

1553

1553



1553

MICROFILMED

DEC 24 1964

ENGINEERING DEPARTMENT  
CITY OF SAN DIEGO  
CALIFORNIA

MADE IN U.S.A.

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4x4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

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**THE FREDERICK POST CO.**  
ENGINEERING and DRAFTING SUPPLIES  
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 BOOK  
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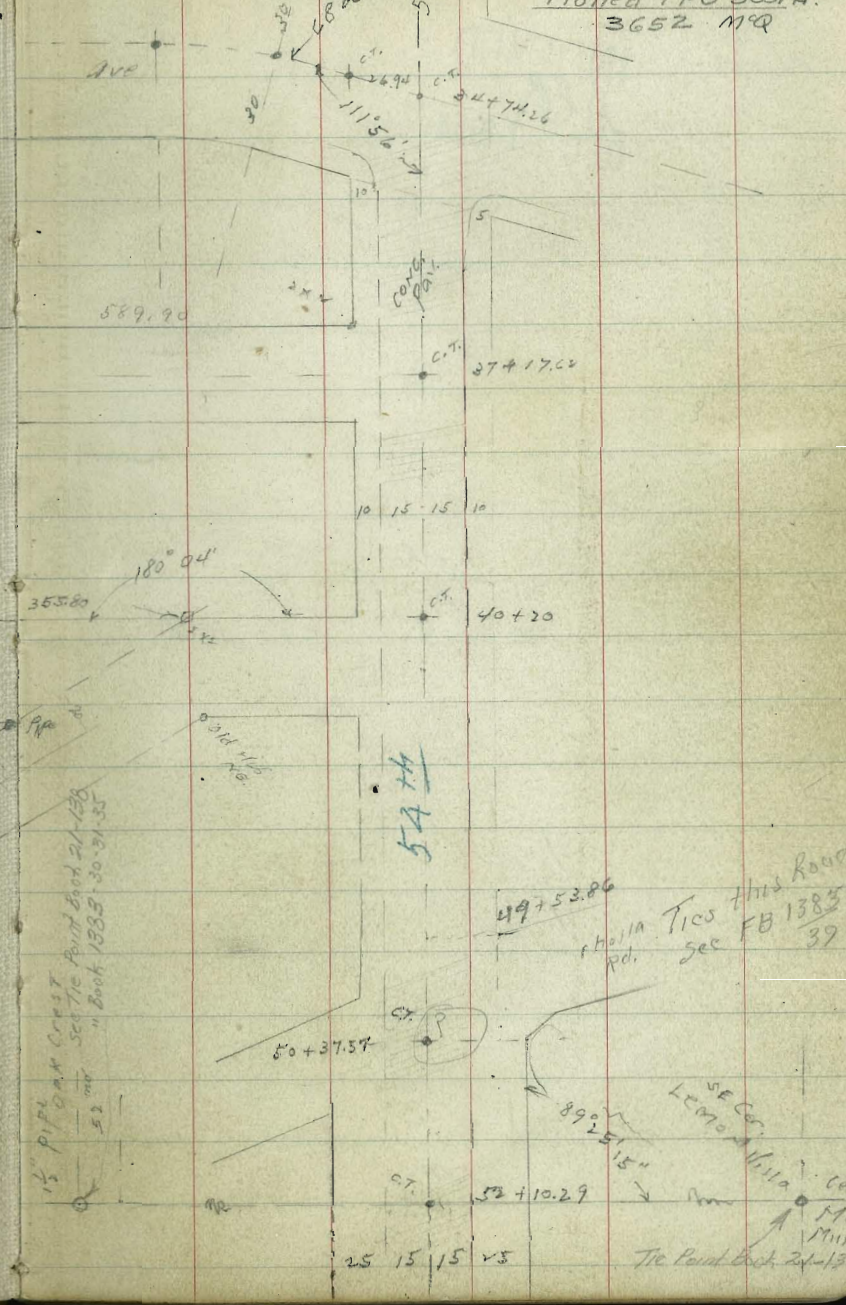
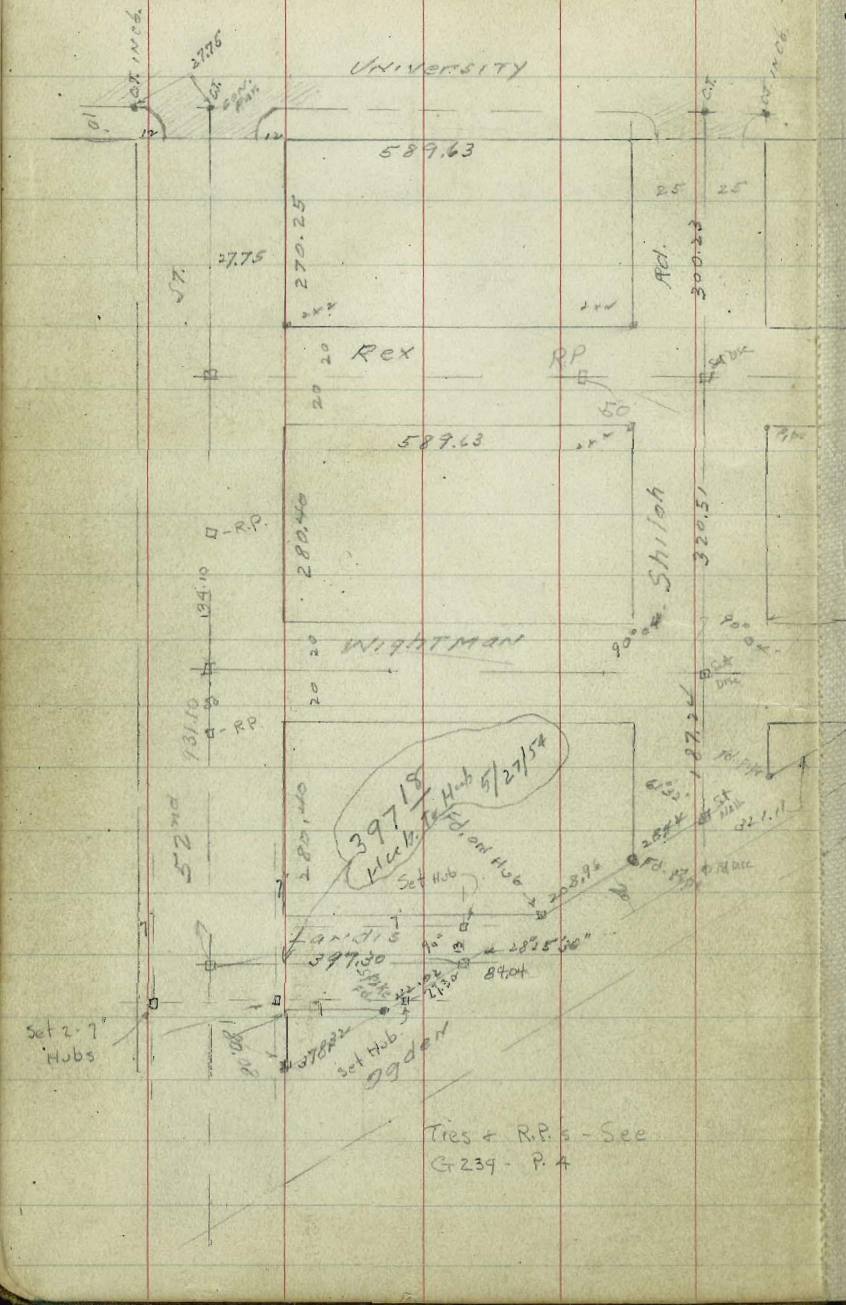
We also carry the following books in stock  
 and are ready to order more at any time.  
 The same quality of work, which can be  
 had at a lower price.

In ordering Fredrick Post's covers, books, etc.  
 the letter "P" is essential.

INDEX

X-SEC. 52nd ST.	1	
Replace Lot. Covers 5307 Ogden	2	

indexed  
PLAN  
Plotted TPS 3651A  
3652 MR



Ties + R.P.s - See  
G-239 - P. 4

15" PIPE  
DRAIN CREEK  
See The Point Book 24-138  
53' in Book 1383 - 30-31-32

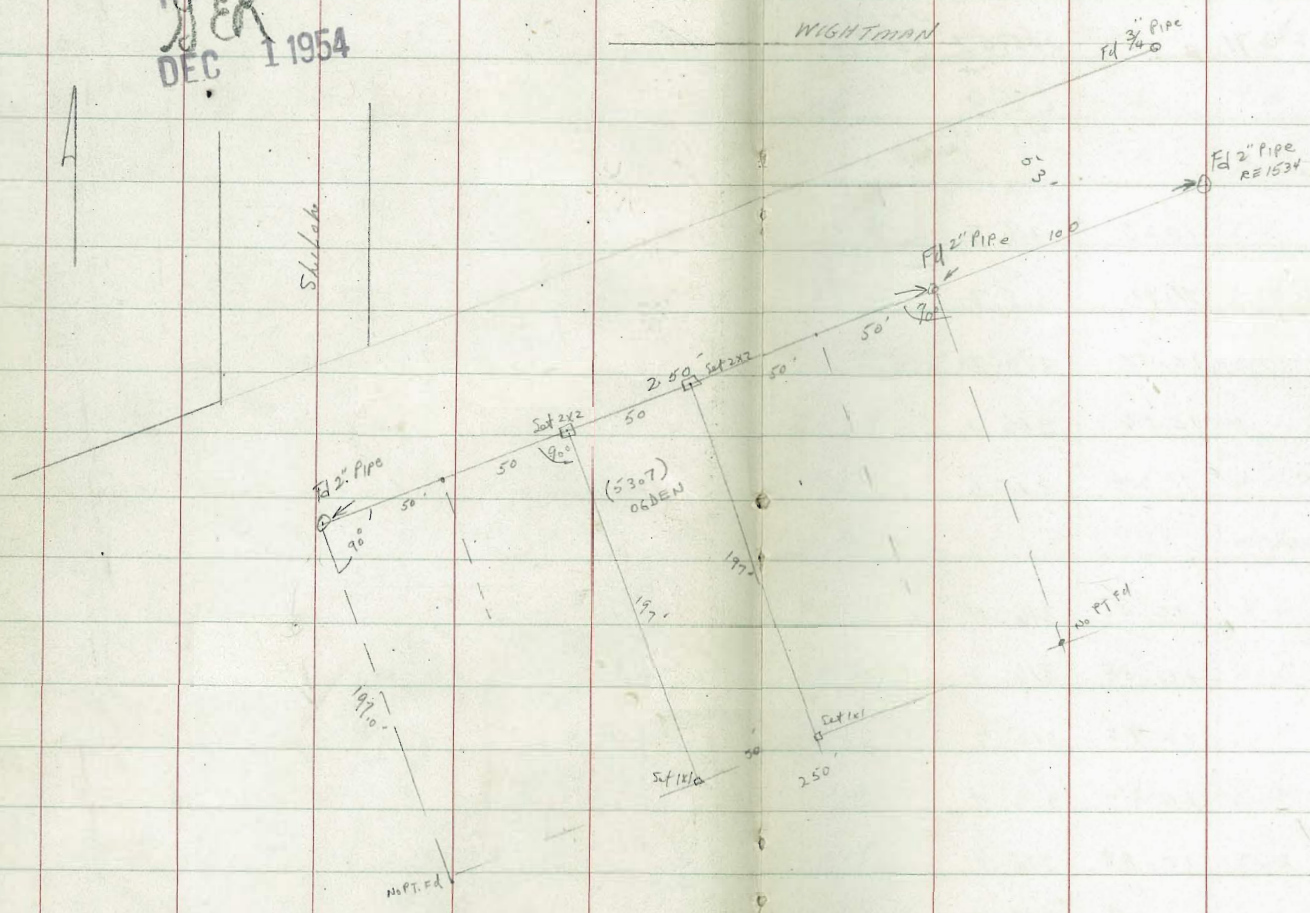
SE COR  
LEMO WILIA  
CONN  
Mon  
Millen  
The Point Book 24-138

Clark  
Shepherd  
Bruner  
8 1/2" W.I.L.  
10-27-54  
W.O. 2000b

REPLACE LOT CORNERS  
5307 OGDEN

INDEXED  
JER  
DEC 1 1954

WIGHTMAN



X sec of 52nd St. 55.5 wide  
UNIV. Sky to  
Ogden St. 12' 0" - 65'

Indexed  
C-S-K

326.71

Blotted 4/29/38 E.A.R.

NWBP 11.14 326.71

315.57 UNIV.  
52nd

cb

9.8

316.9

c

9.9

316.8

E.A.R.  
4/27/38

cb

9.8

316.9

0-10 Sec UNIV.

+6

7.7

319.0

W cb

10.28

316.4

+9

1.1

325.6

gut

11.01

315.7

E

1.2

325.5

C

10.51

316.2

0+25

E cb

10.56

316.1

E

+1.7

328.4

gut

11.24

315.5

+5

+1.7

328.4

0+0=SL UNIV.

+9

4.3

322.4

E

10.3

316.4

cb

7.6

319.1

cb

10.38

316.3

+2

8.5

318.2

gut

10.95

315.7

c

8.5

318.2

C

10.32

316.4

+8

8.2

318.5

gut

10.83

315.9

+13

5.2

321.5

cb

10.19

316.5

cb

+4.1

330.8

W

10.1

316.6

+4

+6.0

332.7

0+05

W

+6.6

333.3

W

6.8

319.9

0+50

+6

8.9

317.9

W

+7.0

334.7

		326.71			327.66			4
+9			+7.0	333.7		1400		
cb			+3.1	329.8	W		3.1	334.6
+7			5.3	321.4	cb		3.2	334.5
c			5.6	321.1	+8		10.8	326.9
+11			5.8	320.9	c		10.7	327.0
+14			4.3	322.4	+10		10.7	327.0
cb			1.8	324.9	cb		4.7	333.0
+3			+3.5	330.2	+4		4.8	333.9
E			+3.6	330.3	E		4.0	333.7
	0+75					1425		
E			+5.7	332.4	E		3.4	334.3
cb			+6.0	332.7	+9		3.7	334.0
+5			2.5	324.2	cb		4.0	333.1
c			2.6	324.1	+5		8.2	329.5
+8			2.6	324.1	c		8.6	329.1
cb			+7.2	333.9	+8		8.8	328.9
W			+7.4	334.1	+11		7.1	329.6
					cb		3.5	334.2
T.P.	11.25	337.66	0.30	326.41	W		3.4	334.3

337.66

1+50

W	3.4	334.1
cb	2.4	334.3
+3	5.9	331.8
+7	7.4	330.3
C	6.9	330.8
+11	7.3	330.4
cb	4.1	333.6
+5	3.2	334.5
E	3.1	334.6

1+75

E	3.1	334.6
+11	3.5	334.2
cb	4.5	333.2
+3	6.2	331.5
C	5.8	331.9
+11	6.3	331.4
+13	5.4	332.3
cb	3.4	334.3
W	3.7	334.0

337.66

2+00

W	4.0	333.7
+10	5.4	334.3
cb	4.2	333.5
+3	5.4	332.3
C	5.4	332.3
+14	5.7	332.0
cb	4.7	333.0
+3	3.5	334.2
E	3.2	334.5

2+51.67 N L King to W

E	4.3	333.4
cb	4.4	333.1
C	4.5	333.2
cb	4.2	333.5
+3	3.6	334.1
W	3.4	334.1

2+70.30 N L Rex to E

W	4.1	333.6
cb	4.6	333.1

5



337.66

337.66

6

+		5.0	332.7	cb	4.2	333.5
c		4.5	333.2	c	4.8	332.9
cb		4.7	333.0	+ 1/2	5.2	332.5
E	old Hub	4.40	338.00 = B.M.	cb	4.7	338.0
	3+01.07	52 King to W		W	4.0	333.1
E		5.1	332.6		4+00	
cb		5.1	332.6	W	5.3	332.4
c		4.8	332.9	cb	5.1	332.6
+ N		4.9	332.8	c	4.8	332.9
cb		4.3	333.4	cb	4.0	333.1
W		4.1	333.6	E	4.5	333.2
	3+10.30 = 52	Tex to E			4+50	
W		4.3	333.4	E	4.4	333.3
cb		4.4	333.3	cb	4.5	333.2
+ 2		5.0	332.7	c	5.1	332.6
c		4.8	332.9	cb	5.8	331.9
cb		4.9	332.8	W	5.8	331.9
E		5.1	332.6		5+01.67	NL Garland 57
	3+50			W	6.4	331.3
E		4.6	333.1	cb	6.1	331.6

337.66

C		5.7	332.0
cb		5.2	332.5
E		4.9	332.8

5+51.67 SL Garland S

F		4.2	333.5
cb		4.6	333.1
C		5.2	332.5
cb		5.6	332.1
W		6.2	331.4

<sup>nail</sup> T.P. Pole	1.20	336.76	2.10	335.56	<sup>SW</sup> WIGHTMAN
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5+90.70 NL WIGHTMAN to E

W		4.0	332.8
cb		3.4	333.2
C		3.0	333.8
cb		2.7	334.1
E		2.4	334.4

6+30.70 S.L. WIGHTMAN to E

E		1.5	335.3
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336.74

7

cb		2.0	334.4
C		2.1	334.7
cb		2.7	334.1
W		2.6	334.2

6+60

W		1.4	335.4
+3		1.9	334.9
cb		2.1	334.7
C		1.5	335.3
cb		1.7	335.1
E		1.2	335.6
+5		+3.0	339.8

7+01.47 NL Towle to W

-7		+5.6	342.4
E		1.3	335.5
cb		1.8	335.0
C		1.6	335.2
cb		2.1	334.7
+8		1.8	335.0
W		0.0	336.8

C		7751.67	S. L. Towle To W.		E		7.3	329.5
cb	W		5.1	333.7		8765		
E	cb		5.3	333.5	E		10.3	326.5
	c		5.0	333.8	cb		10.0	326.8
E	cb		5.3	333.5	+8		9.7	327.1
cb	E		5.2	333.6	C		9.6	327.2
c	+5		2.4	334.4	16		9.8	327.0
cb	+8		+2.0	338.8	+9		9.8	327.0
W		8400			W		10.7	326.1
	E		5.2	331.6	+5		11.5	325.3
TP	cb		5.0	331.8		8790		
	c		5.1	331.7	-10		14.2	322.6
	cb		5.7	331.1	W		12.1	324.7
W	+2		5.2	331.6	+8		10.7	326.1
cb	W		5.3	331.5	cb		10.9	325.9
c		8430			c		10.7	326.1
cb	W		7.6	329.2	+5		10.9	325.9
E	cb		7.5	329.3	+11		12.5	324.3
	c		7.2	329.6	cb		13.4	323.4
E	cb		7.1	329.7	E		14.6	322.2
					+10		13.3	324.5

C 9+11.10 NL Landis to E

9+51.10 SL Landis

cb	-10		14.9	321.9
E	E		15.2	321.5
	+9		14.8	322.0
E	cb		14.2	322.6
cb	+12		11.3	325.5
c	c		11.2	325.6
cb	cb		11.4	325.2
W	W		11.9	324.9
	+15		17.6	319.2

-10		8.3	328.5
E		9.2	327.6
cb		10.0	326.8
c		10.8	326.0
cb		11.2	325.4
W		11.6	325.2
+12		14.3	322.5
+15		16.2	320.6

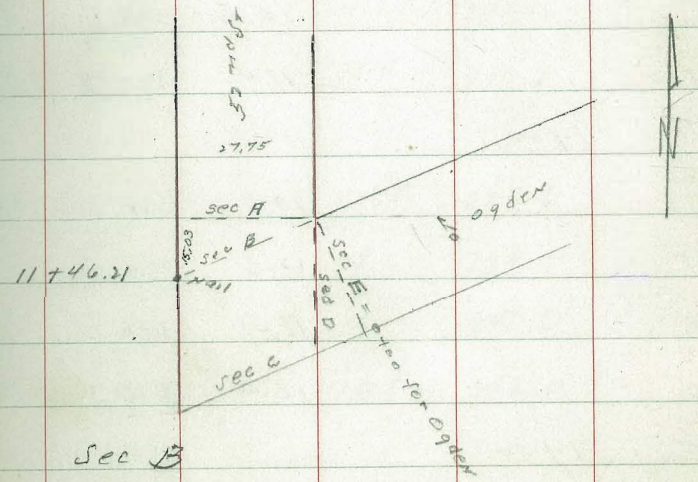
TP 9+31.10 E Landis to E

9+61.65 P.C. PT. on Lennox St.  
To West

	-20	BOTTOM	20.9	315.9
	W		13.4	323.4
W	cb		11.6	325.2
cb	C	OH HUB	11.41	325.35 517
c	+3		11.3	325.5
cb	+9		13.0	323.8
E	cb		13.2	323.6
	E		12.2	324.6
E	+10		11.2	325.5

-15		12.6	324.2
W		11.8	325.0
cb		11.0	325.8
c		10.4	326.4
+7		9.7	327.1
+11		8.4	328.4
cb		8.1	328.7
E		7.6	329.2
+10		6.5	330.3

			336.76		
				25.5	
C		9+90	= 52 <sup>nd</sup> ST = 37.75' wide		346.71
cb	E		1.0	335.8	T.P. 814 352.06 0.80 345.94
E	+11		2.3	334.5	
	+21		4.7	332.1	11+00
E	W		8.2	328.6	W 6.2 345.9
cb					+10 5.6 346.5
c	T.P.	11.57	346.72	1.55	335.21 E 4.9 347.2
cb					11+31.18 = Sec. A
W		10+15			E ON + VL RW 5.09 347.0
E			7.8	338.9	W 4.5 347.6
T.P.	+12		8.6	338.1	
	W		12.3	334.4	
		10+50			
W	E		5.2	341.5	
cb	+13		6.1	340.6	
c	W		8.2	338.5	
cb		10+70			
E	E		4.1	342.6	Sec B
	+13		4.8	341.9	W 5.0 347.1
E	W		6.3	340.4	



46.21  
31.18  
15.03

		352.06	
C	Sec C		
C	W	7.8	344.3
E	E	6.2	345.9
	Sec E - beg. Opden = 0+00		
E	S	7.0	344.8
C	C	6.0	342.1
C	N Hub	5.09	347.0
	0+50		
		7.2	344.9
		8.7	343.4
		10.6	341.5
		11.4	340.7
	1+00		
		13.6	338.5
		12.6	339.5
		11.0	341.1
		10.4	341.7
	1+50		
		10.6	341.5
		10.6	341.5

	Included c.s.k.	Dated 4/28/39 ST/52	352.06	Opden	11
	✓			12.1	340.0
	+10			12.6	339.5
		2+00			
	-10			11.7	340.4
	S			10.7	341.4
	C			9.5	342.6
	N			9.8	342.3
		2+50			
	N			10.0	342.1
	C			10.2	341.9
	✓			11.1	341.0
	+10			11.9	340.2
		3+00			
	-10			14.5	337.6
	S			13.1	339.0
	C			11.1	341.0
	N			10.1	342.0
		3+50			
	N			8.0	344.1
	C			9.0	342.8

S			13.7	338.4	
+10			14.7	337.4	
	W + 78.00 = SL Landis				
-10			15.3	336.8	
S			14.2	337.9	
C			10.1	342.0	
N	on spike		7.72	344.34	B.M.
T.P. spike	10.00	357.54	7.72	344.34	
	E Landis to W				
N			13.5	343.8	
C			17.3	340.0	
S			21.2	336.1	
+20			26.8	330.5	
	N.L. Landis = 00				
-10			18.2	339.1	
S			17.0	340.3	
C			13.7	343.6	
N			11.0	346.3	

					0+50		
				N		6.5	350.8
				O		7.2	350.1
				S		8.4	348.9
					1+0		
				S		4.3	353.0
				C		4.1	353.2
				N		4.3	353.0
					1+50		
				N		4.8	353.5
				C		3.8	353.5
				S		3.7	353.0
					2+08.96 = W.L. Shiloh		
				S		3.4	353.9
				C		3.4	353.9
				N		3.4	353.9
					E Shiloh		
				N	Set B.M. 2x2	2.35	354.99 RW Hub
				C		2.8	354.5
				S		3.1	354.2

357.54

EC 5/16" = 00

S		2.6	354.7
C		2.1	355.2
N		2.8	354.5

T.P. <sup>3/4"</sup> pipe 4.95 361.44 2.85 354.49

0+50

N		6.7	354.7
C		6.4	355.0
S		6.4	355.0

0+75

S		6.7	354.7
C		5.3	356.1
N		5.1	356.3

1+0

N		6.4	355.0
C		6.7	354.7
S		6.6	354.8

361.44

13

1+25

S		6.1	355.3
C		5.9	355.5
N		5.4	356.0

1+50

N		6.2	355.2
C		6.6	354.8
S		6.1	355.3

2+0

S		5.8	355.6
C		5.8	355.6
N		5.4	356.0

2+30

N		4.7	356.7
C		4.9	356.5
S		5.0	356.4

2+50

S		5.8	355.6
C		5.6	355.8
N		5.6	355.8



361.44

99den St.

Invented  
C.S.K.

X sec Landis St No

14

4+0

BM

Plotted  
4/25/38  
C.S.K.

12.34

337.71

325.35

P9

N 6.2 355.2

E.L. 52<sup>nd</sup> = 00

C 4.1 355.3

0+50

S 5.6 355.8

S

6.8 330.9

3+21.11 SW WIGHTMAN to W

C

9.6 328.1

S 6.4 355.0

+7

10.9 326.8

C 4.6 354.8

+17

14.2 323.5

N 5.4 356.0

N

12.9 324.8

E WIGHTMAN to W

+5

11.0 326.7

N 6.4 355.2

+15

10.0 327.7

C 6.5 354.9

1+0

S 6.5 354.9

-20

7.1 330.6

-10

10.3 327.4

T.P. 3/4" pipe SW Cor  
99den + WIGHTMAN 5.8 356.21 BM

N

7.6 330.1

C

6.5 331.2

+10

6.4 331.3

S

4.7 333.0

1+50

S

0.6 337.1

+7

2.5 335.2

337.71

350.69

15

c			2.1	335.6
N			3.0	334.7
+10			3.9	334.4
T.P.	13.02	350.69	0.04	337.47

2+0

N			10.5	340.2
C			10.4	340.3
S			10.8	339.9

2+50

S			7.6	343.1
C			7.1	343.6
N			6.8	343.9

2+0

N			3.2	347.5
C			4.1	346.6
S			5.3	345.4

2+32.60

S	spike piv		6.40	344.29	344.34
---	-----------	--	------	--------	--------

C			2.6	346.1
N			3.2	347.5
			2+49.55	
N			3.5	347.2
C			6.9	343.8

X 500 WIGHTMAN do

Platted 223  
4/30/38Indexed  
C.S.K.I.

348.21

16

B.P.

12.65 348.21

335.56 P7

FL 52 = 00

0 + 05

J

9.9

338.3

1 + 50

C

12.4

335.8

S

4.8

349.8

N

12.5

335.7

C

8.1

346.5

0 + 40

N

10.5

344.1

N

9.7

338.5

+ 5

11.0

343.6

C

9.0

339.2

1 + 75

J

6.6

341.6

- 10

10.0

344.6

0 + 75

N

9.0

345.6

J

3.1

345.1

C

6.9

347.7

C

5.6

342.6

J

4.9

349.7

N

7.5

340.5

2 + 0

1 + 00

S

5.1

349.5

N

6.0

342.2

C

6.6

348.0

C

4.0

344.2

N

7.9

346.7

+ 4

3.9

344.3

+ 10

8.8

345.8

+ 8

2.5

345.7

2+50

3+50

-10	9.2	345.4
N	8.2	346.4
+5	7.4	347.2
0	7.0	347.6
S	5.0	349.6

S	5.8	348.8
C	10.1	344.5
+13	11.7	342.9
N	13.4	341.2
+10	15.0	339.6

3+0

+15

S	5.0	349.6
C	6.6	348.0
+15	7.0	347.6
N	8.8	345.8
+10	10.0	344.6

3+75

+15	11.2	343.4
N	12.0	342.6
C	11.1	343.5
+2	9.7	344.9

3+25

S

-10	12.4	342.2
N	10.3	344.3
+7	8.4	346.2
C	7.6	347.0
+2	5.9	348.7
S	5.0	349.6

4+0

S	5.5	349.1
+18	8.6	346.0
C	9.9	344.7
+15	10.8	343.8
N	9.8	344.8
+10	8.1	346.5

		354.60			354.60		Wiphtan 18
	4435				5470		
N		7.8	346.8		N	3.5	351.1
C		7.4	347.2		C	3.0	351.6
+4		6.1	348.5		S	2.8	351.8
S		4.7	349.9			5489.00	W L Shiloah
	4465				S	2.4	352.2
S		2.9	351.7		+10	1.0	353.3
+10		4.4	350.2		C	1.2	353.4
C		5.4	349.2		N	3.2	351.4
N		5.5	349.1			E Shiloah	
	5400				N	2.6	352.0
N		3.6	351.0		C	on 2 x 2 Hub	1.80 352.8
C		4.0	350.6		S	1.7	352.9
S		3.4	351.2				
	5450				T.P.	849	361.29 1.80 352.80
S		2.6	352.0				2 x 2 E HUB
+10		1.4	353.2			E.L. Shiloah = 0.0	
C		2.3	352.3		S	6.8	354.5
N		3.5	351.1		C	8.1	353.2
					N	8.8	352.5

0+50  
 N 7.7 353.6  
 C 7.2 354.1  
 S 6.8 354.5

1+0  
 S 6.7 354.6  
 C 7.2 354.1  
 N 7.2 354.1

1+25  
 N 7.0 354.3  
 C 6.8 354.5  
 S 6.4 354.9

1+50  
 S 6.1 355.2  
 C 5.3 356.0  
 N 6.3 355.0

1+75  
 N 6.4 354.9  
 C 6.4 354.9  
 S 6.1 355.2

2+0  
 S 5.8 355.5  
 C 6.0 355.3  
 N 6.5 354.8

2+25  
 N 6.3 355.0  
 C 5.6 355.7  
 S 4.9 356.4

2+50  
 S 6.1 355.2  
 C 6.1 355.2  
 N 6.3 355.0

2+84 approx opp. S.W. cor <sup>of den</sup> <sup>W. 957000</sup>  
 N 6.4 354.9  
 C 5.0 356.3  
 S 5.3 356.0  
 S on pipe 4.99 356.30 356.31  
 P. 4

3+0  
 S 6.0 355.3  
 C 5.8 355.5  
 N 6.0 355.3

0°04' RT

3 + 55.80 Δ Pt. N. L. WIGHTMAN

N	on 242	6.04	355.25
E		5.7	355.6
S		5.9	355.4

<sup>242</sup>  
 T.P. Hub 2.86 358.11 6.04 355.25 Δ Pt.

346 approx.

S	old hub	2.5	355.6
E		2.0	356.1
N		2.6	355.5

440

N		5.2	354.9
E		3.2	354.9
S		2.8	355.3

4430

S		2.2	355.9
<sup>+10</sup> E		2.4	355.7
		3.7	354.4
N		3.7	354.4

4465

N		5.4	352.7
E		5.2	352.9
S		5.3	352.8

540

S		10.0	548.1
E		10.8	347.3
N		11.6	346.5

T.P. 1.22 346.89 12.42 345.67

5425

N		6.1	340.8
E		4.5	342.4
S		3.1	343.8

5450

S		10.7	336.2
E		11.5	335.4
N		13.2	333.7

346.89

5+65

N		16.8	330.1
C		16.5	330.4
S		16.0	330.9

5+83

S		18.6	328.3
C		19.0	327.9
N		19.4	327.7

T.P.	0.44	334.40	12.93	333.96
------	------	--------	-------	--------

T.P.	2.83	325.30	11.93	322.47
------	------	--------	-------	--------

5+89.70 = N.L. 547th St.

N		1.1	324.2
C		1.3	324.0
S		3.0	322.3

5+96

S		7.0	318.3
C		5.5	319.8
N		4.5	320.8

325.30

WIGHTMAN 21

5+92

w edge 30' CORO. PAR.

N		5.53	319.77
C		6.46	318.84
S		7.75	317.55

T.P.

	1.12	324.18	nail in Tel. Pole
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	X 500 Rex St. 40	Indexed			337.04		22
			c.s.K.				
			Platted				
			4/28/38				
			ETB				
			52nd		1750		
N.E. Cor. old hub	3.98	337.04	333.06	Rex St. P.6	-5	9.0	328.0
	F.L. 52nd = 00				N	9.0	328.0
	0+40				0	8.1	328.9
N		4.3	332.7		+4	7.6	329.4
C		4.8	332.2		+6	6.8	330.2
S		4.6	332.4		5	5.9	331.1
	0+75				+5	6.0	331.0
S		4.8	332.2				
					1+75		
C		4.6	332.4		-5	8.6	328.4
N		3.5	333.5		5	9.1	327.9
	1+0				+15	10.6	326.4
N		4.3	332.7		+17	11.7	325.3
C		4.5	332.5		0	12.2	324.8
S		4.6	332.4		N	12.9	324.1
	1+25				+10	14.1	322.9
S		4.7	332.3				
C		5.2	331.8		T.P. 429	328.75	12.58
N		4.9	332.1				324.46

> +0			
-15		11.4	317.4
N		9.8	319.0
C		8.1	320.7
+3		7.9	320.9
+5		7.1	321.7
✓		5.5	323.3
+10		4.2	324.6
> +25			
-15		7.8	321.0
✓		9.4	319.4
C		10.0	318.8
+7		10.3	318.5
+15		12.9	315.9
N	bot. wash	14.1	314.7
+10	" "	14.2	314.6
+20		12.8	315.0
> +42			
-20		10.3	318.5
N		10.1	318.7

+10		10.8	318.0
+13		9.9	318.9
0		10.2	318.6
+5		10.5	318.3
+7		11.6	317.2
✓	bot. wash	11.0	317.5
+20	" "	9.8	319.0
> +60			
-10		9.2	319.6
✓		9.4	319.4
C		9.5	319.3
N		8.4	320.4
+20		7.7	321.1
> +80			
-10		1.3	327.5
N		1.9	326.9
C		4.3	324.5
✓		5.3	323.5
+20		6.4	322.4
T.P.	11.86	340.93	0.48
			328.27

340.13

340.13

Rex

24

	✓ +35					5+0			
-10		10.2	329.9		N		4.1	336.0	
N		11.0	329.1		C		2.9	337.2	
C		12.0	328.1		+3		2.3	337.8	
✓		13.6	326.5		S		0.2	339.9	
+10		13.6	326.5						
	✓ 475				T.P.	1264	349.88	2.89	337.24
✓		10.2	329.9						
C		9.2	330.9			5+40			
+3		8.5	331.6		S		10.1	339.8	
+10		8.7	331.4		C		12.3	337.6	
N		7.7	332.4		N		13.2	336.7	
	4+0					5+89.46			W.L. Skiloh
N		7.3	332.8		N		11.8	338.1	
C		7.7	332.4		C		11.2	338.7	
S		7.6	332.5		+3		10.0	339.9	SW con
	4+50				S	Hub	7.91	341.97	Rex Skiloh
✓		3.0	337.1			E Skiloh			
C		4.6	335.5		S		7.3	342.6	
N		5.1	335.0		C		9.1	340.8	

24		349.88				356.73		25	
N			10.0	339.9		+2		9.4	347.3
	EL Station - 00					+4		8.2	348.5
N			8.2	341.7		5		7.2	349.5
C			7.1	342.8			1 + 0		
+3			6.0	343.9		5		6.4	350.3
5			3.9	346.0		+14		7.5	349.2
	0 + 35					+14		8.3	348.4
5			2.0	347.9		0		8.5	348.2
+16			3.6	346.3		+12		8.5	348.2
+17			4.6	345.3		N		10.5	346.2
0			4.7	345.2			1 + 35		
+12			5.4	344.5		N		8.2	348.5
N			6.3	343.6		+8		7.2	349.5
						0		6.7	350.0
T.P.	9.41	356.73	2.56	347.32		+4		6.7	350.0
						+6		6.0	350.7
	0 + 70					5		5.2	351.5
N			12.1	344.6			1 + 70		
+8			10.2	346.5		5		4.4	352.3
C			9.4	347.3		0		5.6	351.1

C + 12		5.8	350.9
N		6.6	350.1
	2 + 0		
N		5.6	351.1
+ 8		5.0	351.7
C		4.8	351.9
+ 5		4.6	352.1
+ 7		4.9	352.8
S		4.0	352.7
	2 + 50		
S		3.0	353.7
C		4.3	352.4
N		4.7	352.0
	3 + 0		
N		4.2	352.5
C		3.4	353.3
S		2.4	354.3
	3 + 14		
S	3' cent. walk	2.55	354.18

		2 + 50	
S			3.2 353.5
C			4.5 352.2
N			4.7 352.0
		3 + 75	
N			5.3 351.4
C			5.4 351.3
S			4.7 352.0
		4 + 0	
S			6.0 350.7
C			7.0 349.7
N			8.0 348.7
		4 + 40	
N			13.2 343.5
C			11.0 345.7
S			10.2 346.5
		T.P.	
		0.06	343.95
		12.84	348.89

	4+70			
S		1.5	342.5	
+10		0.8	340.2	
0		5.0	339.0	
N		6.6	337.4	
	5+0			
N		10.0	334.0	
c		9.5	334.5	
+17		9.2	334.8	
S		8.1	335.9	
	5+30			
S		15.0	329.0	
C.		16.0	328.0	
N		16.3	327.7	
T.P.	0.9	331.24	12.90	331.05
	5+60			
N		10.1	321.1	
c		9.5	321.7	

S		8.7	322.5	
	5+89 <sup>20</sup>	W = 5.4		
S		12.8	317.4	
+7		15.5	315.7	
0		14.0	317.2	
N		14.4	316.8	
	N.M. Rex			
	T.P. Nail Pole 5.4h	12.74	318.54	

X 500 Station Univ. to Ogden		50' wide 10 10' obs 7 1/4 1/4	Indexed O.S.K.	Plotted 5/11/38 D.F.B.	327.26		28
SW Rev Shiloh	1.82	343.79	341.97	pr+	cb	6.2	321.1
T.P.	1.11	331.90	13.00	330.79	+4	7.8	319.5
T.P.	3.30	327.26	7.94	323.96	c	8.5	318.8
					cb	9.2	318.1
	0-10-5	cb UNIV.			+v	8.0	319.3
E cb			8.21	319.05	w	8.4	318.9
E gut			8.69	318.57		0+80	
E Pav	1st C.T.		9.44	317.82	w	6.6	320.7
w cb			9.71	317.55	cb	6.0	321.3
w gut			10.41	316.85	+v	7.5	319.8
	00-5	UNIV.			+4	6.3	321.0
w			9.2	318.1	c	5.9	321.4
w cb			9.58	317.53	+13	5.9	321.4
gut			10.13	317.13	cb	4.8	323.0
C Pav.			9.03	318.23	E	3.4	323.9
gut			9.07	318.19		0+70	
E cb			8.22	318.84	E	1.9	325.4
E			8.2	319.1	+v	2.8	324.5
	0+05				cb	3.6	323.7
F			4.4	322.9	c	3.6	323.7

		327.26		
C 410		1.8	322.5	
cb		1.0	323.3	
W		3.8	323.5	
	140			
W		2.4	324.9	
cb		2.4	324.9	
C		2.3	325.0	
cb		2.1	325.2	
E		1.4	325.9	
T.P.	1266	339.86	0.06	327.20
	1435			
E		12.4	327.5	
cb		12.4	327.5	
C		12.5	327.4	
FB		12.4	327.5	
cb		11.2	328.1	
W		12.0	327.9	

		339.86		
	1470			
W		7.8	332.1	
cb		7.8	332.1	
	147	8.4	331.5	
C		8.5	331.4	
cb		8.5	331.4	
E		7.8	332.1	
	240			
E		4.8	335.1	
cb		5.0	334.9	
C		4.8	335.1	
	145	5.3	334.6	
cb		4.0	335.9	
W		4.3	335.6	
	2435			
W		2.8	337.1	
cb		1.9	338.0	
11		2.1	337.8	
C		1.7	338.2	
cb		1.7	338.2	



E		1.6	338.3
T.P.	12.08	351.69	0.55 339.31
	2 + 70.28 = N.L.	12X	
	0 + 0 = S.L.	"	
	0 + 30		
W		7.0	344.5
cb		6.2	345.3
c		6.0	345.7
±N		5.9	345.8
cb		5.0	346.7
E		4.5	347.2
	0 + 65		
E		2.6	349.1
cb		2.7	349.0
±N		3.5	348.2
c		4.5	348.2
cb		3.9	347.8
W		4.2	347.5

		1 + 0	
W		2.0	349.7
cb		2.1	349.6
c		2.0	349.7
cb		1.5	350.2
E		1.0	350.7
T.P.	7.58	358.24	1.01 350.68
		1 + 50	
E		6.4	351.7
cb		6.6	351.7
c		6.5	351.8
cb		6.7	351.6
W		7.1	351.2
		2 + 0	
W		6.9	351.4
cb		6.8	351.5
c		6.6	351.7
cb		6.4	351.9
E		5.3	353.0

	2+40			
E		6.2	352.1	
cb		5.9	352.4	
c		6.1	352.2	
+9		6.5	351.8	
cb		5.8	352.5	
W		5.9	353.0	
	2+80.51	NL	WIGHTMAN	
	00 =	SL	"	
	0+25			
W		5.2	353.1	
cb		5.2	353.1	
0		5.4	352.9	
cb		5.0	353.3	
E		4.7	353.6	
	0+60			
E		4.0	354.3	
cb		4.1	354.2	
c		5.9	354.4	
cb		4.8	354.5	

		W		3.8	354.7	
			1+0			
		W		4.4	353.9	
		cb		4.2	354.1	
		c		4.0	354.3	
		cb		2.9	355.4	
		F		2.9	355.4	
			1+30			
		E		3.7	354.6	
		cb		4.2	354.1	
		c		4.4	353.9	
		cb		4.8	353.5	
		W		5.0	353.3	
			1+67.24	NL	Ogden & E Shiloh	
			ch. to BMT	5.51	352.75	352.80
						918

KING CT.  
Rex

Level  
50' wide

Indexed  
C.S.K.

32

BM. above 542 338.48

333.06 P 0

338.48

2 + 45 = END

00 = WL 53<sup>rd</sup> ST.

N 10.6 327.9

0 + 50

0 8.4 330.1

N 4.0 334.5

S 7.3 331.2

0 4.5 334.0

2 + 75

S 5.1 333.4

S 10.3 328.2

1 + 0

0 11.6 326.9

S 5.5 333.0

N 13.6 324.9

0 5.3 333.2

N 5.0 333.5

1 + 50

N 6.3 332.2

0 5.5 333.0

S 5.9 332.6

2 + 0

N 7.7 330.8

0 6.4 332.1

S 5.7 332.8

Garland St levels  
50' wide  
Wrightman

	345	336.51	1	333.06
	00 = W.L. 5 <sup>th</sup> md			
	0 + 50			
S			7.2	329.3
C			8.3	328.2
N			7.3	329.2
	1 + 0			
N			9.1	327.4
+10			9.9	326.6
+13			11.7	324.8
C			11.4	325.1
+15			12.3	324.2
S			10.5	326.0
	1 + 50			
S			12.1	323.4
+8			14.5	322.0
+11			16.5	320.0
+13			15.3	321.2
C			15.0	321.5
+14			15.7	320.8
+16			14.0	322.5

Included  
e.s. 1/4 336.51

N			12.9	323.6
T.P.	029	323.91	12.89	323.64
	2 + 0			
S			3.2	320.7
+8			7.7	316.2
+10			7.7	316.2
C			5.9	318.0
+12			5.5	318.4
+15			4.7	319.2
N			2.7	321.2

2 + 45 = C N.L. Sec. on split

N			2.5	321.4
+11			4.4	319.5
+21			8.9	315.0
C			9.0	314.9
S			10.6	313.3
+5			7.1	316.8

Towle CT 50' wide

skated  
5/21/34  
EBS

3.14 338.70 335.56 P7

WL 52=00

0403

S 4.2 334.5

+11 4.6 334.1

C 4.4 334.5

+14 4.0 334.7

+16 2.1 336.6

N 1.9 336.8

0450

N 4.4 334.3

C 5.6 333.1

S 6.0 332.7

140

S 8.2 330.5

C 6.5 332.2

N 5.5 333.2

1750

S 9.7 329.0

C 8.8 329.9

indexed  
C.S.K.

338.70

34

N 8.3 330.4

240

N 12.2 326.5

C 11.7 327.0

S 12.7 326.0

2445 END

S 14.6 324.1

C 13.5 325.2

N 13.8 324.9

2475

N 14.0 324.7

C 14.2 324.5

S under shack 14.9 323.8

W.L. Sta.	X sec	Lennox St. Landis	50' wide 10' cbs	81 P 9
	11.61	336.96	325.35	
	B.C. on 54500			
W		11.7	325.3	
cb		11.4	325.6	
C		10.8	326.2	
	O + 30.23			
W		9.4	327.6	
cb		9.4	327.6	
C		8.3	328.7	
	O + 60.46			
W		7.4	329.6	
cb		7.1	329.9	
C		5.7	331.3	
+7		4.9	332.1	
cb		0.6	336.4	
E		+1.0	338.0	
	O + 87.61			
W		6.5	330.5	
cb		5.8	331.2	
C		5.0	332.0	

Included Platted  
C.S.R. B.R.B. 336.96

35

C + 7		4.2	332.8
C + 13		0.9	336.1
cb		0.0	337.0
E		+ 2.4	339.4
	+ 14.76		
W		5.7	331.3
cb		4.9	332.1
C		4.5	332.5
+8		4.0	333.0
cb		0.0	337.0
E		+ 2.1	339.1
	+ 41.91		
W or N		6.4	330.6
cb		6.0	331.0
C		5.8	331.2
+8		6.1	330.9
cb		1.8	335.2
E or S		0.0	337.0

336.96

36

1449.06

N	7.8	329.2
cb	7.5	329.5
c	7.8	329.2
+7	8.1	328.9
+12	4.0	333.0
cb	3.7	333.3
5	3.0	334.0

1496.71 EC

N	10.2	326.8
cb	9.9	327.1
c	9.7	327.3
+10	10.3	326.7
cb	8.4	328.6
5	7.7	329.3

X SEC 54TH 50' Wide  
 UNIT to Cholla Road.

Indicated Plastic 319.23  
 c.s.r. 4/29/38  
 8783

37

					+5	10.3	308.9
N.W. BR	921	319.23	310.02	UNIT 54TH	+8	12.2	307.0
	34+95.82	S 927 UNIT			E	12.2	307.0
W cb		9.87	309.36		+5	12.5	306.7
" gut		10.40	308.83		36+0		
C		11.05	308.18		-5	11.8	307.4
E gut		11.72	307.51		E	11.0	308.2
					+✓	10.6	308.6
	35+0660	S 4 UNIT Diag			+5	9.0	310.2
E +5	cb	11.21	308.02		cb	9.70	309.5
E +5	gut	11.82	307.41		C	9.62	309.61
C		10.93	308.30		cb	9.86	309.37
W gut		10.81	308.42		+✓	9.7	309.5
" cb		10.31	308.92		W	6.4	312.8
	+52	@ east edge par.			+50		
W		6.9	312.3		W	4.5	314.7
+4		9.9	309.3		+2	5.7	313.5
cb par		10.57	308.66		cb	8.36	310.87
C		10.65	308.58		C	8.12	311.11
cb		10.23	308.40		cb	8.35	310.88



319.23

319.23

38

+5		8.0	311.2
E		11.3	307.9
+5		13.7	305.5
	36 + 97.0 <sup>v</sup> N + Rex		
-5		13.5	305.7
E		11.6	307.6
+5		6.8	312.4
cb		6.98	312.25
c		6.72	312.51
cb		7.0 <sup>v</sup>	312.21
W		2.7	316.5
	37 + 17.6 <sup>v</sup> E Rex		
W		2.0	317.2
+7		6.1	313.1
cb		6.44	312.79
c	C.T.	6.09	312.14
cb		6.35	312.88
+5		6.3	311.9
E		9.9	309.3
+6		13.5	305.7
+10		13.9	305.3

+5			
-10		12.8	306.4
-6		11.8	307.4
E	FL. 12" Corr 1.P.	9.80	309.43
W	cb Pax	5.96	313.26
+3.5	Hd Wgt	5.95	313.27
+3.5	FL.	8.17	311.06
	+ 37.0 <sup>v</sup> J + Rex		
W		2.9	316.3
+7		6.0	313.2
cb		5.81	313.42
c		5.50	313.73
cb		5.80	313.43
+5		5.7	313.5
E		8.8	310.4
+6		11.8	307.4
+10		12.8	306.4
	38		
-10		12.5	306.7
-5		11.1	308.1

319.23

F			8.3	310.9
+6			3.9	315.3
cb			4.91	315.32
c			2.52	315.71
cb			2.89	315.34
W			2.8	315.4
W			0.0	319.2
	+50			
W			3.0	316.2
+7			1.9	317.3
cb			2.37	316.86
c			2.03	317.20
cb			2.37	316.86
+5			2.3	316.9
E			5.7	313.5
+7			10.3	308.9
+15			11.7	308.5
T.P.	60v	324.51	0.74	318.49

324.51

39

				39400			
				-10		12.0	312.5
				E		8.9	315.6
				+5		5.9	318.6
				cb		4.10	318.41
				c		6.00	318.51
				cb		6.24	318.27
				+5		5.5	319.0
				W		2.4	322.1
					+50		
				W		0.5	324.0
				+6		4.1	320.4
				cb		4.70	319.81
				c		4.44	320.07
				cb		4.57	319.94
				+6		4.1	320.4
				E		6.3	318.2
				+10		8.5	316.0
					+75		
				-5		7.2	317.3
				E		5.7	318.8
				+4		2.7	320.8

324.51

cb	4.09	320.42
C	4.90	320.61
cb	4.06	320.45
+4	4.3	321.2
W	0.0	324.5

check to nail pole <sup>5274</sup> Wightman 0.07 324.12 324.18

40+00

W	0.7	323.8
+6	4.7	320.8
cb	4.21	320.30
C	4.04	320.47
cb	4.25	320.26
+6	4.7	320.8
E	5.3	319.2
+5	7.2	317.3

40+20 NL Wightman

E	4.8	319.7
+2	4.2	320.3
+5	4.9	319.6

324.51

40

cb	4.76	319.75
C	4.54	319.97
cb	4.77	319.74
+4	4.1	320.4
W	0.9	323.6

40+40

W	2.4	321.9
+5	4.8	319.7
cb	5.70	318.81
C	5.54	318.97
cb	5.72	318.79
+5	5.8	318.7
+7	4.3	320.2
E	5.0	319.5

40+60

J.L. Wightman

E	5.4	318.9
+2	6.0	318.5
+5	7.1	317.4
cb	6.98	317.53
C	6.82	317.69

324.51

cb		7.00	317.51
+4		7.0	317.5
W		3.2	321.3
41+0			
W		4.8	319.7
+5		8.4	315.9
cb		10.20	314.31
c		9.96	314.55
cb		10.14	314.37
+4		10.3	314.2
+8		7.0	317.5
E		7.0	317.5

T.P.	0.40	312.22	12.69	311.82
------	------	--------	-------	--------

41+50

E		2.0	310.2
+5		1.1	311.1
cb		1.76	310.46
c		1.63	310.59

312.22

41

cb		1.87	310.35
+3		1.4	310.6
W		+3.0	315.2
42+00			
W		+2.8	315.0
+2		4.2	308.0
cb		5.90	306.32
c		5.70	306.52
cb		5.84	306.38
+6		5.6	306.6
E		7.4	304.8
+5		7.4	304.8

+50:

-5		11.0	301.2
E		10.4	301.8
+4		9.5	302.7
cb		9.79	302.43
c		9.65	302.57
cb		9.84	302.38
+2		9.8	302.4
W		5.0	307.2

		312.22		
T.P.	0.58	299.70	13.10	299.12
	43+00			
W			+4.3	304.0
+8			1.2	298.5
cb			1.02	298.38
c			1.17	298.53
cb			1.26	298.44
+6			0.7	299.0
E			1.1	298.6
	+50			
E			4.8	294.9
+5			4.7	295.0
cb			5.18	294.52
c			5.02	294.68
cb			5.30	294.40
+5			4.9	299.8
W			0.9	298.8
	44+00			
-5			10.3	289.4
W			11.8	287.9

		299.70		
			+4	8.4
			cb	9.24
			c	8.98
			cb	9.18
			+4	9.0
			+7	8.2
			E	9.9
			+5	10.0
T.P.	0.51	287.21	13.00	286.70
			44+50	
			-18	9.9
			-10	7.2
			E	4.0
			+5	0.4
			cb	0.46
			c	0.48
			cb	0.83
			+5	0.0

287.21

W	2.9	284.3
+8	7.4	279.6
+15	6.5	280.7
45+00		
-15	12.7	274.5
-7	12.0	275.2
W	7.5	279.7
+4	4.3	282.9
cb	4.80	282.41
c	4.36	282.85
cb	4.60	282.61
+5	4.4	282.8
E	8.0	279.2
+7	12.2	275.0
+15	13.5	273.7
+50		
-15	16.4	270.8
-5	15.2	272.0
E	11.8	276.4
+6	8.3	278.9

287.21

43

cb	8.72	278.49
c	8.60	278.61
cb	8.87	278.34
+6	8.4	278.8
W	11.4	275.8
+8	14.4	270.8
+15	16.4	270.8
46+00		
-15	19.3	267.9
-7	19.2	268.0
W	15.3	271.9
+5	12.6	274.6
cb	12.99	274.22
c	12.63	274.58
cb	12.82	274.39
+5	12.4	274.8
E	15.8	271.4
+5	18.7	268.5
+15	19.8	267.9
T.P.	0.24	274.44
	13.01	274.20

46+50

+50

-10

7.4 266.8

E

11.8 263.1

E

6.5 267.9

+7

12.0 262.4

+6

3.7 270.7

cb

11.98 262.46

cb

4.10 270.34

c

11.82 262.61

c

3.94 270.50

cb

12.10 262.4

cb

4.22 270.22

+4

11.7 262.7

+5

4.0 270.4

+7

10.2 264.2

W

7.4 266.8

W

10.8 264.1

+10

9.0 265.4

T.P.

0.70 262.22, 2.92 261.52

47+00

-5

9.1 265.3

W

9.1 265.3

48+0

+4

7.7 266.7

W

1.2 260.9

cb

8.07 266.37

+2

1.3 260.9

c

7.86 266.58

+5

4.0 258.2

cb

7.98 266.46

cb

3.92 258.30

+5

7.4 266.8

c

3.64 258.58

E

9.1 265.3

cb

2.80 258.42

+5

9.2 265.2

+4

3.7 258.5

E

2.7 259.5

48+50			
E	8.2	254.0	
+5	7.4	254.8	
cb	7.25	254.49	
c	7.60	254.62	
cb	7.87	254.35	
W	7.4	254.8	
49+0			
-10	16.3	245.9	
W	12.6	249.6	
+3	11.0	251.2	
cb	11.21	250.91	
c	11.00	251.22	
cb	11.14	251.10	
+6	10.9	251.3	
F	13.5	248.7	
+5	15.5	246.7	
+10	15.5	246.7	
49+20			
-10	15.4	246.8	

E			15.4	246.8
+9			11.4	250.8
cb			12.22	250.00
c			12.11	250.11
cb			12.40	249.82
+6			12.1	250.1
W			14.6	247.6
+5			16.7	245.5
+10			16.8	245.4
T.P.	2.61	251.91	12.92	249.30
			49+53.84	N L Cholla Rd.
-10			8.2	243.7
W			7.6	244.3
+			3.5	248.4
cb			3.53	248.38
c			3.29	248.62
cb			3.31	248.60
+3	FH.			
E			3.2	248.7



49+95.71 E Cholla Rd

E	4.2	247.7
cb	4.38	247.53
c	4.45	247.46
cb	4.70	247.21
+5	4.1	247.8
W	7.7	244.2
+10	9.0	242.9

50+37.57 S4 Cholla Rd

-10	10.3	241.6
W	8.6	243.3
+5	4.8	247.1
cb	5.01	246.90
c	4.85	247.06
cb	4.88	247.03
+5	5.9	248.0
E	4.7	247.2
+5	5.7	246.2

51+00

-10	9.5	242.4
-5	9.2	242.7
E	7.5	244.6
+5	4.0	247.9
cb	4.75	247.16
c	4.65	247.26
cb	4.90	247.01
W	5.4	246.5
+5	6.1	245.8

Top Curb  
N.W. Cor Conc. Bridge.  
approx 52+35

3.94	247.97
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XSEC of Loring St  
E of LAMONT

Moore  
6-13-38.

Indexed  
C.S.K.

47

See T.P. 20 p57

S.E. 3' S. 94.

7' c.t. 12.73 219.58

Loring  
of  
Lamont

206.85

0-50 W of Lamont

S cb 12.71 206.87

S Pav. 13.34 206.24

0-20 E of

S cb 12.70 206.88

S pav 13.30 206.28

20' S " 14.84 204.74

20' S cb 14.17 205.41

0 to E.L. Lamont

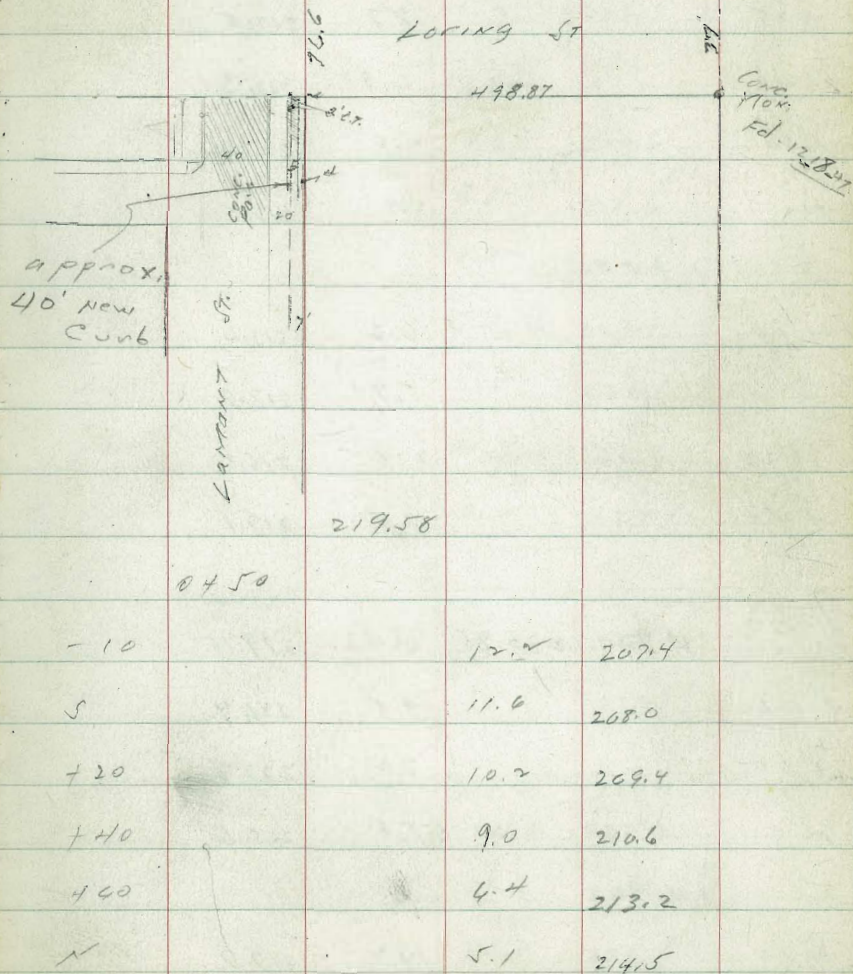
S.L. Loring 12.2 207.4

+20 10.0 209.6

+40 8.8 210.8

+60 7.9 211.7

N 6.2 213.4



LORING ST

498.87

77

C.C. 170' S  
Ed. 12.28.37

70' S  
70' S  
70' S

-10

12.2 207.4

S

11.6 208.0

+20

10.2 209.4

+40

9.0 210.6

+60

7.9 211.7

N

6.2 213.4

	1 + 00			
- 10		12.4	207.2	
S		11.7	207.9	
+ 25		8.8	210.8	
+ 40		6.8	213.3	
+ 60		4.6	215.0	
N		2.1	217.5	
	1 + 50			
- 10		6.6	213.0	
S		5.7	213.9	
+ 20		2.8	216.8	
+ 40		0.5	219.1	

T.P	11.70	230.85	0.43	219.15
+ 46			9.5	226.4
+ 60			7.2	223.7
N			5.8	225.1
	1 + 90			
- 10			13.2	217.7
S			12.3	218.6

+ 28		8.0	222.9	
+ 42		7.7	223.2	
+ 50		5.2	225.7	
N		1.2	229.7	
	2 + 00			
- 10		10.3	220.6	
S		9.3	221.6	
+ 20		8.5	222.6	
+ 25		7.0	223.9	
+ 42		6.8	224.1	
+ 47		4.3	226.6	
+ 60		2.0	228.9	

T.P	7.74 <del>11.74</del>	236.77	1.82	229.03
N			5.1	231.7
	2 + 25			
- 10			15.2	221.4
S			14.8	222.0
+ 25			11.6	225.2
+ 44			10.0	226.8
+ 46			8.2	228.6

~~40.77~~  
236.77

+55	5.9	230.9
N	2.8	234.0
2+55		
-10	13.8	223.0
5	12.1	224.2
+20	9.6	227.2
+42	8.4	228.4
+50	5.6	231.2
N	1.9	234.9

3+00

-10	13.8	223.0
5	12.2	224.6
+20	9.4	227.4
+40	7.4	229.4
+55	5.5	231.3
N	3.8	233.0

3+50

-10	14.8	220.0
5	15.8	221.0
+85	11.8	225.0

~~40.77~~  
236.77

49

+45	9.2	227.6
+65	6.7	230.1
N	5.3	231.5
2+00		
-10	17.3	218.5
5	16.1	220.7
+20	13.4	223.4
+40	10.1	226.7
+60	7.5	229.3
N	6.0	230.8

4+35

-10	16.4	220.4
5	14.4	222.2
+20	11.4	225.4
+40	9.0	227.8
+60	6.1	230.2
N	4.7	232.1

4+65

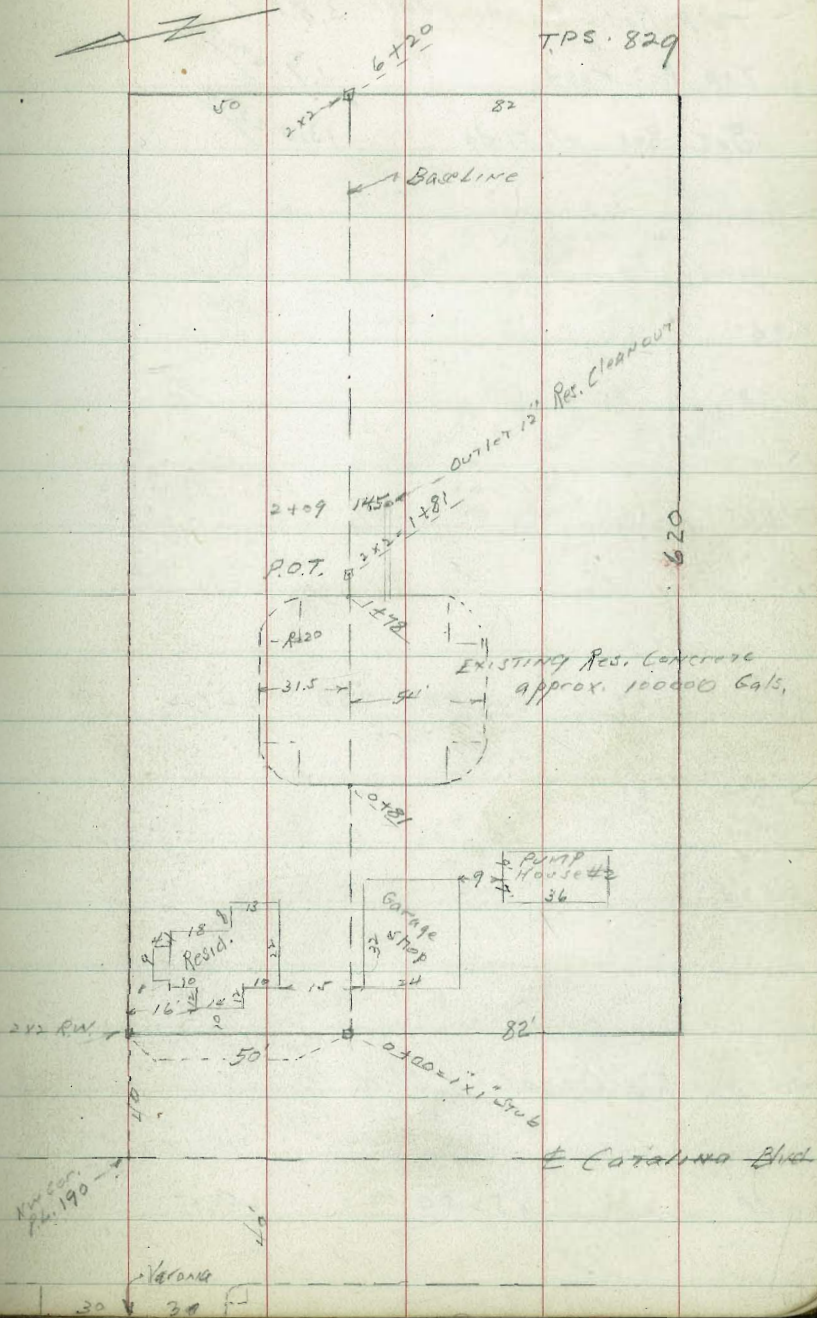
-10	16.9	219.9
5	15.0	221.8
+20	12.6	224.2

240.77  
236.77

+40		9.5	226.3	
+50		8.1	228.2	
N		4.9	231.9	
+98.87				
-10		18.6	218.2	
S		17.4	219.4	
+8.5	Top 4' Cem. st	15.78	220.99	
+20		14.5	222.3	
+40		11.7	225.1	
+60		9.0	227.8	
N		7.3	229.5	
N	Top Stone cut	7.11	229.66	
T.P.	0.72	224.49	223.77	
		<del>228.49</del>	13.00	227.77
T.P.	1.16	213.10	12.55	211.94
		<del>217.10</del>		215.94
		6.25	206.85	206.85

Location & Levels for proposed  
New Water Res. at Site of Existing  
Res. & Pump Sta. #2, Pueblo Lot #190  
Catalina Blvd. & Varona.

Moore  
Lisson  
Northern 6-17-38.



Top Res. Cent. wall 3.85 <sup>244.74</sup>  
 Top Res. roof 1.7 <sup>246.9</sup>  
 Bot. Res. W. side 13.0 <sup>235.6</sup>

LT. Gasoline RT. 52

0+81

241.1 248.7  
 7.5 4.9  
 Jo Jo

244.3 244.5 243.9  
 4.3 4.1 4.7  
 Jo Jo Jo

0+65

241.9  
 6.7  
 Jo

244.5 245.3 246.46 244.9  
 4.1 3.3 2.13 2.7  
 Jo Jo Pump House ft. Cent. Jo

T.P. 2.47 248.59 7.38 245.12

248.59  
 2

0+25

245.0 247.4  
 7.5 5.1  
 Jo Res. H. E. L. 6.6 Gar. ft. Cent. 6.0 247.3 248.0  
 Jo Jo Jo 5.2 4.5  
 Jo Jo 8.2

0+00 = Ely Catalina Blvd.

247.9 247.9 249.7 250.4  
 4.6 4.6 3.8 2.1  
 Jo Jo Jo Jo

NWBP 2.33 252.50 250.17

SWBP Cat. Varona 1.62  
 Cat. 4 Varona  
 252.50

Lt.

Passette

Rt.

+25

$$\begin{array}{r} 229.7 \\ 6.8 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 227.5 \\ 9.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 228.1 \\ 229.1 \\ 231.1 \\ 7.8 \\ 7.4 \\ 5.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 231.2 \\ 5.3 \\ \hline 82 \end{array}$$

+12

Toe Emb. }

$$\begin{array}{r} 231.2 \\ 1.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 230.4 \\ 231.8 \\ 4.7 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 232.8 \\ 4.7 \\ \hline 82 \end{array}$$

+09

Fl. 12" Clearout Outlet

$$\begin{array}{r} 230.95 \\ 5.5 \\ \hline 50 \end{array}$$

T.P.

0.36 236.45 12.50 236.09

$$\begin{array}{r} 236.45 \\ 2 \\ \hline \end{array}$$

+84

$$\begin{array}{r} 234.2 \\ 12.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 242.3 \\ 6.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 243.6 \\ 243.6 \\ 5.0 \\ 7.3 \\ \hline 50 \quad 67 \end{array}$$

$$\begin{array}{r} 241.3 \\ 235.8 \\ 12.8 \\ \hline 82 \end{array}$$

+78

$$\begin{array}{r} 235.9 \\ 12.7 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 235.9 \\ 12.7 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 243.0 \\ 5.6 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 243.8 \\ 243.3 \\ 5.3 \\ 7.0 \\ \hline 48 \quad 55 \quad 70 \end{array}$$

$$\begin{array}{r} 241.6 \\ 236.2 \\ 12.4 \\ \hline 82 \end{array}$$

1400

$$\begin{array}{r} 241.1 \\ 7.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 244.1 \\ 4.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 244.1 \\ 4.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 243.0 \\ 5.6 \\ \hline 82 \end{array}$$

248.59

$$\begin{array}{r} 248.59 \\ 2 \\ \hline \end{array}$$



+50

210.6	209.1	209.2	210.4	211.3	215.0	217.0
$\frac{13.0}{50}$	$\frac{14.7}{40}$	$\frac{14.6}{15}$	13.2	$\frac{12.1}{25}$	$\frac{8.8}{50}$	$\frac{6.8}{82}$

+25

215.8	215.7	218.2	218.5	220.0	220.0
$\frac{8.0}{50}$	8.1	$\frac{5.6}{15}$	$\frac{5.6}{50}$	$\frac{3.8}{50}$	$\frac{3.8}{82}$

2400

218.7	219.5	219.8	220.0	221.5
$\frac{5.1}{50}$	$\frac{4.0}{25}$	$\frac{3.8}{50}$	$\frac{2.8}{82}$	

T.P. 0.30 223.75 13.00 223.45

223.75

+65

222.0	221.4	221.4	222.4	224.1
$\frac{12.5}{50}$	$\frac{15.1}{25}$	15.1	$\frac{14.1}{50}$	$\frac{12.4}{82}$

2437

226.5	224.4	223.8	228.3	228.8	228.5
$\frac{10.0}{50}$	$\frac{12.1}{25}$	12.7	$\frac{8.2}{30}$	$\frac{7.7}{50}$	$\frac{8.0}{82}$

236.45

236.45

6+00

$\begin{array}{r} 178.7 \\ 20.8 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 177.4 \\ 22.1 \\ \hline 45 \end{array}$ 
 $\begin{array}{r} 179.5 \\ 20.0 \\ \hline 25 \end{array}$ 
 $\begin{array}{r} 186.3 \\ 13.2 \\ \hline 10 \end{array}$ 
 $\begin{array}{r} 189.7 \\ 10.3 \\ \hline 10 \end{array}$ 
 $\begin{array}{r} 191.8 \\ 7.7 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 192.1 \\ 7.1 \\ \hline 82 \end{array}$

5+50

$\begin{array}{r} 186.4 \\ 12.7 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 187.6 \\ 11.9 \\ \hline 14 \end{array}$ 
 $\begin{array}{r} 190.3 \\ 9.2 \\ \hline 25 \end{array}$ 
 $\begin{array}{r} 196.3 \\ 10.2 \\ \hline 25 \end{array}$ 
 $\begin{array}{r} 198.9 \\ 0.6 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 198.9 \\ 0.6 \\ \hline 82 \end{array}$

T.P. 0.84 199.47 12.94 198.63

199.47

5+00

$\begin{array}{r} 194.5 \\ 17.1 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 193.6 \\ 18.0 \\ \hline 42 \end{array}$ 
 $\begin{array}{r} 192.1 \\ 19.5 \\ \hline 17 \end{array}$ 
 $\begin{array}{r} 193.0 \\ 18.6 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 199.4 \\ 12.2 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 201.6 \\ 10.0 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 202.2 \\ 9.4 \\ \hline 82 \end{array}$

4+50

$\begin{array}{r} 197.1 \\ 14.5 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 196.6 \\ 15.0 \\ \hline 25 \end{array}$ 
 $\begin{array}{r} 197.8 \\ 13.8 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 204.0 \\ 7.6 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 206.7 \\ 4.9 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 207.1 \\ 4.5 \\ \hline 82 \end{array}$

4+00

$\begin{array}{r} 204.2 \\ 7.4 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 202.4 \\ 9.2 \\ \hline 55 \end{array}$ 
 $\begin{array}{r} 203.8 \\ 7.8 \\ \hline 35 \end{array}$ 
 $\begin{array}{r} 207.3 \\ 4.3 \\ \hline 35 \end{array}$ 
 $\begin{array}{r} 211.6 \\ 0.0 \\ \hline 55 \end{array}$ 
 $\begin{array}{r} 213.2 \\ 1.6 \\ \hline 82 \end{array}$

T.P. 0.81 211.57 12.39 211.36  
223.75

211.57

L.T.

B.L.

R.T.

			3.96	250.16	250.17
T.P	7.33	254.12	0.20	246.79	
T.P	12.44	246.99	0.35	234.55	
T.P	12.24	234.90	0.03	222.66	
T.P	12.36	222.69	0.34	210.33	
T.P	12.04	210.67	0.84	198.63	

46+20

199.47

175.7	175.0	176.1	183.5	186.6	189.3	189.9
$\frac{23.8}{50}$	$\frac{24.5}{45}$	$\frac{23.4}{30}$	$\frac{16.0}{20}$	$\frac{12.9}{20}$	$\frac{10.2}{50}$	$\frac{9.6}{82}$

199.47

7-21-38  
Miller  
Walker  
Blas

X Sec Alleys B/Ks 38 & 39  
H. P. Whitney's Add.

B.M. B.P. 10.64 58.69 48.05 + Boston

10' W. of E. = e. cl. 30<sup>th</sup> st

S. cmt. cl. 6.39 52.30

S. pav 7.06 51.63

± " 6.88 51.81

N " 6.58 52.11

N. cmt. cl. 5.87 52.81

0+00 = E. line 30<sup>th</sup> st

0.35 N. of N. cmt. cl. E. End 5.60 53.09

" " " Pav " " 5.96 52.73

± " " " " " 6.42 52.25

0.35 N. of S " " " 6.24 52.45

" " " " cmt. cl. " " 6.04 52.65

0+25 E

S. 5.4 53.3

± 5.2 53.5

+ 4.7 54.0

N 4.2 54.5

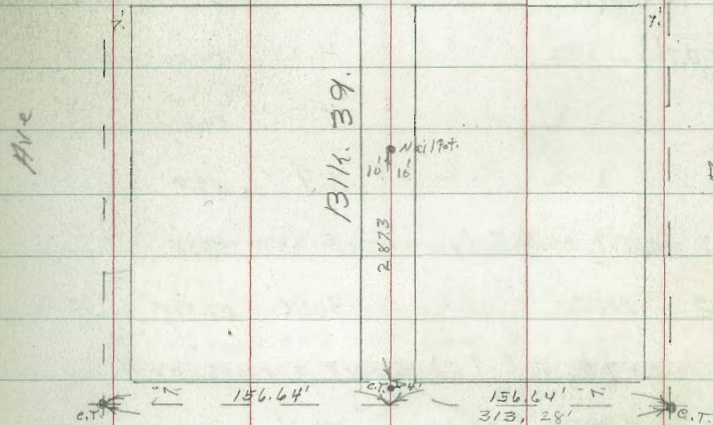
index of  
c.s.R.

32<sup>nd</sup>

312.70

st 57

Flotted TPS-353



31<sup>st</sup>

313.23

st



Newton

B/K. 38

Boston



30<sup>th</sup>

st

B.M. SW 31 + Boston 50.52

58.69

SW End 4 garages on N. side floors 27 Back  
 0+38 W " garage on S. ent. floor 0.1 in Alley.

N-0.7	4.29	54.40
N	4.6	54.1
⊕	4.9	53.8
+7.8 = N. End. cone Apron	5.34	53.35
+9.9 = floor	5.14	53.51
0+70. = E. End. above garages on N		
S	4.4	54.3
+2	5.0	53.2
⊕	5.0	53.2
N	4.4	54.3
+0.7 = floor	4.10	54.59
0+88 double garage on N. dirt floor		
N-0.4	4.3	54.4
1+00 W. side garage on S. dirt floor on Line.		
S = dirt. floor	4.5	54.3
⊕	4.5	54.2
N.	4.3	54.4

58.69

58

1+36 garage on N. dirt. floor 0.9 Back  
 N-0.9 = floor 3.5 55.2

N.	3.5	55.2
⊕	3.6	55.1
S	3.8	54.9

1+37 W. End. ent. foundation on S. 0.4 in Alley

0.4 N of S Line Top. d. 3.45 55.24  
 Garage on S. ent. floor on Line  
 1+70 " " N dirt. " 2.0 Back

S = floor	3.03	55.64
⊕	2.9	55.8
N	3.0	55.2
+2.1 floor	3.0	55.2

1+73 = E. End above ent. foundation

0.3 N of S. = Top. ent 3.05 55.64

1+88 double garage on N. ent. floor 2.0 Back

N-2.0 = floor 2.50 56.19

1+95 garage on S. dirt floor 0.5 Back

S-0.5 = floor 3.0 55.2

58.69

2+00

N 2.8 55.9

E 2.4 56.1

S 2.8 55.9

2+09 garage on S. dirt floor 0.2 Back.

S-0.2 floor 2.5 56.2

garage on S. dirt floor 3.5 Back

S-3.5 floor 2.2 56.5

2+50

S 2.2 56.5

E 2.3 56.4

N 2.5 56.2

2+72 garage on N. dirt floor on line

N = floor 2.9 55.8

E 2.9 55.8

S 2.6 56.1

2+93 garage on S. dirt floor 0.4 Back.

S-0.4 = floor. 2.8 55.9

58.69

59

3+00 { Garage on N dirt floor 0.2 Back.  
W. End. 4 garages on S. dirt floor 0.1 Back.

S-0.1 = floor 3.4 55.3

E 3.7 55.0

N 3.4 55.3

T.P. 5.31 60.24 3.76 54.93

3+25 etc<sup>4</sup> garages on S.

N 5.6 54.7

E 6.1 54.2

E 6.1 54.2

S-0.1 = floor 5.6 54.7

3+50 = E. End above 4 garages on S. 0.1 Back

S-0.1 = floor 6.3 54.0

E 6.6 53.7

E 6.6 53.7

N 6.2 54.1

3+69 garage on N dirt floor 0.1 in Alley

N+0.1 = floor 6.8 53.4

3+84 garage on N. dirt floor 0.3 in Alley

N+0.3 = floor 7.0 53.2

60,24

0.5 S of N<sup>4</sup> Barn to W. Fence to E. 4+00

7.0 53.3

E

7.1 53.2

S

6.8 53.5

4+24 = E. End. above fence 0.3 in Alley

4+35 garage on N. dirt floor 3.5' Back.

N-3.5 = floor

6.1 54.2

{ to Point in block.

4+50 = W. End garage on N. cnt. floor 4.5' Back.

S-25.

7.7 52.6

S

7.1 53.2

E

6.8 53.5

N

6.4 53.7

+4.5 = floor

5.92 54.34

+15 In yard

6.0 54.3

4+93 garage on S. dirt floor 13.0' Back.

S-13.0 = floor

6.6 53.7

5+00

N-20

5.8 54.5

N

6.1 54.2

E

6.1 54.2

S

6.5 53.8

+13

6.6 53.7

60.24

60

5+06 garage on S. cnt. floor 13' Back

S-13.0 = floor

6.6 53.64

S-0.3 = N. End. cnt. apron.

6.54 53.90

5+35 Garage on N. cnt. floor 13' Back.

S-10

6.5 53.8

S = N End. 24" cnt. walk

6.0 54.3

+4

5.4 54.9

E

5.4 54.9

N

5.0 55.3

+1.0 = S. End. cnt. apron

5.02 55.22

+13.0 = floor

4.90 55.34

5+89 W. End cnt. db. on N. 0.2 in Alley.

N+0.2 = Top. W. end. db

4.20 56.04

" ground.

4.7 55.6

E

4.8 55.5

+8

4.8 55.5

S

5.3 55.0

60.24

		5+995 = W line 31 <sup>st</sup> St.		
S	cmt. d.	W. End	5.06	55.78
S	pav	" "	5.04	55.20
☿	"	" "	5.09	55.18
N	"	" "	4.50	55.74
N	cmt. d.	" "	4.50	55.74
		10' E. of W. = W. d. of 31 <sup>st</sup> St.		
N.	cmt. d.		4.74	55.50
N.	pav		5.37	54.89
☿	"		5.60	54.64
S.	"		5.83	54.41
S.	cmt. d.		6.36	54.88
		10' W of E. = N. d. line of 31 <sup>st</sup> St.		
N.	cmt. d.		4.76	55.48
N.	pav		5.39	54.85
☿	"		5.64	54.56
S	"		5.93	54.31
S	cmt. d.		5.34	54.89

60.24

61

		0+00 = E. Line 31 <sup>st</sup> St.		
		0.1 S. of S. = W. End. 3" cmt. d. on S.	4.63	55.61
		0.15 N. of S = $\left\{ \begin{array}{l} \text{cmt. d.} \\ \text{+ Pav} \end{array} \right.$ E. End	5.13	55.11
	☿	pav " "	5.20	55.04
		0.1 N. of N. = cmt. d. + " " "	4.51	55.73
		6+15		
		-0.3 Brick fire Place	4.7	55.54
	N		4.4	55.9
	☿		4.5	55.8
	S.		4.6	55.7
		+0.4 Top. 3" d.	4.60	55.62
		0+37 E. End. cmt. d. on S. = W. End. cmt. walk on S. 0.4 Pav. 1/2		
		0+55		
	S-5	A on N. side cmt. walk	4.36	55.88
	S		4.5	55.8
	☿		4.5	55.8
	N		4.7	55.6
	+30		4.4	55.9

Drain this area N of Alley

Lower grade of pav. in Alley W. of E. line 31<sup>st</sup> St.





2+65 { E. End above Fence on S. 1.7' in Alley  
 W " Shed " 1.7' " "  
 2+74 { E. " above shed. " 1.7' " "  
 W " Fence " 1.7' " "  
 T.P. 1.59 59.96 1.87 58.37  
 2+90 double garage on N dirt floor 2.7 Back  
 N-2.7 = floor 1.2 58.8  
 3+00 W. End Shed on N 1.3' in Alley  
 N 1.4 58.6  
 E 1.8 58.2  
 +9.6 = Fence 1.6 58.4  
 3+20 Fence on S. Line  
 3+24 garage on N dirt floor 1.3 in Alley  
 1.3 in Alley = floor 1.6 58.4  
 3+32 Pepper Tree 40" Diam. 2.0 in Alley  
 3+29 { E. End Garage on N }  
 W " Fence " " } 1.3 in Alley  
 3+40 Δ above " " " " "  
 3+43 " " " " on N. Line

S. 2.3 57.2  
 E 2.5 57.5  
 N 1.6 58.4  
 Garage on N dirt floor 2.5 Back  
 3+53 { " " " " " " 1.2 " "  
 N-2.5 = floor 1.8 58.2  
 N 1.8 58.2  
 E 2.4 57.2  
 S 3.0 57.0  
 S+1.2 = floor 3.0 57.0  
 3+63 garage on N dirt floor 2.6 Back  
 N-2.6 floor 2.35 57.61  
 0.9 in Alley = S. End. cut apron. 2.45 57.51  
 { E. End. garage on N dirt floor 3.6 Back  
 3+76 { " " " " " " 1.2 " "  
 S-1.3 + S = floor 3.2 56.8  
 E 3.4 56.8  
 N 2.8 57.2  
 N+3.6 2.5 57.5

59.96

3+82 W. End. Fence on N. 1.3 in Alley		
4+00		
1.3 S. of N. Fence	3.4	56.6
⊥	3.7	56.3
S.	3.9	56.1
4+22 ⊥		
{ E. End. garage on N. dirt floor 0.8 in Alley.		
" " " " 0.6 Back		
0.8' S of N. = floor	4.2	55.8
⊥	5.0	55.0
S.	5.0	55.0
to 4 floor	4.9	55.1
4+33 garage on N dirt floor 8.0' Back		
N - 8.0 = floor	5.1	54.9
4+50 W. End. Fence on S. 1.0' in Alley		
1. N of S.	7.0	53.0
⊥	7.0	53.0
+L	7.0	53.0
N	6.7	53.9

4+67 E. End. Above Fence on S. 1.0 in Alley

59.96

4+73 garage on S. dirt floor 1.0' Back		
N	7.7	52.3
+5	8.8	51.2
⊥	9.0	51.0
S	8.9	51.1
S+1. = floor	8.9	51.1
4+65 - 4+70 - 4+77 3 slumps of Trees		
20' Diam 1.5 S. of N. Line		
4+80 - W. End. Fence on S. 1.0' in Alley		
4+88 E " " " " " "		
4+94 garage on S. dirt floor 4' Back.		
S - 4 = floor	10.8	49.2
S	10.8	49.2
⊥	11.1	48.9
+7.	10.6	49.4
N S	10.1	48.9
5+01. W. End. Fence on S. 0.4 in Alley		

64

59.96

5+02

65

S-5		12.1	47.9	
S		12.1	47.9	
S+1		11.5	48.5	
±		11.5	48.5	
N.		11.5	48.5	

5+30 above fence on S. 9.3' Back  
 + 5+49.5 = W. Line 32<sup>nd</sup> St.

N.	ent. ch	W. End	11.53	48.43	
N.	par	" "	12.04	47.92	+ dirt
±	"	" "	12.43	47.53	
S.	"	" "	12.25	47.71	
S.	ent. ch	" "	12.25	47.71	+ dirt

30' E. of W. = W. ch. Line of 32<sup>nd</sup> St.

S.		12.64	47.32	
S.		13.27	46.69	
±		12.89	47.07	
N		12.49	47.47	
N		11.73	48.23	

T.P.	4.15	59.06	5.05	54.41	at E. 711 <sup>th</sup> E. 4 <sup>th</sup> Line 31 <sup>st</sup> St.
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B.M. B.P	S.W. 31 <sup>st</sup> Boston	8.54	50.51	50.52	
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Survey Fire Sta. Site  
 P.L. 190 Catalina & Varona

Moore  
 Hoopes  
 5-25-42

Indexed  
 C.S.K.

Plotted TDS 829  
 6-16-48-NPS

66

LT. Baseline RT.

1+20	242.6 15.4 20	242.4 15.6	242.9 15.1 30	242.5 15.5 60	243.3 14.7 80	
1+00	242.9 15.1 20	243.3 14.7	244.0 14.0 30	244.3 13.7 60	249.4 13.6 80	
0+65	245.2 12.8 20	245.9 12.2	246.8 11.4 30	248.4 9.4 50	248.0 10.0 60	247.2 10.8 80
0+35	247.4 10.6 20	247.9 10.1	251.1 6.9 9	251.2 6.8 30	251.7 6.3 60	251.7 6.3 80
0+20	248.7 9.3 20	248.8 9.2 10	251.3 6.7 30	252.1 5.9 60	252.5 5.5 80	253.0 5.0 80
0+00 E.L. Catalina	250.6 7.4 20	252.3 5.7	252.7 5.3 30	253.7 4.3 60	254.2 3.8 80	
00-16	251.5 6.5 20	252.9 5.1	253.5 4.5 30	254.4 3.6 60	254.8 3.2 80	
00-22	251.3 6.7 20	251.7 6.3	252.5 5.5 60	252.5 5.2 80		
00-40 9 00/Var.	251.9 7.15	252.3 5.1	253.5 4.5 60			
SWBP	7.15	257.97		250.84		

REDUCED & PLOTTED BY H. COLE  
 5-26-42

CATALINA  
 AND  
 VARONA

SET foundation Cons. & Elev.

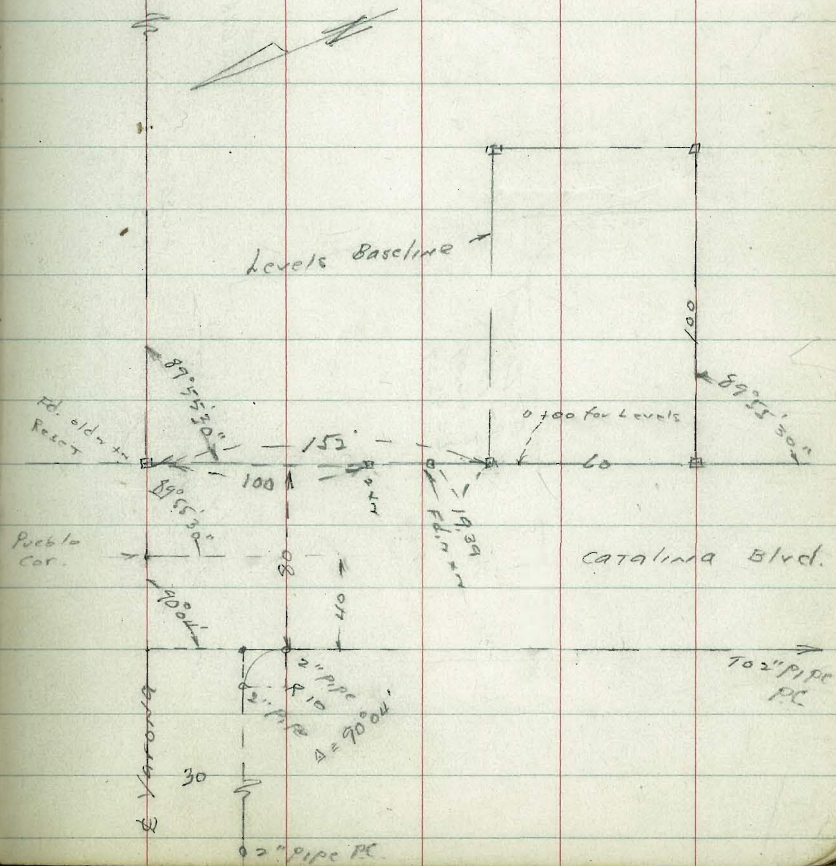
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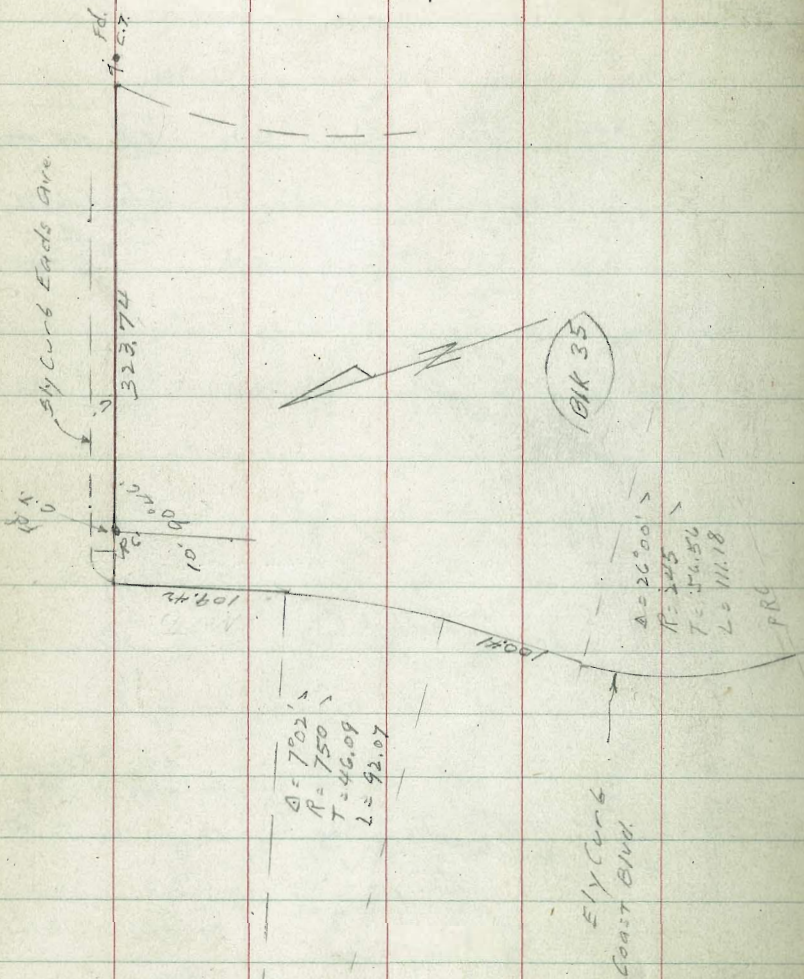
E.L. FOUNDATION

Floor 254.50

CON. MON  
 NE. 190

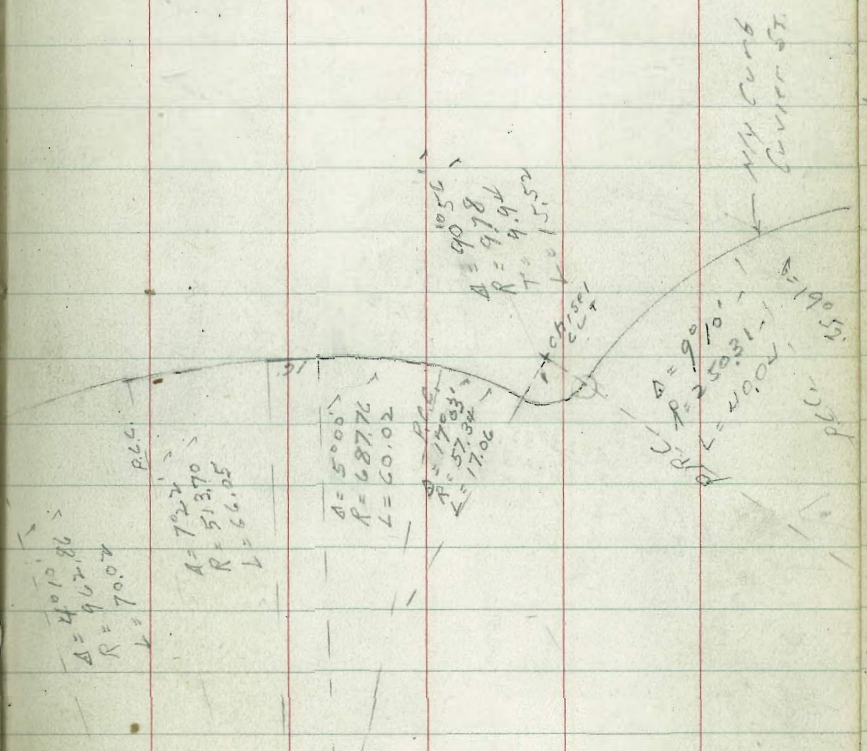


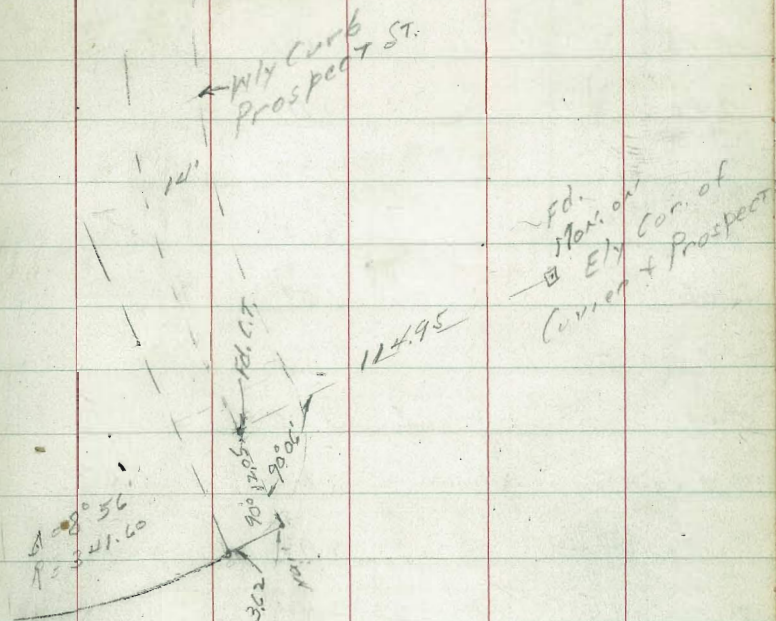
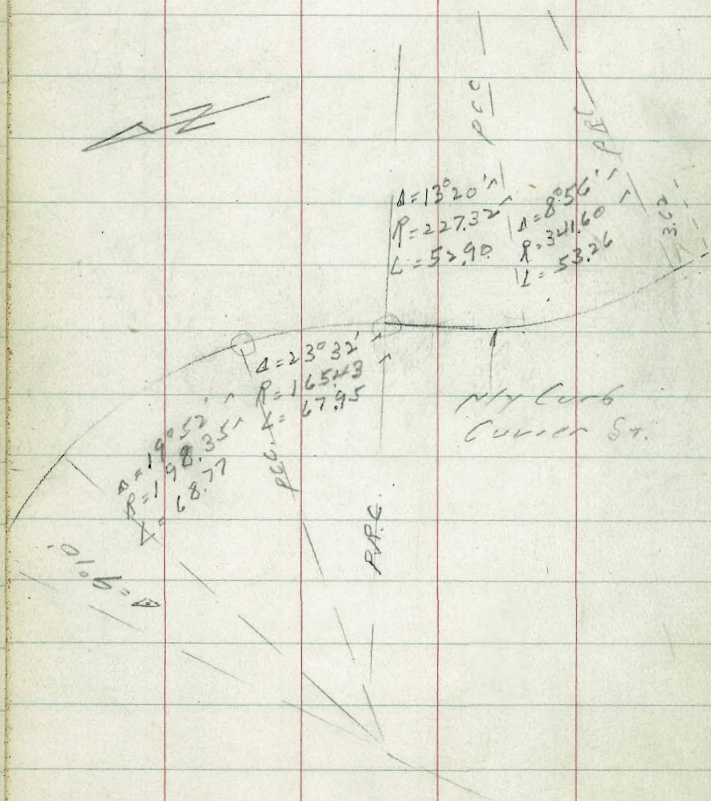
Indexed  
C.S.K.



Curb align. on Coast Blvd.  
and Currier St.  
BIK 35 La Jolla Park  
chisel cuts on curve pts.

67.  
Moore  
8-3-38.





Day Levels on Beech St.  
Key. to Pac.

NW 80	109	21.07	19.98	Ret. Beech
00 = Wly Ret.				
N cb		1.11		
gut		1.81		
C		1.25		
gut		2.15		
S cb		1.59		
+ 50				
S cb		2.25		
gut		3.84		
C		2.92		
gut		2.41		
N cb		2.72		
1700				
N cb		4.33		
gut		5.09		
C		4.58		
gut		5.58		
S cb		4.85		

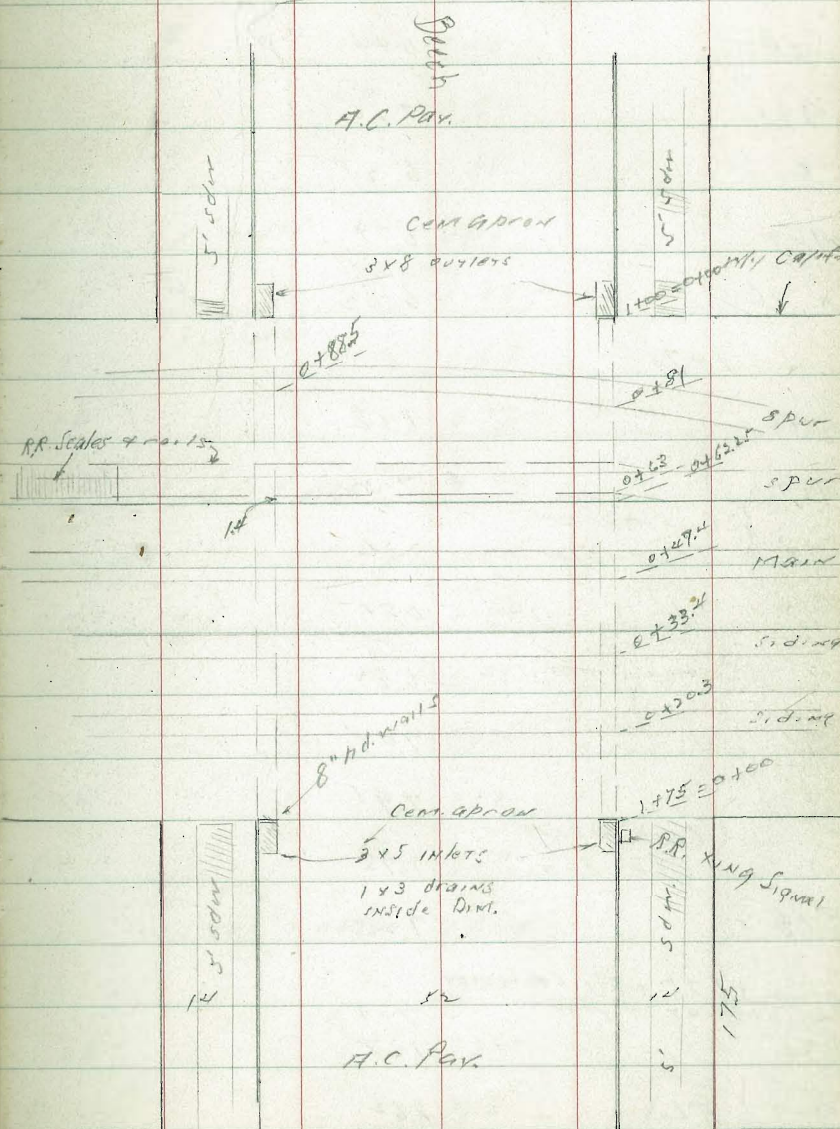
Plans  
shown  
for term  
2-13-36.

Indexed

NOTE

STATION ON  
CURB LINE of Beech St.  
DRAIN-2

69



Wly Retner



1750	
S cb	6.44
qut	7.26
c	6.21
qut	6.79
N cb	6.02

1770		
N cb	6.68	
qut	7.42	
+3	} Cent. apron to drain	7.36
1/4		6.81
c	6.82	
1/4	7.02	
+10	} Cent. apron to drain	7.91
qut		7.95
S cb	7.25	

1775 = Ely cald. 2100	
S.L. cb. var. + Pav.	7.09
S cb	7.27
qut FL)	8.62
+3 " } drain	8.02

+3 hd wall	7.30	
1/4	7.08	
c	6.92	
1/4	6.87	
+10 hd. wall	6.55	
"	8.23	
qut	} F.L. Drain	8.17
N cb		6.77
N.L. cb var + Pav	6.55	
"	at 30.3 = E rail side	
N.L. rail	6.84	
N cb	"	6.89
c	"	7.14
S cb	"	7.37
S.L.	"	7.50
	WL rail above siding	
S.L.		7.42
S cb		7.34
c		7.13
N cb		6.92
N.L.		6.86

	0433.4	E rail	Siding	
NL			6.81	
cb			6.92	
C			7.11	
cb			7.32	
SL			7.36	
		W rail	above siding	
SL			7.36	
cb			7.32	
C			7.10	
cb			6.96	
NL			6.84	
	0447.4	E rail	Main S.P.R.	
NL			6.85	
cb			6.91	
C			7.06	
cb			7.24	
SL			7.31	
		W rail	Main S.P.R.	
SL			7.30	

		cb	7.22	
		c	7.06	
		cb	6.93	
		NL	6.85	
	0462.25	E rail	spur	
		NL	6.89	
		cb	6.80	
		C	6.73	
		cb	6.70	
		SL	6.66	
			W rail	above siding
		SL	6.69	
		cb	6.69	
		C	6.71	
		cb	6.80	
		NL	6.90	
	0481	E rail	spur	
		NL	7.74	
		cb	7.96	
		C	8.60	

Rails &  
Scales  
Same fl. 95 ex 62.25

cb		9.50
SL		9.98
	W rail above spur	
SL		9.89
cb		9.40
E		8.58
cb		7.91
NH		7.68
	1+00 w/y Calif. = 0+00	
NL cb + par		8.73
cb + "		8.60
gut FL drain		10.02
+3 " "		10.00
+3 bd wall		8.65
1/4		8.77
c		8.84
1/4		9.09
+10 bd wall		9.50
+10 FL drain		10.84
gut " "		10.87

cb		9.49
SL cb		9.00
SL gut		9.77
	0+08	
S cb		9.76
gut		10.90
+3	FL. Cont apron of drain	10.89
1/4		9.57
c		9.27
1/4		9.19
+10	FL. Cont. Apron	10.07
gut	" " "	10.11
N cb		8.93
	0+50	
N cb		10.52
gut		11.29
c		10.92
gut		11.92
S cb		11.04
T.P.	4.13 14.07	11.13 9.94

1400

C cb 5.94

gut 6.65

c 5.05

N gut 6.12

N cb

1450

N cb 7.26

gut 7.96

c 7.40

gut 8.38

S cb 7.70

1488 = Pl. cb return

S cb in drive in 9.53

gut 9.54

c 8.80

gut 9.40

N cb in drive 9.39

1400 Ely Pac.

cb - 4.72 cb return 8.91

" gut 9.49

N cb pay 9.55

c 9.25

cb 9.73

T.P. 3.98 9.53 8.52 5.55

cb. 4.41 gut 5.20

top cb return 4.48

check to M.F.B.P. Pac. + Beech 4.22 5.31 5.27

9.04

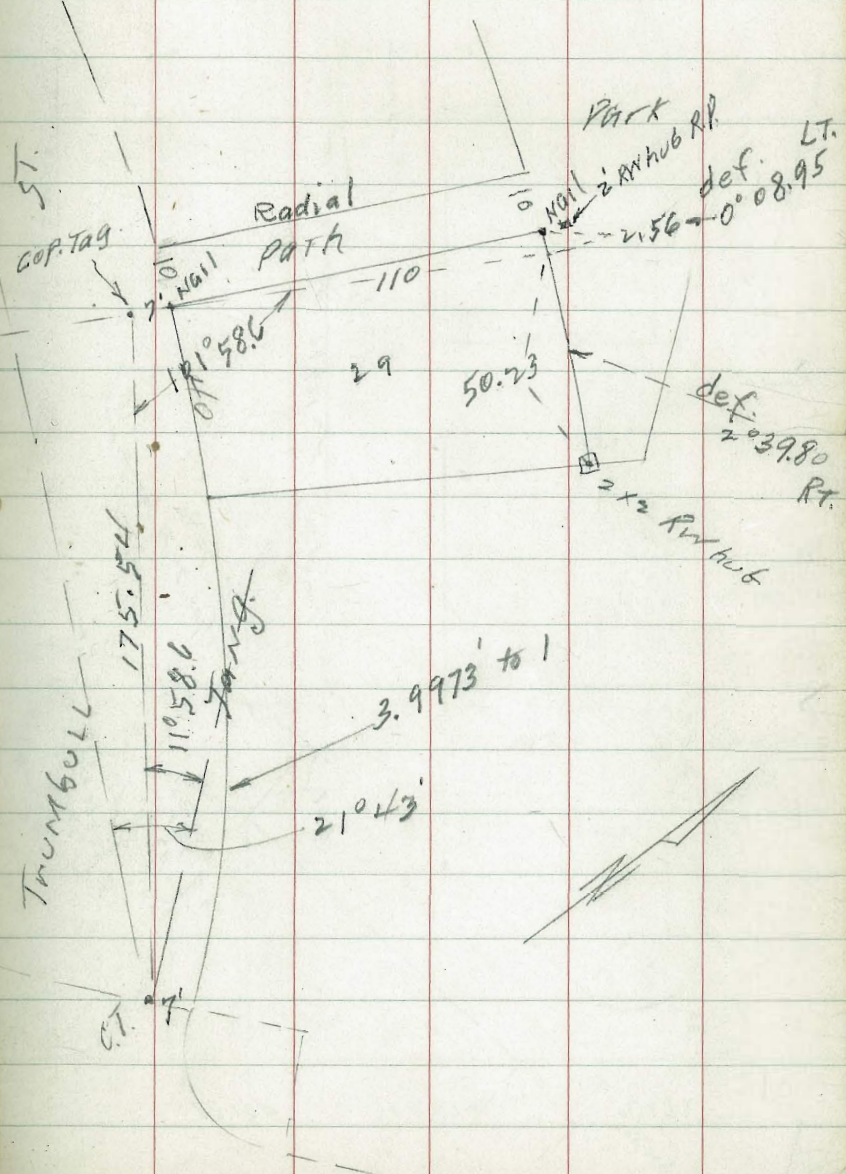
this BM. from Bdwy 4 Pac

Survey lot  $\frac{29}{H}$  Cabrillo Ter.

INDEXED  
EPB

Moore  
Osborn  
Hale  
6-5-40,  
2 hrs.

7' C.T. E.C.  
TO C.T. E.C.



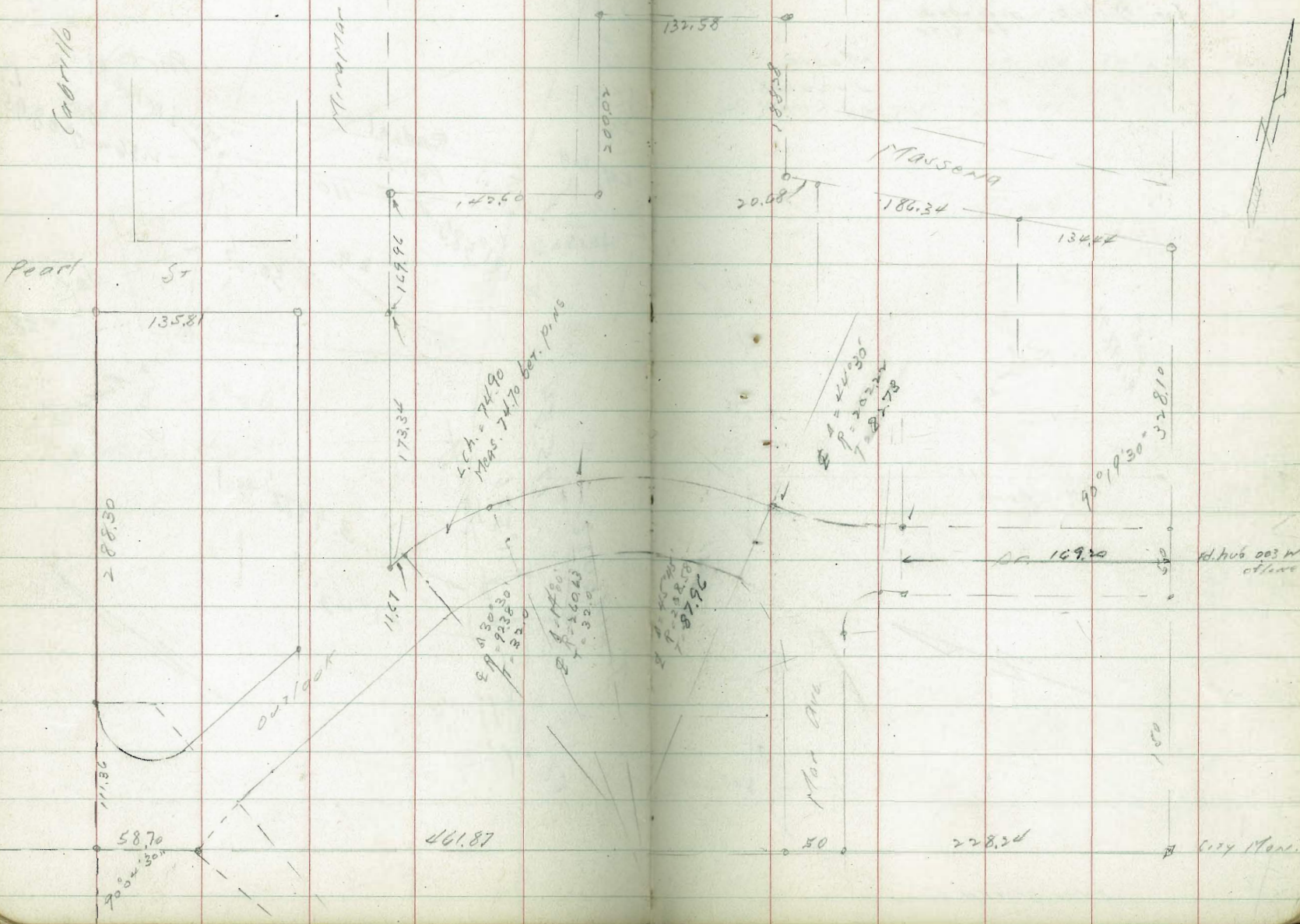
$\Delta 43^{\circ}26'$

7' LINE R 423'

Check Beverly Hts.  
 Resub of Carter add,  
 in La Jolla -

Moore  
 515504  
 Northern  
 8-26-38.

Indexed  
 C.S.K.



Survey Sly Line Lot 28 Cabrillo Ter.  
for Bishop, Freeman  
for City

Moore  
4-20-38.

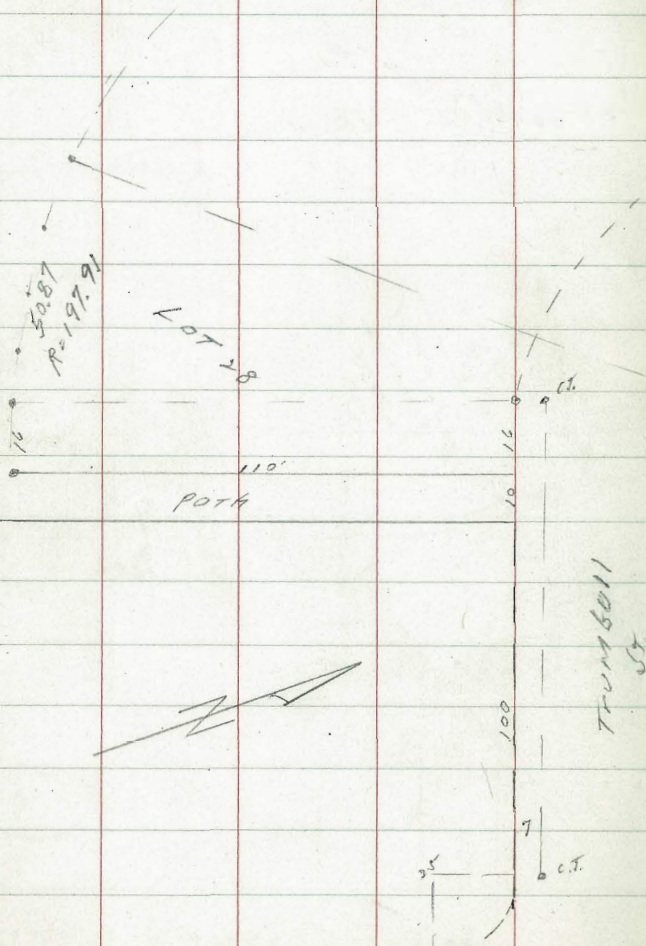
8.685 = 1'

1° 50' 30" RT.

4 parts 12.74 3° 41'

5° 31' 30"

7° 22'



Evergreen

Indexed  
C.S.R.

Levels at Scene of Auto accident on March 2, 1938.  
at Sunset Cliffs N of Osprey St.

Bk.  
"A" 77

Moore  
Sisson  
Northern Mar. 3, 1938

0 + 60

$\frac{2.6}{5.7}$   $\frac{2.9}{5.4}$   $\frac{4.5}{5.0}$   $\frac{5.5}{5.5}$  6.1

0 + 40

$\frac{2.7}{5.6}$   $\frac{4.2}{5.2}$   $\frac{4.9}{5.0}$  6.2

0 + 20

$\frac{2.6}{6.5}$   $\frac{4.7}{6.0}$   $\frac{4.9}{3.0}$  4.3

+ 10

TOP LINE →  $\frac{2.7}{8.5}$   $\frac{4.6}{7.0}$   $\frac{4.5}{6.0}$   $\frac{6.6}{5.0}$  7.0

00 = W.L. Sunset Cliffs Blvd.

$\frac{6.1}{8.0}$   $\frac{8.0}{5.0}$  8.2

0 - 06 = W. edge Pav.

$\frac{8.30}{7.5}$   $\frac{8.49}{5.0}$  8.83

S.E.B.P. 6.57 39.71

33.14

SUNSET CLIFFS  
of  
OSPREY

39.71



LT.

BL. 78  
"A"

1460

 $\frac{3.7}{100}$  $\frac{5.2}{95}$  $\frac{4.7}{50}$  $\frac{6.3}{25}$  $\frac{6.8}{10}$  $\frac{5.2}{5}$ Top Exhb.  
6" edge clift

1455

6.3

1440

Top of  
most of LT. shots = EM's. $\frac{4.4}{97}$  $\frac{4.7}{92}$  $\frac{5.8}{50}$  $\frac{6.2}{25}$ 

6.5

1420

 $\frac{3.5}{115}$  $\frac{4.5}{108}$  $\frac{5.2}{75}$  $\frac{5.7}{50}$  $\frac{6.0}{25}$ 

6.5

1400

 $\frac{3.2}{92}$  $\frac{3.7}{88}$  $\frac{5.1}{75}$  $\frac{5.6}{50}$  $\frac{5.9}{25}$ 

6.5

0480

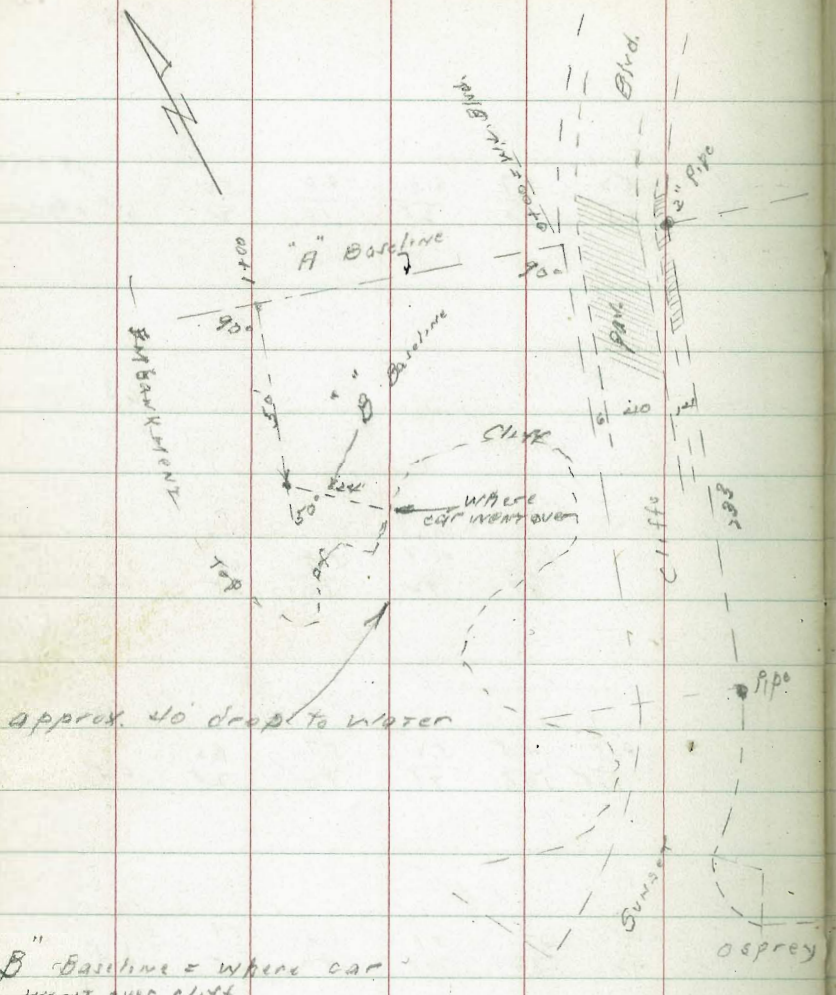
 $\frac{2.9}{66}$  $\frac{4.8}{58}$  $\frac{5.3}{50}$  $\frac{5.6}{25}$ 

6.2

39.71

39.71  
4

B.L.  
"B"



"B" Baseline = where car went over cliff

1400 on "A" & 50' S or LT, = "B" B.L.

39.71

approx. 13.0 / 20 = water

16.0	4.0	3.8	3.1	3.1	4.3	5.2	5.6 - Δ 50'
31	22	25	54	23	21	17	

39.71

TOP Emb.

DIRECTIONS FOR USE OF TABLES

TABLE I

Directions of slope take from side of elevation  
taken for any width roadway, slope 1 to 1  
If ground is sandy, level the cut or fill as well  
Rate is limited by the double curve method in  
the column and top row. The number in bold

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# IMPROVED TABLES

AND

# INFORMATION

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To find Tangent and Elevation for any  
any other degree, divide by degree of curve and  
and constant found in column of constants  
Degree of curve with a given tangent found  
by dividing tangent by constant degree of curve  
given tangent (for constant)

The distance from a point on the tangent to  
the curve is very nearly the square of the tangent  
multiplied by two the radius

58963  
52.75  
642.38

196

2436  
82°-40'-S.E.

9.6  
11.2  
2081 -