1554

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

The paper stock of this book is made of a **high grade 50% rag** paper having a **water resisting surface** and is sewed with Bing **Special Enamel Waterproof Thread.**

Made in U. S. A.

Xsec Verona Ct. Indexed C.S.K.

SWBP	0.58	7.71	7.13	Sea wall San Rafael Pt
	0+12 ± E edge sdw		Ocean Front walk	
S			3.02	4.69
N			3.06	4.65
	0+00 E.L. O.F walk			
N			3.2	4.5
S			3.0	4.7
	0+40			
S			2.7	5.0
+9	℄ 3' Cem N		2.82	4.89
	0+52			
N +1	℄ 3' Cem		2.92	4.79
S			3.0	4.7
	0+71			
S	5' Bd walk		3.1	4.6
N			3.1	4.6
	0+80 N			
N			3.3	4.4
S			3.3	4.4

7.71

	0+00 E.L. S7			
S			3.2	4.5
N			3.3	4.4
	0+29			
N	3' Bd walk		6.3	1.4
S			6.0	1.7
	0+62			
S			7.1	0.6
N	4' Bd walk		7.1	0.6
	0+88			
N	4' Bd walk		7.7	0.0
+9	3' Cem "		7.67	0.06
	1+16			
S	ground		8.7	-1.0
+1	Bd walk		7.8	-0.1
+9	4' Cem. "		7.90	-0.19
	1+44			
N	grd		8.7	-1.0
+1	Bd walk		7.9	-0.2
S	4' " "		7.8	-0.1

Plotted 8F6

1

Ocean Front walk to 5' Bd. walk to 4' Bd. walk to Bayview walk to N Blvd.

	1+70.79 WL N. Blvd		
S	Bd walk	8.10	-0.39
N	" "	7.98	-0.27
	W cb		
N	cb	8.09	-0.38
"	gut	8.54	-0.83
S	cb	8.09	-0.38
S	gut	8.29	-0.78
	E cb " N. Blvd		
S	cb	8.48	-0.77
S	gut	8.78	-1.07
N	cb	8.40	-0.69
N	gut	8.75	-1.04
	0+00 EL Blvd		
N	Bd walk	8.4	-0.7
S	" "	8.5	-0.8
T.P.	4.60 3.83	8.48	-0.77
	0+24		
S	grd.	5.2	-1.4

S	Bd walk	4.4	-0.8
N	3' Cent. "	4.65	-0.82
	0+		
N	1' Cent walk	4.78	-0.90
S	Bd "	4.8	-1.0
S	grd	5.2	-1.4
	0+		
S	3' Cent. walk	4.79	-0.96
N	Bd "	4.7	-0.9
N	grd	5.2	-1.4
	0+75		
N	grd	5.4	-1.6
N	Bd wk	4.9	-1.1
S	" "	4.9	-1.1
S	grd	5.3	-1.5
	0+95.56 = WL Bay side Land		
S	Bd wk	5.0	-1.2
N	" "	5.0	-1.2
	WL Bayside Land = 00		
N	" "	4.9	-1.1
S	" "	4.8	-1.0

3.83

	0+40		
S	grd	5.2	-1.4
S	8d wk	4.8	-1.0
N	" "	4.9	-1.1
	0+83.09 wL	B.S. W. to S	
N		4.5	-0.7
S		4.5	-0.7
	0+90		
S		4.7	-0.9
N		4.6	-0.8
	1+00		
N		4.8	-1.0
C		4.6	-0.8
+1		6.6	-2.8
S		6.6	-2.8
	1+19		
S		8.4	-4.6
+1		8.4	-4.6
C		5.7	-1.9
N		5.4	-1.6

3.83

1+21 approx W. Line to N of opening

N	8.6	-4.8
S	8.6	-4.8
1+30		
S	9.4	-5.8
N	9.4	-5.8
El. of new walk to be built	4.28	-0.40

Indexed
C.S.I.K.

Plotted
EDB

Xsec Whiting Ct.

Seaman York Ct

B.M.B.P.	2.22	9.30		7.08	
	w/ Strandway				
N	edge cem. sdw		4.94	4.36	
S	" "		4.93	4.37	
	E.L. Strandway = 0+00				
S	Bd. W		5.4	3.9	
N			5.4	3.9	
	0+40				
N	grd		7.4	1.9	
S		Bd. walk	6.9	2.4	
S	"		7.2	2.1	
T.P.	1.10	3.27	7.13	2.17	
	0+76				
S	Bd walk		2.7	1.1	
N	± Cem "		2.47	0.80	

3.27

	0+87			
N	3' Ext. step		3.05	0.22
S	Bd walk		2.7	0.6
	1+00			
S	Bd walk		3.0	0.3
N	" "		3.1	0.2
	1+37			
N		Bd. walk	3.8	-0.5
S	"	"	3.7	-0.4
	1+70			
S		" "	4.0	-0.7
N		" "	4.1	-0.8
N	grd		5.0	-1.7
	2+00			
N	"	" "	5.1	-1.8
N	"		4.25	-1.02
S		" "	4.0	-0.7
S	"		4.9	-1.6
	2+13.36	w/ N.M. Blvd		
S		Bd walk	3.93	-0.66
N		" "	3.90	-0.63

3.27

W ob M. Blvd

N	ob	3.85	-0.58
N	gut	4.34	-1.07
S	ob	3.88	-0.61
S	ob	4.31	-1.04

E. ob M. Blvd.

S	ob	3.98	-0.71
S	gut	4.28	-1.01
N	ob	3.99	-0.72
N	gut	4.25	-0.99

E.L. M. Blvd. = 0+00

N	Bd. walk	3.9	-0.6
S	Cem "	4.00	-0.73

0+09.4

S	Cem walk	3.98	-0.71
N		3.9	-0.6

0+47

N	grd	4.7	-1.4
N	Bd walk	4.0	-0.7
S	" "	4.0	-0.7
S	grd	4.9	-1.6

3.27

1+00

S	Bd walk	4.0	-0.7
N	" "	4.0	-0.7

T.P.	4.29	3.61	3.95	-0.68

1+31

N	4' Brick wk. "	4.47	-0.86
N	Bd. "	4.28	-1.01
S	" "	4.3	-1.0

1+34

S	2' Cem. "	4.3	-1.0

1+40.78

S	Bd. walk	4.25	-0.98
N		4.28	-1.01

1+72.48

N	sand	4.6	-1.3
S	"	4.6	-1.3

1+79.3

S	E 4' Cem. walk	4.52	-1.31
N	" " " "	4.53	-0.94

3.61

	≥ +0			
N	Top Wood Bulkhead		4.2	−0.6
S	" " "		4.2	−0.8
	≥ +0			
S	Sand		8.1	−4.5
N	"		8.1	−4.5
	≥ +15.95 = M.H.T. according to Miller = Ely prop. 10' dredging			
N	Sand		8.4	−4.8
S	"		8.4	−4.8

Xsec Portion of Windermere Ct.

	5.73	7.90		2.17	T.P. P4
	El. ocean walk=00				
	0+39				
S	℄ 4' cem. walk		2.96	4.94	✓
T.P.	4.51	3.81	8.60	-0.70	✓
	E cb M. Blvd.				
S	cb		4.53	-0.72	✓
S	gut		4.85	-1.04	✓
N	cb		4.52	-0.71	✓
N	gut		4.84	-1.03	✓
	E.L. M. Blvd=00				
N	Bd. wk.		4.4	-0.59	✓
S	" "		4.3	-0.5	✓
	0+50				
S	Bd wk		4.35	-0.54	✓
N	" "		4.35	-0.54	✓
	0+71				
N	3' cem wk		4.42	-0.61	✓
S	Bd "		4.4	-0.6	✓

Indexed C.S.K. 3.81 Plotted EFB 7

	1+11				
S	end Bd wk		4.3	-0.5	
N	" " "		4.36	-0.55	
	1+13.38				
N	sand		4.8	-1.0	
S	"		4.8	-1.0	
	1+40				
S	sand		4.0	-0.2	
N	"		4.2	-0.4	
	1+47				
N			5.5	-1.7	
S			5.8	-2.0	
	1+65				
S			7.9	-4.1	
N			7.9	-4.1	
	1+78.05 = M.H.T. = EL 10' opening				
N			8.2	-4.4	
S			8.2	-4.4	
check	to 1+79.8 writing		4.71	-0.90	-0.92 P5

Indexed C.S.K. 9.49 Plotted E.A.S.

	4566 Yarmouth Ct,			
BMSP	2.41	9.49	7.08	Seawall Yarmouth Ct
	0-12			
N	S' conc walk	ocean walk 4.83	4.66	
S		4.84	4.65	
	0+00 EL. "			
S	conc wk	4.83	4.66	
N	" "	4.87	4.62	
	0+26 = E end S' conc wk.			
N	conc	4.88	4.61	
S	"	4.89	4.60	
	0+54			
S	Bd. wk	4.7	4.8	
N		4.75	4.74	
	0+68			
N	3' conc wk	5.22	4.27	
N	Bd wk	5.0	4.5	
S	"	4.85	4.64	
	0+80 = WL Strand Way			
S	Bd. wk	5.1	4.4	
N	" "	5.3	4.2	

	0+00 WL Str. Way			
N			5.75	3.74
S			5.7	3.8
	0+11			
S	Bd. wk		6.0	3.5
N	4' conc wk		6.03	3.46
	0+40			
N	Bd. wk		7.4	2.1
S	" "		7.45	2.04
	0+61			
S	" "		8.55	0.94
N	4' Conc "		8.45	1.04
	0+83			
N	2' " "		9.10	0.39
S	Bd "		9.2	0.3
	1+00			
S	" "		9.5	0.0
N	3' Conc "		9.40	0.09
T.P.	4.53	4.35	9.67	-0.18

	1+50		
N	1 Cem wk	4.52	-0.17
S	Bd. wk	4.67	-0.30
	2+00		
S	Bd wk	4.8	-0.4
N		4.7	-0.3
	2+50		
N	Bd wk.	5.0	-0.6
S		5.1	-0.7
	2+65		
S	grd	6.1	-1.7
S	Bd wk	5.07	-0.70
N	" "	5.05	-0.70
N	grd	5.4	-1.0
	2+94.13		
N		4.74	-0.41
S	Bd wk	4.72	-0.37
	W/ C6 M. Blvd		
S	C6	4.59	-0.24
S	gut	5.02	-0.67
N	C6	4.60	-0.25
N	gut	5.02	-0.67

	E C6 M. Blvd		
N	C6	5.05	-0.70
N	gut	5.09	-1.04
S	C6	5.08	-0.73
N	gut	5.42	-1.07
	E.L. M. Blvd 0+00		
S	Bd. wk.	5.1	-0.7
N	" "	5.2	-0.8
	0+30		
N	Bd wk	5.0	-0.6
S	" "	5.15	-0.80
	0+28.95 = W/L to opening in Blvd		
S	Bd wk	5.1	-0.7
N	" "	5.15	-0.80
	0+57		
N	-9 & 9' gar. cem. fl.	4.45	-0.10
N	Bd. wk	5.1	-0.7
S	" "	5.1	-0.7
	0+77.77 = Elv. Line M.B.		
S	Bd. wk.	4.96	-0.61
N	" "	5.0	-0.6

Blk 240

X sec 16' alley So. of Yarmouth

E of

		4.35			
T.P.		3.66	1.86	2.49	
	E cf N. Blvd.				
N	pav.		4.77	-1.11	
S	"		4.81	-1.15	
	E.L. N. Blvd.				
S	cf		4.30	-0.64	
S	Pav		4.86	-1.20	
C	S. N. H. Blvd		4.73	-1.07	
N	cf		4.39	-0.73	
N	pav		4.90	-1.24	
	0+08				
N	wedge double gar		4.52	-0.88	Conc Fl
C			4.8	-1.1	
S			4.5	-0.8	
	0+24				
S			4.5	-0.8	
C			4.4	-0.9	
N	Edge gar	conc fl	4.59	-0.93	

Indexed C.S.K.

3.66

10

0+48.57 s WL 16' opening to North

N			4.4	-0.7
C			4.5	-0.8
S				
S +1 E 9' gar.		conc fl.	4.49	-0.83
	0+91.12			
S			4.5	-0.8
C			4.5	-0.8
N			4.7	-1.0
	1+15			
N			4.6	-0.9
C			4.1	-0.4
S			4.1	-0.4
	1+35			
S			3.5	0.2
N			4.5	-0.8
	1+45			
N			4.7	-1.0
S			3.2	0.5

3.66

1+50

S		5.1	-1.4
N		5.3	-1.6

1+58.73 E.L. 10' opposing to So.

N		5.5	-1.8
S		4.4	-2.7

Check 1+79.3 Whiting -0,89 -0,9✓

Xsec York Ct.

BM. B.1°	1.04	8.12		7.08	Seawall York Ct.
	0-12 E. edge Ocean walk				
S	Concr		3.46	4.66	
N	"		3.44	4.68	
	0+00 E.L. Ocean wk.				
N	sand		3.9	4.2	
S	"		3.8	4.3	
	0+25				
S			3.8	4.3	
N			4.0	4.1	
	0+45 hump on Bd. walk				
N			3.5	4.6	
S			3.4	4.7	
	0+65				
S			3.9	4.2	
N	Brick (loose)		3.80	4.32	
	0+80 W.L Strand Way				
N	Loose brick		4.19	3.93	

Indexed C.S.K. 8.12 Plotted D.F.S.

12

N	Bd wk	3.8	4.3
S	Bd. wk.	3.95	4.17
	0+00 = E.L. Strand Way		
S	sand	4.6	3.5
N	"	4.7	3.4
	0+05		
N	Bd. wk.	4.3	3.8
S	" "	4.35	3.77
	0+37		
S	Bd wk	5.38	2.74
N	4' Brick wall	5.30	2.82
	0+49		
N	3' Brick wk	5.59	2.53
	0+62		
N	2' Conc wk	6.00	2.12
S	Bd "	6.25	1.87
S	sand	7.1	1.0
	0+95		
S	Sand	7.9	0.2
S	Bd wk	7.1	1.0
N	" "	6.9	1.2
N	Sand	7.9	0.2

	1+07		
N	sand	7.8	0.3
N	Bd. wk	7.1	1.0
S	3' Cem "	7.18	0.94
	1+12		
N	3' Cem wk	7.25	0.87
	1+37		
N	3' Cem walk	7.58	0.54
S	2' " "	7.58	0.54
	1+50		
S	sand	8.4	-0.5
S	Bd wk.	7.7	0.4
N	"	7.7	0.4
N	"	8.4	-0.3
	1+75		
N	Bd. wk.	8.0	0.1
S	" "	8.0	0.1
	2+07		
N	Bd. wk	8.7	-0.6
S	3' Cem. "	8.44	-0.34

	2+27		
S	2' Cem. wk	8.80	-0.68
N	Bd "	8.8	-0.7
	2+38		
N	Bd wk	8.7	-0.6
S	3' Cem. "	8.74	-0.60
	2+44		
N	4' Cem. wk	8.74	-0.67
	2+70		
N	sand	9.4	-1.3
N	Bd wk	8.7	-0.6
S	" "	8.7	-0.6
S	sand	9.5	-1.4
	3+10.93 w.c. N. Blvd		
S	Bd wk	8.47	-0.35
N		8.45	-0.33
	w/ cb N. Blvd.		
N	cb	8.45	-0.33
N	gut	9.01	-0.89
S	cb	8.41	-0.29
S	gut	9.00	-0.88

Indexed C.S.K. 9.53 Plotted

xsec Zanzabar Ct.

B.M.	2.45	9.53		7.08	York Ct. Seawall
	0-12 edge Ocean wk				
S	Cem. walk		4.89	4.64	
N	" "		4.87	4.66	
	0+00 ℄ W.L. Ocean wk				
N	sand		4.7	4.8	
S	"		4.7	4.8	
	0+06				
N	4' Cem. wk.		4.52	5.01	
	0+12				
S	4' Bd wk		4.93	5.20	could be lowered
	0+25 W end 4' Bd wk				
S	Bd. wk.		4.4	5.1	
N	" "		4.8	4.7	
	0+45				
N	Bd. wk.		5.4	4.3	
S			5.0	4.5	
	0+60				
S	sand		5.7	3.8	
S	Bd wk.		5.2	4.3	
N	" "		5.4	4.1	
N	sand		6.0	3.5	
	0+75 = end Bd. walk				
N	sand		6.5	3.0	
N	Bd. wk.		5.5	4.0	
S	" "		5.7	3.8	
S	sand		6.4	3.1	
	0+80 ℄ W.L. Strand way				
S	sand		6.4	3.1	
S	~~Bd. wk~~		5.7		
N	~~" "~~		~~5.5~~		
N	sand		6.5	3.0	
	0+00 = E.L. Strand way.				
N	Bd. walk		6.2	3.3	
S	" "		6.3	3.2	
	0+20				
S	Bd wk		6.6	2.9	
N	" "		6.5	3.0	

9.53

0+37		
N Bd wk	7.2	2.3
S E 5' Bd walk	7.15	2.38
S sand	8.2	1.1
0+64		
S sand	8.9	0.6
S Bd wk	7.9	1.6
N 5' Cent. "	7.87	1.66
0+86		
N 4.5' Cent. wk	8.60	0.93
S Bd "	8.2	1.3
S sand	8.6	0.9
1+07		
S 2.5' cent. walk	8.68	0.85
N Bd "	8.7	0.8
1+12.5		
N W. edge cent. yard	8.77	0.76
1+37		
N E edge " "	9.14	0.39
S Bd wk	9.3	0.2
S sand	9.7	-0.2

9.53

1+70		
S Bd. wk.	9.7	-0.2
N .. "	9.7	-0.2
1+89		
N 2' Cent wk	10.18	-0.65
N Bd ..	9.9	-0.4
S .. "	10.0	-0.5
2+04		
S Bd wk	10.2	-0.7
N	10.2	-0.7
N 4' Cent "	10.36	-0.83
2+40		
N sand	11.2	-1.7
N Bd wk	10.5	-1.0
S 2'	10.5	-1.0
2+70		
S sand	11.3	-1.8
S Bd wk	10.7	-1.2
N	10.4	-1.1
N sand	11.2	-1.7

9.53

2+90

S 2' brick mk. 10.0 -1.1

3+12.59 w/c N. Blvd.

S Bd mk. 10.38 -0.85

N. " 10.42 -0.89

W. cb. N. Blvd.

N cb 10.21 -0.68

N gut 10.67 -1.14

S " 10.45 -1.12

S cb 10.20 -0.67

X Sec. Venice Co.

SWBP	2.93	10.06	7.13	San Rafael Seawall
	0+12 E edge cem. sdw.		Ocean wk.	
S	cem.		5.30	4.76
N	"		5.29	4.77
	0+00 = WL Ocean Front wk.			
N			4.8	5.3
S			4.8	5.3
	0+13			
S	4' Cem. wk		4.53	5.53
N			4.7	5.4
	0+26			
N	4' Bd. wk.		5.10	4.96
	0+37			
S	3' Cem. wk.		4.61	5.45
N			5.0	5.1
	0+50			
N	Porch fl. wood		4.95	5.11
	0+67			
S	Bd. walk		4.85	5.21

Indexed c.s.k. 10.06 Plotted DFS

17

	0+80 W.L. Strand Way		
S	grd	5.0	5.1
N	"	5.0	5.1
	0+00 EL. Strand Way		
N	Bd. wk.	4.8	5.3
S	" "	4.8	5.3
	0+09		
N	W. edge 4' Cem. wk.	5.15	4.91
S		5.3	4.8
	0+18		
N	E. " "	5.32	4.74
S		5.6	4.5
	0+32		
N	Bd wk	7.1	3.0
S	" "	7.1	3.0
	0+50		
S	Bd wk	8.6	1.5
N	" "	8.7	1.4
	0+75		
N	Bd. wk	9.6	0.5
S	" "	9.6	0.5

10.06

	0+92		
S	4' Bd. wk	9.8	0.3
S	Sand	10.6	0.1
N	Bd "	9.8	0.3
	1+01		
N	3' Bd wall	9.9	0.2
	1+19		
S	4' " "	10.3	-0.2 Low
S	Bd. wk.	10.0	0.1
N	" "	9.95	0.11
	1+38.07 WL N.T. Blvd.		
N	Bd. wk	10.1	0.0
S		10.15	-0.9
	N c6. N.T. Blvd.		
S	c6	10.10	-0.04
S	gut	10.62	-0.56
N	"	10.64	-0.50
N	c6	10.25	-0.19
	E c6		
N	c6	10.60	-0.54

10.06

N	gut.	11.04	-0.98
S	"	11.09	-1.03
S	c6	10.54	-0.48
	E.L. N.T. Blvd=00		
S	Bd. wk	10.7	-0.6
N	" "	10.7	-0.6
	0+34		
N	Bd wk	11.0	-0.9
S	" "	11.0	-0.9
	0+68		
S	3' Cem. wk.	11.16	-1.10
N	Bd. "	11.1	-1.0
	1+01.56 WL Bayside Lane		
N	Bd. wk	11.1	-1.0
S	" "	11.1	-1.0
	E.L. Bayside Lane = 0+00		
S	Bd. wk	11.1	-1.0
N	" "	11.1	-1.0
	0+40		
N	Bd wk	10.9	-0.8
S		10.9	-0.8

10.06

W.L. Bayside main

N	Bd wk		10.6	-0.5
S			10.45	-0.59

X sec Vanatie Ct.

Platted 5.62

SWBP	2.45	9.58	7.13	Rafael Seawall

0-12 E. edge sdw Ocean E. wk

N.	cent.	4.92	4.66
S	"	4.93	4.65

0+00 E.L. O.E. wk.

S	sand	5.7	3.9
N	"	4.8	4.8

0+07

S	Inl. end Bd wk	4.5	5.1
N	" "	4.4	5.2

0+23

N	2' Cent. in wk	4.09	5.49

9.58

S	Bd. WALK	4.2	5.4
S	sand	4.9	4.7

0+56

S	3' cent. wk	3.77	5.81
N	Bd "	3.7	5.9

0+80 W.L. strand Way

N	Bd wk	3.4	6.2
S		3.4	6.2

E.L. Strand = 0+00

S		3.5	6.1
N		3.4	6.2

0+13

N	W edge Cent wk	4.04	5.54
S		4.0	5.6

0+20

N		4.5	5.1
N	E edge Cent. wk	4.51	5.07

0+50

N	Bd wk	6.4	3.2
S	" "	6.4	3.2

9.58

0+75

S	Bd. wk	8.0	1.6
N		7.9	1.7

0+98.17 W.L. M. Blvd.

N	Bd wk	9.3	0.3
S	" "	9.5	0.1

W c6 M. Blvd

S	S c6	9.38	0.20
S	90'	10.0	-0.4
N	"	10.0	-0.4
N	c6	9.42	0.16

T.P. 3.07 3.26 9.09 0.19

E c6 M. Blvd.

N	c6	3.63	-0.37
N	90'	3.96	-0.70
S	"	3.96	-0.70
S	c6	3.61	-0.35

3.26

E & M Blvd 0+00

S	Bd wk	3.5	-0.2
N	" "	3.6	-0.3

0+53

N	Bd wk	4.0	-0.7
S	3' Cem. "	3.95	-0.69

0+60

S	3' Cem. wk	4.00	-0.74
N	Bd "	4.1	-0.8

0+81

N	3' Cem. wk	4.26	-1.00
S	Bd "	4.1	-0.8

0+95

S	Bd. wk	4.3	-1.0
N	3' Cem. "	4.28	-1.02

1+28 = W Bayside Lane

N	Bd. wk	4.3	-1.0
S	" "	4.3	-1.0

0+00 E.L. Bayside Lane

S	Sand	4.5	-1.2
N	"	4.4	-1.3

3,2 4

0 + 15

N - sand 4.7 -1.4

S 35 Cem wk 4.2 -0.98

0 + 45

S sand 4.4 -1.1

N " 4.4 -1.1

W.L. B.S. walk

N Bd wk 4.3 -1.0

S " " 4.22 -1.06

Indexed C.S.K. Plotted SRS 21

Xsec Toulon CT

S.W.B.P. 2.62 9.75 7.13 Rafael Seaway

0-12 = W E. edge Ocean F. wk.

N cent. 5.13 4.62

S " 5.10 4.65

0+00 = E.L. O.F. wk.

S sand 4.8 5.0

N " 5.0 4.8

0 + 35

N sand 4.3 5.5

S " 4.0 5.8

0 + 53

S 3.8 6.0

N 3.8 6.0

0+80 = W.L. Strand W/ay

N sand 4.1 5.7

S " 4.0 5.8

0+00 = E.L. Strand Way.

S Bd wk 3,9 5.9

N " " 3.8 6.0

9.75

	0+15		
N	Bd wk	4.6	5.2
S	3' Cem. "	4.68	5.12
	0+50		
S	Bd. wk	6.8	3.0
N	" "	6.8	3.0
	0+92,37 = wk M. Blvd		
N	Bd wk	9.6	0.2
S	" "	9.55	0.20
	W cb		
S	cb	9.40	+0.15
S	gut	10.7	-0.42
N	"	10.18	-0.43
N	cb	9.59	+0.16
T.P.	3.61 3.30	10.06	-0.31
	E. cb		
S	cb	3.61	-0.31
S	gut	4.01	-0.71

3.30

N	cb	3.60	-0.30
N	gut	3.99	-0.69
	EL. M. Blvd = 00		
N	Bd. wk.	3.5	-0.2
S	" "	3.5	-0.2
	0+47		
S	Bd. wk	4.0	-0.7
N	W. edge Cem. yd.	3.82	-0.52
	0+67		
N	E edge " "	3.92	-0.62
V	Bd wk	4.2	-0.9
	1+00		
S	Bd wk	4.3	-1.0
N	" "	4.3	-1.0
	1+27		
N	Bd. wk	4.5	-1.2
S	3' Cem. "	4.41	-1.11
	1+42		
S	3.5 Cem. wk	4.33	-1.03
N	Bd "	4.4	-1.1

3.30

1+47.51 W. Bayside Lane

N	Bd. wk.	4.6	-1.3	
S		4.4	-1.1.	
	0+00 E.L. B.S. Lane			
S	Sand	4.6	-1.3	
N	Cent. B.S. Wedge	4.55	-1.25	
	0+24			
N	E edge Cent	4.45	-1.15	
S	Sand	4.5	-1.2	
	0+40			
S		4.3	-1.0	
N	3' Cent. wk	4.35	-1.05	
	0+60			
N	Sand	4.4	-1.1	
S	"	4.1	-0.8	
	W.L. B.S. wk.			
S	Sand	4.4	-1.1	
N		4.4	-1.1	
Check to Vanatta Bd wk. and B.S. Lane		4.36	-1.06	-1.06
T.P. Tangiers B.S. Lane		4.20	-0.90	

Indexed C.S.R.

X 500

Tangiers Ct.

Plotted

23

Seawall Retard

B.M.	2.30	9.43		7.13
T.P. —	5.90	10.59	4.74	4.69
0 -1.2 W	E edge O.F. wk.			
N	cent. wk.		5.90	4.69
S	" "		5.91	4.68
	0+00 E W.L. O.F. wk.			
S	Sand		6.4	4.0
N	"		6.0	4.6
	0+27			
N	Sand		5.9	4.7
S			6.2	4.4
	0+40			
S	Sand		5.0	5.6
N			5.0	5.6
	0+60			
N	Sand		4.1	6.5
S			4.7	5.9
	0+80 W/L Strand way			
S			4.7	5.9
N			4.8	5.8

10.59

0400 Et, Strand Way

N	Bd. wk	4.60	6.0
S	" "	4.55	6.1
	0+12		
S	2' Cem. wk	4.69	5.90
S	Bd "	4.8	5.8
N	" "	4.8	5.8
	0+23		
N	Bd wk	5.1	5.5
S	2' Cem "	5.01	5.58
	0+35		
S	W edge 4" Cem wk	5.80	4.79
	0+39		
S	E edge 4" " "	6.04	4.55
	0+50		
S	Bd wk	6.96	3.63
N	2' Cem "	6.96	3.63
	0+95.14 - w/ NB.		
N	Bd wk	10.4	0.0
S	" "	10.4	0.0

10.59

W c6 N. Blvd

S	c6	10.43	0.16
S	gut	11.01	-0.42
N	"	11.00	-0.41
N	c6	10.42	0.17

E c6 N.B

N	c6	10.90	-0.31
N	gut	11.23	-0.64
S	"	11.22	-0.63
S	c6	10.88	-0.29
	00-2.5		
S	Bd wk	11.0	-0.4
C	Cem "	10.80	-0.21
N	" "	10.80	-0.21
	0+00 Et N. Blvd.		
N	Bd. wk.	11.0	-0.4
S	" "	11.0	-0.4
T.P.	3.99	3.57	11.01	-0.42

	0+37		
S	Bd. wk	4.1	-0.5
N	6' Cem. "	4.11	-0.54
	0+65		
N	Bd. wk.	4.2	-0.6
S		4.1	-0.5
	1+00		
S	Bd. wk.	4.3	-0.7
N	" "	4.3	-0.7
	1+35		
N	Bd wk	4.4	-0.8
S		4.5	-0.9
	1+67.14	= W.L B.S. Land	
S	Bd wk	4.46	-0.91 -0.90
N	" "	4.6	-1.0
	0+00 E.L B.S. Land		
N	W. edge Cem. yd.	4.47	-0.90
S	Sand	4.4	-1.0
	0+21		
S	Sand	4.5	-0.9

N	Edge cem. yd	4.30	-0.73
	0+70		
N	Sand	4.1	-0.5
S	"	4.2	-0.6
	W.L Bayside wall		
S	Sand	3.9	-0.3
N	"	3.9	-0.3

Indexed C.S.K. 9.42 Platted CAB

Xsec Sunset Ct.

T.P.	4.78	9.42		4.64	Seawall Tangent
	0-12 E edgewalk O. Front				
N	Cem.		4.65	4.77	
S	"		4.65	4.77	
	0+00 ± E.L. O. F. walk				
S	Sand		4.7	4.7	
N	"		4.7	4.7	
	0+25				
N	Sand		4.3	5.1	
S	"		4.2	5.2	
	0+50				
S	Bd wk		3.5	5.9	
N	" "		3.4	6.0	
	0+57				
N	2' Cem wk		3.46	5.96	
S	4.5 Slate "		3.53	5.89	
	0+70				
S	4.5 Slate "		3.54	5.88	

	0+80 ± W.L. Str. Way			
S	Bd wk	3.5	5.9	
N	" "	3.4	6.0	
	0+00 E.L. Strand Way			
N	Bd. wk.	3.6	5.8	
S		3.4	6.0	
	0+10			
S	Bd. wk	3.8	5.6	
N	3' Cem. wk	3.77	5.65	
	0+23			
N	2' Cem. wk	4.35	5.07	
S	Bd "	4.4	5.0	
	0+50			
S	Bd wk	5.9	3.5	
N	" "	5.8	3.6	
N	3' Cem. "	5.60	3.82	could be Lowered
	0+59			
S	Bd wk	6.4	3.0	
N	" "	6.3	3.1	
N	Top of Lower Cem. Step	5.77	3.65	

9.42

0+80

N	2' Cem. wk	7.63	1.79
S	Bd "	7.6	1.8
	1+06.33 wk. N. Blvd.		
N	Cem sdw.	9.13	0.29
S	sand	9.2	0.2
	W edge sdw		
S	cem.	9.14	0.28
N	"	9.12	0.30
	0-2.5		
N	E. edge sdw.	9.70	-0.28
S	" " "	9.72	-0.30
	0+00 E.L. N. Blvd.		
S	Bd. wk.	9.9	-0.5
N	" "	9.9	-0.5
T.P.	3.84	3.56	9.70	-0.28

3.56

0+50

N	Bd wk	4.0	-0.4
S	" "	4.0	-0.4
	1+00		
S	Bd wk	3.9	-0.3
N	" "	3.9	-0.3
	1+40		
N	Bd. wk.	4.2	-0.6
S	" "	4.1	-0.5
	1+73.84 wk S.S. Lane		
S	Bd wk	4.1	-0.5
N	" "	4.1	-0.5
	0+00 E.L. S. Lane		
N	Bd. wk.	4.1	-0.5
S	" "	4.1	-0.5
	0+40		
S+N	Bd. wk.	3.9	-0.3
	W.L. Bayside wk		
S+N	Bd wk	3.45	-0.09
check to T.P.		4.45	-0.89	P 23
T.P.		4.28	-0.72	Seagirt

Xsec of Seagirt Ct.

SW.BP.	1.79	8.87	7.08	Seawall San Jose
	0+12 E edge cem sdw O.F. wk.			
N	cem	4.15	4.72	
S		4.11	4.76	
	0+00 E W.L.			
S	Sand	5.1	3.8	
N	"	4.4	4.5	
	0+15			
N	Sand	4.5	4.4	
S	"	5.6	3.3	
	0+23			
N	Bd wk	3.5	5.4	
S	" "	3.8	5.1	
S	Sand	4.8	4.1	
	0+40			
S	Sand	4.2	4.7	
S	Bd. wk	3.4	5.5	
N	4' Cem. "	3.31	5.56	

Indexed C.S.K. 8.87 Plotted OFS 23

	0+51		
N	3' Cem. wk.	3.12	5.75
S	Bd "	3.4	5.5
	0+67		
S	Bd "	3.1	5.8
N	3' Cem. wk.	2.90	5.97
	0+80 W.L. Stroadway		
N	Bd "	2.7	6.2
S		2.8	6.1
	0+00 E.L. Str. Way		
S	Sand	3.0	5.9
N	"	2.9	6.0
	0+23		
N	Bd wk	3.7	5.2
S	2' Cem. "	3.74	5.13
	0+50		
S	Bd wk	4.7	4.2
N		4.8	4.1
	0+65		
N	Bd. wk.	4.4	2.5
S	" "	62	2.7

8.87

0+91

S	Bd wk	7.1	1.8
N		7.1	1.8
+1 E 2.8	door fl. el.	7.00	1.87

1+20

N	Cem. sdwk.	8.60	0.27
C	" "	8.57	0.30
S	Bd "	8.5	0.4

1+25.85 = W.L. N. Blvd.

S	Bd. walk	8.6	0.3
C	Cem "	8.60	0.27
N	" "	8.58	0.29

+25 w edge cem sdwk

N	Cem.	8.60	0.27
S	"	8.63	0.24

T.P.	3.72	3.37	9.22	−0.35

0+00 − 2.5

S	cem. sdwk.	3.71	−0.34
N	" "	3.72	−0.35

3.37

0+00 = E.L. N. Blvd.

N	Bd. wk.	3.8	−0.4
S	" "	3.8	−0.4

0+50

S	Bd "	4.0	−0.6
N	" "	4.0	−0.6

1+00

N	Bd. "	4.1	−0.7
S	" "	4.1	−0.7

1+40

S	Bd. wk	4.2	−0.8
N	" "	4.2	−0.8

1+76.48 W.L. B.S. Lane

N	Bd. wk.	4.13	−0.76	Bum −0.77 T.P.
S	" "	4.2	−0.8	

0+00 E.L. B.S. Lane

S	sand	4.7	−1.3
N	"	4.6	−1.2

W.L. Bayside wk.

N	Sand	3.6	−0.2
S	"	3.8	−0.4

X Sec Queenstown
N. Blvd. to Bayside walk

Stake	4.86	4.51	−0.35	Bayside walk
0+00 = E.L. N. Blvd.				
N	Conc. walk	4.69	−0.18	
S	" "	4.69	−0.18	
0+50				
S	Bd walk	4.9	−0.4	
N	" "	5.0	−0.5	
0+70				
N	6' Conc. wk	4.97	−0.46	
S		4.9	−0.4	
1+00				
S	Bd wk	5.1	−0.6	
N	" "	5.1	−0.6	
1+43				
N	4' Conc wk	4.98	−0.47	
S	Bd wk	5.1	−0.6	
1+67				
S	Bd wk.	5.2	−1.7	
N	5' Conc. wk	5.22	−0.71	

Indexed C.S.K.

4.51 Plotted DB3

2+00			
N		5.0	−0.5
S		5.0	−0.5
2+29.7	W.L. B.S. Lane		
S	Bd. wk.	5.0	−0.5
N	" "	5.1	−0.6
0+00	E.L. B.S. Lane		
N	Bd wk	4.9	−0.4
S		5.0	−0.5
0+40			
S	Bd. wk.	4.7	−0.2
N	" "	4.7	−0.2
	W.L. Bayside walk		
N	Bd. wk.	4.3	+0.2
S	" "	4.4	+0.1

Bd. wk. bad condition

Xsec P,S170 Ct, M. Blvd. to Bayside Walk

Stake	4.86	4,51		−0,35	Bayside walk
T.P.	3.46	4,41	3.56	0.95	
	0+00 = E.L. M. Blvd				
N	Conc. wk.		4.64	−0.23	
+8 S	" "		4,64	−0.23	
S	" "		4,64	−0.23	
	0+25 E. end of conc. wk.				South side P,S170
S	Conc. wk.		4.71	−0.30	
+ N	" "		4,71	−0.31	
" N	Bd "		4.71	−0.31	
N	" "		4.7	−0.3	
	0+50				
N	Bd. "		4.6	−0.2	
S	" "		4.7	−0,3	
	1+00				
S	Bd "		4.5	−0.1	
N	" "		4.5	−0.1	

Indexed C.S.K. 4,41 Platted EPD

	1+50		
N		4.5	−0.1
S		4.4	−0.2
	1+72		
S	beg. of 5' wide slab rock wk.	4.47	−0.26
N	"	4.47	−0.26
	2+05 end slab rock walk		
N		4.9	−0.5
S		4.9	−0.5
	2+38.44 W.L. B.S. Lane		
S	grd.	5.2	−0.8
N	"	5.2	−0.8
	0+00 E.L. Bayside Lane		
N	Bd walk.	4.9	−0.5
S	" "	4.9	−0.5
	0+13		
S-1	Porch Fl. El.	5,04	−0.63
S	Bd walk	4,99	−0.58
N	" "	5.0	−0.6

4+21

0+21				
N	Bd WK		4.9	-0.5
S	" "		5.0	-0.6
+1	fl. el. Po-cth		5.07	-0.66
0+50				
S			4.4	0.0
N			4.4	0.0
W.L. 0.S. WK.				
N	Bd WK		3.3	0.6
S	" "		3.7	0.7
				p 30
check to Q. ct.	1+47		5.19	-0.70 -0.71

Indexed C.S.K.

Platted DFS

32

X sec Liverpool Ct.

M. Blvd. to Bayside WK.

S.W.S.P.	2.40	9.38		6.98
T.P.	1.61	2.79	8.20	1.18

San Luis Obispo pl. Seawall

0 - 2.5 = E. edge cem. sdw.

S	cent.	1.63	1.16
N		1.60	1.19
0+00 = E.L. M. Blvd.			
N	Bd. WK.	1.8	1.0
S	" "	1.8	1.0
0+15			
S	3' Cem. WK	2.06	0.73
N	Bd. "	2.2	0.6
0+51			
N	3' Cem. WK	2.98	-0.19
S	Bd "	2.9	-0.1
0+89			
S	Bd WK	3.6	-0.8
N	3' Cem. "	3.41	-0.82

1+04

N	Bd. wk.	3.9	-1.1
S	2' Cem. "	3.80	-1.01

1+20

S	3' Cem. "	4.09	-1.30
N	Bd "	4.0	-1.2

1+24.50 W.L. Bayside Lane

N	Bd "	4.2	-1.4
S	" "	4.1	-1.3

0+00 E.L. B.S. Lane

S	" "	4.3	-1.5
N	" "	4.1	-1.3

0+40

N	Bd. wk	4.0	-1.2
S	" "	4.0	-1.2

W.L Bayside Wk.

S	Bd. wk	3.4	-0.6
N	" "	3.4	-0.6

Indexed C.S.K. Platted 1903

Xsec Lido Ct.

S.W.B.P.	1.16	8.14		6.98 San Loren Obispo Pl. Sea Wall

0+12 E. edge Cem. wk

S	Cem.	3.56	4.58
N	"	3.53	4.61

0+00 wk O.E. wk.

N	sand	4.8	3.3
S	"	3.8	4.3

0+29

S	2' Cem wk.	3.23	4.91
S	sand	4.0	4.1
N	"	4.3	3.8

0+55

N	sand	2.9	5.2
S	"	3.1	5.0

0+80 wk St. way

S	sand	3.0	5.1
N	"	3.0	5.1

8.14

0+00 E.L. 5th Ave

N	Sand	3.1	5.0
S	"	3.1	5.0
	0+31		
S	Bd. wk	5.2	2.9
N	Wedge 2' Cem. Wk	5.23	2.91
	0+33		
N	E edge 2' " "	5.44	2.68
S	Bd "	5.4	2.7
	0+48		
S	" "	6.5	1.6
N	Wedge 2' Cem	6.60	1.54
	0+50		
N	E edge 2' " "	6.73	1.41
	0+60.77 W.L. M. Blvd.		
N	Bd wk	7.5	0.6
S	" "	7.6	0.5
	+2.5 = Wedge Cem walk		
S	Cem. Sdwk	7.59	0.55
N	" "	7.52	0.62

8.14

0 – 2.5

N	Cem. wk	7.97	0.17
S	" "	8.02	0.12
	0+00 EL M. Blvd.		
S	Bd wk	8.0	0.1
N	" "	8.0	0.1
	0+41		
N	E 6' Cem wk	8.70	-0.56
S	Bd "	8.7	-0.6
	0+90		
S	Bd wk	9.2	-1.1
N	" "	9.3	-1.2
	1+26		
S	3' Cem. wk.	9.48	-1.34
	1+32.53 W.L B.S. Lane		
S	Bd wk	9.5	-1.4
N	" "	9.6	-1.5
	0+00 EL. B.S. Lane		
N	Bd. wk	9.6	-1.5
S	" "	9.6	-1.5

8.14

0+40

S	Bd. mk	9.3	-1.2
N	" "	9.3	-1.2
	W.L. Bayside walk		
N	Bd mk	8.6	-0.5
S	" "	8.6	-0.5

Indexed C.S.K.

Platted EBB

35

Xsec KINGSTOWN CT.
6' Cem. sdw. & rods

SWBP 2.24	9.42		6.98
0-12 E		4.89	4.53
OD = EL OD. F. mk		4.65	4.77
0+40		3.86	5.56
0+80 W.L. Str. way		3.14	6.28
0+00 E.L. " "		3.27	6.15
0+40		5.96	3.46
0+60		7.80	2.12
0+80		8.61	0.81
1+00		9.27	0.15
1+29.41 W.L. Mt Blvd		10.19	-0.77
W CB		10.33	-0.91
W CUT		10.77	-1.35
E CB		10.77	-1.35
E CUT		11.13	-1.71
0+00 E.L. Mt. Blvd.		10.63	-1.21
0+50		10.58	-1.16
1+00		10.64	-1.22

San Luis Obispo A. Seaman

9.42

1+50		10.65	-1.23
1+60.01	WL B.S. Lane	10.72	-1.30
0+0	E.L. " "	10.72	-1.30
0+40		10.58	-1.11
	WL B.S. W.K.	10.22	-0.80

Indexed
C.S.K.

Platted

36

Xsec Kennebeck Ct.

6' cem. sdw Σ levels

SMBP	249	9.47	6.98	SAINT LOUIS OBISPO PK. SEAWALL
0-12		4.90	4.57	
0+00	E.L. O.F. WK	4.70	4.77	
0+40		3.79	5.68	
0+80	W.L. Str. W'y.	3.04	6.43	
0+00	E.L. " "	3.03	6.44	
0+50		6.35	3.12	
0+90		8.67	0.80	
1+00		9.10	0.37	
1+10		9.34	0.13	
1+50		9.83	-0.36	
1+76.78		10.25	-0.78	
W CB		10.23	-0.76	
W gut		10.65	-1.18	
E CB		10.62	-1.15	
E gut		10.90	-1.43	
0+00	E.L. M.B. W.L.	10.41	-0.94	

9.47

0+50	10.39	-0.92
1	10.47	-1.00
+50	10.54	-1.07
1+85.9 = W.L. B.S Lane	10.58	-1.11
00 EL " "	10.60	-1.13
+20	10.20	-0.73
W.L. " WK.	9.94	-0.47

Indexed
C.S.K.

Plotted Feb 3

37

X sec Jersey CT.

6.3 Cent. Sdw. & levels

Santa Barbara Pl. Seawall

SW.BP.	3.89	10.92		7.03
0-12			6.41	4.51
0+00 EL O.F. WALK			6.18	4.74
+40			5.15	5.77
0+80 W.L Str. W/y.			4.28	6.64
0+00 E.L. " "			4.24	6.68
0+30			5.55	5.37
0+50			6.64	4.28
0+70			7.94	2.98
0+90			9.25	1.67
1			9.77	1.15
+10			10.29	0.63
+30			10.77	0.15
+50			11.04	-0.12
✓			11.34	-0.42
2+26.43 W.L. FT.B.			11.52	-0.60
W.C.B			11.44	-0.52
W 9WT			11.64	-0.72

	10.92			
E 6		11.77	-0.85	
E 9UT		12.09	-1.17	
0+00 EL. 11.8/Vcl.		11.60	-0.68	
50		11.56	-0.64	
1 School		11.62	-0.70	
+50		11.74	-0.82	
"		11.75	-0.83	
" +25.23 = WL B.S. Lane		11.77	-0.85	
00 EL " "		11.92	-1.00	
0+50		11.43	-0.51	
WL " walk		11.37	-0.45	

Indexed C.S.K.

Plotted ✓ L2

Proc Jamaica Cr.
6' Cont. conc. ⊆ levels

Sw 8P	2.35	9.38	7.03	Santa Barbara Pl. Seawall
0-1		4.89	4.49	
0+00	Ft. C.F. wtr.	4.70	4.62	
+10		4.70	4.68	
+18	Settled	4.38	5.00	
+25	"	3.81	5.57	
+37		3.44	5.94	
+49		3.10	6.28	
+50 WL St. wy		2.21	7.17	
00	EL " "	2.18	7.20	
+50		5.05	4.33	
1		7.98	1.40	
+25		9.01	0.37	
+35		9.34	0.04	
+50		9.71	-0.33	
+60		9.80	-0.42	
"		9.78	-0.40	
+50		9.80	-0.42	

Indexed C.S.K.

Platted

9.38

		9.7+	-0.34	
+07.78	W.L. 11th Blvd	9.7+	-0.34	
T.P.	4.31	3.97	9.7+	-0.34
W 06		4.14	-0.17	
W 00		4.64	-0.67	
E 06		4.6+	-0.65	
E 00		4.95	-0.98	
0+0	E.L. M. Blvd.	4.37	-0.40	
+50		4.5+	-0.55	
		4.5+	-0.58	
+50		4.56	-0.59	
		4.6+	-0.68	
+50		4.7+	-0.78	
		4.8+	-0.85	
+38.81	W.L. B.S. Lane	4.9+	-0.95	
0+00	E.L. " "	4.90	-0.93	
+50		4.60	-0.63	
W.L. B.S. Wk.		4.33	-0.36	

Xsec / Status C.L. & levels

4' Conc. Sdwk.

Ventura Pl. Seawall

Swk.	1.98	9.49	7.51	
0+1+		4.88	4.61	
00 = E.L. O.F. Wk		4.60	4.89	
+40		3.29	6.20	
+80 W.L. 5th Way		2.06	7.43	
0+0 E.L. " "		2.0+	7.47	
+65		5.74	3.75	
+80		7.0+	2.47	
		8.87	0.62	
+20		10.1+	-0.65	
+40		10.95	-1.46	
+60		11.2+	-1.73	
		11.19	-1.70	
+50		10.75	-1.26	
T.P.	5.09	3.83	10.75	-1.26
3			4.83	-1.00
+37.07	W.L. 7th Blvd.		4.66	-0.83

W. 06		4.55	-0.72	
W 90 ft		5.03	-1.20	
E 06		5.01	-1.18	
E 90 ft.		5.30	-1.47	
0+00 - E.L.M.H.W.L.		4.83	-1.00	
+50		4.81	-0.98	
		4.80	-0.97	
+50		4.86	-1.03	
		4.90	-1.07	
+50		4.98	-1.15	
		5.05	-1.22	
+50		5.08	-1.25	
+86 end sdw.		5.17	-1.34	Short
+88.24	W.L. B.S. Lake S.V.		-1.4	ground
0+00	E.L. " "	5.15	-1.32	
+41		4.87	-0.99	
	W.L. " Walk	4.69	-0.86	

Indexed
C.S.K.

Plotted 9-52

40

Xsec / Island Ct.

6' Cent. sdw. 2 Levels

SW BP	3.19	10.70	7.51	Ventura Pl. Seawall
0-12		6.24	4.46	
0+0 E.L. Oc. F. WK.		5.92	4.78	
+40		4.80	5.90	
+80 W.L. St. Way		3.83	6.87	
00 E.L. " "		3.86	6.84	
+50		5.97	4.73	
		8.14	2.56	
+50		10.24	0.46	
		11.69	-0.99	
+40		12.45	-1.75	
+60		12.63	-1.93	
		12.50	-1.80	
T.P.	5.07	3.26	12.57	-1.81
3+50			4.57	-1.31

3.26

3	+59.5 W.L.M. B/W.	4.48	-1.22	
	W c6	4.48	-1.22	
	in/ gut	4.95	-1.69	
	E c6	4.92	-1.66	
	E gut	5.17	-1.91	
00	E.L.M. B/W.	4.77	-1.51	
	+50	4.78	-1.52	
1		4.75	-1.49	
	+50	4.81	-1.55	
2		4.82	-1.57	
	+50	4.90	-1.64	
3		4.92	-1.66	
3	+55.5 W.L.B.S. tone	4.97	-1.71	To N.
	00 E.L. " "	5.08	-1.82	To S
	+40	4.76	-1.50	
	+82 end old cem. wk	4.55	-1.29	W.L.
1	+12 New walk	4.39	-1.13	

Bayside Walk
added by W.P.A.

Block 41 Stetson's Add.

Sewer El. E alley N of Florence and W of 38th.

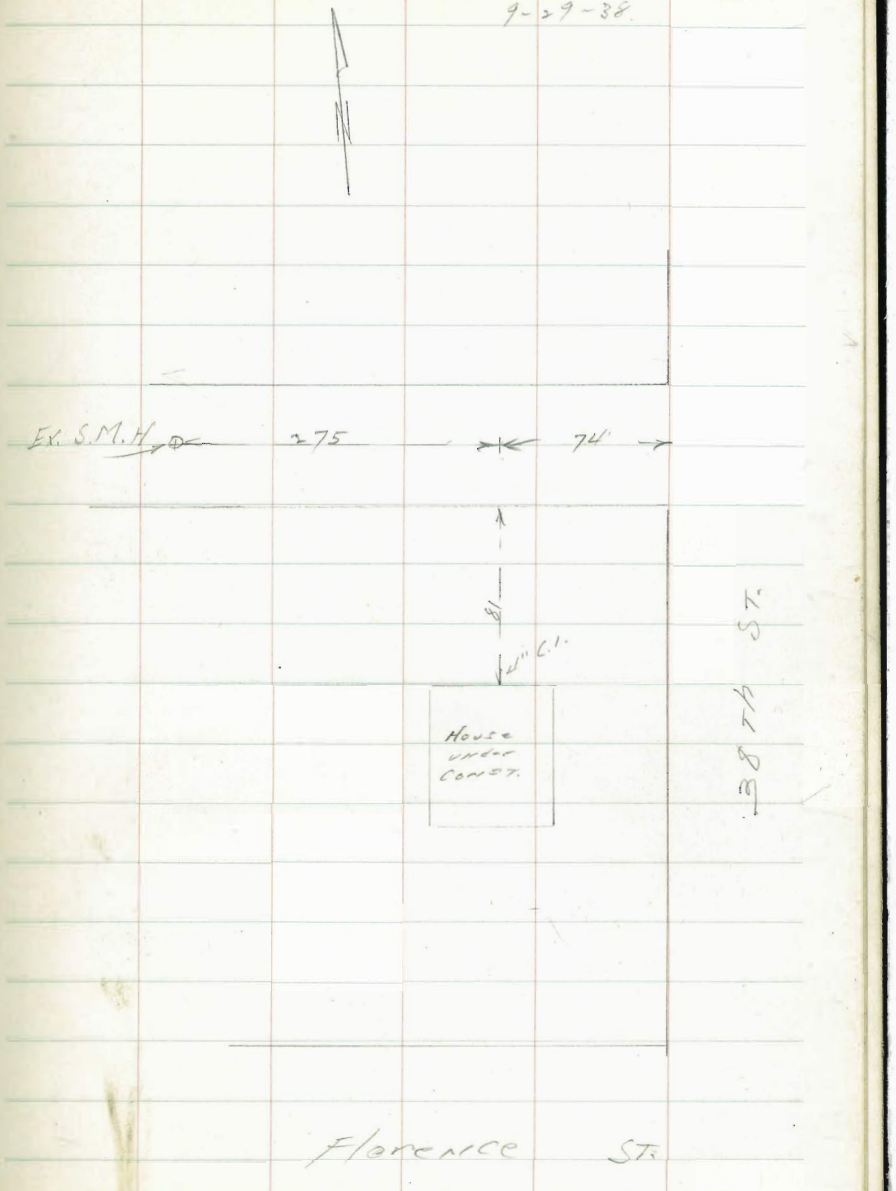
S.E.B.P.	11.95	88.53		76.58	38th Natl.
T.P.	5.35	93.80	0.08	88.45	
74' W of W.L. 38th E alley			8.12	85.68	Top pipe
" " " " "			2.7		ground
91' S of above at rear of House			8.73		Top 4" C.I.
349' W of W.L. 38th E alley			8.60		Rim M.H.
" " " "			15.74		F.L. "

at 75' W of W.L. 38th & E alley about 1.5 cut has been made in grading the alley. apparently this was done by private contract.

Indexed
C.S.K.

Moore
Sisson
9-29-38

42



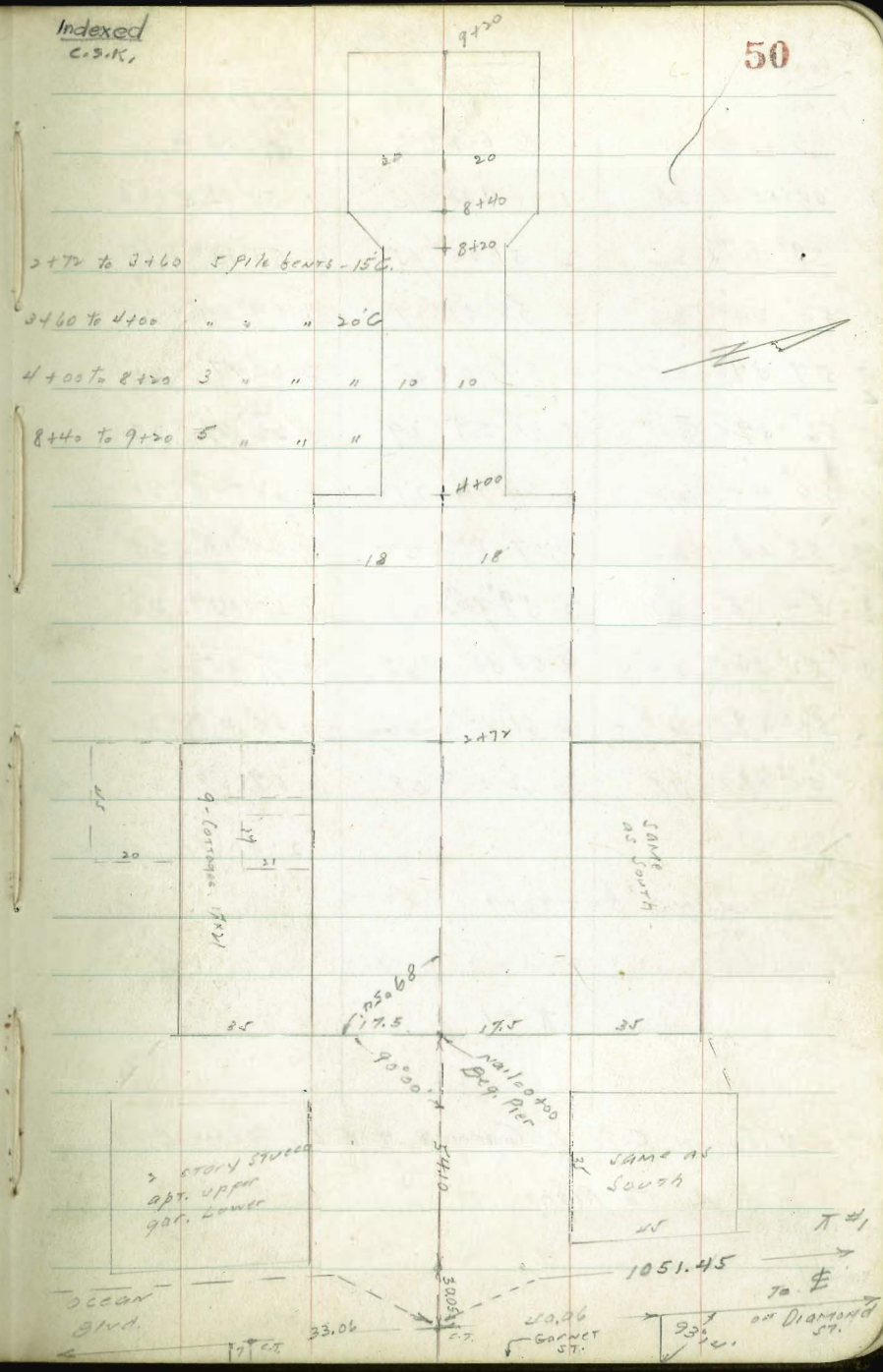
Soundings for proposed Ext. of Crystal Pier Garnet and Ocean Blvd.

Moore 4-20-38

Indexed C.S.K.

B.P. N.E. Garnet Ocean Blvd.	4.90	30.06		16.15 = 4.74 9.01 25.16 = U.S.C. & G.	
0+00	Pier Floor	Beg. Pier	4.73	25.33	
3+80	"	"	4.67	25.38	
3+90	"	"	4.28	25.78	
4+00	"	"	3.95	26.11	
9+20	"	" end	" 4.58	25.48	
"	El. water		27.6	2.5	10:20 A.M. 4-20-38.
"	"	Sand bottom	37.5	-7.4	

To C.T. on N 7° line of Grand Ave. on E.L. Ocean Blvd. — 664.20 — π #2



Crystal Pier Soundings

Moore Gibson Northern 4-21-38

Return 1:40 P.M.

	S. of ℄	Sdg.
①	60° 15'✓	28'
②	59° 57'✓	26'
③	58° 28'✓	26'
④	57° 39'✓	25'
⑤	56° 39'✓	24'
⑥	56° 11'✓	22'
⑦	55° 08'✓	22'
⑧	54° 05'✓	21'
⑨	52° 36'✓	20'
⑩	51° 29'✓	20'
⑪	50° 38'✓	19'

Sand Bottom

π #1 1:30 P.M.

	℄ beg. OUT	Sdg.
①	49°08'✓	13'
②	51°00'✓	15'
③	52° 51'✓	17'
④	54° 00'✓	18'
⑤	54° 59'✓	19'
⑥	56° 23'	21'✓
⑦	57° 55'✓	22
⑧	59° 10'✓	23'
⑨	60° 38'✓	25'
⑩	61° 14'✓	26'
⑪	62° 00'✓	28'

π #1

1:51 P.M.

	N. of ℄ OUT	Sdg.
①	55° 13'✓	16'
②	57° 38'✓	17'
③	59° 09'✓	19'
④	60° 47'✓	21'
⑤	62° 15'✓	22'
⑥	62° 46'✓	24'
⑦	64° 18'✓	25'
⑧	65° 43'✓	26'
⑨	67° 05'✓	27'
⑩	68° 29'✓	28'
⑪	69° 29'	28'

2:00 P.M. ended

F.S. on C.T. & Garnet & E.L. Ocean Blvd.

△ to Right

Miller Walker & Ss

π #2

	Return S of ℄	℄ beg. OUT	N of ℄ OUT
1	69°28'✓	58°12'✓?	55°30'✓
2	68°57'✓	58°03'✓	56°42'✓
3	68°29'✓	58°33'✓	57°40'✓
4	67°54'✓	60°09'✓	58°16'✓
5	67°59'?✓	61°38'✓	58°57'✓
6	67°09'✓	62°28'✓	60°04'✓
7	66°56'✓	63°12'✓	61°12'✓
8	66°56'✓?	63°50'✓	62°20'✓
9	66°06'✓	64°34'✓	63°09'✓
10	66°05'✓	66°20'✓	64°37'✓
11	64°27'✓	67°32'✓	65°53'

π #2

F.S. on C.T. & Garnet & E.L. Ocean Blvd.

△ to Left.

Indexed
c-sik.

X sec of 10' Path
Bet. Elev. Rd. and Buenos

Moore
6-25-38.

	1.68	107.58		105.90	
27.5 SEly from P.R.C.		T.P. End Curb	1.18	106.40	
43.5 " " "		Top Cb	0.47	107.11	Break
	0-10				
S	Top Iron Pin set for Cb. Const.		2.16	105.42	
C			2.1	105.5	
N			2.0	105.6	
	0+00 Sly Elev. Rd				
N			5.5	102.1	
C			5.8	101.8	
S			5.4	102.2	
	0+15.				
S			12.8	94.8	
C			13.3	94.3	
N			13.1	94.5	
T.P.	0.74	95.58	12.78	94.84	

95.58

	0+25				
N			5.6	90.0	
C			5.6	90.0	
S			5.4	90.2	
	0+50				
S			8.2	87.4	
C			8.7	86.9	
N			8.6	87.0	
T.P	0.25	82.87	12.96	82.42	
	0+75				
N			2.3	80.6	
C			2.8	80.1	
S			2.4	80.5	
	1+00				
S			8.4	74.5	
C			8.5	74.4	
N			8.2	74.7	
T.P.	0.88	71.05	12.70	70.17	

71.05

	1+25			
S			2.9	68.2
C			3.2	67.9
N			3.3	67.8
+1			3.9	67.2
+5			3.7	67.4
+7	wash		5.3	65.8
+9			3.7	67.4
	1+50			
-5			9.1	62.0
N	wash		9.3	61.8
C			9.2	61.9
S			8.8	62.3
	1+60			
S			10.8	60.3
C			11.1	60.0
+3	wash		12.0	59.1
N	"		11.7	59.4
+4	"		11.9	59.2
T.P.	072	58.87	12.90	58.15

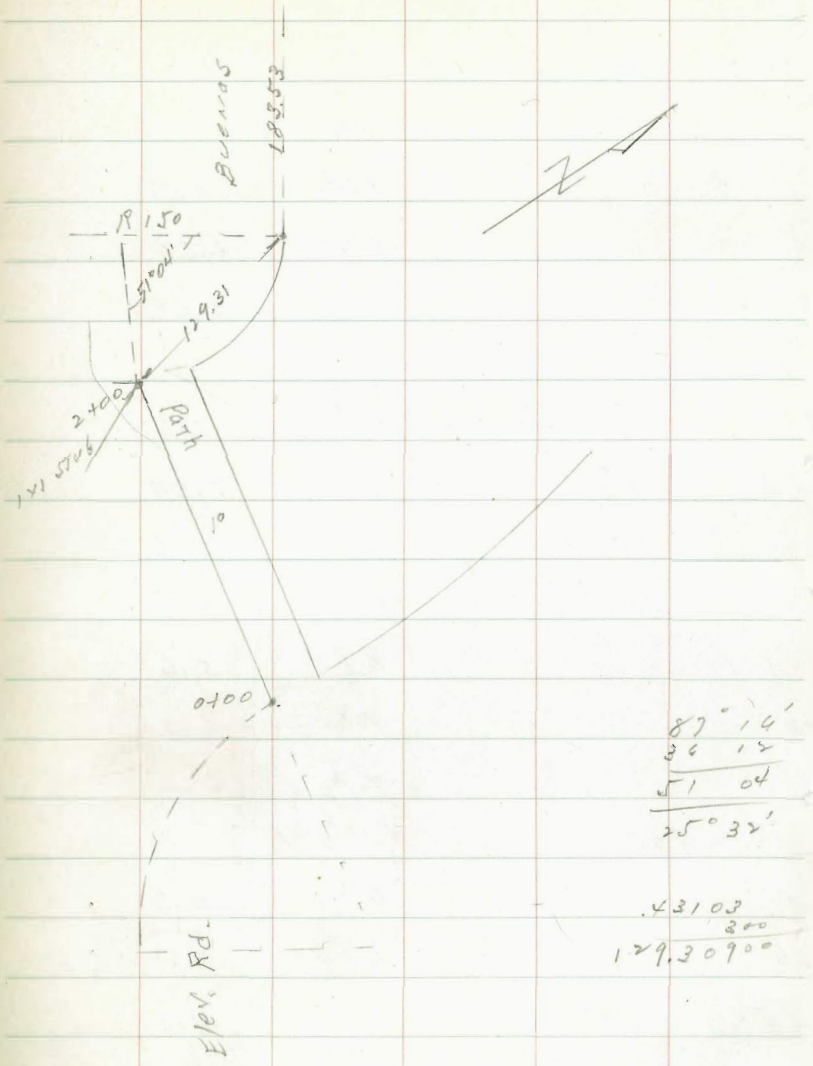
58.87

	1+75		
S		1.6	57.3
C		2.5	56.4
+4		2.5	56.4
N		4.6	54.3
+1		4.6	54.3
+2		3.4	55.5
+5		2.2	56.7
	1+88		
S		5.0	53.9
C		5.0	53.9
+3	wash	7.2	51.7
+N	"	7.6	51.3
+1	"	7.6	51.3
+3		5.3	53.6
	1+95		
S		10.8	48.1
C		10.0	48.9
N		10.0	48.9

58.87

2+00 = Ely Bueno St

N		10.6	48.3
C		10.9	48.0
S	on 1x1 stub	11.25	47.62
	on 2x2 E Hub P.C. 180°	11.12	47.75



87° 14'
36 12
51 04
25° 32'

.43103
200
129.30900

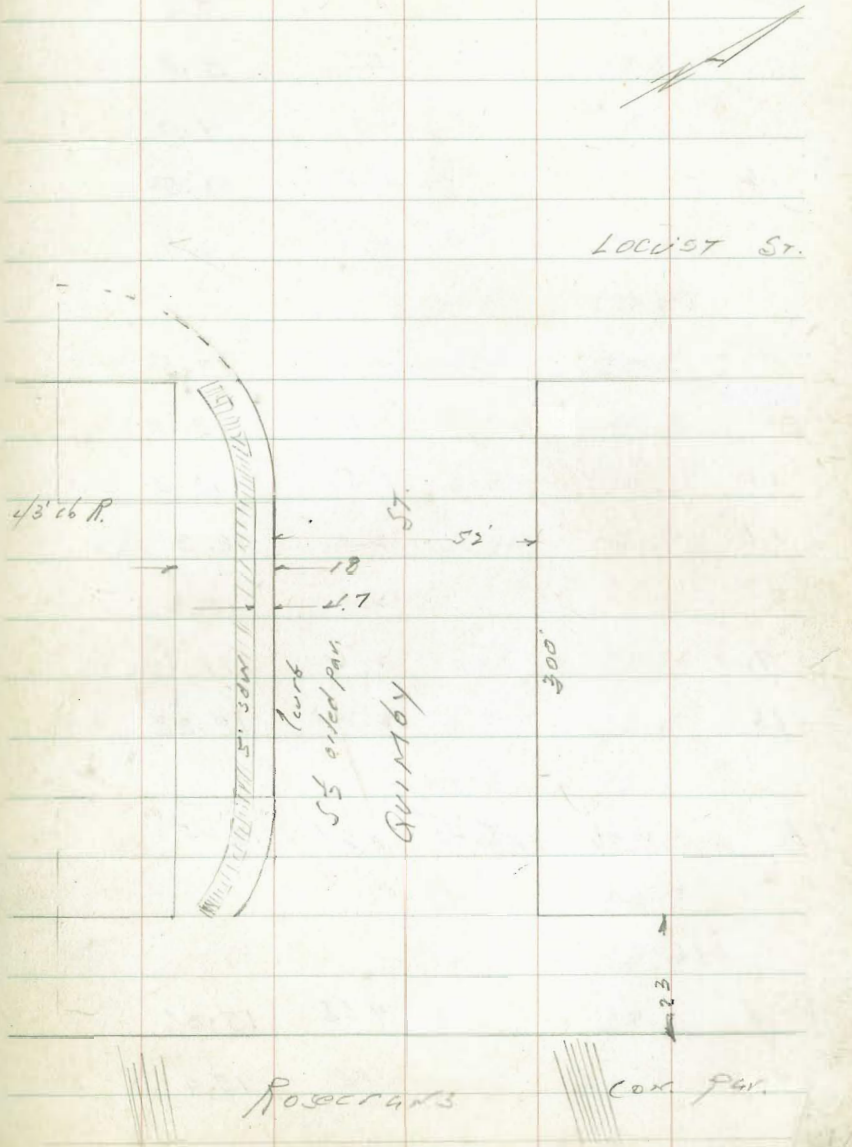
X sec Quimby St. 70' wide 18' curbs
Rosecrans to Evergreen

SW 7'Mon	9.03	14.26	5.23	Russell Rosecrans
0-73 : W edge Conc. Pav.				
N		9.53	4.73	
C		9.60	4.66	
S		9.60	4.66	
0+00 Wly Rosecrans				
S		8.7	5.6	
+8.5 Top cb		8.72	5.54	
cb		8.7	5.6	
C		8.6	5.7	
+15		8.7	5.6	
cb		7.8	6.5	
N		7.9	6.4	
0+75				
N.		6.0	8.3	
cb		6.72	8.1	
+7		7.0	7.3	
C		7.0	7.3	
9W7		7.9	6.4	
cb		7.50	6.76	

Indexed
C.S.K.

Moore Sisson 9-30-36

55



		14.26		
	0450			
S	cb		5.70	8.56
	QUT		6.1	8.2
	C		5.5	8.8
	+1.4		5.3	9.0
	cb		4.8	9.5
	N		4.6	9.7
	1+00			
	N		0.8	13.5
	cb		1.3	13.0
	+4		1.5	12.8
	+6		2.0	12.3
	C		2.1	12.2
	QUT		2.4	11.7
	cb		2.04	12.22
T.P.	11.96	25.41	0.81	13.45
	1450			
S	cb		9.55	15.86
	QUT		10.0	15.4

		25.41		
	C		9.3	16.1
	+12		8.9	16.5
	+14		8.4	17.0
	cb		8.2	17.2
	N		7.3	18.1
	2+00			
	N		3.5	21.9
	cb		4.4	20.8
	+4		5.2	20.2
	C		5.6	19.8
	QUT		6.3	19.1
S	cb		5.90	19.51
	2+50			
S	cb		2.28	23.13
	QUT		3.0	22.4
	C		2.3	23.1
	+12		1.4	23.8
	+14		0.7	24.7
	cb		0.5	24.9
	N		1.7	27.1
T.P.	11.64	36.60	0.45	24.96

34.60

2+75		
N	8.9	27.7
cb	10.1	26.5
+4	10.3	26.3
+6	11.2	25.4
C	11.8	24.8
gut	12.4	24.2
S cb	11.70	24.90
3+00 Ely Locust 70' wide		
S	11.5	25.1
+10.5 End cb	10.80	25.80
cb	10.6	26.0
L	10.0	26.6
+12	9.1	27.5
+14	8.7	27.9
cb	8.5	28.1
N	7.2	29.4
E Locust		
N	4.5	32.1
cb	5.7	30.9
+6	6.0	30.6

36.60

+8	6.6	30.0
C M.H. RIM	6.85	29.75
cb	8.2	28.4
S	9.3	27.3
0+00 Wly Locust		
S	6.2	30.4
cb	5.4	31.2
C	4.4	32.2
+9	3.8	32.8
+10	3.3	33.3
cb	2.9	33.7
N	1.7	34.9
TP 12.10	4809'	0.61 35.99
0+50		
N	8.3	39.8
cb	10.1	38.0
+7	10.6	37.5
+8	11.2	36.9
C	11.9	36.2

48.09

cb	13.1	35.0	
+2	13.0	35.1	
+10	13.5	34.6	
S	14.9	33.2	
1+00			
S	10.6	37.5	
+6	9.7	38.4	
cb	9.3	38.8	
C	8.3	39.8	
+7	7.7	40.4	
+9	7.1	41.0	
cb	6.3	41.8	
N	4.4	43.7	
1+50			
N	0.0	48.1	
cb	1.3	46.8	
+8	2.1	46.0	
+10	2.6	45.5	
C	2.9	45.2	
cb	3.4	44.7	
S	4.5	43.6	

48.09

T.P.	12.68	60.76	0.07	48.09
1+75				
S		11.5		49.2
cb		11.3		49.4
C		11.0		49.7
+7		10.6		50.1
+9		10.0		50.7
cb		9.6		51.1
N		8.6		52.1
2+00				
N		3.7		57.0
cb		4.7		56.0
+8		5.1		55.6
+9		5.6		55.1
C		6.2		54.5
cb		7.1		53.6
S		8.4		52.3
T.P.	12.38	72.40	0.08	60.02

7+40

2+25

S			13.6	58.8
cb			12.7	59.7
C			11.7	60.7
cb			10.0	62.4
N			9.7	63.2

2+50

N			1.5	70.9
cb			3.2	69.2
C			5.1	67.3
cb			6.3	66.1
S			7.6	64.8
T.P	9.9	8+10	0.2	72.16

2+75

S			9.9	72.2
cb			7.8	74.3
C			7.1	75.0
cb			6.3	75.8
N			3.8	78.3

8+10

TP	7.57	88.47	1.00	81.10

3+00 Elk Evergreen

N			1.2	87.47
cb			4.3	84.4
C			5.1	83.6
cb			5.7	83.0
S			6.9	81.77

Indexed C.S.K.

× Sec Poe St. 70' wide 18' c6s

Willow to Clove

SW BP	10.25	188.04	177.79	Willow Poe

00 - 18 W c6 Willow

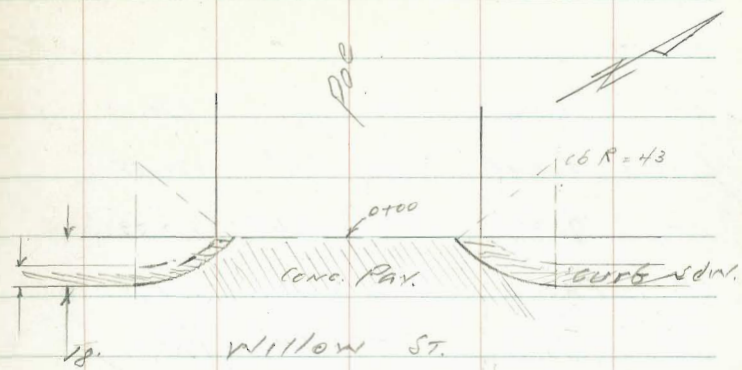
S - 25	P.C. c6	13.18	174.86
"	" gut	13.99	174.05
S	Par	11.20	176.84
c6	"	10.01	178.03
1/4	"	9.69	178.35
C	"	9.47	178.57
1/4	"	9.33	178.71
c6	"	9.25	178.79
N	"	9.44	178.60
+25	gut	10.47	177.57
"	c6 P.C.	9.65	178.39

0 - 10.5

N	Top c6	8.93	179.11
N	gut	9.72	178.32
c6	Par	9.40	178.64
1/4	"	9.47	178.57
C	"	9.54	178.52

Moore 10-4-38

60



188.04

0 - 10.5

S 1/4	Par	9.78	178.26
c6	"	10.13	177.91
S	gut	11.33	176.71
S	Top c6	10.55	177.49

1880 ↓

00 = W ⊥ W, 1/ow

S		10.1	178.03
+ 10.3	Top cb	9.89	177.15
"	gut.	10.65	177.39
cb	par.	10.26	177.78
1/4	"	9.98	178.06
c	"	9.76	178.28
1/c	"	9.67	178.37
cb	"	9.61	178.43
+7.7	gut	9.57	178.47
"	cb	8.86	179.18
N		8.6	179.4
0 + 06			
N'		2.1	185.9
cb		2.2	185.8
+ 2		5.3	182.7
1/4		6.1	181.9
c		4.7	183.3
+4		7.9	180.1
1/4		8.3	179.7

1880 ↓

cb		8.1	179.9
+3		5.2	182.8
S		4.5	183.5
0 + 11			
S		4.6	183.4
+15		4.7	183.3
cb		7.1	180.9
1/4		7.5	180.5
+2		7.0	181.0
+5		4.1	183.9
C		3.9	184.1
1/N		2.8	185.2
cb		2.7	185.3
N		2.3	185.7
0 + 25			
N		3.5	184.5
cb		3.4	184.6
1/4		3.4	184.4
c		4.5	183.5
+5		4.4	181.6

	1880+		
1/2		6.4	181.4
cb		6.5	181.3 5
S		4.8	181.2
	0+50		
S		7.5	180.5
cb		6.9	181.1
1/4		8.4	179.8
c		7.9	180.1
1/4		5.8	182.2
cb		5.4	182.6
N		5.0	183.0
	0+75		
N		6.1	181.9
cb		6.8	181.2
1/2		8.7	179.3
+4		9.7	178.3
c		10.0	178.0
1/4		9.7	178.3
cb		9.8	178.2 8
S		11.0	177.0
+5		11.4	176.8

	1880+		
	1+00		
-10		17.0	171.0
S		15.4	172.8 2
cb		13.0	175.6
1/4		12.7	175.3
c		12.4	175.6
1/4		12.4	175.6
+4		10.7	177.3
cb		10.1	177.9
N		8.8	179.2
	1+25		
N		10.7	177.3
cb		14.1	173.9
+4		14.8	173.2
1/4		15.0	173.0
c		15.3	172.7
1/4		15.4	172.8
cb		16.4	171.8
S		19.4	168.8
+15		21.5	166.5

		188.04		
1+60				
−15			25.3	162.7
S			23.0	165.0
cb			20.4	167.8
1/4			20.0	168.0
c			20.6	167.4
1/4			19.7	168.3
cb			19.5	168.5
+2			19.0	169.0
+7			16.8	171.2
N			15.7	172.3
T.P.	0.87	176.44	1.47	175.57
1+72				
N			5.5	170.9
+10			4.7	169.7
+14			9.3	167.1
cb			9.8	166.6
1/4			10.1	166.3
c			11.5	164.9

		176.44		
1/4			11.3	165.1
cb			11.3	165.1
+7			14.7	161.7
S			17.1	159.3
+20			21.7	154.7
2+00				
−20			27.6	148.8
S			23.9	152.5
+10			21.6	154.8
cb			18.2	158.2
1/4			17.7	158.7
c			17.2	159.2
+6			17.1	159.3
1/4			15.1	161.3
cb			14.1	162.3
+10			14.3	162.1
+14			11.6	164.8
N			10.8	165.6
T.P.	0.44	164.11	1.79	163.45

2+10	1641		
N		1.0	163.1
+5		3.8	160.3
c6		3.7	160.4
1/2		4.0	160.1
+2		6.0	158.1
C		6.8	157.3
1/2		7.1	157.1
c6		8.3	155.8
+8		12.2	151.9
S		14.3	149.8
+20		17.4	146.5
2+18			
-20		21.1	143.0
S		16.5	147.6
+12		14.0	150.1
c6		10.5	153.6
1/2		9.7	154.4
C		9.1	155.0
+5		8.6	155.5
1/2		5.8	158.3

	1641		
c6		5.0	159.1
N		5.1	159.0
2+50			
N		9.2	154.9
c6		11.0	153.1
1/2		13.8	150.3
+2		15.2	148.9
C		16.2	147.7
1/2		17.1	147.0
c6		18.7	145.4
S		23.5	140.6
+20		29.5	134.6
T.P.	0.22	151.21	13.12	150.99
2+70			
-20		24.4	126.6
S		18.2	133.0
+14		15.0	136.2
c6		11.8	139.4

151.21

1/L			11.0	140.2
C			10.2	141.0
+6			8.5	142.7
1/R			6.6	144.6
cb			3.6	147.6
+10			1.8	149.4
N			+ 1.3	152.5
3+00 Ely Clove St. 70' wide				
N			11.8	139.4
T.P.	0.23	139.03	12.41	138.80
cb			2.9	136.1
1/2			4.8	134.2
+3			7.0	132.0
C			7.5	131.5
1/4			9.0	130.0
cb			10.8	128.2
+5			13.4	125.6
S			18.0	121.0
+20			22.7	116.3

139.03

E Clove

-20			31.6	107.4
S			27.6	111.4
+13			24.6	114.4
cb			23.3	115.7
+21			21.8	116.2
1/4			21.2	117.8
C M.H. Pins			20.9	118.1
+6			20.0	119.0
1/4			17.6	121.4
cb			15.3	123.7
N			10.8	128.2
W/y Clove St.				
N			13.6	115.4
cb			28.7	116.3
1/4			29.6	109.4
+21			31.6	107.4
C			33.4	106.6
1/4			32.8	106.2
cb			33.5	105.5
+8			34.1	102.9
S			37.4	101.6
+25			41.3	97.7

139.03
0.23
138.80
12.30
151.10
0.10
151.00
12.95
163.95
0.28
163.67
12.58
176.25
0.30
175.95
7.85
183.80
6.00
177.80
177.79
0.01

Reduced & Plotted 10/10/38 JLF

11-25-38
Miller
Walker
13 Deg.

X See (Fairmont St) Pav. at Home Ave
Wadsworth Road
20 Wide

Home Ave Datum.

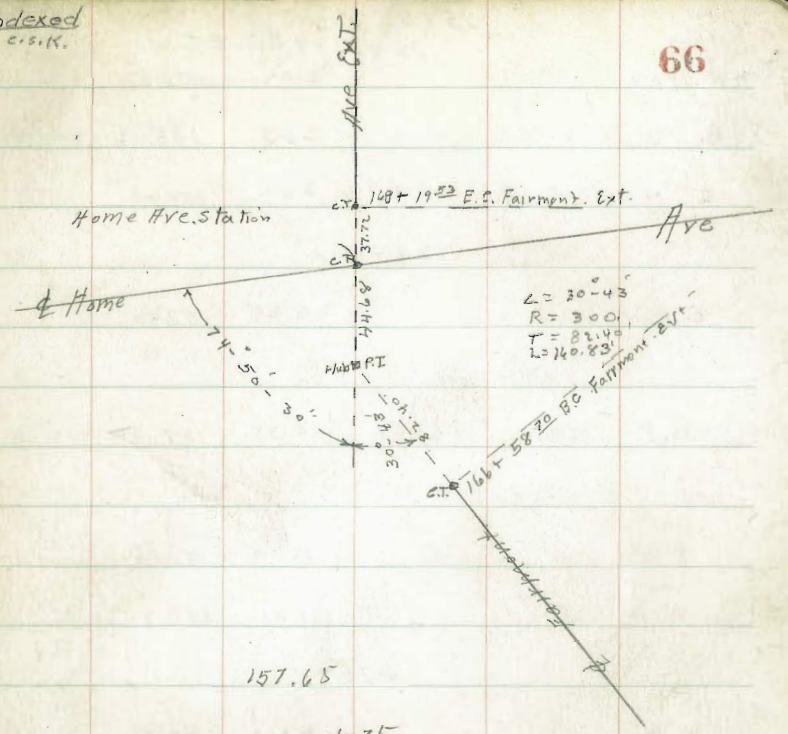
B.M.B.P.	9.43	157.65	148.22	Elev End. Box Culvert on Fairmont S. of Home 148.05

166+58.70 B.C. Fairmont Extension

E. Pav		9.92	142.73
℄		9.25	148.40
W. Pav		8.76	148.89
	+75		
W Pav		8.64	149.01
℄		9.17	148.48
E. Pav.		9.83	147.82
	167+00		
E. Pav		9.54	145.11
℄		8.82	148.83
W. Pav.		8.26	149.39
	+25		
W Pav		7.52	150.13
℄		8.02	149.63
E. Pav		8.70	148.95
	+50		
E. Pav		7.69	149.96
℄		7.04	150.61
W. Pav		6.57	151.08

Profile 150.4

Indexed
C.S.K.



W. Pav		5.21	152.44
℄		5.64	152.01
E. Pav		6.20	151.45
	148+00		
E Pav		4.74	152.91
℄ "		4.09	153.56
W "		3.60	154.05

157.65

168+19 53 E.C.

W. Pav			2.02	155.63
℄ "			2.53	155.12
ℰ. "			3.22	154.43
		+50		
ℰ Pav			0.25	157.40
T.P.	12.65	169.95	0.35	157.30
℄ Pav			12.09	157.86
W "			11.81	158.14
		+75		
W. Pav			9.24	160.71
℄ "			9.44	160.51
ℰ. "			984	160.09
		169+00		
ℰ. Pav			9.86	
℄ "			6.55	163.40
W. "			4.45	163.50

169.95

+75

67

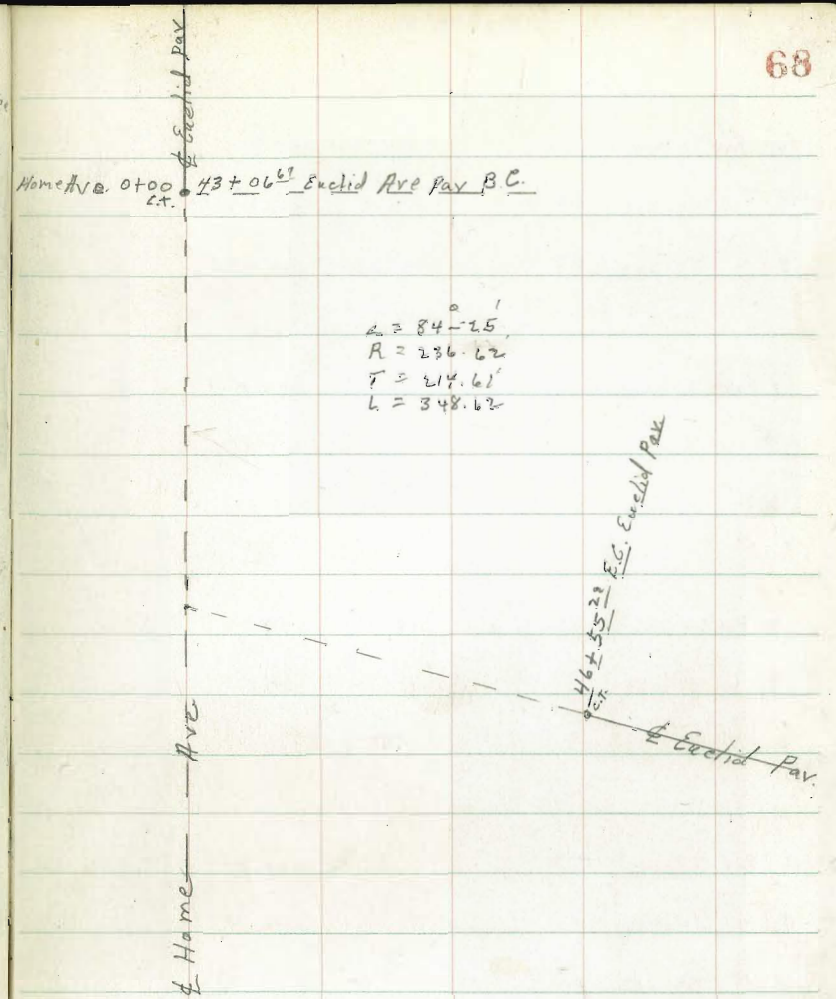
W. Pav	3.55	166.46	
℄ "	3.65	166.30	
ℰ. "	3.95	166.00	
169+50			
ℰ. "	0.93	169.02	
℄ "	0.69	169.26	169.1 Proj's Inv
W. "	0.60	169.35	

11-25-38
Miller Walker Blvd

X See Euclid Pav. at Home Ave
20' wide

Indexed
C.S.K.

				Sta 43+06.63 P.C. Euclid Pav.
B.M. & C.T.	9.21	238.34	229.13	
		42+00		
W. Pav			2.32	236.02
℄ "			2.21	236.13
E "			2.32	236.02
		+25		
E Pav			4.64	233.70
℄ "			4.53	233.81
W "			4.63	233.71
		+50		
W. Pav			6.37	231.87
℄ "			6.46	231.88
E. "			6.79	231.55
		+75		
E. Pav.			8.44	229.90
℄ "			7.93	230.41
W. "			7.61	230.73



238.34

43+06.67 B.C.

W. Pav			8.75	229.59
℄ "			9.21	229.13
E. "			9.93	228.41
		+25		
E Pav			10.54	227.80
℄ "			9.81	228.53
W "			9.35	228.99
		+50		
W. Pav			10.05	228.29
℄ "			10.52	227.82
E. "			11.23	227.11
		+75		
E. Pav			11.92	226.42
℄ "			11.20	227.14
W. "			10.72	227.62
		44+00		
W. Pav			11.48	226.86
℄ "			11.97	226.37
E. "			12.68	225.66
T.P.	2.48	228.62	12.20	226.14

228.62

		+25		
E. Pav			3.65	224.97
℄ "			2.97	225.65
W. "			2.49	226.13
		+50		
W. Pav			3.24	225.34
℄ "			3.75	224.87
E. "			4.46	224.16
		+75		
E. Pav			5.16	223.46
℄ "			4.48	224.14
W. "			4.03	224.59
		45+00		
S.W. Pav			4.75	223.87
℄ "			5.20	223.42
N.E. "			5.84	222.78
		+25		
N.E Pav			6.53	222.09
℄ "			5.92	222.70
S.W. "			5.53	223.09

228.62

45+50

S.W. Pav	6.28	222.34
℄ "	6.70	221.92
N.E. "	7.40	221.22

+75

N Pav	8.24	220.36
℄ "	7.55	221.07
S "	7.06	221.56

46+00

S. Pav	7.80	220.82
℄ "	8.22	220.36
N "	8.97	219.65

+25

N. Pav	9.82	218.80
℄ "	9.07	219.55
S "	8.66	219.96

+55.29 E.C.

S. Pav	9.69	218.93
℄ " E.T.	10.03	218.59
N. "	10.70	217.92

Levels for New Proposed Drain
at Date & State Sts.

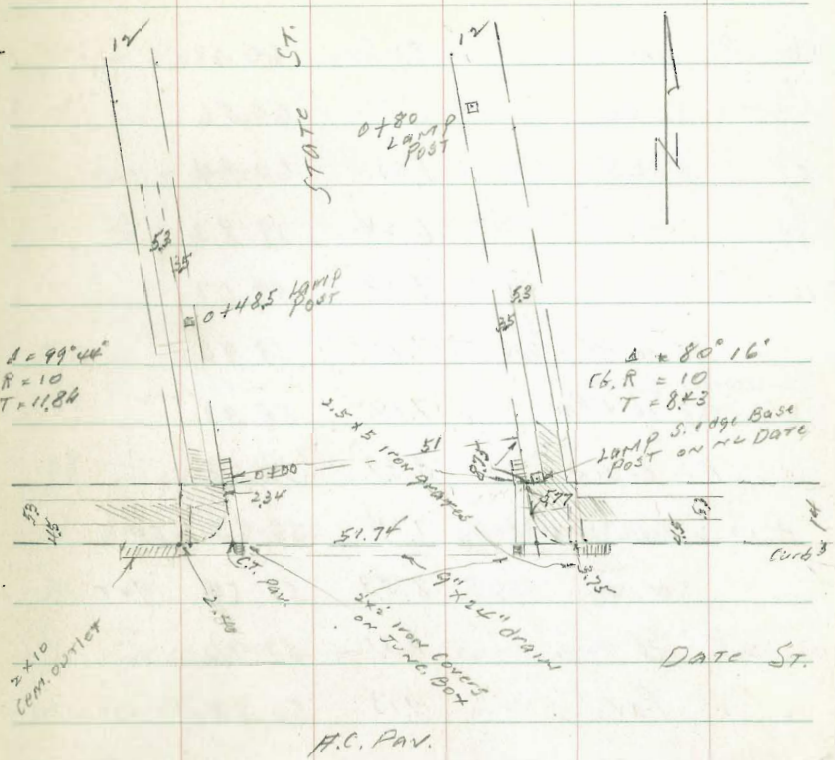
Indexed
C.S.K.

SWBP	7.07	66.07 ✓	59.00	Date & State
	N ½ of Date = 13' S of ℄ Curbline of Date			
-25		8.45		
W		7.12		
cb		6.55		
½		6.08		
C		5.59		
½		5.55		
cb		5.32		
E		5.02		
+25		4.08		
	N cb Date			
-25	gut	4.64	61.43	
-25	cb	4.01	62.06	
-5	"	4.78	61.29	
-5	gut grate	5.50	60.57	
E	cb. Pav. "	4.98	61.09	
E	FL. drain	6.25	59.82	
+3.75	cb P.C. cb + Pav	4.99	61.08	

Platted B & B.
5664-L

Moore
2-4-39

71



Lamp Base = 24" Octagonal

2.2 Center to Curbline

Note! N.W. 7' C.T. to be Tied out.

cb P.I. on Pav.	5.25	60.82	
1/4	5.51	60.56	
c	5.63	60.44	
1/4	6.24	59.83	
cb P.I.	7.00	59.07	
+11.86 cb. P.C. cb & Pav.	7.11	58.96	
W.L. Top cb & Pav. (State to South)	7.14	58.93	
" FL drain	8.39	57.68	
+10 2 wide Conc Apron outlet	7.64	58 43	cb
" " " "	8.53	57.54	out
+25 cb	8.31	57.76	
" " Pav	9.13	56.94	
N.L. Date St.			
W Top ret.	6.83		
W cb & Pav.	7.06		
" cb FL drain	8.04		
1/4	6.24		
c	5.74		
1/4	5.49		
E cb & Pav & grate	5.01		
" " FL dr	6.79		
E.L. Top Ret.	4.81		

N.L. Date to Sec. Parallel with Date St.

E cb	4.98	61.09
E " out & grate	5.88	60 19
+5 Pav	5.71	
1/4	5.50	
c	5.29	
1/4	6.23	
+8	7.08	
W out & grate	7.40	58.67
W cb	7.00	59.07

N.L Date & W cb State = 0+00 Sec. at 90° with State

W edge sdw	6.45	
W cb	6.74	59.33
W out	7.08	5899
1/4	6.07	
c	5.69	
1/4	5.29	
E out	5.09	
E cb = 8.75 N of N.L Date & E cb State	4.88	
E edge sdw	4.74	

0+50		
E edge sdw		4.53
E cb		4.67
E		5.44
1/4		5.24
C		5.42
1/4		5.77
W out		6.09
W cb		6.44
W edge sdw		6.12
0+75		
W cb		5.98
W out		6.23
1/4		5.46
C		5.16
1/4		4.99
E out		5.36
E cb		4.55
1+00		
E cb		4.19
out		5.08

66.07

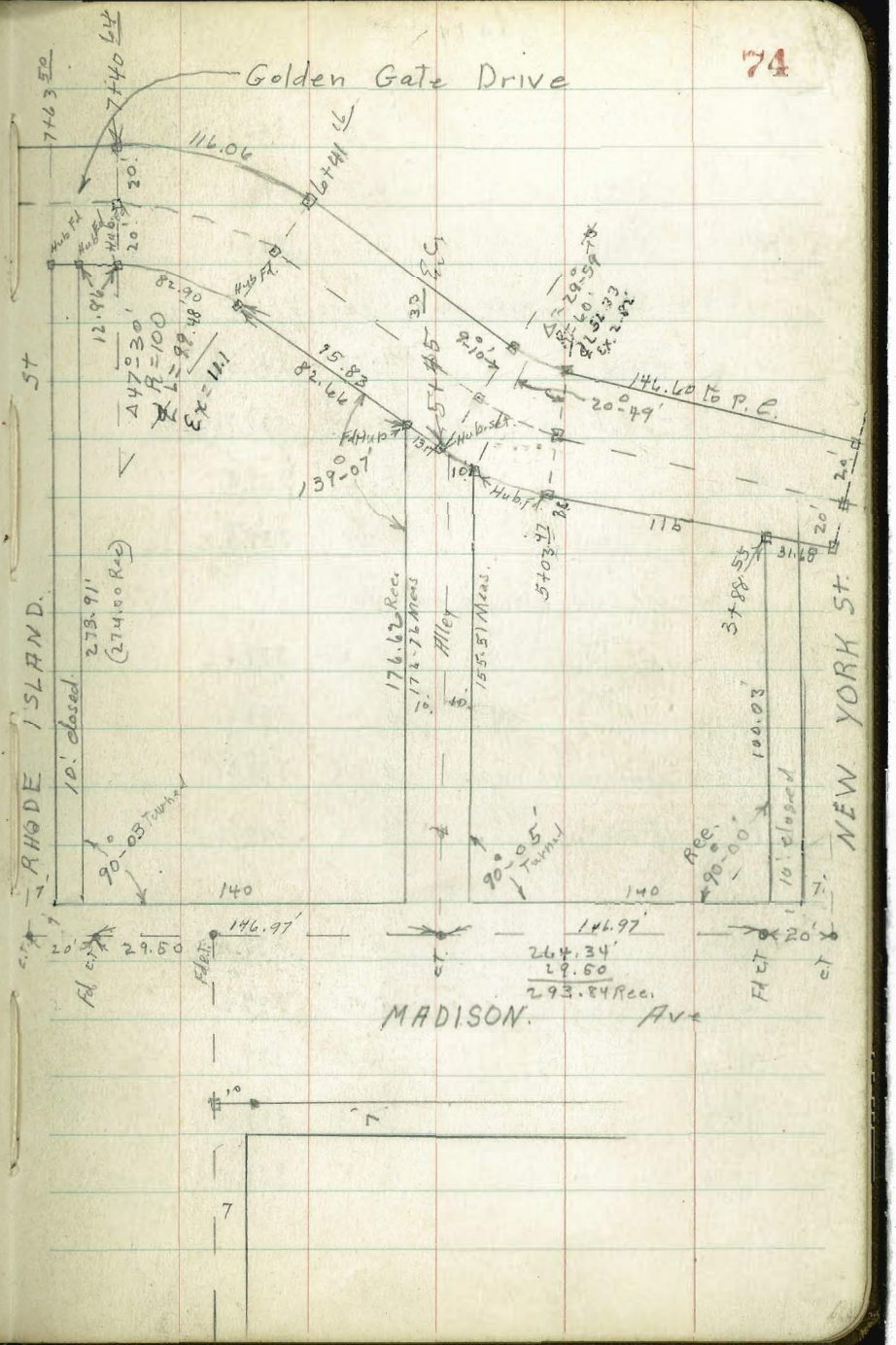
1/4		4.09
C		4.79
1/4		5.11
out		5.81
W cb		5.51

4-4-39
Miller
Walker
Bliss

X See Alley Blk. 31 U.14.

Indexed
E.5.151.
Madison
S.W. Monroe
& New York.

BM.	4.33	344.84	340.51	
	14' S. of N = N. eb. Line			
E. eb		5.31	339.53	
E par		5.90	338.94	
℄ "		5.95	338.89	
W. "		6.07	338.77	
W		5.42	339.38	
	0+00 = N. Line Madison			
W	eb & par N. End.	5.09	339.75	E. End Lawn
℄	" " "	5.17	339.67	
E	eb & " " "	4.96	339.88	
	0+25 N.			
E		4.8	340.0	
℄		4.7	340.1	
+8.	N. End. E. Edge Lawn	4.7	340.1	
W.	= N. End. Lawn	4.2	340.6	
	0+50 N			
W		4.5	340.3	
℄		4.4	340.4	
E		4.4	340.4	



344.84

0+75

℄	4.7	340.1
℄	4.7	340.1
W	4.7	340.1

0+84 S. End Garage on W. conc. floor 4.0 Back.

W - 4.' = floor	4.78	340.06
W. = E. edge conc. apron	5.08	339.76
℄	5.0	339.8
E	5.0	339.8

1+00 = N End. above garage.

E	5.2	339.6
℄	5.2	339.6
W = E. edge conc. apron	5.03	339.81
+4.' = floor	4.73	340.11

1+25

W - 5	5.4	339.4
W -	5.6	339.2
℄	5.8	339.0
W E	5.8	339.0
+5	5.8	339.0

344.84

75

1+55 -51 on E. Line } = S. Line Golden Gate Ave
1+76 24 " W " }

E	6.2	338.6
℄	5.9	338.9
W	6.4	338.4

Crystal Pier
Location of cottages

Sommermeyer
Begg
Shepard
Oltman.

6-June '51
W.O. 20825

Ref.

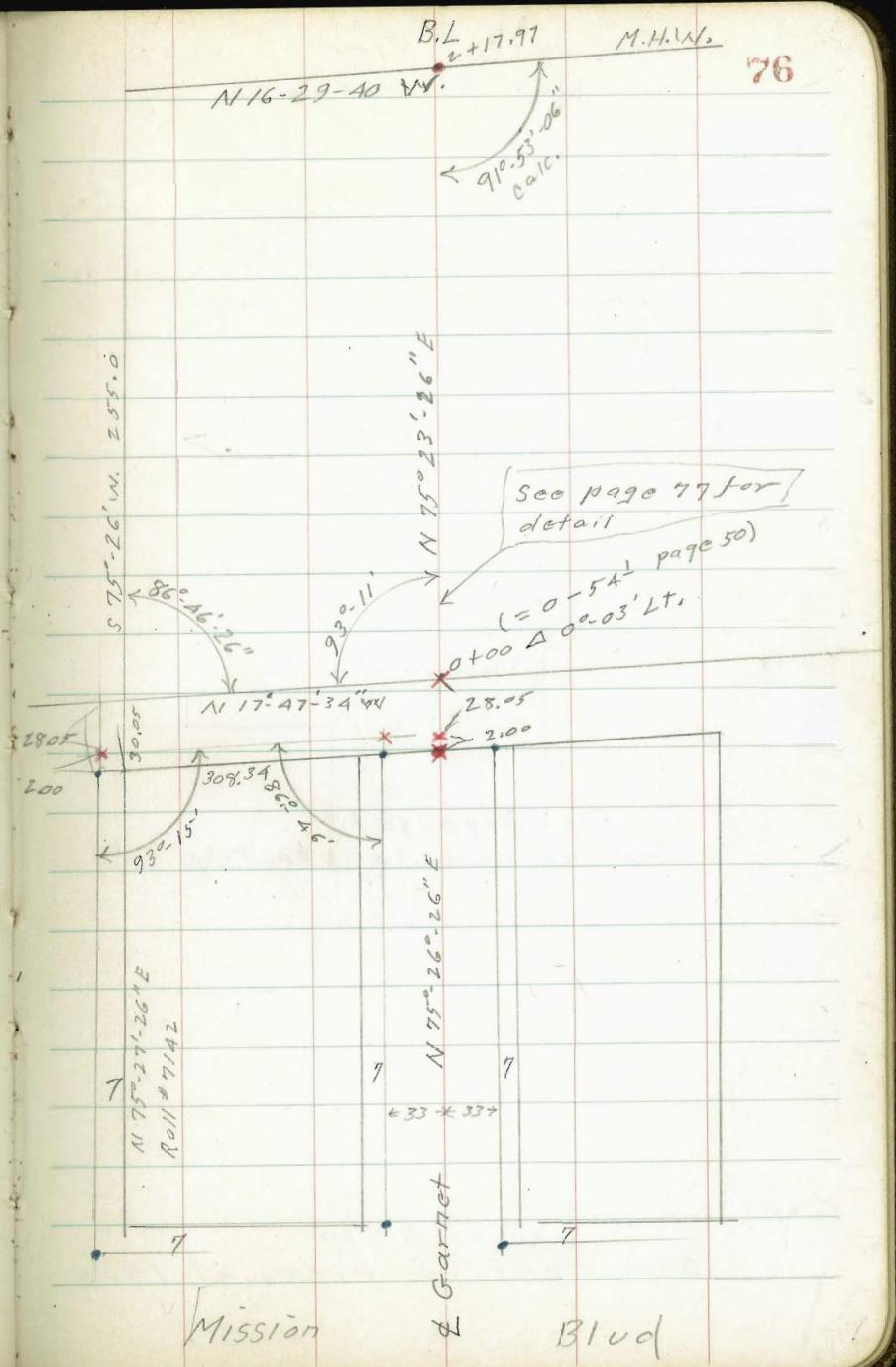
Roll # 7142

Tie sheet # 1755

● = Fd. L&T.

● = Set Nail

× = cut cross in conc.



Crystal Pier
Location of cottages

1+50±

1+18±

0+97.5

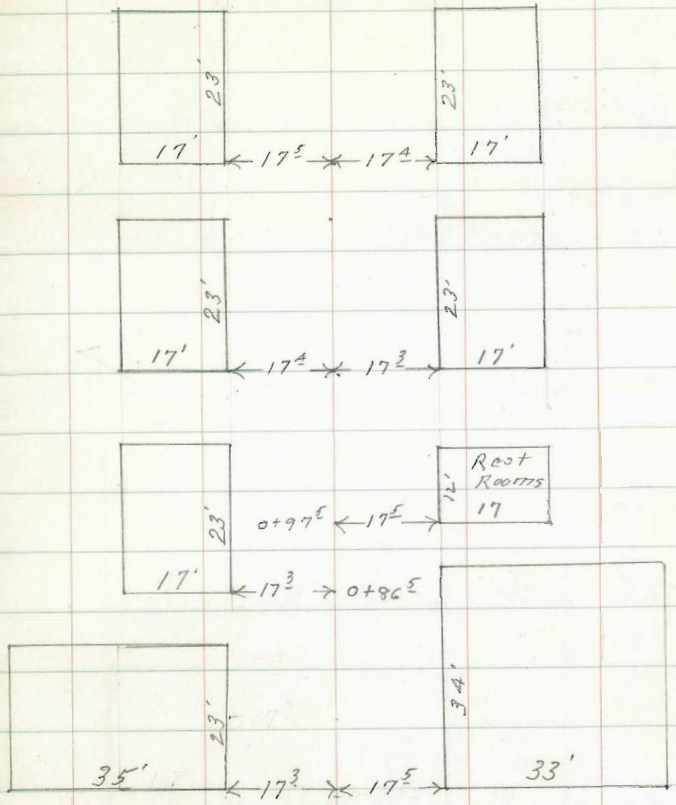
0+86.5

(=0+00 - page 50)
End of conc. = start pier
0+54±

0+00

and at 3+30
B.L. = split of pier at 1+18

B.L.
1+80



3+30

3+26 = start 36^{6} wide pier

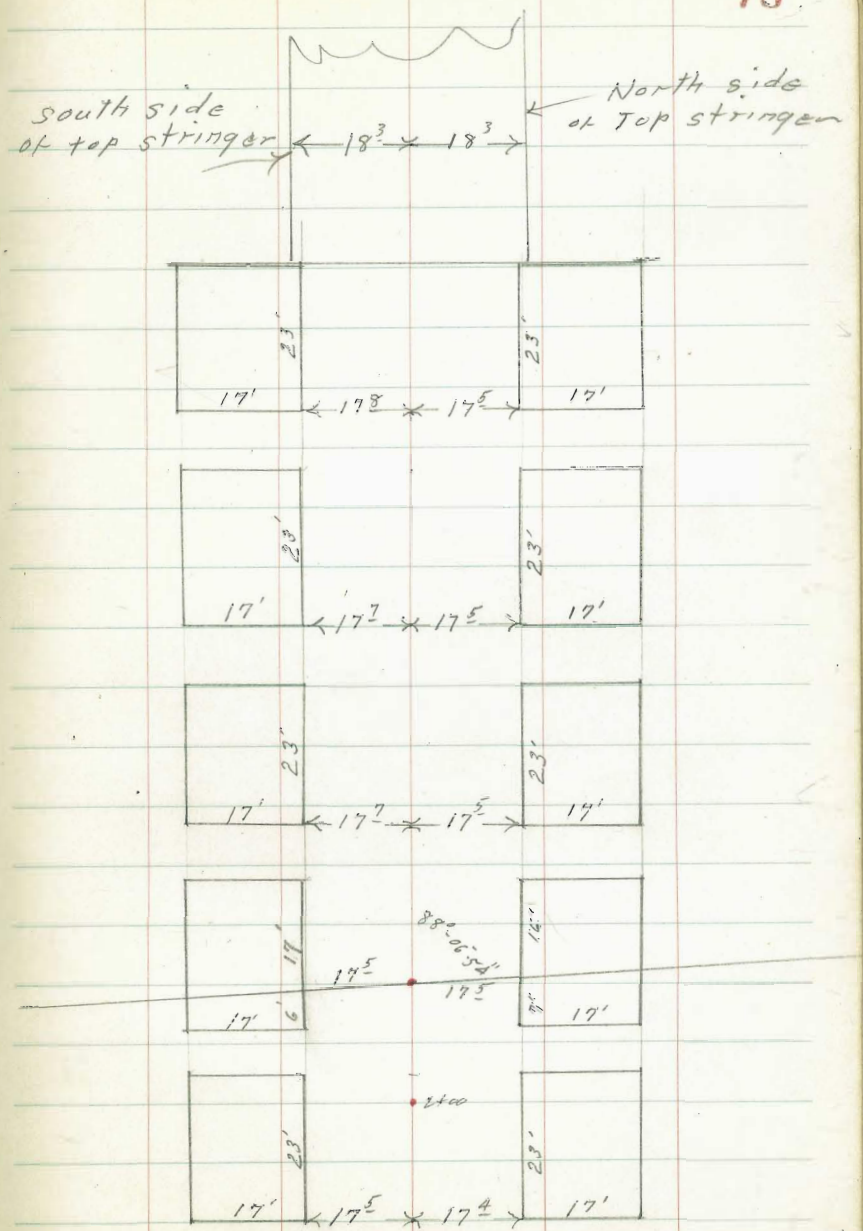
3+03

$2+72^{5}$

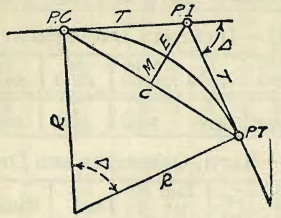
2+42

Bears N 16°-29'-40" W
2+17.97 = intersect. M.H.W. Line (Roll #7142)

$1+81^{5}$



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\sin. D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=R tan $\frac{\Delta}{2}$ (3) Length of Curve=L=100$\frac{\Delta}{D}$ (4)

Middle ordinate=M= R(1—cos. $\frac{\Delta}{2}$) (5) =R vers $\frac{\Delta}{2}$ (6)

External=E=T tan $\frac{\Delta}{4}$ (7) =R÷cos.$\frac{\Delta}{2}$—R (8)=R exsec $\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin.$\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157+45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 (54.50÷100)²=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus (54.50)²÷(2 x 688.26)=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=91.27 and from Table V correction=.10 or E=91.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and÷42=5.5 or D=5° 30′.

19396
14698
mea

14697

19394

York Cr. 7.08
San Rafael 7.13
" Jose 7.08
" Clara 7.19
" Juan 7.07

.98
1.27
6.25

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

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