

1556

DECEMBER  
1947

EXHIBITS

EXHIBITS

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1556

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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ENGINEERING DEPARTMENT  
CITY OF SAN DIEGO,  
CALIFORNIA.

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface and is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.



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E  
to be  
of road  
examp  
30.6 =

College Way Extension	1 - 21
Manzanita Pl. M. Dr. to Fairmount	22 - 24
Litchfield Rd. Mt. V. Dr. N.	26 - 29
Russell St. Willow to Evergreen	30 - 33
Alley Blk. 1 Center Add La Jolla Park	34 - 37
Drain 36 & University	38 - 41
Marcey Ave. 28-29	42 - 46
26 St. Russ Blvd. Pershing	47 - 67
Final Meas. Alley Blk 147 M. B.	68 -
Drain Rosecrans Rogers N.	69 -
✓ Camino de la Costa to Ave Cortez	70 - 72
✓ F at Glendale bet. 25-26	73 -
Alley Blk 2 Chester Park	74 - 77
Guy - Clark	78 -
opening Gillette from 36th St	79 -



3-29-38  
Miller  
Walker  
Bless.

# College Way Extension South of El Cajon Blvd.

See Page 10 for X Sec.

Def. L.S.

6+96<sup>47</sup> B.C. Hub  $\angle$  24°-45' Rt.

5+13<sup>26</sup> Hub.  $\frac{1}{2}$  Carol St to West 50' wide

4+96<sup>31</sup> E.C. Hub. 12-22-50

4+50 9-43.4

4+00  $\angle$  = 24°-45'-40" Lt. 6-51.5

3+90<sup>04</sup> P.I. Lt. R = 500'  
T = 169.75'  
L = 216.08' 3-59.6

3+50 3-59.6

3+00 1-07.7

2+80<sup>29</sup> B.C. Hub  $\angle$  24°-45'-40" Lt.

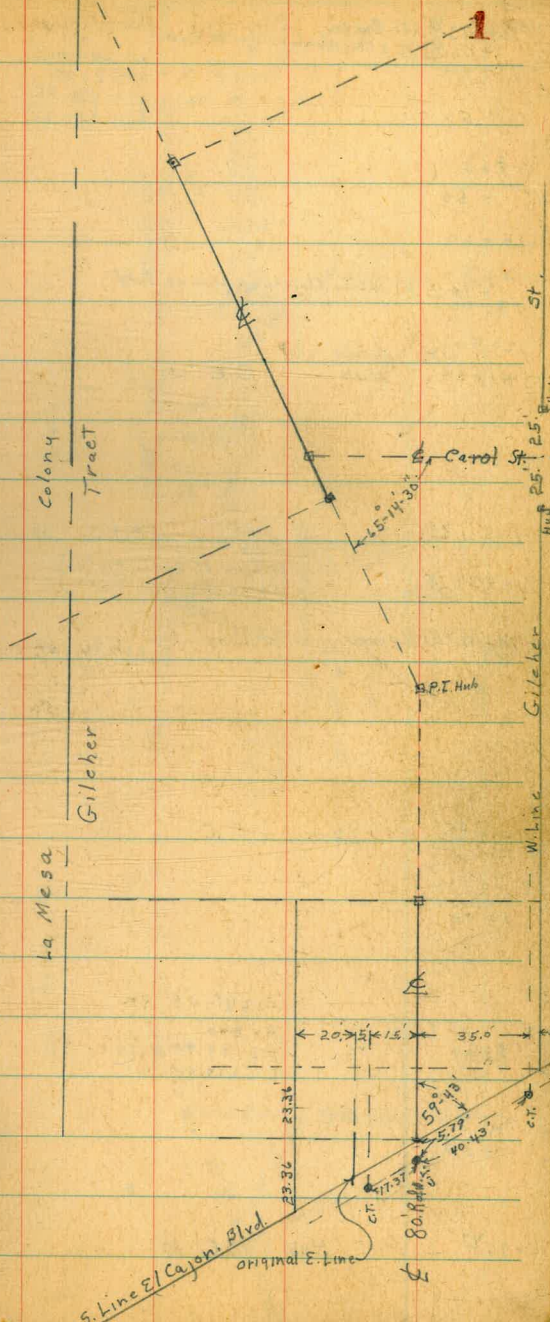
0+23<sup>26</sup> Pt  $\angle$ s to S.W. Cor

0+00 S. Line El Cajon Blvd.  $\frac{1}{2}$  80' St.

0-23<sup>26</sup> S. E. Cor. 80' R. of W.

Indexed  
C.S.K.

R.F. Hub. 38



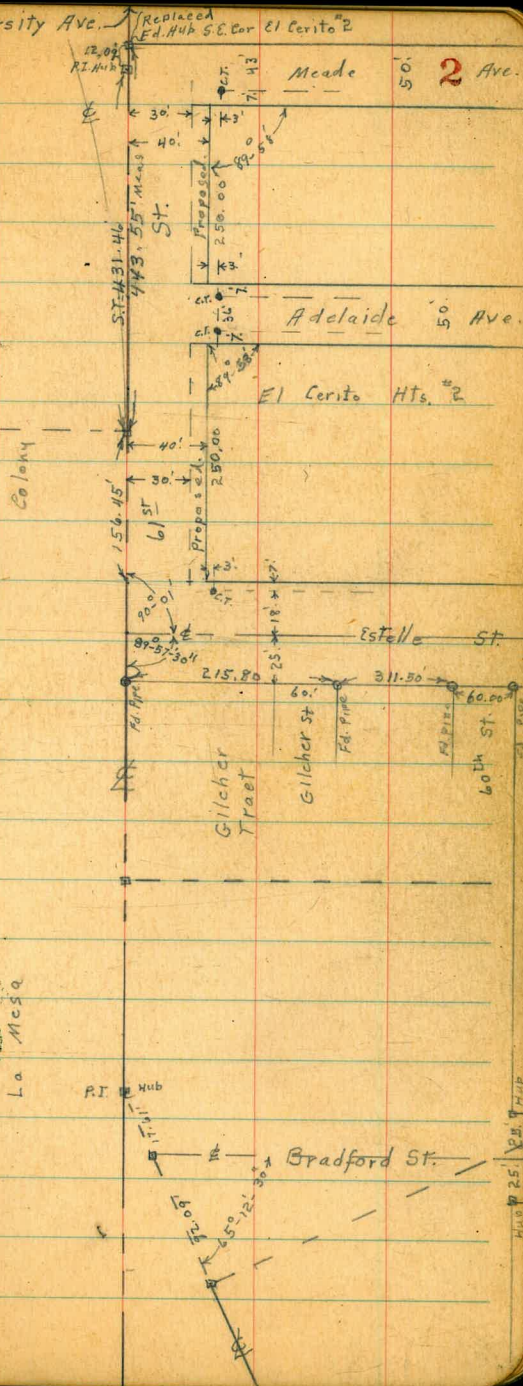


College Way South Extension. Def. Cs.

16+43 <sup>14</sup>	ctr Curve		
+0643	P.I. N. Line Meade + W. Line 80' Rgt. W.		
16+80		$\angle = 24^{\circ} 20' - 50'$	12-10.25
		$R = 2000'$	
		$T = 431.46'$	
		$L = 877.88'$	4+45
15+50			
15+00			4-02.1
+50			3-19.1
14+00			2-36.2
+50			1-53.2
+10.13	P.I. N. Line Adelaide + W. Line 40' Rgt. W.		1-10.3
12+50			0-27.3
12+18 <sup>20</sup>	Hub	B.C. Lt.	
10+61 <sup>75</sup>		S. Line Estelle St	
10+31 <sup>75</sup>		{ N. Line El Cerito Hts #2 S. Line Gilcher Tract }	
10+11 <sup>75</sup>	pipe	N. Line Estelle St.	
9+12 <sup>45</sup>	Hub	E.C.	12-22.5
8+50			8-47.7
8+00		$\angle = 24^{\circ} - 45'$ Rt.	
		$R = 500'$	
		$T = 109.70'$	5-55.8
		$L = 215.98'$	
7+50			3-03.9
6+96 <sup>47</sup>	Hub	B.C. Rt.	

To C.T. & University Ave.

TR 0710-  
8-4-38

































College Way South Extension  
See Page 1.

Indexed  
c.s.K.

2+23<sup>4</sup> ± 9' cmt. Drive

2+14.4 ± 4' cmt. walk

2+00

1+50

1+00

0+50

S. Line El Cajon. on Diagonal

B.M. BP.

2.76

468.03

465.27

Lt.

±

Rt.

10

459.67  
8.36  
40.  
N. Line  
cmt Drive

459.85  
8.18  
40.  
N. Line  
cmt walk.

459.5			459.8			460.0
8.5	8.5	8.2	8.2	8.0	8.1	8.0
40	20.	10.		70	20	40

461.1			461.6			461.5
6.9	6.6	6.6	6.4	6.4	6.7	6.5
40.	20.	10.		10	20	40

462.3			462.4			462.7
5.7	6.1	6.3	5.6	5.4	5.1	5.3
40	20.	10.		10.	20.	40

464.0			463.4			463.6
4.0	4.0	4.6	4.6	4.5	4.3	4.4
40	20	10.		10.	20.	40.

464.6				465.29				464.9
3.4	3.4	3.4	3.32	3.86	2.74	3.62	3.70	3.74
46.4	23.2	11.6	7.6	9.5	Pav. 0+00	11.4	23.2	33.1
E. Line			cmt. cb.	gutter		pav	pav	Gutter
								33.2
								46.4
								N. Line

468.03

N.W. College & El Cajon Blvd.

±



T.P. 1.56 446.89 12.85 445.33

H+00

+50

3700

T.P. 3.06 458.18 12.91 455.12

2180<sup>29</sup> B.C. Lt.

R+50

468.03

448.7 447.0 447.6  
 9.5 9.8 10.6 11.2 12.0 11.6 10.6  
 40 20 10 10 20 20 40

451.8 451.0 451.4  
 6.4 6.4 6.8 7.2 7.2 7.4 6.8  
 40 20 10 10 10 20 40

455.6 455.6 456.0  
 2.6 2.4 2.6 2.6 2.7 2.7 2.2  
 40 20 10 10 10 20 40

458.18

456.1 456.74 457.4  
 11.9 11.4 11.2 11.29 11.2 11.0 10.6  
 40 20 100 E Hub 10 20 40

457.5 458.5 458.6  
 10.5 9.8 9.8 9.5 9.6 9.7 9.4  
 40 20 10 10 10 20 40

468.03

±



6+00

438.5				435.5			432.9		
7.4	8.4	9.2	10.3	11.4	12.0	13.1	14.0	15.6	
60	40	20	10		10	20	40	65 wash	

5+80 Low. spot ok. for Culvert

434.9				434.1			432.9		
11.2	12.0	12.5	12.7	12.8	13.2	13.3	14.0	15.0	
60 wash	40	20	10		10	20	40	60 wash Δ	

5+50

436.1				434.5			434.1		
10.3	10.8	12.4	12.6	12.4	12.3	12.4	12.8	11.9	
60 wash	40	20	10		10	20	40	60	

5+25

437.0				435.5			437.1		
9.9	10.8	11.1	11.3	11.4	11.1	11.1	9.8	8.5	
60	40	20	10		10	20	40	55	

5+13<sup>26</sup> P.I. & Car. of St Readings on & Carol St. Not at 90°

436.2									
10.7	6.2	3.8	0.8	+2.3	+5.3				
	45.	60.	100.	160.	200.				

4+96<sup>37</sup> E.C.

440.7				438.0			440.6		
6.2	7.6	8.9	9.3	8.90	9.5	9.0	6.3	5.4	
60	40	20	10	440.	10	20	40	50	

4+50

444.0				441.8			444.5		
2.9	4.0	4.6	5.1	5.4	5.1	2.4			
40	20	10		10	20	40			

446.89

446.89



8+50

T.P. 10.19 444.92 12.16 434.73

8+0.0

7+85 approx. P.I.  $\perp$  Bradford. st. Readings on  $\perp$  Bradford. st. Not. 90°

7+50

6+96 <sup>47</sup> BC Rt.

6+50

446.89

437.2

7.7 9.1 9.7 10.5 11.1 11.3 12.0 12.5  
40 20 10 10 20 40 50

434.4

444.92

432.9

439.6

7.3 8.9 9.6 10.4 10.7 11.1 12.2 13.4  
40 20 10 10 20 40 50

436.5

434.7

436.8

10.1 12.0 15.6 18.3 17.4  
45 100 130 200

440.5

6.4 8.5 8.8 9.6 10 20 40  
40 20 10 10.1 10.5 11.2

437.3

435.7

439.9

7.0 8.6 8.8 9.51 9.7 9.9 11.5  
40 20 10 446 10 20 40

437.38

535.4

439.3

7.6 8.5 8.8 9.4 10.4 11.5 12.6 14.2  
40 20 10 10 20 40 60

437.5

434.3

446.89



10+51<sup>75</sup> = S. Curb. Line = N. side E. Combination Curbe Walk.

10+36<sup>75</sup> Division Line & Estelle = N. Edge Pav

10+34

10+11<sup>75</sup> N. Line Estelle St

9+50

9+12<sup>45</sup> E.C

8+85 Low spot. O.K. for Culverts

College way S.

444.7

0.2  
40

2.2  
20

4.1  
10

439.8

5.1

5.6  
10

5.8  
20

6.50

6.06

6.25

7.09

10.12

10.53

438.2714

30  
C. Pav  
E. End

40  
E. End

40  
C. Pav

40  
E. End

100  
C. Pav

100  
E. End

444.8

0.1  
40

2.0  
20

4.8  
10

440.0

4.9

5.5  
10

5.9  
20

6.40

6.99

10.57

100

40

40

100

437.9

30  
Pav.  
E. End

40  
Pav

40  
Pav

100

40

100

444.9

0.0  
40

1.7  
20

2.7  
10

441.5

3.4

4.8  
10

4.5  
20

5.0

6.1

9.6

100

40

40

100

438.8

442.7

2.2  
40

3.4  
20

3.9  
10

440.7

4.2

4.8  
10

5.4  
20

7.1

8.0

50

437.8

438.7

6.2  
40

7.2  
20

7.7  
10

437.0

7.9

9.2  
10

9.4  
20

10.4

11.1

50

434.5

436.1

8.8  
40

9.4  
20

9.7  
10

435.0

9.9

10.4  
10

11.1  
20

11.9

12.1

50

333.0

434.2

9.6  
60

10.7  
40

11.1  
20

11.3  
10

433.4

11.5

12.1  
10

12.3  
20

12.8

13.1

40

40

432.1

444.92



11+75

T.P. 11.06 464.61 1.78 453.55

11+50

11+00

10+65

T.P. 10.94 455.33 0.53 444.39

10+61<sup>25</sup> = S. Line Estelle

B.M.C.T.R.P.

6.77 438.15

444.92

452.8			451.7			448.3
11.4 40	13.0 20	12.0 10	12.9	14.8 10	15.4 20	16.3 40
464.61						

451.5			448.7			446.5
3.8 40	4.2 20	5.7 10	6.6	7.4 10	7.7 20	8.7 40

448.8			446.2			443.5
6.5 40	8.3 20	8.7 10	9.1	10.0 10	10.2 20	11.8 40

445.4			445.5			441.4
9.9 40	11.5 20	11.0 10	9.8	10.8 10	11.0 20	13.9 40
455.33						

445.4			440.2			438.5
10.5 40	1.6 20	3.9 10	4.7	5.3 10	5.7 20	6.4 40

5.7' Line Estelle 51.43' 0 w. of  $\phi$ 

444.92



13 + 10<sup>12</sup> P.I. N. Line Adelaide + W. line 80' B. of W.

460.2

44  
404.2  
205.5  
10

458.9

5.7  
106.2  
106.0  
20

458.0

6.6  
40

N. Line of Adelaide

12 + 90

458.2

6.4  
405.9  
205.3  
10

459.8

4.8  
106.0  
106.6  
20

457.6

7.0  
40

12 + 58

460.0

4.6  
408.3  
209.0  
10

456.2

8.4  
109.1  
108.5  
20

455.4

9.2  
40

12 + 38

456.8

7.8  
309.1  
2010.0  
10

454.9

9.7  
1010.0  
109.9  
20

454.0

10.6  
4012 + 18<sup>20</sup> B.C. Lt.

456.5

8.1  
4010.2  
2010.6  
10

453.8

10.75  
4011.4  
1011.7  
20

452.3

12.3  
40

12 + 00

455.7

8.9  
4011.3  
2012.1  
10

452.1

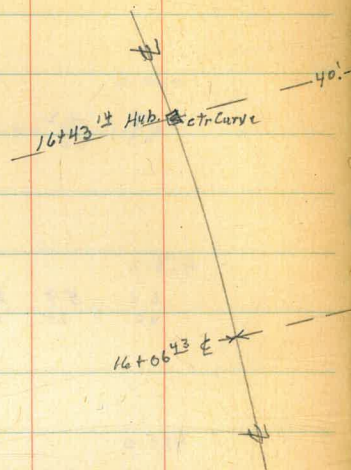
12.5  
1012.9  
1013.6  
20

450.4

14.2  
40

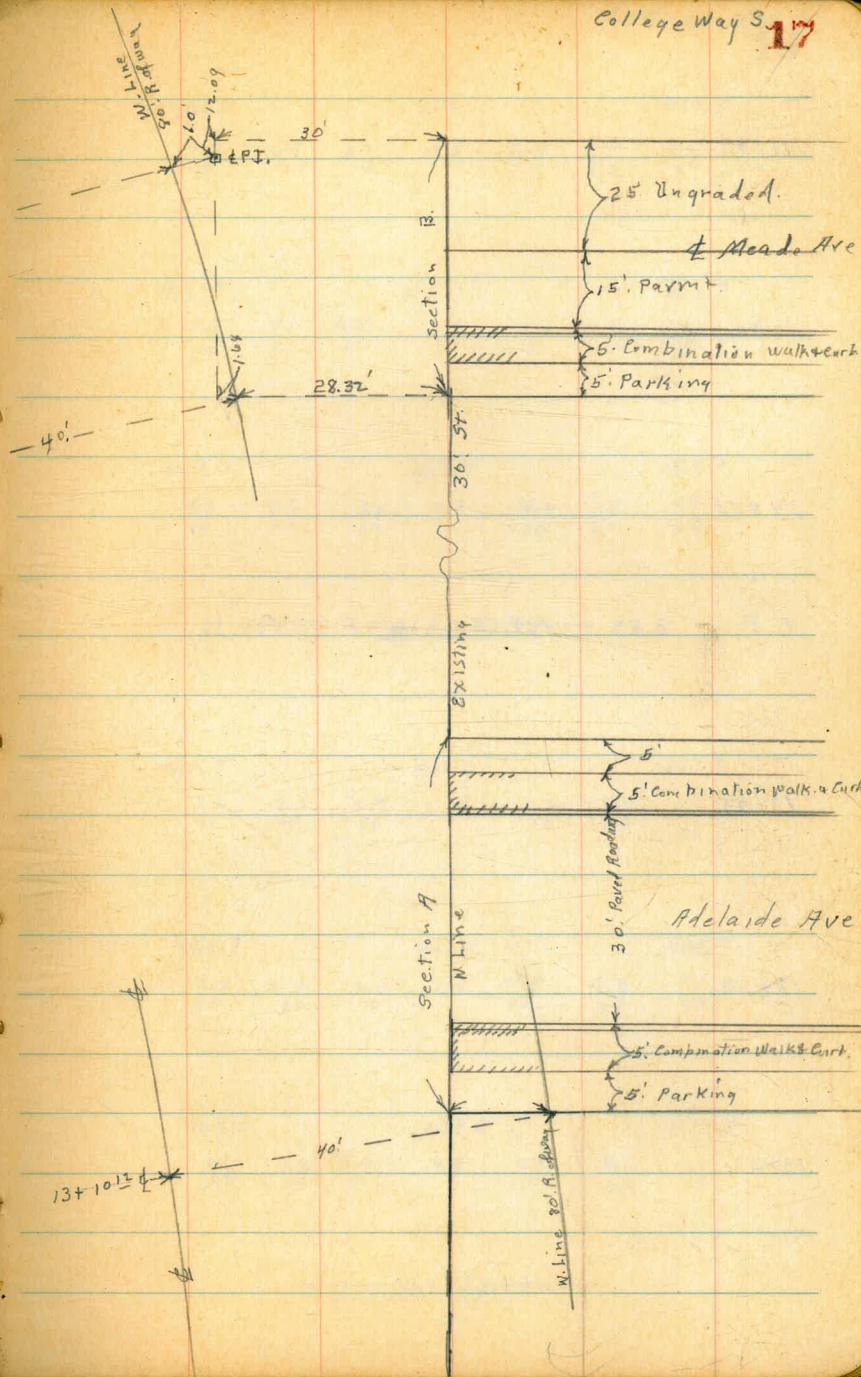
464.61





see A. Levels across E End. of Adelaide Ave  
X. 444.61

N. Line	6.6	458.0
N. d. E. End.	6.55	
G. pav. E End.	7.04	
N. 1/2 " "	6.61	
E " "	6.42	458.19
S. 1/2 " "	6.36	
G. " "	6.52	
S. d " "	6.05	
S.	5.5	459.1





14+85

14+50

14+15

T.P. 3.89 468.05 0.45 464.16

13+95

13+60

13+35

464.61

460.0

8.0	6.5	5.7	5.5	6.0	6.0	4.5
40	20	10		10	20	40

462.5

463.5

462.4

5.6	5.6	5.5	5.3	4.6	4.2	4.8
40	20	10		10	20	40

462.7

463.7

462.7

5.3	3.6	3.5	4.3	4.0	3.8	4.9
40	20	10		10	20	40

463.7

463.1

468.05

461.5

3.1	2.5	2.7	2.4	2.2	2.0	2.4
40	20	10		10	20	40

462.2

462.2

460.8

3.8	2.4	2.3	1.6	2.0	3.0	3.7
40	20	10		10	20	40

463.0

460.9

460.0

4.6	5.2	5.0	4.8	4.7	5.4	6.6
40	20	10		10	20	40

459.8

458.0

464.61

£



N.W. Cor Meade + 61 <sup>st</sup> St.	1.4	457.5
10' S. = cmt. ab. E. End	1.74	
10' S. = G. pav. " "	2.16	
25' S. = S. side E. End. Pav.	1.83	
27' S. = Ungraded.	+ 3.0	
50' S. = S. line "	+ 2.5	461.4

16+06<sup>93</sup> P.I. X Line Meade + W. Line 80' R. of W.

	446.1		452.6		456.7				
	16.3 60	12.8 40	7.6 20	6.6 10	6.3	5.2 10	4.0 20	2.2 40	28.32

16+00

	448.4		453.0		459.4			
	14.9 60	10.5 40	7.2 20	6.2 10	5.7	3.9 10	2.5 20	+0.5 40
	458.93							

T.P. 0.84 458.93 9.96 458.09

C.T. N. 7' Line of Meade Ave - 13' W. of W. line original 61<sup>st</sup> St.

15+60

	453.0		458.0		460.7			
	16.0 60	15.0 40	12.0 20	11.0 10	10.0	9.3 10	8.6 20	7.3 40

15+20

	458.3		459.8		462.3		
	9.7 40	8.4 20	8.3 10	8.2	7.7 10	6.7 20	5.7 40

468.05

468.05

1.4  
 N.W. Cor 61<sup>st</sup> St  
 + Meade Ave



CHK. BM.

9.96

438.87 = 438.84

BM.

10.67

438.16 = 438.15

T.P.

2.24

448.83

10.40

446.59

T.P.

1.05

456.99

12.40

455.94

T.P.

10.25

468.34

0.84

458.09

16+43 <sup>14</sup> Ctr Curve.

16+33

16+30

458.93

College Way S.  
20

E. End. Int. ch. s. side Estelle

S. 7' E. T. Estelle 13' W. of Original Line of 67<sup>th</sup> St

442.4			450.25			456.3	
21.7	16.5	10.2	9.0	8.68	8.2	6.6	2.6
60	40	20	10	Hub.	10	20	40

444.6			451.1			457.5	
20.5	14.3	9.4	8.6	7.8	6.6	6.2	1.4
60	40	20	10		10.	20.	40.

444.6			451.3			454.9	
20.5	14.3	9.4	8.0	7.6	6.6	5.8	4.0
60	40	20	10.		10.	20.	40

458.93











## W. Line Fairmont

90.8' N = P.C. 30.35 Prop. Rad.	6.2	314.2
79.8' N = P.C. 40' cl. Rad.	6.4	314.0
53.4' N = Top w. End 40' R. cl. Ret.	6.69	313.69 + ground. to w
53.4' N Gutter pav. w. edge	7.02	313.36 " " " "
40' N " " "	7.24	313.14 " " " "
30' N " " "	7.50	312.88 " " " "
20' N " " "	7.90	312.48 " " " "
10' N " " "	8.53	311.85 " " " "
10' N. cnt. cl. Ret. " "	7.94	312.44 " " " "
S. Line = S.W. cor. cnt. walk.	7.79	312.59
" " Ground. to W.	8.3	312.1
30.35' W. of W. Line Fairmont.		
S.	8.3	312.1
+10 = cl. Line	8.1	312.3
+11 N	8.5	311.9
+20 N	7.8	312.6
+30 N	7.6	312.8
+39.8' N North curb line if existing 40' cl. Radius were continued	7.3	313.1
+45.1' N	7.9	312.5
+53.4' N	7.8	312.6
+79.8' N	7.3	313.1
+90.8' at 30.35 Property Radius	7.1	313.3

49.49' W. of W. Line Fairmont = P.C. 30 Prop. Rad. on S.

53.4' N	8.0	312.4
46.1' N	7.0	313.4
40' N	7.2	313.2
30' N at 30' S. Prop. Rad.	7.7	312.7
20' N	7.9	312.5
11' N	8.7	311.7
10' N = S. cl.	8.2	312.2
S.	8.3	312.1

See. 00-20.80 NW. E.C. above S. Prop. curve

W	8.2	312.2
+10 = cl. Line	8.1	312.3
+11	8.5	311.9
+20	7.8	312.6
+30 30' S. prop. line Rad.	7.7	312.7

See. 0100 see plat. at P.C. N.E. 30.35 Prop. Radius

W on N.E. End. cnt. walk. to house	7.99	312.39
+10 = cl	7.9	312.5
+11	8.3	312.1
+20	7.6	312.8
+30 = cl	7.4	313.0



320.38  
0+00 (con)

+40	7.8	312.6	
+50	7.9	312.5	
+60 = E. Line	7.6	312.8	
+90.35 at 30.35 Prop Rad	7.1	313.3	(Same as 90.35 N. at Sec. 30.35' w of W. line - Fairmont.)
	0+50		
E	6.7	313.7	
+10 d	6.6	313.8	
+20 1/4	6.6	313.8	
+30 d	6.8	313.6	
+40 1/4	6.8	313.6	
+49	7.1	313.3	
+50 = d	6.9	313.5	
+60 = W.	6.8	313.6	
	1+00		
W	6.9	313.5	
d	6.9	313.5	
1/4	6.4	314.0	
d	6.3	314.1	
1/4	6.0	314.4	
d	5.8	314.6	
E	6.0	314.4	

320.38

Manzanita PL 24

1+29<sup>27</sup> = S. Line Manzanita Drive

Sec at Rt. Ls. to S.W. Cor Man. Dr + Man Pl

E	5.6	314.8	
d	5.5	314.9	
1/4	5.6	314.8	
d	5.9	314.5	
1/4	6.4	314.0	
d	6.6	313.8	
W	6.7	313.7	
+50' W	8.5	311.9	
+100' W	9.9	310.5	
	1+54 <sup>79</sup> = Rt. L. to d Man. Dr on W.		
W-100'	10.1	310.3	
W-50'	8.7	311.7	
W	6.7	313.7	
d	6.3	314.1	
1/4	6.1	314.3	
d	5.9	314.5	
1/4	5.6	314.8	
d	5.3	315.1	
E	5.3	315.1	



320.38

1+79<sup>24</sup> at Rt. 25 to N. W. Cor Manzanita Dr. + Pl.

E.	5.6	314.8
dr	5.7	314.7
1/4	6.0	314.4
1/2	6.3	314.1
3/4	6.5	313.9
dr	7.1	313.3
W	7.4	313.0
+50'	9.4	311.0
+100'	10.6	309.8

2+20

W-10	10.4	310.0
W	9.7	310.7
dr	9.2	311.2
1/4	8.4	312.0
1/2	7.6	312.8
3/4	7.2	313.2
dr	6.9	313.5
E	6.6	313.8

2+24<sup>25</sup> at Rt. 4 from S. E. Cor Thorh + Manzanita Pl.

E	7.5	312.9
dr	8.1	312.3

25

1/4	8.7	311.7
1/2	9.6	310.8
3/4	10.6	309.8
dr	11.6	308.8
W	13.2	307.2
+10	13.7	306.7



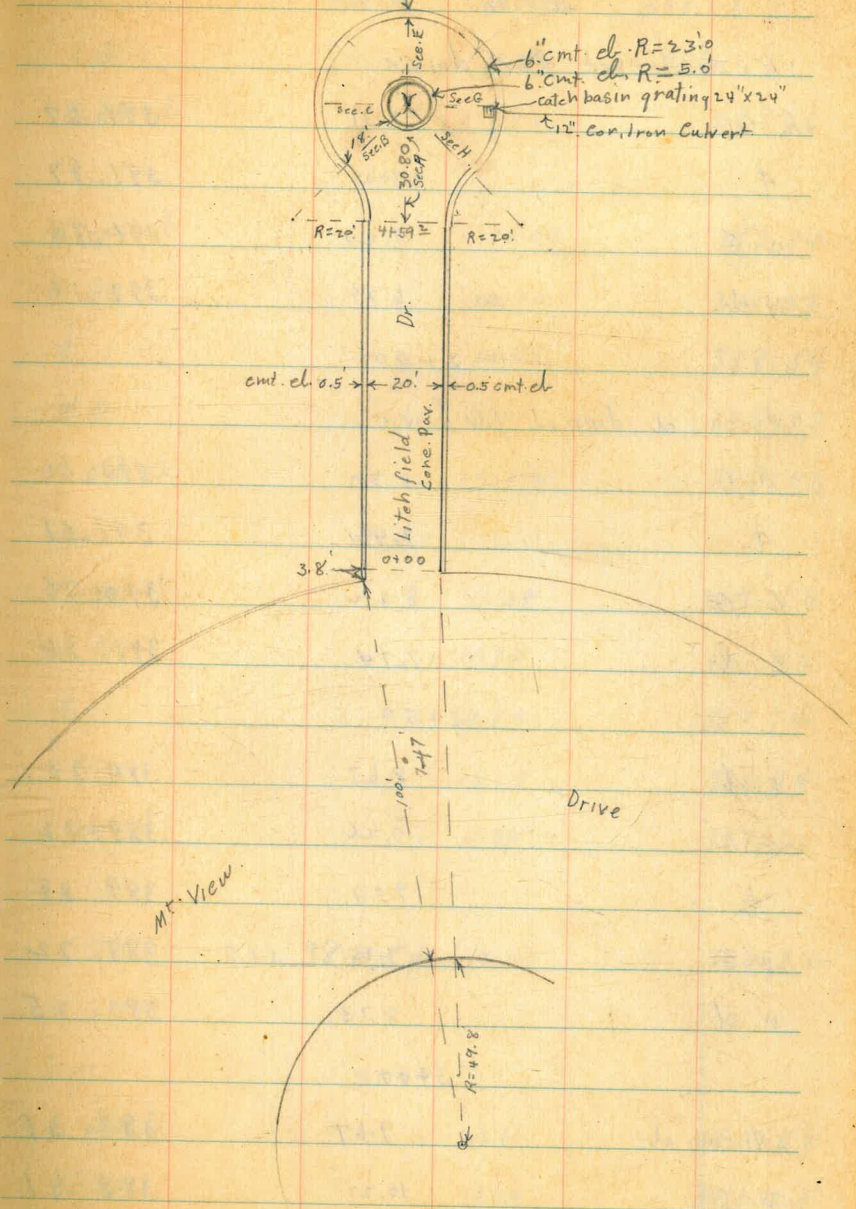
7-12-38  
Miller  
Walker  
Bliss

Litchfield Rd. X. Sec. Mt View. Dr. North

B.M. B.P.	4.44	398.98	394.54	N. W. Mt View. Dr. + Litchfield.
0+00 - 3.8' on W } = N. Line Mt. View. Drive (on curve)				
W. cmt. ch	4.06	394.92		
W. Gutter pav	4.44	394.54		
±	4.35	394.63		
E. G.	4.69	394.29		
E. cmt. ch	4.20	394.78		
0+50 X at Rt. Ls				
E. cmt. ch	5.01	393.97		
E. G	5.49	393.49		
±	5.24	393.74		
W G	5.42	393.56		
W. cmt. ch.	4.94	394.04		
1+00				
W. cmt. ch	5.79	393.19		
W. G	6.32	392.66		
±	6.11	392.87		
E. G	6.32	392.66		
E. cmt. ch	5.81	393.17		

Indexed  
C.S.K.

Lot 15





398.98 1+50

E. dr. dipped for drive		
E. G	7.31	391.67
♀	7.01	391.97
W. G	7.24	391.74
W. dr.	6.79	392.19
	2+00	
W. cnt. dr. dipped for drive		
W. G	8.32	390.66
♀	7.97	391.01
C. G	8.22	390.76
E. dr.	7.74	391.24
	2+50	
E. dr.	8.67	390.31
E. G	9.26	389.72
♀	9.09	389.89
W. G	9.26	389.72
W. dr.	8.73	390.25
	3+00	
W. cnt. dr.	9.67	389.31
W. G	10.27	388.71

Litchfield Drive

E	398.98	10.06	388.92 <sup>27</sup>
E. G.		10.32	388.66
E. cnt. dr.		9.72	389.26
	3+10		
E. cnt. dr.		10.04	388.94
E. G		10.70	388.28
♀		10.44	388.54
W. G		10.61	388.37
W. cnt. dr.		10.02	388.96
	3+50		
W. cnt. dr.		11.39	387.59
W. G		11.95	387.03
♀		11.84	387.14
E. G		12.04	386.94
E. cnt. dr.		11.38	387.60
T. P	2.22	388.54	12.66
	4+00		
E. cnt. dr.		2.71	385.83
E. G		3.29	385.25



£	388.54	4+00 (con) 3.06	384.52
W. G		3.36	385.18
W. cnt. dr.		2.75	385.79
		4+59 <sup>2</sup> P.C. Banjo.	
W. cnt. dr.		4.60	383.94
W. G		5.15	383.39
£		4.98	383.56
E. G		5.28	383.26
E. cnt. dr.		4.71	383.83
		Sec. A	
ctr. Banjo ground		5.0	383.54
+ 5' S = dr.		5.17	383.37
+ 5' S = G		5.55	382.99
+ 14 S.		5.32	383.22
+ 30 <sup>8</sup> S = £ at 4+59 <sup>2</sup>		4.98	383.56
		Sec. B	
ctr. Banjo		5.0	383.54
+ 5' = cnt. dr.		5.03	383.51
+ 5' = G		5.51	383.03
+ 14		5.26	383.28
+ 23 = G.		5.34	383.20
+ 23 = cnt. dr.		4.14	384.40

		Sec. C	
ctr. Banjo	388.54	5.0	383.54
+ 5 = cnt. dr.		5.00	383.54
+ 5 = G.		5.50	383.04
+ 14		5.40	383.14
+ 23 = E		5.57	382.97
+ 23 = cnt. dr.		5.05	383.49
		Sec. E.	
ctr. Banjo		5.0	383.54
+ 5 = cnt. dr.		5.11	383.43
+ 5 = G		5.56	382.98
+ 14		5.61	382.93
+ 23 = G		5.89	382.65
+ 23 = cnt. dr.		5.31	383.23
		Sec. G.	
ctr. Banjo		5.0	383.54
+ 5' = cnt. dr.		5.18	383.36
+ 5' = G.		5.74	382.80
+ 14		6.06	382.48
+ 23 = G at N.E. Cor C.B. Grating		6.48	382.06
+ 23 = F.L. C.B.		8.12	380.42
+ 23 = cnt. dr.		5.82	382.72



see H.

ctr. Bango	388.54	5.0	383.54
+5 = amt. d.		5.24	383.30
+5 = G.		5.64	382.90
+14		5.52	383.02
+23 = G		5.82	382.72
+23 = amt. d.		5.12	383.42

T.R	11.34	39910	0.82	387.72
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Orig. B.M.			4.56	394.54
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Indexed  
C.S.K.

70' wide  
18' cbs  
8.5 1/2

Xsec Russell St. 5 1/2

Willow to Evergreen

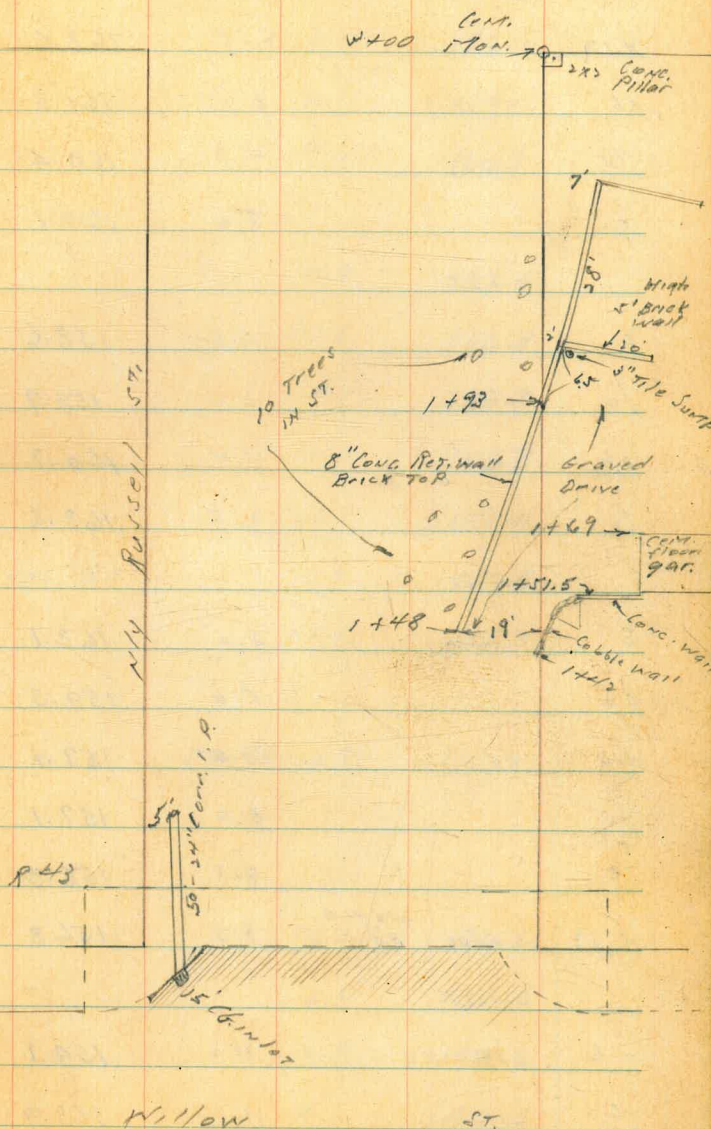
S.W. B.P.	3.81	165.14	161.33	Willow Russell
- 18 Ely cb Willow				
S - 25	cb		2.80	162.34
" "	gut		4.57	161.57
S	par.		4.94	160.80
C	"		5.03	160.11
N	"		5.15	159.99
+ 25	cb		3.55	161.59
"	gut		4.24	160.90
0+00 Ely Willow				
N. Top	cb		4.85	160.29
"	gut		5.81	159.33
C	par		4.94	160.20
S	Top	cb	3.97	161.17
"	gut		4.75	160.39
S.L.			2.4	162.7
FL. Bot.	inlet Box		10.51	154.63
"	OUTLET 24" PIPE		14.2	150.9

Moore  
7-21-28

Evergreen

ST.

30





0+03		
S	1.3	163.8
+12	2.5	162.6
cb	3.6	161.5
1/4	4.7	160.4
c	5.0	160.1

0+25

c	6.5	158.6
1/4	6.2	158.9
cb	4.2	160.7
S	2.5	162.6

0+50

S	3.0	162.1
cb	5.6	159.5
+6	8.0	157.1
1/4	8.0	157.1
c	8.3	156.8

+13	w edge graded Rd.	8.3	156.8
-----	-------------------	-----	-------

0+75

-c	edge Rd	11.0	154.1
c		11.2	153.9

1/4		11.4	153.7
+7		11.2	153.9
cb		8.5	156.6
+8		6.1	159.0
S		5.0	160.1

1+00

S		7.7	157.4
+12		11.3	153.8
+15		14.3	150.8
cb		12.3	150.8
1/4		13.7	151.4
c	edge Rd	13.3	151.8
+10		19.4	145.7

T.P.	0.26	152.48	12.92	152.22
------	------	--------	-------	--------

1+25

-20		16.0	136.5
c		6.2	146.3
1/4		2.9	149.6
cb		3.1	149.4



152.48

cb + 11	3.3	149.2	
S	+ 1.0	153.5	
1 + 42			
S	4.0	148.5	
cb N edge Rd. gravel	4.2	148.3	
1/4	8.3	144.2	
c	12.5	140.0	
+ 25	23.4	129.1	
1 + 48			
beg. Top Ret wall	7.06	149.42	19' N S.L.
... grd ... "	4.8	147.7	
1 + 51.5			
S - 24.6 Cem Apron	3.39		
S - 26 W & Gar.	3.36	149.12	fl. level
1 + 69			
S gravel str.	5.0	147.5	
+ 9 grid	5.1	147.4	
+ 9.5 Top wall	4.0	148.5	
+ 14	6.3	146.2	
cb	8.4	144.1	
1/4	14.3	138.2	

152.48

32

c	20.6	131.9	
+ 25	32.8	119.7	
1 + 93			
S grid	6.1	146.4	
S Top Ret wall	4.97	147.51	
+ 3	6.7	145.8	
cb	16.6	135.9	
1/4	21.2	131.3	
c	25.5	127.0	
+ 30	41.3	111.2	
N + 5 bot. cañon	43.3	109.2	
2 + 25			
S - 7 Top wall	5.60	146.88	
S - 6 grid	7.8	144.7	
S	12.2	140.3	
T.P.	0.14	139.74	12.88 139.60
cb	10.7	129.0	
1/4	14.8	124.9	
c	18.5	121.2	



129.74

C + 25	29.0	110.7
N + 5 bot. cañon	37.2	102.5
2 (+50)		
N bot. cañon	38.6	101.1
N + 15	31.1	108.6
C	23.0	116.7
cb	14.5	125.2
S	7.0	132.7

T.P.	153	128.47	12.80	126.94
------	-----	--------	-------	--------

2 + 75

J	0.0	128.5
cb	8.1	120.4
1/4	17.2	116.3
C	17.7	110.8
+ 6	18.8	109.7
+ 25 bot. cañon	30.8	98.2
N	26.5	102.0
3 + 00 WC Evergreen		
N	33.3	95.2

128.47

33

N + 5 bot. cañon	24.8	94.7		
N + 10	28.4	100.1		
C	20.4	108.1		
1/4	16.0	112.5		
cb	12.1	116.4		
S ON MON.	5.09	122.78		
T.P.	0.38	116.45	1240	116.07

Russell  
SW Evergreen

F Evergreen

S	3.2	113.3
cb	11.5	105.0
1/4	14.8	101.7
C	18.7	97.8
+ 20 bot. cañon	27.3	89.2
E.L. Evergreen		
N + 10	26.2	90.3
N + 22 bot. cañon	24.2	82.3
C	20.5	86.0
cb	24.4	92.1
S	17.8	98.7

Please check  
to Profile



Indexed  
C.S.K.

Moore  
Northbrook  
8-12-38.

X sec alley 20' wide

BK1 Center add. to La Jolla Park

S.E.C.P. 0.75 115.92 115.17 Pearl Girard

0-17 edge Con Gut.

W 2.93 112.99

E 2.81 113.11

0-14 N. cb Pearl

E top cb 2.16 113.76

E gut 3.07 112.85

C " — —

W " 3.16 112.76

W cb 2.23 113.69

0-100 NLY Pearl

W cb 2.05 113.87

W 3.1 112.8

C 2.9 113.0

E 2.8 113.1

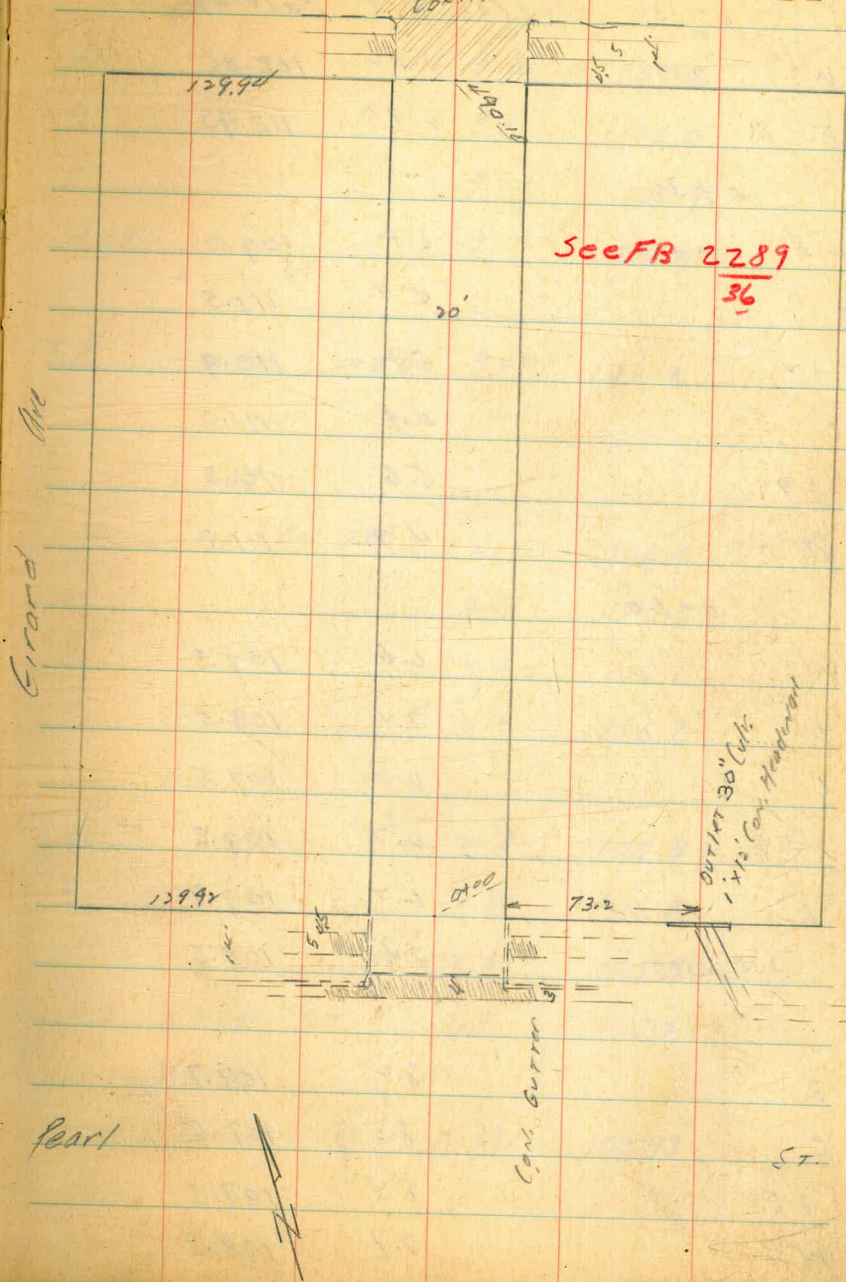
E cb 2.03 113.89

73.2 Ely Top headwall 1.24 114.68

" " FL. 30" Pipe outlet 7.39 108.53

Virginia Way

Con. Pav.





0-13 Nly edge gut. Back up.

W	gut	3.06	112.86
E		2.99	112.93

0+30

-40	wash	6.9	109.0
-----	------	-----	-------

E		4.4	111.5
---	--	-----	-------

+2		5.0	110.9
----	--	-----	-------

C		4.9	111.0
---	--	-----	-------

+9		5.6	110.3
----	--	-----	-------

W		4.7	111.2
---	--	-----	-------

0+60

W		6.6	109.3
---	--	-----	-------

+1		7.4	108.5
----	--	-----	-------

C		6.4	109.5
---	--	-----	-------

+8		6.7	109.2
----	--	-----	-------

E		6.4	109.7
---	--	-----	-------

+35	wash	7.4	108.5
-----	------	-----	-------

1+00

E		8.2	107.7
---	--	-----	-------

C		8.3	107.6
---	--	-----	-------

+5		8.4	107.5
----	--	-----	-------

W		7.7	108.2
---	--	-----	-------

1+30

W		8.3	107.6
---	--	-----	-------

C		9.0	106.9
---	--	-----	-------

E		9.0	106.9
---	--	-----	-------

+10		9.0	106.9
-----	--	-----	-------

T.P.	248	108.60	9.80	106.12
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1+69

-3	S edge 3 car gar.	2.2	106.4	dirty fl.
----	-------------------	-----	-------	-----------

W		2.4	106.2
---	--	-----	-------

C		2.5	106.1
---	--	-----	-------

E		2.4	106.2
---	--	-----	-------

1+97

E		2.8	105.8
---	--	-----	-------

C		2.8	105.8
---	--	-----	-------

W		2.8	105.8
---	--	-----	-------

+3	N edge gar.	2.5	106.1	dirty
----	-------------	-----	-------	-------

2+00

W-2	15 CON. WALK	2.47	105.93
-----	--------------	------	--------



108.60

2+02

-3	Sledge & car gas	2.7	105.9	dirty
W		2.8	105.8	
c		2.9	105.7	
E	original wash	2.9	105.7	

2+37

E		3.5	105.1	
+4		2.1	104.5	
c		3.0	105.0	
W		2.9	105.7	

+3 Sledge &amp; car gas 2.7 105.9 dirty

2+65

-5		4.7	103.9	
W		4.2	104.4	
c		4.5	104.1	
+5		5.3	103.6	
E		4.4	104.2	

3+00

E		5.0	103.0	
c		5.7	102.9	
W		5.4	103.2	
+2		6.6	102.0	
+5		4.6	102.0	

108.60

3+35

-5		7.0	101.6	
-2		7.0	101.6	
W		6.1	102.5	
c		6.3	102.3	
E		6.4	102.2	

3+70

E		6.7	101.9	
c		6.9	101.7	
W		6.6	102.0	
+2		7.4	101.2	
+5		7.4	101.2	

3+90

W	beg. brick wall	7.5	101.1	
c		7.5	101.1	
+5		8.2	100.4	
E		7.0	101.6	

4+30

E		8.1	100.5	
+7		9.5	99.1	
c		8.8	99.8	
W		7.8	100.8	

36



108.60

4+60

W	8.7	99.9
+5	8.7	99.9
C	10.2	98.4
+3	9.0	99.6
E	8.5	100.1

4+80

E	10.0	98.6
C	10.9	97.7
W	9.8	98.8

4+90.1 S'y Virginia

W cb.	11.25	97.35
W Pav	11.38	97.22
C "	11.48	97.12
E "	11.15	97.45
E cb.	10.77	97.83

S cb Virginia

E Pav. gut.	11.60	97.00
W " "	12.00	96.60

Please check to profile

37



Miller Walker 8-22-38		Levels 36 <sup>th</sup> & Univ. for Drainage		36 <sup>th</sup> 80' wide 14' cbs. 13' 1/2	
BM. B.P.	6.09	365.63		359.54	N.W. 36 <sup>th</sup> & Univ. Ave.
	0+00 - 75				
w. d			4.96	360.67	
G			5.46	360.17	
1/4			5.12	360.51	
±			4.96	360.67	
1/4			5.11	360.52	
G			5.82	359.81	
E. d			5.37	360.26	
T.P.	5.08	365.62	6.09	359.54	
	0+00 - 25				
E. d			5.00	359.62	
G			5.57	359.06	
1/4			4.92	359.70	
±			4.72	359.90	
1/4			4.84	359.78	
G			5.34	359.28	
w. d			4.80	359.82	
	0+00 - 6				
w. d			5.04	359.58	
G			5.82	358.80	
FL	End. wing wall		5.75	358.87	

indexed  
C.S.K. 36<sup>th</sup>

38

Plat. E.C.B. 8-24-38		5.11	359.51
1/4			
±		4.94	359.64
1/4		5.06	359.56
+11	End wing wall	5.73	358.89
G		5.82	358.80
E. d		5.18	359.44
	0+00 = N. Line Univ.		
E. d		5.31	359.31
G	F.L. intake N. End. N+S. Culvert	6.15	358.47
+1.5	" " "	4.15	358.47
+2	Head. wall + pav	5.31	359.31
1/4		5.09	359.53
±		5.03	359.59
1/4		5.12	359.50
+11	H.W. + pav.	5.11	359.51
+11.5	F.L. N. End. <sup>N+S.</sup> Culvert	6.00	358.62
G	" " " "	6.00	358.62
w. d		5.12	359.50



365.62

0+14 = N. of Line Univ

W - 50'	cl	5.05	359.57
W - 50'	G	5.55	359.07
W - 25'	G	5.62	359.00
W - 25'	cl	5.14	359.48
W - 06'	"	5.23	359.39
W - 6'	G	5.71	358.91
W	<small>2 end. culverts opening 18' x 4'</small> G	5.94	358.68
W	cl	5.30	359.32
d		5.35	359.27
1/4		5.13	359.49
±		5.14	359.48
1/4		5.27	359.35
d		5.66	358.96
E.	G	4.14	358.48
E	cl	5.75	358.87
+ 25	cl	5.67	358.95
+ 25	G	6.20	358.42
+ 50	G	6.23	358.39
+ 50	cl	5.76	358.86

365.62

0+20 = 6' S. of N. cl

39

E		5.71	358.91
cl		5.53	359.09
1/4		5.28	359.34
±		5.20	359.42
1/4		5.14	359.48
cl		5.26	359.36
W		5.46	359.16

0+32.5 = N. Rail N. Track.

W		4.94	359.68
cl		4.98	359.64
1/4		5.02	359.60
±		5.05	359.57
1/4		5.09	359.53
cl		5.16	359.46
E		5.23	359.39

0+47.5 = S. Rail S. Track

E		5.25	359.37
cl		5.18	359.44
1/4		5.11	359.51
±		5.07	359.55



365.62

0+47 E con

14	5.03	359.59
cl	5.00	359.62
W	4.96	359.66

0+60 = 4' N of S. cl.

W	5.58	359.04
cl	5.41	359.21
14	5.30	359.32
cl	5.26	359.36
14	5.44	359.18
cl	5.53	359.09
E	5.80	358.82

0+66 = S. cl. Univ.

E-50	cl	6.05	358.57
E-50	G	6.43	358.19
E-25	G	6.36	358.26
E-25	cl	5.91	358.71
E	cl	5.80	358.82
E	G	6.12	358.50
cl		5.70	358.92
14		5.48	359.14

365.62

40

cl	5.33	359.29
14	5.44	359.18
cl	5.54	359.08
+12	5.97	358.65
W. G. <sup>(E. end. culvert)</sup> opening 18' x 4'	6.23	358.39
W. cl	5.63	358.99
+3 G	6.08	358.54
+6 cl	5.62	359.00
+6 G	6.00	358.62
+25 G	5.98	358.64
+25 cl	5.53	359.09
+50 cl	5.46	359.16
+50 G	5.91	358.71

0+80 = S. Line Univ.

W. cl	5.63	358.99
G F.L. outlet N + S. culvert	6.63	357.99
+1.5' " " " "	6.61	358.01
+2 Wing wall + pav.	5.71	358.91
14	5.66	358.96
cl	5.47	359.15
14	5.69	358.93
+11 wing wall + pav	5.90	358.72



		365.62	
711.5	F.L. Outlet	N+S. Culvert	6.77 357.85
G	"	"	6.77 357.85
E.d			5.86 358.76
0+85 = S. End. Wing walls			
E.d			5.94 358.68
G			6.85 357.77
72	S. End. Wing wall		6.76 357.86
14			5.75 358.87
⊕			5.51 359.11
14			5.72 358.90
711	S. End. Wing wall		6.48 358.14
G			6.58 358.04
W.d			5.75 358.87
1+05			
W.d			6.19 358.43
G			6.83 357.79
14			6.22 358.40
⊕			5.90 358.72
14			6.23 358.39
G	in drive		7.01 357.61

		365.62	
		1+30	
E.d			6.83 357.79
G			7.42 357.20
14			6.46 357.96
⊕			6.43 358.19
14			6.58 358.04
G			7.15 357.47
W.d			4.61 358.01



8-25-34  
Miller  
Walker  
Bliss  
B.M.B.P.

Marcey St. X Sec. 28<sup>th</sup> to 29<sup>th</sup>  
Spacing of N. ch. + 1/4 vary see Plat Page 44.  
10' ch. on S.

N.W. 28<sup>th</sup> ↓  
Logan.

	9.18	75.20	66.02
00-10' = E. ch. 28 <sup>th</sup>			
S. Line N. End. cut-d.	6.73		69.07
" " "	6.80		68.40
ch	6.60		68.60
"	6.45		68.75
±	6.34		68.86
"	6.15		69.05
ch	6.00		69.20
N G	5.77		69.43
N. ch.	5.20		70.00

0+00 = E. Line 28<sup>th</sup> st

N. cut. d.	5.18		70.02
G. par. E. End.	5.65		69.55
1/4 " " "	5.74		69.46
± " " "	5.83		69.57
" " " "	6.08		69.12
1/8 " " "	6.1		69.1
d div. d.	5.7		69.5
S.	5.8		69.4

No ch or walk. Return S. E. cor

10' Conc. walk + curb combination on N from 0+00 to 4+55

68.45 NW  
29<sup>th</sup> + Logan  
Indexed  
C.S.K. 75.20

		0+35	
S		4.6	70.6
d		4.2	71.0
1/4		4.7	70.5
±		4.7	70.5
1/4		5.0	70.2
G		5.5	69.7
N cut. d		4.66	70.54
		1+00	
N. cut. d		3.64	71.56
G		4.6	70.6
1/4		4.0	71.2
±		3.6	71.6
1/4		3.6	71.6
d		3.3	71.9
S.		3.4	71.8
		1+50	
S		3.0	72.2
d		2.8	72.4
1/4		2.9	72.3
±		3.0	72.2



75.20

N. 1/4		3.2	72.0	
G		3.6	71.6	
N. ent. d.		2.96	72.24	✓
1 + 58 W. End. ent. d. on 40's. of N. d.				
40' s. of N. d.	W. End. ent. d.	2.37	72.83	
" " "	ground	2.8	72.4	
1 + 65 W. Edge ent. walk.				
N. ent. d.		2.79	72.41	✓
G. on N. End w. side walk		3.26	71.94	
1/4	" " "	2.75	72.45	
⊕	" " "	2.56	72.64	
1/4	" " "	2.46	72.74	
⊕	" " "	2.37	72.83	
40' s. of N. d.	" " "	2.33	72.87	
" " " "	E. End. ent. d.	2.38	72.82	
1 + 79 = E. Edge ent. walk.				
40' s. of N. d.	W. End. ent. d.	2.32	72.88	
40' s. of N. d.	E. side ent. walk.	2.26	72.94	
⊕	" " " "	2.32	72.88	
1/4	" " " "	2.34	72.86	
⊕	" " " "	2.46	72.74	

75.20

Marcey

43

1/4	E. side ent. walk.	2.64	72.56	
G. N. End	" " "	3.01	72.19	
N. ent. d.		2.54	72.64	
2 + 00 Brk. Grade N. ent. d.				
N. ent. d.		2.17	73.03	
G		3.0	72.20	
1/4		2.9	72.3	
⊕		2.8	72.4	
1/4		2.7	72.5	
⊕		2.3	72.9	
S		2.4	72.8	
2 + 50				
S		2.6	72.6	
⊕		2.5	72.7	
1/4		2.7	72.5	
⊕		2.6	72.6	
1/4		2.8	72.4	
G		3.2	72.0	
N. ent. d.		2.55	72.65	



75.20

3+00

N. ent. d		2.88	72.32
G		3.4	71.8
1/4		3.0	72.20
Φ		3.0	72.2
1/4		3.2	72.0
cl		3.3	71.9
S		3.9	71.3

3+03

Drain pipe under cl gutter = F.L. 3.74 71.46 Wheek side

T.P. 3.34 75.51 3.03 72.17

3+30

N. cl. dipped for drive & gutter 4.04 71.47

3+15 double garage on S. dirt floor on S. line

S-2 floor 4.3 71.2

cl 3+30 garage on S. dirt floor on S. line

S-2 floor 4.5 71.0

75.51

Marcey

44

3+50

S		4.7	70.8
cl		4.1	71.4
1/4		3.8	71.7
Φ		3.5	72.0
1/4		3.6	71.9
G		4.0	71.5
N. ent. d		3.64	71.87

3+62 clv tripple garage on S. dirt floors 1.0 m st

S-2 Back 4.8 70.7

3+96 garage on S. dirt floor 1.0 m st.

S-2 floor 4.1 70.9

4+00

N. ent. d		4.00	71.51
G		4.4	71.1
1/4		3.6	71.9
Φ		3.5	72.0
1/4		3.6	71.9
cl		3.9	71.6
S		4.1	70.9



75.51

4+08 garage on S. dirt floor 0.8 in st.

S-2 floor 4.2 71.3

4+07 E. End. ent. wall on N.

4+32 garage on S. dirt floor 0.8 in st.

S-2 = floor 4.0 71.5

4+55 = E. End. ent. d. on N.

S. 4.1 71.4

ch 4.1 71.4

1/4 4.0 71.5

d 4.0 71.5

1/4 4.0 71.5

G 4.6 70.9

N. ent. d. 4.35 71.6

X Line 4.1 71.5

4+88 double garage on S. dirt floor on S. Line

Floor 4.0 71.5

5+00

N 4.5 71.0

d 4.8 70.7

1/4 4.6 70.9

d 4.5 71.0

75.51

Marcy

45

1/4 4.5 71.0

d 4.5 71.0

S. 4.5 71.0

5+20 garage on S. dirt floor on S. Line

floor 4.7 70.8

5+47 garage on S. dirt floor on S. Line

floor 5.0 70.5

5+50

S 4.9 70.6

d 4.9 70.6

1/4 5.2 70.3

d 5.1 70.4

1/4 4.9 70.6

d 4.9 70.6

N 4.5 71.0

5+60 garage on S. dirt floor on S. Line

5.0 70.5

5+20 garage on S. dirt floor Baels

5.0 70.5











6+50

6+00

5+50

4+97<sup>87</sup>

F.C.

Nail  $\phi$ 

Def. 2.

7° 30'

4+50

6° 15'

Curve  $\bar{\gamma}$ 

4+00

 $\Delta = 152.00'$ 

4° 57'

 $R = 1100.00$ 

3+50

 $T = 144.81$ 

3° 39'

 $L = 287.94$ 

3+00

 $EY = 9.50$ 

2° 20.8'

2+50

1° 02.7'

2+09<sup>89</sup>

B.C.

15200' Rt.

Nail  $\phi$ 

R.P. Hub

14.0'

30.0'

R.P. Hub

Nail P.I.

R.P. Hub

12.0'

20.0'

R.P. Hub



11+00

10+50

10+19.4 E.C.

Def. Ls  
9-51'

10+00

9-14.5'

9+50

7-39'

Curve 2

9+00

$\Delta = 19-42'$  6-03.5'

R = 900.0'

8+50

T = 156.27' 4-28'

L = 309.45'

8+00

E<sub>x</sub> 13.5' 2-52.5'

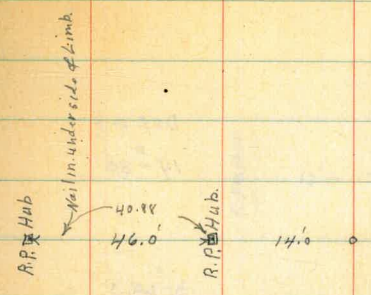
7+50

1-17'

40.34'

7+09.66 B.C.  $\angle 19-42'$  Lt

7+00



R.P. Hub.

13.0'

20.0'

R.P. Hub.



15+00

14+70<sup>26</sup> E.C.Def Ls  
14°-30'

14+50

13°-20.3'

14+00

Curve 3 10°-28.4'  
Δ=29°-00'

13+50

R=500' 7°-36.5'

T=129.31

13+00

L=253.07 4°-44.6'

E=16.5

12+50

1°-52.7'

12+17.1<sup>19</sup> BC

Δ 29°-00'

12+00

11+50

R.P. Hub.

12.6

Nail

22.6

R.P. Hub.

R.P. Hub.

20.0

Nail

R.P. Hub.

18.35

Nail

50.21



19+00

18+50

✓ 18+15<sup>54</sup> E.C.

• 45-47

18+00

42-36.3

□  
curve

+50

Δ 91-34 32-22.4

R = 140.0

17+00

T = 143.88 22-08.5

L = 223.74

+50

11-54.6

16+00

1-40.7

✓ 15+91<sup>80</sup> B.C. L 91-34 Lt.

15+50

R.P. Hub

25.0

R.P. Hub

25.0

0

R.P. Hub

45.0

25.0

R.P. Hub



22+96<sup>89</sup> B.C. C.T.L.P.  $\phi$

15.69

22+81<sup>85</sup> C.T.L.P.  $\phi$  R.P.  
22+80<sup>70</sup> End. of conc. Ford.

22+73<sup>20</sup> E.C.

D = 4.2  
35-19'

Curv<sup>+</sup> 5

22+50

$\Delta 70-38'$  31-24.3

R = 170.0

22+00

T = 120.44 22-58.7

L = 209.57

+50

14-33.2

21+00

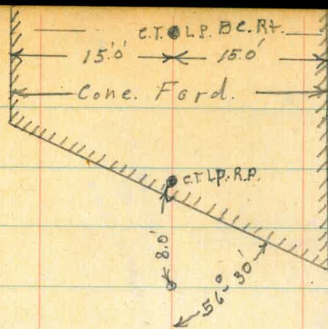
6-07.7

20+63<sup>63</sup> B.C.  $\angle 70-38'$  R.P.

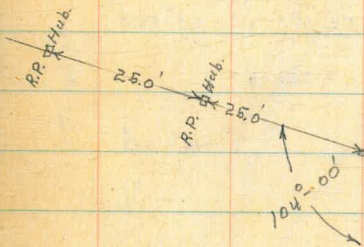
20+50

20+00

19+50

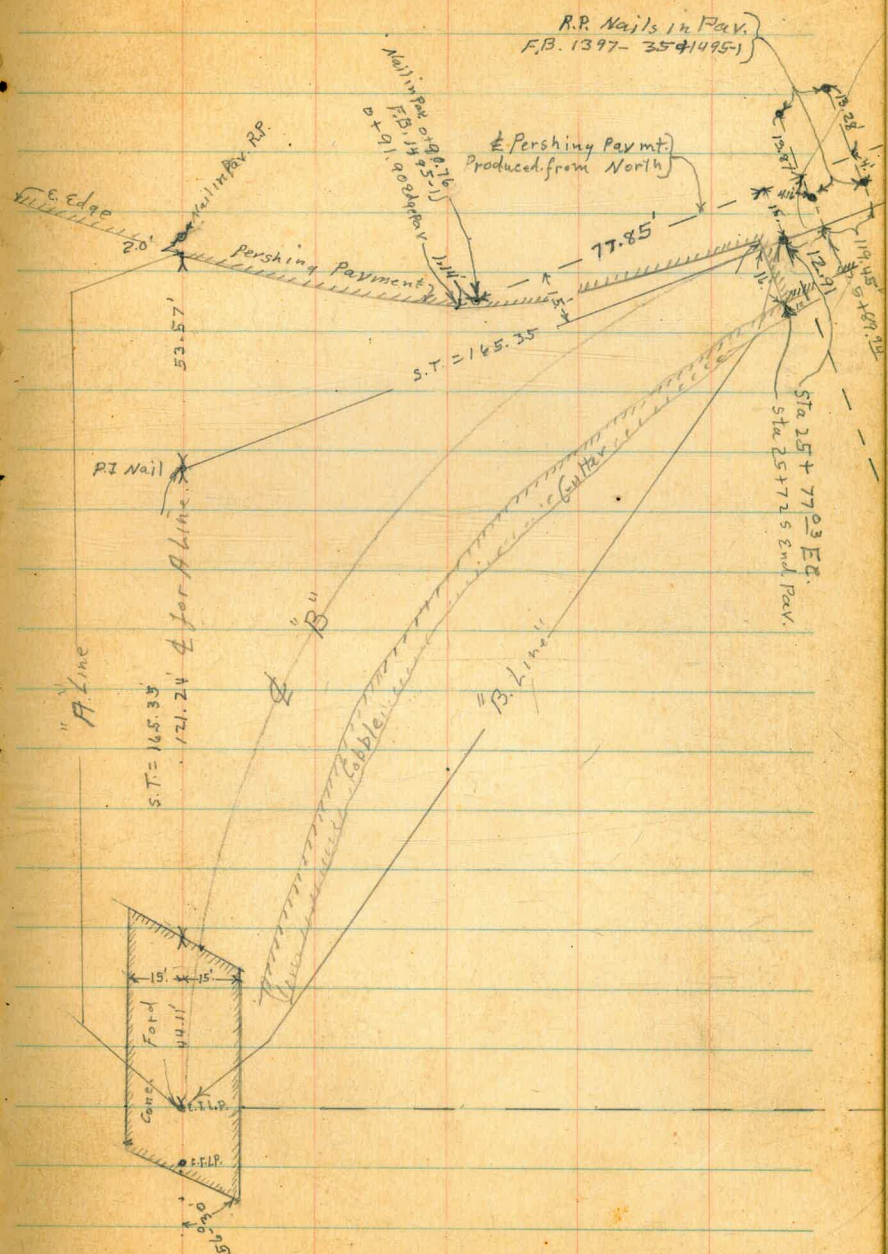


52





25+77 <sup>03</sup> E.C.	Def Ls 38°-13'
25+50	34°-32'
25+00	$\Delta 76^{\circ}-26'$ R=210'
24+50	T=165.35 20°-53.5'
	L=280.14
24+00	14°-04.3'
23+38 <sup>29</sup> N. End. conc. apron	5°-40'
22+96 <sup>89</sup> B.C. $\Delta 76^{\circ}-26'$ Rt.	
13.69 A.P.C.T.L.P. $\nabla$	
22+81 <sup>20</sup> $\nabla$	
22+80 <sup>20</sup> $\nabla$ S. End. Conc Ford.	









X Sec. 26<sup>th</sup> St. Russ to Park

B.M. N.W. 1/4	241	207.53 ✓	205.12	26 <sup>th</sup> 1/4 A. St.
B.M. B.P. N.W. 26 <sup>th</sup> 1/4 A.	247	205.06 ✓		
	0+00 =	{ S. Line Russ. Bl. rd. " " Balboa Park.		
20' Lt = d	N. End	4.42	203.11	
20" "	E. pav. N. End	5.07	202.46	
15" "	" "	4.83	202.70	E. edge oil pav
16" "	" "	4.60	202.93	
±	" "	4.31	203.22	
10' Rt	" "	4.63	202.90	E. edge oil pav. N
2' "	" "	5.10	202.43	
20' "	d " "	4.45	203.08	
	0+24 1/2	P.C. Edges of Rd. E. & W.		
20' Rt. d		4.71	202.82	
20' "		5.4	201.1	
15" "	E. edge oil pav.	5.45	202.08	
10' Rt	" "	5.24	202.2	
±	" "	5.00	202.5	
10' Lt	" "	5.46	202.07	
15" "	W. edge " "	5.70	201.83	
18" "		5.9	201.6	
20" "		5.1	202.4	

207.53

0+32 1/2 ± Δ 19-18 Lt { Sec. at 86-42 to 26<sup>th</sup> St  
produced from S. 26<sup>th</sup> St

55

20' Lt		6.3	201.2
10' "	N.W. Edge oil Pav	5.6	201.9
4' "	N.W. " " "	5.18	202.35
±	" " "	5.11	202.42
10' Rt	" "	5.40	202.13
17' Rt	E. edge " "	5.66	201.87
20' Rt		5.5	202.0
	0+50	Sec. at 86-42 to 26 <sup>th</sup> produced from S.	
20' Rt	on oil pav	5.60	201.9
10' "	N.W. edge " "	5.38	202.15
±		5.6	201.9
10' Lt		6.2	201.3
20' Lt		7.0	200.5
	0+70 1/2	Sec. at 86-42 to 26 <sup>th</sup> St.	
20' Lt		7.1	200.4
10' "		6.9	200.6
±		6.4	201.1
10' Rt		5.9	201.6
20' "		5.5	202.0
24' "	W. Edge oil Pav.	5.45	202.08



207.53

1+01.75 sec at 86-42 to 26<sup>th</sup> st

20' RT	oil Pav	8.0	199.5
14' "	W. edge " "	8.2	199.3
10' RT		8.5	199.0
±		8.7	198.8
10' LT		8.8	198.7
20' LT		8.9	198.6

1+15 sec at 86-42 to 26<sup>th</sup> st

20' Lt		10.7	196.8
10' "		10.1	197.4
±		10.3	197.2
10' RT		10.2	197.2
12' "	N.W. Cor Oil Pav	10.2	197.3
20' E r. "	End " "	10.5	197.0

1+43 86

20' RT		12.5	195.0
12.8" Top	E. db. at P.C.	12.78	194.75
12' "		13.2	194.3
±		13.2	194.3
14' LT	W. edge Rd.	13.0	194.5 Limit
T.P.	0.03	194.54	13.02 194.51 ✓

194.54 ✓

2+02 36

56

16' Lt = W. edge Rd		4.1	190.4	Limit
±		4.6	189.9	
11' RT = N. end. ch. cat. Rd.		4.87	189.77	18" x 18"
12.7 "		4.5	190.0	
12.8 " N. end. cut. ch.		4.17	190.37	
17. "		4.0	190.5	
20' "		2.4	192.1	

2+30

20' RT		3.3	191.2	
14 RT		5.7	188.8	
13' "	E. Rd.	7.4	187.1	
±		7.5	187.0	
10' Lt	W. Rd	7.4	187.1	Limit

3+00

10' Lt	W. Rd.	10.3	184.2	Limit
±		10.5	184.0	
14 RT	E. Rd.	10.4	184.1	
16 RT		8.6	185.9	
20' "		7.1	187.4	



194.54

20' RT		3+50 10.9	183.6	
13" E.Rd		13.6	180.9	
⊕		13.9	181.1	
1' Lt = W. Rd		13.0	181.5	Limit

T.P. 0.41 181.91 13.04 181.50

4+00

12' Lt W. Rd		3.1	178.8	Limit
⊕		3.5	178.4	
11' RT E. Rd.		3.7	178.2	
13' "		2.5	179.4	
20' "		2.8	179.1	

4+50

20' RT		5.9	176.0	
13' "		5.4	176.5	
11' " E. Rd		6.9	175.0	
⊕		6.5	175.4	
12' Lt = W. Rd		6.3	175.6	Limit

181.91

12' Lt = W. Rd.		5+00 9.5	172.4	57 Limit
⊕		9.5	172.4	
11' RT		9.6	172.3	
13' "		8.7	173.2	
20' "		8.7	173.2	

5+50

20' RT		11.0	170.9	
11' "		12.0	169.9	
10' " = E. Rd		12.7	169.2	
⊕		12.5	169.4	
12' Lt W. Rd.		12.6	169.3	Limit

T.P. 0.42 169.43 12.90 169.01

5+65

12' Lt = W. Rd.		1.0	168.4	Limit
⊕		0.9	168.5	
10' RT = E. Rd		0.9	168.5	
20' "		4.0	173.4	



169.43 ✓

20' RT	6+00 +0.7	170.1	
11' " = E. Rd	3.3	166.1	
⊕	2.9	166.5	
12' Lt = W. Rd	2.9	166.5	Limit

6+50

11' Lt = W. Rd	5.6	163.8	Limit
⊕	5.5	163.9	
13' RT = E. Rd	5.7	162.7	
20' "	3.6	165.8	

6+75

11' RT = W. edge catch Basin	7.24	162.19	18" x 18" Top
------------------------------	------	--------	------------------

6+80

12' Lt = E. edge catch Basin	7.16	162.27	18" x 18" Top
------------------------------	------	--------	------------------

6+97

20' RT	4.0	165.4	
14 "	5.0	164.4	
12 " E. Rd	8.5	160.9	
⊕	8.3	161.1	
11.4 = W. Rd	8.1	161.3	Limit

169.43

11' Lt = W. Rd	7+00 8.2	166.2	58 Limit
⊕	8.5	160.9	
11' RT = E. Rd	8.7	160.7	
20' "	7.0	162.4	

7+50

20' RT	11.5	157.9	
12' " = E. Rd	10.9	158.5	
⊕	11.2	158.2	
11' Lt = W. Rd	10.9	158.5	Limit

T.P. 1.80 / 58.26 12.97 156.46

8+00

11' Lt = W. Rd	2.0	156.3	Limit
⊕	2.3	156.0	
13' RT = E. Rd.	2.5	155.8	
20' "	1.5	156.8	

8+39

20' RT	+0.7	158.33	
17 "	3.1	155.2	
13' " E. Rd	3.7	154.6	



158.26

±	4.0	154.3	
10' Lt = W. Rd	3.8	154.5	Limit
	8+60		
10' Lt = W. Rd	4.5	153.8	Limit
±	4.7	153.6	
13' Rt = E. Rd	4.3	154.0	
20''	3.8	154.5	
	9+00		
20' Rt	3.2	155.1	
14''	5.4	152.9	
13'' = E. Rd.	5.4	152.9	
±	5.8	151.5	
10 Lt = W. Rd	5.4	151.9	
	→ out of place 8+86		
12' Rt. = W. edge	18" x 18"		
catch Basin	6.08	152.18	
	→ out of place 8+92		
11' Lt = E. edge	18" x 18"		
catch Basin	6.15	152.11	
	9+50		
12' Lt = W. Rd	6.8	151.5	Limit
±	7.2	151.1	
14 Rt = E. Rd	7.0	151.3	
15''	3.2	155.1	
20''	1.4	156.9	

158.26

10+00

59

20' Rt	3.3	155.0	
16''	3.8	154.5	
12'' = E. Rd.	8.5	149.8	
±	8.6	149.7	
11' Lt = W. Rd.	8.4	149.9	Limit
	10+38		
11.4 = W. Rd.	9.4	148.9	Limit
±	9.6	148.7	
12 Rt = E. Rd.	9.4	148.9	
20''	8.3	150.0	
	10+40		
11.5 Rt = W. edge	15" x 18"		
catch Basin	10.08	148.18	Top



158.26

20. RT	1/2 ditch	10+41	10.4	147.9	
13 "	E. End. intel	14' Iron pipe culvert	11.8	146.5	FL.
12 "	E. Rd.		9.4	148.9	
⊕			9.6	148.7	
11' Lt	= W. Rd.		9.4	148.9	Limit

10+44

12' Lt	= E. Edge catch Basin	18' x 14"	9.49	148.77	Top.
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10+60

11' Lt	= W. Rd.		9.9	148.4	Limit
⊕			10.2	148.1	
12' Rt	= E. Rd.		9.9	148.4	
15 "			5.3	153.0	
20' Rt			3.8	154.5	

11+00

20 Rt			5.4	152.9	
14 "			6.4	151.9	
13 "			12.0	146.3	
⊕			11.6	146.7	
11' Lt	= W. Rd.		11.1	147.2	Limit

T.P.

158.26

11' Lt	= W. Rd.	11+50	14.0	144.3	Limit
⊕			14.5	143.8	
11' Rt	= E. Rd.		14.8	143.5	
15 "			8.8	149.5	
20 "			8.0	150.3	

T.P.	0.28	146.41	12.13	146.13	
------	------	--------	-------	--------	--

12+00

20' Rt			0.2	146.2	
14 "			3.0	143.4	
12' Rt	= E. Rd.		5.9	140.5	
⊕			5.8	140.6	
12' Lt	= W. Rd.		5.4	141.0	Limit

12+50

12' Lt	= W. Rd.		8.6	137.8	Limit
⊕			8.8	137.6	
11' Rt	= E. Rd.		8.7	137.7	
20 "			8.2	138.2	



146.41

13+00

20' RT	9.1	137.3	
10' = E. Rd	11.1	135.3	
±	11.7	134.7	
14' Lt = W. Rd	11.9	134.5	Limit
30' R		138	

T.P. 1.82 135.18 13.05 133.36

13+21

15.3 Rt = E. end inlet Culvert			covered with dirt
7.3 Rt = W. edge catch Basin	1.55	133.63	Top. 18" X 18" Grate

13+33

13.5 Lt = E. edge catch Basin 2.74 132.40 Limit

13+50

12' Lt = W. Rd. 4.1 132.3 Limit

± 3.7 132.5

11' Rt = E. Rd. 3.4 132.8

20' " + 0.4 135.6  
40' " 142.9

14+00

20' Rt 2.7 132.5

16' " 4.4 130.8

14' Rt = E. Rd 6.9 128.3

40' R 141.7  
65' R 151.6

135.18

61

± 7.1 128.1

11' Lt = W. Rd 7.3 127.9 Limit

14+50

10' Lt = W. Rd 10.4 124.8 Limit.

± 10.3 124.9

14 Rt = E. Rd 10.0 125.2

16' " 6.9 128.3

20' " 5.9 129.3

40' " 138.3  
75' " 152.4

15+00

20' Rt 9.9 125.3

45' " 134.3

16' " 12.3 122.9

75' " 144.8

14' " = E. Rd. 13.5 121.8

85' " 148.9

± 13.9 121.3

10' Lt = W. Rd 13.4 121.4 Limit.

T.P. 0.40 122.73 12.85 122.33

15+50

12' Lt = W. Rd. 4.7 118.0 Limit.

± 4.5 118.2

14' Rt = E. Rd 4.2 118.5

20' " 2.1 120.6

55' " 130.8

85' " 141.2



122.73

16+00

20' RT	6.3	116.4	
50' "		125.0	
14' " = E. Rd.	6.4	116.3	
65' "		128.4	
⊕	7.3	115.4	
16' Lt = W. Rd	8.1	114.6	Limit
16+50			
16' Lt S.W. Rd.	10.8	111.9	Limit
⊕	10.1	112.6	
25' Rt = Ave. Rd	7.8	114.9	
33' Rt		110.8	Limit
36' " edge of grass		112.4	
60' "	17+00	113.1	
28' Rt			Limit
22' Rt = N. Rd.	10.9	111.8	
⊕	12.8	109.9	
14' Lt = E. End. N. edge conc gutter	13.5	109.2	
30' R. edge of grass		108.4	
60' "		107.5	

T.P. 0.33 110.08 12.98 109.75

17+50

15.4' Lt = N. edge conc gutter	2.40	107.7	Limit
⊕	2.9	107.2	
20' Rt	2.0	108.1	
28' Rt Fence edge Fairway	2.9	107.2	Limit
50' Rt	5.5	104.6	

110.08

Edge of Fairway 18+00

19.5' Rt Golf Fence.	6.2	103.9	
16' dirt waterway	7.0	103.1	
14' Rt = N. Rd.	4.3	105.8	
⊕	5.5	104.6	
16.7' Lt = N. edge conc gutter	5.80	104.3	Limit
18+50			
15.4' Lt N. edge conc gutter	8.05	102.03	Limit
⊕	7.9	102.2	
14' Rt	7.3	102.8	
18' " Waterway	9.2	100.9	
20' " edge of Fairway	8.9	101.2	

19+00

20' Rt. edge Fairway	10.7	99.4	
17' R Waterway	11.2	98.9	
14' " = N. Rd	9.5	100.6	
⊕	10.0	100.1	

15.2' Lt = N. edge conc Gutter 10.13 99.95 Limit

19+12

15.2' Lt N. End N. edge conc gutter 10.40 99.68 Limit



	110.04			
15' Lt = S. Rd.	19+50	11.4	98.7	limit
ϕ		11.6	98.5	
12 Rt = N. Rd.		11.1	99.0	
17' "		13.0	97.1	
20' "		13.5	96.6	
40' " = Fairway		14.0	96.1	
	20+00			
20' Rt.		15.1	95.0	
11' " N. Rd.		12.7	97.4	
ϕ		12.9	97.2	
16' Lt S. Rd.		12.6	97.5	limit
T.P.	1.41	98.51	12.98	97.10
	20+50			
16' Lt = S. Rd.		1.3	97.2	limit
ϕ		2.3	96.2	
11' Rt = N. Rd.		2.7	95.8	
14' "		4.2	94.3	
20' "		4.4	94.1	

	98.51			63
20' Rt	21+00	4.7	93.8	
14' " N. Rd.		4.2	94.3	
ϕ		3.3	95.2	
16' Lt = S. Rd.		1.9	96.6	limit
	21+50			
20' Lt S. Rd.		3.4	95.1	limit
ϕ		4.2	94.3	
6' Rt		5.3	93.2	
16' Rt = N. Rd.		5.5	93.0	
20' "		5.4	93.1	
	22+00			
20' Rt		5.9	92.6	
17' " N. Rd.		6.3	92.2	
ϕ		5.2	93.3	
20' Lt S. Rd.		4.9	93.6	limit
	22+50			
11' Lt = S. Rd.		6.3	92.2	
ϕ		6.5	92.0	
16' Rt = N. Rd.		6.5	92.0	
20' "		6.4	92.1	







104.75 -  
"A" 24+50

20' Lt	14.3	90.5
11.4 S. Rd.	14.1	90.7
ϕ	13.0	91.8
20' Rt	11.3	93.5
"A" 24+80		
40' Rt	9.9	94.9
20' Rt	11.1	93.7
ϕ	12.9	91.9
20 Lt. S. Rd.	14.6	90.2

Measurements Lt + Rt are on axes along E. edge Pav.  
 "A" According to Latest Widening Plans.  
 "A" 25+15<sup>SE</sup> ϕ = E. Side Pershing Drive

100 Lt = E. Edge Pav.	16.0	88.8
80 " " " "	15.5	89.3
60 " " " "	15.1	89.7
40 " " " "	14.5	90.3
20 " " " "	13.7	91.1
ϕ " " "	12.7	92.1
20 Rt " " "	11.5	93.3
40' " " " "	10.2	94.6
60' " " " "	8.9	95.9
80' " " " "	7.5	97.3

104.75 -  
"B" 24+00

65

"B" Line = Curve "6"

16' Rt = W. edge cobble gutter	12.1	92.7
ϕ	11.9	92.9
20' Lt	12.0	92.8
24+50		
20' Lt	10.2	92.6
ϕ	10.1	92.7
16' Rt	10.1	92.7
17.5' " = wedge cobble gutter	10.4	92.4
"B" 25+00		
19.5' Rt = wedge cobble gutter	7.4	97.4
18	7.0	97.8
ϕ	7.1	97.7
20' Lt	7.3	97.5
"B" 25+50		
7 Lt = E. Edge Pershing Pav	3.93	100.82
ϕ	4.0	100.8
16' Rt	4.4	100.4
16.5' " = w. edge cobble gutter	4.7	100.1



104.75 -

16. Rt = s. Edge Pav. 25+72 S. End. Pav.  
W. " Cobble gutter 3.2 101.6

ϕ S. Edge Pav 2.52 102.23

0.8 Lt } E. " Pershing Pav. 2.50 102.25

15. " on pav. 3.03 101.72

25 = 89.24

15. Lt. 1.87 102.88

ϕ 1.41 103.34

14.8 Rt } E. Edge Pav.  
W. edge conc gutter 2.00 102.75

chk. B.M. S. E. Cor Cobble Bridge

Pershing Drive West of } 14.73 90.02 = 89.88

Powder House Lane Road



10-8-38

Realignment 26<sup>th</sup> St  
See Page 47.

See C. Books 188-54

67

5+13<sup>12</sup>

E.C.

Defn.  
0  
6-36

4+80

5-48

Δ 13-12

4+40

4-40.6

R = 1200.

T = 138.84

L = 276.41

4+00

3-53.3

3+60

2-56

3+20

1-58.7

2+80

1-01.4

2+37<sup>21</sup>

B.C.

∠ 13-12 Rt.

0+32<sup>75</sup>

∠ 17-30 Lt.

0+24<sup>48</sup>

P.C. Edge of Road. on E. & W.

0+00 = S. Line Balboa Park.



Final Meas. of Alley

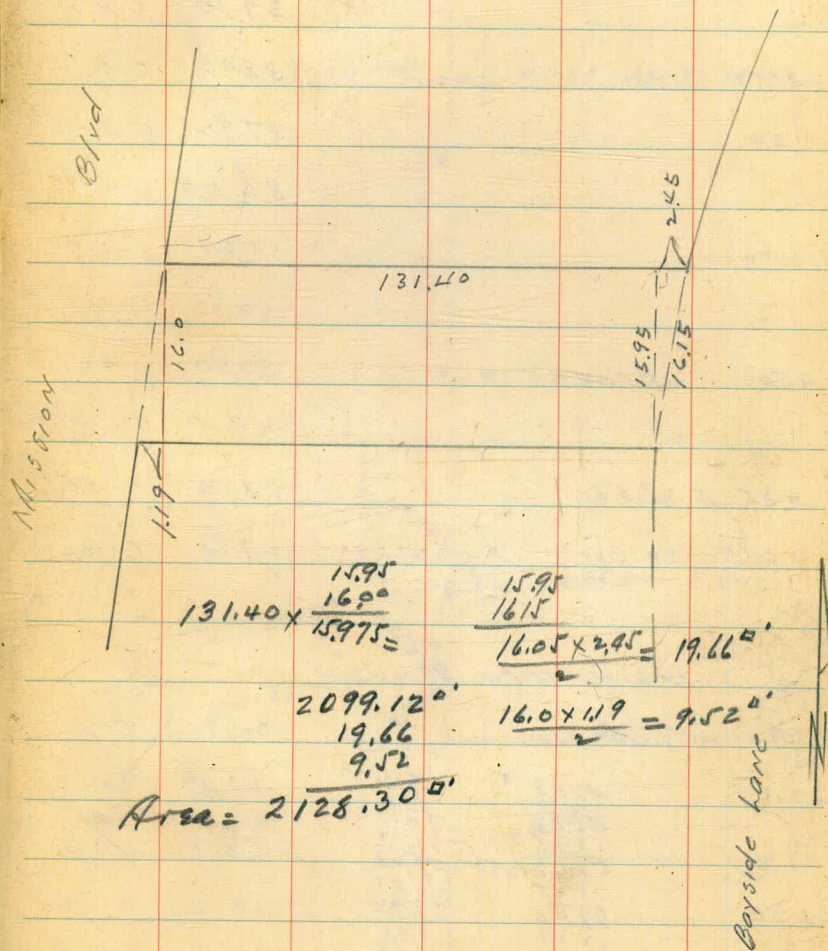
Blk 147 Mission Beach

Moore

Hale 9-25-40

INDEXED  
E.F.B.

68





10" Drain on Rosecrans  
Rogers N.Y.

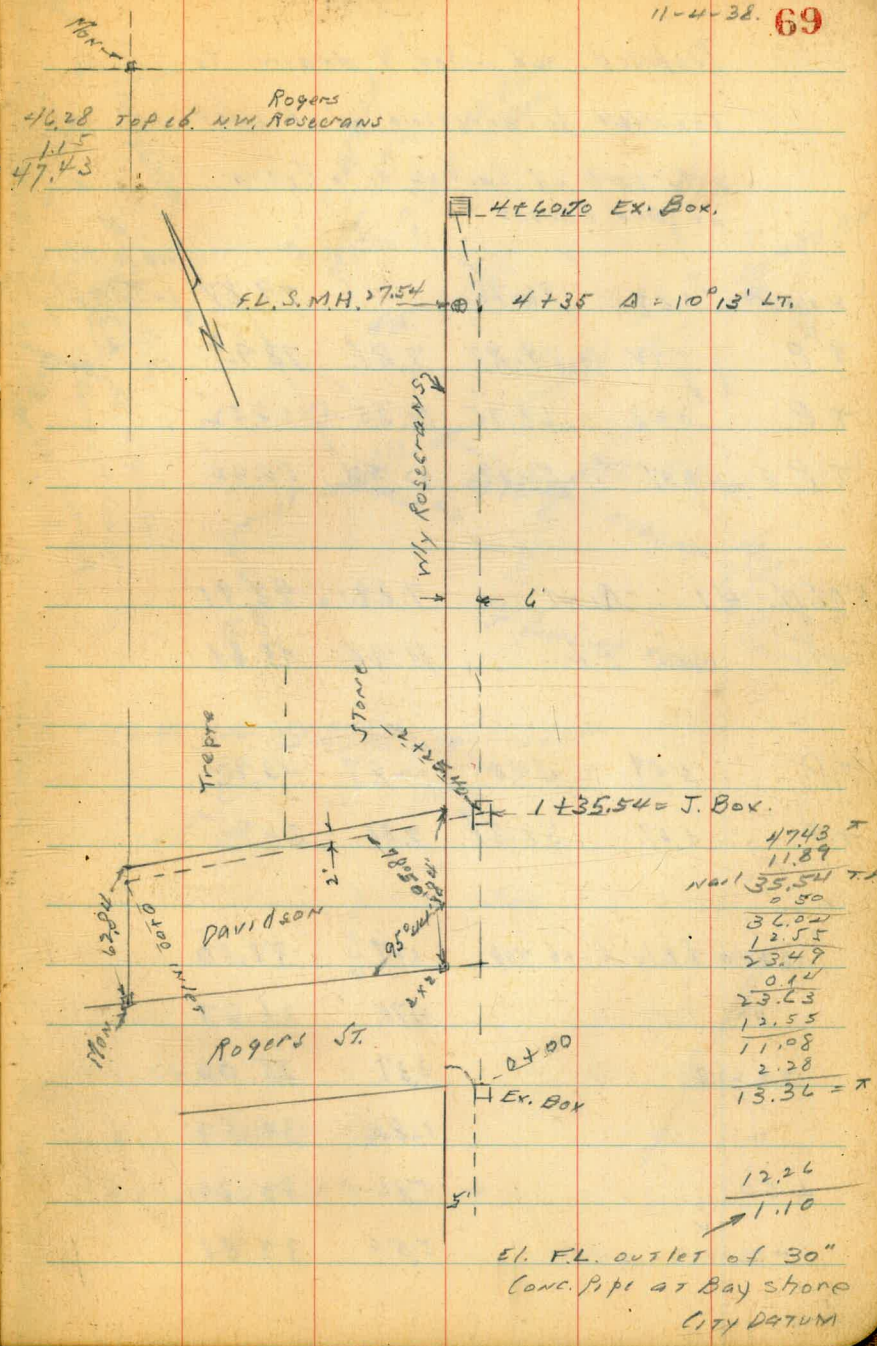
Indexed  
C.S.K.

	FL.	
0+00 Ex. Box Sly Rogers	43.50	ON C6. C 3.80
0+53 Nly Rogers	41.60	C 4.70
1 +00	39.70	C 4.12
1 +35.54 J. Box	38.46	C 3.55
1 +50	37.92	C 3.40
2	36.06	C 4.40
+50	34.21	C 3.40
3	32.25	C 4.03
+50 Break	30.50	C 4.10
4	29.32	C 3.67
+35 A 10°13' LT.	28.50	C 3.87
+60.70 Ex. Box. F.L. = 26.23	27.50	C 3.80

Drain thru Davidson

0+00 = Wly Davidson		74.90	C 2.0
+50	47.43 π 0.80 46.63	69.02 T.P. 1.13 70.15	66.82 C 2.20
1	12.05 58.68	11.72 58.43	58.74 C 2.74
+50	0.25 58.43	0.51 58.94	50.66 C 2.22
2	12.69 71.14	13.05 45.89	42.58 C 3.37
	2.10 69.02	46.63	
+25.4 - J. Box.	8.71 77.73 π 8.71	0.74 ✓	38.46 C 3.55
	69.02 T.P.		

Moore  
11-4-38. 69



4743 π
11.89
Nail 35.54 T.P.
0.50
36.02
12.55
23.47
0.12
23.63
12.55
11.08
2.28
13.36 = π

12.26  
1.10  
El. FL. outlet of 30"  
Conc. Pipe at Bay shore  
CITY DATUM







3837

0+75	cb	5.99	32.38
"	gut	6.48	31.89
1+00	cb	6.24	32.13
"	gut	6.68	31.69
1+15	cb	6.26	32.11
"	gut	6.70	31.67
1+30	cb	6.18	32.19
"	gut	6.64	31.73

NE 1/4 RETURN 5 equal parts

B.C. = 0+00	cb	1.25	37.12
"	gut	1.74	36.63
0+13.4	cb	2.39	35.98
"	gut	2.84	35.53
0+26.8	cb	3.35	35.02
"	gut	3.81	34.56
0+40.2	cb	4.30	34.07
"	gut	4.77	33.60
0+53.6	cb	5.18	33.19
"	gut	5.63	32.74

3837

71

0+67	E.C. cb	5.64	32.73
"	gut	6.37	32.20
13' W of E.C. & ST		6.44	31.93
0+100 = 20' N of E.C.	ON W 1/4 cb		CONTAINING COAST
0+100	cb	7.27	31.10
"	gut	7.65	30.72
0+105	cb & Ex. 10' in 100'	7.21	31.16
"	grate	8.25	30.12
0+20	cb opposite 0+67	7.22	31.15
"	gut	7.61	30.76
0+50	cb	7.07	31.30
"	gut	7.56	30.81
0+75	cb	6.94	31.43
"	gut	7.37	31.00
1+00	cb	6.88	31.49
"	gut	7.27	31.10
1+25	cb	6.77	31.60
"	gut	7.21	31.16

where water  
now crosses  
St. from  
Nly outer of  
CORTAZ



1+50 gut & drive	7.12	31.25	W. end of shallow Valley Gut
5' W of above edge sdry	6.49	31.88	where water overflown through ways to Annex Prop.
1+75 cb.	6.64	31.75	
" gut	7.04	31.35	
1+85 gut in drive	7.00	31.37	
5' W edge sdry	6.78	31.59	
2+00 cb	6.55	31.82	
" gut	6.90	31.47	
S.M.H. #2 RIM	6.01	32.36	
" " F.L.	11.99	26.38	
Levels for Prop. drain to Prop. 15' inlet S.C. Cortez thru 6" Cor. Pav.			
0+00 = E Ex. 10' inlet			
0+00 cb	7.21	31.16	
" grate	8.25	30.12	
" F.L. Ex. 18" Cor. I.P.	9.21	29.16	inlet to ocean
0+08 Pav.	7.10	31.27	
0+15.3 " Int. Sewer	6.60	31.77	#2 to #3
0+25 "	6.23	32.14	

0+50 Pav	4.84	33.53	
0+75.2 " Int. Sewer <sup>bet. #1 to #2</sup>	3.58	34.79	
0+99.4 gut & Prop. 15'	3.80	34.57	S.C. Cortez Ave
" cb inlet	3.37	35.00	

## Levels for drain from Ex. 10' cb inlet to Ocean

0+00 Top cb & 10' cb inlet	7.21	31.16	
" grate	8.25	30.12	
" F.L. Ex. 18" Cor. I.P.	9.21	29.16	Box too shallow
0+05 W. edge Cor. sdry.	7.14	31.23	
0+50 ground	11.0	27.4	
0+60 "	9.9	28.5	
0+83 "	10.9	27.5	
T.P.	1.03	26.84	
0+92 Top Wood Bulkhead	2.4	24.4	
0+92 ground	5.1	27.7	1+00 to
1+00 " 4" Top 18" Pipe	8.7	18.1	1+39 =
1+18 End F.L. "	13.00	13.8	Hard sand- STONE
1+20 ground	14.0	12.8	
1+33 "	17.1	9.7	
1+39 "	17.5	9.3	
1+39 Sand Beach	38.5	-1.7	
38.37 T			

S.M.H. #3 RIM	4.80	33.57	
" " F.L.	9.44	28.93	
SET S.M. OR 11' LD. G.T. P.A.G.	5.63	32.74	NEW COR COSTA & CORTES

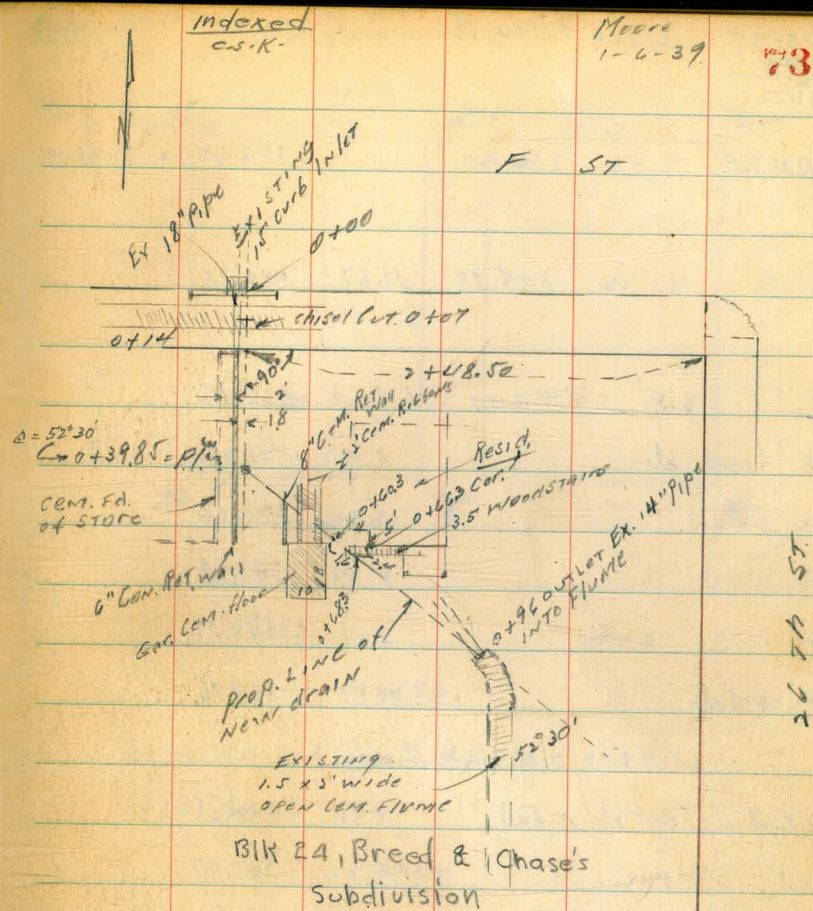


PROP. LOCATION OF NEW DRAIN  
ON F ST. AT Glendale. bet. 25th + 26th  
Should be 24" PIPE MIN.

BM				N.E. Cor F. St. and Glendale
Top curb	3.74	151.72	748.0	
0+00 cb top		4.91	146.81	
" gutter on grate		6.04	145.68	
" F.L. Box		9.57	142.15	
0+4.5 ledge Cern. Sidw.		5.38	146.34	
0+9.7 S " " "		5.33	146.39	
0+14 = S.L. F ST. ground		7.2	144.5	
0+20		8.6	143.1	
0+29.85 @ 52°30'		9.8	141.9	
0+46.5 Top 8" Ret wall Cern.		11.03	140.69	
0+50.7 @ 2' Cern. Ribbon		11.82	139.90	Gar. fl. El. Cern.
0+54.5 " " " "		11.90	139.82	
T.P	2.92	142.71	11.93	139.79
0+68.3 ground		4.0	138.7	
0+96 ground		4.9	137.8	
" F.L. of 14" pipe outlet and Beginning Conc. Flume		0.45	136.26	

old 14" EXISTING drain is under House

JUNCTION of 18" to 14" (?)



Property Owner is willing to have  
drain installed bet. House + Garage.



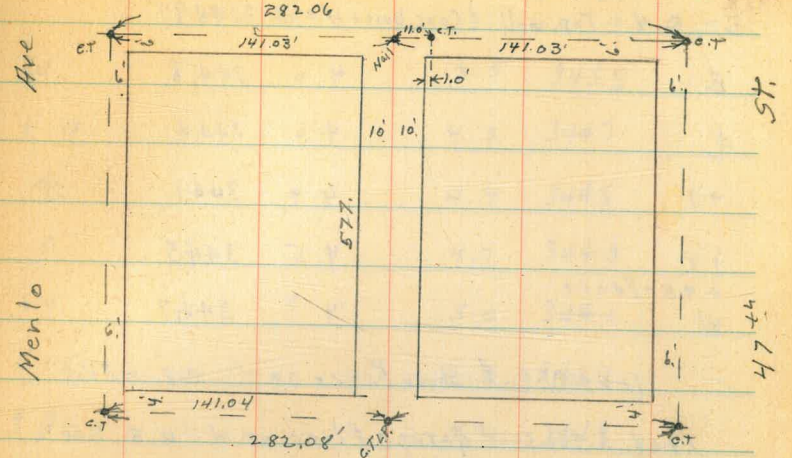
1-25-39 X See Alley. BIK. 2. Chester Park.

Miller  
Walker  
Bliss

B.M. B.P.	1.80	356.40	354.60	N.W. 47 <sup>th</sup> & Orange.
T.P.	4.26	348.99	11.67	344.73
6.5' s. of N Line = N. Curb of Polk.				
E. cont. dr		5.37		343.62
E. Pav		5.97		343.02
±		5.74		343.25
W		5.47		343.52
W. cont. dr		4.83		344.16
0+00 = N. Line Polk				
0.1 E. of W. = cont. dr. N. End.		4.81		344.18
" " " " = pav " "		5.22		343.77
± = " " "		5.66		343.33
E " " "		5.61		343.38
E cont. dr " "		5.14		343.85
0+05 N.				
E		5.1		343.9.
±		5.7		343.3
+ 8		5.0		344.0
W.		3.2		345.8

Indexed  
C.S.K.

Orange Ave 74



Polk Ave

348.99

0+0.6 = S. End. Cypress Hedge 1' W. of W. Line

0+38 = N " " " " " " " " " "

0+50

W	4.0	345.0
+ 2	4.5	344.5
±	4.6	344.4
E	4.2	344.8
0+08 = S. End. conc. wall	4.10	344.89
0+58 Garage on W. conc floor	4.3	Buck
W-4.2 = floor	3.36	345.63
0+66 S. End. Fence on W. 0.5 in Alley		



348.99

0+82  $\pm$  Conc. Drive on E. to garage on back of LotE - 0.8 = Top. wall =  $\pm$  Conc. Drive 4.02 344.97

E	4.2	344.8
$\pm$	4.6	344.4
+7	4.9	344.1
+8	4.5	344.5
+9.5 = Fence		
W	4.3	344.7

1+00 = N End. above fence on W. 0.7' in Alley

1+09. S. End. conc garage floor on W. 4.5' Back

W - 4.5 = Floor.	3.14	345.85
W,	4.1	344.9
+3	4.7	344.3
$\pm$	4.6	344.4
E	4.4	344.6
+0.8. Top. conc. wall	3.94	345.05

1+25 = N End. above conc wall on E.

E - 0.5	3.83	345.16
E	4.5	344.5
$\pm$	4.5	344.5
+6	4.3	344.7
W	3.5	345.5

348.99

1+30

75

W	3.5	345.5
+4	4.3	344.7
$\pm$	4.5	344.5
E	4.7	344.3
+4	5.0	344.0
+25	5.3	343.7
+50	4.2	344.8

1+71 N. End. above garage floor on W. 4.5' Back

E - 50	3.0	346.0
E - 25	4.0	345.0
E	3.8	345.2
$\pm$	4.2	344.8
+6	4.4	344.6
W	3.8	345.2

+4.5 = floor

1+75 S. End. Fence on W. 0.5' in Alley

1+80

W - 5	4.2	344.8
W	4.5	344.5
+4	4.7	344.3
$\pm$	4.2	344.8



348.99

1+80 (con.)

E		3.4	345.6
2+24 = N End above Fence 0.7 in Alley			
E		3.2	345.8
☉		3.3	345.7
+8		3.7	345.3
W	ground.	4.0	345.0
W	In Drainage ditch to W	4.5	344.5
W+34	" " " W End	5.0	344.0
W+34	ground	3.9	345.1
0+50	" "	3.6	345.4
2+28			
W-50		3.4	345.6
+34		4.6	344.4
W		3.1	345.9
☉		3.2	345.8
E		3.1	345.9
2+70			
E		2.0	347.0
☉		2.3	346.7
W		2.0	347.0

348.99

76

2+75 S. End. Fence on W 2.0 in Alley.

3+00			
W		1.4	347.6
☉		1.5	347.5
E		1.5	347.5
3+02 = N. End. above Fence on W. 2.1 in Alley			
T.P.	8.70	356.37	1.32 347.67
Board.			
3+20 } S. End. Fence on W. 0.7 in Alley			
Garage on E. conc. floor 14.0 Back			
E-14.0	= floor	8.1	348.3
3+43 N. End. N. Entrance garage on E. dirt floor 0.2 Back			
E-0.2	= floor	8.1	348.3
3+50			
E		7.9	348.5
☉		8.0	348.4
W		8.1	348.3
3+75			
W		7.3	349.1
☉		7.3	349.1
E		7.3	349.1



356.37

3+85  $\phi$  = Ex. M.H.

Top of M.H.	7.05	349.29
E	4+00	6.8 349.6
$\phi$		7.0 349.4
W		7.3 349.1
4+27	N. End. above Board Fence on W 0.9' in Alley Lattice " " " 0.9' " "	
	4+50	
N		6.4 350.0
$\phi$		6.2 350.2
E		6.2 350.2
4+58	N. End. of above Lattice Fence 0.9' Back.	
4+67	double garage on W. ext. floor 5.8' Back.	
W-5.8 = floor.		6.07 350.30
4+80	garage on E. dirt. floor 0.3' Back	
E-0.3 = floor		5.7 350.7
4+85	garage on W. ext. floor 13.6' Back	
W-13.6 = floor		6.09 350.28
	5+00	
E		5.7 350.7
$\phi$		5.6 350.8
W.		6.0 350.4
+5		6.3 350.1

356.37

5+20	garage on W. cone. floor 15.0' Back	
W-15. = floor		5.8 350.6
	5+30	
W		5.3 351.1
$\phi$		5.1 351.3
E		5.2 351.2
	5+45	
E		5.2 351.2
$\phi$		5.0 351.4
W		5.3 351.1
5+77	= s. line Orange Ave Unpaved.	
W ext. dr. s. End.		4.94 351.43
W		5.2 351.2
$\phi$		5.1 351.3
E		4.9 351.5
E ext. ch. s. End.		4.43 351.94
14' N. of S. Line = S. ch. Line Orange Unpaved.		
E. ext. ch.		4.60 351.77
E r ground.		5.3 351.1
E "		5.4 351.0
E "		5.6 350.8
E. ext. ch.		5.07 351.30
chk. Orig. BM		1.75 354.42



Indexed  
C.S.K.

Moore  
4-14-29

Sewer levels & Cuts for Sewer Dept.

Guy & Clark Sts.

N.W. 1/4 Curb	13.12	112.95		99.83	Miss. H. Blvd.
T.P.	12.00	122.75	2.54	110.39	3' STUBS.
M.H. R.M. = 0+00		8.40		114.35	✓
" FL.		14.00		108.15	✓
0+30		10.4		112.3	✓
0+40 Δ	LT	4.8		118.0	✓ 4.92
T.P.	11.67	134.13	0.24	122.51	✓
0+60		8.7		125.4	✓
0+80		3.3		130.8	✓ 3.35
T.P.	14.79	146.26	0.66	133.47	✓
1+00		10.0		136.3	✓
+20		5.5		140.8	✓ 5.23
T.P.	12.66	158.45	0.27	145.79	✓
+60		12.1		146.3	✓ 11.38
2+00		6.7		151.7	✓ 5.96
+60		4.7		153.7	✓ 4.73
+45.5 S of Clark		5.25		153.20	✓
" FL. 12" Pipe drain of curb inlet	11.29			147.16	✓

158.45

2+75.5 NLY curb 3.90 152.55 STUB <sup>78</sup>

2+85.5 NLY Clark 2.3 154.1 2.30

E.L. STUBS  
F.L. Grade

156.15 STUB  
151.5 Grade  
C 5.5

108.15

117.83 110.50 B C 7.33

GUY

125.3 122.0 B C 3.30

130.78 127.0 C 3.78 CLARK

2+85.5

141.03 137.0 B C 4.03

147.07 142.50 C 4.57

152.49 148.0 B C 4.49

0+40 = A

153.72 149.40 C 4.32

M.H. STUB 0.25

CANYON LINE

Mission Hills Blvd.



8-8-39

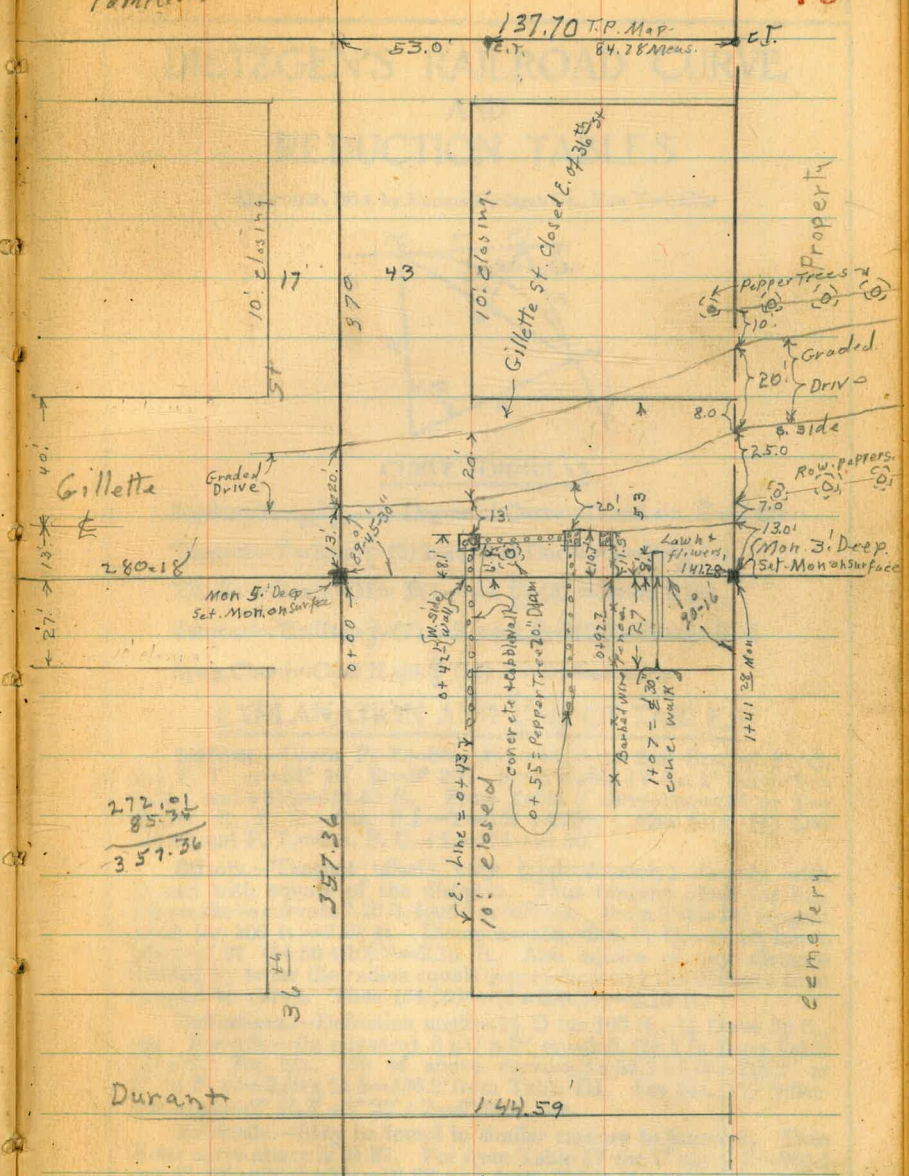
Survey for Opening of Gillette St  
from 36<sup>th</sup> St.

Miller  
Wallen  
Bliss

Indexed  
C.S.K.

Tankins

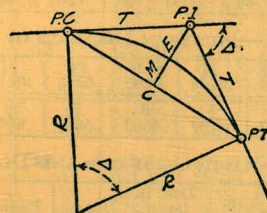
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# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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## CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of Curve= $D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)

Tangent= $T = R \tan \frac{\Delta}{2}$  (3) Length of Curve= $L = 100 \frac{\Delta}{D}$  (4)

Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2}) = R \text{vers} \frac{\Delta}{2}$  (5)

External= $E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)

Long Chord= $C = 2 R \sin \frac{\Delta}{2}$  (10)  $\Delta =$  Central Angle

## EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.—Sta. 161 + 60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8\frac{1}{2} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C. = Sta. P. I. —  $T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T. = Sta. P. C. +  $L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158 — Sta. P. C. = 54.50, hence offset = 7.27  $(54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft. = (in minutes)  $.3 \times C \times D^\circ$  or = defl. for 1 ft. from Table III  $\times C$ . For Sta. 153 of above curve =  $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$  or  $2^\circ 16.2'$ , or  $= 2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 91.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 91.27$  and from Table V correction = .10 or  $E = 91.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .



75  
 27  
 102  
 744.59  
 137.70  
 1009.3  
 737 | 6.890  
 6633  
 2570  
 2211  
 38  
 3  
 11.4  
 84.78  
 53  
 137.28  
 141.23  
 141  
 1.03  
 157.82  
 28.91  
 233.36  
 58.2  
 380  
 357  
 737  
 380  
 6093  
 1140  
 3420  
 35340  
 13770  
 141.23  
 3.32  
 144.55  
 114  
 30.55  
 2480.29 BC.  
 1409.75  
 3490.04  
 3495.79  
 3495.83  
 1054  
 13  
 114  
 357  
 93  
 1071  
 32261  
 4.74  
 14  
 18.5  
 32.5  
 32.5  
 650  
 25  
 32.5  
 7  
 75  
 14  
 47.5  
 125  
 6.00

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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