$	$\frac{401.4}{16.8}$	$\frac{406.4}{11.8}$	$\frac{413.5}{11.7}$	$\frac{417.4}{0.8}$
$\frac{50}{50}$	$\frac{25}{25}$	$\frac{15}{15}$		$\frac{25}{25}$	$\frac{50}{50}$

$\frac{401.00}{60}$	$\frac{398.3}{8.7}$	$\frac{393.5}{13.5}$	$\frac{402.6}{X}$	$\frac{409.0}{+2.0}$	$\frac{414.2}{+7.2}$
$\frac{50}{50}$	$\frac{20}{20}$	$\frac{20}{20}$		$\frac{25}{25}$	$\frac{50}{50}$

$\frac{392.4}{12.6}$	$\frac{386.9}{20.1}$	$\frac{396.1}{16.9}$	$\frac{398.1}{8.9}$	$\frac{404.7}{2.3}$	$\frac{407.6}{+0.6}$
$\frac{50}{50}$	$\frac{35}{35}$	$\frac{25}{25}$		$\frac{25}{25}$	$\frac{50}{50}$

$\frac{388.5}{12.4}$	$\frac{378.3}{16.6}$	$\frac{383.3}{11.6}$	$\frac{390.2}{11.7}$	$\frac{395.7}{+0.8}$	$\frac{400.7}{+5.8}$
$\frac{60}{60}$	$\frac{40}{40}$	$\frac{25}{25}$		$\frac{25}{25}$	$\frac{50}{50}$

394.88

62 + 72.81 Mission Valley Rd.

1498-74

21 + 07.54 on hub

P.R.C.

440

440.07

443.74
-0.27

+75

J.P.

820

447.93

2.71

439.27

+50

+25

30

+75

J.P.

12.71

442.38

0.40

429.07

29 + 50

430.07

4

8

8

10

441.5
-0.2
441.3

441.3
-0.2
441.1

440.3
-7.0
433.3

439.7
-2.2
437.5

438.8
-9.1
429.7

447.93

440.3
-2.7
437.6

439.9
-2.5
437.4

438.6
-3.5
435.1

438.5
-3.9
434.6

437.0
-5.2
431.8

436.2
-0.2
436.0

436.9
-1.5
435.4

436.2
-0.2
436.0

435.1
-7.3
427.8

434.5
-7.9
426.6

430.0
-12.2
417.8

432.6
-9.8
422.8

432.4
-10.0
422.4

431.2
-11.2
420.0

430.8
-11.0
419.8

423.6
-18.8
404.8

423.6
-18.8
404.8

427.9
-14.5
413.4

427.2
-15.2
412.0

428.1
-16.3
411.8

442.38

419.5
-10.6
408.9

416.2
-13.9
402.3

418.9
-11.2
407.7

422.0
-8.1
413.9

424.0
-9.1
414.9

426.0
-11.1
414.9

430.07

Xsec at Lt. Wye 27+03.21 B.C. = 00
 To 2+38.96 E.L. = 58+39.24 Mission Valley Rd.

TP 12.77 405.94 0.97 399.17

+50

379.9
 $\frac{14.2}{70}$
 385.4
 $\frac{8.7}{30}$
 389.3
 $\frac{4.8}{15}$
 393.1
 $\frac{1.0}{25}$
 397.6
 $\frac{4.5}{25}$

+25

350.1
 $\frac{14.0}{70}$
 382.5
 $\frac{11.0}{30}$
 382.8
 $\frac{11.4}{15}$
 386.1
 $\frac{8.0}{20}$
 390.1
 $\frac{4.0}{25}$

377.6
 $\frac{12.5}{70}$
 376.0
 $\frac{15.1}{30}$
 375.3
 $\frac{18.8}{15}$
 378.6
 $\frac{15.5}{10}$
 379.2
 $\frac{14.9}{15}$
 386.0
 $\frac{6.1}{25}$

+75

373.6
 $\frac{20.5}{70}$
 373.0
 $\frac{21.1}{20}$
 369.7
 $\frac{24.4}{15}$
 372.7
 $\frac{21.2}{7}$
 370.5
 $\frac{17.0}{170}$
 381.7
 $\frac{12.4}{15}$
 391.0
 $\frac{9.1}{25}$

+50

370.6
 $\frac{23.5}{70}$
 369.5
 $\frac{24.6}{45}$
 366.9
 $\frac{27.2}{35}$
 369.0
 $\frac{25.1}{30}$
 375.7
 $\frac{18.4}{15}$
 380.5
 $\frac{13.6}{13.6}$
 385.0
 $\frac{9.1}{15}$
 388.5
 $\frac{5.6}{40}$
 391.1
 $\frac{5.0}{25}$

0+00 see p 7

B.M. old Hub 10.99 394.14

383.15 27+12.90
 old B.C.
 1402-70

394.14
 $\frac{7}{7}$

9.9 394.04 396.3 = 58 + 50 5.0 1498-72

2 + 38.96 EC

2

+ 75

405.94

$\frac{379.9}{20.0}$	$\frac{388.1}{17.8}$	$\frac{395.4}{10.5}$	$\frac{401.5}{4.4}$	$\frac{405.5}{0.4}$
$\frac{380.1}{25.8}$	$\frac{389.6}{14.0}$	$\frac{396.6}{9.3}$	$\frac{401.8}{4.1}$	$\frac{404.9}{1.0}$
$\frac{381.7}{24.2}$	$\frac{390.2}{15.7}$	$\frac{394.6}{11.3}$	$\frac{399.1}{6.8}$	$\frac{402.4}{3.5}$

405.94

12-21-36 Adams Ave B. M. Levels

miller
walker

see F. B. 1296-30. B.M.s.

BM. B.P.				✓ 370.87	S.E. 39 th + Adams
BM. B.P.	5.40	394.65		✓ 389.25	S.W. 34 th + Adams
T.P. Hydt.	3.04	396.50	1.19	✓ 393.46	S.E. Hawley St + Adams
T.P. B.M. B.P.			3.94	✓ 392.56	S.E. Adams + Mansfield
				= 392.78	

BM. B.P.	7.18	391.30		✓ 384.12	
T.P.	3.62	391.81	3.11	388.19	
B.M. B.P.			3.10	✓ 388.71 = 388.36	

N.W. 34th St. + Meade Ave F.B. 1296-33

S.E. 34th St + Monroe Ave

T.P.	5.70	393.32	4.19	387.62	
T.P.	5.45	394.53	4.24	389.08	
T.P. B.M. B.P.	5.40	394.93	5.00	✓ 389.53 = 389.25	

S.W. 34th St. + Adams Ave.

NEW T.P. B.M.	3.04	396.78	1.19	✓ 393.74	
T.P. B.M. B.P.	3.61	396.45	3.94	✓ 392.84 = 392.78	
T.P.	4.07	395.20	5.32	391.13	
T.P. B.M. B.P.	2.36	392.48	5.08	✓ 390.12 = 390.07	
T.P. B.M. B.P.	0.38	386.23	6.63	✓ 385.85 = 385.78	
T.P.	2.14	377.18	11.19	375.04	
T.P. B.M. B.P.	0.63	371.53	6.28	✓ 370.90 = 370.87	
T.P.	1.22	359.75	13.00	358.53	
B.M. C.T.P.			6.65	✓ 353.10	

Fire Hydt S.E. Hawley + Adams Ave

S.E. Mansfield + Adams Ave

S.E. Wilson + Adams Ave

S.E. Cherokee + Adams Ave.

S.E. 39th St. + Adams Ave.

S. 10' Line Adams Ave + W. 6' Line of Terrace Drive.

		359.75			
T.P.	8.44	367.59	0.60	359.15	
T.P. B.M. C.T.	2.62	361.12	9.09	✓358.50	C.T.L.P. in walk. S.E. L. Pt. Edgeware Road. + Adams Ave.
T.P. B.M. C.T.	11.25	368.69	3.68	✓357.44	C.T.L.P. in walk S.E. L. Pt. Biona Road. + Adams Ave.
^{New} T.P. B.M. B.P.	6.03	365.92	8.80	✓359.89	N.W. Biona Drive + Madison Ave
T.P.	3.15	365.05	4.02	361.90	
^{New} T.P. B.M. B.P.	4.70	363.69	6.06	✓358.99	S.W. Copeland St + Palace Place
T.P.	7.63	368.29	3.03	360.66	
B.M. B.P.			3.86	✓364.43 = 364.47	N.W. Copeland. + Meade Sts
B.M. B.P.	4.20	368.67		364.47	" " " "
T.P. B.M. B.P.	6.09	369.04	5.72	✓362.95 = $\frac{369.76}{6.76} - 363.09$	(State Highway Elev. U.S.G.S. Datum S.W. El. Cajon + Copeland,
T.P. B.M. B.P.	3.77	367.33	5.48	✓363.56 = 363.56	S.W. El Cajon + Van Dyke St.
T.P. B.M. B.P.	5.50	366.51	6.32	✓361.01 = 361.03	N.W. Orange Ave + Van Dyke.
T.P.	2.52	365.06	3.97	362.54	
T.P. B.M. B.P.	5.13	363.40	6.79	✓358.27 = 358.25	N.W. Univ. Ave + Van Dyke St.
U.S.G.S. B.M. Standard. Plate			1.34	✓362.06 ← city datum	Cor. Bank. Building N.W. Cor. University + Van Dyke.
				$\frac{6.12}{368.18}$ U.S.G.S. Datum = 368.346	

54th St. Culvert

57000
515504
Northern
1-19-07

27

E 54th

16

Culv. 4+70

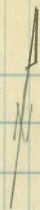
RT

4+70

4+70

4+43	14.20	275.80	359.60	ground el.
57' LT		+2.0	375.8	
35' LT		7.7	366.1	
20' LT		14.0	359.8	
2'		21.0	357.8	
20' RT		28.2	345.6	
40' RT		35.0	338.8	
60' RT		40.2	333.4	
75' RT		45.4	328.4	
95' RT		47.4	326.4	
100' RT		49.8	326.0	

900

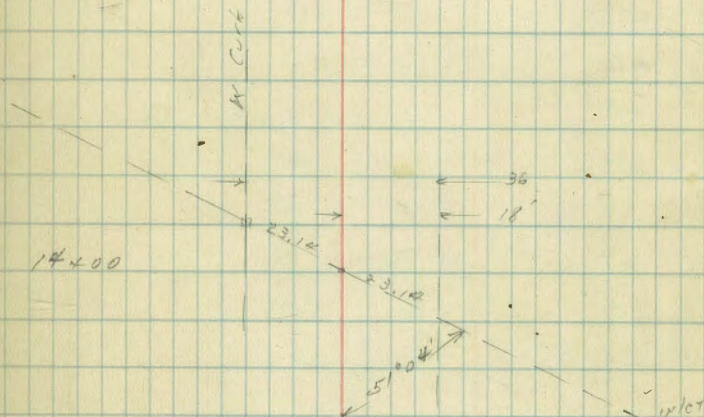


54th St. Culv.
Sta. 14+00

St.	Dist.	HT.	LT.
86.	14+71.84	6.80	278.80
			207.0
			Stub
Σ 54th = 14+00		10.1	263.7
23.14 RT		9.4	264.6
50 RT		7.1	266.7
75 RT		7.4	266.4
100 RT		6.4	267.4
124 RT = Top Slope inlet		5.8	268.0
150 RT		4.5	269.3
177 RT		2.8	271.0
180 edge crest		4.3	269.5
190 E		4.4	269.7
23.14 LT = W cb		10.05	263.7
50 LT		11.3	264.5
75 LT		12.8	261.0
100 LT		13.8	260.0
108 LT		13.9	259.9
114 LT		11.9	261.9
132 LT = outlet		12.4	261.6

LT.

RT.



See F.B. 1575/79.

Ground Levels over
 Ex. Sewer. 13+67 54TH ST.

LT.

RT.

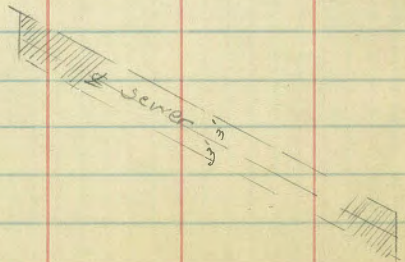
18

BC 14+71.82 519 - 272.19 267.0 STUB D.M.

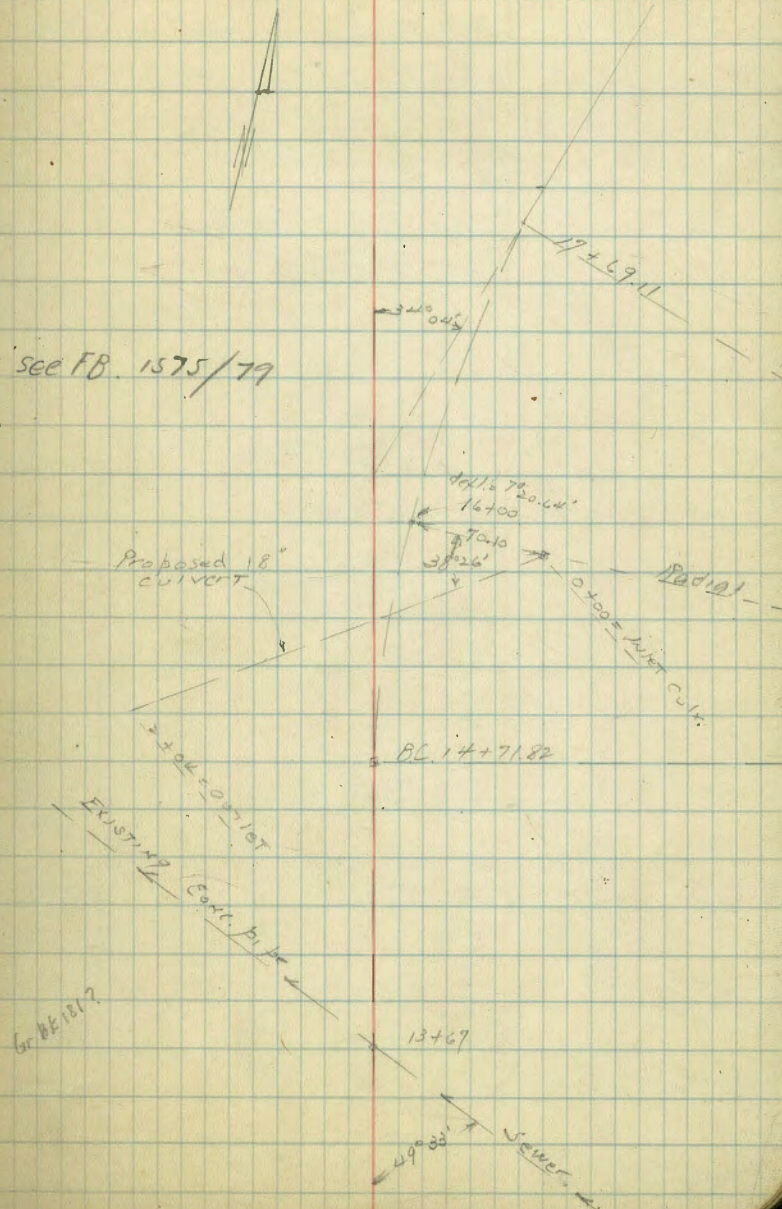
Φ 54TH - 13+67	8.6
45 RT	7.8
55 RT	6.1
75 RT	3.9
100 RT	3.2
125 RT	3.0
20 LT	10.2
50 LT	8.5
75 LT	8.4
100 LT	9.9
144 LT	10.2

Ex. sewer approx. 5' deep

CONST. REIN. CONC. SLAB OVER EX. SEWER
 MIGHT BE O.K.



see FB. 1575/79



Gr. BE 101?

13+67

49° 00'

547557.
Prop. Culv. 18" pipe
Sta. 12+00

B.C. inlet 12.98 279.98 267.0 556
T.P. 12.68 292.39 0.27 279.71

0+00 = inlet Culv.

0+07

0+30

+46

0+50

0+62

0+73

T.P. 0.72 280.43 12.08 279.71

0+83

0+94

+96

17

Culvert

17

19

292.39 = H.I.

$$\begin{array}{r} 290.0 \\ 2.4 \\ \hline 292.4 \end{array}$$

$$\begin{array}{r} 286.4 \\ 0.23 \\ \hline 286.63 \end{array}$$

$$\begin{array}{r} 285.0 \\ 2.4 \\ \hline 287.4 \end{array}$$

$$\begin{array}{r} 291.1 \\ 1.3 \\ \hline 292.4 \end{array}$$

$$\begin{array}{r} 289.7 \\ 2.7 \\ \hline 292.4 \end{array}$$

$$\begin{array}{r} 284.6 \\ 7.8 \\ \hline 292.4 \end{array}$$

285.8

$$\begin{array}{r} 285.0 \\ 0.8 \\ \hline 285.8 \end{array}$$

$$\begin{array}{r} 285.0 \\ 7.4 \\ \hline 292.4 \end{array}$$

$$\begin{array}{r} 280.4 \\ 12.0 \\ \hline 292.4 \end{array}$$

279.9

$$\begin{array}{r} 278.4 \\ 1.5 \\ \hline 279.9 \end{array}$$

$$\begin{array}{r} 278.4 \\ 14.0 \text{ ditch} \\ \hline 292.4 \end{array}$$

$$\begin{array}{r} 279.4 \\ 13.0 \\ \hline 292.4 \end{array}$$

277.6

$$\begin{array}{r} 277.6 \\ 14.8 \text{ ditch} \\ \hline 292.4 \end{array}$$

280.7

$$\begin{array}{r} 280.7 \\ 11.7 \\ \hline 292.4 \end{array}$$

277.9

$$\begin{array}{r} 277.9 \\ 14.5 \\ \hline 292.4 \end{array}$$

280.43 = H.I.

274.4

$$\begin{array}{r} 274.4 \\ 6.0 \\ \hline 280.4 \end{array}$$

$$\begin{array}{r} 274.4 \\ 6.2 \text{ ditch} \\ \hline 280.6 \end{array}$$

$$\begin{array}{r} 274.0 \\ 6.4 \\ \hline 280.4 \end{array}$$

273.3

$$\begin{array}{r} 273.3 \\ 7.1 \\ \hline 280.4 \end{array}$$

$$\begin{array}{r} 273.0 \\ 7.4 \text{ ditch} \\ \hline 280.4 \end{array}$$

$$\begin{array}{r} 274.0 \\ 6.4 \\ \hline 280.4 \end{array}$$

275.1

$$\begin{array}{r} 275.1 \\ 5.3 \\ \hline 280.4 \end{array}$$

280.48

1 + 14

1 + 30

1 + 55

T.P. 1.50 269.80¹ 12.10 268.00

1 + 64

1 + 88

2 + 00

2 + 04 = Out for Cult.

17

← E
← Cult.

RT

20

280.43 = H.I.

274.5
5.9

267.1
1.3
5

266.1 266.6
14.3 13.8
5

= ditch

264.7
11.7

269.80¹ = H.I.

260.8
9.0

260.3
9.5

258.5

11.3 = Main creek

260.9
8.9

6-19-37
Miller
Walker
Bless

Survey Alley BIK. 60 Park Villas
Complaint of James E. Resline 3320 Grimm St.
of wall in Alley

3+00 offset in wall on W. wall to S. 1.3' in Alley

4.1 in wall { S. End. conc. wall on W. 2.95 in Alley

2+94.2 = W. End. Brick wall on W. 2.95 in Alley

2+79 Brick wall on W. = 2.95 in Alley

2+79 ϕ Alley = W. edge Boundary St. Paymt

on W.

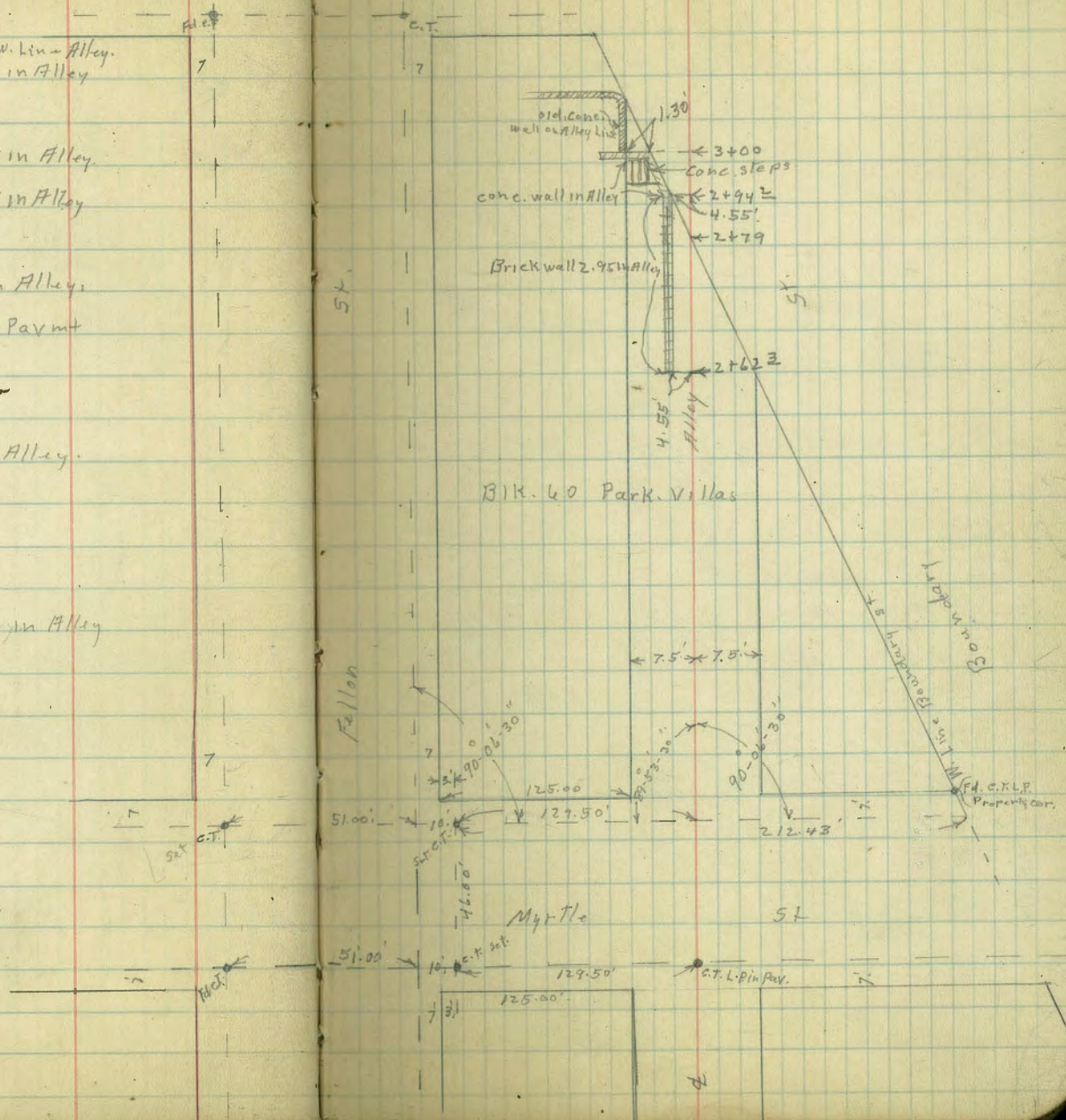
2+62.2 = S. End. Brick wall on W. 2.95 in Alley

1+00 = E. End. Brick wall on W. 0.2 in Alley

0+84 N. End Fence 0.1 in Alley

0+00 = N. Line Myrtle

Indexed
C.S.K.

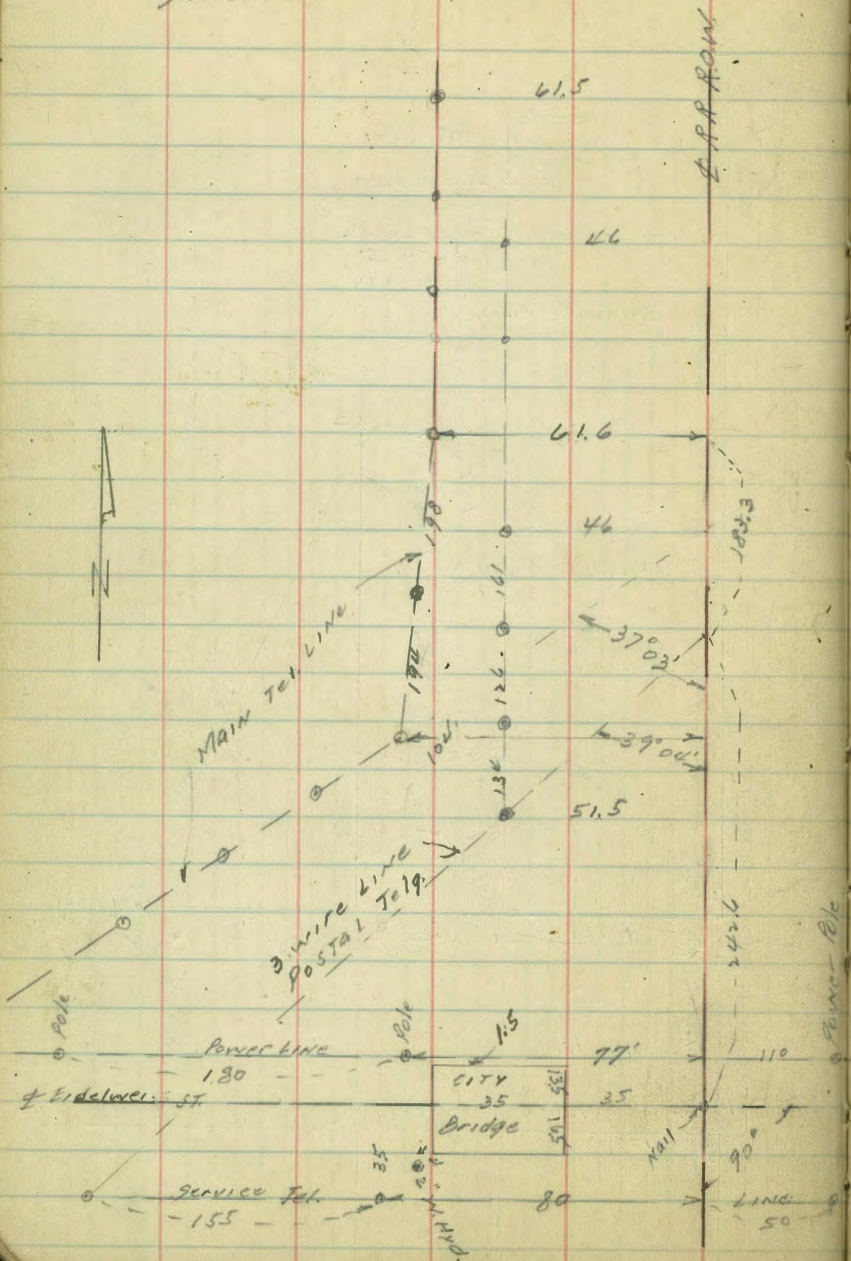


INDEXED
C.S. 116.

LOCATION of Tel. Lines etc
at Edelweiss & Santa Fe R.R.
Gorontalo

Moore
3-30-39.

22



Indexed
CS.KI

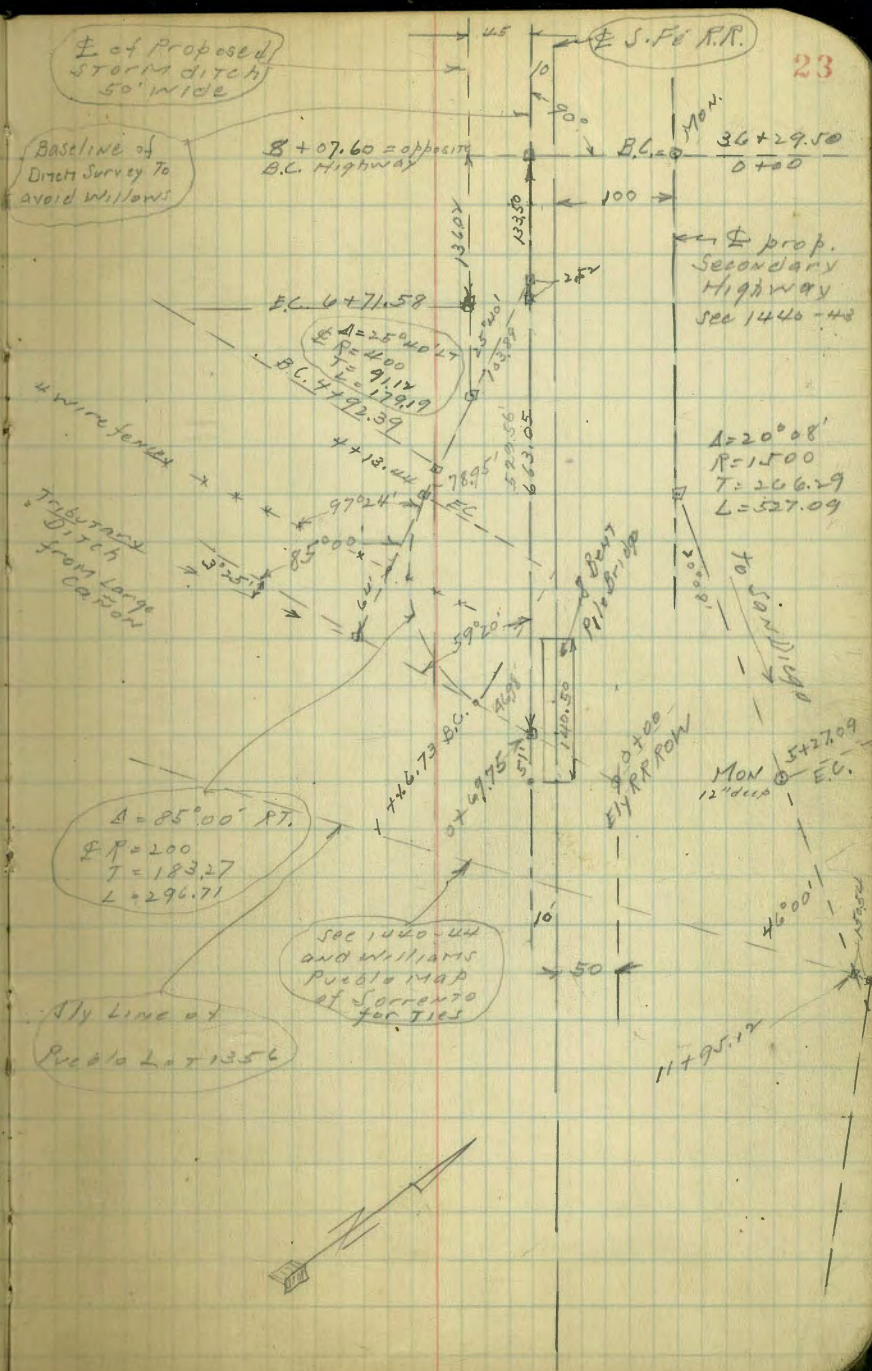
14000
4-30-37

Survey for R.O.W. of Proposed
Storm Ditch, S.Ely line of
Baker Property & S.F. RR Sta. 1246+58.70
to N'wly Towards Del Mar
see F.B. 1440 & F.B. #P = Edelweiss Nwly
to City Line, Proposed Highway Survey
for Property Ties.

width of Proposed ditch 50'
R.R. giving 20' of wly R.R. R.O.W.
and private property 30'

Santo Fe RR Sta. S.Ely end of Bridge = 1246+58.70

Location of Sycamore trees	Indexed CS.KI		
+93 Group 5	3-3' 2-1'	100' LT	E RR Track
+745 Group 5	1-6' 2-3' 1-7'	115' LT	"
+55	1 - 18" diam	125' LT	"
+45	1 - 24" diam.	125' LT	"
+30	Group of 2 3' diam.	130' LT	"
+20	Group of 2	130' LT	"
	1-1' 1-4'		
26+10	Group of 4	130' LT	"
26+08	1 3' diam.	110' LT	"
+64	1 - 5' diam	106' LT	"
25+42	Group of 4	146' LT	"
	1-5' 3-2'		
11440	Sycamore 5' diam.	55' LT	E RR Track
8+07.60 = Storm Ditch Sta.			



5-3-37
MillerAlley BIK 46 Resub. BIK H+I Teratta
Orange to El Cajon bet. 33rd & Felton

See F.B. 1497-26.

Rc X. Sec. 15' wide

S.W. 33rd &
El Cajonindexed
c.s.N

378.80

25

BM. 5.55 379.80 374.25

0+00 = S. Line El Cajon Blvd.

0+50 S.

W 5.2 374.6

φ 5.3 374.5

E 5.3 374.5

0+68^E = N. End cnt. walk. on W. 0.65 in Alley

E 5.5 374.3

φ 5.5 374.3

+ 6.85 N. End E. Edge cnt. walk 5.57 374.23

0+78 = N. End 3. garages on E

E-10.2' floor 5.6 374.2

E 5.7 373.9

φ 5.7 374.1

+ 6.9 = cnt. walk. E. edge 5.52 374.25

0+89^E = S. End. above cnt. walk. on 0.5 in Alley.
S. End walk.

0.5 E of W. line = E. Side 5.47 374.33

φ 5.6 374.2

E 5.6 374.2

0+99 = φ 2. walls. 0.4 in Alley on W.

7.1 W. of φ = φ walls E. End. 5.46 374.39

1+04 = S. end 3. garages on E.

TP. 4.55 378.80 5.55 374.25

E-10.2 = ground 4.9 373.9

E 4.9 373.9

φ
W

4.8 374.0

4.7 374.1

1+09

W-30. 5.2 373.6

W-2'. 5.3 373.5

W. 4.9 373.9

φ 4.7 374.1

E 4.7 374.1

+3 5.7 373.7

+30 4.9 373.9

1+40

E-25' 5.1 373.7

E-2'. 5.1 373.7

E 5.0 373.8

φ 5.0 373.8

W. 4.9 373.9

+3 5.4 373.9

1+60

W-3 5.4 373.9

W 5.3 373.5

φ 5.2 373.6

E 5.0 373.8

E+25 5.0 373.8

378.80

1+64 garage on w. cnt. floor 8. Back

26

W-8. = floor.	5.22	373.58
---------------	------	--------

1+72

E-3 = W. side House

E	5.1	372.2
♀	5.1	372.0
W	5.5	373.3
+3	5.6	373.2

2+00

W-30	6.1	372.7
W-3	6.0	372.8
-W	5.4	373.4
♀	5.3	373.5
E	4.9	372.9
E+5	5.1	373.7
E+15	4.9	372.9

2+30

E-10	4.9	373.9
E	5.1	373.7
♀	5.2	373.6
W	5.3	373.5
+2	5.8	373.0
+30	5.9	372.9

Moore
4-13-47

Cross Sec. of Bessemer St. 60' wide
10' curbs
10' '1/2'

Harbor View Dr. to Talbot.

SW
Top Curb 6.59 113.56 106.97
Bessemer
Harbor View
500 Gr. Book

0-10 = curb line

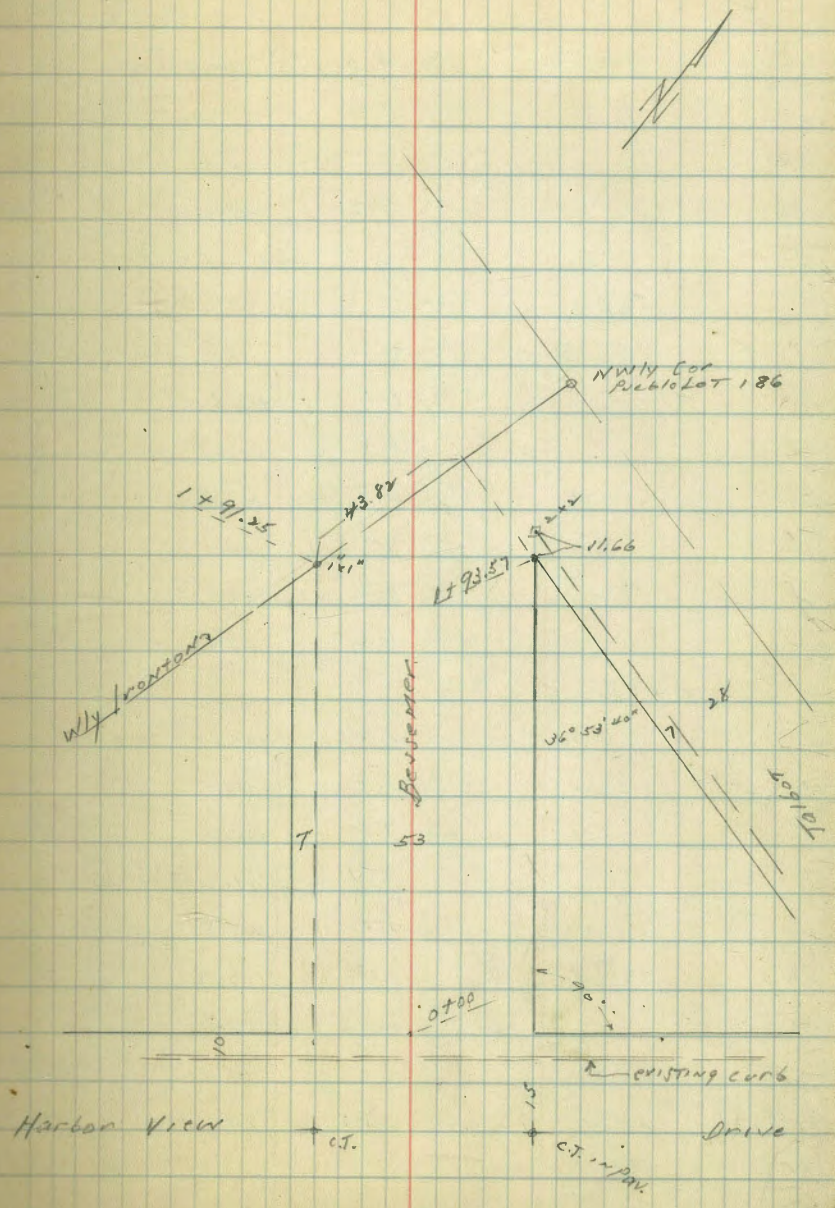
S	par. in gut.	7.20	106.36
cb		8.12	105.44
1/4		8.94	104.60
c		9.74	103.82
1/4		10.54	103.00
cb		11.37	102.19
N		12.39	101.19

0-10

S	Top curb	6.57	106.99
cb		7.41	106.15
1/4		8.24	105.32
c		9.03	104.53
1/4		9.90	103.66
cb		10.69	102.87
N		11.50	102.06 101.95

0+00

N		11.44	102.2
cb		10.1	103.5



113.56

1/4	9.6	104.0
c	8.0	105.0
1/4	7.7	105.9
cb	7.4	105.2
S	6.5	102.1

0+05

S	2.2	111.4
cb	3.5	110.1
1/4	5.8	107.8
c	7.7	105.9
1/4	9.2	104.4
cb	9.7	103.9
N	11.0	102.6

0+25

-S	9.1	104.5
N	8.2	105.4
cb	7.2	106.4
1/4	7.2	106.4
c	5.4	108.2
1/4	3.8	109.8
cb	1.4	112.2
S	10.5	114.1

T.P.	1309	126.60	0.05	113.51
------	------	--------	------	--------

126.60

28

0+50

S	9.1	117.5
cb	10.0	116.6
1/4	12.5	114.1
c	14.9	111.7
1/4	16.5	110.1
cb	16.8	109.8
N	18.2	108.4
+10	20.4	106.2

0+75

-10	19.2	107.4
N	16.7	109.9
cb	14.8	111.8
1/4	12.6	114.0
c	10.9	115.7
1/4	9.3	117.3
cb	7.6	119.0
S	6.2	120.4

0+90

S	5.0	121.6
cb	5.9	120.7
1/4	7.0	119.6
c	8.9	117.7
1/4	11.3	115.3
cb	14.1	112.5
N	17.0	109.6
+10	20.3	106.3

1+10

- 10		26.8	99.8
N		21.3	105.3
cb		16.5	110.1
1/2		14.0	113.6
c		10.8	115.8
1/4		6.9	119.7
cb		4.7	124.9
S		2.6	124.0
	1+28		
S		2.5	124.1
cb		5.8	120.8
1/2		9.9	116.7
c		12.5	113.1
1/4		18.0	108.6
cb		23.2	103.4
N		27.2	99.4
+15		33.2	93.4

1+63

- 15		40.5	86.1
N		35.5	91.1
cb		31.8	94.8
1/2		27.1	99.5
c		22.4	104.2
1/4		16.5	110.1
cb		12.5	114.1

S		9.7	116.9	
T.P.	1.27	115.02	12.82	113.76
T.P.	0.93	106.07	9.94	105.09
				ON STUB 1+91.25
				1+91.25 to 1+93.57
S			+1.5	107.5
cb			2.0	104.0
1/2			5.5	100.5
c			9.8	96.2
1/4			13.0	93.0
cb			16.9	89.1
N			24.4	81.6
+15			25.4	80.6
				Sly Talbot & Pueblo Line to 1+91.25
S.L. Talbot		24.0		72.0
+5		17.1		88.9
+10		15.8		90.2
+20		11.4		94.4
+30		7.4		98.4
+43.82		0.93		105.09
				ON STUB
S.L. Bessemer & Pueblo Line		+2.8		108.8
T.P.	0.89	93.9945	12.93	93.10 09
T.P.	0.92	87.20 11	12.74	81.27 10
T.P.	0.45	69.60 59	13.05	69.15 14
T.P.	0.54	57.20 19	12.94	56.66
check			5.41	51.79 28

 NW BR
 Talbot
 Engstrom
 51.77

Moore
5-13-37

indexed
C.S.K.

8.42

30

Cross Sec. Whiting Ct. 10' wide.

Ocean walk to Bay side walk

B.M. B.P.	2.35	942	7.09
T.P.	3.77	842	4.78
			4.65

York Ct. +
Sea wall
Ct. 0-3
Whiting Ct.

0+64	N	SAND	3.6	4.8
	C	Bd walk	3.40	5.02
	S	SAND	3.50	5.02

00 = Ely edge cent. ocean walk

S		3.76	4.66
C		3.75	4.67
N		3.77	4.65

0+65	S	SAND	4.6	3.8
	C	Bd walk	3.40	5.02
	N	SAND	3.6	4.8

0+14

N	sand	4.1	4.3
C	"	4.0	4.4
S	"	4.0	4.4

0+93 WL Strandway	N	sand	4.5	3.9
	C	Bd walk	3.91	4.51
	C	SAND	4.5	3.9
	S	"	4.5	3.9

0+22

S	"	4.0	4.4
C	"	3.9	4.5
N	"	3.5	4.9

00 = EL "	S	SAND	4.7	3.7
	C	Bd walk	4.50	3.92
	C	SAND	4.7	3.7
	N	"	4.8	3.6

→ Top of bot. step 8" wide 1.65 5.77

0+41

N	sand	3.7	4.7
C	on Bd walk	3.37	5.05
+4.6	cent walk 2.5 wide	3.38	5.04

0+25	N	sand	6.1	2.3
	C	Bd walk	5.63	1.79
	S	SAND	6.6	1.8

0+52

S + 0.4	cent walk 3.5 wide	3.41	8.01
C	Bd walk	3.17	5.25
N	" " 3.5 wide	3.15	5.24

0+76.5	S	SAND	8.1	0.3
	C	Bd walk	7.50	0.92

C + 2.7	CON walk 3' wide	7.60	0.82
	0 + 87.5		
N + 1.2	Bot. step corr. 3' wide	8.18	0.24
C	Bd walk	8.04	0.38
S	sand	8.4	00
	1 + 12		
S + 0.7	3.5 Bd walk	8.39	0.03
C	Bd. walk	8.39	0.03
N	sand	8.5	-0.1
	1 + 24		
N	sand	8.8	-0.4
C	Bd walk	8.6	-0.2
C + 4.4	3' wide Bd walk	8.57	-0.15
	1 + 37		
S + 0.5	4' wide " "	8.85	-0.43
C	Bd walk	8.87	-0.45
N	sand	9.8	-1.4
	1 + 40		
N	Sand	10.1	-1.2
C	Bd walk	9.07	-0.60
S	sand	10.0	-1.6
	2 + 00		
S	sand	9.9	-1.5
C	Bd walk	9.23	-0.81
N	sand	10.7	-1.8

2 + 13.36 = Wly Mission Blvd			
N	Bd walk	8.95	-0.43
C	"	8.95	-0.43
S	"	9.02	-0.60
2 + 23.8 = W. 6th Mission			
S	TOP curb	8.97	-0.55
C	"	8.96	-0.54
N	"	8.95	-0.53
T.P.	3.89	3.35	8.96 - 0.54
Ely Curb Mission			
N	Tot curb	4.03	-0.68
C	" "	4.03	-0.68
S	" "	4.02	-0.67
0 + 00 = E. Mission Blvd			
S	Bd walk + ^{wedge} corr walk	4.02	-0.67
C	"	3.96	-0.61
N	"	3.93	-0.58
0 + 09.5 E edge walk ^{corr}			
N	sand	4.5	-1.1
C	Bd walk	3.99	-0.64
S	on cement	4.02	-0.67
0 + 25			
S	Sand	5.1	-1.2
C	Bd walk	4.11	-0.76
N	sand	5.0	-1.3

0+47

N	Sand	4.8	-1.4
C	Bd walk	4.06	-0.71
S	1/2" " "	4.04	-0.69
S	Sand	4.9	-1.5

0+92

S	1/2" wide Bd walk	4.07	-0.72
C	Bd walk	4.10	-0.6
N	Sand	4.1	-0.7

1+25

N	Sand	4.1	-0.7
C	Bd walk	3.96	-0.61
S	1/2" " "	4.07	-0.67

1+31

N	Brick walk	4.15	-0.80
---	------------	------	-------

1+36

N	Sand	4.0	-0.70
C	Bd walk	4.04	-0.69
S	2' corr walk	4.04	-0.67

1+63.78

S	Sand	4.0	-0.6
C	Bd walk	4.07	-0.67
N	" "	4.01	-0.66

1+77.78 = wedge of 1/2" corr walk at Dayside walk

N		4.23	-0.88
S		4.28	-0.93

325

J.P.	9.94	9.40	-3.89	-0.54
check to 811.			2.32	7.08
				<u>7.08</u>
				200

5-25-37
Miller
Walker
Bliss

X Sec. F. St. at Glendale

80' wide
14' elev
13' 1/2

Indexed
c-s-k

157.68

33

BM.BP.	0.14	180.34	180.40	N.W. 25 th + F. Sts
T.P.	0.12	167.89	12.77	167.77
	0+00 = E. Line of 25 th St. (E. Line of Alley to N. 1+40 E. of E. Line of 25 th St. = " " " S.)			
N. el.		5.30	162.59	✓
G		5.80	162.09	
"		5.52	162.32	
±		5.59	162.30	
"		6.01	161.88	
G		6.58	161.31	
s. el.		6.17	161.72	
	1+90			
s. el.		12.89	155.50	
G		12.98	154.91	
"		12.30	155.59	
±		11.90	155.99	
"		11.92	155.97	
T.P.	0.97	157.68	11.18	156.71
G		2.00	155.68	
N. el.		1.37	156.37	
	2+30	26		
N. el.		6.43	151.25	✓
G		7.13	150.55	✓
"		6.77	150.91	✓
±		6.77	150.91	
"		7.20	150.48	
G		7.86	149.92	
s. el.		7.45	150.23	

Indexed c-s-k	2+40	26
s. el.	8.62	149.06
G	9.03	148.65
"	8.33	149.35
±	7.92	149.76
"	7.88	149.80
G	8.27	149.41
N. el.	7.54	150.14
	2+50	26
N. el.	8.16	149.57
G	8.88	148.80
"	8.58	149.10
±	8.53	149.15
"	9.04	148.64
G	9.66	148.02
s. el.	9.12	148.56
	2+60	26 = W. Line Glendale 60' wide - 10' elev 10' 1/2
s. el.	9.67	148.01
G	10.19	147.49
"	9.56	148.12
±	9.10	148.58
"	9.08	148.60
G	9.34	148.34
N. el.	8.63	149.05

157.68 ✓

W. el. Line Glendale

N. Line	cont. el	8.69	148.79
N. "	gutter.	9.42	148.76
N. el		9.89	148.09
"		9.39	148.29
£		9.46	148.22
"		9.90	147.78
G		10.60	147.08
S. el	in drive no el.		
	W. "y		
S. el		10.31	147.37
G		10.99	146.71
"		10.22	147.46
£		9.74	147.94
"		9.67	148.01
N. el Line		9.78	147.90
N. Line		9.37	148.31
	£		
N. Line		9.62	148.06
N. el Line		9.98	147.70
"		9.88	147.80
£ on N. H.		10.12	147.56
"		10.60	147.08
G		11.34	146.34
S. el		10.74	146.94

157.68 ✓

E. "y

34

S. el		11.03	146.65
G		11.76	145.92
"		11.06	146.62
£		10.56	147.12
"		10.38	147.30
N. el Line		10.30	147.38
N. Line		9.93	147.75
	E. el. Line		
N. Line	cont. el	9.83	147.85
"	" G	10.40	147.28
N. el. Line		10.73	146.95
"		10.98	146.70
£		11.20	146.48
"		11.54	146.14
G	catch basin grating	12.14	145.54
S. el		11.34	146.34
	0+00 = E. Line Glendale		
S. el	in drive no el		
G		11.87	145.81
"		11.17	146.51
£		10.67	147.01
"		10.48	147.20
G		10.53	147.15
N. el		9.73	147.95

157.68 ✓

0 + 10.2

N. cl	9.25	148.43
G	10.05	147.63
ly	10.05	147.63
£	10.18	147.50
ly	10.75	146.93
G	11.59	146.09
s. cl	11.18	146.50

0 + 20.2

s. cl	10.72	146.96
G	11.17	146.51
ly	10.15	147.53
£	9.53	148.15
ly	9.38	148.30
G	9.50	148.18
N. cl	8.80	148.88

0 + 30

N. cl	7.55	150.13
G	8.24	149.44
ly	8.16	149.52
£	8.25	149.43
ly	8.92	148.76
G	9.91	147.77
s. cl	9.53	148.15
T.P.	8.08	161.12 ✓
	4.64	153.04

161.12

0 + 20

35

s. cl	7.66	153.46
G	8.13	152.99
ly	7.12	154.00
£	6.44	154.68
ly	6.30	154.82
G	6.43	154.69
N. cl	5.86	155.26

1 + 10

N. cl	0.40	160.72
G	0.89	160.73
ly	1.01	160.11
£	1.09	160.03
ly	1.77	159.35
G	2.75	158.37
s. cl	2.35	158.77

T.P. 12.87 173.65 0.34 160.78

T.P. 8.41 186.95 1.11 172.54

E.H.K. B.M. N.W. 26th + F. 2.82 178.13 = 178.12

6-2-37
Miller
Walker
B. Liss

X See: City Police Station Site
Kettner to Pacific S. of Market
See Page 78. Re X. Seen

See F.B. 1531 - P. 47 for this B.M. 7
U.S. Coast & Geodetic
S.E. Pacific
11.905 + Market.

B.M. B.P. 2.79 14.69

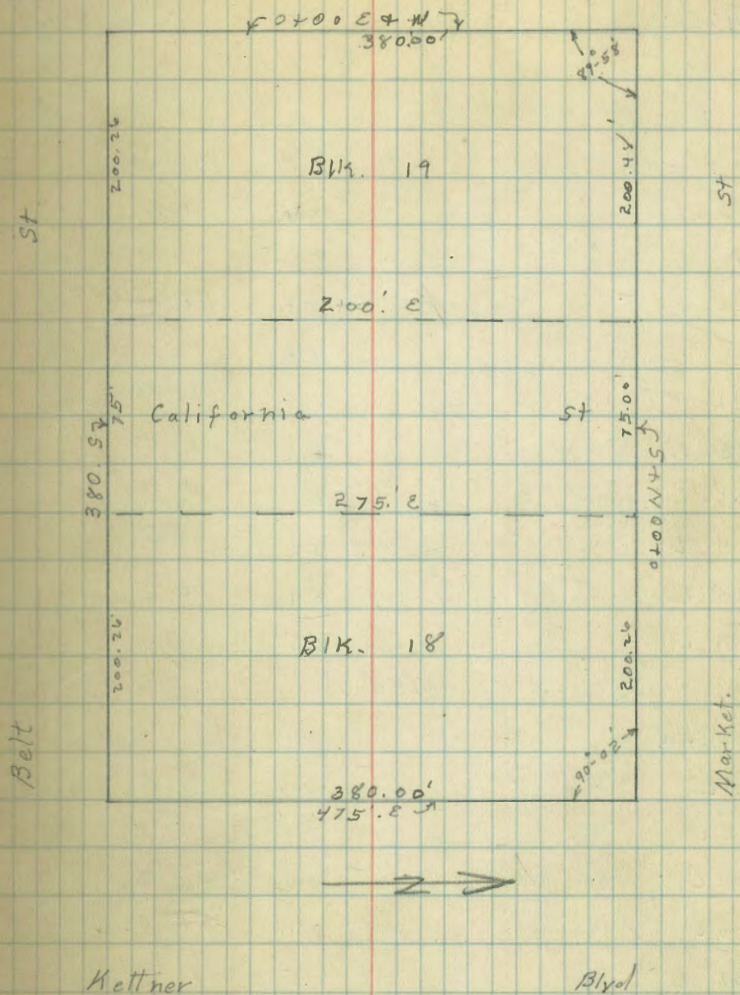
0+00 N+S = S. Line Market St.

0+00 E+W = E. Line Pacific	2.7	12.0		
50' E	3.1	11.6		
100' E	3.8	10.9		
150' E	4.2	10.5		
200' E = W. Line Calif	5.0	9.7		
237 ⁵ E = "	5.2	9.5		
275' E E " "	4.9	9.8		
325' E	4.8	9.9		
375' E	4.8	9.9		
425' E	4.4	10.3		
475' E = W. Line Kettner	4.5	10.2		
T.P.	8.74	18.55	4.88	9.81
		50' S.		
0+00 E+W	7.1	11.5		
0+50 E	7.1	11.5		
1+00 E	7.8	10.8		
1+50 E	8.1	10.5		
2+00 E	8.5	10.1		
2+37 ⁵ E	8.2	10.4		
2+75 E	8.6	10.0		
3+25 E	8.9	9.7		
3+75 E	9.8	8.8		
4+25 E	9.8	8.8		

Indexed
C.S.K.
Pacific

Blvd

36



18.55

0+50 S. 20h

475' E	9.0	9.6
1+00 S		
0+00 E+W	7.0	11.6
50' E	7.6	11.0
100' E	8.0	10.6
150' E	8.1	10.5
200' E	8.3	10.3
237 ⁵ E	7.7	10.9
275' E	8.6	10.0
325' E	8.7	9.9
375' E	8.7	9.9
425' E	8.4	10.2
475' E	8.5	10.1

150' S

0+00 E+W	6.9	11.7
50' E	7.6	11.0
100' E	7.9	10.7
150' E	8.4	10.2
200' E	8.1	10.5
237 ⁵ E	7.5	11.1
275' E	8.1	10.5
325' E	8.3	10.3
375' E	8.4	10.2
425' E	8.4	10.2
475' E	8.5	10.1

18.55

200' S.

37

0+00 E+W	6.8	11.8
50' E	7.1	11.5
100' E	7.1	11.5
150' E	7.9	10.7
200' E	8.1	10.5
237 ⁵ E	7.3	11.3
275' E	8.5	10.1
325' E	8.5	10.1
375' E	7.4	11.0
425' E	7.8	10.8
475' E	8.1	10.5

265' S

100' E	7.1	11.5
--------	-----	------

250' S

0+00 E+W	6.3	12.3
50' E	7.0	11.6
55' E	6.4	12.2
100' E	6.3	12.3
140' E	5.6	13.0
145' E	7.2	11.4
200' E	8.1	10.5
237 ⁵ E	7.2	11.4
275' E	8.2	10.4
325' E	7.8	10.8
375' E	7.7	10.9
425' E	7.8	10.8
475' E	7.9	10.7

18.55
300' S

0+00 E+W	5.1	13.5
50' E	5.6	13.0
100' E	5.5	13.1
150' E	5.4	13.2
200' E + 294' S	7.1	11.5
200' E	5.0	13.6
208' E	7.0	11.6
237' E	6.8	11.8
275' E	6.8	11.8
325' E	7.5	11.1
375' E	7.8	10.8
425' E	7.8	10.8
475' E	7.6	11.0

350' S

0+00 E+W	4.0	14.6
50' E	5.1	13.5
100' E	4.8	13.8
150' E	4.6	14.0
200' E	6.0	12.6
237' E	6.4	12.2
275' E	6.6	12.0
325' E	7.7	10.9
375' E	7.4	11.2
425' E	7.2	11.4
475' E	6.9	11.7

18.55
380' S

0+00 E+W	3.7	14.9
50' E	5.0	13.6
100' E	4.6	14.0
150' E	4.1	14.5
190' E	4.9	13.7
200' E	4.5	14.1
230' E	5.0	13.6
237' E	6.2	12.4
275' E	6.5	12.1
325' E	6.6	12.0
375' E	7.4	11.2
425' E	6.8	11.8
475' E	7.2	11.4

T.P. 4.72 15.34 7.93 10.62

orig BM 3.44 11.90

38

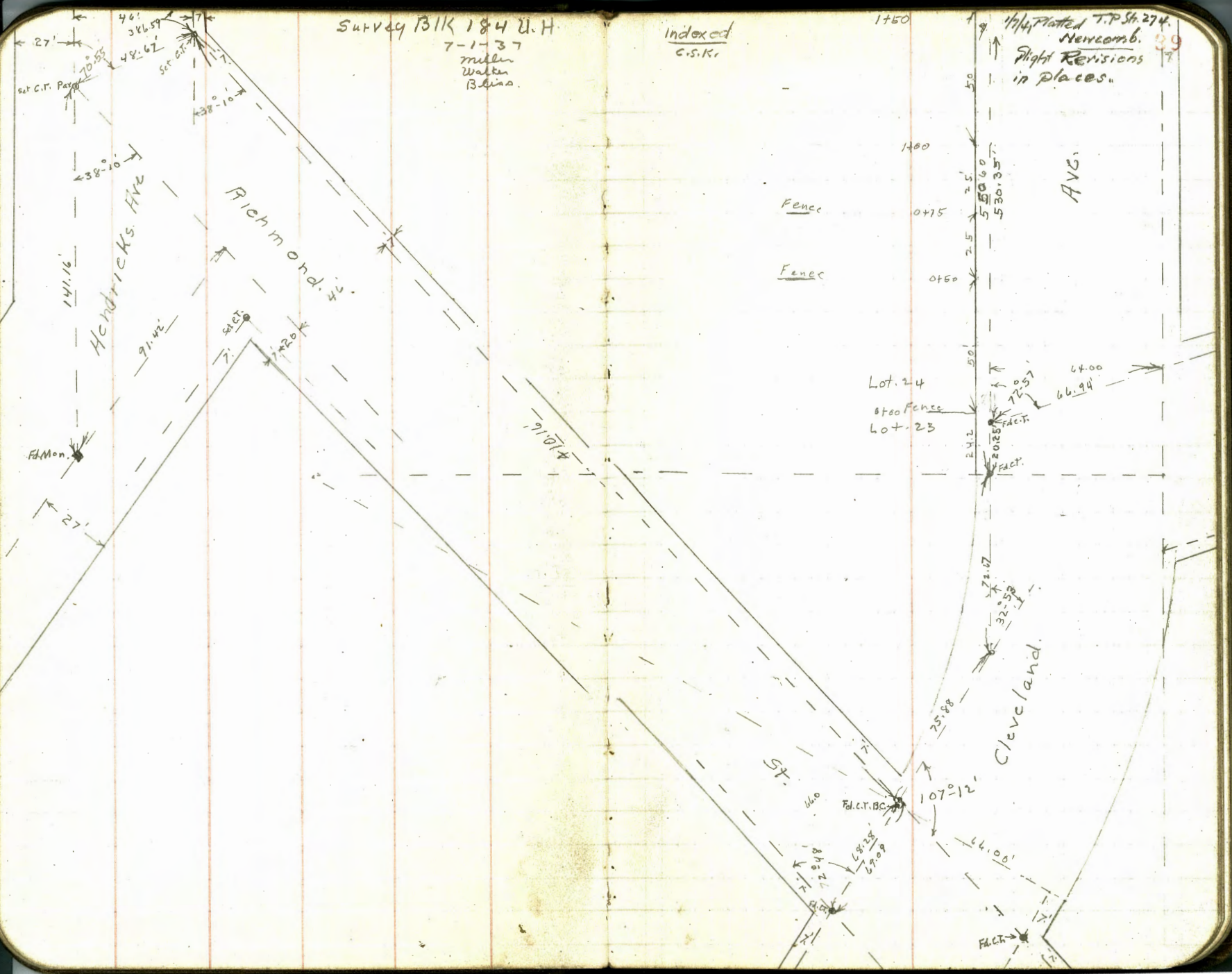
Survey Blk 184 U.H.

7-1-37
Miller
Walker
Blinn.

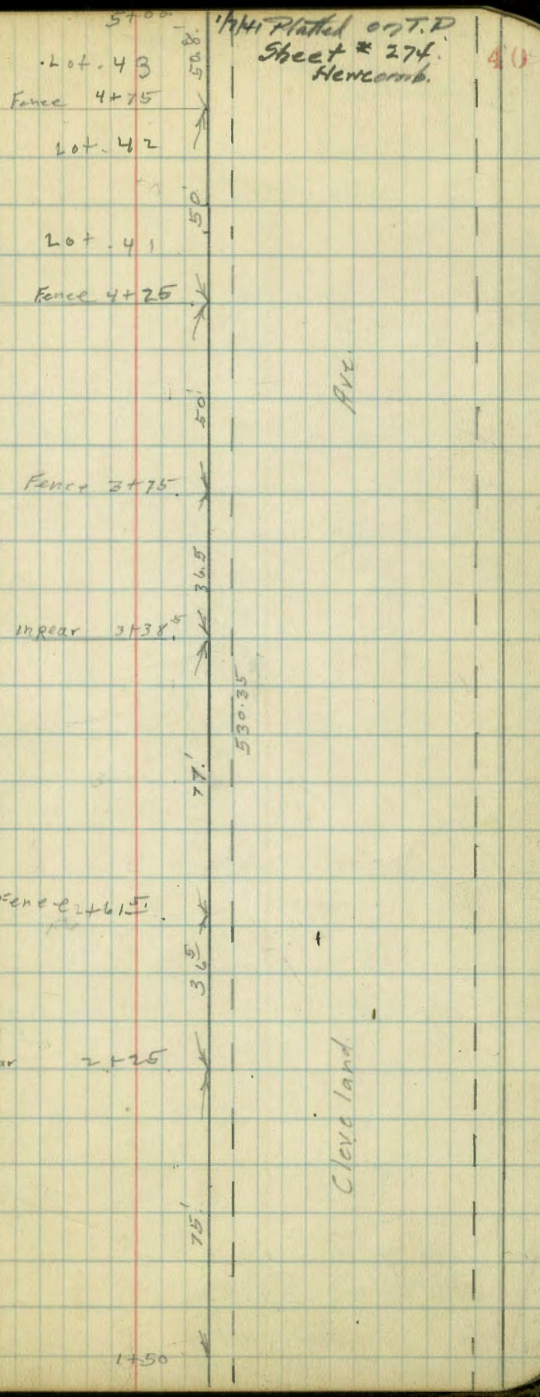
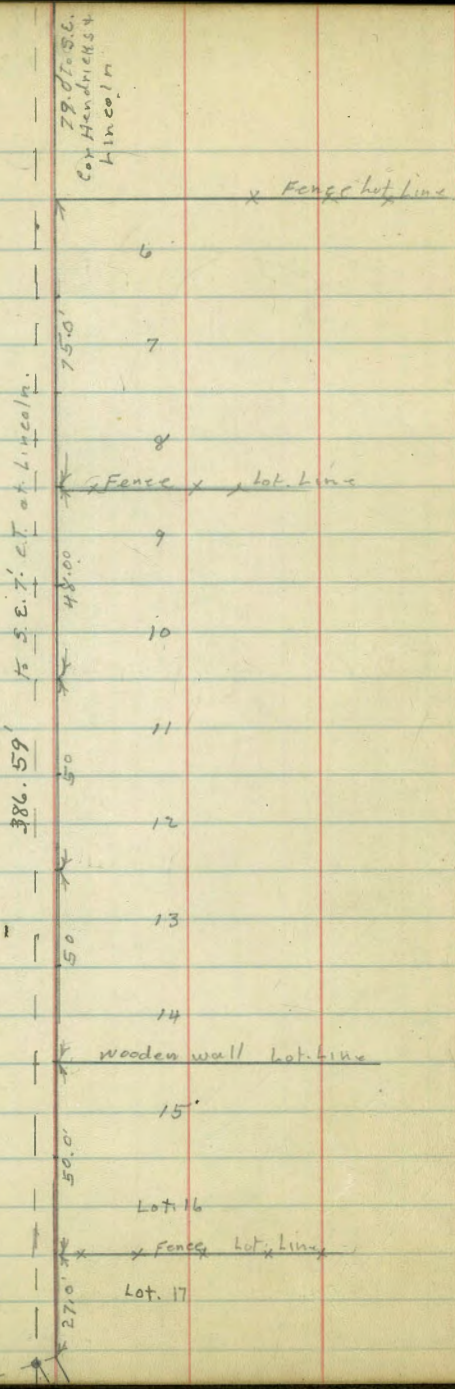
Indexed
C.S.K.

1750

1/4 Platted T.P. St. 274.
Newcomb.
Slight Revisions
in places.



Hendricks.



1-7-41 Platted on
Sheet 274
Newcomb. 41

W 1/2 Lin. Hendricks St

Hendricks

Lincoln

AVG

Clinch

Cleveland

East of Cleveland Produced from S.

East of 1/2-7/8 Lin. Normal.



Indexed

C.S.K.

Map Plotted on Tie Pt
Sheet 274.
at present

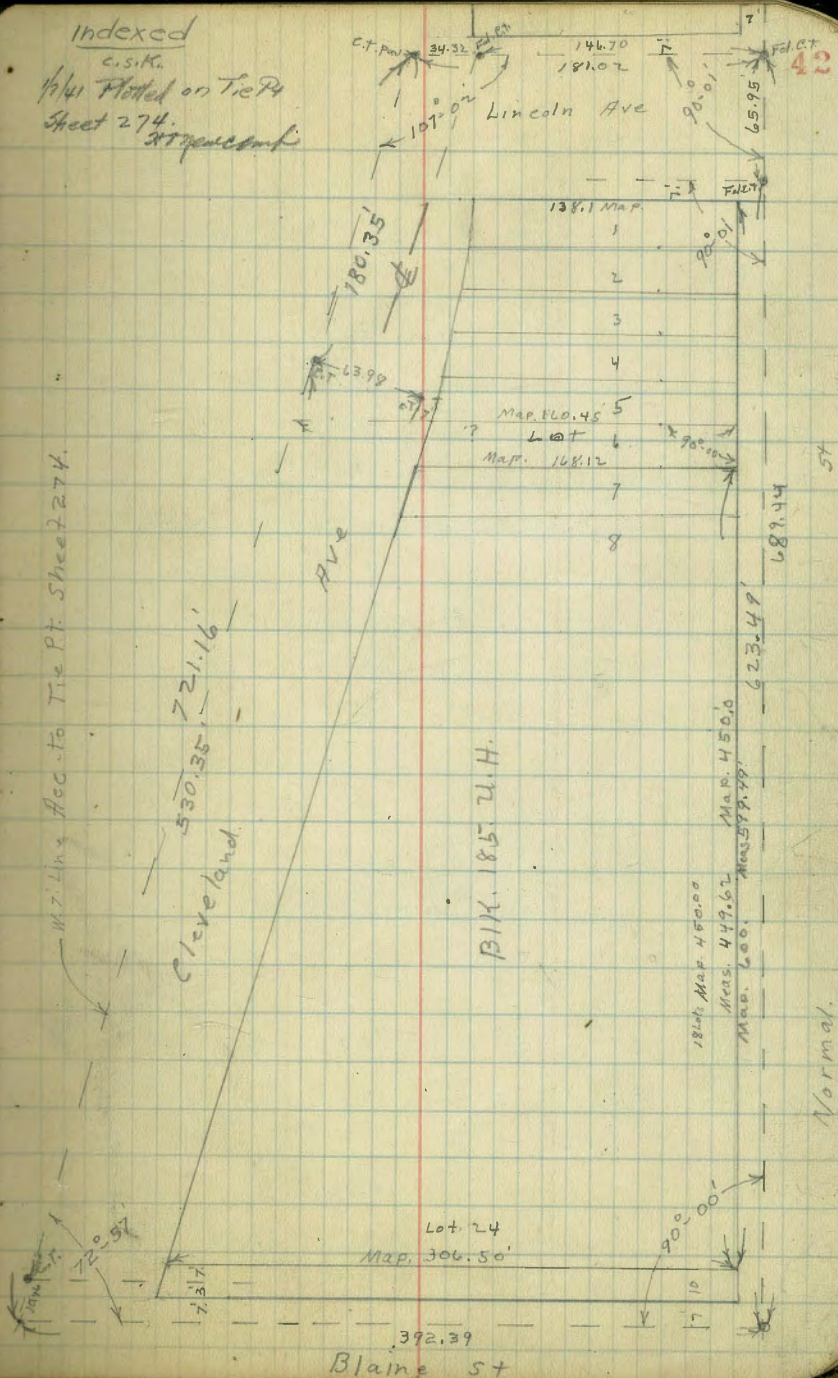
17.7 Lin. Acc. to Tie Pt. Sheet 274.

Cleveland Ave
530.35' 721.16'

B.K. 185 U.H.

Lot 24
Map. 306.50'

Blaine St



42

7-31-37

milk
Walker2 Sec. Alley BIK 16 Nordica Hts. 2
Marine View to Division bet. 40th & 41stB.M. R.P. 0.00 57.34 57.34 N.W. 41st
& Division

0+00 - 15 = N. edge Line of Division

E. ent. st	8.35	48.99
E. g. pay	8.96	48.38
± "	9.25	48.09
W "	9.57	47.79
W. dr	9.04	48.26

0+00 - 9.6 = S. Edge - ent. walk N. End. Pav. returns

W. dr + walk + pay	8.91	48.43
± " " "	8.56	48.78
E. dr + " " "	8.28	49.06

0+00 - 4.5 = N. edge - ent. walk

E. walk	8.12	49.22
± "	8.43	48.91
W "	8.73	48.61

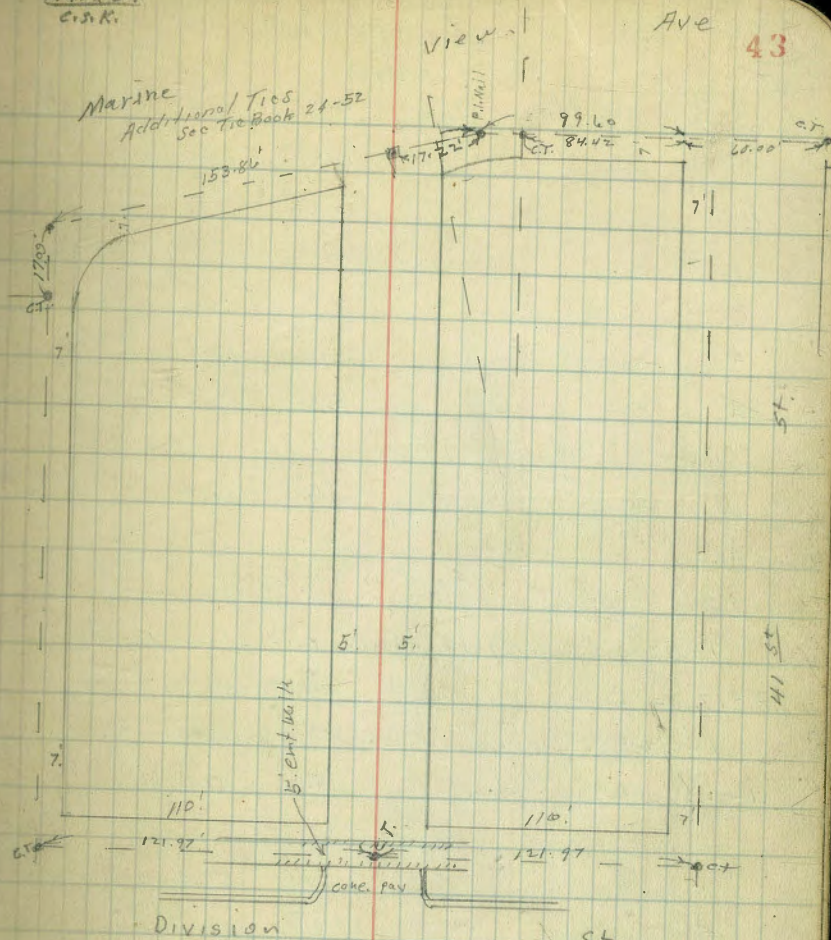
0+00 = N. Line Division

W	8.4	48.9
±	8.2	49.1
E	7.9	49.4

-TP- 7.30 - 56.62 - 8.02 - 49.32 -

0+15

E	6.4	50.2
±	6.4	50.2
W	6.6	50.0

indexed
c.s.K.

56.62

0+30

W	5.6	51.0
±	5.6	51.0
E	5.6	51.0

0+50

E	5.6	51.0
±	5.8	50.8
W	5.8	50.8

1+00

W	5.8	50.8
±	5.7	50.9
E	5.4	51.2

1+33. ± double garage on e. cnt. floor 17' Back.

E-17. = floor 4.35 52.27

1+33. S. sid. garage on W. cnt. floor 5 entrance 2.6 Back

W-4.6 = E. side door way 5.6 51.0

1+50

W	4.8	51.8
±	4.9	51.7
E	4.9	51.7

1+56 garage on W. cnt. floor 7.3' Back

W-7.3 = floor 5.60 51.02

W. Lin. = E. end. cnt. runways. 5.30 51.32

1+75

E	4.8	51.8
±	5.0	51.6
W	5.1	51.5

56.62

2+00

W	4.9	51.7
±	4.8	51.8
E	4.5	52.1

2+41 ³⁵ ± = S. Lin. Marvin+View Ave on diagonal

E	4.0	52.6
±	4.4	52.2
W	4.6	52.0

2+44. ± = S. edge cnt. walk on diagonal

W-0.8 = E. end. cnt. walk. 4.60 52.02

W 4.6 52.0

± 4.4 52.2

E. walk N.E. 3.8 52.8

+8 = W. end. good. walk. 3.10 53.52

2+50 ± = N. Edge of cnt. walk. 4.23 W. side second rise

E-9 = W. end. good. walk 3.25 53.37

E 3.9 52.7

± 4.6 52.0

W 4.9 51.7

W+35 = E. end of walk 4.75 51.87

2+55 = S. edge graded Roadway

W 5.4 51.2

± 5.0 51.6

E. 4.7 51.9

T.P. 964 58.98 7.30 49.32

Orig. B.M. 1.64 51.34

44

9-5-37
Miller
Walker
Bliss

X See Alley BIK 2 West Teratta
Meads to Monroe bet. Iowa + 32nd Sts.

N.W. 10W
+ Meads

BM BP 4.10 — 387.32 — 383.22

	0+00-12 = N. of Meads		
W-25	gutter	6.40	380.92
W	"	6.45	380.87
W	cmt. el	6.04	381.28
♀	gutter	6.54	380.78
E	"	6.60	380.72
E.	cmt. el	6.19	381.13
+28	gutter	6.90	380.42

0+00 = N. Line Meads Ave

E.	cmt. el	N. End.	5.97	381.41
E.	pav	" "	6.02	381.30
♀	"	" "	6.13	381.19
W	"	" "	6.01	381.31
W	cmt. el	" "	5.75	381.57

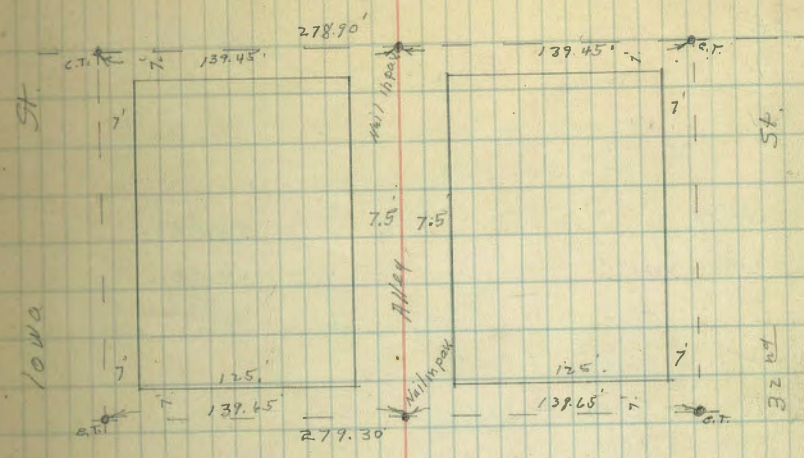
0+08 N

W		4.7	382.6
+3		5.0	382.3
♀		4.7	382.6
+4		4.9	382.4
E		4.6	382.7

0+30

E		3.6	383.7
♀		3.8	383.5
W		3.7	383.6

Monroe Ave 45



Meads Ave

387.32

	0+44 = garage on E dirt floor	16.7	Back
	E-16.7 = floor	3.5	383.8
	0+50 N		
W		3.9	383.4
♀		3.9	383.4
E		3.7	383.6
	1+00 S end Fence on W. side in Alley		
E		4.1	383.2
♀		4.1	383.2
W		4.2	383.1
	1+50 = N. End. above fence on W. side in Alley		
W		4.2	383.1
E		4.2	383.1
E		3.9	383.4

387.32

2+00

E	3.8	383.5
☉	3.8	383.5
W	3.6	383.7

2+50

W	3.8	383.5
☉	3.8	383.5
E	3.7	383.6

— T.P. — 5.62 — 389.69 — 3.25 — 384.07 —

3+00

E	5.8	383.9
☉	5.8	383.9
W	5.8	383.9

3+12 garage on E. dirt floor 0.5 Back

E-0.5 = floor 5.9 383.8

3+50

W	5.5	384.2
☉	5.6	384.1
E	5.4	384.3

3+75

E	4.6	385.1
☉	5.2	384.5
W	5.4	384.3

389.69

4+00

W	5.4	384.3
☉	5.2	384.5
E	5.2	384.5

4+08 Fence on E. End

4+38 { W. End. above Fence
S. " Shed. 11' Long 9.3' Wide } 0.9 in Alley

4+50 N. End. above shed 0.9 in Alley

4+50

E	5.2	384.5
☉	5.2	384.5
W	5.0	384.7

5+00

W	5.1	384.6
☉	5.1	384.6
E	5.1	384.6

5+50

E	4.6	385.1
☉	4.5	385.2
W	4.5	385.2

5+70

N. End. garage under construction
W = North. Entrance 4.75 384.94 on Top SPIKE

☉	4.7	385.0
E	4.7	385.0

5+90

E	5.4	384.3
☉	5.9	383.8
+5	6.0	383.2
W	5.3	384.4

46

389.69

47

6+00 = S. Line Monroe Ave

W.	amt. d	S. End	6.16	383.53
W	pay	" "	6.62	383.00
φ	"	" "	6.42	382.87
+7.0	"	" "	6.72	382.97
+7.0	amt. d	" "	6.32	383.36
E			6.3	383.4

6+12 = S. eb.

E-25	cb		6.65	383.04
E-25	pay		7.14	382.53
E	"		6.91	382.78
E	d		6.45	383.24
φ	pay		6.94	382.75
W	"		6.86	382.83
W	d		6.32	383.37
+25	"		6.29	383.40
+25	pay.		6.91	382.78
+50			6.90	382.79
+75			6.81	382.88
1+00			6.66	383.03
B.M. B.P.			7.20	382.49 = 382.37 + Monroe
T.P.	4.53	387.44	6.74	382.91
CHK orig B.M.			4.23	383.21 = 383.22

8-13-37
Miller
Walker
Bless

4319 St. X Sec. Gamma
To Keeler
Indexed
C.S.K.

0+50

85.1
2.5
50.

0+50

84.8 84.2 83.1 82.1 79.3 79.82 79.98
2.8 3.4 4.5 5.5 8.3 27 76.7
40 38 30 16.5 14 6.0
E.P.V. W.P.V.

0+33

82.5
3.1
50

0+33 = C.T. E.W. of # 18 Pav. = S. Line Palm Hill Sub.

84.8 83.8 82.0 80.8 78.2 78.78 78.95 79.00 79.03
3.4 3.8 5.6 6.8 9.4 8.8 8.66 8.59 8.56
40 34 20 17 14 1.5 1.5 2.5 2.5
E.P.V. W.P.V. C.T.P.V. E.P.V. C.T.P.V.

0+20

84.0
3.6
50

81.0 78.6 74.6 74.6
6.6 9.0 13.0 13.0
50 50 61 70

0+20

83.7 82.8 81.2 79.8 77.6 78.02 78.17
3.7 4.8 6.4 7.4 10.0 9.57 9.42
40 30 16 13 12 6.5 6.5
E.P.V. W.P.V.

78.16 78.15 77.6 81.0 80.8 76.6
9.43 9.44 10.0 6.6 6.8 11.0
E.P.V. E.P.V. 21. 23 30 40

0+00

81.9
5.7
50.

71.9 69.3
15.7 18.3
50 70

0+00 = N. Line Gamma St.

82.6 82.3 77.8 76.2 76.82 76.94 76.96 76.89 76.6 76.6 78.4 74.8 73.9
5.0 5.3 9.8 11.4 10.77 10.65 10.63 10.70 11.0 11.0 9.2 10.8 10.7
40 30 20 15 15 15 15 15 20 22 30 30 40
W.P.V. E.P.V. E.P.V. E.P.V. E.P.V. E.P.V. E.P.V. E.P.V. E.P.V. E.P.V. E.P.V. E.P.V. E.P.V.

B.M. Hub. S. Line Gamma

Old City Boundaries

13.07

87.59

74.52

FB 1521-52

87.59

00-53 = C.T. L.P. 3. W of # 18 Pav.

C.T.L.P.

2+00

5.8	5.8	6.1	6.5	5.86	5.74
50.	40.	25.	14.	6.0 W.PAV	
86.7	86.7	86.4	86.0	86.68	86.80

5.67	5.77	6.6	6.2	6.2
40 W.PAV	30	40	50	50
86.87	86.77	85.9	86.3	86.3

T.P. — 5.66 — 92.54 — 0.71 — 86.88 —

92.54

1+75

0.9	0.9	2.1	1.42	1.32	2.38
50.	40.	13	6.0 W.PAV	0.0 E.PAV	12.0 E.PAV
86.7	86.7	85.5	86.17	86.27	86.21

1.75	1.32	3.0	2.1	2.4	3.1
	0.0 E.PAV	18	20	40	50
86.24	86.27	84.6	84.9	85.2	84.5

1+50

1.0	1.4	2.4	2.30	2.17	2.0
50	40	13	6.0 W.PAV	0	12 E.PAV
86.6	86.2	84.7	85.3	85.39	

2.25	2.32	3.0	2.1	2.4	3.1
	0	18	20	40	50
85.34	86.27	84.6	84.9	85.2	84.5

1+25

0.870	0.870	2.1	1.33	1.32	2.38
50.	40.	13	6.0 W.PAV	0.0 E.PAV	12.0 E.PAV
86.9	85.8	84.6	83.8	84.24	84.24

3.35	3.45	3.0	2.1	2.4	3.1
	0	18	20	40	50
84.24	84.24	84.6	84.5	84.5	83.5

1+25

1.2	1.2	3.0	3.45	3.45	3.35
40.	32.	30.	6.0 W.PAV	0	12 E.PAV
86.9	85.8	84.6	83.8	84.24	84.24

3.45	3.45	3.0	2.1	2.4	3.1
	0	18	20	40	50
84.24	84.24	84.6	84.5	84.5	83.5

1+00

0.866	0.866	2.1	1.33	1.32	2.38
50.	40.	13	6.0 W.PAV	0.0 E.PAV	12.0 E.PAV
86.5	85.3	83.7	83.4	82.84	82.84

3.35	3.45	3.0	2.1	2.4	3.1
	0	18	20	40	50
84.24	84.24	84.6	84.5	84.5	83.5

1+00

1.1	1.1	3.0	3.45	3.45	3.35
40	32	30	6.0 W.PAV	0	12 E.PAV
86.5	85.3	83.7	83.4	82.84	82.84

3.45	3.45	3.0	2.1	2.4	3.1
	0	18	20	40	50
84.24	84.24	84.6	84.5	84.5	83.5

87.59

87.59

3+50

3+48.56

1st Pav. C.T.P. 0.10 E. of ϕ St. = 5' W. of ϕ Pav.

County Road 59+00

2+89.75

W. Line Palm Drive on E

2+84.2

P.E. Pav.

2+72.3

2+64.75

ϕ Palm Drive C.T.P. on ϕ 4.3' W. of ϕ 18' Pav.

2+56.60

2+44.65

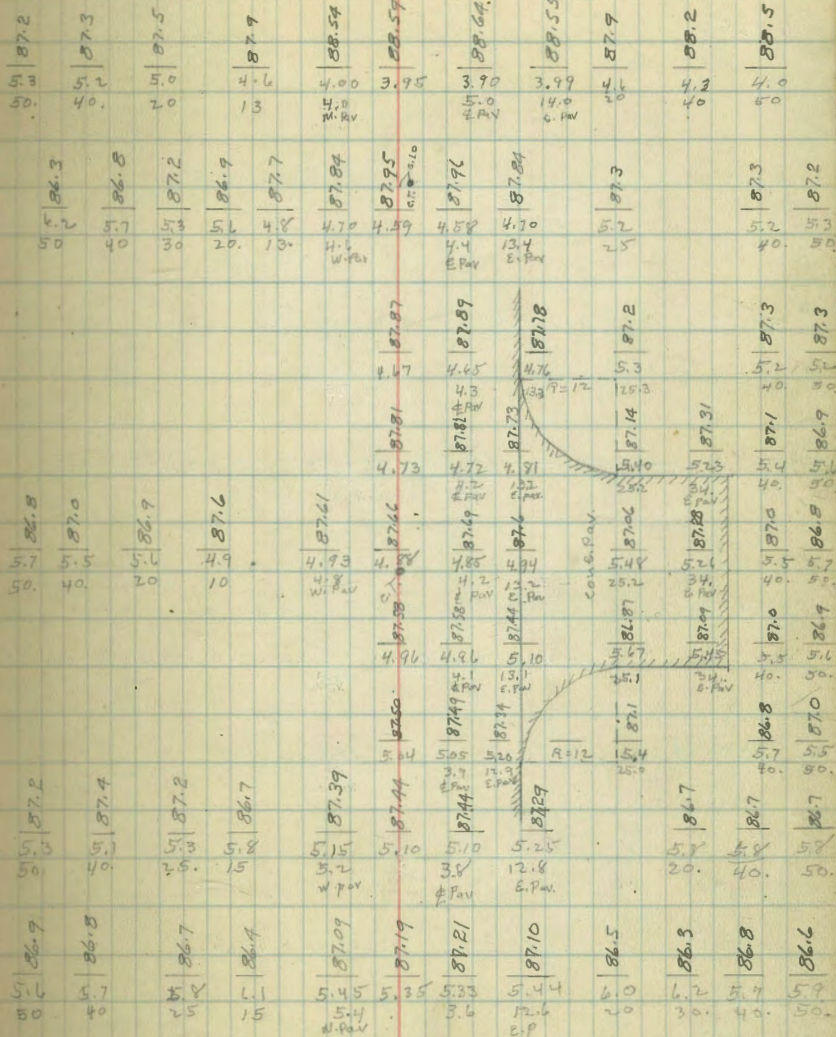
P.E. Pav.

2+39.75

S. Line Palm Drive on E

2+25

92.54



6+25

90.8	90.9	90.8	90.3	91.08	91.1	91.03	91.2	91.8
50.3	4.2	4.3	4.8	103	395	408	39	33
90.3	4.0	3.0	2.0	8.6		9.0	4.0	5.0

6+00

91.1	91.1	90.8	89.9	90.6	91.5	91.27	91.27	91.1	91.3	91.8
4.0	4.0	1.3	5.2	4.5	3.97	3.84	3.84	4.00	3.8	3.4
50	40	29	23	17	8.2	8.2	8.2	8.2	4.0	5.0

5+75

90.6	90.6	90.5	89.7	90.4	90.95	91.06	91.06	91.1	91.1	91.8
4.5	4.5	6.6	5.4	4.7	4.6	4.5	4.5	4.12	4.0	3.3
50	40	30	23	17.0	7.8	7.8	7.8	7.8	4.0	5.0

T.P. Tappin & Man

490

95.11

2.33

90.21

50' W. of E.C.T.
5+40

95.11

5+50

5+40 48 C.T. L.P. on 2 1.7 W. of Pav. = S. Line Ocean Vista Gardens Sub

90.1	90.3	89.9	89.5	90.3	90.71	90.84	90.85	90.79	90.7	90.9	91.4
2.4	2.7	2.6	3.0	2.2	1.83	1.70	1.69	1.75	1.8	1.6	1.1
50	40	28	22	15	2.4	2.4	2.4	2.4	2.0	4.0	5.0

5+00

89.0	89.0	89.0	88.6	89.9	90.18	90.32	90.34	90.28	90.1	90.1	91.2
3.5	3.5	3.5	3.9	2.6	2.36	2.12	2.29	2.26	2.4	2.4	1.3
50	40	30	20	15	2.7	2.7	2.3	2.3	2.0	4.0	5.0

4+50

4+32 64 E.T. of St. 3.7 W. of Pav. N. Line Pam Hill Sub.

88.2	88.4	88.5	88.1	87.0	88.54	89.64	89.67	89.64	89.6	89.8	90.5
4.3	4.1	4.0	4.4	3.5	3.00	2.90	2.87	2.80	2.9	2.7	2.0
50	40	27	20	14	5.0	5.0	5.2	5.2	2.0	4.0	5.0

4+00

87.7	87.6	87.8	87.4	88.3	88.88	89.06	89.08	89.02	88.8	89.0	89.1
4.8	4.9	4.7	5.1	4.2	3.5	3.48	3.46	3.52	3.7	3.5	3.4
50	40	30	17	15	5.0	5.0	4.0	3.0	2.0	4.0	5.0

92.54

92.54

7+50.47 = N line Alpha St.

7+40.47 = Ncb line Alpha St.

7+20.47 = S line Alpha St.

7+00.47 = S cb line Alpha St.

6+90.47 C.T.L.P. & Rd. & 18' Pav. S. line Alpha.

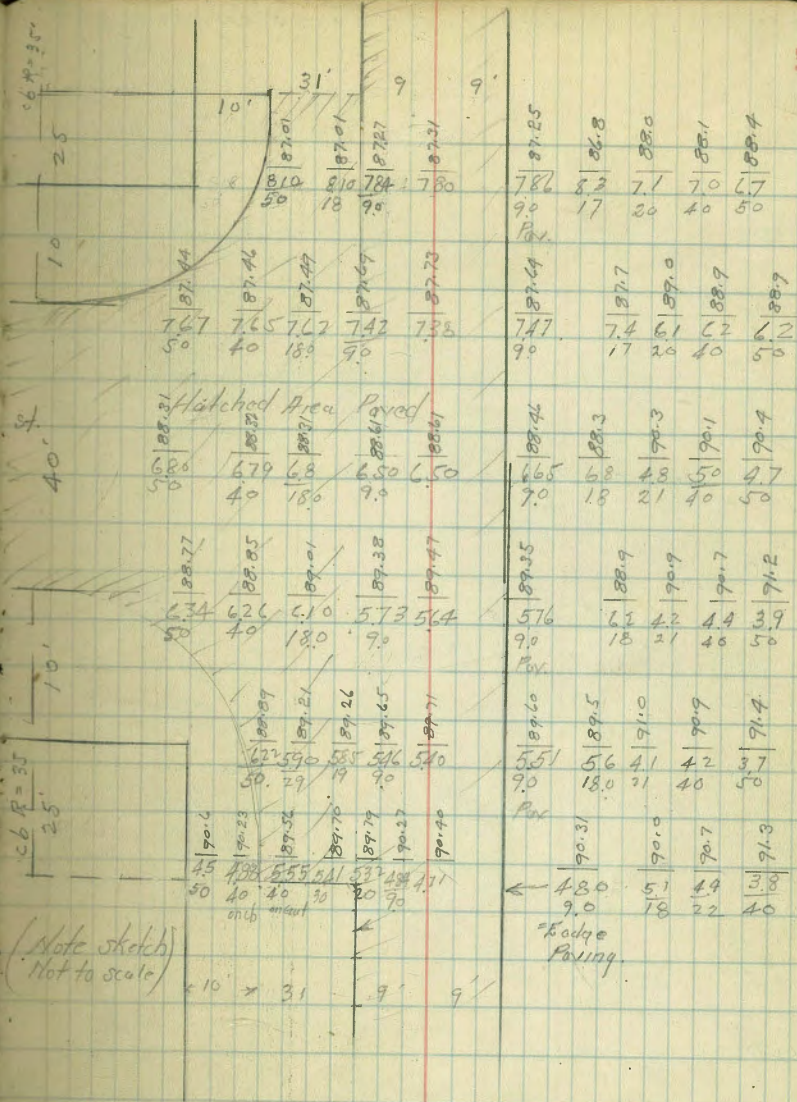
6+65.47 S. Edge Pav. on W = End of Return

6+50

6+48.56 C.T. & St. & 18' Pav. County Road Survey Sta 59+00

95.11

95.11



(Note sketch)
Not to scale

← Edge Paving

9+50

74.8	74.8	75.5	76.0	77.6	79.16	79.26	79.21	79.9	79.4	80.0	80.4	80.5
94	94	87	82	46	499	491	496.43	48	42	38	37	37
60	50	40	21	15	90	90	90	15	25	30	40	50
					Por	Por	Edge	Edge	Edge	Edge	Edge	Edge

9+25

78.1	78.2	78.3	79.8	79.89	80.14	80.10	80.2	80.5
61	60	59	44	128	403	407	40	37
40	40	25	18	90	90	90	40	50
				Por	Por	Edge	Edge	Edge

9+00.16 Copper tack to Paving - N/A Subdivision on West

9+00

81.4	81.7	80.0	80.9	81.8	81.10	80.7	81.2	81.9	81.8
2.8	3.5	4.2	3.7	3.5	3.07	3.5	3.0	2.3	2.4
50	40	23	90	90	90	15	18	40	50
			Por	Por	Edge	Edge	Edge	Edge	Edge

C.T. Lead plug in paving

8+75

83.0	82.9	82.9	81.3	81.91	82.09	82.05	81.6	82.5	82.0	82.2
12	13	13	29	22	208	212	26	17	12	10
50	40	35	23	90	90	90	15	18	40	50
			Por	Por	Edge	Edge	Edge	Edge	Edge	Edge

TP 127 84.17 12.21 82.90

8+50

83.5	83.8	83.4	82.5	82.91	83.04	83.03	82.5	83.0	83.9	85.1	86.1
11.6	11.3	11.7	12.6	12.20	13.07	12.8	12.6	12.1	11.2	10.0	9.0
50	40	25	15	9	90	90	15	17	36	40	50
				Por	Edge	Edge	Edge	Edge	Edge	Edge	Edge

8+00

85.3	85.1	85.14	85.13	85.11	84.6	85.5	86.1	86.6
9.8	10.0	9.7	9.9	10.00	10.5	9.6	9.0	8.5
50.0	40	90	90	90	16.0	19.0	40	50
		Por	Por	Edge	Edge	Edge	Edge	Edge

7+75.47 = End 35' Rad of Return on West.

87.0	86.23	85.67	86.0	86.23	86.26	86.26	85.5	86.7	87.1	87.5
81	888	944	911	888	885	895	96	84	80	76
50	40	40	18.0	90	90	90	17	19	40	50
	oncb.	ent.	oncb.	oncb.	Por	Edge	Edge	Edge	Edge	Edge

95.11

95.11

43rd St. Cross Section

11+25

5.8	5.4	5.0	5.7	4.75	4.9	4.78	5.1	2.0	1.7	1.7
50	40	28	25	90	90	9.0	18	24	40	50
				Par.	Par.	Edge				

11+00

7.4	6.6	6.3	5.0	4.89	4.83	4.91	5.3	2.9	2.6	3.0
50	40	19	16	90	90	90	18	24	40	50
				Par.	Par.	Edge				

10+75

9.5	8.4	7.3	6.4	4.7	5.19	5.26	5.3	4.7	4.9
50	40	25	18	14	90	90	25	40	50
					Par.	Edge			

10+50

10.5	7.1	7.3	7.3	7.8	7.8	7.8	7.8	7.7	7.6	7.5
10.7	13.1	11.9	10.7	5.4	5.53	5.47	5.59	5.4	6.5	7.1
60	50	40	25	15	90	90	70	15	25	30
					Par.	Par.	Edge			

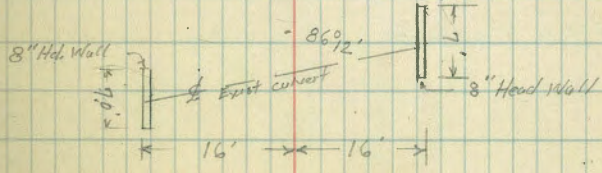
10+25

6.8	6.7	6.4	7.0	7.8	7.8	7.8	7.9	7.6	7.4	7.4
16.0	15.5	14.8	13.3	5.4	5.58	5.52	5.71	5.2	9.6	10.0
80	50	40	27	14	90	90	90	15	25	40
					Par.	Par.	Edge			

10+10 Section on projection culvert line

6.8	6.8	6.8	6.8	7.1	7.3	7.7	7.8	7.8	7.8	7.8
16.0	15.6	14.8	14.4	12.4	10.34	6.88	5.7	5.70	5.59	5.70
25	50	40	35	25	14	16	15	90	90	15
					Floor here	on top of wall		Edge	Par.	Edge

10+10 = 12" Existing Concrete Culvert



9+90

6.9	6.9	7.0	7.1	7.9	7.8	7.8	7.8	7.8	7.8	7.7
15.0	14.3	13.6	12.6	5.2	5.47	5.40	5.51	4.4	3.5	7.8
60	50	40	25	14	90	90	90	15	25	35
					Par.	Par.	Edge			

84.17

84.17

4319 Jt. Cross Sections.

15 + 27.7 = EC. cb Ret. on E

14 + 81.7 = N. cb. line Keeler on E

14 + 66.7 = E. Keeler on East.

14 + 51.7 = S. cb line on E

14 + 2.7 = Bit in paving.

14 + 05.7 = PC. cb Ret. on E

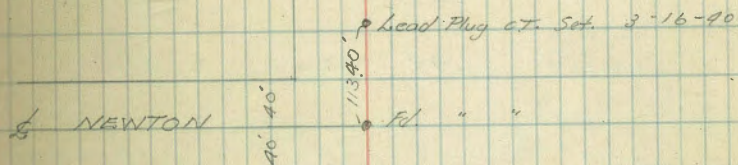
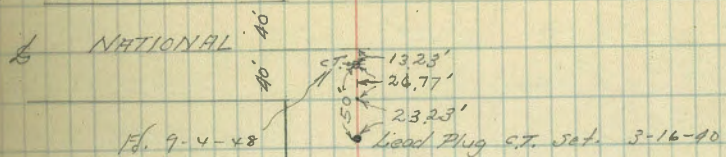
13 + 50

13 + 00

12 + 71 = Bit in cb on E

82.71

72.81	73.21	73.50	73.58	72.56	73.11	73.64
99	95	921	913	915	960	907
40	24	9.	9.	90	24	24
		Pay.	Pay.	Pay.	out.	on cb
73.81	74.11	74.64	74.70	74.63	74.32	74.93
89	86	807	801	808	839	778
40	24	90	90	9	24	10
		Pay.	Pay.	Pay.	on Pay.	on Pay.
74.21	74.61	75.07	75.09	75.00	74.68	75.53
85	81	764	762	771	803	718
40	24	9.	9.	90	24	40
		Pay.	Pay.	Pay.	Pay.	Pay.
74.81	75.01	75.34	75.43	75.38	75.03	74.93
79	77	737	738	733	768	678
40	24	9	9	9	24	40
		Pay.	Pay.	Pay.	Pay.	Pay.
75.11	75.31	75.90	75.74	75.81	75.46	75.77
76	74	681	677	690	725	694
40	24	9	9	90	24	295
		Pay.	Pay.	Pay.	Pay.	out.
75.21	75.51	76.25	76.34	76.26	75.82	76.51
75	72	646	637	645	689	620
40	24	9	9	90	24	24
		Pay.	Pay.	Pay.	out.	on cb
76.21	76.71	76.21	76.15	77.23	77.12	76.23
65	69	65	556	548	559	598
40	30	24	90	90	9	24
			Pay.	Pay.	Pay.	out.
76.91	77.61	77.41	77.96	78.01	77.93	77.55
58	51	53	475	470	478	516
40	30	24	90	90	9	24
			Pay.	Pay.	Pay.	out.
78.01	78.43	78.53	78.44	78.04	78.27	78.20
47	428	418	427	467	391	391
40	90	90	90	24	24	24
	Pay.	Pay.	Pay.	out.	out.	on cb.
		82.71				



0.00 = ✓

72.47 = BM.

chk. NW B. Keeler ^{TP.} _{Ad. 83rd}

10.24

72.47

15 + 788 = EC. Return NW. cor Keeler

15 + 62.8 = North sb line Keeler on West

15 + 45 = South edge pouring on West. ^{Keeler}

83.71

North Prop. line
Keeler

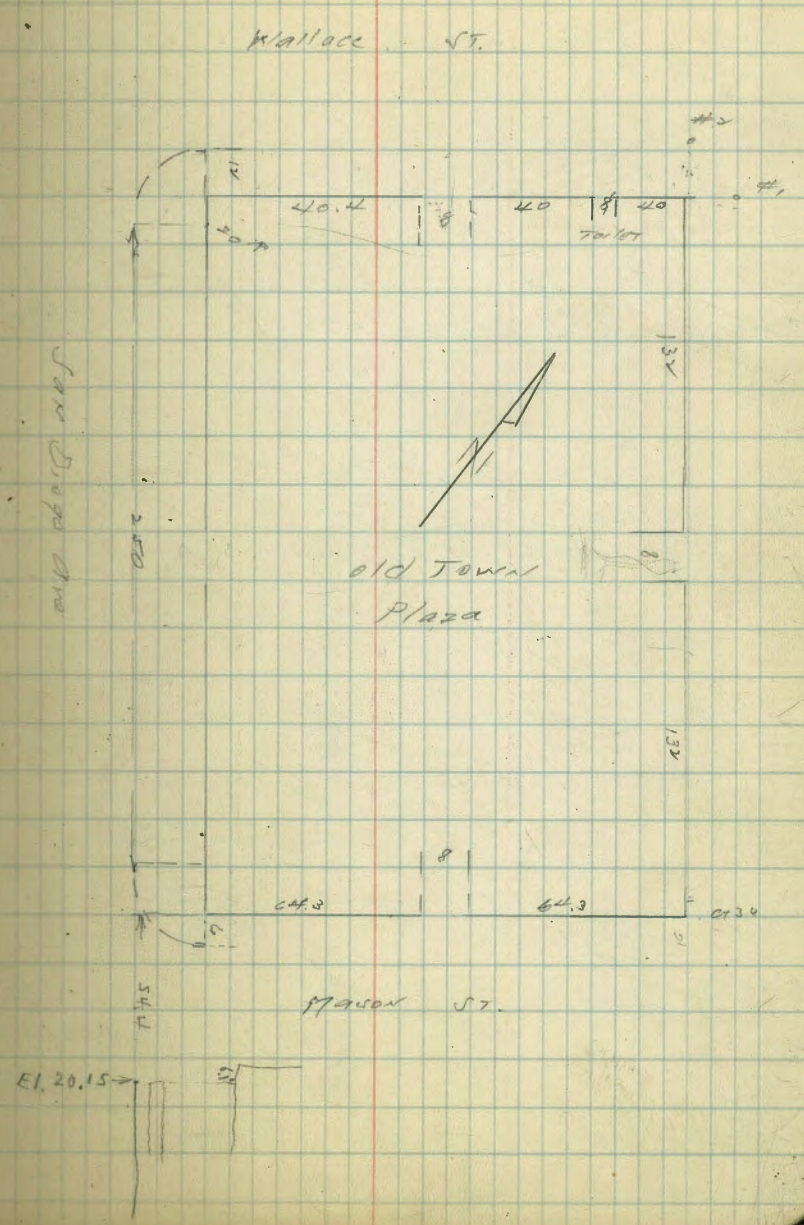
	72.45	71.89	72.47	72.47	72.36	71.94	72.45
	1026	1082	1027	1022	1035	1077	1026
	24	24	9		9.0	24	24
	on cb.	gut.	Par.	Par.	Par.	gut	top cb.
72.67	72.07	72.26	72.80	72.81	72.73	72.30	72.85
1064	1064	1051	991	990	998	1041	989
40	20	24	9	9	9	24	24
on cb.	gut.	on Par.	Par.	Par.	Par.	Par.	on cb.
	72.71	72.60	73.21	73.25	73.27	72.71	73.21
	1000	1011	950	946	944	1000	950
	40	24	9.0	Par.	9	24	24
	Par.	Par.	Par.	Par.	Par.	Gutter	top cb.
				83.71			

Levels on
Old Town Plaza

Indexed
c.s.k.

Level	2.57	24.79	22.22	Indexed c.s.k.
SWISP				Mason U.D.
S. Cor. Top 6' curb			5.14	19.65
Mason St. ENT.			4.55	20.24
Top walk at Grocery			1.52	23.27
ground E. Cor Plaza			3.7	21.6
T.P.	0.40	21.99	3.20	21.59
Calhoun ENT.			4.80	17.19
N. Cor. Plaza on ground #1			7.5	14.5
" " " #2			7.0	15.0
T.P.	3.78	18.89	6.88	15.11
Toilet ENT.			4.05	14.84
Wallace "			4.10	14.79
W. Cor Plaza Top in ct			3.66	15.23
opposite above			4.67	14.22

Mason
11-13-37



	4.59
1/4	3.92
rail	3.80
"	3.80
"	3.82
"	3.81
1/4	3.93
gut	Culv. under track
N 06	inlet to Car Barn 4.54
	3.80
	0+50 outlet Culv.
N 06	4.16
gut	outlet Culv. 4.85
	Top head wall 4.00
+05	rail of track to Barn 4.02
+11	" " " " 4.00
rail	Main tracks 3.98
"	3.97
"	3.98
"	3.98
1/4	4.07
gut	4.72
5 06	4.21
	0+75
5 06	4.02
gut	4.82
1/4	4.19

rail	4.00
"	4.02
"	4.02
"	4.03
+04 rail	4.07
1/4	4.22
gut	4.92
N 06	4.23
	1+00
N 06	4.48
gut	5.08
1/4	4.28
rail	4.09
"	4.09
"	4.07
"	4.07
1/4	4.31
gut	4.96
5 06	4.22
	1+20
5 06	4.24
gut	5.11
1/4	4.47
rail	4.18
"	4.18
"	4.20

rail	4.20
1/4	4.49
gut	5.22
N cb	4.60
1 + 40	
N cb	4.70
gut	5.34
1/4	4.40
rail	4.98
"	4.39
"	4.34
"	4.36
1/4	4.63
gut	5.97
S cb	4.77
1 + 50 ¹³ w + alley	
S.L. curb + gut.	4.74
S cb	4.99
gut	5.42
1/4	4.79
rail	4.53
"	4.57
"	4.52
"	4.52
1/4	4.78
gut	5.52

N cb	4.86
1 + 56 + drain across Adams under tracks	
N cb \$ 7.5 ⁶ w + opening	4.85
6" x 7.5'	
gut on grate	5.41
1/4	4.92
rail	4.46
"	4.65
"	4.65
"	4.68
1/4	4.89
gut on grate	5.46
1 + 70 ¹³ Ely alley	
S.L. curb	4.79
PAV.	4.86
S cb	4.92
gut	5.48
1/4	4.97
rail	5.02
"	5.02
"	5.00
"	5.00
1/4	5.18
gut	5.44
N cb	4.99
1 + 80	
N cb	5.01

gut	5.64
1/2	5.35
rail	5.28
"	5.23
"	5.20
"	5.20
1/2	4.88
gut	5.41
5 cb	4.82
1 + 90	
5 cb	4.64
gut	5.23
1/2	4.75
rail	5.07
"	5.18
"	5.26
"	5.38
1/4	5.29
gut	5.48
5 cb	5.00
2 + 00	
5 cb	4.87
gut	5.38
1/2	5.22
rail	5.11
"	5.02

rail	4.87
"	4.74
1/4	4.63
gut	5.12
5 cb	4.51
2 + 10	
5 cb	4.49
"	5.04
1/2	4.50
rail	4.52
"	4.64
"	4.68
"	4.77
1/4	4.90
gut	5.25
5 cb	4.92
2 + 20	
5 cb	4.72
gut	5.18
1/4	4.73
rail	4.52
"	4.45
"	4.48
"	4.39
1/2	4.51
gut	5.00

S cb	4.50
2 + 40 approx. N cb P.C. 2 + 42.88 = curb P.C.	
S cb	4.33
gut	4.89
1/4	4.40
rail	4.39
"	4.44
"	4.27
"	4.36
1/2	4.42
gut	4.81
N cb	4.28
2 + 60	
S cb	4.27
gut	4.78
1/4	4.35
+ 9.4 = 5 rail of S track Prod. Pav.	4.21
+ 38 rail	4.28
"	4.30
"	4.15
"	4.26
1/4	4.25
tot gut = plus of N cb produced	4.64
N cb	4.35
2 + 80	
S cb	4.19

gut	4.77
1/4	4.25
+ 9.4 = 5 rail of S track produced by	4.12
+ 10.6 = rail	4.19
rail	4.28
"	4.14
"	4.18
Prod. cb LINEN + 07 = gut.	4.52
N cb	4.22
3 + 10.27 = wly Ala. ST.	
S cb	4.07
gut	4.59
1/4	4.12
+ 9.4 = S rail of S track	3.90
+ 15.2 " " "	3.82
+ 30.4 = S rail of S track	3.93
N " " "	3.88
S " " N "	3.75
N " " " "	3.71
+ 32 from N curb Prod. by	4.30
N cb = 84' cb to cb	3.94

= gutier

Xsec of Fern Glen
La Jolla Blvd. to Monte Vista

70.5 wide
10 curbs
17.62 1/2"

Indexed
G.S.K.

Moore
12-37

See F.B. 1357 p 36 No change

" " 1370 p 43 for ties

S.E. B.P.	1.16	80.17'	79.01	WEST SIDE OF LA JOLLA BLVD.
T.P.	2.96	75.15'	72.19	

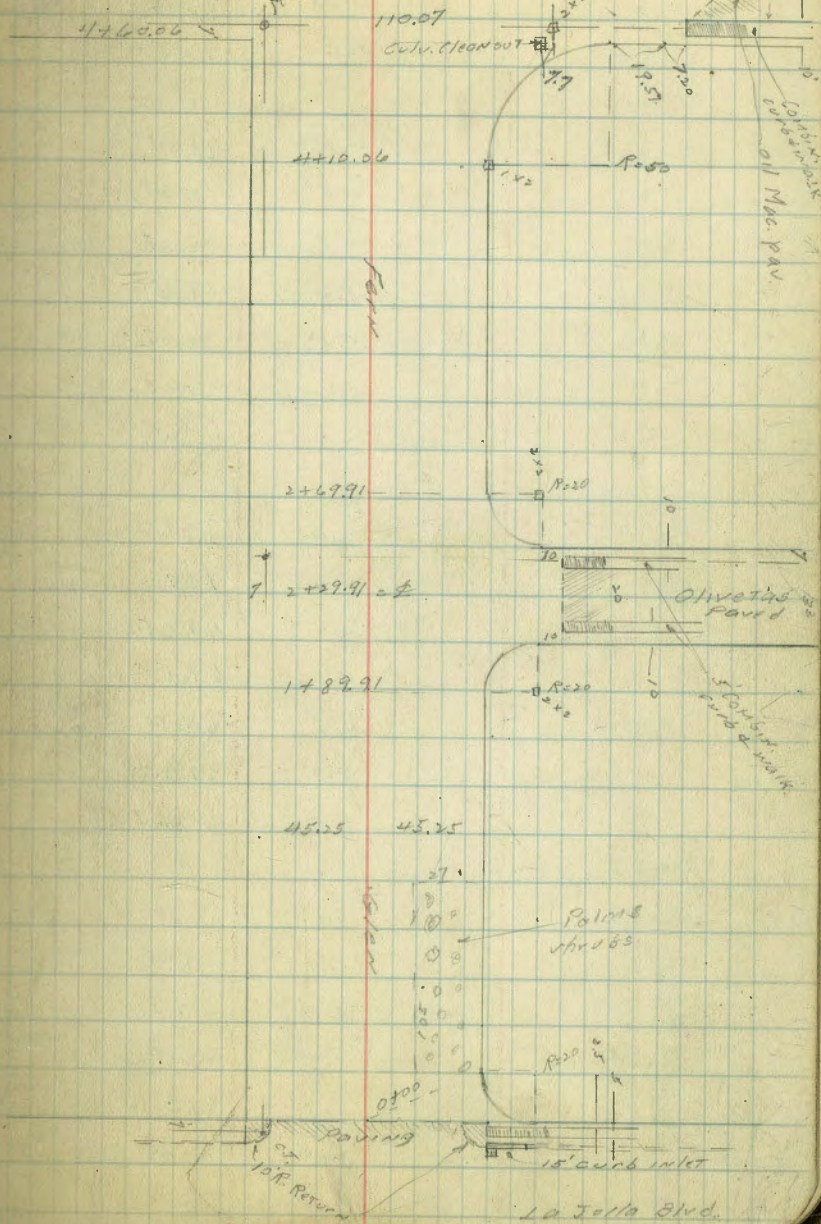
0+0 = W of La Jolla Blvd.

S	gvt pav.	4.48	70.67
S	cb	3.80	71.35
cb	pav	4.57	70.58
1/4	"	4.60	70.55
"	"	4.76	70.39
1/4	"	4.94	70.21
cb	"	5.23	69.92
N	" gvt. on grating	5.38	69.77
N	cb	4.40	70.75
+20	cb	4.52	70.63
+20	gvt	5.31	69.84

0+00 = W of La Jolla Blvd.

N	"	4.6	70.55
cb	top	4.73	70.42
gvt	pav	5.44	69.71
1/4	"	4.77	70.38
"	"	4.57	70.58
1/4	"	4.50	70.65
cb	gvt pav.	4.56	70.59

Monte Vista



75.15

cb top	3.88	71.47
S	3.6	71.55
0+55		
S	4.3	70.85
cb	4.3	70.85
1/2	4.8	70.35
c	5.3	69.85
1/4	5.1	70.05
cb	5.1	70.05
N	4.8	70.35
0+50		
N	6.0	69.15
cb	6.3	68.85
1/2	6.1	69.05
c	5.5	69.65
1/4	5.6	69.55
cb	5.4	69.75
S	5.5	69.65
0+75		
S	6.1	69.05
cb	6.1	69.05
1/4	6.3	68.85
c	7.4	67.75
1/4	7.8	67.35
cb	6.8	68.35
N	6.6	68.55

75.15

66

1+00		
N	7.6	67.55
cb	8.8	66.35
1/4	9.1	66.05
c	8.0	67.15
1/4	7.2	67.95
cb	7.0	68.15
S	6.7	68.45
1+25		
S	7.4	67.75
cb	7.9	67.55
1/4	7.6	67.55
c	8.2	66.95
1/4	9.4	65.75
cb	9.7	65.45
N	9.9	65.25
1+50		
N	10.1	65.05
cb	9.7	65.45
1/4	9.0	66.15
c	9.0	66.15
1/4	8.4	66.75
cb	8.4	66.75
S	8.2	66.95
1+89.91 = PC on N		
S	9.7	65.45

75.15

cb	9.7	65.45
1/4	9.9	65.45
c	12.0	63.15
1/4	11.7	63.45
+8	11.9	63.45
+14	9.1	66.05
cb	9.8	65.85
N	10.8	64.35

T.P. on I.P. 1.16 65.48 ✓ 10.83 64.32

Glover
B.C.

2+09.91 = Ely Olivetas

N - 20 = E.C. of P. Line	3.2	64.48
N	2.6	64.88
cb	2.7	64.78
+8	5.9	59.58
1/4	4.7	60.78
+8	5.0	60.48
c	3.6	61.88
1/4	1.1	64.38
cb	0.7	64.78
S	0.8	64.68
2+19.91 = E cb		
S	1.0	64.48
cb	0.8	64.68
1/4	1.2	64.48

65.48

67

C	4.1	61.38
1/4	5.2	60.48
+14	4.9	60.58
cb	4.9	60.58
N	3.1	64.38 ✓
+20	3.8	61.68
+30 Top cb end	3.51	61.97
+30 gut par.	4.03	61.45
+40 " "	4.22	61.46
+40 Top cb	3.67	61.81
2+29.91 = E Olivetas		
-40 par	4.30	61.18
-30 end "	4.13	61.35
N	3.5	61.98
cb	3.2	64.48
+9	3.6	61.88
1/4	6.2	59.28
C	6.5	58.98
+5 Rim S.M.H.	4.60	60.88
+12	1.6	63.88
1/4	1.7	63.98
cb	1.2	64.28
S	1.3	64.18
2+39.91 Wly cb Olivetas		
S	1.3	64.18
cb	1.5	63.98

1/2		1.6	63.88
C		5.4	60.08.
+10		6.9	58.58.
1/2		4.0	61.48.
+8		1.8	63.68.
cb		3.8	61.68.
N		4.1	61.38.
+20		4.2	61.48.
+30	Top cb end	4.06	61.48
+30	gut. par.	4.53	60.98.
+40	"	4.67	60.81.
+40	Top cb	4.21	61.27.
	2 + 49.91 = Wly olivetas		
-20	= B.C. on NL.	4.3	61.18.
N		4.2	61.48
cb		3.9	62.18.
+11		2.0	63.48
1/2		4.2	61.48.
+7		8.1	57.38.
C		3.3	62.18.
1/2		2.0	63.48
cb		2.0	63.48
S		1.7	63.78.
	2 + 69.91 = E.C. on N.L.		
S		2.7	62.78
cb		2.8	62.68

1/2		3.0	62.48
C		3.0	62.48
+8		7.9	57.58.
1/2		9.2	56.48.
+12		1.4	64.08
cb		3.9	61.58.
N		4.0	61.48.
	3 + 00		
N		5.2	60.28
cb		5.6	59.88.
1/2		7.3	58.18
C		5.9	59.58.
1/2		4.2	61.48.
cb		3.8	61.68.
S		3.7	61.78.
	3 + 25		
S		4.2	61.48.
cb		4.8	60.68.
1/2		5.9	59.58.
C		8.2	57.78.
+12		11.9	53.58.
1/2		11.0	54.48
+8		7.4	58.08.
cb		4.7	58.78.
N		6.5	58.98

3+50

N		9.0	56.48
cb		9.2	56.78
+10		12.1	51.38
1/2		12.4	51.48
+10		14.2	51.48
C		11.1	54.38
1/2		8.5	56.98
cb		7.1	58.38
S		5.8	59.68
	3+75		
S		6.4	59.08
cb		7.1	58.38
1/2		9.8	55.68
+12		14.4	57.08
C		14.9	50.58
1/2		11.2	54.78
cb		10.8	54.68
S N		10.8	54.68
	4+10.06 B.C		
N		12.87	54.61 on HUB
cb		12.3	53.18
1/2		14.0	51.48
+8		12.0	53.48
C		11.1	54.38
+12		8.6	56.88

1/2		7.8	57.68
cb		7.2	58.48
S		6.8	58.68
TR	1.92	59.66	824 57.24
	4+45.42 = center of curve on N2.		
S		1.9	57.26
cb		2.2	56.96
1/2		3.5	55.66
C		4.8	54.36
1/2		5.6	53.56
cb		7.9	51.26
N		8.8	50.36
	+14.65 = E curve	8.8	50.36
	4+60.06 = Ely Monte Vista		
	Sec. now taken on " "		
	S.L. of Fern Glen to east		
			10' cbs 17.00' WS
E of Monte Vista		2.5	56.66
+7		3.0	56.16
cb		3.8	55.36
+4		5.0	54.16

50' wide
10' curbs
7.5' WS

E 1/2	4.4	54.96
E MONTA VISTA	4.4	54.96
1/4	4.3	54.86
cb	4.2	54.96
+4	4.0	55.16
w.l.	4.3	54.86

S cb Farm Glen to east

w +	4.5	54.66
+0	6.1	53.06
cb	4.8	54.36
1/4	4.9	54.46
c	4.7	54.46
1/4	4.8	54.36
+3	5.2	53.96
cb	4.6	54.56
+3	3.4	55.96
E	2.6	56.56

S 1/2 Farm Glen to east

E MONTA VISTA	4.0	55.16
cb	4.6	54.56
+4	6.0	53.16
1/4	5.8	53.36
c	5.7	53.46
1/4	5.9	53.46
cb	6.2	52.96
w	8.3	50.86
+5	9.3	49.86

E Farm Glen to east

-10	9.9	49.46
w	8.7	50.46
cb	7.3	51.86
1/4	7.1	52.06
c	6.9	52.26
1/4	6.9	52.26
+3	7.4	51.76
cb	6.2	52.96
E	5.0	53.56

N 1/2 Farm Glen to east

E	7.0	52.16
cb	8.2	50.96
1/4	8.1	51.06
c	8.0	51.16
1/4	8.2	50.96
cb	8.8	50.36
N	9.3	49.86
+10	10.3	48.86

N cb Farm Glen to east

-10	10.9	48.46
w	10.5	48.66
cb	9.4	49.56
1/4	9.2	49.76
c	9.1	50.06
1/4	9.0	50.16

cb	9.3	49.86
E of Moore Vista	7.2	51.96
N.L. Fern Glen to east = 0+00		
E	8.5	50.66
cb	9.4	49.76
1/4	9.7	49.46
c	9.7	49.46
1/4	9.9	49.46
cb	10.2	48.96
W	10.8	48.36
+10	11.4	47.76

0+19.57 = S.L. Fern Glen to West

-20	12.3	46.86
W	11.6	47.56
cb	11.2	47.96
1/4	10.8	48.36
c	10.6	48.56
1/4	10.6	48.56
cb	10.2	48.96
E Top grate of cleanout	10.54	48.64
" F.A. CULV	17.82	41.34

0+44.57 = E Fern Glen to West

E	9.2	49.96
+5	11.0	48.16
cb	11.2	47.96
1/4	11.4	47.76

c	11.8	47.36
1/4	12.0	47.16
cb	12.1	47.06
W	12.4	46.76
+20	12.4	46.76

0+50

-20	12.5	46.66
W	12.5	46.66
cb	12.3	46.86
1/4	12.0	47.16
c	11.9	47.26
1/4	11.6	47.56
cb	11.4	47.76
+5	10.9	48.46
E	8.1	51.06 = E.C. of 50' S CURVE

0+69.57 = N.L. Fern Glen to West = 0+00

E	8.1	51.06
+5	10.8	48.36
cb	11.3	47.86
1/4	11.7	47.46
c	12.0	47.16
1/4	12.4	46.76
cb	12.2	46.96
W NW cor of Moore Vista = end of Fern Glen to West	13.2	45.96
+20	13.3	45.86

59.16

0 + 07.2 = end of Corb. cb + 5' down on E side

W - 10	15.6	43.56
W	15.0	44.16
+ 7	12.0	47.16
cb	12.0	47.16
1/4	12.2	46.96
c	11.9	47.46
1/4	11.6	47.56
cb dir. gut	11.7	47.46
cb Top	11.15	48.01
+ 5 edge sidewalk	11.04	48.14
E	8.2	50.96

0 + 50.5 = end of cb

E	9.5	49.66
+ 5 edge sidewalk	11.31	47.85
cb	11.40	47.76
" gut par	12.08	47.08
1/4	11.84	47.32
c	11.75	47.41
1/4	12.07	47.09
cb gut "	12.41	46.55
cb end	11.98	47.18
+ 5	12.0	47.16
W	13.3	45.86
+ 10	16.7	44.46

59.16

72

1 + 00

W Top cb	12.40	46.76
" gut par	12.06	46.10
C "	12.10	47.06
E gut "	12.48	46.68
E cb	11.77	47.39

T.P. 6.27 63.48 ✓ 1.95 57.21 ✓
 3.96 59.52 59.52 ✓

S.W. B.P.
 Belvedere
 Monte Vista

12-14-37 Survey Drainage Ditch Orange to El Cajon
at Bancroft

Miller
Walker
Bliss

Indexed
C.S.K.

N.W. Orange

BM. 0.98 347.64 366.66 4.33

N. ch. line Orange

E. End. ch. inlet.	Top curb	9.51	358.13
" "	" gutter	10.45	357.19
4	" " grating	10.61	357.03
4	" " F.L. Box	16.30	351.34
W	" " " gutter	10.55	357.09
W	" " " Top ch	9.65	357.99

T.P. B/M R.P. 8.11 366.22 9.53 358.11

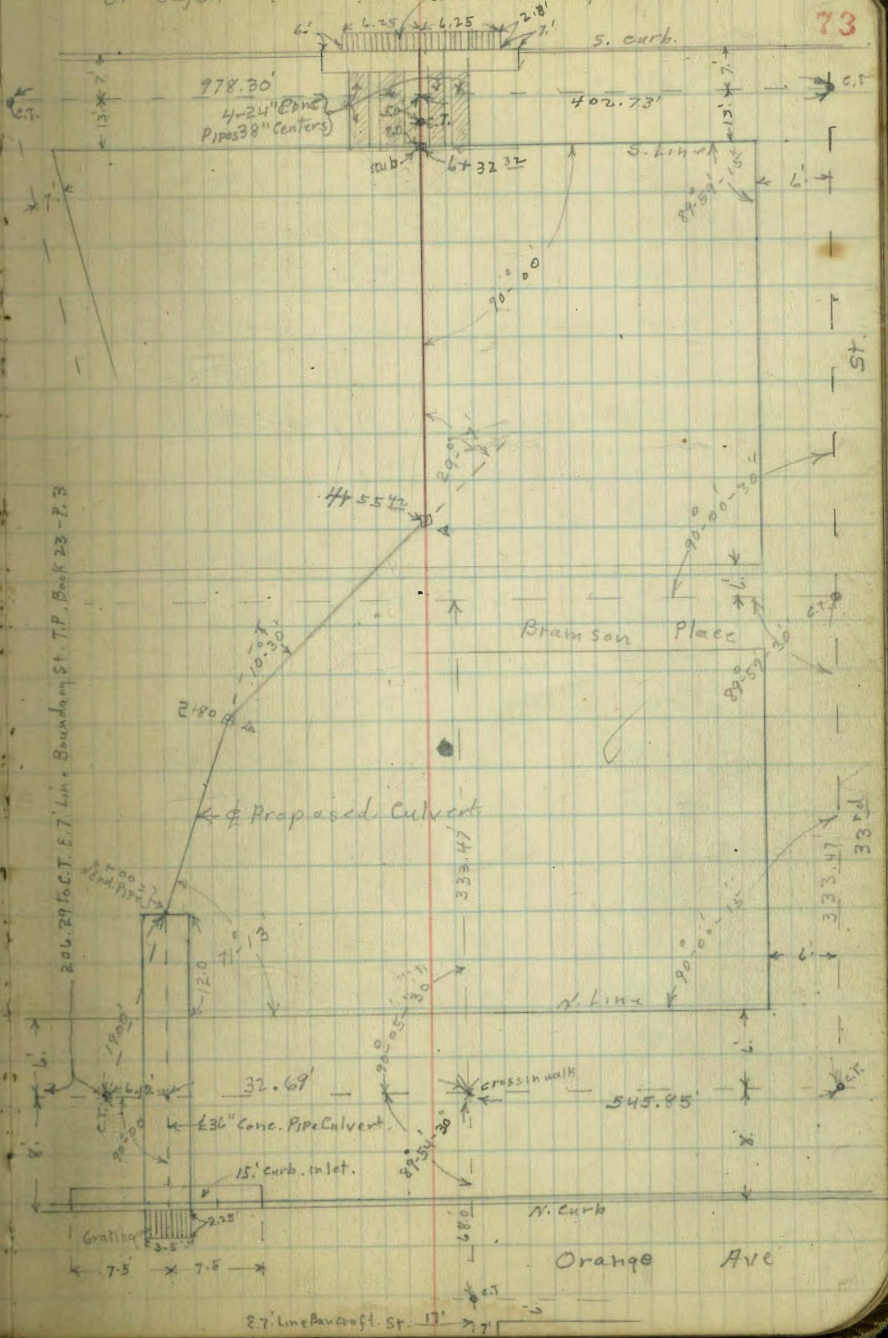
N. Line of Orange

15' Lt. of 4" Pipe	7.7	358.5
4" "	9.0	357.2
15' Rt. of 4" Pipe	7.7	358.5
12' N. of N. Line = N. End. 36" Pipe = 0+0.0 at 90° to 6" Pipe		
15' Rt	8.1	358.1
9' Rt	8.3	357.9
4' F.L.	14.45	351.77
8' Lt.	11.4	354.8
12' Lt.	7.0	359.2
20' Lt.	6.3	359.9
	0+30	
25' Lt.	4.4	361.8
17' "	4.4	361.8
11' "	7.1	359.1
9' "	11.0	355.2
4	12.4	353.8

El Cajon

curb inlet. Grating Blvd.

73



E.T. Line Bancroft St. 17'

366.22

9' Rt	11.7	354.5
13' "	6.5	359.7
20' "	5.6	360.6
	0+50	
25' Rt	4.8	361.4
20' "	5.4	360.8
5' "	10.9	355.3
♀	9.9	356.3
+ 3' Lt. wash	11.7	354.5
+ 8' Lt	7.5	358.7
15' "	4.4	361.8
20' "	3.4	362.8
	1+00	
25' Lt	4.1	362.1
20' "	4.7	361.5
13' "	6.3	359.9
♀	8.2	358.0
9' Rt. wash.	9.7	356.5
17' "	7.5	358.7
25' "	3.9	362.3
30' "	2.8	363.4
	1+50	
40' Rt.	2.0	364.2
30' "	2.0	364.2
17' "	7.4	358.8
11' " = wash	8.5	357.7

366.22

74

♀	7.4	358.8
10' Lt	4.4	361.4
18' "	4.0	362.2
	1+85	
20' Lt	3.6	362.6
10' "	4.7	361.5
♀ = wash	8.0	358.2
12' Rt	6.6	359.6
23	7.5	364.7
28' "	4.1	365.1
	2+10	
18' Rt	1.7	364.5
9' "	3.8	362.4
♀ = wash	8.0	358.2
10' Lt.	5.4	360.8
20' "	2.7	363.5
	2+50	
12' Lt	4.4	361.8
6' Lt	4.6	361.6
4' Lt.	6.6	359.6
♀ = wash	7.3	358.9
5' Rt	6.6	359.6
7' "	4.2	362.0
18' "	1.4	364.8
25	1.4	364.8

366.22

2+80 Δ 10° 30' Rt. on split. of Δ

21 RT		1.9	364.3
15 "		3.3	362.9
6 "		3.7	362.5
⊕	wash	6.6	359.6
9' Lt.	"	6.0	360.2
13 "		3.2	363.0
20 "		3.0	363.2

3+00

13		3.8	362.4
10. Lt	wash	5.5	360.7
⊕	wash	5.7	360.5
3 RT		4.5	361.7
14 "		3.8	362.4
20 "		1.8	364.4

3+25

20 RT		1.9	364.3
13 RT		2.5	363.7
3 RT		4.8	361.4
⊕	wash	6.3	359.9
3 Lt		4.9	361.3
11 Lt		3.4	362.8
17 "		1.5	364.7

3+50

15 Lt.		2.1	364.1
5 "		2.1	364.1
2 "		6.3	359.9

366.22

75

⊕	wash.	6.3	359.9	
2 RT		6.3	359.9	
3 "		4.1	362.1	
8 "		2.5	363.7	
15 "		2.2	364.0	
T.P.	8.13	373.71	0.64	365.58

4+00

17 RT		7.5	366.2
12 "		9.5	364.2
5 "		9.8	363.9
⊕ = wash		12.6	361.1
2 Lt	"	12.6	361.1
8 "		9.7	364.0
16 "		9.7	364.0

4+40

15 Lt		8.6	365.1
7 Lt.		8.8	364.9
2 Lt wash		11.8	361.9
⊕	"	11.8	361.9
6 RT.		8.7	365.0
15 "		6.9	366.8

4+55 Δ 29° 17' Lt. on split. of Δ

10		6.6	367.2
6		8.4	365.3
⊕ stub		10.73	362.98
4 Lt		11.2	362.5

Δ (con)

7' Lt		9.0	364.7
12' Lt		8.5	365.2
		4+75	
9' Lt		8.2	365.5
3' Lt		8.5	365.2
♀	wash	11.0	362.7
4' Rt	"	11.3	362.4
7' "		8.7	365.0
12' "		7.0	366.7
		5+00	
15' Rt		7.0	366.7
8' Rt	wash	10.1	363.6
3' Rt	"	10.1	363.6
♀		8.1	365.6
10' Lt		7.0	366.7
		5+50	
12' Lt		4.7	369.0
7' Lt		4.7	369.0
♀		8.5	365.2
2' Rt	wash	10.0	363.7
5' "	"	10.0	363.7
11' "		5.3	368.4
		5+95	
15' Rt		3.0	370.7
5' "	wash	10.2	363.5
1' "	"	10.2	363.5

♀		8.4	365.3
8' Lt		3.0	370.7
12' "		2.8	370.9
		5+98	
9' Lt		3.0	370.7
0.3' Lt	Top s. End Rubble wall	5.80	367.91
♀	wash	10.2	363.5
9' Rt		10.2	363.5
11' "		5.4	368.3
15' "		3.0	370.7
		6+15	
14' Rt		4.0	369.7
9' "	Top s. End Rubble wall	6.2	367.5
7' "	wash	10.2	363.5
♀	"	10.2	363.5
3' Lt	"	10.2	363.5
5' "		3.7	370.0
10' "		3.7	370.0
		6+32	
	³² Wooden Bulkhead S. End. of 4. Conc Pipes. 24" diam outlet.		
10' Lt		2.3	371.4
7' "		3.1	370.6
6' "	wash	10.0	363.7
F.L. of 4-24" Pipes		10.52	363.19
6' Rt wash		10.0	363.7
7' "		5.4	368.3
14' "		4.1	369.6

S. line El Cajon 6 + 32.32 Top of wood Bulkhead

14' RT	3.2	370.5
⊕	3.2	370.5
7' Lt.	3.0	370.7
14' Lt.	2.5	371.2

6 + 40 = S. edge emb. wall

12' 25 Lt.	2.21	371.50
⊕	2.26	371.45
13.25 RT	2.19	371.52

6 + 52.3 = S. ch. El Cajon

13.25 RT = E. End. ch. inlet. ch.	2.37	371.34
" " " " " gutter	3.39	370.32
6.25 " " " grating "	3.65	370.08
⊕	3.63	370.08
⊕ F.L. Box	10.05	363.66
6.25 Lt. = W. End. grating gutter	3.62	370.09
12.25 " = " " ch. inlet "	3.33	370.38
12.25 " " " " ch.	2.35	371.36

T.P.C.T.	7.57	279.01	2.27	371.44
B.P. B.P.			4.69	374.32

374.25

⊕ Culvert S.
S. Line of El Cajon
S.W. 33rd
+ El Cajon Blvd

3/2/38 Re. X Sec. City Police Station Site

22.45

see page 36 for original X. Sec.

1+00 South.

B.M. B.P. S.E.
Pacific + Market
T.P.

3.22 15.12
12.63 22.45
0+00 N + S = 9.

11.905 4 Geodetic
9.82 U.S. Coast

00 E+W

10.5 12.10

50' E

10.7 11.8

100 "

10.9 11.6

150 "

11.5 11.0

200 "

12.0 10.5

237.5 "

12.0 10.5

275 "

12.7 9.8 ✓

325 "

12.7 9.8 ✓

375 "

12.7 9.8 ✓

425 "

12.3 10.2 ✓

475 "

12.5 10.0 ✓

1450 S.

00 E+W

10.0 12.5

50' E

10.3 12.2

100' E

10.7 11.8

150' "

11.0 11.5

200 "

11.5 11.0

237.5 "

11.5 11.0

275 "

11.8 10.7

325 "

12.3 10.2

375 "

12.5 10.0

425 "

11.7 10.8

475 "

11.8 10.7

2400 S.

0+00 E

9.5 13.0

50' E

10.0 12.5

0+50 South.

0+00 E+W

10.5 12.0

50' E

10.9 11.6

100' "

10.9 11.6

150' "

11.8 10.7

200 "

12.2 10.3

237.5 "

12.0 10.5

275 "

12.7 9.8

325 "

12.6 9.9

375 "

12.6 9.9

425 "

12.3 10.2

475 "

12.4 10.1

22.45

2+00 South

100 E.	10.5	12.0
150 "	10.7	11.8
200 "	11.0	11.5
237 ⁵ "	11.0	11.5
275 "	12.3	10.2
325 "	11.8	10.7
375 "	11.5	11.0
425 "	11.2	11.3
475 "	11.3	11.2

2+50 South

0+00 E+W	9.2	13.3
50 E	9.8	12.7
100 "	10.3	12.2
150 "	10.6	11.9
200 "	11.1	11.4
237 ⁵ "	10.8	11.7
275 "	11.4	11.1
325 "	11.5	11.0
375 "	11.5	11.0
425 "	11.5	11.0
475 "	11.5	11.0

3+00 South

0+00 E+W	8.9	13.6
50 E	9.7	12.8
100 "	10.0	12.5
150 "	10.4	12.1

22.45

79

200 E	11.0	11.5
237 ⁵ "	10.7	11.8
275 "	11.0	11.5
325 "	11.3	11.2
375 "	11.6	10.9
425 "	11.6	10.9
475 "	11.7	10.8

3+50 S

0+00 E+W	8.6	13.9
50 E	9.3	13.2
100 "	9.7	12.8
150 "	10.1	12.4
200 "	10.7	11.8
237 ⁵ "	10.6	11.9
275 "	11.1	11.4
325 "	11.0	11.5
375 "	11.4	11.1
425 "	11.5	11.0
475 "	11.4	11.1

3+80 South

0+00 E+W	8.3	14.2
50 E	8.8	13.7
100 E	9.2	13.3
150 "	9.8	12.7
200 "	10.5	12.0

22.45

3+80. South

237.5 E	10.5	12.0
275 "	11.0	11.5
325 "	11.0	11.5
375 "	11.4	11.1
425 "	11.3	11.2
475 "	11.3	11.2

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1%. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in both

IMPROVED TABLES

AND

INFORMATION

To find Tangent and External for curve of any other degree divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external) opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

545.85
38.91

29-17
29-17
58-34

153.86
17.22
106.64

Monroe BM 1534
34^m S.E. R.P. 388.36 7.90
Wilson S.E. R.P. 391.51 3.04 } 202.43 18.
300 12.5 189-59-60 7.5
68 7.5 96-06-30 179.30 2.5
68 132.5 89-53-30 13 (218.90)
75 3 89-53-30 37.65 1.3 139.45
78 127.5 179-47 7.50
78 111.32 2.95
76 78.94 4.55
231.54 165 146.70
65 78.94 63.09
206.54 243.94 174.41 34.32
33.42 121.97 530.35 181.02
240.07 65 10.40
50 532 153.96
290.07 167.96 382.39 S.E. Monroe 49.60
142.96 25 7.78 26.44
433.03 142.46 7.28 63-12
7.4 8.5 7.0 20 20 8.74 N.W. Iowa 383.22
4 11 17 30 30 4.78
3. 32.52 388.00
7 2.25 2.25
40.0 390.77
383.22
BM + 7.20
- 6.98
44.53
BM - 4.93
4.25
68

30+20 80
25
105
25
130