

1559

1888

1888

1888

1888

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.
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ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface and is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.

Road Survey
Wly side Lower OTAY DAM.

B.C. LT. $613 + 06.31$

$5.46^{\circ}39'E$ ✓

$5 + 50.94$ E.C.

$A = 31^{\circ}34' RT.$

$R = 1000$

$T = 282.66$ ✓

$410 + 04.28$ P.I.

$L = 550.94$ ✓

282.66

1.7189

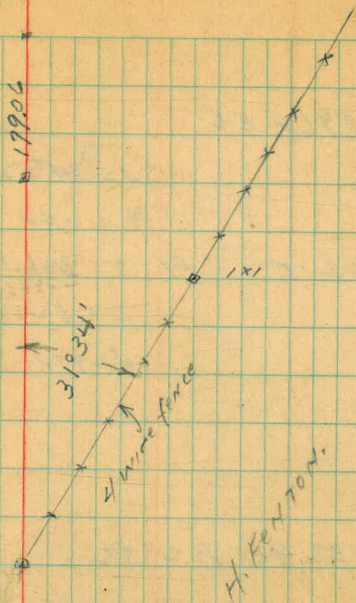
$0 + 00 = 407 + 21.62$ ✓ B.C. RT. $578^{\circ}13'E$ ✓

← See Co. Survey of Road
Wly of OTAY Lake

Moore 8-15-38.
Northern
Huntley
Ed. PIN by Rickie
W.P.H. Co. Engr.

Ed. Sp. Ac

5 + 50.94	$15^{\circ}47.00$	
5	$14^{\circ}19.40$	
+ 50	$12^{\circ}53.46$	
4	$11^{\circ}27.52$	
+ 50	$10^{\circ}01.58$	ixi
3	$8^{\circ}35.62$	
+ 50	$7^{\circ}09.70$	
2	$5^{\circ}43.76$	
+ 50	$4^{\circ}17.82$	
1	$2^{\circ}51.88$	
+ 50	$1^{\circ}25.94$	
0.0		

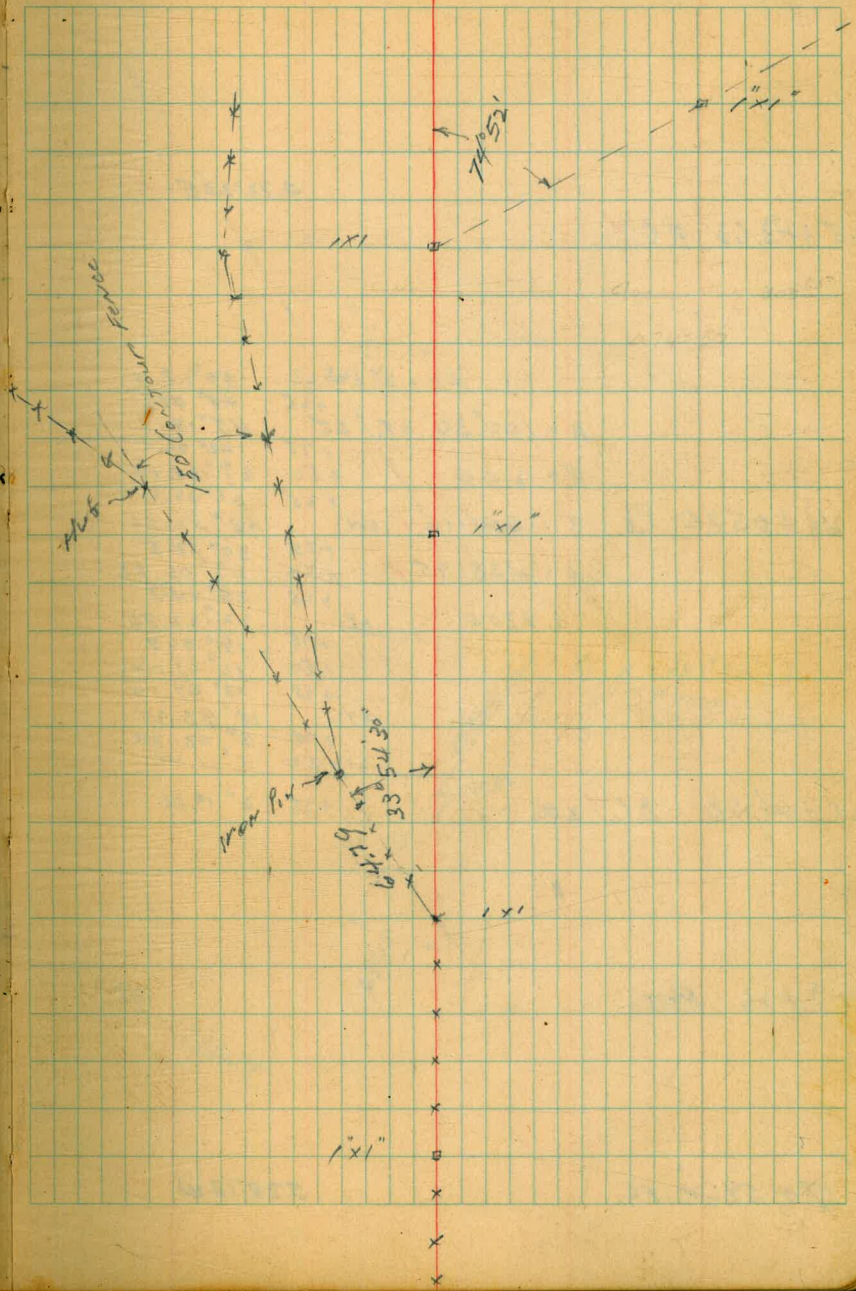


EC	17+59.62	37°56.00
	+50	36°44.71
	17	38°09.60
	+50	29°34.74
$\Delta = 74^\circ 52'$	RT. 16	26°00.00
$R = 400$	+50	22°25.02
15+43.15	PI	$T = 306.19$ ✓
	15	18°50.16
$L = 522.66$ ✓	+50	15°15.20
4.2972	14	11°40.44
	+50	8°05.58
	13	4°30.72
	+50	0°55.86

12+36.96 B.C. ✓ RT.

7+36.29 INT. T.C

5+50.94 E.C. 546°39'E



25+43.63 E.C. ✓

5.72°23'E ✓

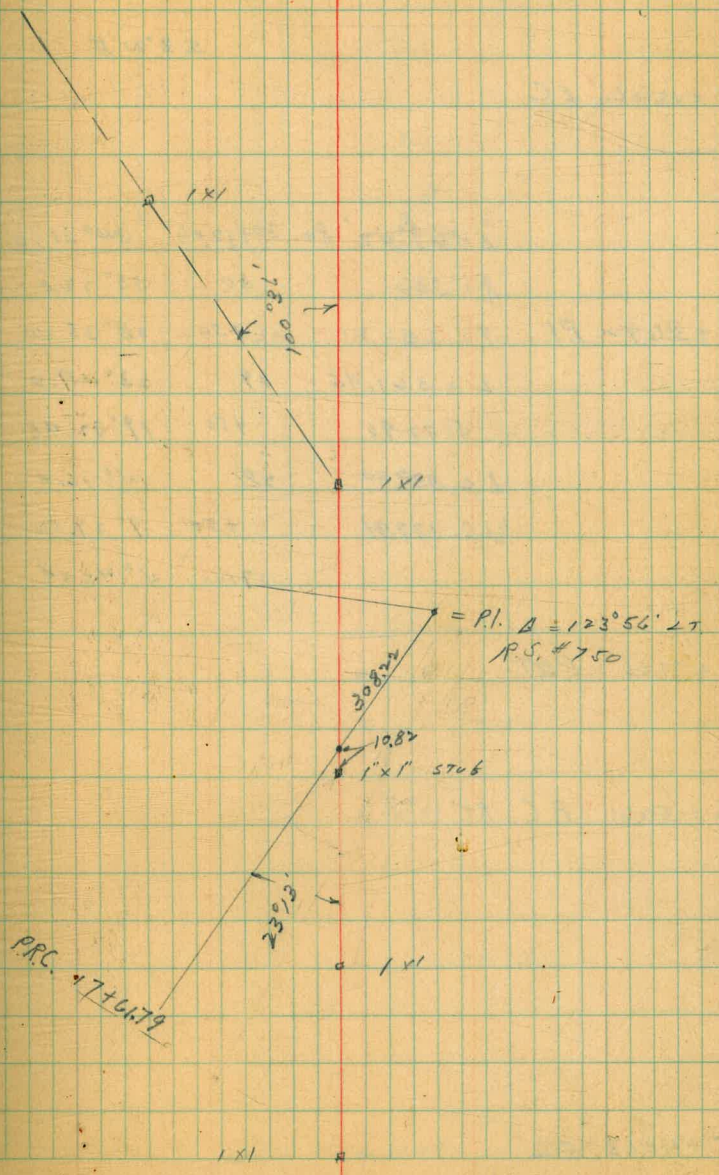
25	25+43.63	50°18.0
+25		48°09.9
25	A = 100°36' LT	45°18.0
+75		42°26.0
+50	R = 250	39°34.14
+25		36°42.2
24	T = 301.12 ✓	33°50.36
+75		30°58.5
+50	L = 438.95 ✓	28°06.58
+25		25°14.7
23	G. 8755	22°22.80
+75		19°30.9
+50		16°39.02
+25		13°47.14
22		10°55.24
+75		8°03.34
21+50		5°11.46
+25		2°19.56

21+04.68 P.C. ✓ LT.

19+26 P.O.T.

17+59.62 E.C.

528°13'W ✓



30 + 12.06 ✓ E.C.

5.3°21'E ✓

$A = 69^{\circ}02'$	Rt	30 + 12.06	34° 31'.0
$R = 300$		30	33° 22.0
28 + 56.92	P.I.	$T = 206.31$ ✓	+50 28° 35.04
$L = 361.45$ ✓		29	23° 49.0
5.7296		150	19° 02.48
$L.C. 339.99$		28	14° 16.0
$\frac{1}{2}L.C. 177.91$		150	9° 29.52
		27100	4° 43.04

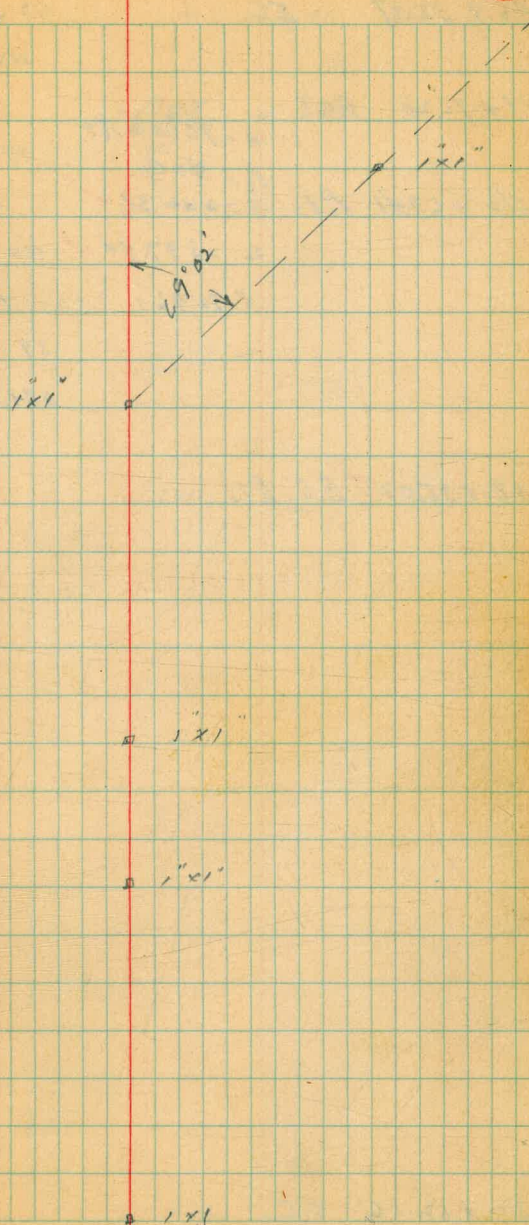
26 + 91.66 P.O.T.

26 + 50.61 ✓ B.C. RT.

25 + 43.63 E.C.

5.72°23'E ✓

4



42 + 32.97 E.C.

42 + 32.97 38° 00.0

42 34° 51.2

41 + 76.28 P.O.T.

$\alpha = 76^{\circ} 00' RT.$

+50 30° 04.8

$R = 300$

41 25° 18.3

40 + 69.41 P.I.

$T = 234.38$ ✓

+50 20° 31.8

$L = 397.94$ ✓

40 15° 45.4

5.7296

+50 10° 58.9

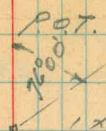
39 6° 12.4

38 + 50 1° 25.9

38 + 35.03 ✓ B.C. RT.

30 + 12.06 E.C.

S. 3° 21' E ✓



1.50
.75

1 x 1

46°

1 x 1

51+49.01 ✓ E.C.

5.70°23'E ✓

EC	51+49.01	71°31'
	+25	68°14.4
	51	64°49.8
	+75	61°25'
	+50	58°00.4
$\Delta = 143°02'$	+25	54°35.6
LT	50	51°11.0
	+75	47°46.3
$R = 210$	+50	44°21.7
$T = 628.23$ ✓	+25	40°57.1
P.I. $L = 524.24$ ✓	49	37°32.5
$8.1851 = i'$	+75	34°07.8
$ch = 49.88$	+50	30°43.2
	+25	27°18.4
$C = 398.33$	48	23°54.0
	+75	20°29.3
	+50	17°04.7
	+25	13°40.1
	47	10°15.5
	+75	7°50.8
	46+50	3°26.2

52+53.00

P.I.

$8.1851 = i'$

$ch = 49.88$

$C = 398.33$

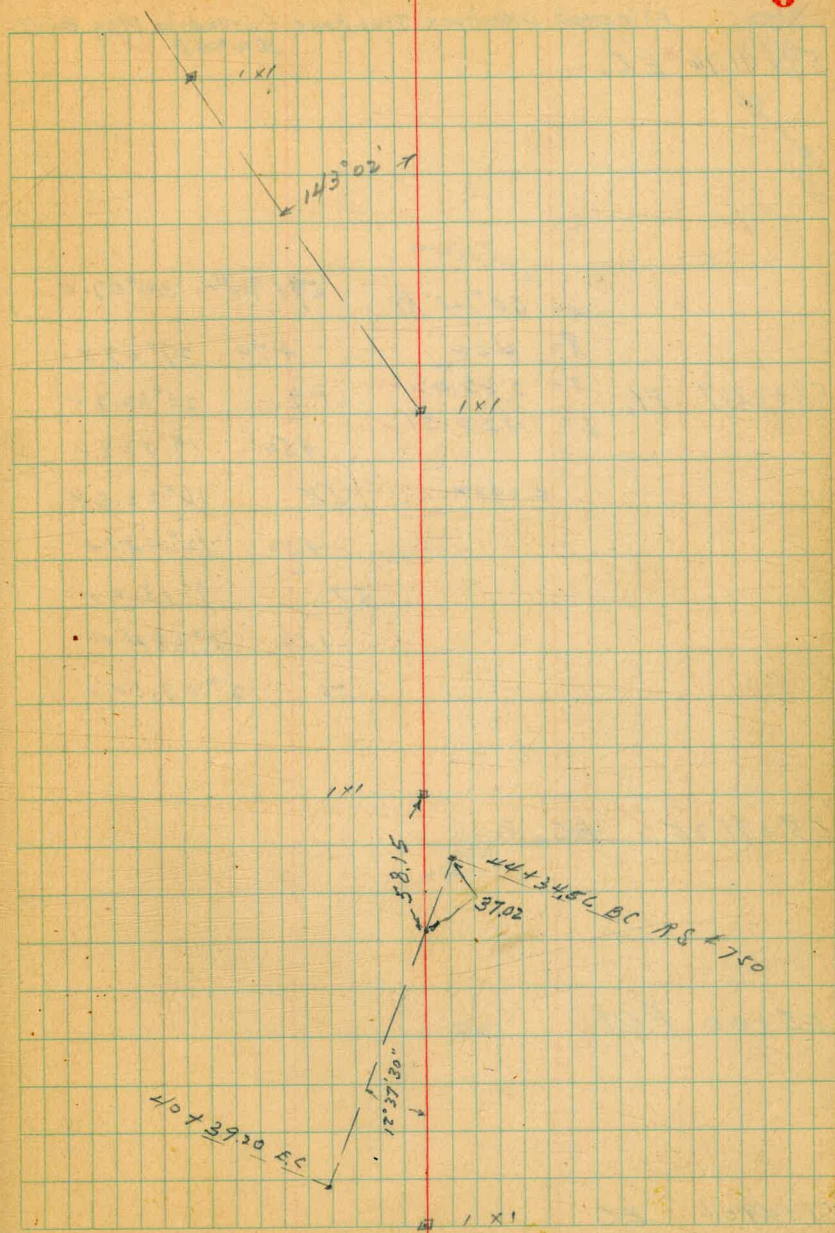
$R = 260 = L = 6.61105$

46+24.77

D.C. LT.

42+37.97 ✓ E.C.

5.72°39'W ✓



Sta Alinement Deflections True Bear Curvedata Mag Bear.
 59+91.76 ✓ E.C. 5.10°09'E ✓

	$\Delta = 60^{\circ}14'$ Pt	59+91.76	30°07.0
	R = 400	+50	27°07.5 ✓
58+03.27 P.I.	T = 232.02 ✓	59	23°32.7 ✓
	L = 420.51 ✓	+50	19°57.8 ✓
	4.297	58	16°23.0 ✓
		+50	13°48.1 ✓
		57	9°13.2 ✓
		+50	5°38.4 ✓
		56	2°03.5 ✓

55+71.25 ✓ B.C. Pt.

55+00 P.O.T.

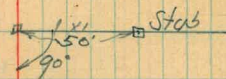
51+49.01 E.C.

5.70°23'E ✓

7



-60°14'



• NAIL

• NAIL

S. 58° 21' W ✓

69+00.77 E.C. ✓

67+85.19 P.O.T.

69+00.77 34° 15'

Δ = 68° 30' Rt. +50. 31° 01.2 ✓

R = 450

T = 306.39 ✓ 68+0 27° 50.2 ✓

66+69.16 P.I. L = 538.0 ✓ +50 24° 39.2 ✓

3.8197 67 21° 28.2 ✓ P.O.C.

+50 18° 17.2

66 15° 06.2

+50 11° 55.2

65 8° 44.2

+50 5° 33.2

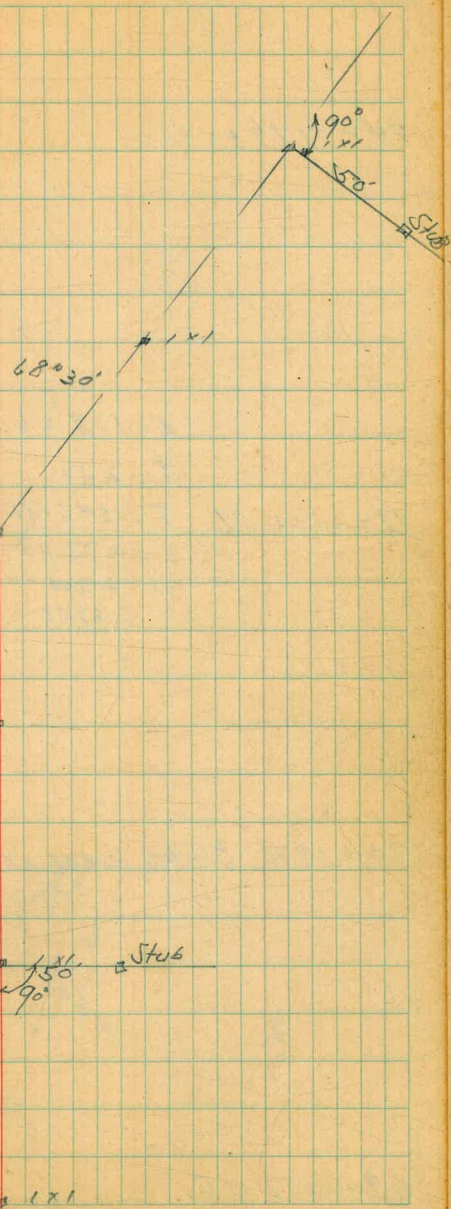
64+00 2° 22.2

63+62.77 ✓ B.C.P.T.

37/01

59+91.70 E.C.

S. 10° 09' E ✓



74+91.89 Ec. Fed Hub

S. 50° 05' E ✓

	74+91.89	54° 13.0
	+75	52° 16.9
	+50	49° 25.1
	+25	46° 33.3
	74	43° 41.2 ✓
	+75	40° 49.1
	+50	37° 57.5 ✓
	+25	35° 05.8
	73	32° 13.7 ✓
	+75	29° 22.0
	+50	26° 30.0 ✓
	+25	23° 38.1
	72	20° 46.1 ✓
	+75	17° 54.2
	+50	15° 02.3 ✓
	+25	12° 10.2
	71	9° 18.1 ✓
	+75	6° 26.7
	70+50	3° 34.8 ✓
	+25	0° 43.0

d = 108' 26" LT.

P = 250

73+65.61 P.I. T = 346.85 ✓

L = 473.13 ✓

L.C. = 405.62

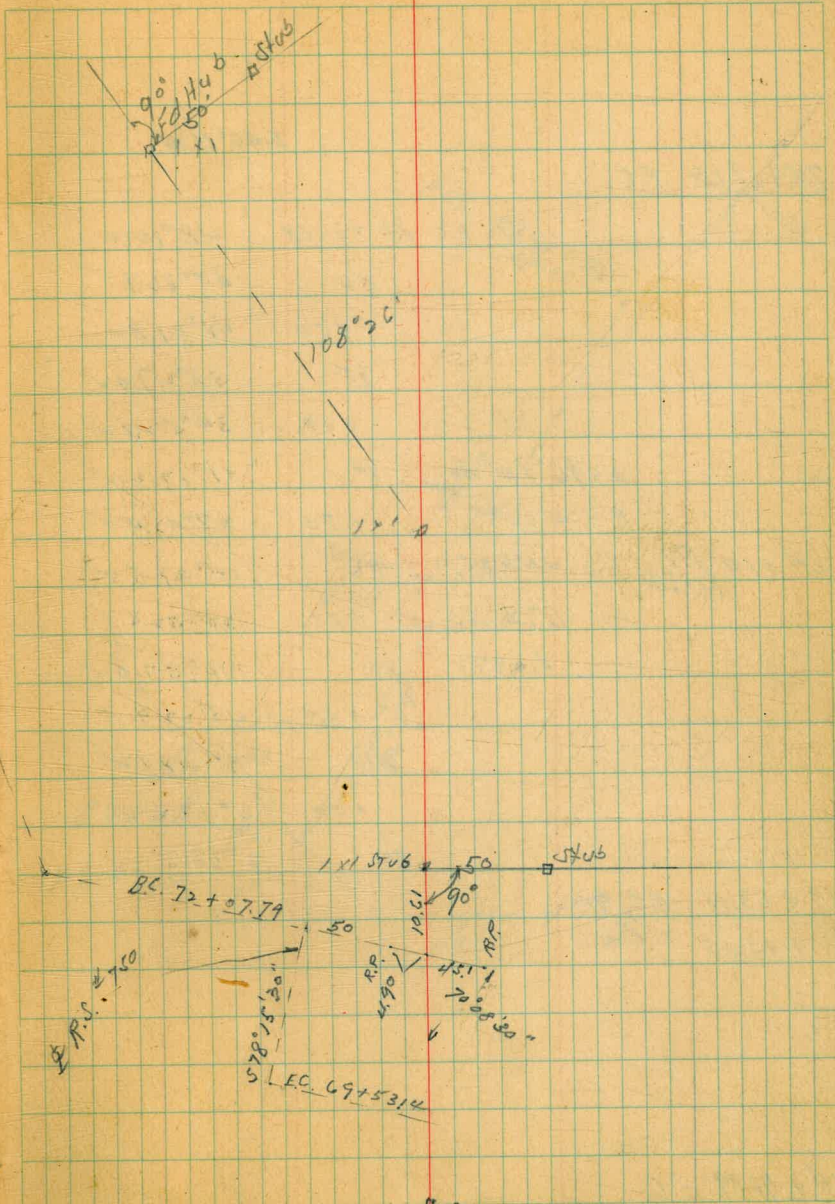
6.8755

72+18.76 BC LT. Hub Ed.

117.99

69+00.77 E.C.

S. 58° 21' W ✓



10 D114

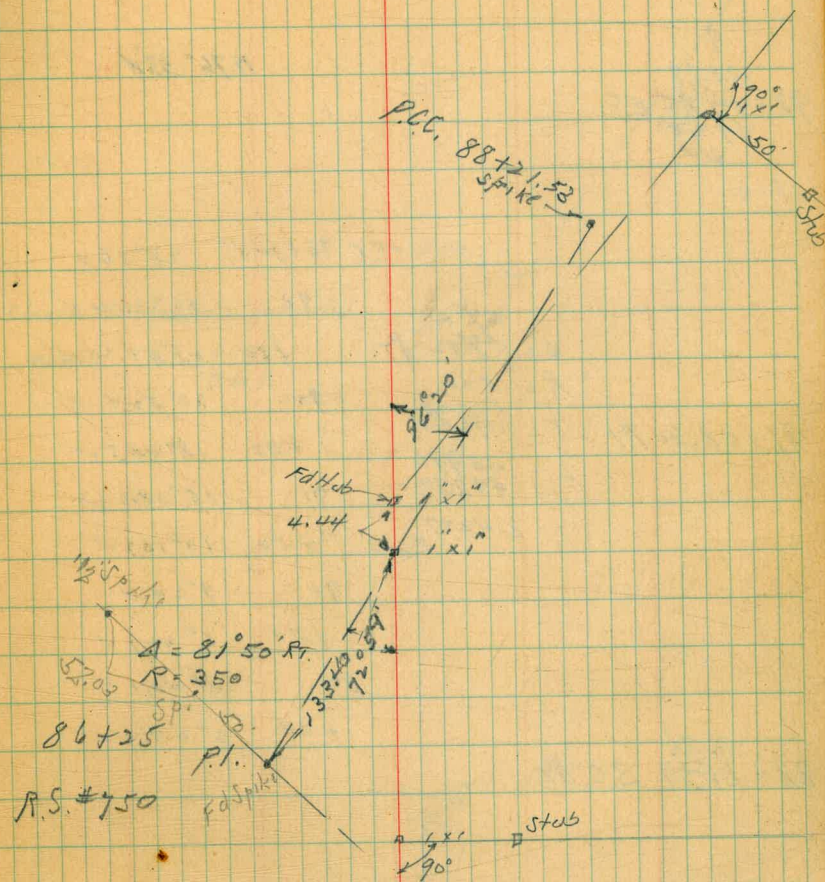
86+35.68 ✓ E.C. S.46°15'W ✓

EC	86+35.68	48°10.0
	80	45°36.7 ✓
	+50	42°01.8 ✓
	85	38°27.0 ✓
	+50	34°52.1 ✓
$\Delta = 96°20'$ Pt.	84	31°17.2 ✓
$R = 400$	+50	27°42.4 ✓
84+10 P.I. $T = 446.85$ ✓	83	24°07.5 ✓
$L = 672.53$ ✓	+50	20°32.5 ✓
4.2972	82	16°57.8 ✓
	+50	13°22.9 ✓
	81	9°48.1 ✓
	+50	6°13.2 ✓
	80	2°38.3 ✓

79+63.15 ✓ B.C. Pt.
80+13.15 = E.C.

74+91.89 E.C.

S.50°05'E ✓



↑
34.28
93 + 34.85 ✓ E.C.
34.55
↓

N.76° 33' W ✓

E.C. 93 + 34.85 28° 36.0

	93	26° 36.2 ✓
57° 06'		
0 = 57° 12' RT.	+50	23° 44.2 ✓
R = 500	92	20° 52.4 ✓
272.04		
91 + 08.30 P.I. T = 272.04 ✓	+50	18° 00.5 ✓
L = 499.14 ✓	91	15° 08.6 ✓
498.29		
3.4377 P.O.C.	+50	12° 16.7 ✓
	90	9° 24.8
	+50	6° 32.9 ✓
	89	3° 41.1 ✓
	+50	0° 49.2 ✓

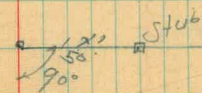
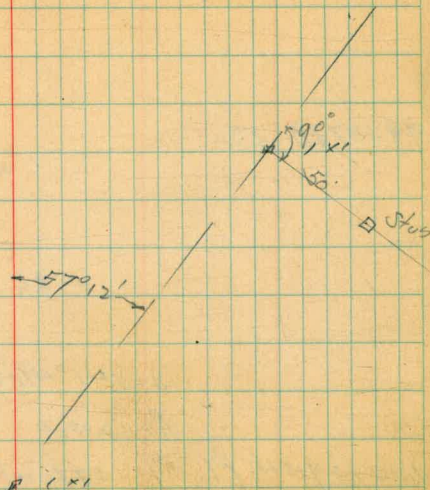
36.26
88 + 35.69 ✓ B.C. RT

86 + 35.68 E.C.

S.46° 15' W ✓

Check C. Moore's original

Work. 4-22-40
R.A.S.



5.38°19'E ✓

99+47.38 EC. ✓

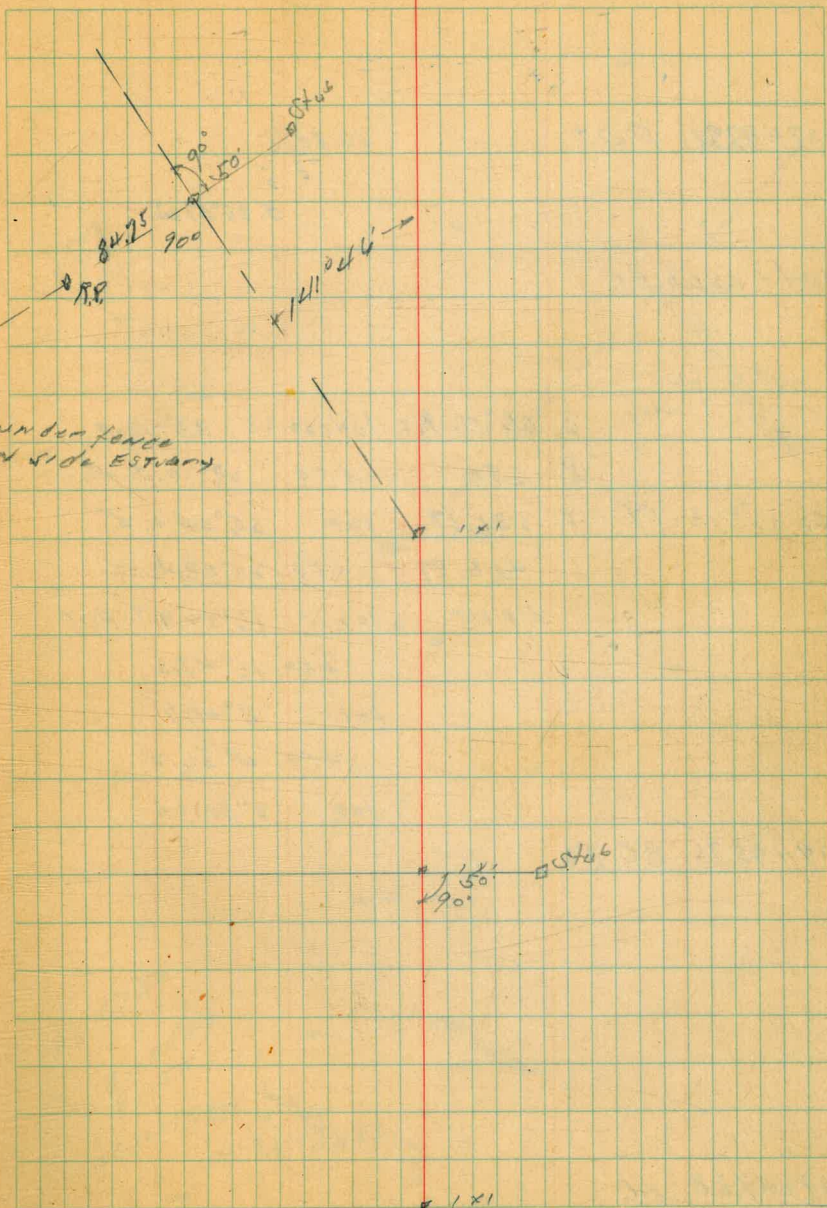
EC 99+47.38	70° 53.0
+25	67° 40.7
99	64° 06.0 ✓
+75	60° 31
a = 141° 40' LT	+50 56° 56.3 ✓
R = 200	+25 53° 21.3
100+29.54 = P.I.	98 49° 44.5 ✓
T = 5770V ✓	+75 46° 11.6
d = 194.84 ✓	+50 42° 30.8 ✓
8.5993	+25 39° 01.9
C = 377.94	97 35° 27.1 ✓
	+75 31° 52.2
	+50 28° 17.4 ✓
	+25 24° 42.5
	96 21° 07.7 ✓
	+75 17° 32.8
	+50 13° 58.0 ✓
	+35 10° 23.1
	95 6° 48.2 ✓
	+75 3° 13.4

94+52.52 BC LT

117.67

93+34.85 FC.

N76°33'W ✓



107+97.90 P.O.T.

saddle

5.28°37'W ✓

104+02.63 ✓ EC

Δ = 66°56' RT. 104+02.63 33°28.0

P = 350 +50 29°10.5 ✓

102+25.13 = P.T. T = 231.37 ✓ 109 25°04.0 ✓

L = 408.87 ✓ +50 20°58.4 ✓

4.911 102 16°52.9 ✓ P.O.C.

+50 12°47.3

101 8°41.7

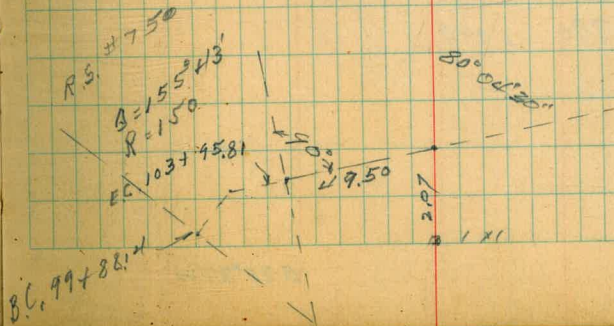
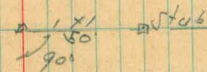
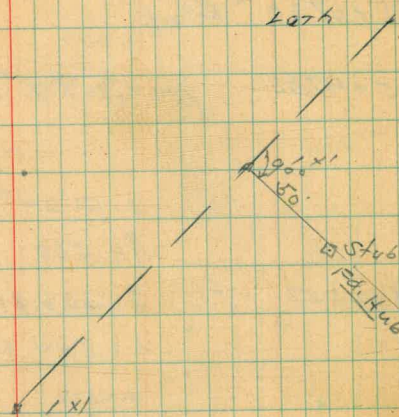
+50 4°36.4

100 0°30.6 ✓

99+93.76 ✓ B.C. RT.

99+47.38 EC

5.38°19'E ✓



5.33°47'E ✓

115+67.30 ✓ E.C.

31°12.0

115+47.88

INT. of T. of R.S. #750

+50 30°12.5

115 27°20.6 ✓

+50 24°28.7 ✓

0-62°24' LT. 114 21°36.8 ✓

R=500 +50 18°45.0 ✓

113+25.57 = P.I.

T=302.81 ✓ 113 15°53.1 ✓

L=544.54 ✓ +50 13°01.2 ✓

3.4377 112 10°09.3 ✓

C=518.03

+50 7°17.4 ✓

111 4°25.5 ✓

+50 1°33.6

110+22.76 ✓

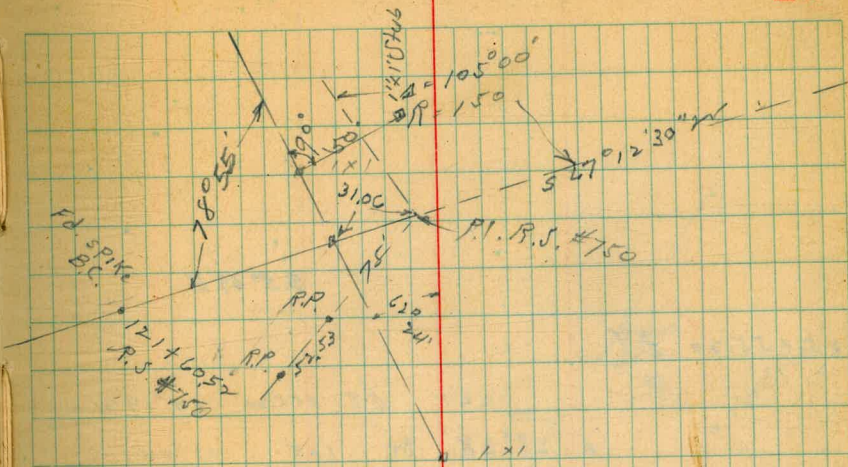
BL. LT.

P.O.T. 107+97.90 earth

104+02.63 E.C.

5.28°37'W ✓

14



125+55.20 ✓ E.C.

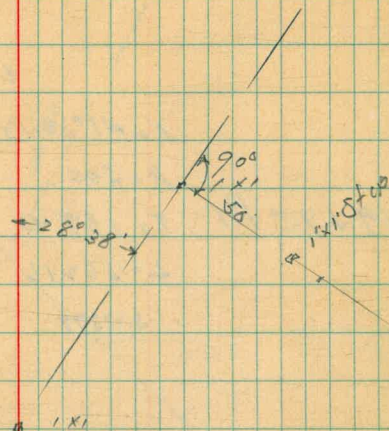
5.5° 09' E ✓

	EC	155.20	14° 19.0
$\Delta = 28^\circ 38'$	Rt.	125	12° 44.1 ✓
$R = 1000$		450	11° 18.1
$T = 255.21$ ✓		124	9° 52.2 ✓
123+10.67 P.I.	$L = 499.74$ ✓	450	8° 26.3 ✓
		123	7° 00.2 ✓
		450	5° 34.4 ✓
		122	4° 08.4 ✓
		450	2° 42.5 ✓
		121	1° 16.6

120+55.46 ✓ B.C. Rt

115+67.30 E.C.

5.33° 47' E ✓



151+47.73 E.C.

	E.C. 447.73	20°45.0
$\Delta = 41°30' R$	151	18°01.0
$R = 500$	+50	15°09.1
149+75 P.I.	$T = 189.43$	150
	$L = 362.16$	+50
	3.4377	149
		+50
		148

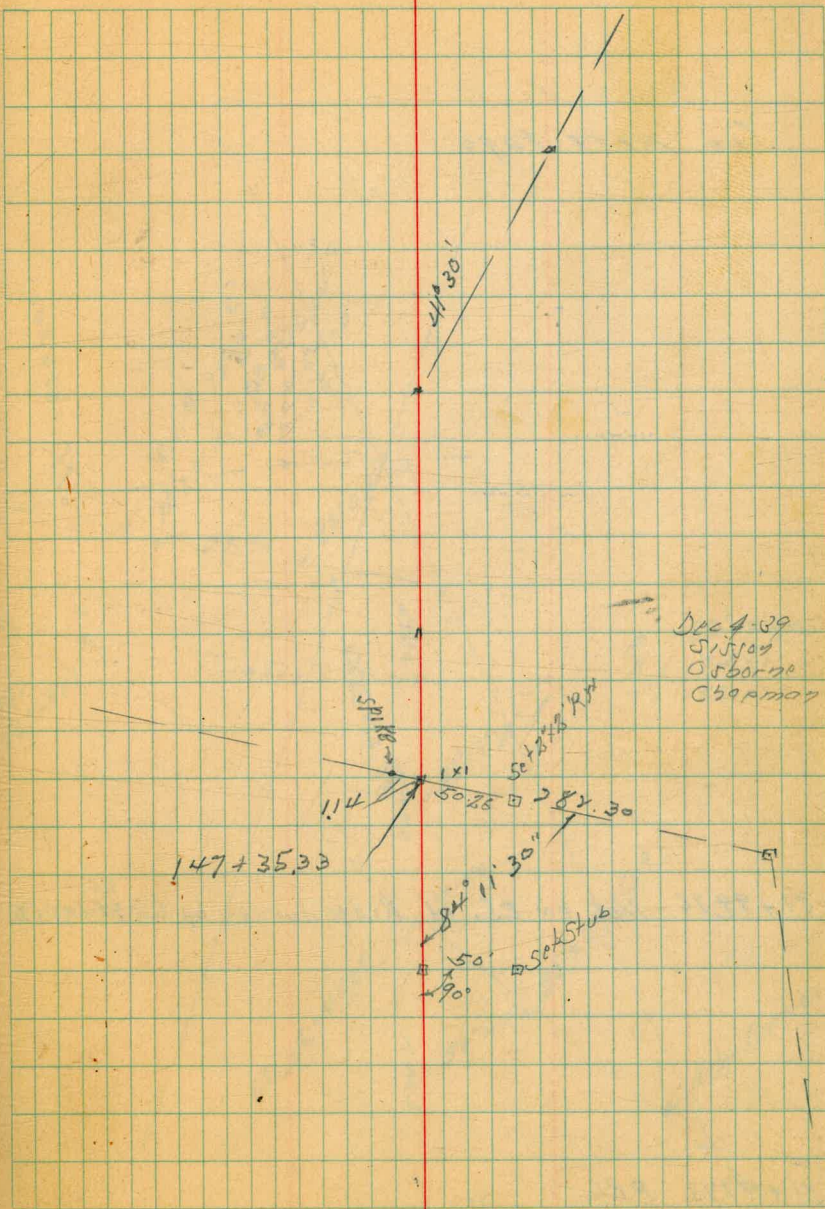
147+85.57 B.C. RT.

Fd. Spike Int. of Grant Line R.S. #750

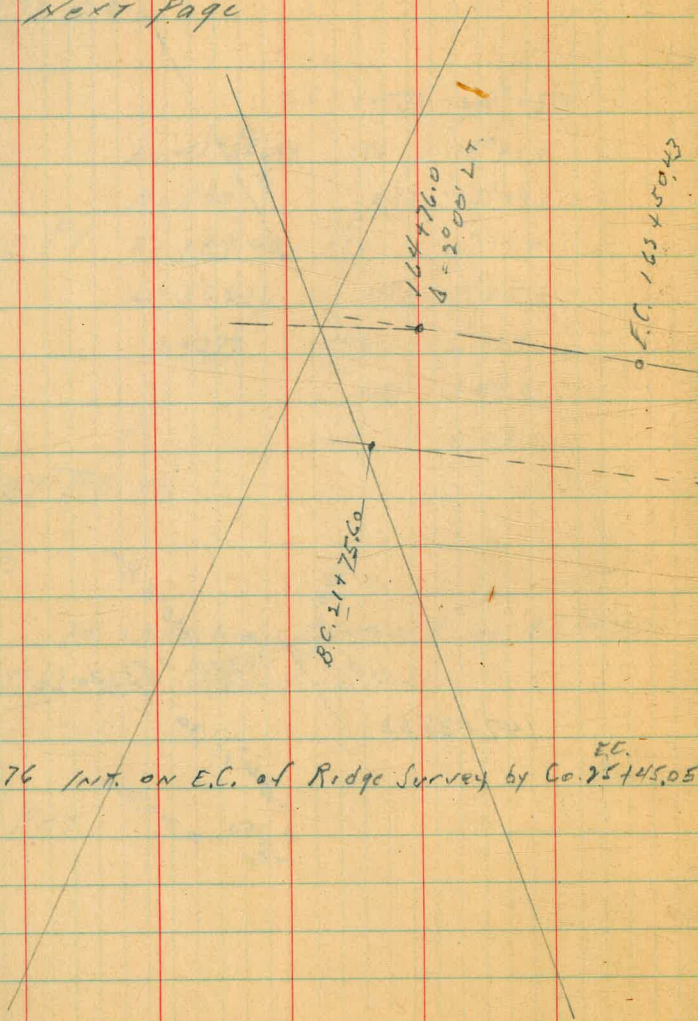
147+35.33 Int. Grant Line 1x1

139+00 P.O.T.

125+55.20 E.C.

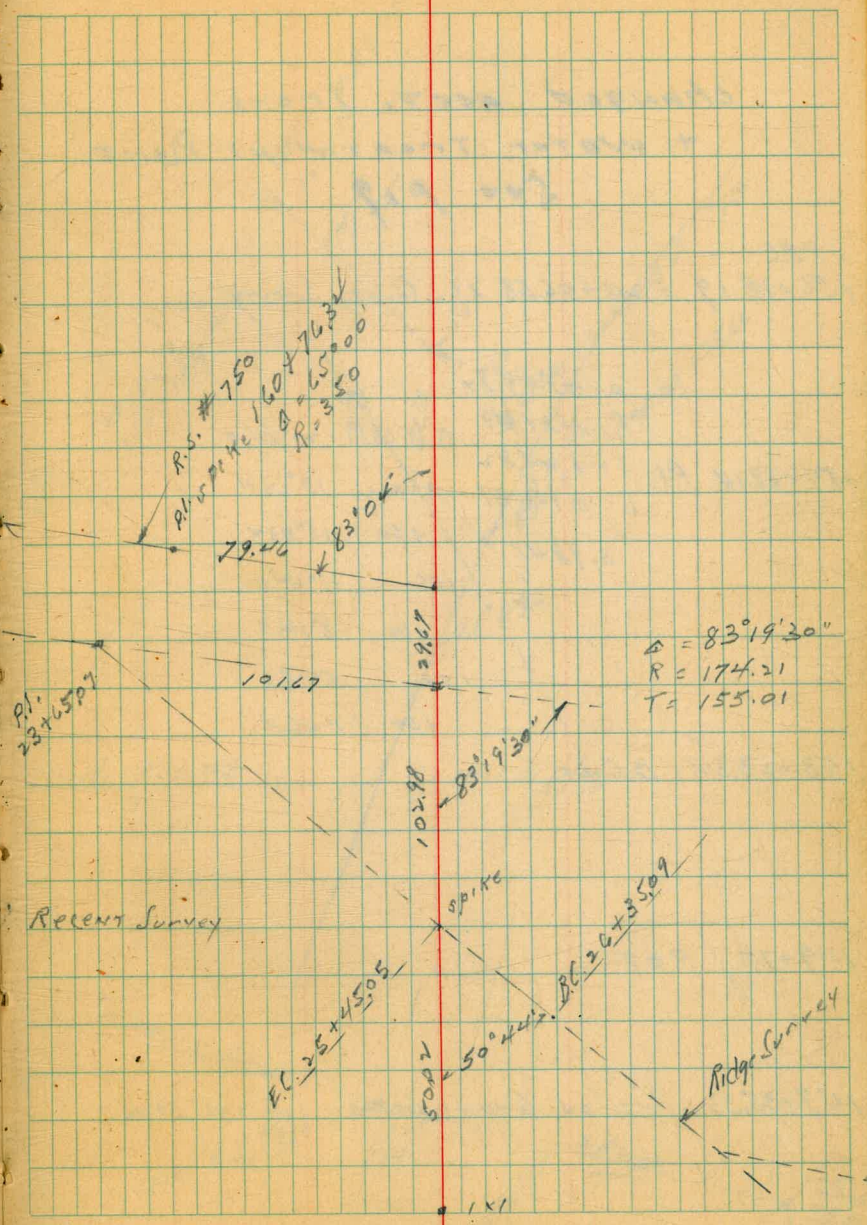


See Next Page



151499.76 INT. ON E.C. of Ridge Survey by Co. 25445.05

151447.73 P.R.C.



Recent Survey

$\Delta = 83^{\circ}19'30''$
 $R = 174.21$
 $T = 155.01$

Ridge Survey

changed acct. Trees
+ Water Treatment Plant
See p19

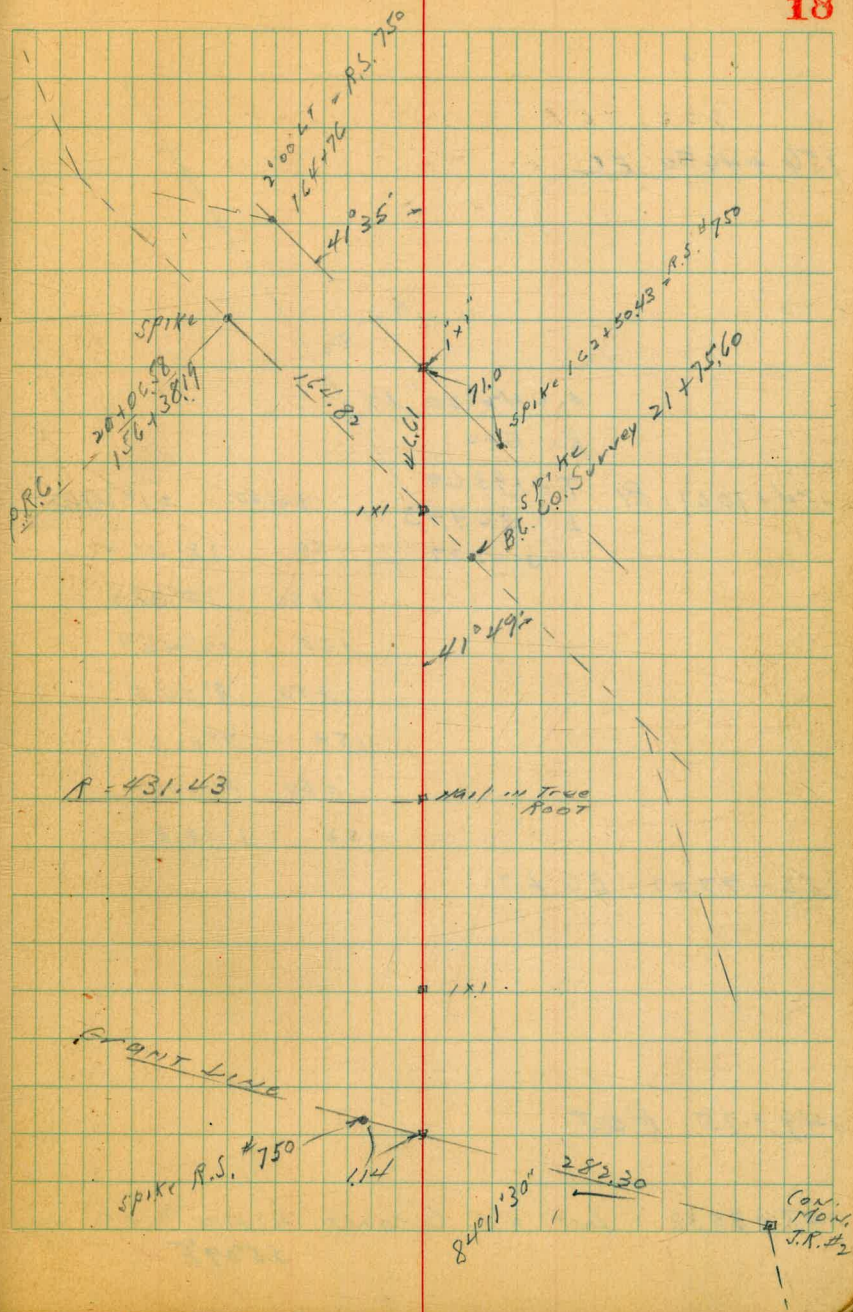
= P.R.C.
156+38.19 = 20+06.58 E.C. County Survey

$\Delta = 41^\circ 49' LT$
 $R = 431.43$ EC + 38.19 $20^\circ 54.5$
 154+88.14 P.I. $T = 164.82$ 156 $18^\circ 22.4$
 $L = 314.87$ 150 $15^\circ 03.2$
 3.9841 155 $11^\circ 44.0$
 150 $8^\circ 24.8$
 154 $5^\circ 05.6$
 150 $1^\circ 46.4$

153+23.37 B.C.Lt.

149+75 P.O.T.

147+35.33 Int. of Grant Line Set ixi'' stub



156 + 46.50 E.C.

$A = 42^{\circ} 20' LT$

$R = 500$

$154 + 70.67 = P.I.$

$T = 193.60$

$L = 309.43$

3.4277

+46.50	$21^{\circ} 10.0$
154	$18^{\circ} 30.4$
+50	$15^{\circ} 38.3$
155	$12^{\circ} 46.4$
+50	$9^{\circ} 54.5$
154	$7^{\circ} 02.6$
+50	$4^{\circ} 10.7$
153	$1^{\circ} 18.8$

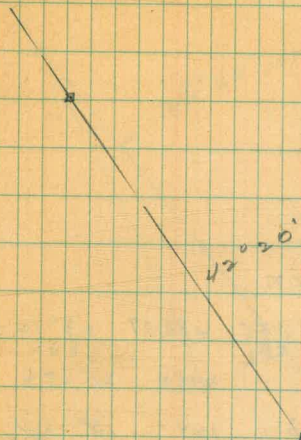
152 + 77.07 BC LT.

149 + 75 P.O.T.

147 + 35.33 Int. of Grant Line

$55^{\circ} 09'E$ ✓

19



See p 18

164+83.37 E.C.

$\Delta = 46^{\circ}20' LT$

$R = 500$ E.C. 783.37 $\Delta 3^{\circ}10.0$

162+93.0 P.I. $T = 213.96$ +50 $21^{\circ}15.3$

$L = 404.33$ 164 $18^{\circ}23.4$

3.4377 +50 $15^{\circ}31.5$

162 $12^{\circ}39.6$

+50 $9^{\circ}47.7$

162 $6^{\circ}55.8$

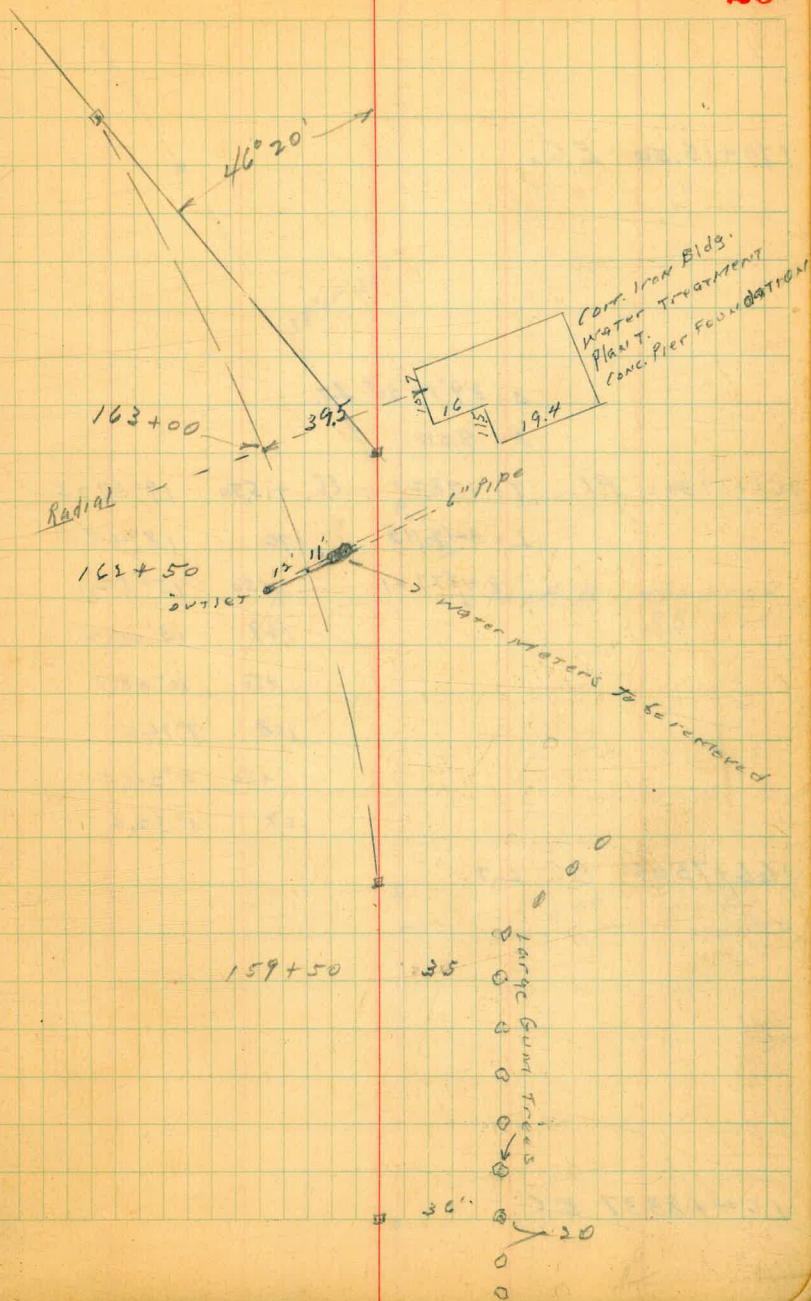
+50 $4^{\circ}03.9$

161 $1^{\circ}12.0$

160+79.04 B.C.L.T.

156+46.50 E.L.

20



170+15.50 E.C.

$\Delta = 39^{\circ}14'30''$ LT.

$R = 500$

168+51.30 = P.I. $T = 178.25$ E.C. +15.50 $19^{\circ}37.25$

$L = 342.45$ 170 $18^{\circ}44.0$

$3.4377 = 1$ 150 $15^{\circ}52.1$

169 $13^{\circ}00.7$

150 $10^{\circ}08.3$

168 $7^{\circ}16.4$

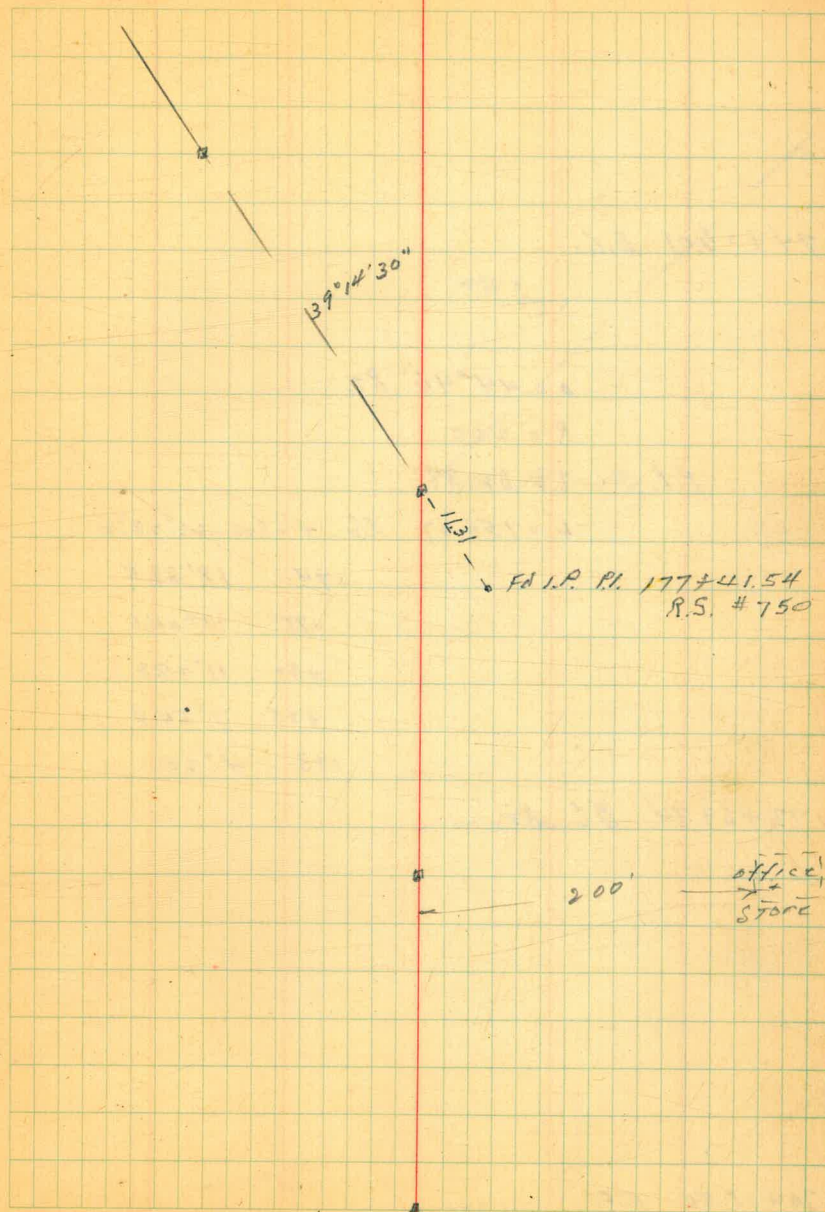
150 $4^{\circ}24.5$

167 $1^{\circ}32.6$

166+73.05 B.C. LT.

164+83.37 E.C.

21



174 + 26.01 E.C.

$\Delta = 44^{\circ}46'$ RT,

R = 200

P.I. T = 82.37

L = 156.27 E.C. + 26.01 $22^{\circ}33.0'$

174 $18^{\circ}39.5'$

175 $15^{\circ}04.6'$

150 $11^{\circ}29.8'$

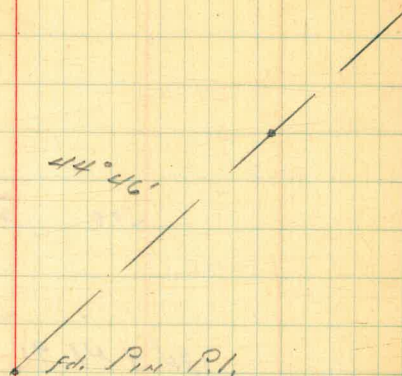
125 $7^{\circ}54.9'$

173 $4^{\circ}20.1'$

172 + 69.74 B.C. RT

170 + 15.50 E.C.

22



rd. spike

1 x 1

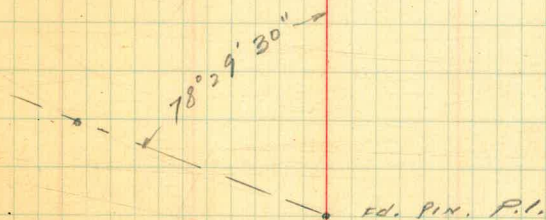
See $\frac{740}{237-2}$ P 38

184 + 41.91 R.S. # 750
 175 + 17.72 E.C. WLY END Savage Dam

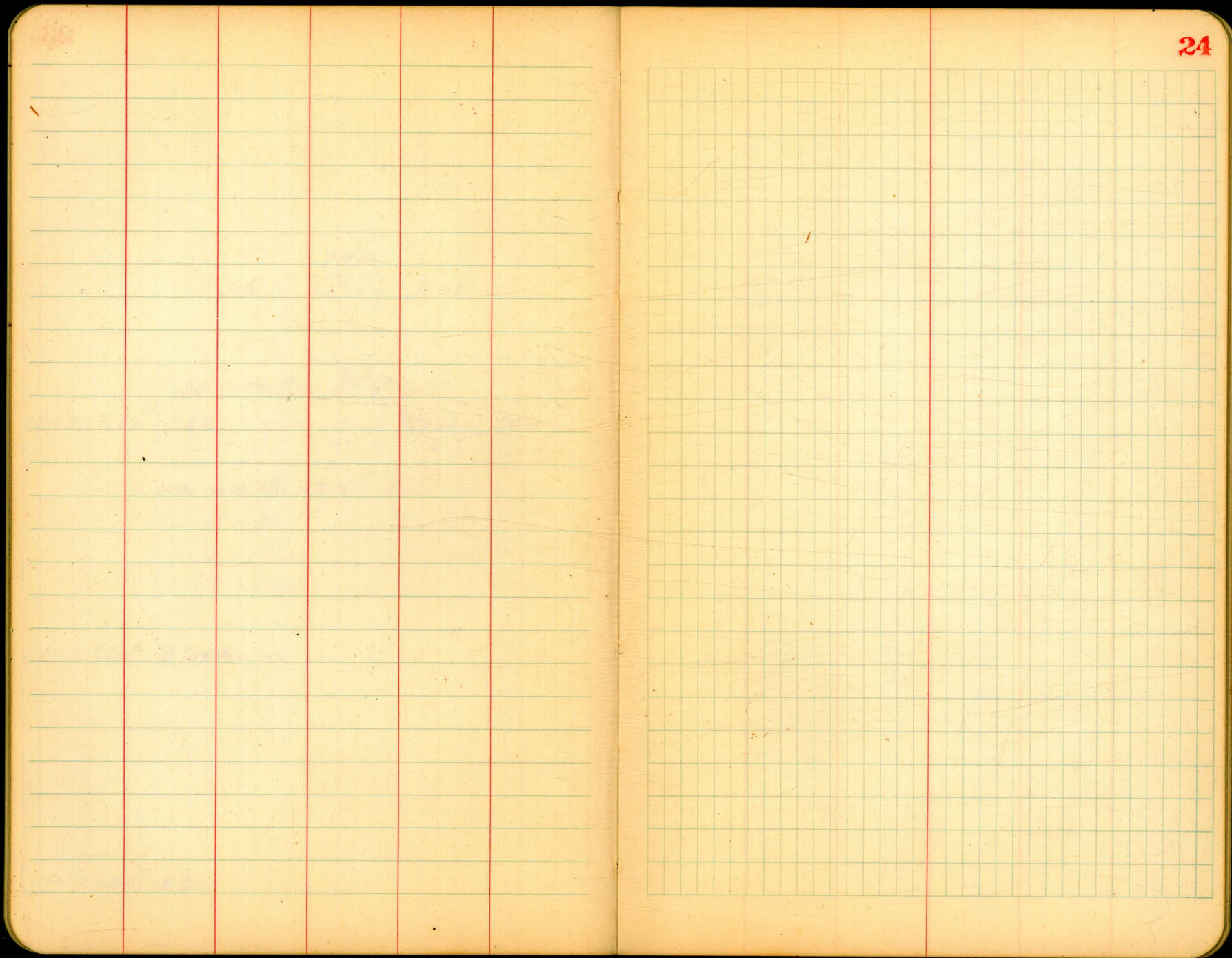
$\Delta = 78^{\circ} 29' 30''$ LT
 $R = 30'$
 $L = 41.10$
 $(T = 24.51)$

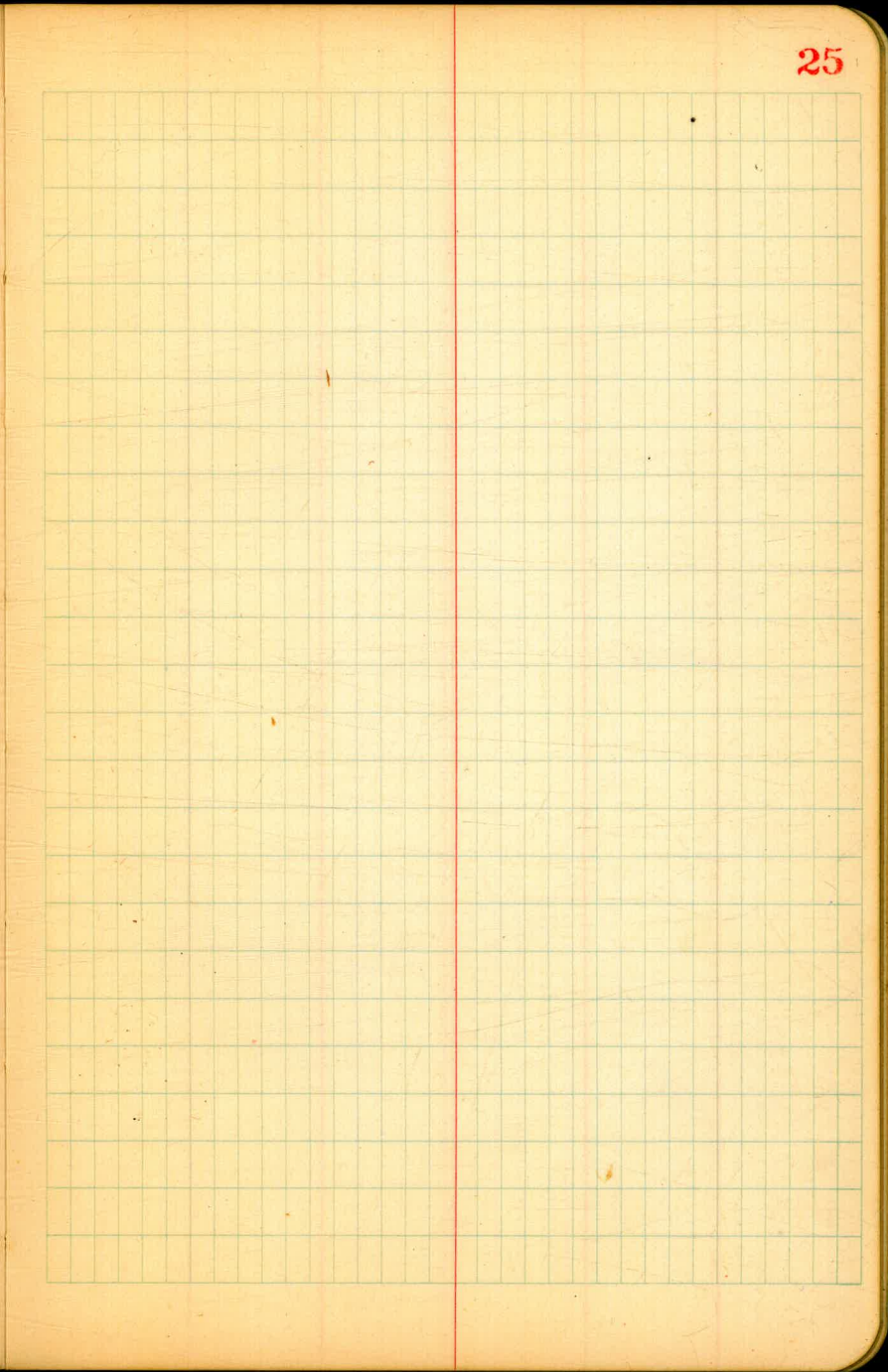
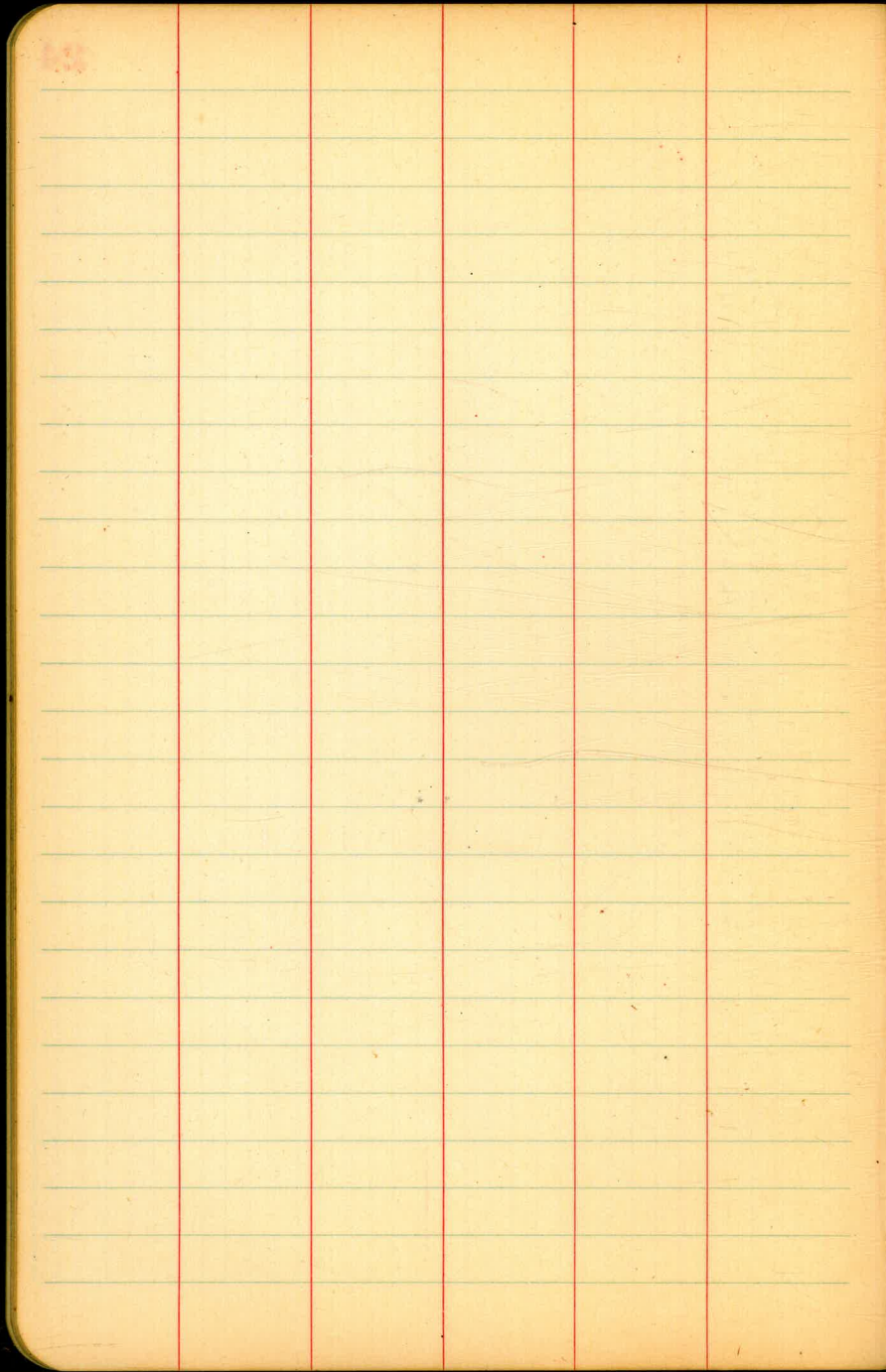
174 + 97.17 B.C. LT.

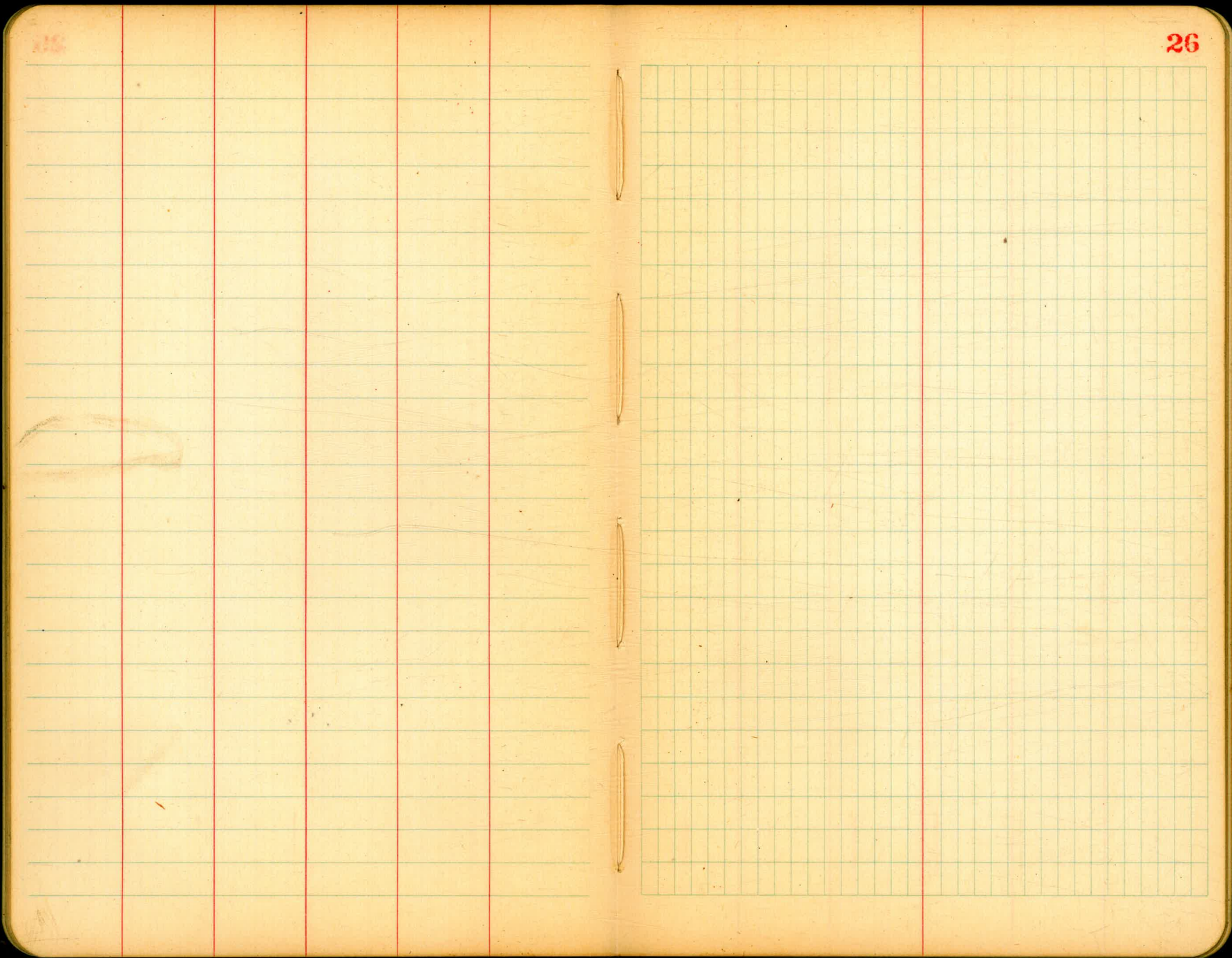
174 + 26.01 E.C.



Fd SPIKE

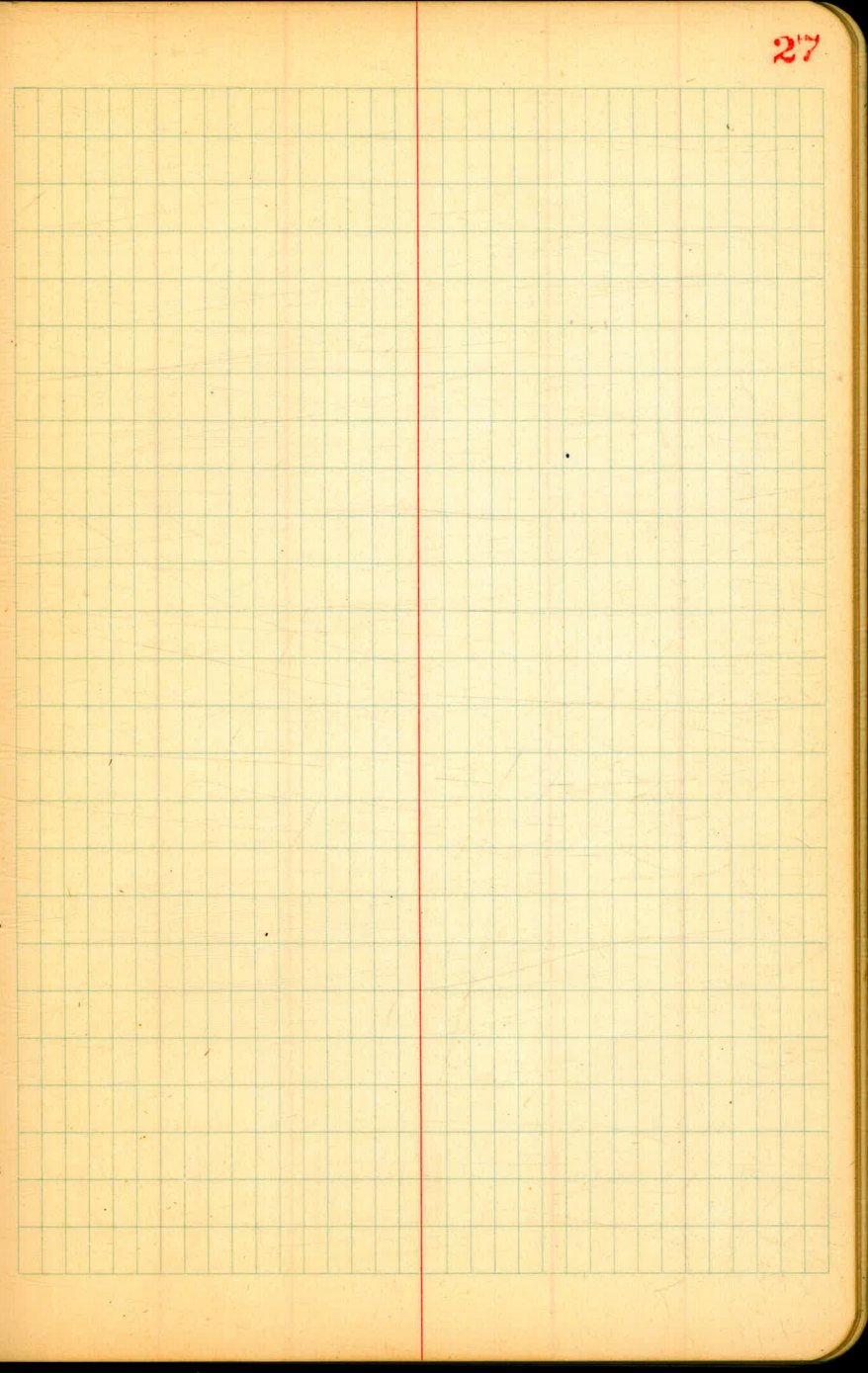
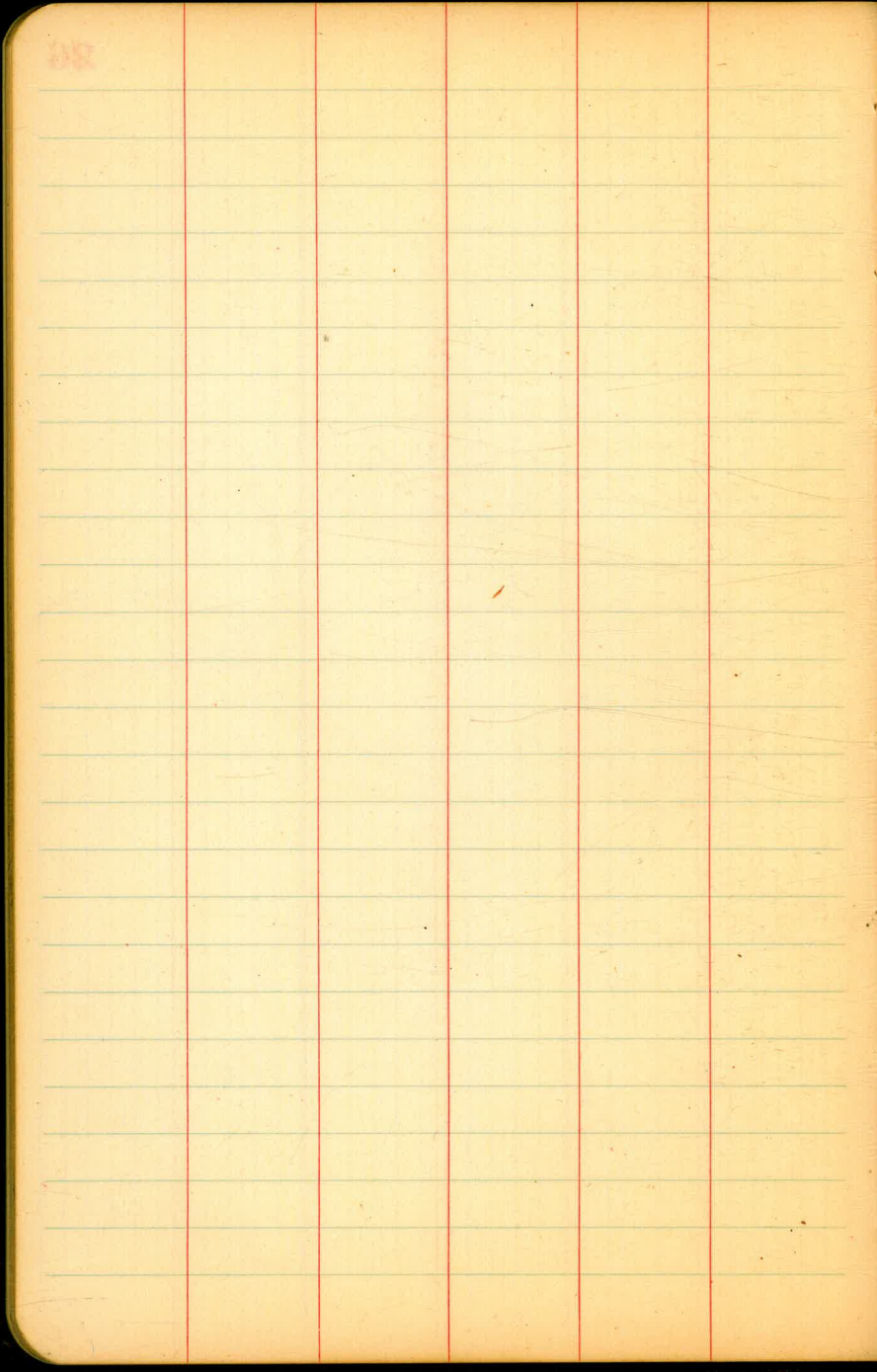


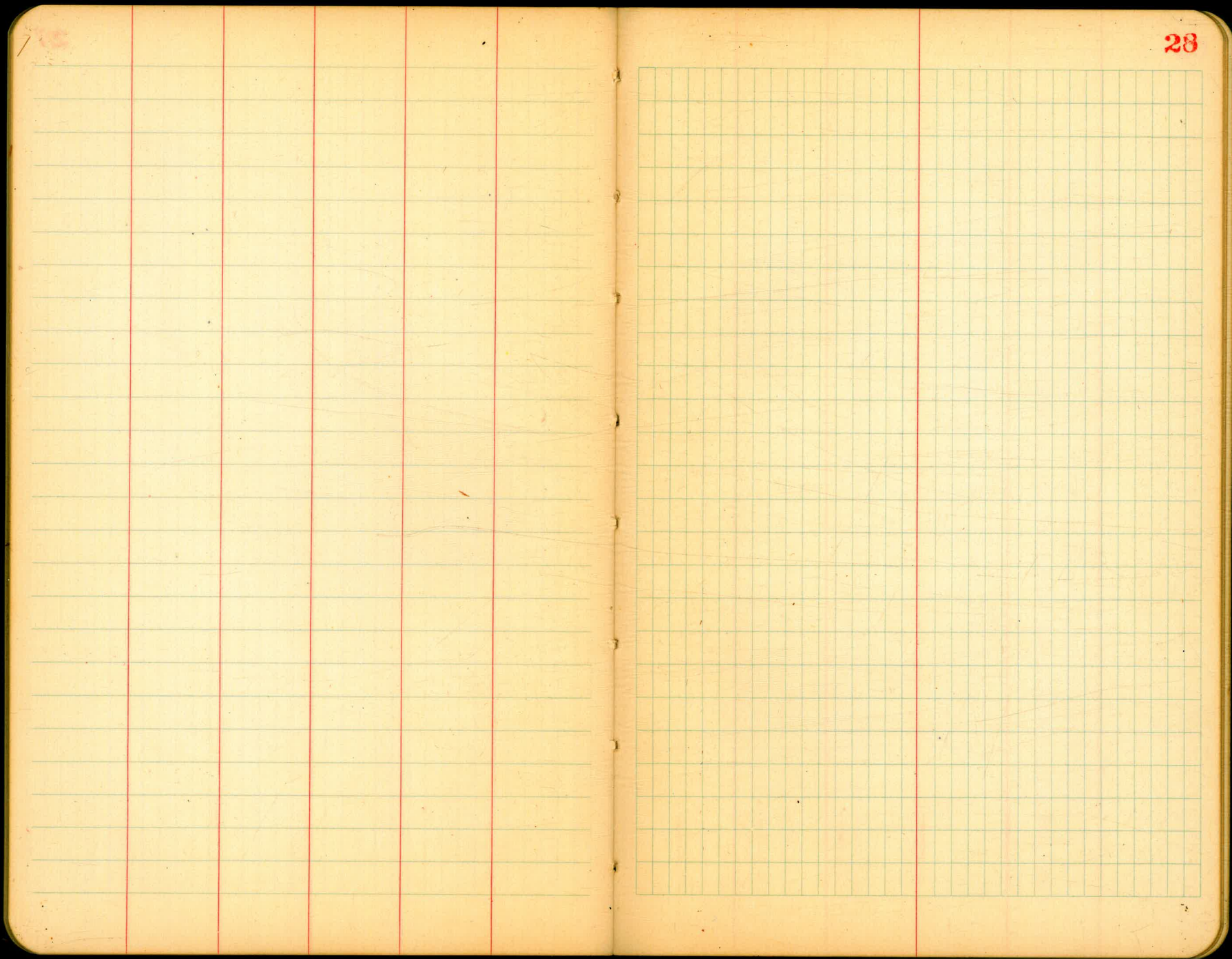


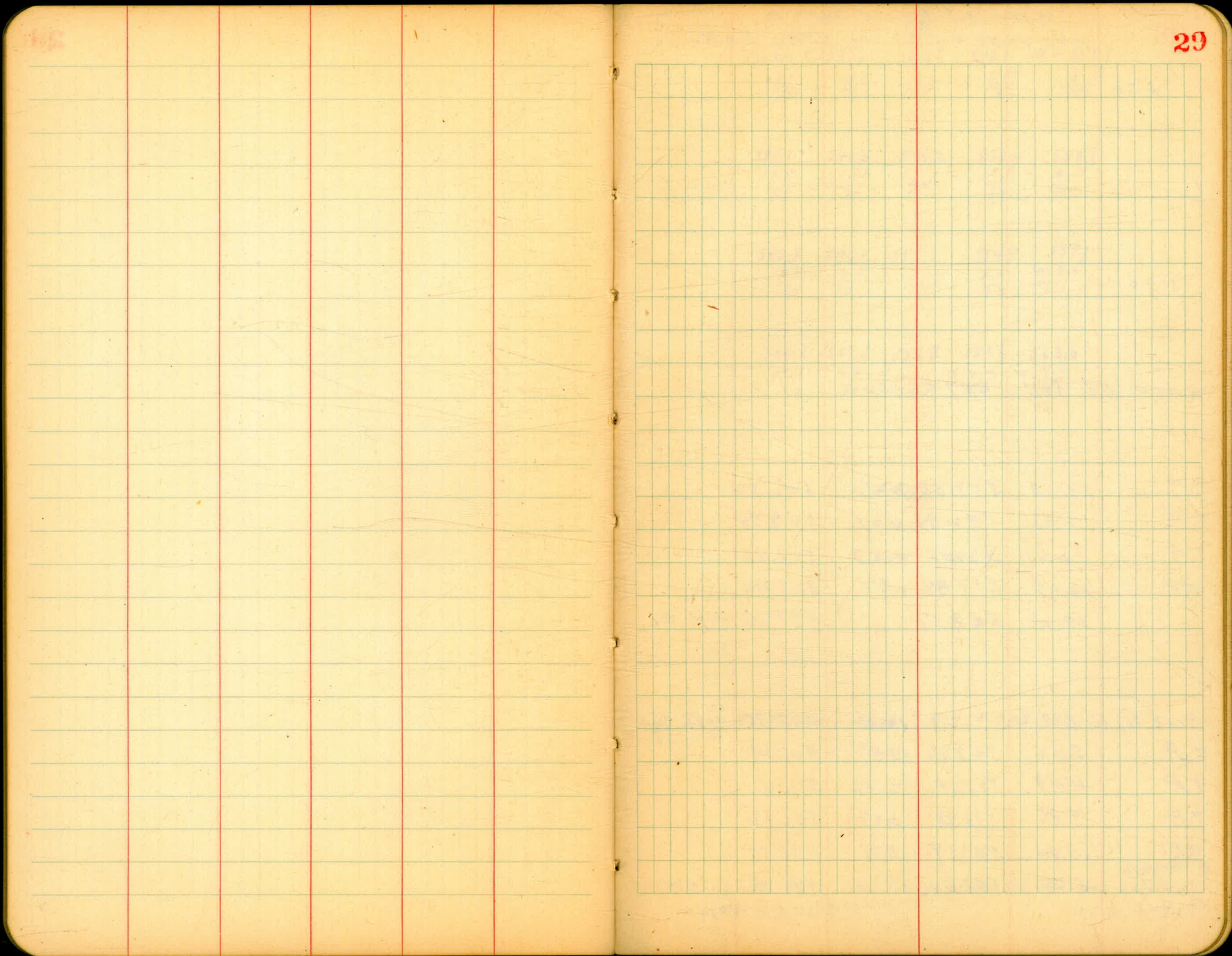


26

27







X sec. of Road on
Wly side of Lower OTAY Lake

+50

1

+50

0+00 B.C. Pt. = 607 + 21.62

T.P.	13.03	555.55	0.40	542.52
T.P.	12.93	542.92	0.07	529.99
T.P.	12.21	530.06	0.09	517.85
T.P.	12.49	517.94	2.92	505.45
	10.61	508.37		497.76 B.M. #1

check to Co. B.M. #1		10.61	497.75	497.76
T.P.	5.22	508.36	12.47	503.14
T.P.	4.49	515.61	2.86	511.12
T.P.	7.86	513.98	3.27	506.12
T.P.	12.60	509.39	5.71	496.79
	5.55	502.50		496.95 Co. B.M. U.S.G.S. DATUM

Moore
Sisson
Northward 9-1-38.

30

532.5 + T	537.3	542.6	547.1	R.P. 551.9
$\frac{23.1}{60}$	$\frac{18.3}{30}$	130	$\frac{8.5}{20}$	$\frac{3.7}{20}$

537.1	540.6	546.2	550.6	554.9
$\frac{18.5}{60}$	$\frac{15.0}{30}$	9.4	$\frac{5.0}{20}$	$\frac{0.7}{20}$

542.3	545.1	550.2	554.5	559.1
$\frac{18.3}{60}$	$\frac{10.5}{30}$	5.2	$\frac{1.1}{20}$	$\frac{+3.5}{20}$

544.3	549.4	553.9	557.6	562.6
$\frac{11.3}{60}$	$\frac{4.5}{30}$	17	$\frac{+2.0}{20}$	$\frac{+7.0}{20}$

555.55
3

Iron pin⁵⁰ R.P. Pl. 7 + 45.38 R.S. #750

spike in Fence Post 140' Sxly from Bridge bet Lower
approx. 633+00 Upper
OTAY LAKES

CT.

P

PT.

+50

d

P.I. 1x1 hub 2+82.66 246 528.83 = B.M. #1
 T.P. 0.26 531.29 1298 531.03 City Survey

+50

3

+50

T.P. 0.85 546.01 1239 543.16

2

555.55

511.6 19.7 <u>20</u>	514.9 16.4 <u>30</u>	517.0 14.3 <u>30</u>	519.1 14.2	520.2 11.1 <u>20</u>	522.1 9.2 <u>20</u>
----------------------------	----------------------------	----------------------------	---------------	----------------------------	---------------------------

514.8 16.5 <u>20</u>	520.2 11.1 <u>30</u>	522.2 9.1	524.3 7.0 <u>30</u>	526.6 2.7 <u>40</u>
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531.29
2

517.4 26.6 <u>20</u>	522.2 21.8 <u>25</u>	523.7 20.3 <u>30</u>	527.3 16.7	530.6 13.4 <u>20</u>	534.8 9.2 <u>40</u>
----------------------------	----------------------------	----------------------------	---------------	----------------------------	---------------------------

524.2 19.8 <u>20</u>	527.8 16.2 <u>30</u>	532.7 16.3	536.9 7.1 <u>20</u>	541.6 2.6 <u>20</u>
----------------------------	----------------------------	---------------	---------------------------	---------------------------

527.3 16.7 <u>20</u>	531.4 12.6 <u>30</u>	537.3 6.7	542.2 1.8 <u>20</u>	547.0 4.8 <u>20</u>
----------------------------	----------------------------	--------------	---------------------------	---------------------------

546.01
2

530.6 25.3 <u>20</u>	534.4 21.2 <u>30</u>	540.1 15.5	544.4 11.2 <u>20</u>	549.5 6.1 <u>20</u>
----------------------------	----------------------------	---------------	----------------------------	---------------------------

555.55
2

Cut new channel
for wash

8

T.P. 4.91 511.54 13.02 506.63

+50

7

+50

6

+50.94 E.C.

5

T.P. 1.06 519.67 12.28 518.61
531.79

LT 8 RT
503.1 501.4 499.3 501.3 503.1 505.8 508.0
8.4 10.1 13.2 10.2 8.4 5.7 3.5
60 54 53 72 20 20 40
Ewash

511.54
7

504.7 504.3 501.3 504.0 506.7 508.7
15.0 15.4 18.2 15.7 13.0 11.0
60 50 30 20 20 40
Wash Ewash
502.6 505.6 506.4 508.0 509.3 511.4
17.1 12.1 13.3 11.7 10.4 8.3
75 60 30 20 20 40

505.0 507.0 510.0 511.4 512.8 513.8
12.7 12.7 9.7 8.3 6.9 5.9
70 60 30 20 20 40
Wash
506.1 509.1 511.6 514.5 515.6 517.3
13.6 10.6 8.1 5.4 4.1 2.2
60 50 30 20 20 40

507.4 511.3 513.7 516.26 517.5 519.1
12.3 8.4 6.0 3.41 2.2 0.6
Wash 60 50 30 40 50 40
Hub

508.7 513.9 515.4 517.9 519.0 520.5
11.0 5.8 4.3 1.8 0.7 10.8
60 50 30 20 40
Wash

519.67
7

+36.96 = B.C. PT.

12

+50

11

+50

10

+50

9

8+50

511.54

33

494.8 $\frac{10.7}{60}$	497.2 $\frac{14.3}{30}$		499.83 11.71	501.9 $\frac{9.6}{20}$	503.9 $\frac{7.6}{20}$		
494.6 $\frac{10.9}{60}$	496.8 $\frac{10.7}{45}$	499.3 $\frac{12.2}{20}$	501.0 10.5	503.2 $\frac{8.8}{20}$	505.3 $\frac{6.4}{20}$		
	496.5 $\frac{15.0}{60}$	499.6 $\frac{11.9}{30}$	503.2 8.3	505.4 $\frac{6.1}{20}$	507.5 $\frac{2.0}{20}$		
	498.3 $\frac{13.2}{60}$	501.3 $\frac{10.2}{30}$	504.0 7.5	506.1 $\frac{5.2}{20}$	508.8 $\frac{2.7}{20}$		
	498.7 $\frac{12.8}{60}$	501.6 $\frac{9.9}{30}$	504.8 6.7	507.5 $\frac{4.0}{20}$	509.5 $\frac{5.0}{20}$		
	498.1 $\frac{13.4}{60}$	501.5 $\frac{10.0}{30}$	504.6 6.9	506.8 $\frac{2.7}{20}$	509.7 $\frac{1.8}{20}$		
	494.4 $\frac{17.1}{85}$	498.5 $\frac{13.0}{60}$	501.2 $\frac{10.3}{30}$	504.5 7.0	506.7 $\frac{2.8}{20}$	509.1 $\frac{2.2}{20}$	
	498.5 $\frac{13.0}{60}$	496.4 $\frac{15.1}{40}$	498.3 $\frac{13.2}{30}$	501.4 $\frac{10.1}{20}$	504.2 7.3	506.3 $\frac{5.2}{20}$	509.0 $\frac{2.5}{20}$
	500.9 $\frac{10.6}{60}$	500.3 $\frac{11.2}{50}$	497.9 $\frac{13.2}{20}$	499.5 $\frac{13.0}{30}$	503.9 7.6	505.9 $\frac{5.6}{20}$	508.1 $\frac{3.4}{20}$

Wash

Wash

Wash

Wash

511.54

+75

+50

T.P. Lark 8.44 517.22 0.17 508.78 14+38

to B.M. Fd. 35' Jt. of
check 13+50 - 2x2 Hub 9.98 498.97 509.52

check to Co. B.M. #1 KOMPIN 11.19 497.76 497.76

14

+50

13

12+50

T.P. 9.12 508.95 11.71 499.83
511.54

508.0 512.3
9.2 4.9
60 30 34 3.2 3.4
20 20

504.1 509.4 510.4 510.9 511.9
13.1 7.8
60 20 48 6.3 3.3
20 40

517.22
5

Elev. mkd. on Lark guard stake. origin unknown

500.0 502.1 505.2 506.4 507.9
9.0 6.9
60 30 3.8 2.6 1.1
20 20 40

496.8 499.0 501.2 502.8 504.3
12.2 10.0
60 30 7.8 6.4 4.7
20 20 40

494.9 496.6 500.0 501.0 502.9
10.1 12.4
60 30 9.0 8.0 6.1
20 20

495.0 497.7 499.7 501.3 503.1
14.0 11.3
60 30 9.3 7.7 5.9
20 20
508.95
5

18

T.P. 10.70 527.24 0.68 510.54

+59.67 E.C.

+50

17

+50

16

+50

15+00

517.22

510.9

17

16.3

60

515.1

12.1

30

520.6

6.9

525.1

2.1

30

528.8

P.T.

+1.6

40

35

527.24

7

508.6

8.6

60

512.6

1.6

30

517.8

+0.6

521.2

+4.0

20

526.0

+8.8

30

508.1

9.1

60

512.1

5.1

30

516.9

0.3

521.5

+4.1

20

526.2

+9.0

40

504.8

12.4

60

508.3

8.9

30

513.1

4.1

517.7

+0.5

20

522.4

+5.2

40

500.7

10.5

60

504.6

12.4

30

509.3

7.9

512.9

4.3

20

517.0

0.2

40

500.4

14.8

60

504.1

13.1

30

508.3

8.9

510.9

6.3

20

514.0

3.2

40

503.7

13.5

60

507.5

9.7

30

510.6

6.6

512.2

5.0

20

514.0

2.2

40

509.2

8.0

60

512.7

1.5

30

514.4

2.8

514.9

2.3

20

514.9

2.3

40

517.22

7

+50

T.P. 0.55 502.03 12.93 501.48

>1104.68 BC LT

T.P. 0.04 514.41 12.87 514.37

+50

20

+50

19

18750

527.24

492.0	492.6	493.5	495.5	497.1	498.2	500.0
10.0	9.4	8.5	6.5	4.9	3.8	2.0
<u>65</u>	<u>50</u>	<u>25</u>	<u>70</u>		<u>25</u>	<u>50</u>

36

502.03
7

495.4	497.9	500.9	502.7	504.9
19.0	16.5	13.5	11.7	9.5
<u>60</u>	<u>30</u>		<u>20</u>	<u>50</u>

514.41

501.0	505.7	510.4	513.0	516.0
26.7	21.5	16.8	12.0	11.2
<u>60</u>	<u>30</u>		<u>20</u>	<u>20</u>

509.3	514.3	519.5	523.5	528.2
17.9	12.9	7.7	3.7	+1.0
<u>60</u>	<u>30</u>		<u>20</u>	<u>20</u>

513.8	518.5	524.0	528.7	533.2
13.4	8.7	3.2	+1.5	+6.0
<u>60</u>	<u>30</u>		<u>20</u>	<u>40</u>

514.1	519.5	525.2	529.9	535.0
13.1	7.7	2.0	+2.7	+7.8
<u>60</u>	<u>30</u>		<u>20</u>	<u>40</u>

512.5	517.5	524.0	528.3	532.5
12.7	9.7	3.7	+1.1	+5.3
<u>60</u>	<u>30</u>		<u>20</u>	<u>40</u>

527.24
7

+ 25

501.34
 9.16
 510.50
 501.97
 8.53 rod = 155

tail in
 T.P. Post. 11.62 512.96 069 501.34

24

edge water

+ 50

23

+ 75 culv. radial

+ 50

22

502.03

488.7 492.7 492.8 494.0 498.3 501.9 504.0
 24.3 20.2 20.2 19.0 14.7 12.1 9.0
 65 50 37 34 25 50

20° Pt of 23 + 80 $\frac{512.96}{8}$

487.8 492.5 493.0 494.4 497.1 499.8 501.4
 12.2 9.5 9.0 7.6 4.9 2.2 0.6
 60 38 23 18 19 25 50

486.3 487.8 491.0 492.8 495.9 498.3
 15.7 14.2 11.0 9.2 6.1 3.7
 60 48 31 25 50
 edge water

486.2 487.8 489.2 491.9 492.6 493.3
 15.8 14.2 10.1 9.2 8.7
 60 6 25 50
 edge water

486.0 487.8 490.9 491.9 492.6
 16.0 14.2 11.1 10.1 9.2
 60 edge water 17 25 40

487.5 487.8 489.3 491.8 491.5 492.7 493.4
 14.5 14.2 12.7 10.2 10.5 9.3 8.6
 60 24 50 18 25 55
 edge water
 491.0 492.2 493.6 494.8 495.4
 11.0 9.8 8.2 7.2 6.6
 65 30 25 50

502.03
 8

+50

T.P. 5.92 530.47 0.08 524.55

27

26 + 50.61 B.C. RT. ON STUB

26

T.P. STUB 12.09 524.63 0.42 512.54 F.C. E 25 + 43.63

+43.63 E.C. ON STUB

25

+50

512.96

498.1	508.2	520.0	526.3	532.1
32.2	21.8		4.7	+1.6
<u>60</u>	<u>30</u>	10.5	<u>20</u>	<u>40</u>

530.47

499.8	508.6	520.8	527.3	534.2
24.8	15.0	3.8	+2.7	+9.6
<u>60</u>	<u>30</u>		<u>20</u>	<u>40</u>

500.4	509.4	519.92	526.1	532.1
24.2	15.2	4.71	+1.5	+7.5
<u>60</u>	<u>30</u>		<u>20</u>	<u>40</u>

500.8	508.3	517.6	523.8	530.2
23.8	16.3	7.0	0.8	+5.6
<u>60</u>	<u>30</u>		<u>20</u>	<u>40</u>

524.63

498.5	504.9	512.54	518.0	522.8
14.5	8.1	0.42	+5.0	+9.8
<u>60</u>	<u>30</u>		<u>20</u>	<u>40</u>

495.5	501.1	506.8	510.2	513.6
17.5	11.9	6.2	3.8	+0.6
<u>65</u>	<u>30</u>		<u>20</u>	<u>40</u>

492.2	492.2	494.2	496.2	500.2	504.0	507.2
20.8	20.8	18.8	16.8		9.0	5.8
<u>65</u>	<u>55</u>	<u>53</u>	<u>30</u>	12.8	<u>25</u>	<u>50</u>

512.96

31

+50

+12.06 E.C.

ON STUB

30

+50

29.

T.P.

0.97

518.50

12.94

517.53

+50

28

530.47

39

497.7	504.2	508.3	511.8	R515.1
188	14.3		6.7	3.4
50	30	10.2	20	40

496.1	498.0	501.7	507.8	511.5	515.0
22.4	20.5	16.8		7.0	3.5
60	55	30	10.7	20	40

493.5	496.2	501.7	507.74	511.8	516.0
24.0	22.3	16.8		4.7	2.5
60	55	30	10.76	20	40

494.5	496.1	500.9	507.3	511.5	516.0
24.0	22.4	17.6		7.0	2.5
60	55	30	11.2	20	40

494.7	494.7	495.7	499.2	505.4	509.9	515.7
23.8	23.8	22.8	19.3		8.6	2.8
60	53	50	30	13.1	20	40

493.0	493.0	495.1	499.7	506.0	510.2	515.3
25.5	25.5	23.4	18.8		8.3	3.2
60	55	53	30	12.5	20	40

$$\frac{518.50}{8}$$

495.0	500.2	508.6	513.9	519.3
35.5	30.3		16.6	11.2
60	30	21.9	20	20

496.0	500.2	506.0	512.9	519.3	525.8
34.5	30.3	24.5		11.2	4.7
60	45	50	17.6	20	40

$$\frac{530.47}{8}$$

34

494.3	496.1	496.0	497.0	501.6	504.5	507.9
$\frac{17.1}{50}$	$\frac{15.3}{34}$	$\frac{15.4}{30}$	$\frac{14.4}{28}$	9.8	$\frac{6.9}{20}$	$\frac{3.5}{40}$

+ 50

495.7	495.2	496.7	499.1	502.1	505.3	509.6
$\frac{15.7}{50}$	$\frac{16.4}{38}$	$\frac{14.7}{35}$	$\frac{12.3}{23}$	9.3	$\frac{6.1}{20}$	$\frac{1.8}{40}$

33

496.0	497.5	499.7	504.1	507.9	511.9
$\frac{15.4}{50}$	$\frac{13.9}{40}$	$\frac{11.7}{25}$	7.3	$\frac{3.5}{20}$	$\frac{10.5}{40}$

+ 50

495.4	496.7	500.0	504.4	508.4	512.2
$\frac{16.0}{50}$	$\frac{14.7}{47}$	$\frac{11.4}{25}$	7.0	$\frac{3.0}{20}$	$\frac{10.8}{40}$

check to Co. BM #2

12.03 499.41 499.38

47' LT of 32 + 00

T.P.

3.56 511.44 10.64 507.88

511.44

32

498.5	502.7	506.9	512.4	514.0
$\frac{20.0}{50}$	$\frac{15.8}{25}$	11.6	$\frac{6.1}{20}$	$\frac{4.5}{40}$

31 + 50

518.50

499.4	503.3	507.5	511.1	515.1
$\frac{19.1}{50}$	$\frac{15.7}{25}$	11.0	$\frac{7.4}{20}$	$\frac{3.4}{40}$

518.50

38

+50

37

+50

T.P. 12.33 512.60 11.17 500.27

30

+50

18" CULV. AT 90°

35

+50

511.44

41

499.8	504.7	510.5	515.1	519.0
<u>12.8</u>	<u>7.9</u>		<u>+2.5</u>	<u>+6.4</u>
50	35	21	20	40

495.2	497.1	499.6	505.8	510.6	515.0
<u>17.4</u>	<u>15.5</u>	<u>13.0</u>	6.8	<u>2.0</u>	<u>+2.4</u>
50	45	32		20	40

495.3	495.0	496.2	498.1	501.8	506.3	511.3
<u>17.3</u>	<u>17.2</u>	<u>16.4</u>	<u>14.5</u>		<u>6.3</u>	<u>1.3</u>
50	34	32	26	10.8	20	40

493.0	495.5	495.3	496.5	500.8	504.7	508.1
<u>19.6</u>	<u>17.1</u>	<u>17.3</u>	<u>16.1</u>		<u>7.9</u>	<u>4.5</u>
50	43	28	25	11.8	20	40

$$\frac{512.60}{2}$$

492.4	495.4	495.3	496.6	499.6	503.1	506.4
<u>19.0</u>	<u>16.0</u>	<u>16.1</u>	<u>14.8</u>		<u>8.3</u>	<u>5.0</u>
50	38	22	18	11.8	20	40

492.6	495.6	495.8	497.2	499.5	502.6	506.4
<u>18.8</u>	<u>15.8</u>	<u>15.2</u>	<u>14.2</u>		<u>8.8</u>	<u>5.0</u>
50	35	20	17	11.9	20	40

492.2	495.7	495.8	497.2	499.4	503.1	506.6
<u>19.2</u>	<u>15.7</u>	<u>15.6</u>	<u>14.2</u>		<u>8.3</u>	<u>4.8</u>
50	35	20	17	12.0	20	40

492.7	495.4	495.4	496.6	500.1	503.7	507.2
<u>18.7</u>	<u>14.0</u>	<u>12.0</u>	<u>14.8</u>		<u>7.7</u>	<u>4.7</u>
50	40	22	20	11.3	20	40

$$\frac{511.44}{2}$$

+50

T.P. 1280 537.96 0.04 525.16

40

+50

39

T.P. 12.61 525.20 0.01 512.59

+50

38+3503 B.C. PK

512.60

526.0	529.8	533.7	536.6	538.8
$\frac{120}{50}$	$\frac{82}{25}$	43	$\frac{1.4}{20}$	$\frac{+0.8}{40}$

$$\underline{537.96}$$

519.0	522.8	525.2	529.7	533.3	536.7
$\frac{42}{50}$	$\frac{24}{37}$	$\frac{0.0}{25}$	+4.5	$\frac{+8.1}{20}$	$\frac{+11.5}{40}$

513.3	518.9	523.1	524.8	529.2	533.3
$\frac{11.9}{50}$	$\frac{6.3}{25}$	$\frac{2.1}{10}$	0.4	$\frac{+4.0}{20}$	$\frac{+8.1}{40}$

507.2	513.4	519.7	524.4	528.7
$\frac{18.0}{50}$	$\frac{11.8}{25}$	5.5	$\frac{0.8}{20}$	$\frac{+3.5}{40}$

$$\underline{525.20}$$

503.5	508.9	515.0	519.6	524.1
$\frac{21}{50}$	$\frac{3.7}{25}$	+2.4	$\frac{+7.0}{20}$	$\frac{+11.5}{40}$

501.8	507.5	512.8	517.7	521.6
$\frac{10.8}{50}$	$\frac{5.1}{25}$	+0.4	$\frac{+5.1}{20}$	$\frac{+9.0}{40}$

$$\underline{512.60}$$

+50

T.P. 0.39 513.63 12.66 513.24

43

+50

+32.97 E.O.

T.P. 0.69 525.90 12.75 525.21

42

+50

537.96

41

498.5	502.0	503.3	504.9	505.4
$\frac{15.1}{20}$	$\frac{11.4}{25}$	10.3	$\frac{8.7}{20}$	$\frac{8.2}{50}$

513.43

502.8	506.8	509.9	511.7	512.6
$\frac{23.1}{20}$	$\frac{19.1}{25}$	16.0	$\frac{14.2}{20}$	$\frac{13.3}{40}$

507.6	511.8	517.3	519.5	521.1
$\frac{18.3}{20}$	$\frac{14.1}{20}$	8.4	$\frac{6.4}{20}$	$\frac{4.8}{40}$

508.6	512.9	518.92	522.4	525.0
$\frac{17.3}{20}$	$\frac{13.0}{20}$	4.98	$\frac{3.5}{20}$	$\frac{0.9}{40}$

525.90

517.4	520.7	524.3	526.6	529.0
$\frac{20.6}{50}$	$\frac{17.3}{25}$	13.7	$\frac{11.4}{20}$	$\frac{9.0}{20}$

525.3	528.4	530.9	532.2	533.9
$\frac{12.7}{50}$	$\frac{9.6}{25}$	7.1	$\frac{5.8}{20}$	$\frac{4.1}{40}$

529.0	532.1	534.6	536.5	538.4
$\frac{9.0}{50}$	$\frac{5.9}{25}$	3.4	$\frac{1.5}{20}$	$\frac{+0.4}{40}$

537.96

+50

+24.77 B.C.L.T

check to Co. 817 #3 Iron Pin 0.45 505.69 505.68
50' RT 46+00
46

+50

45

+65

+40 18" CULV 90°

T.P. 5.53 506.14 130.7 500.61

44

513.63

44

492.4	494.9	494.9	496.0	497.9	500.1	502.8
$\frac{13.7}{60}$	$\frac{11.4}{39}$	$\frac{11.2}{34}$	$\frac{10.1}{23}$	8.2	$\frac{6.0}{25}$	$\frac{3.3}{50}$

493.1	495.1	495.1	496.5	498.6	501.1	504.8
$\frac{13.0}{60}$	$\frac{11.0}{38}$	$\frac{11.0}{20}$	$\frac{9.6}{18}$	7.5	$\frac{5.0}{25}$	$\frac{1.3}{50}$

493.1	495.8	495.6	497.1	499.0	501.6	504.7
$\frac{13.0}{60}$	$\frac{10.3}{35}$	$\frac{10.5}{18}$	$\frac{9.0}{10}$	7.1	$\frac{4.5}{25}$	$\frac{1.4}{50}$

492.8	496.5	495.8	497.4	499.0	501.8	504.4
$\frac{13.3}{60}$	$\frac{9.6}{34}$	$\frac{10.3}{17}$	$\frac{8.7}{15}$	7.1	$\frac{4.3}{25}$	$\frac{1.7}{50}$

492.8	495.0	494.5	496.2	497.6	499.5	501.9
$\frac{13.3}{60}$	$\frac{11.1}{38}$	$\frac{11.6}{23}$	$\frac{9.9}{22}$	8.5	$\frac{6.6}{25}$	$\frac{2.2}{50}$

491.1	492.9	493.9	496.4	497.9	499.9
$\frac{15.0}{60}$	$\frac{13.2}{45}$	$\frac{12.2}{25}$	9.7	$\frac{8.2}{25}$	$\frac{6.2}{50}$

491.3	492.5	493.3	494.4	495.2	496.3
$\frac{14.8}{60}$	$\frac{13.6}{50}$	$\frac{12.8}{30}$	11.7	$\frac{10.9}{25}$	$\frac{9.8}{50}$

506.14

2

494.8	496.6	498.5	499.9	500.3
$\frac{18.8}{60}$	$\frac{17.0}{30}$	15.1	$\frac{13.7}{25}$	$\frac{13.3}{50}$

513.63

3

+50

50

+50

49

+80 24" CULV. Radial

+50

48

+50

47

wash

506.14

cut channel
to divert this
wash to 48+80

Σ

45

497.0	499.8	501.3	503.6	506.6	
$\frac{9.1}{65}$	$\frac{6.3}{30}$	48	$\frac{2.5}{25}$	$\frac{+0.5}{50}$	

496.7	499.0	500.6	501.9	503.3	
$\frac{2.4}{65}$	$\frac{7.1}{30}$	55	$\frac{4.2}{25}$	$\frac{3.8}{50}$	$\frac{155}{50}$
				49+65	

495.8	497.5	498.8	499.3	500.7	
$\frac{10.3}{65}$	$\frac{8.6}{30}$	73	$\frac{6.8}{25}$	$\frac{5.2}{50}$	$\frac{155}{65}$

495.4	496.5	497.6	498.3	499.5	
$\frac{10.7}{65}$	$\frac{9.6}{30}$	85	$\frac{7.8}{25}$	$\frac{6.6}{50}$	$\frac{155}{102}$

494.6	494.4	496.1	494.5	495.5	498.4	
$\frac{11.5}{65}$	$\frac{10.7}{40}$	$\frac{10.0}{10}$	11.6	$\frac{10.9}{25}$	$\frac{7.7}{50}$	$\frac{155}{115}$

491.4	492.8	496.1	497.8	498.9	
$\frac{12.7}{65}$	$\frac{13.3}{30}$	10.0	$\frac{8.3}{25}$	$\frac{7.7}{50}$	$\frac{155}{120}$

494.1	495.7	497.0	498.4	499.3	
$\frac{12.0}{65}$	$\frac{10.4}{30}$	9.1	$\frac{7.7}{25}$	$\frac{6.8}{50}$	$\frac{155}{115}$

493.8	494.3	495.5	496.6	498.0	499.5	501.0	
$\frac{12.3}{65}$	$\frac{11.8}{53}$	$\frac{10.6}{50}$	$\frac{9.5}{30}$	81	$\frac{6.6}{25}$	$\frac{5.1}{50}$	$\frac{155}{68}$

493.4	494.4	494.8	496.0	497.3	498.5	
$\frac{12.7}{65}$	$\frac{11.7}{50}$	$\frac{11.3}{31}$	101	$\frac{8.8}{25}$	$\frac{7.6}{50}$	$\frac{155}{100}$

506.14
9

+50

54

+50

53

+50

52

+49.01 E.C.

ON STUB

51

T.P.

11.36 513.50 4.00 502.14
 506.14

504.1 508.0 513.5 516.5 519.0
 $\frac{9.4}{60}$ $\frac{5.5}{30}$ 00 $\frac{+3.0}{20}$ $\frac{+5.5}{40}$

503.1 506.8 510.9 514.6 516.5
 $\frac{10.4}{60}$ $\frac{6.7}{30}$ 26 $\frac{+1.1}{20}$ $\frac{+3.0}{40}$

501.5 504.4 507.7 511.0 513.3
 $\frac{12.0}{60}$ $\frac{9.1}{30}$ 58 $\frac{2.5}{25}$ $\frac{0.2}{40}$
 \triangle

497.1 501.5 503.2 505.5 507.5
 $\frac{14.4}{45}$ $\frac{12.0}{30}$ 10.3 $\frac{8.0}{25}$ $\frac{6.0}{50}$

497.2 501.1 501.7 503.5 505.3
 $\frac{16.3}{25}$ $\frac{12.4}{30}$ 11.8 $\frac{10.0}{25}$ $\frac{8.2}{50}$

496.3 498.2 500.5 502.4 504.2
 $\frac{17.4}{25}$ $\frac{15.3}{30}$ 13.0 $\frac{11.1}{25}$ $\frac{9.3}{50}$

496.9 498.2 500.42 503.0 506.3
 $\frac{14.4}{25}$ $\frac{15.3}{30}$ 13.08 $\frac{10.5}{25}$ $\frac{7.2}{50}$

497.2 499.2 501.5 503.9 506.7
 $\frac{16.3}{25}$ $\frac{14.3}{30}$ 12.0 $\frac{9.6}{25}$ $\frac{6.8}{50}$

513.50
 $\frac{2}{2}$

58

+50

57

+50

56

+71.25 BCR₇

TR 8.94 518.29 4.15 509.35

+50

55

513.50

501.3	505.5	509.5	513.3	515.5
$\frac{17.0}{50}$	$\frac{12.8}{25}$	8.8	$\frac{5.0}{20}$	$\frac{2.8}{40}$

47

501.8	505.7	509.4	512.5	516.2
$\frac{16.5}{50}$	$\frac{12.6}{25}$	8.9	$\frac{5.8}{20}$	$\frac{2.1}{40}$

502.2	506.5	510.3	513.9	517.6
$\frac{14.1}{50}$	$\frac{11.8}{25}$	8.0	$\frac{4.4}{20}$	$\frac{0.7}{40}$

503.0	506.8	511.7	515.4	519.0
$\frac{15.3}{50}$	$\frac{11.5}{25}$	6.4	$\frac{2.9}{20}$	$\frac{+0.7}{40}$

505.0	508.4	513.0	516.5	519.5
$\frac{13.3}{50}$	$\frac{9.9}{25}$	5.3	$\frac{1.8}{20}$	$\frac{+1.1}{40}$

504.7	508.1	513.2	516.5	520.3
$\frac{13.6}{50}$	$\frac{10.2}{25}$	5.1	$\frac{1.8}{20}$	$\frac{+2.0}{40}$

518.29

504.6	508.9	513.2	516.5	520.0
$\frac{8.9}{50}$	$\frac{4.6}{25}$	0.3	$\frac{+3.0}{20}$	$\frac{+6.5}{40}$

505.3	509.1	513.8	517.6	520.5
$\frac{8.7}{50}$	$\frac{4.4}{25}$	+0.3	$\frac{+4.1}{20}$	$\frac{+7.0}{40}$

513.50

+50

61

+50

60

+91.76 E.C.

T.P. on 8.68 523.37 3.45 514.64
 E.C. 4.06
 +91.76

+50

59

+50

518.29

509.27 511.1 513.4 515.2 RT 517.2
 $\frac{13.6}{50}$ $\frac{12.4}{25}$ 9.9 $\frac{8.1}{20}$ $\frac{6.1}{40}$

512.0 513.8 516.1 518.2 520.0
 $\frac{11.3}{50}$ $\frac{9.5}{25}$ 7.2 $\frac{5.1}{20}$ $\frac{3.3}{40}$

512.7 514.6 517.0 519.2 521.4
 $\frac{10.6}{50}$ $\frac{8.7}{25}$ 6.3 $\frac{4.1}{20}$ $\frac{1.9}{40}$

509.9 512.6 515.2 517.6 520.5
 $\frac{13.4}{50}$ $\frac{10.7}{25}$ 8.1 $\frac{5.7}{20}$ $\frac{2.8}{40}$

509.7 511.9 514.64 517.3 520.2
 $\frac{13.4}{50}$ $\frac{11.4}{25}$ 8.68 $\frac{6.0}{20}$ $\frac{3.1}{40}$

523.32

505.7 508.8 512.5 515.1 518.2
 $\frac{12.6}{50}$ $\frac{9.5}{25}$ 5.8 $\frac{3.2}{20}$ $\frac{0.1}{40}$

504.3 506.7 510.5 512.3 515.4
 $\frac{14.0}{50}$ $\frac{11.6}{25}$ 7.8 $\frac{6.0}{20}$ $\frac{2.9}{40}$

502.3 505.8 509.1 512.6 514.9
 $\frac{14.0}{50}$ $\frac{12.5}{25}$ 9.2 $\frac{5.7}{20}$ $\frac{3.4}{40}$

518.29

64

+64.77 B.C. RT. on STUB

450

63

SMALL CULV.

62450

9.07 521.19 512.12 T.P.

14 to Co. BM. #4 17.22 500.57 500.56

10' RT. of
T.P. 62412 5.67 ~~517.79~~ 11.20 512.12 2 nails in
Cor. Fence Post

LY

523.32

49

507.3	510.7	512.6	514.2	516.7
$\frac{13.9}{50}$	$\frac{10.5}{25}$	8.4	$\frac{7.0}{20}$	$\frac{6.5}{40}$

505.2	507.5	509.70	511.8	514.2
$\frac{16.0}{50}$	$\frac{13.7}{25}$	11.49	$\frac{9.4}{20}$	$\frac{7.0}{40}$

504.9	507.0	509.2	511.2	513.6
$\frac{16.3}{50}$	$\frac{14.4}{25}$	12.0	$\frac{10.0}{20}$	$\frac{7.4}{40}$

502.2	505.0	507.3	510.0	513.0
$\frac{19.0}{50}$	$\frac{16.4}{25}$	13.7	$\frac{11.2}{20}$	$\frac{8.2}{40}$

503.8	505.9	508.4	510.2	512.8
$\frac{17.0}{50}$	$\frac{15.8}{25}$	12.8	$\frac{11.0}{20}$	$\frac{8.4}{40}$

$$\frac{521.19}{2}$$

60' LT of 56440 Iron Pin, BM. #4

506.2	508.3	510.3	512.0	514.2
$\frac{17.1}{50}$	$\frac{15.0}{25}$	13.0	$\frac{11.3}{20}$	$\frac{9.1}{40}$

$$\frac{523.32}{2}$$

750

67

750

66

750

65

T.P. 6.92 527.73 0.38 520.81

750

521.19

518.7	518.9	518.9	518.8	519.4
$\frac{9.0}{50}$	$\frac{8.8}{25}$	88	$\frac{8.9}{20}$	$\frac{8.8}{40}$

520.0	521.8	523.0	523.6	524.1
$\frac{7.7}{50}$	$\frac{5.9}{25}$	47	$\frac{4.1}{20}$	$\frac{3.4}{40}$

519.3	521.6	523.7	525.2	526.5
$\frac{8.4}{50}$	$\frac{6.1}{25}$	40	$\frac{2.5}{20}$	$\frac{1.2}{40}$

519.2	521.7	523.9	525.6	526.8
$\frac{8.5}{50}$	$\frac{6.0}{25}$	38	$\frac{2.1}{20}$	$\frac{0.9}{40}$

520.8	522.5	524.0	525.3	526.4
$\frac{6.9}{50}$	$\frac{5.2}{25}$	37	$\frac{2.4}{20}$	$\frac{1.3}{40}$

519.2	521.4	522.2	523.4	524.8
$\frac{8.5}{50}$	$\frac{6.3}{25}$	52	$\frac{4.3}{20}$	$\frac{2.9}{40}$

527.73

514.1	516.5	517.8	519.4	520.6
$\frac{2.1}{50}$	$\frac{4.7}{25}$	34	$\frac{1.8}{20}$	$\frac{0.4}{40}$

521.19

70 + 18.76 B.C. LT ON STUB

+95 18" C/V 90°

+50

T.P. 474 507.68 12.81 502.92

69400.77 E.C. ON STUB

+50

T.P. 0.57 515.73 12.57 515.16

68

507.73

492.7	493.7	496.02	498.0	500.0	$\frac{1.55}{100}$
$\frac{1.50}{60}$	$\frac{14.0}{30}$	STUB 1166	$\frac{9.7}{30}$	$\frac{7.7}{40}$	

492.7	494.4	495.1	495.8	496.5	$\frac{1.55}{120}$
$\frac{1.50}{60}$	$\frac{13.3}{30}$	12.4	$\frac{11.9}{30}$	$\frac{11.2}{40}$	

496.5	496.8	498.0	499.5	500.2
$\frac{11.2}{60}$	$\frac{10.9}{30}$	9.7	$\frac{8.2}{30}$	$\frac{7.5}{60}$

69420 = $\frac{1.55}{50}$

507.68

500.4	501.2	501.62	502.6	503.8
$\frac{1.53}{50}$	$\frac{14.5}{25}$	14.11	$\frac{13.1}{20}$	$\frac{11.9}{40}$

505.4	506.4	507.4	508.0	509.0
$\frac{10.8}{50}$	$\frac{9.8}{25}$	8.3	$\frac{7.7}{20}$	$\frac{6.7}{20}$

515.73

512.3	512.7	512.8	513.2	513.4
$\frac{15.4}{50}$	$\frac{15.0}{25}$	14.9	$\frac{14.5}{20}$	$\frac{14.3}{40}$

527.73

74 24" Culv. Radial

155
135

+50

To 74+00

73 Wash to Pt. divert by channel

155
110

+50

72

72+15 155
50

+50

71

+50

507.68

492.0	493.0		494.3	495.5	496.5	496.5	497.1
15.7 60	14.7 30		13.4	12.2 30	11.2 43	11.2 5.7	10.6 60

492.5	493.0	493.3	494.7	495.9	496.4	497.9
15.2 60	14.7 50	14.4 30	13.0	11.8 20	11.3 39	9.8 60

492.9	494.5	495.9	496.0	496.0	496.6	497.5	499.2
14.8 60	13.2 30	11.8 10	11.7	11.7 8	11.1 10	10.2 30	8.5 60

494.1	495.3	495.5	496.5	497.9	499.5	501.3
13.6 60	12.4 42	12.2 25	11.2 30	9.6	8.2 30	6.4 60

495.7	495.5	496.6	497.3	500.2	503.1	505.6
12.0 60	12.2 42	11.1 40	10.4 30	7.5	4.6 30	2.1 60

495.7	495.3	496.8	498.8	502.0	505.9	509.5
12.0 60	12.4 54	10.9 54	8.9 30	5.7	1.8 30	1.8 60

494.6	494.3	495.5	497.3	500.8	504.8	508.5
13.1 60	13.4 54	12.2 53	10.4 30	6.9	2.9 30	10.8 60

493.1	493.7	495.3	497.5	499.8	503.7
14.6 60	14.0 50	12.4 30	10.2	7.9 30	4.0 60

155
50

507.68

77

+50

76

check to I.P. & B.M. #5 1208 503.98 503.95

T.P. 8.61 516.06 0.23 507.45

+50

75

+91.89 E.C. on stub

+50

507.68

501.7	505.5	510.6	513.9	PT 517.5
14.7	10.6	5.5	2.7	+ 1.4
<u>60</u>	<u>30</u>		<u>20</u>	<u>40</u>

501.1	505.0	509.2	512.7	516.9
15.0	11.1	6.9	3.4	+ 0.8
<u>60</u>	<u>30</u>		<u>20</u>	<u>40</u>

498.1	501.7	506.3	509.8	512.8
18.0	14.4	9.8	6.3	3.3
<u>60</u>	<u>30</u>		<u>20</u>	<u>40</u>

65' PT 04 74 + 91.89 E.C.

516.06

493.1	494.3	497.7	503.0	505.3	508.3
14.6	13.4	10.0	4.7	2.4	+ 0.6
<u>60</u>	<u>52</u>	<u>30</u>		<u>20</u>	<u>40</u>

492.7	494.9	494.6	496.0	496.7	498.8	504.6
15.0	12.8	13.1	11.7	11.0	7.9	3.1
<u>60</u>	<u>30</u>	<u>70</u>	<u>8</u>		<u>30</u>	<u>60</u>

492.3	494.3	495.3	494.84	494.8	498.8	502.9
15.4	13.4	12.4	12.84	11.9	8.9	4.8
<u>60</u>	<u>26</u>	<u>22</u>		<u>2</u>	<u>30</u>	<u>60</u>

491.3	492.5	494.5	496.3	496.7	498.0
16.4	15.2	13.2	11.4	11.0	9.7
<u>60</u>	<u>30</u>		<u>55</u>	<u>42</u>	<u>60</u>

507.68

80 + 13.15 = 93.15 B.C. Pt.
ON STUB

80

+50 Small Culu 90°

79

+50

78

T.P. 11.01 521.73 5.34 510.74

+50

516.06

54

512.3	512.2	511.44	510.8	511.6
$\frac{9.4}{20}$	$\frac{9.5}{20}$	10.29	$\frac{10.9}{20}$	$\frac{10.1}{20}$

509.4	509.5	508.8	509.0	509.9
$\frac{12.8}{50}$	$\frac{12.2}{25}$	12.9	$\frac{12.7}{20}$	$\frac{11.8}{20}$

500.5	501.3	502.9	504.5	506.5
$\frac{21.2}{20}$	$\frac{20.4}{30}$	18.8	$\frac{17.2}{20}$	$\frac{15.2}{20}$

497.2	499.3	501.3	504.2	507.0
$\frac{22.5}{20}$	$\frac{22.4}{30}$	20.4	$\frac{17.5}{20}$	$\frac{14.7}{20}$

491.8	500.5	503.7	507.6	510.0
$\frac{25.9}{20}$	$\frac{21.2}{30}$	18.0	$\frac{14.1}{20}$	$\frac{11.7}{20}$

497.8	502.9	507.1	511.1	514.7
$\frac{23.9}{20}$	$\frac{18.8}{30}$	14.6	$\frac{10.6}{20}$	$\frac{7.0}{20}$

521.73

506.6	504.9	509.2	512.7	516.1	516.7
$\frac{15.5}{20}$	$\frac{11.2}{30}$	6.9	$\frac{3.4}{20}$	$\frac{0.0}{20}$	$\frac{40.6}{20}$

516.06

+50

83

+50

82

+50

81

+50

80+00 original 500.

521.73

512.7	513.6	513.3	514.1	514.7
$\frac{9.4}{40}$	$\frac{8.1}{20}$	8.4	$\frac{7.6}{20}$	$\frac{7.0}{40}$

513.2	514.2	514.8	514.3	515.4
$\frac{8.5}{40}$	$\frac{7.5}{20}$	6.9	$\frac{7.4}{20}$	$\frac{6.8}{40}$

514.8	514.6	515.2	516.0	516.9
$\frac{6.9}{40}$	$\frac{7.1}{20}$	6.5	$\frac{5.7}{20}$	$\frac{4.8}{40}$

515.9	514.9	516.1	516.9	517.3
$\frac{5.8}{40}$	$\frac{6.8}{20}$	5.6	$\frac{4.8}{20}$	$\frac{4.4}{40}$

516.3	516.4	516.3	517.7	518.3
$\frac{5.4}{40}$	$\frac{5.3}{20}$	5.4	$\frac{4.0}{20}$	$\frac{3.4}{40}$

517.4	517.9	518.1	518.7	519.7
$\frac{4.3}{40}$	$\frac{3.8}{20}$	3.4	$\frac{3.0}{20}$	$\frac{2.0}{40}$

517.5	518.4	518.7	519.1	519.7
$\frac{2.2}{40}$	$\frac{3.8}{20}$	3.0	$\frac{2.4}{20}$	$\frac{2.0}{40}$

516.5	516.5	516.7	516.1	516.7
$\frac{5.2}{40}$	$\frac{5.2}{20}$	5.0	$\frac{5.6}{20}$	$\frac{5.0}{40}$

521.73

+50

80 + 35.68 E.C.

84

+50

85

+50

T.P. 593 519.62 8.04 513.69

84

521.73

510.5	511.2	511.8	512.2	514.0
$\frac{9.1}{40}$	$\frac{8.4}{20}$	7.8	$\frac{6.4}{20}$	$\frac{5.6}{40}$

510.5	511.9	512.5	513.0	513.4
$\frac{9.1}{40}$	$\frac{7.7}{20}$	7.1	$\frac{6.6}{20}$	$\frac{6.2}{40}$

510.9	511.5	512.3	512.4	513.8
$\frac{8.7}{40}$	$\frac{8.1}{20}$	7.3	$\frac{7.2}{20}$	$\frac{5.8}{40}$

510.1	511.3	512.4	513.6	513.3
$\frac{9.5}{40}$	$\frac{8.3}{20}$	7.2	$\frac{6.0}{20}$	$\frac{6.3}{40}$

510.9	512.0	511.8	513.5	514.1
$\frac{8.7}{40}$	$\frac{7.6}{20}$	7.8	$\frac{6.1}{20}$	$\frac{5.5}{40}$

511.3	511.9	512.7	513.2	514.1
$\frac{8.3}{40}$	$\frac{7.7}{20}$	6.9	$\frac{6.4}{20}$	$\frac{5.5}{40}$

519.62

511.9	512.0	513.3	514.0	514.3
$\frac{9.8}{40}$	$\frac{9.7}{20}$	8.4	$\frac{7.7}{20}$	$\frac{7.4}{20}$

521.73

+50

89

+50

+3569 BC Rr ON STUB

88

+75

+46 small wash

87

51962

508.7	511.1	513.1	515.3	517.6
$\frac{10.9}{40}$	$\frac{8.5}{20}$	6.5	$\frac{4.3}{20}$	$\frac{2.0}{40}$

512.2	513.0	514.0	515.0	516.3
$\frac{7.4}{40}$	$\frac{6.6}{20}$	5.0	$\frac{4.4}{20}$	$\frac{3.3}{40}$

512.3	513.4	514.3	514.4	515.1
$\frac{7.3}{40}$	$\frac{6.7}{20}$	5.3	$\frac{5.4}{20}$	$\frac{4.5}{40}$

512.6	513.5	514.46	514.9	514.9
$\frac{7.0}{40}$	$\frac{6.1}{20}$	5.16	$\frac{4.7}{20}$	$\frac{4.8}{40}$

512.0	511.6	511.6	512.5	513.1
$\frac{7.6}{40}$	$\frac{8.0}{20}$	8.0	$\frac{7.1}{20}$	$\frac{6.5}{40}$

509.6	509.6	510.3	510.4	511.5
$\frac{10.0}{40}$	$\frac{10.0}{20}$	9.3	$\frac{8.8}{20}$	$\frac{8.1}{40}$

505.9	507.0	507.5	507.6	509.6
$\frac{13.7}{40}$	$\frac{12.6}{20}$	12.1	$\frac{12.0}{20}$	$\frac{10.0}{40}$

507.0	508.0	509.7	510.9	512.6
$\frac{12.6}{40}$	$\frac{11.6}{20}$	9.9	$\frac{8.7}{20}$	$\frac{7.0}{40}$

51962
5

93

517.6	524.7	527.1	530.0	533.3
$\frac{13.9}{50}$	$\frac{8.8}{25}$	44	$\frac{1.5}{20}$	$\frac{+1.8}{40}$

+50

517.5	521.3	525.6	528.3	532.0
$\frac{14.0}{50}$	$\frac{10.8}{25}$	5.9	$\frac{3.7}{20}$	$\frac{+0.5}{40}$

92

517.1	520.7	524.2	527.2	529.8
$\frac{14.4}{50}$	$\frac{10.8}{25}$	7.3	$\frac{4.3}{20}$	$\frac{1.7}{40}$

+50

516.1	520.2	523.0	525.9	528.1
$\frac{15.4}{50}$	$\frac{11.3}{25}$	8.5	$\frac{5.0}{20}$	$\frac{3.4}{40}$

91

514.8	518.5	521.7	523.8	525.9
$\frac{16.7}{50}$	$\frac{13.0}{25}$	9.8	$\frac{7.7}{20}$	$\frac{5.0}{40}$

T.P. 11.98 531.49 0.11 519.51

+50

512.4	515.8	518.8	521.1	523.1
$\frac{7.7}{50}$	$\frac{3.8}{25}$	0.8	$\frac{+1.5}{20}$	$\frac{+3.5}{40}$

90

508.8	512.6	515.3	518.0	520.0
$\frac{10.8}{50}$	$\frac{7.0}{20}$	4.3	$\frac{1.6}{20}$	$\frac{+0.4}{40}$

519.02

519.02

Check to B.M. #6 1674 489.94 489.89
 T.P. 0.32 504.72 12.73 506.40

750

95

T.P. 0.24 519.13 12.80 518.69

152.52 B.C. LT. ON STUB

94

+50

93 +34.85 EC ON STUB
 531.49
 519.62

LY

R

RT

59

B.M. #6 Iron P.N. approx 120 Lt. 95+25

502.0 504.2 506.1 507.1 508.1
 $\frac{17.1}{50}$ $\frac{14.9}{25}$ 130 $\frac{12.0}{20}$ $\frac{11.0}{40}$

508.7 513.2 516.6 519.5 521.3
 $\frac{10.4}{50}$ $\frac{5.9}{25}$ 25 $\frac{+0.4}{20}$ $\frac{+2.2}{40}$

519.13

512.4 518.2 522.88 526.0 529.6
 $\frac{19.1}{50}$ $\frac{13.3}{25}$ 8.41 $\frac{5.5}{20}$ $\frac{1.9}{40}$

516.0 521.5 526.4 529.7 532.3
 $\frac{15.5}{50}$ $\frac{10.0}{25}$ 5.1 $\frac{1.8}{20}$ $\frac{+0.8}{40}$

518.1 523.0 527.8 531.0 534.5
 $\frac{13.4}{50}$ $\frac{8.5}{25}$ 37 $\frac{0.5}{20}$ $\frac{+3.0}{40}$

518.0 523.6 527.66 531.1 534.3
 $\frac{13.5}{50}$ $\frac{7.9}{25}$ 3.83 $\frac{0.4}{20}$ $\frac{+2.8}{40}$

531.49

519.62

+65

+40

18" Culv. Radial

98

+50

97

$$\begin{array}{r} 496.6 \\ 12.1 \\ \hline 508.7 \\ 501.97 \\ \hline 6.73 \end{array}$$
edge water
8-6-38

+65

+35

18" Culv. Radial

96

506.72

493.3	493.7	495.3	499.2	500.8	501.9
$\frac{13.4}{65}$	$\frac{13.0}{50}$	$\frac{11.4}{25}$	$\frac{7.5}{25}$	$\frac{5.9}{25}$	$\frac{4.8}{50}$

 $\frac{1.55}{50}$

491.8	492.7	494.3	495.9	497.5	500.0
$\frac{14.9}{65}$	$\frac{14.0}{50}$	$\frac{12.4}{25}$	10.8	$\frac{9.2}{25}$	$\frac{4.7}{50}$

 $\frac{1.55}{75}$

491.7	492.5	494.5	493.9	495.3	496.8	499.0	500.7	502.0
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$\frac{16.0}{65}$	$\frac{14.2}{25}$	$\frac{12.2}{25}$	$\frac{12.8}{16}$	$\frac{11.4}{15}$	9.9	$\frac{7.7}{15}$	$\frac{6.0}{50}$	$\frac{4.7}{50}$
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 $\frac{1.55}{50}$
97496 = 50

499.7	491.6	495.4	494.7	496.7	499.1	502.3	505.3
-------	-------	-------	-------	-------	-------	-------	-------

$\frac{17.0}{65}$	$\frac{15.1}{50}$	$\frac{11.3}{30}$	$\frac{12.0}{17}$	$\frac{10.0}{15}$	7.6	$\frac{6.2}{50}$	$\frac{1.2}{50}$
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487.7	488.9	490.5	494.8	494.4	496.6	500.7	504.4
-------	-------	-------	-------	-------	-------	-------	-------

$\frac{19.0}{90}$	$\frac{17.8}{65}$	$\frac{16.4}{40}$	$\frac{11.9}{17}$	$\frac{12.3}{3}$	10.1	$\frac{6.0}{17}$	$\frac{2.3}{50}$
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 $\frac{1.55}{75}$

488.7	490.1	491.0	493.6	493.6	495.5	501.2
-------	-------	-------	-------	-------	-------	-------

$\frac{18.0}{65}$	$\frac{16.6}{40}$	$\frac{15.7}{15}$	13.1	$\frac{13.1}{15}$	$\frac{11.2}{20}$	$\frac{5.5}{50}$
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 $\frac{1.55}{50}$

489.4	490.9	492.1	496.5	494.6	495.1
-------	-------	-------	-------	-------	-------

$\frac{17.3}{65}$	$\frac{15.8}{30}$	14.6	$\frac{13.2}{25}$	$\frac{12.1}{50}$	$\frac{11.6}{60}$
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 $\frac{1.55}{190}$

492.6	493.0	494.9	495.8	496.7	498.0
-------	-------	-------	-------	-------	-------

$\frac{14.1}{20}$	$\frac{13.7}{25}$	$\frac{11.8}{25}$	10.9	$\frac{10.0}{25}$	$\frac{8.7}{50}$
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506.72

 $\frac{1.55}{50}$
95495 = 50

+50

101

¹⁰⁷⁴
T.P. 101150 10.23 541.80 0.0x 531.17

100 + 50

99 + 93.76 B.C. RT.

T.P. 1290 531.21 0.37 518.31

+47.38 E.C. ON 5746

99

T.P. 1293 518.68 007 506.65
506.72

531.4	533.7	535.4	537.8	539.4
$\frac{10.4}{20}$	$\frac{8.1}{20}$	6.4	$\frac{4.0}{20}$	$\frac{2.4}{40}$

524.0	527.3	530.7	533.1	535.3
$\frac{17.8}{20}$	$\frac{12.5}{20}$	11.1	$\frac{8.7}{20}$	$\frac{6.5}{40}$

541.80

517.0	520.7	525.2	528.1	531.4
$\frac{14.2}{50}$	$\frac{10.5}{25}$	6.0	$\frac{3.1}{20}$	$\frac{7.0}{40}$

509.3	515.2	520.03	523.7	526.8
$\frac{21.9}{50}$	$\frac{16.0}{25}$	11.18	$\frac{7.5}{20}$	$\frac{4.4}{40}$

531.21

503.3	510.7	515.29	519.0	522.1
$\frac{15.4}{60}$	$\frac{8.0}{25}$	3.39	$\frac{4.0}{25}$	$\frac{3.4}{50}$

496.5	498.9	502.2	506.0	508.8	511.5
$\frac{32.2}{65}$	$\frac{19.8}{50}$	$\frac{16.5}{25}$	12.7	$\frac{2.9}{25}$	$\frac{7.7}{50}$

518.68

750

105

750

104 + 02.63 E.C.

750

103

750

102

541.80

62

518.6 523.3 528.2 532.0 535.2

$\frac{23.7}{50}$ $\frac{18.5}{25}$ 13.6 $\frac{9.8}{20}$ $\frac{6.6}{40}$

521.2 525.4 529.3 532.2 534.9
 $\frac{20.4}{50}$ $\frac{16.4}{25}$ 12.5 $\frac{9.6}{20}$ $\frac{6.9}{40}$

517.7 522.7 527.1 530.2 533.1
 $\frac{24.1}{50}$ $\frac{19.1}{25}$ 14.7 $\frac{11.6}{20}$ $\frac{8.7}{40}$

513.7 518.4 524.0 527.1 530.0
 $\frac{28.1}{50}$ $\frac{23.4}{25}$ 17.8 $\frac{14.7}{20}$ $\frac{11.8}{40}$

523.7 526.4 529.2 531.2 533.4
 $\frac{18.1}{50}$ $\frac{15.4}{25}$ 12.6 $\frac{10.6}{20}$ $\frac{8.4}{40}$

531.0 531.7 533.6 535.1 536.7
 $\frac{10.8}{20}$ $\frac{10.1}{20}$ 8.2 $\frac{6.7}{20}$ $\frac{5.1}{40}$

535.3 536.2 537.1 538.2 539.9
 $\frac{6.5}{40}$ $\frac{5.6}{20}$ 4.7 $\frac{3.6}{20}$ $\frac{1.9}{40}$

536.6 537.8 538.3 539.6 540.9
 $\frac{5.4}{40}$ $\frac{4.0}{20}$ 3.5 $\frac{2.4}{20}$ $\frac{0.9}{40}$

541.80

750

108 Saddle good cut here

Set B17 #7

1.39 550.44

750

107

T.P. 1201 551.83 228 539.52

750

106

541.80

547.4	545.8	545.3	545.3	545.7
$\frac{4.4}{40}$	$\frac{0.0}{30}$	6.5	$\frac{6.5}{20}$	$\frac{6.1}{40}$

550.4	550.2	550.4	550.4	550.8
$\frac{11.4}{40}$	$\frac{1.4}{20}$	11.4	$\frac{1.4}{20}$	$\frac{1.0}{40}$

50' LT. of 108 + 00 2 x 2 P.W.

545.7	545.7	546.2	547.1	549.2
$\frac{4.1}{40}$	$\frac{6.1}{20}$	5.0	$\frac{4.7}{30}$	$\frac{2.4}{20}$

536.4	537.2	539.0	541.5	544.1
$\frac{7.54}{20}$	$\frac{12.4}{20}$	12.8	$\frac{10.3}{20}$	$\frac{7.7}{20}$

551.83

525.7	529.8	534.0	537.5	540.7
$\frac{10.1}{20}$	$\frac{12.0}{25}$	7.8	$\frac{4.3}{20}$	$\frac{1.1}{40}$

519.7	524.5	528.9	533.2	536.1
$\frac{22.1}{50}$	$\frac{17.3}{25}$	12.9	$\frac{8.0}{20}$	$\frac{5.7}{40}$

541.80

111

+50

+24.76 B.C. + T. STU 6

110

T.P. 0.24 527.35 12.65 527.13

+50

T.P. 0.55 539.78 12.60 539.23

109

551.83

516.8	513.1	510.8	510.2	509.2
$\frac{11.1}{50}$	$\frac{12.3}{25}$	14.6	$\frac{17.2}{25}$	$\frac{18.2}{50}$

521.1	517.6	516.4	515.4	515.7
$\frac{6.3}{50}$	$\frac{9.8}{25}$	11.2	$\frac{12.0}{25}$	$\frac{11.7}{50}$

523.0	521.6	520.50	518.4	518.3	520.2
$\frac{4.4}{40}$	$\frac{5.8}{20}$	6.85	$\frac{9.0}{20}$	$\frac{9.1}{36}$	$\frac{7.2}{50}$

526.9	525.2	523.8	522.9	521.2	523.6
$\frac{0.5}{40}$	$\frac{2.2}{25}$	4.6	$\frac{4.5}{15}$	$\frac{6.2}{25}$	$\frac{3.8}{40}$

527.35

533.7	531.7	529.3	527.6	528.8	530.0
$\frac{6.1}{40}$	$\frac{8.1}{20}$	10.5	$\frac{12.2}{8}$	$\frac{11.0}{20}$	$\frac{9.8}{40}$

539.78

540.1	538.1	537.1	537.4	538.3
$\frac{11.7}{40}$	$\frac{13.7}{20}$	14.7	$\frac{12.2}{20}$	$\frac{13.5}{40}$

551.83

+50

114

+50

51701 wash to RT div.

113

+50

112 18" culv. diag. Plot location

T.P. 0.35 514.67 18.03 514.32

111 +50

527.35

494.2	496.7	499.8	504.4	507.9	511.1
20.5	18.0	14.9		6.8	3.6
65	44	25	10.3	20	40

495.7	493.6	496.7	500.5	505.0	508.4	511.5
19.0	21.1	18.0	14.4		6.3	3.4
70	65	50	25	9.7	20	40

wash

497.6	497.1	499.7	500.9	503.4	506.5	509.8
15.1	17.4	15.0	13.8		8.2	4.9
65	53	42	25	11.3	20	40

wash

501.0	501.0	503.8	508.5	512.8
13.7	13.7		6.2	1.9
50	78	10.9	25	50

wash

503.3	502.4	503.2	507.3	511.9
11.4	12.5	11.5	7.4	2.8
50	25 E wash		25	50

506.8	504.6	504.0	505.7	509.8
2.9	10.1		9.2	4.9
50	25	10.7 E wash	25	50

514.67

510.7	507.7	506.3	506.3	507.1
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16.6	19.6	21.0	21.0	20.2	E wash
50	25		25	50	

527.35

+50

117

^{nail}
T.P. Post 7.56 509.15 13.08 501.59

116+50

116+07 small wash Pt.

115+47.30 E.C.

+50

115

514.67

	LT	E	RT
	491.0	491.2	499.9
	499.0	501.7	504.0
	505.9		
	18.7	18.0	16.3
	10.2	7.5	5.2
	7.5	5.2	4.0
	487.4	490.6	492.2
	493.2	499.2	501.7
	504.0		
edge	21.8	18.6	17.0
Water	5.7	4.5	3.0
	10.0	7.5	5.2
	20	20	20

509.15

Nail in Post 20' Pt of 116+40

488.7	490.5	490.7	493.0	494.1	497.7	501.0	497.3 502.3
26.0	24.2	24.0	21.7	20.6		13.7	12.4
6.5	3.8	3.2	2.0	1.7	17.0	5.0	4.0

488.3	490.3	492.6	493.7	495.6	497.5	499.8	500.9
26.4	24.4	22.1	21.0	19.1		14.9	13.8
6.8	5.0	4.0	3.0	1.7	17.2	2.0	4.0

490.2	491.7	493.1	493.2	495.5	499.7	502.0	504.1
24.5	23.0	21.0	21.5	19.2		12.7	10.6
7.0	6.0	4.5	3.4	3.0	15.0	5.0	2.0

491.8	493.2	495.4	499.1	500.8	503.2	505.3
22.9	21.5	19.3	15.6		11.5	9.4
2.5	2.2	4.0	2.0	13.9	5.0	4.0

492.5	495.6	499.7	503.1	505.4	507.6
22.2	19.1	15.0		9.3	7.1
6.5	5.0	3.5	11.6	2.0	4.0

514.67

+ 50

121

+ 55.46 BC Pt. on stud

120

+ 50

119

+ 50

118

509.15

501.3	502.4	506.5	508.4	511.2
$\frac{7.9}{50}$	$\frac{5.8}{25}$	2.7	$\frac{0.8}{20}$	$\frac{+2.0}{40}$

501.0	503.7	506.2	509.2	512.0
$\frac{8.2}{50}$	$\frac{5.5}{25}$	3.0	$\frac{0.0}{20}$	$\frac{+2.8}{40}$

501.3	503.7	506.5	509.5	512.3
$\frac{7.9}{50}$	$\frac{5.5}{25}$	2.63	$\frac{+0.3}{20}$	$\frac{+3.1}{40}$

500.3	502.5	506.2	509.2	512.4
$\frac{8.9}{50}$	$\frac{4.7}{25}$	3.0	$\frac{0.0}{20}$	$\frac{+3.2}{40}$

499.6	502.4	504.5	506.2	508.7	511.7
$\frac{9.4}{50}$	$\frac{4.8}{25}$	$\frac{4.7}{17}$	3.0	$\frac{0.5}{20}$	$\frac{+2.5}{40}$

499.8	502.1	505.1	507.7	511.2
$\frac{9.4}{50}$	$\frac{7.1}{25}$	4.1	$\frac{1.5}{20}$	$\frac{+2.0}{40}$

499.7	502.1	504.7	506.9	509.7
$\frac{9.5}{50}$	$\frac{7.1}{25}$	4.5	$\frac{2.3}{20}$	$\frac{+0.5}{40}$

497.1	500.8	503.9	506.0	508.1
$\frac{12.1}{50}$	$\frac{8.4}{25}$	5.3	$\frac{3.2}{20}$	$\frac{1.1}{40}$

509.15

8

+ 50

124

+ 50

123

122 + 50

T.P.

9.98

516.23

506.25

check to
Co. B.M. #8

10.65

495.04

495.01

T.P.

3.26

505.69

12.88

507.43

T.P.

9.06

515.31

2.90

506.25

122

50915

499.0	498.9	500.2	501.7	504.9	507.5	510.1
17.2	17.3	16.0	14.5		8.7	6.1
<u>50</u>	<u>40</u>	<u>38</u>	<u>25</u>	11.2	<u>20</u>	<u>40</u>

499.9	499.9	501.7	503.2	507.0	508.9	511.5
16.3	16.3	14.5	13.0		7.3	4.7
<u>55</u>	<u>47</u>	<u>45</u>	<u>25</u>	9.2	<u>20</u>	<u>40</u>

501.6	504.9	507.1	509.6	512.0
12.6	11.3		6.6	4.2
<u>50</u>	<u>25</u>	9.1	<u>20</u>	<u>40</u>

500.9	503.9	506.9	509.6	511.8
15.3	12.3		6.6	4.4
<u>50</u>	<u>25</u>	9.3	<u>20</u>	<u>40</u>

501.1	503.6	506.0	508.5	511.3
15.1	12.6		7.7	4.9
<u>50</u>	<u>25</u>	10.2	<u>20</u>	<u>40</u>

516.23

9

Top Iron Dial 110 LT 123 + 10

499.3	503.3	506.0	507.8	511.0
9.9	5.9		1.4	+1.8
<u>50</u>	<u>25</u>	3.2	<u>20</u>	<u>40</u>

50915

T.P. 421 511.8V 84V 507.41

128

+50

127

+50

126

+55.20 EC ON STUB

125

516.23

500.2	503.0	505.9	508.1	511.0
$\frac{16.0}{50}$	$\frac{13.4}{25}$	10.3	$\frac{8.1}{50}$	$\frac{5.2}{40}$

500.4	503.6	507.1	509.4	511.5
$\frac{15.8}{50}$	$\frac{12.0}{25}$	9.1	$\frac{6.6}{20}$	$\frac{4.7}{40}$

500.2	501.6	503.8	506.9	509.9	512.2
$\frac{16.0}{50}$	$\frac{14.6}{28}$	$\frac{12.4}{25}$	9.3	$\frac{6.3}{50}$	$\frac{4.0}{40}$

499.6	499.2	501.0	503.2	506.5	508.6	512.5
$\frac{16.6}{50}$	$\frac{17.0}{43}$	$\frac{15.2}{40}$	$\frac{13.0}{25}$	9.7	$\frac{7.6}{50}$	$\frac{3.7}{40}$

499.6	499.5	501.0	503.0	506.5	509.2	511.8
$\frac{16.6}{50}$	$\frac{16.7}{44}$	$\frac{15.2}{42}$	$\frac{13.2}{25}$	9.7	$\frac{6.9}{20}$	$\frac{4.4}{40}$

500.1	500.0	499.4	501.4	503.2	506.21	509.7	512.7
$\frac{16.1}{50}$	$\frac{16.2}{46}$	$\frac{14.8}{42}$	$\frac{12.8}{40}$	$\frac{13.0}{25}$	10.2	$\frac{6.5}{20}$	$\frac{3.5}{40}$

499.4	499.0	500.0	501.5	505.6	509.1	511.1
$\frac{16.8}{50}$	$\frac{17.2}{40}$	$\frac{16.2}{38}$	$\frac{14.7}{25}$	10.6	$\frac{7.1}{25}$	$\frac{5.1}{40}$

516.23

+50

131

+50

+25 Small Cult. 90°

130

+50

129

+50

511.82

499.4	501.3	504.2	507.2	509.5
$\frac{13.4}{50}$	$\frac{10.5}{25}$	7.6	$\frac{4.6}{20}$	$\frac{2.3}{40}$

498.6	500.6	503.8	506.2	509.2
$\frac{13.4}{50}$	$\frac{11.2}{25}$	8.0	$\frac{5.6}{20}$	$\frac{2.6}{40}$

495.4	497.6	499.8	502.2	505.7
$\frac{16.0}{50}$	$\frac{14.2}{25}$	12.0	$\frac{9.6}{20}$	$\frac{6.1}{40}$

495.5	498.5	500.3	502.2	504.0
$\frac{16.3}{50}$	$\frac{13.3}{25}$	11.5	$\frac{9.6}{20}$	$\frac{7.8}{40}$

496.5	498.4	500.9	502.8	504.9
$\frac{15.3}{50}$	$\frac{13.4}{25}$	10.9	$\frac{9.0}{20}$	$\frac{6.9}{40}$

498.1	500.4	503.9	506.5	508.8
$\frac{13.7}{50}$	$\frac{11.4}{25}$	7.9	$\frac{5.8}{20}$	$\frac{3.0}{40}$

498.6	501.3	504.6	507.3	510.4
$\frac{13.7}{50}$	$\frac{10.5}{25}$	7.4	$\frac{4.5}{20}$	$\frac{1.4}{40}$

499.1	502.1	505.6	508.4	511.3
$\frac{12.7}{50}$	$\frac{9.7}{25}$	6.7	$\frac{3.4}{20}$	$\frac{0.5}{40}$

511.82

+50

+25

small Culv.

90°

134

T.P.

90° 510.83 10.03 501.79

+50

133

+50

132

511.82

27

28

29

31

491.1	491.1	494.0	498.9	502.3	505.9
$\frac{19.7}{50}$	$\frac{19.7}{37}$	$\frac{16.8}{25}$	11.9	$\frac{8.5}{20}$	$\frac{4.9}{40}$

490.4	492.1	496.6	500.5	503.8
$\frac{20.4}{50}$	$\frac{18.7}{25}$	14.4	$\frac{19.3}{20}$	$\frac{7.0}{40}$

490.4	491.5	492.5	497.5	500.8	504.4
$\frac{20.4}{50}$	$\frac{19.3}{35}$	$\frac{18.3}{25}$	13.3	$\frac{10.0}{20}$	$\frac{4.4}{40}$

510.83

492.8	496.1	500.6	503.9	506.8
$\frac{19.0}{50}$	$\frac{15.7}{25}$	11.4	$\frac{8.5}{20}$	$\frac{5.0}{40}$

494.1	497.6	501.5	504.6	508.0
$\frac{17.7}{50}$	$\frac{14.2}{25}$	10.3	$\frac{7.2}{20}$	$\frac{3.8}{40}$

496.9	500.2	503.7	507.0	509.0
$\frac{14.9}{50}$	$\frac{11.6}{25}$	8.1	$\frac{4.8}{20}$	$\frac{2.8}{40}$

498.5	501.8	507.4	507.1	509.4
$\frac{13.3}{50}$	$\frac{10.0}{25}$	7.4	$\frac{4.7}{20}$	$\frac{2.4}{40}$

511.82

+50

138

+50

137

+50

136

+50

135

510.83

506.2	505.7	508.0	510.8	514.6	517.8	521.0
$\frac{4.6}{50}$	$\frac{5.1}{58}$	$\frac{2.8}{55}$	$\frac{0.0}{55}$	+3.8	$\frac{+7.0}{20}$	$\frac{+10.2}{20}$

504.2	503.2	505.7	509.3	512.3	515.7	518.8
$\frac{6.6}{50}$	$\frac{7.0}{38}$	$\frac{5.1}{36}$	$\frac{1.5}{20}$	+1.5	$\frac{+4.9}{20}$	$\frac{+8.0}{40}$

501.6	501.0	504.0	505.7	510.0	512.7	515.8
$\frac{9.2}{50}$	$\frac{9.8}{29}$	$\frac{6.8}{56}$	$\frac{5.1}{25}$	0.8	$\frac{+1.9}{20}$	$\frac{+5.0}{40}$

498.8	498.8	501.2	504.4	507.9	511.9	515.8
$\frac{12.0}{50}$	$\frac{12.0}{43}$	$\frac{9.6}{50}$	$\frac{6.4}{55}$	2.9	$\frac{+1.1}{20}$	$\frac{+2.0}{10}$

499.3	502.5	504.1	507.7	511.8	514.3
$\frac{11.5}{50}$	$\frac{8.3}{36}$	$\frac{6.7}{55}$	3.1	$\frac{+1.0}{20}$	$\frac{+3.5}{40}$

497.8	502.3	506.6	509.8	513.1
$\frac{13.0}{50}$	$\frac{8.5}{25}$	4.2	$\frac{1.0}{20}$	$\frac{+2.3}{40}$

495.7	500.9	504.7	508.0	511.6
$\frac{15.1}{50}$	$\frac{9.9}{25}$	4.1	$\frac{2.8}{20}$	$\frac{+0.8}{40}$

491.5	494.2	497.2	502.5	505.7	509.7
$\frac{19.3}{50}$	$\frac{16.6}{41}$	$\frac{13.6}{25}$	8.3	$\frac{5.1}{20}$	$\frac{1.1}{20}$

510.83

+50

145

+50

144

T.P. 12.66 539.14 236 526.48

+50

143

+50

528.84

515.1 521.9 524.6 527.4 527.1 529.7 534.0 537.3

$$\frac{24.0}{60} \quad \frac{17.2}{20} \quad \frac{14.5}{20} \quad \frac{11.7}{15} \quad 12.0 \quad \frac{9.1}{1} \quad \frac{5.1}{20} \quad \frac{1.8}{40}$$

508.8 518.4 522.4 525.3 524.8 525.1-527.8 531.3 534.7

$$\frac{30.3}{20} \quad \frac{20.7}{30} \quad \frac{16.7}{15} \quad \frac{13.8}{10} \quad 14.3 \quad \frac{14.0}{6} \quad \frac{11.3}{9} \quad \frac{7.8}{25} \quad \frac{4.7}{20}$$

499.0 503.1 513.4 519.8 522.8 523.2 525.8 531.0

$$\frac{40.1}{60} \quad \frac{36.0}{50} \quad \frac{25.7}{25} \quad \frac{19.3}{15} \quad 16.5 \quad \frac{15.9}{16} \quad \frac{13.3}{19} \quad \frac{8.1}{20}$$

487.8 493.6 499.0 510.7 518.8 523.0 524.7 524.7 527.9

$$\frac{51.3}{75} \quad \frac{45.5}{65} \quad \frac{40.1}{50} \quad \frac{28.4}{25} \quad 20.3 \quad \frac{16.1}{10} \quad \frac{16.4}{23} \quad \frac{14.4}{25} \quad \frac{11.2}{40}$$

539.14

✓ mark in fence post

497.3 503.2 511.3 517.7 522.3 521.8 524.7 527.4

$$\frac{31.5}{65} \quad \frac{25.6}{50} \quad \frac{17.5}{25} \quad 11.1 \quad \frac{6.5}{13} \quad \frac{7.0}{28} \quad \frac{4.1}{32} \quad \frac{1.6}{40}$$

495.8 500.6 507.6 514.9 517.8 520.2 520.1 522.4 524.4

$$\frac{33.0}{65} \quad \frac{22.2}{50} \quad \frac{21.0}{25} \quad 13.9 \quad \frac{11.0}{12} \quad \frac{8.4}{16} \quad \frac{8.7}{30} \quad \frac{6.4}{32} \quad \frac{4.4}{40}$$

495.3 501.4 508.5 514.6 519.8 519.6 521.7 523.5

$$\frac{33.5}{65} \quad \frac{27.4}{50} \quad \frac{20.3}{25} \quad 14.2 \quad \frac{9.0}{12} \quad \frac{9.2}{30} \quad \frac{7.1}{32} \quad \frac{5.3}{40}$$

528.84

+50

148

+50

T.P. 12.70 551.84 0.00 539.14

147

+90

+50

146

539.14

538.4 542.1 545.3 548.1 550.0

$\frac{13.4}{50}$ $\frac{9.7}{25}$ 65 $\frac{3.7}{24}$ 1.8

534.8 539.5 543.0 545.7 548.1

$\frac{17.0}{50}$ $\frac{12.3}{25}$ 8.8 $\frac{6.1}{20}$ $\frac{5.7}{20}$

529.1 529.3 534.0 535.1 539.6 542.8 546.0

$\frac{22.7}{50}$ $\frac{22.5}{45}$ $\frac{19.8}{42}$ $\frac{16.7}{25}$ 12.2 $\frac{9.0}{20}$ $\frac{5.8}{40}$

551.84

525.6 531.1 533.6 533.4 535.3 530.6 541.6 544.9

$\frac{13.5}{50}$ $\frac{8.0}{30}$ $\frac{5.5}{23}$ $\frac{5.7}{10}$ $\frac{3.8}{8}$ 1.5 $\frac{+2.5}{20}$ $\frac{+5.8}{40}$

515.5 516.4 533.9 533.5 535.9 536.8 540.9 544.6

$\frac{23.6}{50}$ $\frac{12.7}{30}$ $\frac{5.9}{22}$ $\frac{5.6}{7}$ $\frac{3.2}{5}$ 2.3 $\frac{+1.8}{20}$ $\frac{+5.5}{40}$

514.1 526.8 530.6 533.1 533.0 535.3 539.1 543.1

$\frac{25.0}{50}$ $\frac{12.3}{34}$ $\frac{8.5}{21}$ $\frac{6.0}{16}$ 6.0 $\frac{3.8}{5}$ $\frac{0.0}{20}$ $\frac{+4.0}{40}$

520.3 525.6 528.6 530.6 530.0 532.4 536.4 540.1

$\frac{18.8}{50}$ $\frac{13.5}{30}$ $\frac{10.5}{19}$ $\frac{8.5}{16}$ 9.1 $\frac{6.7}{1}$ $\frac{2.7}{20}$ $\frac{+1.0}{40}$

539.14

750

T.P. 0.45 527.88 12.07 524.73

151

0.55 539.40 538.85 T.P.
check to B.M. #10 5.54 544.82 544.81
T.P. 11.51 550.30 12.99 538.85

750

150

750

149

551.84

515.5 515.6 517.6 518.7 520.7 522.6 526.4
 $\frac{11.9}{50}$ $\frac{11.8}{50}$ $\frac{9.8}{50}$ $\frac{8.7}{35}$ 4.7 $\frac{4.8}{20}$ $\frac{1.0}{20}$

527.38

526.0 527.9 530.2 531.8 533.8
 $\frac{13.4}{50}$ $\frac{11.5}{35}$ 9.2 $\frac{7.6}{20}$ $\frac{5.0}{40}$

539.40

12' 27" 0.4 149.400? 55' P.P. iron pin #750 P.S.

532.8 535.2 537.6 539.7 541.7
 $\frac{19.0}{50}$ $\frac{16.6}{25}$ 14.2 $\frac{11.9}{20}$ $\frac{10.1}{40}$

537.3 540.5 543.6 545.8 547.4
 $\frac{14.5}{50}$ $\frac{11.3}{35}$ 8.2 $\frac{6.0}{20}$ $\frac{4.4}{40}$

538.8 542.8 546.1 548.4 550.6
 $\frac{13.0}{50}$ $\frac{9.0}{25}$ 5.7 $\frac{3.4}{20}$ $\frac{1.2}{40}$

539.3 543.4 546.3 548.7 550.7
 $\frac{12.5}{50}$ $\frac{8.4}{25}$ 5.5 $\frac{3.1}{20}$ $\frac{1.1}{40}$

551.84

152

+50

153

152 + 77.07 BC LT.

put in small culv.

+50

+25

152

+75

527.38

510.4	514.6	518.7	522.0	524.4	527.3	525.5		
$\frac{17.0}{5.0}$	$\frac{12.8}{2.5}$	8.7	$\frac{5.2}{1.8}$	$\frac{3.0}{2.3}$	$\frac{4.1}{3.8}$	$\frac{1.9}{2.0}$		
507.6	512.0	516.2	519.7	522.1	521.9			
$\frac{19.8}{5.0}$	$\frac{15.4}{2.5}$	11.2	$\frac{7.7}{2.0}$	$\frac{5.3}{2.7}$	$\frac{5.5}{4.0}$			
502.5	506.6	510.3	514.2	517.2	519.2			
$\frac{24.9}{5.0}$	$\frac{20.8}{2.5}$	17.1	$\frac{13.2}{2.0}$	$\frac{10.2}{3.4}$	$\frac{8.2}{7.0}$			
502.5	504.7	509.2	512.4	517.4				
$\frac{24.9}{5.0}$	$\frac{22.7}{2.5}$	18.7	$\frac{15.0}{2.0}$	$\frac{10.0}{4.0}$				
503.4	506.4	510.2	513.2	516.1	516.4			
$\frac{24.0}{5.0}$	$\frac{21.0}{2.5}$	17.2	$\frac{14.2}{2.0}$	$\frac{11.3}{3.0}$	$\frac{11.0}{4.0}$			
506.8	508.6	512.4	515.8	515.6	517.4	518.4		
$\frac{22.0}{5.0}$	$\frac{18.8}{2.5}$	15.0	$\frac{11.6}{1.3}$	$\frac{11.8}{3.0}$	$\frac{10.0}{3.1}$	$\frac{9.0}{2.0}$		
509.0	509.4	510.8	515.4	514.9	515.5	516.9	518.8	521.4
$\frac{18.4}{5.0}$	$\frac{18.0}{4.2}$	$\frac{16.6}{2.0}$	$\frac{12.0}{1.2}$	12.5	$\frac{11.9}{1.2}$	$\frac{10.5}{1.3}$	$\frac{8.6}{2.5}$	$\frac{6.0}{4.0}$
512.0	515.0	514.8	516.0	516.7	520.0	523.7		
$\frac{15.4}{5.0}$	$\frac{13.4}{3.2}$	$\frac{12.4}{1.7}$	$\frac{11.4}{1.5}$	10.7	$\frac{7.4}{2.0}$	$\frac{3.7}{4.0}$		
						527.38		

527.38

161

160 + 79.04 B.C. 4Y.

ON STUB

T.P. 0.45 518.83 12.28 518.28

+50

160

+50

159

158 + 50

T.P. 5.16 530.66 7.97 525.50
533.47

498.6	502.9	507.4	512.2	516.0
$\frac{20.2}{50}$	$\frac{15.9}{25}$	11.4	$\frac{4.6}{20}$	$\frac{2.8}{40}$

500.5	505.1	509.57	513.8	518.0
$\frac{18.3}{50}$	$\frac{13.7}{25}$	9.26	$\frac{5.0}{20}$	$\frac{0.8}{40}$

518.83
2

503.7	508.3	513.8	517.8	520.5	522.1
$\frac{27.0}{50}$	$\frac{22.4}{25}$	16.9	$\frac{12.9}{20}$	$\frac{10.7}{27}$	$\frac{8.0}{42}$

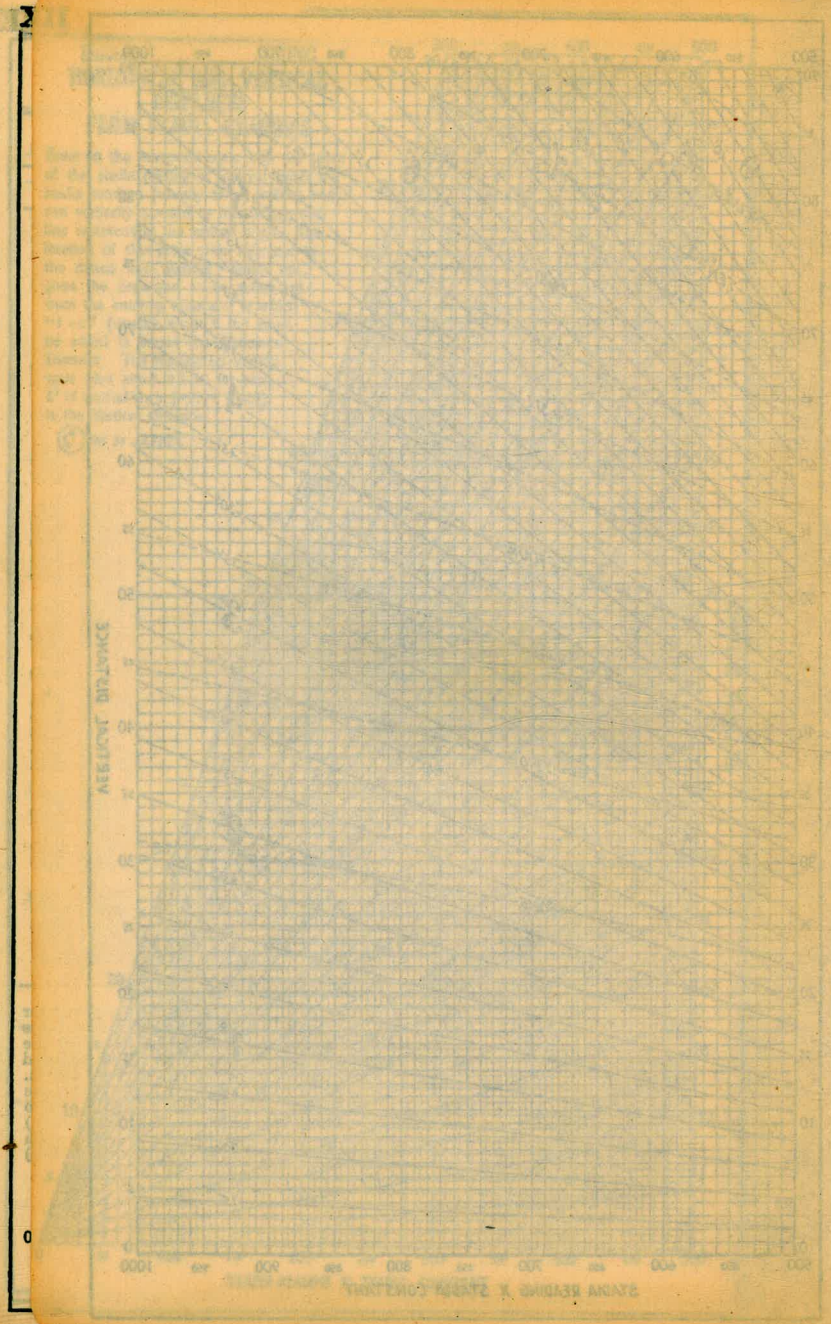
510.7	516.4	521.3	523.4	524.8	525.8	525.7
$\frac{20.0}{50}$	$\frac{14.3}{25}$	10.4	$\frac{7.3}{20}$	$\frac{5.9}{32}$	$\frac{4.9}{26}$	$\frac{5.0}{40}$

518.1	522.2	525.4	527.8	528.7	528.5
$\frac{12.6}{50}$	$\frac{8.5}{25}$	5.3	$\frac{2.9}{27}$	$\frac{2.0}{20}$	$\frac{2.7}{20}$

520.4	523.9	526.0	528.4	530.1	529.9
$\frac{10.3}{50}$	$\frac{6.8}{25}$	4.7	$\frac{2.3}{20}$	$\frac{0.6}{30}$	$\frac{0.8}{40}$

519.4	521.9	525.2	527.9	530.3	530.3
$\frac{11.3}{50}$	$\frac{8.8}{25}$	5.5	$\frac{2.8}{20}$	$\frac{0.4}{32}$	$\frac{0.4}{40}$

530.66
2



$99 + 93.76$
 $99 + 47.38$

 46.38

4.2977
 2148.60

 180
 54

491.82 = Co. assmd. el. of B.M.
 31.03 CORRECTION
 522.85 = U.S.G.S. 5076
2724

502.2 USGS

501.97 = 155' Contour. (to be run out)
 USGS

499.55 = 150' " (existing)
 USGS

88+36.26 B.C.Rt
 4+98.79
 93+34.53

120+55.46
 115+67.3
 488.16

31
 30+12.06
 87.94
 192-44
 96-22

206.26
 103+13.00
 66
 40

179-60
 141-46
 38-14

6.8755
 50
 343.7750
 34
 43

8625
 500000
 206.31
 41.05
 165.26
 3 65
 35.90

DISTANCES FROM CENTER OF ROADWAY FOR
 CROSS-SECTIONING.
 Roadway 16 feet wide. Side Slopes 1 on 1 1/2
 For Single Track Embankment.

88+36.26
 86+35.68
 200.58

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.