1557

MADE IN U.S.A.

Proposed Channel   Moore
for Cholla Valley   5-20-38
Main to Market St.

0+00 = 8' Line Main St. Ld. & C.T. € Bridge
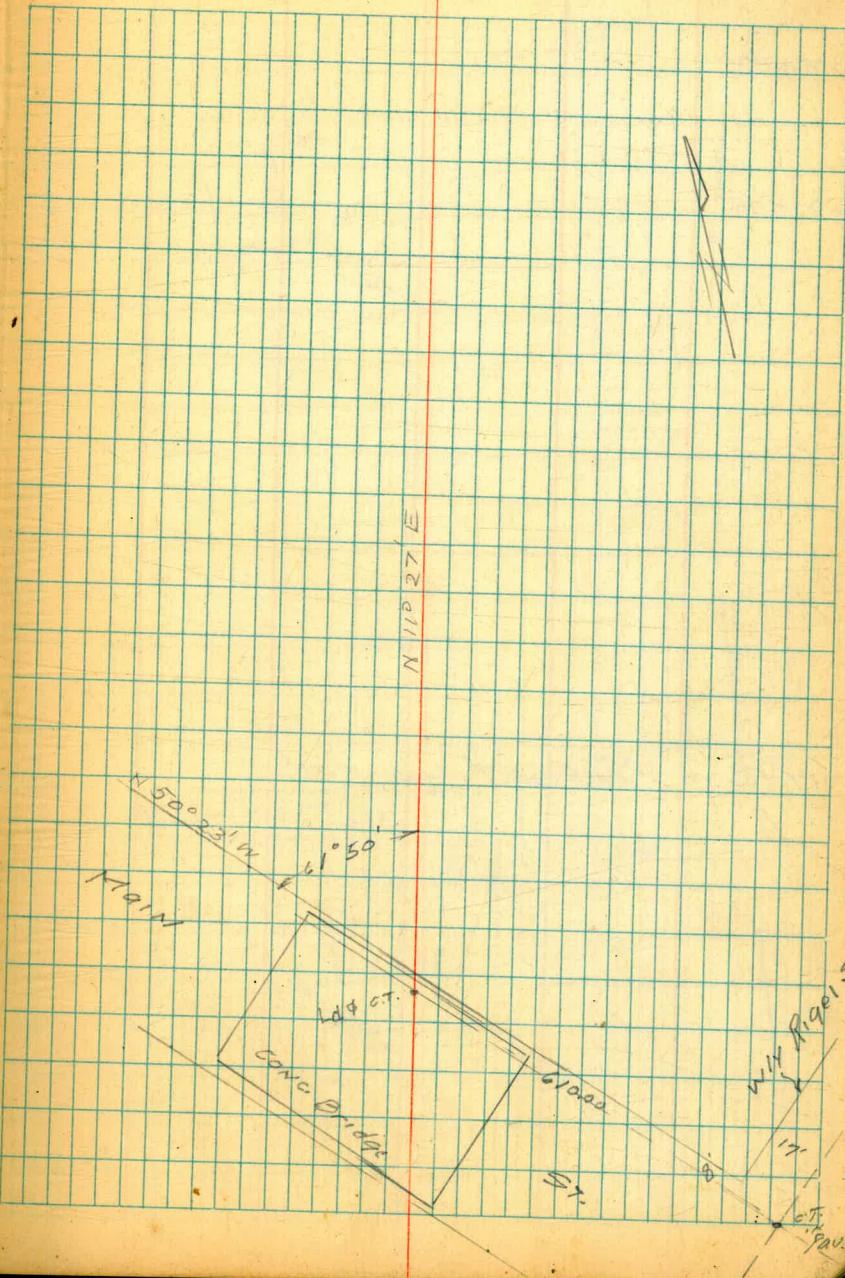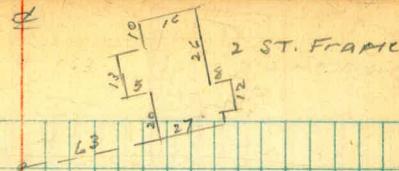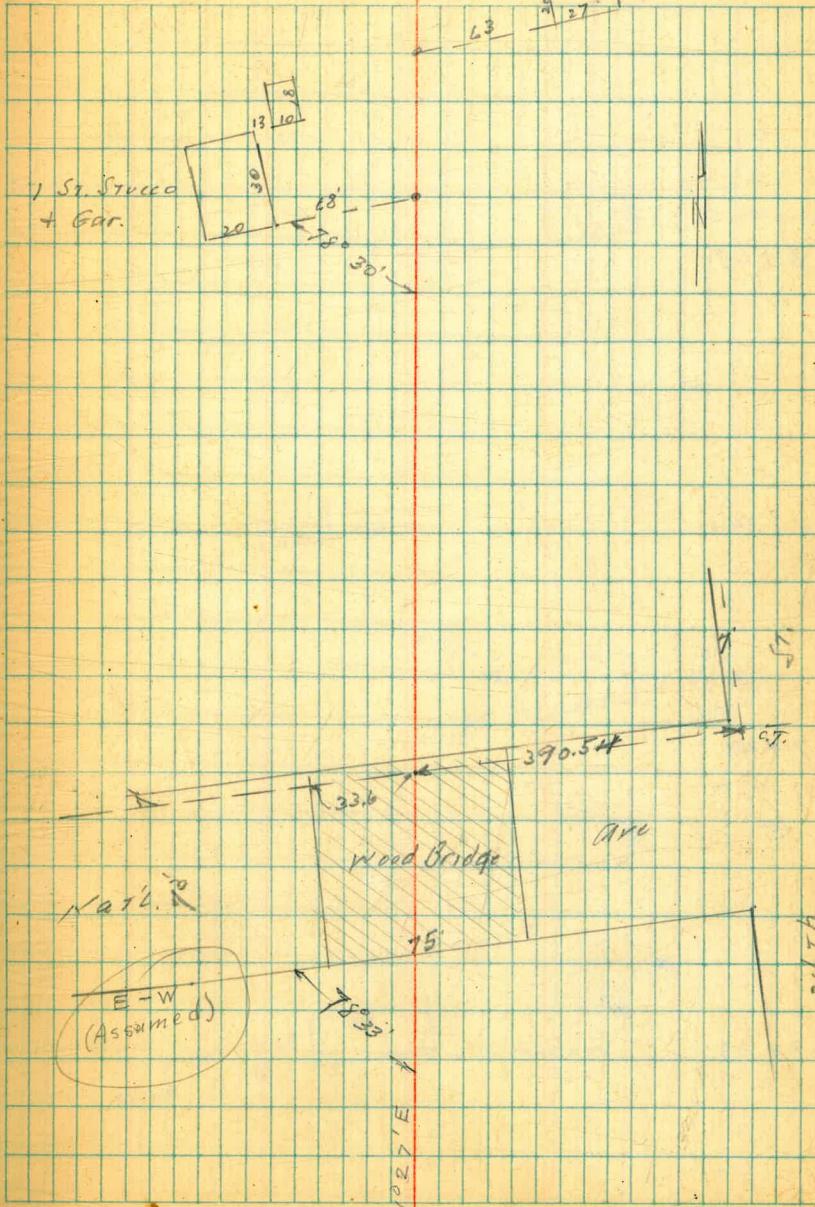
22 + 42

22 + 04

17 + 86.10   Nail N 7' line Natl.

2 ST. Frame

1 St. Stucco
+ Gar.

Natl. ○

E - W
(Assumed)

Wood Bridge

390.54

33.6

75'

78.33'

ave

C.J.

34 TH

28+69

28+34

27+44

23+33

53 — 28 / 1 St. Frame

1 St. Frame 24 / 30

→ 78.0 ′0
79 / 30 / 1 St. Ft.

N 11° 27 E

chick yd. 30 / 20 / 24 / Bd. Garage

34 + 10

32 + 4r

31 + 00

∠ 78° 30'

92?

water shaft

N 11° 27' E

10 x 10 water Plant
+ well

9 | 12 | 6 | 4 sq. ft.

39+24.95   2x2 R.W. P.I.

37+28.6   chisel +   Nly 7' line Ocean View Blvd.

36+11

35+26

34+72

8°25' LT.
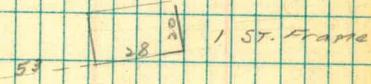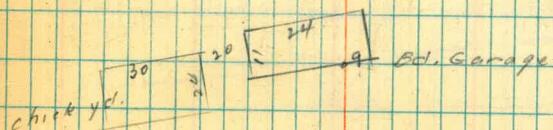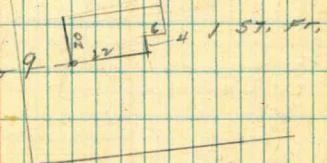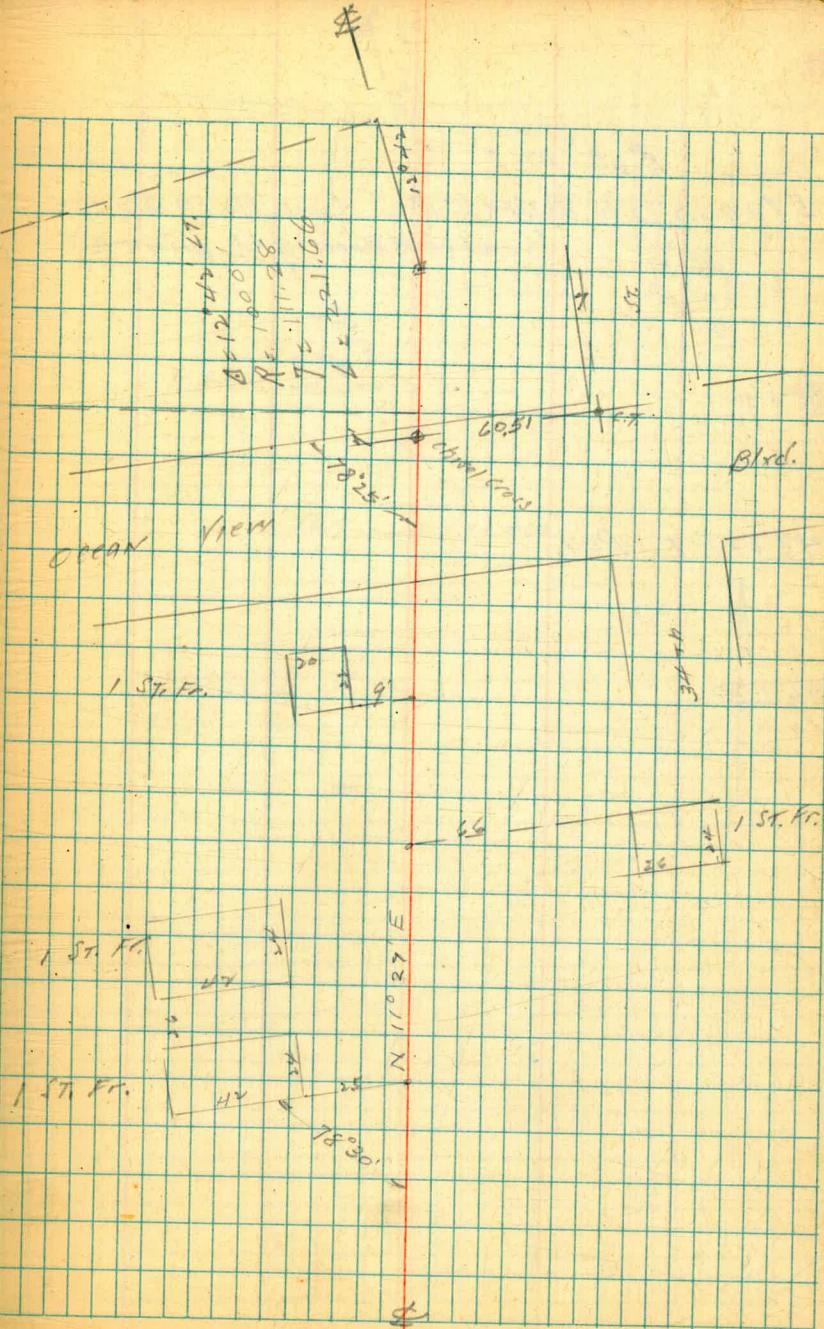
57+06.0 = ±x± ₵ Imp. Ave. Conc. Arch Bridge
(See Field Book 1521 page 2)

49+20

48+27.17 P.O.T.

46+90
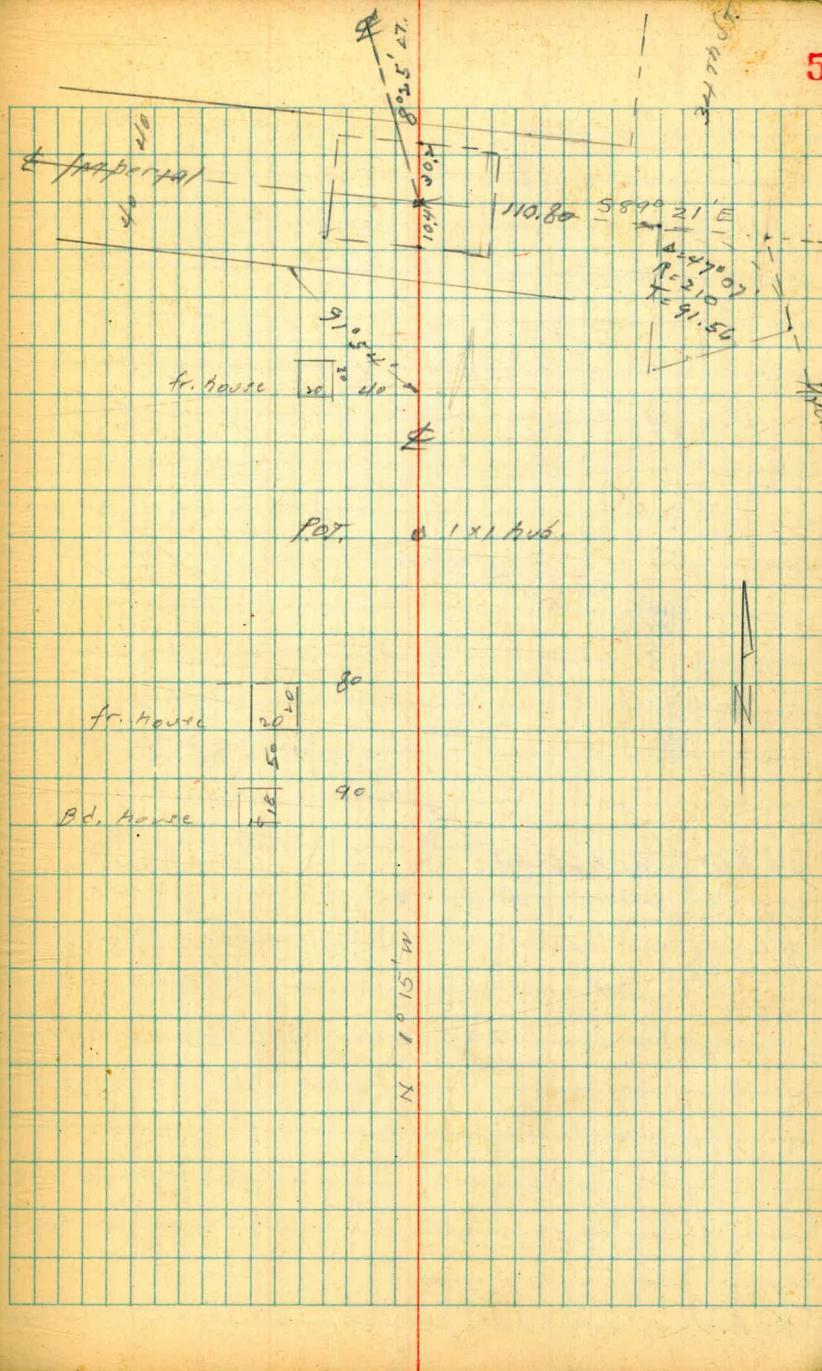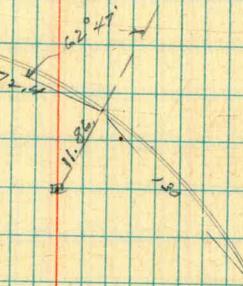
64+61 1x1 Hv6 P.I.

San Diego, Cuyamaca
R.R. Bridge

N 5° 25' E

-15°05'

62°47'

72.1

11.82

N 9° 40' W

Δ = 15°05' Rt.
R = 1000
T = 132.3 9
L = 263.25

76+05.22 2x2 S.L. Market St.

73+78.14 P.I.

Ꭼ Market St. 30/30

chisel cut

37.5 3.75

190

Conc. Bridge

2x2

39.9' N44°54'E

N00°54'E

2x2

Δ=39°19' Rt.
R=600
T=215.3
L=411.3.47

N

N 5°25'E
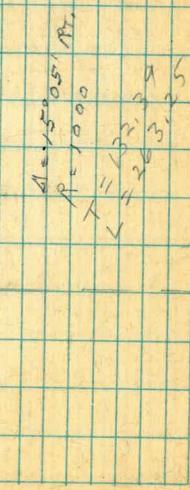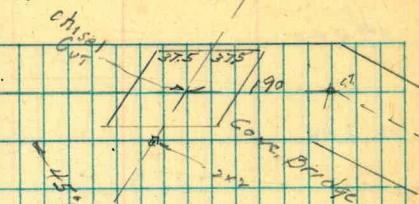
approx. location of
Ex. Channel of Chella Creek.

14+00

12+00

9+50

9+00

8+50

7+00

6+00

4+40

3+20

2+45

1+00   30' R to ℄   50' wide

0+00

℄ Prop. Channel

30   115

35   135

20   96

70

90   40

40

25   10

So. Chella

10   50

Main St.
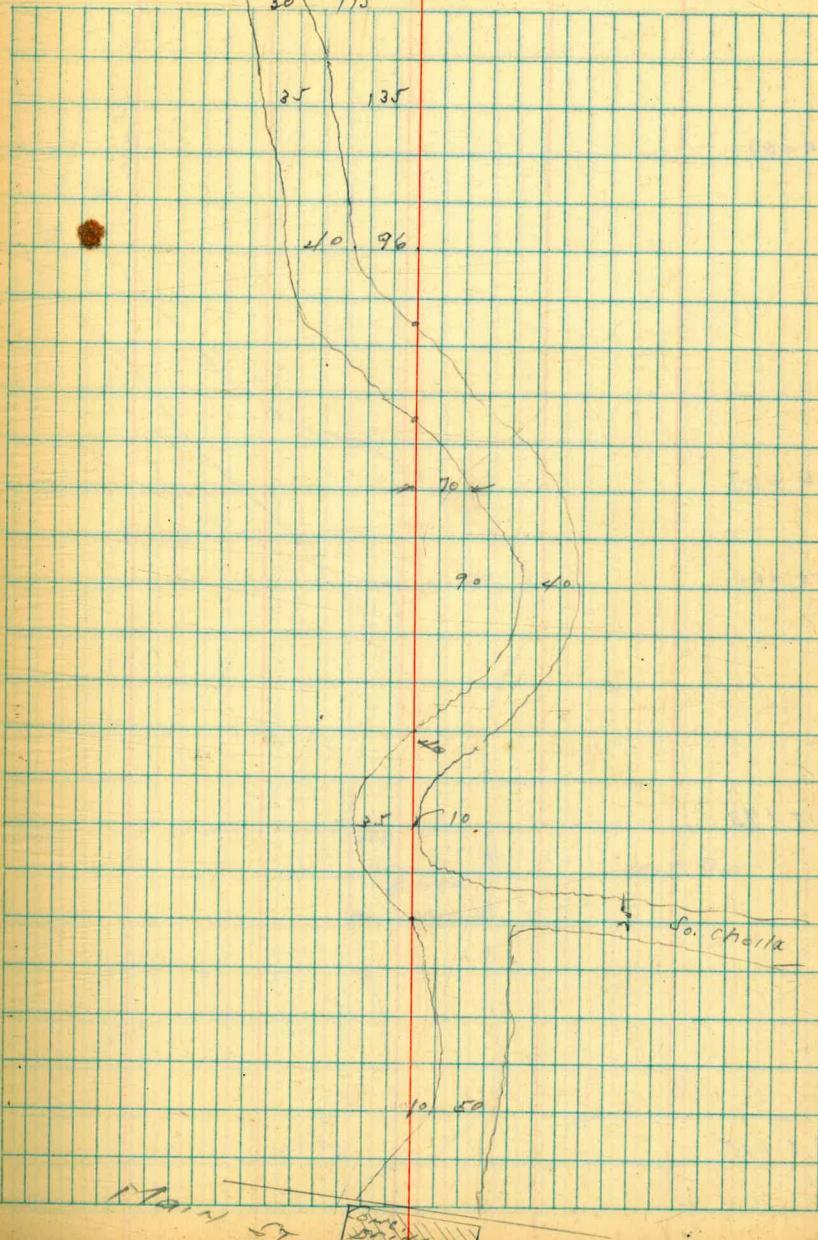
24+00

mag nail 100

20+67

20+00

17+93

16+15

c20

10

20   50

33.6
Wood
Bridge   Natl. Ave
← 15 →

20

50+00

47+00

44+00

43+00

41+30

39+24.95

¢ Bancroft

Bridge 104
82

230

310

65 75

70

40 20

35 40

32 35

33d St.

50

125

56 58

40

34th St.

Ocean View Blvd.

6472.86   Cuyamaca R.R.

64+00

60+00

58+50

57+06 E Imp'l

55+0

54+0

52+0

E

75   130

R.R. Bridge

110   85

120   115

30.50

Conc Arch
Bridge
48   E Imperial

30 70   Creek N. of Crystal

100

120   65

73+78.14 P.l.

71+0

69+0

66+0

⊄

Marker to | Bridge |

75

105

15   35

70   85

110   85

Bliss
Isbell
Chapman

"X" Section Alley Block 8   Indexed C.S.K.
Sub Lots 20-50   Teralta
Wilson to 36 - Polk to Orange

B.M. N.W. Br. Orange & Wilson		3.48	380.53		377.05
T.P.		3.26	376.56	7.23	373.30
T.P.		6.50	375.17	7.89	368.67

Section on N. Gutter of Polk & ⅔ S. of N. Roof.

E-50	Gutter		6.55	368.62
E	"		6.33	368.84
E Top cb.			5.75	369.42
₵			6.29	368.88
W	Gutter		6.29	368.88
W Top cb			5.77	369.40
W 450	Gutter		6.17	369.00

0+00 N. Line Polk

W. Top cb		5.48	369.69
Gutter		5.78	369.39
₵		5.96	369.21
E Gutter		5.95	369.22
E Top cb		5.66	369.51

Plot by C.B.H. 12/30/39

Walk Parallels to alley 2° wide
0+06 Conc Sidewalk on East   W Edge 1.3 in alley   Beginning of cypress hedge 2.3 in alley

S-End walk		4.17	371.00
Ground		4.2	371.0
+2		4.7	370.5
₵		5.6	369.6
+8		5.0	370.3
W		4.6	370.6

311 69 chained
311 60 Record

Orange   6°   Ave
155.82   20

op TK in Perring   op TK L.P.   op TK out

op TK L.P.   155.56   4°   30   op TK in Perring St.   op TK L.P.
Polk

311 72 chained
311 65 Record

375.17

0+20   Elev

W		4.0	371.2
+2		4.4	370.8
₵		4.6	370.6
E		4.0	371.2

0+27 End Hedge on East 2½ in alley
0+35 End Walk on East 1½ in alley   2° Walk

E end of walk		3.72	371.45

0+42 Single Garage on East   (? floor)

Lip 0.2 in alley		3.81	371.36
Garage 1.7 Back		3.48	371.69

0+50   0

E		4.1	371.1
₵		4.1	371.1
W		3.8	371.4

	+	TP 375.17	−	Eler
0+51 Light Pole on East 12 Dia inside Face 10¹ from ₵ on Line				
0+55 Single Garage on East Concrete Floor				
₵ Garage on concrete Floor		4.02		371.15
0+65 Single Garage on East		0.3 in alley		
₵ Garage on concrete Floor		3.82		371.35
0+68 Single Garage on West			8.2 Back concrete Floor	
₵ Garage on concrete Floor		3.24		371.93
0+75				
W-10		3.1		372.1
W		3.5		371.7
₵		3.8		371.4
E		3.8		371.4
E+10		3.8		371.4
1+00				
E-37		4.0		371.2
-15		3.6		371.6
E		3.4		371.8
₵		3.7		371.5
W		3.7		371.5
W-+13		3.8		371.4
+28		3.4		371.8
1+06 Single Garage on East			7.2 Back	
₵ on concrete Floor		3.25		371.92
1+10				
W-25		4.0		371.2

	+	TP 375.17	−	Eler
W		3.6		371.6
₵		3.7		371.5
+4		3.4		371.8
E		3.4		371.8
1+16 Eucalyptus Tree, on East 2.0 in Dia, W Face 1.6 in alley				
1+21 Single Garage on East			7.2 Back	
₵ on concrete Floor		3.20		371.87
1+47 Light Pole on West 1.2 in Dia West Face 9.6 From ₵				
1+50				
E-10		3.2		372.0
E		3.1		372.1
₵		3.5		371.7
W		3.6		371.6
1+69 Single Garage on West			Dirt Floor 8.0 Back	
₵ on dirt		2.9		372.2
2+00				
W-20		3.2		372.0
W		3.2		372.0
₵		3.2		372.0
E		2.8		372.4
E+10		2.8		372.4
T.P	5.25	379.01	1.41	373.76
2+41 Single Garage on West			5.8 Back Dirt Floor	
₵ on dirt Floor		6.3		372.7

2+43 Light Pole on West 1'dia. West Face 9.4 from ℄

2+15 on East S.End of Residence 0.1 in alley

2+30 " " N " " " 0.9 in alley

2+30 on " Beginning Picket Fence 0.9 in alley

2+55.

E-10	5.7	373.3
E	5.7	373.3
E+9	5.5	373.5
℄	6.0	373.0
W	6.0	373.0
W+30	6.6	372.4
+45	6.2	372.8

2+74 S.End Residence on East   0.5 in alley

2+74 End of Fence on East   0.5 in alley

2+97⁵ N End of Residence   0.7 in alley

2+76

W-20	6.1	372.9
W	5.7	373.3
℄	5.6	373.4
E	5.3	373.7

2+93 Single Garage on West   5.2 Back

W-5.2 on ℄ concrete Floor	5.31	373.70
-2.2 on lip	5.39	373.62

3+00

E-10	5.7	373.3
E	5.7	373.3

E+3	5.2	373.8
℄	5.6	373.4
W	5.4	373.6
W+10	5.7	373.3

3+01 Concrete Wall on East 1.3'   5.33   373.68

3+46 Single Garage on East   0.1 in alley

℄ dirt Floor	50	374.0

3+50

W-20	5.0	374.0
W	5.1	373.9
℄	5.1	373.9
E	4.9	374.1

3+51 Power Pole. West Face 9.3 from ℄   1.3 dia   0.8 in alley

3+62 Single Garage on East

℄ dirt floor	4.9	374.1

0.5 in alley

3+69 Beginning Picket Fence on East

3+96 Picket Fence on line

4+00

E-10	4.7	374.3
E	4.8	374.2
℄	4.7	374.3
W	4.6	374.4
W+5	4.5	374.5

4+50

W-10	3.9	375.1
W	4.1	374.9

¢		4.2	374.8
+7		3.8	375.2
E		3.7	375.3
+10		3.9	375.1 ✓

4+70 Single Garage on West   1.9 Back

W-0.3 on lip		3.75	375.26 ✓
W-1.9 on concrete Floor	3.60		375.41 ✓

4+76 Light Pole on West 1.0 diameter   West Face 10° West of ¢

4.91 " " Deadman .92 West of ¢ to center

4.92 " " " 9.1 " " " "

5+00 South Section Dbl Garage on West   0.5 Back Wood Floor ✓

E-10		2.7	376.3 ✓
E.		3.2	375.8
¢		3.4	375.6
W.		3.3	375.7
W-0.5 on Wood Floor		3.3	375.7 ✓

5+10 North Section Dbl Garage on West   0.3 Back Wood Floor

W-0.3 on ¢ Wood Floor		3.4	375.6 ✓

5+06 Single Garage on East   On line concrete Floor

¢ on Concrete Floor		2.50	376.51 ✓
5+22			
W-30		3.6	375.4 ✓
-15		3.6	375.4 ✓
-1		3.9	375.6 ✓
W.		3.2	375.8

¢		2.8	376.2
E		2.5	376.5
5+5		2.4	376.6 ✓

5+26 Sand Shed on West   0.1 in alley ✓

5+32 N " " " " 0.3 " " ✓

5+45

E-5		2.2	376.8 ✓
E		2.2	376.8
¢		2.5	375.5
W		2.8	376.2
W+5		3.1	375.9 ✓
5+60			
W		2.6	376.4
¢		2.5	376.5
+6		2.9	376.1
E		2.2	376.8

5+70 ¢ S line of Orange

E Top cb 9.85 E of ¢		3.36	375.65 ✓
Paving		3.34	375.67 ✓
¢ on Paving		3.58	375.43 ✓
W on Paving		3.41	375.60 ✓
W Top cb 10.30 West of ¢		1.41	375.60 ✓
T.P. 5.01	380.72	3.30	375.71

Section on South Gutter of Orange St   14 North of Prop Line

W-2.5		5.49	375.23 ✓

T
380.72

W in Gutter		5.54	375.18 ✓	
W Top Cb		5.30	375.42	
E in Gutter		5.54	375.18 ✓	
E in Gutter		5.49	375.23 ✓	
E Top Cb		5.10	375.62	
E + 25 in Gutter		5.60	375.12 ✓	
E + 60 " "		5.62	375.10 ✓	
Check starting BM N W Orange + Wilson		3.69	377.05 BM 377.03	
			0.02 error	

Guard Fence

Graded Area

15.0'

28th St.

12'

Grape St.

5'

Fd Mon

2-2' Pipe
Guard Fence

20'

9'

35'

25'

12'

Fd Balboa Park

Graded Area

220.0'

Fd 28th St.

Guard Fence
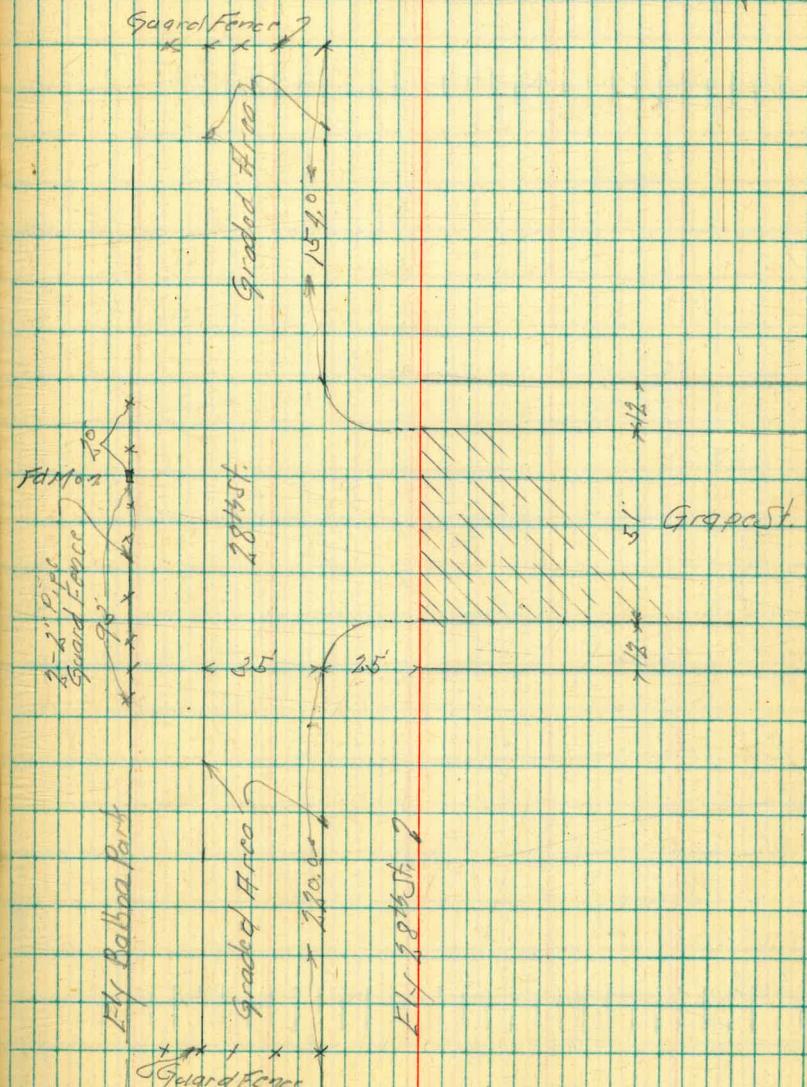
BM. B.P. ——— 5.08 ——— 379.46 ——————— 374.38 — N.W. 38th 4 Meade Ave

14 S. of N. Line = S. ol. Meade

E − 25	gutter		4.78	374.68
E	"		4.56	374.90
E	cmt. ol		4.05	375.41
₵	gutter		4.56	374.90
W	cmt. ol		3.81	375.65
W	gutter		4.48	374.98
+ 25	"		4.20	375.26

0.2's S. of N. Line Meade

W. + 0.1	pav		4.01	375.45
₵	"		4.18	375.28
+ 7.4	"		4.10	375.36
+ 7.4	N. End. Good ol.		3.77	375.69

0 + 00 = N. Line Meade

E + 0.1	cmt. ol (Busted ol N. End)		3.94	375.52
E + 0.1	pav.	" "	4.15	375.31
₵	"	" "	4.19	375.27
+ 7.4	"	" "	4.05	375.41
+ 7.4	ol	" "	3.65	375.81

0 + 10

E		3.4	376.1
E'		3.8	375.7
W		3.2	376.3

279.23

Meade ————— 379.46 ————— Ave
                    0 + 50

W		2.6	376.9
₵		3.0	376.5
E		3.1	376.4
+2		3.5	376.0
+5		3.5	376.0

1 + 00

E		2.7	376.8
₵		2.6	376.9
W		2.7	377.3

1 to 7 garage on W. dirt floor 9.0 Back.

E + 9.0 floor		3.0	376.5

	1+50			
W — 5			2.5	377.0
W			2.5	377.0
₵			2.5	377.0
E			2.5	377.0
	1+75			
E — 5,			2.6	376.9
E			2.3	377.2
₵			2.4	377.1
W			2.4	377.1
+5			2.6	376.9
	2+00			
— 5,			2.5	377.0
W			2.2	377.3
₵			2.4	377.1
E			2.4	377.1
+5			2.6	376.9
	2+03			
₵ Top. Sewer M.H.			2.27	377.19
	2+50			
E — 5			2.4	377.1
E			2.0	377.5
₵			2.0	377.5
W			2.1	377.4
+5			2.3	377.2
	2+59 garage on W. cmt floor		9.0 Back	
W — 9.0 = floor,			1.35	378.11

2+91 garage on W. cmt. floor			9.5 Back	
W — 9.5 = floor.			1.15	378.31
T.P.	5.02	382.83 ✓	1.65	377.81
	3+00			
W — 5.			5.0	377.8
W.			5.0	377.8
+0.4 = S. End. E. side (Brick & conc. Wall) 4.7' High			5.0	377.8
₵			5.1	377.7
E			5.2	377.6
+5			5.5	377.3
	3+20			
E.—			5.4	377.4
E.			5.0	377.8
₵			4.9	377.9
+7.1 = N. End. E. Side above wall			4.5	378.3
W.			4.5	378.3
+5.			4.1	378.7
	3+44			
7.0 W. of ₵ = S. End. E. side conc & Brick. Wall 2.5' High				
	3+50			
W — 5			4.8	378.0
W			4.7	378.1
+0.5 = W. End. E. side above Brick & conc. Wall 2.5'+4'			4.7	378.1
₵			4.7	378.1
E			4.8	378.0
+5			5.3	377.5

4+00		
E – 5	5.0	377.8
E	4.8	378.0
¢	4.7	378.1
W	4.7	378.1
+5	4.6	378.2

4+18 S. End Conc. Apron on W. 0.3' in Alley.

W cone apron	3.81	379.02
+0.5 E. Edge " "	3.81	379.02
+1	4.2	378.6
¢	4.5	378.3
E	4.6	378.2
+5	5.2	377.6

4+50 = N. End above apron on W. 0.3 in Alley
(" " garage cone floor 6.7 Back.

E – 5	5.1	377.7
E	4.7	378.1
¢	4.6	378.2
+7.2 E. edge cone.apron	3.82	379.01
+W " "	3.80	379.03
+6.7 garage floor	3.77	379.06

4+55		
W – 5	4.4	378.4
W	4.7	378.1
¢	4.7	378.1
E	4.8	378.0
+5	5.2	377.6

5+00		
– 5	5.0	377.8
E	4.5	378.3
¢	4.4	378.4
W	4.1	378.7

5+40		
W	3.9	378.9
+0.2 S.E. Cor. Stucco Garage	3.9	378.9 N. Entrance
¢	4.2	378.6
E	4.2	378.6
+1	4.9	377.9
+5	5.0	377.8

5+50		
E – 5	4.3	378.5
E	4.3	378.5
¢	4.3	378.5
+7.3 = N.E. Cor above Garage	4.0	378.8
W	3.8	379.0

5+80		
W	3.8	379.0
+5.0 = W. edge Flush Tank	4.48	378.35
¢ " " "	4.51	378.32
+2.5 = E. " " "	4.47	378.36
E	4.4	378.4

5+85 N. End N. Entrance Garage on E. 2.2 Back

E - 2.2 W. edge conc Drive   4.90   377.93

6+00 ᵇ = S. Line Monroe

E + 0.15' = emt. d. S. End.		5.61	377.22	
E + 0.15 pav.	" "	5.83	377.00	
₵ "	" "	5.83	377.00	
+ 7.4 "	" "	5.46	377.37	
+ 7.4 c one. d " "		5.20	377.63	

12' N of S. = S. d Monroe

W. d		5.40	377.43
W pav		5.82	377.01
₵ "		5.90	376.93
E "		6.08	376.75
E el		5.74	377.09

BM. B.P.   5.21   379.91   8.13   374.70 ⟹ S.W 38th & Monroe.

= 374.50

chk. Orig BM.   5.53   374.38 ✓

BM	5.99	380.37	374.38 Marker	
TP	6.65	381.03	5.30	3.75.07
TP	4.49	383.09	3.12	378.60

3+50

N +0.7 = S½ Conc Drive   4.13   378.96

N -5.8 = N½ S Garage   3.60   379.92
     Conc floor

3+96.5

N +0.7 = N½ Conc Drive   4.12   378.97

N -5.8 = N½ S Garage   3.76   379.33
     Conc Floors

4+40

E -0.2 = ₵ Conc Apron   4.86   378.23

E -6.3 = ₵ Garage Conc Flr   4.16   378.93

Survey for creek channel
N. of Ocean View Blvd. bet. 33d & 34th

+ 33.87 E.C.   33° 11.0

5   28° 19.8   Δ = 66° 22'
                                R = 200
+ 50   21° 10.4   T = 130.79
                                L = 231.66

4   14° 00.5

+ 50   6° 50.8

3 + 02.21 = B.C.

0 + 00 = Ely 33d St

Ocean View Blvd

Contour pg 30.
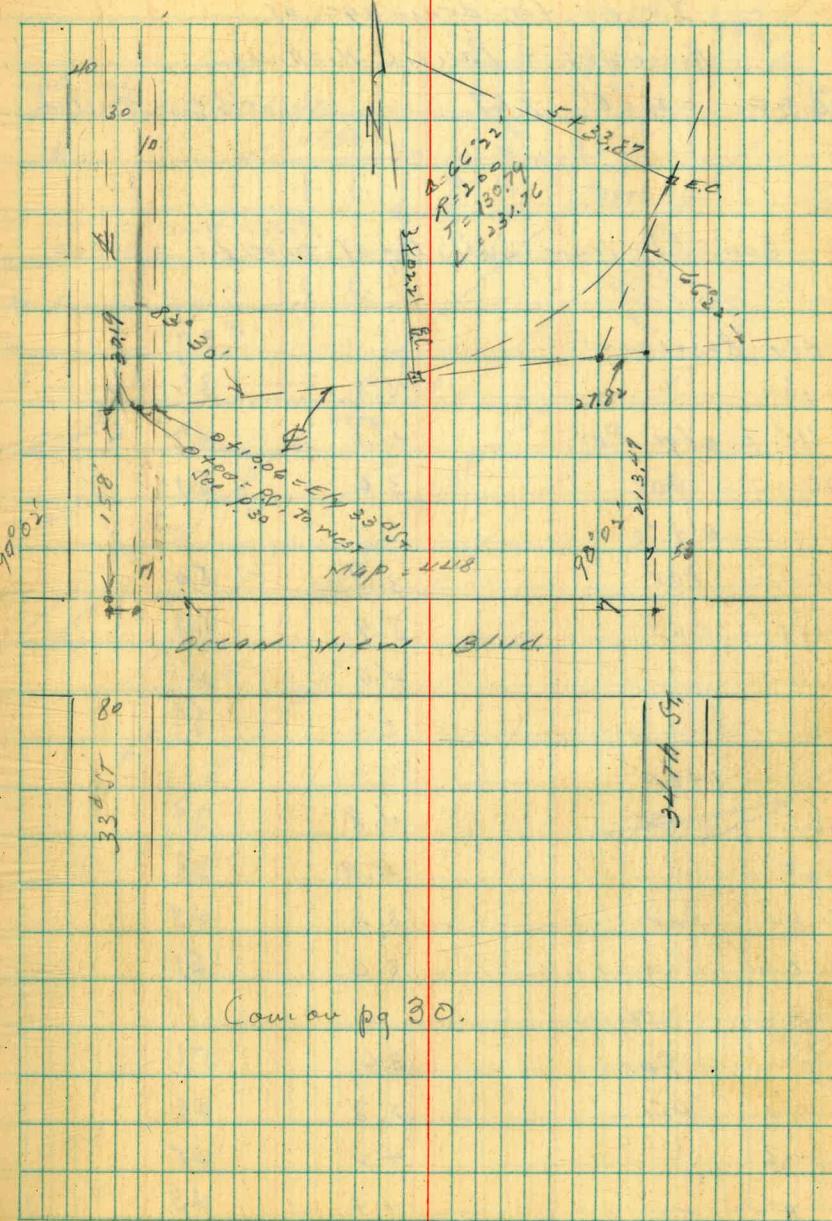
Levels for drainage at
Rosecrans + Pacific Highway

S.E.B.P.	4.05	8.67		4.62	San Diego Taylor

300' S'ly from SW'ly cor of Rosecrans + Pacific = 0+00

E'ly Rosecrans		5.0	3.7	
cb		5.1	3.6	
1/4 = edge Pav.		4.0	4.7	0+00
c Pav.		3.6	5.1	
0+50				
c Pav		3.7	5.0	
1/4 "		3.9	4.8	
cb		4.6	4.1	
E		5.0	3.7	
1+00				
E		4.8	3.9	
cb		4.9	3.8	
1/4 Pav		3.8	4.9	
c "		3.6	5.1	
1+50				
c Pav		3.6	5.1	
1/4 Pav		3.8	4.9	
cb		4.2	4.5	
E		4.4	4.3	

Left page
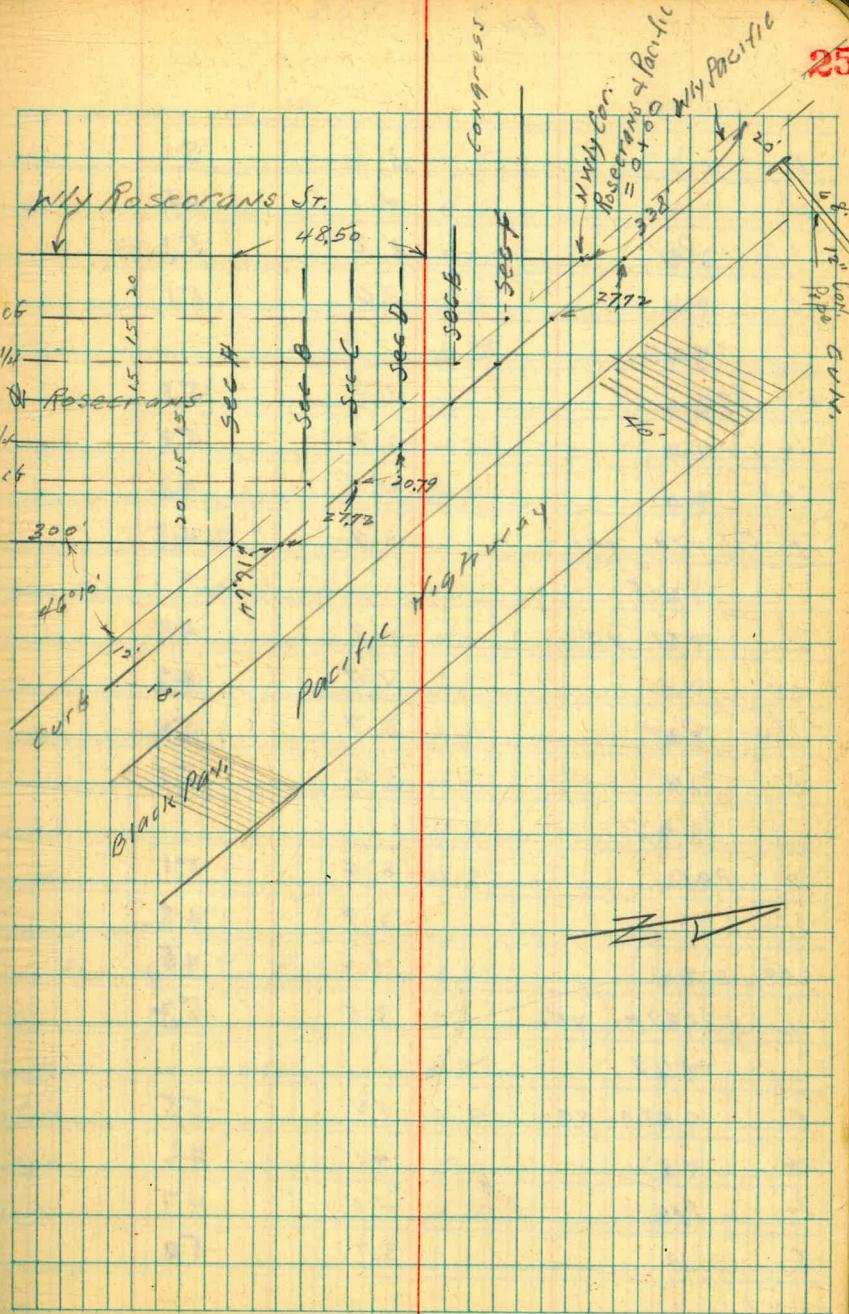
1 + 75		
E	3.6	5.1
cb	4.1	4.6
1/4 Pav	3.6	5.1
c "	3.6	5.1
2+00		
c Pav	3.6	5.1
1/4 "	3.7	50
cb	4.4	43
E 0.1 sta. yard	3.9	4.8
2+25		
E sta. yd.	3.8	4.9
cb	4.4	43
1/4 Pav	3.7	50
C "	3.6	5.1
2+50		
c Pav	3.6	5.1
1/4 "	3.9	4.8
cb	4.2	45
E sta. yd.	3.5	5.2
2+75		
E sta. yd.	3.2	55
cb	4.1	46
1/4 Pav	4.0	47
c "	3.7	50

Right page

3+00 a Sec A		
W	4.5	42
cb	4.4	41
1/4 Par	4.1	46
c "	3.8	49
1/4 "	3.9	48
+6 "	4.1	46
cb	4.2	45
E sta. yard	3.8	49
Sec B		
W+ Pac + Feb Rosecrans	4.1	46
+4 Pav edge	4.0	47
1/4 "	3.8	49
c "	3.9	48
1/4 "	4.2	45
cb	4.9	3.8
W	4.7	4.0
Sec C		
W+ Pac + 5 1/4 Rosecrans	3.8	49 Pav
C Pav	4.0	47 "
+10 " edge	4.2	45
1/4	4.4	43
cb	5.0	37
W	4.6	41

Sec. D

W L Pac. & Roseerans	4.0	4.7	Pav
+ 7 edge	4.2	45	
1/4	4.5	42	
c6	5.2	35	
W	4.8	39	

Sec E

W L Pac & W 1/4 R "	4.5	4.2
c6	5.3	3.4
W	5.6	3.1

Sec F

W L Pac. W c6 "R"	5.3	3.4
W	5.9	2.8

Levels on Pacific

200' Sly from SWly Cor Pac. + Roseerans = 0+00

0+00

W L Pacific	3.1	5.6
c6	3.4	5.3
+ 9	3.6	5.1
+ 18 edge pav	3.2	5.5
c.	2.9	58

0+50

W L Pac	3.3	54
c6	3.4	53

+ 9		3.5	
+ 18 edge pav		3.1	5.6
C "		2.9	58

1+00

W L	3.2	55
c6	3.5	5.2
+ 9	3.5	5.2
+ 18 edge pav	3.2	5.2
C pav	2.9	58

1+50

W L	3.9	5.7
c6	3.5	5.2
+ 9	3.4	5.1
+ 18 edge pav	3.3	54
C pav	3.9	57

2+00

W L	3.8	49
c6	3.9	48
+ 9	3.6	51
+ 18 edge pav.	3.4	53
C pav.	3.2	55

2+27.7x

W L Pac	4.1	46
c6	4.1	46
+ 18 edge pav	3.6	51
C pav.	3.4	5.3

2+48.51		
Wt Pac. Pav	3.8	49
cb "	3.8	49
+18 "	3.8	49
c "	3.4	53
2+49.30		
Wt Pac Pav	4.0	4.7
cb "	3.9	4.8
+18 "	3.8	49
c "	3.6	51
2+90.09		
Wt Pac	4.5	4.2
cb	4.2	4.5
+18 edge Pav.	4.0	4.7
c Pav	3.7	50
3+10.88		
Wt Pac	5.3	3.4
cb	4.8	39
+18 edge Pav	4.1	46
c. Pav	3.8	4.9

3+38.60 = INT. of Wly LINES of Rosecrans Pacific
= 0+00

0+00		
Wt Pac.	5.6	3.1
cb	5.1	36
+18 edge Pav.	4.2	45

c Pav.	3.9	4.8
0+50		
Wt Pac oil sta yd	5.2	35
cb	5.3	34
+18 edge Pav	4.4	43
c Pav.	4.2	45
1+00		
Wt Pac oil sta yd	5.2	35
cb	5.4	33
+18 edge Pav.	4.7	40
c Pav.	4.4	43
1+50		
Wt Pac	6.0	27
cb	5.8	29
+18 edge Pav.	5.0	37
c Pav	4.7	40
2+00		
Wt Pac	6.1	26
cb	6.0	27
+18 edge Pav	5.2	35
c Pav	5.0	37
2+50		
Wt Pac	6.3	24
cb	6.3	24
+18 edge Pav	5.5	32
c Pav	5.3	34

		8.67		
3+00				
WL Pac		6.0	2.7	
cb		6.0	2.7	
+18	edge Pav	5.9	2.8	
C	Pav	5.5	3.2	
3+38				
WL Pac		6.9	1.8	
cb		6.9	1.8	
+8	F.L. 12" Conc. Pipe Culv. inlet	8.68	-0.01	
+8	hd wall	6.7	2.0	
+18	edge Pav.	6.2	2.5	
C	Pav.	5.6	3.1	
C +20	edge Pav	5.3	3.4	
C +38	F.L. 12" Culv. Outlet	9.25	-0.58	

Survey for Cholla Valley Creek Channel So. of

$\Delta = 83°30'$

$R = 231.08$

$T = 206.25$

$L = 336.76$

$\Delta = 43°47'30''$

$R = 200$

$T = 78.36$

$L = 149.37$
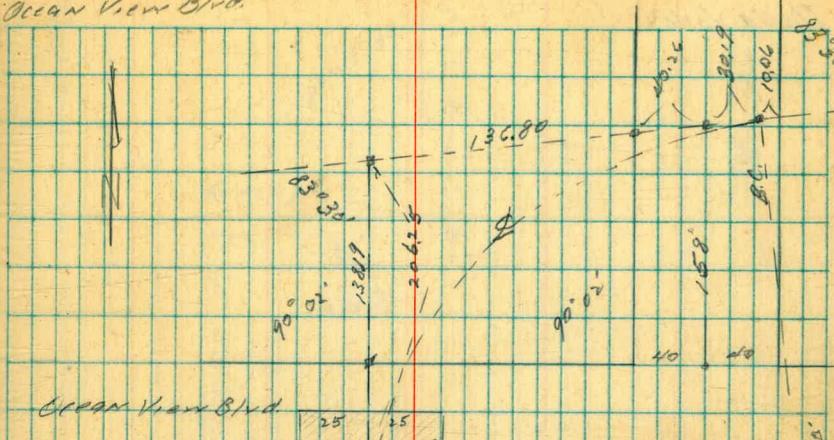
Ocean View Blvd.

Cholla Valley

Pueblo Line

194.11
17
r11.11
1.5
22.11

Logan Ave
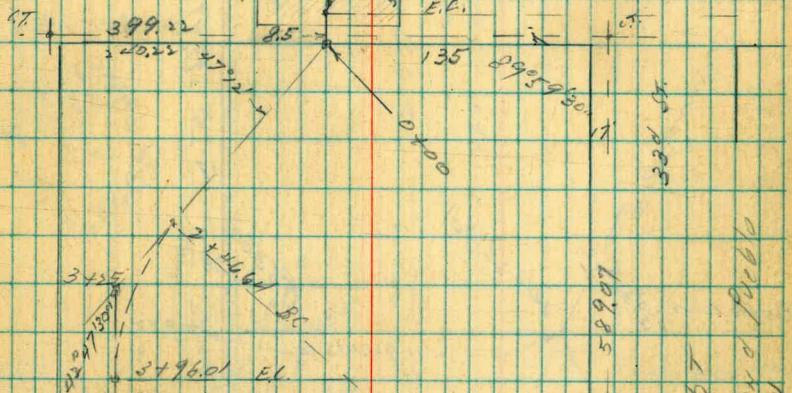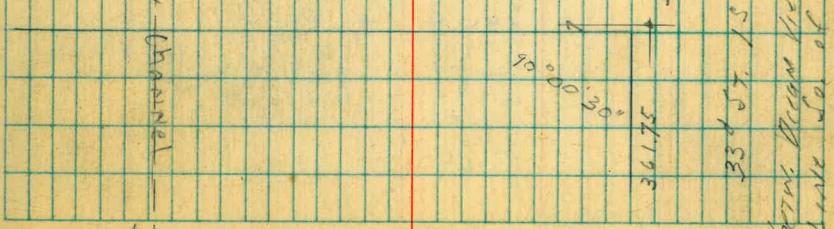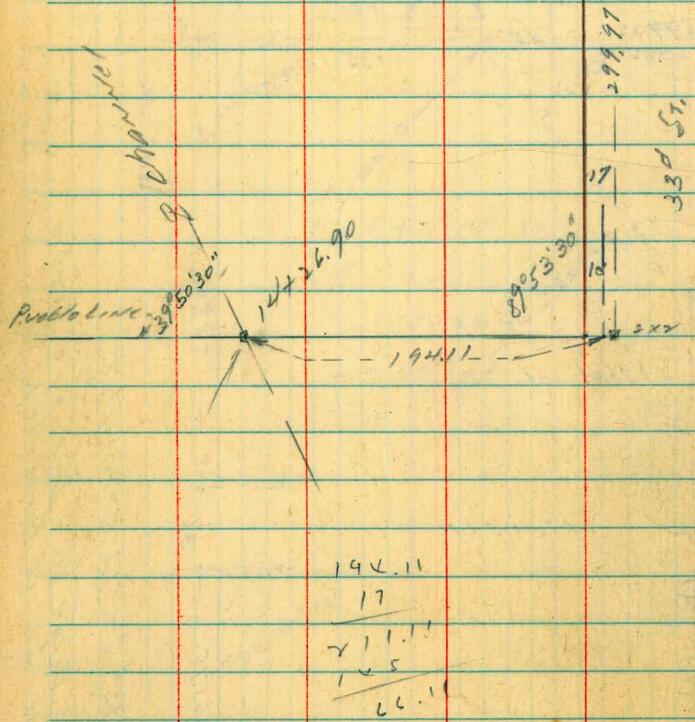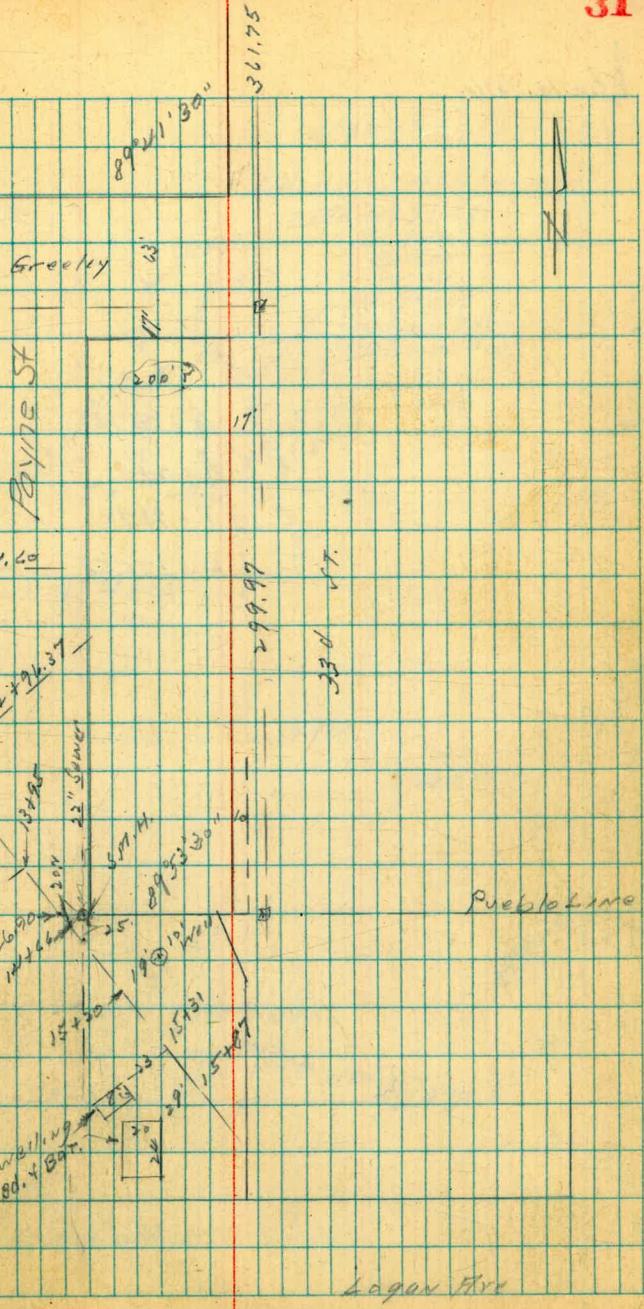
Cholla Valley

$\emptyset = 50°18$

$R = 200$

$T = 93.90$

$L = 175.58$

598.16

56.47½"

Chollas Creek Alignment

March 21-52
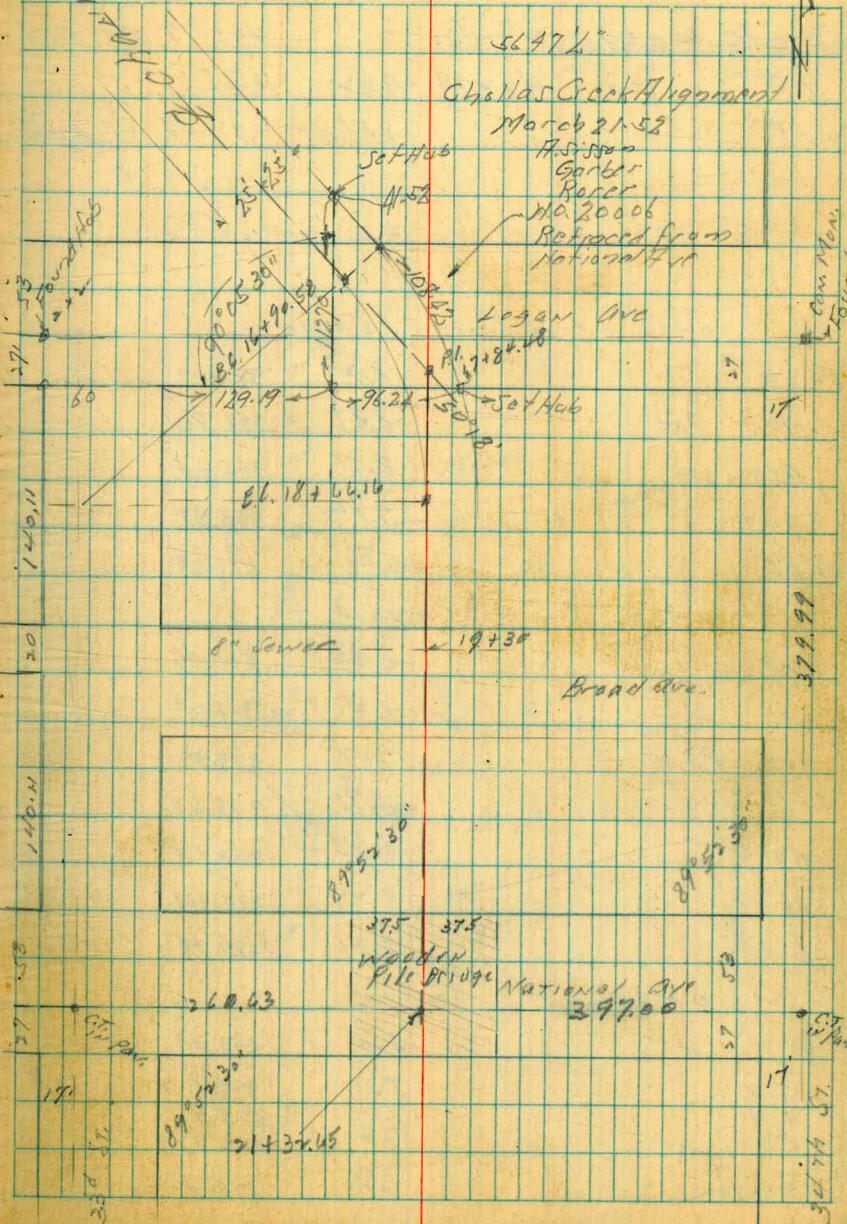
Assessor
Garber
Reese
No. 20006
Retraced from
National Ave.

Logan Ave.

Set Hub

Broad Ave.

8" Sewer

National Ave.
397.00

Wooden
Pile Bridge

260.43

21+3x.45

South of El Cajon

S.E.B.P.	0.56	404.33		403.77	54th El Cajon
T.P.	7.08	402.39	9.02	395.31	
S.W.B.P.			8.51	393.88	53d El Cajon

℄ 53d = Baseline to S. end of curve

0-10 = S. cb line El Cajon

Fl. cb			8.29	394.10
gut Pav			8.89	393.50
C "			8.91	393.48
gut "			9.04	393.35
W.L. cb			8.36	394.03

0+00 S.L. El Cajon

W			8.33	394.06
cb			8.37	394.02
gut Pav			9.07	393.32
C "			8.71	393.68
gut "			8.85	393.54
cb			8.24	394.15
E			8.21	394.18

0+03

E			5.0	393.4
+5			5.3	393.1
+7			7.0	395.4
C			7.6	394.8
+10			27	399.2
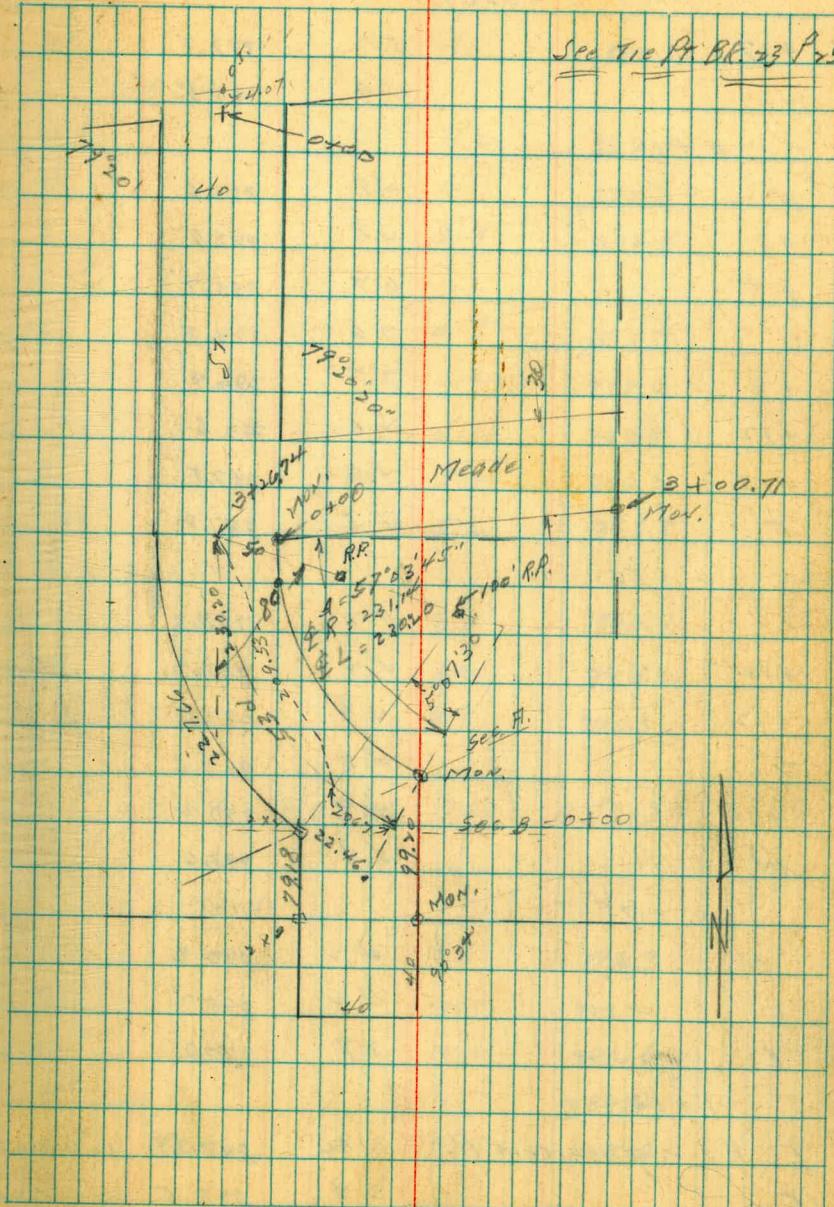
402.39

C +17		5.1	392.3
W		4.9	392.5
0+10			
W		4.8	392.6
+3		4.8	392.6
+5		4.7	395.7
C		7.6	394.8
+6		7.5	394.9
+12		4.8	392.6
+15		4.6	392.8
E		4.5	392.9
0+50			
E		4.2	398.2
+10		4.2	398.2
+12		4.9	392.5
C		4.8	397.6
+10		4.9	392.5
W		4.4	398.0
0+75			
W		4.2	398.2
C		4.2	398.2
E		3.7	398.2
1+00			
E E.s.v. gar. cem fl.	3.80	398.59	12' wide
C		3.9	398.5

402.39

W		4.1	398.3	
1+50				
W		4.6	392.8	
C		4.1	398.3	
E		3.9	398.5	
2+00				
E		4.9	392.5	
+10		4.4	398.0	
+12		5.1	392.3	
C		5.2	392.2	
W		5.6	396.8	
2+50				
W		8.0	394.4	
C		7.2	395.2	
E		6.1	396.3	
T.P.	9.24	402.63	9.00	393.39
N. Meade				
E		9.3	393.3	
C		10.4	392.2	
+15		10.0	392.6	
W		12.8	389.8	
+5		14.0	388.6	

Left page

402.63   B curve

E.L. 53d = 0+00

S on Mon.	12.68	389.95
+7	9.6	393.0
C	9.8	392.8
N	9.3	393.3
0+50		
N	5.9	396.7
C	6.9	395.7
S	7.6	395.0
1+00		
S	5.2	392.2
C	5.3	392.1
N	5.0	392.4
1+50		
N	4.7	392.7
C	4.4	393.0
S	5.1	392.3
+9.5 Porch fl. el.	4.5	392.9
2+00		
S	5.2	392.2
C	4.5	392.9
N	4.7	392.7
2+50		
N	5.4	392.0
C	5.4	392.0

Right page

S		6.0		396.4
3+00.71 = Ely end				
S on Mon		6.86		395.57
C		6.5		395.9
N		6.5		395.9

Resume xsec of 53d St

T.P	1.8	391.23	12.68	389.95
3+19				
E		+1.8		393.0
C		+0.4		391.6
+12		1.2		390.0
W		4.9		386.3
+10		8.2		383.0
3+26.74 = B.C. = 0+00				
+10		8.9		382.3
W		6.9		384.3
+10		2.5		388.7
C		0.6		390.6
+10		0.3		390.9
E		1.8		389.95

391.28   379.04

0+46.04	5°42'22"			
−10	Top Cut		1.5	389.7
E			7.3	383.9
C			8.5	382.7
+10			9.5	381.7
W			13.0	378.2
+10			15.3	375.9
0+92.08	11°24'44"			
−10			18.9	372.3
N			16.6	374.6
+10			13.0	378.2
C			12.3	378.9
+15			11.5	379.7
E			10.0	381.2
+7	Top Cut		5.7	385.5
T.P.	0.67	379.04	12.86	378.37
1+38.12	17°07'06"			
−4	Top Cut		+2.6	381.4
E			0.9	328.1
+4			2.8	326.2
C			3.4	325.6
+10			3.8	325.2
W			7.1	321.9
+10			10.0	369.0

1+84.14	22°49'28"			
−10			12.7	366.3
N			9.8	368.2
+5			8.1	370.9
C			6.5	372.5
+16			5.7	373.3
E			3.8	375.2
+6	Top Cut		0.5	378.55
2+09.53 = E.C. on W+	5°58'07"			
−X			3.9	375.1
E			5.5	373.5
+7			7.3	371.7
C			8.2	370.8
+10			9.6	369.6
N	on hub		11.82	367.22
+10			14.0	365.0
	Sec "A" EC to EC			
W	on hub		11.82	367.22
C			9.0	370.0
E	on Mon.		7.55	372.49
	Sec "B" = 0+00			
E			10.9	368.1
C			11.1	367.9
W	on hub		11.82	367.22
T.P.	0.34	366.52	12.88	366.18

	366.57			
0 + 39.59				
– 10			6.0	360.5
W			5.9	360.6
C			5.4	361.1
E			5.9	360.6
+ 10			5.8	360.7
0 + 79.18				
E			11.5	355.0
C			11.4	355.1
W on hub			12.04	354.48
1 + 19.18 – Sly end 53d St.				
W			16.6	349.9
C			16.1	350.4
E			16.5	350.0
T.P.	12.36	378.52	0.36	366.10
T.P.	12.54	390.68	0.38	378.14
T.P.	13.04	403.53	0.19	390.49
T.P.	4.01	406.13	1.41	402.12
check to B.M.			.33	403.80 403.77
				0.03
SE of 54th & El Cajon				

xsec of 67th 60'wide 10' cbs
Akins to Brooklyn
℄ = Baseline

S 7'LINE IMP LB C.I.	449	234.89'		230.40	WOODMAN IMP.

℄ R.R.

S.L. Akins - 50.5   Sec at 81°46' with 67th

W Top N rail		3.68	231.21 ✓
E " " "		2.58	232.31 ✓
S.L. -17			
E		8.7	226.2 ✓
cb		8.8	226.1 ✓
c		9.2	225.7 ✓
cb		7.2	227.7 ✓
W		7.7	227.2 ✓
S.L. -13			
W		14.0	220.9 ✓
cb		14.0	220.9 ✓
c		13.9	221.0 ✓
cb		12.7	222.2 ✓
E		12.6	222.3 ✓
S.L. Akins in Enanto Creek channel			
E		13.5	222.4 ✓
cb		13.6	222.3 ✓
c		13.8	221.9 ✓
cb		13.3	221.6 ✓
W		13.8	221.1 ✓

Red'd Plot 10-8-41 GDH.

S cb
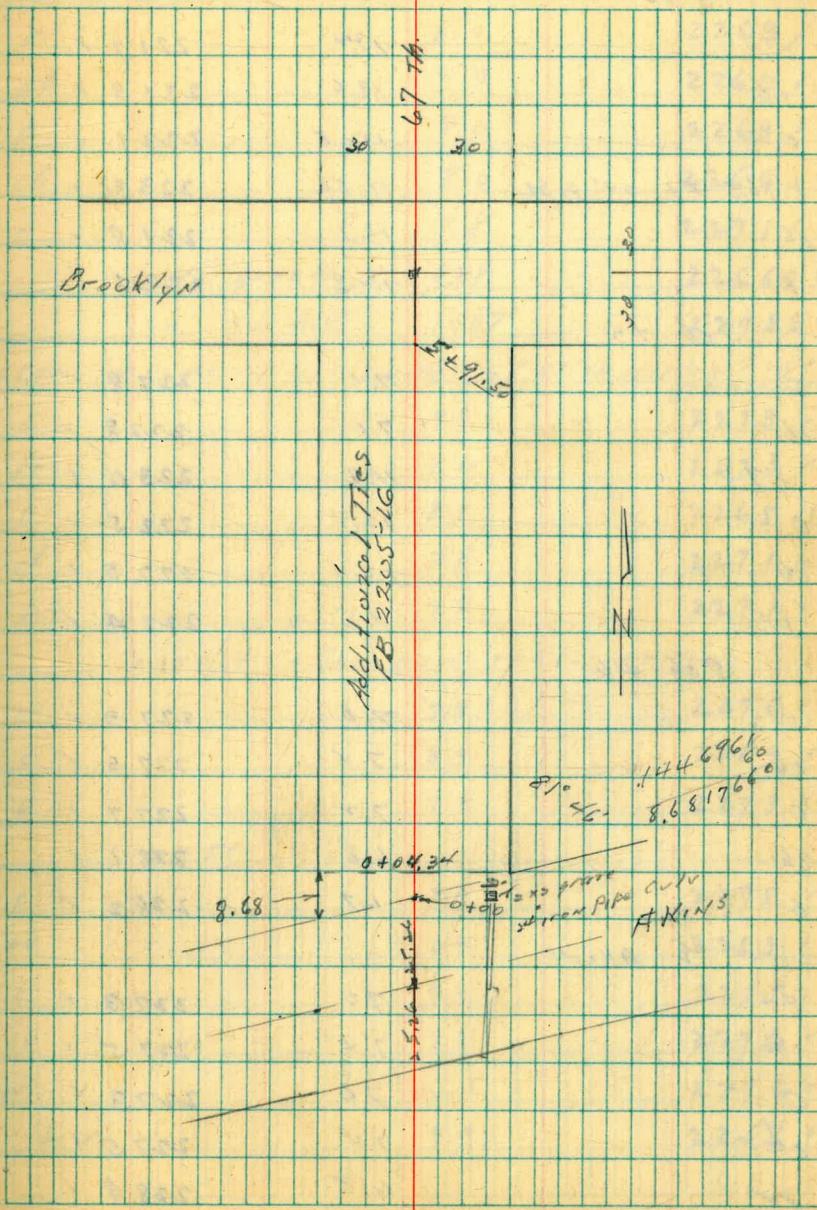
n		13.2	221.7 ✓
cb		13.6	221.3 ✓
c		12.8	222.1 ✓
+ 16.5 ft. 24" pipe		11.58	223.31 ✓
cb		13.1	221.8 ✓
E		12.8	222.1 ✓

S cb + n

E		7.1	227.8 ✓
cb		7.1	227.8 ✓
+ 7		11.9	223.0 ✓
C		12.4	222.5 ✓
cb		12.4	222.5 ✓
N		7.5	227.4 ✓

S cb + 4

W		7.0	227.9 ✓
cb		7.4	227.5 ✓
c		7.2	227.7 ✓
cb		6.8	228.1 ✓
E		6.7	228.2 ✓

E Akins

E		7.6	227.3 ✓
cb		7.4	227.5 ✓
C		7.6	227.3 ✓
cb		7.4	227.5 ✓
N		6.5	228.4 ✓

N cb

W		8.0	226.9 ✓
cb		7.9	226.0 ✓
C		8.0	226.9 ✓
cb		8.0	226.9 ✓
C		7.8	227.1 ✓
culv. grate		8.29	226.60 ✓
" fl box		10.07	224.82 ✓

0+00 = Mt. Akins on angle of el'va with 67 ∟
& Baseline

E		7.6	227.3 ✓
cb		7.6	227.3 ✓
S		8.1	226.8 ✓
cb		7.8	227.1 ✓
N		7.8	227.1 ✓

0+0+36 = sec. now taken at 90°

W		7.9	227.0 ✓
c		8.0	226.9 ✓
E		7.6	227.3 ✓

0+50

E		7.1	227.8 ✓
cb		6.6	228.3 ✓
c		7.4	227.5 ✓
cb		7.3	227.6 ✓
W		7.3	227.6 ✓
+ n		9.3	225.6 ✓

1+00			
-5		8.7	226.2 ✓
N		8.7	226.2 ✓
+5		5.3	229.6 ✓
c6		5.3	229.6 ✓
c		5.7	229.2 ✓
c6		5.0	229.9 ✓
E		5.3	229.6 ✓
1+25			
E		2.5	232.4 ✓
c6		3.0	231.9 ✓
c		3.2	231.7 ✓
c6		4.8	230.1 ✓
N		6.5	228.4 ✓
+5		7.3	227.6 ✓
T.P.	12.56 246.46	0.99	233.90 ✓
1+50			
-5		11.5	235.0 ✓
N		11.4	235.1 ✓
c6		10.7	235.8 ✓
c		10.9	235.6 ✓
c6		11.4	235.1 ✓
E		10.9	235.6 ✓
2+00			
E		1.9	244.6 ✓
+8		1.5	245.0 ✓

c6		2.7	243.8 ✓
c		2.1	244.4 ✓
c6		1.8	244.7 ✓
N		1.6	244.9 ✓
+5		1.6	244.9 ✓
T.P.	12.59 258.76	0.79	246.17 ✓
2+25			
N		8.4	250.4 ✓
c6		9.1	249.7 ✓
+3		10.0	248.8 ✓
C		9.9	248.9 ✓
c6		10.4	248.2 ✓
+2		10.7	248.1 ✓
+3		9.2	249.6 ✓
E		9.3	249.5 ✓
2+50			
E		4.5	254.3 ✓
+9		3.7	255.1 ✓
c6		6.1	252.7 ✓
c		5.5	253.3 ✓
+16		5.3	253.5 ✓
c6		3.5	255.3 ✓
N		2.8	256.1 ✓

T.P.	12.75	271.38	0.13	258.63 ✓
3+00				
N			7.5	263.8 ✓
cb			8.5	262.9 ✓
+3			10.7	260.7 ✓
c			10.8	260.6 ✓
cb			11.2	260.2 ✓
+1			11.2	260.2 ✓
+2			8.8	262.6 ✓
E			8.2	263.2 ✓
3+50				
E			1.3	270.1 ✓
+9			1.3	270.1 ✓
cb			4.3	267.1 ✓
c			3.9	267.5 ✓
+17			4.0	267.4 ✓
cb			2.8	268.6 ✓
N			2.8	268.6 ✓
T.P.	12.87	284.22	0.03	271.35 ✓
3+75				
N			12.3	271.9 ✓
cb			12.2	272.0 ✓
+4			13.9	270.3 ✓

C		13.8	270.4 ✓
cb		13.5	270.7 ✓
+1		12.5	271.7 ✓
E		12.2	272.0 ✓
4+00			
E		9.7	274.5 ✓
cb		10.8	273.4 ✓
C		10.6	273.6 ✓
+17		10.4	273.8 ✓
cb		9.9	274.3 ✓
N		9.9	274.3
4+50			
W		6.0	278.2 ✓
cb		6.3	277.9 ✓
C		6.4	277.8 ✓
cb		6.0	278.2 ✓
E		5.1	279.1 ✓
5+00			
E		2.2	282.0 ✓
+7		2.2	282.0 ✓
+8		3.2	281.0 ✓
cb		3.2	281.0 ✓
C		2.9	281.3 ✓
+16		3.4	280.8 ✓
cb		2.7	281.5 ✓
N		2.8	281.4 ✓

			284.22			
T.P.		990	294.09	0.03	284.19	✓
	5+50					
N				9.2	284.9	✓
cb				9.2	284.9	✓
+6				10.0	284.1	✓
C				9.1	285.0	✓
cb				9.5	284.6	✓
+3				9.6	284.5	✓
+X				8.1	286.0	✓
E				8.0	286.1	✓
	5+91.5					
E				5.5	288.6	✓
+6				5.7	288.4	✓
cb				6.9	287.2	✓
C				6.3	287.8	✓
+10				6.8	287.3	✓
cb				6.3	287.8	✓
W				6.4	287.7	✓
					SW 67th	
Nail in Pole T.P.				4.51	289.58	Brooklyn
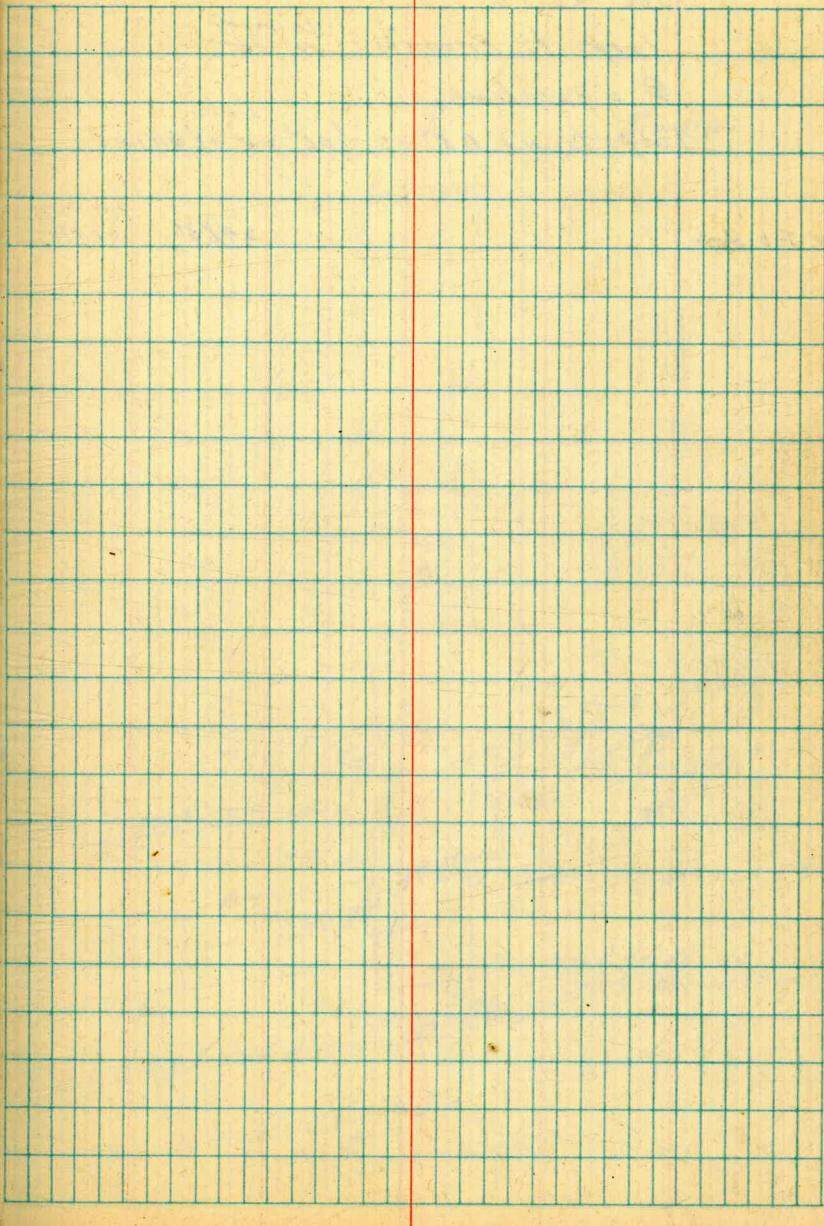
xsec 68th
Imp. to Brooklyn 10' cos co'mode
℄ = Baseline
Imp. to N. Akins Sec° or of Akins

S.W. Top Hyd.   24831   Imp.
                                    68th

Cross Section 68th St
Imperial Ave to Brooklyn Ave

Sketch Page 43

0+89.8 = S End Bridge on Diagonal	176	175	170	
	45	30	23	

0+81   on Diagonal

0+61   21.3 Lt of ℄ - N'ly 8"×8" RR Crossing Sign
0+50.8 = ℄ SD & E RR   on Diagonal

0+25

37.1 = N'ly Power Pole
0+0 = N.L. Imperial   on Diagonal ✓

0-20.5 = N'ly Paving Strip on Diagonal

| BM | 2.93 | 252.24 | | 249.31 | St. & Top F. Hyd Imperial & 68th St |

Lt:L   L   Rt:L

240.1 239.7 249.2 249.3 249.3 249.4 239.3 239.6 239.7
13.1   12.5   3.0   3.9   2.9   2.8   12.9   12.6   13.5
22 on Curb 1.5 Ground 14 N'ly Foot 1.66 N'ly Foot B'dg Deck 9.7 E'ly N'ly Ft Rail 10 Ground 8.0 1.5

246.9 247.0 247.4 249.0 249.1 249.4 248.2 248.5
5.3   5.2   4.8   3.9   3.1   3.8   3.0   3.8
40   30.3   4.2   1.5   1.2   6.0.3

247.29   247.97   248.40
4.95   4.27   3.84
30.3-Top Rail   1.27-Top Rail   30.3-Top Rail

243.9 244.1 243.7 245.6 245.6 246.4 246.5 245.2 245.6
8.6   8.1   8.5   6.6   1.6   5.8   5.7   7.0   6.8
40   30   30   1.5   11   20   30   40

242.4 243.0 243.2 244.6 244.8 244.8 244.2
9.8   8.3   9.0   7.6   7.4   7.1   8.0
40   30.3   1.8   1.5   30.3   40

240.74   242.03   242.83   243.57   244.76
11.58   10.21   9.11   8.67   7.18
86.5   30.3   30.3   30.3

253.24

TP	10.20	265.70	0.59	255.50

2+35   21' Rt of L = Ely 6" Acacia T ✓

2+0

1+77   218' Lt of L = N'ly Telp Pole ✓

1+55   218' Lt of L = N'ly & S'ly 0.19 6" Acacia Tree

        222.2 Lt of L = N'ly Power Pole ✓
1+53.6   on Diag

TP	5.54	256.09	1.69	250.55

1+26.3 = L Akins

1+07   on Diag

1+03.8 = N End Bridge on Diagonal ✓

	2350	2345	2352
	172	177	170
	45	303	24

252.34

Right page (grid):

2535   2535   2530   2044   2537   2554   2552
26   26   31   47   24   07   05
30   20   16   15   19   30

252.1 252.19 252.1 2515   2525   254.4 253.1 2539
40   0.90   40   16   36   40   30   28
30   398   20   16   14   18   30
       Curb Corner

251.02 249.8 250.4 246.80 250.2 250.8 2436 247.57 2506 2525
507   603   57   920   59   653   355   857   556   36
300   303   28   13   18   11   18   15   30
        TopCorb   Inlet   256.09 Inlet
                       Corner   Corner

        2488   2496   2502   2502   250.2
        31   21   20   20   20
        80   10   20   30

2484   2489   249.4 2498   249.6 250.0 249.8
30   30   30   704   26   22   24
40   203   14   16   603

2401 244.27 240.6 249.3 249.4 249.6 249.4 239.9 245.17 240.3 240.4
141   797   146   78   28   26   28   160   207   130   118
      181   18   110   9   110   205   388   45
Brdg   Ground   Foot Walk   Head   outF
Brkwl   wk   Cul wl

252.34

Cont on Page 49

4+50				
		.		
4+32				
4+31	21.6 Lt of ℄ = N'ly 10" Acacia Tree			
TP	11.63	276.81	0.52	265.18
4+0				
3+55	21.6 Lt of ℄ = N'ly & W'ly of 9 Acacia Tree			
3+50				
3+48	31' Rt of ℄ = E'ly of 6" Tree ✓			
3+26	19.8 Rt of ℄ = E'ly 6" Tree ✓			
2+16	23' Lt of ℄ = N'ly Power Pole ✓			
3+04	21.0 Rt of ℄ = E'ly 6" Tree ✓			
3+0				
2+70				
		265.70		

Right page (grid):

269.3	268.7	267.4	267.8		266.8	267.9	268.1
7.5	8.4	9.1	9.0		10.0	8.9	8.7
30	18	14			16	19	30

269.18	268.84
7.63	7.98
10.07 Hole	2.96 Lt/Cen

Hol Cen 276.81 ✓

276.81

266.1	265.7	264.3	264.5	263.2	261.2	265.3
+.04	0.0	1.4	1.2	7.5	1.5	9.4
30	18	15		15	18	30

261.5	261.2	260.0	261.1	259.9	261.1	262.2
1.2	4.5	5.7	9.6	5.8	4.6	6.35
30	20	16		16	18	30

257.5	257.5	256.7	257.9	257.3	258.2	259.2
8.8	8.7	9.0	7.8	8.4	7.5	8.5
30	20	15		15	17	30

255.9	255.7	254.7	252.2		255.6	257.4	257.7
8.8	10.0	11.0	9.5		10.1	8.9	8.0
30	20	15			15	17	30

265.70 ✓

Xsec 69th
Imp. to Brooklyn 30' wide

S.W. Bor Cor.
2" Pipe   253.44   Imp.
                                   69th

Brooklyn   60   EMon.
                          3+78.77

                        15   15

              1+83.57

                                  AKINS

                    O. I. In Pav. Sta 0+00

Imp.   LISBON
            30   50.
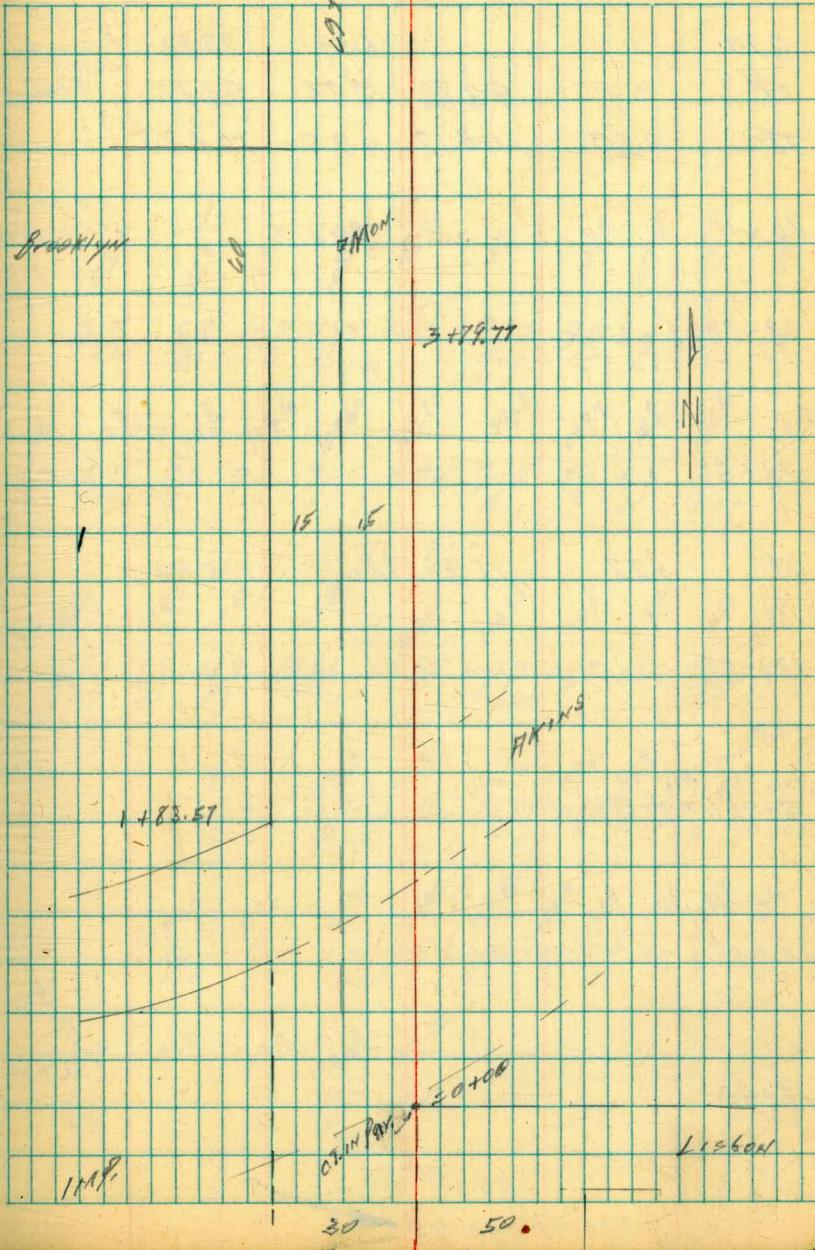
From Page 78

Station	BS	HI	FS	Elev	Notes
BM			6.59	87.23	SNBP Plug Lowell 87.22
TP	0.95	93.82	12.25	92.87	
TP	0.27	105.12	14.95	104.85	
BM			8.94		on Mon NL Macauley + PL 13+78.18
13+78.18					
13+50					
TP	1.22	116.80	12.42	115.58	
13+02.6					
12+72.6 = ℄ Clove					
12+42.6 = ℄ Clove on N					
12+40					128.00
			128.00		

From Page 78

	Lt			℄		Rt			
108.8	108.3	106.6	107.0	106.24	107.10	107.0	108.4	108.8	108.8
8.0 37.5	8.8 21	10.2 18	9.80 15.50	9.56	9.20 4.50	9.8 10	8.4 12	8.0 37.5	8.0 60
110.1	111.7	112.8	109.6	109.60	109.86	109.68	109.7	110.8	112.6 / 113.8
4.7 50	5.1 37.5	6.0 21	9.3 19	7.30 16.50	6.94	7.12 4.50	7.1 9	6.0 11	4.3 37.5 / 5.0 60
				116.80					
111.59	115.2	114.2	114.35	114.45	114.93	114.5	116.0	116.1	116.8 / 116.6
12.1 37.5	13.8 21	13.8 19	12.65 15.50	10.55	13.57 4.50	13.5 9	12.0 11	11.9 20	11.2 23 / 11.4 87.5
117.3	117.53	117.30	117.13	117.0	118.8	119.0	120.9	117.5 120.8 120.5	121.4
10.2 37.5	10.47 19.50	10.70	10.87 4.50	11.0 9	9.2 11	9.0 18	7.1 23	7.2 87.5	4.6 60
120.9	119.6	120.30	120.09	119.95	120.0	121.7	122.0	123.7	123.6 / 124.1
8.0 37.5	8.4 27	7.70 15.50	7.91	8.05 3.50	8.0 8	6.2 11	5.0 19	4.3 42	4.4 37.5 / 3.9 50
121.2	121.2	119.7	120.48	120.35					
8.8 37.5	6.8 30	8.8 24	7.52 18.50	7.65					
				128.00					

Cont From Page 46

BM		3.76	279.52	Brooklyn 68+45t
6+20.55 = St Brooklyn				
6+16	22.0 Rt of ₵ = Ely Fire Hyd			
6+0	22.0 Lt of ₵ = Nly Power Pole			
TP	7.20	283.28	0.73	276.08
5+76	31.6 Lt of ₵ = Nly 10" Acacia Tree			
5+53				
5+46	= ₵ 6.6 Conc Drive on Lt			
5+0				
4+80	22.0 Lt = Nly Power Pole			
4+56	= ₵ 7' Conc Drive on Lt			
	276.81 BkFord From Page 46			

Lt			₵		Rt	
279.4	279.1	277.7	278.4	277.3	277.9	278.5
3.9	4.2	5.6	4.9	6.0	5.1	4.8
30	20	14		18	30	38
278.4	278.0	276.6	277.2	276.4	277.1	277.3
4.9	5.3	6.9	6.1	6.9	6.2	6.0
30	20	14		19	30	30
			283.28			
	275.43	275.00				
	188	181				
	300 Driveway	210 End of Conc Driveway				
274.76	274.18	273.5	273.9	272.9	273.5	273.8
2.05	2.63	3.8	2.9	3.9	3.3	3.0
300 Drive	188 Edge of Conc Drive	14		19	20	30
271.7	271.6	270.6	270.9	270.2	271.0	271.0
5.1	5.3	6.3	5.9	6.6	5.8	5.8
30'	20	14		19	20	30
269.97	269.41	268.96				
6.31	2.40	7.8				
10 of Dr.	30 of Dr.	210 End of Conc Dr.				
			276.81			
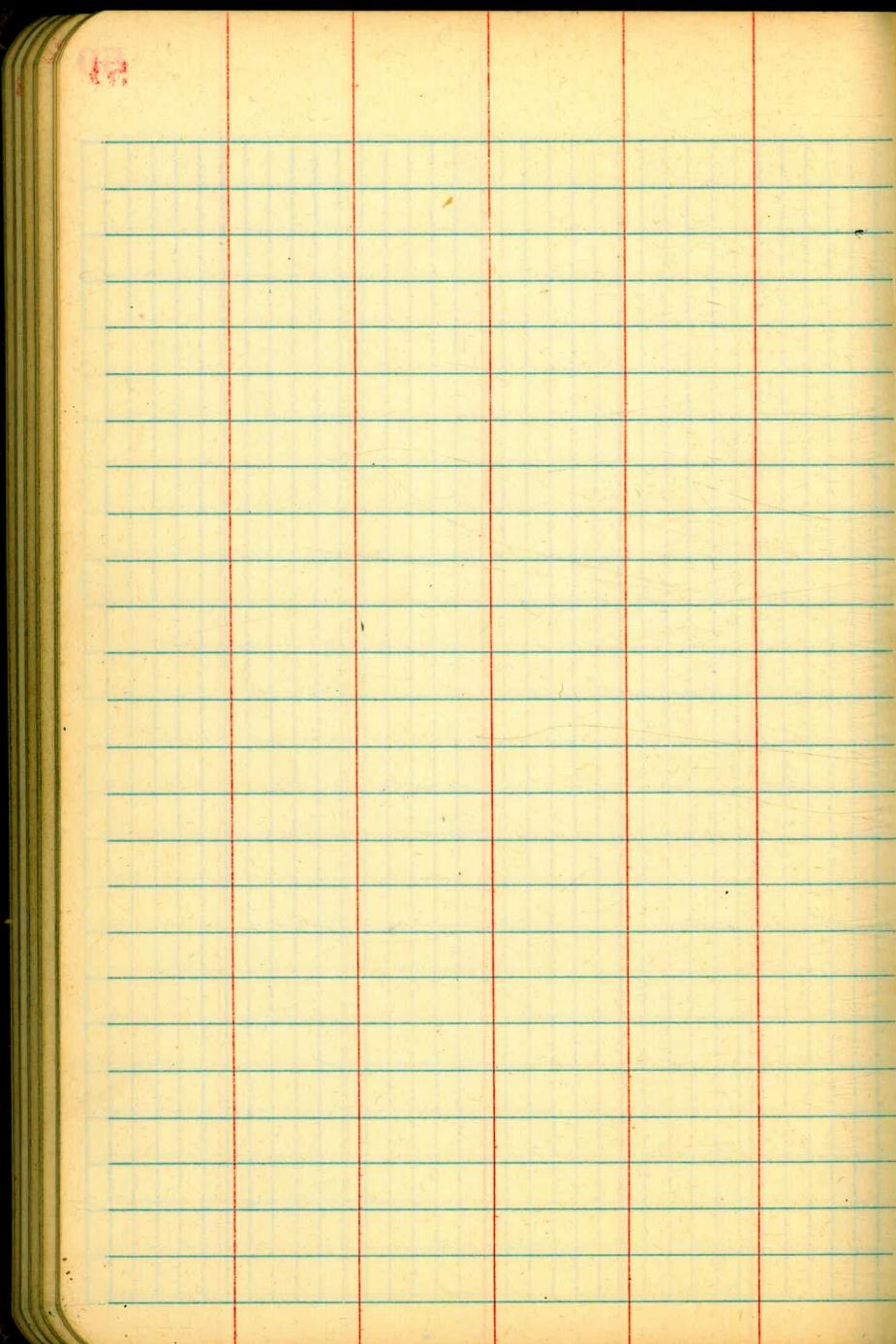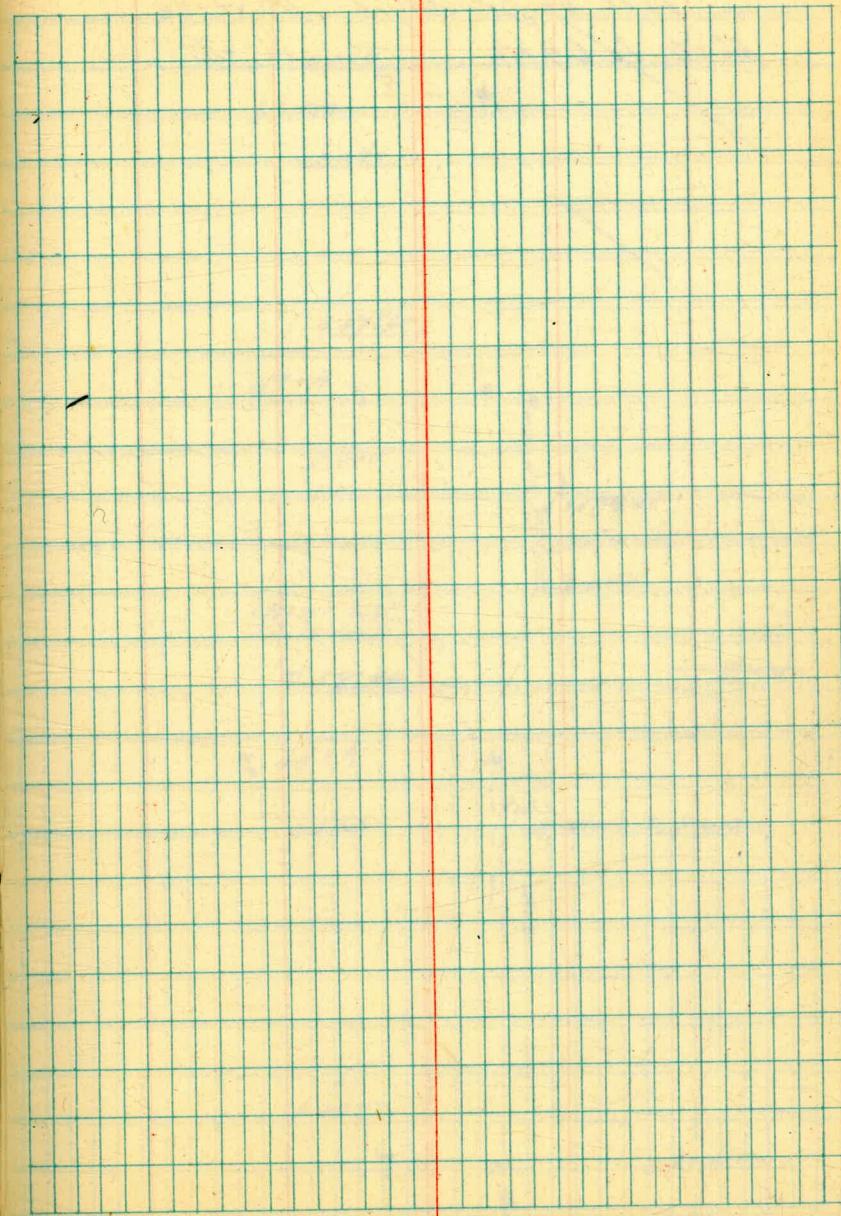
XSec of Brooklyn   60' wide
66th to 69th   10' cbs

0+00
66th
0+40

4+75.61
67th   60
0+00

Brooklyn   1+89.48
wide centerwalk
3+46

chisel
cross row
7+86.44

60   68th
0+00

cross top wall

6+05.72
30   69th

X Sec of Proposed 80' Ext.
of 34th St. & Chollascreek
Market to Federal Blvd.

4+86.20 EC.

A = 38° 00' LT.
R = 400
T = 137.73
L = 265.29
4,297 = 1

3+58.64 P.I.

2+20.90 B.C. LT.

0+92.53 P.O.T.

0+00 N.L Market St.

Moore
Osborn
Hale
3-14-40

4+86.20 EC.

2+20.40 B.C.

4+86.7   19° 00.0
+50   16° 24.5
4   12° 49.6
+50   9° 14.7
3   5° 39.9
2+50   2° 05.0

Nail

Nail

Conc.
Bridge
75'

See T.P. BK
for 34th opening

To 20° 30' & Market St.
Conc. Pavt.

Federal Blvd.

17   43

22   44

4 + 86.20 E.C.

35th

See Map # 1172

264.93 — 100 —

555'

24°0.36'

90.7

39.24

11+79.50
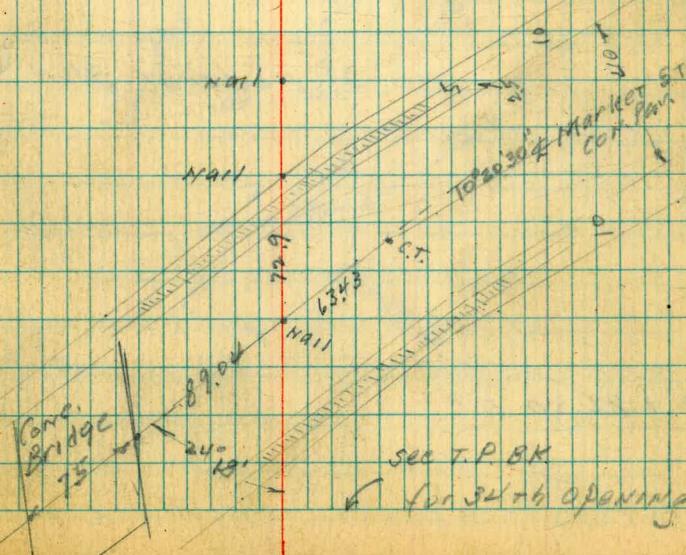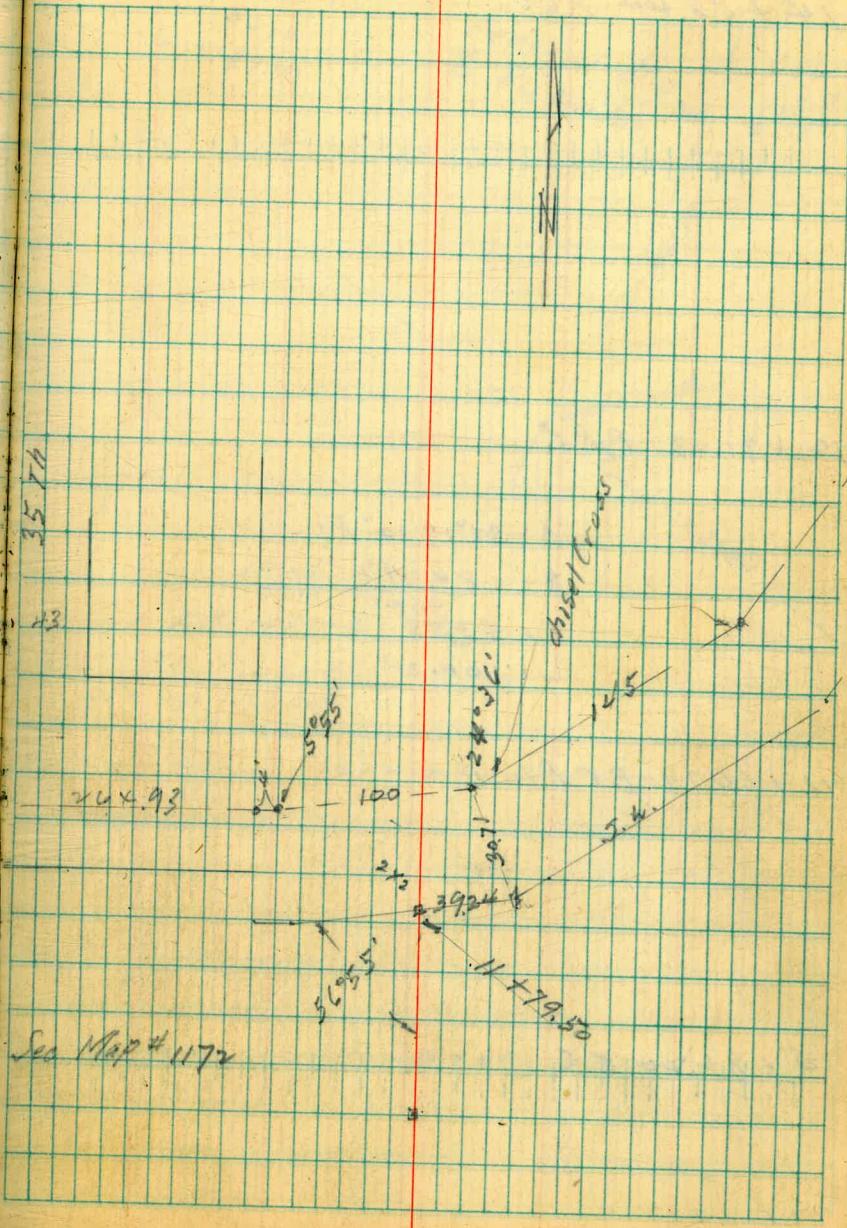
14 + 58.44 P.C.C.

12 + 71.03 PRC

$\Delta = 32°19'30" Rt$

$R = 184.77$

$T = 53.55$

$L = 104.24$

11 + 66.79 B.C. Rt.

4 + 86.20 E.C

$\Delta = 12°47'$ Lt.

$R = 840$

$T = 94.10$

$L = 187.41$

Federal Blvd
℄ 36' Con Pav

Pt.
chisel
cross

94.10'

nail in Pav.

PRC 12 + 71.03

chisel Rt.
cross

0.25

See F.B. 1561-3

" FB. 1602-2

Set cap tack set

2 x 2 6

1 x 1

41^{70}	41^{10}	33^{60}	33^{40}	57^{60}	63^{00}	63^{20}	59^{40}	✓
$\frac{27.4}{15.0}$	$\frac{27.5}{97}$	$\frac{30.0}{75}$	$\frac{30.2}{37}$	6.0	$\frac{0.6}{15}$	$\frac{0.4}{12}$	$\frac{4.2}{40}$	

41^{70}	33^{60}	33^{50}	39^{60}	47^{80}	55^{70}	55^{40}	✓
$\frac{27.6}{135}$	$\frac{30.0}{105}$	$\frac{30.1}{65}$	$\frac{24.0}{35}$	1.58	$\frac{8.4}{10}$	$\frac{8.2}{17}$	

41^{70}	33^{40}	34^{90}	40^{50}	53^{50}	✓
$\frac{27.4}{115}$	$\frac{30.2}{100}$	$\frac{28.7}{50}$	$\frac{23.1}{32}$	10.1	

47^{2}	53^{50}	59^{40}	✓
$\frac{15.7}{80}$	10.1	$\frac{4.2}{80}$	

47^{37}	48^{28}	51^{87}	53^{48}	57^{36}	✓
$\frac{16.23}{75}$	$\frac{15.32}{50}$	11.73	$\frac{10.12}{23}$	$\frac{6.24}{73}$	

approx. parcel

63.60

---

0 + 60

0 + 25

0 + 00   AT 90° WITH ₵ of Prop. EXT.

0 + 00   on N ₵ Market

0 -24.3 N c₵ Market

T.P.	1.97	63.60	12.94	61.63
T.P.	0.58	74.57	12.63	73.99
NEBP	0.97	86.62		85.65 Market 35??

T.P.	3.43	64.87	0.71	61.44

2 + 50

41⁶⁵	41⁵⁵	41⁵⁵
20.5 / 200	20.6 / 100	20.6 / 90

43³⁵   42⁰⁵   38⁴⁵   34⁵⁵   37³⁵   35³⁵   44⁰⁵   57⁷⁵   70¹⁵   85⁷⁵
18.8/75   20.1/65   23.7/37   27.6/30   24.8/27   24.8   18.1/70   4.4/20   +8.0/40   +23.0/60

Top S.M.H.

2 + 20.90 BC LT.

41²⁵	41¹⁵
20.9 / 200	21.0 / 100

41¹⁵   43¹⁵   40⁹⁵   35⁰⁵   34⁸⁵   34⁸⁵   40⁰⁵   56⁹⁵   67¹⁵   85⁸⁵
21.0/90   19.0/75   21.2/50   27.1/20   27.3   27.3/8   22.1/19   5.7/24   +5.0/40   +23.7/65

1 + 70

41²⁵	41²⁵
20.9 / 200	20.9 / 100

43¹⁵   41⁵⁵   39³⁵   38¹⁵   34⁴⁵   34⁰⁵   44⁵⁵   73⁸⁵   89⁸⁵   90¹⁵
19.0/80   20.6/70   22.8/50   24.0/32   27.7/23   28.1   17.6/14   +11.7/40   +27.7/60   +28.0/70

1 + 40

41⁰⁵
21.1 / 200
Field El. →

41¹⁵   42⁶⁵   36⁰⁵   33⁹⁵   34⁰⁵   37³⁵   43⁵⁵   80⁸⁵   82⁵⁵
21.0/100   19.5/75   26.1/35   28.4/30   28.1/13   24.8   18.6/11   +18.7/40   +20.4/60

0 + 92

41⁴⁵	41³⁵
20.7 / 200	20.8 / 150

41⁴⁵   35⁵⁵   34⁰⁵   34⁰⁵   55⁴⁵   76¹⁵   74²⁵   72⁵⁵
20.7/86   24.6/60   28.1/65   28.1/25   6.5/27   +14.0/40   +12.4/50   +10.4

T.P.	3.13	62.15	4.58	59.02
		63.60		

62.15

43⁹⁷	43⁸⁷	44⁵⁷	36²⁷	37⁶⁷	42⁶⁷	52⁶⁷	62²⁷	71⁴⁷	74⁹⁷

5

43^{97} / $\frac{20.9}{500}$

43^{87} 44^{57} 36^{27} 37^{67} 42^{67} 52^{67} 62^{27} 71^{47} 74^{97} ✓
21.0 20.3 28.1 27.2 22.4 12.7 7.4 +6.6 +10.1
85   70 58 32 18   20 40   50

+86.20 E.C.

43^{67} / $\frac{21.2}{200}$

43^{67} 44^{47} 36^{67} 37^{57} 41^{57} 53^{57} 62^{27} 67^{47} 71^{27} ✓
21.2 20.4 28.2 27.3 23.3 11.3 2.6 +2.6 +4.4
85   70 58 32 17   20 40   50

+50

43^{47} / $\frac{21.4}{200}$

43^{87} 44^{77} 36^{77} 37^{27} 42^{67} 55^{27} 70^{87} 81^{07} 87^{27} ✓
21.0 20.1 28.1 27.6 22.2 9.6 +6.0 +14.2 +22.6
90   80 56 30 17   20 40   50

4

42^{77} / $\frac{27.1}{200}$

42^{77} 42^{87} 43^{77} 36^{47} 36^{57} 46^{77} 62^{57} 73^{97} 80^{37} ✓
27.1 22.0 21.1 28.4 28.3 18.1 2.3 +9.1 +15.5
200   90 75 50 20   20 20   50

3 +50

42^{87} / $\frac{22.0}{200}$

42^{77} 43^{47} 36^{37} 36^{47} 52^{7} 63^{07} 73^{87} 80^{97} ✓
22.1 21.4 28.5 28.4 12.7 1.8 +7.0 +16.1
90   70 40 18   20 40   50

3 +00

42^{67} / $\frac{22.2}{200}$

42^{87} 44^{47} 42^{47} 36^{27} 36^{27} 47^{77} 58^{87} 71^{87} 78^{17} ✓
22.0 20.4 22.4 28.6 28.6 17.1 6.0 +7.0 +13.3
90   77 61 38 11   20 40   50

1

44.87

64.87

E

Left page:

+45

	45^{61}	45^{61}	46^{01}
	18.8	18.2	17.8
	250	150	130

7

	45^{41}	45^{31}	45^{51}	43^{21}
	18.8	18.5	18.3	20.6
	200	130	120	105

+50

	45^{21}
	18.6
	200

+18

	44^{31}
	19.5
	200

6

	44^{31}	44^{21}
	19.6	19.6
	200	110

S.M. H. RIM   5+88 = 57 LT   23.31

5+50

	43^{81}
	20.0
	200

T.P.   3.24   63.81 ✓   4.30   60.57 ✓

      64.87 ✓

Right page:

41^{81}	44^{71}	38^{81}	38^{61}	39^{81}	43^{61}	57^{61}	73^{81}	80^{51}	
22.0	19.1	25.0	25.4	24.0	20.2	4.2	+10.0	+16.7	✓
89	83	70	48	20		20	40	50	

47^{21}	38^{81}	38^{21}	38^{61}	40^{81}	52^{91}	65^{51}	76^{21}	82^{71}	
21.6	25.0	25.6	25.2	23.0	10.9	+1.7	+12.4	+18.9	✓
75	64	52	30	15		20	40	50	

45^{51}	43^{61}	44^{21}	38^{41}	37^{81}	51^{41}	64^{51}	65^{41}	64^{21}	
18.3	20.2	19.6	25.4	26.0	12.4	+0.7	+1.6	+0.4	✓
120	105	70	50	22		23	40	65	

44^{71}	41^{41}	41^{81}	37^{81}	37^{51}	47^{61}	51^{11}	64^{31}	66^{91}	
19.1	22.4	22.0	26.0	26.3	16.2	12.7	+0.5	+3.1	✓
100	85	60	50	27		20	40	50	

44^{61}	41^{11}	41^{61}	37^{21}	37^{41}	54^{51}	61^{31}	67^{51}	72^{51}	
19.7	22.7	22.2	26.1	26.4	9.3	2.5	+3.7	+8.7	✓
100	85	60	50	27		20	40	50	

44^{11}	44^{81}	39^{81}	42^{11}	37^{41}	36^{81}	50^{71}	56^{41}	61^{41}	72^{41}	78^{01}	
19.7	19.0	24.0	21.7	26.4	27.0	3.1	7.1	2.6	+8.0	+14.3	✓
110	100	80	70	55	27	14		13	40	50	

63.81 ✓
—
5

+50		48^{45}	48^{35}	44^{85}	52^{85}	44^{15}	41^{25}	42^{65}	43^{75}	47^{35}	48^{95}	49^{85}	55^{65}	67^{55}	✓
		8.4	8.5	12.0	4.0	12.7	15.6	14.8	13.1	9.5	7.0	1.2	+10.7	
		200	150	140	125	115	70	40	20	18	7.9	10	20	40	
10		48^{35}	48^{35}	41^{65}	40^{75}	49^{75}	40^{65}	40^{75}	42^{15}	43^{95}	42^{45}	47^{65}	47^{85}	48^{15}	56^{05}	68^{55}	✓
		8.5	8.5	15.2	14.1	7.1	16.2	16.6	14.7	13.7	14.4	9.2	9.0	8.7	0.8	+11.7
		200	145	135	127	110	99	79	61	20	18	11	5	20	40
+50		47^{45}	47^{35}	40^{45}	41^{85}	44^{85}	39^{85}	40^{35}	41^{55}	41^{85}	44^{85}	45^{75}	54^{85}	$64.^{45}$	✓
		9.4	9.5	16.4	15.0	12.0	17.0	16.5	15.3	15.0	12.7	2.0	+7.6	
		200	144	133	106	100	92	60	40	27	20	11.1	20	40	
9		46^{75}	46^{35}	39^{95}	40^{85}	45^{85}	40^{15}	38^{95}	41^{45}	42^{85}	44^{45}	44^{45}	47^{45}	63^{05}	✓
		10.1	10.5	16.9	16.0	11.0	16.7	17.7	15.4	14.0	12.4	9.4	+6.2	
		200	130	128	101	92	82	80	34	25.	13.4	7	18	40
+50	46^{75}	46^{65}	43^{75}	39^{85}	40^{15}	45^{75}	40^{35}	38^{85}	39^{25}	40^{65}	40^{45}	42^{65}	43^{35}	43^{85}	46^{05}	68^{75}	✓
	10.1	10.2	13.1	17.0	16.7	11.1	16.5	18.0	17.4	18.2	16.4	14.2	13.0	10.8	+1.4
	200	135	125	118	100	90	82	75	55	27	27	25	12.5	15	24	40
8+00		46^{65}	46^{65}	44^{65}	43^{65}	40^{45}	45^{85}	39^{65}	38^{95}	40^{85}	42^{35}	44^{35}	53^{05}	61^{85}	✓
		10.2	10.2	12.2	13.2	16.4	11.0	17.2	17.9	16.0	17.5	3.8	+5.0	
		200	140	135	110	99	85	72	48	40	14.5	15	25	40

T.R	2.90	56.85 ✓	3.07	53.95	B.C. Hub 11+66.79
T.P.	4.30	57.02 ✓	13.09	50.72	
		63.81			56.85 ✓

12 + 18.91

+ 92.85

+ 80

+ 66.79 B.C. RT

+ 50

11 + 00

56.85

54³⁶	54⁸⁰	54⁶⁷	54⁷¹	55³⁵ 63⁴⁵		72²⁵

N edge 2.49 / PAV. 17   2.05 / 13   2.18 / 45 S edge pav   2.14   1.5 / 17   + 6.6 / 25   + 15.4 / 40 ✓

54⁷⁶	54⁴⁴	55²⁵	55⁵⁵	69⁸⁵

2.79 / 40   2.41 / 55.5 S edge pav   1.6   1.3 / 18   + 13.0 / 40 ✓

PAV

54⁶⁰	54³³	55¹⁵	55²⁵	68⁰⁵

℄ E end   2.25 / 64   2.52 / 33   pp are st. ℄ bent / 18   1.7   1.6 / 19   + 11.2 / 40 ✓
bridge   S edge pav

54⁶⁰	51⁹⁵	53¹⁵	53⁹⁵	54⁸⁵	66⁸⁵

Deck   2.25 / 64   4.9 / 43   3.7 / 28   2.9   2.0 / 50   + 10.0 / 40 ✓
SE Cor.
Bridge

43⁵⁵	43⁸⁵	48³⁵	52³⁵	54³⁵	65⁵⁵

under   13.3 / 90   13.0 / 60   8.5 / 40   4.5   2.5 / 20   + 8.7 / 40 ✓
bridge

47²⁵ 44³⁵ 41⁹⁵	43³⁵ 47²⁵	50⁵⁵ 52⁴⁵ 57⁴⁵	62⁹⁵

5.6 12.5 14.9 / 137 130 87   13.5 9.1 / 37 51   4.4 + 10.6 + 6.1 / 14 30 20 ✓

54³⁵	51⁵⁵

2.5 / 158   5.3 / 142

56.85

Left page:

14 + 58.44 PCC

14 + 11.58

+ 64.73

13 + 17.88

12 + 71.03 PRC

12 + 44.97

$$\frac{60.22}{5.19 4} \begin{array}{r} 8.28 \end{array} = 51.87 \quad \begin{array}{l} NWBP \\ 35^{th}4\ Fed. \end{array}$$

T.P.   6.27   60.22 ✓ 2.90   53.95 ✓

        56.85 •

Right page (survey grid):

48^{12}	49^{22}	56^{22}	56^{02}	56^{39}	56^{19}	57^{02}	65^{22}	66^{22}✓
$\frac{12.1}{50}$	$\frac{11.0}{40}$	$\frac{4.0}{30}$	$\frac{4.20}{18}$	3.83	$\frac{4.03}{18}$	$\frac{3.2}{30}$	$\frac{+3.5}{35}$	$\frac{+9.0}{40}$

	55^{42}	55^{61}	56^{11}	55^{98}	56^{72}	60^{82}	61^{82}
	$\frac{5.0}{40}$	$\frac{4.61}{18}$	4.11	$\frac{4.24}{18}$	$\frac{3.5}{30}$	$\frac{+0.6}{34}$	$\frac{+1.61}{40}$ ✓

	49^{32}	54^{62}	55^{35}	55^{83}	55^{76}	56^{42}	67^{42}	✓
	$\frac{10.9}{30}$	$\frac{5.6}{28}$	$\frac{4.87}{18}$	4.39	$\frac{4.46}{18}$	$\frac{3.8}{30}$	$\frac{+7.2}{40}$	

48^{32}	48^{82}	54^{82}	54^{92}	55^{41}	55^{38}	57^{22}	76^{62}	78^{82}
$\frac{11.9}{50}$	$\frac{11.4}{40}$	$\frac{5.4}{30}$	$\frac{5.30}{18}$	4.71	$\frac{4.84}{18}$	$\frac{3.0}{35}$	$\frac{+16.4}{38}$	$\frac{+18.6}{40}$

48^{22}	49^{22}	54^{92}	54^{64}		55^{16}	55^{02}	55^{22}	59^{82}	80^{32}	✓
$\frac{12.0}{50}$	$\frac{10.5}{40}$	$\frac{5.3}{28}$	$\frac{5.58}{18}$	5.06	$\frac{5.20}{18}$	$\frac{5.0}{25}$	$\frac{0.4}{35}$	$\frac{+20.1}{40}$		

47^{22}	48^{62}	55^{02}	54^{47}	54^{99}	54^{86}	56^{22}	70^{52}	✓
$\frac{13.0}{50}$	$\frac{11.6}{40}$	$\frac{5.2}{30}$	$\frac{5.75}{2.13}$	5.25	$\frac{5.36}{14.6}$	$\frac{4.0}{27}$	$\frac{+10.3}{40}$	
			N edge pail		S edge			

60.22 ✓

S E B P	2.41	34.51		32.10	Sunset Cliffs Narragansett
	0 - 17				
S pav.			5.86	28.65 V.	
N "			6.13	28.38 V.	
0+00 E.h. Sunset Cliffs Blvd.					
N cb			5.30	29.21 V.	
N pav.			5.48	29.03 V.	
C "			5.65	28.86 V.	
S "			5.36	29.15 V.	
S cb			5.09	29.42 V.	
0+03					
S			4.1	30.4	
+4			5.3	29.2	
C			5.4	29.1	
+6			5.5	29.0	
N			4.5	30.0	
0+28					
N			3.4	31.1	
C			4.0	30.5	
S			3.1	31.4	
+0.75 cem. Porch			1.66	33.05	
0+67					
S			2.8	31.7	
C			3.2	31.3	

Red't Plot on new Profile 6-4-40 EJH

Ebers ST.

Niagara

Narragansett

A.C. Pav.
C.T.
140
140
5+98.65

10 10

0+00

140.02   140.03

A.C. Pav.

Sunset Cliffs Blvd.

53

West   C.T.   7' Line

	34.51			
N		3.0	31.5	
+r w.L apron		3.04	31.47	
+3.8 " 2 car gar		r.85	31.66 Cem	
0 + 86				
+ 3.6 E.L. r car. gar		2.77	31.74 "	
- 4x " apron		2.90	31.61	
0 + 94				
- 3.5 Sin. gar		2.85	31.66 "	
N apron		2.88	31.63 "	
C		2.9	31.6	
S "		2.68	31.83 "	
+ 2.8 Sin gar.		2.64	31.87 "	
1 + 00				
S + 0.6 P. P.				✓
N + 0.6 Tel. P.				✓
1 + 12				
S - 4.5 E do. strip Dr.		2.40	32.11 "	
S - 60 " gar.		1.20	33.31 "	
1 + 50				
S		2.3	32.2	
C		2.3	32.2	
N		2.3	32.2	
1 + 83				
N - 27 Sin. gar.		1.7	32.8 dirt	

1 + 89

beg. Bd. fence on N 1.3 in alley ✓

End " " " " " " at 1 + 96.5 ✓

and w/L of Bd. shed 10' wide ✓

2 + 00

N		1.2	33.3
C		1.2	33.3
S		1.0	33.5

2 + 06.5

beg. of Bd. fence on N 1.3 in alley .

2 + 20

S + 0.5 P.P. ✓

2 + 30

end of Bd. fence on N 1.3 in alley ✓

2 + 28

S - 4.5 Sin. gar.		0.0	34.5 dirt	
2 + 40				
N - 2.9 E do. gar.		0.3	34.2 "	?
2 + 51				
N + 0.9 Tel. P.				✓

T. P.	13.15	47.35	0.31	34.20

2 + 50

S		13.0	34.4
C		13.2	34.2
N		13.1	34.3

2 + 64			
N - 20 E do. gar.	13.1	34.3	con. strips
2 + 73			
N - 20 S.N. "	13.0	34.4	dirt
2 + 92			
S - 1.0 S.N gar.	11.6	35.8	"
3 + 0.0			
N	12.0	35.4	
C	11.8	35.6	
S	11.6	35.8	
3 + 10			
S - 1.1 E do. gar.	11.0	36.4	wood fl.
N - 3.4 " S.N "	11.5	35.9	dirt
3 + 35			
S	10.8	36.6	
C	10.9	36.5	
N			
+ 3.2 S.N. gar.	11.4	36.0	cent.
+ 4.7 inside gar. on floor	11.2	36.2	"
3 + 49			
S + 0.9 P.P.			
3 + 90			
S - 36 S.N. gar.	6.70	40.65	cent.
4 + 00			
N - 10	9.0	38.4	✓

N		8.0	39.2
C		8.1	39.3
S		7.8	39.6
4 + 08			
S 7.2 S.N. gar.			dirt
4 + 24	7.3	40.1	
N + 0.6 Tel. P.			
4 + 50			
S	5.2	42.2	
+ 0.3 P.P.			
C	5.9	41.5	
N	5.7	41.7	
4 + 92			
S - 6.6 E S.N. gar.	3.0	44.4	dirt
5 + 03			
N	2.6	44.8	
C	2.7	44.7	
S	2.7	44.7	
+ 6.8 W.L. do. gar.	1.90	45.45	cent.
5 + 22			
S - 6.8 E.L. do. "	1.97	45.38	E ½ dirt
T.P.	1.30 59.48	0.17	47.18

	5 + 54		51.03
- 4.7	Sin gar. 9' wide	8.45	Cem
S		8.6	50.9
c		8.9	50.6
+ 7		9.0	50.5
N		8.0	51.5
	5 + 60		
S	4' wide cem. walk	8.00	51.48
	5 + 65		
N	Tel. P.		
	5 + 62		
beg	Con. Ret. wall on S. on Line		
	5 + 85		
N		4.2	55.3
+ 2		5.0	54.5
c		5.1	54.4
S		4.4	55.1
S	Top wall	1.84	57.64
5 + 98.65 W L Ebers St.			
Ret. wall joins c6.			
S c6		2.94	56.54
S Pav.		3.35	56.13
c "		3.86	55.62
N "		3.73	55.75
N c6		3.62	55.86

W c6 Line Ebers

N Pav.		4.18	55.30
S "		3.67	55.81
T.P. 8.55	64.95	3.08	56.40

check to BM. S E B?
Narr. & Ebers   0.82   64.13   64.19

Narragansett St. Extension And Macaulay St.

Grades G.199~

6+09.85 F.C.

Δ 22° 43' 18"
R 500.0
T 100.38

5+59 = Pole 29' Lt of ℄   L 198.14
D 3.4377

4+11.71 B.C.Rt

(See 2005
51-77
1/6/50)

1+98.14 F.C.

Δ 22° 43' 18"
R 500.0
T 100.38
L 198.14

0+0   B.C.Lt

6+97 = Pon Pole

5' Conc Walk

Capistrano
3' Conc Walk

Stucco House

Mendota

N. H. Pole Distance to Property Edge

Chatsworth

Macaulay

℄ Narragansett Ext. 2

℄ Narragansett

Plum 157+87.50 St.

Fd Mon 30.5 37.5

Mon 95° 120°02′46″ SPA 13+78.18

13+35 = Pole 29.5

13+02.62

Clove

12+42.62

12+10 Port Pole 30.2

Fd Conc Mon

R.P. Fd Mon 25 75.02 10+ 47.72 R 2.30′
Pole 81.2 25 100 Split
R.R.

W/conc1 W/9col. 76″wide 76″wide

9+86.2 Mon R.P. 110.00 30x 9+56 = Pole 30″

Olympia St. Fd Mon

Tustin ← C.T. to window sill

9+26.2

9+22 = Pole 60.0 30.5x 9+25 = 30′ Pole tall
-50+ R.R. 46...
50.0 Fd Mon 51880
8+52.70
8+51 = Pole

37.50 37.50

8+09 = Pole 29.8

For Re Cross Section 6+09.85 to 16+50.5 See #172-P 54

X Sec. Plotted 11-22-1943 C.B.H.

1+0

0+75

0+53

0+44 = Fly Paving Taken on Line Par.

0+25

0+14.2 = N C of Chatsworth

Test & Plot 9-24-40 C.B.H.
new Profile

0+0 = n. L Chatsworth or So.

B.N.   5.85   139.04   133.19   N P of Narragansett & Chatsworth

Lt				R't		
128.4	129.9	131.0	132.7	134.5	135.1	135.3
10.6 / 50	10.1 / 40	8.0 / 30	6.3	4.5 / 20	3.9 / 10	3.7 / 50
131.3	131.6	133.1	133.8	135.0	135.5	136.0
9.7 / 50	7.4 / 40	5.9 / 30	5.2	4.0 / 20	3.5 / 10	3.0 / 50
130.4	131.2	132.5	133.7	133.1	136.0	136.4
8.6 / 50	7.8 / 40	6.5 / 30	5.3	3.9 / 20	3.0 / 40	2.6 / 50
132.19	132.74	133.72	134.51	135.34	136.28	136.91
6.85 / 50	6.80 / 40	5.77 / 20	4.53	3.70 / 20	2.76 / 40	2.13 / 50
132.69	133.69	134.62	135.61	136.59		
6.625 / 40	5.85 / 20	4.12	3.13 / 20	2.15 / 40		
133.03	132.2	132.57	133.17	133.63	134.51	135.33	135.90	136.40	137.03
6.01 6.8 / 46.01 46 Gut	6.17 / 40	5.87 / 30	5.41 / 30	4.17	3.71 / 20	3.14 / 40	2.64 2.01 / R't Gut 46.06
133.9	133.97	133.37	134.51	134.93	135.13	135.63	136.04	136.9
5.1 / 40	5.07 / 30-06 30-5 Gut	5.17 / 30-5 Gut	4.53 / 10	4.11 / 08 Par	3.91 / 10	3.51 / 30 Gut	2.80 / 30-06 Gut	2.1 / 40
			139.04			

Cont Page 75

3+53				
2+23				
2+0+			$HI = 132.86$	
2+50				
TP	5.55	132.86	11.73	127.31
1+981/ = F.C.				
1+50				
1+25				
	139.04			

Right page:

Lt			℄		Rt	
126.0	126.3	127.1	128.1	128.1	128.9	128.9
6.9 50	6.6 40	5.2 30	1.8	4.7 20	4.0 40	4.0 50
125.7	125.9	126.8	127.4	127.6	128.2	128.4
7.2 50	7.0 40	6.1 30	5.5	5.3 20	4.7 40	4.5 50
126.3	126.4	126.8	126.9	128.1	127.8	128.2
6.6 50	6.5 40	6.1 30	6.0	4.8 20	5.1 40	4.7 50
125.9	126.1	126.2	126.6	126.8	127.9	127.5
7.0 50	6.8 40	6.7 30	6.3	6.1 30	5.9 40	5.4 50
			132.86			
126.1	125.9	126.3	126.8	127.0	127.8	128.3
13.9 50	13.1 40	12.7 30	12.2	12.0 20	11.2 40	10.7 50
126.9	127.0	127.2	127.2 128.9	130.5	131.6	131.7
13.1 50	13.0 40	11.8 30	11.8 10.1 15	8.5 20	7.1 40	7.3 50
127.4	127.5	128.4	131.2	134.9	134.3	134.5
11.6 50	11.5 40	10.6 30	7.8	4.6 20	4.7 40	4.5 50
			139.04			

X. Sec. Alley Blk. 4. Normal Hts.

3-2-39					
Miller					
Walker					
Bliss					
B.M. B.S.	4.22	398.20		393.98	S.E. Sidney + Mt.View Drive
T.P. B.M. B.P	6.35	398.09	6.46	391.74	S.W. Arthur + 35th St. Dr.
12' S. of N = N.d. Arthur					
125.' E. of E. Line Alley cb			6.49	391.60	= W. Line 35th
" " " " " pav. W. End.			6.92	391.17	
E. ground			6.2	391.9	
E. cnt. cl			5.73	392.36	
₵ ground.			6.1	392.0	
W "			6.0	392.1	
W. cnt. cl			5.59	392.50	
+ 125.' = E. Line Mansfield. pav. E. End.			5.38	392.71	
" = " " cl			5.01	393.08	
1.67' S. of N. (N. End cl. Ret.) (N edge walk)					
N cl + ground			5.32	392.77	
₵ "			5.5	392.6	
E " + "			5.39	392.70	
0+00 = N. Line Arthur					
E			4.6	393.51	
+ 3			5.2	392.9	
₵			5.4	392.7	
+ 5			5.1	393.01	
+ 6			4.5	393.6	
W			3.7	394.4	

Indexed
C.S.K.

Mt. View

Drive

W	2.2	395.9 ✓
+2	2.2	395.9 ✓
+3	4.5	393.6 ✓
¢	4.5	393.6 ✓
+5	4.4	393.7 ✓
E	2.6	395.5 ✓

0+35

E	1.2	396.9 ✓
+2	1.2	396.9 ✓
+3	2.6	395.5 ✓
¢	2.6	395.5 ✓
+4	2.6	395.5 ✓
+5	0.9	397.2 ✓
W	0.9	397.2 ✓

0+46 S. End. Board Fence on W. 0.8' in Alley

0+70

N	1.5	396.6 ✓
+3	1.6	396.5 ✓
+4	2.0	396.1 ✓
¢	2.0	396.1 ✓
+6	2.0	396.1 ✓
E	1.6	396.5 ✓

1+00 = N. End. above Fence on W 0.8' in Alley

E	2.0	396.1 ✓
¢	2.2	395.9 ✓
+5	1.9	396.2 ✓
W.	1.4	396.7 ✓

W	2.6	395.5 ✓
E	2.4	395.7 ✓
¢	2.4	395.7 ✓

2+00

E	3.0	395.1 ✓
¢	2.8	395.3 ✓
W	2.7	395.4 ✓

2+06 garage on W. dirt floor 1.9 Back.

W - 1.9 = floor	2.6	395.5 ✓

2+15 S. End Picket Fence on W. 0.2' in Alley

2+50 Fence on W 0.1 in Alley

W	2.8	395.3 ✓
¢	2.9	395.2 ✓
E	3.1	395.0 ✓

3+00 above picket Fence on W 0.4 Back.

E	3.1	395.0 ✓
¢	3.1	395.0 ✓
W	3.0	395.1 ✓

T.P.	5.96	401.12 ✓	2.93	395.16

3+20 above Fence on W line
3+50 N. End. " " " 0.5 in Alley

W	5.5	395.6 ✓
¢	5.7	395.4 ✓
E	5.5	395.6 ✓

4+00 = S. End Fence on W. 1.2' in Alley

E		5.5	395.6	✓
₵		5.3	395.8	✓
W		5.3	395.8	✓

4+50 above Fence on W. 1.2 in Alley

W		5.4	395.7	✓
₵		5.2	395.9	✓
E.		5.4	395.7	✓

4+66 To 4+81 both House Fence on W. 1.0' in Alley

5+00 Fence on W 0.9 " "

E		5.2	395.9	✓
₵		5.2	395.9	✓
W.		5.4	395.7	✓

5+50 above Fence on W. 0.9' in Alley

W		5.1	396.0	✓
₵		5.3	395.8	✓
E		5.3	395.8	✓

5+76 above Fence on W. 0.8' in Alley
5+76 ₵ = ∠ 22° 30' At. see on split ∠.

E		5.1	396.0	✓
₵		5.2	395.9	✓
W		5.4	395.7	✓ Low. Pt.

5+79 above Fence on W. 0.2' Back.
6+00

W - 5		5.6	395.5	✓ Low. pt
W		5.4	395.7	✓
₵		5.3	395.8	✓
E		5.5	395.6	✓
+5		5.6	395.5	✓

6+50

E.		5.5	395.6	✓
₵		5.5	395.6	✓
W		5.7	395.4	✓

7+00

W		5.3	395.8	✓
E		4.8	396.3	✓
E		4.8	396.3	✓

7+12 garage on W. first floor 7.8 Back

W - 7.8 = floor		4.4	396.7	✓

7+50

E		5.1	396.0	✓
₵		5.1	396.0	✓
W		5.3	395.8	✓
+5		5.3	395.8	✓

8+00

W		5.1	396.0	✓
E		4.9	396.2	✓
E		4.9	396.2	✓

T.P.		3.78	400.45 ✓	4.45	396.67

8+26 garage on W. cmt. floor 8.8 Back
W - 8.8 = floor

		3.72	396.73	✓

8+36 = S. End. garage under Cons. on E. 12.4 Back

E - 12.4 Top. R.W. Sill		3.65	396.80	✓
E - 12.4 ground.		4.3	396.1	✓
E - 3		4.6	395.8	✓
E		3.7	396.7	✓
₡		3.8	396.6	✓
W		3.8	396.6	✓

8+64 = N. End. above garage on E.   12.4 Back

W		4.4	396.0	✓
₡		4.5	395.9	✓
E		4.6	395.8	✓
+12.4		4.3	396.1	✓
+12.4 Top. R.W. Sill		3.64	396.81	✓

9+04.5 ₡ = S. Line - Mt. View Drive (on Diagonal)

W - 0.25 = conc. ct. S. End.			4.69	395.76	✓
W - 0.25 pav " "			4.92	395.53	✓
W " " "			4.92	395.53	✓
₡ " " "			5.06	395.39	✓
E " " "			4.95	395.50	✓
E conc ct " "			4.71	395.74	✓

9+ 14.50 C.T. R.P. ₡ Alley

2.5' N. of S. Line = S. Curb

E - 50. gutter		5.60	394.85	✓
E "		5.68	394.77	✓
E. conc. ct.		5.18	395.27	✓
₡ gutter		5.66	394.79	✓
W. gutter		5.65	394.80	✓

W. conc. ct.		5.19	395.26 ✓
W + 50. gutter		5.80	394.65 ✓
BM. BP.		5.01	495.44 = 495.42
			S.W. Mt. View. Drive
			& 35th Sts

6+09.85 = EC *

6+0

5+62

5+50

5+0 *

132.86

4+50

4+11.71 20 R'

3+83

132.86

Bt. Ford Page 70

	Lt				C		Rt		
	130.0	130.5	130.13	130.16	130.2	131.3	131.6	132.1	132.3
	2.9	3.1	2.73	2.70	2.7	1.6	1.6	0.8	0.8
	40	33	40=F.P.	=F.P.		63	20	40	50
	129.8	130.2	129.58	129.56		129.6	130.9	131.4	131.3	131.6
	3.1	3.7	6.38	6.20		3.3	2.0	1.5	1.6	1.3
	40	34	40=F.P.	=F.P.		8	65	40	50
128.40	128.43								
4.16	4.13								
	6.35=Concrete							
123.9	127.7	127.40	127.39	127.6	128.2	127.6	128.3	128.5
9.0	5.7	5.46	5.47	5.3	4.7	5.5	4.6	4.4
45	40	45=F.Br.	3=F.P.			55	40	50
125.7	126.2	126.01	126.06	127.0		126.9	127.15	128.2
7.2	6.7	6.85	6.80	5.9		6.0	5.4	4.7
.50	40	33=F.P.	13=F.Br.			20	40	50
124.9	124.88	125.02	124.91	125.6	125.8	126.5	126.3	127.3	127.5
8.0	7.98	7.81	7.96	7.5	7.4	6.1	6.6	5.6	5.4
50	48=F.Br.	40	26=F.Br.	20		65	30	40	50
124.4	124.38	124.3	125.3	125.3	126.6	125.8	126.0	126.8	127.7	128.0
8.5	8.48	8.6	7.6	7.6	6.3	7.4	6.9	6.1	5.3	4.9
50	13=F.Br.	10	37	30	20	12		20	40	50
124.13	125.1	125.3	125.6	126.8	127.7	128.1	128.5	128.9
8.73	7.8	7.6	7.3	6.1	5.2	4.8	4.4	4.0
55=F.Br.	50	40	33	25		20	40	50
			132.86					

7+81				
7+50				
7+30				
TP	11.34	152.02	1.51	140.68
7+0				
6+72				
6+62 = FCb Capistrano				
6+22 = HCb Capistrano				
TP	12.32	142.19	2.99	129.87 / NW SLYT Capistrano + Macaulay
		132.86		

Right page (grid):

L↑   ↑   R↑

145.25   143.7   141.62   141.75   141.5   143.2   143.3   146.6   146.9   146.4   146.8
6.77   8.3   10.40   10.77   10.5   8.8   8.7   5.1   5.7   5.6   5.2
5.7   3.75   22.5p   1.5p   6.3   10   14   20   37.5   50

141.1   140.1   138.6   139.52   139.85   139.7   140.7   141.1   143.3   143.8   143.0   144.0
10.9   11.9   12.1   12.70   12.17   12.0   11.3   10.9   8.7   8.2   8.2   8.0
37.5   27   24   22.5p   1.5p   10   14   60   37.5   50

139.32   138.5   137.0   137.87   138.34   138.0   139.7   139.1   142.2   142.3   142.0   141.7
12.70   13.5   15.0   14.15   12.68   14.0   12.3   12.0   9.8   9.7   10.0   10.3
38.38   37   24   22.5p   2.5p   16   30   37.5   50

152.02

137.2   136.5   135.2   135.82   136.27   135.1   137.5   137.4   140.5   139.8   139.1
5.0   6.7   7.0   6.67   5.97   6.1   4.7   4.8   1.7   2.1   2.5
37.5   25   23   22.5p   2.5p   3   11   13   37.5   50

139.9   139.9   133.2   133.89   134.12   133.7   135.7   136.2   138.8   137.7   137.9
8.2   8.3   9.0   8.20   8.07   8.0   7.5   7.0   5.4   3.5   3.3
37.5   27   25   22.5p   2.5p   3   10   13   37.5   50

131.96   130.97   133.29   133.49   133.2   134.1   134.4   137.9   137.4   137.1
10.23   11.23   8.90   8.70   9.0   8.1   7.8   4.8   4.8   5.1
37.5   37   22.5p   2.5p   3   10   13   37.5   50

129.93   128.63   130.67   130.74   130.9   131.8   133.5   133.4   134.1
12.26   13.28   11.58   11.45   11.3   10.4   8.7   8.8   8.1
37.5   37   22.5p   2.5p   11   13   37.5   50

142.19

TP	4.87'	150.12	12.37	145.25
9+86 = F.L. Tustin				
9+56				
9+26 = W.L. Tustin				
9+0				
8+75				
8+52.70				
TP	11.97	157.62	6.37	145.65
8+0				
		152.02		

Right page (grid of readings):

L					₵				R
146.2	144.7	143.2	143.67	143.97	144.1	145.3	145.6	153.0	153.3	154.1
11.4 / 87.5	12.9 / 25	14.1 / 24	13.95 / 26.50	13.65 / 2.50	13.5	12.8 / 9	12.0 / 8	4.6 / 16	13.5 / 37.5	3.5 / 50
	147.1	146.1	146.05	145.99	146.2	147.6	148.0	155.0	155.4	157.0
10.5 / 87.5	14.5 / 26	14.57 / 21.50	14.63 / 2.50	11.2	10.0 / 9	9.6 / 10	2.6 / 18	2.2 / 87.5	1.6 / 50
149.3	149.0	147.7	147.47	147.42	147.6	148.8	149.1	157.2	157.3	157.7
8.2 / 87.5	8.6 / 26	9.9 / 24	10.15 / 31.50	10.72 / 2.50	10.0	8.8 / 9	8.5 / 9	2.0 / 18	1.0 / 87.5	0.9 / 65
147.97		147.96		147.67	147.62	147.0	149.1	149.3	155.3	155.5	156.0
9.65 / 88.5	9.66 / 13.25	9.95 / 31.50	10.00 / 2.50	9.6	8.5	8.3 / 9	2.2 / 15	2.1 / 87.5	1.50
148.5	148.2	146.8	146.77	146.75	146.7	148.3	148.7	154.0	155.2	156.3
9.1 / 87.5	9.4 / 24	10.8 / 28	10.85 / 31.50	10.87 / 2.50	10.9	9.7	8.9 / 9	8.6 / 17	2.4 / 37.5	3.8
147.4	147.3	145.4	145.57	145.62	145.7	147.2	147.9	153.0	153.3	153.7
10.2	10.3	12.2 / 23	12.05 / 31.50	12.00 / 2.50	11.9	10.4	9.7 / 18	2.6 / 18	1.0 / 37.5	3.8
					157.62					
	144.4	143.85	142.77	142.6	143.9	144.7	148.2	148.8	148.7	149.5
7.6 / 87.5	9.17 / 22.50	9.25 / 1.50	9.4	9.1 / 7.0	7.3 / 10	4.0 / 14	3.3 / 33	3.8 / 87.5	3.5 / 50
					152.02					

	Cont on Page 48			
TP	0.73	128.00	12.24	127.27
12+0				
11+50				
11+24				
TP	1.86	139.51	12.47	137.65
11+0				
10+47.72 Δ				
10+25				
	150.12			

Right page (graph paper survey data):

Lt ℄ Rt

125.1			123.88	124.19	124.06	124.0	126.0	126.1	127.8	128.2	
	125.2									128.5	
	14.4	14.3	15.63	15.32	15.15	15.5	12.5	13.9	11.7	11.3	11.0
	37.5	30	19:EP		6:EP	5	10	15	9.	37.5	50
	130.3	130.2	128.94	128.98	128.91	128.8	130.7	131.0	132.3	134.3	134.8
	9.2	9.3	10.57	10.53	10.60	10.7	8.8	8.5	7.5	5.2	4.7
	37.5	30	20:EP		2:EP	5	8	14	17	37.5	5.0
132.61	132.8	132.8	131.70	131.61	133.4	133.6	133.3	134.7	136.1	136.9	
6.90	6.7	6.2	7.81	7.90	8.1	5.9	6.2	4.8	6.4	3.6	
37.5	37.5	32	22:EP	2:EP6	6	13	16	37.5	50	

139.51

		134.1	133.39	133.92	133.9	135.1	136.1	138.0	139.0	139.4	
		16.0	16.23	16.20	16.2	15.0	15.0	13.1	14.1	10.7	
		37.5	28:EP	EP	8.5	5	11	16	37.5	5.0	
140.3	140.6	138.4	138.82	139.17	139.35	140.5	140.9	143.3	146.3	146.1	
9.8	9.5	11.7	11.30	10.96	10.77	9.6	9.2	6.8	4.8	4.0	
37.5	31	28	29:EP	2:EP	Stud	3	10	14	37.5	50	
142.5	142.5	139.4	140.84	141.01	141.3	142.6	142.9	147.1	144.5	149.2	
7.6	7.6	9.7	9.28	9.11	8.8	7.5	7.3	3.0	1.5	0.9	
37.5	30	27	21:EP	2:EP	3	10	15	37.5	55	

150.12

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent lenth divided by twice the radius.
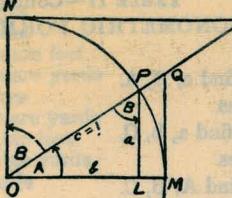
TABLE II
## TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$$
$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \ \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$
$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2 A = \cos^2 A - \sin^2 A$$

Law of Lines $\qquad \dfrac{\sin A}{a} = \dfrac{\sin B}{B} = \dfrac{\sin C}{C}$

Law of Cosines $\quad c^2 = a^2 + b^2 - 2 ab \cos C$

Law of Tangents $\dfrac{a+b}{a-b} = \dfrac{\tan \frac{1}{2} (A+B)}{\tan \frac{1}{2} (A-B)}$

W. L. Cap. = 2 + 25.37

E. L. '' 2 + 85.37 = 0 + 00

$\dfrac{\begin{array}{r}90\\22\end{array}}{112}$

$2\,\big|\,\overline{279.40}$
$\overline{139.70}$

$\dfrac{\begin{array}{r}125.10\\125\end{array}}{137.6}$

Fed. Blvd
34 th NE 61.60
35 th NW 51.87