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CITY OF SAN DIEGO,  
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*ENGINEERING and DRAFTING SUPPLIES*  
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MIC

Canyada Way, Richmond St. Extension N.	1 - 22
Torrence St. Reynard Way	23 - 29
Arthur. St Hawley to 35 <sup>th</sup>	30 - 33
✓ 6 <sup>th</sup> St. extension to S.D. River Bridge	34 - 48
Culvert. Arizona & Univ. Ave.	49 -
Drainage Ray to Univ. Ave	51 - 56
41 <sup>st</sup> St Epsilon to Gamma	57 - 64
Alley Blk 97 City Hts. Myrtle Dwight	65 - 69
College Way, to 200' South.	70 - 72
Alley Blk 50 City Hts. Univ to Nightman Milborough & 42	73 - 77
Survey Lot B - Blk 97 Hortons	78 -
" Per. Lot G - La Mesa Colony	79

9-1-37  
Miller  
Walker  
Bliss

Canyada Way  
Richmond St. Extension North to  
N. Line Balboa Park.

F.B. 1515-P62  
F.B. 1446-P16

+73 80 No. End. Bridge  
+69 58 B.C. spike  $\Delta 10^{\circ} 54' Lt.$

+56 80 S. End. Bridge

+50

+50

0+00

E.C.

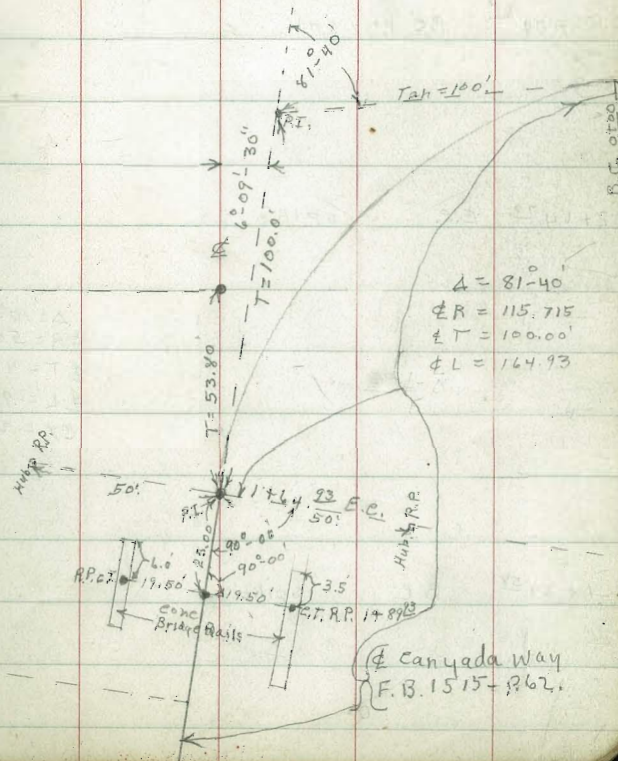
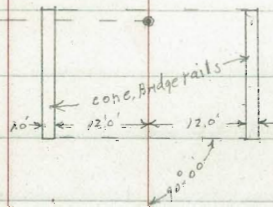
Spike

$\Delta = 6^{\circ} 09' 30''$   
 $\phi R = 1000'$   
 $\phi T = 53.80'$   
 $\phi L = 107.50'$   
 $\Sigma X = 1.45'$

B.C.

Indexed  
C.S.Kr

1



Canyada Way  
F.B. 1515-1262

£

129<sup>63</sup> B.C.

6

5+09<sup>31</sup> E.C. SPIKE

5

+50

$\Delta = 23-29 RT$   
 $\phi R = 500$   
 $\phi T = 103.92$   
 $\phi L =$   
 $\phi X = 10.67$

P.I. SPIKE

4

+50

+04<sup>38</sup> B.C. RT. SPK.

3

2+64<sup>70</sup> E.C. SPIKE

$\Delta = 10^{\circ}-54 Lt.$   
 $\phi R = 500.0$   
 $\phi T = 47.70$   
 $\phi L = 95.12$   
 $\phi X = 2.27$

P.I. SPIKE

1+69<sup>58</sup> B.C. spike

£

+14<sup>51</sup> B.C. SPIKE

9

8+53<sup>2</sup> = N. End. Bridge

8+30<sup>05</sup> E.C. SPIKE  
8+29 = S. End. Bridge

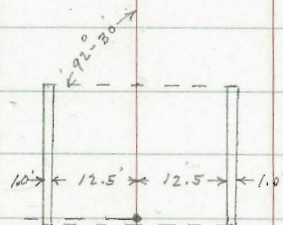
$\Delta = 8-50 \text{ Lt}$

$\phi R = 1300.0'$

$\phi T = 100.41'$

$\phi L = 200.42'$

$\epsilon X, 3.87$



P.I. spike

6+29<sup>63</sup> B.C. SPIKE

⊕

109<sup>75</sup> B.C. spike

12

11

10+29<sup>75</sup> F.C. spike

$$\Delta = 47.24 \text{ LT}$$

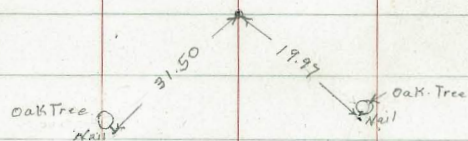
$$\phi R = 1500.0$$

$$T = 57.63$$

$$L = 115.19'$$

$$E = 1.10'$$

9+14<sup>56</sup> B.C. spike



P.I. spike

75+24<sup>44</sup> P.O.C. SPIKE

14+64<sup>49</sup> P.O.C. SPIKE N. End. Bridge

14+41<sup>03</sup> P.O.C. SPIKE S. End. Bridge

14+21<sup>48</sup> P.R.C. SPIKE

12+09<sup>95</sup> B.C. SPIKE

$$\Delta = 13.28 \text{ Lt}$$

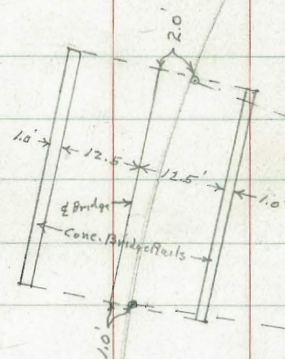
$$\phi R = 900.0$$

$$T = 106.25$$

$$L = 211.53$$

$$E_y = 6.30$$

N. Line Balboa Park



$$\Delta = 6.06$$

$$\phi R = 510.0$$

$$\phi d = 57.58$$

$$L = 59.67$$

$$\Delta = 2.24$$

$$\phi R = 510.0$$

$$\phi d = 23.45$$

$$L = 53.46$$

$$\Delta = 2.00$$

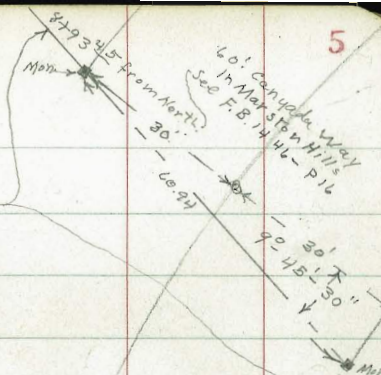
$$\phi R = 510.0$$

$$\phi d = 19.54$$

$$\phi L = 19.55$$

7.0' to Oak Tree

Oak Tree  
Nail







La Canyada X. 500.

B.M. 5.

7

B.M. Nail in

15' Lt. of sta  
14+64.00 P.O.C.  
F.B. 1446 - P.28

Lead. N.W. Gr. Bridge 2.06 188.38 186.32

T.P. 0.97 178.81 10.54 177.84

T.P 0.58 168.05 11.34 167.47

T.P. B.M. C.T.  
L.P. 19.5 R.P.  
Cof 1+89 93  
La Canyada Way

1.39 162.05 7.39 160.66

Chk. B.M. 7 1"x1" stake 55' Lt. of 5+54 9.49 152.56

152.64  
F.B. 1515 - P.73

B.M. N  
Lead. N

T  
0+55

0+48 38' Lt. of  $\phi$  sycamore 12" Diam

T.P.B.M  
L.P. 19.5  
E. of 14  
Lucanya

0+37 19' Lt. of  $\phi$  sycamore 14" Diam

Ch.M. B.

0+34

0+14 41' Lt. of  $\phi$  sycamore 14" Diam

0+08 23' Lt. of  $\phi$  sycamore Tree 20" Diam

0+00 = F.C.

12' S of 0+00 36' Lt. of  $\phi$  Sycamore Tree 12" Diam.  
37' S of 0+00 23' Lt. of  $\phi$  Sycamore Tree 18" Diam

47' S. of 0+00 41' Lt. of  $\phi$  = N. End. cobble wall w. side ditch

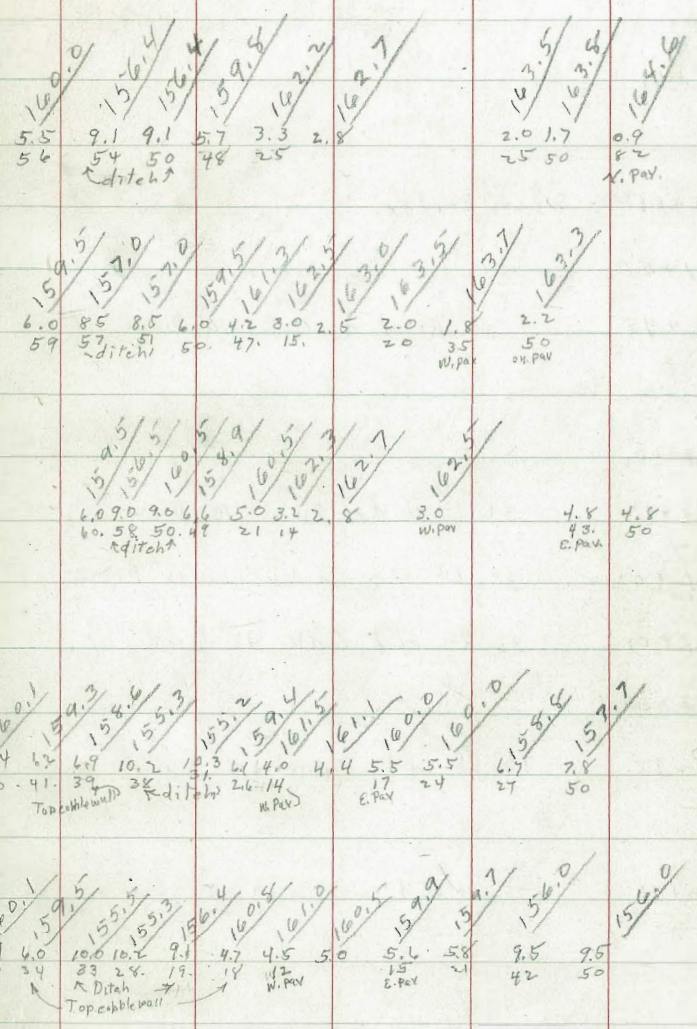
53.80 S. of 0+00 = ctr Curve.

65' S. of 0+00 23' Lt. of  $\phi$  = N. End. cobble wall E. side ditch

73' S. of 0+00

B.M. 19<sup>5</sup> R.P. — 4.84 — 165.50 —

— 160.66 — Page 7 —



— 165.50 —

B.A

Lea

1+61

T.P.

L.P.

C. of

L. ca

1+50

Chk

1+45

30' Rt of  $\phi$  Oak 16" Diam

1+25

1+12

36 Lt.  $\phi$  Pine 18" Diam.

1+02

35 Lt of  $\phi$  Torrey Pine 18" Diam

1+01

36' Rt. of  $\phi$  Oak 18" Diam

1+00

0+98

18' Lt. of  $\phi$  Pepper 12" Diam.

6+91

17.5 Rt. of  $\phi$  catch Basin 24x24 grating 12" pipe

0+75

165.50

$\phi$

9

161.5	161.3	159.4	157.3	158.9	161.0	163.0	162.3	162.3	162.2	161.5	161.5	161.5	163.5
4.0	4.2	5.7	8.2	6.6	4.5	2.5	3.2	3.2	3.3	2.5	4.0	4.0	2.6
50	34	28	27	24	5	12	12	12	12	14	18	20	50
		ditch											

161.3	161.3	160.0	157.5	157.9	161.1	162.6	162.3	162.3	162.1	162.7	163.1	164.2
42.2	5.5	8.0	7.6	4.4	2.7	3.2	3.2	3.2	3.4	2.9	2.4	1.3
50	40	31	34	27	24	29	10. Rd.		21	14	25	50
			ditch						E. Rd.			

161.0	160.5	157.7	157.4	160.3	161.3	162.3	162.3	161.9	162.4	162.2	163.7
4.5	5.0	7.8	7.7	5.2	4.2	3.2	3.2	3.6	3.1	3.3	1.8
50	44	42	36	34	30	30	11	16	15	25	50
			ditch					E. Rd.			

161.0	160.4	157.7	157.7	160.4	161.9	162.2	161.9	162.1	163.1
4.5	4.7	7.8	7.8	5.1	3.6	3.3	3.6	3.4	2.4
60	50	48	40	39	30	30	30	25	50
		ditch			W. Rd.		W. Rd.		

159.4	160.9
5.70	4.60
17.5	17.5
P.L.	grating

160.2	157.0	157.0	160.2	161.2	162.3	163.1	163.1
5.3	8.5	8.5	5.3	4.3	3.2	2.4	2.4
55	53	50	48	25	30	25	50
		ditch					

145.50

B  
L  
T  
L  
Lo  
Ch

2710  
2703 21' Lt of d Pine 16" Diam  
1798 31' Lt of d Pine 14" Diam  
1790  
1788 34' Lt of d Pine 14" Diam  
1788 21' Lt of d Pine 18" Diam

1770  
T.P.N.E  
Cor Bridge 6.55 169.65 2.40 163:10 1773<sup>80</sup>

1773<sup>80</sup> N. End. Bridge

1770  
1768 28' Lt. of d Pine 18" Diam

1769

1762

165.50

162.2  
7.5  
50

162.55  
7.4  
50

163.5  
6.2  
11

162.85  
6.9  
10  
N Rd

162.9  
6.8  
6

163.0  
6.4  
10  
ERd

163.4  
6.3  
14

162.4  
7.3  
30

159.1  
10.6  
33  
Ditch

162.5  
7.2  
37

163.0  
6.7  
39

163.0  
6.4  
50

162.0  
7.7  
50

162.4  
7.3  
25

163.2  
6.5  
13

162.7  
7.0  
12  
N Rd

162.7  
7.0  
12  
ERd

163.3  
6.1  
28

162.4  
6.1  
31

158.9  
10.8  
32  
Ditch

158.6  
11.1  
37

161.6  
8.1  
37

163.0  
6.7  
43

163.4  
6.4  
50

161.4  
7.9  
50

162.3  
7.4  
25

163.3  
6.4  
13  
W Rd

162.6  
7.2  
12  
W Rd

162.5  
7.1  
12  
ERd

162.6  
6.5  
13

162.9  
6.8  
23

161.2  
8.5  
24

158.9  
10.6  
25  
Ditch

158.4  
11.8  
32  
Ditch

161.3  
6.0  
33

163.0  
6.0  
37

163.0  
6.0  
50

169.65

161.5  
4.0  
50

161.9  
3.6  
30

161.3  
4.2  
14

162.1  
2.4  
13  
conc  
Rail

162.3  
3.2  
12  
W Rd

162.3  
3.2  
12

162.3  
3.2  
12  
ERd

162.1  
2.4  
12  
conc  
Rail

161.3  
4.2  
15  
ditch

158.4  
6.7  
7.1  
7.1  
15  
ditch

158.4  
7.1  
2.9  
2.9  
3.0  
3.3  
5.0

161.5  
4.0  
50

161.9  
3.6  
30

161.1  
4.4  
16.14  
Ditch

158.3  
4.2  
13  
conc  
Rail

163.1  
2.4  
12  
W Rd

162.3  
3.2  
12  
W Rd

162.3  
3.2  
12

162.3  
3.2  
12  
ERd

162.1  
2.4  
12  
conc  
Rail

161.2  
4.2  
13  
ditch

158.4  
6.7  
7.1  
7.1  
13  
ditch

161.0  
4.5  
2.9  
2.9  
3.1  
5.0

161.5  
4.0  
50

161.3  
4.2  
31

159.6  
5.7  
27

158.7  
6.8  
26  
Ditch

163.0  
2.5  
18  
conc  
Rail

162.3  
3.2  
12  
W Rd

162.3  
3.2  
12  
W Rd

162.2  
3.3  
17  
ERd

162.0  
2.5  
12  
conc  
Rail

158.0  
7.5  
13  
Ditch

158.1  
7.4  
17

161.4  
4.1  
18

162.9  
2.6  
20

163.0  
1.7  
50

165.50

E  
L  
T  
C.  
L  
C

3+00

2+99 26 Lt of Pine 24" Diam

2+98 36 Lt of Pine 16" Diam

2+95 41 Rt of Oak 14" Diam

2+79 19 Rt of Oak 14" Diam

2+73 38 Lt of Pine 16" Diam

2+70 23 Lt of Pine 18" Diam

2+60 34 Lt of Pine 14" Diam

2+60 28 Lt of Pine 14" Diam

2+52 21 Lt of Pine 16" Diam

2+50

2+48 30 Lt of Pine 18" Diam

2+39 20 Lt of Pine 18" Diam

2+38 37 Lt of Pine 14" Diam

2+37 16 Rt of Oak 18" Diam

2+30 28 Lt of Pine 5" Diam

2+25 39 Lt of Pine 14" Diam

2+17 24 Lt of Pine 10" Diam

2+12 35 Lt of Pine 14" Diam

~~169.65~~

$\frac{166.4}{3.3}$	$\frac{164.7}{5.0}$	$\frac{164.7}{5.0}$	$\frac{164.2}{5.4}$	$\frac{163.8}{5.9}$	$\frac{163.9}{5.8}$	$\frac{164.3}{5.6}$	$\frac{163.1}{6.6}$	$\frac{160.7}{9.0}$	$\frac{160.4}{9.3}$	$\frac{162.6}{7.1}$	$\frac{163.1}{6.2}$	$\frac{163.7}{6.0}$
50	20	12	11	11	13	14	24	27	32	33	37	50
			W.R.		E.R.			Ditch				

$\frac{162.4}{6.9}$	$\frac{163.1}{4.4}$	$\frac{164.0}{5.7}$	$\frac{163.4}{6.3}$	$\frac{163.3}{6.4}$	$\frac{163.6}{4.1}$	$\frac{163.8}{5.9}$	$\frac{163.0}{6.7}$	$\frac{161.2}{10.1}$	$\frac{159.1}{10.1}$	$\frac{164.4}{10.1}$	$\frac{162.2}{7.5}$	$\frac{163.4}{6.3}$	$\frac{162.6}{6.1}$
50	20	13	11	11	11	12	24	27	28	33	36	39	50
			W.R.		E.R.					Ditch			

~~169.65~~

+70 39 RT of  $\phi$  Oak 12" Diam

+64 25 Lt of  $\phi$  Pine 6" Diam

+50

+44 39 RT of  $\phi$  Oak 4" Diam

+42 32 Lt of  $\phi$  Pine 8" Diam

+32 28 Lt of  $\phi$  Pine 8" Diam

+25

+25 40 RT of  $\phi$  Oak 10" Diam

4+00

3+83 37 RT of  $\phi$  Oak 10" Diam

3+75

3+64 41 RT of  $\phi$  Oak 6" Diam

3+50

3+50 35 RT of  $\phi$  Oak 8" Diam

3+42 12 RT of  $\phi$  Catch basin gratin, 23 RT Outlet 12" Cor. I Column

3+32 38 RT of  $\phi$  Oak 10" Diam

3+25

3+15 30 Lt of  $\phi$  Pine 8" Diam

3+13 38 RT of  $\phi$  Oak 8" Diam

169.65

172.5	172.2	169.9	167.6	167.2	166.6	166.1	165.5	166.4	166.2	164.7	161.6	161.6	161.6	165.1
+3.8	+1.5	+0.2	2.1	2.5	3.1	3.6	4.2	3.3	3.5	5.0	8.1	8.1	5.1	4.5
40	35	22	16	13	W.Rd.	14	2 Rd	15	21	23	26	30	34	50
											Ditch			

173.7	170.9	167.1	166.7	166.2	165.7	164.9	166.0	165.2	164.5	161.3	161.2	161.2	164.0	165.2
+4.0	+1.2	2.1	3.0	3.5	4.0	4.8	3.7	3.9	5.2	8.9	8.4	5.7	4.0	4.5
40.	26.	17.	13	12	W.Rd.	24	E.Rd.	15	21	25	29	32	37	50
											Ditch			

175.4	174.7	166.3	166.3	165.7	165.2	164.5	165.3	165.6	164.3	161.1	161.3	163.7	164.7	165.2
+6.7	+5.0	3.4	3.4	4.0	4.5	5.2	4.4	4.1	5.4	8.6	8.4	5.0	5.0	5.0
40	35	20	12	11	W.Rd.	13	E.Rd.	14	17	21	23	28	31	50
											Ditch			

176.7	175.0	166.0	165.2	164.7	164.2	165.0	165.0	163.1	161.1	161.1	162.7	164.2	164.5	165.2
+7.0	+5.3	3.7	4.5	5.0	5.5	4.7	4.7	4.6	8.6	8.7	7.0	5.5	5.2	5.2
45	38	26	12	12	W.Rd.	13	14	19	23	24	31	35	50	50
											Ditch			

174.2	172.7	167.7	165.5	165.2	164.7	164.3	164.1	164.7	164.1	162.5	160.7	160.7	162.2	163.9	163.7
+4.5	+3.0	2.0	4.2	4.5	5.0	5.6	4.5	5.6	5.6	7.2	8.0	7.0	7.5	5.5	5.0
40.	36.	30	24	13	12	W.Rd.	12	13	14	19	23	24	30	33	50

168.7	167.9	165.2	164.6	164.1	164.1	164.7	164.3	163.9	160.7	160.7	162.2	160.5	163.5	163.5
4.0	1.8	4.5	5.1	5.6	5.6	5.6	5.0	5.4	6.7	7.0	6.0	6.2	6.2	6.2
40	28	25	11	5	12	W.Rd.	12	13	18	22	23	30	33	50

169.65

+85 31. RT of  $\phi$  Oak 16" Diam  
 +77 47. RT of  $\phi$  Oak 10" Diam.

+75 19. LT of  $\phi$  Oak 8" Diam.

+58 29. RT of  $\phi$  Oak 14" Diam.

+60

+49 { 26. LT of  $\phi$  Oak 12" Diam.  
 22. LT of  $\phi$  Acacia 4" Diam.

+43 27. LT of  $\phi$  Eucalyptus 6" Diam.

+36 19. LT of  $\phi$  oak 5" Diam.

+25 { 26. LT of  $\phi$  Oak 6" Diam.  
 44. RT of  $\phi$  Oak 8" Diam.

+09 41. RT of  $\phi$  Oak. 12" Diam

5400

T.P. 7.24 173.97 2.92 166.73

+91 43. RT of  $\phi$  Oak 8" Diam.

+88 23. LT of  $\phi$  Pine 12" Diam.

+81 20. RT of  $\phi$  Oak. 14" Diam.

+75

+75 21. LT of  $\phi$  Pine 10" Diam

169.65

173.35  
 0.5 4.0 5.1 5.7 6.2 6.4 5.8 6.0 7.0 7.7 11.9 11.9 12.0 7.8 7.0  
 40 16 13 13 H. Rd. 15 16 19 24 35 38 44 47 50  
 E. Rd. Ditch

173.0  
 1.0 1.9 5.0 6.5 7.0 7.6 6.8 7.1 8.6 11.5 11.5 8.5 7.2  
 40 35 15 12 13 13 14 21 25 27 34 38 50  
 H. Rd. E. Rd. Ditch

172.2  
 12.5 11.5 0.4 2.2 2.7 3.1 3.6 3.0 3.3 5.1 7.5 7.5 4.6 4.3  
 36 35 18 13 12 12 12 13 19 25 27 35 37 50  
 H. Rd. E. Rd. Ditch

169.65



+15 12" Cor. I. Culvert.

$\frac{173.9}{0.9}$	$\frac{172.5}{2.3}$	$\frac{168.4}{6.4}$	$\frac{170.6}{4.2}$	4	$\frac{170.4}{4.4}$	$\frac{170.3}{4.5}$	$\frac{171.0}{3.8}$	$\frac{170.1}{4.7}$	$\frac{165.5}{9.3}$	$\frac{166.0}{8.8}$	$\frac{165.5}{9.3}$	$\frac{167.6}{7.2}$	$\frac{168.7}{6.1}$
40	22	11.5 F.L.	10. Cath. B. Grading		10. E. Rd.	14 C. B. Grk.	21	21	26 ditch	30 ditch	36	50	

+05 34.4t Oak 12" Diam

$\frac{173.5}{1.3}$	$\frac{172.2}{2.6}$	$\frac{171.1}{3.7}$	$\frac{170.1}{4.7}$	$\frac{170.2}{4.6}$	$\frac{170.3}{4.5}$	$\frac{170.8}{4.0}$	$\frac{169.3}{5.5}$	$\frac{164.6}{10.2}$	$\frac{164.6}{10.2}$	$\frac{167.4}{7.0}$	$\frac{168.5}{6.3}$
40	22	17	13 W.Rd.		11 E. Rd.	19	20	22 Ditch	35	34	50

+00 { 40.4t Oak 14" Diam  
+91 { 23.1t Oak 6" Diam

+87 87.8t Oak 14" Diam

+85

$\frac{173.2}{1.6}$	$\frac{172.0}{2.8}$	$\frac{170.8}{4.0}$	$\frac{169.8}{5.0}$	$\frac{169.9}{4.9}$	$\frac{170.2}{4.5}$	$\frac{165.4}{6.0}$	$\frac{167.6}{7.2}$	$\frac{164.0}{10.4}$	$\frac{164.0}{10.4}$	$\frac{167.1}{7.7}$	$\frac{168.0}{6.2}$
40	22	15	13 W.Rd.	12 E. Rd.	15	20	28	30 Ditch	38	39	50

+71 29.8t Oak 10" Diam

+70 51.8t Oak 14" Diam

+53 45.8t Oak 18" Diam

+50

$\frac{173.6}{1.2}$	$\frac{172.6}{2.1}$	$\frac{171.2}{3.6}$	$\frac{169.6}{5.0}$	$\frac{169.1}{5.7}$	$\frac{169.2}{5.6}$	$\frac{169.3}{5.5}$	$\frac{169.4}{5.0}$	$\frac{165.4}{6.4}$	$\frac{167.1}{7.7}$	$\frac{164.7}{10.1}$	$\frac{164.7}{10.1}$	$\frac{168.5}{8.0}$	$\frac{168.4}{6.4}$
40	30	17	13 W.Rd.	13 W.Rd.	15 E. Rd.	18	22	22	32	31 ditch	37	40	50

+37 22.4t Oak 5" Diam

+35 27.8t Oak 14" Diam

T.P 8.10 — 174.83 — 7.24 — 166.73

174.83

+28 85.8t of Sewer M.H.

+12 20.4t of Oak 14" Diam

+00

$\frac{173.4}{0.6}$	$\frac{170.3}{3.7}$	$\frac{168.4}{5.6}$	$\frac{168.4}{5.6}$	$\frac{169.0}{5.6}$	$\frac{169.0}{5.6}$	$\frac{167.6}{6.4}$	$\frac{165.4}{8.2}$	$\frac{163.5}{10.5}$	$\frac{163.5}{10.5}$	$\frac{167.2}{6.8}$
40	17	12 W.Rd.	13 W.Rd.	14 E. Rd.	14	18	23	37 Ditch	39	50

173.97

173.97

E

- +20 78 Rt. Oak. 8" Diam
- +13 33 Lt. Oak. 8" Diam
- +11 51 Rt. Oak. 6" Diam
- +10 { 65 Rt. Oak. 12" Diam  
20 Rt. Oak. 5" Diam
- +05 21 Lt. Oak. 8" Diam
- 8700
- +99 64 Rt Oak. 10" Diam.
- +95 { 42 Lt. Oak 6" Diam  
29 Lt. Oak 15" Diam
- +86 { 34 Rt. Oak. 8" Diam  
21 Lt. Oak. 7" Diam
- +83 54 Rt. Oak. 10" Diam.
- +75 { 33 Lt Oak 6" Diam.  
40 Rt. Oak 16" Diam
- +72 23 Rt. Oak. 8" Diam.
- +65 22 Lt. Oak 10" Diam
- +53 30 Lt. Oak 10" Diam
- +50
- +41 20 Lt. Oak, 8" Diam
- +36 33 Lt. Oak 10" Diam
- +23 33 Lt Oak. 10" Diam

174.6  
80  
40

173.4  
15

172.7  
21  
14  
W.Rd

172.2  
2.6  
12  
E.Rd

172.2  
2.0  
15

172.4  
31  
25

171.7  
4.7  
50

170.1  
1.1  
70

168.7  
7.7  
71  
Ditch

167.1  
7.7  
77

167.1  
6.1  
80

174.3  
0.5  
40

173.1  
1.7  
20

172.2  
2.6  
16

171.2  
3.6  
13  
W.Rd

171.1  
3.7

170.8  
4.0  
12  
E.Rd

172.0  
2.8  
15

170.6  
4.2  
20

168.4  
6.4  
36

166.8  
8.8  
38  
Ditch

166.0  
8.8  
45

165.2  
4.6  
47

165.9  
5.9  
50

174.83

174.83

+52

$\frac{175.4}{28.55}$	$\frac{172.7}{9.3}$	$\frac{168.9}{9.3}$	$\frac{165.9}{1.0}$	$\frac{172.2}{3.8}$	$\frac{174.4}{4.5}$	$\frac{173.7}{4.8}$	$\frac{173.4}{4.8}$	$\frac{173.4}{4.8}$	$\frac{173.1}{5.1}$	$\frac{171.6}{6.6}$	$\frac{169.9}{8.3}$	$\frac{172.2}{8.0}$
SS 50	43	ditch	34	14	12 W.Rd.	12 W.Rd.	12 E.Rd.	14	14	15	70	90

+45

$\frac{175.4}{2.8}$	$\frac{173.7}{4.5}$	$\frac{168.9}{9.3}$	$\frac{165.9}{9.3}$	$\frac{168.6}{9.2}$	$\frac{172.6}{5.4}$	$\frac{173.6}{4.6}$	$\frac{173.3}{9}$	$\frac{173.3}{4.9}$	$\frac{168.5}{9.7}$	$\frac{168.5}{9.7}$	$\frac{165.2}{10.0}$	$\frac{167.6}{10.6}$	$\frac{167.2}{11.0}$	$\frac{162.2}{11.0}$	$\frac{152.2}{14.0}$
50	45	44	33	15	14	12 W.Rd.	9	12 E.Rd.	14	30	60	90	105	106	106

N. edge ditch  
90° on 2 N. E. side ditch

+37

$\frac{175.4}{2.8}$	$\frac{173.2}{5.0}$	$\frac{172.6}{5.4}$	$\frac{165.7}{9.5}$	$\frac{164.6}{9.6}$	$\frac{173.2}{5.4}$	$\frac{173.5}{4.7}$	$\frac{173.2}{5.0}$	$\frac{173.2}{5.0}$	$\frac{168.5}{9.7}$	$\frac{165.5}{9.7}$	$\frac{165.0}{10.2}$	$\frac{167.5}{10.7}$	$\frac{167.2}{11.0}$	$\frac{151.2}{11.0}$	$\frac{150.2}{12.0}$
50	40	33	32	15	14	12 W.Rd.	12 E.Rd.	14	14	30	60	90	107	108	108

S. Bank  
ditch  
S. side

+35

$\frac{175.4}{2.8}$	$\frac{173.4}{4.8}$	$\frac{172.4}{5.4}$	$\frac{164.7}{9.5}$	$\frac{172.6}{5.4}$	$\frac{173.5}{4.7}$	$\frac{173.5}{4.7}$	$\frac{173.1}{5.0}$	$\frac{173.1}{5.1}$	$\frac{173.2}{6.0}$	$\frac{168.5}{9.7}$	$\frac{165.2}{10.0}$	$\frac{167.4}{10.6}$	$\frac{167.2}{11.0}$	$\frac{167.2}{11.0}$	$\frac{150.2}{12.0}$
50	46	37	32	28	14	12 W.Rd.	12 E.Rd.	14	14	30	60	90	73	109	110

S. Bank  
S. side  
S. Bank

+32

$\frac{175.4}{2.8}$	$\frac{174.2}{4.0}$	$\frac{173.4}{4.4}$	$\frac{173.4}{4.7}$	$\frac{173.5}{4.7}$	$\frac{173.5}{4.7}$	$\frac{173.1}{5.1}$	$\frac{173.1}{5.1}$	$\frac{174.7}{5.1}$	$\frac{171.4}{3.5}$	$\frac{170.5}{7.7}$	$\frac{169.5}{8.1}$	$\frac{167.2}{11.0}$	$\frac{167.2}{11.0}$	$\frac{172.2}{11.0}$	$\frac{172.2}{11.0}$	$\frac{172.2}{11.0}$
50	40	27	14	13	12	12 W.Rd.	12 E.Rd.	12	13	30	60	90	93	110	111	111

conc. Rail  
S. side  
S. Bank  
Ditch

+25 40 H. Oak. 9" Diam.

87 24 12 H. Oak. 10" Diam.

Σ

+ 13

7.7	7.8	9.0	4.7	4.0	3.2	3.0	4.0	3.8	4.5	0.0	+ 4.0
75	62	53	52	33	26	17	16	13	16		30
Ditch		E. side		W. Rd							
78-102 N.S.W. side											

10+00

5.0	7.8	9.0	4.7	3.6	4.6	4.6	4.7	0.0	+ 3.5
64	62	46	44	16	15	13	17		30
Ditch		W. Rd		E. Road					

+ 50

6.0	9.0	9.0	5.2	4.1	4.8	4.8	4.6	0.5	+ 3.2
54	50	40	39	17	15	13	18		30
Ditch		W. Rd							

+ 49

37 Lt. Oak. 10" Diam  
 47 Lt. Eucalyptus 6" Diam  
 55 Lt. Oak. 8" Diam

+ 17

35 Rt. Oak 7" Diam  
 38 Lt. Oak 10" Diam

+ 84

34 Rt. Oak. 9" Diam  
 31 Lt. Oak 10" Diam

9+00

6.0	9.5	9.5	6.0	4.7	5.2	5.6	5.4	3.3
53	50	40	39	14	13	13	13	30
Ditch				W. Rd		E. Rd		

+ 92

44 Rt. Oak 11" Diam

+ 81

26 Lt. Oak 8" Diam

+ 79

38 Rt. Oak. 12" Diam

+ 75

6.2	10.2	10.2	6.4	4.8	5.6	6.0	5.7	6.6
52	47	41	40	14	13	13	13	30
Ditch				W. Rd		E. Rd		

+ 69

21 Lt. Oak 7" Diam  
 50 Rt. oak. 7" Diam  
 31 Lt. Oak 16" Diam

+ 61

8+59

37 Rt Oak. 18" Diam.

179.53

179.53

+97 37 Lt. Oak. 14" Diam

+88 22 Lt. Oak. 16" Diam

+79 33 Lt. Oak 10" Diam

+74 Culvert catch basins #12" Cor. I. Culvert to W.

T.P. 7.55 185.84 124 178.29

+65 { 42 Lt Oak 8" Diam

{ 27 Lt. Oak. 12" Diam

+50 35 Lt. Oak 5" Diam

+43 24 Lt. Oak 8" Diam

+26 28 Lt. Oak. 12" Diam.

+16 37 Lt. Oak. 5" Diam

1100

+94 31 Lt. Oak 6" Diam

+69 36 Lt. Oak. 12" Diam

+58 28 Lt Oak. 6" Diam

+50

10725

8.6 53	10.8 50	12.0 46	10.74 44	6.2 30	1.79 15	6.9 18	7
177.2	178.0	175.6	175.1	179.0	179.6	179.6	178.7
N. Rd.							E. Rd.
ditch							Catchment
HL							
185							84

2.5 86	5.0 83	5.0 72	2 70	1.4 50	0 35	0.179 15	1.0 14	3	1.3 14	+23 17	+3.7 30	
177.0	174.5	174.5	172.3	175.1	179.5	179.5	178.5	175.5	178.2	175.2	151.6	153.2
Ditch												
C.R.D.												

2.6 50	0.6 26	1.0 16	2.2 15	2.0 14	2.0 14	3.0 14	2.2 14	3.0 20	
176.9	178.9	178.5	177.3	177.5	176.5	175.5	181.8	183.9	
M.R.D.									E.R.D.

4.0 50	3.1 35	2.0 12	3.2 15	3.0 14	3.9 14	4.2 18	4.2 18	4.2 18	4.0 18	4.0 30
175.5	176.4	177.5	176.3	176.5	175.6	181.5	181.5	181.5	181.5	183.5
W.R.D.										
C.R.D.										

8.5 72	4.7 53	4.0 37	2.8 17	3.7 15	3.5	4.2 13	4.2 13	4.2 13	4.2 13	4.2 13	4.2 13	4.2 13	4.2 13	4.2 13	4.2 13
171.0	174.8	174.4	173.5	176.7	175.4	176.0	175.3	182.2	182.2	182.2	182.2	182.2	182.2	182.2	182.2
North Bank															
E.R.D.															

179.53

179.53

13+00 { 23 Rt. Oak 8" Diam.  
 +99 { 29 Lt. Oak 7" Diam  
 +90 13 Rt. Oak. 14" Diam  
 +84 21 Lt. Oak 6" Diam  
 +81 26 Lt. Oak. 11" Diam.  
 +75  
 +69 22 Rt. Oak. 13" Diam  
 +50  
 +49 27 Rt. Oak. 14" Diam  
 +48 25 Lt. Oak 8" Diam  
 +46 38 Lt. Oak 7" Diam  
 +37 17 Rt. Oak 13" Diam.  
 → +25 out. of place  
 +35 31 Rt. Oak 17" Diam  
 +33 30 Lt. Oak 7" Diam  
 +21 { 21 Rt. Oak 12" Diam  
 { 32 Lt. Oak. 16" Diam  
 +19 22 Lt. Oaks. 14" Diam  
 +08 28 Lt. Oak 12" Diam  
 12+00 19 Rt. Oak 12" Diam.

185.84

②

	$\frac{180.0}{58}$	$\frac{152.2}{3.6}$	$\frac{150.7}{5.1}$	$\frac{151.4}{4}$	$\frac{151.6}{4.2}$	$\frac{153.0}{2.8}$	$\frac{154.2}{1.6}$
	50	11	W.Rd	E.Rd	12	30	
	$\frac{175.5}{56}$	$\frac{179.7}{55}$	$\frac{162.0}{3.8}$	$\frac{150.3}{5.5}$	$\frac{150.9}{4.9}$	$\frac{151.0}{4.4}$	$\frac{152.2}{3.0}$
	56	55	W.Rd	W.Rd	E.Rd	E.Rd	13
	$\frac{175.5}{54}$	$\frac{175.5}{52}$	$\frac{151.5}{14}$	$\frac{129.2}{6.0}$	$\frac{150.3}{5}$	$\frac{150.5}{5.4}$	$\frac{153.8}{3.0}$
	54	52	E.Rd	W.Rd	E.Rd	E.Rd	14
	$\frac{175.2}{7.6}$	$\frac{175.4}{10.4}$	$\frac{175.4}{10.4}$	$\frac{175.5}{7.0}$	$\frac{180.6}{5.0}$	$\frac{179.3}{6.5}$	$\frac{179.6}{6.2}$
	54	52	52	45	15	14	14
			Ditch			W.Rd	E.Rd
	$\frac{175.5}{8.3}$	$\frac{175.5}{10.3}$	$\frac{175.5}{10.3}$	$\frac{175.5}{7.0}$	$\frac{180.2}{5.6}$	$\frac{179.1}{6.7}$	$\frac{179.3}{6.5}$
	50	49	47	41	12	12	5
					W.Rd	E.Rd	E.Rd
	$\frac{175.5}{8.3}$	$\frac{175.5}{10.3}$	$\frac{175.5}{10.3}$	$\frac{175.5}{7.0}$	$\frac{180.2}{5.6}$	$\frac{179.1}{6.7}$	$\frac{179.3}{6.5}$
	50	49	47	41	12	12	5
					W.Rd	E.Rd	E.Rd
	$\frac{175.5}{8.3}$	$\frac{175.5}{10.3}$	$\frac{175.5}{10.3}$	$\frac{175.5}{7.0}$	$\frac{180.2}{5.6}$	$\frac{179.1}{6.7}$	$\frac{179.3}{6.5}$
	50	49	47	41	12	12	5
					W.Rd	E.Rd	E.Rd

185.84

+36 17 Lt. Trippte Eucalyptus Each 14" Diam

+21<sup>38</sup>

+17 38 Lt. Oak 12" Diam

+10 19 Lt Oak 8" Diam

14+00

94 22 Lt Oak 6" Diam

89 34 Lt. Oak 11" Diam

{43 " Oak 12" Diam

77 {28 Lt. Oak 10" Diam

+71 27 Rt. oak 5" Diam

+62 24 Lt. Oak 6" Diam

+54 28 Rt. Oak 11" Diam

+50

+46 17 Rt. Oak 7" Diam

+42 33 Lt. Oak 12" Diam

+40 30 Rt. Oak 7" Diam

+30 26 Lt. Oak 12" Diam

+23 24 Rt. Oak 18" Diam

+18 14 Rt. Oak 9" Diam

+13 22 Lt. Oak 7" Diam

13+10 25 Rt. Oak 10" Diam

185.84

182.3  
3.5 7.0 7.0 5.1 3.7 1.3  
59 57 50 44 27 20  
Rd. ditch

178.8

178.5

150.7

152.1

154.3

155.1

154.0

154.2

154.5

153.6

153.0 20

181.5  
4.0 7.7 7.7 5.2 3.5 1.2 1.3 2.4 2.3  
17 65 55 50 26 20 15 14 23  
Rd. ditch

176.1

175.1

150.6

152.3

154.6

154.5

153.4

153.5

153.8

153.1

153.1

179.6  
5.0 8.5 8.5 6.0 5.2 4.8 4.0 3.7 3.4 2.1 2.1  
79 74 67 66 50 44 13 13 13 5 30  
ditch W. Rd. E. Rd.

177.3

177.3

179.5

150.6

153.0

151.5

152.1

152.5

153.0

153.7

185 84

+58

$\frac{183.0}{7.3}$	$\frac{155.0}{5.3}$	$\frac{154.4}{5.9}$	$\frac{155.1}{5.0}$	$\frac{155.1}{5.2}$	$\frac{154.8}{5.5}$	$\frac{150.3}{5.0}$
35	25	15	14 W.R.A.	5 E.R.A.	11	5.0

+56

$\frac{183.5}{6.8}$	$\frac{183.5}{10.5}$	$\frac{179.8}{10.5}$	$\frac{179.8}{10.5}$	$\frac{185.0}{5.3}$	$\frac{185.0}{5.3}$	$\frac{185.3}{5.0}$	$\frac{179.8}{7.0}$	$\frac{150.1}{10.2}$	$\frac{183.3}{7.0}$	$\frac{184.3}{6.0}$
35	27	W.Ditch	15	14 W.R.A.	3	10 E.R.A.	12 W.Ditch	7.5	40 N. Bank.	5.0

+48

$\frac{152.1}{8.2}$	$\frac{152.1}{8.2}$	$\frac{150.0}{10.3}$	$\frac{150.1}{10.2}$	$\frac{184.3}{6.0}$	$\frac{184.6}{5.5}$	$\frac{184.9}{5.4}$	$\frac{155.3}{5.0}$	$\frac{179.9}{10.4}$	$\frac{150.0}{10.3}$	$\frac{152.5}{10.0}$
41	35	34 Ditch	19	18	14 W.R.A.	5.4	10 E.R.A.	12 S. Ditch	30 N. side	5.0 ditch

+43

$\frac{150.4}{9.9}$	$\frac{178.9}{11.4}$	$\frac{179.6}{10.7}$	$\frac{152.8}{7.5}$	$\frac{184.1}{6.2}$	$\frac{155.5}{4.8}$	$\frac{184.6}{5.7}$	$\frac{184.6}{5.7}$	$\frac{185.1}{5.2}$	$\frac{184.6}{5.7}$	$\frac{183.0}{7.3}$	$\frac{150.0}{10.3}$	$\frac{150.2}{10.1}$
45	41 Ditch	29	26	23	14 W.R.A.	13	5 E.R.A.	11.2 E.R.A.	13	24 S. Bank	10.1 S.S.	5.0 de Ditch

+41<sup>03</sup>

$\frac{150.4}{7.9}$	$\frac{178.9}{11.4}$	$\frac{179.6}{10.7}$	$\frac{152.8}{7.5}$	$\frac{184.1}{6.2}$	$\frac{155.5}{4.8}$	$\frac{184.6}{5.7}$	$\frac{184.6}{5.7}$	$\frac{185.1}{5.2}$	$\frac{184.6}{5.7}$	$\frac{183.0}{7.3}$	$\frac{150.0}{10.3}$	$\frac{150.2}{10.1}$
45	41 Ditch	29	27	23	14 W.R.A.	13.5 W.R.A.	5	11.5 E.R.A.	12.9 S. Bank.	7.0	5.0	5.0

T.P. — 5.56 — 190.28 — 1.112 — 184.72 —

— 185.84 —

— 190.28 —

— 185.84 —



orig B.M. Nail in lead  
N.W. Cor Bridge

3.96 186.32 1.4+6.4

15 Lt. of etc

+06

9 Rt. Oak, 7" Diam

15+00

+93

28 Lt. Eucalyptus 36" Diam

+84

20 Lt. Eucalyptus 24" Diam

+82

17 Lt Eucalyptus 24" Diam

+79

20 Rt. Oak 20" Diam

+75

190.28

$\frac{185.6}{1.5}$	$\frac{185.1}{2.2}$	$\frac{187.1}{3.2}$	$\frac{186.1}{4.2}$	$\frac{185.8}{4.5}$	$\frac{185.8}{4.5}$	$\frac{185.6}{4.7}$	$\frac{185.8}{5.0}$
50	40	18	17	5	E. Rd	12	50

$\frac{187.7}{2.6}$	$\frac{186.0}{4.3}$	$\frac{185.4}{4.9}$	$\frac{185.4}{4.9}$	$\frac{185.4}{4.9}$	$\frac{184.8}{5.5}$	$\frac{184.3}{5.0}$
50	30	14	9	E. Rd	15	50
	W. Rd					

190.28

Xsec of Torrence St.  
~~Goldfinch Ely 240'~~  
 Reynard Way

50' wide  
 10' c60  
 75' 114'

17000  
 Sisson  
 Walker  
 10-14-37

Indexed  
 C.S.K.

23

N.E.B.P.	0.25	257.24		256.99	SUTTER Goldfinch
T.P.	0.73	248.92	9.05	248.19	
T.P.	0.48	237.12	12.28	236.64	
T.P.	7.28	231.90	12.50	224.62	

Sec. B

N	Top cut of Reynard Way Goldfinch	16.1	215.8
+06	" " Torrence	16.8	215.1

Sec C. #0+00

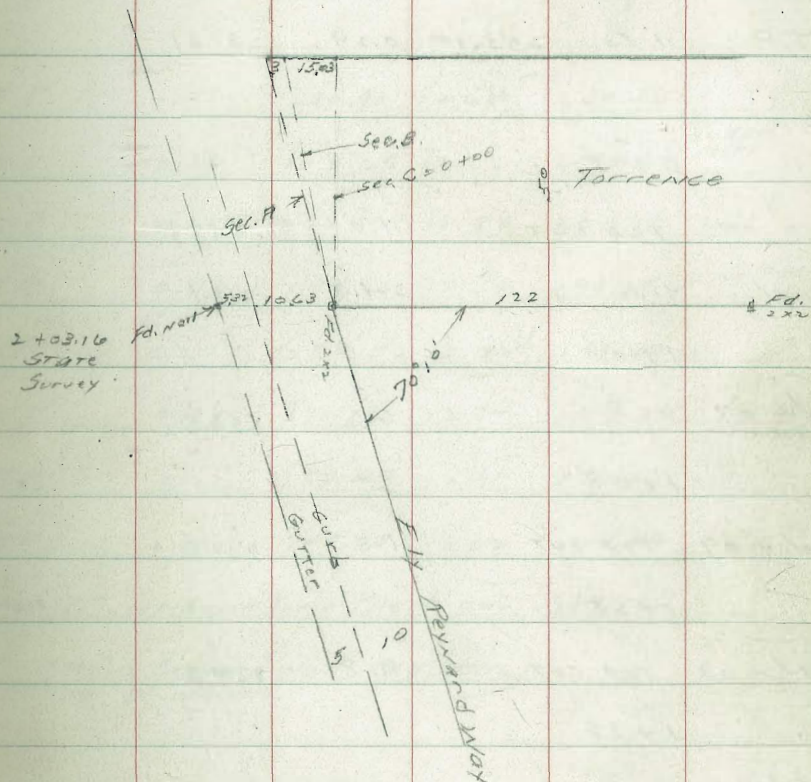
N		15.7	216.2
+07	TOP CUT	17.4	214.5
cb		21.8	210.1

0+06

N		14.7	217.2
+02	TOP CUT	14.9	217.0
cb		22.5	209.4

0+25

N		12.1	219.8
+02	TOP CUT	12.5	219.4



231.90

0+50

N Top cut 6.4 226.5

T.P. 11.53 243.14 0.29 231.61

0+75

-04 Top cut 11.0 232.1

N side " 24.0 219.1

1+00

N-07 6.6 232.5

1+08

N-09 Top cut 5.8 232.8

1+25

N-03 Top cut 9.8 234.3

1+38

N-05 Top cut 11.6 231.5

N side " 24.6 218.5

1+50

N-08 Top cut 14.5 228.6

1+60

N-01 Top cut 19.5 223.6

N side " 27.6 215.5

T.P. 0.43 230.93 12.64 230.50

T.P. 0.38 218.65 12.66 218.27

on com. 570 PS

T.P. 0.03 206.18 12.50 206.15

T.P. 0.97 194.62 12.53 193.65 ✓ on pav.

T.P. 0.26 182.06 12.82 181.80

T.P. 0.84 170.18 12.74 169.32

T.P. 0.22 157.49 12.91 157.27

T.P. 1.23 145.70 13.02 144.47

State B.M. spike in Power Pole 6.00 139.70

NW Cor. Reynard Way call State  
4 N. WALNUT

cont p 25

					C	2.9	196.4
	6.65	200.30	193.65	T.P. P 24	+5	2.4	197.9
	Sec A - 10.68 = cb on Reynard Way.				1/4	0.0	200.3
- 10	cb	6.35	193.95		1/4 + 06	0.0	200.3
"	gut.	6.88	193.72		Sec. C = 0 + 00		
S	cb	5.58	194.72		S	0.1	194.2
"	gut.	6.16	194.14		cb	5.0	194.9
N	cb	1.27	199.03		1/4	5.8	194.5
"	gut.	1.84	198.46		C	4.4	195.7
+ 10	cb	0.48	199.82		+ 04	3.2	197.1
"	gut.	1.08	199.22			0 + 06	
	Sec. A = Ely Reynard way				S	6.6	193.7
S	on 2 wheel	6.14	194.16		cb	6.4	193.9
cb		5.3	195.0		1/4	6.2	194.1
C		3.9	196.4		C	5.3	195.0
cb		1.4	198.9		1/4	4.4	195.9
N		0.7	199.6		+ 5	0.5	199.8
	Sec. B					0 + 25	
S		6.1	194.2		S	7.2	193.1
cb		5.3	195.0		cb	7.3	193.0

1/4		8.6	191.7
c		8.1	192.2
1/2		6.8	193.5
+6		5.7	194.6
	0+50		
5		6.5	193.8
+08		6.9	193.4
c6		8.0	192.3
1/4		7.9	192.4
c		7.7	192.6
1/4		7.3	193.0
+06		6.0	194.3
	0+75		
5		4.7	195.6
+7		5.0	195.3
c6		6.5	193.8
1/4		6.6	193.7
c		6.6	193.7
1/4		6.4	193.9
+06		5.3	195.0

			1+00		
		5		2.9	197.4
		+08		2.3	197.0
		06		5.7	194.6
		1/4		6.1	194.2
		c		5.6	194.7
		+04		5.4	194.9
		1/4		3.0	197.3
		c6		0.0	200.3
		+07		+4.0	204.3
		T.P.	11.15	210.17	1.28
			1+08		
		5		12.1	198.1
		c6		12.4	197.6
		+01		15.3	194.9
		1/4		15.5	194.7
		c		15.5	194.7
		+05		15.0	195.2
		1/4		10.7	199.5

210.17

✓cb		6.8	203.4
+06		4.8	205.4
	1725		
S		10.4	199.8
cb		10.6	199.6
+04		11.0	199.2
+06		14.6	195.6
1/4		14.6	195.6
c		15.0	195.2
+04		14.5	195.7
1/4		6.6	203.6
cb		5.3	204.8
+08		1.0	209.2
	1738		
S		8.8	201.4
cb		9.1	201.1
+06		8.8	201.4
1/4		11.5	198.7
c		12.6	197.6

210.17

27

1/4		9.9	200.3
cb		0.0	210.2
	1750		
S		7.2	203.0
cb		7.3	202.9
1/4		7.6	202.6
c		7.6	202.6
1/4		4.7	205.5
cb		2.5	207.7
	1760		
S		5.7	204.5
cb		5.8	204.4
1/4		4.6	205.6
c		2.3	207.9
1/4		1.9	208.3
cb		1.0	209.2
	1783		
S		2.3	207.9
cb		1.4	208.9

210.17

1/4		0.6	209.6	
C		0.4	209.8	
1/4		0.2	210.0	
cb		0.4	209.8	
N	TOP CUT	+ 6.5	216.2	
T.P.	8.58	218.37	0.43	209.74
	1796			
-10		17.4	201.1	
S		12.4	205.9	
cb		7.4	210.9	
1/4		6.4	211.9	
C		5.7	212.6	
1/4		3.3	215.6	
cb		2.8	215.5	
+08		2.1	216.2	
N	ON TOP 2 <sup>nd</sup> STEP	1.07	217.25	
ON T.P.	CEM. STEPS P 24	0.02	218.30	218.27

218.32

28

2+03

N	Wly edge Double gar	1.47	216.830	CEM. floor
	2+10			
	-15	16.5	211.8	
S	N	17.5	200.8	
	cb	11.3	207.0	
	1/4	4.4	213.9	
	C	3.3	215.0	
	1/4	2.9	219.4	
	cb	2.7	215.6	
	+08	2.5	215.8	
	N	gar. floor	1.47	216.85
	2+19 - Fly edge garage			" "
	-10	13.0	205.3	
	S	15.3	203.0	
	cb	10.6	207.7	
	1/4	4.8	213.5	
	C	3.5	214.8	
	1/4	3.0	215.3	
	cb	2.4	215.7	





10-16-37 Arthur St. X Sec. Hawley East.  
 60' wide curb + walks in  
 12' el's  
 9' 1/4's  
 Miller  
 Walker  
 Blass

399.01

30

- BM BP - 5.48 - 398.94 - 393.46

W. End Arthur  
 N.E. Arthur  
 Mt. View Blvd  
 N.W. Harten

1+00 E

- BM BP - 3.90 - 399.01 - 3.83 - 395.11 -

+ Arthur

0+00 = E. Line Hawley Black. Pav  
 No Cross Cuts

N. d 4.25 394.76

gutter pav. E. End 4.65 394.36

1/4 " " " 4.31 394.70

1/4 " " " 4.26 394.75

1/4 " " " 4.42 394.59

gutter " " " 4.93 394.08

S. d 4.43 394.58

0+50 E.

S. d 4.60 394.41

E 5.01 393.9

1/4 4.6 394.4

1/4 4.4 394.6

1/4 4.4 394.6

E 4.7 394.3

N. d 4.29 394.72

Note: See 157 p 65 notes taken 7-22-40

N. d

G

1/4

1/4

1/4

G

S. d

10.33' S. of S. d

S. d

G

1/4

1/4

G

N. d

10.33' N of N. d

10.33' N of N. d

N. d

G

12.25 = W. Line Alley

{ S. Edge walk  
 S. End Retn

{ N. side walk  
 N. End. el. ret

12.40 = E. Line Alley

4.50 394.51

4.9 394.1

4.5 394.5

4.7 394.3

4.7 394.3

5.0 394.0

4.74 394.27

4.45 394.56

5.06 393.95

4.9 394.1

4.7 394.3

4.7 394.3

4.6 394.4

4.55 394.43

4.19 394.82

4.31 394.70

4.63 394.38

4.7 394.3

399.01

1440 (Coin)

N 14	4.7	394.3
¢	4.6	394.4
14	4.8	394.2
G	5.0	394.0
S. dr	4.82	394.19
410.33 = S. End Red	4.65	394.36
2.400		
S. dr	5.05	393.96
G	5.3	393.7
14	4.9	394.1
¢	5.0	394.0
14	5.0	394.0
G	5.3	393.7
N. dr	4.89	394.12
2465 = W. Lin - Mansfield Black Pav. E + W. Gutters on N + S. Curb Lints		
N. dr	5.12	393.89
G pay W. End	5.52	393.49
14 " " "	5.23	393.78
¢ " " "	5.15	393.86
14 " " "	5.31	393.70

399.01

Alhur St

31

G pay W. End.	5.70	393.31
S. dr	5.37	393.64
0400 = E. Lin - Mansfield		
S. dr	5.62	393.39
G pay E End	6.03	392.98
14 " " "	5.72	393.29
¢ " " "	5.69	393.32
14 " " "	5.90	393.11
G " " "	6.33	392.68
N dr	5.96	393.05
0750 E		
N. dr	6.27	392.74
G	6.9	392.1
14	6.3	392.7
¢	6.2	392.8
14	6.3	392.7
G	6.5	392.5
S. dr	5.92	393.09
— T.P. — 3.67 — 396.22 — 6.46 — 392.55 —		

396.22

1+00 E.

s. cl		3.41	392.81
G		4.0	392.2
<sup>1</sup> / <sub>4</sub>		3.6	392.6
ϕ		3.6	392.6
<sup>1</sup> / <sub>4</sub>		3.7	392.5
G		4.3	391.9
N. cl		3.70	392.52
	1+25 = W. Line Alley N edge walk		
10.33' N of N. cl = W. End. Ret.		3.46	392.76
N. cl		3.73	392.49
G		4.3	391.9
<sup>1</sup> / <sub>4</sub>		3.8	392.4
ϕ	M.H. Prim	3.60	392.62
<sup>1</sup> / <sub>4</sub>		3.6	392.6
G		4.1	392.1
S. cl		3.72	392.50
+ 10.33 = S. End. cl. Ret.		3.26	392.96

396.22

Arthur St

32

s. cl - 10.33 = S. End. cl. Ret.	1+40 = E. Line Alley S. edge walk.	3.26	392.96
s. cl		3.54	392.68
G		4.1	392.1
<sup>1</sup> / <sub>4</sub>		3.7	392.5
ϕ		3.7	392.5
<sup>1</sup> / <sub>4</sub>		3.9	392.3
G		4.5	391.7
N. cl		3.85	392.37
+ 10.33 = N. End. cl. Ret.		3.53	392.69
	2+00		
N. cl		4.22	392.00
G		4.7	391.5
<sup>1</sup> / <sub>4</sub>		4.2	392.0
ϕ		3.8	392.4
<sup>1</sup> / <sub>4</sub>		4.0	392.2
G		4.5	391.7
S. cl		4.04	392.18

2 + 65<sup>l</sup> = W. Line 35<sup>th</sup> St. Black Pav

S. el		4.46	391.76
gutter Pav	W-End	4.90	391.32
"	" " "	4.85	391.37
±	" " "	4.71	391.51
"	" " "	4.83	391.39
G	" " "	5.06	391.16
N. el		4.64	391.58

12' E = W. el. Line

N. Line	gutter pav	5.25	390.97
el	" "	5.12	391.10
"	" "	5.06	391.16
±	" "	4.99	391.23
"	" "	4.94	391.28
el	" "	4.97	391.25
S.	" "	4.99	391.23
+ 40	" "	4.83	391.39

- BM. B.P. -

4.49 - 391.73

S.W. Mt. View  
Bldg +  
Arthur E. Ed

- T.P. - 6.13 - 397.58 - 4.77 - 391.45 -

- ch. BM. B.P. -

3.60

- 393.98 -

S.E. Sidney

+ Mt. View  
393.98 V

indexed  
e.s.R.

Xsec of 6th St. EXT.

STA 48 + 92.02 to San Diego

River Bridge STA.

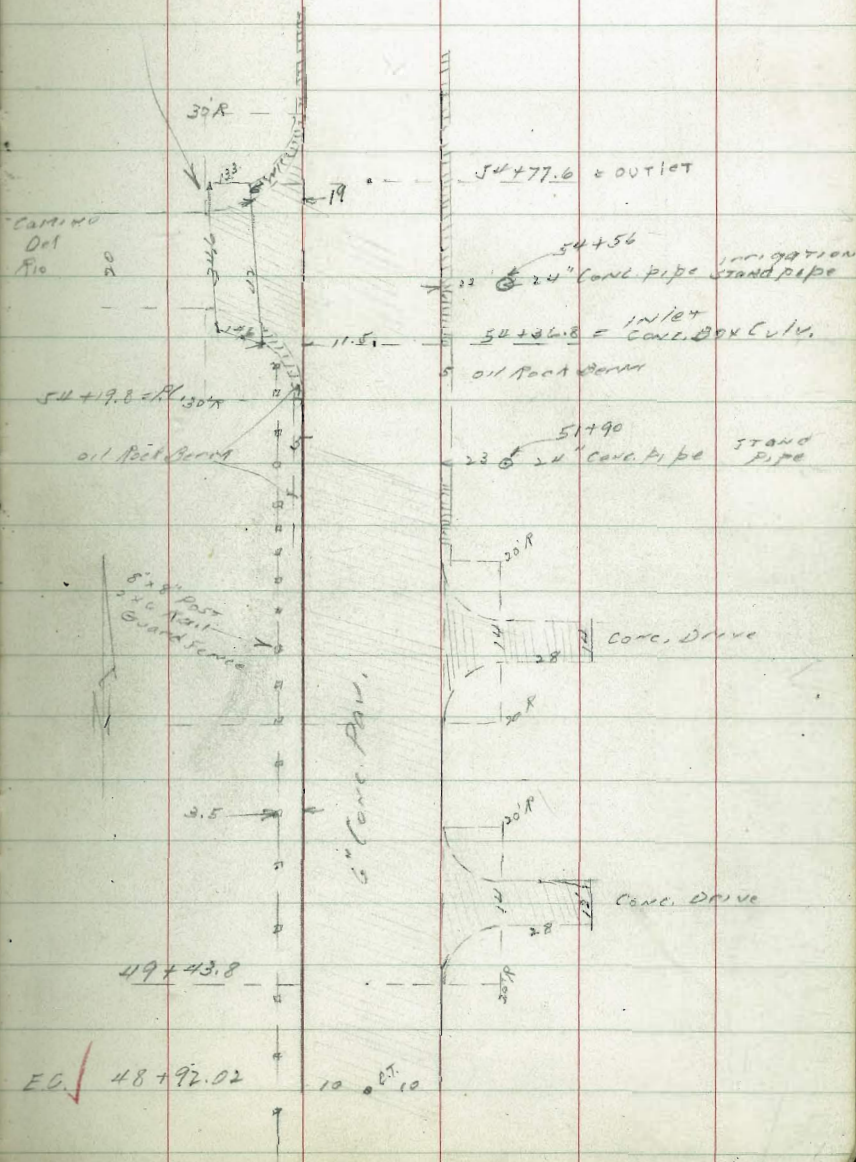
Moore  
Sisson  
Northern  
10-26-37



TOP SLAB  
15' PAVING

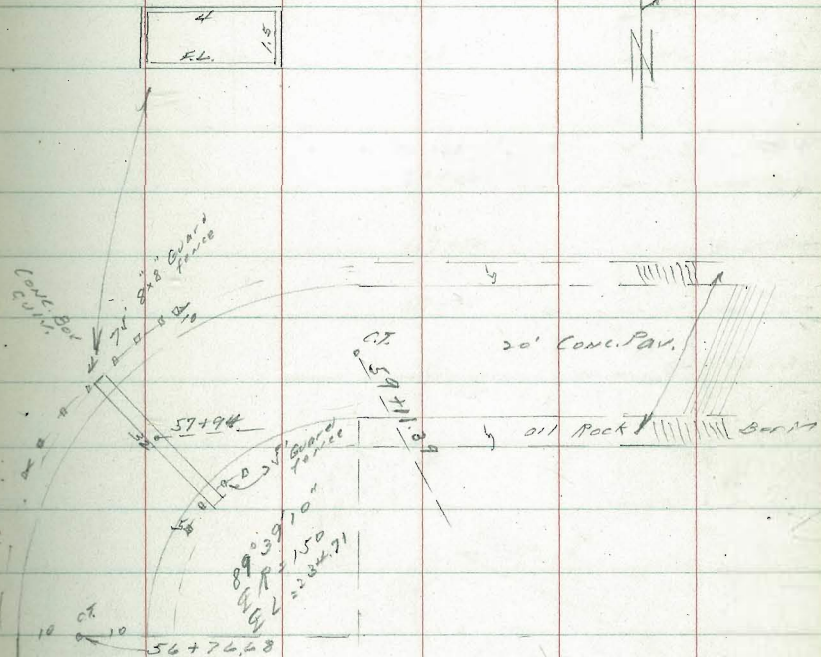
34

See G.B. 154-4



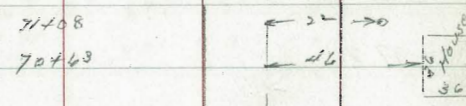
EC ✓ 48 + 92.02

10' 0" 10'

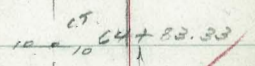
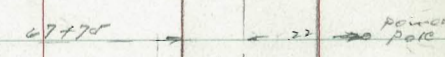




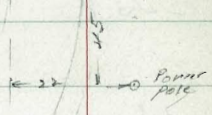
71+16 end Conc. Pav. & Beg. of oil rock spec.



69+50



89°58'30"  
E.P. = 121.34  
S.L. = 190.89



20' Conc. Pav.

NOT  
62+92.44 B.C.

oil rock berm

Conc. Pav. not shown on inside

50 + 50

27.2	29.4	29.8	27.5	27.7	29.3	29.27	29.47	29.46	29.3	29.3	26.0
8.1	5.4	5.5	7.8	7.6	6.0	5.98	5.78	5.79	6.0	6.0	7.4
40	35	39	25	19	13	10	10	10	20	25	30

+97.8

28.8	31.0	31.3	28.3	28.3	30.1	30.30	30.46	30.44	30.4	29.6
6.5	4.3	4.0	7.0	7.0	5.7	4.95	4.81	4.9	5.7	
40	35	30	25	19	15	10	10	10	30	30

+70.8 £ Drive on Rt.

29.7	31.9	31.9	29.0	29.4	30.9	30.94	31.09	31.04	30.91	31.00
5.6	3.4	4.4	6.3	5.9	4.4	4.31	4.16	4.34	4.25	
40	35	30	24	16	13	10	10	30	38	

+43.8

30.4	32.7	32.8	29.3	29.6	31.8	31.70	31.74	31.64	31.8	31.4
5.1	2.6	2.5	4.0	5.7	3.5	4.55		3.63	3.5	3.9
40	35	30	25	19	15	10	3.5	10	20	30

49

31.3	34.3	29.4	30.7	30.0	34.89	34.85	34.68	33.0	32.6
4.0	1.0	5.9	5.1	2.3	2.36		2.57	2.3	2.7
20	30	33	29	15	10	240	10	20	30

48 + 92.02 = EC.

31.25	34.25	29.5	30.3	30.1	33.07	33.06	32.85	32.9	32.4
4.0	1.0	5.8	5.0	2.2	2.18		2.40	2.4	2.9
20	30	33	29	15	10	219	10	20	30

T.P. C.T. 2.19 35.251 0.61 33.06

35.251

RT.  
 Cont. Man. 12.63 33.67 21.04  
 6th St. +  
 Camino  
 del Rio.



+50

23.3	27.5	27.4	25.4	24.0	24.1	26.1	26.03	26.11	26.06	26.1	26.4	23.4
12.0	7.8	7.9	10.1	11.3	11.4	8.2	9.22	9.14	9.19	9.2	9.1	12.1
20	33	30	27	25	21	18	10	10	20	20	30	25

57

23.7	27.7	27.3	25.4	25.3	26.7	26.7	26.75	26.70	26.7	26.5	23.6
11.4	7.2	7.5	9.9	10.0	8.4	8.40	8.50	8.55	8.6	8.8	11.5
20	34	30	25	21	18	10	10	10	20	20	25

+50

24.3	28.3	28.4	26.7	26.3	27.6	27.54	27.65	27.61	27.4	27.5	25.4
11.0	7.0	6.9	9.1	9.0	7.7	7.75	7.60	7.60	7.9	7.8	9.9
20	35	30	25	19	13	10	10	10	20	20	25

51432

24.6	28.3	28.8	26.4	26.2	28.0	27.85	28.00	27.95	27.9	28.0
10.7	7.0	6.5	8.9	9.1	7.3	7.40	7.25	7.27	7.6	7.5
20	35	21	24	21	18	10	10	10	20	20

51405  $\Phi$  CONC DRIVE ON RT

26.6	29.0	28.9	26.7	26.6	28.3	28.36	28.48	28.48	28.71	28.2
8.7	6.3	6.4	8.6	8.7	7.0	6.89	6.77	6.77	6.54	7.13
20	35	32	25	22	13	10	10	10	30	28

50+78

26.7	29.3	29.3	27.3	27.2	28.8	28.94	29.00	29.00	28.91	28.8	27.6
8.6	6.0	6.0	8.0	8.1	6.5	6.26	6.25	6.25	6.34	4.5	7.7
20	35	30	26	21	18	10	10	10	17	25	30

35.251

35.251

W. S. Gas Co. 174

+36.8 = 14/17 C/V

20.4	20.6	20.34	20.69	20.9	20.97	20.90	21.1	21.9	22.3
60	2.4	7.83	4.48	4.30	4.27	4.27	2.1	2.2	5.9
45	34	50	21.5	15	10	10	17	25	35

FL. 55 TOP  
TOP BOX

+19.8 PC

22.3	26.0	25.9	24.6	24.6	24.2	23.8	24.13	24.1	24.5	24.5	22.4
5.9	2.2	2.3	5.6	5.6	4.0	4.4	4.0	4.10	3.7	3.4	5.8
45	35	22	24	16	13	10	10	10	20	28	35

54

24.5	26.0	26.0	24.5	24.9	24.5	24.25	24.25	24.29	24.6	25.1	21.6
5.7	2.2	2.2	5.7	5.3	5.7	5.9	5.88	5.88	3.6	3.1	6.6
40	32	30	25	19	13	10	10	10	20	30	45

24.5	24.1	24.2	24.7	23	24.6	24.4	24.5	24.5	24.5	25.1	21.8
------	------	------	------	----	------	------	------	------	------	------	------

+50

24.5	26.5	26.6	23.1	23.1	25.0	24.94	24.94	24.90	24.5	25.2	22.3
5.7	1.7	1.6	5.1	5.1	3.2	3.23	3.23	3.27	3.7	3.0	5.9
40	24	30	24	20	15	10	10	10	20	30	35

T.P 201 28171 949 25.56

28171

53

27.3	26.8	27.0	24.9	23.2	23.2	24.5	24.44	24.52	24.49	24.6	25.3	22.7
13.0	8.5	8.3	10.4	12.1	12.1	9.8	9.81	9.78	9.78	9.7	10.0	13.6
40	33	30	27	25	21	13	10	10	10	20	30	35

35.251

35.251

56+74.08 B.C. C.T.

40.4	40.8	43.9	43.84	43.54	43.10	43.8	44.4	44.1
7.8	7.4	4.3	4.33	4.63	5.07	4.4	3.8	4.1
35	25	17	10		10	20	30	35

+50

40.7	41.0	43.8	43.65	43.47	43.07	43.6	44.0	41.9
7.5	7.2	4.4	4.52	4.75	5.10	4.0	4.2	4.3
35	25	18	10		10	20	30	35

50

40.8	41.7	43.3	43.34	43.26	43.01	42.9	43.3	41.9
7.4	7.0	4.9	4.83	4.91	5.10	5.3	4.2	4.3
35	25	18	10		10	15	30	35

+50

44.0	44.0	43.7	43.35	43.25	43.14	43.2	43.5	41.7
6.2	6.2	5.0	4.92	4.92	5.07	5.0	4.7	6.5
35	25	18	10	492	10	18	30	35

55

41.9	44.0	43.3	43.5	43.56	43.5	43.6	44.4	42.7
6.3	6.2	4.9	4.70	4.61	4.70	4.6	3.8	4.0
35	25	20	10		10	19	28	35

54+77.6 = outer Curb

43.5	40.04	43.44	43.44	43.70	43.54	44.1	44.6	42.3
4.7	8.5	4.53	4.73	4.47	4.53	4.1	3.6	5.9
40	35	29	19.2		12	19	28	35

FL  
REC'D  
TOP BOX

28.171

28.171

T.P.B.P. 410 27.184 509 23.08

ST E PT  
Set by Miller on Camino del Rio Survey  
H.B.P. Top Hd. wall 16 FT of Sta. 57494

59 + 11.39 = E.C.

21.5	21.6	21.6	23.8	23.8	23.57	23.15	22.7	21.8	21.8
6.7	6.0	6.6	4.4	4.4	4.25	5.02	5.5	6.2	6.2
35	35	25	7.8	10	425	10	20	35	50

58 + 24.44

21.5	23.9	24.00	23.72	23.17	22.8	21.7	21.5
6.7	4.3	4.7	4.45	5.0	5.4	6.5	6.7
35	20	10	445	70	20	25	35

58 + 17.50

20.6	20.6	24.7	23.84	23.54	23.09	22.1	21.7
7.6	7.6	4.0	4.23	5.08	5.1	6.5	6.5
35	34	7.8	10	465	10	20	35

57 + 94 E Box Cul.

20.54	23.82	23.08'	20.75
7.63	4.35	5.09 = B.M. B.P.	7.42
10	10	10	16 = Ft in/105
FL.	Top Head wall	Top Head wall	

57 + 70.50

21.0	21.0	23.8	23.92	23.57	23.22	23.4	21.7
7.2	7.2	4.4	4.35	4.60	4.95	4.8	6.5
35	30	20	10	460	10	20	25

57 + 23.62

20.8	21.9	24.7	23.94	23.60	23.2	22.4	23.8	21.7
7.4	6.5	4.0	4.35	4.57	5.0	4.8	4.4	6.5
35	25	7.8	70	457	10	20	28	35

28.7

28.17

62

21.9	21.9	23.1	22.3	23.1	22.79	22.83	22.83	23.2	21.4	23.1	21.8	21.9
5.3	5.3	4.1	4.9	4.1	4.29	4.35	4.35	4.0	5.8	4.1	5.4	5.3
50	35	35	21	18	10	4.35	10	18	21	25	35	50

+50

21.9	21.8	22.7	23.2	22.77	22.94	22.94	23.1	21.8	23.4	22.0	21.9
5.5	5.4	4.5	4.0	4.41	4.26	4.26	4.1	5.4	3.8	5.2	5.3
50	35	35	18	10	4.26	10	18	21	25	35	50

61

21.7	21.7	22.6	23.5	22.90	23.04	22.96	23.0	21.4	23.1	21.8	21.7
5.5	5.5	4.6	3.7	4.28	4.22	4.2	5.8	4.1	5.4	5.5	
50	35	25	18	10	4.14	10	18	21	25	35	50

+50

21.5	21.5	22.4	23.9	22.94	23.08	23.07	23.2	21.2	23.3	21.6	21.5
5.7	5.7	4.8	3.2	4.24	4.11	4.0	6.0	3.9	5.6	5.7	
50	35	23	18	10	4.10	10	18	21	25	35	50

60

21.3	21.2	22.4	23.3	23.13	23.23	23.16	23.2	21.2	22.8	21.4	21.6
5.9	6.0	4.8	3.9	4.05	4.02	4.3	6.0	4.4	5.8	5.6	
50	35	25	18	10	3.95	10	18	22	25	35	50

59+50

21.3	21.4	22.2	23.4	23.41	23.40	23.2	23.0	21.4	22.2	21.3	21.5
5.9	5.8	5.0	3.3	3.77	4.0	4.2	5.8	4.6	5.9	5.7	
50	40	50	18	10	3.78	10	18	20	25	35	50

27.184

27.184

64 + 45.16

22.7	22.0	22.7	22.45	22.69	22.86	22.9	22.1	22.3	22.3
5.0	5.2	4.5	4.73	4.82	4.3	4.1	4.9	4.9	
50	35	25	14.2	10	20	30	35	50	

64 + 08.98

21.7	21.9	22.7	22.36	22.66	22.84	22.8	22.0	
5.5	5.3	4.5	4.82	4.32	4.4	4.4	4.4	
50	35	25	14.8	10	25	50		

63 + 68.80

21.6	21.9	22.2	22.33	22.67	22.89	22.7	22.8	
5.6	5.3	5.0	4.85	4.29	4.0	4.4	4.4	
50	35	25	14.9	10	25	50		

63 + 30.62

21.6	22.4	22.7	22.26	22.60	22.81	22.1	22.4	21.9
5.6	4.8	4.5	4.92	4.58	4.37	4.1	5.0	5.3
50	35	21	14.6	10	30	40	50	

62 + 92.04 = BC LT

21.4	21.8	22.4	22.0	22.5	22.32	22.55	22.74	23.0	21.7	22.0	21.8	21.9
5.8	5.4	4.8	5.2	4.7	4.86	4.62	4.44	4.2	5.5	4.2	5.4	5.3
50	35	25	21	18	11.2	10	18	21	25	35	50	

62 + 50

21.6	22.7	22.4	22.4	22.9	22.54	22.73	22.75	23.0	21.8	22.7	22.0	22.3
5.6	5.0	4.8	4.8	4.0	4.64	4.45	4.43	4.2	5.8	4.0	5.2	4.9
50	35	25	21	18	10	4.45	10	18	21	25	35	50

27.181

27.181

27 2 27

+50

22.0	21.8	22.7	22.73	22.85	22.79	22.7	23.4	23.4	23.1
$\frac{6.0}{40}$	$\frac{6.2}{30}$	$\frac{5.3}{15}$	$\frac{5.31}{10}$	4.9	$\frac{5.25}{10}$	$\frac{5.8}{15}$	$\frac{4.6}{20}$	$\frac{4.6}{25}$	$\frac{4.9}{30}$

67.9 5.9 2804 4.33 22.85

2804 ✓

66

21.9	21.9	22.9	22.7	22.78	22.86	22.79	22.7	23.3	22.4	22.7
$\frac{5.4}{40}$	$\frac{5.3}{30}$	$\frac{4.3}{25}$	$\frac{4.5}{15}$	$\frac{4.40}{10}$	4.32	$\frac{4.39}{10}$	$\frac{4.5}{15}$	$\frac{3.9}{25}$	$\frac{4.8}{30}$	$\frac{4.5}{40}$

+50

21.9	21.7	22.8	22.7	22.70	22.93	22.76	22.8	23.4	22.4	22.7
$\frac{5.3}{40}$	$\frac{5.5}{30}$	$\frac{4.4}{25}$	$\frac{4.5}{15}$	$\frac{4.50}{10}$	4.35	$\frac{4.42}{10}$	$\frac{4.4}{15}$	$\frac{3.8}{25}$	$\frac{4.8}{30}$	$\frac{4.5}{40}$

65

22.2	22.2	23.1	22.9	22.87	22.78	22.56	22.5	22.6	21.8	21.9
$\frac{5.0}{40}$	$\frac{5.0}{30}$	$\frac{4.1}{25}$	$\frac{4.3}{15}$	$\frac{4.31}{10}$	4.40	$\frac{4.62}{10}$	$\frac{4.7}{15}$	$\frac{4.6}{25}$	$\frac{5.4}{30}$	$\frac{5.3}{40}$

64+83.33 EC.

22.4	21.8	23.5	22.8	22.57	22.77	22.93	22.9	23.2	23.1	22.3	22.3
$\frac{5.0}{40}$	$\frac{5.4}{35}$	$\frac{3.7}{22}$	$\frac{4.7}{15}$	$\frac{4.66}{17.5}$	4.11	$\frac{4.25}{10}$	$\frac{4.3}{15}$	$\frac{4.0}{18}$	$\frac{4.1}{25}$	$\frac{4.9}{30}$	$\frac{4.9}{40}$

27.181

27.181

+50 E 18' DIRT DRIVE TO RT

21.7	21.9	22.8	22.7	22.84	22.9 <sup>v</sup>	22.86	22.7	23.1	23.2
$\frac{4.3}{40}$	$\frac{4.1}{30}$	$\frac{5.2}{25}$	$\frac{5.5}{15}$	$\frac{5.20}{10}$	$\frac{5.2}{10}$	$\frac{5.3}{15}$	$\frac{4.9}{40}$	$\frac{4.8}{70}$	

69

22.1	21.9	23.0	22.6	22.8 <sup>o</sup>	22.9 <sup>v</sup>	22.84	22.8	23.2	23.0	22.4	22.4
$\frac{5.9}{40}$	$\frac{6.1}{30}$	$\frac{5.0}{25}$	$\frac{5.4}{15}$	$\frac{5.24}{10}$	$\frac{5.2}{10}$	$\frac{5.2}{15}$	$\frac{4.8}{20}$	$\frac{4.0}{25}$	$\frac{5.4}{30}$	$\frac{5.6}{40}$	

+50

22.4	22.4	22.9	22.6	22.82	22.90	22.84	22.8	23.2	23.1	22.3	22.7
$\frac{5.8}{40}$	$\frac{5.8}{30}$	$\frac{5.1}{25}$	$\frac{5.4}{15}$	$\frac{5.21}{10}$	$\frac{5.2}{10}$	$\frac{5.2}{15}$	$\frac{4.8}{20}$	$\frac{4.9}{25}$	$\frac{5.7}{30}$	$\frac{5.3}{40}$	

68

22.0	22.3	22.6	22.7	22.82	22.91	22.84	22.8	23.4	23.2	22.5	22.8
$\frac{6.0}{40}$	$\frac{5.7}{30}$	$\frac{5.4}{25}$	$\frac{5.3}{15}$	$\frac{5.22}{10}$	$\frac{5.19}{10}$	$\frac{5.2}{15}$	$\frac{4.6}{20}$	$\frac{4.8}{25}$	$\frac{5.5}{30}$	$\frac{5.2}{40}$	

+50

22.3	22.2	23.1	22.8	22.83	22.89	22.84	23.0	23.7	23.3	22.5	22.8
$\frac{5.7}{40}$	$\frac{5.8}{30}$	$\frac{4.9}{25}$	$\frac{5.2}{15}$	$\frac{5.21}{10}$	$\frac{5.2}{10}$	$\frac{5.0}{15}$	$\frac{4.3}{20}$	$\frac{4.7}{25}$	$\frac{5.5}{30}$	$\frac{5.2}{40}$	

67

22.7	22.9	23.9	22.7	22.75	22.86	22.80	22.7	24.0	23.7	22.5	23.0
$\frac{5.3}{40}$	$\frac{5.1}{30}$	$\frac{4.1}{25}$	$\frac{5.3}{15}$	$\frac{5.29}{10}$	$\frac{5.8}{10}$	$\frac{5.2}{15}$	$\frac{4.0}{20}$	$\frac{4.3}{25}$	$\frac{5.5}{30}$	$\frac{5.0}{40}$	

28,041

28,041



21.4	21.8	19.6	22.4	23.45	23.60	23.45	21.2	21.4
10.0	9.6	11.8	8.0	7.94	7.94	8.2	10.2	10.0
40	33	26	19	10	7.9	10	17	40

20.5	21.4	21.9	23.4	23.04	23.21	23.15	23.0	22.2
10.9	10.0	8.5	8.2	8.05	8.18	8.24	8.4	9.2
40	30	25	15	10	8.18	7.8	15	25

71+10 = END CONC. Pav, covered with 1" Black

GR. 1.54-5.8 covered with ASP

T.P. Pav. 8.41 31.39' 500 22.98 23.09

31.391

71

20.9	21.5	22.8	22.9	22.98	23.05	22.99	22.8	22.0	22.0
7.1	6.5	5.2	5.1	5.06	5.05	5.05	5.2	6.0	6.0
40	30	25	15	10	4.99	10	15	25	40

+50

21.3	21.5	22.4	22.7	22.89	22.97	22.91	22.7	22.2	22.2
6.7	6.7	5.6	5.3	5.15	5.07	5.13	5.3	5.8	5.8
40	40	25	15	10	7.9	10	15	25	40

70

21.7	21.8	22.4	22.6	22.8	22.94	22.89	22.5	23.0
6.3	6.2	5.6	5.4	5.20	5.15	5.3	4.5	5.0
40	30	25	15	10	5.0	10	15	25

28041

28041

+75

19.0	23.4	25.1	25.8	25.36	25.50	26.42	26.1	27.4	27.2
$\frac{12.4}{50}$	$\frac{8.0}{40}$	$\frac{6.3}{36}$	$\frac{5.6}{20}$	$\frac{5.23}{10}$	$\frac{4.86}{10}$	$\frac{4.97}{10}$	$\frac{5.3}{18}$	$\frac{9.0}{27}$	$\frac{9.2}{40}$

+50

21.3	21.2	21.4	21.05	21.07	21.09	21.0	21.4	21.3	18.4
$\frac{10.1}{40}$	$\frac{10.2}{33}$	$\frac{6.0}{22}$	$\frac{5.34}{10}$	$\frac{5.72}{10}$	$\frac{5.32}{10}$	$\frac{5.4}{16}$	$\frac{8.0}{19}$	$\frac{13.1}{33}$	$\frac{13.0}{40}$

+25

21.7	21.7	21.7	21.6	21.8	21.91	21.77	21.8	20.3	24.4
$\frac{9.7}{20}$	$\frac{9.7}{30}$	$\frac{9.2}{24}$	$\frac{5.8}{16}$	$\frac{5.60}{10}$	$\frac{5.62}{10}$	$\frac{5.6}{18}$	$\frac{11.1}{28}$	$\frac{7.0}{40}$	

73

22.8	22.9	22.7	22.47	22.56	22.41	22.4	22.7	23.3	23.3
$\frac{8.6}{20}$	$\frac{8.5}{34}$	$\frac{5.7}{16}$	$\frac{5.92}{10}$	$\frac{5.83}{10}$	$\frac{5.98}{10}$	$\frac{6.0}{17}$	$\frac{9.2}{32}$	$\frac{8.1}{37}$	$\frac{8.1}{40}$

+50

24.4	24.4	24.8	24.77	24.92	24.77	25.0	24.1	23.9	21.9
$\frac{7.0}{40}$	$\frac{7.2}{25}$	$\frac{6.6}{15}$	$\frac{6.62}{10}$	$\frac{6.47}{10}$	$\frac{6.62}{10}$	$\frac{6.4}{15}$	$\frac{7.3}{21}$	$\frac{7.5}{35}$	$\frac{9.5}{40}$

72

23.6	23.7	24.1	24.18	24.17	24.08	24.2	21.0	20.6
$\frac{7.8}{40}$	$\frac{7.7}{25}$	$\frac{7.3}{15}$	$\frac{7.21}{10}$	$\frac{7.22}{10}$	$\frac{7.31}{10}$	$\frac{7.2}{13}$	$\frac{10.4}{25}$	$\frac{10.8}{40}$

31.39

31.39

74 + 44 S. end of bridge

20.7	20.7	18.0	17.7	17.8	17.05	17.06	16.98	17.0	16.6	17.1	18.1
10.7	10.7	13.4	13.7	13.6	4.31	4.31	4.41	12.4	12.8	14.3	13.8
50	35	30	25	15	11.5	4.31	8.5	10	20	40	50

deck

+ 361

21.4	21.9	22.7	24.7	24.4	26.1	27.04	27.15	26.99	26.4	26.4	26.9	18.7	18.8	17.7
10.0	9.5	8.7	6.7	5.0	5.3	4.35	4.22	4.40	5.0	5.2	9.1	12.7	12.0	13.7
50	40	23	20	20	15	10	9	17	17	21	33	40	50	

ground

74

24.7	24.3	24.8	24.7	24.6	24.76	24.67	23.2	23.9	23.0
7.2	7.1	6.6	5.2	4.77	4.63	4.77	5.0	8.2	8.5
50	40	30	20	10	463	10	30	30	50

31.39

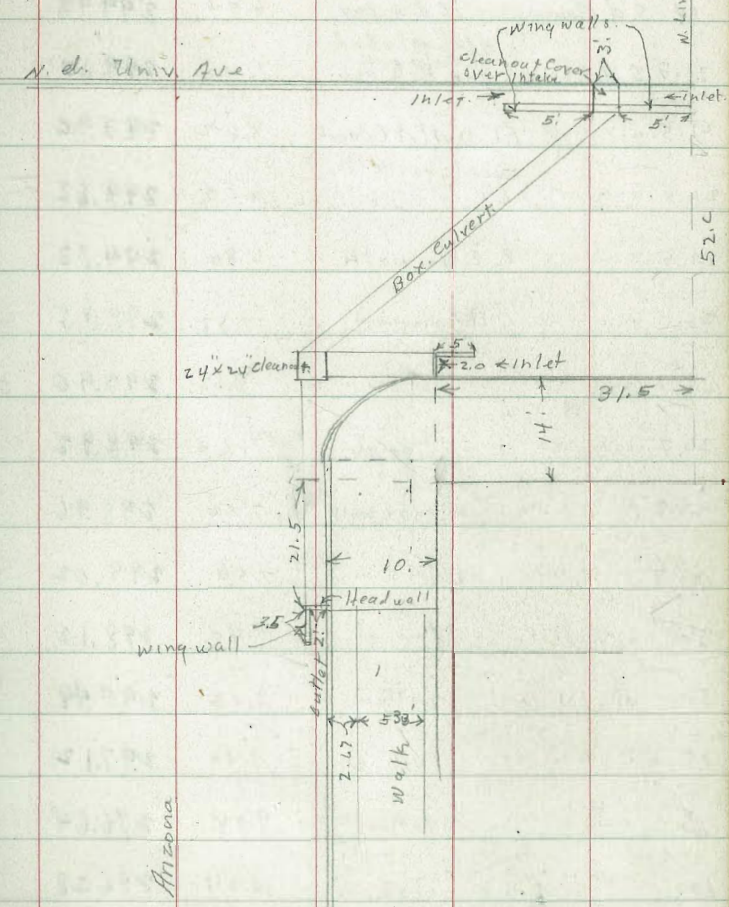
31.39

1-4-38  
Miller  
Walker  
Bliss

Levels for Culvert Arizona + Univ Ave

Indexed  
C.S.K.

B.M.	0.12	306.52	306.40	S.E. Univ. + Arnold
W. d. Arizona N. Line Univ. } Top. d.		5.54	300.98	
" " } pav		6.07	300.45	
W. Line Arizona N. d. Univ. } Top. d.		5.50	301.02	
" " } pav, End. Wingwall		6.38	300.14	
6.5 W. of W. Line Ariz	Top. d.	5.50	301.02	
" " " " }	Top. Pav = = Top. Cover	5.95	300.57	
" " " " "	F.L. Culvert	7.18	299.34	
13' W. of W. Line Ariz	Top. d.	5.48	301.04	
13' " " " " "	Pav	6.28	300.24	
38' " " " " "	Top. d.	5.53	301.19	
38' " " " " "	Pav	6.01	300.51	
18.2 S. of N. d. = N. Rail N. Trac. on. of Ex. Culvert.		5.65	300.87	at 90° to Univ
18.2 N. of S. d. = S. Rail S. Trac. S. d. Univ		5.56	300.96	
Top. deancut. at. P.I	E " Ariz.	6.68	299.84	
F.L.	" " " "	7.86	298.66	
40' E. of deancut.	Top. S. d.	6.47	300.05	
" " " "	pav	6.82	299.70	
15' " " " "	" "	7.06	299.46	
15' " " " "	Top. S. d. = = E. End. Wingwall.	6.60	299.92	

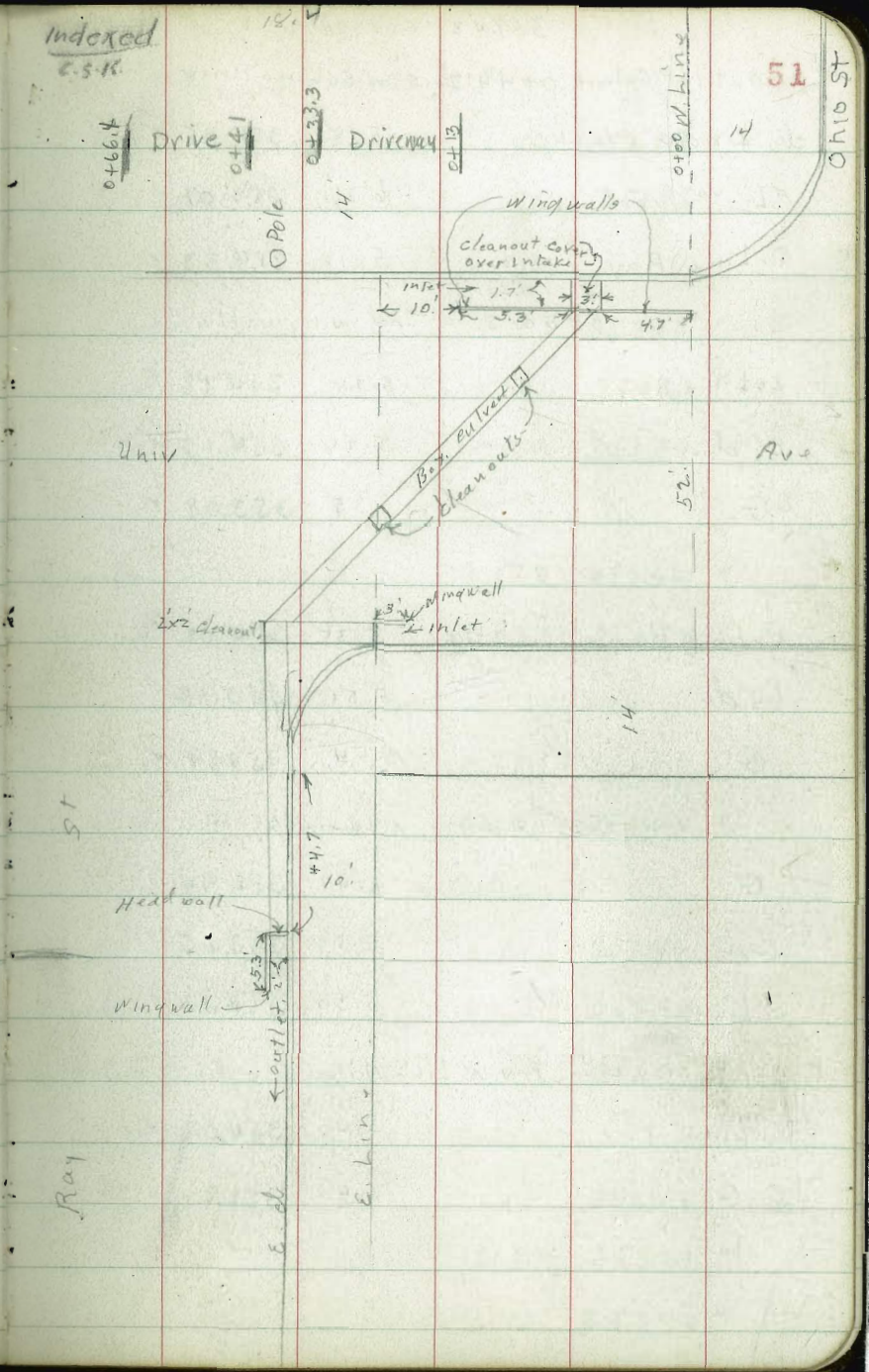


10'	E. of clean out = Head wall = Top dr.	6.57	299.95	= E. Line Aris
11	" " " = F.L. Culvert.	7.68	298.84	" " "
14'	S. of clean out = } S. Line Univ C. d + pav.	6.54	299.98	
21.5	S. of S. Line = } Head. wall + End. of Culvert Top. dr & Pav	7.02	299.50	
21.5	" " " " F.L. Outlet Culvert	8.62	297.90	
21.5	" " " " w. edge walk	6.90	299.62	
21.5	" " " " E. Edge walk	4.80	299.72	
25'	" " " " = End. wing wall	7.57	298.95	Top. dr
25'	" " " "	8.62	297.90	☉ Pav
26.7	" " " " Top. dr	7.60	298.92	
26.7	" " " " w. edge walk	7.56	298.96	
26.7	" " " " E. " "	7.50	299.02	
50'	" " " " Top. dr	8.40	298.12	
50.	" " " " gutter	9.03	297.49	
75'	" " " " Top. dr	9.40	297.12	
75'	" " " " gutter	9.88	296.64	
100	" " " " Top. dr	10.24	296.28	
100.	" " " " Gutter	10.76	295.76	
125	" " " " gutt	11.65	294.87	

1-4-38 Levels for Drainage  
Ray + Univ Ave

Indexed  
2.5.11

BM	Station	Level	Elevation	Notes
W. ch. Ohio	4.12	359.43	355.31	N.W. Ohio + Univ
N. Line Univ	Top. ch	4.12	355.31	✓
" " "	gutter	4.66	354.77	✓
W. Line Ohio	Top. ch	4.30	355.13	✓
N. ch. Univ	gutter	5.08	354.35	✓
6.2 W. of W. Line	Top. cleanout	4.28	355.15	✓
6.2 " " " "	Top. ch	4.28	355.15	✓
6.2 " " " "	F.L. Culvert	5.48	353.95	✓
11.4 W. " " "	Top. ch	4.15	355.28	✓
11.4 " " " "	gutter	4.95	354.48	✓
35 " " " "	Top. ch	4.31	355.07	✓
35 " " " "	gutter	4.99	354.44	✓
18.4 S. of N. ch. = N. Rail N. Track	± 8x Culvert	4.27	355.16	at 90° to Univ
18.4 N. of S. ch. = S. Rail S. Track	± 8x Culvert	4.30	355.13	✓
at P.I. { S. ch. Ray } { S. ch. Univ }	Top. cleanout	4.97	354.46	✓
" " " "	F.L. "	6.18	353.25	✓
0+00 = S. Line Univ				
E. Line Ray		4.87	354.86	✓
E. ch. " "	pav. flush.	4.85	354.58	✓



Outlet culvert	0+44.7	s. of S. Line Univ	
ch. + pav. flush	5.18	354.25	✓
F.L. Culvert	6.36	353.07	✓
E. Line Ray	5.10	354.33	✓
0+50 s. = End wing walls			
E. Line Ray	5.25	354.18	✓
E. ch	5.28	354.15	✓
E.G.	6.35	353.08	✓
0+75			
E. Line Ray	5.35	354.08	✓
E. ch	5.51	353.92	✓
G	6.54	352.89	✓
1+02.3 = N. ch ret. N. Line Alley			
G.	6.49	352.94	✓
E. ch	5.58	353.85	✓
E. Line	5.30	354.13	✓
1+02.4 = Pav. N. Line Alley			
E. Line Pav.	5.40	354.03	✓
E.G.	6.50	352.93	✓

1+17.1 = Pav. S side Alley			
E. G.	Pav.	6.54	352.89 ✓
E. Line	4	5.48	353.95 ✓
1+17.2 = ch. Ret. S. Line Alley			
E. Line		5.48	353.95 ✓
E. ch		5.81	353.62 ✓
G		6.54	352.89 ✓
1+50			
G		6.81	352.62 ✓
E. ch		5.93	353.50 ✓
1+75			
G		6.97	352.46 ✓
E. ch		6.13	353.30 ✓
2+06.4 = N. edge ent. drive			
G.		6.97	352.46 ✓
ch		6.13	353.30 ✓
3'E. of ch. drive meets walk		6.08	353.35 ✓
2+15.6 s. End. ent. Drive			
G		7.10	352.33 ✓
ch		6.32	353.11 ✓
3'E. of ch. drive meets walls		6.13	353.30 ✓

359.43

2+50

G 7.23 352.20 ✓

d 6.51 352.92 ✓

2+75

G 7.47 351.96 ✓

d 6.76 352.67 ✓

3+00

G 7.53 351.90 ✓

d 6.88 352.55 ✓

3+77<sup>0</sup> = N. Lin - Wightman

G 7.55 351.88 ✓

d 7.03 352.40 ✓

S. ch. Univ. }  
E. Line Ray } st at mlet. Top. ch 4.93 354.50 ✓

" " " " " " F.L. 5.97 353.46 ✓

S. ch. Univ. }  
3' E. of E. Line Ray } Top. ch 4.90 354.53 ✓

" " " " " " gutter 5.62 353.81 ✓

S. ch. Univ. }  
20' E. of E. Line Ray } Gutter 5.19 354.24 ✓



		X sec Gamma St 42nd to 43rd	80 wide	Indexed c.s.k.		86.28		54
							9.0	77.3
BM. CT.	7.35	86.28	78.93	see 1536-48	N		5.0	81.3
		0+0 x W.L. 43rd St.			N			
							5.4	80.9
N			3.8	82.5	+5		8.2	78.1
+8			8.8	77.5	+21		8.7	77.6
+25			10.7	75.6	+23		9.5	76.8
C			10.6	75.7	C		8.5	77.8
+10			11.0	75.3	+10		9.1	77.2
+20			12.2	74.1	+20		9.8	76.5
+26			8.1	78.2	+22		8.5	77.8
S			8.8	77.5	S		9.2	77.1
		0+25						
S			9.0	77.3	S - 15 E double gap dirt		9.4	76.9
+18			8.9	77.4	S		9.5	76.8
+20			10.2	76.1	+18		9.2	77.1
+30			9.8	76.5	+30		8.2	78.1
C			9.4	76.9	C		7.6	78.7
+14			10.0	76.3	+14		8.4	77.9
+16			9.4	76.9	+30		7.0	79.3

N	I 9' Conn. Drive	5.36	80.92		+ 21	7.1	79.2
+15	Break " "	2.91	83.37		+ 22	6.0	80.3
+33	I double gear. comp. fl.	2.47	83.81		N	4.5	81.8
	1+39				2+00		
N		5.0	81.3		N	4.0	82.3
+4		4.3	80.0		+17	5.3	81.0
+18		6.6	79.7		+19	7.2	79.1
+22		7.5	78.8		C	6.8	79.5
C		6.8	79.5		+10	7.2	79.1
+10		7.3	79.0		+20	8.0	78.3
+20		9.1	77.2		+34	9.0	77.3
+30		10.3	76.0		S	10.7	75.6
S	on hub	11.79	74.49	74.52	2+50		
	1+65			1536-48	S	9.5	76.8
S		11.6	74.7		+18	7.7	78.6
+15		9.8	76.5		+30	7.3	79.0
+20		8.1	78.2		C	7.0	79.3
+30		7.2	79.1		+20	7.6	78.7
C		6.9	79.4		+24	3.6	82.7

N		2.7	83.6
	S+100		
N		1.7	84.6
+17		2.9	83.4
+21		7.7	78.6
C		7.2	79.1
+10		7.5	78.8
+20		8.1	78.2
+22		7.1	79.2
S		9.0	77.3
	S+30		
S		9.3	77.0
+18		7.5	78.8
+20		8.3	78.0
+30		7.5	78.8
C		7.3	79.0
+18		7.8	78.5
+21		2.7	83.6
N		1.3	85.0

	3 + 54.49 = EL	42 md.	ST
N		2.0	84.3
+19		3.6	82.7
+22		7.3	79.0
C		7.4	78.9
+10		7.6	78.7
+17		8.2	78.1
+20		7.6	78.7
S		9.3	77.0

X sec. of 41 5th St.  
Epsilon to Gamma

60 wide  
10' above  
10' below  
March  
2-7-38.

Indexed  
c.s.R.

65.86

57

N.W.B.P.	7.60	60.66		53.06	Epsilon 1-2074	+8		8.3 57.6
T.P.	12.95	65.86	7.75	52.92		06		8.2 57.7
						W		7.9 58.0
NL Epsilon = 0+00							0+25	
W. cb	Top corr.		12.56	53.30		W		6.9 59.0
W cb	ground		11.9	54.0		06		7.4 58.5
1/4			12.4	53.5		+4		7.5 58.4
C			12.1	53.8		+0		11.2 54.7
1/2			12.2	53.7		1/4		10.6 55.3
E			12.50	53.33		C		10.4 55.5
ET			12.1	53.8		1/4		10.9 55.0
	0+04					+3		8.4 57.5
F			10.5	55.4		06		9.3 56.6
06			9.7	56.2		E		11.1 54.8
+7			9.4	56.7			0+50	
1/4			12.0	53.9		E		11.4 54.5
C			11.5	54.4		06		9.6 56.3
1/4			12.0	53.9		+8		8.1 57.8
+4			12.2	53.7		1/4		9.0 56.7
						C		8.5 57.4

1/4		8.8	57.1
+4		9.0	56.9
+6		7.2	58.7
cb		6.9	59.0
W		6.6	59.3
	1400		
W		6.1	59.8
cb		6.7	59.2
1/2		7.0	58.9
c		7.1	58.8
1/4		7.3	58.6
cb		9.0	56.9
E		9.7	56.2
	1405		
W	cent walk	5.92	59.84
	1450		
E		5.3	60.6
cb		5.4	60.5
1/2		5.4	60.5
c		5.1	60.8

1/4		5.2	60.7	
cb		4.8	61.1	
W		4.6	61.3	
	2400			
W		1.5	64.4	
cb		1.7	64.2	
1/2		2.3	63.6	
c		2.0	63.9	
1/4		2.2	63.7	
cb		2.2	63.7	
E		2.6	63.3	
T.P.	12.34	77.91	0.29	65.57
	2450			
E		11.6	66.3	
cb		11.4	66.5	
1/2		11.1	66.8	
c		11.0	66.9	
1/4		11.1	66.8	
cb		11.0	66.9	

77.91

77.91

59

W		10.5	67.4
	3400 JL Delta		
W		7.0	70.9
cb		7.0	70.9
1/2		7.2	70.7
c		7.2	70.7
1/4		7.4	70.5
cb		7.3	70.6
E		7.4	70.5
	S cb		
E		5.7	72.2
cb		5.5	72.2
1/2		5.6	72.3
c		5.7	72.2
1/2		6.0	71.9
cb		5.7	72.2
W		5.6	72.3
	S 1/4		
W		3.6	74.3
cb		3.7	74.2

	ON 13 <sup>th</sup> Mon.	4.24	73.67
1/2		4.2	73.9
c		4.1	73.8
1/2		3.8	74.1
cb		3.0	74.3
E		3.2	74.7
	F		
	E	2.2	75.7
	cb	2.1	75.8
	1/2	2.1	75.8
	c	2.2	75.7
	1/4	2.4	75.5
	cb	2.5	75.4
	W	2.6	75.3
	N 1/4		
	W	1.7	76.2
	cb	1.2	76.7
	1/4	0.7	77.2
	c	0.4	77.5
	1/2	0.5	77.4

41 ST. 4  
DELTA

77.91

90.25

60

cb			0.7	77.2
E			0.8	77.1
T.P.	12.58	90.25	0.24	77.67
	N cb			
E			10.2	79.9
cb			10.6	79.7
1/4			10.7	79.6
0			10.8	79.5
1/4			11.0	79.0
cb			11.9	78.4
+5			10.4	79.9
W			10.6	79.7
	N.L. DATA=00		80' wide	14' cb 13' 1/4
W			8.2	82.1
cb			7.9	82.4
+6			8.2	82.1
+7			9.0	81.0
1/4			9.0	81.3
c			8.8	81.5

1/4			9.2	81.1	
+5			8.5	81.8	
cb			7.4	82.9	
E			7.5	82.8	
			0+30		
E-7 E			at 2' walk	4.78	85.47
			0+35		
E			3.2	86.9	
cb			3.4	86.8	
1/4			4.1	86.2	
c			3.9	86.4	
1/4			2.6	85.7	
+2			4.9	86.4	
cb			0.7	86.6	
W			4.0	86.3	
T.P.	3.02	92.82	0.45	89.80	
			0+70		
W			3.4	89.4	
cb			3.6	89.2	

1/4		2.6	89.2
c		3.0	89.8
1/4		2.0	89.8
cb		3.3	89.5
E		2.5	90.3
43.5	5 walk	2.04	90.25
	0+90		
E		1.7	91.1
c		2.1	90.7
1/4		2.2	90.6
c		2.3	90.5
1/4		2.8	90.0
cb		2.9	89.9
W		2.8	89.5
	1+10		
W		4.0	88.8
cb		3.7	89.1
1/4		3.6	89.2
c		3.0	89.8
1/4		3.2	89.6

cb		3.0	89.8
E		2.4	90.4
	1+35		
E		4.4	88.4
cb		4.9	87.9
1/4		5.6	87.2
c		5.2	87.6
1/4		5.5	87.3
+3		5.6	87.2
cb		5.0	87.8
W		4.8	88.0
	1+50		
W		6.1	86.7
cb		6.2	86.6
1/4		6.6	86.2
c		6.2	86.6
1/4		6.7	86.1
cb		6.3	86.5
E		6.1	86.7



	1+75			
E-3	J.W. gar.	dirt	8.7	84.1
E			8.7	84.1
cb			8.9	83.9
1/4			8.7	84.1
c			8.4	84.4
1/4			9.0	83.8
cb			8.8	84.0
W			8.8	84.0
	2+00			
W			10.7	82.1
cb			10.8	82.0
1/4			10.9	81.9
c			10.5	82.3
1/4			11.0	81.8
cb			11.2	81.6
E			11.4	81.4
	2+85			
E			14.5	78.3
cb			14.7	78.1

			14.5	78.3
			14.0	78.8
			13.8	79.0
			14.3	79.5
			13.2	79.6
T.P.	1.53	82.41	11.94	80.88
	2+70			
W			4.4	78.0
cb			5.0	77.4
1/4			6.5	75.9
c			6.3	76.1
1/4			6.6	75.8
cb			6.6	75.8
E			6.5	75.9
	3+00	J+ GAMMA	80' wide	12' cb 13' 1/4
E			7.2	75.2
cb			7.3	75.1
1/4			7.4	75.0
c			7.4	75.0

		7.6	74.8		E		
cb		7.5	74.9		W		7.4 75.0
W		7.4	75.0		cb		7.5 74.9
	5cb				1/4		7.6 74.8
W		7.7	74.7		o		7.7 74.7
cb		7.7	74.7		1/4		7.8 74.6
1/4		7.7	74.7		cb		7.7 74.7
c		7.5	74.9		E		7.7 74.7
1/4		7.6	74.5		N 1/2		
cb		7.7	74.7		E		8.1 74.3
E		7.4	74.8		cb		8.4 74.0
	5 1/4				1/4		8.5 73.9
E		7.7	74.7		o		8.5 73.9
cb		7.5	74.9		1/4		8.7 73.7
1/4		7.6	74.8		cb		8.7 73.7
c		7.5	74.9		W		8.5 73.9
1/4		7.7	74.7		N cb		
	13' Mon.	8.39	74.02	4157 CARRON	W		9.2 73.2
cb		7.7	74.7		cb		9.3 73.1
W		7.8	74.6		1/4		9.5 72.9

82.41

64

0		9.2	73.2
1/2		9.4	73.0
c6		9.0	73.4
E		8.8	73.6

112 GUMMA

E		9.8	73.1
c6		9.8	73.0
1/2		10.0	72.7
c		9.9	72.5
1/4		9.9	72.5
c6		9.9	72.5
W		9.6	72.8

T.P.	7.25	83.35	6.31	70.10
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ctn. to 1706 p 55		8.86	74.49	74.49 ✓
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X sec alley 30' wide  
BIR. 97 City Hrs.  
amended Map.

Moore  
2-21-88.

indexed  
C.S.K.

+ HI - R<sub>0</sub>

NWBP 0.22 W 21.74 321.32 Myrtle 41 ST.

DWIGHT NOT paved

00-14 = N. of Myrtle

E.L. 41.57 TOP CB. 0.60 321.14

W<sub>2</sub> alley " " 5.71 316.03

" ground 4.7 315.0

C " 7.1 314.6

E " 7.5 314.2

W<sub>2</sub> Marlborough Top CB. 11.84 309.90

0+00 = N.E. Myrtle

E 5.8 315.9

C 5.8 315.9

W 5.6 316.1

W Top CB. 5.57 316.17

0+05

W 2.6 319.1

+ 5 4.8 316.9

C 5.2 316.5

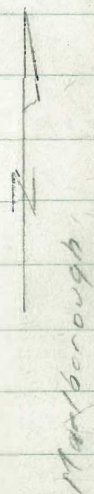
E 5.2 316.5



ST

10 10

ST  
41 ST



140.02

0+00

140.02

Myrtle NOT paved

0+19

F		U. V	318.2
C		U. 4	318.1
+d		U. 5	318.2
W		2.2	318.5
+10 Sin gar.	dirt	1.4	320.3

0+25

-12 Sin. gar	dirt	1.5	320.4
W		1.9	319.5
C		2.4	319.3
E		2.6	319.1

0+50

E		3.2	318.5
+5		1.8	319.9
C		2.0	319.7
W		1.4	320.3

0+91

-4.5 Sin. gar.	dirt	1.4	320.3
W		1.8	319.9
C		2.0	319.7

E

3.0 318.7

1+04

-3.5 Sin gar	dirt	2.7	319.6
E		2.4	319.3
C		1.9	319.8
W		1.8	319.9

1+20

W	Cent. walk	1.57	320.12
W		1.9	319.8
C		1.7	320.0
E		2.2	319.5

1+40

-3.5 Sin. gar	Cent.	2.13	319.61
E		2.0	319.7
C		1.5	320.2
W		1.5	320.2

T.P. 9.85 330.00 1.56 320.18

	1+60		
-8	Sin. gar dirt	8.80	321.23
-W		9.20	320.80
-W		9.0	320.7
-C		9.5	320.5
-E		9.0	320.4

	1+85		
-E		8.7	321.3
-O		8.6	321.4
-W		8.5	321.5
+3	E apron	8.65	321.40
+8	" gar. cent.	7.98	322.05

	1+91		
-4.5	E 16' gar dirt	8.1	321.9 (H. Level)
-E		8.6	321.4
	2+25		
-W		7.0	323.0
-C		7.3	322.7
-E		7.5	322.5

	2+60		
-E		6.4	323.6
-C		6.3	323.7
-W		6.4	323.6

	3+00		
-W		5.4	324.7
-C		5.5	324.5
-E		5.4	324.4

	3+25		
-E		4.9	325.1
-C		4.8	325.2
-W		4.6	325.4

	3+51		
-W		4.7	325.8
-C		4.4	325.6
-E		4.4	325.6
+7	E Sin. gar. dirt	4.6	325.4
	4+00		
-E		4.1	325.9
-C		3.8	326.2

ENTRANCE  
FROM AILEY

W	4 3 +40	3.4	326.6
W		2.9	327.1
C		3.2	326.8
E		3.4	326.6
+10		4.5	325.5
	4+69		
-10		4.5	325.8
E		3.2	326.8
C		3.1	326.8
W		3.1	326.9
+8	Six. gar. dirt 5+00	2.8	327.2
W		2.9	327.1
C		3.2	326.8
E		3.7	326.3
+10		4.6	325.4
	5+25		
-10		4.0	326.0
E		3.4	326.6

C		3.0	327.0	
W'		2.9	327.1	
T.P.	7.48	334.83	2.68	327.25
	5+50			
W		7.1	327.7	
C		7.5	327.3	
E		7.2	327.6	
+5	Wedge com. drive	6.52	328.31	
+6	E gar. "	6.52	328.31	N. end of front st.
	5+75			
E		6.4	328.4	
C		7.2	327.6	
W		6.9	327.9	
+7	Six. gar. dirt	7.0	327.8	N. entrance from alley
	5+75			
W		6.4	328.2	
C		6.6	328.2	
E		6.2	328.6	

## 6 + 00 - 5 L Dwight

F	cb	2.90	329.95
K		5.1	329.7
C		5.4	329.4
W		5.3	329.5
W	cb	4.95	329.90

## S cb Dwight

EL	41ST TOP cb.	5.02	329.51
W	L alley " "	5.07	329.81
W	41ST	5.4	329.4
C	"	5.3	329.5
E	"	5.2	329.6
E	TOP cb.	4.89	329.74
W.L.	Marlborough cb.	4.57	330.26

NW 07	Marlborough Dwight	3.85	330.98 + 30.99
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3-25-38  
Miller  
Walker  
Bliss

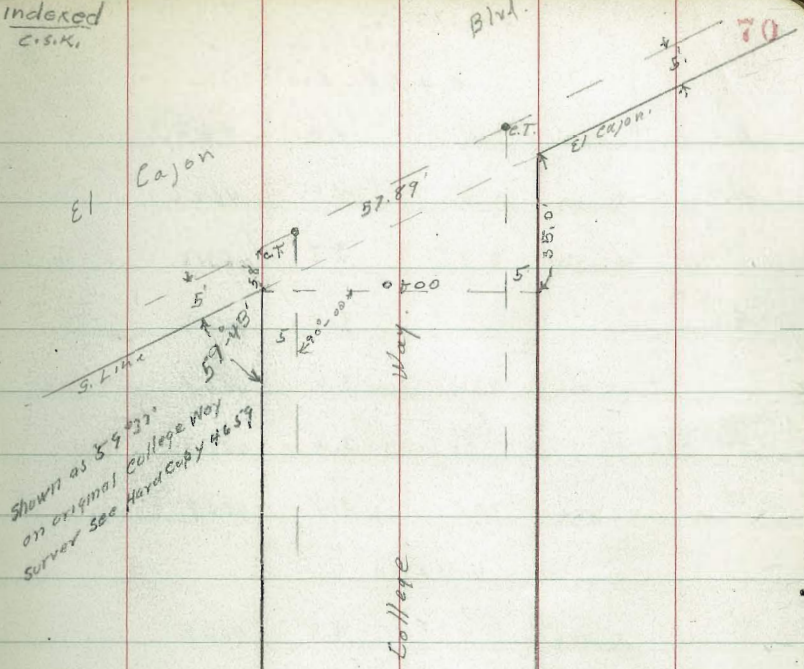
X See College Way.  
El Cajon Blvd. to 280' South  
60' wide 12' chs 9' ins

N.W. El Cajon  
+ College Way

B.M. BP.	1.45	466.72	465.27	
0.6 N. of S. line of El Cajon = S. End. ent. walk, curb, & Parvt.				
E		1.9	464.8	
e ch.	Top.	2.02	464.70	
G.	PAV	2.58	464.14	
"	"	2.42	464.30	
±	"	2.32	464.40	
"	"	2.38	464.34	
W ch. line "		2.47	464.25	
+ 1' = G. "	on 10' P. Curve.	2.47	464.25	
+ 1. Top. ch		1.81	464.91	
W.	ent. walk	1.91	464.81	S. W. Cor
0+00 = 90°-00' from S.W. Cor.				
W	ent. walk	1.91	464.81	S. W. Cor
ch		2.6	464.1	
"		2.7	464.0	
±		2.8	463.9	
"		2.8	463.9	
ch		2.6	464.1	
E		2.4	464.3	

Indexed  
C.S.K.

Blvd.



70

466.72

0 + 50 South

e	4.0	462.7
dr	4.1	462.6
"	3.7	463.0
±	3.5	463.2
"	3.6	463.1
d	3.4	463.3
w	3.8	462.9
1 + 00		
w	4.8	461.9
dr	5.0	461.7
"	4.5	462.2
±	4.4	461.9
"	4.8	461.9
d	5.0	461.7
E	4.7	462.0
1 + 16 = N. End. Stucco wall 4.0' High along W. Line		
1 + 50		
E	6.0	460.7
dr	6.0	460.7
"	5.8	460.9
±	5.6	461.1

466.72

College

71

"	6.0	460.7
dr	6.0	460.7
w	5.8	460.9
1 + 91.		
W. = ± . E. End. cmt. walk 3.5' wide 6.88		
2 + 00		
W = ± E. End. cmt. Drive 9' wide		
dr	7.0	459.67
"	7.4	459.7
±	7.2	459.5
"	7.3	459.4
d	7.6	459.1
E	7.8	458.9
2 + 07 E = S. End. Stucco Wall on W. Line		
2 + 50		
E	9.4	457.3
dr	9.6	457.1
"	9.5	457.2
±	9.9	456.8
"	9.4	457.3
dr	9.5	457.2

466.72

2+50 (con)

W.

9.1

452.6

2+80 South

W

10.9

453.8

d

11.4

455.3

114

11.6

455.1

E

11.5

455.2

114

11.6

455.1

d

11.7

455.0

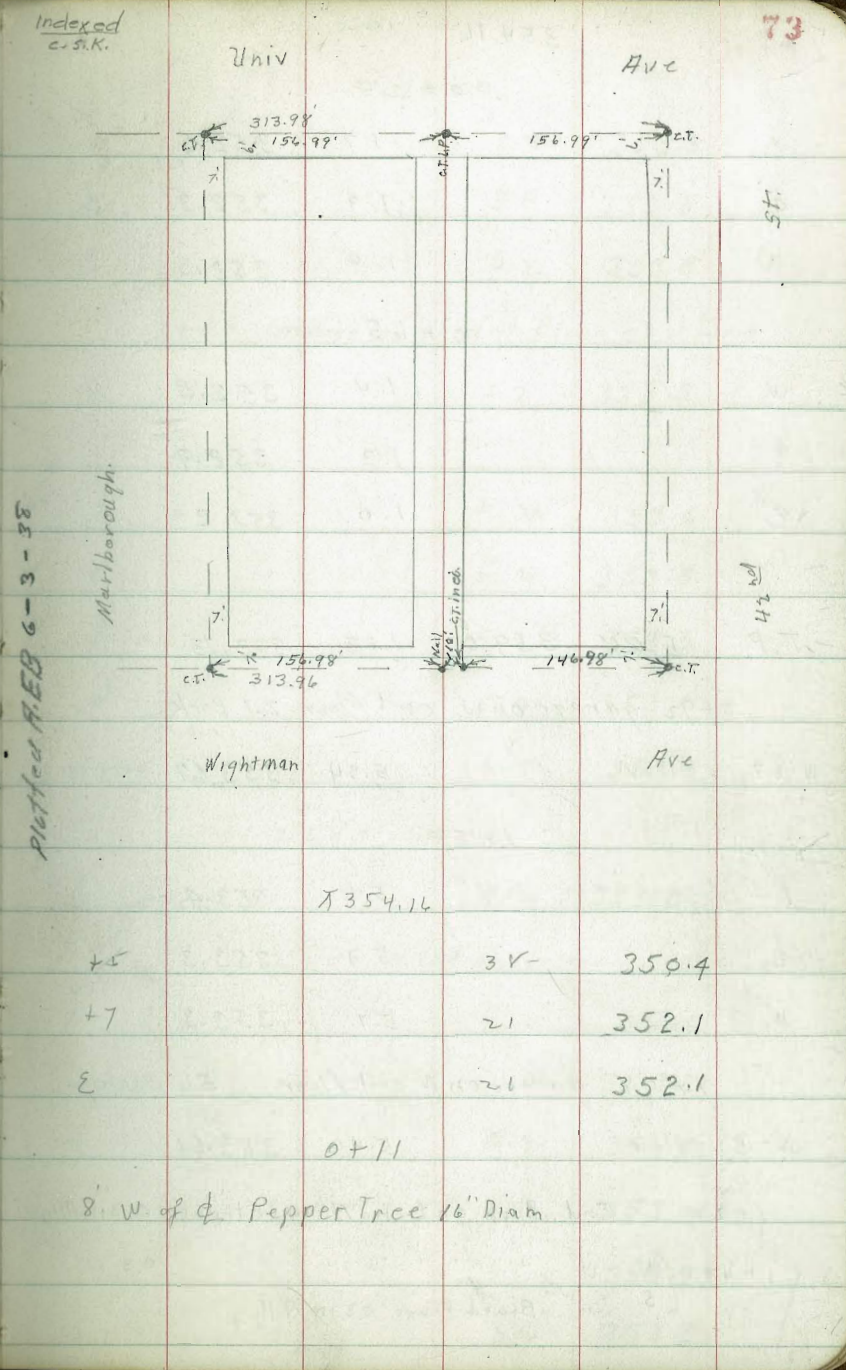
E

11.3

455.4

See F.B. 1568-38 Notes 9/5/39.

6-2-38. Miller Walker Bliss	X Sec. Alley Bk. 50. City Hts								
B.M. B.P.	6.71	349.79		343.09	N.W. Landis + Marlborough				
T.P. B.M. B.P.	7.13	354.16	2.76	347.03	N.W. Wightman + Marlborough				
					Wightman Unpaid.				
					14' S. of N. Line = N. cb. of Wightman				
W - 140' =	E. Line Marlborough.	6.64		347.52	cmt. cl.				
" " "	" " "	7.26		346.90	gutter Pav. E. End.				
W.	dirt-gutter	5.0		349.2					
W.	cmt. cl.	4.46		349.70					
⊕		4.8		349.4					
E.	cmt. cl.	4.03		350.13					
E.	dirt-gutter	4.7		349.5					
E + 140' =	W. Line + 2 1/2"	1.63		352.53	cmt. cl.				
" " "	" " "	2.27		351.89	Gutter Pav W. End.				
	0+00 = N. Line Wightman.								
	0.4' W. of E. Line = cmt. cl. N. End. + dirt.	3.89		350.27					
⊕		4.1		350.1					
	0.1' E. of W. Line = cmt. cl. N. End. + dirt.	4.20		349.96					
	0+03								
W		2.7		351.5					
+3		3.7		350.5					
⊕		3.8		350.4					



354.16

0+25

E 1.7 352.5

E 1.9 352.3

W 1.9 352.3

0+65

W 1.4 352.8

E 1.3 352.9

E 1.0 353.2

T.P. 5.88 359.01 1.03 353.13

0+92 garage on W. cnt. floor 2.7 Back.

W-2.7 = floor 5.34 353.67

1+00

E 5.6 353.4

E 5.7 353.3

W 5.7 353.3

1+08 garage on W cnt. floor 5.6 Back

W-5.6 = floor 5.40 353.61

1+28 S. End. Barb on E. no Alley Entrance 0.3 in Alley

1+49 { N " " " " " 0.3 " "  
S " Board. Fence 0.3 in Alley.

359.01

1+50

W 5.7 353.3

E 5.5 353.5

E 5.2 353.8

1+57 Garage on W. dirt floor on W. Line

W = floor 5.7 353.3

2+00

E-10 5.4 353.6

E 5.2 353.8

E 5.5 353.5

W 5.7 353.3

W+15 6.0 353.0

2+40

E Top. M.H. 5.12 353.89

2+50 N. End. above fence on E. 0.3 in Alley.

W-15 6.0 353.0

W-1 5.8 353.2

W 5.2 353.8

E 5.1 353.9

E 5.1 353.9

E+10 5.2 353.8

74

359.01

From 3+70 to 3+82 <sup>frame</sup> dwelling on E. 0.15 in Alley  
Plumbing 0.8 in Alley.

3+00

E -10 4.9 354.1  
E 4.8 354.2  
E 5.1 353.9  
W 5.2 353.0  
+ 1. 5.4 353.6  
+ 2.5 6.0 353.0

3+09 garage on E. cnt. floor 3.0 Back

E-3.0 = floor 4.70 354.31

3+50

W-25 7.0 352.0  
W 5.5 353.5  
E 5.5 353.5  
E 4.8 354.2  
E+15 4.8 354.2

3+64 garage on E cnt. floor 3.2 Back

E-3.2 = floor 4.63 354.38

359.01

75

3+76 Garage on E dirt floor 3.2 Back  
E-3.2 floor 5.1 353.9

3+82 garage on W dirt floor 7.5 Back

W-7.5 floor 6.1 352.9

3+88 garage on E dirt floor 3.2 back

E-3.2 = floor 5.14 353.87

4+00

E-15 5.1 353.9

E 5.6 353.4

E 5.9 353.1

W 5.9 353.1

+ 1 6.5 352.5

+ 2.0 7.0 352.0

4+13. garage on E. cnt. floor 2.2 Back

E-2.2 floor 5.05 353.96

4+24. garage on E. dirt. floor 2.0 Back

E-2.0 = floor 5.6 353.4

4+29. garage on W dirt. floor 0.5 in Alley

0.5 E. of E. line = floor 6.1 352.9

4+ garage on E cnt. floor Back ?

E-1.8 = floor 5.38 353.63

359.01

4+41 garage on W dirt floor 0.7' in Alley  
 0.7' E of W line = floor 5.8 353.2

4+47 to 4+66 Fence on W 0.5' in Alley

4+66 to 4+75 Shed on W 0.5' in Alley

4+50

E- 5.5 353.5

E 5.6 353.4

⊕ 6.0 353.0

W 5.9 353.1

4+80

W-25. 6.6 352.4

W-1. 6.0 353.0

W 5.6 353.4

⊕ 5.6 353.4

E 5.6 353.4

+10 5.4 353.6

4+84 ctn double garage on E ext. floor 0.7' Back

E-0.7' = floor. 5.20 353.81

359.01

76

5+00

E-15. 4.6 354.4

E, 5.2 353.8

⊕ 5.4 353.6

W 5.6 353.4

W+15 6.0 353.0

5+50

W-15 4.1 354.9

W 4.3 354.7

⊕ 4.7 354.3

E 4.4 354.6

5+55 = S. End. Tile Bldg on W 0.2' in Alley.

5+90

E 3.8 355.2

+3 4.1 354.9

⊕ 4.2 354.8

W 4.1 354.9

5+93 = N. End. above Tile Bldg on W 0.15' in Alley

359.01

77

5 + 99 = S. Line - Univ. Ave

W. amt. db 4.03 354.98

W pay 4.20 354.81

E " 4.37 354.64

E pay. 4.00 355.01

E. amt. db below pay. 4.95 354.96

T.P. 6.29 360.90 4.40 354.61

15' N. of S. Line - S. db Line of Univ. Ave

E-25 gutter 6.17 354.73

E " 6.47 354.43

E. db 6.01 354.89

E gutter 6.58 354.32

W " 6.68 354.22

W db 6.31 354.59

W+25 gutter 6.90 354.00

T.P. 5.12 362.85 3.17 357.73

B.M. B.P. N.W. Van Dyke + Univ. 4.53 358.32 = 358.25







DIRECTIONS FOR USE OF TABLES

TABLE I

Distance of ship's side from side of direction  
table for any wind, read down side of table  
If ground is nearly level, the course will be  
true as found by the angle every minute in  
for column and top row. The number in  
row side table to right side of table

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## IMPROVED TABLES

AND

## INFORMATION

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To find Latitude and Longitude for course in  
any other degree, divide by degree of course and  
add correction found in column of correction  
Degree of course with a given latitude found  
by dividing tangent of course by tangent of  
given tangent (or course)  
The distance from a point on the tangent to  
the curve is very nearly the square of the tangent  
both divided by twice the radius

2613.98  
156.99

2317.96  
156.98

4515

20.8 3.8 E.L. Ray

4.90 4.93d

6519 5.82 5.976  
5

5105  
27  
5078

MIN BP 4075 + EPSILON 5306

3 123  
77

6 46 40  
77  
44

4

b.

6 24  
046

57.047

50.046  
0.93

90-01.647

89-59.747

56.90-00

89-59.40

51-89-59