

1544

PASTS

WEL BOOK

No. 33 T

1544

MICROFILMED
DEC 24 1964

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO
CALIFORNIA

MADE IN U. S. A.

Our Leather Bound Engineers Note Books
are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page
the same as Left Hand Page
of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this
Book, Right Hand Page 4x4
to the inch, Center Line Red.
- No. 384 MINING TRANSIT
BOOK. Left Hand Page as in this
Book, Right Hand Page 8x8
to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this
Book, Right Hand Page 8 ver-
tical and 4 horizontal lines to
the inch, Center Line Red.

We also carry the Note Books listed above,
bound in extra strong Fabri-Hide (otherwise
the same quality of book,) which can be fur-
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In ordering Fabri-Hide covered books, add
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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

P. O. Box 803

CHICAGO

Entire Book Indexed 9-28-37
C.S.K.

Also F.B. 1791

✓ C.B. 246

✓ G.B. 252

Our Eastern Books Engineers Note Books
are carried in the following manner
No. 100 LEVER BOOK
No. 101 FIELD BOOK
No. 102 MINING TRANSMIT
BOOK
No. 103 FIELD BOOK

We also carry the Note Books listed above
bound in extra strong fabric like (otherwise
the same quality of book) which can be
bound at a somewhat lower price.
In ordering fabric-like covered books add
the letter "F" to catalog number.

THE FREDERICK POST CO.
ENGINEERING and DRAWING SUPPLIES
R. L. BOX 503
CHICAGO

X sec of Buenas St. 50' wide.
Beg. Nly of Weeks Add.

Moore
S. 1150N
Northern
8-23-37

Indexed
C.S.K.

LT.

RT.

4

1 + 44.74 33° 10' 21"

46.5	47.8	47.8	47.2	48.1	48.5	49.3	49.8	50.7
13.0	11.7	11.7	12.8	11.4	11.0	10.3	9.7	8.8
1.8	1.5	1.0	1.6	1.4	1.8	1.9	2.7	1.0

A = 88° 27' 37"
ER = 125
T = 121.68
EL = 192.99
ELL = 231.59

0 + 96.49 22° 06' 54"

45.7	46.4	45.3	46.6	46.7	47.7	48.7
13.8	13.1	14.2	12.9	12.8	11.8	10.8
3.8	1.9	1.7	1.9	1.7	1.9	3.0

T.P. 1211 59.50 021 27.39

59.50

0 + 48.24 11° 03' 27" LT

43.5	43.3	42.5	43.6	43.4	44.1	45.8
4.1	4.3	5.1	4.0	4.2	3.5	1.8
2.8	2.3	1.8	4.0	1.4	1.6	3.0

0 + 0⁸⁰ = Nly Weeks Add. St. 60' wide to 50' wide at EL

40.1	39.7	39.2	39.6	39.4	40.1	40.6
7.5	7.9	8.4	8.0	8.2	7.5	7.0
5.0	2.5	2.0	8.0	1.6	1.8	4.0

NOTE / £ STA.

T.P. 12.84 47.60 022 34.76

47.60

T.P. 12.61 34.98 291 22.37

BM. Mon. 8.42 25.28 16.86

near Dyke
near Weeks
add.

4 + 11.94 taken on Tang. of Buenos

<u>15.4</u>	<u>13.8</u>	<u>11.5</u>	<u>11.3</u>	<u>11.5</u>
25	20	25	25	25
44.1	45.7	48.0	48.2	48.0

3 + 76.52 B.C. RT. D 180° RT

<u>14.2</u>	<u>14.4</u>	<u>12.6</u>	<u>11.7</u>	<u>11.0</u>	<u>11.6</u>	<u>11.5</u>
23	23	9	5	11.0	25	25
43.1	45.1	46.9	47.8	47.9	47.9	48.0

+50

<u>14.2</u>	<u>12.8</u>	<u>11.5</u>	<u>11.6</u>	<u>11.7</u>
25	25	25	25	25
45.3	46.7	48.0	47.9	47.8

3

<u>14.1</u>	<u>12.2</u>	<u>12.8</u>	<u>11.4</u>	<u>11.5</u>
25	20	12	20	25
45.4	47.1	46.7	47.8	48.1

2 + 50

<u>16.1</u>	<u>15.2</u>	<u>12.8</u>	<u>12.2</u>	<u>12.6</u>	<u>11.9</u>	<u>11.2</u>	<u>11.1</u>
25	25	20	12	10	15	25	25
43.4	44.3	46.7	47.2	46.9	47.6	48.2	48.4

1 + 92.99 = E.C. 44° 13' 48"

<u>14.0</u>	<u>11.8</u>	<u>11.6</u>	<u>11.9</u>	<u>11.0</u>	<u>10.2</u>	<u>10.0</u>
30	21	12	10	19	21	25
45.5	47.7	47.9	47.6	48.3	48.5	49.3

59.50

59.50

Indexed
0.51K1

Elev. Rd.

6

T.P. 12.80 72.02 0.28 59.22 ROCK

5+72.87 $\Delta = 90^\circ 00'$ Fly Dorcas

$\begin{array}{r} 0 \\ 10 \\ \hline 59.5 \end{array}$	$\begin{array}{r} 0 \\ 22 \\ \hline 59.5 \end{array}$	$\begin{array}{r} 1.7 \\ 18 \\ \hline 57.8 \end{array}$	$\begin{array}{r} 2.4 \\ 57.1 \end{array}$	$\begin{array}{r} 2.6 \\ 56.9 \end{array}$	$\begin{array}{r} 2.0 \\ 57.5 \end{array}$	$\begin{array}{r} 1.6 \\ 57.9 \end{array}$

5+723.78 $67^\circ 30' = \Delta$

$\begin{array}{r} 2.9 \\ 1.5 \\ \hline 52.5 \end{array}$	$\begin{array}{r} 6.9 \\ 1.5 \\ \hline 52.6 \end{array}$	$\begin{array}{r} 6.7 \\ 52.8 \end{array}$	$\begin{array}{r} 7.2 \\ 1.5 \\ \hline 52.3 \end{array}$	$\begin{array}{r} 5.8 \\ 1.9 \\ \hline 53.7 \end{array}$	$\begin{array}{r} 5.4 \\ 2.5 \\ \hline 54.1 \end{array}$
--	--	--	--	--	--

4+74.69 $45^\circ 00' = \Delta$

$\begin{array}{r} 1.2 \\ 1.5 \\ \hline 48.3 \end{array}$	$\begin{array}{r} 10.2 \\ 1.5 \\ \hline 49.2 \end{array}$	$\begin{array}{r} 9.8 \\ 49.7 \end{array}$	$\begin{array}{r} 9.8 \\ 1.5 \\ \hline 49.7 \end{array}$	$\begin{array}{r} 8.8 \\ 2.5 \\ \hline 50.7 \end{array}$
--	---	--	--	--

4+2561 $23^\circ 30' = \Delta$
ON CURVE CONTINUING ON Elev. Rd.

$\begin{array}{r} 2.2 \\ 1.5 \\ \hline 46.3 \end{array}$	$\begin{array}{r} 12.1 \\ 1.5 \\ \hline 47.4 \end{array}$	$\begin{array}{r} 11.3 \\ 48.2 \end{array}$	$\begin{array}{r} 11.4 \\ 1.6 \\ \hline 48.1 \end{array}$	$\begin{array}{r} 11.2 \\ 2.5 \\ \hline 48.3 \end{array}$
--	---	---	---	---

4+72.36 = Fly Dorcas & Buencas

$\begin{array}{r} 14.8 \\ 2.5 \\ \hline 44.7 \end{array}$	$\begin{array}{r} 13.0 \\ 46.5 \end{array}$	$\begin{array}{r} 10.6 \\ 2.5 \\ \hline 48.9 \end{array}$
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4+47.36 = B.C. LT. 25' P.P.

$\begin{array}{r} 15.8 \\ 2.5 \\ \hline 43.7 \end{array}$	$\begin{array}{r} 14.1 \\ 2.0 \\ \hline 45.4 \end{array}$	$\begin{array}{r} 12.0 \\ 47.5 \end{array}$	$\begin{array}{r} 11.1 \\ 1.0 \\ \hline 48.4 \end{array}$	$\begin{array}{r} 11.6 \\ 2.5 \\ \hline 47.9 \end{array}$
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59.50

59.50
2

T.P. 13.00 97.67 0.21 84.67

8

7+69.27 = E.C. of $\Delta 130^\circ$ 8.54 76.36 on \pm Hub B.M.

7+13.48 = P.R.C. on LT $\Delta = 154^\circ 27'$

T.P. 13.00 84.88 0.14 71.88

6+71.04 $135^\circ 00' = \Delta$

6+21.95 $112^\circ 30' = \Delta$

72.02

LT.

\pm

Pt. Elev. Rd.

7

70.2	75.8	77.2	76.9	76.4	76.5	75.5	76.0	75.9	75.1	64.7
14.7	9.1	7.7	8.0	8.5	8.4	9.4	8.7	9.6	9.8	10.2
35	35	27	12	10		12	15	25	28	45

Location for Prop. Culvert

73.8	72.2	71.1	71.8	70.8
11.7	13.7	13.8	13.1	14.1
25		10	14	25

84.88

67.4	63.6	62.7	61.9	62.2	63.0
7.6	8.4	9.3	10.1	9.4	9.0
25	25		12	16	25

72.02

9+77.48

1053' 22"

9+52.75 = DC RT

A = 7° 23' 30"
EP = 375
T = 24.77
EL = 49.47

T.P.

1298

11029

0.36

97.31

11029

9

8+84.22

8+96.22 E MONITOR

8+69.22 WL MONITOR to LY.

8+59.22

8+49.22 = PC ON LY.

97.67

97.67

107.3	106.8	104.3	102.7	102.4	101.7	102.3	101.8	100.6
2.0	2.4	2.2	2.8	2.9	2.6	2.0	2.5	2.7
2.5	2.8	2.7	3.5	3.3	3.2	2.5	2.2	2.5
102.1	100.5	100.0	99.4	100.1	97.8	10.2	10.5	12.7
8.2	9.8	10.3	10.9	10.2	10.5	15	2.2	3.5
7	5	6	14	15	14	15	2.2	3.5
97.0	95.1	94.2	93.3	94.1	93.5	91.7	91.6	91.2
5.0	5.7	6.5	7.2	7.6	8.0	8.0	8.1	8.7
5.0	5.7	6.5	7.2	7.6	8.0	8.0	8.1	8.7
73.1	74.5	72.7	71.9	71.2	71.7	71.7	71.6	70.0
5.0	5.7	6.5	7.2	7.6	8.0	8.0	8.1	8.7
71.0	89.4	88.4	87.7	88.1	87.3	87.3	87.3	87.3
6.7	8.0	9.3	10.0	9.6	10.2	10.2	10.2	10.2
5.5	1.3	1.3	1.3	1.4	1.5	1.5	1.5	1.5

14+29.73 $\Delta = 70^\circ 01'$

$\frac{5}{25}$	$\frac{5}{19}$	$\frac{5}{18.4}$	$\frac{5}{5.5}$	$\frac{5}{9}$	$\frac{5}{20}$	$\frac{5}{25}$
115.7	115.7	115.2	115.2	114.7	114.9	112.0

13+88.81 $\Delta = 46^\circ 40' 20''$ $\Delta = 140^\circ 02'$
 $R = 125$
 $L = 305.51$

$\frac{9.9}{25}$	$\frac{10.0}{20}$	$\frac{10.0}{19}$	$\frac{10.4}{10.3}$	$\frac{10.7}{8}$	$\frac{11.2}{20}$	$\frac{14.1}{25}$
110.8	110.7	110.0	110.4	110.0	109.5	106.6

13+07.90 $\Delta = 20^\circ 20' 20''$

$\frac{13.0}{52}$	$\frac{13.0}{50}$	$\frac{13.5}{49}$	$\frac{13.0}{13.0}$	$\frac{13.9}{10}$	$\frac{14.2}{18}$	$\frac{18.3}{25}$
107.7	107.7	107.2	107.7	106.1	106.5	102.4

T.P. 12.95 120.70 254 107.75

120.70

12+86.98 PRC. of $\Delta 180^\circ$
 $21^\circ 45' 15''$

$\frac{2.4}{5}$	$\frac{2.8}{15}$	$\frac{3.7}{15}$	$\frac{5.0}{14}$	$\frac{5.0}{15}$
106.1	106.5	106.6	105.0	102.1

12+39.5 $18^\circ 07' 40''$ Proposed curb outlet on Rt.

$\frac{4.1}{25}$	$\frac{4.5}{15}$	$\frac{4.1}{12}$	$\frac{4.9}{12}$	$\frac{5.0}{12}$	$\frac{5.1}{15}$
106.2	105.8	106.2	105.4	105.0	103.1

110.29

110.29

17

10+50.

15792.49

P.C. LT. = Δ 140°02'
P.C. RT.

T.P.

1240

145.9

0.18

132.53

15441.57

 $\Delta = 116^\circ 41' 40''$

14+90.65

 $\Delta = 98^\circ 21' 20''$

T.P.

12.44

132.71

0.43

120.27

120.70

4.5
140.9
137.74.0
141.2
137.94.0
141.2
137.94.8
140.4
137.24.2
141.0
137.74.0
141.2
138.14.5
140.2
134.212.8
132.4
12.612.6
132.6
12.912.9
132.3
12.712.7
133.0
12.712.7
132.5
12.012.0
133.2
11.611.6
133.6
11.011.0
134.2
11.05.2
127.3
5.65.6
127.1
5.05.0
127.7
5.75.7
127.0
4.94.9
127.8
5.55.5
127.9
5.510.4
122.26
10.710.7
121.95
10.710.7
122.0
11.411.4
121.3
11.711.7
121.0
12.112.1
120.2
11.811.8
120.9
11.811.8
120.5
15.615.6
117.1
15.610.4
10.7
10.7
11.4
11.7
12.1
11.8
11.8
11.8
15.6

132.71

Elev. Rd.

11

17 19

15	153.7
25	149.7
40	150.0
23	149.4
43	150.5
12	149.9
17	150.4
25	150.6
25	152.9
25	153.2
25	152.4
25	153.2
25	152.9

16 + 50

7.8	149.7
25	149.7
7.5	150.0
14	150.0
8.1	149.4
13	149.4
7.0	150.5
14	149.9
7.1	150.4
16	150.4
6.9	150.6
25	150.6

15 18

11.0	146.5
25	146.5
10.3	147.2
14	147.2
11.0	146.5
13	146.5
10.2	147.3
14	147.3
10.9	146.6
14	146.6
10.1	147.4
15	147.4
10.2	147.3
25	147.3

T.P. 17+66.96 PC ON LT.

12.9	144.6
25	144.6
12.3	145.2
14	145.2
12.8	144.7
13	144.7
12.2	145.3
14	145.3
12.7	144.8
16	144.8
10.1	145.4
15	145.4
10.1	145.4
25	145.4

154 T.P. on Rock 12.82 157.48 0.53 144.66

143.9	157.48
15	143.9
144.2	157.48
14	144.2
143.7	157.48
13	143.7
0.9	144.3
15	144.3
143.7	157.48
15	143.7
0.9	144.3
17	144.3
0.6	144.6
25	144.6

14 + 17 + 50

T.P.

145.19

145.19

17 29 + 43.20 13° 11' 24"

$\Delta = 39^{\circ} 34' 10''$
 $EP = 215.17$
 $T = 76.70$
 $EL = 148.60$

16 20 + 93.44 6° 35' 42"

15 20 + 44.13 PRC. 17° 18' 44"

T.P. 19 + 94.22 8° 39' 20"

15 4 T.P. 11.47 168.35 0.60 156.88 B.M.

$\Delta = 34^{\circ} 37' 28''$
 $EP = 165.17$
 $T = 51.48$
 $EL = 99.81$

14 19 + 44.32 B.C. LT

157.48

166.1	164.7	164.8	164.4	165.4	164.8	165.7	165.5
2.2	2.7	3.6	4.0	3.0	3.6	2.7	2.9
164.9	162.5	162.5	162.5	162.5	161.5	162.2	162.1
160.0	159.8	159.8	159.8	159.8	159.5	159.5	159.2
157.3	156.6	157.4	156.5	156.5	156.9	156.7	156.7
11.1	11.8	11.0	11.9	11.5	11.7	11.7	11.7
2.5	3.1	2.5	2.5	2.5	2.5	2.5	2.5

LT
 30 RP CT. IN CORR APRON

158.5	156.13	152.3	155.3	154.4	155.2	154.4	155.2	154.6
1.35	1.2	2.7	3.1	2.3	2.3	2.3	2.3	2.3
157.18	154.93	152.6	152.6	152.6	152.6	152.6	152.6	152.6
157.48	157.48	157.48	157.48	157.48	157.48	157.48	157.48	157.48

Edge corr apron
 Est. Gar. correction

157.48

17 26+2175 = Sly on road

16 25+96.7N

15 T.P. +195.4

11.88

201.87

3.09

189.99

ON E Hub

3 of N. Solar St.

201.87

T.P. +50

15 25+19.52 EC on Hub.

3.09

189.99

BM. ON E Hub

13°51'20"

14 24+66.24

POC

PRC on Rt. at Solar St.

11°35'15"

193.08

193.08

193.0	192.0	192.0	191.6	192.2	191.4	192.1	193.1
19	7.9	9.9	10.3	9.7	10.5	9.8	8.8
25	23	14	21	26	16	17	25
192.6	191.0	190.9	190.3	190.3	189.9	190.3	189.9
1.5	2.1	2.1	2.8	2.3	4.1	2.8	4.2
193.8	190.3	190.2	189.8	190.3	189.9	189.2	189.9
1.7	2.8	2.9	1.3	2.8	3.2	3.9	4.9
192.6	189.1	188.9	188.3	188.5	187.7	188.2	188.1
1.5	2.0	2.2	1.8	2.2	1.7	2.9	2.0

Elev. Rd.

28+1353 T.P. 12.03 213.51 0.39 201.48 B.M. 2x2
E Hub

17 28+1353 EC.

16 27+54.9 E Curve

$\Delta = 20^{\circ}38'$
E.P. = 325.62
T = 57.27
PL = 117.26

15 27+20

37+18 N 1.5' ribbon
37+14 S 1.5' ribbon
27+05 E 4' walk
26+96.27 D.C. RT.

197.30
197.14
197.0

15 26+71.27

14 20+46.27

201.87

NL Brownell St, 4 Elev. Rd.

201.9 0.0 25	201.2 0.7 23	201.2 0.7 24	200.7 0.2 24.2	201.6 0.2 24.6	200.9 0.2 24.0
199.7 0.2 25	199.0 0.2 23	198.8 0.2 24	198.3 0.2 24.2	199.5 0.2 24.6	197.5 0.2 24.0
197.4 0.2 25	197.5 0.2 23	197.2 0.2 24	197.9 0.2 24.2	197.5 0.2 24.6	198.2 0.2 24.0
196.1 0.2 25	196.1 0.2 23	195.7 0.2 24	196.7 0.2 24.2	196.1 0.2 24.6	196.8 0.2 24.0
194.1 0.2 25	194.5 0.2 23	195.1 0.2 24	194.4 0.2 24.2	194.9 0.2 24.6	195.4 0.2 24.0
194.3 0.2 25	194.1 0.2 23	193.7 0.2 24	194.4 0.2 24.2	194.1 0.2 24.6	194.1 0.2 24.0

201.87

17 30+13.73 Sky Overview Rd.

16 29+88.73 R.C.

15 29+50

14 29

15 28+60

14 28+38.53

213.51

203.0	203.7	204.6	205.1	205.1	205.1	205.5	205.5
10.4	9.8	9.9	9.1	9.4	9.8	10.0	10.0
25.4	25.8	25.9	25.5	25.4	25.4	25.4	25.4
202.3	204.0	205.1	205.1	205.3	206.2	206.4	206.7
11.2	9.5	9.0	9.0	9.2	9.7	9.9	10.0
25.5	25.5	25.5	25.5	25.5	25.5	25.5	25.5
202.3	204.3	205.5	205.5	206.3	206.8	206.8	207.3
11.2	10.0	9.0	9.0	9.2	9.7	9.9	10.0
25.5	25.5	25.5	25.5	25.5	25.5	25.5	25.5
202.3	204.3	205.5	205.5	206.3	206.8	206.8	207.3
11.2	10.0	9.0	9.0	9.2	9.7	9.9	10.0
25.5	25.5	25.5	25.5	25.5	25.5	25.5	25.5

213.51

Elev. Rd.

17

X sec of Solar St

Indexed
C.S.K.

LT = 5

PT = N

18

1+25

175.9	179.1	179.3	178.8	180.0	179.4	180.0	180.0
15.7	12.5	14.3	12.8	11.6	12.2	11.6	11.6
33	25	16	15		14	15	15

1+00

172.4	175.2	177.4	177.6	177.3	178.7	178.3	178.9	179.6
19.4	16.4	14.2	14.0	14.3	12.9	13.3	12.7	12.0
33	25	21	25	14		14	15	25

0+75

Proposed
Curb outlet on left

172.0	175.3	176.6	177.2	178.5	178.5	179.1	179.7
19.6	16.3	15.0	14.4	13.1	13.1	12.5	11.9
33	25	22	14		12	15	25

0+50

175.7	177.2	177.8	177.5	179.2	179.3	180.1	180.7
15.7	14.4	13.8	14.1	12.4	12.6	11.5	10.9
25	22	14	13		15	14	25

0+25 w/ly Cushman

177.6	178.8	180.3	181.2	182.0
14.0	12.8	11.3	10.4	9.6
25	19		15	25

Pueblo Line = 00 = E Cushman

178.2	179.7	181.3	183.1	183.7
13.4	11.9	10.3	8.5	7.9
25	15		15	25

25+19.52 EC
Fluv. Rd.

159

191.58

189.99

BM. 2x2
E.C.

191.58

12 2 + 07.52 = PC. on PT = NL Solar

13 1 + 81.82 = PL. on LT = SL Solar

14 1 + 50

191.58

10.4	181.4	9.4	185.1	7.0	187.6	6.0	188.1	5.0	188.8
25		25		25		25		25	
10.3	181.3	9.3	185.3	7.6	184.0	6.2	184.9	5.2	185.3
14		14		14		14		14	
9.7	181.9	6.5	185.4	6.5	185.4	6.5	185.4	6.5	185.4
15		15		15		15		15	
9.5	182.1	6.7	184.9	6.7	184.9	6.7	184.9	6.7	184.9
22		22		22		22		22	
10.4	181.2	6.8	185.3	6.8	185.3	6.8	185.3	6.8	185.3
25		25		25		25		25	

191.58

X sec of Brownell St.

Indexed
C.S.K.

2+00

+50

1+00

0+50 = PC

0+25 = w/ly Cushman

00 = Reel Line

28+13.53 AC

Elev. Rd
N.L. Brownell

646 207.94

20148 BM
2x2 Hub198.8
 $\frac{9.1}{25}$ 197.6
 $\frac{8.3}{25}$ 200.1
 $\frac{7.8}{25}$ 197.6
 $\frac{8.2}{24}$ 200.8
 $\frac{7.1}{21}$ 200.4
 $\frac{7.5}{25}$ 201.0
 $\frac{6.9}{26}$ 201.1
 $\frac{6.8}{25}$ 201.5
 $\frac{5.4}{25}$ 202.2
 $\frac{5.7}{25}$ 202.5
 $\frac{5.4}{24}$ 202.1
 $\frac{5.8}{23}$ 203.1
 $\frac{4.8}{24}$ 202.6
 $\frac{5.8}{26}$ 203.1
 $\frac{4.8}{27}$ 203.6
 $\frac{4.6}{25}$ 203.1
 $\frac{4.8}{25}$ 203.5
 $\frac{4.4}{25}$ 203.1
 $\frac{4.8}{24}$ 204.3
 $\frac{3.6}{26}$ 204.2
 $\frac{5.4}{26}$ 204.8
 $\frac{4.1}{27}$ 205.2
 $\frac{4.7}{24}$ 202.7
 $\frac{5.2}{24}$ 204.7
 $\frac{3.2}{25}$ 205.7
 $\frac{4.7}{24}$ 203.4
 $\frac{4.5}{24}$ 204.9
 $\frac{4.0}{26}$ 205.9
 $\frac{4.0}{25}$

207.94

2 + 25.62 PC ON N = RT

2 + 57.50 PC ON LT = S

2 + 40

207.94

9.2 35	198.7	8.7 14	199.2	8.6 15	199.3	8.1 14	199.5
8.3 15	199.6	8.2 15	199.7	8.2 15	199.7	8.5 17	199.7
8.8 14	199.1	8.2 14	199.1	8.2 14	199.1	8.5 17	199.4
7.7 15	200.2	7.6 16	200.3	7.6 16	200.3	7.4 16	200.5
7.5 16	199.8	7.4 17	199.9	7.4 17	199.9	7.7 16	200.2
7.3 15	200.4	7.3 15	200.5	7.3 15	200.5	7.2 17	200.7
	200.6	7.3 15	200.6	7.3 15	200.6	7.2 15	200.7

207.94

X sec of Cushman
Solar to Everview

indexed
c.s.k.

LF = W

⊕ = Pueblo Line

22

1750 = P.C.

201.4	201.2	200.6	201.1	201.3	201.9
9.4	9.6	10.2	9.7	9.5	
<u>25</u>	<u>21</u>	<u>30</u>	<u>17</u>	<u>2</u>	8.9

1725

198.9	198.2	198.8	199.3	199.8
11.9	12.6	12.0	11.5	11.0
<u>25</u>	<u>30</u>	<u>12</u>	<u>2</u>	

T.P.

12.22 210.77 0.32 198.55

210.77

0+75

194.1	193.4	194.1	194.7	195.5
4.8	5.5	4.8	4.2	
<u>25</u>	<u>21</u>	<u>12</u>	<u>2</u>	

0+25

188.4	187.7	188.8	189.2	190.0
10.5	11.2	10.1	9.7	
<u>25</u>	<u>22</u>	<u>12</u>	<u>4</u>	8.9

25' N of Solar = P.C. = 0+00

185.1	184.6	185.9	186.2	186.9
13.8	14.3	13.0	12.7	
<u>25</u>	<u>22</u>	<u>12</u>	<u>2</u>	12.0

25+19.52 EF
Elev. Rd.

8.88 198.87

189.99

⊕ 2x2
Hub

198.87

1 1475 = 51/2 Even View Rd

2 1450 PC.

3 1400

4 TP. 6.78 216.97 0.58 210.19

5 0450

6 25' N of Brownell = PC. = 0400

210.77

25	211.8	25	211.9	25	212.0
25	211.7	25	211.3	25	211.8
25	211.0	25	210.7	25	211.1
25	210.8	25	210.9	25	211.1
25	210.6	25	210.8	25	210.8

25	209.3	25	209.1	25	209.4
25	207.0	25	206.7	25	207.0
25	207.1	25	207.1	25	207.1
25	207.3	25	207.9	25	207.3

214.97

210.77

17 = West

Q = Pueblo
Line Cushman 24

1 2+25 = NE Elevation

2 2+00 E Elevation

21697

$\frac{4}{2} 212.5$	$\frac{4}{2} 212.1$	$\frac{6}{3} 210.5$
$\frac{5}{2} 212.0$	$\frac{5}{2} 211.8$	$\frac{7}{4} 207.4$
$\frac{5}{2} 212.0$	$\frac{5}{2} 211.2$	$\frac{8}{4} 208.9$
$\frac{5}{2} 211.7$		$\frac{8}{4} 216.97$

T.P. 12.83 129.29 0.34 116.46

2+00

1+79.49 P.O.C. ON RT B.C. ON LT. $\Delta 82^{\circ} 16' 30''$

1+45

1+19.66 $\Delta = 54^{\circ} 51'$

0+59.83 $\Delta = 27^{\circ} 25' 20''$

NOTE 1 \neq STA.

0+00 = 10+02.22 Elev. Rd X

10+02.22
 \neq Hub Elev. Rd 12.85 116.80 103.95

B.M.

116.80

112.7	115.3	115.0	114.6	115.0	115.3	115.4
$\frac{4.1}{25}$	$\frac{1.5}{22}$	$\frac{1.0}{11}$	$\frac{2.2}{10}$	1.8	$\frac{1.5}{22}$	$\frac{1.4}{22}$
106.9	109.6	110.9	110.0	110.7	112.1	112.6
$\frac{9.9}{25}$	$\frac{7.2}{21}$	$\frac{8.4}{10}$	$\frac{6.8}{9}$	6.1	$\frac{4.7}{4}$	$\frac{4.2}{25}$
106.9	105.0	104.6	106.0	110.1	109.7	110.2
$\frac{12.9}{25}$	$\frac{11.0}{14}$	$\frac{12.2}{12}$	10.8	$\frac{6.7}{6}$	$\frac{2.1}{22}$	$\frac{6.6}{25}$
98.9	101.3	106.6	108.3	108.5	109.2	
$\frac{17.9}{25}$	$\frac{15.5}{10}$	10.2	$\frac{8.1}{7}$	$\frac{8.3}{21}$	$\frac{7.6}{25}$	
98.0	99.4	105.3	107.0	107.2	107.8	
$\frac{18.8}{25}$	$\frac{17.4}{14}$	11.5	$\frac{9.8}{6}$	$\frac{9.6}{22}$	$\frac{9.0}{25}$	

see p 9 for sec.

1761.22 7° 23' 33"

CURVE ON EILSWORTH
Δ = 43° 30' 30"
EP = 625
PL = 474.59

1707.48 4° 45' 42"

045374 PRC ON LT def. 2° 27' 51" RT

3+92.70 = Δ 180° = 0+00 for EILSWORTH XSEC

± HUB
T.P. 2+92.70 714 147.09 179 139.97

3+57.13 Δ = 160° 57'

NOTE! ± STA.

141.76

142.6	142.4	142.0	142.1	141.4	141.9	141.2
4.5	4.7	5.1	5.0	5.7	5.2	5.9
14	15	14	14	12	13	15
142.9	142.6	142.2	142.0	141.3	141.7	141.3
4.4	4.5	4.9	5.1	5.8	5.4	5.7
14	15	15	15	11	12	13
143.0	142.8	142.0	141.7	140.8	141.3	140.7
4.1	4.3	4.7	5.4	6.0	5.8	6.2
14	16	17	14	12	13	15
142.7	141.9	140.3	138.7	139.3	139.1	139.5
4.2	5.2	6.8	8.4	7.8	8.0	8.0
14	15	14	12	13	15	15
138.7	138.3	137.7	136.8	137.1	137.1	137.4
4.1	4.5	4.1	5.0	4.7	4.7	4.4
14	15	14	12	13	13	15
147.09						
141.76						

Ellsworth Pt

0.77 144.63 144.66 = T.P. rock P. 1 V

Center of M Curve on Ellsworth + Elev. Rd.
NOT graded back enough

143.6	142.9	142.0	141.8	141.8
1.8	2.5	3.4	3.6	4.5
25	15	10		

5+61.79 = P.C.C. on Elev. Rd = 2579 15+92.49
SC

see p 11 for loc.

5+18.19 = def. 9°59'00" Δ = 39°58'
EA = 125
EL = 8720
T = 45.45

136.6	136.6	136.8	135.7	136.0	136.2	138.0
8.8	8.8	8.6	8.7	9.4	9.2	7.4
25	15		12	12	22	25

4+74.59 21°45'15 PCC on RT = SL

140.6	140.0	138.8	138.0	138.5	138.4
4.8	5.2	6.5	7.2	6.9	7.0
25	15		16	25	

4+29.91 19°42'48"

141.6	141.5	140.8	139.8	139.2	139.2	139.3	137.5
3.8	3.9	4.6	5.6	6.2	5.8	5.1	7.9
25	21	17		10	11	20	25

3+95.17 PRC on LT = N def. 18°06'49"

141.3	140.9	140.3	140.3	139.2	139.6	139.2	138.0
4.1	4.2	5.1	5.1	6.2	5.5	5.2	7.4
25	10	15		12	15	12	11

145.40

145.40

CONT. Xsec of Monitor Rd.
from p26

LT $\frac{1}{2}$ RT MONITOR 30

510.63
460.87
50.26

T.P. 12.63 161.47 0.21 148.84

4+60.37 10° 08' 54"

$\Delta = 81^\circ 11' 30''$ LT.
EP = 425.47
ET = 364.78
EA = 602.20

4+46 $\frac{1}{2}$ cont. apron 7' wide

4+10.10 6° 45' 56"

3+59.84 3° 22' 58"

3+09.57 = P.P.C. see p26 for Xsec.

NOTE! $\frac{1}{2}$ STA.

check to spike in Pole
Ely. Cor. Monitor
Ely. Sta. F.B. 1128-3

BM. 3+92.70 9.08 149.05
 $\frac{1}{2}$ Hub
P 27

0.99 148.06
139.97

148.23
0.17
Pole has
settled

149.05

148.9	147.9	148.3	147.8	148.2	148.4
$\frac{0}{2}$	$\frac{1}{2}$	$\frac{0}{2}$	$\frac{1}{2}$	$\frac{0}{2}$	$\frac{1}{2}$
146.23	146.4	146.7	146.3	146.7	146.5
$\frac{0}{2}$	$\frac{1}{2}$	$\frac{0}{2}$	$\frac{1}{2}$	$\frac{0}{2}$	$\frac{1}{2}$
144.1	143.8	143.5	143.7	143.7	143.5
$\frac{0}{2}$	$\frac{1}{2}$	$\frac{0}{2}$	$\frac{1}{2}$	$\frac{0}{2}$	$\frac{1}{2}$
139.2	139.2	138.7	138.9	138.8	137.9
$\frac{0}{2}$	$\frac{1}{2}$	$\frac{0}{2}$	$\frac{1}{2}$	$\frac{0}{2}$	$\frac{1}{2}$

T.P. 9.78 182.90 0.47 173.12

6+01.43 23°40'46"

6+11.17 20°17'48"

5+89.09 POC.
RRC ON RT. = EL. for beg. of
180°48'45"
Curve on
CROWN ST.
see p. 37

T.P. on Rock 12.72 173.59 0.60 160.87

5+00.90 16°54'50"

5+10.63 13°51'32"

161.47

L7

⊕

RT

MONITOR

31

171.1

170.9

170.2

170.8

170.3

169.5

$\frac{2.5}{2.5}$

$\frac{2.7}{2.5}$

$\frac{2.5}{2.4}$

2.8

$\frac{2.2}{2.4}$

$\frac{2.1}{2.5}$

164.7

164.5

164.1

164.6

164.3

164.9

$\frac{2.9}{2.5}$

$\frac{2.1}{2.5}$

$\frac{2.5}{2.4}$

9.0

$\frac{2.2}{2.1}$

$\frac{2.7}{2.5}$

162.1

162.1

161.6

162.1

162.1

162.9

162.3

$\frac{11.5}{2.5}$

$\frac{11.5}{2.5}$

$\frac{12.0}{2.4}$

11.5

$\frac{11.5}{2.4}$

$\frac{10.7}{2.5}$

$\frac{11.1}{2.6}$

159.9

159.3

158.7

159.1

159.1

159.5

159.5

$\frac{2.1}{2.5}$

$\frac{2.2}{2.5}$

$\frac{2.8}{2.4}$

2.4

$\frac{2.4}{2.4}$

$\frac{2.5}{2.0}$

$\frac{2.8}{2.0}$

154.4

154.1

153.4

154.0

153.6

153.9

154.3

$\frac{7.1}{2.5}$

$\frac{7.4}{2.4}$

$\frac{8.1}{2.3}$

7.5

$\frac{7.9}{2.4}$

$\frac{7.6}{2.5}$

$\frac{7.2}{2.4}$

161.47

8+13.23

30° 39' 40"

7+86

7+01.96

30° 26' 42"

7+25

7+11.70

27° 03' 44"

6+81

182.90

9.5	173.4	6.0	176.3	4.7	178.2	4.4	178.7	4.4	178.4	4.4	179.0	3.8	179.07	3.7	179.2
10.2	172.4	6.6	175.9	4.7	177.8	4.0	178.6	4.5	178.6	4.9	179.0	3.8	179.07	3.7	179.2
9.7	173.2	6.5	176.4	4.8	178.1	4.7	179.2	4.6	179.2	4.6	179.3	3.8	179.30	3.7	179.2
10.5	172.4	7.1	175.8	4.8	177.5	4.7	178.9	4.6	178.9	4.9	179.0	3.8	179.07	3.7	179.2
10.1	172.8	6.7	176.2	4.8	178.0	4.7	179.1	4.6	179.1	4.9	179.0	3.8	179.07	3.7	179.2
10.0	172.9	6.5	176.4	4.8	178.0	4.7	179.1	4.6	179.1	4.9	179.0	3.8	179.07	3.7	179.2

182.90

old walk

old walk

old walk

10+1300 SL ONSTAD

9+8806 PC SL ONSTAD

9+70 Prop. Curve center

9+50

9+1270 EC 40° 35' 45"

8+62.50 37° 12' 38"

18290

24

25

27

MONITOR 33

176.2
57
25

196.6
57
25

176.5
57
25

175.1
28
25

175.4
25
15

175.7
25
16

175.4
25
16

175.8
25
17

175.9
25
15

172.1
10.8
55

173.3
9.1
25

174.7
8.2
26

174.9
8.0
25

175.8
7.0

172.1
10.8
25

174.6
9.2
20

175.0
7.9
22

174.7
8.2
21

175.8
7.7

175.0
7.9
15

175.4
7.5
16

175.6
7.2
25

172.9
10.0
25

174.9
8.0
21

175.4
7.5
22

175.1
7.8
21

175.8
7.1

175.5
7.4
15

176.0
6.9
16

176.3
6.2
25

175.7
7.2
25

176.7
6.4
22

176.9
6.0
24

176.5
6.4
23

177.2
5.7

176.8
6.1
14

177.2
5.7
15

177.2
5.7
25

18290

11+91.70 5°09'30"

11+39.88 2°24'45"

A = 20°38' RT
EP = 575.62
T = 104.78
SL = 207.29

T.P. 11.40 192.82 1.48 181.22

10+88.00 BC RT.

10+63.00 N/A

10+38.06 I ONSTAD

18290

1882	186.9	187.1	186.8	187.6	187.4	187.7	188.0
4.4	5.9	5.7	6.0	5.2	5.2	5.1	4.8
25	23	24	23	25	25	26	25

186.2	183.7	183.7	184.3	184.3	184.8	184.7
6.6	9.1	9.1	8.5	8.5	8.0	8.1
25	21	23	25	25	26	25

182.6	180.1	180.3	179.9	180.5	180.4	180.9	181.1
2.0	2.0	2.4	2.0	2.4	2.4	2.0	1.8
25	25	25	25	25	25	26	25

177.8	178.4	179.1	179.3	179.2
5.1	4.5	3.8	4.6	5.7
25	25	25	25	25

177.5	177.6	177.8	178.1	178.5
5.4	5.2	5.1	4.8	4.4
25	25	25	25	25

18290

11.91 192.25 192.36 spike in Pole Sine Cor. ONTAD BK 1129-3 Elev. Rd

check to B.M. \pm 2 x 2 Hub 2.67 201.49 201.48 = \pm 579 28+13.53 E.C. Hub on Elev. Rd + Nly Brownell St
0.01

T.P. 4.53 204.16 0.87 199.63

3 north B.M. in pole 2.10 198.35 B.M.
Sly Cor. MONITOR
EVERVIEW

12 14 + 70.58 = P.C. = 50' S \pm EVERVIEW RD.

T. + 50

13 14

200.45

4.9	4.3	4.7	4.0	4.3	4.0	4.3
25	12	13	14	15	10	25
195.4	195.9	195.7	196.3	196.0	196.5	196.5
5.1	4.6	4.9	4.2	4.5	4.0	4.0
25	12	13	14	15	10	25
195.3	195.7	196.3	195.7	196.2	196.5	196.5
5.2	4.8	4.2	4.5	4.0	4.0	4.0
25	13	14	15	10	25	25

200.45

X sec of Crown St.
MONITOR to Elev. Rd.

Indexed
C.S.R.

1+25 4° 12.78'

0+75 2° 31.67' RT

0+25 2° 50.56' RT

P.C.
0+34.73 = 0+00 on Sly Crown St.

0+18.36

$\Delta = 84^{\circ} 10' 25''$
SL P = 25
" L = 34.73

5+89.09 on Ely MONITOR = 0+00 = P.R.C.

Note! SL Sta.

1297 173.84

160.87 p 31

on T.P. Rock

164.0	163.5	163.2	163.5	162.9	163.2	163.2	162.5
9.8	10.3	10.4	10.2	10.9	10.4	10.4	11.3
50	21	20	25	14	13	5	
165.4	165.0	164.6	164.9	164.3	164.7	164.1	162.6
8.4	8.8	9.3	8.9	9.5	9.1	9.7	11.2
50	41	40	25	14	14	4	
167.3	166.9	166.3	166.1	165.4	165.7	165.1	163.6
6.4	6.9	7.5	7.7	8.4	8.1	8.7	10.2
50	41	40	25	17	14	6	
168.3	167.9	167.2	166.8	165.6	165.8	165.4	164.2
5.5	5.9	6.4	7.0	8.2	8.0	8.4	9.6
50	25	44	25	15	13	4	
168.3	166.5	164.4	164.8	164.4	164.8	164.5	164.5
5.5	7.3	9.4	9.0	9.4	9.0	9.0	9.3
50	25	10	9	9	9	9	

\$ 37
Crown St

p 31 for this sec.

173.84
3

check to BM. C.T. in Apron 6.60 156.87 156.88
 3rd Cor Crown + Elev Rd p.13
 0.01

Center Curve on Nly Cor Crown + Elev

0.8
N.L. 1.0
N curb

3 + 13.86 = EC. see p.13 for this section
 19 + 44.32 on Elev. Rd.

2 + 89.24 Center Curve on S.L.

158.6	158.6	158.1	157.4	158.0	158.1	159.7
4.9	4.9	5.2	6.1	5.4	5.4	5.8
50	40	25	15	14	10	8
156.5	155.7	156.6	156.7	156.7	156.7	156.7

2 + 64.66 P.C.C. 8°55'18"

12 T.P. 2.63 163.47 13.00 160.84

163.47

T. 2 + 25 7°35'00"

161.0	161.0	159.3	159.7	160.3
12.8	13.7	14.5	14.1	13.5
50	25	13	12	10.5
161.0	160.1	159.3	159.7	160.3

11 14N 5°53'89"

162.5	162.0	162.0	161.4	161.8	161.6
11.3	11.8	11.6	12.4	12.0	12.2
50	46	25	13	3	12.2
162.5	162.0	162.0	161.4	161.8	161.6

173.84

173.84

T.P. 12.64 121.67 0.36 109.03

1 3+54.77 12°46'30"

1 2+99.03 8°31'04"

L T.P. 12.81 109.39 0.13 96.58

A = 59°37'30"

EP = 375

T = 214.88

EL = 390.24

T. 2+43.28 4°18'32" RT

96.71

1 1+87.53 BC. RT

107.8	107.7	107.5	108.1
<u>1.6</u>	<u>1.7</u>	<u>1.9</u>	<u>1.6</u>
25	17	25	25

99.4	99.7	99.5	99.6
<u>10.0</u>	<u>9.9</u>	<u>9.8</u>	<u>9.8</u>
25	14	25	25

109.39

91.7	87.3	86.9	86.5	86.7	86.8	87.4	87.4
<u>5.0</u>	<u>9.4</u>	<u>9.8</u>	<u>10.2</u>	<u>10.0</u>	<u>9.9</u>	<u>9.3</u>	<u>9.0</u>
25	21	11	9	100	15	16	25
93.1	93.1	92.4	92.9	92.6	93.2	93.2	
<u>6.6</u>	<u>6.6</u>	<u>1.2</u>	<u>4.8</u>	<u>4.1</u>	<u>5.5</u>	<u>4.5</u>	
5	16	5	8	5	7	5	

96.71

4+96

T.P. 12.87 146.95 0.54 133.48

4+66.27 21° 17' 40"

4+51

T.P. 12.52 134.02 0.17 121.50

T 4+10.52 17° 02' 08"

3+85

121.67

$\frac{92}{55} \overline{)137.2}$

$\frac{10.1}{15} \overline{)136.3}$

$\frac{10.6}{12} \overline{)136.3}$

$\frac{10.7}{12} \overline{)135.8}$

$\frac{10.5}{12} \overline{)135.9}$

$\frac{10.7}{12} \overline{)135.7}$

$\frac{9.7}{14} \overline{)136.7}$

$\frac{9.8}{23} \overline{)136.6}$

$\frac{9.2}{25} \overline{)137.2}$

$\frac{5.2}{25} \overline{)130.7}$

$\frac{5.2}{25} \overline{)130.5}$

$\frac{5.2}{25} \overline{)130.1}$

$\frac{5.2}{25} \overline{)130.7}$

$\frac{5.2}{25} \overline{)130.8}$

$\frac{5.1}{25} \overline{)129.9}$

$\frac{5.1}{25} \overline{)131.4}$

$\frac{5.1}{25} \overline{)130.9}$

$\frac{6.2}{14} \overline{)127.6}$

$\frac{6.1}{16} \overline{)127.9}$

$\frac{6.1}{14} \overline{)127.3}$

$\frac{6.2}{14} \overline{)127.8}$

$\frac{6.6}{12} \overline{)127.4}$

$\frac{6.0}{15} \overline{)128.0}$

$\frac{6.6}{25} \overline{)127.7}$

$\frac{6.4}{27} \overline{)117.3}$

$\frac{6.3}{23} \overline{)118.4}$

$\frac{6.4}{10} \overline{)118.3}$

$\frac{6.4}{12} \overline{)117.3}$

$\frac{6.1}{10} \overline{)118.6}$

$\frac{6.4}{25} \overline{)119.3}$

$\frac{9.2}{25} \overline{)112.5}$

$\frac{8.6}{10} \overline{)113.1}$

$\frac{8.6}{10} \overline{)113.1}$

$\frac{9.6}{15} \overline{)112.1}$

$\frac{8.6}{10} \overline{)113.1}$

$\frac{8.3}{25} \overline{)113.4}$

121.67

7+27.12 24°21'27"

A = 81°11'30"
Σ P = 175.67
Σ I = 150.54
Σ L = 248.93

6+77.34 16°14'18"

T.P 13.06 158.96 0.45 145.90

6+27.50 8°07'09" LT

T 5+77.77 PRC 290°48'45"

5+22.02 25°33'12"

146.35

148.0	147.9	147.4	147.9	147.8	146.9	146.8	147.0
7.6	7.5	8.0	7.6	7.9	7.7	8.2	7.7
151.4	151.5	151.0	151.4	151.1	151.3	150.8	151.0
146.1	145.8	145.2	145.5	144.8	145.2	144.7	143.1
143.5	143.4	143.0	143.2	142.9	143.3	143.1	142.6
141.2	140.0	139.2	139.2	139.0	139.8	139.6	140.2
146.35			146.35				

9+02.10 = P.C.

T.P. 12.01 183.26 0.22 171.25

8+50

8+26.70 EC. $40^{\circ}35'40''$

T.P. 12.88 171.47 0.37 158.59

7+76.92 $32^{\circ}28'30''$

158.96

LT.

#

PT.

Everview

43

172.9	172.2	172.4	172.1	172.9	172.6	173.3	173.4
10.4	11.1	10.9	11.2	10.4	10.7	10.0	9.9
25	22	13	12	16	16	17	25

183.26

168.7	167.1	167.5	167.0	167.5	167.1	167.6	167.6
4.8	4.4	4.0	4.5	4.0	4.4	4.9	4.9
25	24	20	12	10	15	17	25

164.1	164.7	164.1	164.4	163.9	164.5
7.4	6.8	7.4	7.6	7.6	7.0
25	15	20	15	15	25

171.47

157.0	157.1	156.5	157.4	157.2	157.3
1.0	1.9	1.4	1.6	1.8	1.7
25	15	14	16	15	25

158.96

13+49.42

13+24.42 PC ON W.

12+99.42 E.C. 10'19"

12+49.86 8°35'50"

12+00.21 6°52'40"

11+50.07 5°09'30"

T.P. 2.73 185.65 0.34 182.92

SET BM. BR IN CORN. PORCH E. SIDE
OF HOUSE ON NLY COR. OF
EVERVIEW 562 177.64

183.26

250	177.7	250	177.4	250	179.2	250	182.7	250	181.2	250	181.4	250	182.8	250	182.7	250	181.2	250	181.4	250	182.8	250	182.7		
5	178.1	5	178.7	5	180.0	5	182.2	5	182.1	5	182.5	5	183.1	5	182.1	5	182.1	5	183.0	5	182.4	5	182.8	5	182.7
5	179.1	5	178.6	5	180.3	5	182.3	5	182.2	5	182.9	5	183.1	5	182.2	5	182.2	5	183.0	5	182.4	5	182.8	5	182.7
5	179.2	5	178.9	5	179.2	5	179.9	5	181.0	5	180.4	5	181.3	5	181.1	5	182.2	5	182.9	5	182.4	5	182.8	5	182.7
5	178.8	5	179.5	5	178.8	5	179.4	5	179.4	5	178.8	5	179.4	5	179.4	5	181.1	5	182.9	5	182.4	5	182.8	5	182.7
5	179.4	5	178.7	5	179.4	5	179.4	5	181.0	5	180.4	5	181.3	5	179.4	5	181.1	5	182.9	5	182.4	5	182.8	5	182.7
5	179.8	5	179.1	5	179.3	5	181.3	5	183.1	5	182.5	5	183.1	5	183.1	5	183.1	5	183.0	5	182.4	5	182.8	5	182.7
5	180.0	5	179.3	5	180.0	5	181.3	5	183.1	5	182.5	5	183.1	5	183.1	5	183.1	5	183.0	5	182.4	5	182.8	5	182.7
5	179.8	5	179.3	5	180.0	5	181.3	5	183.1	5	182.5	5	183.1	5	183.1	5	183.1	5	183.0	5	182.4	5	182.8	5	182.7
5	179.8	5	179.3	5	180.0	5	181.3	5	183.1	5	182.5	5	183.1	5	183.1	5	183.1	5	183.0	5	182.4	5	182.8	5	182.7

14 + 88.69 15° PT

$\Delta = 90^\circ$
 $\Sigma P = 75$

T.P. 12.77 197.97 0.45 18520

14 + 49.42 B.C. PT

14 + 24.42 P.C. on W.

13 + 99.42 N.L. KNOX

13 + 74.42 E. KNOX

18565

25	11.0	187.0
28	11.5	186.5
14	11.3	186.7
13	11.7	186.3
11.0		187.0
14	11.5	186.5

PT 46
Everview

17	10.8	187.2
25	10.8	187.2

183.8

1.9

25

183.2

2.5

25

183.7

2.0

25

183.3

2.2

25

183.9

1.8

25

183.6

2.1

25

184.4

1.6

25

184.4

2.6

25

181.8

3.9

25

182.2

3.5

25

181.7

4.0

25

182.4

3.3

25

182.1

6.6

25

182.8

2.9

25

183.0

4.7

25

180.5

5.5

25

180.7

5.0

25

184.3

4.4

25

180.9

4.8

25

181.6

4.1

25

179.2

5.5

25

179.6

5.0

25

180.5

5.2

25

180.1

5.6

25

180.7

5.0

25

180.8

4.9

25

185.65

17 + 17.75 wly Morrison

16 + 92.75

1717.75
1567.25
150.5

+ 50

16

15 + 67.43 EC + 50 RR

15 + 27.96 30° RR

197.97

	1903	1909	1913	1915	1918	1921	1927	1929	1930	1936	1938	1949	1952	1957	1958	1959	1961	1962	1964	1966	1967	1968	1969	1971	1972
	7.2	8.1	8.5	8.8	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2
	1903	1899	1895	1901	1892	1898	1897	1901	1892	1898	1897	1899	1895	1901	1901	1903	1901	1901	1901	1901	1901	1901	1901	1901	1901
	4.2	4.6	4.7	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2	4.2
	1931	1927	1923	1915	1918	1927	1927	1927	1930	1936	1938	1949	1952	1957	1958	1959	1961	1962	1964	1966	1967	1968	1969	1971	1972
	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
	1946	1946	1942	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943	1943
	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
	1959	1957	1954	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949	1949
	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
	1966	1965	1961	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966	1966
	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
	1969	1968	1964	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967
	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
	1969	1968	1964	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967	1967
	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2

197.97

PT. 47
EVENING

19

18+50

17+92.75 PG. ON S.L.

17+67.75

T.P. 11.69 209.27 0.39 197.58

17+42.75 E MONITOR

197.97

10.95 198.32 198.32

check to B.M. & mark pole Sly E MONITOR

199.1	199.2	198.9	199.6	198.7	198.5	198.9
10.2	10.1	10.2	9.7	10.4	10.8	10.4
25	16	15	14	15	25	25
198.4	198.2	197.6	198.4	197.3	197.8	197.8
10.9	11.1	11.7	10.9	12.0	11.5	11.5
25	24	25	25	24	25	25
198.1	198.1	197.2	197.9	197.6	197.0	197.0
11.2	11.2	11.1	11.4	11.7	12.8	12.8
25	26	25	25	24	25	25
197.6	197.5	196.9	197.5	197.3	197.1	197.1
10.4	10.5	11.1	10.5	10.7	10.9	10.9
25	25	25	25	24	25	25

197.97

20+42.66 PC 54

I.P. 9.28 218.25 0.30 208.97

20+17.66

19+92.66 E Elev. Rd.

19+67.66

19+44.66 PC SV

209.27

209.2
9.1
25

LY

208.9
9.4
16

208.9
9.4
15

207.3
9.0

208.4
9.9
15

208.7
9.6
14

208.5
9.8
25

EVERVIEW 49

207.9
206.4
1.5

206.4
205.9
0.5

205.0
204.5
0.5

203.1
202.6
0.5

207.8
206.4
1.4

206.4
205.9
0.5

205.0
204.6
0.4

203.1
202.6
0.5

207.3
206.0
1.3

206.0
205.6
0.4

204.6
204.2
0.4

202.6
202.1
0.5

218.25
7

208.3
207.0
1.3

207.0
206.5
0.5

205.4
204.9
0.5

203.4
202.9
0.5

207.9
207.1
0.8

207.1
206.6
0.5

205.3
204.8
0.5

203.3
202.8
0.5

207.3
207.0
0.3

207.0
206.5
0.5

204.9
204.4
0.5

203.4
202.9
0.5

209.27

see p 24 for Cushman St

22 +69.24 P.C. on SL Everview

+30

22

+50

21

218.25

22	211.1	212.7	213.7	213.5	212.8
21	210.9	212.7	213.6	213.2	212.7
20	210.6	212.3	213.3	212.9	212.3
19	211.0	212.8	213.8	213.7	212.9
18	209.9	211.9	213.1	213.0	212.2
17	210.3	212.3	213.5	213.4	212.4
16	210.4	212.3	213.4	213.5	212.6

218.25

LT

Q

PT

EVERVIEW 50

X sec of ONSTAD ST. ^{Indexed}
C.S.K.

LT = ST

10

PT = 1

51

T.P. 0.49 185.35 12.77 184.86

1700

0+75

0+50

0+25 P.C.

Wly Elev. Rd = 0+00

25+195. EC
± Hub Elev. 198
B.M.
P.15

7.64

197.63

189.99

197.63

189.0	187.6	188.0	187.4	187.6	187.9	188.0	188.5
2.6	10.0	9.6	10.2	10.0	10.2	9.6	9.1
25	25	14	25	25	14	15	25
191.6	189.8	190.0	189.6	190.0	189.8	190.4	190.7
4.0	7.8	7.6	8.0	7.6	7.8	7.2	6.9
25	25	12	15	20	14	15	25
193.6	192.1	192.0	191.5	192.0	191.8	192.4	192.6
4.0	5.5	5.6	6.1	5.6	5.8	5.2	5.0
25	22	20	23	20	12	15	25
194.4	193.2	193.1	192.5	193.4	193.1	193.6	194.0
3.2	4.2	4.5	4.5	4.2	4.5	4.0	4.6
25	23	15	15	12	12	15	15
192.7	193.1	194.1	194.4	194.7	194.7	194.7	194.7
4.9	4.5	3.5	3.5	4.0	4.2	4.0	4.0
14	14	15	15	12	12	15	15

X sec. of Dorcas St.

Indexed
C.S.K.

LT=W

~~RT~~

RT=E

55

1+50

47.5	48.3	48.3	48.4	48.9
11.7	10.9	10.9	10.8	10.6
<u>25</u>	<u>15</u>		<u>15</u>	<u>25</u>

T.P.

1246 5918 0.80 46.52

59.18

1+00

43.0	43.5	44.1	44.1	44.5
4.6	5.0	5.2	5.2	5.0
<u>25</u>	<u>15</u>		<u>15</u>	<u>25</u>

0+71

40.9	41.0	41.4	41.8	42.3
5.4	6.0	5.9	5.4	5.0
<u>25</u>	<u>15</u>		<u>15</u>	<u>25</u>

0+46

38.8	38.9	38.4	39.2	39.6
8.2	8.9	8.1	7.9	7.7
<u>25</u>	<u>15</u>		<u>15</u>	<u>25</u>

0+00 = Sly of Overlook HTS

34.5	35.4	35.5	35.6	35.5
12.8	11.9	11.8	11.7	11.8
<u>25</u>	<u>15</u>		<u>15</u>	<u>25</u>

T.P.

0.80 47.32 13.02 46.52

47.32

0.32 59.54 59.22

T.P. Rock
see p6

T.P. 12.68 108.84 0.14 96.16

4 + 9/38 = P.C. ON E = 1 + 87.50 EVERVIEW

4 + 04.54 = P.C. ON E = 1 + 00.69 EVERVIEW. see p 39
for sections

T.P. 12.92 9630 0.25 8338

T.P. 12.40 8363 0.06 71.23

+50

	76.1	76.1	70.1	69.8	70.4	70.8	71.0
	+4.8	+4.8	1.2	1.5	0.9	0.4	0.6
	55	22	12	11	11	15	25
	69.1	67.7	64.7	63.5	63.7	63.6	63.3
	45	21	10	11	7.6	7.7	8.0

3+00

T.P. 12.38 71.29 0.27 58.91

71.29

+50

	60.6	58.5	57.7	57.3	58.3
	+1.4	0.7	1.9	1.9	0.9
	45	10	15	15	25
	54.2	53.5	52.7	52.6	52.0
	5.0	5.7	5.7	5.6	7.2
	25	8	15	15	25

2+00

59.8

T.P. 12.63 133.93 0.12 121.30

7+47.95 = B.C. on E.L. line of Curve $\Delta = 139^{\circ}33'$
P.P. = 25.01

7+50

7+40

7+00

T.P. 12.88 121.42 0.30 108.54

6+50

6+00

5+50

108.84

5.2	116.2
5.4	116.8
5.1	119.3
6.2	120.2

11.3	110.1	114.1
11.3	110.1	115.2
10.0	111.4	116.4
9.7	112.3	117.2
8.6	113.0	118.3

13.6	91.2	103.9
15.7	93.1	103.4
16.3	92.5	104.8
15.9	92.9	105.9
15.4	93.4	106.3

1.3	120.1
0.7	120.7
0.7	120.7

118.7	118.7
118.7	118.7
118.7	118.7
118.7	118.7
118.7	118.7

121.42	108.84
108.84	108.84
108.84	108.84
108.84	108.84
108.84	108.84

10 + 72 + 48 22° 47' 10"

10 + 44.66 11° 23' 35" LT.

10 + 12.83 B.C. RT

T.P. 12.76 159.22 0.35 146.26

9 + 50

9 + 00

T.P. 13.03 146.81 0.15 133.78

8 + 50

8 + 00

133.93

$$\Delta = 68^\circ 21' 30''$$

$$\begin{aligned} \frac{1}{2} P &= 75 \\ T &= 50.93 \\ \frac{1}{2} L &= 89.48 \end{aligned}$$

150.0	150.3	150.9	158.1	157.9	157.0	157.0
9.2	8.9	8.3	4.1	4.3	5.0	4.4
6.5	2.5	7.6	8	4.3	1.7	1.8
140.8	143.9	148.0	151.1	151.1	151.8	152.2
18.4	15.2	11.2	8.1	8.1	7.4	7.0
6.5	2.5	7	8.1	1.8	1.9	2.5
134.4	136.3	139.4	142.2	142.9	143.3	143.5
12.2	10.5	7.4	4.2	4.9	4.5	4.6
6.5	2.5	6	4.2	1.7	1.8	2.6
127.8	128.3	130.0	135.4	136.0	136.4	136.6
19.0	18.5	14.8	11.4	10.8	10.4	10.2
6.0	2.5	9	11.4	1.7	1.8	2.5
123.4	124.0	125.1	126.3	129.0	130.0	129.9
10.5	9.9	8.8	7.6	4.9	3.9	4.0
6.5	2.5	1.9	5	4.6	1.9	2.5
119.0	121.4	122.7	123.7	123.8	124.3	124.6
14.9	12.5	11.4	10.2	10.2	9.6	9.6
2.5	2.5	2	2	10.2	1.7	2.5
146.81						
133.93						

133.93

check to B.M.B.P. See p 45 336 177.66 177.64

12+54.8^m Wly Evon. CW Rd.

12+29.8^m P.C.

T.P. 9.63 181.02 0.22 171.39

12+00

11+50

11+02.31 EC. 34° 10' 45"

T.P. 12.65 171.61 0.26 158.96

159.22

173.8	173.6	172.8	172.9	171.9	172.3	172.8
7.2	7.4	8.2	8.1	9.1	8.7	9.2
25	15	14		15	16	25
5.5	5.5	5.7	6.0	7.1	7.2	7.5
175.5	175.5	175.3	175.0	173.9	173.8	

170.7	170.4	169.7	170.1	168.9	169.4	169.2
0.9	1.2	1.9	1.5	2.7	1.5	2.4
25	15	14	15	17	17	25
165.5	165.5	165.0	165.1	163.7	164.3	164.2
5.1	6.1	6.6	6.5	7.9	7.6	7.4
25	15	14	15	14	15	25
161.4	161.4	160.7	160.6	159.2	159.6	159.4
10.2	10.2	10.9	11.0	12.4	12.0	12.2
25	15	14	14	14	15	25
170.7	170.4	169.7	170.1	168.9	169.4	169.2
181.02						

171.61

DIRECTIONS FOR USE OF TABLES

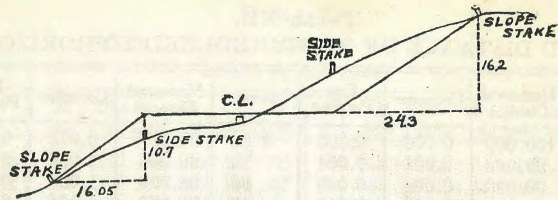
Distance of shore from side of shoals
case for any other roadway, show 1/2 to
I found it was, but the table is not
made is found by the bookkeeper, and
the column and the row. The number of

IMPROVED TABLES

AND

INFORMATION

To find length and lateral for curve of
any other degree, divide by 3.14159, and
the result will be the length of the curve.
Degrees of curve will be given by
dividing length of curve by 3.14159, and
the result will be the degrees of curve.
The diameter of a circle is found by
dividing the circumference by 3.14159, and
the result will be the diameter.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

110 0222
 945 275
 749 22
 183.53
 49.47

1540

15-D

14 + 63.44

13,44

636

708