

1539

POSTS

INDEX

NOTES

MICROFILMED
DEC 24 1964

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

MADE IN U. S. A.

333/2
3303
23

Our Leather Bound Engineers Note Books
are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page
the same as Left Hand Page
of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this
Book, Right Hand Page 4x4
to the inch, Center Line Red.
- No. 384 MINING TRANSIT
BOOK. Left Hand Page as in this
Book, Right Hand Page 8x8
to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this
Book, Right Hand Page 8 ver-
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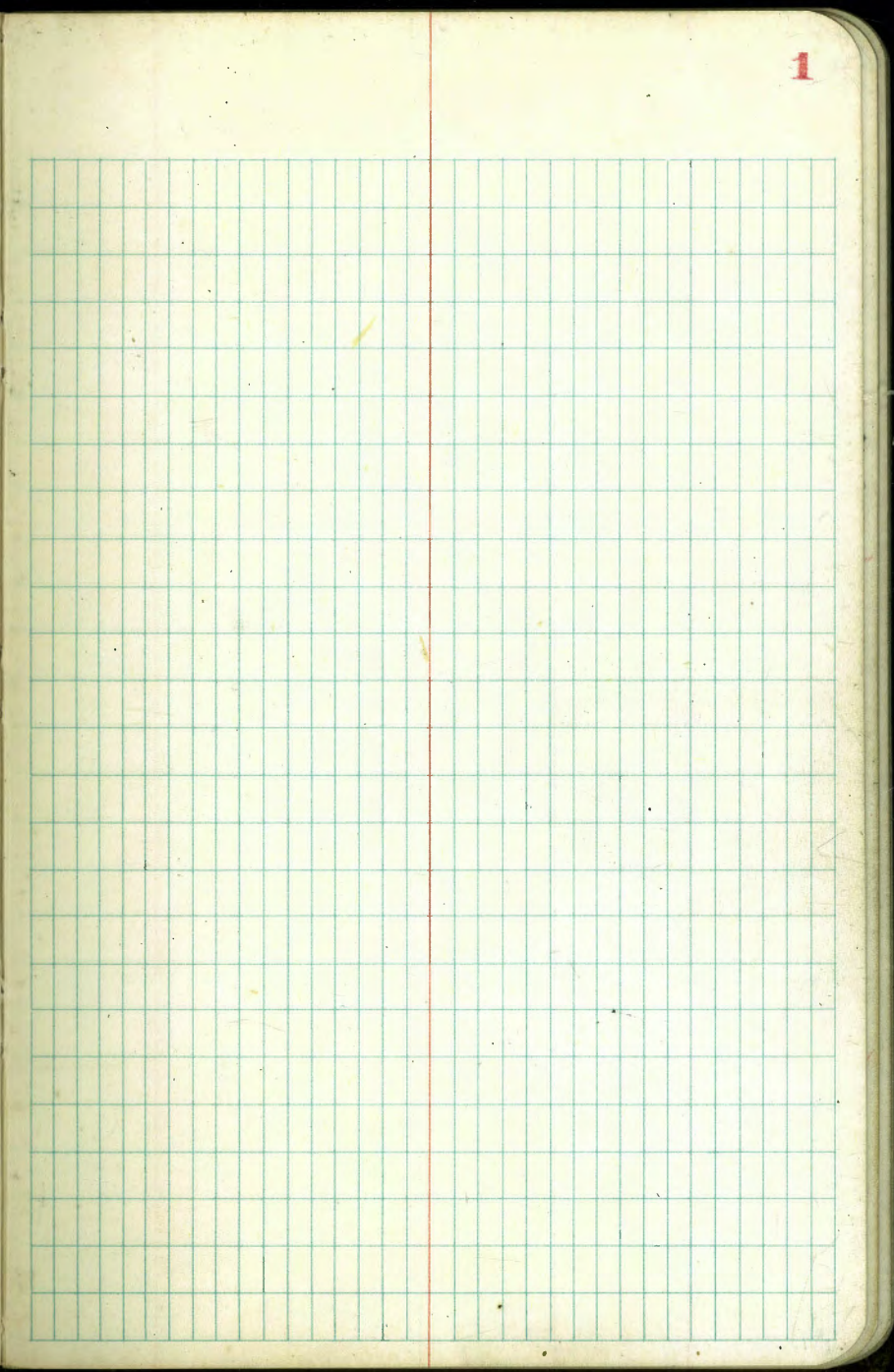
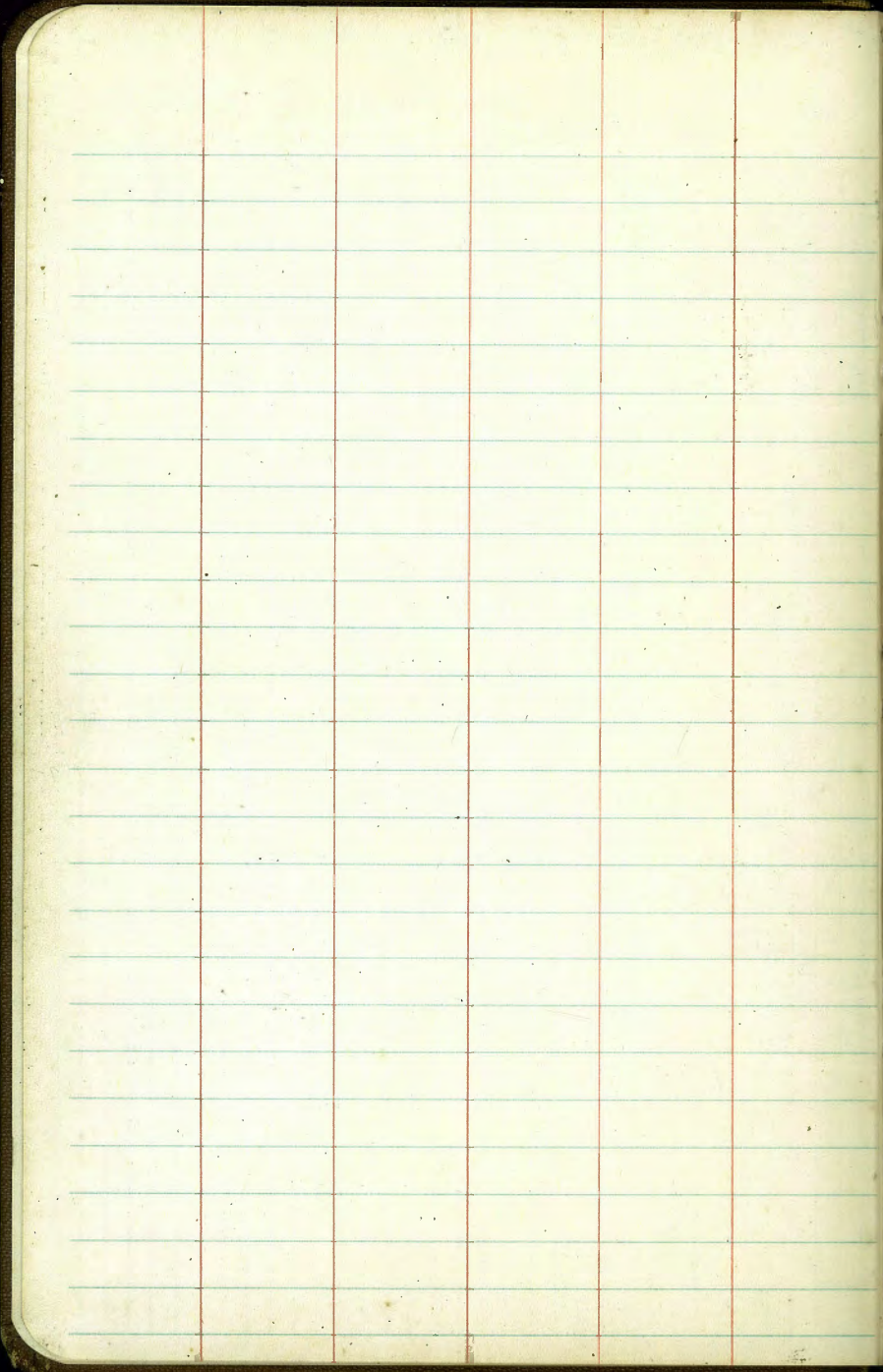
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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

P. O. Box 803

CHICAGO



3+45.29 = Ely Dove to north.

4' wide concave conc. water flume
approx 15" deep to drain inlet.

2+95.29 = Wly Dove to north

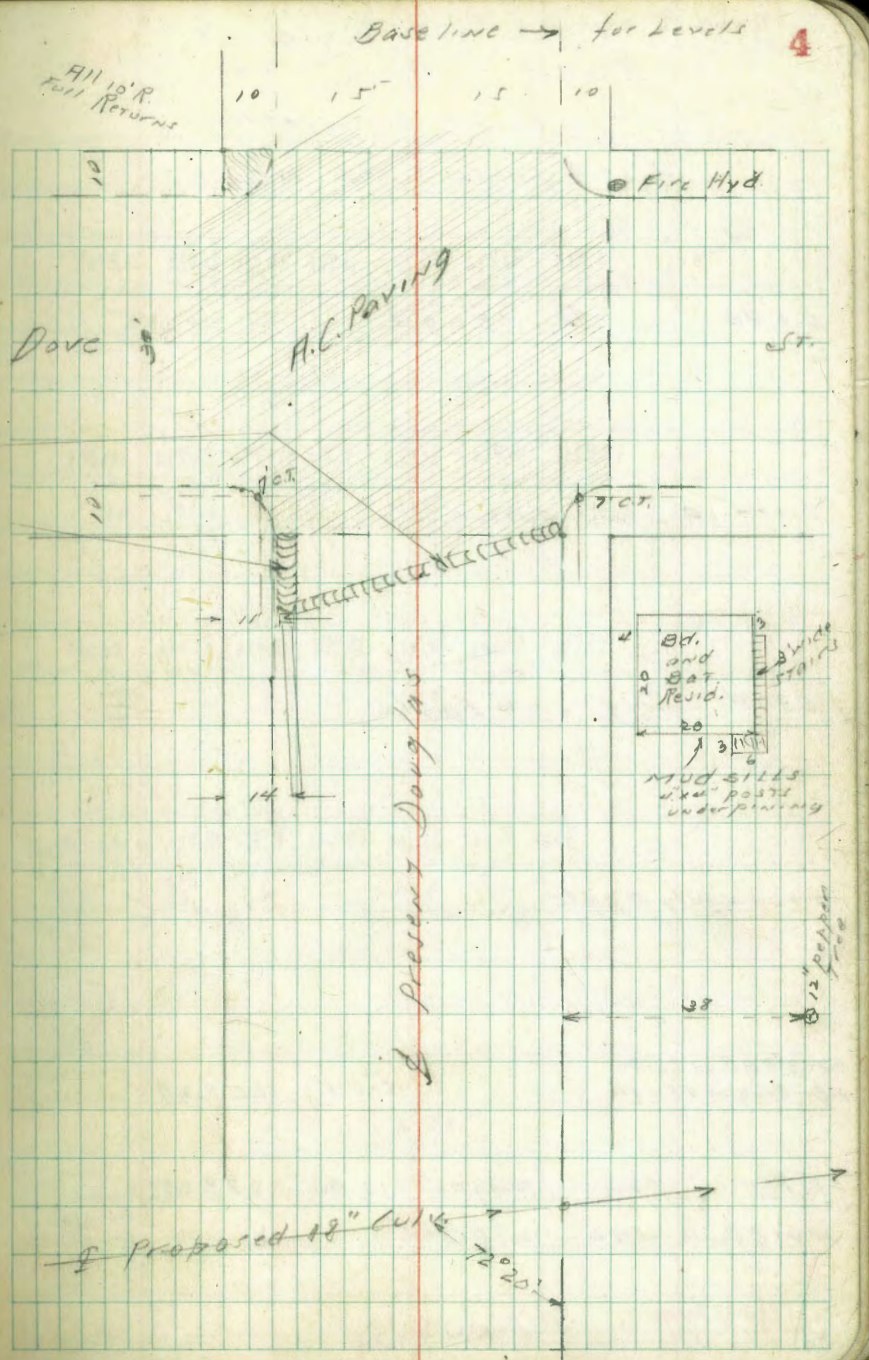
2+77 = inlet of Ex. 16" wood stave drain

2+57 = Wly end of Board and Bat. residence

2+29 = outlet of existing 16" wood stave pipe drain

2+12 12" diam. poplar tree

1+87 proposed 18" culv.



X sec. of Douglass St.
Eagle to Dove.

for proposed 30' width

Using present N.E. as 15.

0+40 Eagle

0+14.10 wly gutter

0+14 wly curb Eagle

0+00 = wly Eagle

Set B.M. B.P. in Curb
N.E. Douglas & Eagle

5.04 258.29 ✓

T.P. 5.28 263.33 ✓ 12.93 258.05 ✓

N.W. B.P. in 4.96 270.98 ✓ 266.02 Douglas Goldfinch

✓ mmo 8/16/37

L.T. = N

← Baseline = S. curb
Line of Douglas St. 5
P.T. = S.

259.47	259.18	258.85	259.11	258.89	259.48	259.11	P ✓
3.80	4.15	4.48	4.24	4.44	4.25	4.28	
60	40	30	45	45	40	40	

259.52	259.49	259.31	259.58	259.38	259.41	259.30	P ✓
4.31	3.84	4.00	3.75	4.05	3.90	4.03	
60	40	30	45	45	40	40	

260.32	260.36	259.31	259.58	259.38	260.07	259.79	P ✓
3.11	2.97	4.00	3.75	4.05	4.16	3.94	
60	40	30	45	45	40	40	

260.70	260.10	259.55	259.98	259.49	260.08	260.7	260.8	P ✓
2.63	3.23	3.78	3.35	3.84	3.75	2.0	2.5	
60	40	30	45	45	40	40	40	

for curb 06
for gutter
for curb
for lawn
for lawn

263.33 ✓

top of Headwall of drain on N.E. cor. Douglas & Eagle

✓ mmo 8/16/37

1 + 62

1 + 53 FL. 12" Conn. 1.0 P outlet

1 + 50

T.P. 0.37 248.04 12.54 247.47

1 + 28

1 + 19

1 + 12.10

200² 206² 246.71 250.81

16.0 14.2 2.5 9.2
75 62 57 53

ground
TOP
LIP
STEP

260.21

8/11/37

235.0 231.5 230.0 231.1 232.7 235.0 236.9 237.1 234.5 232.3 239.9 230.7

13.0 14.5 18.0 16.9 15.0 12.0 11.1 14.9 13.5 15.7 18.1 17.1
90 70 50 40 30 28 78 70 25 40 60 80

2349.4

18.10
27

233.5 233.4 237.0 238.6 236.0 242.8 243.2 242.9 236.8 239.7 238.3 238.9

14.5 12.0 11.0 9.4 12.0 5.2 4.8 5.1 11.2 12.3 14.7 14.4
80 60 40 25 40 28 48 26 35 40 60 80

248.04
5

244.8 248.5 250.8 255.2 256.8 255.1 247.0 246.6 244.1 244.1

32.6 19.4 11.7 9.4 5.0 3.4 5.1 13.0 12.0 10.1 14.1
85 60 40 30 25 34 15 30 40 60 UNDER
200

244.8 253.4 257.0 257.4 256.2 257.1 256.7 256.0 253.1 252.7

15.4 6.8 3.2 3.0 4.0 3.1 3.5 4.2 7.1 7.5
88 40 25 2 15 10 25 40 40 50

FL.
2.5
DRAIN

250.81 252.31 257.11 257.11 257.41 256.91

9.4 6.9 3.0 3.0 2.8 3.3
24 40 24 30 15 33

TOP
STEP
BOT
STEP

260.21

8/16/37

2 + 57

260.8	258.7	252.2	251.4	248.0	242.5	240.8	239.6	238.5	236.1	235.4
+12.8	+10.7	+4.2	+3.4	0.0	4.5	7.5	8.4	9.5	14.9	12.6
48	20	30	20	15	15	40	60	60	85	70

249.3

28
26

2 + 29 outlet fl. of 10" wood stave drain

2 + 25

218	252.0	247.0	244.2	238.5	235.6	232.5	231.5	228.6	227.9	227.6	224.8	217.8
+13.8	+4.0	1.0	5.8	9.5	12.4	12.5	12.5	19.4	20.1	20.4	23.2	30.2
65	30	40	30	25	15	15.5	15	30	40	39	60	90

2 + 05

217.5	248.0	244.5	238.6	234.4	230.5	227.0	227.9	223.4	221.5	219.9	221.3
+6.5	0.0	3.5	9.4	13.6	17.5	21.0	24.1	24.6	26.5	28.1	26.7
75	30	50	40	30	15	20	40	40	60	90	100

1 + 87 Levels taken on line of proposed cut.

233.6	230.3	230.2	229.7	229.3	226.8	225.2	222.4	220.5	217.8	217.1
14.4	13.2	17.8	18.3	18.7	21.2	22.8	25.6	27.5	30.2	30.9
90	60	45	30	20	30	50	70	95	105	

1 + 81

238.4	232.9	230.0	230.0	228.8	227.6	226.9	225.9	224.4	226.2	226.3
9.4	15.1	18.0	18.0	19.2	20.4	21.1	22.1	23.0	21.8	21.7
80	55	40	30	15	20.4	20	40	60	80	100

248.0

8/16/37

248.0

8/16/37

3 + 20.29 = F. Dove

3 + 05.29 W. cd.

2 + 95.29 = Wily Dove to North

T.P. 9.89 269.69 0.47 259.80 ✓

2 + 77

T.P. 12.30 260.27 ✓ 0.07 247.97 ✓
248.04 ✓

✓ maw 8/16/37

L.T.

Subline

R.T.

9

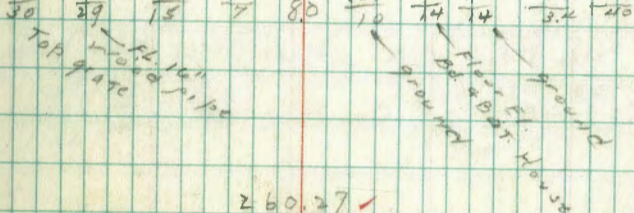
260.96 260.79 261.01 261.07 261.08 260.29
 $\frac{8.73}{40}$ $\frac{8.90}{30}$ $\frac{8.48}{15}$ 8.24 $\frac{8.21}{10}$ $\frac{9.21}{10}$

260.01 260.49 261.14 260.87 260.25 260.94 260.04 259.29 266.29 255.69
 $\frac{9.68}{40}$ $\frac{9.20}{40}$ $\frac{9.55}{30}$ $\frac{9.12}{15}$ 9.24 $\frac{9.15}{10}$ $\frac{9.05}{10}$ $\frac{10.44}{15}$ $\frac{13.2}{40}$ $\frac{14.0}{50}$

269.9 260.49 259.83 260.19 259.81 260.47 260.7 257.3 255.2 253.9
 $\frac{8.8}{40}$ $\frac{9.20}{30}$ $\frac{9.86}{30}$ $\frac{9.50}{15}$ $\frac{9.38}{15}$ 9.24 $\frac{9.0}{10}$ $\frac{12.2}{17}$ $\frac{11.5}{40}$ $\frac{13.8}{50}$

269.69

260.7 259.7 257.2 252.3 247.9 255.2 249.3 248.9 247.9 246.3
 $\frac{10.4}{40}$ $\frac{1.0}{30}$ $\frac{2.8}{29}$ $\frac{0.6}{15}$ $\frac{3.1}{7}$ 80 $\frac{10.4}{10}$ $\frac{5.1}{14}$ $\frac{11.0}{14}$ $\frac{11.4}{3.2}$ $\frac{12.4}{40}$ $\frac{14.0}{55}$



260.27 ✓

✓ maw 8/16/37

SW. Douglas
check to M.B.P. Albarross 3.27 270.63 270.53
0.10

T.P. 6.58 273.90 2.37 267.32

3+45.29 - E.A. Dove to N.

3+35.29 Ely ck Dove N/y

269.69

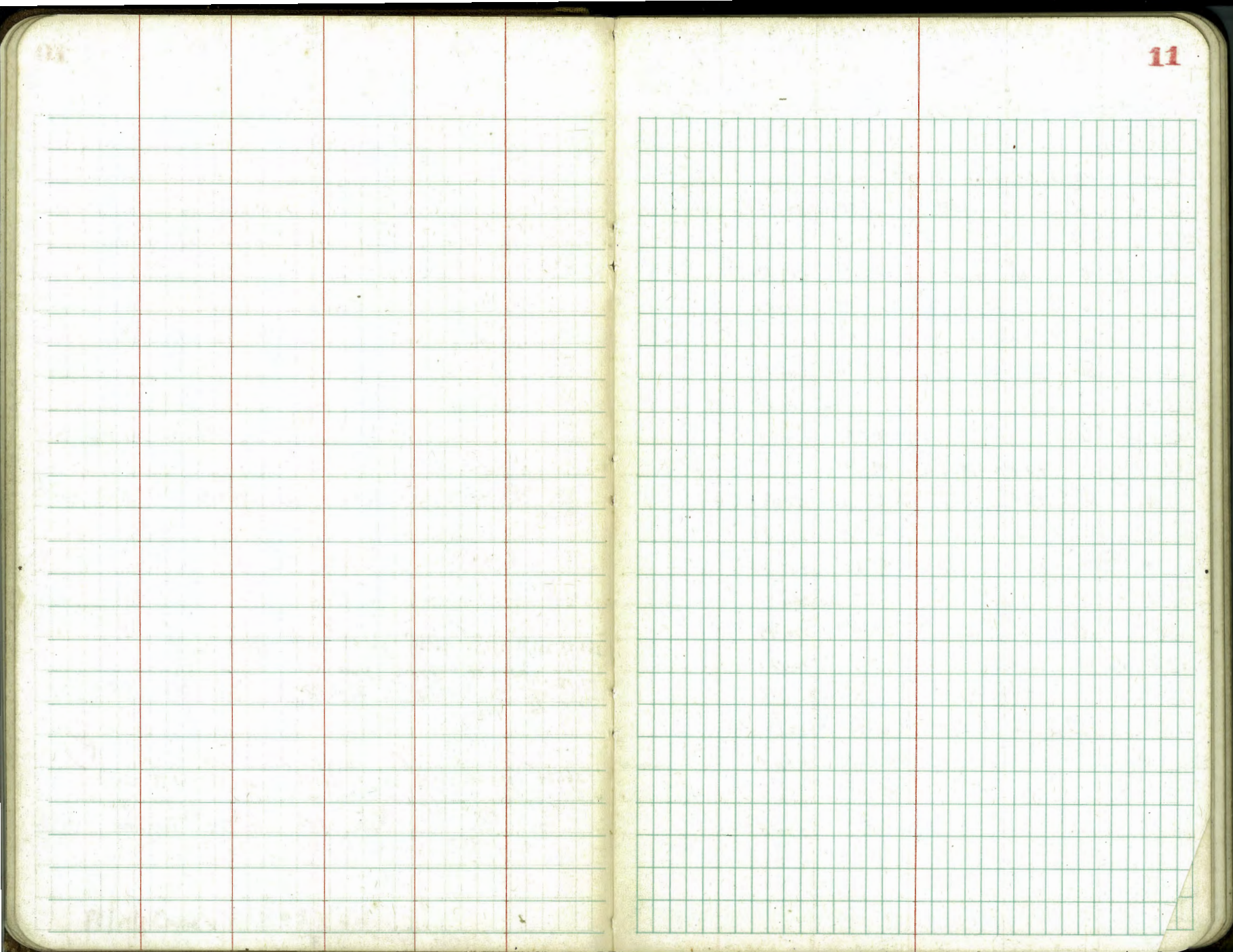
mmw 8/16/57

262.23	261.99	261.31	261.81	261.49	261.99	262.19	261.39	P
746	770	838	788	820	770	7.5	83	
40	65	30	15	907	26	10	40	

261.34	262.04	261.18	261.53	261.38	261.25	261.97	260.69	P
835	765	851	816	831	8.00	7.70	9.0	
40	40	30	15	907	10	10	40	

269.69

mmw 8/16/57



1-15-38
miller
Walker
Bliss

X See Alley BIK H7 Park Villas indexed
C.S.K.

S.W. 32^m
+ Myrtle

BM. B.P.
This B.P. Gound
Used Top of Curb.

5.34 335.69

330.35

10' S of N line = N. of Line Myrtle

W-25	dr.	5.04	330.65
W-25	G	5.61	330.08
W.	G No ch. in drive	5.77	329.92
φ	G	5.87	329.82
E	G	5.83	329.86
E	ch	5.20	330.49
E + 25	"	5.28	330.41
E + 25	G.	5.95	329.29

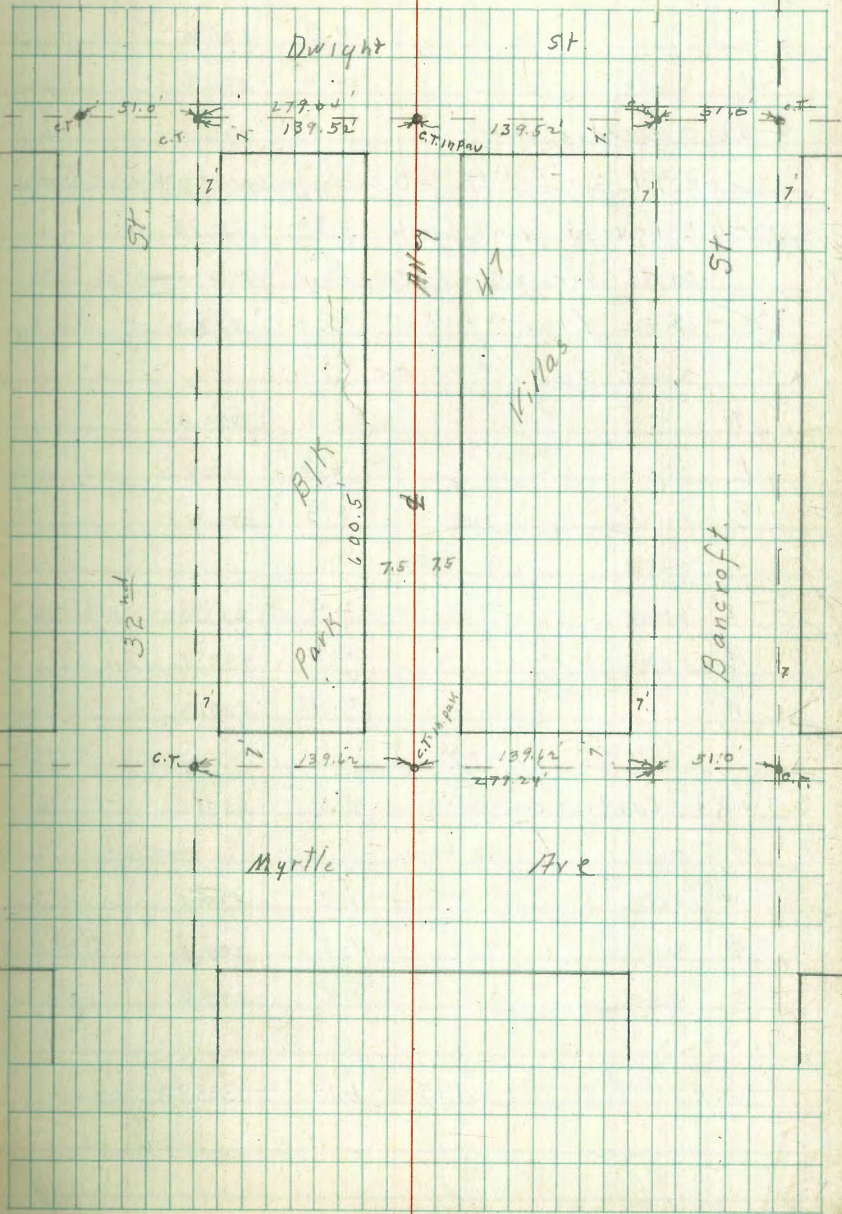
0+00 = N. Line Myrtle

E.	ch N. End.	5.01	330.68
E	pay " "	5.10	330.59
φ	" " "	5.30	330.39
W	" " "	4.97	330.72
W	ch " "	4.90	330.78
+0.5 E. edge Drive to N.		4.88	330.81

0+15

W-26 = E. Edge cut drive		4.46	331.23
W		4.6	331.1
φ		5.0	330.2
E		4.8	330.9

12



335.69

0+50

E	4.1	332.2
E	4.3	331.4
W	4.0	331.7
+ 0.6 = E edge drive	3.55	332.14

0+74 = S. End of S. Entrance garage on W. cont. floor.

W - 0.6 Drive at front of garage 2.93 332.76

0+91 garage on E. cont. floor 8.5 Back

E - 8.5 = floor 3.2 332.5

1+00

W	3.0	332.2
E	3.3	332.4
E	3.3	332.4

1+50

E	2.4	332.3
E	2.5	332.2
W	2.4	332.3

1+79

6.3 W. of E = E. End 24" cont. walk 2.1 333.6

2+00

W	1.6	334.1
E	1.8	333.9
E	1.8	333.9

T.P. 5.81 339.75 1.75 333.94

339.75

13

2+11 E Double Garage on E. cont. floor 9.8 Back

E - 9.8 = floor 5.64 334.11

2+50

E	5.1	334.7
E	5.2	334.6
+7.0 = S. End shed	5.1	334.6

2+60 N. End shed = S. End. Back Fence 0.5 in 1784 on W.

3+00 = N. End. above Fence 0.1 in 1784

W + 0.1 Fence N. End.	4.7	335.1
E Top. M.H.	4.95	334.80
E	4.7	335.1

3+50

E	4.3	335.5
E	4.4	335.4
+6.	4.4	335.4

+6.5 Drainage ditch from Here North 5.0 334.8

W 4.6 335.2

3+75

W - 5. in yard 4.6 335.2

W 4.6 335.2

+1 Drainage ditch 4.6 335.2

+2 4.0 335.8

E 4.0 335.8

E 4.1 335.2

4+00 N. End drainage Ditch

E	3.6	336.2
E	3.4	336.0
+ 6.	3.7	336.1
+ 7. drainage ditch N. End.	4.5	335.3
W	4.5	335.4
W+5 in yard.	4.5	335.3
4+25		
W-5 in yard	3.9	335.9
W	3.4	336.4
E	3.5	336.3
E	3.9	335.9
+ 0.7 W-End 24" walk.	3.70	336.05
+ 1 in yard at side of walk	4.0	335.8
4+50		
E	3.7	336.1
E	3.6	336.2
W.	3.7	336.1
5+00		
W	3.8	336.0
E	3.7	336.1
E	3.4	336.4
5+50		
E	3.2	336.6
E	3.6	336.2
W	3.6	336.2

5+67 N. End of N. Entrance garage on W. Line Brick floor

W	3.4	336.4
E	3.6	336.2
E	3.6	336.2
5+87		
E	3.7	336.1
+ 4	3.7	336.1
+ 5	4.6	335.7
E	4.6	335.2
W	4.1	335.6
5+99		
W	6.0	333.8
E	6.5	333.3
+ 3	6.1	333.7
+ 4	3.8	336.0
E	3.8	336.0
6+00 ⁵ = S. Line Dwight St		
E. ch. S. End	6.39	333.34
E Pav " "	6.50	333.25
E " " "	6.63	333.12
+ 7.3 Pav " "	6.45	333.30
+ 7.3 ch " "	6.27	333.48
10' N. of S. = S. ch. Dwight		
W. G. Pav.	7.10	332.45
E " "	7.22	332.53
E " "	7.27	332.48

XSEC. alley 20' wide.
BIR 24 O.B.

Moore
1-26-38

Indexed
C.S.K.

66.444

15

bet. Newport & Niagara, Ebers - Froude

SW SP	11.41	54.47	43.06	Newport Ebers
0-12 E curb Ebers				
N pav		6.80	47.67	
C "		6.63	42.84	
J "		6.35	42.12	
0+0 E.L. Ebers				
J cb		5.49	48.98	
J pav		5.92	48.55	
C "		6.36	48.11	
N "		6.22	48.25	
N cb		6.05	48.42	
0+05				
N		4.8	49.7	
+4		4.5	50.0	
C		4.9	49.6	
+9		4.8	49.7	
J		4.2	50.3	
T.P.	12.68	66.44	0.71	53.76
0+50				
J		8.3	58.1	
+1		9.0	57.4	
C		9.4	52.0	

+5		9.2	57.2	
N		10.4	56.0	Fence 0.2 alley
+5		11.8	54.6	
0+50				
-10		8.4	58.0	
N		6.0	60.4	
+6		4.5	61.9	
C		4.6	61.8	
+8		4.0	62.4	
J		2.5	63.9	
T.P.	12.64	78.85	0.20	66.21
1+05				
-12.7	W edge	15' g ^{dist} ft	7.65	71.20 Level
-0.7	"	4' curb, rib. apron	11.02	67.23
J			11.4	67.36
C			12.6	66.3
N	Fence	alley 0.3	12.8	66.1
+5			13.8	65.1
1+20				
-0.5			13.5	65.4
N			12.0	66.9
+5			10.0	68.9
C			10.1	68.8

78.85

S	Edge corr. ribbon	9.08	69.77
	1 + 50		
S		4.1	74.8
C		5.1	73.8
	+ 5	5.0	72.9
N		6.9	72.0
	+ 3 Top corr. Ret wall	7.27	71.58
	1 + 59		
- 3	Top wall	5.70	73.13
N		5.8	73.1
	+ 5	3.7	75.2
C		3.7	75.2
S		2.6	76.3
	+ 15 Sin. gap dir. fl.	0.8	75.1
T.P.	12.68	91.22	0.31
	1 + 93		
S		11.4	79.8
	+ 2	12.5	78.2
C		12.7	78.5
N		13.9	77.3
	+ 3 Cent. wall	14.35	76.87
	2 + 25		
- 5		12.6	78.6

91.22

16

N		10.3	80.9
C		10.6	80.6
S		10.3	80.9
	2 + 50		
S		8.2	83.0
C		8.8	82.4
N	Hedge 4' in alley	9.3	81.9
	+ 5	10.0	81.2
	3 + 00		
N	Top corr.	5.6	85.6
	+ 1.2 wall in alley	4.41	86.61
	+ 1.5	5.3	85.9
C		4.7	86.5
	+ 8	4.3	86.9
S		3.2	88.0
	3 + 50		
S		1.0	90.2
	+ 2	2.0	89.2
C		2.1	89.1
	+ 9.3	2.1	89.1
	+ 9.9 Top wall	1.14	90.08
N		2.5	88.7
	+ 5	3.7	87.5
T.P.	12.84	103.69	0.37
			90.85

S + 75			
S		10.1	90.6
N Fence in alley 0.7		10.1	90.6
C		12.9	90.8
+ 9		12.2	91.4
S		11.4	92.3
4 + 00			
S		8.8	94.9
+ 1		9.8	94.9
C		10.2	93.5
N Fence in alley 0.4		10.8	92.9
+ 5		11.2	92.5
4 + 25			
N		7.1	96.6
C		6.8	95.9
+ 9		6.8	95.9
S		6.4	92.3
4 + 50			
S		4.4	99.3
C		4.6	99.1
N Fence in alley 0.7		4.4	99.3
5 + 00			
N		0.8	102.9
C		0.2	102.5
S		0.2	102.5
T.P.	12.79	116.29	0.19
			103.50

5 + 30			
S		9.1	107.2
C		9.4	106.9
N		9.8	106.5
+ 5		10.2	106.1
5 + 50			
- 5		8.2	108.1
N		7.7	108.6
+ 6		6.2	110.1
0		6.2	110.1
S		5.5	110.8
5 + 75			
S		0.3	116.0
0		1.3	115.0
+ 5		1.4	114.9
N		4.5	111.8
+ 10		4.3	110.0
T.P.	4.35	121.99	0.65
			115.64
5 + 85			
- 10		10.5	111.5
N		7.7	114.3
+ 5		5.0	117.0
C		5.2	116.8
S		4.1	112.9

5+99 - W.L. Froude

S	curb	1.79	120.20
S	par.	2.52	119.47
C	"	3.41	118.58
N	"	4.04	117.95
N	cb	4.57	118.42

6+03

N	cb	3.68	118.36
N	par.	3.84	117.15
C	"	3.19	118.80
S	"	2.35	119.64
S	cb	1.79	120.20

6+11 W. cb. Froude

S	par.	2.36	119.63
C	"	3.24	119.75
N	"	4.15	117.84

T.P. 1.24 112.18 11.05 110.94

SWBP Newport & Froude 7.94 104.24 104.31

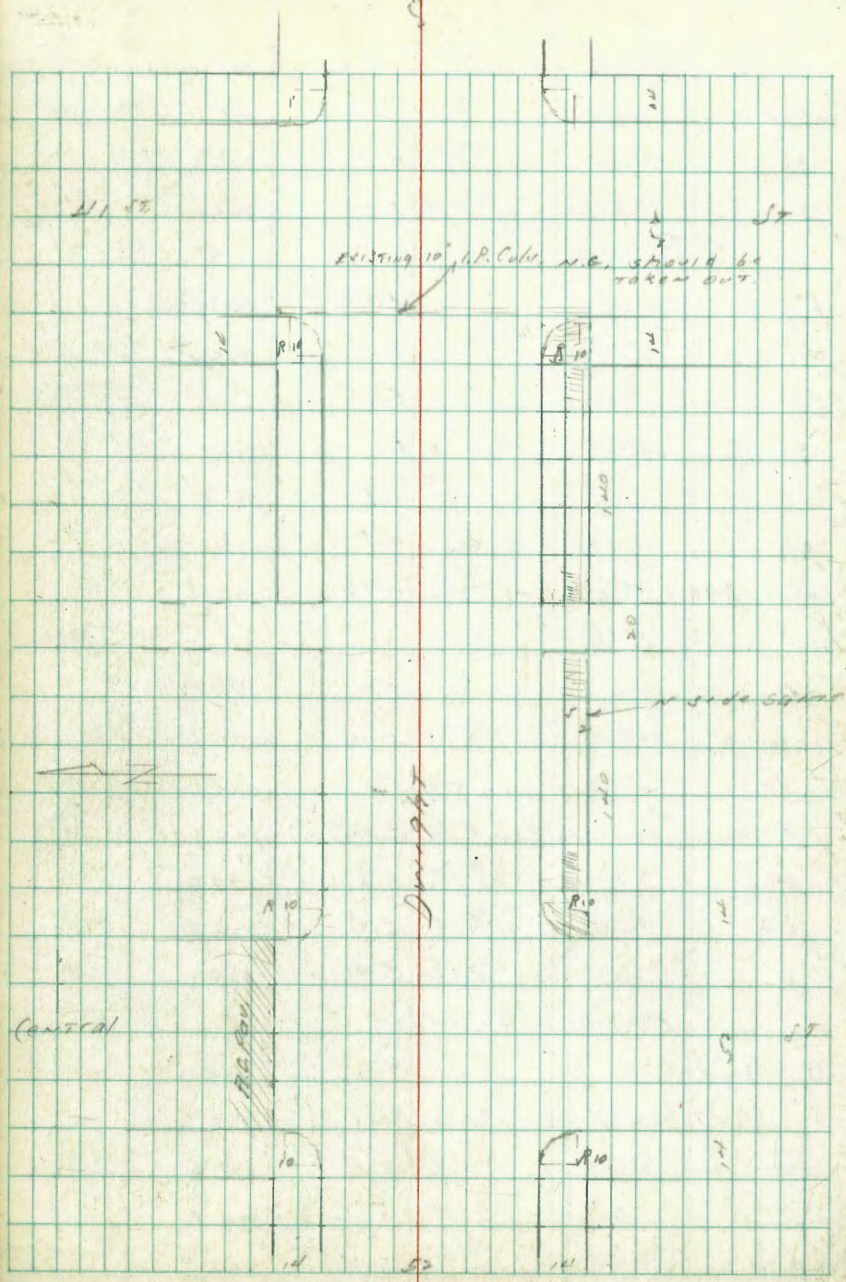
Xsec Dwight St. do side
Central to 41 57. 15' 1/2"

Place
Set
Punch
2-3-38

Indexed
CSK.

19

NW. BP	4.70	334.74	330.04	Central & Dwight
W.L. Central ✓				
1/4 ob		4.83	329.91	
1/4 cut		5.8	329.2	
1/4		5.3	329.4	
c		5.0	329.5	
1/4		5.5	329.2	
cut		5.8	328.9	
5 ob		5.38	329.36	
W ob ✓				
Pl. ob		5.29	329.35	
cut		6.0	328.7	
ob ground		5.9	328.8	
1/4		5.5	329.2	
c		5.0	329.5	
1/4		5.2	329.5	
ob		5.3	329.4	
N Pav.		5.48	329.26	
N Top ob.		4.71	330.03	
+ 20 Pav		5.44	329.37	
W 1/4 ✓				
N Pav.		5.01	329.23	
ob		5.0	329.7	
1/4		5.2	329.5	



c	5.8	329.4
1/4	5.4	329.3
cb	5.5	329.2
S	5.7	329.0
✓ E		
S	5.4	329.3
cb	5.3	329.4
1/4	5.2	329.5
c	5.1	329.6
1/4	4.9	329.8
cb	4.9	329.8
N PAV	4.76	329.98
✓ E 1/4		
N "	5.01	329.73
cb	5.1	329.6
1/4	5.2	329.8
c	5.2	329.8
1/4	5.3	329.4
cb	5.4	329.3
S	5.4	329.2
✓ E cb		
S TOP CB	5.3	329.4
S QUT	6.1	328.6
cb ground	5.8	328.9
1/4	5.4	329.1
c	5.4	329.3

1/4	5.4	329.3
cb ground	5.4	329.3
N QUT PAV	5.52	329.20
N cb	4.83	329.91
+ 20 "	5.44	329.30
✓ EL CENTRAL 100		
N TOP CB	4.87	329.87
QUT	5.4	329.3
1/4	5.5	329.2
c	5.5	329.2
1/4	5.7	329.0
QUT	5.9	328.8
S cb	5.97	328.32
✓ 0 + 50		
S cb	5.4	329.60
QUT	5.5	329.2
1/4	5.2	329.5
"	4.9	329.5
1/4	4.9	329.8
QUT	5.2	329.5
N cb	4.75	329.89
✓ 1 + 00		
N cb in drive	5.20	329.54
QUT	5.2	329.5
1/4	4.8	329.9
c	4.7	330.0

1/4		5.2	329.5
9UT		5.2	329.4
S CB		4.92	329.82
	✓ 1 + 20 = WZ alley		
S L CB	return	4.74	330.00
S "	"	4.95	329.79
S 9UT		5.2	329.5
1/4		4.9	329.5
c		4.7	330.0
1/4		4.7	330.0
9UT		4.8	329.9
N CB		4.41	330.33
N L "	return	4.30	330.49
	✓ 1 + 60 FL alley		
N L CB	return	4.38	330.36
N "	"	4.47	330.27
9UT		4.7	330.0
1/4		4.7	330.0
c		4.7	330.0
1/4		5.0	329.7
9UT		5.2	329.5
S CB		4.99	329.75
S L CB		4.90	329.84
	✓ 2 + 00		
S CB		4.87	329.87
9UT		5.1	329.6

1/4		5.0	329.7	
c		4.7	330.0	
1/4		4.5	330.2	
9UT		4.6	330.1	
N CB		4.40	330.34	
	✓ 2 + 50			
N CB		4.38	330.36	
9UT		4.6	330.1	
1/4		4.5	330.2	
c		4.7	330.0	
1/4		5.0	329.4	
9UT		5.1	329.6	
S CB		4.79	329.85	
	✓ 2 + 00 = WZ 41 ST			
S CB		4.73	330.01	
9UT		5.0	329.7	
1/4		4.7	330.0	
c		4.4	330.3	
1/4		4.5	330.2	
9UT		4.6	330.1	
N CB		4.31	330.43	
	W CB 41 ST			
N CB	NWBIP	4.24	330.50	330.55
9UT	drain FL - NKT	5.10	329.64	11 ST +
CB		4.4	330.3	DW 927
1/4		4.4	330.3	

C		4.4	320.3	
1/4		4.6	320.1	
cb		4.7	320.0	
S cb		4.79	329.95	
S	OUTLET Ft. 10" drain	5.74	329.00	
	E CB 41 ST			
S L cb		5.25	329.99	
S	gut	5.8	328.9	
cb	ground	5.8	328.9	
1/4		5.5	328.2	
C		5.8	329.4	
1/2		5.1	328.6	
cb		5.2	329.5	
	gut	5.1	328.6	
N L cb		4.79	320.01	?
	E L 41 ST			
N cb		4.80	329.94	
gut		5.9	329.4	
1/4		5.3	329.4	
C		5.9	329.4	
1/2		5.5	329.2	
S gut		5.8	328.9	
S cb		5.21	329.53	

X sec of alley 15' wide
 BIK 7 Harold N. Park
 " B McFadden & Burton

bet. Green & 31st Lands to Wightman

Moore
 2-3-38

Indexed
 ask.

Re cross Sectioned
 FB 2069
 29

23

SEOP 4.50 345.41 340.91

Lands
 a
 Fay

N.L. Land = 0.0

W cb 4.22 341.19

W Pav. 4.35 341.06

" 4.56 340.85

E " 4.83 340.08

E cb 4.24 341.17

0+03

E 2.6 342.8

W 3.9 341.5

C 3.9 341.8

W 3.5 341.9

at 16

- 8 I 8' cone drive to 90°
 SOUTHWEST ENTRANCE 1.68 343.73

W 2.3 342.1

C 2.1 343.3

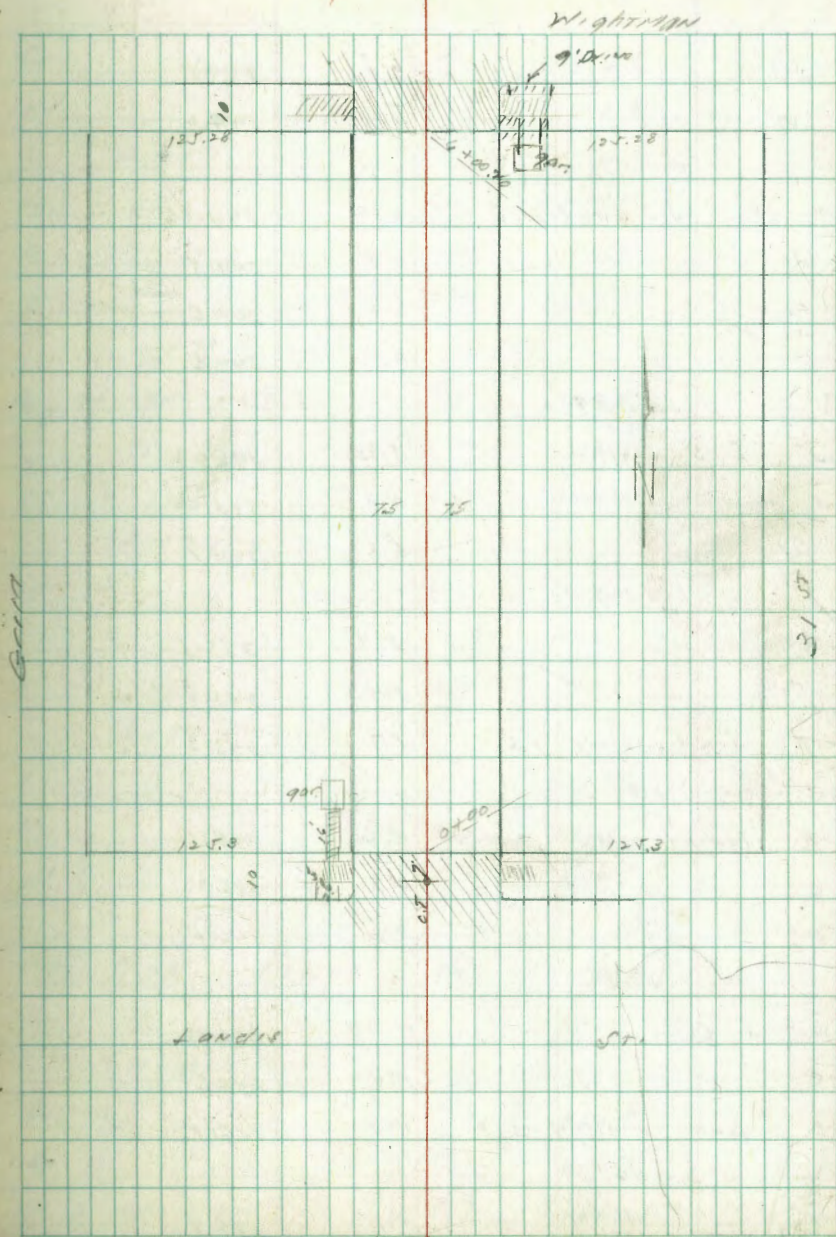
to 2.1 343.3

E 1.4 344.0

T.P. 7.07 350.96 1.52 343.89

0+40

E 6.4 344.6



H+00			
E	7.2	350.9	
C	7.2	350.9	
W	7.3	350.8	
H+50			
W	6.3	351.5	
C	6.3	351.5	
E	6.2	351.9	
J+00			
E	5.4	352.7	
C	5.4	352.7	
W	5.5	352.6	
J+25			
W	4.8	353.3	
C	4.8	353.3	
E	4.8	353.3	
+ 3.5	Gas. corr. fl.	4.89	353.18
J+38			
W	4.7	353.4	
+ 4	double gas corr. fl. level	5.05	353.02
J+57			
E	4.6	353.5	
C	4.7	353.4	
W	4.7	353.4	
J+89			
W	5.3	352.8	

C	5.3	352.8	
E	5.0	352.1	
TP	4.27	356.92	5.41 352.66
J+89			
E + 5	Gas. corr. fl. to gas.	5.67	352.20 No entrance
W+00.2 SL W, 9.5 IN W.			
E cd		5.37	351.56
E par.		5.52	351.41
C		5.82	351.11
W		5.74	351.19
W cb		5.57	351.36
SEBP	Ray + Nightman	5.27	351.66 351.68

XSEC BIK 4 W. White Pt 15' wide
bet 42nd & Copeland

El Cajon to Meade

NWBP	510	369.76	364.66	12nd Meade
				SL Meade = 0+00
W cb		4.98	364.78	
W par		5.25	364.81	
C		5.40	364.36	
E		5.32	364.44	
E cb		5.08	364.65	
				0+20
E		4.5	365.3	
C		4.7	365.1	
W		4.9	364.9	
				0+47
-7.5	Six gar corr.	4.80	364.96	
W		5.0	364.8	
C		4.7	365.1	
E		4.5	365.3	
				1+00
E		5.0	364.8	
C		4.9	364.9	
W		5.1	364.7	
				1+16
W		5.0	364.8	
C		5.0	364.8	
E		5.2	364.6	

Indexed
c.s.k.

369.76.

Moore
2-3-38

26

				1+16		
E	+9	Six gar corr.	5.32	364.44		
						1+23
E			5.1	364.7		
C			4.9	364.9		
W			5.1	364.7		
+1		hand corr. apron	4.90	364.86		
+35		double gar.	4.65	365.11	corr. fl.	
						1+50
-3.5		S end double gar.	4.95	365.11		
-1		corr apron	4.85	364.91		
W			5.1	364.7		
C			5.1	364.7		
E			5.1	364.7		
+3		E corr apron	4.98	364.78		
+10		Six gar corr.	4.87	364.89		
						1+87
E			5.3	364.8		
C			5.2	364.6		
W			5.4	364.4		
+4		along corr. apron	5.91	364.45		
+7		gar corr. fl	5.20	364.56		
						2+03
-7		S end gar	5.20	364.56		
-4		S corr apron	5.30	364.46		
W			5.3	364.5		

		5.2	364.6	
E		5.2	364.6	
+ 5.5	♀ com. apron	5.00	364.76	
+ 10	sin gar cent. fl.	5.00	364.76	
	2 + 2x			
- 10	♀ sin gar. cent. fl.	4.92	364.84	
- 4	com apron	5.09	364.67	
E		5.2	364.6	
e		5.1	364.7	
W		5.3	364.5	
	2 + 50			
W		5.5	364.3	
C		5.3	364.8	
E		5.2	364.6	
+ 3	sin gar dirt	5.1	364.6	
	2 + 00			
E		5.1	364.6	
C		5.1	364.6	
W		5.4	364.4	
T.P.	4 + 1	369.07	5.10	364.66
	2 + 50			
W		4.3	364.8	
C		4.5	364.6	

E		4.3	364.5
	3 + 57		
- 9	♀ sin gar. cent. fl.	4.11	364.96
E		4.3	364.8
C		4.2	364.9
W		4.2	364.9
	3 + 92		
W		4.4	364.9
C		4.2	364.9
E		4.0	365.1
+ 9	♀ com. apron	3.96	365.11
+ 15	♀ sin gar cent. fl.	4.02	365.08
	4 + 25		
E		4.7	364.4
E		4.7	364.4
W		4.5	364.6
	4 + 50		
W		4.3	364.8
C		4.6	364.5
E		4.4	364.7
	5 + 00		
E		4.4	364.7
C		4.9	364.2
W		4.4	364.5

369.07

5725

W 4.4 364.7

C 5.0 364.1

E 4.5 364.6

5750

E 4.2 364.9

C 4.7 364.4

+H 4.5 364.6

W 3.8 365.3

5775

W 3.8 365.3

+S 4.7 364.4

C 4.8 364.3

E 4.4 364.7

6400

E 4.5 364.6

C 4.7 364.4

W 4.7 364.4

6407.70 = N.L. El CAYON Ave

W c6 4.78 364.79

W pav 4.94 364.13

C " 5.82 363.95

E " 5.19 363.86

E c6 5.02 364.05

369.07

28

6437.40 N curb El CAYON

E 5.76 363.21

C 5.82 363.25

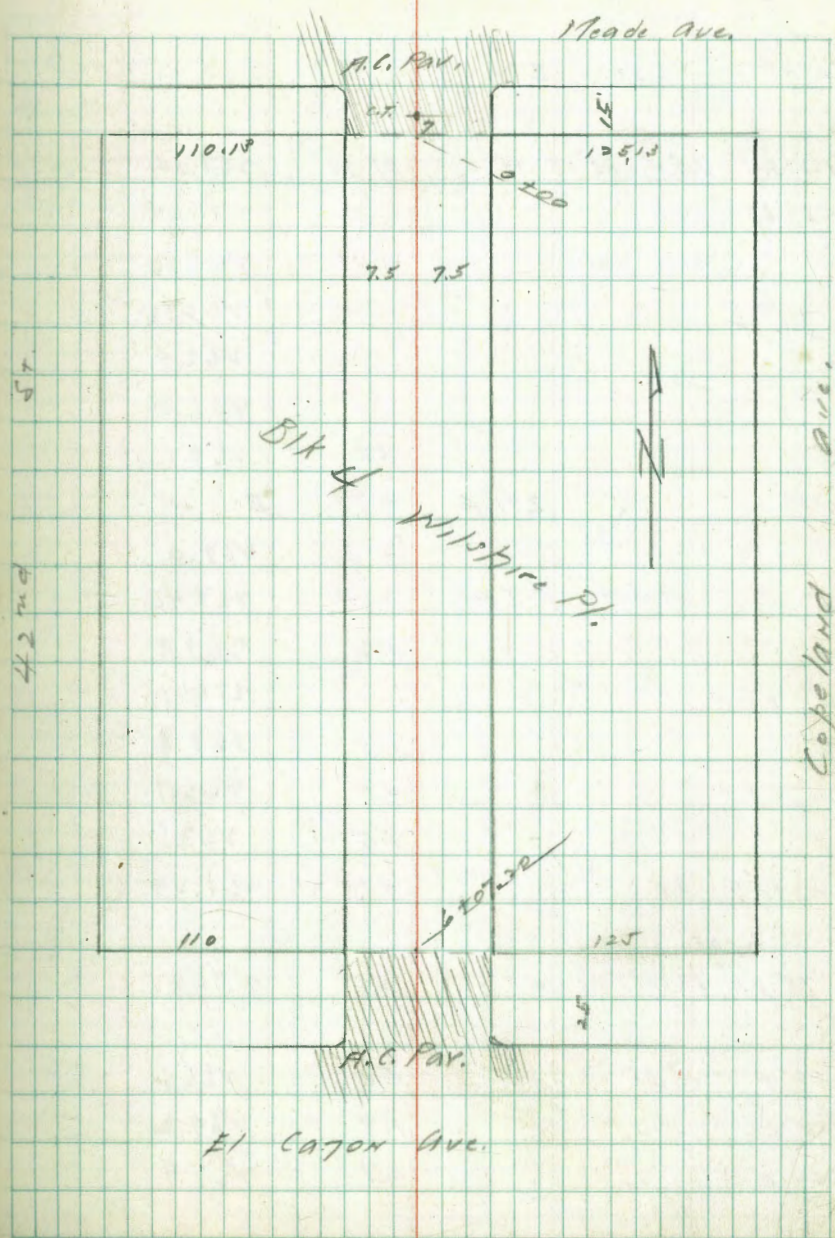
W 5.76 363.31

TIP 497 369.01 5.03 364.04

SWBP 42nd El CAYON 4.50 364.51 363.96

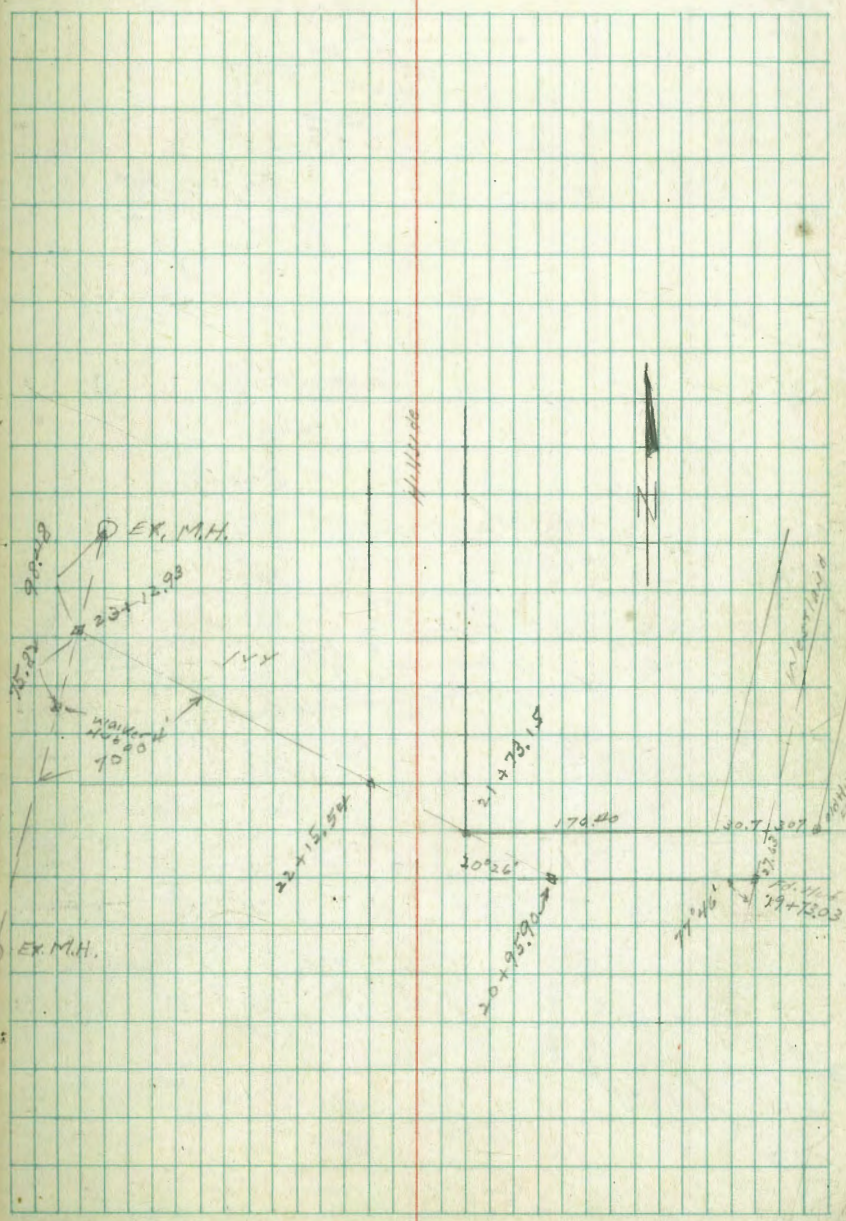
SWBP Marlborough 4 El CAYON 3.68 365.33 365.14

See next page for sketch



Change of Sewer (B)
at Ivy + Hillside

207 STUB 7+30	0.84	248.50		247.68	Sec 1316 P 78.
20+95.90 - S 20°26' N			10.47	237.83	7+87.87 STUB
T.P.	910	235.98	12.62	235.88	
21+25			4.6	232.4	8+16.97
+50			9.3	226.7	8+41.97
T.P.	0.27	223.73	12.52	223.46	
21+73.15 MECOR ^{IVY} Hillside.			4.1	219.6	8+65.14
T.P.	012	210.84	13.03	210.70	
22			3.0	207.8	8+91.97
+15.54 SW Cor ^{IVY} Hillside			9.85	201.47	9+07.51 HUB
T.P.	0.04	198.21	12.65	198.17	
+50			11.6	186.6	9+41.97
T.P.	0.30	185.67	12.84	185.37	
+65			5.3	180.4	9+56.97
+80			12.4	173.3	9+71.97
T.P.	532	178.42	12.57	173.10	
+90			4.6	171.8	9+81.97
+96			8.5	169.9	9+89.97
22+02			6.5	171.9	9+93.97
23 +1293 - S Ex. Sewer			7.21	171.11	10+02.90
98.48 N M.H. RM			1.08	177.34	177.28



BM. B.P.	113	29.18	28.05	N.W. Bessemer + Rosecrans
T.P.	2.42	23.27	8.33	20.85
00-275 ^S	Ex M.H. Rim	San Antonio Pl.	11.70	11.57
00-245 ^E	4 " F.L.		20.95	2.32 Profile 2.41
0+00	C.T. Pav. Δ		1.89	21.38
E. 1st of Sta 0+03 =	Ex M.H. Rim		1.77	21.50
" " "	" " " " F.L.		13.77	9.50
set. B.M. Mon	Line	San Antonio Place at R.C. East s. of Bessemer	3.76	19.51
0+52	pav. s. End	San Antonio Pl	0.72	22.55
0+52 ^E	Curb " "		0.41	22.86
T.P.	1.59	24.69	0.17	23.10
0+73			1.8	22.9
1+00			4.4	20.3
1+53 ⁸⁶	on Lot Hub		5.92	18.77
2+00			7.2	17.5
2+50			7.9	16.8
3+00			7.2	17.5
3+50			8.4	16.3
4+00			10.9	13.8
4+55 ⁵⁷	Hub. N. Line	P.L. 175	12.27	12.42
T.P.	10.67	23.09	12.27	12.42
5+06			11.2	11.9
5+07			13.4	9.5
5+14			16.0	7.1
5+19			11.2	11.9

5+55	φ		9.5	13.6
5+55	φ	7.8.4 φ = W. side of N. Entrance of (Garage - ent floor)	10.2	12.9
5+55	φ	30' S. of φ Ground. N. of House	10.8	12.3
6+14	φ		6.3	16.8
6+14	φ	4' S. of φ ent. patio B. side House	9.32	13.77
6+14	φ	20' S. of porch floor " " "	8.13	14.96
6+40	φ		5.1	18.0
6+93 ²⁷	φ	Spk 3' S. of L. + Line	4.21	18.38
7+03	φ		4.8	18.3
7+04	φ		3.6	19.5
7+50	φ	15' E of φ at 7+04	7.3	15.8
7+50	φ		3.9	19.2
7+50	φ	12' E of 7+50	6.2	16.9
8+00	φ		3.7	19.4
8+50	φ	5' E of 8+00	4.9	18.2
8+50	φ		3.3	19.8
8+50	φ	5' E of 8+50	4.4	18.7
T.P.		10.06	30.49	2.66
9+00			12.3	18.2
9+20 ¹⁶	Hub. N. Line	Rogers St.	11.85	18.64
9+50			10.8	19.7
9+75			9.8	20.7
9+85			10.9	19.6
10+00			11.0	19.5
10+25			10.3	20.2

5' Lt of sta 10+25	11.4	19.1
10+50	6.2	24.3
8' Lt. of sta 10+50	10.7	20.3
T.P. 11.86	34.90	7.45 23.04
0+00 H. Line = 6+93 ²⁹ Main Line		
H. Line 3' S. of Lot Line		
0+00	16.52	18.34
0+50	9.8	25.1
T.P. 12.84	45.86	1.84 33.02
0+97 = E. Line Rosecrans (E. edge of cut. ch.)	9.72	36.14
0+97 ⁶ Gutter Pav	10.15	35.71
0+99 ⁶ cross 2.5' wide E. Line		
1+17 W. edge Pav	9.10	36.76
1+46 ² gutter	9.8	36.1
1+47 ²⁵ W. Line Rosecrans (S.W. edge of cut. ch.)	8.87	36.99
1+56	8.5	37.4
1+58	3.0	42.9
7' Lt of 1+58 graded dirt Drive	8.0	37.9
22 " " 1+58 S. side Drive	8.0	37.9
T.P. 12.50	58.36	0.00 45.86
	1+80	
φ	12.7	45.7
8' Lt	13.6	44.8
7' " N. side Drive	14.5	41.9
22 " S. side of Drive	16.5	41.9
Grade of Drive acc. to Cut stake	17.0	41.4

2+30

φ	3.5	54.9
2' Lt	3.8	54.6
3' " N. side of Drive	7.8	50.6
22 " S. side of Drive	7.7	50.7
Grade of drive acc. to cut stake	8.3	49.1 50.1
T.P. 12.90	70.97	0.29 58.07
	2+80	
φ	9.0	62.0
+2 Lt N. side Drive	11.9	59.1
+22 Lt S " "	11.9	59.1
Grade of drive acc. to Cut stake	12.3	58.7
	3+30	
φ	0.0	71.0
+3 Lt N. side Drive	3.7	67.3
22 " S " "	3.4	67.6
Grade of Drive acc. to Cut stake	3.7	67.3
T.P. 12.83	83.78	0.02 70.95
	3+79 I = W. Line	94.174
φ = 3' S. of lot line	1.3	85.1
7' Lt	0.0	83.8
12 Lt = N. side of Drive	7.4	76.2
22 Lt = S " " "	8.0	75.8
Grade acc. to Cut stake	8.0	75.8
T.P. 12.60	94.98	1.40 82.38

"D" Line

94.98

0+03				
2 L. S of 0+00		18.2	76.8	
0+12		18.7	76.3	
0+17		11.0	84.0	
0+24	3' W of E Line of PL 174	9.4	85.6	
	0+00 3' S. of E PL 175			
0+47		5.3	89.7	
0+23 N		3.7	91.3	
0+62		2.2	92.8	
0+38 N		3.0	92.0	
0+89		2.4	92.6	
0+65				
1+11				
0+87				
1+24				
1+00				
T.P.	12.92 105.41	2.49	92.49	
1+47		14.1	91.3	
1+23		12.4	92.6	
1+62		9.2	96.2	
1+38		7.9	97.5	
1+84		4.06	101.35	on Moh
1+60				
2+10.6				
1+86.6	S. Line Finney Lot			
2+60.6				
2+36.6	NE Cor PL 174			
T.P.	12.87 117.23	1.05	104.36	
T.P.	13.19 130.42	0.00	117.23	
Top. M.H.	0+00 F.B. 1519-35	11.00	119.42 = 119.08	
T.P.	12.40 142.69	0.13	130.29	
T.P.	12.53 154.96	0.26	142.43	
T.P.	7.95 160.78	2.13	152.83	

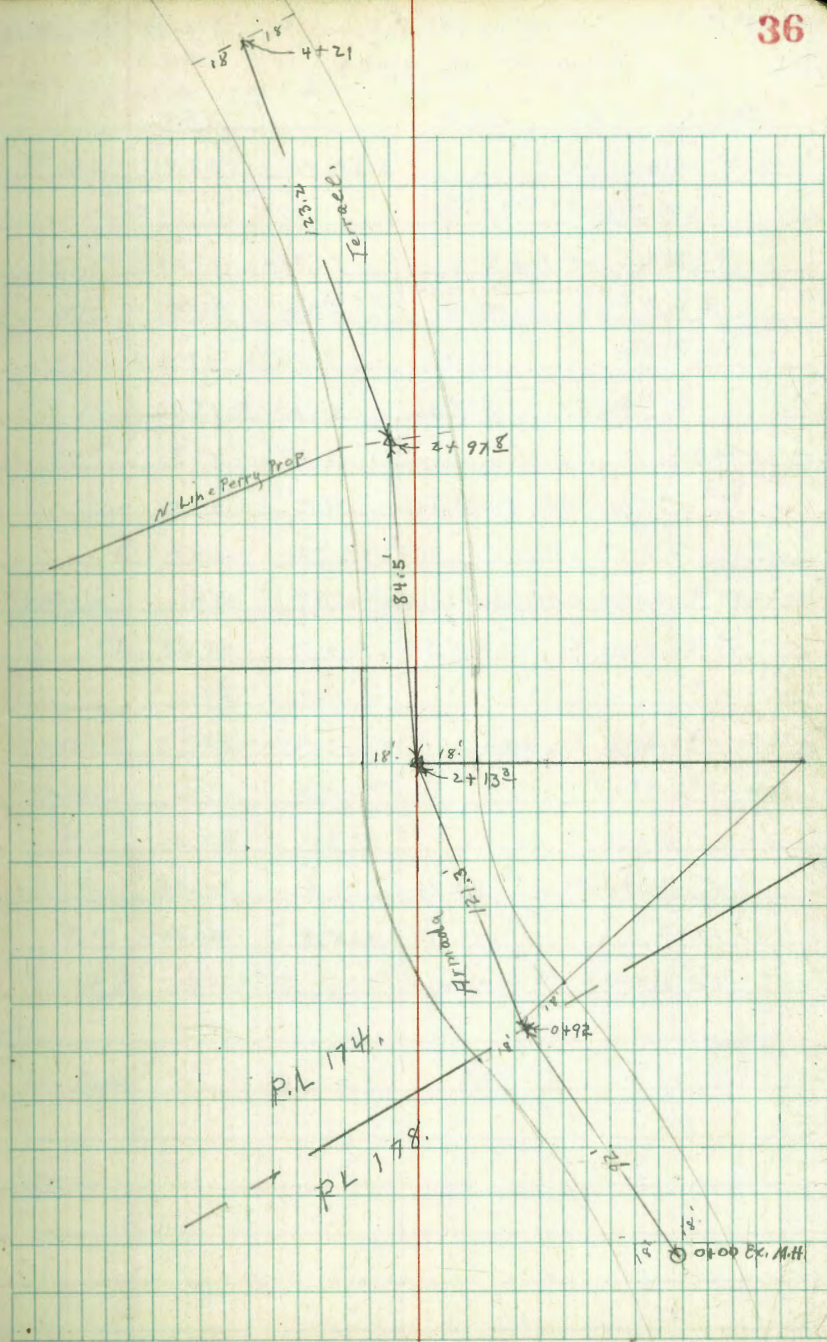
-B. Line
New Stations

= 0+00

0+09	
0+14	
0+21	
0+24.5 Lot. line	
0+44	
0+57.6 M.H. 0+00 E Line	
0+59	
0+86	
1+08	
1+21	
1+44	
1+59	
1+81	
2+07.6	
2+57.6	

4-5-38 Sewer Levels Armada Terrace from ex.
M.H. at Armada bet. Lots 445 Cuesta Loma South

		π/60.78		
0+00	Ex M.H.	Rim	5.55	155.23
11	" " "	F.L.	11.45	149.33
0+92	chd. #1	N. Line P.L. 174 S. End Pav. Δ	6.14	154.64
13	W of 0+92	ent. d.	5.98	154.80
13	" " "	" "	6.45	154.33
1+50			5.8	155.0
2+13 ³ _{4.5}	at Armada	at P.C. Δ	4.50	156.28
2+97.8	Δ		2.05	158.73
4+21.0			4.25	156.53



0+99² "C" Line from 0+99² "A" Line to

"C" Line

3+87 "C" Line = 00-21 "B" Line

"B" Line

"D" Line 2' E of W. Curb of Rosecrans St.
from 1+51² "C" Line = 0+00 "D" Line to + "D" Line

T.P. Page 34	0.00	45.86		45.86
0+99 ² } 2.5' W. of 6. Line Rosecrans. Cross Δ 24.00 ft. 2.0' W. of E. Curb Rosecrans 3.0' S. of Lot Division Line	10.05			35.81 on Pav.
1+19 ² W. Edge Cont. Pav.	8.77			37.09
0+00 } 2' E of W. Curb Rosecrans. 1+51 ² stub } 2' N. of S. side 25' Drive	8.92			36.94
0+10.4 1+62 ²		8.0		37.9
T.P.	12.50	58.36	0.00	45.86
0+32.9 1+84.3			14.5	41.9
0+32.9 1+84 ²	Grade of Alley Acc. to Stake		17.0	41.4
0+82.9 2+34 ²			7.7	50.7
0+82.9 2+34 ²	Grade of Alley acc. to Cut Stake		8.3	50.1
T.P.	12.90	70.97	0.29	58.07
1+32.9 2+84 ²			11.9	59.1
1+32.9 2+84 ²	Grade of Alley acc. to Cut Stake		12.3	58.7
1+82.9 3+34 ²			3.4	67.6
1+82.9 3+34 ²			3.7	67.3
T.P.	12.83	83.78	0.02	70.95
2+32.6 3+84 ²			8.0	75.8
2+35.6 3+87 ²	0+00 "F" 0+00 "B" Line New			

T.P. Page 34	1.77	47.63		45.86
0+00 "D" Line = 1+51 ² "E" Line	3+21	10.69		36.94 stub
0+47.5 "D"	3+68.5	8.8		38.8
2' W. of 0+47.5 "D" = curb of Menl		7.51		40.12
1+00 "D"	4+21	6.7		40.9
1+30 "D"	4+51	5.6		42.0

"E" Line From 3+87² "C" To serve (Norris) (Schieffer) Lot

T.P. Men NE 3 PL 174	13.10	114.45		101.35	Page 35
T.P.	12.67	120.07	2.05	112.40	
0+82.9 "E"	S. E. Cor Norris Lot.	2.04		118.03	on Pin.
0+60		9.5		110.6	
T.P.	0.24	107.71	12.66	102.77	
0+25		6.7		101.0	
T.P.	0.20	95.20	12.71	95.00	
0+00 "E" = 0+57 ² "B" New Sta		4.0		90.8	

T.P. Pipe 1.54 87.24 9.50 85.70 W. Line Clr P.L. 175

"F" Line
"C" Line

	87.24			
2+35.6 st 00 "F" = 3+87 "C"	10.38	76.86	on stub	
2+93.6 0+58	5.0	82.2		
2+88.6 0+63	7.1	80.1		
3+01.6 F 0+66 stub = arco G.	4.82	82.42		

T.P. 12.93 99.79 0.38 86.86

3+21.6 0+86	5.0	94.8		
3+32.66 0+98 "F" = N.P. Cor Schieffer	0.17	99.62	on pin	

"G" Line = bottom of canyon

	87.24			
0+00 "G" = 0+66 "F"	4.82	82.42	stub	
T.P.	12.93	99.79	0.38	86.86
0+29	13.0	86.8		
0+35	11.8	88.0		
0+53	7.5	98.3		
0+67	0.5	99.3		
5' ht of 0+67 ditch	3.3	96.5		
0+77	0.2	99.6		
3' ht of 0+77 = ditch	1.6	98.2		
1+00	+5.2	104.0		
3' ht. of 1+00 ditch	+3.3	103.1		
1+10 & = ditch	+5.3	105.1		

"A-1" Line

5.35 23.73 18.38

7+03	5.0	18.7
7+04	3.8	19.9
+50	5.0	18.7
+58	5.8	17.9
8+00	5.6	18.1
+50	5.1	18.6
9+00	5.7	18.0
+06	7.3	16.4
+10	5.7	18.0
+50	5.1	18.6
+72	6.0	17.7
+73	9.0	14.7
+82	12.0	11.7
+87	5.7	18.0
10+00	5.8	17.9
10+50	3.7	20.0

N.G.
Use line on page 33.

"C" Line $\frac{1}{2}$ 20' Easement
 Prelim Sewers. from 5+38⁶ "H"
 W to Rosecrans. & S to 0+00 "D"

"B" Line

B.M. $\frac{1}{2}$ Hub 4+55⁵⁷ 8.97 21.39 12.42 N. Line R.L. 175

bet 0+00 & 0+95 "C" Line there is a rough loose
 fill approx. 15' wide

0+00 "C" = 5+38⁶ "H" Line

10' Rt.	Nat. Gr.	9.3	12.1	
$\frac{1}{2}$	"	8.8	12.6	✓
10' Lt.	"	8.5	12.9	

0+05

10' Lt.	N. g.	7.2	14.2	
$\frac{1}{2}$	Fill	5.3	16.1	(13.5)
10' Rt.	N. G.	8.7	12.7	

0+29

10' Rt.	N. g.	4.4	12.0	
4' Rt.	Fill.	2.0	19.2	
$\frac{1}{2}$	Nat. Gr.	4.0	17.4	✓
10' Lt.	" "	3.6	17.8	

F.P. 10.23 31.48 0.14 21.25

0+45

8' Lt.	Nat. Gr.	11.2	20.3	
$\frac{1}{2}$	Fill	6.5	25.0	(4.5)
10' Rt.	Nat. Gr.	13.0	18.5	

31.48

0+60

47.7
 $\frac{97}{144.7}$

6+32⁵⁴
 $\frac{17}{17}$

39

17' Rt.	Nat. Gr.	11.0	20.1	
10' "	Fill	5.7	25.8	
$\frac{1}{2}$	"	4.5	27.0	(21.9)
6' Lt.	"	5.5	26.0	
8' "	Nat. Gr.	9.0	22.5	
0+71				
8' Lt.	Nat. Gr.	7.1	24.4	
$\frac{1}{2}$	Fill	0.0	31.5	(20.6)
10' Rt.	"	3.6	27.9	
17' Rt.	Nat. Gr.	8.3	23.2	
T.P. 10.60 40.30 1.78 29.20				
0+85				
10' Rt.	Fill	9.2	31.1	
$\frac{1}{2}$	"	5.7	34.6	?
8' Lt.	Nat. Gr.	8.7	31.6	
0+97 = E. Line Rosecrans.				
0+97 ²	Top. e.d.	8.80	31.5	
0+97 ²	Gutter Pav	9.36	30.94	
1+17	W. Edge Pav.	8.40	31.9	
1+44 ²	2 Lt. 25 E. of W. Line Rosecrans	8.2	32.1	
2' W. of 1+44 ²	Top. v. ch.	7.86	32.44	
2+00	$\frac{1}{2}$	7.3	33.0	
2' W. of 2+00	Top. v. ch.	6.11	33.69	

40.30

2+50

6.0

34.3

3+00

4.8

36.0

3+21 stub (6+00 D line)
1+51 1/2 }

3.33

36.97

36.94

Page 37

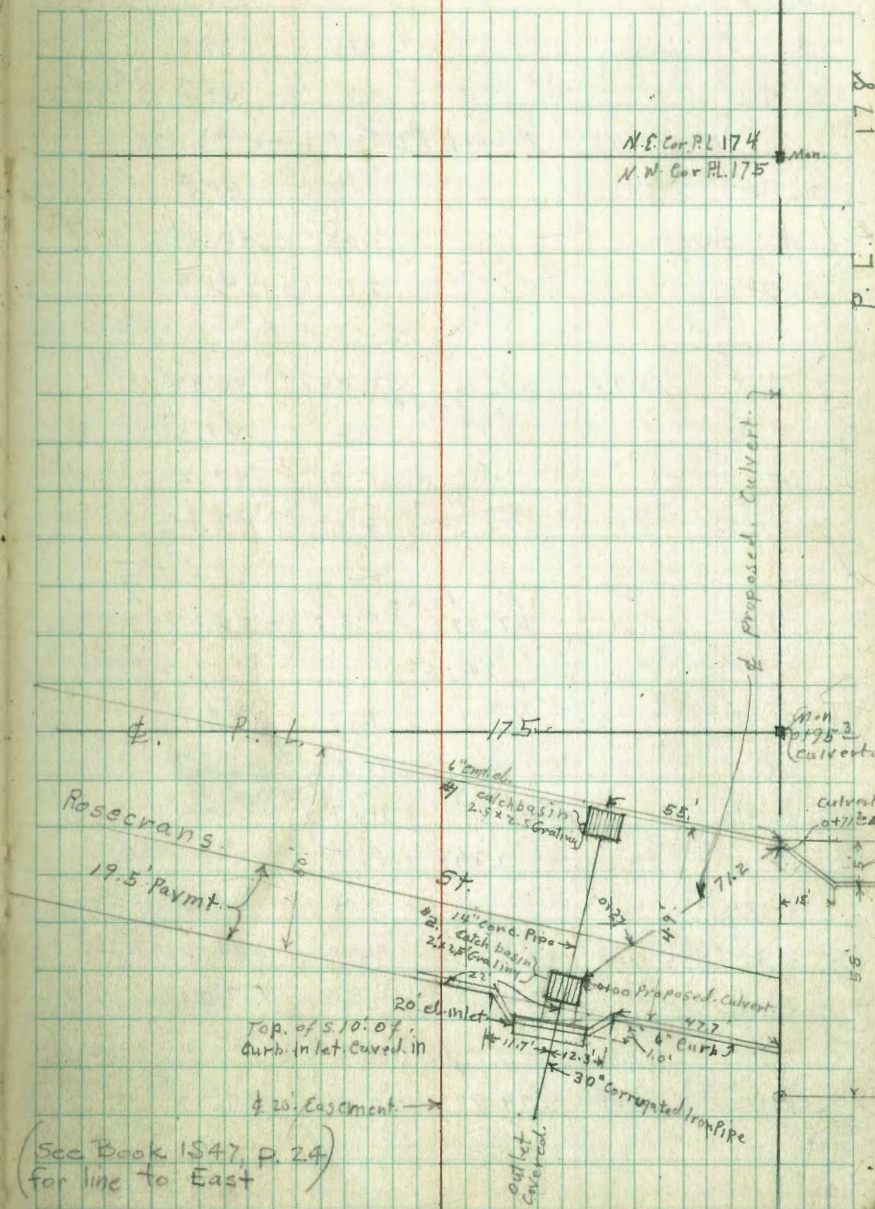
Levels Proposed Culvert
in P.L.s. 174 - 175 + 178

index
c.s.k.

P.L. 174

41

B.M. stub	7.53	44.42	36.94	(page 37 0+00 D line)
catch basin #1 W. side Rosecrans.				
Top ch.		12.18	32.29	
Gutter on grating		13.16	31.31	
+2.5 East "		13.07	31.40	
+2.5 " F.L. 14" Pipe outlet		15.14	29.29	
catch basin #2 E. side Rosecrans.				
2.5 W. of E. ch. = W. edge Grating		13.57	30.90	
" " " " " F.L. 14" Pipe inlet		19.70	24.77	
20' curb. Inlet E. side Rosecrans				
S. End ch.		13.10	31.37	
" " Gutter pavmt.		13.95	30.52	
±		14.0	30.5	
± ch.		13.05	31.42	
± F.L. 30" Pipe outlet		20.40	24.07	
N. End Gutter pavmt		13.90	30.57	
" " ch.		13.03	31.44	
0+00 Proposed Culvert = N.W. Ly Cor. Catch Basin #2				
Grating		13.57	30.90	
F.L. Box		19.70	24.77	
0+27				
W. Edge Pavmt.		12.61	31.86	
0+71.2				
dir. Gutter		12.2	32.3	
ent. ch.		11.40	33.07	



44.47

0+83

3' RT 46 39.9

¢ = P.L. Line 47 39.8

3' Lt. 48 39.7

Mon 0+95 $\frac{3}{2}$ N. Line $\frac{1}{2}$ P.L. 175 S. Line P.L. 178

3' Lt 3.0 41.5

¢ on Mon 3.03 41.44

3' Rt 3.1 41.4

T.P. 12.74 55.16 2.05 42.42 ✓

3' Rt 7.9 47.3

¢ 8.0 47.2

3' Lt. 8.1 47.1

T.P. 12.61 67.39 0.38 54.78 ✓

3' Lt 11.7 55.7

¢ 11.7 55.7

3' Rt. 11.7 55.7

3' Rt. 3.4 64.0

¢ = P.L. Line 3.2 64.2

3' Lt. 2.8 64.6

T.P. 12.77 79.89 0.27 67.12 ✓

79.89

Culvert.

42

2+50

3' Lt 0.4 79.1

¢ 1.0 78.9

3' Rt 1.0 77.9

T.P. 12.70 92.40 0.19 79.70 ✓

2+75

3' Rt 6.2 86.2

¢ 6.2 86.2

3' Lt. 6.2 86.2

T.P. 12.69 102.91 0.18 92.72 ✓

3+00

3' Lt. 9.4 93.5

¢ 9.4 93.5

3' Rt 9.4 93.5

9+26
~~3+75~~ E. end Outlet Small 8" Conc. Culvert

1' Rt. F.L. = ground. 2.05 100.86

¢ 2.0 100.9

3' Lt. 1.9 101.0

3+28 = Mon. N.W. Cor. P.L. 175

3' Lt 1.8 101.1

¢ on Mon 1.56 101.35 ✓

3' Rt. 1.3 101.6

Page 35.

9-29-38

Miller
Walker
Bliss

X Sec. BIK. L. Hatadena

Indexed
C.S.K.

Re Cross Sec 4580 Bp. 73

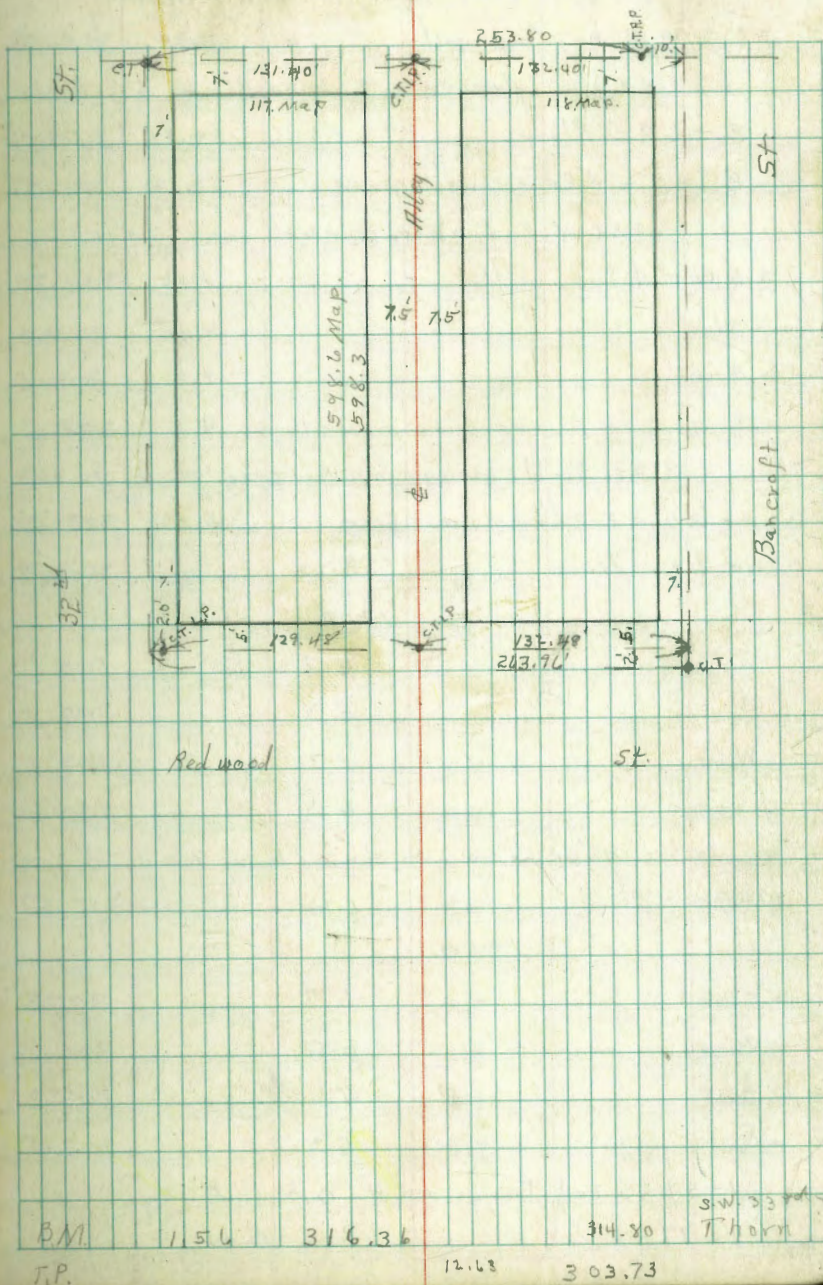
N.W. 33rd
+ Redwood

BM	6.94	319.55	311.61	
T.P.	5.88	312.96	11.63	306.92
10' S. of N. line of Redwood st.				
W.	ch		5.84	306.96
W.	pav		6.43	306.37
E.	"		5.82	306.98
E.	"		5.29	307.51
E.	ch		4.60	308.20
0+00 = N. Line Redwood				
E.	ch. N End		4.45	308.35
E.	pav	"	5.00	307.80
E.	"	"	5.63	307.17
W.	"	"	5.26	307.04
W.	ch	"	5.65	307.15
0+03 N.				
W.			4.6	308.2
+1			4.6	308.2
+3			5.5	307.3
E.			5.5	307.3
+4			5.4	307.4
E.			4.1	308.7
0+20				
E.			4.1	308.7
E.			4.4	308.4
W.			4.3	308.5

45

Thorn

ST



BM

11.50

316.36

314.80

SW 33rd
Thorn

T.P.

12.63

303.73

0+38 S. End. conc wall on W. 0.7 in Alley		
6.8 W. of ϕ Top. wall	3.84	308.96
0+42 garage on E. conc. floor 6.9 Back		
E - 6.9 = floor	2.79	310.01
E = W. Edge conc. apron	3.93	308.87
0+56 N. End. above conc. wall on W. 1.0' in Alley		
6.5 W. of ϕ Top. wall	4.06	308.74
W	4.5	308.3
ϕ	4.6	308.2
E	4.5	308.3
0+68 Double garage on W. conc. floor 9.0 Back		
W - 6.0 = E. Edge conc. apron	5.38	307.42
W - 9.0 = floor	5.22	307.58
	1+00	
E	4.7	308.1
ϕ	5.3	307.5
W	5.7	307.1
+10	6.5	306.3
1+23 garage on W. conc. floor 9.0 Back		
W - 9.0 = floor	6.13	306.67
	1+50	
W - 5	6.3	306.5
W	6.0	306.8
ϕ	5.6	307.2
E	5.3	307.5
1+59 = S. End. Fence on W. 0.5' in Alley		
1+77 N " " " " on W. Line		

T.P.	5.00	311.72	6.08	306.72
1+89 garage on W. conc. floor 7.0 Back				
W - 4.7 = E. Edge conc. apron	5.36	306.36		
W - 7.0 = floor	5.24	306.48		
	2+00			
E	4.5	307.2		
ϕ	5.0	306.7		
W	5.3	306.4		
+10	5.8	305.9		
2+06 garage on W. conc. floor 12.0 Back				
W - 9.0 = E. Edge conc. Apron	5.74	305.98		
W - 12.0 = floor	5.69	306.03		
2+20 = S. End. Fence on W. 0.5' in Alley				
2+38 = W " " " " 0.1 " "				
	2+40			
W - 10	5.5	306.2		
W	5.0	306.7		
ϕ	4.9	306.8		
E	4.5	307.2		
	2+75			
E	4.5	307.2		
ϕ	4.8	306.9		
W	5.1	306.6		
+10	5.7	306.0		

311.72

3+11 Garage on E. cone floor 24.7 Back

N-10	6.4	305.3
W	6.2	305.5
E	5.4	306.3
E	5.2	306.5
+6.5 = W-End. cone Apron.	4.40	307.12
+24.7 = floor.	3.6	308.1

3+15

Φ Top. M.H.	5.12	306.60
Φ ground	5.3	306.4

3+50

E	6.1	305.6
+2	6.9	304.8
Φ	6.7	305.0
W	7.2	304.5
+10	8.2	303.5

3+90

W-10	11.2	300.5
W	10.1	301.6
Φ	9.2	302.5
+3	8.2	303.5
E	8.0	303.7

T.P. 3.69 303.17 12.24 299.48

303.17

47

4+30

E-5 on New fill 2.3 300.9

E	4.3	298.9
Φ	5.0	298.2
W	5.5	297.7
+10	6.9	296.3

4+42

N-15	11.0	292.2
W	8.0	295.2
Φ	7.3	295.9
+3	4.3	298.9
E	4.6	298.6
+2	4.4	298.6
+3 New fill	2.5	300.7
+10 " "	2.5	300.7

4+55

E-15	10.2	293.0
E	10.1	293.1
Φ	11.2	292.0
W	10.5	292.7
+4	9.0	294.2
+15	9.0	294.2

4+75

W-12 floor level	5.8	297.5
W-12. E side House.	9.0	294.2
W.	13.1	290.1
Φ	15.2	288.0
+5	15.2	288.0

303.17

E		14.8	288.4
E+15		14.5	288.7
	4+85		
E-25		14.5	286.7
E. 4 wash to E.		19.0	284.2
4		17.0	286.2
W		14.4	288.8
+12 = E. side House		9.5	293.7
	5+05		
W-8.5 ground under Porch		8.8	294.4
W-3.5 " " E. edge Porch		11.1	292.1
W-3.5 " " "		5.8	297.4 = Floor of House
W		12.4	290.4
4		14.8	288.4
E		14.4	288.8
E+17 4 wash		18.7	284.5
E+30		17.0	286.2
	5+20		
3-37		15.6	287.6
E-27 4 wash		17.6	285.6
E-10		13.6	289.6
E		12.8	290.4
4		12.0	291.2
W		11.8	291.4
+10		9.0	294.2

303.17

48

5+39 = S. End Stucco Stone on W 3. Back.

W-10		5.7	297.5
W-3 = S. E. Cor		4.7	298.5
W-3. " " (Bottom of one Joist (dist. can spill) under the Building)		1.5	301.7
W		4.7	298.5
4		5.0	298.2
C		5.5	297.7
+15		9.7	293.5
+38 4 wash.		14.9	286.3
T.P. G.L.	307.62	2.17	301.00
	5+49		
E		5.2	302.4
4		6.0	301.6
W		5.9	301.7
+3 (W. end of opening under Conc Beam)		5.9	301.7
+3 = Door way of stone		3.5	304.4
	5+75		
W-3 E. side Bldg		5.0	302.6
W		5.0	302.6
4		5.3	302.3
E		5.0	302.6

5498³ = S. line Thorn St.

E	db	S. End	3.76	303.86
E	pav	" "	3.99	303.63
±	"	" "	4.21	303.41
W	"	" "	4.15	303.47
W	db	4 "	3.91	303.71

10' N of S. Line = S. db. of Thorn.

W.	db		4.15	303.47
W	pav		4.75	302.87
±	"		4.61	303.01
E	"		4.53	303.09
E	db		3.84	303.74

T.P.	12.63	316.34	2.91	303.71	S. line Thorn
chk. BM	S.E. 33 rd	Thorn	1.56	314.78	Top. W. Curb of Alley

= 314.80

9-29-38
 12.00
 13.00

X Sec. 56th St. Mead to Trojan
 50 W. id. 10. cl. 7.5 1/4 s.

N.E. 56th +
 El Cajon
 NE 7th C.T. St.
 + Melrose
 walk on W

B.M.	0.00	437.77	-	437.77
T.P.	1.28	426.75	12.20	425.47
			10' N of S. line = S. E. line Meads.	
E. cont. ed. w. End		4.67		422.08
E. pay. S. edge		5.25		421.50
dr. " " "		5.50		421.25
1/4 " " "		5.24		420.47
1/2 " " "		5.21		421.54
1/4 " " "		5.52		421.23
ed. " " "		5.92		420.83
concret. S. End		5.27		421.48
+5 1/2 5' walk		5.24		421.51
W		4.2		422.6
			0+00 = S. line Meads	
W		3.4		423.0
ed		4.7		422.1
1/4		5.7		421.1
+4		5.7		421.1
1/2		5.7		421.1
1/4		5.3		421.5
ed		4.8		422.0
E		4.0		422.8
2.5 N of C. = S. W. for conc. walk.		4.57		422.18

Indexed
 426.75

426.75

	0+10	
E	2.7	424.1
ed	2.8	424.0
1/4	3.4	423.2
+2	5.3	421.5
1/2	6.1	420.7
+2	6.1	420.7
+5	3.8	423.0
1/4	3.8	423.0
ed	3.8	423.0
W	3.4	423.4
	0+30	
W	4.1	422.7
ed	4.2	422.6
1/4	3.8	423.0
+3	4.0	422.8
+4	5.5	421.3
1/2	7.5	419.3
+6	6.6	420.2
1/4	4.1	422.7
ed	2.8	424.0
E	2.5	424.3

426.75

0+75

E	3.1	423.7
el	3.7	423.1
1/4	4.3	422.5
+2	4.9	421.9
4	7.3	419.5
±	9.1	417.7
+5	8.1	418.7
1/4	6.3	420.5
el	4.7	420.1
W	6.1	420.7
1+20		
W	10.4	416.4
el	10.7	416.1
1/4	10.4	416.4
+3	10.4	416.4
+5	13.4	413.4
±	14.0	412.8
+5	14.0	412.8
+6	9.4	417.4
1/4	9.1	417.7
el	7.3	419.5
E	5.5	421.3
1+60		
E	10.1	416.7
el	11.0	415.8
1/4	11.6	415.2

426.75

56th 51

51

+5		13.0	413.8	
W.P.	0.83	415.23	12.35	414.40
±		3.9	411.3	
1/4		5.1	410.1	
+1		1.4	413.8	
el		1.4	413.8	
W		1.6	413.6	
2+00				
W		3.6	411.6	
el		3.6	411.6	
1/4		3.4	411.8	
+5		3.4	411.8	
±		2.6	405.6	
1/4		5.4	409.8	
+3		3.1	412.1	
el		2.8	412.4	
E		2.7	412.5	
2+50				
E		6.2	409.0	
el		6.2	409.0	
±		6.3	408.9	
1/4		10.6	404.6	
+3		13.6	401.6	
+6		13.6	401.6	

415.23

2+50 (con)

£	6.6	408.6
1/4	7.0	408.2
cl	7.1	408.1
W	7.0	408.2

2+70

W	8.8	406.4
cl	8.8	
1/4	8.8	406.4
+6	8.8	406.4
£	14.8	400.4
1/4	15.3	399.9
+4	15.1	400.1
d	8.8	406.4
E.	8.5	406.7

3+00

E	11.8	403.4
cl	12.2	403.0
+5	12.2	403.0
1/4	16.7	398.5
+5	16.7	398.5
+6	12.3	402.9
£	12.3	402.9
1/4	12.2	403.0
cl	12.2	403.0
W	12.2	403.0
T.P.	0.20	402.98
	12.45	402.78

402.98

56th st 52

3+50

W	5.2	397.8
cl	5.3	397.7
1/4	5.4	397.6
+3	5.5	397.5
+5	7.5	395.5
£	7.8	395.2
+6	2.8	395.2
1/4	5.3	397.7
cl	5.4	397.6
E	5.1	397.9

3+70

E	7.2	395.8
cl	6.8	396.2
1/4	6.6	396.4
£	6.9	396.1
F1 wash	9.8	393.2
1/4 wash	10.1	392.9
+2	7.3	395.7
cl	7.4	395.6
W	7.2	396.0

4+00

W	10.1	392.9
cl	10.2	392.8
1/4	10.3	392.7
+2 wash	12.5	390.5
£ wash	12.5	390.5

402.98

4+00 (con)

4+2		10.1	392.9
"4		10.0	393.0
cl		9.8	393.2
E		9.9	393.1

T.P. 0.39 390.59 12.78 390.20

4+50

E		1.0	389.6
cl		1.4	389.2
"4		1.1	389.5
4		1.6	389.0
"4	wash	3.4	387.2
+6	wash	4.0	386.6
cl		1.9	388.7
W		2.0	388.6

4+45

W		2.7	387.9
+2		3.0	387.6
+4	wash	4.5	386.1
cl	"	4.6	386.0
+1		2.3	388.3
"4		2.0	388.6
4		1.7	388.9
"4		2.0	388.6
cl		2.4	388.6
2		2.0	388.6

390.59

56th ST

53

4+70

E		2.4	388.2
cl		2.5	388.1
"4		2.2	388.4
4		2.0	388.6
"4		2.2	388.4
cl		2.5	388.1
+4		2.4	387.8
+5	wash	5.0	385.6
W	"	5.0	385.6
+3	"	5.0	385.6
+5		3.0	387.6
+10		3.0	387.6

4+75

-15		3.4	387.2
-10		3.4	387.2
-9	wash	5.2	385.4
-2	"	5.0	385.6
W		3.0	387.6
cl		2.8	387.8
"4		2.4	388.2
4		2.2	388.4
"4		2.4	388.2
cl		2.7	387.9
E		2.7	387.9

390.59

5+00

e	4.1	386.5
d	4.1	386.5
1/4	4.1	386.5
1/2	4.0	386.6
1/4	4.3	386.3
d	4.6	386.0
w	4.6	386.0
5+45		
w	7.3	383.3
d	7.0	383.6
1/4	6.6	384.0
1/2	6.6	384.0
1/4	6.5	384.1
d	6.9	383.7
e	6.5	384.1
5+50		
e	7.9	382.7
d	7.2	383.4
1/4	6.8	383.8
1/4 wash N end	8.4	381.8
1/2	7.0	383.6
1/4	7.0	383.6
d	7.0	383.6
w	7.4	383.2

390.59

56th St.

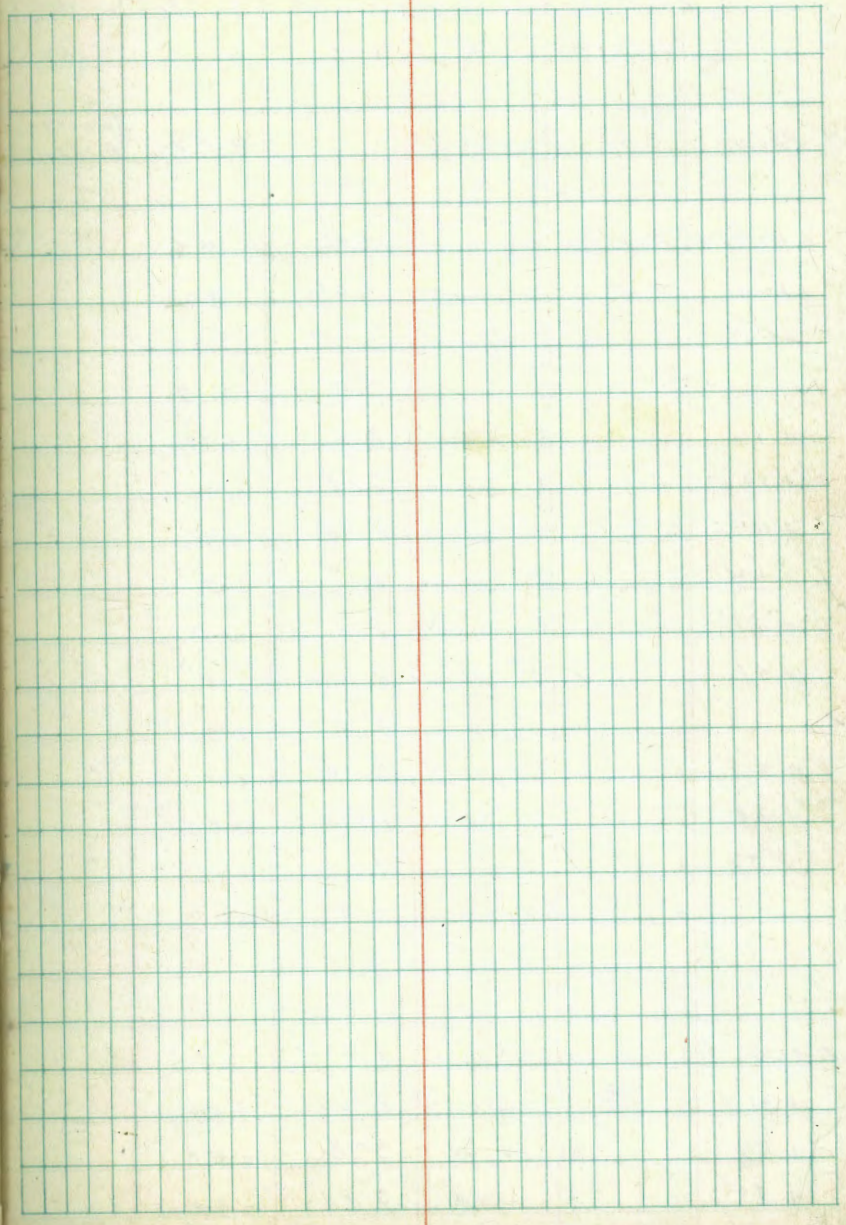
54

5+80³ P.C. 20' Prop. Red.

w	9.0	381.6
d	9.2	381.4
1/4	9.7	381.2
1/2	10.0	380.6
1/2 wash	11.1	379.5
1/4	11.0	379.6
1/4	9.6	381.0
d	9.8	380.8
e	10.0	380.6
6+00 ² N. line Trojan.		
e	12.5	378.1
d	12.1	378.5
1/4	11.8	378.8
1/3 wash	13.1	377.5
1/2	12.7	378.9
1/4	11.3	379.3
d	10.7	379.9
w	10.5	380.1
6+30 ³ = S. line Trojan		
w	13.2	377.5
d	13.4	377.2
1/4	14.0	376.6
1/2	15.0	375.6
1/4	15.2	375.4
d	16.0	374.6
1/2	16.2	374.4
+10	17.4	373.2

		390.59		
Set. B.M.	Top Mon	(Sta 5+80 ² E. Line P.C. 20' Prop. Rad.)	10.03	380.56
T.P.	0.73	378.70	12.22	378.37
T.P.	1.14	371.10	8.78	369.92
B.M. B.P. Headwall			7.30	363.80 = + Orange
				363.75

S.W. 54th
+ Orange



Levels on EMERSON ST. 70' wide
Rosecrans to Scott

7' Mon. 0.57 10.49 9.92 Rosecrans
Dickens

1+00	at S.L.	7.4	2.8
+50	" "	7.5	3.0
	" "	6.9	3.6
+50	" "	6.3	4.2
3	" " = Ely Rosecrans	5.4	5.1

North Line EMERSON

0+00	= Ely Rosecrans	5.9	4.6
+24	N.L. E 2' walk	6.26	4.23
+45	" " 7' Drive	6.57	3.92
1	" " "	7.8	2.7
+12	" " 3' walk	8.10	2.39
+30	" " 7' Drive	8.09	2.40
+44	" " 4' walk	8.33	2.16
+64	" " 7' Drive	8.37	2.12
+81	" " 3' walk	8.44	2.05
+95	" " 7' Drive	8.34	2.15
✓	" " "	8.5	2.0
+25	" " 3' walk	8.38	2.11
+38	" " 7' Drive	8.48	2.01
+50	" " "	9.1	1.4
3	" = WL SCOTT	9.9	0.6

S.L. EMERSON

0+00	S.L. or WL SCOTT	8.9	1.6
+31	" E 3' walk	8.20	2.29
+59	" " 10' Drive	7.98	2.51
+84	" " 3' walk	7.51	2.98

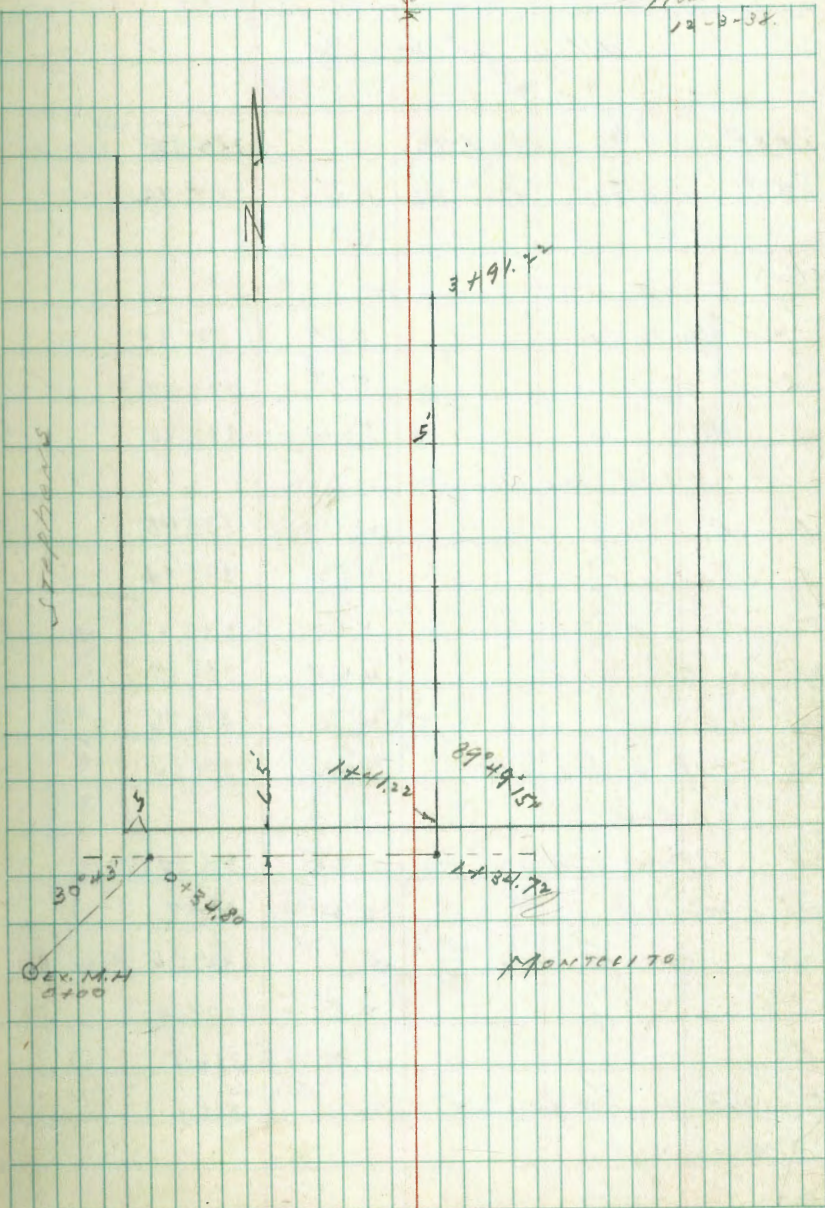
PROP. SEWER
 BIK 3 N. Florence Hys.

INDEXED
 C.S.K.

Station	Description	Offset	Height	Elevation	Notes
SEBP		2.22	278.00	275.78	LEWIS STEPHENS
0+00	EX M.H. F.L.		7.33	270.67	
"	RINT & PAV.		4.78	273.22	
0+28	94T "		4.93	273.07	
"	TOP CB		4.41	273.59	
0+34.80	Δ ON STUB		4.23	273.77	
450	LAWN		4.1	273.9	
1	"		2.4	274.6	
1+18	WEDGE CON. DR.		3.27	274.73	
1+27	E " " "		3.22	274.88	
1+34.74	Δ STUB		2.93	275.07	
1+36.22	S EDGE CON. SDW.		2.96	275.04	
1+41.22	N " " "		2.85	275.15	
"	TOP 8" REPAIR WALL		1.88	276.12	
TP		9.06	284.32	274	275.26
1+91.22			7.1	277.2	
2+41.22			6.1	278.2	
2+91.22			5.1	279.2	
3+41.22			3.8	280.5	
3+91.22			2.5	281.8	

D Block

Floor
 12-9-32



337.86

	0 + 45		
E	1.7	336.2	
C	1.7	336.2	
W	1.5	336.4	
+ 3' E apron 8' wide	1.30	336.56	
+ 5.5' S.W. gar. cent. fl.	1.28	336.58	
	1 + 00		
W	1.6	336.3	
C	2.1	335.8	
E	2.1	335.8	
2' shed in alley 0.5			
	1 + 29		
E	fence in alley 0.4	2.40	335.46 2' cent. walk
	1 + 50		
E	fence in alley 0.5	2.5	335.4
C	2.4	335.5	
W	2.3	335.6	
	2 + 00		
W		335.2	
W	2.4	335.3	
C	2.7	335.2	
E	2.7	335.2	
	2 + 50		
E	2.6	335.3	
C	2.4	335.3	
W	2.5	335.4	
W + 10		335.2	

337.86

T.P	5.45	335.97	2.44	335.42
W	1 + 00			
W			5.0	335.8
C	M.H. Rim		5.0	335.9
C	ground		5.0	335.3
E			5.3	335.6
			5.3	335.6
			5.6	335.3
	2 + 50			
			5.4	335.5
E			5.2	335.7
C			5.1	335.8
W			4.9	336.0
W + 10				335.8
W	1 + 00			
W			5.1	335.8
C			5.1	335.8
E			5.3	335.6
W			5.4	335.5
	4 + 26			
E	E 3' cent. walk		4.6	336.23
	4 + 30			
W	3' " "		4.8	336.05
	4 + 50			
E			4.6	336.3
C			4.7	336.2
W			4.9	336.0
W + 10				336.4

34087

4+8d			
W-19 Sin. gar. cem.	4.27	336.64	
W	4.4	336.5	
4+96			
W-19 Sin. " "	4.06	336.81	
W	4.4	336.5	
5+00			
W-10		336.5	
W	4.3	336.6	
C	3.8	337.1	
E	3.6	337.3	
5+37			
-5 Sin. gar. Cem.	3.13	337.74	
E	3.4	337.5	
C	3.2	337.7	
W	3.7	337.2	
+2 10' apron	3.70	337.17	
+9 Sin. gar	3.54	337.33	
5+70			
-2.5 Cem. Walk	2.34	338.51	2 1/2 wide
W	2.8	338.1	
C	3.0	337.9	
E	2.7	338.2	
T.P.	4.30	342.19	298 337.89

34219

60

5+90

E	4.8	337.4	
C	4.5	337.7	
W	4.4	337.8	
+2.5 Cem Walk	4.0	338.2	
6+00.25 SL Landis			
W ob	4.61	337.58	
W Pav	4.75	337.44	
C "	5.01	337.18	
E "	4.97	337.22	
E ob	4.88	337.31	
6+10.25 S ob Landis			
E Pav	5.29	336.70	
C "	5.44	336.75	
W "	5.39	336.80	
T.P.	9.82	348.21	379 338.40 338.39
T.P.	9.62	340.07	876 339.45
T.P.	4.88	338.24	671 333.36
			5.58 332.66 (332.52)
9.70	348.09		338.39
S.W.B.P. 32nd W. Highway	1.69	346.40	346.40

Use this as a guide and make corrections
 SW B.P. 32nd x Landis
 NO
 original
 etc

RT'S in BURN shape in this vicinity

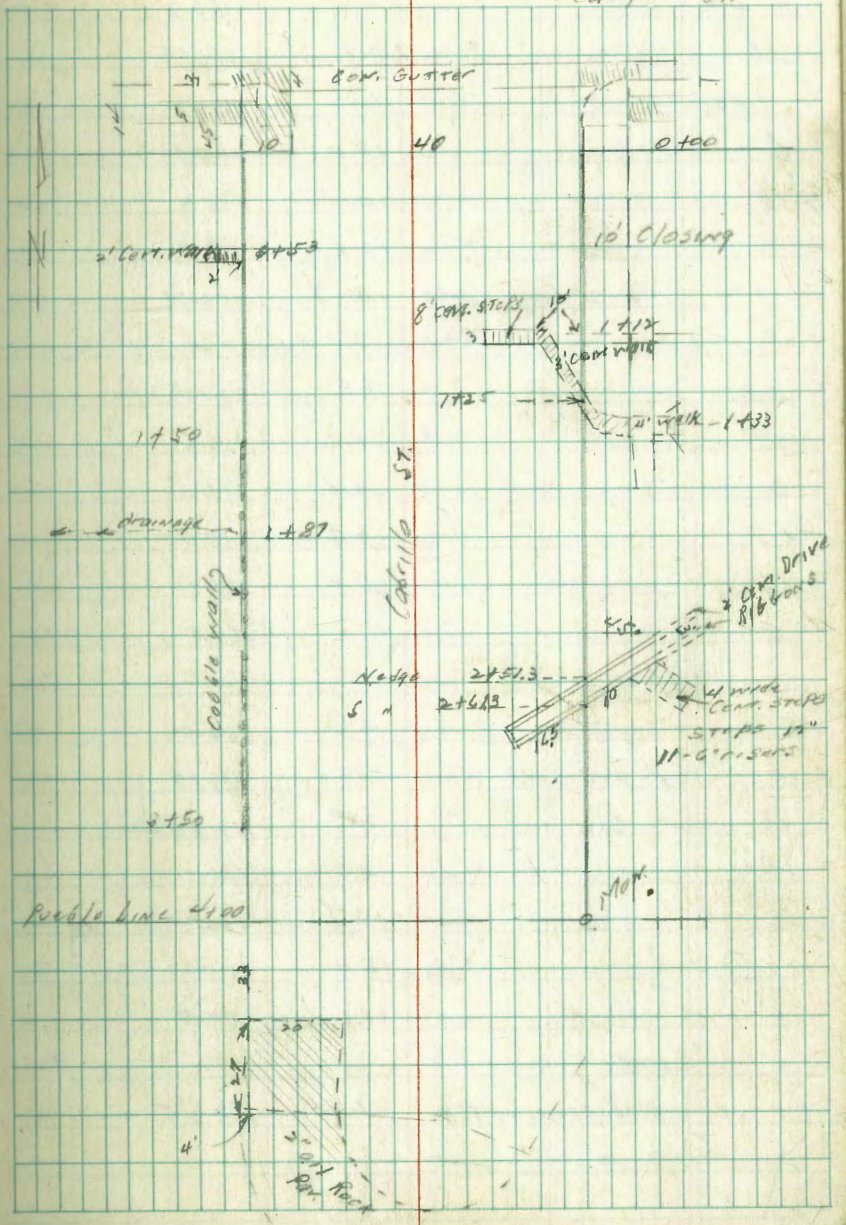
Moore
2-2-39

Index
C.S.K.

X sec Cabrillo St. 50' wide 10' curb
Pearl St. 400'

SW Top curb	10.89	166.93	156.04	Pearl Cabrillo 1440-35
0-14 S of Pearl				
WL cb	10.93		156.00	
" gut	11.90		155.03	
C "	11.37		155.56	
EL. "	10.99		155.94	
+10 5/8" cb PL	10.73		156.20	
+10 gutter	9.83		157.10	
0+00 St Pearl				
E top cb	9.92		156.96	
gut	10.5		156.4	
C	10.9		156.0	
cb gut	11.2		155.7	
cb top	10.89		156.04	
0+25				
W	10.3		156.6	
cb	10.5		156.4	
C	10.4		156.5	
+6	10.3		156.6	
cb	5.0		161.9	
E	3.9		163.0	
0+53				
E	3.1		163.8	

Pearl St.



E + 6	4.2	162.7	
cb	5.8	164.1	
+10	9.4	152.3	
C	10.0	156.9	
cb	10.5	156.4	
W	10.2	156.2	
+2	E of Cent walk	10.27	156.76
1+00			
W	9.9	152.0	
cb	10.6	156.6	
C	10.4	156.5	
+5	9.9	152.0	
cb	5.8	161.1	
E	4.1	162.8	
1+12			
E	4.1	162.8	
cb	TOP TOP STEP	5.40	161.53
+8	" BOT "	9.49	152.44
+9		10.1	156.8
C		10.7	156.2
cb		11.0	155.9
W		11.1	155.8
1+25			
E	E of 3' cent. walk	3.68	163.25

1+33

-10	12.6	154.3	
W	11.9	155.0	
cb	11.8	155.1	
C	11.5	155.4	
+8	10.4	156.3	
cb	6.2	160.2	
E	4.2	162.2	
+10	E 4' cent walk	1.48	165.45
1+50			
E	4.4	162.5	
+4	5.7	161.2	
cb	8.1	158.8	
+5	10.5	156.4	
C	11.3	155.6	
cb	12.0	154.9	
W	12.4	154.7	
+10	12.8	154.1	
1+87			
-10	Low spot in St	12.9	154.0
W	12.0	154.9	
cb	11.6	155.3	
C	10.8	156.7	
+12	9.9	152.0	
cb	8.7	158.2	
E	6.1	160.8	

166.93

2+00			
-5 yard	0.9	166.0	
E	3.8	163.6	
cb	9.9	157.0	
C	11.0	155.9	
cb	11.4	155.5	
W	11.7	155.2	
+10	12.7	154.2	
2+40			
-10	11.3	155.6	
W	10.2	156.7	
cb	10.2	156.7	
C	9.7	157.2	
+12	8.7	158.2	
cb	7.4	159.5	
E	2.3	164.6	
2+51.3 ledge N of Cent. Ribbon			
E	3.72	163.21	
cb	5.5	161.4	
+7	8.4	158.5	
C	8.9	158.0	
cb	9.7	157.2	
W	10.0	156.9	
+10	10.5	156.4	

166.93

63
S. ribbon
level with

2+51.3 sec. on N. of 2' Cent. Ribbon N. ribbon			
E	3.72	163.21	
+23. bot ribbon	7.17	159.76	
E-10	2.35	164.58	
2+61.3 TANK 90°			
E-5	0.9	166.0	
E ledge of S ribbon	4.75	162.18	
cb N " " " "	5.96	160.97	
+8	7.8	159.1	
C	8.4	158.5	
2+68			
-10	9.6	157.3	
W	8.9	158.0	
cb	8.7	158.2	
C	8.7	158.7	
+8 rest ribbon	7.17	159.76	
cb	6.4	160.5	
+4 " "	6.01	160.92	
E	2.1	164.8	
T.P. 1306 178.84	11.5	165.78	
2+00			
E	9.7	169.1	
cb	13.1	165.7	
+10	17.3	161.5	

c		18.0	160.8
cb		18.0	160.8
W		18.6	160.2
+14	LAWN	20.8	158.0
3+44			
-25	LAWN	20.8	158.0
-15		19.0	159.8
-2		15.5	163.3
W		13.6	165.2
cb		13.5	165.3
c		13.6	165.2
+6		12.7	166.1
cb		7.7	171.1
E		3.6	175.2
3+50			
-10		14.7	164.1
W		13.2	165.6
cb		13.2	165.6
3+70			
E		2.6	176.2
+6		3.8	175.0
cb		6.1	172.7
+7		10.0	168.8
+13		10.0	168.8
c		11.4	167.2
cb		11.5	167.3
W		11.8	167.0
+10		13.0	165.8

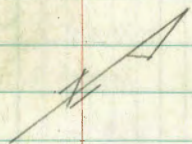
+400			
-10		11.0	167.8
W		9.4	169.4
cb		9.3	169.5
+13		9.7	169.1
E		8.6	170.2
+9		7.8	171.0
cb		3.5	175.3
E		+1.3	180.1
33' S of P.G.			
E	20' Pav	7.30	171.5
W	" "	7.15	171.69
40' S of P.G.			
W	20' Pav	5.4	173.4
E	" "	6.4	172.4

2 sec of Wabaska
Tennyson to Voltaire

Indexed
C.S.K.

Proposed widening
to 80'

Tennyson



15.70

47.76

1496.60
EC. 1479.35

42.49

$\Delta = 42.49$ Rt.

BR = 240

Pl. Ld. Ct. Pav.

T = 94.09

L = 179.35

B.S. 0400 Ld. Ct. Pav.

229.95

55' WASHINGTON

Ld. Ct. Pav.

30

25

Pt. Loma Hts.

Public Line

Western field

42.28

E Wabaska St.

Moore
2-14-39

65

2435.26

Plotted on Tie sheet.
C.S.K.

101.82

5.37

50

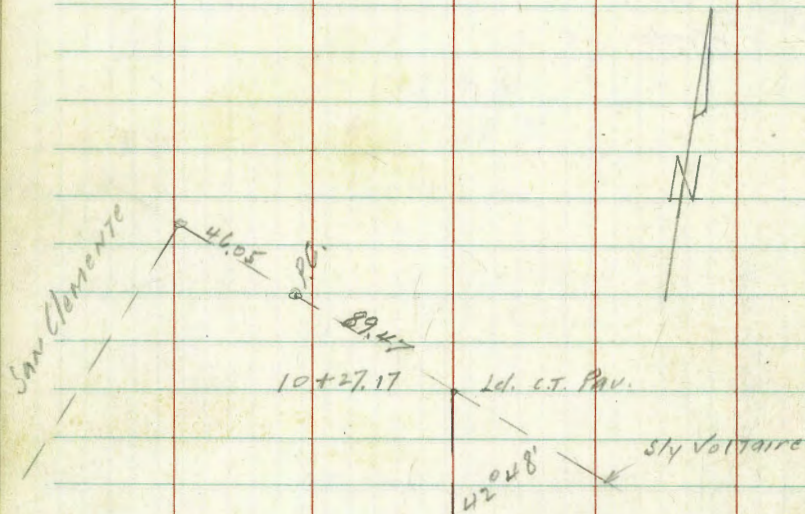
Warden St.

Wabaska St.

Tennyson to Voltaine

Moore

2-14-89.



Wabaska St.

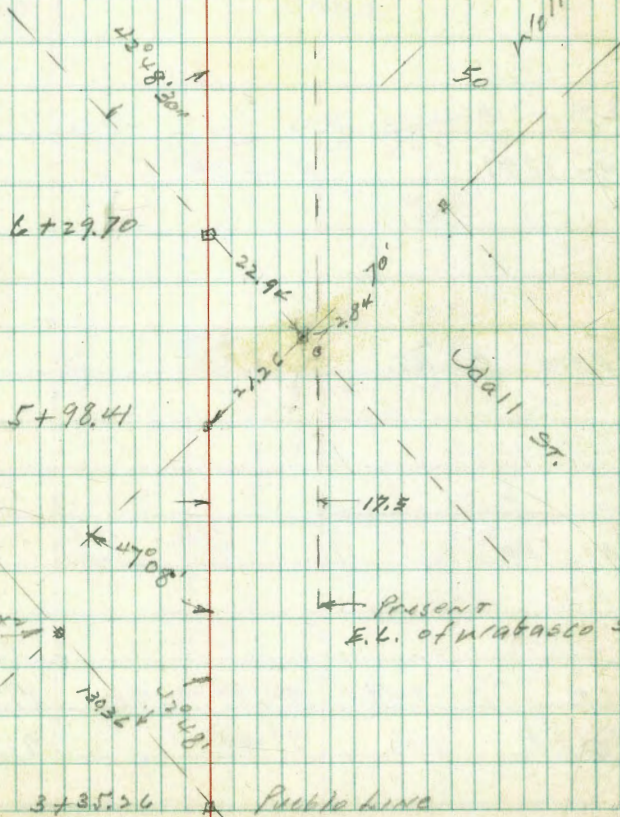
10+41.89

10+27.17

Ld. C.T. Pav.

42048'

Present sly Voltaine ST
10' Curve Line



1+43.48

17° 07' 36"

1+07.61

12° 50' 42"

0+71.74

8° 33' 48"

0+35.87

4° 16' 54"

0+00 B.C.R.T.

00-50

T.P.	7.48	94.48	11.08	87.00	
SWBP	143	98.08	96.65		Tennyson Chatsworth

$\frac{91.35}{2.10}$
40
Pav

$\frac{91.17}{3.30}$
13
Pav

$\frac{91.6}{2.9}$

$\frac{90.3}{4.3}$
10

$\frac{89.3}{5.4}$
12

$\frac{88.7}{5.8}$
23

$\frac{88.5}{5.0}$
40

$\frac{91.58}{2.92}$
40

$\frac{91.03}{3.45}$
20

$\frac{90.7}{4.31}$

$\frac{89.15}{4.33}$
7 Pav

$\frac{89.2}{5.3}$
35

$\frac{88.9}{4.6}$
40

$\frac{91.02}{3.12}$
34
of

$\frac{90.47}{4.00}$
34
947

$\frac{90.44}{4.04}$
20

$\frac{89.80}{4.68}$

$\frac{88.05}{5.00}$
21
949 Pav

$\frac{89.0}{5.5}$
30

$\frac{89.5}{4.0}$
30

$\frac{89.85}{4.65}$
24
of

$\frac{89.22}{5.24}$
24
947

$\frac{89.29}{5.19}$

$\frac{88.86}{6.14}$
25
947

$\frac{88.92}{5.34}$
25
of

$\frac{89.5}{4.0}$
35

$\frac{90.9}{5.2}$
40

$\frac{88.32}{6.11}$
20
947

$\frac{88.41}{6.07}$

$\frac{87.24}{6.74}$
20
947

$\frac{88.80}{6.18}$
20
of

$\frac{88.20}{6.28}$
20
of

$\frac{87.57}{6.96}$
20
947

$\frac{87.53}{6.95}$

$\frac{86.92}{7.71}$
20
947

$\frac{87.35}{7.13}$
20

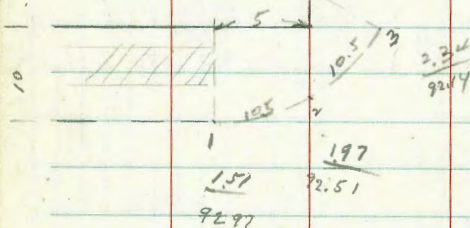
9448
?

2+50

2+00

NEW RETURN

TENNYSON
+
Worben



1+79.35 E.C. 21° 24' 30"

94.48

LT.

±

RT.

68

$\frac{92.0}{2.5}$ 40	$\frac{92.3}{3.0}$ 30	$\frac{92.4}{4.0}$ 22.5	$\frac{92.7}{6.0}$ 15.45	$\frac{92.7}{6.0}$ 15.45	$\frac{92.3}{2.0}$ 46.15	$\frac{92.5}{4.0}$ 23.125	$\frac{92.5}{2.0}$ 46.25	$\frac{92.1}{2.0}$ 46.05
--------------------------	--------------------------	----------------------------	-----------------------------	-----------------------------	-----------------------------	------------------------------	-----------------------------	-----------------------------

$\frac{92.1}{1.0}$ 92.1	$\frac{92.2}{2.0}$ 46.1	$\frac{92.5}{3.0}$ 30.833	$\frac{92.5}{6.0}$ 15.416	$\frac{92.7}{2.0}$ 46.35	$\frac{92.7}{3.0}$ 30.9	$\frac{92.8}{2.0}$ 46.4
----------------------------	----------------------------	------------------------------	------------------------------	-----------------------------	----------------------------	----------------------------

$\frac{92.9}{1.5}$ 61.933	$\frac{92.8}{2.0}$ 46.4	$\frac{92.7}{4.0}$ 23.175	$\frac{92.5}{3.0}$ 30.833	$\frac{92.6}{5.0}$ 18.52	$\frac{92.5}{2.0}$ 46.25	$\frac{92.3}{3.0}$ 30.766	$\frac{92.9}{5.0}$ 18.58
------------------------------	----------------------------	------------------------------	------------------------------	-----------------------------	-----------------------------	------------------------------	-----------------------------

94.48

$\frac{84.3}{6.1}$	$\frac{84.3}{8.1}$	$\frac{83.8}{8.0}$	$\frac{82.2}{10.2}$	$\frac{81.4}{11.0}$	$\frac{82.6}{9.8}$	$\frac{81.6}{10.8}$	$\frac{80.4}{12.0}$
$\frac{40}{20}$	$\frac{35}{35}$	$\frac{30}{30}$	$\frac{25}{25}$		$\frac{2}{2}$	$\frac{20}{20}$	$\frac{40}{40}$

$\frac{84.4}{6.0}$	$\frac{84.4}{8.0}$	$\frac{84.4}{8.4}$	$\frac{83.0}{9.2}$	$\frac{82.6}{9.8}$	$\frac{83.8}{8.6}$	$\frac{82.8}{9.6}$	$\frac{81.7}{10.7}$
$\frac{40}{40}$	$\frac{33}{33}$	$\frac{25}{25}$	$\frac{22}{22}$	$\frac{18}{18}$	$\frac{2}{2}$	$\frac{20}{20}$	$\frac{20}{20}$

$\frac{82.3}{4.1}$	$\frac{82.5}{4.9}$	$\frac{84.9}{7.5}$	$\frac{83.9}{8.5}$	$\frac{83.5}{8.6}$	$\frac{83.5}{8.6}$	$\frac{84.6}{7.8}$	$\frac{83.9}{8.7}$	$\frac{82.9}{9.7}$
$\frac{40}{40}$	$\frac{24}{24}$	$\frac{22}{22}$	$\frac{22}{22}$		$\frac{3}{3}$	$\frac{2}{2}$	$\frac{20}{20}$	$\frac{40}{40}$

$\frac{85.5}{3.6}$	$\frac{86.3}{4.1}$	$\frac{86.2}{6.2}$	$\frac{84.0}{7.4}$	$\frac{84.9}{7.5}$	$\frac{84.8}{7.6}$	$\frac{85.6}{6.8}$	$\frac{85.1}{7.5}$	$\frac{85.1}{7.3}$
$\frac{40}{40}$	$\frac{25}{25}$	$\frac{22}{22}$	$\frac{20}{20}$	$\frac{15}{15}$	$\frac{6}{6}$	$\frac{6}{6}$	$\frac{20}{20}$	$\frac{40}{40}$

T.P. 645 92.36 857 8591

$\frac{92.36}{7}$

3 + 100

$\frac{88.9}{4.6}$	$\frac{89.0}{5.5}$	$\frac{82.1}{7.4}$	$\frac{86.4}{8.1}$	$\frac{86.3}{8.3}$	$\frac{85.6}{8.9}$	$\frac{82.1}{7.4}$	$\frac{86.3}{8.3}$	$\frac{85.3}{9.0}$
$\frac{40}{40}$	$\frac{30}{30}$	$\frac{24}{24}$	$\frac{18}{18}$		$\frac{7}{7}$	$\frac{8}{8}$	$\frac{20}{20}$	$\frac{40}{40}$

94.48

$\frac{94.48}{7}$

+50

7

+50

6+00

T.R. 0.84 82.57 10.63 81.73

5+50

92.36

$\frac{72.8}{48}$	$\frac{74.3}{43}$	$\frac{76.6}{6.0}$	$\frac{75.8}{6.8}$	$\frac{75.2}{6.9}$	$\frac{72.0}{5.0}$	$\frac{76.9}{57}$	$\frac{76.0}{66}$	$\frac{68.6}{14.0}$	$\frac{64.3}{18.3}$	$\frac{59.0}{23.6}$
$\frac{1.5}{40}$	$\frac{1.7}{33}$	$\frac{12.7}{37}$	$\frac{11.0}{35}$	$\frac{10.9}{3}$	$\frac{14.4}{4}$		$\frac{1.2}{7}$	$\frac{4.3}{20}$	$\frac{3.5}{20}$	$\frac{2.5}{60}$

$\frac{72.6}{5.0}$	$\frac{72.5}{4.8}$	$\frac{74.8}{5.8}$	$\frac{76.1}{5.5}$	$\frac{72.5}{5.1}$	$\frac{72.1}{5.5}$	$\frac{67.8}{14.7}$	$\frac{65.5}{17.1}$	$\frac{65.6}{17.0}$
$\frac{14.4}{20}$	$\frac{15.2}{27}$	$\frac{12.9}{25}$	$\frac{13.8}{2}$		$\frac{13.1}{5}$	$\frac{4.7}{20}$	$\frac{3.8}{40}$	$\frac{3.6}{40}$

$\frac{76.3}{38}$	$\frac{79.4}{3.0}$	$\frac{78.0}{4.0}$	$\frac{77.2}{4.4}$	$\frac{77.9}{37}$	$\frac{72.3}{5.3}$	$\frac{67.5}{18.1}$	$\frac{67.6}{15.0}$	$\frac{64.5}{18.1}$
$\frac{1.8}{40}$	$\frac{13.3}{26}$	$\frac{12.0}{25}$	$\frac{12.3}{1}$		$\frac{13.6}{8}$	$\frac{3.8}{20}$	$\frac{4.5}{40}$	$\frac{3.6}{65}$

$\frac{81.3}{1.3}$	$\frac{82.4}{3.4}$	$\frac{82.3}{3.3}$	$\frac{80.4}{2.4}$	$\frac{82.0}{4.6}$	$\frac{78.2}{10.4}$	$\frac{69.2}{13.0}$	$\frac{64.3}{18.3}$
$\frac{10.2}{40}$	$\frac{24.1}{25}$	$\frac{25.0}{1}$		$\frac{16.3}{12}$	$\frac{7.8}{20}$	$\frac{5.2}{20}$	$\frac{3.6}{60}$

82.57

$\frac{82.8}{8.6}$	$\frac{82.4}{10.4}$	$\frac{81.8}{10.6}$	$\frac{80.9}{11.5}$	$\frac{80.2}{11.5}$	$\frac{81.2}{12.3}$	$\frac{76.6}{12.8}$	$\frac{72.5}{14.9}$	$\frac{72.9}{15.2}$
$\frac{9.5}{40}$	$\frac{7.8}{35}$	$\frac{7.7}{25}$	$\frac{7.8}{24}$	$\frac{7.5}{15}$	$\frac{7.7}{1}$	$\frac{6.0}{20}$	$\frac{4.9}{40}$	$\frac{4.5}{45}$

92.36

+50

9

T.P. 2.88 76.07 9.38 73.19

76.07

+60

+35

8

82.57

<u>23.3</u>	<u>23.1</u>	<u>22.4</u>	<u>22.4</u>	<u>23.2</u>	<u>24.0</u>	<u>24.5</u>	<u>58.4</u>	<u>57.8</u>	<u>63.4</u>
2.8	3.0	3.7	3.7	2.4	2.1	2.2	17.7	18.3	12.7
20	34	30	20	3	21	10	35	40	55

<u>24.4</u>	<u>24.1</u>	<u>23.1</u>	<u>23.0</u>	<u>24.0</u>	<u>23.6</u>	<u>22.1</u>	<u>63.1</u>	<u>58.6</u>	<u>53.1</u>
1.9	2.0	3.0	3.1	2.1	2.5	4.0	15.0	17.5	23.0
20	33	30	4	3	25	8	23	40	45

<u>24.5</u>	<u>24.2</u>	<u>22.6</u>	<u>23.6</u>	<u>24.6</u>	<u>24.0</u>	<u>22.5</u>	<u>65.1</u>	<u>60.4</u>	<u>54.4</u>
8.1	7.7	2.0	9.0	8.0	2.0	10.1	17.5	22.7	23.2
20	36	30	4	3	86	9	22	20	65

<u>24.0</u>	<u>24.1</u>	<u>24.1</u>	<u>23.2</u>	<u>23.9</u>	<u>23.9</u>	<u>24.8</u>	<u>66.4</u>	<u>57.2</u>
8.0	8.5	8.5	8.7	7.7	2.9	10.7	16.2	25.4
40	30	28	4	3	77	27	40	65

<u>25.3</u>	<u>24.0</u>	<u>24.2</u>	<u>25.8</u>	<u>25.2</u>	<u>25.0</u>	<u>22.9</u>	<u>68.6</u>	<u>62.4</u>
7.3	8.0	7.8	6.3	2.2	26	7.7	14.0	20.2
40	36	3	3	48	13	25	40	60

82.57

57
 check to S&BP Carolina ^{Voltaire} 7.50 62.40 62.37
 T.P. 107 69.96 7.18 1889 0.03

10 + 41.89 9UT

10 + 41.89 Sly Curb Voltaire

10 + 27.17 Sly Voltaire
LD + C.T. IN Pav. TAKEN ON A

10 + 00

9 + 75

7607

<u>21.24</u> 4.83 1.00 9UT	<u>21.84</u> 4.93 78 9UT	<u>71.49</u> 4.58 58.87 Pav	<u>71.69</u> 4.88 30 Pav	<u>21.63</u> 4.44 Pav	<u>20.91</u> 5.36 41 9UT	<u>20.36</u> 5.71 58.87 9UT	<u>69.95</u> 6.12 80 9UT
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<u>71.9</u> 42 700 cc	<u>72.04</u> 4.07 78 cc	<u>21.49</u> 4.58 58.87 Pav	<u>21.69</u> 4.88 30 Pav	<u>21.63</u> 4.44 Pav	<u>21.34</u> 4.93 41 cc	<u>21.02</u> 5.85 58.87 cc	<u>70.59</u> 5.48 80
--------------------------------	----------------------------------	--------------------------------------	-----------------------------------	-----------------------------	----------------------------------	-------------------------------------	----------------------------

<u>72.4</u> 5.7 45	<u>23.15</u> 3.92 35 cc	<u>21.67</u> 4.50 3.5 9UT	<u>21.38</u> 4.75 Pav	<u>20.27</u> 5.30 25.8 9UT	<u>21.22</u> 4.80 5.8 25	<u>71.1</u> 5.0 50
--------------------------	----------------------------------	------------------------------------	-----------------------------	-------------------------------------	-----------------------------------	--------------------------

<u>72.4</u> 3.7 40	<u>22.1</u> 2.0 50	<u>71.2</u> 2.4 2	<u>23.2</u> 2.9	<u>72.8</u> 5.2 13	<u>71.6</u> 4.5 25
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<u>22.9</u> 3.2 40	<u>22.0</u> 3.1 34	<u>22.1</u> 4.0 30	<u>22.1</u> 4.0 3	<u>22.2</u> 2.4 2	<u>23.6</u> 2.5	<u>22.1</u> 2.0 8	<u>61.7</u> 12.44 25	<u>40.6</u> 7.5 40	<u>70.6</u> 5.5 50
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76.07
5

X sec alley 20' wide
 BIK 40 La Jolla Park.

Floor
 2-3-39

W.B.P. 6.05 111.78 105.73 ^{wall} Herschel

0+14 S of wall st.

W Pav 4.71 107.07
 C " 4.64 107.14
 E " 4.56 107.22

0+00 S of wall

E cb 3.81 107.97
 E Pav 4.01 107.77
 C " 4.33 107.45
 W " 4.00 107.78
 W cb 3.95 107.83

0+20

W E 3' door side to 3.39 108.39
 W 3.8 108.0
 C 3.8 108.0
 F 3.8 108.0

0+29

E 3.8 108.0
 C 3.7 108.1
 W E 4' cent mark 3.76 108.02

0+50

W 3.5 108.13
 C 3.6 108.12

111.78

73

E 3.8 108.0
 T.P. 6.53 115.21 3.10 108.68

0+96

E E 2' cent mark 5.97 109.24
 1+00
 E-G N edge do. gar. 5.75 109.46 Corr.
 E-44 " " APRON 5.80 109.41 "
 E 5.9 109.3
 C 6.4 108.8
 W 6.2 109.0

1+18

W 6.1 109.1
 C 6.1 109.1
 E 5.9 109.3
 +4.2 S edge APRON 5.8 109.4 CORR.
 +4 " " do gar. 5.74 109.47 "

1+22

E-4 E 2' cent mark 5.68 109.53

1+27

E-4 N edge do gar. 5.04 110.17 "
 E outside cent. APRON 5.65 109.56
 C 6.0 109.2
 W 6.1 109.1

1+47

W		5.5	109.7
C		5.6	109.6
E	apron on line	5.08	109.93
+4	S edge do. gar	5.08	110.13 cem

1+54

E	S edge of 8' cem. wk	5.4	110.07 on line
---	----------------------	-----	----------------

1+59

E-5	N edge do. gar	4.33	110.88 cem,
-----	----------------	------	-------------

1+76

E-5	S edge " "	4.36	110.85 "
-----	------------	------	----------

E		5.0	110.2
---	--	-----	-------

C		5.4	109.8
---	--	-----	-------

W		5.3	109.9
---	--	-----	-------

1+87

E		4.8	110.4
---	--	-----	-------

+8.5	S. W. gar. wood fl.	4.03	111.18
------	---------------------	------	--------

1+99

E-5	E 2' cem. wk.	4.35	110.86
-----	---------------	------	--------

E		4.8	110.4
---	--	-----	-------

C		4.8	110.4
---	--	-----	-------

W		4.7	110.5
---	--	-----	-------

2+00

W-5.8	N edge do. gar	4.7	110.5 dirt
-------	----------------	-----	------------

		4.6	110.6
--	--	-----	-------

2+21

W-58	S edge do. gar	4.8	110.9	dirt
------	----------------	-----	-------	------

W		4.4	110.8
---	--	-----	-------

C		4.1	111.1
---	--	-----	-------

E		4.7	111.0
---	--	-----	-------

2+50

E		3.3	111.9
---	--	-----	-------

C		3.7	112.0
---	--	-----	-------

W		3.4	111.8
---	--	-----	-------

2+75

W ^{-0.7}	E 11' entrance	2.67	112.54	to gar. fl. Level
-------------------	----------------	------	--------	-------------------

W+1	cem apron	2.83	112.38
-----	-----------	------	--------

C		2.6	112.6
---	--	-----	-------

E		2.1	113.1
---	--	-----	-------

3+00

E-4.5	E 12' entrance	1.07	114.14	to gar. fl. Level
-------	----------------	------	--------	-------------------

E		1.4	113.8
---	--	-----	-------

C		1.4	113.6
---	--	-----	-------

W		1.7	113.5
---	--	-----	-------

3+05

W-5	N edge do. gar,	1.6	113.6	dirt
-----	-----------------	-----	-------	------

3+22

W-5	S edge " "	1.6	113.6	"
-----	------------	-----	-------	---

C		1.4	113.8
---	--	-----	-------

E		1.7	114.0
---	--	-----	-------

T.P.	8.34	122.42	113	114.08
------	------	--------	-----	--------

3+29				
W-5	N edge do. gar	8.2	114.2	dirt
W		8.2	114.2	
3+45				
W-5	S edge "	8.2	114.2	"
W		8.2	114.2	
3+51				
E		7.7	114.7	
C		8.0	114.4	
W		8.0	114.4	
+2.5	N edge do. gar	8.0	114.4	"
3+56				
E-24	S.W. gar dirt	7.0	115.4	
3+66				
-2.5	S edge do. " "	7.8	114.6	
W		7.7	114.7	
C		7.8	114.6	
E		7.3	115.1	
3+68 on W beg. fence 1.3 in alley				
4+00 " " end " " "				
4+04				
-2	N edge do. gar	6.02	116.40	CEM.
E	" " apron	6.33	116.09	"
C		7.1	115.3	
W		7.0	115.4	

4+23				
W		6.88	115.54	
+1	E 6' corr walk	6.88	115.54	
C		6.8	115.6	
E	CEM. APRON	6.23	116.19	
+2	S edge gar. cem	5.92	116.50	
4+72				
E		5.7	116.7	
C		5.8	116.6	
W		5.6	116.8	
+1	E 2-6 door	5.18	117.24	H. elev.
5+00 N.L. Silverado ST.				
W	cb	4.83	117.59	✓
W	Par	4.94	117.46	
C	"	4.91	117.51	
E	"	4.56	117.86	
E	cb	4.23	118.19	✓
5+14 N cb LINE Silverado ST.				
E	Par	4.94	117.48	
C	"	5.30	117.12	
W	"	5.57	116.85	
TP	10.42	132.72	0.12	122.30
TP	0.93	120.55	13.10	119.24
TP	3.98	111.92	12.41	107.92
check to B.M.			6.20	105.72 105.73

X sec. alley 20' wide

Blk 28 LA Jolla Park

TOP CB
Soc P. 75 4.76 124.35 117.59

no Silverado
W.L. alley

00-14 S. 6. Silverado

E Pav. Conc. gut 5.34 119.01

W " " " 5.98 118.37

00 = S. 6. Silverado

W of 5.11 119.24

W Pav Conc. 5.26 119.09

C " " 5.18 119.17

E " " 4.47 119.68

E CB 4.31 120.09

0 + 14

E on Conc fl. 3.85 120.50

+ 3.5' edge apron 4.44 119.93

C " " 5.00 119.35

W " " 5.2 119.15

0 + 25

W beg. Con. slab 5.66 118.69

+ 0.6 " wall 4.68 119.67

C " " 5.1 119.3

+ 6.5 Sedge apron 4.35 120.00

E Con. floor 3.89 120.46

0 + 36

W on Conc fl. 5.09 118.66

+ 0.6 Top wall 4.74 119.61

Slab removed
was 8" wide

Moore
7-27-29 '26

Lay grade for
2" Pav. by St. Dept.

124.35

0 + 34.10

W cement fl. 5.03 119.32

W + 0.4 wall 4.74 119.61

0 + 50

W cement fl. 4.97 119.38

+ 0.6 " wall 4.70 119.65

C " " 4.8 119.6

+ 6 " " 4.8 119.6

E on cement fl. 4.00 120.35

0 + 54

E cement fl. 4.00 120.35

+ 3.5 Sedge Conc apron 4.44 119.89

0 + 68

E cement fl. 3.93 120.42

+ 3.5 Sedge apron 4.37 119.95

C " " 4.4 119.8

W " " 4.6 119.8

0 + 89

W-3 E do. gar. dirt 4.5 119.9

S " " 4.5 119.9

C " " 4.3 120.1

E " " 3.9 120.5

124.35

1407			
-1	SIN. gar. dirt	4.7	119.7
W		4.7	119.7
+5		4.1	120.3
C		4.0	120.4
E		3.6	120.8

1450

W-10		4.4	120.0
W		3.8	120.6
+2 = E of 4 diam	Date Point		
+5		3.1	121.3
C		3.2	121.2
E		2.7	121.7

2403

-9	N edge da. gar.	0.6	124.09	CEM
-1	leg. CEM apron	1.40	122.95	
E		1.4	123.0	
C		2.0	122.4	
W		2.4	122.0	

2421

-4	Sedge SIN gar	2.0	122.4	dirt
W		2.0	122.4	
C		1.4	122.8	
E		1.4	123.2	
+1	CEM apron	1.7	123.2	
+9	Sedge da. gar	0.6	124.09	CEM

124.35

T.P. 591 128.64 142 122.73

2430			
E	E 2' CEM. WALK	4.43	124.61
2442			
E	-11 E SIN gar CEM	3.17	125.47
E	-1 CEM apron	4.56	124.05
E		5.0	123.4
C		5.4	123.4
W		5.9	122.7
+5		6.4	122.7
2491			
-20		8.1	122.5
W		5.1	123.5
E		4.8	123.8
E		4.5	124.1
+15 E	SIN gar. dirt	3.5	125.1
2408			
-3	SIN. gar dirt	4.5	124.1
E		4.6	124.0
C		4.9	123.7
W		5.3	123.3
+5		5.4	123.0

3750

-5		6.1	122.5
W		5.5	123.1
C		5.0	123.6
E		4.8	123.8

3781

-4	N edge do gar.	4.26	124.38	Cem
E	"	4.51	124.13	
C		4.9	123.2	
W		5.4	123.2	

3797

-2	SW 990 dirt	5.8	122.8	
W		5.8	122.8	
C		5.4	123.4	
E	S edge Cem apron	4.60	124.64	
+4	" do gar.	4.20	124.44	Cem

4708

E		5.3	123.3	
C		5.4	123.2	
W		5.5	123.1	
+2	SW 990 dirt	5.4	123.2	

T.P. 297 126.04 5.55 123.09

4716

-12.5	SW 990 Cem	1.10	124.26	126.06
E		2.9	123.2	10.40
C		2.9	123.2	115.40
W		3.0	123.1	

4738

-3	E do. gar. dirt	3.3	122.8	
W		3.4	122.7	
C		3.7	122.9	
E		3.0	123.1	

4757

E		3.5	122.6	
C		3.5	122.6	
W		3.8	122.3	
+3	E SW 990 dirt	3.7	122.2	

5700 = NE KLING LOT PAR.

W	cb	4.30	121.76	
W	dirt	4.8	121.3	
C	"	4.4	121.2	
E	"	4.0	122.1	
E	cb	3.64	122.44	

5714 N cb KLING

E	TOP cb	3.60	122.46	
E	dirt	4.5	121.6	
E	"	4.7	121.4	
W	"	5.3	120.8	
W	TOP cb	4.61	121.45	

S.W. COR. 11.10
+ Hatched
please look up
11.5.51
11.5.51

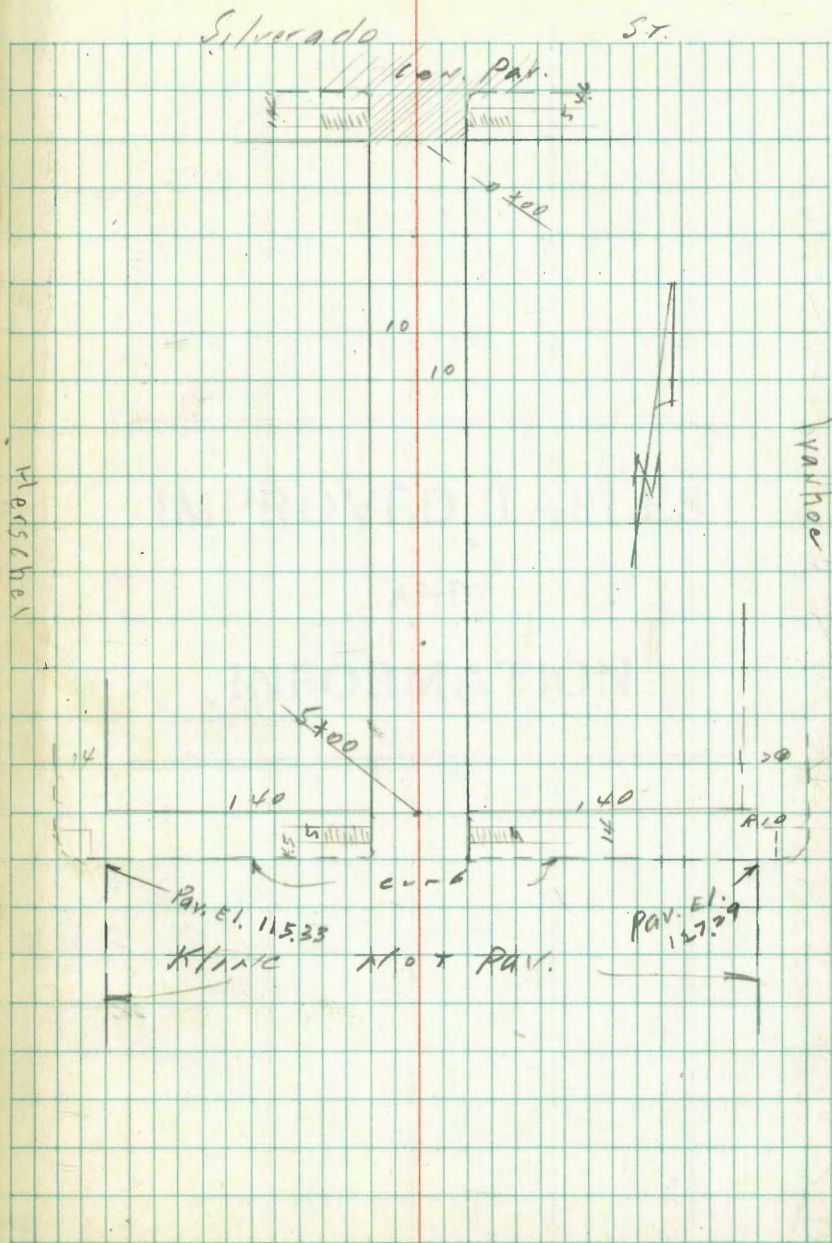
126.06
 T.P. 510 129.78 1.44 124.67

N.W. Cor Kline + Ivanhoe
 Top cb 1.84 122.94
 " Pav 2.49 127.29

B.M.S.E. 541 120.87 115.46 Kline + Herschel

N.E. Cor Kline + Herschel
 Top cb 4.86 116.01
 gut Pav. 5.54 115.33

Power Poles in clear



T.P.

To P

B.M. 6

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1 1/2 to 1.
If roadway is nearly level, the cut or fill at any
stake is located by the double entry method in
left column and top row. The number in both

IMPROVED TABLES
AND
INFORMATION

To find length and extension for curves
and other degree double or degree of curve and
add constant found in column of constant
Degree of curve with a given length
by dividing length of curve by constant
given constant for curve
The distance from a point on the tangent to
the curve is vertically the square of the
half divided by twice the radius

363.75 = sw. orange - Headwall

351.67 = Trojan - R

71	23 ✓	693
44	7 ✓	
<u>27</u>	16 0	3453
		950
		<u>12.96</u>

371.10
<u>363.75</u>
7.35

137.2
605.32

59
<u>26</u>
31

104.31
102.91
<u>1.56</u>
101.35

61
<u>33</u>
528
<u>24</u>
22

5.55
<u>590</u>
11.45
12.92
<u>213</u>
2133
123.2
12.90
67
<u>13.57</u>
6.63
19.70
13.05
7.35
20.40
150.5
35
13.00
2.11
<u>63.07</u>
15.14