

1561

CHOLLAS  
VALLEY

SEWERS

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on 1½ see inside of back cover.

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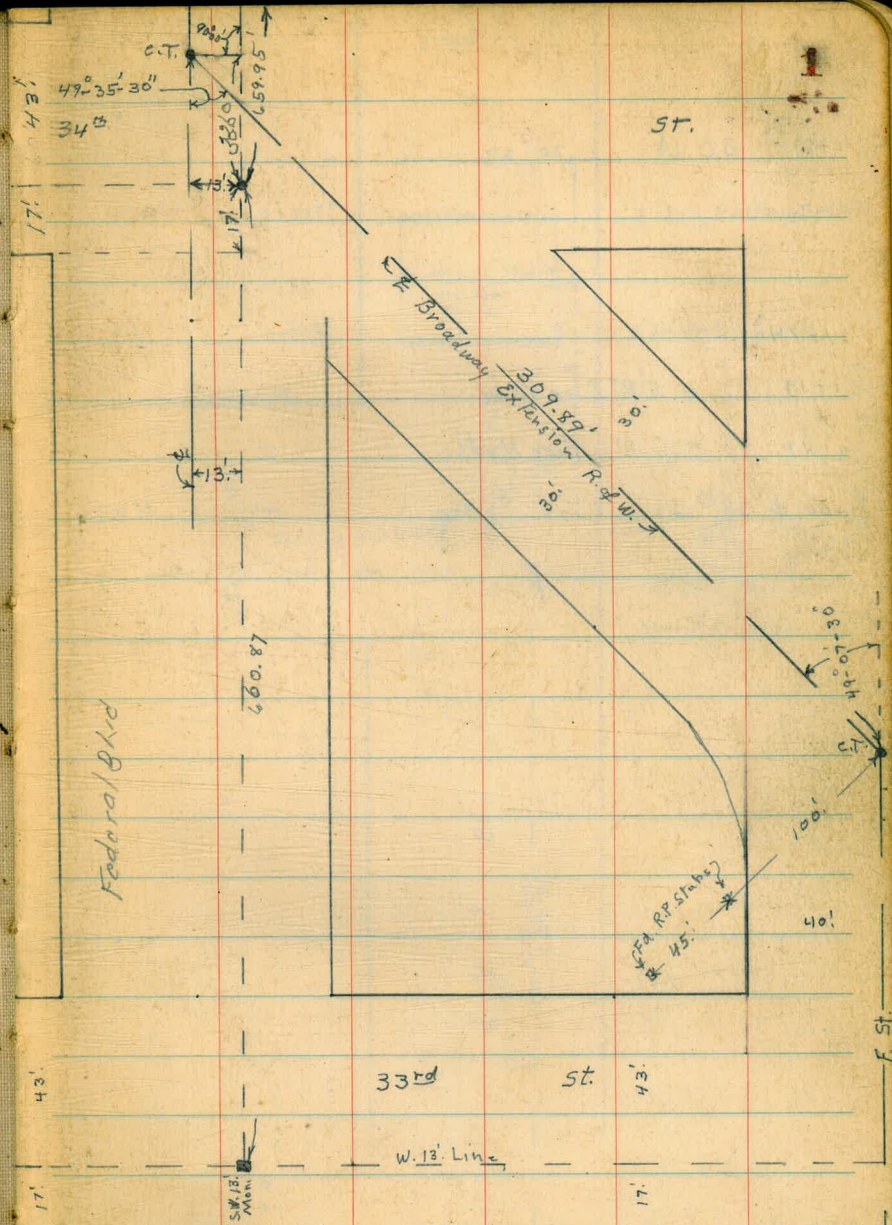
# 1561

ENGINEERING DEPARTMENT,  
CITY OF SAN DIEGO,  
CALIFORNIA.

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface and is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.

Prelim. Sewers. from 35<sup>th</sup> & Lemon Grove Ave  
N. Ely to Home Ave thence N. Ely to Home Ave.



2+89<sup>3</sup> B.C. Lt.  $\angle 30^{\circ}-30'$

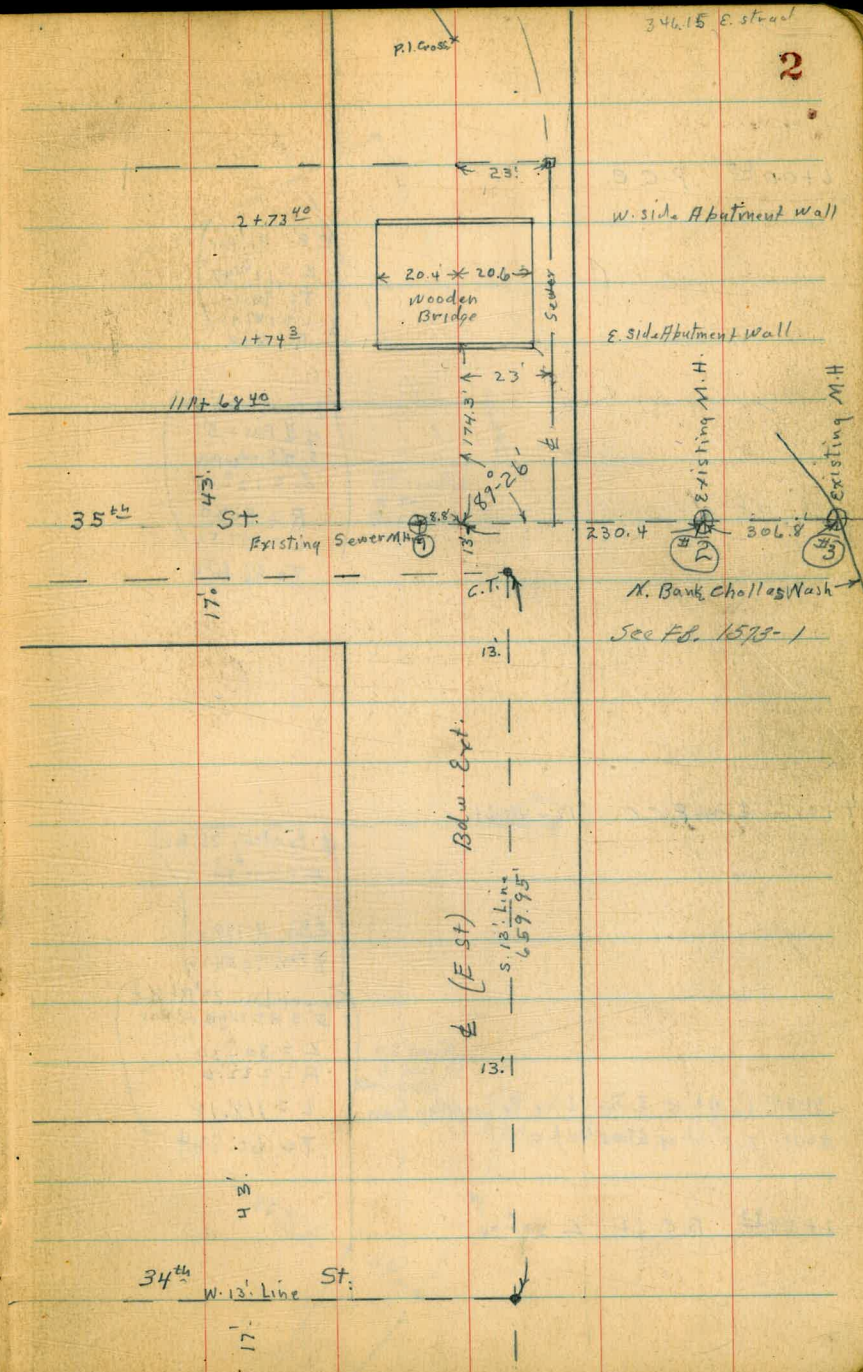
2+73.40

1+74<sup>3</sup>

1+19 4.5' RT Elec Pole

0+40 3.5' RT Fire Hydr.

0+00  $\phi$  35" St



6+00<sup>55</sup> P.C.E.

± 27 36. Par  
L = 12° 47'  
T = 94.10  
L = 147.40  
R = 84°

± Sewer 23' Rt  
of Pav = 5'  
S. of S. edge pav  
L = 12° 47'  
R = 863.0  
L = 192.54  
T = 96.674

4+08.11 ± Sewer P.C.C. 12° 47' Lt.

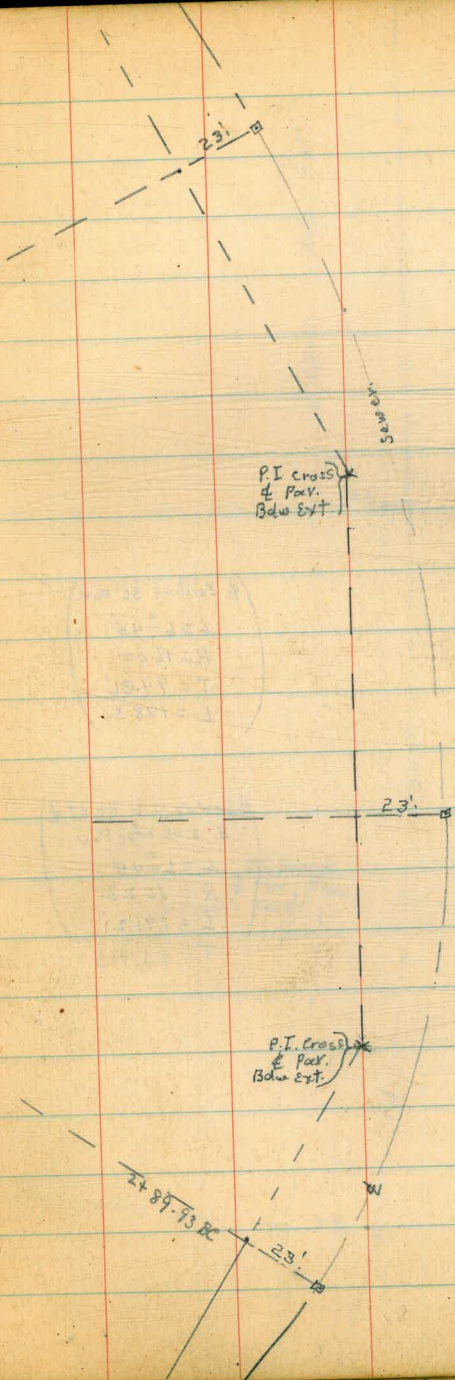
± Existing 36. Par  
L = 30° 30'

± Pav. R = 199.00  
± Pav. T = 54.26

Sewer Line 23' Rt of Pav  
= 5' S. of S. edge of Pav  
L = 30° 30'  
R = 222.0  
L = 118.18  
T = 60.524

3+35 1' Rt of S. Tan Elec Co Dead Man Guy.  
3+11 3.5' Rt of S. Tan Elec Light Pole

2+89<sup>23</sup> B.C. Lt. L 30° 30'



+50

9

+50

8+00

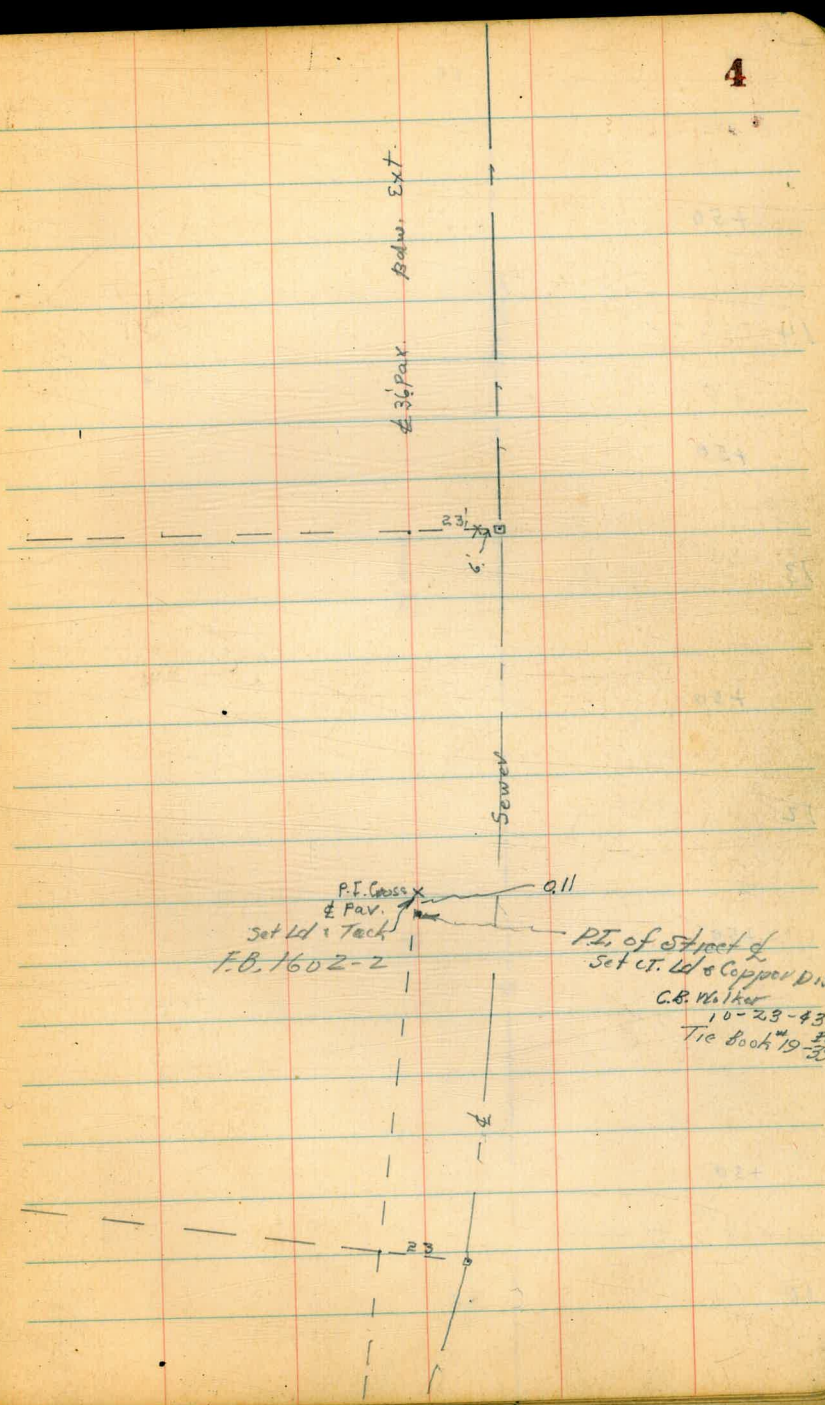
7+91.86 E.C.

Existing 36" Pav.  
 $L = 6.45'$   
 $R = 16.00'$   
 $T = 94.36'$   
 $L = 188.50'$

Sewer 23" Rt. of  $\phi$   
 = 5' s. of edge Pav.  
 $L = 6.45'$   
 $R = 16.23'$   
 $L = 191.21'$   
 $T = 95.713'$

7+00.65 P.C.C.

4



+50

14

+50

13

+50

12

+50

11

+50

10

23

5

Sewer

36' PLY

4

4

23

+50

18

+50

17

16+55<sup>13</sup>

E.C.

(Imp. Map.  
L = 20° 16' 47"

(Ex. 36' Pav  
L = 20° 22'  
R = 562.43  
T = 101.03  
L = 199.93

(Sewer 25' Rt.  
up of Pav = 5'  
Rt. of E. Edge  
L = 20° 22'  
R = 539.43  
L = 191.75  
T = 96.897

14+63<sup>38</sup>

B.C Rt

36' Pav Bd w. Ext

23

6

4

SEWER

23

P.I. Cross  
E Pav

Set Ld + CT  
FB 1602-2

23

23



+50

23

+50

22

+50

21

+50

20

+50

19

36' Pav

Sewer

4 Bldg. Ext.

4

+50

26

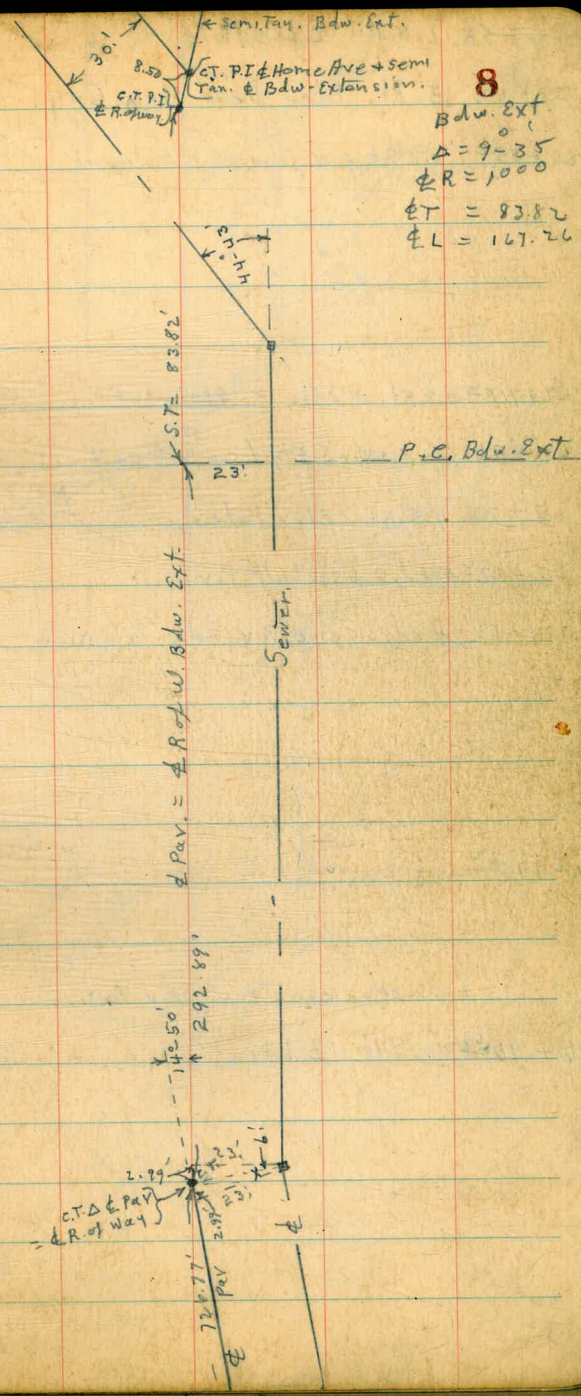
+50

25

+50

24

23+78<sup>90</sup>  $\angle 14-56$  RT.  
Sewer



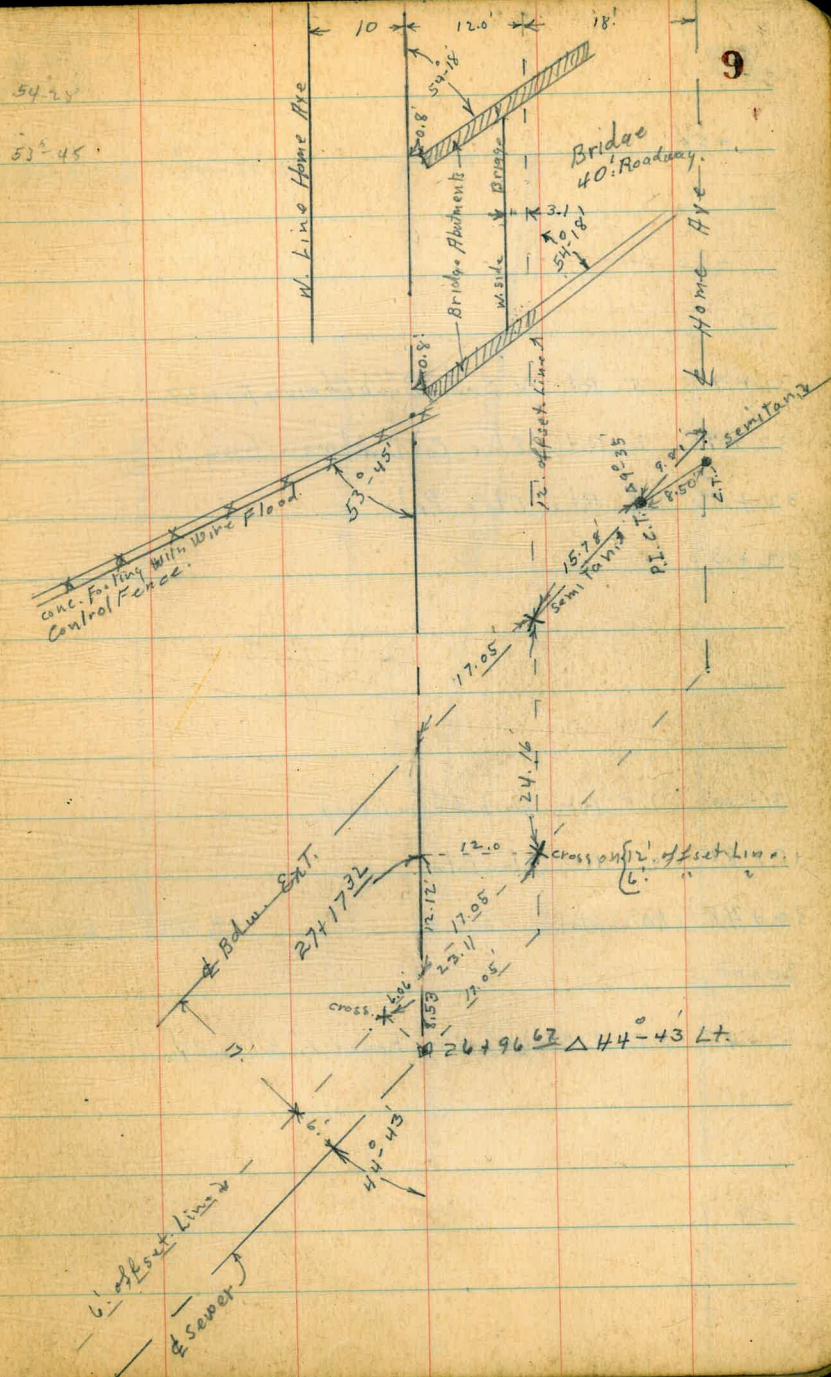
28+75 2.5 RT. Elee Pole  
28+62 3' RT. Elee Dead Man Gulch  
28+55<sup>1/2</sup> 0.8 RT = N. Edge N. Abutment

27+79<sup>1/2</sup> 0.8 RT. N. edge S. Abutment.  
27+76 Conc. & Wire Flood control Wall  
27+75 4.5 RT. Elee Pole  
27+62<sup>1/2</sup> N. edge asphalt. Pav  
27+53 N. edge cone. Pav Bdw. Extension

27+17.32

27+03 ± = S. edge cone Pav. Bdw. Ext.

26+96<sup>1/2</sup>  $\Delta 44^\circ-43'$  LT.



35

+50

34

+50

33

32+95 5' RT. N End. Barbed wire Fence

32+95 2' RT Elec Co Dredman Guy

32+86 2' RT. Elec Pole

32+50

32

31+00 1.5' RT. Barbed wire Fence

30+80 2.5 RT. Elec Pole

30+78 Pot. stub

30+00

29+45 S. End. Barbed wire Fence 1' to Lt. of

+50

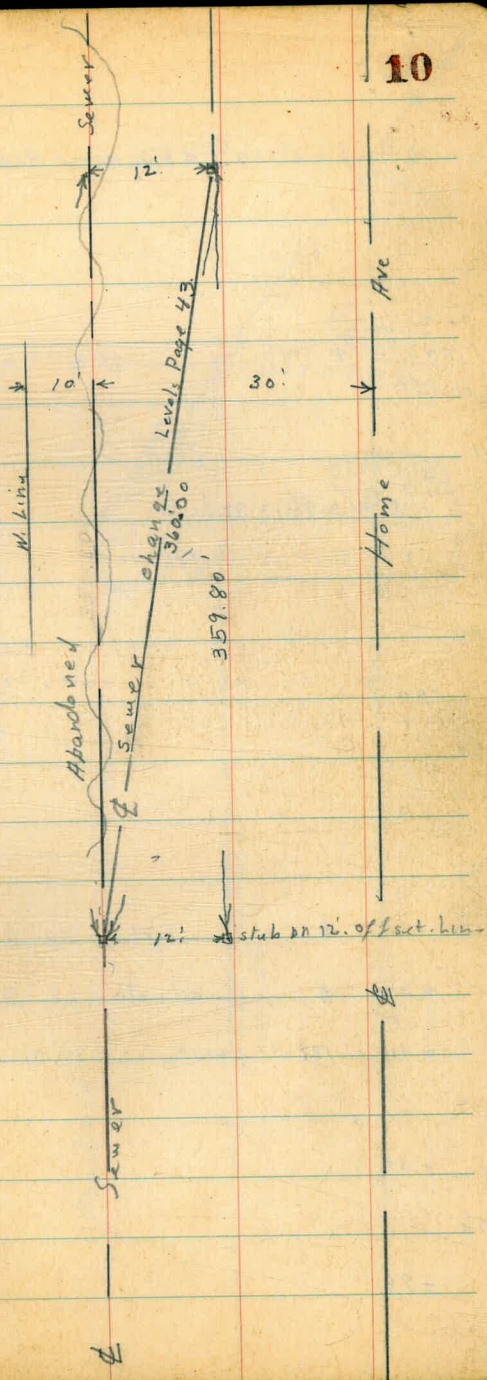
29

change

change  
In d. sewer  
11-16-38

34+08 Δ 1-54-30 Lt.

30+48 Δ 1-54-30 Rt



42 + 56<sup>26</sup>  $\phi$  = 79 + 60<sup>72</sup>  $\phi$  E.C. Home Ave.

42

+ 43.62 O.K.  
+ 43.88  $\phi$  Stub

41

OK + 48.70  
N.G. 96  
+ 48.96  $\Delta$  9°-13' RT.

{ + 48.96 stub 12' Rt. of Sewer }  
original line

40

50

39

50

38

+ 39  $\phi$  Eucalyptus 30" Diam.

+ 34  $\phi$  Eucalyptus 18" Diam.

+ 11 12' Lt Eucalyptus 30" Diam.

37

+ 50

36

+ 50

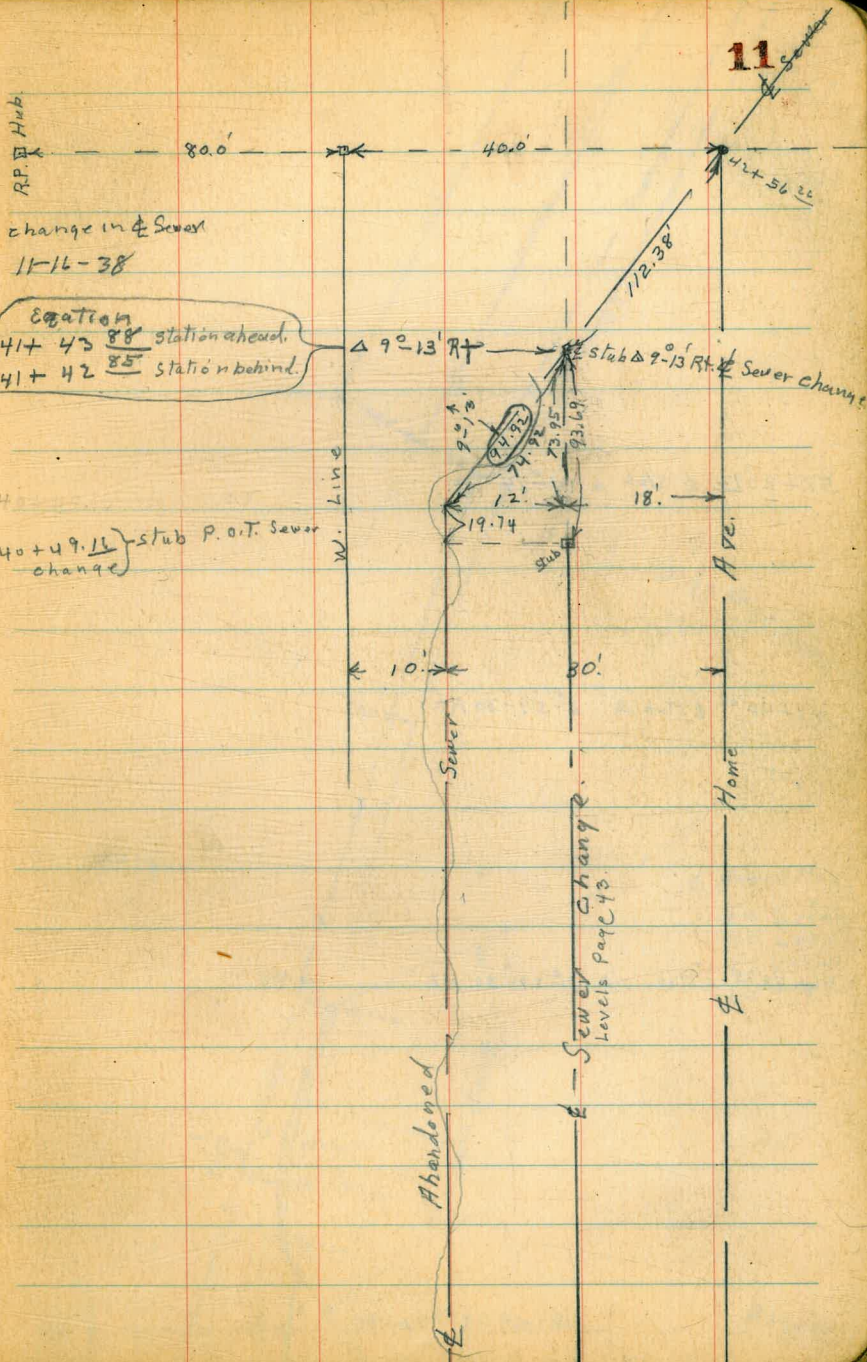
Change  $\phi$

R.P. Hub

change in  $\phi$  Sewer  
11-16-38

Station  
41 + 43<sup>88</sup> station ahead.  
41 + 42<sup>85</sup> station behind.

40 + 49.11 } stub P.O.T. Sewer  
change

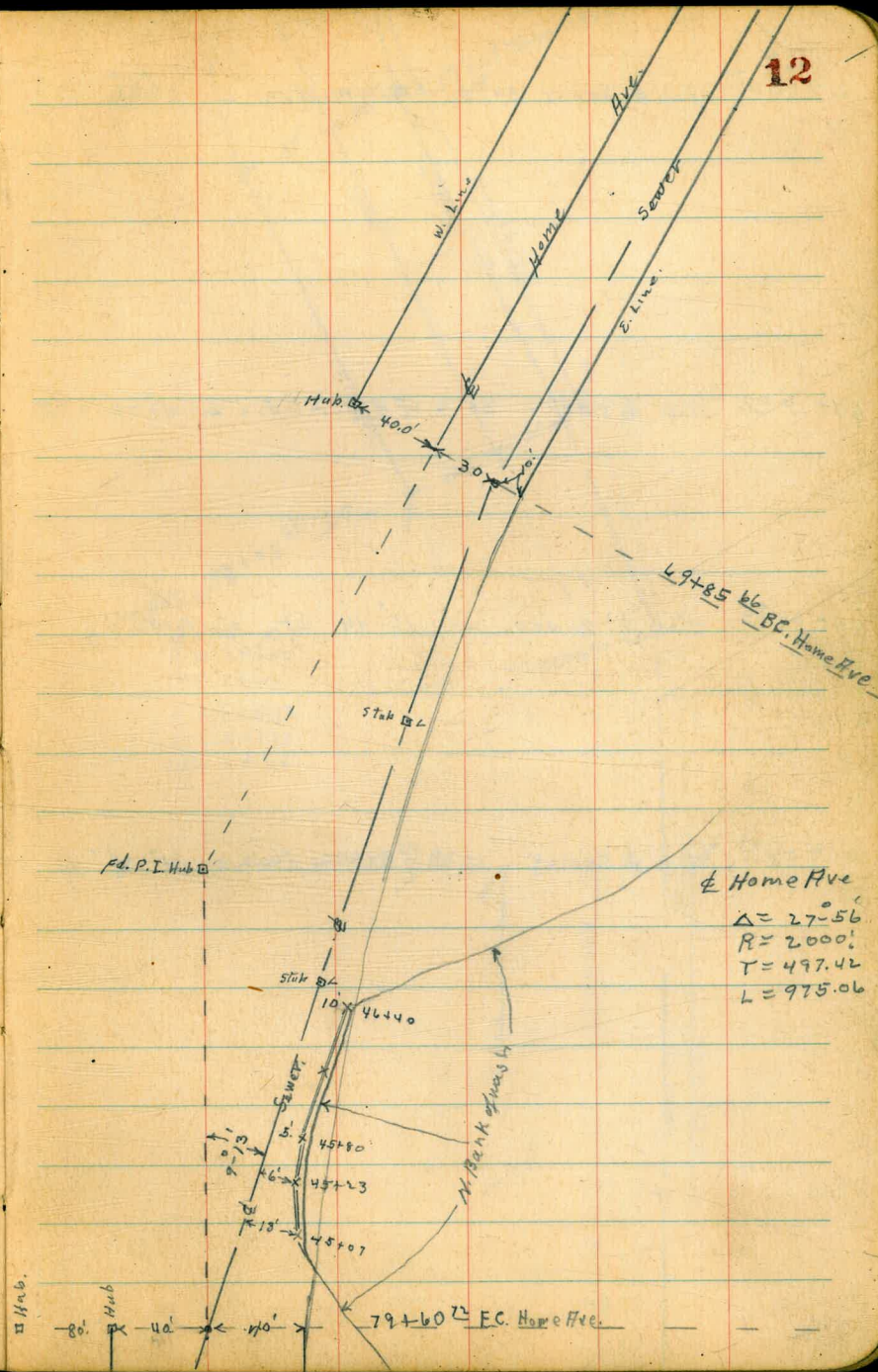


52+2092 ± Stub Δ 4°-14' RT.

49+4006 ± Stub Δ 6°-59'-30" RT.

46+4824 ± Stub. Δ 7°-29'-30" RT.

42+5625



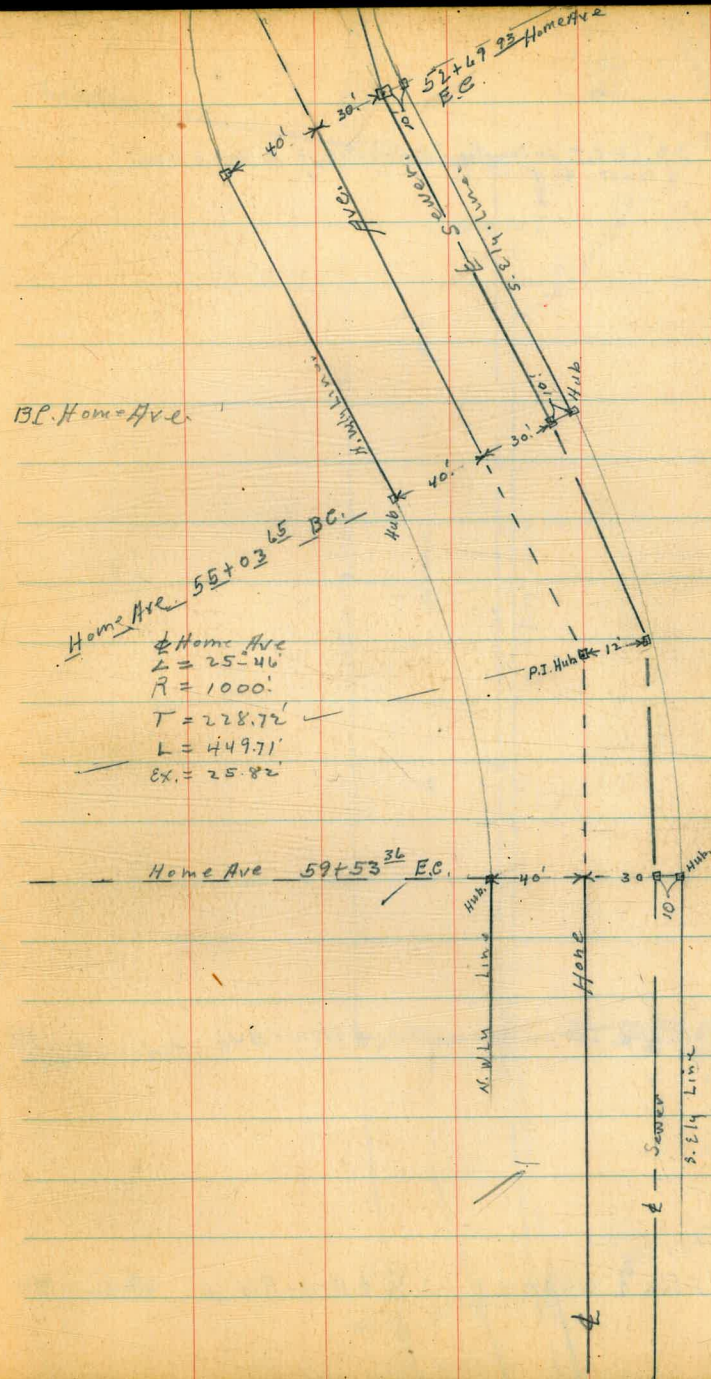
69+50<sup>79</sup> stub & sewer 30' s. of & Home Ave  $\angle$  6-41' Rt.

67+17<sup>92</sup> stub & sewer 30' s. of & Home Ave  $\angle$  4-31' Lt.

64+84<sup>95</sup> stub & sewer  $\angle$  16-44' Lt. cts Curve

62+52<sup>93</sup> stub & sewer 30' s. of & Home Ave  $\angle$  4-31' Lt

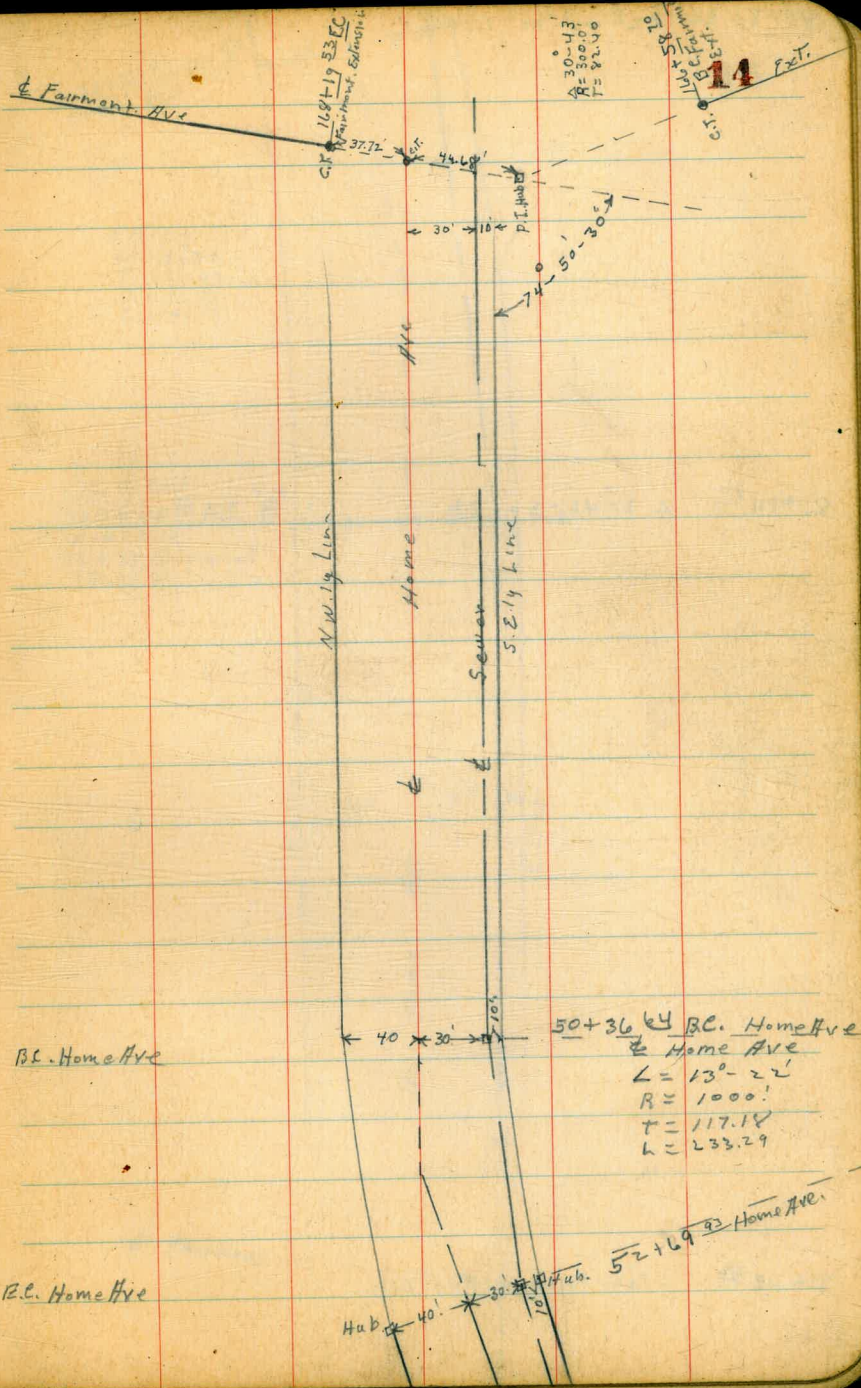
13



81+57<sup>35</sup> 30' Lt. c.t. on Semitan Fairmont Ext & Home Ave  
 81+49<sup>22</sup> & sewer. " " " " " "

71+76<sup>57</sup> stub & sewer 30' S.E.ly & Home Ave  $\angle$  6°-41' Rt.

69+50<sup>29</sup> stub & sewer 30' S.E.ly & Home Ave  $\angle$  6°-41' Rt.



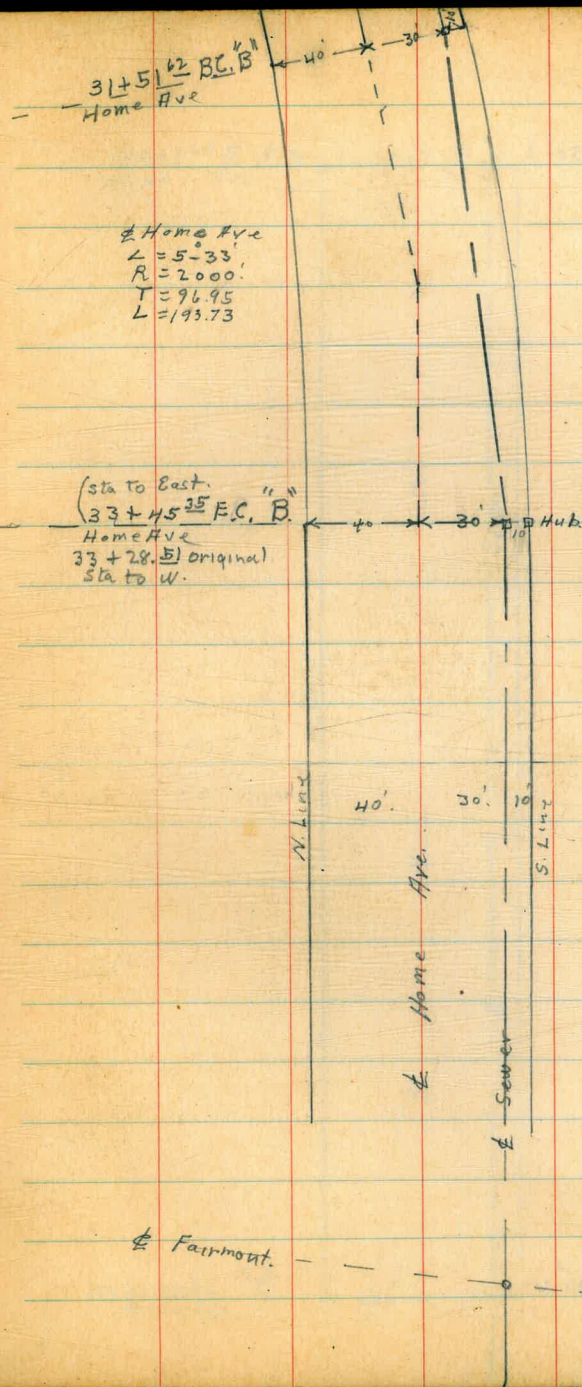


90+81 <sup>24</sup>  $\angle 2^{\circ} 46' - 30''$  Lt.

88+84 <sup>70</sup>  $\angle 2^{\circ} 46' - 30''$  Lt.

81+49 <sup>22</sup> S. Tan. Fairmont Ave Ext.

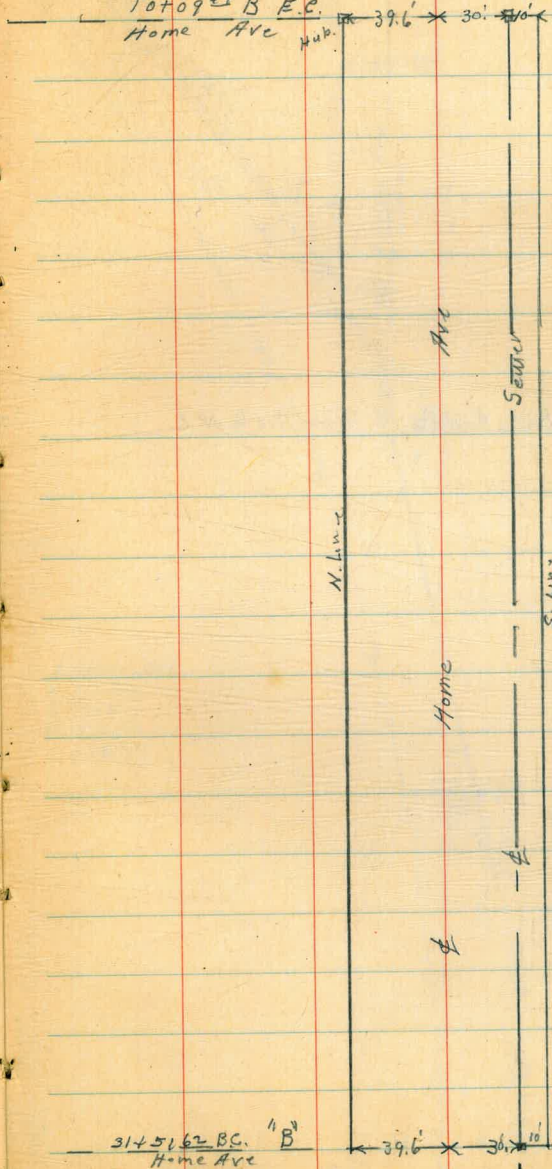
15



112+23<sup>22</sup> 30' s. of  $\frac{1}{2}$  Home Ave

90+81<sup>24</sup>  $\angle 2-46-30$  Lt.

10+09<sup>24</sup> "B" E.C.  
Home Ave Pub.





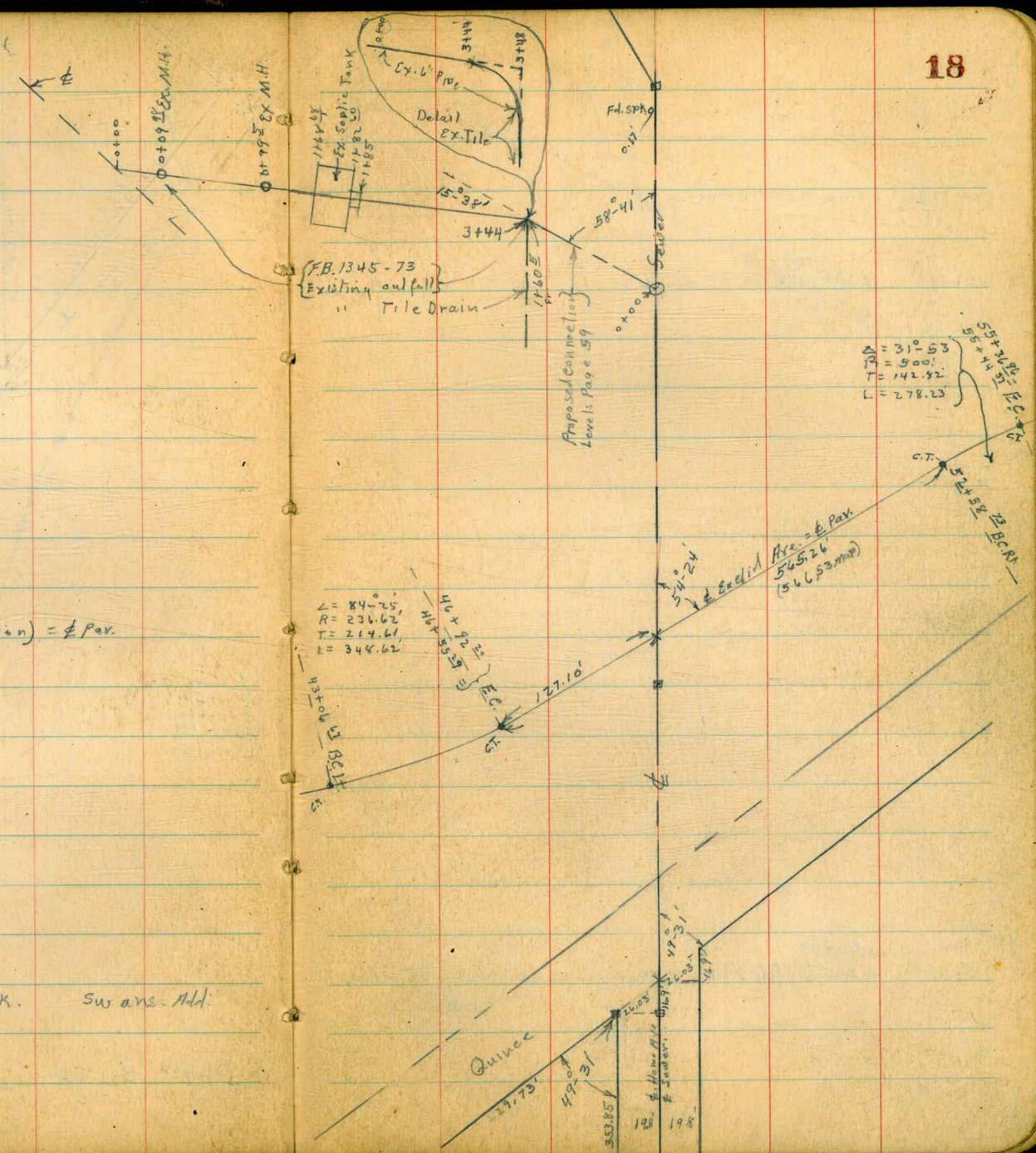
131+35<sup>14</sup> Δ stub & M.H. 39  
131+25<sup>13</sup> 41/2" x 4" Fd. spk. Rumseys. Δ

127+52<sup>14</sup> M.H. 38

121+42<sup>14</sup> cross. of 60' st. (Euclid Ave Extension) = & Par.

121+24 & stub P.O.T.

120+22<sup>03</sup> P.I. s. Line Quince st.  
120+05<sup>13</sup> stub of Rt. C to Mon NE. cor. BIK. Sur ans. Ad.



$L = 84.25$   
 $R = 236.62$   
 $T = 214.61$   
 $E = 344.62$

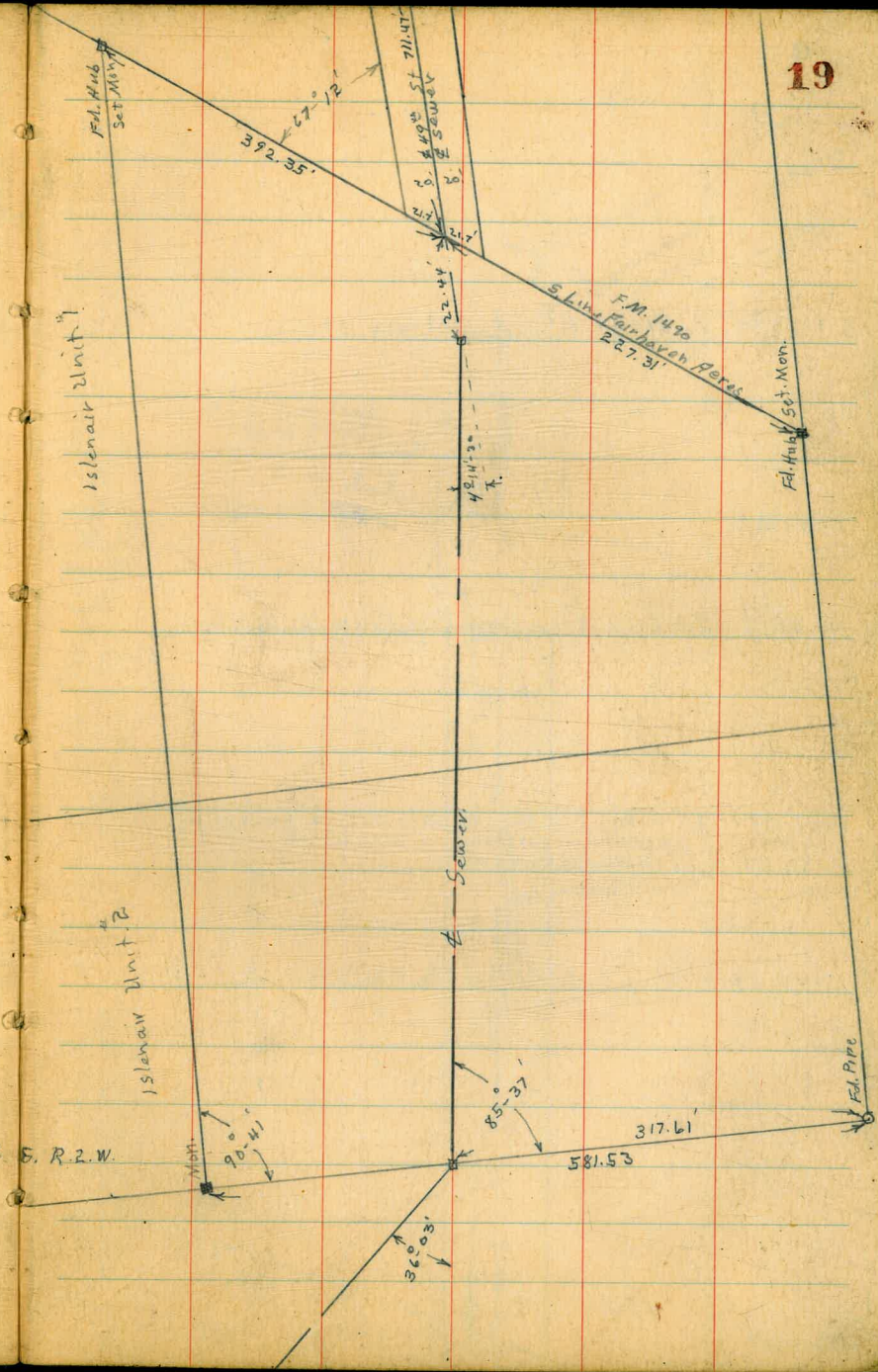
$\Delta = 31.53$   
 $T = 500.$   
 $E = 142.82$   
 $L = 278.23$

Area = & Par.  
 $565.26$   
 $(566.53 \text{ m}^2)$

142+37.10 S. Line Fairhaven Acres.

142+14<sup>66</sup> ± stub  $\angle$  4-14-30" Lt

131+35<sup>14</sup>  $36^{\circ}03'$  Lt.  
 $\triangle$  stub E. P.I. S. Line N. 15 Acres. of S.W.  $\frac{1}{4}$  of N.E.  $\frac{1}{4}$  of sec 33, T.16 S. R.2.W.



155+12<sup>83</sup>

151+62<sup>71</sup>  $\angle$  37'-47" Rt.  $\perp$  Ontario St.

150+58<sup>5</sup>

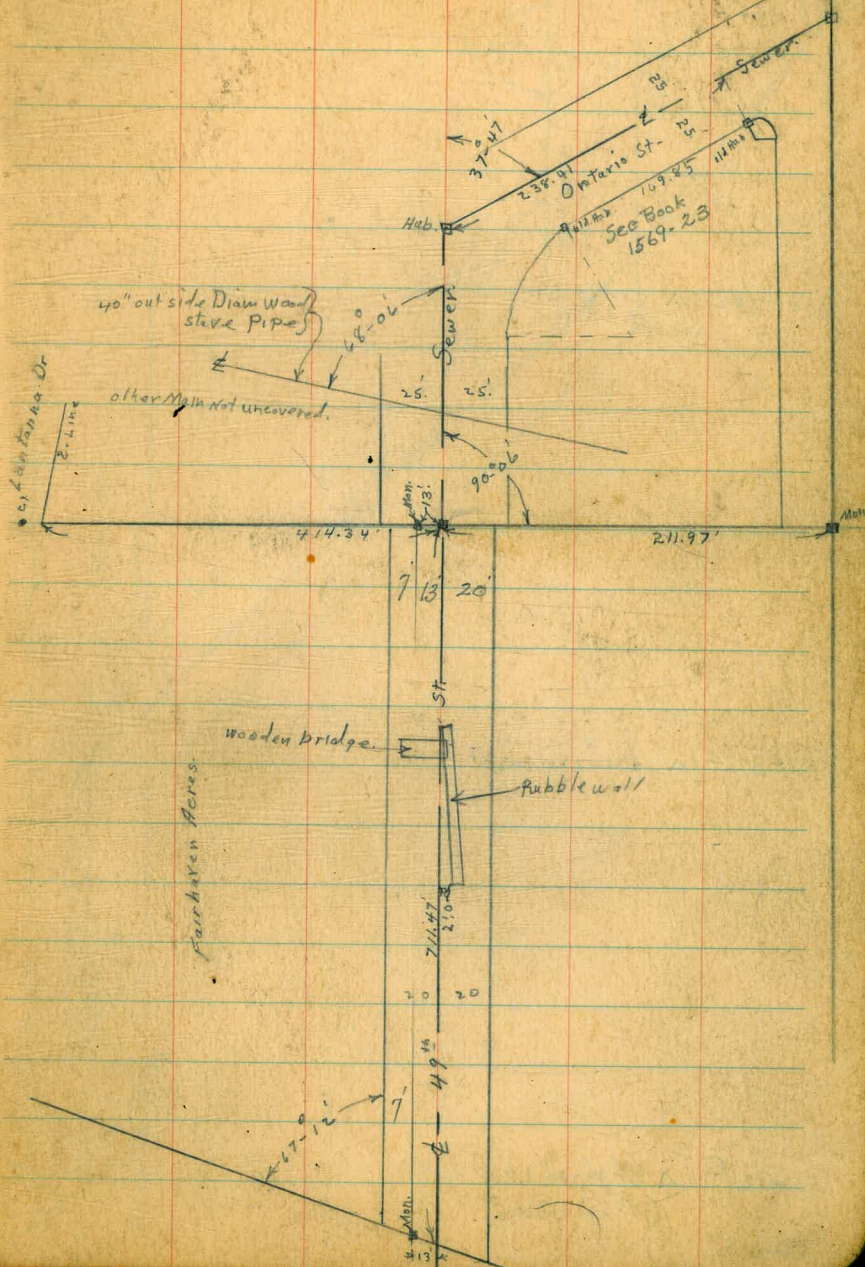
149+48<sup>57</sup> P.O.T. N. Line Fairhaven Acres.

145+38  $\perp$  - W. Face N. End Rubble wall  $\perp$  Bank of wash  
145+31 N side wooden bridge  
145+23 S side wooden bridge

144+54  $\perp$  Rt. - S. End Rubble wall  $\perp$  bank of wash

142+37<sup>10</sup>

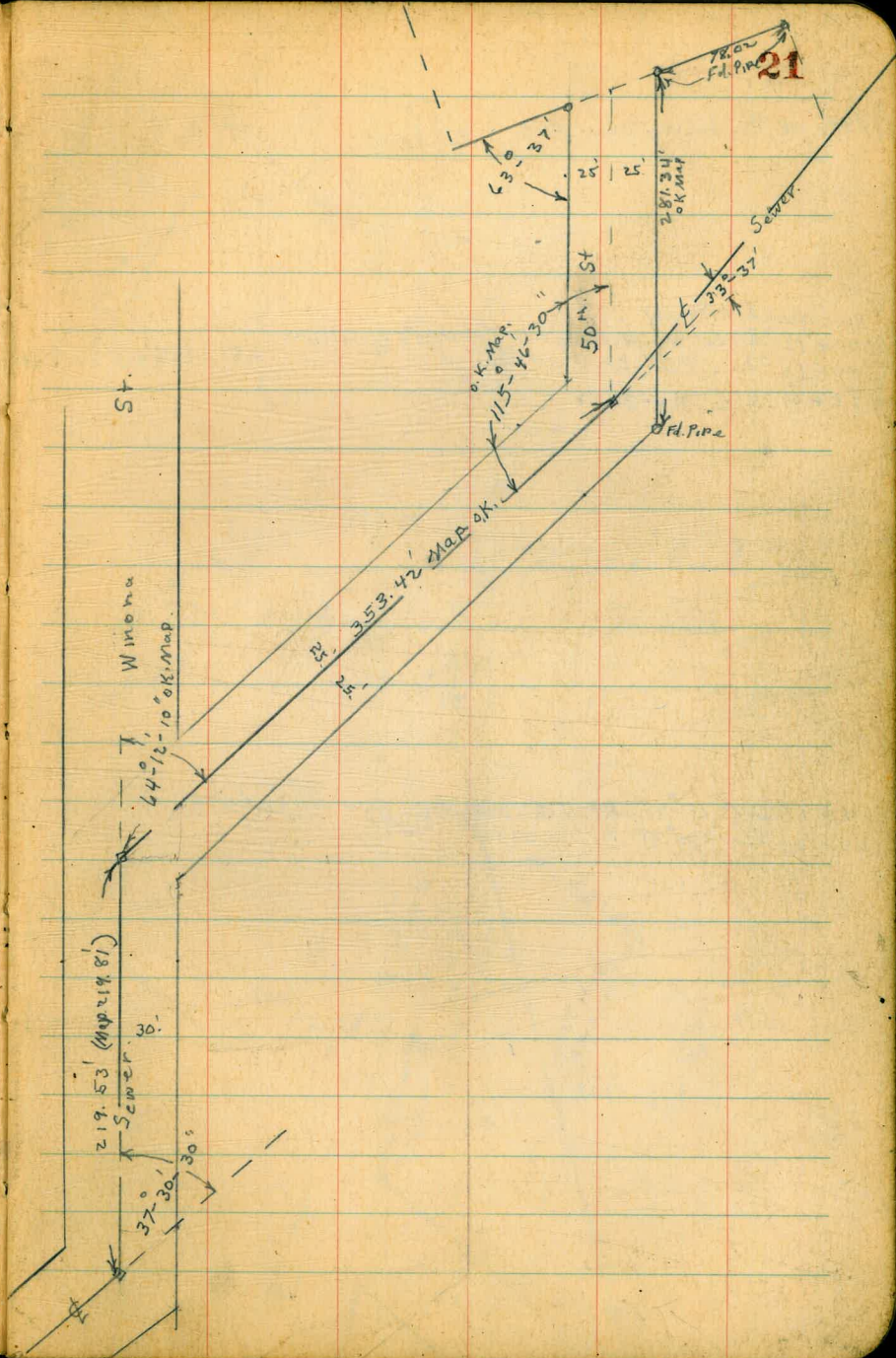
20



160+85.78  $\Delta$  33°-37' Lt  
o.k. Plans.

157+32.36  $\Delta$  64°-12'-10" Rt

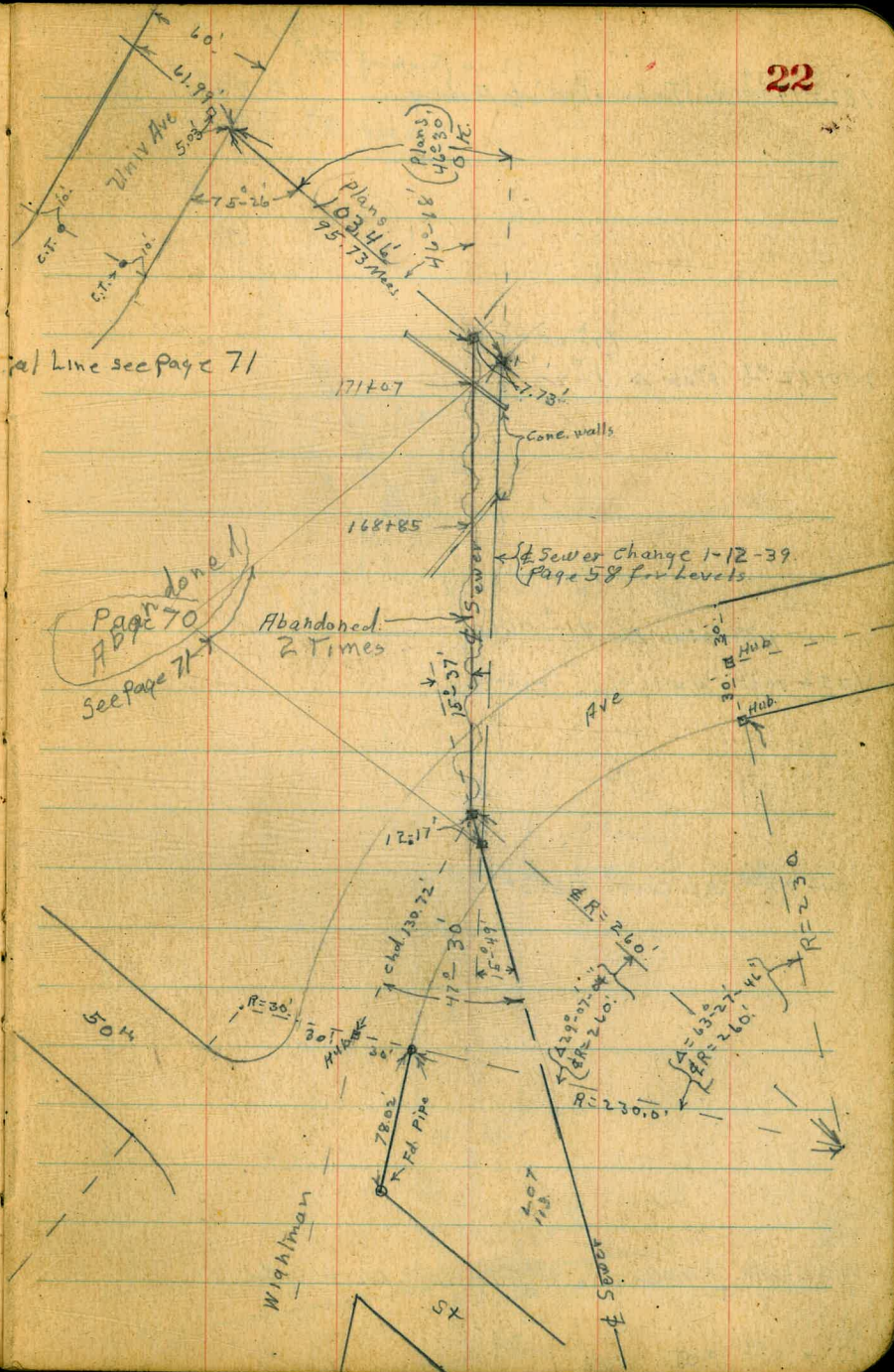
155+12.83  $\Delta$  37°-30'-30" Lt.  
(37°-29'-40" Map)



17240871 S. Line Univ. Ave

Use ahead. original  
(171+12.98  $\Delta$  46-18.4 = P.O.T. change) Equation  
(171+15.09 P.O.T. change  
171+0736  $\Delta$  46-30.14. — } = 171+16.13 Final Line see page 71

164+97.51  $\Delta$  15-37' RT.  $\ominus$  Wightman Ave Abandoned.  
164+84.83  $\Delta$  15-49' RT change





182+94<sup>39</sup> Nail Top Fence Post } (S. Line Fairmont Add)  
 } Δ 59°-17' RT  
 } Alley

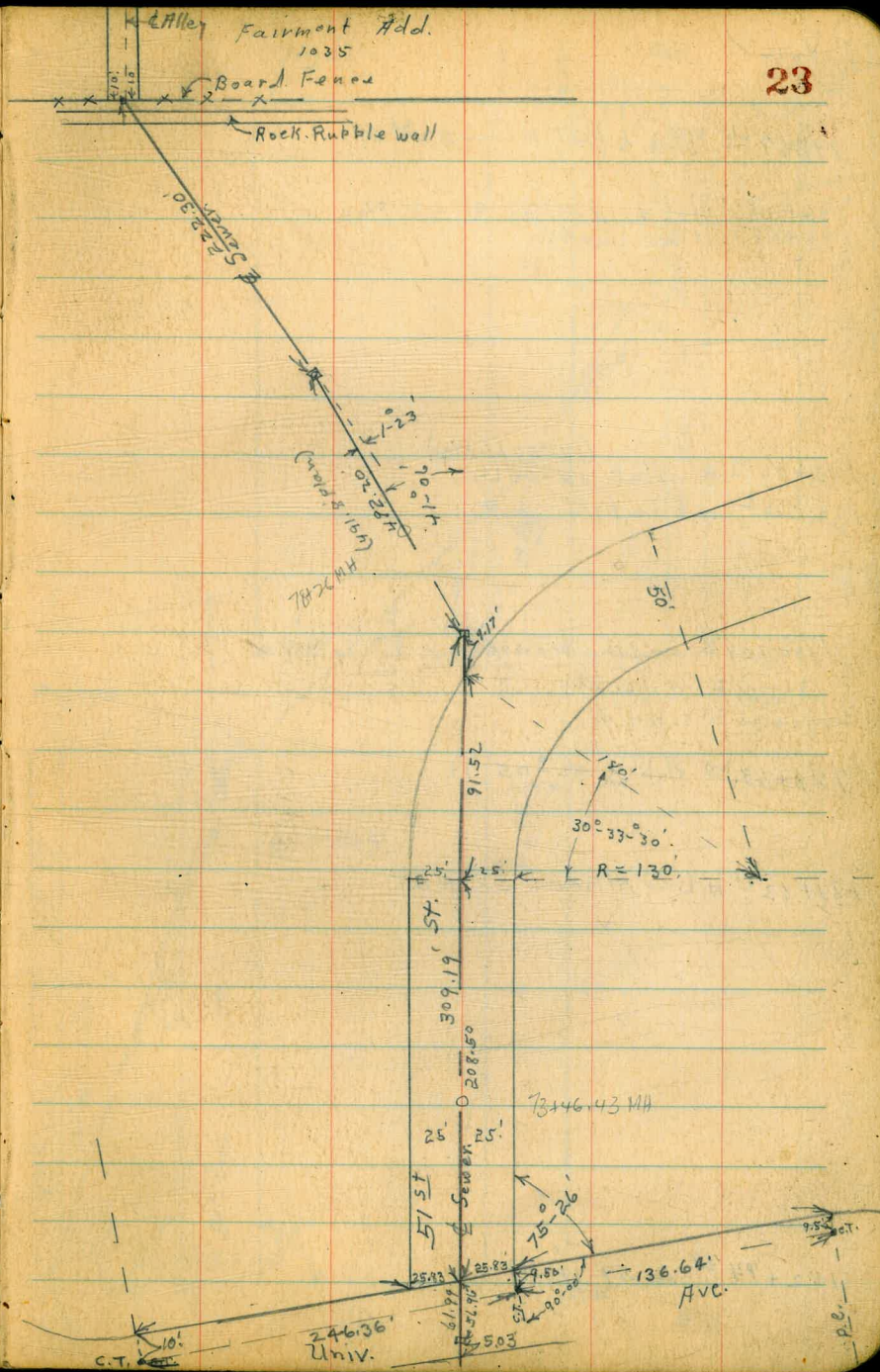
(12-25' Plan)  
 180+72<sup>09</sup> stub Δ 1°-23' Lt.

(41°-08' Plan)  
 175+79<sup>89</sup> stub Δ 41°-06' Lt.  
 175+70<sup>22</sup> N.W. ly line 51<sup>st</sup> St.

174+79<sup>20</sup> B.C. Curve 51<sup>st</sup> St.

172+70<sup>72</sup> N. Line Univ. Ave P.O.T. Cross. in Pav.

172+13<sup>74</sup> P.O.T. stub



197769 <sup>66</sup> stub  $\triangle$  P.O.T. W. Line 52<sup>nd</sup> St.

196+28<sup>27</sup> stub  $\triangle$   $41^{\circ}55'$  Rt.  $\triangle$  O.K. Plan  
 196 to 87<sup>6</sup> stub W. Line Alley

193+06<sup>59</sup>  $\triangle$  stub  $17^{\circ}50'$  Lt. Plan  
 $18^{\circ}00'$  Lt.  
 192+26<sup>67</sup> W. Line 51<sup>st</sup>

190+29<sup>44</sup> = N. Line Orange Ave

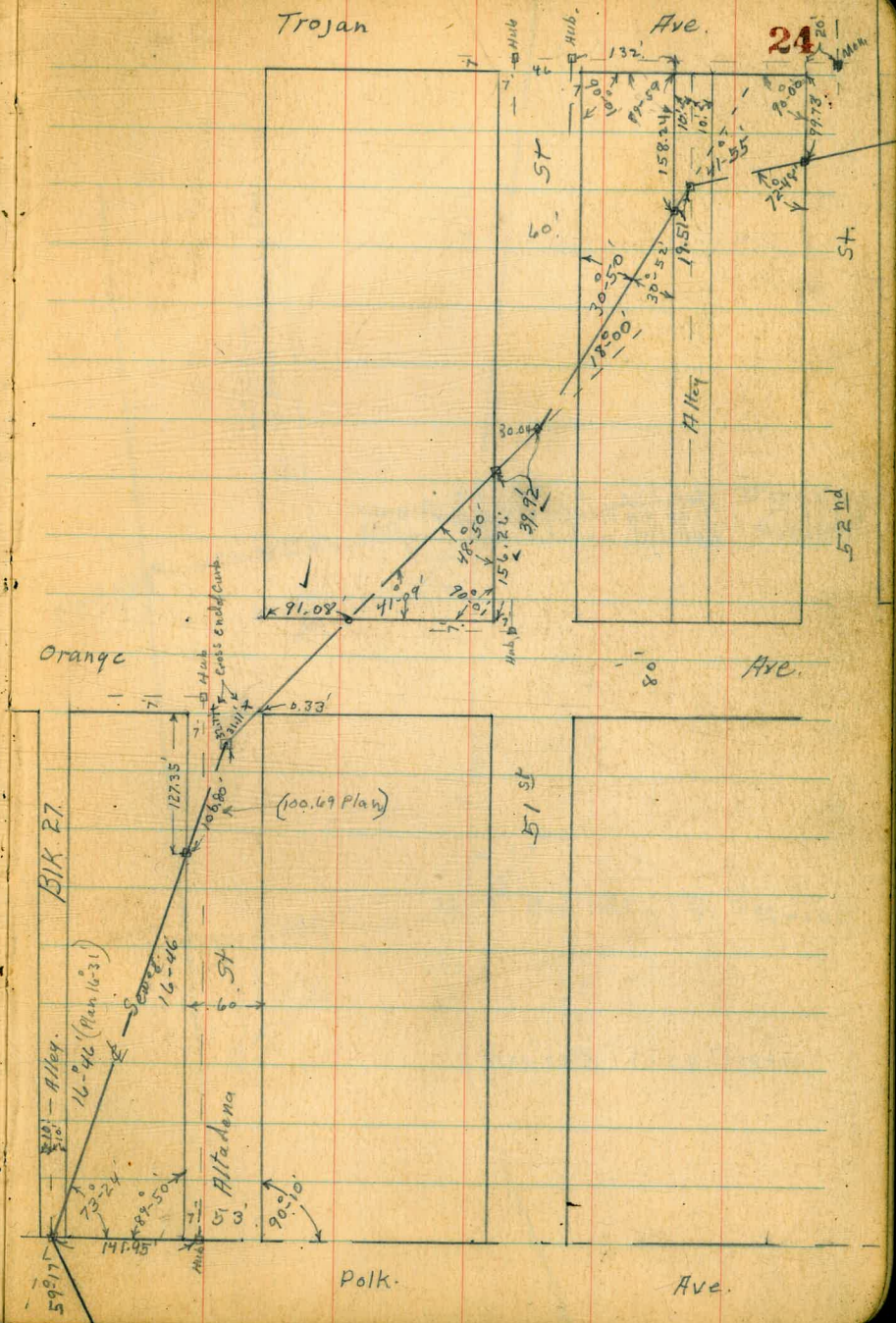
190+06<sup>7</sup> N. conc'd

189+30<sup>30</sup> S. conc'd.

188+69.40 stub  $\triangle$   $32^{\circ}05'$  Rt.  
 O.K. Plan

187+62<sup>40</sup> W. Line Altadena St. P.O.T.

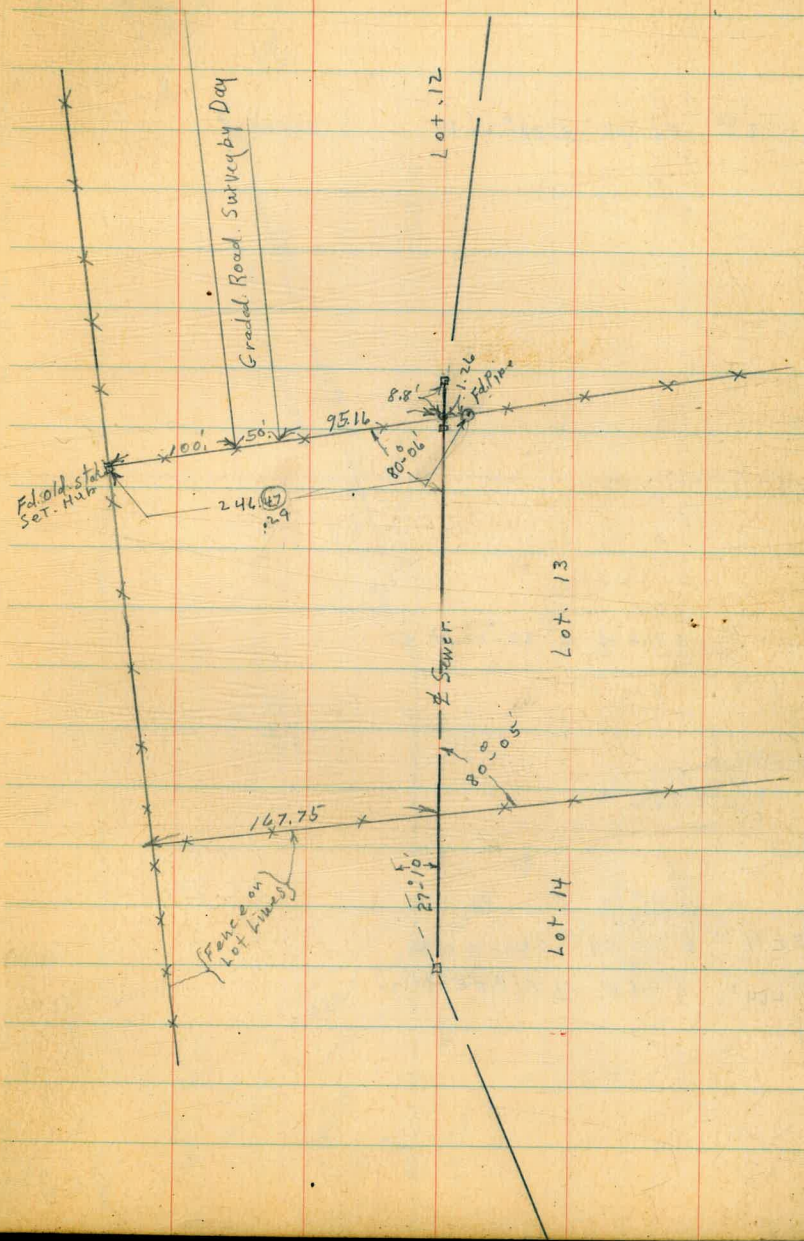
182+94<sup>39</sup>  $\triangle$   $59^{\circ}17'$  Rt.  
 O.K. Plan.



207+42<sup>96</sup> Hub.  $\angle 5^{\circ}30'$  RT.  
 207+37<sup>14</sup> i. RT = N. side Cypress Tree 30" Diam  
 207+34<sup>14</sup> Hub. Pot. on Lot Line

202+72<sup>57</sup> Lot Line bet. Lots 14 & 13

201+83<sup>57</sup>  $\phi$  stub  $\angle 27^{\circ}18' RT$

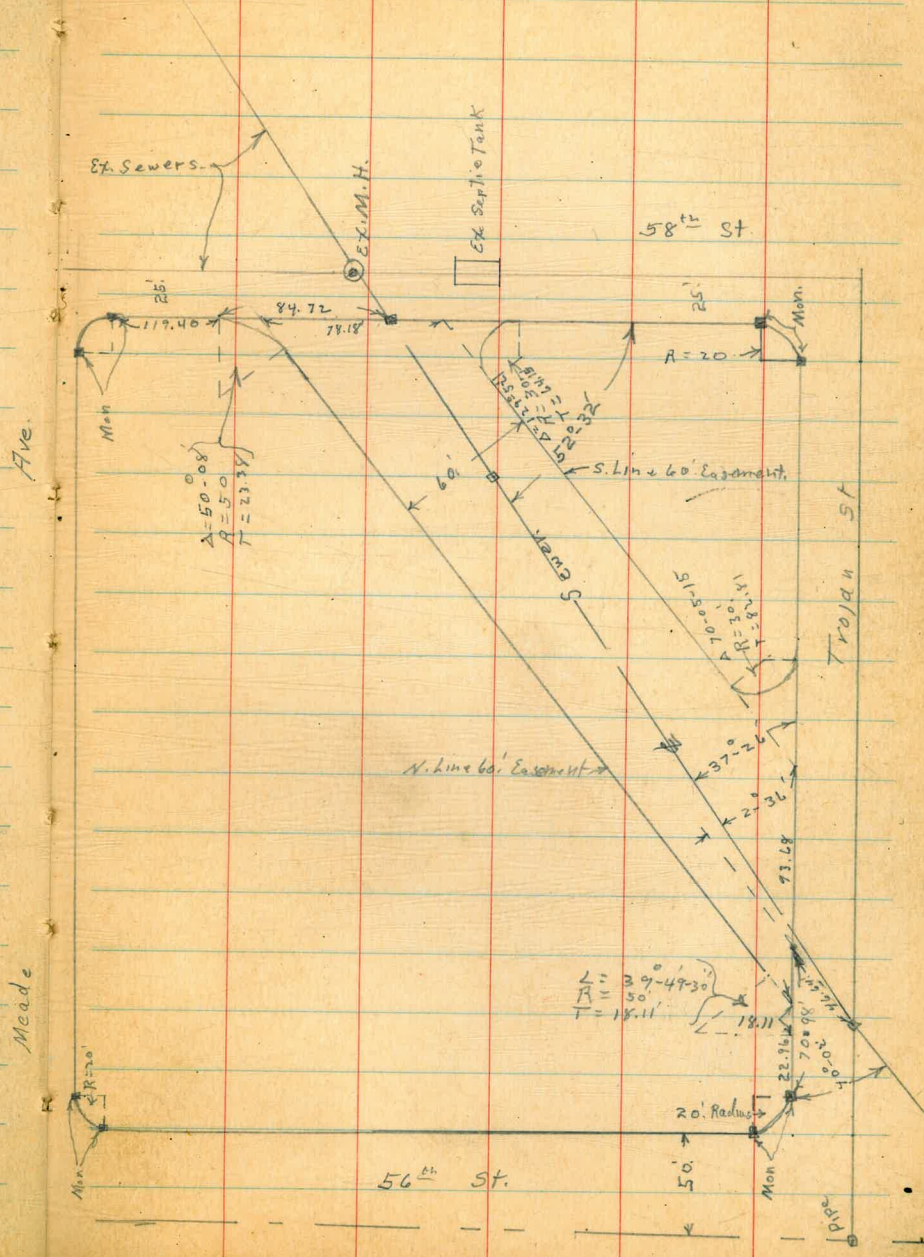




234+23<sup>3</sup> Ex. M.H.  
 233+91<sup>62</sup> P.O.T. W. Line 58<sup>th</sup> St.

232+20 & stab P.O.T.

227+24<sup>56</sup> & Hub  $\angle 2^{\circ}36'$  RT.







10-31-38 Levels on Prelim Sewer in Bdw.  
Extension from 35<sup>th</sup> to Home Ave.  
in Home Ave from Bdw Extension

To Euclid

BM. B.P.	0.82	52.69	51.87	N.W. 35 <sup>th</sup> + 8 <sup>th</sup> (Bdw. Ext.) Federal Blvd.
M.H. (1)	35 <sup>th</sup> + 8.8 N of Bdw Ext.	0.88	51.81	Top.
" " " "	" " " " "			Top. sealed in
" " " "	" " " " "			F.L.
M.H. (2)	35 <sup>th</sup> + 230.4 S. of Bdw Ext.	5.65	47.04	Top.
" " " "	" " " " "	15.85	36.84	F.L.
M.H. (3)	33 <sup>rd</sup> + 306.8 S. of M.H. (2)	12.25	40.44	Top.
" " " "	" " " " "	18.79	33.90	F.L.

BM	7.18	59.05	51.87	30
0+00 = 35 <sup>th</sup> St	on pav.	8.03	51.02	
+50		7.50	51.5	
+50	2' RT =	Top. d.	6.90	52.15
1+00		pav	6.57	52.48
1+00	2' RT	Top. d.	5.97	53.08
1+50	" "	" "	5.10	53.95 2 incl.
1+50		pav	5.64	53.41
1+60 <sup>9</sup>	Face of curb	pav	5.50	53.55
2+61	" " "	Top. d.	5.04	54.01
1+74 <sup>3</sup>	Top. E. Face W. Bridge Abutment		5.20	53.85
1+74 <sup>3</sup>	Bed of wash.		16.8	42.3
1+74 <sup>3</sup>	Bridge Deck.		5.00	54.00
2+00		wash	16.7	42.4
2+50		wash	17.8	41.3
2+67		wash	16.0	43.1
2+68	Top. Conc. Footing		14.2	44.9
2+74 <sup>4</sup>	{ W. face E. Abutment		14.2	44.9
2+74 <sup>4</sup>	Top " " " "		4.75	54.30
2+74 <sup>4</sup>	Bridge decks		4.55	54.50



		59.05		
2+89 <sup>23</sup>	BC Lt. $\phi$ Sewer	4.3	54.8	
"	5' Lt = S Pav.	4.81	54.24	
3+50	" " " "	4.45	54.60	
3+50	$\phi$ Sewer	4.4	54.7	
4+08 <sup>"</sup>	" " " " P.C.C.	4.24	54.81	$\phi$ stub
4+08 <sup>"</sup>	5' Lt. = S. Pav. P.C.C.	4.05	55.00	
4+50	" " " "	3.77	55.28	
4+50	$\phi$	3.7	55.4	
5+00	$\phi$	3.5	55.6	
5+00	5' Lt S. Pav	3.38	55.67	
5+50	" " " "	3.14	55.91	
5+50	$\phi$	3.1	56.0	
6+00	$\phi$	1.7	57.4	
6+00	5' Lt. = S. Pav. P.C.C.	2.95	56.10	
+50	" " " "	2.72	56.33	
+50	$\phi$	2.6	56.5	
7+00	"	2.5	56.6	
7+00	5' Lt. = S. Pav	2.50	56.55	
+50	" " " "	2.23	56.82	
+50	$\phi$	1.8	57.3	
8+00	"	1.8	57.3	

		59.05		
8+00	5' Lt. S. edge pav.	1.90	57.15	31
T.P.X in Pav. 6' Lt of 7+91 <sup>24</sup> EC.		6.27	63.39	1.93
8+50	$\phi$ Sewer	6.3	57.1	
8+50	5' Lt = Pav	6.04	57.35	
9+00	" " "	5.60	57.79	
9+00	$\phi$	5.7	57.7	
9+50	"	5.2	58.2	
9+50	5' Lt = pav	5.28	58.11	
10+00	" " "	4.92	58.47	
10+00	$\phi$	4.8	58.6	
10+50	"	4.4	59.0	
10+50	5' Lt = pav	4.58	58.81	
11+00	" " "	4.20	59.19	
11+00	$\phi$	4.1	59.3	
11+50	$\phi$	4.0	59.4	
11+50	5' Lt. pav	3.90	59.49	
12+00	" " "	3.53	59.86	
12+00	$\phi$	3.8	58.6	
12+03	5.5 ft of $\phi$ sewer = 5' Lt. End 18" Con. Iron Pipe Culvert Inlet. Rt. to Pav.	8.6	54.8	FL.

63.39

12+50	5' Lt. = pay	3.21	60.18	
12+50	ϕ sewer	3.2	60.2	
13+00	" "	3.0	60.4	
13+00	5' Lt. = pay	2.88	60.51	
+50	" " "	2.67	60.72	
+50	ϕ	2.62	60.77	Top. Headwall
+53	Not for profile SE 1/4 End 18" Cor. Iron Fl.	5.00	58.39	culvert at Rt 4s
14+00	" "	2.7	60.7	
14+00	5' Lt. = pay	2.47	60.92	
+63 <sup>38</sup>	" " " B.C. Rt.	2.38	61.01	
+63 <sup>38</sup>	ϕ B.C. Rt.	2.6	60.8	
T.P. X in Pav. 6' Lt				
ϕ 14+63 <sup>38</sup> P.C.	8.66	69.66	2.39	61.00 ✓
15+00	ϕ	8.5	61.2	
15+00	5' Lt. pay	8.53	61.13	
+50	" " "	8.10	61.56	
+50	ϕ	8.3	61.4	
16+00	" "	8.1	61.6	
16+00	5' Lt. pay	7.80	61.86	
+55 <sup>13</sup>	" " " F.C.	7.42	62.24	
+55 <sup>13</sup>	ϕ F.C.	7.6	62.1	

69.66

32

17+00	ϕ sewer	7.1	62.6	
17+00	5' Lt. pay	6.86	62.80	
+50	" " "	6.31	63.35	
+50	ϕ	6.2	63.5	
18+00	" "	5.7	64.0	
18+00	5' Lt. pay	5.87	63.79	
+50	" " "	5.40	64.26	
+50	ϕ	5.5	64.2	
19	" "	5.1	64.6	
19	5' Lt. pay	4.98	64.68	
+50	" " "	4.31	65.25	
+50	ϕ	4.8	64.9	
20	" "	4.4	65.3	
20	5' Lt. = pay	3.73	65.93	
+50	" " "	3.14	66.52	
+50	ϕ	3.5	66.2	
21	" "	2.8	66.9	
21	5' Lt. pay	2.45	67.21	
+50	" " "	1.80	67.86	
+50	ϕ	2.2	67.5	
22	" "	1.5	68.2	

		69.66		
22	5' Lt = pav	1.20	68.46	
T.P.	7.70	76.52 ✓	0.84	68.82 ✓
+50	5' Lt = pav	7.56	68.96	
+50	φ Sewer	7.7	68.8	
23	" "	7.3	69.2	
23	5' Lt = pav	7.12	69.40	
+78 <sup>20</sup>	Δ 2.74 "	6.43	70.09	
+78 <sup>20</sup>	φ Sewer Δ stub	6.67	69.85	
24+50	" "	5.3	71.2	
24+50	5' Lt = pav	5.42	71.10	
24+79	0.3 Lt φ Sewer line	7.55	68.97	Not for profile F.L.
	S. End. inlet 12" Cor./non Culvert. at R/L to Pav. With Conc. Box. Inlet			
25	5' Lt = pav	4.80	71.72	
25	φ	4.7	71.8	
+50	"	4.3	72.2	
+50	5' Lt = pav.	4.23	72.29	
26	" " "	3.65	72.87	

				76.52	
26	φ Sewer	3.4	73.1		33
+50	" "	3.2	73.3		
+50	5' Lt = pav	3.17	73.35		
+96 <sup>67</sup>	A 44-43 Lt. φ Sewer	2.8	73.7		
T.P. C.T. φ Home	4.61	79.51	1.62	74.90 =	75.12
Ave. 8.5' E. of P.I.					
φ 13 dw. Ext.					
					0.22 Below Home Ave. B.M. s.
27+03	φ = S. Edge cone pav	5.70	73.81		
27+53	φ = N " " "	5.13	74.38		
27+62 <sup>1/2</sup>	φ = N " Asphalt "	5.10	74.41		
27+70	Top. Bank	5.2	74.3		
27+76	Top. conc. Footing Flood control	12.70	66.81		
	Nail				
27+77	bed of wash.	14.4	65.1		
27+77 <sup>1/2</sup>	0.8 Rt. Top. w. End. bridge abutment	4.73	74.78		
	0.8 Rt.				
27+79 <sup>1/2</sup>	Top. Footing " " "	13.70	65.81		
27+80	φ bed of wash	15.5	64.0		
	10' Rt. of φ = Deck S.W. Cor. Bridge	4.80	74.7		
27+92	wash	12.0	67.5		
28+45	"	12.0	67.5		
28+55	"	10.8	68.7		
28+55 <sup>1/2</sup>	0.8 Rt. = Top. w. End N. Abutment	7.02	72.49		
	10' Rt. of φ = Deck N.W. Cor. Bridge	4.34	75.17		

		79.51		
28+65			8.5	71.0
+80			7.2	72.3
+85			5.5	74.0
29+00			5.3	74.2
+10			7.0	72.5
+50			6.4	73.1
30+00			5.6	73.9
+50			4.5	75.0
31+00	¢ Sewer		4.0	75.5
31+00	10' Rt = Home Ave Rdw.		2.7	76.8
+50			3.3	76.2
32+00			2.4	77.1
+50			1.8	77.7
33+00			0.9	78.6
T.P.	7.69	86.75	0.45	79.06
				Nail Tel Pole 2 Side Home Ave
+25			7.1	79.7
+30			5.2	81.6
+50			2.9	83.9
+90			2.2	84.6

		86.75			34
34+00			3.3	83.5	
34+00	10' Rt. W edge <sup>Home Ave</sup> Rdw		6.7	80.1	
+50			5.5	81.3	
35+00			5.1	81.7	
35+00	-60' Rt = W. side wash.		9.8	77.0	
+45	2.5' RT. F.L. Inlet to 22" steel pipe Ewrest		6.9	79.9	
+46	¢ ground		6.0	80.8	
+55	" "		8.9	77.9	Wash to W.W.
+80			7.4	79.6	" " " "
+85			4.8	82.0	
36+00			4.4	82.0	
36+00	10' Rt. Home Ave Rdw.		4.0	82.8	
+50			4.2	82.6	
37+00			3.2	83.6	
T.P.	10.78	96.20	1.33	85.42	
+50			12.5	83.7	
38+00			12.3	83.9	
+50			12.1	84.1	
39+00			11.5	84.7	

		96.20		
39+00	-10' RT. = Home Ave Rdw.	8.2	88.0	
39+00	-60' RT. W. edge Wash	13.5	82.7	
+50		10.5	85.7	
40+00		9.6	86.6	
+48 <sup>26</sup>	Δ 9-13' RT.	7.8	88.4	
" " " "	12' RT. Stub	5.93	90.27	✓
41+00		6.3	89.9	
+25		4.0	92.2	
+43 <sup>88</sup>	Δ Stub	3.57	92.63	✓
+50	Δ = W. Home Ave Rdw.	4.0	92.2	
42+00		3.3	92.9	
+56 <sup>26</sup>	Δ Home Ave at E.C.	2.3	93.9	
43+00		1.2	95.0	
+50		0.4	95.8	
T.P.	11.69	106.86	1.03	95.17
44+00		10.1	96.8	
+35	E. side Rdw. Home Ave	9.9	97.0	
+50		9.0	97.9	
+70		8.6	98.3	

		106.86		
+85		10.0	96.9	35
45+00		10.3	96.6	
+07'	-13' RT. = S. End. Flood control Fence	11.6	95.3	Top Bank.
+07'	15' " = W. edge Wash.	16.5	90.4	
+23'	-6' RT Δ in Flood control Fence	11.0	95.9	Top Bank.
+50	Δ	10.3	96.6	
+80'	-5' RT. Δ in Flood control Fence	11.7	95.2	Top Bank.
46+00	Δ	11.1	95.8	
46+00	-9' LT = S. Home Ave Rdw	6.7	100.2	
+25	Δ	11.9	95.0	
+30'	Δ	7.6	99.3	
+40'	-10' RT. E. End. Flood Control Fence	9.8	97.1	Top Bank
+40'	-11' RT. NW side wash.	15.3	91.6	
46+48 <sup>24</sup>	Δ 7-29-30' RT.	6.91	99.95	Δ stub
T.P.	11.61	111.56	6.91	99.95
+95		13.0	98.6	
+97		16.0	95.6	
47+06		14.2	97.4	
+70		8.4	103.2	
48+00		8.2	103.4	
+50		6.4	105.2	

		111.56		
49+00		5.6	106.0	
+40 <sup>06</sup>	L & stub	5.84	105.72	
+40 <sup>06</sup>	12' Lt = S. Home Ave Rdw.	5.1	106.5	
+50		7.0	104.6	
+75		9.1	102.5	
50+00		9.5	102.1	
+50		7.5	102.1	
51+00		2.9	101.7	
+50		8.8	102.8	
+74		9.3	102.3	
+80		7.3	104.3	
52+20.92		7.0	104.6	
" " "	13' Lt = S. Home Ave Rdw.	3.2	108.4	
" " "	340' Rt. & wash.	12.7	98.9	
+50		6.7	104.9	
+85		5.0	106.6	
+87		8.0	103.6	
53+00		8.0	103.6	
+50		4.8	106.8	
T.P.	9.68	119.84	1.40	110.16

		119.84		36
54+00		11.6	108.2	
+50		9.3	110.5	
+53		11.4	108.4	
55+00		10.0	109.8	
+25		8.6	111.2	
+35		6.8	113.0	
+80		7.0	112.8	
56+00		5.2	114.6	
" " "	12' Lt Home Ave Rdw	7.5	112.3	
+50		6.5	113.3	
57+00		5.4	114.4	
+40		5.3	114.5	
+60		6.5	113.3	
+73		2.0	117.6	
+85.3	16' S. End. Outlet Box Culvert 4' wide	7.0	112.8	Top. Box FL. covered.
+85	& sewer	8.9	110.9	
+93		4.6	115.2	
58+00		4.2	115.6	
+50		4.7	115.1	
59+00		5.6	114.2	
" " "	65' RT = wash	11.0	108.8	
" " "	11' Lt Home Ave Rdw.	3.9	115.9	

		119.84		
59+50			6.8	113.0
60+00			7.8	112.0
+50			5.5	114.3
61+00			5.0	114.8
+50			4.7	115.1
62+00			3.8	116.0
T.P.	9.30	129.03	0.11	119.73
+52 <sup>87</sup>	L 4-31 Lt.		12.3	116.7
63+00			11.4	117.6
+50			10.8	118.2
64+00			9.7	119.3
" "	35' Rt wash		13.0	116.0
+50			10.0	119.0
+84 <sup>95</sup>	L 16-44 Lt.		9.34	119.69
65+00			8.9	120.1
" "	16' Lt. Home Ave Rdw.		5.2	123.8
+50			8.5	120.5
+50	10' Rt. N. edge wash.		11.8	117.2
+50	100' N. S. " "		11.2	117.8

		129.03		
66+00			8.7	120.3
+50			9.3	119.7
+60			8.0	121.0
67+00			7.1	121.9
+12	{ 1' Lt. S. End. Outlet 18" Conc. Pipe Culvert.		9.1	119.9 F.L.
+170	L 4-31 Lt.		6.23	122.80 $\neq$ stub
+170	10' Lt. Home Ave Rdw.		3.1	125.9
+50			5.8	123.2
68+00			5.0	124.0
+50			4.5	124.5
69+00			3.8	125.2
" "	20' Rt. wash		6.0	123.0
T.P.	9.07	136.92	1.18	127.85
69+50 <sup>79</sup>	L 6-41 Rt stub.		11.03	125.89
70+00			10.2	126.7
+50			10.0	126.9
71+00			9.2	127.7
+50			7.8	129.1
+61	{ 5' Lt. S. End Outlet 18" Conc. Pipe Culvert.		10.5	126.4

37

136.92

71+64		10.00	126.9
+66		7.3	129.6
+76 <sup>57</sup>	6'-41" RT stub	7.09	129.83
"	10' Lt = Home Ave Rdw	5.6	131.3
72+00		6.8	130.1
"	4' 200' RT = wash.	10.2	126.7
+50		6.1	130.8
73+00		5.7	131.2
+50		4.8	132.1
74+00		4.1	132.8
+50		3.8	133.1
T.P.	9.04	145.67	0.29
75+00		10.8	134.9
+50		8.5	137.2
76+00		7.2	138.5
76+00	9' Lt. Home Ave Rdw	8.0	137.7
+50		7.7	138.0
77+00		7.6	138.1
77+00	65' Rt. = wash.	13.6	132.1

145.67

+50		8.6	137.1	38
+61	32' Lt = S. End Outlet 24" Conc. Pipe Culvert.	10.3	135.4	FL.
+70		6.8	138.9	
79+00		6.0	139.7	
+50		5.4	140.3	
79+00		3.8	141.9	
"	9' Lt Home Ave Rdw	1.3	144.4	
T.P.	12.34	157.91	0.10	145.57
+50		13.7	144.2	
80+00		11.2	146.7	
"	9' Lt = Home Ave Rdw	9.6	148.3	
+50		9.3	148.6	
81+00		8.0	149.9	
"	10' Lt = Home Ave Rdw	6.0	151.9	
B.M. B.P. 2 1/4 Cor. Box Culvert	6.92	155.00	9.83	148.08 = Fairmont Ave = 148.22 S. of Home Ave 0.14 Below Home Ave



		155.00		
81+10	¢ Sewer	6.2	148.8	
+32	"	7.6	147.4	
+32	11' Lt. Home Ave Rdw	3.1	151.9	
+32	96' Rt. Wash	16.6	138.4	
+39	¢ Sewer	3.3	151.7	2.5' Lt of ¢ Elec Light Pole
+47	W. Edge Farrmont. Pav.	3.97	151.03	
+67	E " " "	5.03	149.97	
81+75	¢	5.3	149.7	
+80		4.1	150.9	
+97	{ Fire Hydt. 2.8' Lt of ¢ Sewer	4.53	150.47	on Flange
82+00		4.5	150.5	
" "	70' Rt = Wash	16.6	138.4	
" "	10' Lt = Home Ave Rdw	4.1	150.9	
+15		6.8	148.2	
+50		8.7	146.3	
83+00		8.0	147.0	
" "	5' Rt. Toe Slope	11.8	143.2	
+50		8.2	146.8	
" "	5' Rt. Toe Slope	10.5	144.5	
" "	45' Rt = Wash	14.0	141.0	
+82	{ s. End. Outlet 2' Rt 40x20 Box Culvert	11.9	143.1	F.L.

		155.00		
84+00		8.1	146.9	
" "	10' Lt Home Ave Rdw	5.2	149.8	
+50		9.5	145.5	
85+00		9.0	146.0	
+50		7.8	147.2	
86+00		7.0	148.0	
+25		4.4	150.6	
+50		4.0	151.00	
+55		6.1	148.9	
+90		4.3	150.7	
87+00		6.3	148.7	
+50		5.8	149.2	
T.P.	10.12	164.85	0.27	154.73
84+00		14.4	150.5	
" "	12' Lt Home Ave Rdw	9.6	155.3	
+25		11.7	153.2	
+50		13.4	151.5	
+58	2' Lt of ¢ Sewer			Elec Co Guy Pole
+84 <sup>20</sup>	2'-46'-30" Lt.	14.0	150.85	

		164.85		
88+90		10.6	154.3	
89+50		9.8	155.1	
90+00	100' RT = Wash	14.0	150.9	
90+00		9.2	155.7	
+50		8.1	155.8	
+81 <sup>24</sup>	∠ 2° 46' - 30" Lt.	7.60	157.20	± stub.
91+00		8.2	156.7	
+50		7.4	157.5	
92+00		5.2	159.7	
" "	9' Lt. Home Ave Rdw	3.4	161.5	
+25		6.0	158.85	
+50		6.3	158.6	
93+00		5.3	159.6	
+31 <sup>E</sup>	{ s. end outlet 1.5 x 2.7 Concr. 2' Lt. } Box. Culvert.	6.90	157.95	F.L. Not for Profile
+50		3.3	161.6	
94+00		3.3	161.6	
" "	10' Lt. Home Ave Rdw.	0.6	164.3	
T.P.	11.52	175.93	0.44	164.41
94+50		13.7	162.2	

		175.93		40
95+00		13.0	162.9	
+50		11.4	164.5	
96+00		11.2	164.7	
+50		10.2	165.7	
97+00		8.5	167.4	
" "	150' RT = Wash.	14.5	161.4	
+50		7.5	168.4	
+70		7.3	168.6	
+77 <sup>E</sup>	{ s. end outlet 2.5 x 4.0 0.5 RT } Conc. Box. Culvert	10.4	165.5	F.L. Not for profile
+78		9.8	166.1	
+88		6.7	169.2	
98+00		7.1	168.8	
+50		7.7	168.2	
+72		7.4	168.5	
+75		9.2	166.7	
99+00		8.7	167.2	
" "	12' Lt = Home Ave Rdw	4.4	171.5	
+19	{ s. end. outlet 1.5 x 3.0 0.5 Lt. } Conc. Box. Culvert	9.4	166.5	F.L. No profile
+50		6.5	169.4	
100+00		6.2	169.7	
+50		4.8	171.1	

		175.93		
101+00			5.0	170.9
+50			5.7	170.2
102+00			3.5	172.4
+17			2.2	173.7
T.P.	10.07	185.79 ✓	6.21	175.72 ✓
+50			13.8	172.0
103+00			12.7	173.1
" "	12.Lt Home Ave Rdw.		9.2	176.6
+50			11.5	174.3
+50	3.Lt of E		13.5	172.3
+75			12.3	173.5
104+00			10.4	175.4
+50			8.7	177.1
105+00			8.6	177.2
+20			10.6	175.2
+50			9.5	176.3
+60			7.7	178.1
106+00			7.2	178.6
+08			6.6	179.2

		185.79		
+10			8.8	177.0
+50			8.0	177.8
+82	3.Lt. { 5-End Outlet 1.5x3.0 Cone. Box. Culvert.		7.7	178.1
107+00			6.7	179.1
+05			5.5	180.3
+25			7.0	178.8
+50			5.5	180.3
+50	90.Rt. = wash		9.8	176.0
108+00			4.3	181.5
T.P.	9.68	195.28 ✓	6.19	185.60 ✓
+50			13.0	182.3
109+00			13.0	182.3
" "	12.Lt = Home Ave Rdw.		9.0	186.3
+50			11.0	184.3
110+00			10.4	184.9
+15			10.1	185.2
+20			11.8	183.4
+50			11.2	184.1
111+00			9.0	186.3

41

F.L. Not profile

195.28				
+50		8.1	187.2	
112+00		7.2	188.1	
+23 <sup>22</sup>	P.O.T. stub & sewer Hub. 5 Lin Home Ave	6.67	188.61	
		7.15	188.13	
+23 <sup>22</sup>	W. N. " " "	6.03	189.25	
+73		6.5	188.8	
+76		8.0	187.3	
112+99 <sup>25</sup>	Δ 9°-25'-30" Lt.	7.8	187.5	
113+50		5.6	189.7	
+50	5' RT Nat. Cr	7.2	188.1	
+50	9' Lt Home Ave Rdw.	0.5	194.8	
T.P.	8.15 201.92 ✓	1.51	193.77 ✓	
114+00		12.1	189.8	
114+00	<del>45' RT = Wash</del>	15.0	186.9	
+50		10.0	191.9	
115+60		9.0	192.9	
+50		7.4	194.5	
116+63 <sup>3L</sup>	Δ 9°-25'-30" RT.	7.17	194.75	φ stub
" "	19.8' RT. P.I. Hub. Home Ave	7.32	194.60	
+28		6.7	195.2	

201.92				
116+30	W. side wash.	8.3	193.6	42
+56	" "	8.8	193.1	
+56	26' Lt S. End Outlet	7.7	194.2	FL 4' x 4' Box Culvert
+61	E. side wash	8.9	193.0	
+62		7.5	194.4	
117+00		7.6	194.3	
+60		7.5	194.4	
+65		5.7	196.2	
118+00		5.3	196.6	
118+00	7' RT. N. side wash	9.0	192.9	
+50		4.5	197.4	
119+00		4.4	197.5	
119+00	10' RT = N. side wash	8.0	193.9	
+50		3.6	198.3	
T.P.	12.35 209.90 ✓	4.37	197.55 ✓	
120+05 <sup>13</sup>	φ Tub. P.O.T.	10.79	199.11	
" "	19.8' Lt. Man Pit Cor.	11.11	198.79	
+50		9.6	200.3	
+90		8.7	201.2	

Cont Page 44.

11-16-34 Line change from Sta 30+48 to Sta 41+42 <sup>85</sup>

T.P. Page 34	7.26	87.02	79.06	Nail in Pole
30+48 $\Delta 1^{\circ} 54' - 30 Rt$		12.0	75.0	
31+00		11.5	75.5	
+50		10.7	76.3	
32+00		9.5	77.5	
+50		8.8	78.2	
33+00		8.3	78.7	
+50		6.0	81.0	
34+08 $\Delta 1^{\circ} 54' - 30 Lt$		6.49	80.53	$\notin$ stub
+50		5.9	81.1	
35+00		5.0	82.0	
+45 = $\notin$ New Culvert - ground		4.4	82.6	
cut stub. Inlet. Cut. 1.05		8.75	78.27	
36+00		4.2	82.8	
+50		3.6	83.4	
37+00		2.9	84.1	
+50		1.9	85.1	
38+00		0.8	86.2	
T.P.	9.24	95.32	0.98	86.04

95.32

43

+50		8.3	87.0	
39+00		7.3	88.0	
+50		6.2	89.1	
40+00		5.6	89.7	
+49 <sup>16</sup> change $\notin$	} stub.	5.05	90.27 = 90.27 Page 35	
+48 <sup>86</sup> original 12' Rt				
41+00		4.0	91.3	
EQUATION $\left\{ \begin{array}{l} +42 45 \Delta 9' - 13' Rt \\ = +43.88 \text{ Station ahead} \end{array} \right.$		2.69	92.63 $\notin$ stub (original P.O.T.)	
See page 35.				

209.90			
121+00	Toeslope Euclid Ave	6.6	203.3
" "	60' Rt = Wash	13.5	196.4
60' Rt + 0.2 -			
FL S. End. Outlet	3-60" Cor Pipe Culverts	10.9	199.0
	under Euclid Ave		
T.P.	8.17	217.91	0.14 209.74
121+24	Stub P.O.T.	2.26	215.65
			215.74 0.09 Below Home Ave
+29	s. edge Euclid Pav	3.00	214.91
+42 <sup>16</sup>	⊥ " "	3.10	214.81
+55 <sup>5</sup>	N " "	3.30	214.61
+62		2.6	215.3
+85	Toeslope Euclid	14.0	203.9
122+10	⊥	14.0	203.9
" "	30' Rt End. Inlet. F.L.	18.55	199.36
			3-60" Cor Pipe Culverts
+30		14.0	203.9
+31		15.5	202.4
123+00		15.0	202.9
" "	30' Rt = wash	16.0	201.9
+50	NWly Bank	14.0	203.9
+60	⊥ wash	16.0	201.9

217.91			
	+80 S Ely Banks	14.5	203.4
124+00		12.6	205.3
	+50	12.0	205.9
125+00		11.6	206.3
	+50	9.6	208.3
	+75	9.3	208.6
	+90	10.4	207.5
126+00		9.0	208.9
T.P.	12.37	221.14	9.14 208.77
126+00	50' Lt = wash	15.4	205.7
	+45	11.5	209.6
	+46	Main wash wly side	14.5 206.6
	+80	" " Ely "	14.0 207.1
	+81		12.0 209.1
127+00		11.5	209.6
	+50	10.5	210.6
128+00		9.4	211.7
	+50	8.6	212.5
129+00		7.0	214.1
129+00	70' Rt = wash	10.5	210.6

		221.14		
129+00	40' Lt ground	8.8	212.3	
+35		6.8	214.3	
+40	W. side Main wash	8.5	212.6	
+79	S.E. " " "	9.3	211.8	
+90		7.2	213.9	
130+50		7.2	213.9	
131+00		5.0	216.1	
+35 <sup>14</sup>	Δ 36 <sup>03</sup> Lt.	3.62	217.52	
T.P.	1278 230.30 ✓	3.62	217.52	
132+00		13.3	217.0	
+10		11.6	218.7	
+50		11.2	219.1	
+50	120' Lt = wash.	14.2	215.6	
133+00		10.0	220.3	
+65		8.2	222.1	
+66	E. side wash	10.6	219.7	
+85	W. " "	9.8	220.5	
134+00		8.3	222.0	
+50		7.8	222.5	
+50	5' Rt = wash W. side	9.3	221.0	
+90		7.8	222.5	

		230.30		
135+00	W. side wash	9.0	221.3	45
+50	in wash.	8.0	222.3	
+50	<del>7' W = W. side wash</del>	<del>8.3</del>	<del>222.0</del>	
+70	W. edge wash	8.2	222.1	
+72	W. Bank.	7.0	223.3	
136+00		6.4	223.9	
" "	20' Rt = W. side wash	7.1	223.2	
+20	20' " = " " "			
+45	W. Bank	6.0	224.3	
+50	W. side wash	6.8	223.5	
+65	E. " "	6.6	223.7	
+66	E. Bank.	4.5	225.8	
137+00		3.8	226.5	
" "	50' Lt = wash	6.0	224.3	
T.P.	9.90 236.38 ✓	3.82	226.48	
+50		8.3	228.1	
138+00		7.6	228.8	
+50		6.7	229.7	
" "	20' Lt = wash			
+72		6.1	230.3	
+75		8.2	228.2	

		236.38		
		236.28		
139+00		7.6	228.8	
+25	E. Bank	7.0	229.4	
+30	E. side wash	8.2	228.2	
+45		9.2	227.2	
+52	W. side wash	8.2	228.2	
+55	W. Bank	6.3	230.1	
140+00		5.0	231.4	
" "	10.0 RT = Wash			
+50		4.2	232.2	
T.P.	9.34	241.89	3.83	232.55
141+00		8.4	233.5	
+50		7.0	234.9	
142+14 <sup>06</sup>		4.8	237.1	ground
142+14 <sup>42</sup>	Δ 4-14-30" LT	5.27	236.62	E stub.
142+37 <sup>10</sup>	Δ 49 <sup>th</sup> S. Line Fairhaven Acres	4.8	237.1	
" "	36 RT = W. side wash	8.4	233.5	
142+65	W. Bank	5.0	236.9	
142+66	W side wash	7.7	234.2	
143+00	in "	7.1	234.8	

		241.89		
+50	1st wash	5.5	236.4	
"	10.0 LT "	6.8	235.1	
144+00	in wash.	5.0	236.9	
+54	" "	5.0	236.9	
+54	2' RT Top Rubble wall	2.1	239.8	E. Bank wash
T.P. 3 Wail 1/2 in Eloc Pol. #35-36 15' LT, 144+75				
	12.68	252.38	2.19	239.70
145+00	Δ	15.2	237.2	
" "	1' RT = Top Rubble Wall	12.2	240.2	E. bank wash
145+35	E. side wash	14.5	237.9	
+38	ground to W Top. N. End Rubble wall	16.5	240.9	Wash his to W.
146+00		11.8	240.6	
+50		10.9	241.5	
147+00		9.3	243.1	
+50		7.5	244.9	
148+00		5.8	246.6	
+50		4.6	247.8	
149+00		4.1	248.3	
+48 <sup>57</sup>	N. Line Fairhaven Acres	3.7	248.7	
150+00		4.1	248.3	
+50		3.3	249.1	
+58 <sup>57</sup>	Top. 46" wood stave Pipe Chollas H's Line	5.5	246.9	



		252.38		
151400			2.8	249.6
T.P.	11.93	261.78	2.53	249.85 ✓
151+62 <sup>21</sup>	Δ 37-47 Rt,		10.6	251.2 ground.
"	" " "		11.05	250.73 ♀ Hub.
152			10.3	251.5
+50			9.9	251.9
153			10.0	251.8
+50			9.6	252.2
154			8.6	253.2
+50			4.7	257.1
T.P.	8.79	267.97 ✓	2.60	259.18 ✓
155			6.7	261.3
+12 <sup>23</sup>	Δ 37-30-30 Lt		5.62	262.35 ♀ stab
+50			2.1	265.9
+50	5 Lt of ♀		8.3	259.7
+65			3.0	265.0
+65	4 Lt of ♀		8.2	259.8

		267.97		
+80			5.3	262.7
+80	2 Lt of ♀		8.3	259.7
156.			7.3	260.7
+25			8.2	259.8
+50			8.7	259.3
157.			9.6	258.4
157	14 Lt of ♀ = 8. side wash.			
T.P.	5.10	264.30 ✓	8.77	259.20 ✓
+18	S. Bank		6.0	258.3
+27	S. side wash		9.6	254.7
+32 <sup>34</sup>	Δ 64-12-10 Rt		9.6	254.7
+80			9.6	254.7
+82			5.5	258.8
158.			4.7	259.6
158.	6 Lt of ♀ = S. Bank		4.7	259.6
158.	8 " " " S. side wash		8.7	255.6
+50			4.0	260.3
+92	S. Bank		4.1	260.2
+92	16 Lt of ♀ = S. Bank wash			
+99	S. side wash		6.2	258.1
159+20	N " " "		6.0	258.3
+22	N. Bank		3.0	261.3

		264.30		
159+50			2.0	262.3
"	55. Rt of $\Delta$ = N Bank wash			
T.P.	6.25	269.00	1.55	262.75
160			5.5	263.5
+39	N. Bank wash		5.4	263.6
+39	8. Rt of $\Delta$ = N side wash			
+41	N. side wash		8.7	260.3
+50	S " "		8.6	260.4
+52	S. Bank wash		5.0	264.0
+52	5. Lt of $\Delta$ = S. side wash			
+85 <sup>28</sup>	$\Delta$		5.11	263.89
161			4.6	264.4
+50			3.6	265.4
162			3.3	265.7
T.P.	10.97	277.39	2.58	266.42
+50			10.8	266.6
163			10.6	266.8
+50			9.8	267.6
+50	10. Lt = S. Sidewash			

		277.39		
+80	S. Bank of wash	10.0		267.4
+85	S. side wash	11.0		266.4
164	" " "	10.8		266.6
164	5. Lt. in wash	12.0		265.4
+61	S. side wash.	10.6		266.8
+63		7.7		269.7
+63	3. Lt = S. side wash	10.6		266.8
+90		6.8		270.6
+95		5.0		272.4
B.M. Nail Pole		5.45		271.94 = 50 <sup>th</sup> St (= 271.83) City B.M. 0.11 Hpts
Wightman St.				140' E of 50 <sup>th</sup> St.
Set B.M. B.P. S. End. Conc Box Culvert		4.41		272.93
B.M.	10.48	283.41		272.93
164+97	$\angle$ 15°-37' RT	11.0		272.4
165+20		11.1		272.3
+23		12.4		271.0
+50		12.3		271.1
166+00		11.7		271.7
+50		11.5		271.9
167+00		10.1		273.3
+07.	Fence W. Line Lot			
+07.	6.5 Rt. = Peach Tree			

Abandoned see Page 58

283.41

+25	3' Rt. Peach Tree			
+50		9.5	273.9	
+68	9' Rt. Apple Tree			
+86	5' Rt. Apple Tree			
from +95	To 168 + 14 = Berry Patch			
168+00		8.8	274.6	
+14	Cross Fence			
+28	" "	8.1	275.3	
+28	S. side Open shed. Cor. Iron Roof No floor			
+63	" " " " " " " "			
+85	Fence on Top of 8" conc. Retaining wall	7.4	276.0	ground 65.
		6.7	276.7	Top wall
+87	" 10' Lt. = S. side wash	8.5	274.9	ground 65
169	= S. side wash	9.2	274.2	
+12	N " "	9.7	273.7	
+20		7.5	275.9	
+50		7.4	276.0	
170		6.3	277.1	
from +06	To +25 Pile of broken glass + dirt 2' High			
+50		5.6	277.8	
+80		4.9	278.5	
T.P.	9.05	288.17	4.29	279.12

288.17

49

171		6.5	281.7	
+07	Top. Conc Retaining wall	8.5	279.7	
+08		10.3	277.9	
+12 <sup>98</sup>	46-18' Lt. & stub	10.29	277.88	
	8' Rt. = wash.	12.4	275.8	
+25	& = wash	11.5	276.7	
+50		9.8	278.4	
+50	3' Lt = wash	12.0	276.2	
+67		9.0	279.2	
+75		7.2	281.0	
+75	15' Lt. Fl. Gullet (4" Conc Pipe) out vent	10.9	277.3	This is the East of R. Pine culvert
+75	" " ground.	12.4	275.8	
T.P.	11.77	299.30	0.64	287.53
+92		9.6	289.7	
172+05		7.2	292.1	
+08 <sup>71</sup>	S. line Univ.	1.7	297.6	
+19 <sup>04</sup>	S. conc ch.	1.80	297.50	
	" gutter Pav	2.47	296.83	
+39 <sup>70</sup>	d	2.22	297.08	

		299.30	
172+60.37	N. d. Line on pay	3.18	296.12
+70.20	N. Line - 1/2 in. = 1 edge Pav.	2.93	296.37
+79		0.9	298.4
+94	FL. Inlet. 48' 30. Lt = Con. Pipe Culvert	20.5	278.8
173		16.8	282.5
+50		16.4	282.9
174		16.4	282.9
+50		16.2	283.1
175		16.2	283.1
+43		16.0	283.3
+60		14.9	284.4
+79 <sup>89</sup>	Δ 41-06 Lt & stub	13.98	285.32
T.P. & stub	8.40	293.72	285.32 ✓
+89	E. Bank	8.7	285.0
+90	E. side wash	11.4	282.3
+96	W. " "	11.4	282.3
+97	W. Bank	8.5	285.2
176+50		8.0	285.7
+85	W. Bank	7.2	286.5
+86	W. side wash	8.7	285.0
177+00	E. side "	8.2	285.5

This is the East of two pipes

		293.72	
+15	E. Bank	6.4	286.9
+50		6.4	286.9
+50	10. Lt = wash.	7.2	286.5
178		6.1	287.6
+50		5.2	288.5
179		4.5	289.2
+50		2.6	291.1
+85	E. Bank	3.0	290.7
+86	E. side wash	5.4	288.3
180	E. " "	4.5	289.2
+05	E. Bank	2.3	291.4
+35	E. " "	2.5	291.2
+36	E. side wash	5.0	288.7
+48	E. " "	3.8	289.9
+50	E. Bank	2.1	291.6
+72 <sup>09</sup>	Δ 1-23 Lt & stub	0.57	293.15
T.P. & stub	9.94	303.09	0.57 293.15 ✓
181+00		10.7	292.4
+06	2. Lt. Fig. Tree		
+16	4. Lt. " "		
+38	4. Lt. " "		

50

		303.09			
+49	3' Lt	Fig Tree			
+50			9.9	293.2	
+72	3' Lt	Fig Tree			
182			9.0	294.1	
+50			7.5	295.6	
+89 <sup>5</sup>	5. side	Rubble wall	7.0	296.1	ground
+90	"	" Top "	3.8	299.3	
+92 <sup>5</sup>	N "	" "	3.8	299.3	
+94	N. side	" "	7.0	296.1	ground
+94 <sup>39</sup>	∠	59-17 Rt.	7.0	296.1	
+94 <sup>29</sup>	26. Lt	= wash	10.5	292.6	
183 + 20			9.0	295.1	
+50			5.4	297.7	
184	E. Bank		5.0	298.1	
+68	E side	wash	7.2	295.9	
+30	W "	"	7.2	295.9	
+40	W. Bank		4.7	298.4	
185			4.6	298.5	
+50			3.8	299.3	
186			2.4	300.7	
T.P.	12.60	314.11	1.58	301.51	

		314.11			
186	25' Rt =	Wash	16.6	297.5	
+35			12.5	301.6	
+37			13.5	300.6	
+50			13.3	300.8	
+55			12.2	301.9	
+80			12.0	302.11	
+85			10.7	303.4	
187			11.0	303.1	
+36			10.5	303.6	
+36	4.5' Rt =	W Bank wash	10.6	303.5	
+36	8' Rt =	W side "	14.6	299.5	
+62 <sup>6</sup>	{	W. Line Altadena W. Bank wash.	11.5	302.6	
+70	W side	wash	15.0	299.1	
+98	E "	"	14.0	300.1	
188 + 0.5	E. Bank	"	10.2	303.9	
+50			7.3	306.8	
+69 <sup>40</sup>	∠	32-05 Rt.	6.7	307.4	
+85			5.1	309.0	
+89			5.7	308.4	
189 + 10			2.6	311.5	
+30 <sup>3</sup>	s. coned.	of Orange Ave	2.46	311.65	
"	"	gutter	3.3	310.8	

		314.11				
189+50			2.2	311.9		90106.3 82.30.3
190+06 <sup>2</sup>	gutter		1.8	312.3		
+06 <sup>2</sup>	N. conc. db. Orange Ave		0.93	313.18		
+27			0.9	313.2		
+37			6.0	308.1		
T.P. Top Fire Hydr		8.45	322.26	0.30	313.81	s.e. Orange + Altadena
	check levels					
T.P. B.M. B.P.		12.50	333.52	1.24	321.02	s.e. Orange + 50 <sup>th</sup> St.
T.P.		3.32	335.23	1.61	331.91	
B.M. B.P.			2.15	333.08	332.95	s.e. 49 <sup>th</sup> + Orange 0.13 High
B.M. Hydr		6.74	320.55		313.81	s.e. Orange + Altadena
+45	s. side wash		14.6	306.0		
+63	N. " "		14.0	306.6		
+65	N. Bank.		12.4	308.2		
191			12.3	308.3		
+50			11.0	309.6		

					320.55		52
192						9.8	310.8
+50						9.0	311.6
+70						7.7	312.9
+94						7.3	313.3
193+06 <sup>59</sup>	A 18'-00' LT					8.4	312.2
+50						8.1	312.5
194						7.4	313.2
+50						7.5	313.1
195						5.8	314.8
+50						5.1	315.5
196						4.3	316.3
+08	W. Bank wash					4.0	316.6
+13	W. side "					6.1	314.5
+28 <sup>27</sup>	φ Stub L 41-55 RT.						
T.P. φ Stub		12.51		327.13		5.93	314.62 in wash
+31	in wash					11.7	315.4
+50	" "					11.0	316.1
+98	W. Bank wash					10.0	317.1
197	W. side "					11.5	315.6
+10	" "					11.5	315.6
+15	E. Bank "					9.8	317.3

		327.13		
+50			7.7	319.4
+69 <sup>kt</sup>	W. line 52 <sup>nd</sup> St		6.2	320.9
+85			4.6	322.5
198			5.8	321.3
Set. B.M. Mon			3.13	324.00 ✓
				<small>S. 7' Line Trojahn 20' S of W. Line 52<sup>nd</sup> St.</small>
+50			5.8	321.3
199			6.0	321.1
+50			5.2	321.9
200			4.4	322.7
+55	W. Bank		4.0	322.5
+60	W. side wash		5.2	321.9
+75	E " "		5.1	322.0
+80	E Bank		4.3	322.8
201			3.7	323.4
+50			3.5	323.6
+83 <sup>57</sup>	∠ stub Δ 27° 10' AT		2.85	324.28
T.P.	11.35	335.63	2.85	324.28
202+00			10.9	324.7
202+00	7. Lt = ∠ Wash.		13.0	322.6

		335.63		
+50			10.5	325.1
+75	S. Bank		12.0	323.6
+75	2. Lt = ∠ wash		12.4	323.2
203			10.2	325.4
203	2. Lt = ∠ Wash		12.0	323.6
+50			8.9	326.7
+50	20. Lt = ∠ Wash.		11.0	324.6
+88	S. Bank		8.8	326.8
+93	S. wash		9.8	325.8
204	E. "		9.8	325.8
+05	N. Bank		8.5	327.1
+30	20. Lt = ∠ wash		9.0	326.6
+55	N. Bank		7.4	328.2
+56	wash		8.7	326.9
.63	wash		8.7	326.9
767	S. Bank		7.3	328.3
205			6.8	328.8
205	20. Lt = ∠ Wash		9.0	326.6
+50			5.8	329.8
206			5.0	330.6
+50			4.5	331.1
+50	15. Lt = ∠ wash		5.6	330.0

		335.63		
+90			3.8	331.8
207			4.5	331.1
207	5. Lt = $\phi$ wash.		5.2	330.4
+42 <sup>96</sup>	5-30 Rt $\phi$ Hub		2.47	333.16
+42 <sup>96</sup>	5. Lt = $\phi$ wash		4.4	331.2
T.P.	12.80	347.00	1.43	334.20
+55	wash s side		15.6	331.4
+75	"		17.0	330.0
207+80	"		14.0	333.0
208+20	"		13.6	333.4
+50	"		12.8	334.2
+90	N. Bank		11.1	335.9
+90	5. Rt. $\phi$ Wash		13.0	334.0
209+50	wash		10.6	336.4
210	"		10.1	336.9
+50	"		9.4	337.6
211	"		9.0	338.0
+50	"		7.8	339.2
212	"		6.8	340.2
+50	"		6.4	340.6
213			5.2	341.8
213	10' Rt = wash		7.0	340.0

		347.00		
+17	W. Bank cross wash		4.5	342.5
+18	$\phi$ wash		5.0	342.0
+19	Ely Bank cross wash		4.5	342.5
+40	"		2.9	344.1
+40	20' Rt = wash		4.0	343.0
T.P.	13.27	359.43	0.94	346.16
+75			11.1	348.3
+81	W. edge Pav.		11.86	347.57
+93	23.5' Rt = W. end. outlet double		15.8	343.6
+94 <sup>90</sup>	24" Pipe Culverts $\phi$ 20' Pav $\phi$ 54" St.		11.76	347.67
214+08 <sup>2</sup>	E " "		11.96	347.47
+14			11.6	347.8
+75	$\phi$ = {W. End. con. Head wall for Double 24" Pipes}		12.60	346.83
+17.5	3.4' Rt = $\phi$ N. Pipe of Double 24" conc. Pipe Culverts. inlet.		15.30	344.13
+24			14.2	345.2
+50			13.3	346.1
215			12.4	347.0
+50			11.8	347.6
216			11.5	347.9
+50			10.3	349.1

54



		359.43		
217			9.3	350.1
+50			8.1	351.3
+60	N. Bank		8.3	351.1
+65	Wash		11.4	348.0
+79	wash		11.0	348.4
+80	S. Bank		8.0	351.4
218+6174	∠ 38-02 LT		7.5	351.9
+50			5.8	353.6
T.P.	12.93	365.38 ✓	6.98	352.45 ✓
chk BM T.P.	AP. Headwall S.W. } orange +54 Sts }	1.45	363.93 =	363.75 0.18 High
BM	1.45	365.38 ✓		363.93
T.P.	6.98	359.43 ✓	12.93	352.45 ✓
T.P.	11.55	364.74 ✓	6.24	353.19 ✓
219			10.6	354.1
+50			9.5	355.2
+50	20' LT = wash		13.5	351.2

		364.74		55
220			8.7	356.0
+15	S. Bank		9.1	355.6
+17	Wash		11.6	353.1
+24	"		11.0	353.7
+30	N. Bank		9.0	355.7
+50			8.4	355.9
221			6.7	358.0
+50			5.5	359.2
222			4.9	359.8
222	18' RT = Wash		6.7	358.0
T.P.	12.98	373.19 ✓	4.53	360.21 ✓
+48	N. Bank		12.6	360.6
+53	Wash		15.0	358.2
+84	Wash		15.6	357.6
+87	"		11.4	361.4
223	"		11.6	361.6
+15	"		11.5	361.7
+20	N. Bank		11.0	362.2
+50			10.4	362.8
224			9.6	363.6

		373.19		
224 + 22	L 17-22 Lt	9.0	364.2	
+50		8.7	364.5	
225		7.9	365.3	
225	7. RT = Wash	9.5	363.7	
+08.	N. Bank	8.1	365.1	
+11	Wash	8.6	364.6	
+50	"	7.5	365.7	
+55	"	6.7	366.5	
+56 <sup>92</sup>	"	4.37	368.2	Pot. & stub
226	"	4.4	368.8	
+25	"	3.0	370.2	
+50	"	2.2	371.0	
T.P. & stub				
225 + 86 <sup>92</sup>	13.27	382.09	4.37	368.82
Chk. B.M. Mon N. End 20' Rad	(N.E. cor 56 <sup>92</sup> ) + Trojan	1.35	380.74 = 380.56	0.18 High
227	Wash	9.8	372.3	
+24 <sup>56</sup>	"	9.4	372.7	
228	"	7.7	374.4	
+50	"	7.2	374.9	
229	"	6.0	376.1	
+50	"	5.1	377.0	

		382.09		56
230	Wash	4.0	378.1	
+50	"	2.0	380.1	
T.P.	12.98	392.56	2.51	379.58
231	Wash	11.5	381.1	
+50	"	10.1	382.5	
+74	"	10.8	381.8	
+84	N. Bank	10.0	382.6	
232		7.6	385.0	
+20	& stub P.O.T.	4.96	387.60	
+42		3.2	389.4	
+42	5. RT = Wash	10.0	382.6	
+58.	N. Bank.	9.0	383.6	
233		6.5	386.1	
233	10. RT = Wash	8.5	384.1	
+25		6.5	386.1	
+60		5.6	387.0	
+91 <sup>62</sup>	& stub P.O.T.	3.00	389.6	
234 + 23 <sup>62</sup>	Ex. M.H.	4.20	388.36	Top + Ground
"	" " " "	9.70	382.86	F.L.
			382.52	Profile
			0.34	High

392.56

57

T.P. 12.86 402.42 ✓ 3.00 389.56 ✓

T.P. 12.35 414.37 ✓ 0.40 402.02 ✓

B.M.B.P. 2.11 412.26 ✓ N.W. 58<sup>th</sup>  
+ Meade.

T.P. 12.64 426.90 ✓ 0.11 414.26 ✓

T.P. 12.76 438.79 ✓ 0.87 426.03 ✓

T.P. 13.06 451.66 ✓ 0.19 434.60 ✓

T.P. 13.23 464.73 ✓ 0.16 451.50 ✓

T.P. 10.11 474.50 ✓ 0.34 464.39 ✓

B.M.B.P. 2.98 471.52 ✓ N.W. 58<sup>th</sup>  
El Cajon.

= 471.24  
0.24 High

1-12-39

change Sta 164 + 84 <sup>83</sup> to  
Sta 171 + 07<sup>36</sup> Δ see Page 22

B.M. B.P.	5.74	278.67	272.93	see Page S. End. Box Culvert
164 + 84 <sup>83</sup>	Δ 15-49 Rt	8.4	270.3	
+ 96	s of Bck	6.6	272.1	
165 + 21	N. side	6.6	272.1	
+ 25		7.7	271.0	
166		7.0	271.7	
+ 40		7.2	271.5	
+ 90	Fence W. Lin. Lot	5.4	273.3	
167 + 05	2' Rt. of d Peach Tree			
167 + 24	3' Lt of d " "			
167 + 50		4.7	274.0	
+ 68	S. Rt Apple.			
+ 76	2' Rt. Grapevine			
+ 84	1' Lt Peach Tree			
+ 96	S. side Berry Patch.			
168		3.9	274.8	
+ 15	N. side Berries = Cross Fence			
+ 30	" "			
+ 50		3.2	275.5	
T.P.	9.00	284.22	3.45	275.22

284.22

58

+ 51	S. side open chicken shed.			
+ 64	N. side above shed.			
+ 93	Cross-Fence	8.2	276.0	
+ 93	Top-wall E. End	7.2	277.0	
+ 95		9.6	274.6	
169 + 04	S. Bank	9.1	275.1	
+ 05	wash	10.0	274.2	
+ 18	"	10.0	274.2	
+ 25	N. Bank	8.2	276.0	
+ 50		8.0	276.2	
170 + 07	w. side Bank filled with dirt. Trash & Broken Glass	6.8	277.4	
+ 11		4.7	279.5	
+ 25		4.7	279.5	
+ 30	Natural Ground	6.7	277.5	
+ 50		6.5	277.7	
+ 80		5.3	278.9	
171		3.4	280.8	
+ 03	Top. conc. wall	4.7	279.5	
+ 04		6.6	277.6	
+ 07 <sup>36</sup> Δ		6.7	277.5	

1-27-39 Connection bet M.H. #38 sta/27+52.18 & Outlet  
Existing Sewer Serving Islenair. See Page 18.

BM # stub 3.74 221.26 217.52 131+35.14

0+00 # stub M.H. #38 sta/27+52.18 10.84 210.42

+33 9.3 212.0

+41 10.7 210.6

+67 wash 11.0 210.3

+80 9.5 211.8

+100 9.7 211.6

+15 7.7 213.6

+18 4.8 216.5

+33 2.6 218.7

T.P. 12.13 231.15 2.24 219.02

+43 9.6 221.6

+53 6.0 225.2

+60<sup>±</sup> ground. 5.2 226.0

+60<sup>±</sup> Top. Ex. 6" conc. pipe 7.14 224.01

223.4 Flow line ?

2-1-39 Change in Line from Station 196+28<sup>27</sup> Δ  
 To Sta 209+27<sup>25</sup>  
 Levels Page 61

$8 \sqrt{3} (207+91^{20} \text{ P.I. } \Delta 4 \text{ W. Line lot 1R}) = (208+50^{22} \text{ "C" Line})$

$(206+53^{28} \Delta 28-19 \text{ Rt. B. Line}) = (207+13 \text{ or P.O.T. "C" Line})$

$206+83^{51} \Delta 29-22 \text{ Rt. "C" Line}$

$202+38^{36} \Delta \text{ Dawson Proposed "C" Line}$

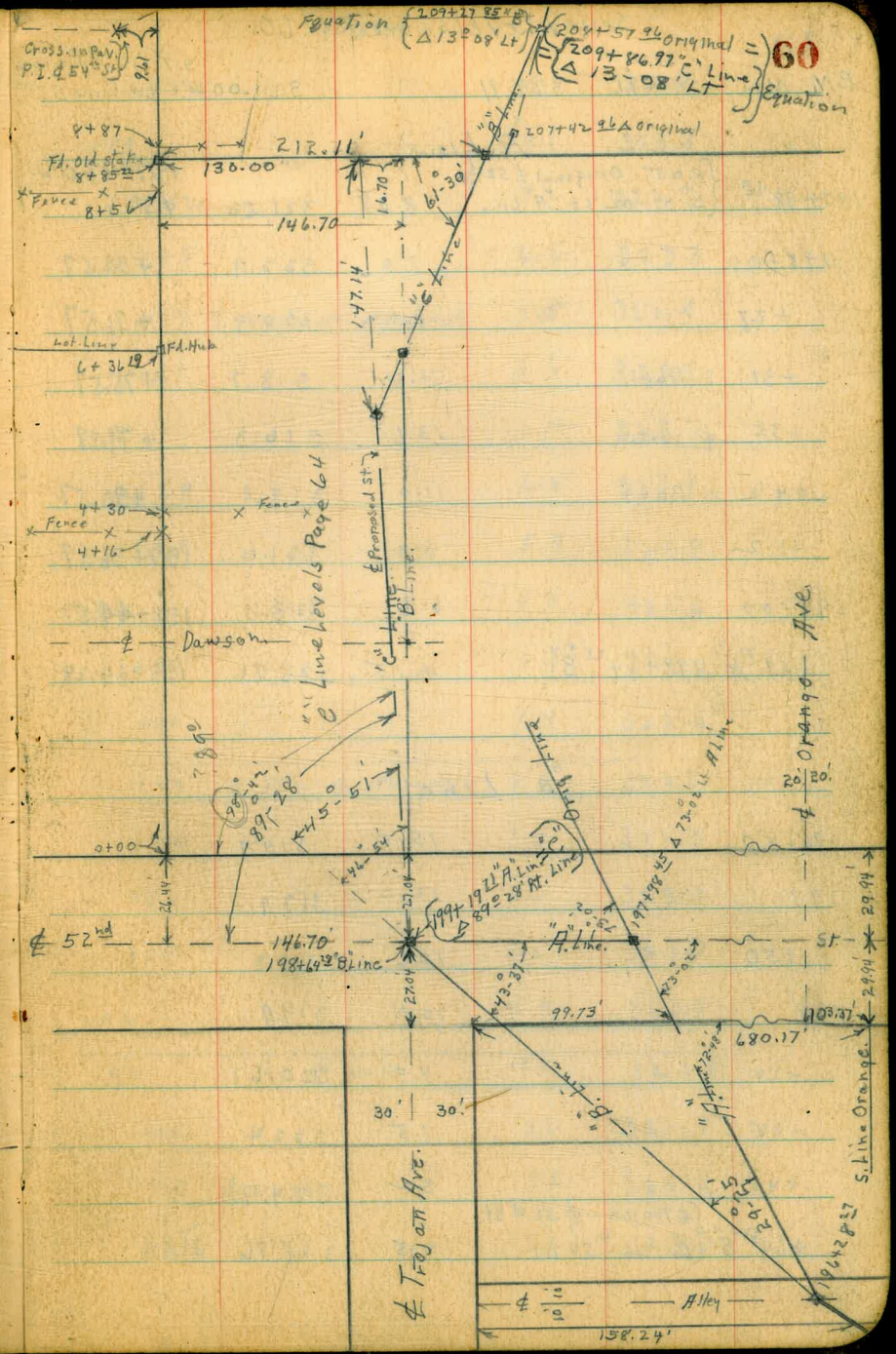
$199+46^{25} \text{ "C" E. Line } \Delta 52^{\text{nd}} \text{ St.}$

$198+91^{32} \text{ E. Line } \Delta 52^{\text{nd}} \text{ St. "B" Line}$

$198+64^{20} \text{ "B" Line } \Delta 46-54 \text{ Rt.}$

$199+19^{21} \text{ "C" Line } \Delta 89-28 \text{ Rt. = "A" Line continuation}$

$196+28^{27} \Delta \text{ Alley. Original = "A" Line = "B" Line}$



Sewer Levels See Page 60.

329.91

61

BM Mon 5.91 329.91 324.00

5.7' Lin - Trojan  
20.8' of W. line - 52<sup>nd</sup> St

"A" Line

197+98 <sup>45</sup>	{ P.O.T. Original $\phi$ 52 <sup>nd</sup> St $\Delta$ 37'-02" Lt. "A" line	8.35	321.56	197+43.02 $\phi$ stub
198+00		7.0	322.9	+44.57
+27		9.0	320.9	+71.57
+31	S. Bank	11.2	318.7	+75.57
+35	$\phi$ Wash	13.6	316.3	+79.57
+46	N Bank	11.0	318.9	+90.57
+52		8.3	321.6	197+96.57
199+00		6.6	323.3	198+44.57
+19 <sup>46</sup>	198+64 <sup>24</sup> "B"	4.15	325.76	198+64.28

"B" Line

196+50		15.0	314.9	
197		12.0	317.9	
+50		10.6	319.3	
198		10.0	319.9	
+24		9.3	320.6	
+34		7.5	322.4	
+45		5.2	324.7	
+64 <sup>24</sup>	{ $\phi$ Trojan - $\phi$ 52 <sup>nd</sup> St $\Delta$ 46'-54" Rt	4.15	325.76	$\phi$ stub

+70

5.0 324.9

199

6.1 323.8

+12

7.2 322.7

+35

6.6 323.3

+44  $\phi$  Wash Not Main Wash

7.5 322.4

+49

6.6 323.3

200

6.2 323.7

+20

6.5 323.4

+50

5.9 324.0

201

4.3 325.6

+33

9.4 326.5

+40

7.4 322.0

+40 3 Rt. =  $\phi$  Main Wash

7.6 322.3

+52

7.6 322.3

+53

6.6 323.3

+75

5.0 324.9

202

6.0 323.9

202 3 Rt.  $\phi$  Wash

7.1 322.8

+05

7.2 322.7

+15  $\phi$  Wash

7.5 322.4

+25

6.2 323.7

	329.91		
+35		6.2	323.7
+50		8.0	321.9
+60		6.5	323.4
203		4.8	325.1
203	11. RT $\phi$ Wash	6.6	323.3
T.P	11.92	337.75	4.08
+50		10.6	327.2
204		9.3	328.5
204	14. RT = wash	13.2	324.6
+60		7.8	330.0
205		5.1	332.7
+50		5.1	332.7
+75		6.7	331.1
206		6.6	331.2
+53 <sup>88</sup>	$\Delta 28-19$ RT.	6.63	331.12
206+53 <sup>88</sup>	12. RT. $\phi$ wash	9.0	328.9
207		6.7	331.1
+20		6.5	331.3
+50		4.4	333.4

	337.75		
+91 <sup>80</sup>	$\phi$ stab	W.L. Lot 12	2.52
208			2.1
+50			2.0
209			2.2
	$\left\{ \begin{array}{l} +27^{85} B = 208 + 57^{96} \text{ Original} \\ \Delta 13^{208} \text{ Lt.} \end{array} \right\}$		2.76
+27 <sup>85</sup>	2. RT = wash		3.3
chk. $\phi$ stab	207 + 42 <sup>92</sup>		4.59



2-6-39. Ppdim Sewers. "B.I." Line Ramsey Level Notes  
 From & Alley BIK 27 Fairmont Addition Page 66.

To & Alley BIK 34. " "

0+00 = S. line Fairmont A.d. & Alley BIK 27  
 1+89<sup>25</sup> E Line 50<sup>th</sup> St  
 2+36<sup>41</sup> Stab " "  $\Delta 8^{\circ} 33' RT$   
 2+80<sup>29</sup> " W Line " "

5+05<sup>10</sup> stub & Alley BIK 28  $\Delta 17^{\circ} 38' LT$

7+44<sup>50</sup> stub W. Line Winona

8+41<sup>23</sup> stub S. Line Orange.

9+10<sup>24</sup> Hub. of Orange Ave  
 1/2 Alley BIKs 36+29  $\Delta 12^{\circ} 30' LT$

10+12<sup>62</sup>

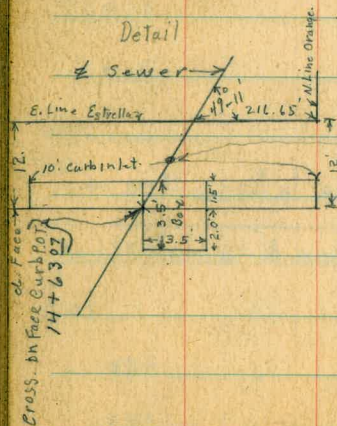
10+69<sup>85</sup> = E. d. 49<sup>th</sup>

11+09 = W. d. 49

11+22<sup>02</sup> stub W. line 49<sup>th</sup>

12+68<sup>27</sup> stub & Alley BIK 35  $\Delta 17^{\circ} 52' RT$

Detail

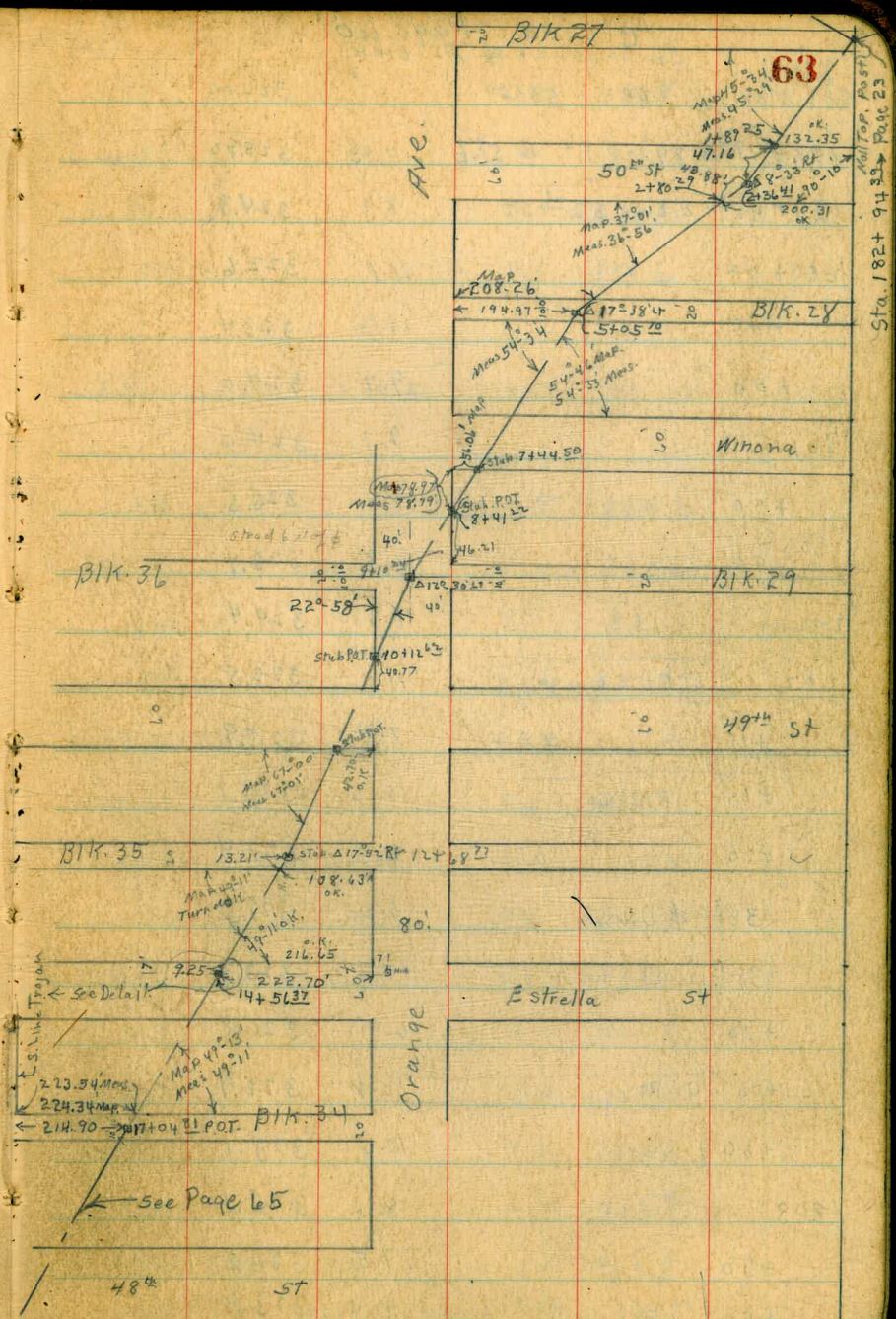


14+56<sup>21</sup> Nail P.O.T. E. Line Estrella  
 14+63<sup>01</sup> Cross P.O.T. Face of E. Curb.

17+04<sup>81</sup> stub P.O.T. & Alley BIK 34

18+99 E. d. Face

19+46 W. d. Face



AM. Mon.	9.69	333.69	324.00
199 + 11 <sup>21</sup> Δ 89°-28' Rt. & Stub	7.93	325.76	
199 + 46 <sup>25</sup> E. Line 52 <sup>nd</sup> St.	8.9	324.8	
200 + 00	11.1	322.6	
+ 05	10.3	323.4	
+ 50	9.7	324.0	
201	9.7	324.0	
+ 50	8.2	325.5	
+ 90	6.8	326.9	
202	9.3	324.4	
202	6' Rt = wash	11.2	322.5
+ 15	7.8	325.9	
+ 15	7' Rt. wash	10.6	323.1
+ 20	6.3	327.4	
+ 38 <sup>36</sup> & Dawson	6.2	327.5	
+ 38 <sup>36</sup> 12' Rt = wash.	10.4	323.3	
+ 70	6.9	326.8	
+ 70	4' Rt = wash	10.8	322.9
+ 80 & Wash	10.6	323.1	
203	8.6	325.1	
+ 50	7.5	326.2	
+ 50	16' Rt = wash	10.4	323.3

204		6.0	327.7
+ 50		3.6	330.1
205		3.0	330.7
+ 50		0.1	333.6
T.P.	5.31	338.81	0.19 333.50
+ 75		4.5	334.3
206		5.2	333.6
+ 40		7.0	331.8
+ 83 <sup>51</sup> Δ		7.24	331.57
207 + 13	P.O.T.	7.69	331.12
+ 50		8.0	330.8
+ 50	10' Rt = wash	9.4	329.4
+ 80		7.4	331.4
208		6.1	332.7
+ 25		4.6	334.2
+ 60		3.0	335.8
209		3.2	335.6
+ 50		3.1	335.7
+ 50	7' Rt = wash	5.0	333.8
+ 86 <sup>21</sup> "E" line = 208 + 57 <sup>96</sup> Original		3.92	334.99

Prelim Sewers "B.I." Line  
Continued from Page 63  
Level Notes Page 66

19+46<sup>7</sup> w. ch.

19+53<sup>17</sup> cross P.O.T. W. 7' Line  
19+62<sup>42</sup> w. line 48" st.

20+36<sup>27</sup> stab &  $\Delta 40^{\circ}-49'-30''$  Lt.

22+62<sup>8</sup> E. ch. Euclid Ave  
22+98<sup>8</sup> w. ch. " "

2408<sup>62</sup>  $\Delta 90^{\circ}-01'-30''$   
2" N of S. Line Trojan

Ex. 12" Pump Line Sewer.

Ex. M.H. with Sealed

A. 30+35

12" Pump Line Sewer

X Line

Ex. M.H. El Cajon

El Cajon Blvd

5.5' ch.

5.5' ch.

5.5' ch.

5.5' ch.

5.5' ch.

5.5' ch.

5.5' ch.

5.5' ch.

5.5' ch.

5.5' ch.

5.5' ch.

5.5' ch.

5.5' ch.

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5.5' ch.

5.5' ch.

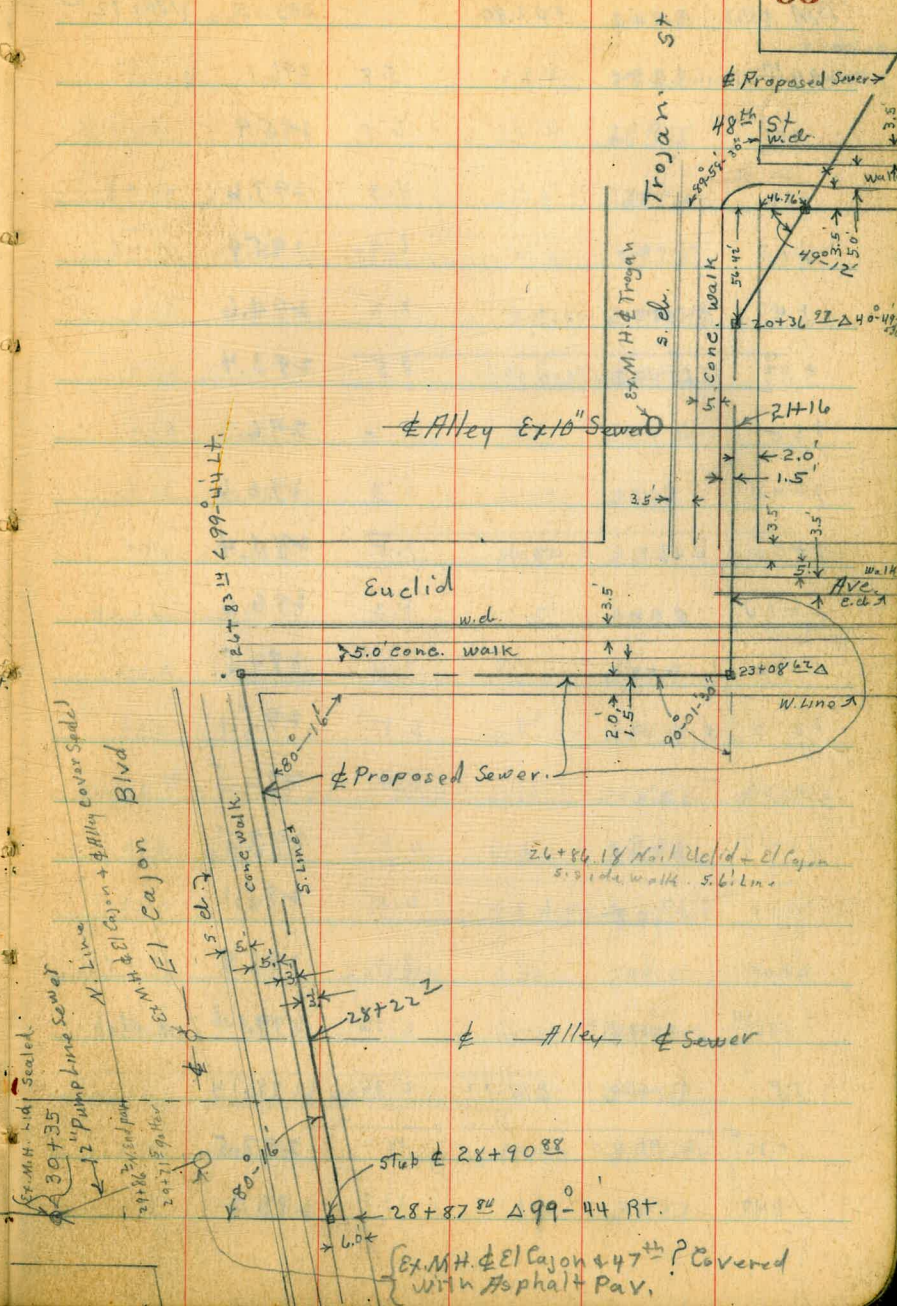
5.5' ch.

5.5' ch.

5.5' ch.

See Page 63

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Levels Prelim Sewer "B1" Line  
Plat. Pages 63 + 65

BM # Sta	8.75	301.90	293.15	(Page 50 180+72.09)
0+00 = 182+94 <sup>39</sup> Main Line			5.8	296.1
+07			6.0	295.9
+12			4.3	297.6
+15			6.0	295.9
+47 $\phi$ cross wash			7.3	294.6
+47 17.Lt = $\phi$ Main wash			8.5	293.4
+50			5.6	296.3
1+00			5.3	296.6
1+00 5.Lt = $\phi$ wash			7.5	294.4
1+04			5.3	296.6
1+10 E. wash			7.4	294.5
1+18 W. "			6.8	295.1
1+20			5.4	296.5
1+50			4.0	297.5
1+50 9.Lt = $\phi$ wash			6.8	295.1
2+00			3.0	298.9
+36 <sup>41</sup> $\Delta$ 8-33 Rt.			2.76	299.14 $\phi$ /stub
T.P. 12.58	311.72		2.76	299.14
+36 <sup>41</sup> 10. Rt. $\phi$ wash.			14.2	297.5
+47			13.5	298.2

311.72

66

750 Wash			14.4	297.3
+57 $\phi$ "			13.4	298.3
+80 " "			12.2	299.5
3+00			10.5	301.2
3+00 12.Lt $\phi$ wash			14.2	297.5
+45			9.3	302.4
+50			11.5	300.2
+53			9.1	302.6
+75 E. Bank			10.0	301.7
+85 S. wash			10.8	300.9
4+00 " "			12.5	299.2
+70 W. Bank			9.8	301.9
+50			6.8	304.9
5+05 <sup>10</sup> $\Delta$ 17-38' Lt E. Bank			6.11	305.61 $\phi$ stub
+18 $\phi$ wash			6.9	304.8
+50			4.5	307.2
T.P. 11.36	320.42		2.66	309.06
6+00			12.3	308.1
6+00 5.Lt. $\phi$ wash			13.3	307.1
+10 wash			13.0	307.4
+25 "			13.3	307.1

		320.42		
6+40	wash	12.5	307.9	
+50		11.3	309.1	
7+00		10.1	310.3	
+0.5	w edge wash	11.5	308.9	
+18		9.4	311.0	
+18	7. Rt = w edge wash	11.8	308.6	
+18	21.5 Rt = S. End Outlet 48" Culvert	11.20	309.22	F.L.
+44 <sup>50</sup>	P.S.T. slab	10.60	309.82	
+84		8.5	311.9	
8+00		4.5	315.9	
+13		1.8	318.6	
T.P.	12.69 332.40	0.71	319.71	
8+41 <sup>20</sup>	S. Line Orange	3.7	328.7	
+65		3.4	329.0	
+70		3.8	328.6	
9+10 <sup>20</sup>	{ E. Line } { Orange } Δ 12=30 Lt.	2.8	329.6	
+70		3.0	329.4	
+76		2.0	330.4	
10+12 <sup>60</sup>	N. Line Orange	1.8	330.6	
+30		2.8	329.6	
+40		1.0	331.40	

		332.40		
10+69 <sup>2</sup>	E. end. d. 49 <sup>th</sup> st	0.87	331.53	17.24 4.36 15.60 <b>67</b>
" "	gutter pav.	1.21	331.19	7.25 3.35 15.60
11+00		0.53	331.87	
11+09	gutter pav	0.75	331.65	
T.P.	5.96 337.81	0.55	331.85	
chk. BM	S. E. Orange + 49 <sup>th</sup>	4.73	333.08	page 52 0.13 High
11+09	w. d. 49 <sup>th</sup>	5.39	332.42	
+25		6.1	331.7	
+35		11.4	326.4	
	{ NW. End Intake } 17. Lt = 48" Culvert	15.60	322.21	F.L.
+50		13.8	324.0	
12+00		14.3	323.5	
+68 <sup>77</sup>	Δ 17=50	13.7	324.1	
13+00		12.8	325.0	
+50		12.1	325.7	
14+00		10.9	326.9	
+15		9.4	328.4	
+15	{ E. End. Outlet } 8.3 Lt = 36" Culvert	10.60	327.21	F.L.
T.P.	8.80 346.04	0.57	337.24	
+43		4.0	340.0	

		346.04		247.8
14+63 <sup>27</sup>	E. cone d	6.32	339.72	23.9
" "	gutter of ch inlet <small>(on N.E. Cor grating)</small>	7.31	338.73	18.99
" "	F.L. ch inlet	16.7	329.3	1822.9
15+00		7.0	339.0	
+34		6.6	339.4	
+40		13.4	332.6	
+42	4.3' $\Delta$ = <small>1/2 inlet w. End</small> 36" Culvert.	18.0	328.0	
+46 $\phi$		18.0	328.0	
16+00		17.0	329.0	
+50		16.8	329.2	
17+04 <sup>81</sup>	P.O.T. $\phi$ Alley BIK 34	15.0	331.0	
+50		14.1	331.9	
18+00		13.2	332.8	
+43	ground	12.0	334.0	
+43 <sup>E</sup>	Top. cone wall E+W.	11.2	334.8	
+81 <sup>E</sup>	E. side cone wall	10.4	335.6	
+82	Top. " "	4.14	341.90	
+83	ground.	4.8	341.2	
+99	E. ent. ch 48 <sup>th</sup> st.	4.84	341.20	
"	gutter pav	5.44	340.60	
19+22 <sup>2</sup>	$\phi$ "	5.34	340.70	
19+46 <sup>2</sup>	gutter "	5.76	340.34	

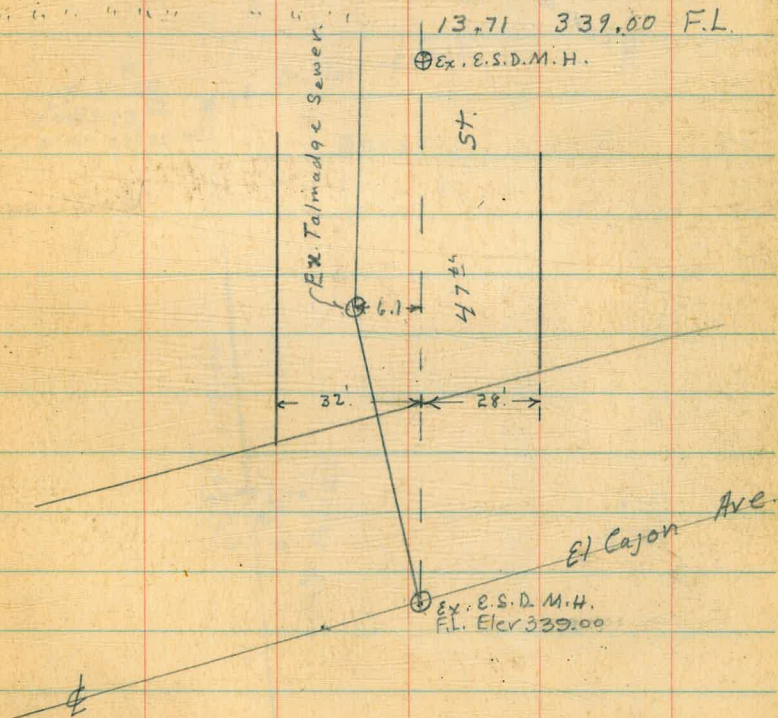
		346.04		68
19+46 <sup>2</sup>	W cone. ch 48 <sup>th</sup>	5.15	340.89	
20+00		4.6	341.4	
20+36 <sup>27</sup>	$\phi$ stub $\Delta$ 40°-49'-30" Lt.	3.88	342.16	
T.P.	6.30	348.84	3.50	342.54
+73	$\phi$ conc walk.	6.32	342.52	
21+06	Top. ch. E. side Alley	6.15	342.69	
+06	Ally pav.	6.47	342.37	
+16	28' Rt. $\phi$ Trojan Ex M.H.	11.52	337.32	F.L. 10" Sewer
+16	" " " "	5.39	343.45	Top 11" = pav
+26	Ally pav.	6.45	342.39	
+26	Top. ch. W. side Alley	6.02	342.82	
+50		6.0	342.8	
22+00		6.0	342.8	
+62 <sup>2</sup>	E. ch. Euclid	5.51	343.33	
"	gutter Pav	6.17	342.67	
+80 <sup>2</sup>	$\phi$ "	5.19	343.65	
+98 <sup>2</sup>	gutter "	5.59	343.25	
+98 <sup>E</sup>	W. ent. ch.	4.98	343.86	
23+08 <sup>62</sup>	$\Delta$ 90°-01'-30" Rt.	4.75	344.09	$\phi$ stub
+50		4.7	344.1	
24+00		4.5	344.3	
+20 <sup>2</sup>	$\phi$ 2.6' ent. walk	4.30	344.54	
+46 <sup>2</sup>	$\phi$ 2.6' ent. walk.	4.20	344.64	

348.84

24+83 <sup>2</sup>	S. side conc drive	3.92	344.92	
+98 <sup>2</sup>	N. " " "	3.84	345.00	
25+26 <sup>5</sup>	E 3' conc walk	3.70	345.14	
+39	E 3' " "	3.59	345.25	
+58 <sup>2</sup>	E+W. conc. wall	3.30	345.54	
26+00		3.4	345.4	
+50		3.0	345.8	
+83 <sup>14</sup>	Estab. $\Delta$ 99-44 Lt.	2.86	345.98	
+83 <sup>10</sup>	3' N-S edge conc. walk	3.00	345.84	
T.P.B.M.	5.0x	350.91	3.01	0.12 Mgn 345.83
				(345.71 S.W. El Cajon & Euclid.)
27+00		4.8	346.1	
+50		5.0	345.9	
28+12 <sup>4</sup>	d. E. Alley	4.83	346.08	
+12 <sup>4</sup>	Alley Pav.	5.14	345.77	
+22 <sup>4</sup>	" "	5.18	345.73	
+22 <sup>7</sup>	to Pt = Ex M.H. Top. scale	3.89	347.02	Top = Pav.
+33	pav. "	4.85	346.06	
+33	W. d. Alley	4.55	346.36	

69

28+87 <sup>24</sup>		4.3	346.6	
28+90 <sup>88</sup>	S. edge walk	4.26	346.65	
3-30-39				
B.M.	6.88	352.71	345.83	opp. page
Ex. M.H. $\phi$ El Cajon in 47 <sup>th</sup> St.		5.20	347.51	pav.
" " " " " " " "		5.30	347.41	Rim
" " " " " " " "		8.41 below		
" " " " " " " "		13.71	339.00	F.L.
				Ex. E.S.D.M.H.



5-10-39

change from 164+84.22 to 171+13.22

" B" Line

Abandoned. See Page 71.

70

M.H. 51  
171+13.22 New = 171+05.22 old  
Δ 55-36-47"

M.H. 50  
164+43.22  
Δ 15-57-36" RT.

51. Bottom of wash

① M.H. 50

358.50

80.58  
6-51

Page 22.

Line 2

M.H. 49  
164+84.22  
8-58" RT.

24-13  
2-57



5-18-37  $\Delta$  change Sta 164+84<sup>43</sup> M.H. 49  
 Line To Sta 171+05<sup>25</sup> M.H. 50. original use ahead.  
 171+05<sup>25</sup> Original station Use ahead. } M.H. 51  
 Use to Rear }

172+04<sup>86</sup>

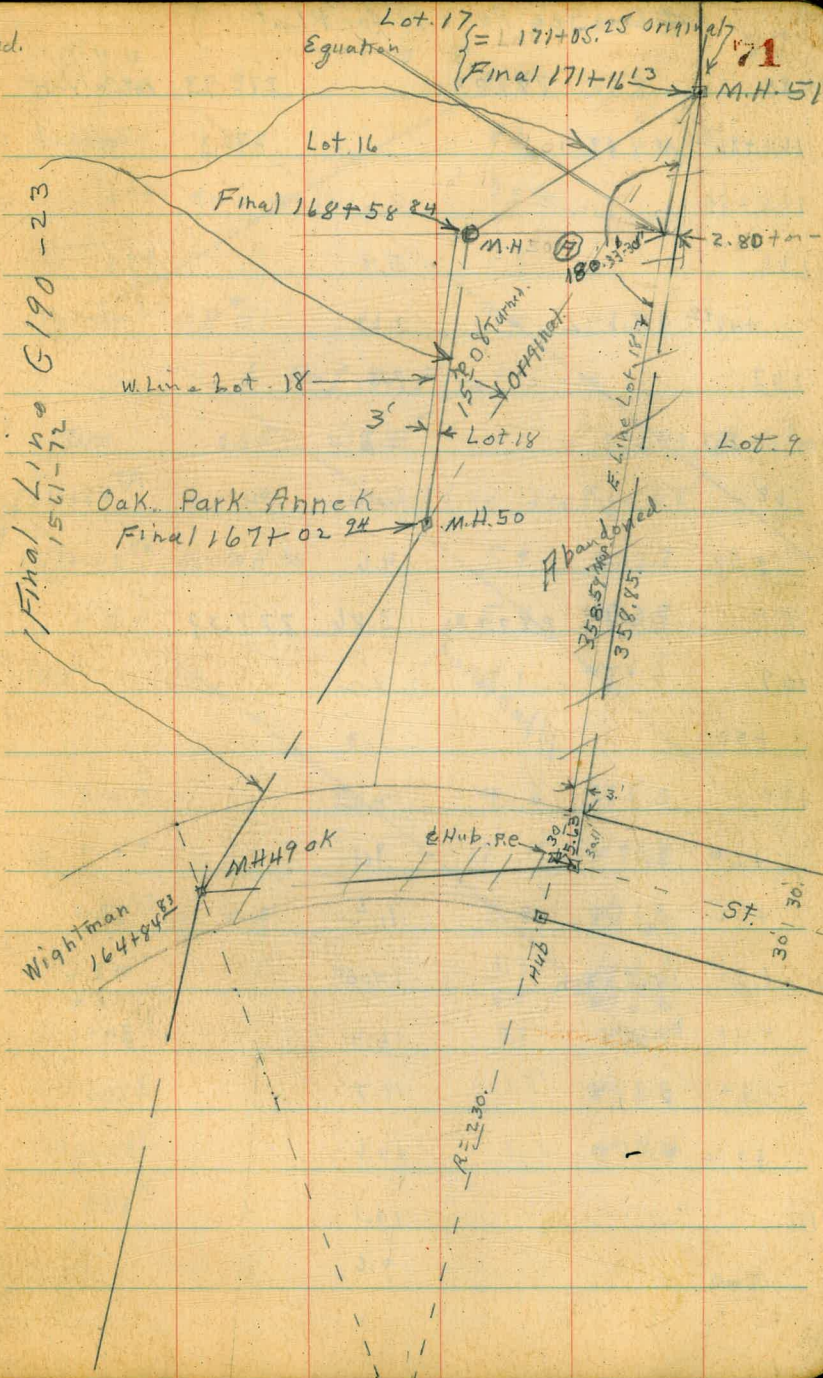
170+35<sup>36</sup> opp. Lot Cor.

→ 60' in Survey Line  
 Put M.H. at station as 50  
 6' offset stubs in + Levels Taken

Abandoned

166+46<sup>40</sup> M.H. 50  $\angle$  74°-10' Lt.  
 164+84<sup>43</sup> M.H. 49  $\angle$  Rt.

changed  $\angle$  Wightman  
 No change



Levels See Page 71 for Plat.

BM.B.P.	8.32	281.25	272.93	wightman in Calvert.
164+84 <sup>83</sup>	M.H. 49		270.3	ground
165+50		8.6		
166		5.9		
+46 <sup>80</sup>	4 stub L	3.63		
167		4.3		
+50		6.6		
168		6.4		
+50		4.6		
T.P.	9.84	287.23	3.86	277.39
169		8.2		
+50		7.3		
170		8.2		
+20		9.1		
+32	Bank	11.2		
+35	Bottom wash	14.5		
+41	Bank	12.4		
+50		11.7		
+52		10.6		
171		10.1		
+20		9.6		

Abandoned

+30		8.3	
+50		8.1	
+98	conc. wall	7.82	
+99		9.6	
172+04 <sup>86</sup>	M.H. #51	9.6	

Profile Final Line

BM.	6.65	279.58	272.93	B.P. Calvert
164+84 <sup>83</sup>	M.H. 49	original Line	See Page 58	
167+02 <sup>84</sup>	New M.H. 50	5.9	273.7	
+50		5.7	273.9	
168		5.1	274.5	
+47	Bank	4.6	275.0	
+49	wash	7.8	271.8	
+58 <sup>84</sup>	M.H. 4.	"	7.8	271.8
+60	Bank	5.1	274.5	
+85		4.4	275.2	
169+02 <sup>88</sup>		3.7	275.9	
+52 <sup>85</sup>		3.3	276.3	
170+02 <sup>85</sup>		2.2	277.4	
+52 <sup>88</sup>				

8/24/39.

# Prelim Sewers.

To serve Andrew Jackson School  
Sec G. 190 - Page 67.

BM. B.P. S.E. El Cajon & 54<sup>th</sup> 403.77

M.H. 64 Chollas Valley Trunk Line  
= 0400 Exp. M.H.  
702.52'  
1446 1/2 William Lot 12.  
90211'

6190-675  
8" Sewer

Chollas Sewer

3100 M.H. #1

# Trojan Sewer

M.H. #2

PAK

1274  
976  
3.02  
976.  
783.2  
192.8  
783.2  
568.3  
214.9

Indexed  
Cusals.

Ex. Septic Tank

1973

D.E. 12+78.8" Line

← 20' → 3.6

7+92

20' Pavmt.  
10' 10'

302

Sewer

72-23'

0400 6" Line

M.H. #3  
9+76.6 Line

15  
10.40.13  
6.1  
10.3  
12

192.8'

S. Line School Property

7+83.20  
#R=299.60  
D=28'-12"

SEE 599

PE  
75.25  
6.1  
15.25  
17.44

25' 25'

83.22'

17.44'

61.90'

54.63'

41.45'

ct.

R.M. C.T.		Σ Sewer		Σ 54 <sup>th</sup> St Σ Trojan Ave
5+28 <sup>3</sup> M.H. 2	12.75	364.42		361.67
6+00			12.5	351.9
6+50			8.5	355.9
6+66 W. Pav.			10.8	353.6
6+75 35' W = N. Side House			10.51	353.9
7+00			13.2	351.2
			10.2	354.2
+40 E. Pav.			9.71	354.7
+50			9.3	355.1
+83 <sup>3</sup> P.C. Pav. Curve			8.2	356.2
8+50			3.2	361.2
T.P.	14.15	377.86	0.71	363.71
9+00			12.5	365.36
9+76 M.H. #3			6.2	371.6
10+00			4.2	373.6
T.P.	12.77	389.89	0.74	377.12
10+50			11.9	378.0
11+00			7.5	382.4
11+50			3.3	386.6
T.P.	12.75	402.48	0.16	389.73
12+00			11.7	390.8
+50			7.7	394.8
12+78			5.7	396.8

				F.L. Grade	84
			Σ 364.42		
stables	12.55	351.87		346.72	+ 5.15 ✓
" 6 W	10.98	353.44		346.90	+ 6.54 ✓
" 6 W	10.80	353.62		347.20	+ 6.42 ✓
Brk	X 4. W	10.16	354.26	347.50	+ 6.76 ✓
Brk	X 4. W	9.13	355.29	349.00	+ 6.29 ✓
Brk	X 4. W	7.97	356.45	351.50	+ 4.95 ✓
	X 4. W	3.20	361.22	356.80	+ 4.42 ✓
			Σ 377.86		
	X 4. W	12.47	365.39	360.75	+ 4.64 ✓
	X 4. W	6.11	371.75	366.75	+ 5.00 ✓
	X 4. W	4.12	373.74	368.74	+ 5.00 ✓
			Σ 389.89		
	X 4. W	11.85	378.04	372.93	+ 5.11 ✓
	X 4. W	7.49	382.40	377.11	+ 5.29 ✓
	X 4. W	3.28	386.61	381.29	+ 5.32 ✓
			Σ 402.48		
	X 4. W	11.65	390.83	385.47	5.36 ✓
	X 4. W	7.68	394.80	389.65	5.15 ✓
	X 4. W	5.64	396.84	392.00	4.84 ✓

6" Line from M.H. #3 N. E. ly.

		377.86	± sewer	
0+00 =	M.H. #3		6.2	371.6
0+50			4.2	373.6
1+00			3.9	373.9
+50			3.4	374.4
2+00			3.0	374.8
+50			2.8	375.0
3+00			2.2	375.6
T.P.	6.31	382.01	2.16	375.70
+50			6.1	375.9
4+00			5.1	376.9
+50			4.5	377.5
5+00			4.5	377.5
+50			4.5	377.5
6+00			4.3	377.7
+50			4.5	377.5
7+00			4.0	378.0
+50			3.1	378.9
+92	5' s. of wall. Δ to Septic Tank.		3.11	378.9

		377.86	FL Grad	cut	75
X4' W.	6.11	371.75	367.10	+4.65	✓
Stable N.W.	4.24	373.62	369.80	+3.82	✓
" " "	3.86	374.00	371.00	+3.00	✓
" " "	3.34	374.52	371.35	+3.17	✓
" " "	3.05	374.81	371.70	+3.11	✓
" " "	2.77	375.09	372.05	+3.04	✓
" " "	2.16	375.70	372.40	+3.30	✓
		382.01			
" " "	6.08	375.93	372.75	+3.18	✓
" " "	5.10	376.91	373.10	+3.81	✓
" " "	4.47	377.54	373.45	+4.09	✓
" " "	4.51	377.50	373.80	+3.70	✓
" " "	4.55	377.46	374.15	+3.31	✓
" " "	4.30	377.71	374.50	+3.21	✓
" " "	4.49	377.52	374.85	+2.67	✓
" " "	3.92	378.09	375.20	+2.89	✓
" " "	3.15	378.86	375.55	+3.31	✓
" " S.E.	3.11	378.90	375.85	+3.05	✓

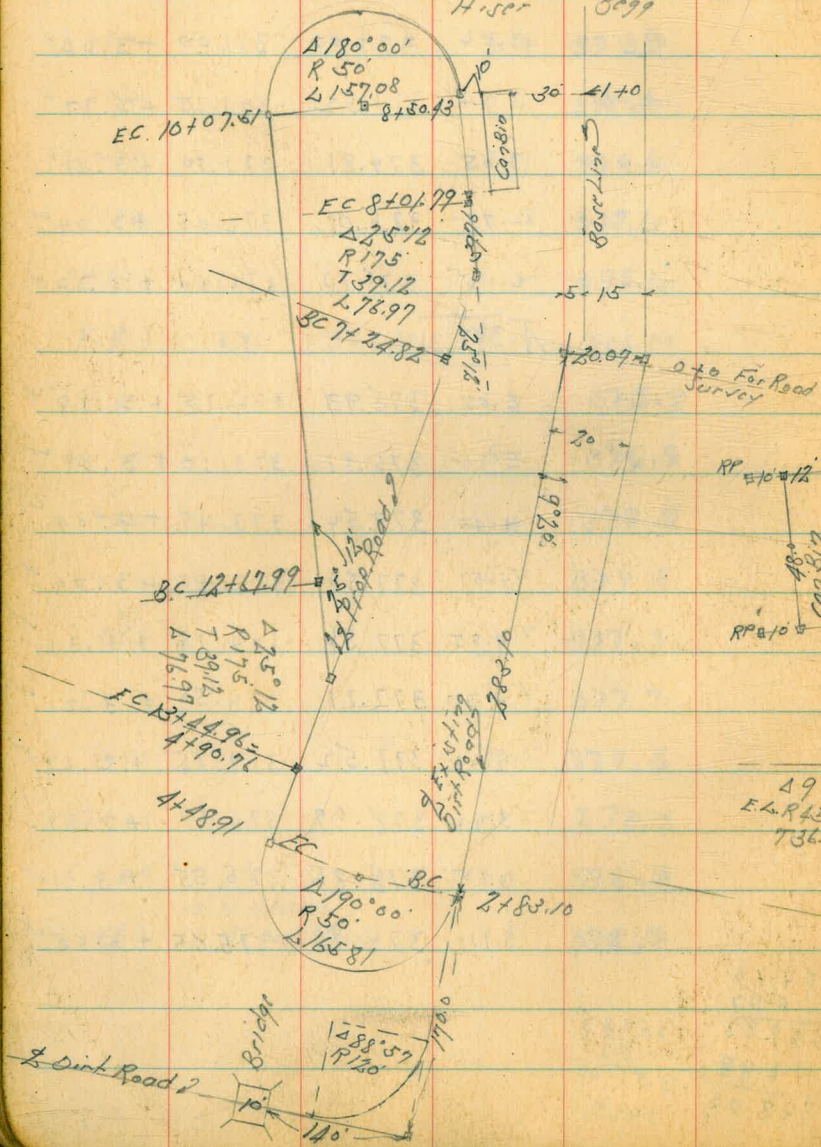
354.26	
5.57	
<u>359.83</u>	359.83
17.98	8.83
<u>348.00</u>	351.00
	349.5

Proposed Can Bin Collier Park

Levels Next Page

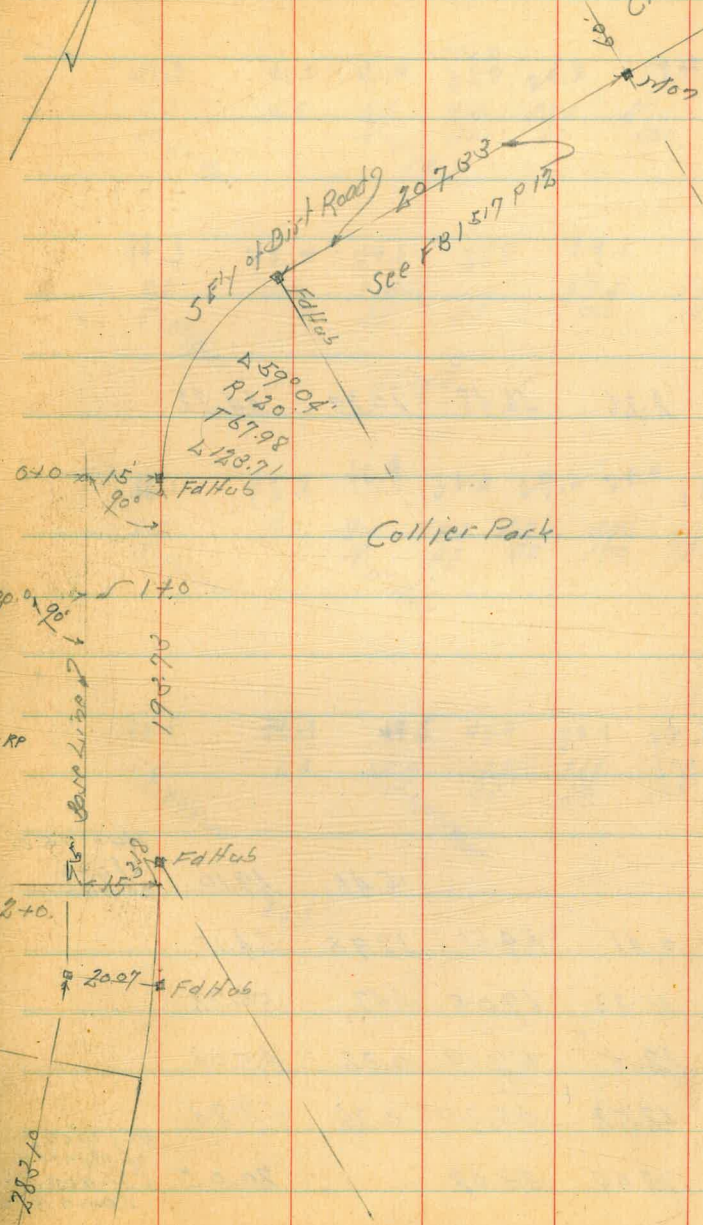
Nov. 19-92.

Sisson B. J. S.  
 Hazard Sommermyal  
 Hiser Begg



Indexed  
 c. S. K.

Clover St. 76

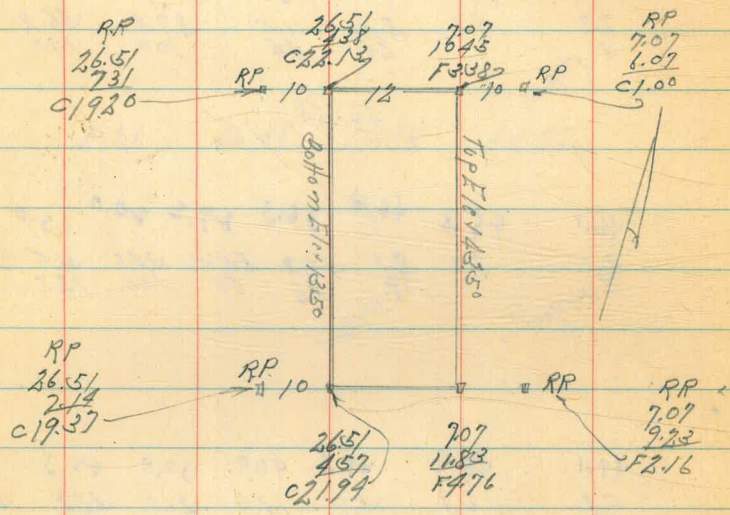


		0.45			
1+50					
1+0					
TP	2.26	46.48	10.29	44.22	
0+50					
0+0					
BM			5.41	49.10	Herb 15 E of 0+0 E. Hub
TP	0.41	54.51	13.95	54.10	
TP	11.33	67.05	1.47	55.72	
TP	12.16	57.19	0.32	45.03	
TP	12.52	45.35	0.26	52.83	
BM	13.04	33.09		20.05	8. W. End of Merion 5 1/2 mi West Pt. Loma 8 mi

47.3	41.0	41.4	37.0	24.2	19.4	9.0
4.6	5.5	5.1	9.5	22.3	27.1	32.5
10 = EY Road		11 = WY Road	130	80	100	140
44.3	43.4	44.1	35.0	19.1	10.3	
2.2	3.1	2.4	11.5	27.4	36.2	
8 = EY Road		24	44	100	130	
			46.48			
46.1	45.8	46.4	36.3	29.2	20.0	3.0 7.2
8.4	8.7	8.1	18.2	25.3	34.5	41.5 47.3
12 = EY Road		19 = WY Road	42	65	100	128 150
49.1	48.1	49.5	40.9	32.9	27.3	14.4
5.4	6.4	5.0	13.6	21.6	32.2	40.1
15 = EY Road		15 = WY Road	33	60	100	130
						54.51

Grades on Cabin

BM	1.47	50.57	49.10	FCHub 040 Ball 4071
TP	1.27	40.01	11.83	38.79



270

46.48

38.5	39.2	38.1	33.5	24.9	18.4	10.0
8.0	7.3	8.4	1.20	21.6	28.1	36.5
8.0		19.0	32	72	100	137
8.0 Road		46.48		19.0 Road		



2 Levels Proposed Road To Con Bin  
 Collier Park  
 Sketch Page 96

Dec 9-48  
 S. S. 100  
 Hazard  
 Hiser  
 Hub 1824  
 040-2800  
 Line

BM	0.66	49.76		49.10	
TP	0.26	38.11	11.91	37.85	
0+0			0.88	37.23	on stub
1+0			6.8	31.3	
2+0			12.3	25.8	
TP	0.46	26.25	12.32	25.79	
+83.10	B.C.		4.54	21.91	on stub
3+0			5.3	21.0	
+20			7.9	18.4	
+30			7.0	19.3	
+50			9.4	16.9	
4+0			15.7	10.6	
+48.91	EC		18.7	7.6	
+90.76			19.0	7.3	
5+0			18.7	7.6	
+50			14.8	11.5	
+50	40' R of 1/2		74	18.9	
6+0			11.0	15.3	
6+0	20' R of 1/2		73	19.0	
TP	11.88	31.13	7.00	19.25	

79

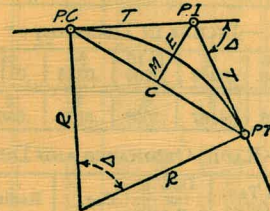
					31.13		
6+50					11.0	20.1	
6+50	30' R of 1/2				54	25.7	
7+0					57	25.4	
7+0	? Lt of 1/2				117	19.4	
+24.82	B.C. Lt				2.98	28.15	on stub
TP	6.16	37.16	0.13		31.00		
+63.3					64	30.8	
8+01.79	EC				425	32.91	on stub
8+50.43	B.C. Lt				448	32.68	" "
+76.61					6.6	30.6	
9+02.79					12.0	25.2	
TP	0.12	25.27	12.01		25.15		
9+28.97					7.0	18.3	
9+55.15					142	11.1	
TP	0.38	13.99	11.66		13.61		
9+81.33					7.9	6.1	
10+07.51	EC				895	5.04	on stub
10+07.51	20' R of 1/2				125	1.5	
10+07.51	50' R of 1/2				120	2.0	
TP	9.39	14.43	8.95		504		
10+50					6.7	7.7	

14.43

11+0		41	10.3	
11+0	30° Rt of 1/2	9.1	5.3	
11+0	60° Rt of 1/2	12.5	1.9	
11+50		4.6	9.8	
12+0		4.4	10.0	
12+0	30° Rt of 1/2	10.3	4.1	
12+0	50° Rt of 1/2	10.3	4.1	
+50		4.5	9.9	
12+67.99	BC Rt	4.85	9.58	on stub
12+67.99	27° Rt of 1/2	9.5	4.9	
12+67.99	? Rt of 1/2	9.8	4.6	
13+06.47		5.4	9.0	
13+94.96	EC=4+9076	7.17	7.26	on stub
13+44.96	20° Rt of 1/2	9.3	5.1	
13+44.96	50° Rt of 1/2	9.2	5.2	
TP	11.75	23.69	2.49	11.94
TP	11.78	35.43	0.04	23.65
TP	10.02	15.15	0.30	35.13
TP	7.81	51.14	1.82	42.33
B.M.		2.05	49.09	Starting 99.10

# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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## CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of Curve= $D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)

Tangent= $T = R \tan \frac{\Delta}{2}$  (3) Length of Curve= $L = 100 \frac{\Delta}{D}$  (4)

Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$  (5)  $= R \text{vers} \frac{\Delta}{2}$  (6)

External= $E = T \tan \frac{\Delta}{4}$  (7)  $= R \div \cos \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)

Long Chord= $C = 2 R \sin \frac{\Delta}{2}$  (10)  $\Delta =$  Central Angle

## EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8\frac{1}{2} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C.—Sta. P. I.— $T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T.—Sta. P. C. +  $L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance =  $158 - \text{Sta. P. C.} = 54.50$ , hence offset =  $7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft.—(in minutes)  $.3 \times C \times D^\circ$  or—defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve =  $3 \times 54.5 \times 8\frac{1}{2} = 136.2'$  or  $2^\circ 16.2'$ , or  $= 2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 91.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 91.27$  and from Table V correction = .10 or  $E = 91.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .

4.80  
 11.05  
 15.85  
 15  
 6.5  
 7.6  
 6.65  
 14 2  
 11.47  
 14237.10  
 14448.6  
 74 4  
 145230  
 21+24  
 21+06  
 60.2  
 135  
 615.5  
 350  
 15  
 50  
 189.25  
 12.67  
 201.92  
 193.77  
 8.15  
 179.60  
 125-14  
 54-46  
 37 80  
 4.75  
 33.09  
 20.8  
 18  
 80.8  
 6.55  
 4199  
 503  
 56.16  
 12.4  
 5.6  
 186  
 1152  
 540  
 612  
 1152  
 614  
 538  
 33  
 128  
 206  
 10.3  
 124  
 227  
 330  
 13.1  
 2.7  
 15.8  
 12.4  
 2.7  
 15.3  
 359.43  
 6.99  
 352.44  
 363.75  
 1.49  
 365.20  
 12.93  
 352.27  
 6.24  
 3.8  
 11.4  
 15.6

6025  
 299.2

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.4	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.