

1549

POSTS

GENERAL

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CHICAGO

Walker
Bliss
1-19-38

Contour Elevations
For Dance Hall

In Pepper Grove Balboa Park
N.W. 1/4 Sec.
Laurel Ave
Park Blvd.

3.33	286.61	283.28
T.P.	0.33	277.60
T.P.	1.03	266.10
T.P.	3.53	258.61

0+00

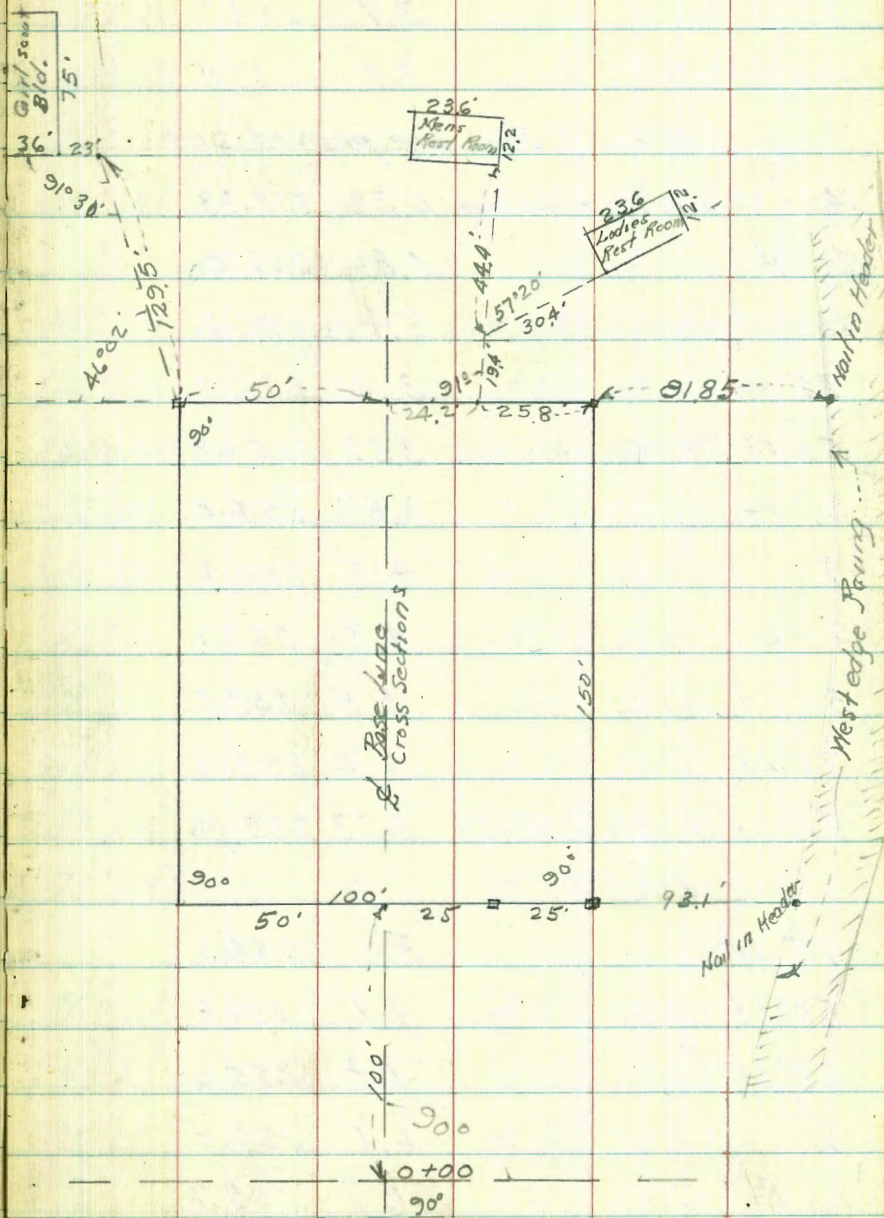
75' Rt.	5.0	253.6
50' Rt.	5.6	253.0
25' Rt.	6.4	252.2
ℓ	7.2	251.4
25' Lt.	7.8	250.8
50' Lt.	8.9	249.7
75' Lt.	8.9	249.7

0+50

75' Lt.	8.1	250.5
50' Lt.	7.1	251.5
25' Lt.	6.4	252.2
ℓ	5.9	252.7
25' Rt.	4.9	253.7
50' Rt.	4.2	254.4

indexed
C.S.K.

1



258.6

75' Rt		3.9	254.7
100' Rt		3.5	255.1
	1+00 = South line proposed site		
143.1' Rt. on West edge paving		0.38	258.23
125' Rt		0.8	257.8
100' Rt		2.4	256.2
75' Rt		3.2	255.4
50' Rt, S.E. Cor. proposed site		3.53	255.08 on stub
25' Rt		3.8	254.8
ℓ		4.5	254.1
25' Lt		4.9	253.7
50' Lt		5.8	252.8
75' Lt		6.2	252.4
TP	7.30 262.38	3.53	255.08
	1+50		
75' Lt		8.1	254.3
50' Lt		7.9	254.5
25' Lt		7.4	255.0
ℓ		6.9	255.5
25' Rt		6.7	255.7
50' Rt		6.1	256.3

262.38

2

75' Rt		5.2	257.2
100' Rt		4.0	258.4
125' Rt		2.7	259.7
144' Rt. ^{on ground} at Paving		2.4	260.0
	2+00		
142' Rt. on Paving		0.48	261.90
125' Rt		0.8	261.6
100' Rt		1.9	260.5
75' Rt. at 4' ^{dia.} Euc. Tree.		3.1	259.3
50' Rt		4.9	257.5
25' Rt		5.7	256.7
ℓ		5.8	256.6
25' Lt		6.1	256.3
50' Lt		6.0	256.4
75' Lt		5.9	256.5
	2+50		
75' Lt		4.7	257.7
50' Lt. = N.Y. Cor. site		4.6	257.8
25' Lt		4.7	257.7
ℓ		4.6	257.8
25' Rt		4.2	258.2

262.38

50' Rt. = NE. Cor site 3.13 259.25 on stub

75' Rt. 2.0 260.4

100' Rt. 0.6 261.8

T.P. 6.53 265.78 3.13 259.25

113' Rt. 2.4 263.4

131.85' Rt. on West edge paving 2.11 263.67

2+75 = 25' North of North end of site

124.5' Rt. on Paving 1.15 264.63

105' Rt. 1.2 264.6

75' Rt. 4.4 261.4

50' Rt. 5.5 260.3

25' Rt. 6.0 259.8

2 6.4 259.4

25' Lt. 6.5 259.3

50' Lt. 6.8 259.0

75' Lt. 7.0 258.8

3+00

75' Lt. 5.2 260.6

50' Lt. 4.9 260.9

25' Lt. 4.7 261.1

2 4.3 261.5

265.78

3

25' Rt. 4.1 261.7

50' Rt. 3.3 262.5

Floor Ladies Rest Room 1.86 263.92 in door way

" Mens " " 0.82 264.96

" Girl Scout Bld. 0.34 265.44 Floor Elev. of Rear Frame Bld.

T.P. 12.30 277.35 0.73 265.05

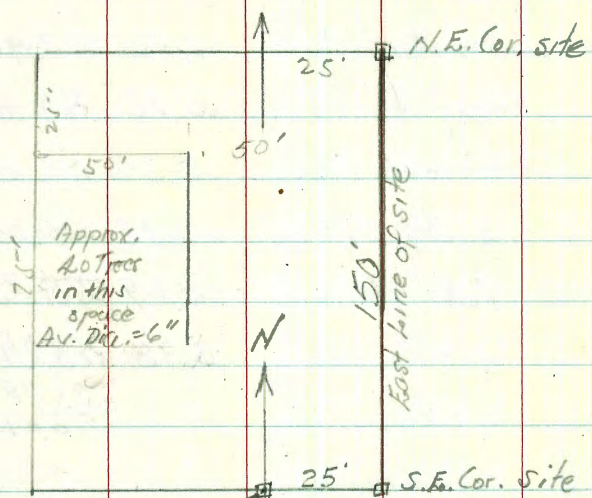
T.P. 9.41 286.67 0.09 277.26

chk. 3.38 283.29 N.W. SP Laurel and Oak Bld.

283.28 = B.M.

0.01 = Error.

Stadia Location Trees
on And Adjacent To proposed
Dance Hall site sketch P. 1



indexed
c.s.K. Readings Sta. # 1
Azimuth from N to East.
Azimuth Horiz.

6" dia. Euc. Tree	172°05'	123'	✓
4" " " "	172°05'	115'	✓
8" " " "	171°00'	107'	✓
30" " " "	166°41'	111'	✓
6" " " "	167°37'	104'	✓
9" " " "	168°07'	92'	✓
10" " " "	161°03'	88'	✓
10" " " "	165°45'	83'	✓
6" " " "	165°22'	74'	✓
8" " " "	158°00'	80'	✓
36" " " "	153°44'	73'	✓
4" " " "	159°35'	69'	✓
4" " " "	162°37'	63'	✓
6" " " "	155°57'	57'	✓
4" " " "	149°48'	52'	✓
4" " " "	154°47'	47'	✓
6" " " "	154°50'	34'	✓
6" " " "	147°10'	42'	✓
6" " " "	140°17'	40'	✓

From
Readings, Stadia # 1
Azimuths from North, Right S
To East, South etc. clockwise

Sta.	Azimuth	Horiz.	
2' dia. Euc Tree	170°49'	147'	✓
8" " " "	169°36'	143'	✓
8" " " "	174°27'	146'	✓
6" " " "	175°05'	140'	✓
8" " " "	173°49'	133'	✓
1" " " "	167°27'	130'	✓
14" " " "	?	124'	✓

READINGS from 1

Readings From 1

Azimuth Horiz.

36" dia. Euc. Tree	123°20'	42	✓
6" " " "	131°55'	30'	✓
8" " " "	143°30'	18'	✓
6" " " "	115°36'	41'	✓
14" " " "	110°14'	25'	✓
6" " " "	102°16'	18'	✓
8" " " "	97°30'	39'	✓
4" " " "	92°12'	27'	✓
18" " " "	84°12'	20'	✓
8" " " "	82°07'	39'	✓
10" " " "	79°46'	29'	✓
4" Lamp Post	73°52'	29'	✓
14" Euc Tree	70°42'	36'	✓
" " " "	65°26'	32'	✓
12" " " "	74°50'	43'	✓
12" " " "	59°14'	47'	✓
8" " " "	46°35'	40'	✓
14" " " "	37°44'	48'	✓

8" dia. Euc. Tree	34°28'	55'	✓
14" " " "	30°36'	60'	✓
12" " " "	23°35'	86'	✓
4" " Lamp post.	16°45'	95'	✓
4" dia. Euc. Tree	21°15'	105'	✓
12" " " "	17°50'	124'	✓
12" " " "	14°46'	129'	✓
8" " " "	18°00'	140'	✓
48" " " "	39°55'	70'	✓
48" " " "	26°24'	109'	✓
48" " " "	19°48'	148'	✓
8" " " "	12°38'	150'	✓
14" " " "	13°08'	156'	✓
12" " " "	13°08'	165'	✓
78" " " "	10°49'	169'	✓
30" " " "	13°03'	184'	✓
4" Lamp post.	8°33'	176'	✓
12" dia Euc. Tree	7°44'	185'	✓
12" " " "	11°03'	193'	✓
10" " " "	5°48'	189'	✓
20" " " "	4°28'	203'	✓

READINGS from □ 1

	Azimuth	Horiz.	
18" dia. Euc. Tree	0° 49'	209'	✓
12" " " "	181° 15'	166'	✓
8" " " "	180° 11'	173'	✓
16" " " "	177° 18'	166'	✓
5" " Lamp post	187° 38'	189'	✓
6" Tree	191° 12'	162'	✓
6" " "	195° 10'	141'	✓
4" " "	196° 30'	132'	✓
8" " "	199° 30'	130'	✓
10" " "	200° 05'	121'	✓
8" " "	204° 16'	115'	✓
10" " "	209° 37'	104'	✓
8" " "	214° 04'	123'	✓
10" " "	216° 52'	128'	✓
6" " "	218° 45'	121'	✓
8" " "	221° 25'	121'	✓
10" " "	224° 14'	109'	✓
14" " "	223° 57'	96'	✓
10" " "	229° 47'	82'	✓

Readings from □ 1

	Azimuth	Horiz.	
10" Tree	240° 39'	68'	✓
5" Lamp post	245° 20'	63'	✓
12" dia. Pepper tree	256° 56'	62'	✓
12" " " "	275° 04'	57'	✓
12" " " "	246° 18'	43'	✓
8" Tree	240° 53'	32'	✓
12" " "	263° 30'	35'	✓
4" " "	262° 47'	26'	✓
8" " "	277° 30'	30'	✓
4" " "	293° 02'	14'	✓
3" stand pipe	301° 32'	24'	✓
6" Tree	288° 35'	26'	✓
6" " "	307° 09'	27'	✓
4" Lamp post	292° 42'	42'	✓
10" Tree	304° 07'	44'	✓
12" " "	326° 38'	39'	✓
4" " "	329° 27'	18'	✓
6" " "	356° 51'	25'	✓
6" " "	355° 01'	35'	✓
4" " "	341° 20'	38'	✓

Water.

Readings from lat 1

7

	Azimuth	Horiz.		
8" Tree	348°32'	46'	✓	
6" "	350°16'	58'	✓	
8" "	355°10'	109'	✓	
3" stand pipe	354°57'	148'	✓	Water
10" Tree	348°47'	132'	✓	
5" Lamp post	346°12'	144'	✓	
24" Exc. Tree	350°10'	160'	✓	
36" " "	343°24'	190'	✓	
5" Lamp post	326°11'	180'	✓	
Barbecue pit	369°56'	144'	✓	
3" stand pipe	303°50'	162'	✓	Water
Elec. pole	314°27'	111'	✓	

Walker
Bliss
1-28-38

CURB LEVELS
Olivewood, T-st. And Jewel Drive

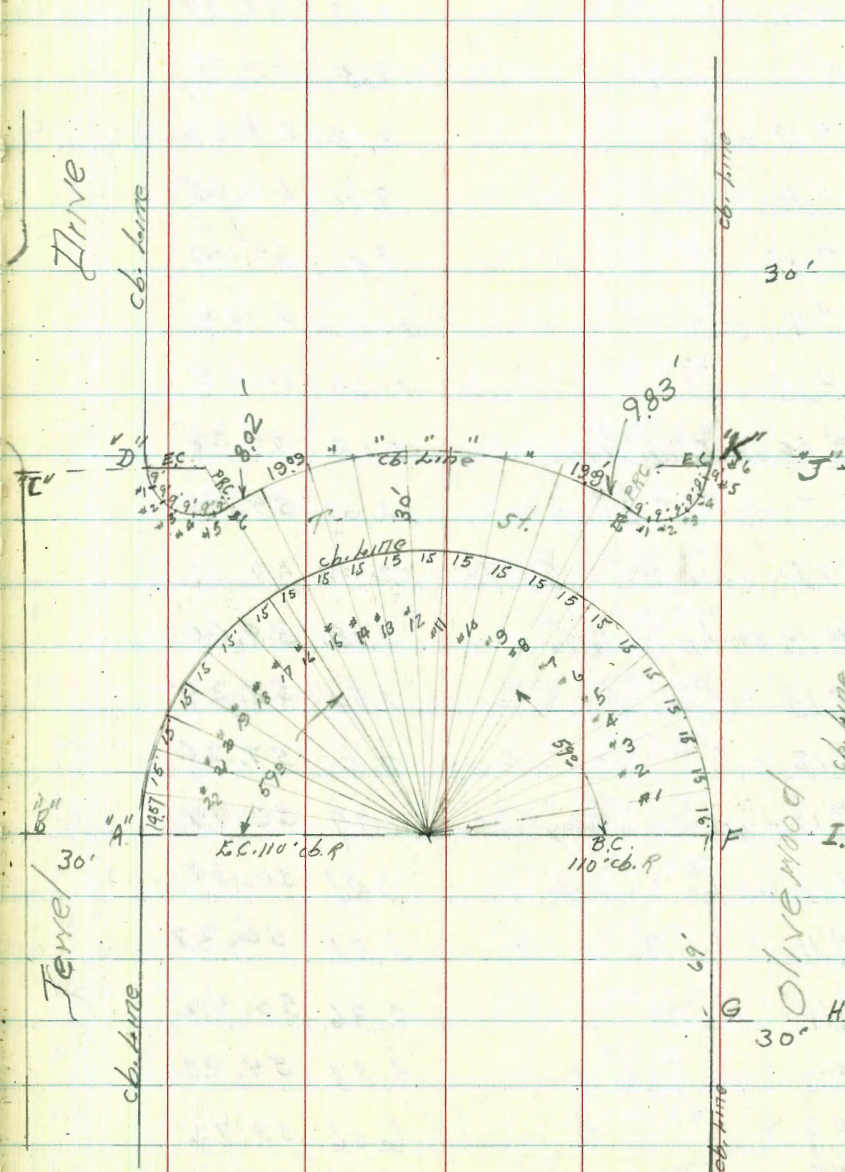
indexed
c/s. 1/4

SE. top Hyd.
Ocean View
+ 37 1/2

	9.58	73.05		63.47
T.P.	9.59	82.09	0.55	72.50
T.P.	1.29	71.76	11.62	70.47

Jewel St. And T-st intersection.

P.C. cb. at "A" on cb. West side	5.05	66.71
" " " " " Gutter-ground.	5.8	66.0
"B" top cb.	3.76	68.00
" Gutter on ground.	4.6	67.2
"C" on top cb.	6.80	64.96
" " Gutter-ground. on cb.	7.3	64.5
"D" on cb. E.C. S.W. T-st Jewel St.	7.59	64.17
" " Ground.	8.1	63.7
#1 on cb.	7.60	64.16
#2 " "	7.80	63.96
#3 " "	8.29	63.47
#4 " "	8.91	62.85
#5 " "	9.52	62.24
#6 = P.R.C. S.W. Jewel + T-st	10.15	61.61
#22 on cb of 110' cb. R.	5.65	66.11



71.76

# 21 on cb.	6.40	65.36
# 20 " "	7.22	64.54
# 20 " Ground	7.3	64.5
# 19 on cb.	8.13	63.63
# 18 " "	9.11	62.65
# 17 " "	9.86	61.90
# 16	10.70	61.06
# 15	11.68	60.08
# 14 on cb. on North	12.68	59.08
" " " " South	12.01	59.75
T.P. 0.36 59.78	12.34	59.42
# 13 on top South cb.	1.18	58.60
# 13 " " N. cb.	1.54	58.24
# 12 " " " "	2.52	57.26
# 12 on drive way on South	2.79	56.99
# 11 on top South cb.	3.41	56.37
# 11 " " N "	3.51	56.27
# 10 " " N "	4.36	55.42
# 10 " " South "	4.83	54.95
# 9 " " " cb.	6.06	53.72
# 9 " " North "	5.15	54.63

59.78

9

# 8 on top N. cb.	5.87	53.91
" " " S. cb.	7.17	52.61
S.E. Return Olive wood + T-st.		
P.R.C. top cb at "E"	7.71	52.07
# 1 on top cb	8.27	51.51
# 2 " " "	9.02	50.76
# 3 " " "	9.89	49.89
# 4 " " "	10.69	49.09
# 5 " " "	11.15	48.63
# 6 = E.C. S.E. Return	11.55	48.23
" " " " Ground	12.3	47.5
# 7 on top cb. 110' cb Rod.	6.71	53.07 on North.
# 6 " " " on North.	7.58	52.20
# 5 " " " " "	8.3	51.5
# 5 on Ground	8.5	51.3
# 4 on cb.	8.93	50.85
" " Ground	8.8	51.0
# 3 on top cb.	9.01	50.77
# 3 " Ground	8.8	51.0
# 2 " top cb.	9.04	50.74
# 2 " Ground.	8.8	51.0

5978

# 1 on top cb 110' cb Red.	8.94	50.84
# 1 " Ground.	8.5	51.3
P.C. 110' cb B on cb. at "F"	8.32	51.46
" " " " Ground	8.3	51.5
20' North of "F" on Top East cb.	7.31	52.47
" " " " " Ground.	7.9	51.9
69 " " "F" = "G" on cb.	4.86	54.92
" " " " on Ground.	5.2	54.6
"H" on top West cb.	5.93	53.85
" " Ground	6.5	53.3
"I" on top cb. ^{on West.} opp. P.C. on East.	7.81	51.97
" " Ground.	8.7	51.1
39' South of "I" on West cb.	9.17	50.61
" " on Ground.	9.9	49.9
89' " of "I" on cb. on West.	10.84	48.94
" " " " " Ground	11.8	48.0
139' South of I = "J" on cb.	12.84	46.94
TP	6.60	53.54
50' South of "J" on West cb.	8.43	45.11
" " on Ground.	8.0	45.5
74' " of "J" on W. cb.	9.46	44.08

53.54

74' South of "J" on Ground.	8.9	44.6
100' South "J" on West cb.	9.89	43.65
" " " " " Ground.	9.4	44.1
100' South of "K" on top E. cb.	8.61	44.93
" " " " " Ground	9.0	44.5
775' " " " " " cb.	8.24	45.30
" " " " " Ground	8.5	45.0
50' South of "K" on cb.	7.40	46.14
" " " " " Ground.	7.8	45.7
25' North of K " "	4.8	48.7
50' " " " " " "	3.8	49.7
75' " " " " " "	2.8	50.7
100' " " " " " "	2.7	50.8
125' " " " " " "	2.4	51.1
TP	11.44	64.41
ocean view 437 th	0.57	52.97
chk. S.E. top Hght	0.94	63.47

10

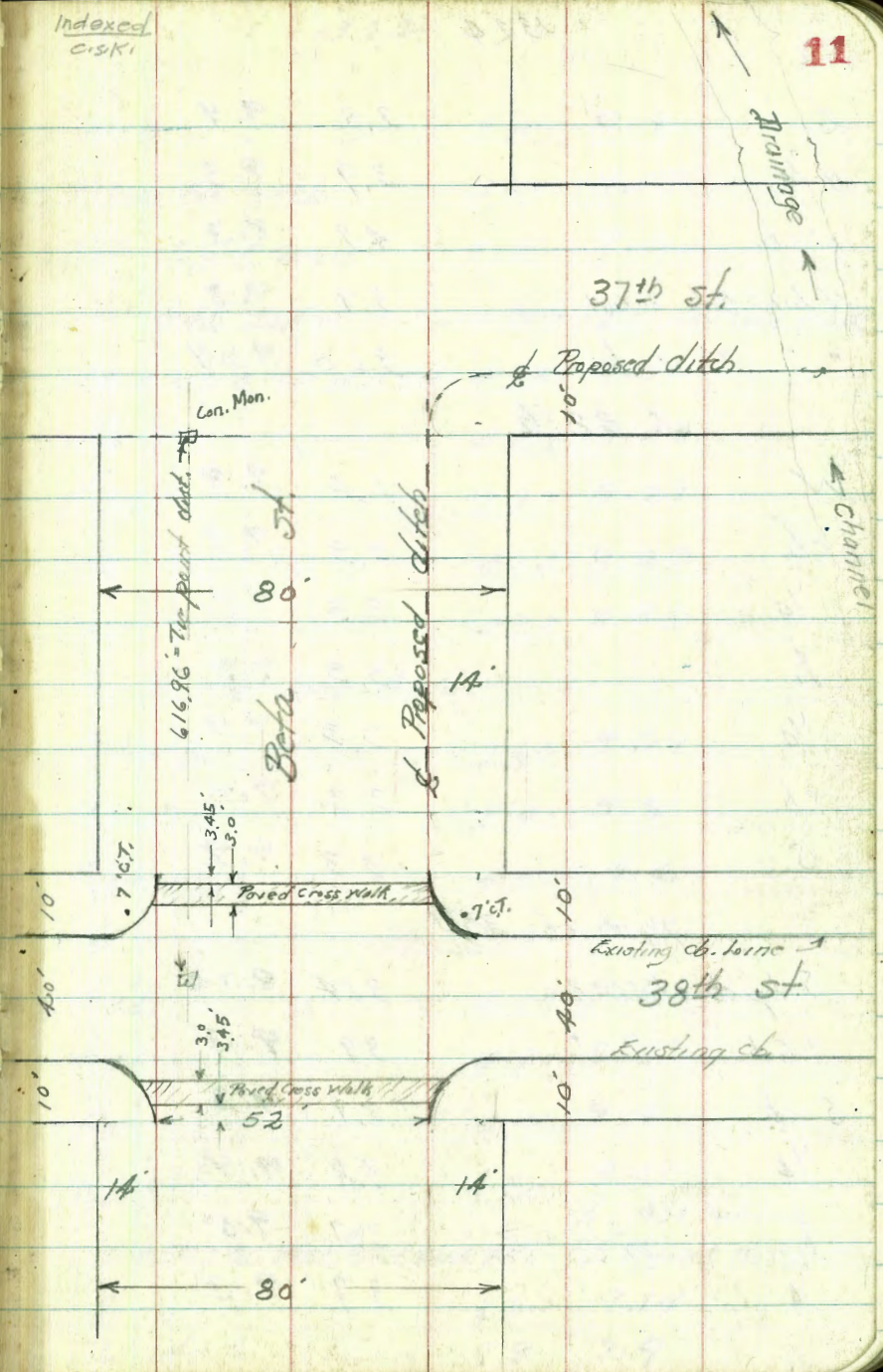
observed
East side

Walker
 1-31-38

LEVELS FOR PROPOSED DRAIN
 BETA And 37th Street.

	3.43	14.49	11.06	Sta. B.P Alpha 38th
T.P	3.54	13.24	4.79	9.70 S.E. 7' curb Beta st + 38th
East Line 38th				
South Top cb.	3.05	10.19		
" Gut.	3.3	9.9		
E Beta	3.3	9.9		
N 1/4	3.5	9.7		
N Gut	3.6	9.6		
N Top cb.	3.6	9.6		
6.45 West of East line 38th = West edge Cross Walk				
N Gut on Cross Walk at ch. Return.	3.20	11.04		
" 1/4 " " "	3.66	9.58		
E Beta " " "	3.52	9.72		
S 1/4 " " "	3.48	9.76		
S Gut " " " " "	3.80	9.44		
East ch. line 38th				
S top cb. at sk. Beta	3.09	10.15		
" Gut.	3.6	9.6		
S cb.	3.7	9.5		
S 1/4	3.7	9.5		

Indexed
 C.S.K.I.



1324

1324

12

	£		3.8	9.4
	N 1/4		3.9	9.3
T.I.	N cb.		4.9	8.3
	N Line Beta on Gut.		3.9	9.3
Se	" " " " cb.		3.60	9.64
	£ 38 th			
£	N		3.4	9.8
N	cb.		3.3	9.9
N	1/4		3.3	9.9
N	£		3.3	9.9
	1/4		3.3	9.9
N Gut	cb.		3.3	9.9
1/4	£		3.3	9.9
£ Beta		West cb 38 th		
S 1/4 "	S top cb.	at Sk. Beta	3.54	9.70
S Gut	" Gut	" " "	3.9	9.3
	S cb.		3.9	9.3
S top	1/4		3.8	9.4
" Gut	£		3.7	9.5
S cb.	1/4		3.9	9.3
S 1/4				

	N cb.		3.8	9.4
	N Line Beta on cb.		4.15	9.09
	" " " " Ground		4.2	9.0
	6.45 East of West line 38 th = East edge Cross Walk			
	N Gut. on Cross Walk at cb Ref.		4.73	8.51
	N 1/4 " " "		4.21	9.03
	£ Beta " " "		3.97	9.27
	S 1/4 " " "		4.04	9.20
	S Gut. " " " " " "		4.28	8.96
	West line 38 th			
	S top cb.		3.60	9.64
	" Gut.		3.4	9.8
	" 1/4		4.0	9.2
	£		3.9	9.3
	N 1/4		4.1	9.1
	+ 11		4.7	8.5
	Gut.		4.2	9.0
	N top cb.		4.20	9.04
	0 + 50 = 50' West, West line 38 th = £ Cross sections = £ Proposed ditto.			
	£		4.1	9.14
	6' Lot.		5.3	7.9

13.24

10' Lt.		5.0	8.2
	1+00		
5' Rt.		4.6	8.6
2		4.6	8.6
6' Lt.		5.0	8.2
7' Lt.		5.4	7.8
10 "		5.0	8.2
	1+50		
5' Rt.		4.6	8.6
2		4.6	8.6
7' Lt.		5.0	8.2
8' Lt.		5.6	7.6
	2+00		
5' Rt.		5.0	8.2
2		5.0	8.2
6' Lt.		5.1	8.1
7' Lt.		5.9	7.3
10' Lt.		5.7	7.5
	2+50		
5' Rt.		5.2	8.0
2		5.2	8.0

13.24

13

7' Lt.		5.2	8.0
8' Lt.		5.9	7.3
15' Lt.		5.6	7.6
	3+00		
5' Rt.		5.3	7.9
2		5.3	7.9
7' Lt.		5.4	7.8
8' "		6.1	7.1
10' "		5.9	7.3
	3+50		
5' Rt.		5.2	8.0
2		5.2	8.0
7' Lt.		5.4	7.8
8' Lt.		6.4	6.8
10' Lt.		6.0	7.2
	4+00		
5' Rt.		5.8	7.4
2		5.7	7.5
7' Lt.		5.7	7.5
8'		6.6	6.6
10' Lt.		6.4	6.8

13.24

4+50

5' RT	5.9	7.3
ℓ	5.9	7.3
7' Lt.	5.9	7.3
8' Lt.	6.9	6.3
10' Lt.	6.7	6.5

5+00

5' RT	6.1	7.1
ℓ	6.1	7.1
7' Lt.	6.3	6.9
8' Lt.	7.0	6.2
10' Lt.	6.8	6.4

5+50

5' RT	6.3	6.9
ℓ	6.3	6.9
7' Lt.	6.5	6.7
8' Lt.	7.0	6.3
10' Lt.	6.8	6.4

6+00 = East Line 37th

5' RT	6.2	7.0
ℓ	6.2	7.0

13.24

14

6' Lt.	6.1	7.1
7' Lt.	6.7	6.5
10' Lt.	6.5	6.7

6+10 = $\frac{1}{2}$ proposed ditch in 37th st
Sections from here = RT, Δ to 37th st

5' RT	6.0	7.2
ℓ	6.0	7.2
7' Lt.	6.8	6.4
10' Lt.	6.8	6.4

6+50

5' RT	6.0	7.2
ℓ	6.0	7.2
6' Lt.	6.0	7.2
7' Lt.	7.0	6.2
10'	7.0	6.2

TR 10.12 18.03 5.33 7.91

7+00

5' RT	10.5	7.5
ℓ	10.5	7.5
4' Lt.	10.4	7.6
5'	11.6	6.4
10' Lt.	11.4	6.6

18.03

7+50

5' Rt. 10.1 7.9

2 10.1 7.9

5' Lt. 9.8 8.2

6' Lt. 11.5 6.5

10' Lt. 11.4 6.6

8+00

5' Rt. 9.3 8.7

2 9.3 8.7

5' Lt. 9.9 8.1

6' Lt. 11.8 6.2

10' Lt. 11.7 6.3

8+50

5' Rt. 9.3 8.7

2 9.4 8.6

4' Lt. 9.4 8.6

5' Lt. 12.1 5.9

10' Lt. 12.0 6.0

9+00

5' Rt. 10.8 7.2

2 10.8 7.2

18.03

15

3' Lt. 11.5 6.5

4' " 13.3 4.7

10' " 13.3 4.7

9+1.3 = South edge of Bottom of Channel

10' Rt. 13.6 4.4

2 13.7 4.3

10' Lt. 13.8 4.2

9+2.5 = 2 drainage Channel

2 13.5 4.5

Ch. on SE. BR Alpha Betu 6.97 11.06 ✓

22.68

Cottonwood And Una.

				SE 7' fact Cottonwood + Una
T.P.	1.42	15.66	8.44	14.24
25' S. East of "A" on ground			6.4	9.3
"A" on ground			7.3	8.4
"A" " Flow line 18" pipe			8.63	7.03
"B" on top cb.			5.10	10.56
"B" " Grating			6.34	9.32
"C" " "			6.33	9.33
"C" on top cb.			5.19	10.47
"D" on ground = end 24" Corrugated pipe			8.4	7.3
" " Flow " " "			11.05	4.61
50' North West of "D" in ditch			8.6	7.1
"E" on ground at ^{end} 24" Conc. Culvert.			9.8	5.9
" " Flow line			11.19	4.47
"F" on top cb. = 15' cb inlet			7.97	7.69
" " on top of Grating			8.74	6.92
"G" " " "			8.45	7.21
G " " " cb = 15' cb inlet on west cb line 400 ft			7.60	8.06
"H" on ground at ^{end of} 24" Conc. pipe			11.2	4.5
"H" " Flow line culvert			12.04	3.62

15.66

Cottonwood + Una
Culverts.

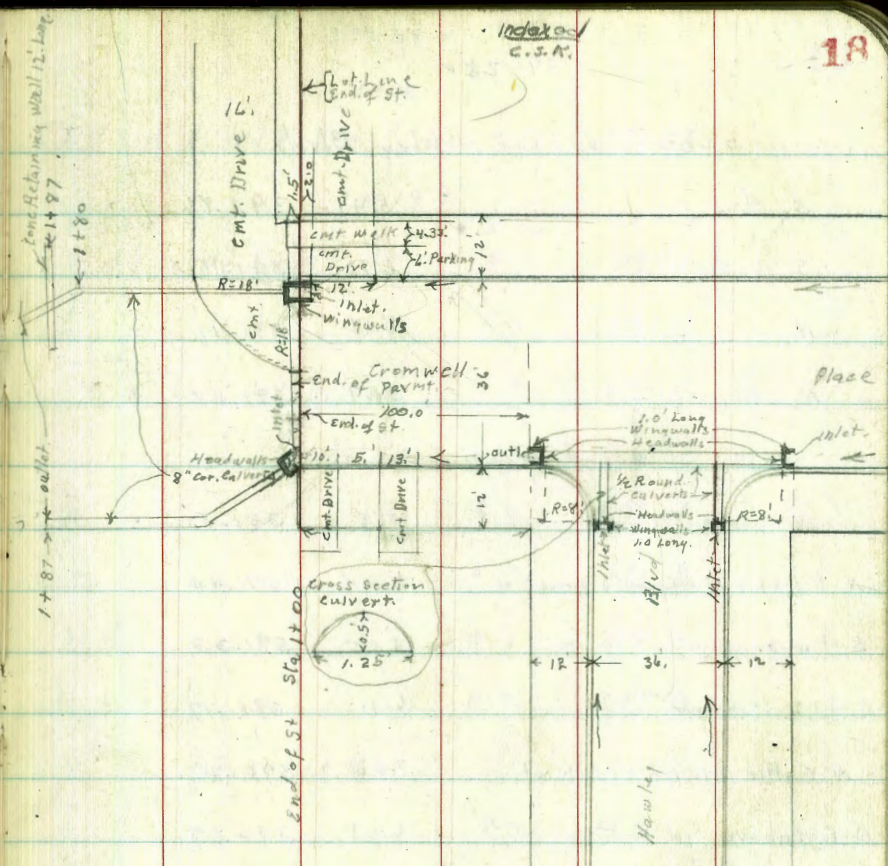
17

"I" in Bottom of ditch	11.7	4.0	76' West of West cb. Una in 2 Alley
50' North West of "I" in Bottom ditch	11.9	3.8	Natural Ground 1.3 Higher.
100' " " " " " " "	12.0	3.7	"
150' " " " " " " "	12.1	3.6	"
200' " " " " " " "	12.2	3.5	"
"J" on Flow line 36" Culvert	12.25	3.41	
" " top Hd. Wall " "	7.74	7.92	
T.P.	9.83	24.67	1.42 14.24
	10.49	13.58	
		13.55 = BM.	
		0.03 Error.	

2-25-38
Miller
Walker
B. L. ...

Levels for Catch Basin + 100' of Culvert
at West End of Cromwell Place

BM. BP	4.43	398.44 ✓	394.01	5. W. Hawley + Mt. View Drive
T.P.	4.65	397.28 ✓	581	392.63
E. Line Hawley Blvd.				
S. d		5.11	397.17	
S. Gutter		5.70	391.58	
N. "		5.94	391.30	
N. d		5.55	391.73	
1.0 W. of E. Line = Inlet Culvert				
		5.81	391.44	
12' W. of E. Line = S. d. Line				
E. End of S. Line Cromwell = F.L. Culvert	5.81	391.47		
S. Line Gutter	5.73	391.55		
S. " d.	5.12	392.16		
12' E. of W. Line Hawley = W. d.				
S. Line Cromwell curb.	5.43	391.85		
" " gutter	6.01	391.77		
1.0 N. of S. Line = F.L. Culvert.	6.06	391.77		
1.0 E. of W. Line Hawley				
W. End. F.L. Culvert.	6.17	391.11		



Index
C.S.N.

1+03

0+00 = W. Line Hawley Blvd.

2' s. of S. ch. FL Inlet 8" Pipe 7.00 390.78

S₁ ch. 5.42 391.86

1+19

S. Line 5.2 392.1

S. Gutter 6.10 391.18

S ch Line Produced 5.2 392.1

N. " 6.17 391.11

♀ " 5.4 391.9

N. ch. 5.67 391.61

N. ch. Lines

W. Edge Cont. Drive 5.8 391.5

1+00 = W. End. of St.

1+55

N. Line 5.8 391.5

N. ch 6.8 390.5

N. + 1.67 = N. ch. walk + Drive to W. 5.84 391.44

♀ 6.0 391.3

N. + 6.0 = S. " " " " 5.95 391.33

S. ch 5.1 392.2

N. + 12 = N. ch 6.11 391.17

S. Line 5.2 392.1

N. Gutter = Inlet 8" Culvert 7.06 390.22

1+80

2' E. of above in Gutter 6.64 390.67

S. 8.2 389.1

ch + 2.5 = Pav. to E. 6.33 390.95

S. ch 8.0 389.3

ch + 9 = 1/4 " " " 6.29 390.99

♀ 7.2 390.1

ch + 18 = 1/4 " " " } 5+ 6.09 391.19

N. ch 6.7 390.6

ch + 27 W. End. Pav. = 1/4 6.15 391.13

1+87

S. Gutter in Drive way 6.46 390.88

N. ch. N. End Ret. wall 10.1 387.2

There is no curb.
Curb. Grade Produced from East. 5.82 391.46

" " + 5' = 8" Pipe Top wall 10.1 387.2

S. ch + 6 = N. side W. End. walk. 5.60 391.68

" " " " Top. Pipe 13.5 383.8

S. ch + 12 = S. Line 5.40 391.88

" " " " ground. 17. 380.3

397.28 ✓

Line 3' N. of S. Line

20

N. ch 172 = s. end wall	10.1	387.2	T.P. OPR page	6.29	394.00 ✓	387.11
⊕	11.0	386.3	2+25			30.0 364.00
s. ch.	10.4	386.9	2+35			38.0 356.00
S. Line ground	8.5	388.8				
" " W. End Fl. Pipe	10.5	386.8				
Set B.M. 8 W. S. of	5.26	392.02	Cromwell + Hawley Blvd.			
T.P.	8.59	393.70 ✓	10.17			387.11
2+00 in gully 10' s. of N. ch	23.5	372.4				
2+00 " 5' N. of N. ch	20.0	375.7				
2+00 N. ch. line	14.0	381.7				
2+14 " " "	26.0	369.7				
2+20 " " "	33.0	364.7				
2+20 8' N. of ch. in gully	44.0	351.7				
2+20 13' S. of ch. in gully	48.0	347.7				

3-4-38
Miller
Walker
Bliss

Soria Drive X Sec.

College Way to Arosa St.

5' Combination Walk + Curb. 10' obs. 30' Roadway

Indexed
C.S.K.

Adams.

Soria Dr.

30 Ave

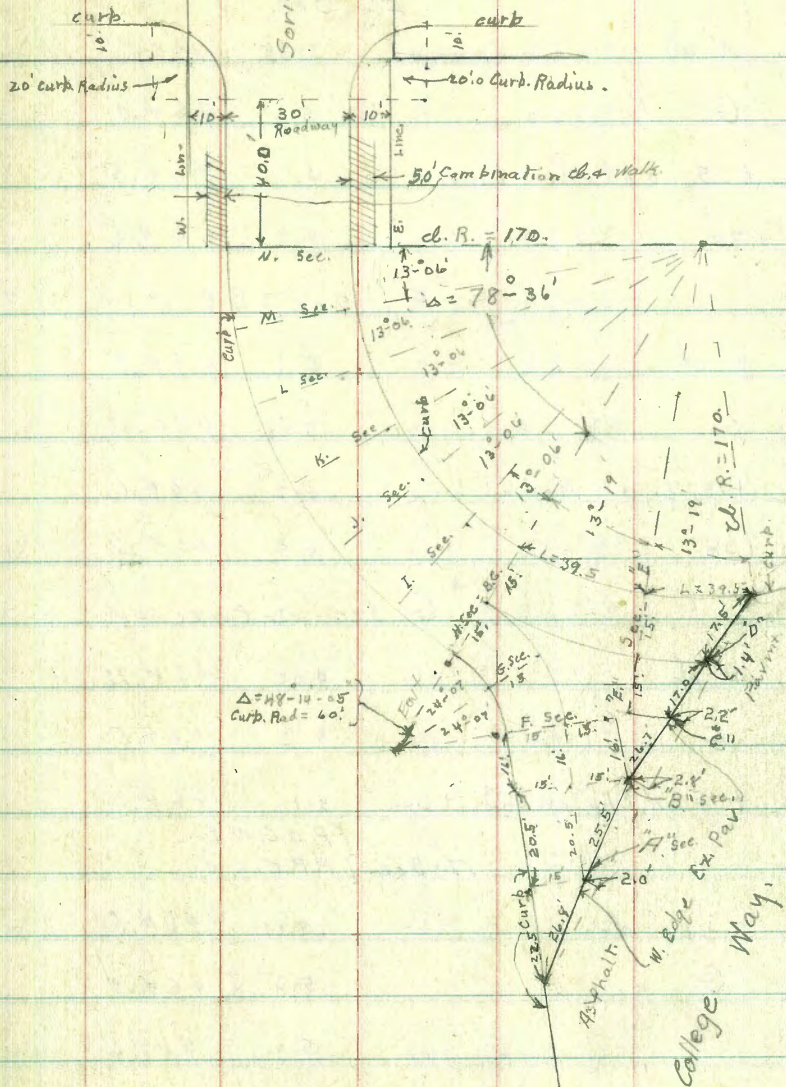
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B.M. B.P. 4.44 469.75- 465.27

N.W. El Cajon
(Gibson)
College way

P.T. W. curb of Soria + w. edge College Way pav

Top ch	4.89	467.86
Gutter Pav	5.50	464.25
8' E. of w. edge pav = W.G. College Way	5.50	464.25
"A" Sec.		
7' E. of w. edge pav = W.G. College Way	5.64	464.07
W. edge pav.	5.63	464.12
15' W. = Gutter	5.3	464.5
Top ch w. side	5.02	464.73
"B" Sec.		
Top. W. ch	5.07	464.68
G.	5.3	464.5
+ 15	5.2	464.6
+ 30 = w. edge pav	5.70	464.05
+ 38 = W. G. College Way	5.73	464.02
W. edge pav at "C"	5.90	463.85
8' E of " " " = W. G. College Way	5.87	463.88
at "D"		
W edge pav	5.88	463.87
80' E. of " " " = W. Curb College way	5.98	463.77
N. Curb. Soria		463.77
W. edge pav. Gutter	5.83	463.92
" " " Top. curb	5.38	464.37



X 469.75

X ch. Soria

10' E. of W. edge pav = W. Gutter Pav 6.04. 463.71

469.75

"E"

Sec.

N. ch.	5.35	464.40
G.	5.8	464.0
+15 on Radial Line	5.3	464.5
+30 " " "	5.2	464.6

"F"

Sec = B.C. w. side

W. ch.	5.1	464.7
G.	5.08	464.67
+15' E. on Radial line	5.2	464.6
+30 " " " "	5.5	464.3

*

G Sec. ctr Curve on W.

W. ch.	5.00	464.75
G.	5.3	464.5
+15 N.E. ly. on Radial line	5.1	464.7

"H" Sec.

P.O.C. N.E.
P.B.C. S.W.

N.E. ly. ch	5.17	464.58
G	5.5	464.3
"	5.2	464.6
±	5.1	464.7
"	5.2	464.6
G	5.3	464.5
W. ch	5.05	464.70

469.75

"I" Sec

W. ch	4.84	464.91
G	5.1	464.7
"	4.9	464.9
±	5.0	464.8

"J"

"	5.2	464.6
G	5.2	464.6
E. ch	5.03	464.72

"J" Sec

E. ch	4.86	464.89
G	4.8	465.0
"	4.9	464.9
±	4.9	464.9
"	4.6	465.2

"K"

G	4.8	465.0
W. ch	4.68	465.07

"K" Sec

W. ch	4.48	465.27
G	4.8	465.0
"	4.5	465.3
±	4.6	465.2

Soria

22

	469.18		
30' E. of E. Line	0 + 60 = S. Carb. Adams	3.90	465.28
10' E. of E. Line = P.C. 20' Ret.	Top. ch. 3.71		465.47
" " " " " " G.	4.4		464.8
E. Line	4.3		464.9
E. of Line	4.2		465.0
"	3.8		465.4
⊕	3.7		465.5
1/4	3.8		465.4
W. of	3.7		465.5
W. Line	3.7		465.5
+10 = P.C. 20' Ret. Gutter	3.7		465.5
" " " " Top. ch.	3.40		465.78
+30	" " 3.20		"
	0 + 75 = ⊕ Adams.		465.78
W. - 10	4.0		465.2
W	4.0		465.2
ch	4.0		465.2
1/4	3.8		465.4
⊕ Top. M.H.	3.56		465.62
1/4	3.9		465.3
ch	4.0		465.2
E	3.9		465.3
+10	3.9		465.3

	469.18	Soria	24
	0 + 90		
E - 20	Top. ch. 4.09		465.09
E - 10 = P.C. 20' R. Ret.	" " 3.28		465.20
" " " " " " G.	4.4		464.8
E. Line	4.2		465.0
E. of	4.1		465.1
"	3.8		465.4
⊕	3.7		465.5
1/4	4.0		465.2
W. of	4.1		465.1
W. Line	4.3		464.9
W. + 10 = P.R. 20' R. Ret. G	4.3		464.9
" " " " " " Top. ch.	3.67		465.57
W + 20	" " 3.54		465.64
	0 + 92.8		
W. Line Soria Top. ch. on Return	3.67		465.57
E " " " " " "	3.97		465.21
	1 + 00 = W. Line Adams. = 0 + 00		
E. Carb. Soria on Return	3.97		465.21
W " " " " "	3.70		465.48

469.18
 0+10 = P.C. 20' Radius Return

w. cl	3.73	465.45
G	4.5	464.7
"4	4.2	465.0
±	3.8	465.4
"4	3.9	465.3
G	4.2	465.0
E. cl	3.99	465.19
	0+50	
E. cl	4.35	464.83
G	4.8	464.4
"4	4.5	464.7
±	4.3	464.9
"4	4.5	464.7
G	4.9	464.3
w. cl	4.11	465.07
	1+00	
w. cl	4.46	464.72
G	5.2	464.0
"4	5.0	464.2
±	4.9	464.3

469.18

Soria

25

"4	5.1	464.1
G	5.3	463.9
E. cl	4.74	464.44
	1+50	
E. cl	5.10	464.08
G	5.7	463.5
"4	5.3	463.9
±	5.3	463.9
"4	5.5	463.7
G	5.4	463.8
w. cl	4.93	464.25
	2+00	
w. cl	5.36	463.82
G	5.9	463.3
"4	5.8	463.4
±	5.6	463.6
"4	5.8	463.4
G	6.1	463.1
E. cl	5.56	463.62

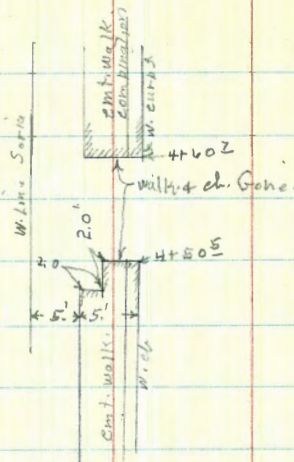
469.18 ✓
2+50

E. cl	6.03	463.15
G	6.7	462.5
"4	6.3	462.9
♀	6.0	463.2
"4	6.0	463.2
G	6.4	462.8
w. cl	5.78	463.40
✓	3+00	
w. cl	6.22	462.96
G	6.7	462.5
"4	6.6	462.6
♀	6.4	462.8
"4	6.6	462.6
G	6.8	462.4
E. cl	6.35	462.83
✓	3+50	
E. cl	6.74	462.44
G	7.3	461.9
"4	7.0	462.2
♀	6.7	462.5

469.18

26

"4	6.8	462.4
G	7.3	461.9
w. cl	6.63	462.55
✓	4+00	
w. cl	7.03	462.15
G	7.7	461.5
"4	7.4	461.8
♀	7.2	462.0
"4	7.4	461.8
G	7.7	461.5
E. cl	7.16	462.02
✓	4+50	
E. cl	7.43	461.75
G	7.8	461.4
"4	7.6	461.6
♀	7.5	461.7
"4	7.7	461.5
G	7.9	461.3
w. cl	7.43	461.85
T.P.	1.67	463.42
	7.43	461.75



463.42

5+00

w. ch	2.10	461.32
G	2.8	460.6
"4	2.4	461.0
±	2.4	461.0
"4	2.4	461.0
G	2.6	460.8
E. ch	2.11	461.33
E. ch	2.51	460.91
G	3.2	460.2

5+50

463.42

Sorin

27

"4	2.7	460.7
±	2.6	460.8
"4	2.9	460.5
G	3.2	460.2
w. ch	2.48	460.94
	6+00	
w. ch	2.95	460.47
G	3.6	459.8
"4	3.2	460.2
±	3.2	460.2
"4	3.5	459.9
G	3.4	460.0
E. ch	2.90	460.52
	6+50	
E. ch	3.52	459.90
G	4.4	459.0
"4	3.9	459.5
±	3.7	459.7
"4	4.0	459.4
G	4.7	458.7
w. ch	3.63	459.79

463.42
7+00

463.42

Soria

28

w. cl	4.26	459.16
G	5.1	458.3
"	4.7	458.7
cl	4.5	458.9
"	4.6	458.8
G	4.9	458.5
E. cl	4.11	459.31
E. cl	4.17	458.75
G	5.2	458.2
"	5.0	458.4
cl	4.8	458.6
"	5.2	458.2
G	5.5	457.9
w. cl	4.91	458.51
w. cl	5.56	457.16
G	5.9	457.5
"	5.6	457.8
cl	5.5	457.9

7+50

8+00

"	5.6	457.8
G	6.0	457.4
E. cl	5.21	458.21
E. cl	5.82	457.60
G	6.7	456.7
"	6.2	457.2
cl	6.0	457.4
"	6.1	457.3
G	6.7	456.7
w. cl	6.18	457.24
8+90, E. end		
8+91 3/4 on w. cl		
w. cl	6.70	456.72
ent. G. S. End	7.51	455.91
+ 3.5 " " S. " E. side	7.24	456.18
"	6.9	456.5
cl	6.8	456.6
"	6.8	456.6
+ 4.2' ent. gutter w edge S. End.	6.95	456.47
ent. Gutter S. End.	7.04	456.38
E. ent. cl	6.27	457.15

8+50

S. End. 20' Curb. Return
" " Concrete Gutter 3.5' wide

9+00.5 = S. Line Arosa st.

7.1 E. of W. Line = ch. on curve	6.90	456.52
7.19 " " = cent. gutter	7.62	455.74
11.3 " " = E. edge cent. gutter	7.44	455.98
13.3 W. of S. Line = W. edge cent. gutter	7.08	456.34
10 " " " " " "	7.17	456.25
7.4 " " " = E. edge " "	6.96	456.46
7.1 " " " = Top cent. ch. on curve	6.33	457.09

9+10.5 = S. ch. Line Arosa st.

E-30 Top. of ch. P.C. 20' Ret.	6.25	457.17
E-10 " " " "	6.35	457.07
E-10 G.	7.3	456.1
E Line	7.2	456.2
+ 7.4 = E. side cent. gutter	7.14	456.28
ch. line = ch. " "	7.36	456.06
+ 13.3 = W. " " "	7.24	456.18
1.4	7.1	456.5
ch	7.0	456.4
1.4	7.0	456.4
ch. line	7.4	456.10
+ 7.7 = Edge cent. gutter	7.85	455.57

W. Line on gutter	8.05	455.37
+ 10 = P.C. 20' Ret. Top. ch.	8.93	454.49
" " " " " " cent. G.	8.76	454.66
B.M. Top. Hydt.	3.74	459.68

S.E. Soria
& Arosa.

Grade Book 121-52

X sec Reynolds Rd,
6th St. EXT. to CITY LINE
Sec 1534-8

Moore
5-26-38

LT

2

RT

30

85

41.2	41.4	42.3	42.6	40.8	40.0	39.6
$\frac{11.5}{40}$	$\frac{11.5}{16}$	10.2	$\frac{10.1}{25}$	$\frac{11.9}{26}$	$\frac{12.7}{40}$	$\frac{13.1}{46}$

+50

42.5	43.1	42.9	42.6	40.8	39.6	39.0
$\frac{10.2}{40}$	$\frac{9.6}{50}$	9.8	$\frac{10.1}{16}$	$\frac{11.9}{19}$	$\frac{12.1}{40}$	$\frac{13.7}{50}$

82

44.9	44.3	43.4	43.3	41.1	39.4	38.7
$\frac{7.8}{40}$	$\frac{8.2}{50}$	9.3	$\frac{9.4}{9}$	$\frac{11.6}{16}$	$\frac{13.3}{57}$	$\frac{14.0}{50}$

+50

45.9	43.7	43.3	40.1	38.4	37.0	36.9
$\frac{6.8}{40}$	9.0	$\frac{9.2}{10}$	$\frac{12.6}{17}$	$\frac{14.3}{40}$	$\frac{15.7}{50}$	

81

42.9	42.79	43.51	43.4	43.1	39.2	37.7	36.6
$\frac{9.8}{40}$	$\frac{9.95}{54}$	$\frac{9.23}{9 \text{ Pav.}}$	9.3	$\frac{9.6}{12}$	$\frac{13.5}{50}$	$\frac{15.0}{40}$	$\frac{16.1}{50}$

80+69.07 B.C. LT

42.3	41.87	42.50	42.53	42.3	37.2	36.2	35.7
$\frac{10.4}{40}$	$\frac{10.85}{54 \text{ Pav.}}$	10.24	$\frac{10.21}{25 \text{ Pav.}}$	$\frac{10.4}{16 \text{ Pav.}}$	$\frac{15.1}{26}$	$\frac{16.1}{40}$	$\frac{17.0}{50}$

B.M. C.T. EC.
95+42.84 0.50 52.72
6th ST. EXT.

52.24 G.B. 1.54
by Chas. Walker 26

52.74

0

Curve 408: p75 of 39.91

+ 55.57 B.C. Pt.

+ 15.34 E.C.

T.P. 2.97 43.77 1194 40.80

84

+ 50

52.74

202.2

40.1	40.3	41.0	41.5	42.0	42.4	41.6	39.3
$\frac{12.6}{40}$	$\frac{12.4}{20}$	$\frac{11.7}{20}$	11.2	$\frac{10.7}{20}$	$\frac{10.1}{33}$	$\frac{11.1}{40}$	$\frac{12.4}{55}$
39.6	40.0	40.9	41.7	40.4	38.7		
$\frac{13.1}{40}$	$\frac{12.7}{30}$	11.8	$\frac{11.0}{22}$	$\frac{12.3}{40}$	$\frac{14.0}{50}$		
37.6	39.5	39.8	40.8	38.5	37.7		
$\frac{4.3}{40}$	$\frac{4.0}{12}$	3.0	$\frac{2.9}{30}$	$\frac{5.5}{55}$	$\frac{6.1}{50}$		
49.8	44.8	39.5	40.1	40.4	36.8	37.6	39.1
$\frac{4.5}{40}$	$\frac{4.0}{30}$	$\frac{4.2}{16}$	3.7	$\frac{2.4}{24}$	$\frac{7.0}{31}$	$\frac{4.2}{40}$	$\frac{4.7}{50}$
51.9	43.8	38.4	39.7	40.1	36.2	36.1	35.6
$\frac{8.1}{40}$	$\frac{0.0}{18}$	$\frac{5.4}{12}$	4.1	$\frac{4.3}{11}$	$\frac{7.2}{29}$	$\frac{7.7}{40}$	$\frac{8.2}{50}$

43.77

52.74

117.02

T.P. 301 38.84 7.94 45.83

87

+50

86+15.22 EC.

③

② = Junction of Murray Canyon Rd.

43.77

10.2	9.7	8.9	4.8	5.5	4.7	11.9	12.2	12.2
50	40	25	17	55	15	30	40	50
33.6	34.1	34.9	39.0	38.3	39.1	31.9	31.5	31.6
11.4	11.2	11.1	10.1	6.0	5.7	12.1	12.2	12.0
50	40	25	17	50	17	30	40	50
32.4	32.6	32.7	37.7	37.8	38.1	30.6	30.2	29.8
12.1	12.1	10.6	7.1	6.7	6.6	15.0	14.0	16.4
50	40	25	15	57	17	28	40	50
31.7	31.7	33.2	36.7	37.1	37.2	28.8	27.8	27.4
44.8	44.8	38.5	39.0	39.0	39.4	35.0	34.5	34.4
5.5	1.0	5.5	4.5	4.5	4.4	8.8	9.3	9.2
40	29	27	40	40	18	38	40	50
49.3	44.8	38.5	39.0	39.0	39.4	35.0	34.5	34.4
43.77	43.77	43.77	43.77	43.77	43.77	43.77	43.77	43.77

43.77

92 + 79 90° double 1-28" Murray
 1-30" Corr. 1. P. Culy. Creek

Fl. $\frac{290}{10}$ 28.94

92

$\frac{7.1}{50}$	$\frac{7.2}{40}$	$\frac{7.2}{40}$	$\frac{5.4}{19}$	$\frac{5.4}{19}$	$\frac{4.0}{16}$	$\frac{10.3}{27}$	$\frac{10.6}{40}$	$\frac{10.6}{50}$
31.7	31.5	31.5	33.2	33.4	34.2	28.5	28.2	28.2

91

$\frac{7.0}{50}$	$\frac{7.2}{40}$	$\frac{7.1}{40}$	$\frac{5.3}{17}$	$\frac{5.1}{17}$	$\frac{4.7}{17}$	$\frac{10.9}{27}$	$\frac{11.1}{40}$	$\frac{11.2}{50}$
31.8	31.6	31.7	33.5	33.7	34.1	27.9	27.7	27.6

90

$\frac{7.3}{50}$	$\frac{7.2}{40}$	$\frac{7.0}{18}$	$\frac{4.1}{13}$	$\frac{4.5}{17}$	$\frac{4.5}{17}$	$\frac{11.4}{27}$	$\frac{11.9}{40}$	$\frac{12.0}{50}$
31.5	31.5	31.8	34.7	34.3	34.3	27.2	26.9	26.8

89

$\frac{7.5}{50}$	$\frac{7.5}{40}$	$\frac{7.2}{31}$	$\frac{4.0}{12}$	$\frac{4.0}{18}$	$\frac{4.1}{18}$	$\frac{11.7}{20}$	$\frac{12.2}{40}$	$\frac{12.2}{50}$
31.3	31.3	31.5	34.8	34.8	34.7	27.1	26.6	26.6

88

$\frac{7.0}{50}$	$\frac{7.2}{40}$	$\frac{7.2}{31}$	$\frac{3.0}{12}$	$\frac{3.2}{17}$	$\frac{3.6}{17}$	$\frac{12.0}{22}$	$\frac{12.8}{40}$	$\frac{13.0}{50}$
31.8	31.4	31.6	35.8	35.6	35.2	26.8	26.0	25.8

38.84

38.84

95

+50.24 BC.LT.

94

T.P. 824 42.76 432 34.52

+50

93

3884

332.01

40	30.5
40	30.5
40	30.3
40	33.5
40	33.5
40	33.2
40	32.6
40	33.2

40	35.2
40	34.4
40	34.3
40	33.9
40	34.1
40	32.2
40	32.4

42.76

3884

40	9.6	33.3	34.6	35.2
40	9.3	33.8	34.6	34.4
40	7.0	35.0	34.2	34.3
40	7.1	35.0	34.6	33.9
40	6.8	35.1	34.8	34.1
40	4.2	39.9	32.2	32.2
40	6.0	39.8	39.6	32.4
40	4.1	38.2		

401.74

+ 50

97

+ 50

94 + 75

7P. 30 Ar.

7.0V

47.58

2.20

40.56

RR spike
Tel. pole

96

95 + 50

42.76

37.6	38.4	43.6	43.2	40.4	41.0	41.6	37.5	37.1	35.3	32.6
10.0	9.2	4.0	4.2	7.2	6.6	6.0	10.1	10.5	12.2	12.7
50	40	35	18	15	15	15	22	33	20	10
3.0	1.0			4.7	4.2	5.2	5.5	5.7	10.0	12.7
40	18			15	15	14	19	31	40	44
50.6	46.4			42.9	43.4	44.2	42.1	41.9		34.5

34.4	34.5	34.4	38.5	39.0	40.0	34.7	33.0	31.0
13.2	12.1	12.2	9.1	8.6	7.6	12.9	12.6	12.6
50	40	35	15	15	15	33	40	50
34.4	34.5	34.4	38.5	39.0	40.0	34.7	33.0	31.0
13.2	12.1	12.2	9.1	8.6	7.6	12.9	12.6	12.6
50	40	35	15	15	15	33	40	50

33.3	33.5	37.9	38.1	37.1	37.4	38.3	33.2	32.6	30.1
9.5	9.3	4.9	4.7	5.7	5.4	4.5	9.6	10.2	12.7
50	40	38	17	16	15	27	26	40	50
36.8	37.2	36.0	36.5	37.7	34.2	31.7			
4.0	5.6	6.8	6.3	6.7	8.6	11.1			
20	18	15	15	15	40	50			

42.76

+50

99

+50

T.P. 10.94 58.05 049 47.09

+25.08 E.C.

98

47.58

$\frac{3.3}{40}$	$\frac{5.4}{40}$	$\frac{51.7}{40}$	$\frac{54.8}{40}$
$\frac{1.5}{17}$	$\frac{6.6}{19}$	$\frac{50.5}{20}$	$\frac{53.0}{20}$
$\frac{8.0}{17}$	$\frac{10.2}{16}$	$\frac{46.5}{16}$	$\frac{50.1}{17}$
$\frac{7.7}{20}$	$\frac{9.3}{20}$	$\frac{47.0}{20}$	$\frac{50.4}{20}$
$\frac{7.1}{20}$	$\frac{8.7}{20}$	$\frac{47.9}{20}$	$\frac{51.0}{20}$
$\frac{7.1}{40}$	$\frac{8.6}{40}$	$\frac{48.0}{40}$	$\frac{50.9}{40}$

$\frac{4.0}{40}$	$\frac{3.5}{19}$	$\frac{2.2}{16}$	$\frac{1.6}{16}$	$\frac{0.8}{20}$	$\frac{1.1}{40}$	$\frac{4.9}{50}$
$\frac{51.2}{40}$	$\frac{51.1}{19}$	$\frac{45.2}{16}$	$\frac{46.0}{16}$	$\frac{46.8}{20}$	$\frac{46.5}{40}$	$\frac{42.7}{50}$
$\frac{50.4}{40}$	$\frac{50.1}{18}$	$\frac{44.5}{16}$	$\frac{45.1}{16}$	$\frac{46.2}{20}$	$\frac{42.4}{40}$	$\frac{42.1}{50}$
$\frac{28}{40}$	$\frac{2.5}{18}$	$\frac{2.1}{16}$	$\frac{2.5}{16}$	$\frac{1.4}{20}$	$\frac{5.2}{35}$	$\frac{5.5}{40}$
						$\frac{5.5}{50}$

47.58

+50

102

+50

101

+50

100

58.05

$\frac{1.1}{40} \overline{) 57.0}$

$\frac{3.4}{19} \overline{) 54.7}$

$\frac{7.0}{16} \overline{) 51.1}$

$\frac{0.2}{20} \overline{) 51.8}$

$\frac{5.6}{20} \overline{) 52.5}$

$\frac{6.0}{40} \overline{) 52.1}$

$\frac{2.4}{40} \overline{) 60.7}$

$\frac{0.0}{19} \overline{) 58.1}$

$\frac{5.0}{15} \overline{) 52.5}$

$\frac{5.2}{20} \overline{) 52.6}$

$\frac{2.8}{20} \overline{) 53.3}$

$\frac{5.0}{40} \overline{) 53.1}$

$\frac{6.0}{40} \overline{) 64.1}$

$\frac{11.9}{19} \overline{) 60.0}$

$\frac{5.0}{14} \overline{) 53.1}$

$\frac{4.6}{20} \overline{) 53.0}$

$\frac{5.3}{40} \overline{) 53.5}$

$\frac{5.3}{40} \overline{) 52.8}$

$\frac{11.4}{40} \overline{) 69.5}$

$\frac{6.8}{22} \overline{) 64.9}$

$\frac{5.2}{15} \overline{) 52.9}$

$\frac{5.2}{15} \overline{) 52.9}$

$\frac{2.0}{20} \overline{) 53.5}$

$\frac{4.9}{21} \overline{) 53.2}$

$\frac{9.3}{40} \overline{) 48.8}$

$\frac{10.0}{50} \overline{) 47.5}$

$\frac{18.1}{40} \overline{) 71.2}$

$\frac{6.1}{22} \overline{) 64.2}$

$\frac{5.2}{15} \overline{) 52.6}$

$\frac{5.2}{15} \overline{) 52.6}$

$\frac{5.2}{20} \overline{) 52.7}$

$\frac{5.2}{21} \overline{) 52.8}$

$\frac{14.6}{20} \overline{) 44.5}$

$\frac{18.5}{45} \overline{) 39.6}$

$\frac{13.2}{40} \overline{) 71.3}$

$\frac{6.5}{22} \overline{) 64.6}$

$\frac{5.2}{15} \overline{) 52.4}$

$\frac{6.0}{18} \overline{) 52.1}$

$\frac{19.2}{40} \overline{) 38.9}$

$\frac{15.5}{60} \overline{) 32.5}$

102

37

58.05

107

$\frac{+ 17.1}{40}$	$\frac{+ 12.2}{40}$	$\frac{2.9}{16}$	$\frac{2.9}{16}$	$\frac{2.9}{15}$	$\frac{18.2}{40}$	$\frac{22.4}{60}$
69.5	62.6	47.5	47.5	47.5	32.2	28.2

+ 67.57 E.C.

$\frac{+ 18.5}{40}$	$\frac{+ 10.0}{40}$	$\frac{2.7}{15}$	$\frac{2.7}{15}$	$\frac{2.8}{15}$	$\frac{18.3}{40}$	$\frac{22.0}{60}$
68.9	60.4	47.7	47.7	47.6	32.1	28.4

+ 50

$\frac{+ 19.0}{40}$	$\frac{+ 11.4}{40}$	$\frac{2.4}{15}$	$\frac{2.6}{15}$	$\frac{2.7}{15}$	$\frac{18.2}{40}$	$\frac{21.2}{60}$
69.4	61.8	48.0	47.8	47.7	32.2	29.0

104

$\frac{+ 17.8}{40}$	$\frac{+ 16.8}{40}$	$\frac{2.1}{15}$	$\frac{1.9}{15}$	$\frac{2.1}{15}$	$\frac{15.1}{40}$	$\frac{21.2}{60}$
68.2	62.2	48.3	48.5	48.3	35.3	29.2

T.P. 116 50.39 8.82 49.23

105 + 50

$\frac{+ 7.4}{40}$	$\frac{+ 0.7}{40}$	$\frac{8.2}{17}$	$\frac{8.8}{17}$	$\frac{8.6}{15}$	$\frac{24.6}{42}$	$\frac{29.1}{60}$
65.5	58.8	49.9	49.3	49.5	33.5	29.0

58.05

58.05

+ 78.26 B.C. Pt.

+ 50

109

+ 50

108

+ 50

50.39

+ 18.1
68.5
40

+ 14.0
64.9
40

+ 16.5
66.9
40

+ 14.7
65.1
40

+ 16.1
67.0
40

+ 14.4 + 10.1
64.8
40

+ 7.1
57.5
22

+ 7.7
58.1
22

+ 4.7
55.1
20

+ 4.7
55.1
20

+ 7.0
57.4
22

+ 10.1
60.5
22

+ 5.1
45.0
15

+ 5.3
45.1
15

+ 4.7
45.7
15

+ 4.5
45.9
15

+ 2.3
46.1
15

+ 3.5
46.9
15

+ 5.1
45.0
15

+ 5.2
45.2
15

+ 4.9
45.5
10

+ 4.4
46.0
16

+ 3.9
46.5
15

+ 3.3
47.1
15

+ 5.2
45.2
19

+ 5.2
45.2
17

+ 4.9
45.5
10

+ 4.0
46.0
16

+ 3.8
46.6
15

+ 3.4
47.0
15

+ 17.4
33.0
40

+ 17.6
32.8
40

+ 17.9
32.5
40

+ 17.9
32.5
40

+ 17.7
32.7
40

+ 18.2
32.2
40

+ 20.2
30.2
40

+ 21.0
29.4
40

+ 21.6
28.8
40

+ 21.9
28.5
40

+ 22.7
27.7
40

+ 22.2
28.2
40

50.39

117

$\frac{66.6}{40}$	$\frac{56.4}{20}$	$\frac{45.9}{15}$	$\frac{45.8}{16}$	$\frac{45.5}{18}$	$\frac{40.4}{27}$	$\frac{39.3}{40}$	$\frac{37.4}{40}$
$\frac{12.2}{10}$	$\frac{3.7}{20}$	$\frac{4.4}{15}$	$\frac{4.4}{16}$	$\frac{4.5}{18}$	$\frac{9.6}{27}$	$\frac{9.8}{40}$	$\frac{9.7}{50}$
66.6	56.4	45.9	45.8	45.5	40.4	39.3	37.4

+50

$\frac{65.1}{40}$	$\frac{57.5}{20}$	$\frac{45.6}{15}$	$\frac{45.4}{16}$	$\frac{45.4}{18}$	$\frac{39.8}{27}$	$\frac{38.40}{40}$	$\frac{35.8}{40}$
$\frac{14.7}{10}$	$\frac{7.1}{20}$	$\frac{4.8}{15}$	$\frac{4.0}{16}$	$\frac{5.0}{18}$	$\frac{10.6}{27}$	$\frac{12.0}{40}$	$\frac{14.6}{50}$
65.1	57.5	45.6	45.4	45.4	39.8	38.40	35.8

111

$\frac{67.5}{40}$	$\frac{58.6}{20}$	$\frac{45.2}{15}$	$\frac{45.2}{16}$	$\frac{45.0}{18}$	$\frac{40.2}{27}$	$\frac{35.8}{40}$	$\frac{33.6}{40}$
$\frac{17.1}{10}$	$\frac{8.2}{20}$	$\frac{5.1}{15}$	$\frac{5.1}{16}$	$\frac{5.4}{18}$	$\frac{10.2}{27}$	$\frac{14.6}{40}$	$\frac{16.8}{50}$
67.5	58.6	45.2	45.2	45.0	40.2	35.8	33.6

+71

18" Corr. I.P. Culv. 90°

FL inlet $\frac{7.75}{15}$ $\frac{42.64}{15}$ $\frac{40.47}{15}$ FL

110

$\frac{68.1}{40}$	$\frac{56.4}{19}$	$\frac{45.1}{15}$	$\frac{45.0}{16}$	$\frac{44.5}{19}$	$\frac{32.8}{40}$	$\frac{31.1}{40}$
$\frac{17.7}{10}$	$\frac{6.0}{19}$	$\frac{5.2}{15}$	$\frac{5.2}{16}$	$\frac{5.9}{19}$	$\frac{17.6}{40}$	$\frac{19.3}{40}$
68.1	56.4	45.1	45.0	44.5	32.8	31.1

50.39

50.39

114

+50

113

+50

T.P.

773

53.67

445

45.94

114 + 30.46 EC

50.39

$$\begin{array}{r} + 10.0 \\ \hline 40 \\ \hline \end{array}$$

$$\begin{array}{r} + 4.6 \\ \hline 40 \\ \hline \end{array}$$

$$\begin{array}{r} + 4.0 \\ \hline 40 \\ \hline \end{array}$$

$$\begin{array}{r} + 4.8 \\ \hline 40 \\ \hline \end{array}$$

$$\begin{array}{r} + 9.7 \\ \hline 40 \\ \hline \end{array}$$

$$\begin{array}{r} + 7.1 \\ \hline 54 \\ \hline \end{array}$$

$$\begin{array}{r} + 2.0 \\ \hline 23 \\ \hline \end{array}$$

$$\begin{array}{r} + 1.0 \\ \hline 19 \\ \hline \end{array}$$

$$\begin{array}{r} + 1.5 \\ \hline 30.5 \\ \hline \end{array}$$

$$\begin{array}{r} + 2.7 \\ \hline 19 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ \hline 11 \\ \hline \end{array}$$

$$\begin{array}{r} 7.0 \\ \hline 16 \\ \hline \end{array}$$

$$\begin{array}{r} 6.8 \\ \hline 15 \\ \hline \end{array}$$

$$\begin{array}{r} 7.6 \\ \hline 16 \\ \hline \end{array}$$

$$\begin{array}{r} 2.8 \\ \hline 15 \\ \hline \end{array}$$

$$\begin{array}{r} 0.5 \\ \hline 0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 6.9 \\ \hline 6.9 \\ \hline \end{array}$$

$$\begin{array}{r} 7.4 \\ \hline 7.4 \\ \hline \end{array}$$

$$\begin{array}{r} 7.6 \\ \hline 7.6 \\ \hline \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 4.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ \hline 19 \\ \hline \end{array}$$

$$\begin{array}{r} 6.6 \\ \hline 18 \\ \hline \end{array}$$

$$\begin{array}{r} 6.9 \\ \hline 18 \\ \hline \end{array}$$

$$\begin{array}{r} 7.9 \\ \hline 24 \\ \hline \end{array}$$

$$\begin{array}{r} 2.4 \\ \hline 19 \\ \hline \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 23 \\ \hline \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline 22 \\ \hline \end{array}$$

$$\begin{array}{r} 7.9 \\ \hline 40 \\ \hline \end{array}$$

$$\begin{array}{r} 11.7 \\ \hline 31 \\ \hline \end{array}$$

$$\begin{array}{r} 8.7 \\ \hline 24 \\ \hline \end{array}$$

$$\begin{array}{r} 4.7 \\ \hline 23 \\ \hline \end{array}$$

$$\begin{array}{r} 4.1 \\ \hline 40 \\ \hline \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline 40 \\ \hline \end{array}$$

$$\begin{array}{r} 11.7 \\ \hline 50 \\ \hline \end{array}$$

$$\begin{array}{r} 9.1 \\ \hline 40 \\ \hline \end{array}$$

$$\begin{array}{r} 13.7 \\ \hline 13.7 \\ \hline \end{array}$$

$$\begin{array}{r} 60.8 \\ \hline 60.8 \\ \hline \end{array}$$

$$\begin{array}{r} 47.2 \\ \hline 47.2 \\ \hline \end{array}$$

$$\begin{array}{r} 47.2 \\ \hline 47.2 \\ \hline \end{array}$$

$$\begin{array}{r} 47.6 \\ \hline 47.6 \\ \hline \end{array}$$

$$\begin{array}{r} 49.3 \\ \hline 49.3 \\ \hline \end{array}$$

$$\begin{array}{r} 49.3 \\ \hline 49.3 \\ \hline \end{array}$$

50.39

+50

+0987 BC RA

116

+50

115

114+50

53.67

$$\begin{array}{r} 61.7 \\ + \frac{80}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 64.3 \\ + \frac{10.0}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 64.8 \\ + \frac{11.1}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 67.4 \\ + \frac{13.7}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 68.4 \\ + \frac{15.4}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 67.8 \\ + \frac{14.1}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 58.7 \\ + \frac{5.0}{19} \\ \hline \end{array}$$

$$\begin{array}{r} 61.0 \\ + \frac{7.0}{23} \\ \hline \end{array}$$

$$\begin{array}{r} 61.8 \\ + \frac{8.1}{23} \\ \hline \end{array}$$

$$\begin{array}{r} 64.7 \\ + \frac{11.0}{27} \\ \hline \end{array}$$

$$\begin{array}{r} 66.0 \\ + \frac{12.0}{28} \\ \hline \end{array}$$

$$\begin{array}{r} 65.8 \\ + \frac{11.6}{27} \\ \hline \end{array}$$

$$\begin{array}{r} 49.6 \\ + \frac{4.1}{17} \\ \hline \end{array}$$

$$\begin{array}{r} 49.6 \\ + \frac{4.1}{17} \\ \hline \end{array}$$

$$\begin{array}{r} 49.5 \\ + \frac{4.2}{17} \\ \hline \end{array}$$

$$\begin{array}{r} 49.0 \\ + \frac{4.7}{17} \\ \hline \end{array}$$

$$\begin{array}{r} 48.4 \\ + \frac{5.0}{17} \\ \hline \end{array}$$

$$\begin{array}{r} 47.7 \\ + \frac{6.0}{16} \\ \hline \end{array}$$

$$\begin{array}{r} 50.0 \\ + \frac{3.7}{17} \\ \hline \end{array}$$

$$\begin{array}{r} 47.8 \\ + \frac{3.9}{17} \\ \hline \end{array}$$

$$\begin{array}{r} 49.7 \\ + \frac{4.0}{17} \\ \hline \end{array}$$

$$\begin{array}{r} 49.1 \\ + \frac{4.6}{17} \\ \hline \end{array}$$

$$\begin{array}{r} 48.4 \\ + \frac{5.0}{17} \\ \hline \end{array}$$

$$\begin{array}{r} 47.7 \\ + \frac{6.0}{16} \\ \hline \end{array}$$

$$\begin{array}{r} 50.2 \\ + \frac{2.0}{21} \\ \hline \end{array}$$

$$\begin{array}{r} 49.9 \\ + \frac{2.0}{21} \\ \hline \end{array}$$

$$\begin{array}{r} 49.9 \\ + \frac{2.0}{21} \\ \hline \end{array}$$

$$\begin{array}{r} 49.2 \\ + \frac{4.5}{20} \\ \hline \end{array}$$

$$\begin{array}{r} 48.6 \\ + \frac{5.1}{20} \\ \hline \end{array}$$

$$\begin{array}{r} 48.0 \\ + \frac{5.7}{20} \\ \hline \end{array}$$

$$\begin{array}{r} 51.4 \\ + \frac{2.0}{24} \\ \hline \end{array}$$

$$\begin{array}{r} 51.3 \\ + \frac{2.0}{24} \\ \hline \end{array}$$

$$\begin{array}{r} 51.3 \\ + \frac{2.4}{24} \\ \hline \end{array}$$

$$\begin{array}{r} 51.1 \\ + \frac{2.6}{23} \\ \hline \end{array}$$

$$\begin{array}{r} 50.5 \\ + \frac{5.2}{23} \\ \hline \end{array}$$

$$\begin{array}{r} 50.1 \\ + \frac{5.2}{23} \\ \hline \end{array}$$

$$\begin{array}{r} 49.9 \\ + \frac{3.0}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 51.1 \\ + \frac{2.0}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 51.0 \\ + \frac{2.0}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 51.1 \\ + \frac{2.0}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 50.3 \\ + \frac{2.0}{40} \\ \hline \end{array}$$

$$\begin{array}{r} 49.7 \\ + \frac{2.0}{40} \\ \hline \end{array}$$

53.67

+50

TP 7.70 59.74 1.63 52.04

118

+50

+28

18" Cul. 40' Corrs 1P.

117

53.67

$\frac{1.2}{1.0} \overline{) 57.5}$

$\frac{4.0}{3.0} \overline{) 55.7}$

$\frac{2.7}{2.1} \overline{) 53.0}$

$\frac{2.0}{2.0} \overline{) 52.4}$

$\frac{7.6}{7.5} \overline{) 52.9}$

$\frac{16.8}{16.0} \overline{) 42.9}$

$\frac{1.8}{1.8} \overline{) 41.10}$

$\frac{20.1}{19.0} \overline{) 39.6}$

$\frac{2.5}{4.0} \overline{) 58.2}$

$\frac{3.0}{3.0} \overline{) 56.7}$

$\frac{0.7}{3.6} \overline{) 53.0}$

$\frac{1.7}{1.4} \overline{) 52.0}$

$\frac{1.7}{1.7} \overline{) 52.0}$

$\frac{1.7}{2.2} \overline{) 52.0}$

$\frac{7.5}{2.9} \overline{) 46.2}$

$\frac{10.0}{4.0} \overline{) 43.7}$

$\frac{11.3}{5.0} \overline{) 42.4}$

$\frac{1.0}{1.0} \overline{) 55.7}$

$\frac{0.0}{0.0} \overline{) 53.7}$

$\frac{1.3}{1.3} \overline{) 52.4}$

$\frac{1.2}{1.2} \overline{) 51.4}$

$\frac{1.4}{1.4} \overline{) 51.3}$

$\frac{1.1}{1.0} \overline{) 51.6}$

$\frac{7.7}{3.0} \overline{) 46.0}$

$\frac{1.8}{1.0} \overline{) 46.9}$

$\frac{5.9}{5.0} \overline{) 44.2}$

$\frac{4.90}{1.4} \overline{) 48.77}$

$\frac{2.4}{1.0} \overline{) 56.1}$

$\frac{0.8}{1.5} \overline{) 54.5}$

$\frac{3.6}{3.6} \overline{) 50.4}$

$\frac{3.0}{3.0} \overline{) 50.7}$

$\frac{2.7}{2.0} \overline{) 51.0}$

$\frac{5.0}{2.0} \overline{) 48.7}$

$\frac{7.2}{4.0} \overline{) 46.5}$

$\frac{10.0}{5.0} \overline{) 47.0}$

53.67

121

+86.93 EC.

+50

120

+50

119

59.74

70	52.5	70	52.7	70	59.6	70	66.8	70	67.1	70	67.7
19.1	52.4	15.9	52.8	16.0	53.7	15.4	54.3	15.1	54.7	14.7	55.0
19.1	52.7	15.9	53.0	16.2	53.5	15.4	54.3	14.8	54.9	14.7	55.0
19.1	53.0	15.8	52.9	16.3	53.6	15.0	54.7	14.4	55.3	14.4	55.3
19.1	40.6	22.2	37.5	22.1	35.6	22.8	36.9	21.1	38.6	21.0	38.7
19.1	39.9	22.1	33.6	21.8	33.9	21.5	34.6	21.0	36.6	21.0	37.0
19.1	38.2	21.5		21.8		21.5		21.0		21.0	
19.1		21.5		21.8		21.5		21.0		21.0	

59.74

+50

134

+50

133

+50

132

57.58

$\frac{13.1}{40}$	$\frac{68.3}{40}$	$\frac{65.9}{40}$	$\frac{63.6}{40}$	$\frac{70.7}{40}$
$\frac{11.1}{32}$	$\frac{65.0}{32}$	$\frac{62.6}{35}$	$\frac{59.5}{22}$	$\frac{68.7}{32}$
$\frac{2.7}{17}$	$\frac{54.2}{19}$	$\frac{54.6}{19}$	$\frac{53.0}{18}$	$\frac{54.9}{17}$
$\frac{2.5}{27}$	$\frac{54.5}{31}$	$\frac{54.0}{24}$	$\frac{53.4}{42}$	$\frac{55.1}{25}$
$\frac{2.0}{27}$	$\frac{54.6}{15}$	$\frac{54.0}{14}$	$\frac{53.5}{15}$	$\frac{55.6}{27}$
$\frac{5.0}{30}$	$\frac{53.9}{66}$	$\frac{49.5}{34}$	$\frac{51.4}{30}$	$\frac{53.6}{30}$
$\frac{5.6}{40}$	$\frac{50.6}{30}$	$\frac{48.0}{40}$	$\frac{44.1}{42}$	$\frac{52.0}{40}$
$\frac{7.5}{50}$	$\frac{49.6}{50}$	$\frac{46.0}{50}$	$\frac{42.8}{50}$	$\frac{50.1}{50}$
$\frac{4.8}{40}$	$\frac{62.4}{40}$	$\frac{56.9}{21}$	$\frac{62.4}{40}$	$\frac{62.4}{40}$
$\frac{0.7}{21}$	$\frac{56.9}{21}$	$\frac{52.0}{18}$	$\frac{52.0}{16}$	$\frac{52.0}{18}$
$\frac{13.3}{32}$	$\frac{44.30}{32}$	$\frac{53.6}{16}$	$\frac{53.6}{16}$	$\frac{53.6}{16}$
$\frac{14.8}{20}$	$\frac{42.8}{20}$	$\frac{44.30}{32}$	$\frac{42.8}{20}$	$\frac{44.30}{32}$
$\frac{15.7}{39}$	$\frac{42.0}{20}$	$\frac{41.9}{50}$	$\frac{41.9}{50}$	$\frac{41.9}{50}$
$\frac{17.7}{50}$	$\frac{41.2}{50}$	$\frac{41.9}{50}$	$\frac{41.9}{50}$	$\frac{41.9}{50}$

85/5

+50

$\begin{array}{r} 74.7 \\ + 1.5 \\ \hline 76.2 \end{array}$

$\begin{array}{r} 67.4 \\ + 1.8 \\ \hline 69.2 \end{array}$

$\begin{array}{r} 53.3 \\ + 1.9 \\ \hline 55.2 \end{array}$

$\begin{array}{r} 54.2 \\ + 1.5 \\ \hline 55.7 \end{array}$

$\begin{array}{r} 54.4 \\ + 1.8 \\ \hline 56.2 \end{array}$

$\begin{array}{r} 40.6 \\ + 1.8 \\ \hline 42.4 \end{array}$

$\begin{array}{r} 38.9 \\ + 1.4 \\ \hline 40.3 \end{array}$

$\begin{array}{r} 33.9 \\ + 1.5 \\ \hline 35.4 \end{array}$

$\begin{array}{r} 33.9 \\ + 1.5 \\ \hline 35.4 \end{array}$

138

+50

$\begin{array}{r} 73.5 \\ + 1.7 \\ \hline 75.2 \end{array}$

$\begin{array}{r} 68.1 \\ + 1.5 \\ \hline 69.6 \end{array}$

$\begin{array}{r} 53.7 \\ + 1.4 \\ \hline 55.1 \end{array}$

$\begin{array}{r} 53.8 \\ + 1.2 \\ \hline 55.0 \end{array}$

$\begin{array}{r} 54.1 \\ + 1.1 \\ \hline 55.2 \end{array}$

$\begin{array}{r} 39.6 \\ + 1.0 \\ \hline 40.6 \end{array}$

$\begin{array}{r} 37.7 \\ + 1.4 \\ \hline 39.1 \end{array}$

$\begin{array}{r} 34.0 \\ + 1.5 \\ \hline 35.5 \end{array}$

$\begin{array}{r} 33.8 \\ + 1.5 \\ \hline 35.3 \end{array}$

139

+27.24 B.C. LT.

$\begin{array}{r} 73.4 \\ + 1.1 \\ \hline 74.5 \end{array}$

$\begin{array}{r} 67.8 \\ + 1.0 \\ \hline 68.8 \end{array}$

$\begin{array}{r} 52.6 \\ + 1.2 \\ \hline 53.8 \end{array}$

$\begin{array}{r} 52.7 \\ + 1.0 \\ \hline 53.7 \end{array}$

$\begin{array}{r} 38.2 \\ + 1.1 \\ \hline 39.3 \end{array}$

$\begin{array}{r} 37.9 \\ + 1.4 \\ \hline 39.3 \end{array}$

+50

$\begin{array}{r} 74.9 \\ + 1.3 \\ \hline 76.2 \end{array}$

$\begin{array}{r} 64.9 \\ + 1.5 \\ \hline 66.4 \end{array}$

$\begin{array}{r} 52.3 \\ + 1.0 \\ \hline 53.3 \end{array}$

$\begin{array}{r} 52.2 \\ + 1.0 \\ \hline 53.2 \end{array}$

$\begin{array}{r} 52.6 \\ + 1.0 \\ \hline 53.6 \end{array}$

$\begin{array}{r} 37.7 \\ + 1.4 \\ \hline 39.1 \end{array}$

$\begin{array}{r} 37.7 \\ + 1.4 \\ \hline 39.1 \end{array}$

$\begin{array}{r} 33.2 \\ + 1.0 \\ \hline 34.2 \end{array}$

$\begin{array}{r} 33.2 \\ + 1.0 \\ \hline 34.2 \end{array}$

59.32

59.32

+65 18° Corr. 1 PCW. 90°

+50

T.P. 5.77 56.92 8.17 51.15

141

+50

140

59.32

FL. INLET

9.20
15

47.52

11.77
27

FL.

45.15

+ 12.1	+ 4.0	60	51.1	51.3	43.9	35.6	34.4
40	23	15	5.8	1.6	2.8	16.0	2.4
69.0	60.9	50.9					

56.92

+ 12.2	+ 5.6	18.2	51.0	51.8	33.7	33.7
40	21	12	8.0	1.5	5.0	10.0
72.5	62.9	50.9				

+ 15.2	+ 7.0	17.7	51.4	52.1	33.8	33.3
40	23	14	1.9	2.0	5.0	7.0
74.9	66.3	51.6				

+ 14.7	+ 9.5	7.4	51.8	52.3	34.1	33.2
40	26	14	7.5	1.7	2.2	7.0
76.0	68.0	51.9				

59.32

+50

144

+50

143

+50

142

56.92

56.92

$$\begin{array}{r} + 20.1 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 19.5 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 13.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 8.1 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 8.1 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 9.2 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 16.4 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 13.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 7.8 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 4.6 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 8.8 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 11.7 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 12.2 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 11.1 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 5.2 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 6.0 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 6.5 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 6.5 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 12.2 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 11.1 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 5.2 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 5.4 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 5.5 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 5.4 \\ \hline 17 \end{array}$$

$$\begin{array}{r} + 15.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 12.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 5.4 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 5.2 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 4.8 \\ \hline 18 \end{array}$$

$$\begin{array}{r} + 12.2 \\ \hline 28 \end{array}$$

$$\begin{array}{r} + 13.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 12.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 14.6 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 19.2 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 16.2 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 12.2 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 22.1 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 21.6 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 2.6 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 20.8 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 10.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} + 24.7 \\ \hline 60 \end{array}$$

$$\begin{array}{r} + 23.4 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 22.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 2.4 \\ \hline 20 \end{array}$$

$$\begin{array}{r} + 20.6 \\ \hline 40 \end{array}$$

$$\begin{array}{r} + 20.0 \\ \hline 60 \end{array}$$

$$\begin{array}{r} + 24.8 \\ \hline 70 \end{array}$$

77.0

73.1

51.6

51.7

51.9

43.9

34.8

33.5

76.4

70.5

51.8

51.7

52.1

43.9

34.5

33.9

70.5

64.7

51.5

51.6

51.5

42.3

35.3

34.5

65.0

59.5

50.9

51.5

51.7

37.7

36.1

36.3

65.0

60.7

50.5

51.4

52.1

40.5

40.6

36.9

36.5

66.1

58.6

50.7

51.1

51.5

42.7

42.7

32.2

32.1

+50

+15

1471 70.00
15 RT
T.P. 147+75

3.43

57.27

3.08

53.84

148 Wly edge of borrow pit

June 1, 38.

Johnson + Cordell
Rock Plant

147+50

146+94 24 BC RT

56.92

+ 3.3
70

+ 3.3
70

+ 3.3
70

+ 3.3
70

78.3
+ 31.2
40

70.5
+ 18.6
26

52.2
4.7
15

52.9
4.0
27

46.2
10.7
38

41.8
15.1
24

34.2
22.7
25

73.0
+ 16.1
20

64.3
+ 7.4
24

51.9
5.0
15

52.2
4.7
18

43.9
13.0
30

35.5
21.4
45

33.9
22.0
60

24.8
5.2
20

80.9

73.3

51.8

52.1

52.0

44.4

34.7

32.7

26.7

+ 24.0
20

+ 16.4
29

5.1
15

4.8
17

12.5
30

58.2
50

24.2
60

30.2
70

+ 3.3
70

+ 3.3
70

+ 3.3
70

+ 3.3
70

54.9
2.2
40

52.9
2.2
15

52.5
4.8

52.6
4.7
44

47.2
10.1
40

43.5
13.8
28

35.3
22.0
45

28.6
28.7
75

57.27

56.92

151

Nail Tel. pole
20 RT.
T.P. 150 + 25

60Y 58.69 4.00 52.67

+51.63 B.C. RT.

150

+58.13 E.C.

149

57.27

57

40 55.7

40 54.5

51 53.6

45 53.1

45 40.0

45 36.3

70 36.3

40 55.3

41 53.4

41 53.2

45 53.3

45 39.4

45 36.3

70 35.5

40 53.6

41 53.2

42 53.1

45 52.8

45 36.0

45 35.1

40 54.3

42 52.9

42 52.7

45 52.9

45 37.2

45 34.8

40 53.8

45 52.3

46 52.0

45 52.1

45 45.1

45 41.5

60 39.3

65 37.1

58.69

57.27

Contd. in 1555 - p 21

T.P.

454 54.15

155

+50

154 + 00.03 B.C. RT

+50

5869

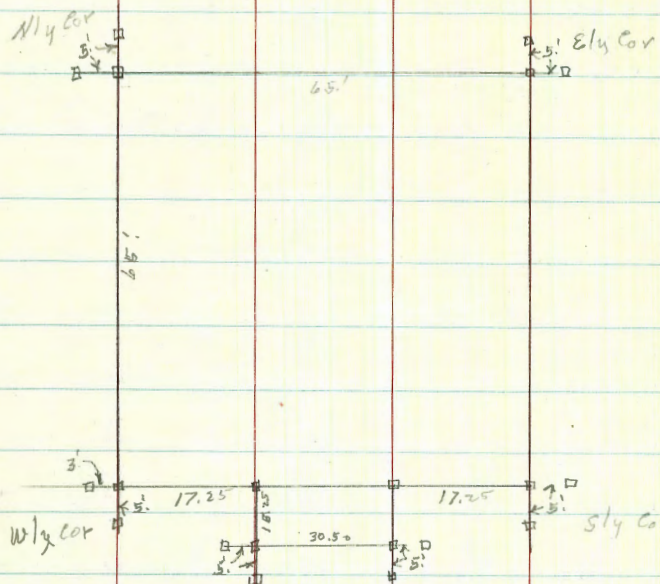
74.9	67.1	53.8	54.1	54.3	32.7	36.8
+ 16.2	+ 8.4	4.9	4.6	4.4	19	22.4
<u>91.1</u>	<u>75.5</u>	<u>58.7</u>	<u>58.7</u>	<u>58.7</u>	<u>51.7</u>	<u>59.2</u>
75.6	64.90	54.0	54.0	54.3	44.7	36.6
+ 14.8	+ 6.2	4.7	4.7	4.4	12.0	22.1
<u>90.4</u>	<u>71.1</u>	<u>58.7</u>	<u>58.7</u>	<u>58.7</u>	<u>56.7</u>	<u>58.7</u>
67.5	60.8	53.6	54.0	54.5	45.2	41.7
+ 8.8	+ 2.1	5.1	4.7	4.2	13.5	17.0
<u>76.3</u>	<u>62.9</u>	<u>58.7</u>	<u>58.7</u>	<u>58.7</u>	<u>58.7</u>	<u>58.7</u>
74.9	68.1	53.2	53.0	54.4	44.7	42.7
+ 16.2	+ 9.4	5.6	4.9	4.3	14.0	16.0
<u>91.1</u>	<u>77.5</u>	<u>58.8</u>	<u>57.9</u>	<u>58.7</u>	<u>58.7</u>	<u>58.7</u>

5869

8-20-34

Miller
Bantet
Walker

Dance plat form in Pepper Grove



BM. Stub	3.37	254.45	255.08	1+00 50. ft.	
Ely Cor	5' N. R.P.	3.73	254.72	253.00	+1.72
Wly Cor	5' N. R.P.	5.50	252.95	252.50	+0.45
Wly Cor	5' S. R.P.	7.34	251.07	252.00	-0.93
Sly Cor	5' S. R.P.	5.16	253.29	252.50	+0.79

Page 2

IMPROVED TABLES AND INFORMATION

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

°	'	sin	tan	sin	tan	sin	tan	sin	tan	sin	tan	sin	tan	sec
0'	0'	10'	10'	20'	20'	30'	30'	40'	40'	50'	50'	60'	60'	0'
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	7314	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	432	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	541	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	660	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	7771	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	880	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3109	969	.3190	987	37
53	986	.3270	8004	.3351	8021	.3432	8039	.3514	8056	.4106	8073	.3680	8090	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	192	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4640	274	.4733	291	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	387	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	481	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	573	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	661	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	8746	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	830	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	910	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	988	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	9063	25
65	9063	1.4445	075	1.609	088	.1775	100	.1943	112	.2113	124	.2286	136	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	206	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	272	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	336	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	397	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	9456	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	511	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	564	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	614	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	660	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	704	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	744	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	781	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	817	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	848	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9877	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	903	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	926	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	946	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	962	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	977	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	987	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	994	2
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	999	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	1.000	0
90	60'	60'	50'	40'	30'	30'	20'	30'	10'	10'	0'	0'	0'	0'
90	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot

TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

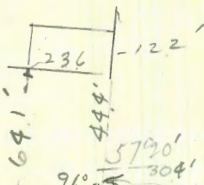
TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20

91° RT,

236 x 12.2

$$\begin{array}{r}
 463.42 \\
 459.64 \\
 \hline
 3.74 \\
 3.73
 \end{array}$$

$$\begin{array}{r}
 508' \quad 483 \\
 \hline
 483 \\
 \hline
 990 \\
 \hline
 495
 \end{array}$$


236

12.2

64.1

44.9

91°

236

19.2

34.5

17.5

1.7.0

2.2

26.7

2.8

25.5

2.0

26.8

1.4

2.0

797

869