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CITY OF SAN DIEGO,  
CALIFORNIA.

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- No. 380 LEVEL BOOK. Left and Right Hand Page  
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to the inch, Center Line Red.
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**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
IRVING PARK STATION  
CHICAGO, ILL.

Xsec Hancock St.  
Hortensia to Arpudria

50' wide  
10 curbs

B.P. BR cb  
W 418 1.04 28.77 27.73

T.P. 9.71 27.81 10.47 18.10

N14 Hortensia 500

I 11.8 16.0

cb 11.6 16.2

c 12.1 15.2

cb 12.1 15.2

W 12.2 15.6

0725

W 12.5 15.3

cb 11.5 16.3

c 11.0 16.8

cb 10.2 17.6

E 10.3 17.5

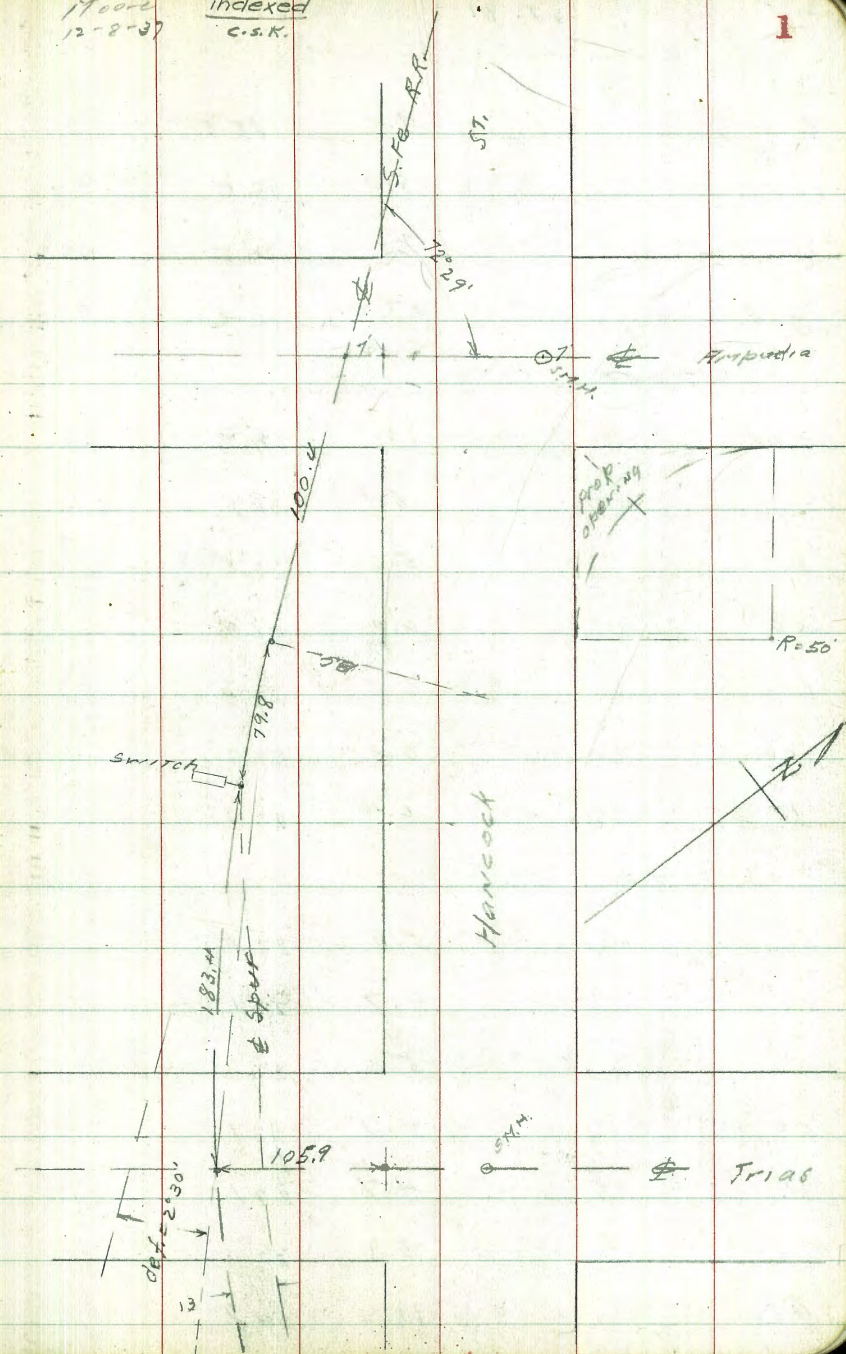
0750 ?

E 8.4 19.4

cb 8.3 19.5

73 9.1 18.7

Moore  
12-2-37  
indexed  
C.S.K.



27.81

C		9.0	18.5
cb		8.0	19.5
W		7.3	20.5
+8		17.2	10.6
	0+80		
-10		16.1	11.2
-4		6.1	21.7
W		5.0	22.8
cb		6.0	21.8
C		6.5	21.3
cb		6.3	21.5
E		6.4	21.4
	1+0		
E		5.0	22.8
cb		4.7	23.1
C		5.3	22.5
cb		4.7	23.1
W		4.7	23.1
+4		5.3	22.5
+10		18.2	9.6

27.81

	1+50		
-6		18.4	9.4
W		4.2	23.6
cb		3.4	24.2
C		3.8	24.0
cb		3.1	24.7
E		3.5	24.3
	2+0		
E		2.3	25.5
cb		3.2	24.6
C		4.2	23.6
cb		5.0	22.8
W		5.6	22.2
	+10	18.7	9.1
	2+50		
-25		18.9	8.9
-8		5.9	24.9
W		5.6	22.2
cb		4.4	23.2
C		3.6	24.2

27.81

cb 2.4 25.4

E 1.3 26.5

3 + 0 = S/W TRIAS = 50' WIDE

E 1.2 26.6

cb 2.3 25.5

C 2.9 24.9

cb 4.6 23.2

W 5.5 22.3

+10 7.0 20.5

E TRIAS

W 5.8 22.0

cb 4.7 23.1

C S/W H RIM 3.34 24.42

cb 1.9 25.9

E 1.5 26.3

N/W TRIAS = 0 + 0

E 1 2.0 25.8

cb 2.7 25.1

C 4.0 23.8

cb 5.5 23.3

27.81

3

W 7.0 20.8

+5 7.7 20.1

0 + 50

-10 9.4 18.4

W 8.6 19.2

cb 7.5 20.3

C 5.7 22.1

cb 4.6 23.2

E 2.8 25.0

T.P. 0.08 23.57 4.32 23.49 Rock

1 + 0

W 0.1 23.4

cb 1.3 22.3

C 2.8 20.8

cb 4.4 18.2

W 5.4 18.2

+10 6.7 16.9

23.57

14.30

4

1+50

-15		10.5	13.1
W		9.2	14.4
cb		7.6	16.0
C		6.0	12.6
cb		4.7	18.9
E		3.0	20.6
	2+0		
E		7.3	16.3
cb		8.7	14.9
C		10.7	12.2
cb		13.4	10.3
W		14.9	8.2
+15		18.0	5.6

cb		7.0	8.3
C		4.6	9.7
cb		1.7	12.6
E		0.2	14.1

3+0 = 5/4 ampudia

E		0.4	13.9
+7		2.2	12.1
cb		4.1	10.2
C		5.9	8.4
W 1/2		7.2	7.1
cb		8.5	5.8
W		9.0	5.3

T.P.	0.37	14.30	9.64	13.93
------	------	-------	------	-------

2+50

-15		9.5	4.5
W		8.6	5.7

X sec Ripudia  
Moore to Hancock

50 wide  
10' curbs  
7.5' /ft

Indexed  
C.S.K.

31.24

5

					cb		5.2	26.0	
T.P. rock ps	775	31.24		23.49	1/4		5.7	25.5	
					0		5.6	25.6	
	Wly Moore = 0+0				1/4		6.2	25.0	
S	TOP curb		3.21	28.03	cb		6.2	25.0	
									Please check to profile
N	" "		3.19	28.03	S		10.8	20.4	
	2+00 wly end curb & cent. sidewalk				+10		10.4	20.8	
N	TOP curb		4.72	26.43		2+75			
S	" "		4.72	26.43	-15		14.3	16.9	
	2+25				S		12.3	18.9	
J			6.6	24.8	cb		10.0	21.2	
cb			5.6	25.6	1/4		8.7	22.5	
1/4			5.2	26.0	0		7.4	23.8	
0			4.1	27.1	1/4		7.7	23.5	
1/4			4.9	26.3	cb		8.0	23.2	
cb			5.2	26.0	N		14.1	17.1	
N			5.8	25.4	+15		18.4	12.8	
	2+50								
- 10			11.7	19.5	T.P.	0.73	19.23	12.74	18.50
N			9.6	21.6					

19.23

2+87

-15	8.3	10.9
N	4.8	14.4
cb	0.0	19.2
+2	+2.0	21.2
1/4	+2.0	21.2
C	1.1	18.1
1/4	0.0	19.2
cb	1.1	18.1
S	2.5	16.7
+15	3.0	16.2

E of proposed 50' R Curve on proposed opening

S	3.0	16.2
cb	3.7	16.0

19.23

3+00 = Fly Hancock

50' wide  
15' curb  
75' / 10

6

S	5.4	13.8
cb	4.6	14.6
1/4	4.7	14.5
C	6.9	12.8
1/4	7.6	11.6
cb	8.4	10.5
N	10.1	9.1
+15	12.0	7.2
E CURB		
-15	14.3	4.9
N	11.1	8.1
cb	9.6	9.6
1/4	9.0	10.2
C	8.8	10.4
1/4	9.3	9.9
cb	9.6	9.6
S	9.0	10.2
E 1/4		
S	9.7	9.5



19.23

cb			9.5	9.7
1/2			9.2	10.0
c			9.8	9.4
1/4			10.5	8.7
cb			11.6	7.6
N			13.5	5.7
+15			15.5	3.7

T.P.	4.00	10.54	12.69	6.54
------	------	-------	-------	------

E

-15			6.5	4.0
N			6.2	4.3
cb			4.9	5.6
1/4			3.4	6.9
c			3.5	2.0
1/2			2.3	8.2
cb			1.9	8.6
5			2.0	8.5

10.54

7

W 1/2

5			3.4	7.1
cb			2.9	6.6
1/4			4.5	6.0
c			4.9	5.6
1/4			5.2	4.7
cb			6.0	4.5
N			6.1	4.7
+15			5.6	4.9

W cb

-15			4.6	5.9
N			5.4	5.1
cb			5.2	5.3
1/4			5.8	4.7
c			6.0	4.5
1/4			5.1	5.4
cb			4.9	5.6
5			4.7	5.5

W Ly Hancock

5			5.3	5.2
---	--	--	-----	-----

10.54

8

cb	cb		4.9	516
1/2	1/2		4.9	56
c	c		5.0	58
1/2	1/2		4.3	62
cb	+4	TOP E rail	3.80	674
N	cb	ON T.O.	4.3	62
+	N	" "	4.3	62
		W.L. + 7 = E	56' AP	Main line
T.P.	N	on rail	3.87	667
	c	" "	3.74	680
	s	" "	3.62	692

- 1

N

cb

1/2

c

1/2

cb

s

X-sec TRIAS 50' wide  
10' curb  
Moore to Hancock to R.R.

Indexed  
C.S.K.

33.68

9

				T.P. Brock	cb		7.0	26.2
10.19	33.68		23.49	P.W.	S		7.4	26.8
Fly Moore 50' wide 10' curb								
N cb	Top curb return	5.74	27.94		S		7.5	26.2
gut		6.2	27.8		cb		7.7	26.0
C		6.1	27.6		C		7.8	25.9
cb		7.2	26.5		cb		7.8	25.9
+4		5.5	28.2		N		7.0	26.7
S		5.5	28.2					
	E cb							
					N		6.8	26.9
S		7.2	26.8		cb		7.5	26.2
cb		7.4	26.3		C		8.0	25.7
C		6.5	27.2		cb		8.2	25.5
cb		6.6	27.1		S		8.8	24.9
N	Top curb	5.75	27.95			0+25		
N	gut	6.5	27.2		S		9.3	24.4
	E				cb		9.0	24.2
N		6.9	26.8		C		8.4	25.8
cb		7.0	26.7		cb		8.0	25.7
C	R.R. S.M.H.	6.87	26.87		N		7.0	26.1

33.68

0+50

n	5.6	28.1
cb	6.1	27.6
c	7.1	26.6
cb	7.7	26.0
s	8.4	25.3

0+75

s	6.8	26.9
cb	6.3	22.4
c	5.9	27.5
cb	5.5	28.2
n	5.2	28.5

1+0

n	4.6	28.1
cb	4.9	28.9
c	5.4	28.3
cb	6.2	27.8
s	6.4	27.3

1+50

s	5.0	28.9
---	-----	------

33.68

10

cb	4.8	28.9
c	4.8	28.9
cb	4.4	29.1
n	4.5	29.2

2+0

n	4.3	29.4
cb	4.1	29.6
c	4.7	29.0
cb	4.8	28.9
s	4.7	29.0

2+50

s	5.0	28.7
cb	4.9	28.8
c	5.2	28.8
cb	5.2	28.8
n	5.2	28.8

3+00 = Ely Hancock

n	7.8	25.9
cb	7.7	26.0
c	7.5	26.2

33.68

22.73

11

cb			7.6	26.1		0+57		
S			7.1	26.6		-15	15.0	2.1
						S	15.8	6.9
T.P.	0.97	22.73	11.92	21.76		cb	14.2	8.5
						+0	11.0	11.7
						C P.M. 5.17.H.	10.50	14.17
	Wly Hancock = 0+0					cb	9.2	13.5
S			0.4	22.3		r	9.5	13.2
cb			0.5	22.2				
						0+75		
c			0.7	22.0		r	14.8	7.9
cb			1.4	26.3		cb	12.5	10.2
r			1.9	20.8		c	11.5	11.2
	0+30					cb	12.4	10.3
r			4.1	18.6		S	13.8	8.9
cb			4.1	16.6		+10	14.0	8.1
c			4.6	18.1				
cb			3.5	19.2		T.P.	1.73	12.04
+7			3.0	19.7			12.42	10.31
S			4.7	18.0				
+10			7.0	15.7		0+85		
						-10	2.3	9.7
						S	4.0	8.0

12.04

12

cb 3.9 8.11

c 4.3 7.7

cb on spur rail 3.89 8.15

N " tie 4.4 7.6

1 + 0.5.9 = E Main S Fe RR on Curve

N W rail 3.32 8.22

" E " 3.52 8.52

E W " 3.21 8.73

" E " 3.42 8.62

S W rail 3.08 8.96

S E " 3.81 8.63

S

X SEC Alley 20' Wide  
 BIK 4 Eastgate

Moore  
 2-15-38,

Indexed  
 C.S.K.

13

NWCP 462 358.56 353.94 Orange 46th

00-16 = N. cb. Orange

NL 46th Top cb 4.58 353.98

" " Pav. 5.25 352.31

E.L. Alley Top cb 5.55 353.01

E " ground 6.2 352.36

W.L. " Top cb 5.76 352.80

E.L. CHAIRHOUSE Top cb 6.80 351.76

" " " Pav. 7.29 350.27

0+00 = N.L. Orange

W Top cb 5.55 353.01

C " 5.0 353.3

E " 5.37 353.19

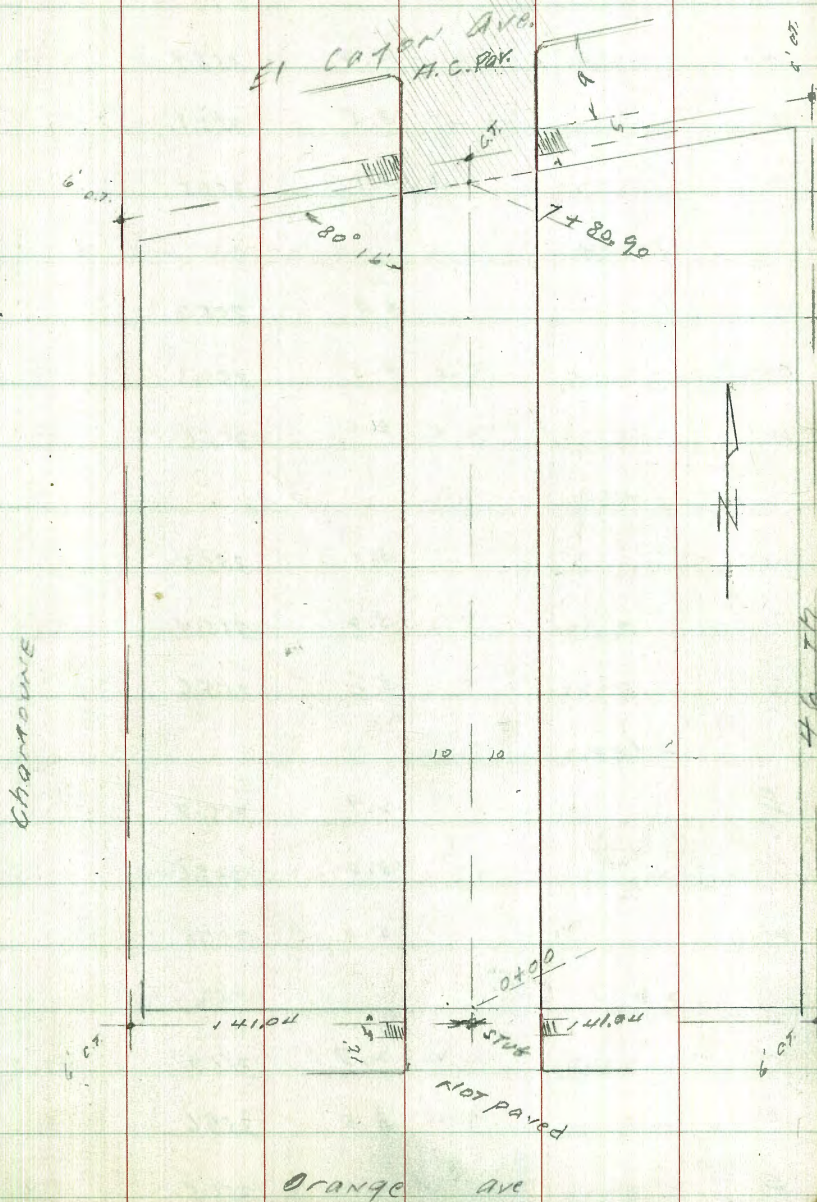
0+N

E 3.9 354.7

C 3.9 354.7

W 3.9 354.7

W Top N end Cent. wall 3.51 355.06



358.56

358.56

14

0+50

2+58

W	3.2	355.4
C	3.5	355.1
E	3.1	355.8

E	3.0	355.6
C	3.1	355.5
W	2.8	355.8

1+00

+2 Sin. gac. dirt

E	3.3	355.3
C	3.3	355.3
W	3.0	355.6

+2	3+04	2.6	356.0
W	2.7	355.9	
C	M.H. P.M	2.85	355.71

1+50

W	3.1	355.5
C	3.2	355.4
E	3.0	355.6

E	3+50	3.1	355.5
E	2.9	355.7	
E	2.7	355.9	

2+00

E	2.9	355.7
C	3.0	355.6
W	2.8	355.8

W	2.5	356.1		
T.P.	4.84	360.70	2.72	355.84

2+35

3+80

W	2.7	355.9
C	3.0	355.6
E	3.1	355.5

W	4.4	356.1
C	4.8	355.9
E	4.8	355.9



360.70

360.70

15

	4+00					W		4.4	356.3	
-6	Sim. 90° dirt	4.8	355.9	faces So.	+2	5' drive entrance	4.5	356.35		To 90° facing north
E		4.7	356.0			5+50				
C		4.8	355.9		W		4.6	356.1		
W		4.7	356.0		C		4.7	356.0		
	4+00				E		4.4	356.3		
W		4.7	356.0			5+90				
C		5.0	355.9		E		4.5	356.2		
E		4.7	356.0		C		4.6	356.1		
	4+00				W		4.4	356.3		
E		4.8	355.9			6+13				
C		4.8	355.9		-4.7	E 18' 90° cem. fl.	4.25	356.45		Level
W		4.5	356.2		W		4.6	356.1		
	5+00				C		4.6	356.1		
W		4.6	356.1		E		4.7	356.0		
C		4.6	356.1			6+26				
E		4.3	356.4		E		4.9	355.8		
	5+15				C		4.6	356.1		
E		4.5	356.2		W		4.5	356.2		
C		4.6	356.1		+2	E 4' walk	4.51	356.19		

360.70

	6+41			
W		4.5	356.2	
C		4.6	356.1	
E		5.0	355.9	
+9	+ walk	5.08	355.62	
	6+63			
-9	18' gar. cem. fl.	5.11	355.59	level
E		4.9	355.8	
C		4.6	356.1	
W		4.9	356.4	
	7+05			
W		4.4	356.3	
C	M.H. Pin	4.37	356.33	
E		4.6	356.1	
	7+20			
E		4.7	356.0	
C		4.5	356.2	
W		4.4	356.3	
	7+60			
W		4.3	356.4	

360.70

16

				C		5.2	355.5	
				E		4.9	355.8	
					7+80.90	J.L. El Cañon Ave		
				E	cb	5.99	354.71	
				E	pav.	6.32	354.38	
				C	"	6.53	354.17	
				W	"	6.14	354.56	
				W	cb	5.88	354.82	
					16' N	= S	cb L. W. El Cañon	
				W	pav.	6.72	353.98	
				C	"	6.77	353.93	
				E	"	6.84	353.86	
					SWBP El Cañon + 4677	7.68	353.02	353.00

Levels on Bayside walk  
Rockaway Ct. N.Y.

Moore  
3-7-98

2.77

17

S.W.P.	0.89	7.97	7.08	San Jose Pl Sea wall	E VANITIC CT.	3.47	-0.70	Bd. walk
T.P.	3.21	3.73	7.45	0.52	" San Rafael Pl.	3.41	-0.44	" "
					" Venice Ct.	3.32	-0.55	" "
					" Verona Ct.	3.47	-0.70	" "
0+00 S.L. Rockaway	Cent. walk	4.46	-0.73	6' W				
0+10 Cent. walk		3.62	0.11					
0+37 " "		2.48	0.25		4.46	4.98	0.52	T.P.
1+40.50 ground		3.83	-0.10	E Santose	50' S of Rockaway	4.70	0.28	Resid. H. El.
1+60 5' wide Cent. Porch		3.03	0.70		E Redondo Ct.	5.0	-0.02	Bd. walk
2+40 H. El. of Resid.		4.43	-0.70		E QueensTown	4.8	0.18	" "
2+71 S.L. Talent		4.50	-0.77	Cent. walk	" Pismo Ct.	4.5	0.48	" "
2+15 E 14' Cent. Porch		3.17	0.54		50' S of Pismo Ct.	4.57	0.41	Cent. " 4' wide
4 S.L. Seagirt		4.0	-0.27	Bd. "				
5+39 N.L. Sunset		3.79	-0.04	" "	T.P. 439	4.62	4.75	0.23
T.P.	2.60	2.77	3.54	0.17	E Portsmouth Ct.	5.38	-0.76	Cent. "
					" " "	4.5	0.12	Bd. "
6+55 S.L. Tangier		2.57	0.20	" "	" Santa Clara Pl	5.0	-0.38	" "
7+84.1 " Toulon		3.47	-0.70	" "	25' N of E Ostend Ct.	5.02	-0.40	Bot. Cent. Step

4.62

3.55

18

E	OSTEND CT.	5.07	-0.40	CEM. WALK	90' S of NANTASKET CT.	4.41	-0.86	3' CEM. WALK
	85' N of ORMOND CT.	5.17	-0.50	2' wide CEM. WALK	E NANTANT "	4.5	-0.95	Bd. "
E	" "	5.07	-0.45	" "	22' S "	4.27	-0.72	4' CEM. "
					42' " "	4.24	-0.69	" "
T.P.	2.95	3.55	5.07	-0.40				
					SW corner of T.P. Porch	3.39	0.16	50' S of NANTANT
	35' S of ORMOND CT.	3.67	-0.17	2' wide CEM. WALK				
	70' N. NANTIC CT.	2.17	0.38	" "				
E	" "	3.04	0.51	Bd. "				
	25' S "	3.00	0.57	Hedge,				
	58 "	3.00	0.55	S "				
	70 "	2.96	0.59	3' CEM. WALK				
	98 "	3.06	0.49	" "				
	132 "	3.14	0.41	" "				
E	SAN JUAN Pt.	3.70	-0.15	Bd. WALK				
	55' S "	3.30	0.25	4' CEM. "				
	72 "	3.33	0.22	3' " "				
E	NANTASKET CT.	3.66	-0.11	CEM. WALK				
	4' W of WIL " 4 Bayside WALK	4.00	-0.45	" "				
	65' S of NANTASKET	4.24	-0.71	3' " "				



x sec Alley 15' wide  
 BIK 28 Fortuna Park Add.

Moore  
 2-10-38

Indexed  
 C.S.K.

20

NET ST	1.07	36.35		35.28
TP	1.75	26.35	11.75	24.60
TP	10.24	31.20	5.39	20.96

JANUARY  
 Pacific

Roosevelt

0 - 37.5 = E Roosevelt

Alley MHRM 5.96 25.24

" ground 5.4 25.8

0 - 26.5

" 5.1 26.1

0 + 00 S L Roosevelt

W 4.7 26.8

C 4.3 26.9

E 3.8 27.4

0 + 12

E 2.8 28.4

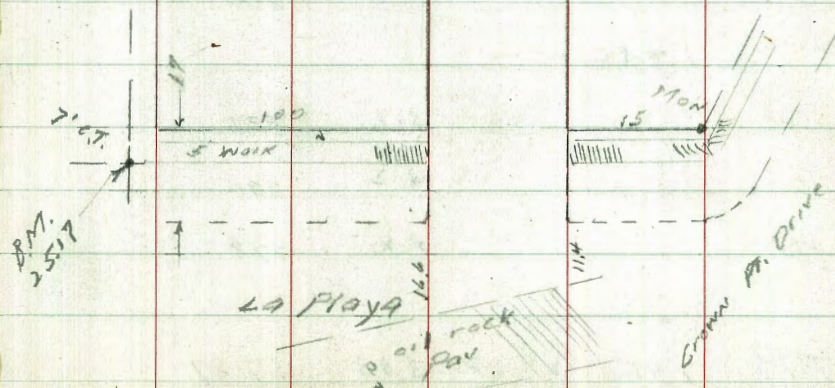
C 2.9 28.3

W 2.8 28.4

0 + 50

W 3.0 28.2

Kendall



3/20

C		2.5	28.7
E		2.7	28.5
	0+75		
F		2.9	28.3
C		2.5	28.7
W		2.2	29.0
	1+00		
W		2.3	28.9
		2.4	28.8
		2.5	28.7
	1+25		
E		2.7	28.0
B		2.9	28.3
W		2.6	28.6
	1+50		
W		3.1	28.1
C		3.2	28.0
E		3.4	27.8
T.P.	1.95	29.82	3.33
			27.87

29.82

21

		1+75	
E	1 edge gap.	2.0	27.8
C		2.0	27.8
W		1.9	27.9
	1+95		
W		2.0	27.8
C		2.2	27.6
F		2.3	27.5
	3 edge +10 E gap. cen. fl.	2.40	27.42
	2+25		
E		2.6	27.2
C		2.6	27.2
W		2.5	27.5
	2+50		
W		2.6	27.2
C		3.0	26.8
E		3.1	26.7
	2+75		
E		3.0	26.8
C		3.1	26.7

29.82

W		3.0	26.8
	4700		
W		3.5	26.3
C		3.5	26.3
E		3.0	26.2
	4750		
E		4.4	25.4
C		4.0	25.8
W		4.1	26.2
	4775		
W		2.9	26.9
C		3.9	25.9
E		4.7	25.1
	4700		
E		5.1	24.2
+6		4.6	25.2
C		4.1	25.7
+3		3.1	26.2
W		2.9	26.9

29.82

22

	4725		
W		4.1	25.7
C		4.8	25.0
E		5.6	24.2
	4750		
E		5.0	24.8
+3		4.7	25.1
C		4.0	25.8
W		3.8	26.0
	4775		
W		3.9	25.9
C		4.3	25.5
E		4.7	25.1
T.P.	3.61	27.89	5.54
	5704		
E		4.4	23.5
C		3.7	24.2
W		2.7	25.2



27.89

5704

cent

W 43.5 Hedge apron 2.36 25.53

+5 " " gar. cent. 2.17 25.22

5721

-5 Hedge gar. cent. fl. 2.19 25.20

-3.5 " cent. apron 2.39 25.60

W 2.8 25.1

C 3.9 24.0

E 4.6 23.3

5724

N end  
W fence in alley 1.7

5750

E 4.8 23.1

C 4.4 23.8

+3 4.2 23.2

+4.2 Sand fence

W 3.4 24.5

5775

W 4.1 23.8

C 4.5 23.4

E 4.6 23.3

27.89

6700.8 N.L. La Playa

4.9 23.0

4.6 23.3

4.2 23.7

+1.8 = N edge sidewalk

W Top cent. walk 4.03 23.56

W 4.3 23.6

C 4.6 23.3

E 4.6 23.3

E " " " 4.29 23.60

+17 = N curb La Playa

E Top cb 4.43 23.46

E 5.0 22.9

C 5.1 22.8

W 4.9 23.0

W Top cb 4.19 23.76

+28.4

E = N edge pav 4.94 22.95

+33.6

W N " " 4.77 23.12

23

27.89

W' S edge 20' strip pav 4.54 23.27

E " " " 4.68 23.24

T.P. 5.72 29.33 4.28 23.61

N.E. Cor. 7' C.T. 4.16 25.17 La Playa and Sequoia

Kendall EL Roosevelt St N curb La Playa 4.43 24.80 Topog.

T.P. 0.81 28.58 1.56 27.77

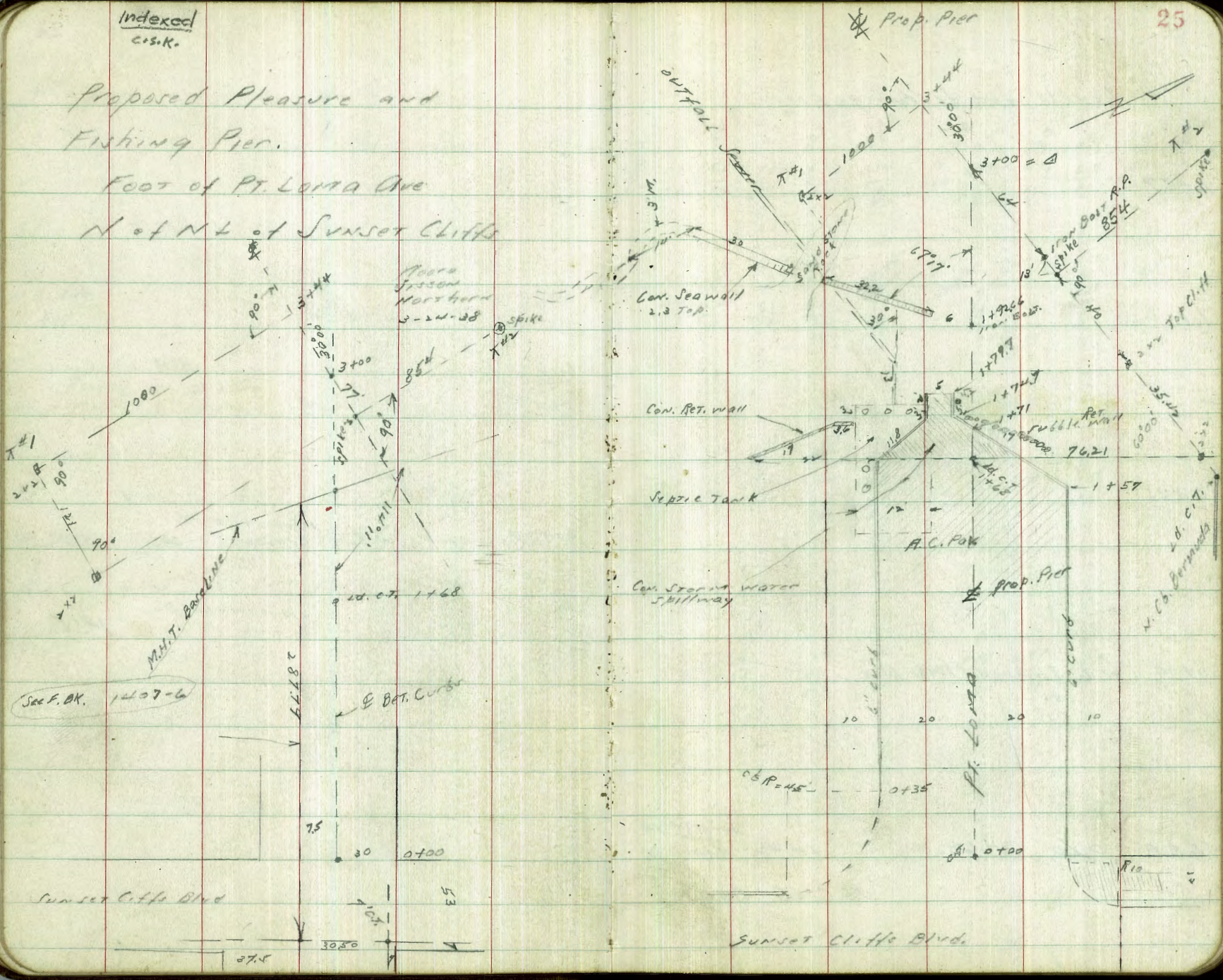
T.P. B.M.B.P. 4.69 26.40 6.87 21.71 Set B.M.B.P. in curb SW Cor. Highland St. Crown Pt. Dr.

T.P. 3.65 21.55 8.50 17.90

3.36 18.19 Fd. " " " " " " La Mancha Dr. Crown Pt. Dr. 1815

# Proposed Pleasure and Fishing Pier.

Foot of Pt. Loma Ave  
N of N of Sunset Cliffs



Levels for fishing pier

1757

31.9	32.9	29.0	27.0	27.06	26.24	26.39	26.25	27.12	28.1	29.5
$\frac{2.7}{45}$	$\frac{1.7}{56}$	$\frac{5.0}{54}$	$\frac{7.6}{50}$	$\frac{7.56}{20}$	$\frac{8.24}{20}$	$\frac{8.23}{20}$	$\frac{8.07}{20}$	$\frac{7.50}{20}$	$\frac{6.5}{30}$	$\frac{5.7}{40}$
				66	907		907	66	30	40

1700

31.4	32.6	28.5	27.62	26.80	27.22	26.62	27.46	28.3	28.6
$\frac{6.2}{57}$	$\frac{5.0}{30}$	$\frac{6.1}{30}$	$\frac{6.80}{20}$	$\frac{7.80}{20}$	$\frac{7.20}{20}$	$\frac{8.0}{20}$	$\frac{7.16}{20}$	$\frac{6.0}{30}$	$\frac{6.0}{40}$
			66	907		907	66	30	40

0735

30.8	31.6	29.0	28.32	27.47	27.40	26.96	27.70	27.9
$\frac{6.8}{20}$	$\frac{3.0}{33}$	$\frac{5.6}{30}$	$\frac{6.30}{20}$	$\frac{7.5}{20}$	$\frac{6.80}{20}$	$\frac{7.66}{20}$	$\frac{6.90}{20}$	$\frac{6.7}{30}$
			66	907		907	66	30

0700 W. L. Sunset Cliffs Blvd.

28.74	27.85	28.11	28.13	27.09	27.75	28.3
$\frac{5.88}{35}$	$\frac{6.77}{35}$	$\frac{6.5}{20}$	$\frac{6.48}{20}$	$\frac{7.50}{20}$	$\frac{6.87}{20}$	$\frac{6.0}{30}$
66	907	907		907	66	30

S.E.B.P. 0.20 34.62

Sunset Cliffs  
and  
34.42 Adair St.

U.S.C. & G. DATUM

34.62

1+85

1+79.7 end FL. Spillway E

1+77.7

1+74.7

1+68

3462

105	8.6	10.2	22.5	21.13.2	22.7	19.8	19.7	23.0	20	20	21.6	23.0	27
60	50	20	25	17	27	8	9	12	20	58	7	20	20
T.P.C.I. Sewer Pipe													

27.9	23.6	27.4	26.9	21.6	19.2	14.5	13.4	27.0	13.5	27.02	24.85	15.7	24.8	27.0	18.5	24.2	31.2	30.2	27.6	20.6	24.9
6.7	11.0	7.2	7.7	12.0	15.4	20.1	21.2	7.6	21.1	7.6	9.77	18.8	7.8	7.0	10.1	10.4	3.2	4.2	7.0	4.0	5.0
70	62	56	50	59	51	59	22.2	23.2	22.2	20.2	20.2	22.2	22.2	22.2	22.2	22.2	22.2	22.2	22.2	22.2	22.2
T.P. Tank																					

27.8	22.1	22.2	14.7	26.9	26.9	27.00	25.26	25.27	27.02	27.3	27.3	27.0	20.3	27.5	30.8	30.0
6.8	7.5	12.4	19.8	7.7	7.7	7.6	9.24	9.5	7.00	7.3	7.3	7.3	2.3	7.1	3.8	2.6
56	28	22	27	26	22	20.2	20.2	20.2	20.2	20.2	20.2	20.2	20.2	20.2	20.2	20.2
T.P. Spillway																

33.6	27.4	26.9	26.92	26.05	25.92	25.46	26.82	27.8	27.6	30.2	29.9
1.0	6.8	7.7	7.70	8.57	8.70	8.76	8.0	6.8	6.0	4.2	4.7
28	39	30	20	20	20	20	20	20	20	20	20
T.P. Spillway											

3462

+12

11.5	12.6	12.39	5.7	9.1	10.2	8.1	10.3	10.5	11.1	12.3
2.0	0.9	1.07	7.8	10.4	6.3	4.8	5.2	6.0	1.8	1.2
50	45	39	33		4	15	20	29	31	50
		TOP	TOP							

T.P. 0.44 13.46 21.60 13.02

2 + 07

10.7	11.3	11.3	12.3	12.3	5.4	6.3	4.1	11.3	10.1	11.7	14.3	16.7	23.9
23.9	22.2	20.8	20.3	22.2	29.2	28.3	30.5	23.3	24.5	22.2	20.3	18.2	20.7
70	40	45	42	35	33	20	5	18	28	21	21	50	60
			TOP	TOP	TOP	TOP							

1 + 97

10.7	11.5	11.9	14.5	12.1	12.9	5.3	11.8	13.0	5.9	12.8	16.3	21.3
23.9	23.1	22.7	20.1	22.5	21.7	22.3	22.8	21.6	18.7	20.8	18.3	19.0
70	55	53	45	37	40	8	8	12	21	21	23	50
				TOP	TOP	TOP	TOP					

1 + 92.66

13.1	14.3	14.6	15.3	12.4	12.3	13.0	13.3	12.5	17.0	16.3	21.1	24.6	22.4
21.5	20.3	16.0	19.3	21.8	22.3	21.6	21.3	22.1	27.6	18.3	13.5	10.0	3.2
60	50	46	40	39	50	4	4	7	10	20	25	25	55
						TOP	TOP	TOP					

3462

3462

4

2

R

+72

	0.1	0.6	2.4	3.4	0.9	0.9
12.8	12.7	10.7	10.1	12.6	12.6	
50	11	10	15	5	50	
		R	R			

+55

11	11	3.5	3.2	11	11	3.0	3.5	1.4	1.0	1.9	5.5
12.4	12.4	10.6	10.3	12.4	12.4	10.5	10	12.1	12.5	5.6	5.0
50	50	22	14	50	5	5	13	50	45	18	50
		R	R			R	R			R	R

+45

0.9	0.9	6.0	1.7	3.2	5	2.0	3.5	3.4	1.1	1.7	2.1	4.2	2.3	2.7
12.6	12.6	6.9	5.8	10.3	12.0	11.5	10.0	10.1	12.4	11.8	10.8	5.3	4.2	4.5
50	34	28	18	15	12	5	10	8	50	18	25	27	50	50
		R	R	R		R	R	R		R	R	R	R	R

2+25

1.3	10.8	9.9	3.7	2.7	2.4	10.7	9.5	11.2	10.1
12.2	2.7	3.6	9.8	10.8	10.7	2.8	4.0	2.3	2.4
50	36	26	25	5	13	28	27	46	50
	R	R			R	R	R	R	R

12.46

12.46

Rock ledge approx 50' RT of J+50  
to 7+00

4+0

14.0  
55.5  
- 0.5

14.0  
55.5  
- 0.5

14.0  
55.5  
- 0.5

7+0

12.0  
55.5  
- 0.5

12.0  
55.5  
- 0.5

12.0  
55.5  
- 0.5

1+0

0.0	0.1	2.1	4.5	6.1	0.0	0.6
13.5	13.4	10.8	9.0	6.8	12.5	12.9
50	55	27	20	15	8	5
		R	R	R		

2+0

0.9	1.0	5.2	6.3	5.5	0.7	0.7
12.6	12.5	8.3	7.7	8.0	12.8	12.8
50	44	46	30	20	5	5
		R	R	R		

12.8  
55.5  
- 0.7

12.46



PT. LOMA AND SOUNDINGS

4-21-38.

Return 10:20 AM. Beg. OUT 10:09 AM. OUT 10:45 AM.

S Sdg.	Water-2.2	Water-2.0	Water-2.4
68° 13' ✓	33'	47° 24' ✓	17'
67° 41' ✓	33'	49° 07' ✓	18'
67° 18' ✓	31'	51° 05' ✓	19'
66° 51' ✓	31'	53° 03' ✓	19'
66° 25' ✓	31'	55° 00' ✓	20'
65° 52' ✓	30'	55° 58' ✓	21'
64° 58' ✓	29'	56° 51' ✓	22'
64° 24' ✓	27'	57° 53' ✓	23'
63° 34' ✓	26'	58° 44' ✓	22'
62° 40' ✓	23'	59° 38' ✓	23'
61° 59' ✓	23'	60° 30' ✓	24'
61° 11' ✓	23'	61° 38' ✓	25'
60° 40' ✓	21'	62° 27' ✓	27'
60° 18' ✓	21'	62° 59' ✓	28'
59° 22' ✓	21'	63° 56' ✓	28'
58° 31' ✓	19'	64° 35' ✓	29'
57° 36' ✓	19'	64° 59' ✓	30'
56° 38' ✓	20'	65° 03' ✓	31'

T #1

S Sdg.	Water-2.4	Q Sdg.	N Sdg.
55° 25' ✓	19'	65° 42' ✓	32'
54° 48' ✓	18'	65° 45' ✓	34'
53° 28' ✓	18'	66° 15' ✓	33'
52° 25' ✓	16'		
			60° 35' ✓ 30'
			61° 09' ✓ 31'
			61° 13' ✓ 32'
			61° 28' ✓ 32'
			62° 18' ✓ 33'
			END 11:01 AM.
			T #1 F.S. ON 3+24 Δ to left
			Some Kelp growing in small bunches denoting rock bottom at approx 54'

4-21-38

17/11/45

Party 4.

T #2 F.S. on (3+00-(A)) - 77' = spike =  $\Delta$  Right

Return	Box out	out	Return	out	
70° 42' ✓	58° 10' ✓	61° 01'	56° 21' ✓	72° 19' ✓	75° 18' ✓
70° 21' ✓	59° 00' ✓	62° 07'	55° 30' ✓	73° 08' ✓	75° 49' ✓
69° 58' ✓	60° 24' ✓	63° 26'	54° 04' ✓	73° 28' ✓	76° 49' ✓
69° 38' ✓	61° 03' ✓	64° 50'	53° 26' ✓		78° 01' ✓
69° 13' ✓	61° 42' ✓	66° 05'			78° 24' ✓
68° 26' ✓	63° 47' ✓	67° 16'			
67° 57' ✓	65° 18' ✓	68° 43'			
67° 03' ✓	66° 25' ✓	69° 51'			
65° 46' ✓	67° 28' ✓	70° 49'			
64° 51' ✓	68° 06' ✓	71° 33'			
64° 02' ✓	68° 56' ✓	72° 21'			
63° 35' ✓	69° 17' ✓	72° 24'			
62° 36' ✓	69° 51' ✓	72° 47'			
61° 58' ✓	70° 08' ✓	73° 20'			
60° 56' ✓	70° 23' ✓	73° 45'			
59° 59' ✓	70° 25' ✓	74° 21'			
58° 37' ✓	70° 59' ✓	74° 10'			
57° 21' ✓	72° 00' ✓	74° 49'			

X. Sec, School Grounds  
 at McKinley School Felton to McKinley Sts  
 bet. Palm & Redwood Sts  
 0+00 N + S = N. Line Palm St.

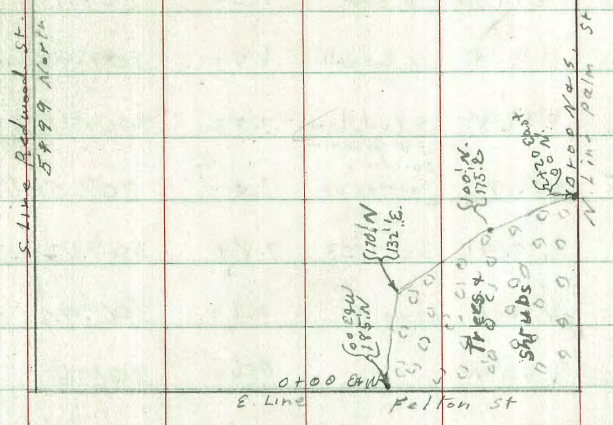
Indexed  
 C.S.K.

0+00 E + W = E. Line Felton St.

W. Line McKinley St  
 5+50 East.

BM BR	1.50	314.51	313.01	N.W. Felton + Redwood.
1.0 W of 0+00 E + W = E. Edge cmt. walk on E. side of Felton.				
1. W	599. N	N. End. Lawn.	1.76	312.75 walks edge s. edge walk
23. E	600. N		1.57	312.94 S. Side Redwood.
23. E	590. N	N.W. corner Bldg. 1, 3	1.13	313.2
1. W	550. N		2.41	312.10 walk
23. E	550. N	s. side school E of 10' walk	1.7	312.8
1. W	512. N	W. End.	2.95	311.56
23. E	512. N	E. End. E 10' walk	2.70	311.81 w. side school.
1. W	500. N	walks	3.14	311.37
23. E	500. N		3.3	311.2 w. side school
4.5 E	454. N	conc. Box Oil inlet.	3.4	311.1
5.7 E	442. N	Meter Box E 5' walk	3.80	310.71
1. W	439. N	W. End.	4.00	310.51
25. E	439. N	E. End. 5' walk.	3.40	311.11 w. side school
1. W	407. N	N. edge walk Main Entrance	4.35	310.16 W. End.
14. E	407. N	" "	3.95	310.56 E. end
14. E	389. N	S. edge walk Main Entrance	3.95	310.56 E. End

7. E	412. N	Flag Pole s. edge walk			
1. W	389. N	Main Entrance W. End.	4.62	309.89	W. End
1. W	359. N	E 5' walk	5.05	309.46	
25. E	359. N	E. End E 5' walk	4.22	310.29	w. side school
0.5 E	374. N	Meter Box	4.85	309.66	
5.7 E	356. N	" "	4.87	309.64	
5.5 E	289. N	Meter Box E 10' walk	6.18	308.33	
1. W	288.7 N	W. End.	6.40	308.11	
30. E	288.7 N	E. End 10' walk	5.70	308.81	W. side school



East.	North										
		314.51									307.23
5.5 E	226. N	Meter box	7.10	307.41		25. E	130. N		8.6	298.6	
1. W	221. N	8' walk W. End.	7.34	307.17		15. E	130. N		4.4	302.8	
25. E	221. N	E. End walk	6.53	307.98	W. side School	5. E	130. N		1.3	305.9	
1. W	205. N	S. End lawn	7.53	306.98		1. W	130. N	walk	0.52	306.71	
25. E	205. N	S. W. Cor Main Building Squared up.	7.0	307.51	W. + S. Sides produced to intersection	25. E	110. N		3.2	304.0	
T.P.	0.61	307.23	7.89	306.62		10. E	110. N		2.2	304.6	
1. W	190. N	walk	0.29	306.94		5. E	110. N		1.1	306.1	
5. E	190. N		0.6	306.6		1. W	110. N	walk	0.41	306.62	
15. E	190. N		1.6	305.6		25. E	100. N		2.4	304.8	
25. E	190. N		2.5	304.7		10. E	100. N		2.1	305.1	
50. E	205. N	S. side - Main Bldg	3.0	304.2		5. E	100. N		1.0	306.2	
50. E	190. N		4.0	303.2		1. W	100. N	walk	0.65	306.58	
25. E	175. N		4.0	303.2		25. E	50. N		1.8	305.4	
15. E	175. N		3.8	303.4		10. E	50. N		1.2	306.0	
5. E	175. N		0.8	306.4		1. W	50. N	walk	0.83	306.40	
1. W	175. N	walk	0.37	306.86		25. E	5. S	N. Edge walk	2.37	304.86	
25. E	145. N		9.0	298.2		1. W	5. S	N. edge + E. Edge walks.	1.00	306.23	
10. E	145. N		4.3	302.9		50. E	5. S	"	3.80	303.43	
5. E	145. N		1.3	305.9		50. E	00 N45.		2.6	304.6	
1. W	145. N	walk	0.46	306.77		50. E	50. N		2.8	304.4	

		307.23							
50'.E	102'.N		3.5	303.7		75'.E	151'.N	Eucalyptus Tree	
50'.E	110'.N		6.8	300.4		74'.E	140'.N	" "	
50'.E	127'.N		11.4	295.8		69'.E	127'.N	" "	
50'.E	136'.N		11.4	295.8		81'.E	120'.N	" "	
50'.E	152'.N		9.2	298.0		78'.E	106'.N	" "	
37'.E	152'.N		7.4	299.8		85'.E	138'.N	" "	
50'.E	164'.N		5.0	302.2		82'.E	161'.N	" "	
37'.E	164'.N		5.0	302.2		102'.E	172'.N	" "	
81'.E	230'.N	E. side Main Bldg.	2.0	305.2		112'.E	161'.N	" "	
81'.E	205'.N	S. E. Cor Main Bldg. Square	3.3	303.9	P.F. S. + E sides produce to Inter section	93'.E	156'.N	" "	
107'.E	192'.N	Sw. Cor. Frame Building	4.7	302.5		116'.E	152'.N	" "	
107'.E	215'.N	Sw. side Frame Bldg.	2.9	304.3		115'.E	190'.N	" "	
107'.E	230'.N	N. side Frame Bldg.	7.4	305.4		104'.E	135'.N	" "	
75'.E	190'.N		4.5	302.7		111'.E	132'.N	" "	
75'.E	172'.N		5.1	302.1		95'.E	115'.N	" "	
75'.E	155'.N		9.1	298.1		103'.E	113'.N	" "	
75'.E	140'.N		13.5	293.7		93'.E	106'.N	" "	
75'.E	133'.N		13.5	293.7		116'.E	105'.N	" "	
75'.E	118'.N		9.5	297.7		132'.E	169'.N	" "	
75'.E	100'.N		6.2	301.0		130'.E	156'.N	" "	

		307.23							
140' E	143' N		Eucalyptus Tree		T.P.	4.03	304.47	6.79	300.44
145' E	117' N		" "		100' E	100' N		6.5	298.0
136' E	113' N		" "		100' E	117' N		8.3	296.2
153' E	151' N		ctr Inclinator	5' x 5' Cone Base	100' E	126' N		11.4	293.1
143' E	168' N		" "	3' x 6' "	100' E	140' N		11.1	293.4
					100' E	150' N		8.8	295.7
		↗ 307.23			100' E	180' N		2.6	301.9
75' E	90' N		5.8	301.4	100' E	192' N		2.0	302.5
75' E	83' N		4.3	302.9	125' E	192' N		1.4	303.1
75' E	75' N		4.3	302.9	125' E	175' N		3.0	301.5
75' E	50' N		3.9	303.3	125' E	157' N		4.7	299.8
75' E	25' N		3.6	303.6	118' E	157' N		6.5	298.0
75' E	4' N		4.1	303.1	125' E	150' N		7.3	297.2
75' E	0+00		4.8	302.4	125' E	130' N		11.1	293.4
100' E	5' S	N. edge walk	6.77	300.46	117' E	130' N		12.5	292.0
100' E	00 N 05		6.3	300.9	125' E	125' N		13.0	291.5
100' E	4' N		4.9	302.3	115' E	125' N		13.0	291.5
100' E	25' N		5.0	302.2	125' E	108' N		13.8	290.7
100' E	57' N		5.1	302.1	133' E	108' N		13.9	290.7
100' E	75' N		7.5	299.7	140' E	108' N		13.0	291.5

304.47

115' E	108' N	9.5	295.0
125' E	87' N	10.7	293.8
138' E	87' N	15.0	289.5
148' E	87' N	15.0	289.5
125' E	50' N	7.1	297.4
117' E	36' N	3.8	300.7
125' E	20' N	4.1	300.4
138' E	20' N	8.6	295.9
125' E	4' N	4.1	300.4
125' E	00' N + S	5.0	299.5
150' E	5' S = edge walk	6.75	297.72
150' E	5' N	7.0	297.5
150' E	14' N	11.6	292.9
150' E	40' N	13.5	291.0
150' E	58' N	14.5	290.0
150' E	62' N	15.2	289.3
160' E	62' N	15.2	289.3
150' E	75' N	16.0	288.5
150' E	100' N	11.4	293.1
150' E	125' N	7.0	297.5

304.47

37

150' E	150' N	3.4	301.1
150' E	160' N	1.4	303.1
138' E	175' N	1.8	302.7
138' E	192' N	0.4	304.1
150' E	200' N	0.5	304.0
175' E	200' N	0.2	304.3
175' E	150' N	1.8	302.7
157' E	150' N	1.8	302.7
175' E	123' N	2.9	301.6
170' E	123' N	4.4	300.1
175' E	100' N	6.5	298.0
175' E	78' N	10.6	294.5
175' E	57' N	12.5	292.0
183' E	57' N	11.2	293.3
186' E	57' N	9.5	295.0
162' E	57' N	17.5	287.0
154' E	57' N	17.5	287.0
175' E	33' N	17.2	287.3
175' E	17' N	17.8	286.7
170' E	17' N	20.4	284.1
170' E	16' N	18.0	286.5

S.E. Cor. Front  
Building.N. End (Inlet)  
24' Conc. Culvert

FL.

304.47

307.95

38

175' E	00 N+S		8.0	296.5	250' E	150' N	4.2	303.8
175' E	5' S	walk	8.12	296.35	250' E	100' N	5.9	302.1
200' E	5' S	walk	8.50	295.97	250' E	50' N	7.5	300.5
200' E	00 N+S		8.5	296.0	250' E	10' N	9.0	299.0
200' E	10' N		10.6	293.9	250' E	5' N	9.8	298.2
200' E	50' N		7.5	297.0	250' E	00 N+S	11.0	297.0
200' E	88' N		3.8	300.7	250' E	5' S = walk	11.73	296.22
T.P.	7.26	307.95	3.78	300.67	300' E	5' S = "	11.18	296.77
200' E	100' N		6.7	301.3	300' E	00 N+S	10.2	297.8
200' E	150' N		5.0	303.0	300' E	5' N	8.4	299.6
200' E	200' N		3.5	304.5	300' E	50' N	6.4	301.6
138' E	250' N	Se. side Frame Bldg.	1.6	306.4	300' E	100' N	5.2	302.8
150' E	300' N		1.03	308.3	300' E	150' N	4.0	304.0
138' E	279' N	N. E. cor Frame Bldg.	0.4	307.6	300' E	200' N	3.1	304.9
					300' E	250' N	2.5	305.5
200' E	300' N		0.6	307.4	300' E	300' N	2.0	306.0
200' E	250' N		1.7	306.3	350' E	300' N	2.8	305.2
250' E	300' N		1.3	306.7	350' E	250' N	3.3	304.7
250' E	250' N		1.9	306.1	350' E	200' N	3.7	304.3
250' E	200' N		2.9	305.1	350' E	150' N	4.1	303.9



307.95

350' E	100' N	4.8	303.2
350' E	50' N	5.8	302.2
350' E	8' N	7.4	300.6
350' E	0+00 N	9.8	298.2
350' E	5' S = walk	10.76	297.19

Sec 400' East

	5' S = walk	10.10	297.85
	00 N+S	9.4	298.6
	8' N	7.0	301.0
	50' N	5.8	302.2
	100' N	5.1	302.9
	150' N	4.9	303.1
	200' N	4.6	303.4
	250' N	4.3	303.7
	300' N	4.1	303.9

450' East

	300' N	6.0	302.0
	250' N	6.0	302.0
	200' N	6.1	301.9
	150' N	6.3	301.7

307.95

39

100' N	6.1	301.9
50' N	6.5	301.5
5' N	7.2	300.8
00 N+S	8.8	299.2
5' S = walk	9.56	298.39

500' East

5' S = walk	8.93	299.02
00 N+S	8.4	299.6
3' N	7.5	300.5
50' N	7.0	301.0
100' N	7.5	300.5
150' N	8.0	300.0
200' N	8.3	299.7
250' N	8.2	299.8
300' N	8.0	300.00

545' East

300' N	13.2	294.8
250' N	10.6	297.4
200' N	10.9	297.1
150' N	9.8	298.2

307.95

545' East (Con)

100' N	8.6	299.4
50' N	7.8	300.2
3' N	7.5	300.5
00 N+S	8.5	299.5

550<sup>E</sup> East = W. edge walk

5' S = walk.	8.50	299.45
00 N+S	8.5	299.5
50' N	9.2	298.8
100' N	10.2	297.8
150' N	11.4	296.6
200' N	12.7	295.3
250' N	14.0	294.0
300' N	14.5	293.5

555<sup>E</sup> East = W. edge walk

200' N	13.17	294.78
150' N	11.95	296.00
100' N	10.81	297.14
50' N	9.64	298.31

307.95

555<sup>E</sup> East 600' N+S W. edge walk 8.50 299.45

T.P.

7.90

300.05

Top  
Fence Post.

B.M.

2.75

315.76

313.01

N.W. Cor  
F.I.T. +  
Redwood.

52' E.	600' N	{ 2 <sup>nd</sup> N. edge walk 9' wide }	2.65	313.11
52' E.	590' N	{ 1 <sup>st</sup> S. end. wall 9' wide }	2.60	313.16
81' E.	590' N.	N.E. Cor. Main Bldg.	2.6	313.16
81' E.	600' N.	S. edge walk	2.64	313.12
81' E.	599' N	S. Line Railroad Meter Box	2.64	313.12
81' E.	550' N	E. side Main Bldg	3.1	312.7
81' E.	500' N	" " "	3.4	312.4
81' E.	450' N	" " "	4.1	311.7
81' E.	400' N	" " "	4.7	311.1
81' E.	350' N	" " "	5.5	310.3
81' E.	300' N	" " "	6.7	309.1
81' E.	286 <sup>5</sup> N.	{ " " " " W. end. 8' walk }	7.05	308.71
127' E.	286 <sup>5</sup> N.	E. end 4' walk	7.47	308.29
107' E.	279' N	N.W. Cor Frame Bldg	7.7.	308.1

40

		315.76		
		100' E		
100' E	600' N	s. edge walk	2.61	313.15
"	550' N		3.4	312.4
"	500' N		3.8	312.0
"	450' N		4.4	311.4
"	400' N		4.9	310.9
"	350' N		5.7	310.1
"	300' N		7.1	308.7
		150' E		
	350' N		6.7	309.1
	400' N		5.8	310.0
	450' N		5.1	310.7
	500' N		4.6	311.2
	550' N		4.1	311.7
	600' N	s. edge walk	3.09	312.67
		200' E		
	600' N	s. edge walk	4.04	311.72
	550' N		4.7	311.1
	500' N		5.5	310.3
	450' N		4.1	309.7
	400' N		2.6	309.2

		315.76		
		200' E		
	350' N		7.5	308.3
		250' E		
	350' N		8.5	307.3
	400' N		7.6	308.2
	450' N		7.0	308.8
	500' N		4.3	309.5
	550' N		5.4	310.4
	600' N = s. walk		5.00	310.76
		300' E		
	600' N = s. walk		5.54	310.22
	550' N		6.2	309.6
	500' N		7.1	308.7
	450' N		7.8	308.0
	400' N		8.7	307.1
	350' N		9.3	306.5
		350' E		
	350' N		10.0	305.8
	400' N		9.5	306.3
	450' N		8.8	307.0
	500' N		7.8	308.0

315.76

350'. E con

550'.N		6.8	309.0
600'.N	= s. edge walk	6.00	309.76
		400'.E	
600'.N	= s. walk	6.81	308.95
550'.N		7.7	308.1
500'.N		8.7	307.1
450'.N		9.7	306.1
400'.N		10.6	305.2
350'.N		11.6	304.2

T.P.	5.56	309.18	12.14	303.62
------	------	--------	-------	--------

309.18

42

450'.E	350'.N		6.8	302.4
450'.E	400'.N		6.8	302.4
430'.E	400'.N		5.3	303.9
420'.E	450'.N		4.0	305.2
450'.E	450'.N		6.3	302.9
420'.E	450'.N		8.2	301.0
480'.E	450'.N		8.2	301.0
460'.E	500'.N		5.6	303.6
450'.E	500'.N		4.8	304.4
430'.E	500'.N		3.0	306.2
430'.E	520'.N		2.1	307.1
450'.E	520'.N		3.8	305.4
450'.E	537'.N		1.7	307.5
450'.E	550'.N		1.7	307.5
450'.E	600'.N	s sidewalk	0.56	308.62
500'.E	600'.N	= s. sidewalk	1.03	308.15
500'.E	550'.N		2.6	306.6
500'.E	500'.N		4.5	304.7
500'.E	475'.N		5.9	303.3

309.18

480' E	475' N	7.3	301.9
500' E	450' N	8.1	301.1
515' E	450' N	6.8	302.4
500' E	425' N	9.4	299.8
520' E	425' N	9.0	300.2
500' E	400' N	9.8	299.4
480' E	400' N	8.6	300.6
500' E	350' N	9.7	299.5
480' E	350' N	9.1	300.1
520' E	350' N	11.3	297.9
520' E	370' N	11.3	297.9
545' E	275' N	12.0	297.2
530' E	300' N	10.6	298.6
545' E	310' N	14.0	295.2
545' E	317' N	11.7	297.5
545' E	350' N	11.7	297.5
" "	400' N	10.1	299.1
" "	420' N	10.1	299.1
" "	433' N	8.0	301.2
" "	450' N	6.8	302.4

309.18

FR 2.13  
48

545' E	500' N	4.8	304.4		
" "	550' N	3.2	306.0		
" "	600' N = s. edge walk	1.62	307.56		
550' E	East = W. Lynx Me Kinley St.				
592' N	{ inside Edge of walk	1.82	307.36		
550' N		3.5	305.7		
522' N		4.5	304.7		
500' N		6.1	303.1		
475' N		7.8	301.4		
450' N		9.2	300.0		
433' N		10.7	298.5		
420' N		11.4	297.8		
555' E	= W. side cmt. walk				
589' N	w. edge walk	2.07	307.11		
550' N	" " "	3.72	305.46 <sup>x</sup>		
524' N	" " "	4.63	304.55		
500' N	" " "	6.54	302.60 <sup>x</sup>		
475' N		8.43	300.75		
450' N		10.17	298.99 <sup>x</sup>		
420' N		12.10	297.08		
<del>350' N</del>	<del>?</del>	<del>6.09</del>	<del>303.09</del>		
T.P.	- 0.39	299.66	9.13	300.05	Top Post Page 40

550.5'E	400'N		3.7	296.0
" "	375'N		5.2	294.5
" "	350'N		5.8	293.9
" "	317'N		6.1	293.6
" "	310'N		6.1	293.6

555.5'E	300'N	w. edge walk	6.35	293.31*
" "	317'N	" " "	6.19	293.47
" "	350'N	" " "	5.73	293.93*
" "	375'N	" " "	4.84	294.78
" "	400'N		3.70	295.96*

From (595'N-108'E) to (595'N-530'E)

Row. of Acacia Trees.

approx 20' ctrs.

5-23-38  
Miller  
Walker  
Bliss

2 Sec. Area North of Ford Bldg.  
Balboa Park for Parade Ground.

Indexed  
C.S.K.

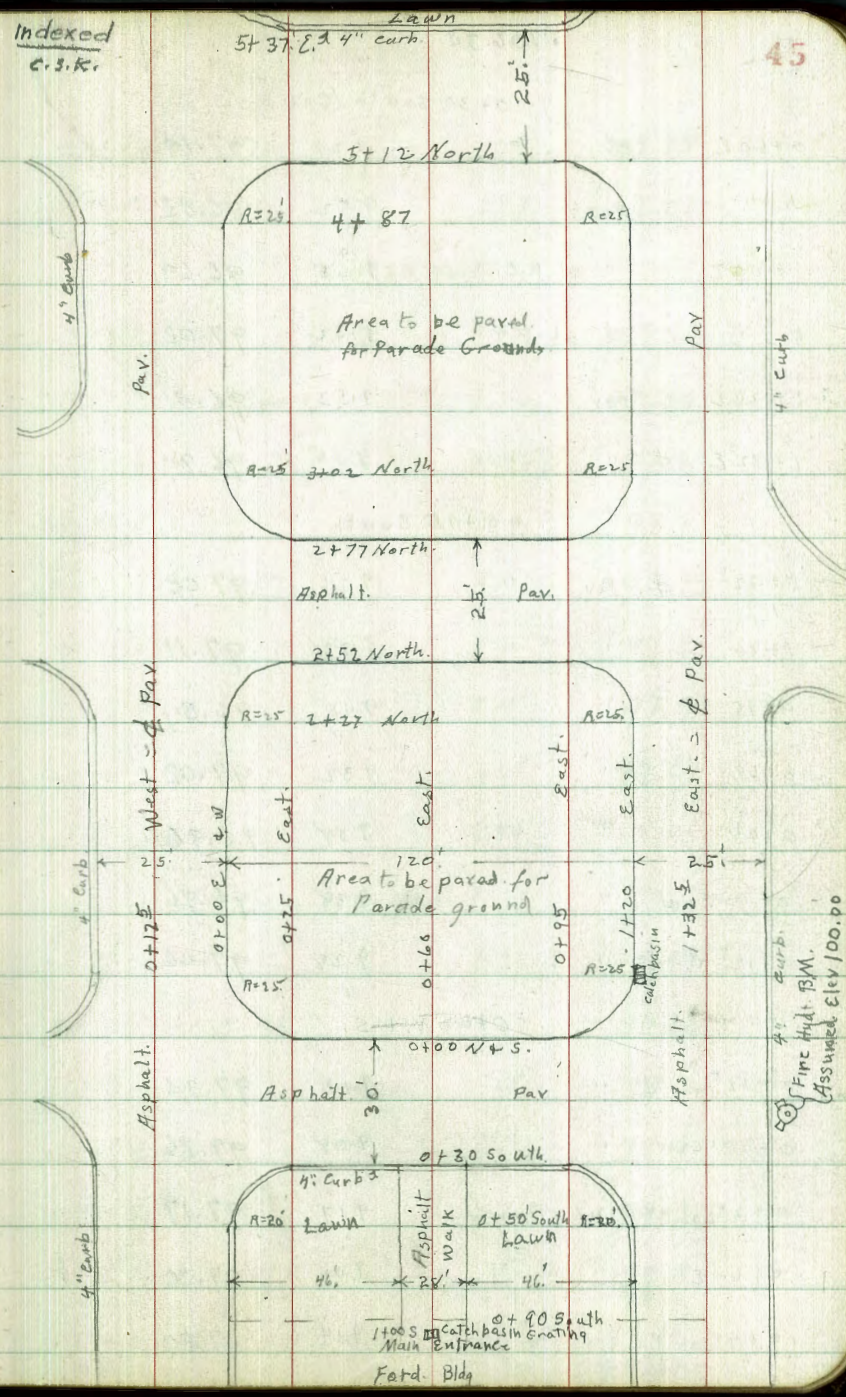
45

B.M. Top Fire Hydr. 6.34 106.34 100.00 Assumed.  
1700S-0+40 E. = catch basin Grating & Walk 11.25 95.09  
0+90 South.

0+12<sup>E</sup> W. & Pav. 11.14 95.20  
0+00 E+W " 11.09 95.25  
" " ch. 10.73 95.61  
0+60 E & Walk 9.92 96.42  
1+20 East ch. 10.28 96.06  
" " Pav 10.61 95.73  
1+32<sup>E</sup> " & " 10.65 95.69  
0+50 South

1+32<sup>E</sup> East & Pav. 10.00 96.34  
1+20 " " 9.95 96.39  
" " ch. at P.C. 9.54 96.80  
0+60 " & Walk 11.00 95.34  
0+00 E+W ch. at P.C. 9.69 96.65  
" " Pav 10.05 96.29  
0+12<sup>W</sup> & " 10.05 96.29  
0+30 South

0+12<sup>W</sup> & Pav 9.64 96.70  
0+00 E+W " 9.67 96.67  
0+25 E " at P.C. 9.67 96.67  
0+25 E ch. at P.C. 9.29 97.05



106.34

0+30 South (con)

0+60 E	cb.	9.20	97.14
" "	pav	9.52	96.82
1+00 E	" at.P.C	9.45	96.69
" "	cb at.P.C	9.32	97.02
1+20 E	pav	9.53	96.81
1+32 <sup>5</sup> E	♀ "	9.55	96.79

0+15 South.

1+32 <sup>5</sup> E	♀ Pav	9.26	97.08
1+20	"	9.23	97.11
0+95	"	9.45	96.89
0+60	"	9.32	97.02
0+25	"	9.38	96.96
0+00 E+W	"	9.38	96.96
0+12 <sup>5</sup> W	♀ "	9.28	97.06

0+00 N. + S.

0+12 <sup>5</sup> W	♀ "	9.00	97.34
0+00 E+W	"	9.08	97.26
0+25 at.P.C	" + Ground.	9.17	97.17
0+60 E	" " "	9.04	97.30
0+95 at.P.C	" " "	9.14	97.20

106.34

46

1+20 E	pav	9.09	97.25
1+32 <sup>5</sup> E	"	8.97	97.37

0+25 North.

1+32 <sup>5</sup> E	pav	8.42	97.92
1+20 E	" + Ground.	8.90	97.44
1+17 E	"	8.4	97.9
0+95 E	"	8.4	97.9
0+60 E	"	8.0	98.3
0+25 E	"	8.5	97.8
0+03 E	"	8.4	97.9
0+00 E	Pav + "	8.67	97.67
0+12 <sup>5</sup> W	♀ Pav	8.44	97.90

0+50 North.

0+12 <sup>5</sup> W	♀ Pav	7.91	98.43
0+00 E+W	" + Grd.	8.17	98.17
0+03 E	"	7.8	98.5
0+25 E	"	7.7	98.6
0+60 E	"	7.1	99.2
0+95 E	"	7.5	98.8
1+17 E	"	7.9	98.4
1+20 E	Pav + "	8.19	98.15
1+32 <sup>5</sup> E	♀ "	7.93	98.41

Catch basin  
Grating



106.34

1+00 North

1+32 <sup>5</sup> E	± Pav	6.87	99.47
1+20 E	" + Grd	7.19	99.15
1+17 E	"	7.0	99.3
0+95 E	"	6.6	99.7
0+60 E	"	6.2	100.1
0+25 E	"	6.7	99.6
0+03 E	"	6.9	99.4
0+00 E + W. Pav	"	7.17	99.17
0+12 <sup>5</sup> W	± "	6.96	99.38

1+50 North

0+12 <sup>5</sup> W	± Pav	5.91	100.43
0+00 E + W	" + Grd	6.16	100.18
0+03 E		5.7	100.6
0+25 E		5.6	100.7
0+60 E		5.3	101.0
0+95 E		5.6	100.7
1+17 E		5.8	100.5
1+20 E	Pav + Grd	6.20	100.14
1+32 <sup>5</sup> E	± "	5.99	100.45

106.34

2+27 North

1+32 <sup>5</sup> E	± Pav	4.43	101.91
1+20 E	" + Grd at Pav. P.C.	4.73	101.61
1+17 E	"	4.4	101.9
0+95 E	"	4.3	102.0
0+60 E	"	3.7	102.6
0+25 E	"	4.3	102.0
0+03 E	"	4.4	101.9
0+00 E + W Pav	+ " at Pav. P.C.	4.60	101.74
0+12 <sup>5</sup> W	± "	4.36	101.98

2+52 North

0+12 <sup>5</sup> W	± Pav	3.92	102.32	
0+00 E + W	"	4.19	102.15	
0+25 E	" + Grd at Pav. P.C.	4.01	102.33	
0+60 E	" " "	4.19	102.15	
0+95 E	" " " at Pav. P.C.	4.16	102.18	
1+20 E	Pav	4.20	102.14	
1+32 <sup>5</sup> E	± "	3.93	102.41	
T.P.	8.21	111.11	3.44	102.90

47

111.11

2+77 North

1+32 <sup>5</sup> E $\phi$ Pav	8.20	102.91
1+20 E "	8.45	102.66
0+95 E " + Grd	8.46	102.65
0+60 E " " "	8.31	102.80
0+25 E " " "	8.38	102.73
0+80 E W "	8.45	102.66
0+12 <sup>5</sup> E $\phi$ "	8.18	102.93

3+02 North

0+12 E $\phi$ Pav	7.60	103.51
0+00 E W " + Grd at Pav P.C.	7.86	103.25
0+03 E "	7.5	103.6
0+25 E "	7.3	103.8
0+60 E "	7.2	103.9
0+95 E "	7.6	103.5
1+17 E "	7.6	103.5
1+20 E Pav + " at Pav P.C.	7.99	103.12
1+32 <sup>5</sup> E $\phi$ "	7.64	103.43

111.11

3+50 North

1+32 <sup>5</sup> E $\phi$ Pav	6.65	104.46
1+20 E " + Gr.	6.91	104.20
1+17 E "	6.6	104.5
0+95 "	6.4	104.7
0+60 E "	6.1	105.0
0+25 E "	6.4	104.7
0+03 E "	6.5	104.6
0+00 E W Pav + "	6.96	104.15
0+12 <sup>5</sup> W $\phi$ "	6.58	104.53

400' North

0+12 <sup>5</sup> W $\phi$ Pav	5.60	105.51
0+00 E W " + Grd.	5.95	105.16
0+03 E "	5.7	105.4
0+25 E "	5.5	105.6
0+60 E "	5.3	105.8
0+95 E "	5.4	105.7
1+17 E "	5.6	105.5
1+20 E Pav + "	6.08	105.03
1+32 <sup>5</sup> E $\phi$ "	5.70	105.41

48

111.11

4+50 North

1+32 <sup>S</sup> E $\phi$ Pav	4.69	106.42
1+20 C " 49rd	4.96	106.15
1+17 E "	4.6	106.5
0+95 E "	4.6	106.5
0+60 E "	4.2	106.9
0+25 E "	4.5	106.6
0+03 E "	4.6	106.5
0+60 E + W pav + "	4.97	106.14
0+12 <sup>S</sup> W $\phi$ "	4.67	106.44

4+87 North

0+12 <sup>S</sup> W $\phi$ pav	3.96	107.15
0+00 E + W " + Grd. at Pav P.C.	4.33	106.78
0+03 E "	4.0	107.1
0+25 E "	4.0	107.1
0+60 E "	3.8	107.3
0+95 E "	4.1	107.0
1+17 E "	4.0	107.1
1+20 E ' pav + " at Pav P.C.	4.26	106.85
1+32 <sup>S</sup> E $\phi$ "	3.92	107.19

111.11

5+12 North

1+32 <sup>S</sup> E $\phi$ Pav	3.46	107.65
1+20 "	3.86	107.25
0+95 " + Grd at Pav P.C.	3.74	107.37
0+60 E " " "	3.49	107.62
0+25 E " " " " " " "	3.70	107.41
0+00 E + W "	3.89	107.22
0+12 <sup>S</sup> W $\phi$ "	3.51	107.60

5+37 North

0+12 <sup>S</sup> W $\phi$ Pav	2.99	108.12
0+00 E + W "	2.34	108.77
0+25 " at ch P.C.	3.25	107.86
0+25 ch " " " "	2.88	108.23
0+60 Pav	3.12	107.99
0+60 ch	2.69	108.42
0+95 pav at ch P.C.	3.22	107.89
0+95 ch " " " "	2.89	108.22
1+20 pav	3.31	107.80
1+32 <sup>S</sup> $\phi$ "	2.97	108.14

chk BM.

11.11

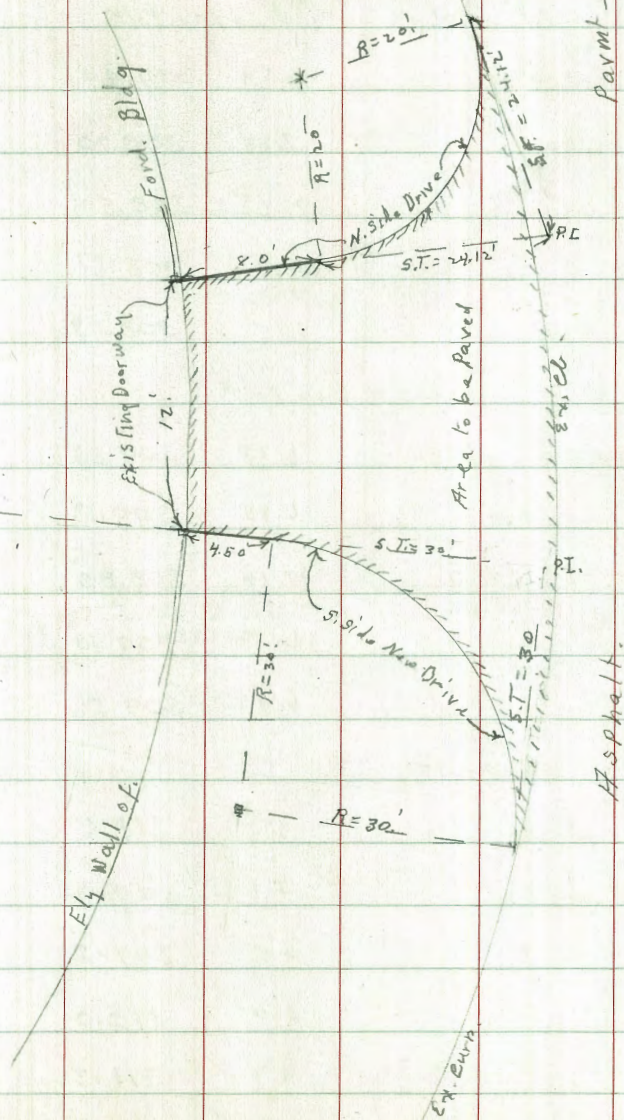
100.00 ✓

49

X Sec for New Paved Driveway  
East Door. Ford. Bldg Balboa Park.

B.M. Top Fire Hydrant

100.00 See Page 45.



7-28-34. X Sec. Alley BIK 146 U.H.

Miller  
Walker  
Bliss

Indexed  
C.S.K.

BM B.P. 6.01 315.98 309.97 g.e. Polk  
+Mississippi

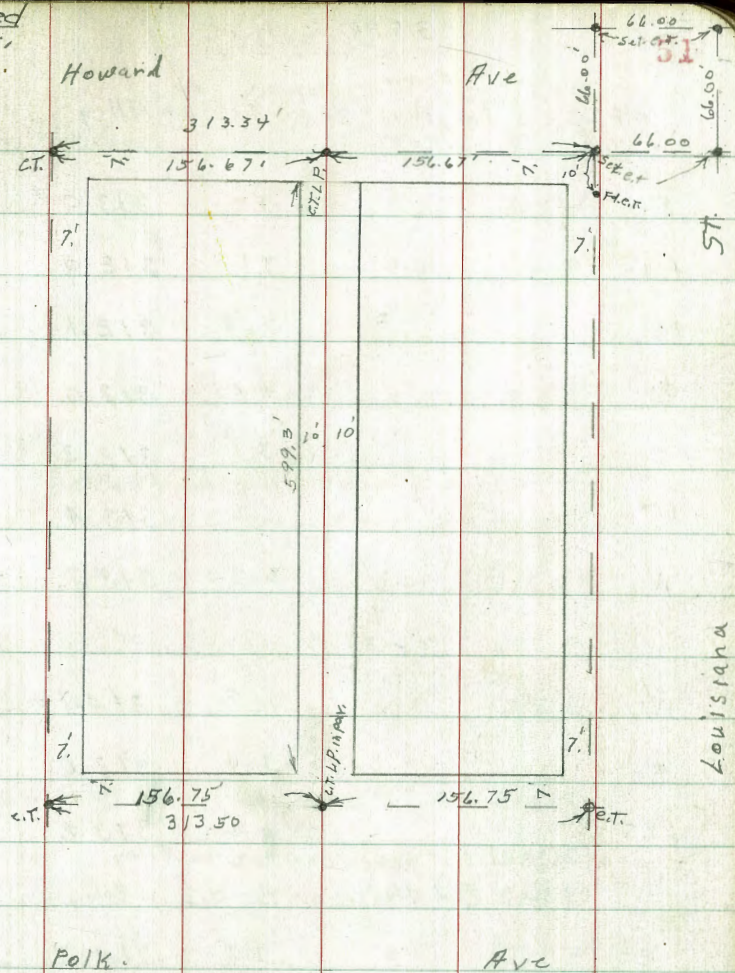
14' S. of N. = N. Line Polk.

W	cont. d		6.54	309.44
W	pay		7.24	308.70
±	"		7.44	308.50
E.	"		7.71	308.27
E.	cont. d		7.15	308.83
0+00 = N. Line Polk.				
0.10 E. of E. line of d	N. End.		6.75	309.23
" " "	Pay " "		6.85	309.13
±	" " "		7.18	308.80
0.10 E. of W. Line	" "		6.40	309.18
" " " "	" "		6.42	309.56

0+05

W			3.4	312.6
+2			6.1	309.9
±			6.5	309.5
+8			6.0	310.0
E			4.7	311.3

BM B.P.



315.94 s.w. Howard  
+Mississippi

315.98

Frame.

0+23 = S. End of House on E, 0.5' in Alley

E 3.0 313.0

+3 3.1 312.9

+5 3.9 312.1

E 4.0 312.0

+5 3.7 312.3

+7 2.6 313.4

W 2.3 313.7

0+33 N.

W 1.9 314.1

E 2.4 313.6

+9.5 2.2 313.8

0+42 S. End slat fence on W. 0.2' in Alley.

0+50 N. End. House on E. 0.3' in Alley

E 2.7 314.3

E 1.7 314.3

W 1.6 314.4

0+78 S. End S. Entrance garage on E dirt-floor 3' Backs.

E-3 = W. Edge doorway 0.7 315.3

315.98

1+00

0.2' E. of W. = fence

0.3 315.7

E 0.4 315.6

E 0.0 316.0

T.P. 7.21 323.04 0.15 315.83

1+43 { N. End. of above Fence on W. 0.2' in Alley  
Garage on E. conc. floor 3.0' Backs

E-30 = floor 6.47 316.57

E 6.6 316.4

E 6.8 316.2

W. 6.9 316.1

+6 7.0 316.0

W-10 6.4 316.6

W 6.3 316.7

E 6.2 316.8

E 6.0 317.0

2+00

E 5.4 317.6

E 4.9 318.1

+9.8 S. End. Bldg 0.2' in Alley.  
W. 4.9 318.1

+1. 5.4 317.6

+10. 6.1 316.9

59

323.04

2+21 S. End double garage on E. ent. floor 4.8' Back		
W+0.2 E side Bldg.	5.5	317.5
⊕	5.2	317.8
E	4.9	318.1
+ 1.8 W. End. ent. apron	4.82	318.22
+ 4.8 floor	4.20	318.84
2+35 N. End. above Bldg on W. 0.2' in Alley		
2+38		
W. line = E. End. ⊕ 24" ent. walls	5.51	317.53
2+45 = N. End. above double garage on E.		
= W. End. ent. apron	4.60	318.44
= floor.	4.23	318.81
2+50		
E-23 = ent. walk W. End.	4.54	318.46
E	4.7	318.3
⊕	4.8	318.2
+ 9.5 = S. End. Board. Fence	5.3	317.7
W+10	5.7	317.3
2+52 S. End. 5 garages. on E. dirt floor. 4.6' Back		
E-4.6 = floor	4.4	318.6

323.04

53

3+00 = N. End of above garages. on E. 4.0' Back		
W-10	4.9	318.1
W = N. End. above fence 0.2' in Alley	4.8	318.2
⊕ Top. Survey M.H.	4.74	318.30
E	4.4	318.6
+ 4.0 = floor	4.1	318.9
3+05 garage on E. dirt. floor on Line		
E = floor	4.4	318.6
3+35 double garage on W. ent. floor 3.0' Back		
W-3.0 = floor	4.67	318.37
0.4 E of W. = E. End. ent. apron	4.95	318.09
3+46		
0.7 W of W. = ⊕ E. End. 30" ent. walk	4.40	318.24
3+50		
E	4.1	318.9
⊕	4.9	318.1
W	5.0	318.0
+ 10 present. waterway.	5.5	317.5
S. End.		
3+54 = A double garage on W. ent. floor 5.5' Back		
W-5.5 = floor	5.28	317.76

323.04

323.04

54

out of place  
 3+75 = S. End. S. Entrance garage on E. dirt floor Back

E-5 = floor. 3.4 319.6

3+70

W-5.5 N. End. garage 5.20 317.84

W 4.6 318.4

⊕ 4.4 318.6

+7 4.1 318.9

⊖ 3.6 319.4

3+80

E 2.6 320.4

+4 3.8 319.2

⊕ 4.0 319.0

W 4.0 319.0

+1. 4.7 318.3

+5.1 5.0 318.0

4+00

W-5 4.4 318.6

W 3.8 319.2

⊕ 3.5 319.5

+6 3.3 319.7

E. 2.5 320.5

4+12 garage on E. floor 0.3 Back.

E-0.3 = floor 2.7 320.3

4+35 N. End. N. Entrance garage on E. dirt floor 0.3 Back  
 E-0.3 = floor 1.9

E 2.2 320.8

⊕ 3.1 319.9

W. 3.5 319.5

4+62 S. End. S. Entrance garage on E. dirt floor 0.5 Back  
 E-0.5 = floor 1.6 321.4

4+75

W-4 2.3 320.7

W 2.2 320.8

⊕ 1.8 321.2

E 1.6 321.4

4+85 garage on E. dirt floor 0.5 Back

E-0.5 = floor 1.6 321.4

5+00

W. 2.2 320.8

+3 1.7 321.3

⊕ 1.7 321.3

E 1.6 321.4



323.04

T.P. 5.97 327.31 170 321.34

5+12 double garage on W. cnt. floor 23' W.

W-23 = floor 6.93 320.38

5+23

1 E 5.2 322.1

E 5.3 322.0

+7 5.6 321.7

W 6.1 321.2

+5 6.3 321.0

{ S. End. garage on W. conc. floor 0.3 Back.  
 5+26 " " 3 " S. W. E dirt. " 8' "

W-0.3 floor 5.13 322.18

W 5.3 322.0

E 5.0 322.3

E 5.2 322.1

+8 = floor 4.6 322.7

5+50 = N. End above 3 garages on E.

E-8' = floor 4.3 323.0

5+43. out of place

W-2.3 = E End cnt. walk. 5.60 322.31

327.31

5+75

E 3.8 323.5

E 4.1 323.2

W 4.2 323.1

5+95

W 3.6 323.7

E 3.3 324.0

E 3.0 324.3

5+99<sup>3</sup> = S. Line Howard Ave.

E = cnt. ch. S. End. 2.14 325.12

E pav. " " 2.45 324.86

E " " " " 3.03 324.28

+5 3.33 323.98

W+0.3 " " 3.25 323.96

W+0.3 cnt. ch. " " 3.30 324.01

14' N. of S. line = S. ch.

W cnt. ch. 3.46 323.85

W pav. 3.80 323.51

E " 3.36 323.95

E " 2.84 324.43

E cnt. ch. 2.36 324.95

T.P. 1.70 325.47 3.54 323.77

B.M. N.W. Miss. + Howard 9.53 315.94

55

8-17-38  
Miller  
Walker.

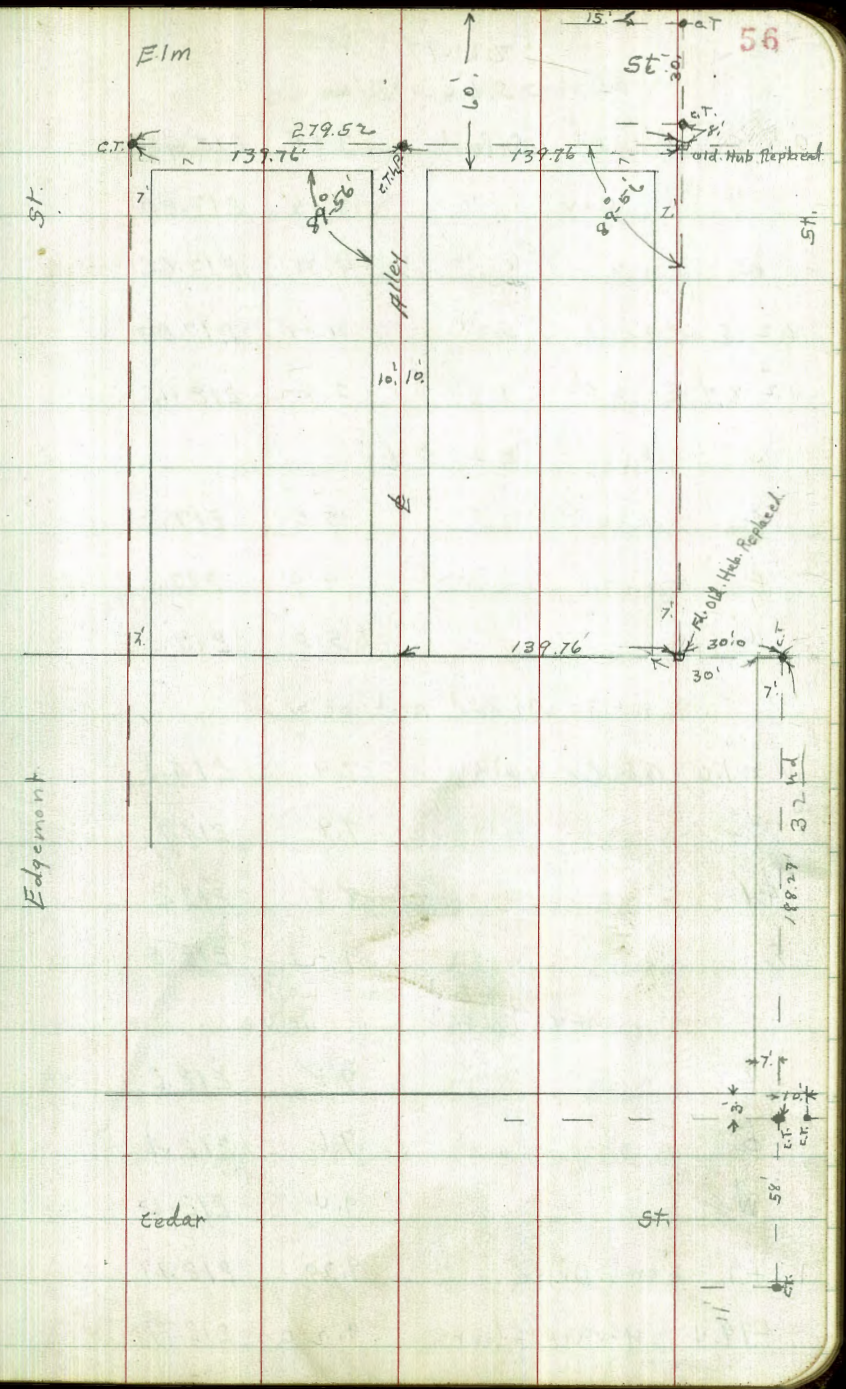
X Sec. Alley BIK. 6 Cullens  
Arlington Hts Add  
Bet. Edgemont + 32nd s. of Elm.

BM. B.P. 279 221.97 270.18

S. E. 32nd  
+ Elm St

17.5' N of S. = S. d. Elm

E.	ch	2.82	219.15
E	Gutter	3.16	218.81
E	"	3.24	218.73
W	"	3.27	218.70
W	ch	2.95	219.02
12' N of S. Line			
W	ch	2.86	219.11
W	G	3.15	218.82
E	"	3.11	218.86
E	"	3.02	218.95
E	ch	2.74	219.23
8' N of S. Line			
E	ch	3.02	218.95
E	G	3.30	218.67
E	"	3.34	218.63
W	"	3.27	218.70
W	ch	2.78	219.19



		221.97		
	0+00 = S. line	E/m		
0.2	E of W = ch	S. End	3.05	218.92
"	"	"	4.04	217.89
"	"	"	4.31	217.66
0.2	E of E	"	4.04	217.89
0.2	E of E	ch	3.82	218.15
		0+08		
E			5.0	217.0
E			4.9	217.1
W			5.0	217.0
		0+30 N. End. ent: on W		
W-1.0	NE. Cor walk		7.9	214.1
W			7.9	214.1
E			8.8	213.2
E			9.2	212.8
		0+46 { S. End. ent. walk W side " Drive		
E			9.8	212.2
E			9.6	212.4
W			9.4	212.6
+1.	= ent Drive		9.20	212.77
+19.4	= garage floor		9.20	212.77

		221.97		
		0+54.5 = S. side ent. Drive		
W-1	= drive		9.27	212.70
		0+58		
W-5			11.7	210.3
W-1			11.7	210.3
W			9.6	212.4
E			9.8	212.2
E			9.5	212.5
+5			11.6	210.4
		0+69		
-10			13.2	208.8
6			13.3	208.7
+5			12.0	210.0
E			10.0	212.0
W			13.0	209.0
+1			13.7	208.3
+5			13.7	208.3
T.P.	0.25	209.39	12.83	209.14

209.39

0+75

-10	1.5	207.9
W	1.5	207.9
±	1.2	208.2
E	1.7	207.7
+10	1.9	207.5

0+93

-10	3.6	205.8
E	3.0	206.4
±	3.0	206.4
W	3.3	206.1
+10	3.4	206.0

1+00

-10	5.5	203.9
W	5.4	204.0
±	6.0	203.4
E	5.7	203.7
+10	7.4	202.0

1+10

-15	9.4	200.0
E	9.0	200.4

209.39

±	9.6	199.8
W	10.0	199.4
+15	10.1	99.3

1+22

-15	12.8	196.6
W	12.6	196.8
±	11.9	197.5
E	11.1	198.3
+15	10.4	199.0

1+33 Proposed Culvert

-15	10.2	199.2
E	11.5	197.9
±	12.3	197.1
W	12.8	196.6
+20	13.7	195.7

1+48

W-20	13.7	195.7
W	12.6	196.8
E	11.9	197.5
E	10.9	198.5
+15	10.2	199.2

209.39  
1455

-15	10.4	199.0
E	10.7	198.7
⊕	11.8	197.6
+7	12.0	197.4
W	10.5	198.9
+5	9.1	200.3
+10	9.2	200.2

1482

-10	7.4	202.0
W	7.2	202.2
⊕	6.8	202.6
E	6.8	202.6
+10	7.1	202.3

2400

-10	4.2	205.2
E	4.4	205.0
⊕	4.3	205.1
W	4.4	205.0
+10	5.4	204.0

209.39

2402

W-10	Top. wall	2.9	206.5
W	" "	2.9	206.5
+1		4.0	205.4
⊕		4.1	205.3
E		3.9	205.5
+10		3.6	205.8

2426

-10		1.3	208.1	
E		0.9	208.5	
T.P.	1272	221.72	0.39	209.00
⊕		12.3	209.4	
W		11.3	210.4	
+10		11.3	210.4	

2452

-10		7.0	214.7
W		7.3	214.4
⊕		7.0	214.7
E		8.2	213.5
+10		9.1	212.6

59

	221.72		
	2+77		
-10	4.2	217.5	
E	3.6	218.1	
⊕	2.5	219.2	
W	2.0	219.7	
+10	2.0	219.7	
T.P.	12.18	233.46	0.44 221.28
	2+88 N. side Garage on W dirt floor 6.4 Back		
W-6.4: floor	9.83	223.63	
W	10.6	222.9	
⊕	11.3	222.2	
+5	11.3	222.2	
E	13.8	219.7	
+10	15.0	218.5	
	3+02		
-10	12.4	221.1	
E	10.3	223.2	
⊕	9.9	223.6	
+7	10.0	223.5	
W	8.2	225.3	

	3+20		
W	6.2	227.3	
⊕	6.9	226.6	
E	7.5	226.0	
+5	7.7	225.8	
	3+30		
E-5	6.1	227.4	
E	5.8	227.7	
⊕	5.3	228.2	
W	5.3	228.2	
	3+35		
W	3.9	229.6	
⊕	3.3	230.2	
+5	3.4	230.1	
E	5.0	228.5	
+5	5.3	228.2	
	3+50 garage on W dirt floor 6.2 Back		
E-5	3.2	230.3	
E	2.9	230.6	
⊕	2.9	230.6	
W - floor	2.5	231.0	

233.46

243.39

61

T.P. 10.78 243.39 ✓ 0.85 232.61

E

4+50

4.1 239.3

E

3.8 ✓ 239.6

3+79 E 30' cont. walk. on W. 0.5 Back

W

3.5 239.9

W - 0.5 = 2 End. walk. 9.4 233.97

4+75

W 9.6 233.8

W

2.5 240.9

E 8.9 234.5

E

2.5 240.9

E 8.5 234.9

E

2.8 240.6

+2 9.4 234.0

5+06<sup>18</sup> S. End. Alley = Board Fence

+5 9.4 234.0

E

2.3 241.1

4+00

E

2.2 241.2

E 7.2 236.2

W

2.2 241.2

E 4.0 236.4

T.P.

0.24 232.85 10.74 232.61

W 6.6 236.8

Orig BM

12.67 220.18 ✓

4+15

W 5.7 237.7

E 5.7 237.7

E 5.9 237.5

9-3-38  
Miller  
Walker  
Bliss

Levels N. E. Cor Ray + Wightman

Indexed  
C.S.K.

357.66

62

BM B.P.	6.02	357.66	351.64	s.w. Ray + Wightman	1.04 N	5.11	352.55
Levels in E. Gutter of Ray N of Wightman							
217. N = S. End. Ex Curb Outlet	4.73	352.93			100' N	5.25	352.41
215 N = N. Line Alley	4.73	352.93			88' N	5.27	352.39
207 <sup>5</sup> N	"	"	4.74	352.90	86' N	5.35	352.31
200' N	S "	"	4.74	352.92	82' N	5.37	352.35
192' N			4.74	352.82	78' N	5.45	352.21
189' N			4.95	352.71	74' N	5.35	352.31
186' N			4.83	352.83	60' N	5.40	352.26
175' N			4.90	352.76	52' N	5.50	352.16
166' N			4.96	352.70	45' N	5.49	352.17
163' N			5.03	352.63	33' N	5.60	352.06
157' N			4.97	352.69	28' N	5.70	351.96
153' N			5.00	352.66	22' N	5.57	352.09
147' N			5.18	352.48	11' N	5.63	352.03
140' N			5.06	352.65	0+00 = N. Line Wightman	5.66	352.00
130' N			5.20	352.46	+4'	5.66	352.00
122' N			5.04	352.62	+8' = ctr Return	5.63	352.03
118' N			5.19	352.47	+12	5.72	351.94
116' N			5.02	352.64	+16 = N. Gutter of Wightman St.	5.81	351.85
					0+00 = E. Line Ray St	5.94	351.68
					0+15 E		



0+25 E	6.03	351.63	2+53 - W. of Lin. Grimm	7.13	350.53	in 45 Gutter
0+45 E	6.23	351.43	20 S. of 2+53 = 4 Wightman	7.32	350.34	351.64 4.06 357.70
0+55 E	6.28	351.38	40 S. " 2+53 = S. of Line	7.67	349.99	
0+65 E	6.29	351.37				Gutter Grades.
0+80 E	6.30	351.34				
0+85 E	6.30	351.36	N. Line Wightman 0+00	Ray St Ray	Wightman	
1+00 E = W. Line Alley	6.30	351.36	352.07 5.63		N. Line Wight	252.07 5.63 ✓
1+07 <sup>5</sup> E	6.35	351.31	0+25		Return 1	252.03 5.67 ✓
1+15 E	6.34	351.32	0+50		Return 2	251.99 5.46 +0.50 51.95
1+34	6.55	351.11	0+75		Return 3	51.95 5.75 ✓
1+36	6.64	351.02	1+00		E. Line Ray 0+00 4	51.91 5.79 ✓
1+40	6.62	351.04	1+25		0+25	51.79 5.71 ✓
1+60	6.77	350.89	1+50		0+50	51.67 6.03 ✓
1+70	6.83	350.83	1+75		0+75	51.55 6.15 ✓
1+80	6.77	350.89	2+00		W. Alley 2+00	51.43 6.27 ✓
1+90	6.90	350.76	2+17		E. Alley 178	51.34 6.36 ✓
2+00	6.92	350.74			E. Alley 1736	51.23 6.47 ✓
2+28	7.04	350.60			+59	51.09 6.61 ✓
2+40 W. Line Grimm St	7.09	350.57			+75	50.98 6.72 ✓
2+46	7.08	350.58			2+00	50.44 6.86 ✓
					2+25	50.70 7.00 ✓
					2+40	50.62 7.08 ✓

9-3-38 Miller Walker Bliss  
 X. Sec. Alley BIK. 1 North Highland Park.  
 Boundary st to 33rd st.  
 bet. Bramson & El Cajon Blvd.

Indexed  
 C.S.K.

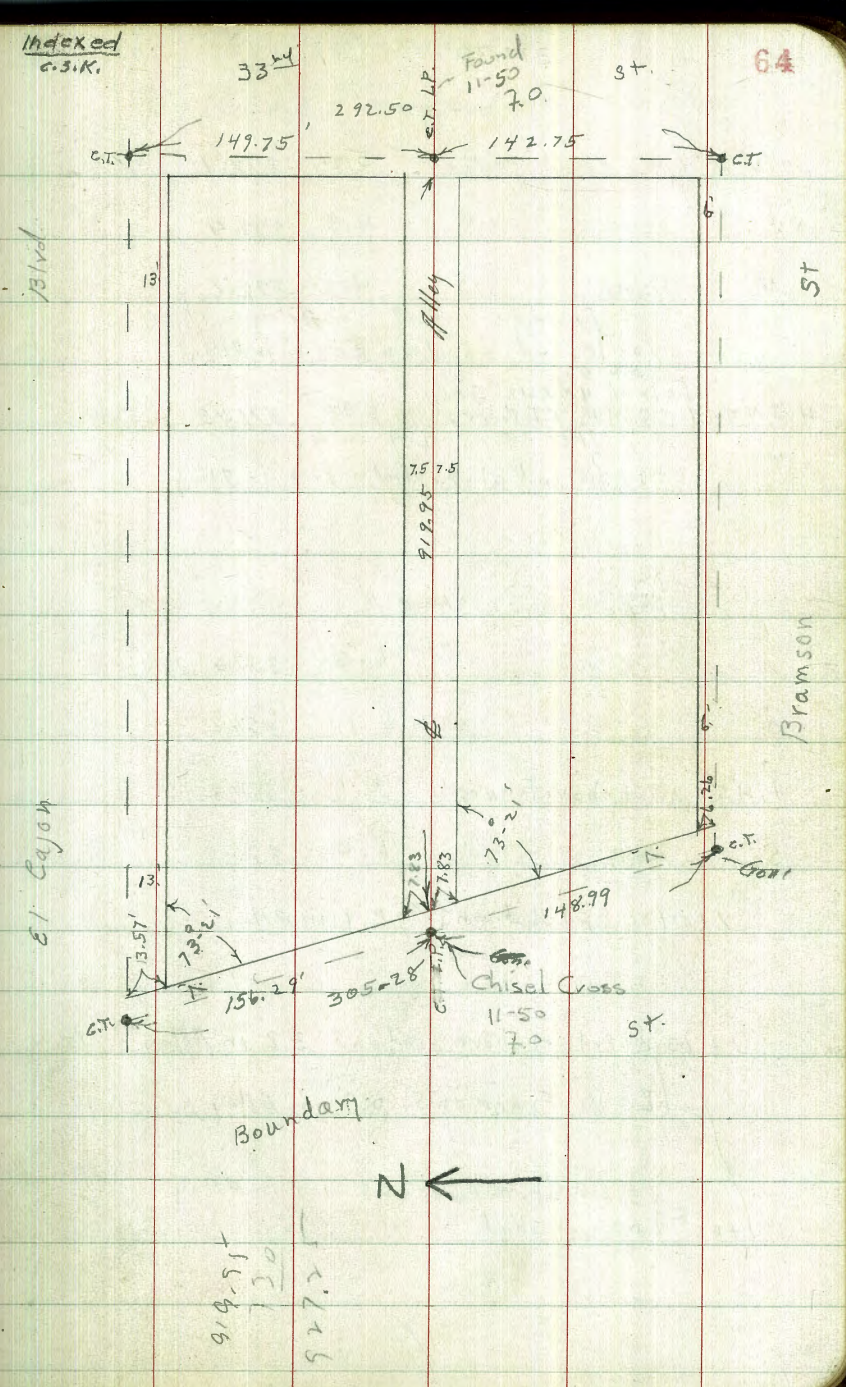
33<sup>rd</sup>

Found  
 11-50  
 70

st.

64

B.M.	3.05	377.80	374.25	S.W. 33 <sup>rd</sup> + El Cajon
14' E. of W. Line = W. ch. of 33 <sup>rd</sup> .				
N-30.	Top. curb.	4.25	373.02	
N-30.	Gutter	4.67	372.63	
N	"	5.14	372.16	
N	Top. ch.	4.67	372.62	
±	pav	5.28	372.02	
S	"	5.41	371.89	
S	ch.	5.02	372.28	
S+23	"	5.14	372.12	
S+23	G. Pav	5.67	371.63	
0+00 = W. Line 33 <sup>rd</sup> st.				
0.2 Wfs.	ch. + pav	W. end.	4.85	372.45
±	pav	" "	5.03	372.27
N.	ch. + Pav	" "	4.60	372.70
0+10				
N		4.2	373.1	
±		4.5	372.8	
S.		4.8	372.5	



377.30

0750

0.5 N. of S. = E. End. Fence 5.2 372.1

E 4.9 372.4

N. 4.7 372.6

Fence 2.9 in Alley

0+90 E. End. shed on S. 2.0 in Alley

4.5 N of E. Co. M.H. C.I. Crer. 5.87 371.43 Top.

Fence 2.9 in Alley

0+94 W. End above shed 1.9 in Alley

1400

N 6.3 371.6

E 6.1 371.2

+ 45 = W. End above Fence 6.1 371.2

S 6.4 370.9

1401 E. End. shed on S. 2.9 in Alley

1+13 W. End. of above shed on S. 3.2 in Alley

E. " Fence on S. 0.9 in Alley

1+42.5 E. End. above Fence on S. 1.7 in Alley

W. " Shed " " " " "

377.30

65

1+50 = W. End. above shed on S. 1.7 in Alley

S 7.4 368.9

E 7.1 370.2

N 6.7 370.6

2+00

N 7.5 368.8

E 7.8 368.5

S 8.0 368.3

+5 8.0 368.3

2+32 garage on S. dirt floor 9.0 Back

S-9.0 = floor 8.6 368.7

2+50

S-5 8.6 368.7

S 8.4 368.7

E 8.2 368.1

N 8.0 368.3

3+00

N 8.3 368.0

E 8.4 368.7

S 8.9 368.4

+5 9.0 368.3

377.30

3+50

S-5	8.4	367.9
S	9.3	368.0
±	9.3	368.0
N	8.4	368.5

3+75

N	9.0	368.3
±	8.9	368.4
S	8.8	368.5
+5	8.6	368.7

T.P.	5.34	375.21	7.43	369.87
------	------	--------	------	--------

3+75

S-5	9.9	365.3
S	9.9	365.3
±	10.0	365.2
N	9.0	366.2
+5	9.0	366.2

375.21

3+90 N.L.	} ± Wash.
3+93 S.	

66

-10	12.1	363.1
N	12.2	363.0
±	12.3	362.9
S	12.5	362.7
+10	13.0	362.2

4+00

-5	9.4	365.8
S	9.4	365.8
±	9.7	365.5
N	8.4	366.8
+5	8.4	366.8

4+25

-5	7.4	367.8
N	7.8	367.4
±	8.7	366.5
S	8.9	366.3
+5	8.4	366.8

375.21 ✓

4+50

-5	7.6	367.6
S	7.4	367.6
±	8.2	367.0
N	8.0	367.2
+5	7.2	368.0

5+00

N	6.9	368.3
±	6.8	368.4
S	7.0	368.2

5+50

S	5.6	369.6
±	5.3	369.9
N	5.1	370.1

5+64 Garage Entrance on N 6' Back

N-6 floor	3.50	371.71
N-1 S. End Conc. apron.	5.02	370.19
N	5.0	370.2

375.21 ✓

6+00

67

N	4.7	370.5
±	4.8	370.4
S	4.9	370.3
+5	5.3	369.9

6+43 Garage on S. cmt. floor 32' 0" Back

S-32' = floor 5.33 369.88

S-1.7' N. End cmt. strips 4.82 370.39

6+50

S-5	5.0	370.2
S	4.7	370.5
±	4.4	370.8
N	4.1	371.1

6+80

N-5	4.0	371.2
N	4.1	371.1
±	3.9	371.3
S	4.0	371.2
+5	4.5	370.7

375.21 ✓

7+06 Garage on S. 0.5' Back

S-0.5

3.8 371.4

7+18 garage on S. 0.3 Back

S 3.5 371.2

E 3.5 371.7

N 3.5 371.2

+10 3.5 371.7

7+40

-10 3.0 372.2

N 3.2 372.0

E 3.2 372.0

S 2.9 372.3

+3 3.7 371.5

7+70

S 2.3 372.9

E 2.4 372.8

N 2.5 372.7

+10 2.4 372.8

TP 5.66 378.66 2.21 373.00 ✓

378.66

3 ✓

7+86. W. End. W. Entrance Garage on S. 1

S-3' = floor N. Edge 5.6 373.1

7+90

N 5.0 373.2

+3 5.5 373.2

E 5.6 373.1

S 5.7 373.0

+10 6.3 372.4

8+07 garage on S. dirt floor 10' Back

-10 5.7 373.0

S 5.4 373.3

E 5.3 373.2

N 5.0 373.2

+10 5.2 373.5

8+31 garage on S. emb. floor 11' Back

S-11 = floor 5.75 372.91

8+50

N 4.6 374.1

E 4.6 374.1

S 4.9 373.8

+5 5.7 373.0

378.64

8+75

S-4	5.2	373.5
S	4.4	373.9
±	4.6	374.1
N.	4.7	374.0
N+0.1 Top of Board wall.	4.1	374.6

9+00

N. Top of Board wall	4.1	374.6
+0.2 Top of Board wall	4.8	373.9
±	4.8	373.9
S	5.0	373.2

9+19 25 ± Sta. = E. Line Boundary st. diagonal

0.2 N. of S. = cl. E. End.	5.17	373.49
0.2 " " pay " "	5.19	373.42
± " " "	5.11	373.55
+7.2 " " "	4.87	373.79
+7.2 cl. " "	4.62	374.04

378.64

10' W. of E. Line = E. cl. Boundary.

N Top. cl.	4.77	373.89
N pay	5.31	373.29
± "	5.49	373.12
S "	5.65	373.01
S. cl.	5.19	373.47

T.P.	2.99	379.95	1.70	376.96
T.P.	4.90	378.06	6.79	373.16
BM. S. E. Iowa + El Cajon	5.25	372.81		372.93

69

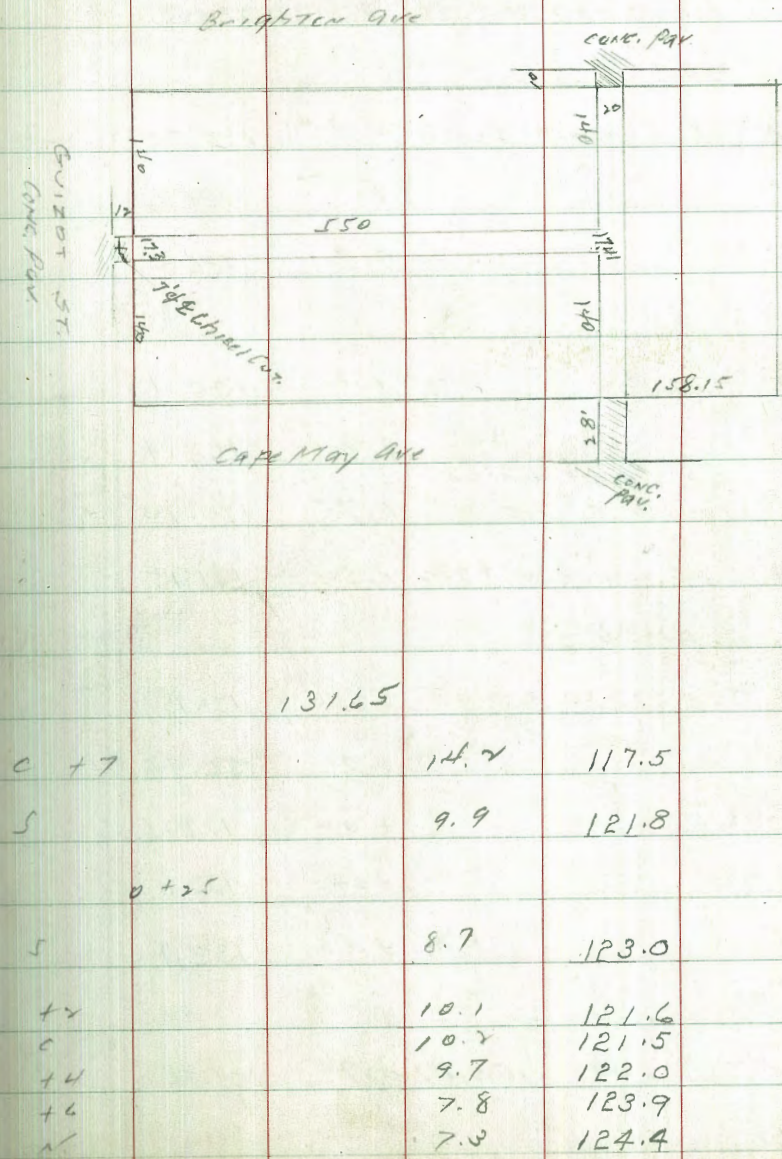
indexed  
e.s.r.

Cross Sec. of alleys BIK 91 Pt. Loma N.S.

SEOP	12.49	119.89	107.40	Brighton Guizot
0-12 = E cb Guizot				
N	par.	2.26	115.63	
C	"	3.72	116.16	
S	"	3.15	116.74	
0+00 FL Guizot				
S	cb.	2.11	117.78	
S	gut par	2.73	117.16	
C	"	3.40	116.49	
N	"	3.55	116.34	
N	cb	3.28	116.11	
T.P. 1282 131.65 106 118.83				
0+02				
N		11.3	120.4	
+3		12.3	119.4	
+4		14.4	117.3	
C		14.7	117.5	

Moore  
Sisson 7-27

70



C +7	14.7	117.5
S	9.9	121.8
0+25		
S	8.7	123.0
+2	10.1	121.6
C	10.2	121.5
+4	9.7	122.0
+6	7.8	123.9
N	7.3	124.4



		131.65	
	0+27		
N <sup>6.9</sup>	S edge of 2' cement wall	6.9	124.73
	0+57		
N	E 5' walk level	4.95	126.70
C		5.1	126.6
S		4.9	126.8
	0+81		
S		1.6	130.1
C		1.8	129.9
N	= end 2' walk and W edge cement apron	0.75	130.90
	+11 W. L apron + gar.	0.50	131.45
	0+96		
	-11 FL apron + gar.	0.50	131.15
N		0.71	130.94
+3		+0.4	132.1
C		+0.4	132.1
S		+1.0	132.7
T.P.	1249	143.87	0.27
			131.38

		143.87	71
	1+00		
S	gr. base of cement wall	11.0	132.9
C		11.2	132.7
N		10.7	133.2
	1+27		
N		6.6	137.3
C		7.1	136.8
S		6.0	137.9
	+0.7 W edge cement apron	5.67	138.20
	1+29		
S	-7.5 W edge double gar.	4.20	139.67
	1+45		
S	-7.5 E " " "	4.17	139.70
S	-1.0 cement apron	4.66	139.21
S		4.7	139.2
C		4.6	139.3
N		4.3	139.6
	+1 yard	6.5	137.4
	+5 "	6.5	137.4

		143.87		
1+51				
S-1	E edge 3' walk	4.10	139.77	
1+71				
S-1	cem walk	1.0	142.9	
C	Top S.M.H.	1.23	142.64	
N		1.1	142.8	
T.P.	1013	153.50	0.50	143.37
1+75				
S-1	wedge cem apron	9.64	143.86	
1+79				
S-8	W.L. gar.	8.44	145.06	floor
S-1	cem apron	9.60	143.90	
S		9.6	143.9	
C		10.0	143.5	
N		9.4	144.1	
+1	yard	10.7	142.8	
1+95				
S-8	EL gar.	8.44	145.06	floor
S-1	EL apron	8.70	144.80	

		153.50		72
2+00				
N	W.L. cem apron	8.67	144.83	
+1.6	edge apron	8.61	144.89	in alley
C		8.5	145.0	
S		8.5	145.0	
+1.3	cem walk	8.46	145.04	
2+05				
N-14	W.L. gar.	9.12	144.38	floor
N	apron	8.63	144.87	
2+22				
S		7.5	146.0	
C		7.2	146.3	
+8	edge apron	8.13	145.37	
N	or "			
+14	EL gar.	9.04	144.46	floor
2+48				
N	on W.L. apron	6.84	146.66	
+1.7	edge "	6.81	146.69	in alley

2+63			
N EL apron	6.57	146.93	
+1.7 edge "	6.44	147.06	in alley
2+68			
N-10 S.L. <sup>West</sup> gar. entrance	7.44	146.06	
2+81			
N	6.1	147.4	
+5	5.2	148.3	
C	5.2	148.3	
S	5.1	148.4	
S+4 N edge apron	4.80	148.70	
S+6 NW gar comp	4.65	148.85	
2+97			
S-6 EL "	4.23	148.87	
S-4 " apron	4.78	148.72	
3+00			
S	4.9	148.6	
C	5.0	148.5	
+5	4.8	148.7	
N	5.8	147.7	

3+50			
N	5.2	148.3	
C	4.8	148.7	
S	4.3	149.2	
+2.2 gd.	3.9	149.6	
+2.2 TOP <sup>Cent. wall</sup>	3.04	150.46	
3+82			
S-2.4 TOP <sup>Cent. wall</sup>	2.85	150.65	
S-2.4 gd.	3.8	149.7	
3+92			
S-7 E Six gar.	3.3	150.2	dirt fl.
4+00			
S	4.0	149.5	
C	4.5	149.0	
N	4.9	148.6	
4+53			
N	4.3	149.2	
C	4.0	149.5	
S	3.5	150.0	
+7.5 NW gar.	2.42	151.08	Cent.

153.50

4468

S - 7.5 EL. gar 2.41 151.09

4483

S 3.1 150.4

C 3.8 149.7

N 4.2 149.3

+5.5 E gar 16' Wide 4.28 149.22 dirty

5400

N 3.8 149.7

C 3.6 149.9

S 3.1 150.4

5450 = WL N &amp; S 20' alley

S 1.9 151.6

C 2.4 151.1

N 3.0 150.5

T.P. 7.49 158.56 243 151.07

xsec N &amp; S alley 20' wide

74

158.56

0-10 S of Brighton

W par 12.0 144.6

C " 13.43 145.13

E " 12.75 145.81

00 = S of Brighton

E cb 11.78 146.78

E par 12.07 146.49

C " 12.95 145.61

W " 13.08 145.48

W cb 13.08 145.48

0450

W 10.9 147.7

C 10.6 148.0

E 10.5 148.1

1400

E 8.9 149.7

C 9.1 149.5

W 9.0 149.6

158.56

1 + 40 = NL E + W alley

W	8.0	150.6
C	7.5	151.1
E	6.9	151.7

1 + 57.41 S.L. alley west

E	6.3	152.3
C	6.7	151.9
W	7.0	151.6

2 + 03

W	4.5	154.1
C	4.4	154.2
E	4.2	154.4

+1 E S.W. gar. 4.19 154.37 floor P

2 + 41

E - 5.0 E gar. 15' wide	1.48	157.08 level
-------------------------	------	--------------

E	2.2	156.4
C	2.5	156.1
W	2.2	156.4

158.56

75

2 + 74

W	1.0	157.6
C	1.1 M. S.M.H.	0.96 157.60
E	1.1	157.5

2 + 97.41 = NL Cape May

E cb	1.0	157.6
E pav	1.08	157.48
C "	1.24	157.32
W "	0.73	157.83
W cb	0.58	157.98

3 + 25.41 = N cb line Cape May

W pav	1.51	157.05
C "	1.67	156.89
E "	1.79	156.77

check to BM 7.21 151.35 151.35

SW Brighton - Venice

2-7-39  
Mill  
Bliss

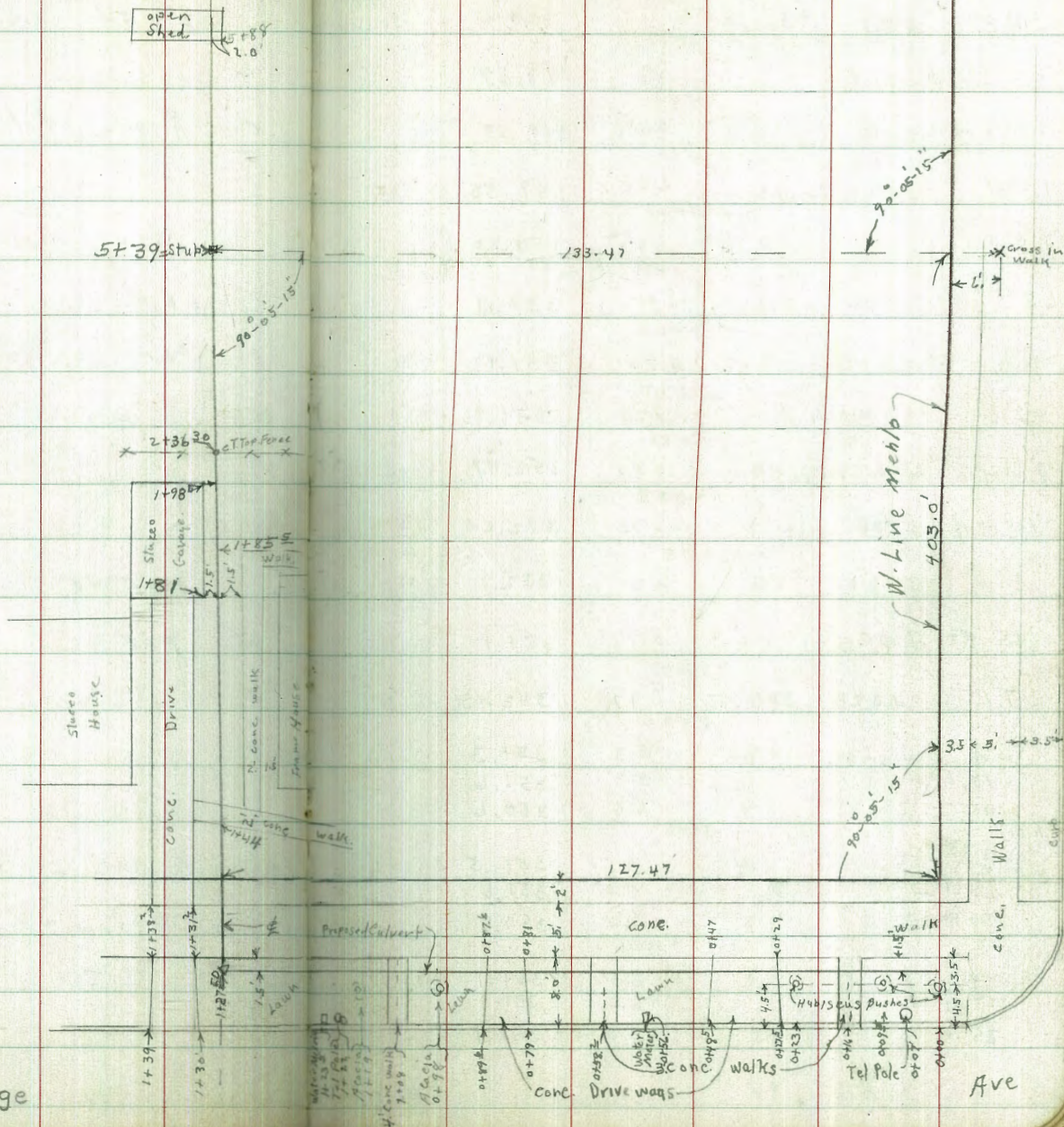
Levels for Proposed Culvert to Drain  
Blk. 4 Chester Park.

Indexed  
c.s.k.

76

Orange

Ave



							356.65		
BM BP	6.77	356.10		349.33	N. & Menlo + Orange	25' Lt		4+00	
		0+100 = W Line	Menlo			ϕ	5.2		351.4
6.5 s. of ϕ = gutter			7.41	348.69		50' Lt	5.2		351.4
6.5' s of ϕ = elv	(cb)?		6.75	349.35		ϕ	6.0	4+40	350.6
1.5 N " " = s. edge ext. walk			6.55	349.55		25' Lt	5.4		350.8
		0 + 50 W				50' Rt	4.4		352.2
1.5 N " " = " Lt	" walk		5.90	350.20		ϕ	6.0	4+75	350.6
			1+27.50	Δ 90° 05' 15" RT		30' Lt	5.0		351.6
6.5' s in " = el			4.91	351.19		30' Rt	5.4		351.2
			1+29			ϕ	5.8	5+00	350.8
ϕ = s. edge walk			4.70	351.40		ϕ	4.1		352.5
			1+44			25' Rt	4.4		351.8
ϕ = " " walk			4.24	351.86		20' Lt	4.0	5+25	352.6
			1+81			ϕ	4.6		352.0
3' Lt of ϕ = E. side garage floor			3.53	352.57		ϕ	5.0		351.6
			1+85.5			ϕ	4.1	5+39	352.29
1.5 Rt of ϕ = ext. walk			3.90	352.20		ϕ	4.0		352.6
			2+35			35' Rt	4.6		352.0
ϕ			4.0	352.1		20' Lt	4.1		352.5
4.5' Rt ϕ ϕ			5.0	351.1		ϕ stairs	4.42		352.29
T.P.	4.52	356.65	3.97	352.13		25' Lt	4.0		352.6
			2+70			30' Rt	4.7		351.9
ϕ			5.3	351.3		4.5' Rt	4.8		351.8
15' Lt			5.0	351.6		ϕ	4.5	5+69	352.1
45			6.0	350.6		25' Lt	4.5		352.1
			3+00			20' Lt	4.8		351.8
ϕ			5.1	351.5		ϕ	4.5		352.1
20' Lt			5.0	351.6		25' Lt	4.5		352.1
50' Rt			6.0	350.6		20' Rt	4.8		351.8
			2+40			4.2' Rt	4.4		351.8
ϕ			5.5	351.1					
25' Rt			5.5	351.1					
25' "			5.5	351.1					

356.65

5+85

Φ			4.6	352.0
20' Lt.			4.5	352.1
42' Rt			4.8	351.8
Φ		5+90	4.8	351.8
25' Lt			5.0	351.6
TIP	4.71	357.28	4.08	352.57
30' Lt		5+90	5.5	351.8
15' Rt			5.4	351.9
45' Rt			5.4	351.9
56' Rt underhouse			6.6	350.7
Φ		6+25	5.4	351.9
30' Lt			5.3	352.0
20' Rt			5.4	351.9
40' Rt			5.1	352.2
Φ		6+25	6.1	351.2
25' Lt.			6.3	351.0
20' Rt			5.7	351.6
40' Rt.			5.4	351.9

357.24

6+55.

Φ			5.2	352.1
30' Rt			5.3	352.0
35' Rt			5.0	352.3
35' Lt			5.6	351.7
50' Lt			5.0	352.3
Φ		6+85		
50' Lt			5.3	352.0
Φ			5.3	352.0
30' Rt			5.0	352.3
Φ		7+20		
Φ			5.0	352.3
30' Lt			5.0	352.3
30' Rt			5.0	352.3
Φ		7+50		
Φ			5.8	351.5
25' Lt			5.7	351.6
50' Lt			5.2	352.1
20' Rt			5.6	351.7
40' Rt			4.8	352.5
Φ		7+85		
Φ			5.5	351.8
40' Rt			5.1	352.2
30' Lt			5.5	351.8
40' Lt			5.0	352.3

78



357.28

8+15

±		5.1	352.2
40' Rt		5.0	352.3
20' Lt		5.0	352.3

8+38

±		5.0	352.3
20' Lt		4.7	352.6
20' Rt		5.0	352.3

8+40

±		5.6	351.7
±	8190	5.6	351.7
S. Line El Cajon	± about 975	3.4	353.5
S. ch. "		5.40	351.88
S. gutter		5.90	351.38

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# DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

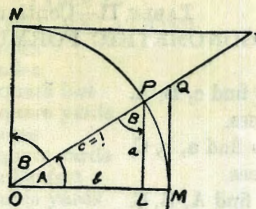


TABLE II  
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Lines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$

121  
~~83~~  
 20.4  
 112  
~~131.8~~  
 1430  
 21  
 17  
 509  
 w. End.  
 595 N. Row  
 1082. Theo.  
 87.5  
~~10.5~~  
 77.0  
 192  
~~57~~  
 27.9  
 54  
 4  
 91  
 47  
 550  
 20  
 530

6.06

6.00  
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