

1562

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to the inch, Center Line Red.
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BOOK. Left Hand Page as in this
Book, Right Hand Page 8x8
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Aley Blk 164	Colo 7410	Univ. Hts	16
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Boston	28 to 30		24
Dickens	Evergreen to M.H.T.		40 also 74
Emerson	Rosecrans to Scott		49 also 76
Ibsen	Rosecrans to Evergreen		52
Beryl St.	Cass to Dawes		56
Aley Blk 190	Ocean Beach		59
Hugo -	Rosecrans to Willow		Page 62

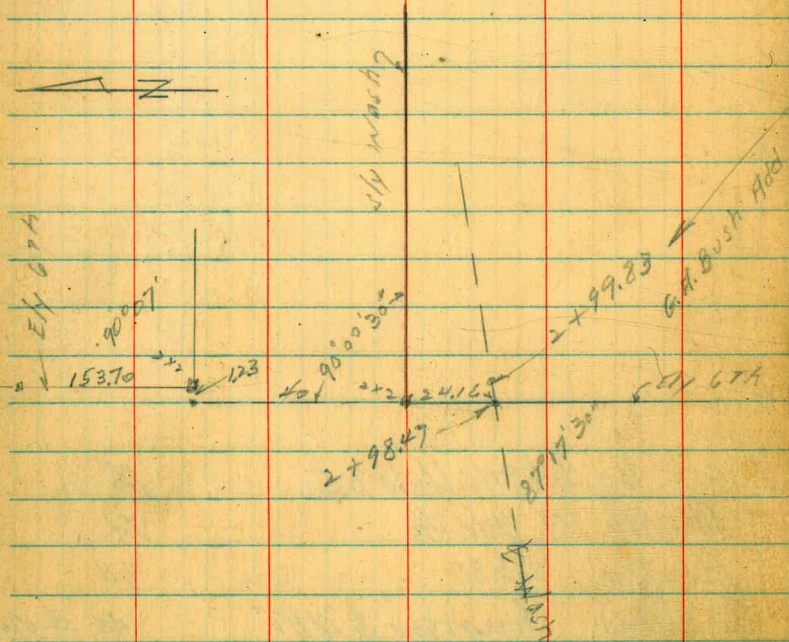
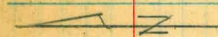
Indexed
C.S.K.

R.O.W. Ties for Washington St. EXT.
5th St. Ely.

Fleisher Add.
Ely 6th

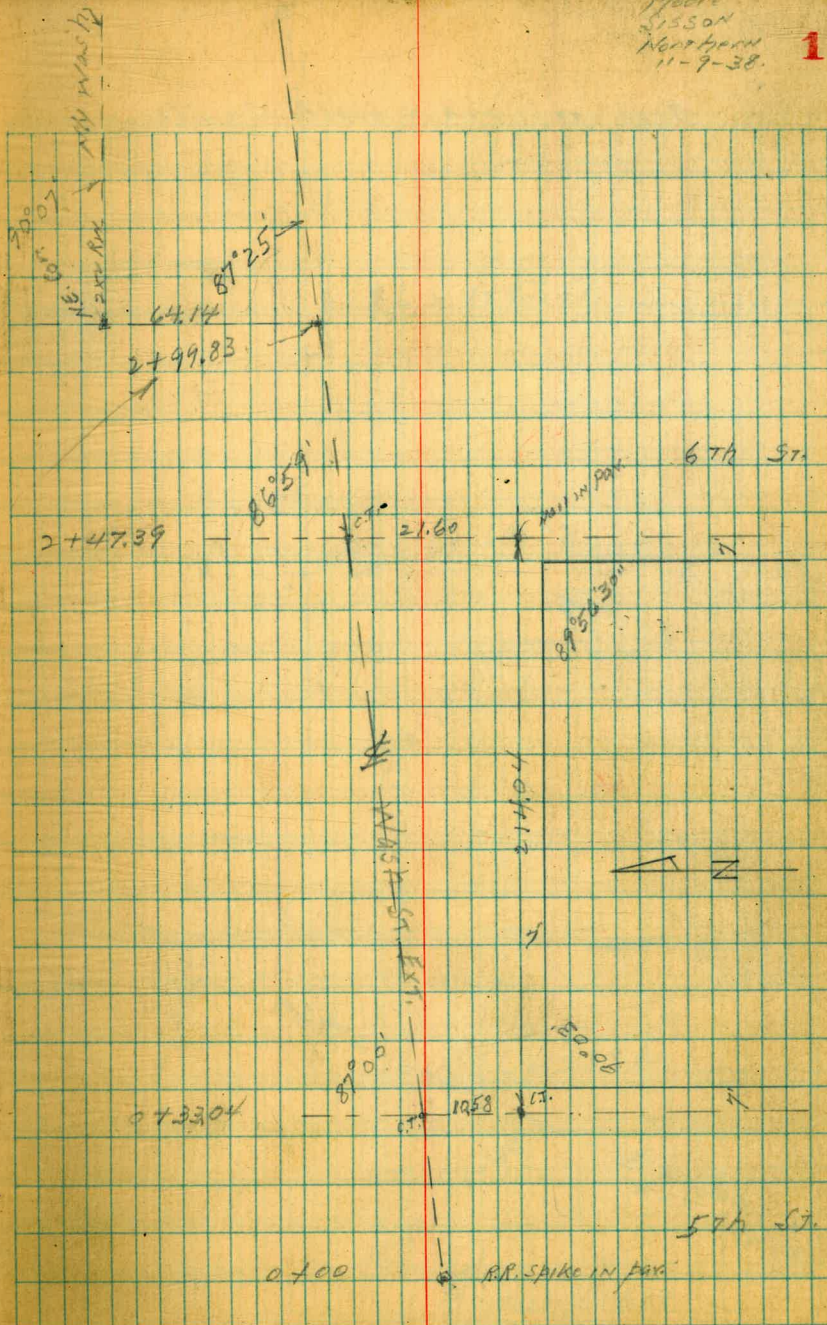
old 2nd RR
to
5th St
153.70

153.70



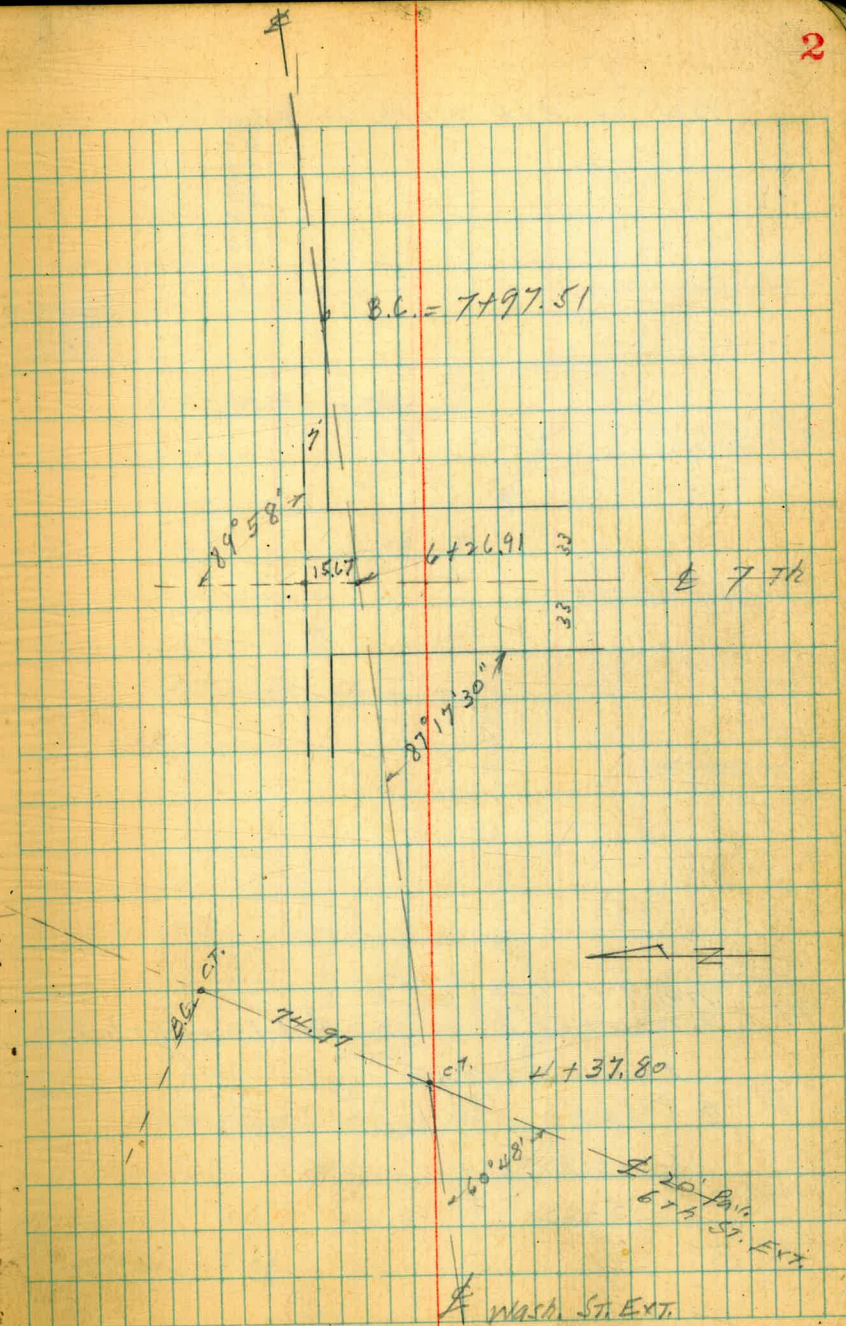
1700
Lisson
Northern
11-9-38

1



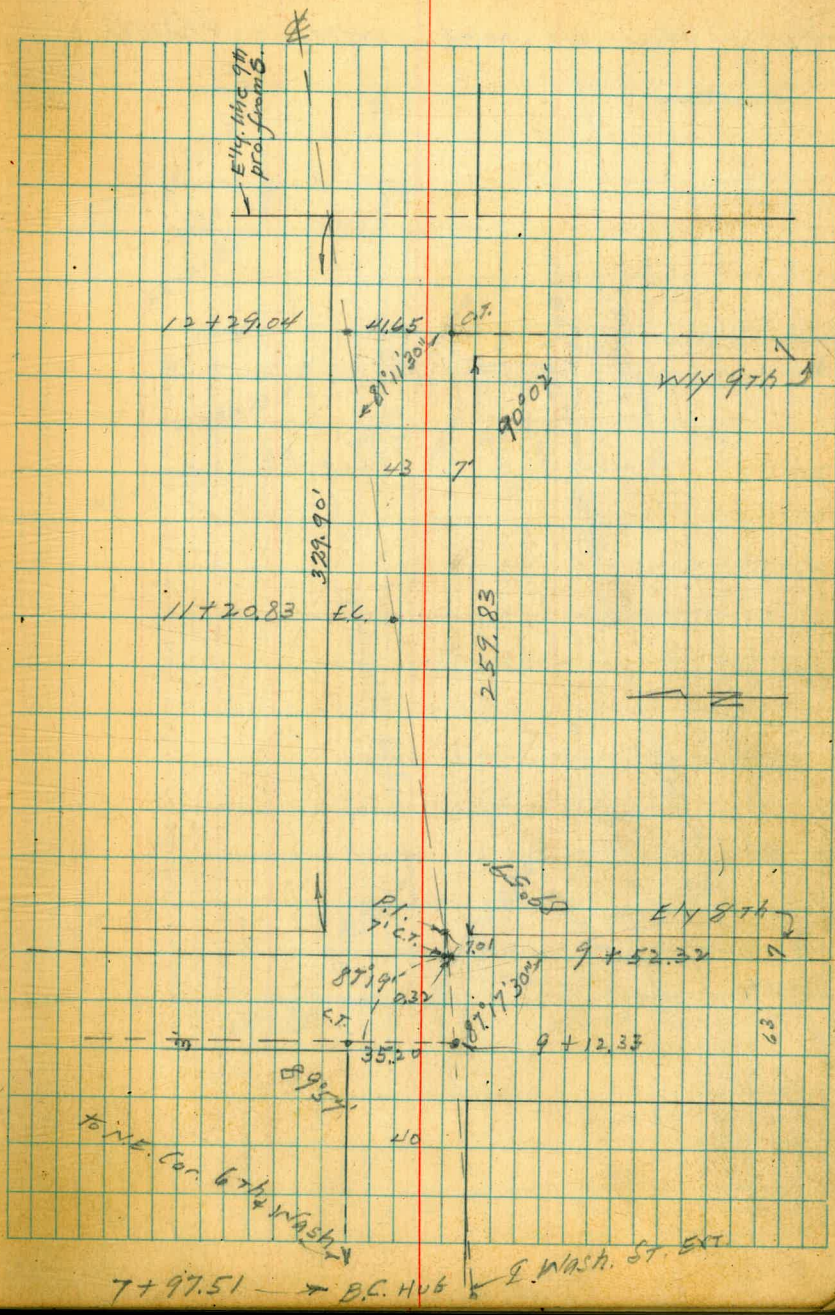
Ties at 7th & Wash. St. EXT.

2

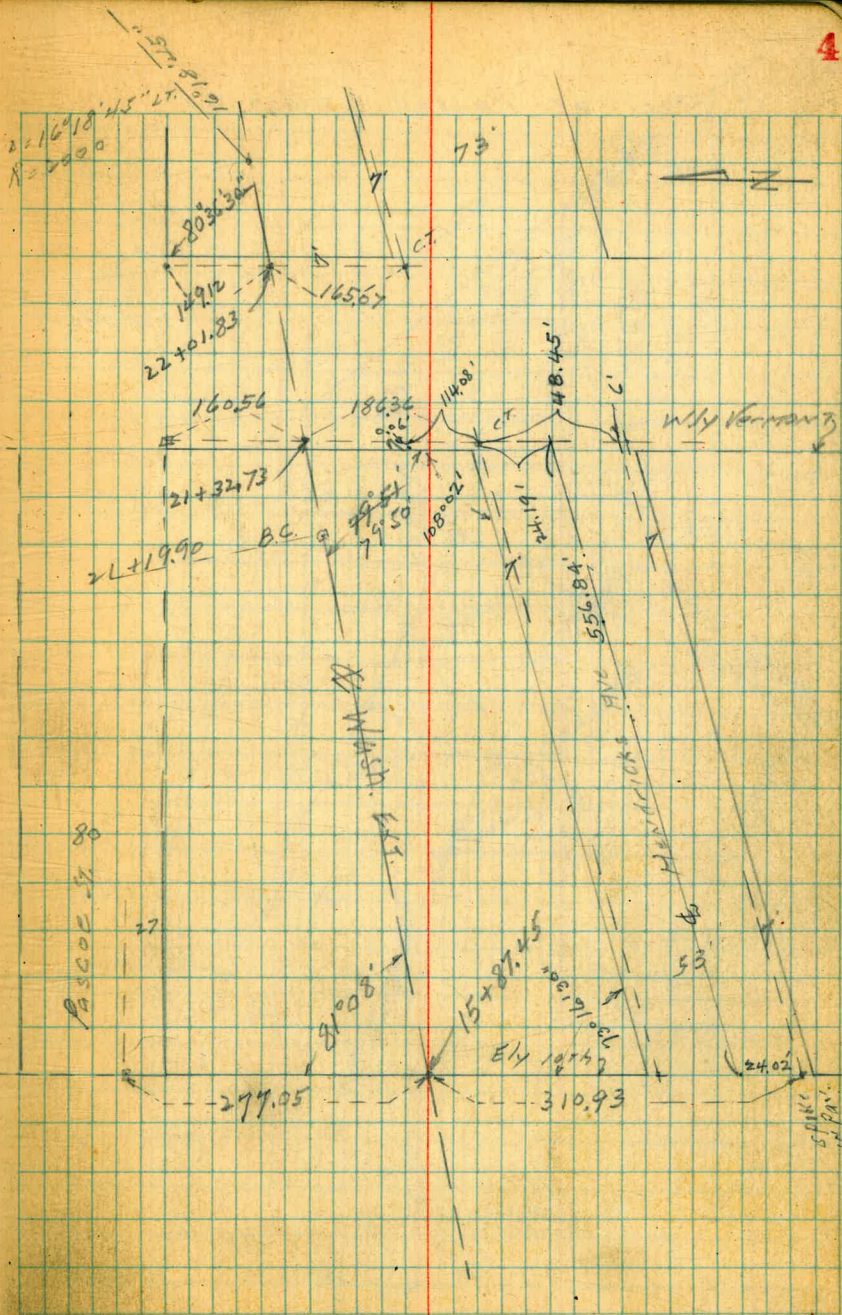


TIES ON 8th & 9th at Wash.

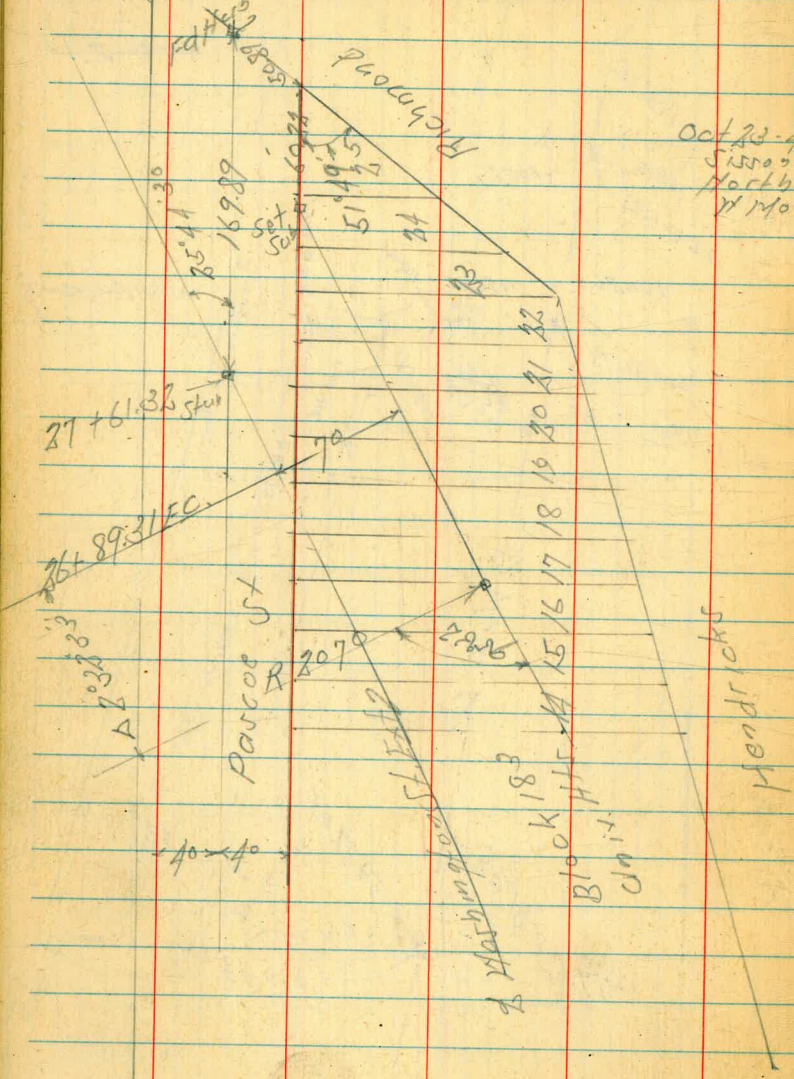
= STA. 9+59.33
 P.I. = S 7 Line of Washington & E.L. of 8th St.
 A = 6°10'30" LT
 ΔP = 3000
 T = 161.87
 L = 323.32



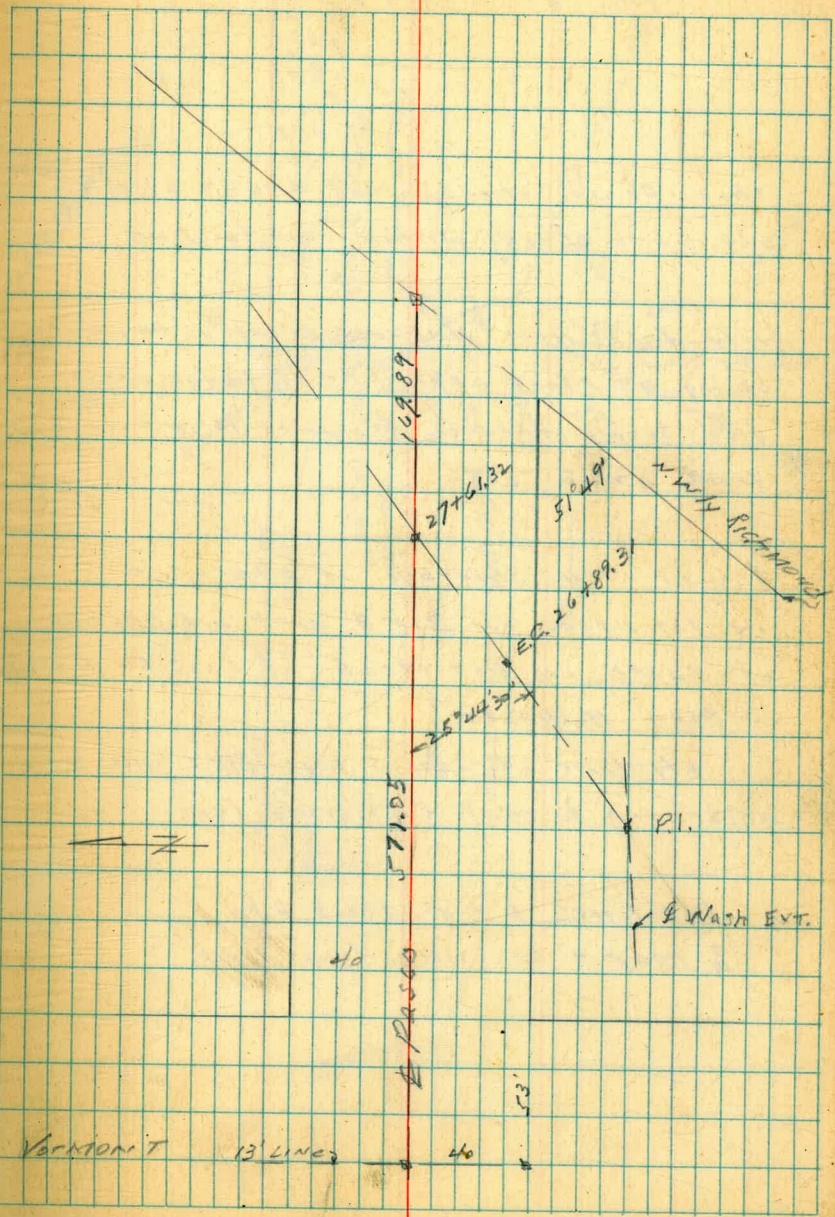
Ties at 1076, Vermont & Wash. Etc.



Ties at Pascoe + Wash. St



Oct 23-40
Sisson
Northberg
H Moore



Vernon T 13 Lines 40 53

Moore
11-30-38

TICS at 5th + Wash St.

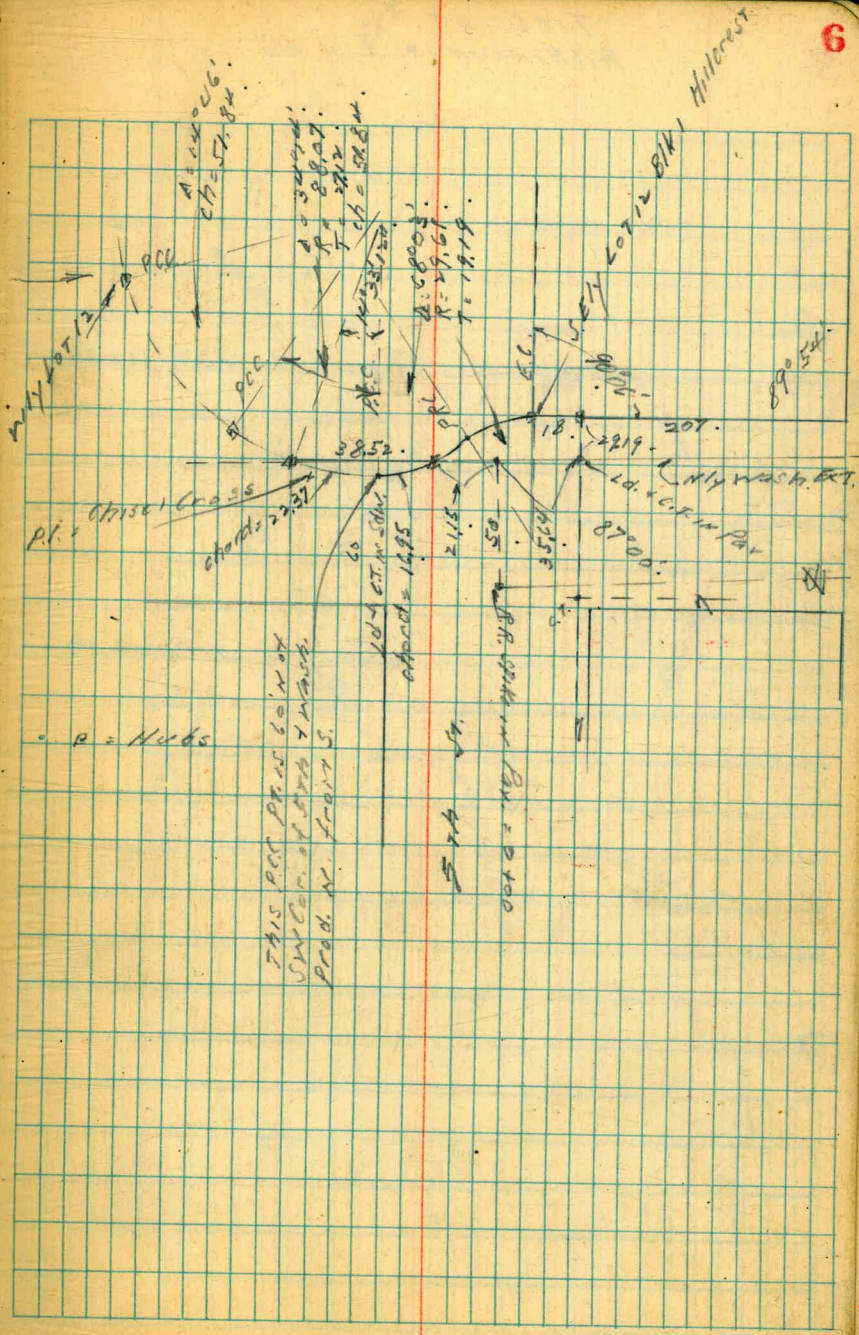
This point checks Map 4. 1069 also
Ely curb checks within 0.10 for line

Nly front here, Hillcrest Drive is hay wire,
being at most, approx. 4.5' too far west,
also between curbs, distance is in excess
from 0.7' to 2.5'

Result is a shortage of approx. 4'
in lot meas. in BIK 3 and an excess
of same, in lot meas. of Lots 5-11 incld.
in BIK 1 Hillcrest.

Ely line of Lots 5 to 11 BIK 1 are O.K.
according to Map 4 existing fence lines.

LOT LINES E 4 in check O.K.
to Map 4 existing fence lines.

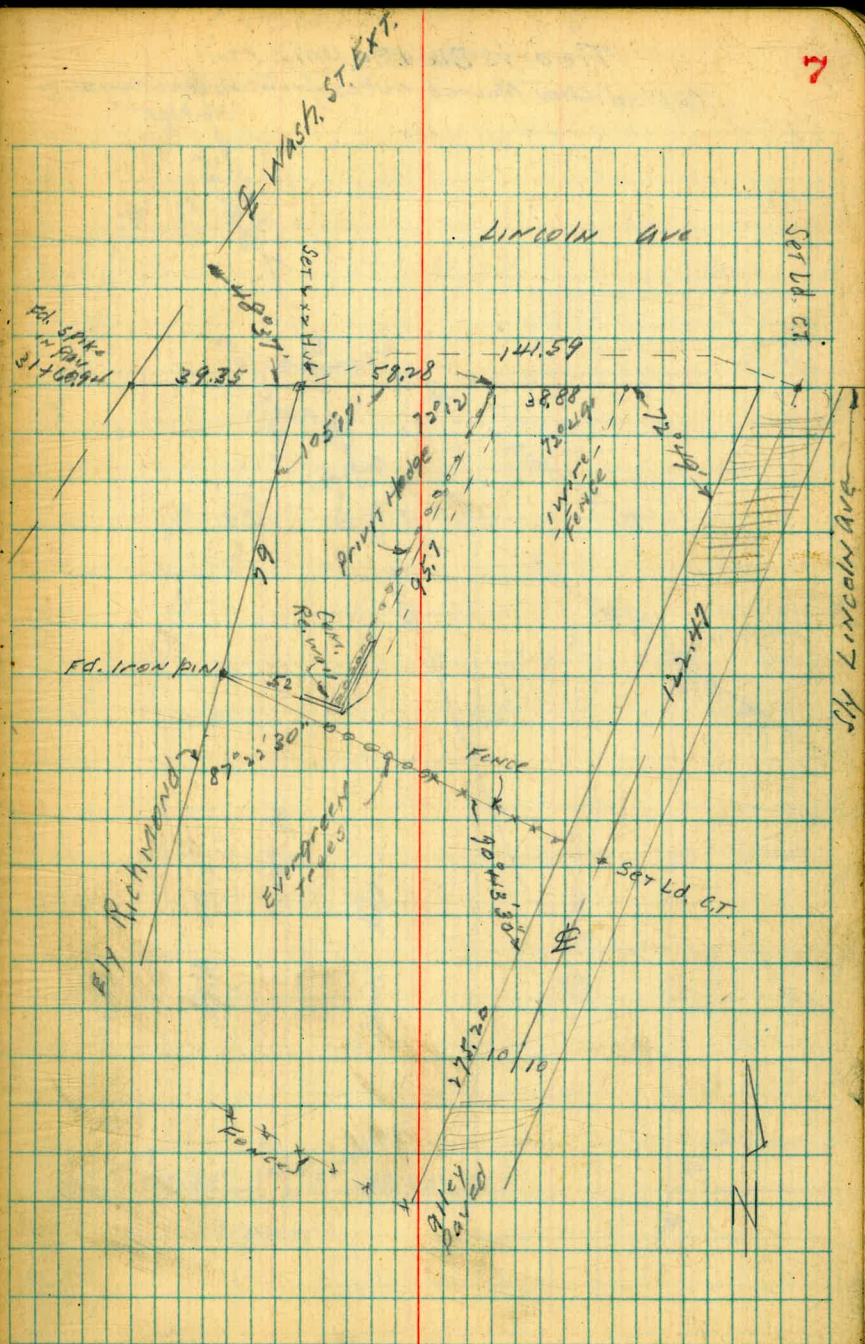


TIES AT
Richmond + Lincoln

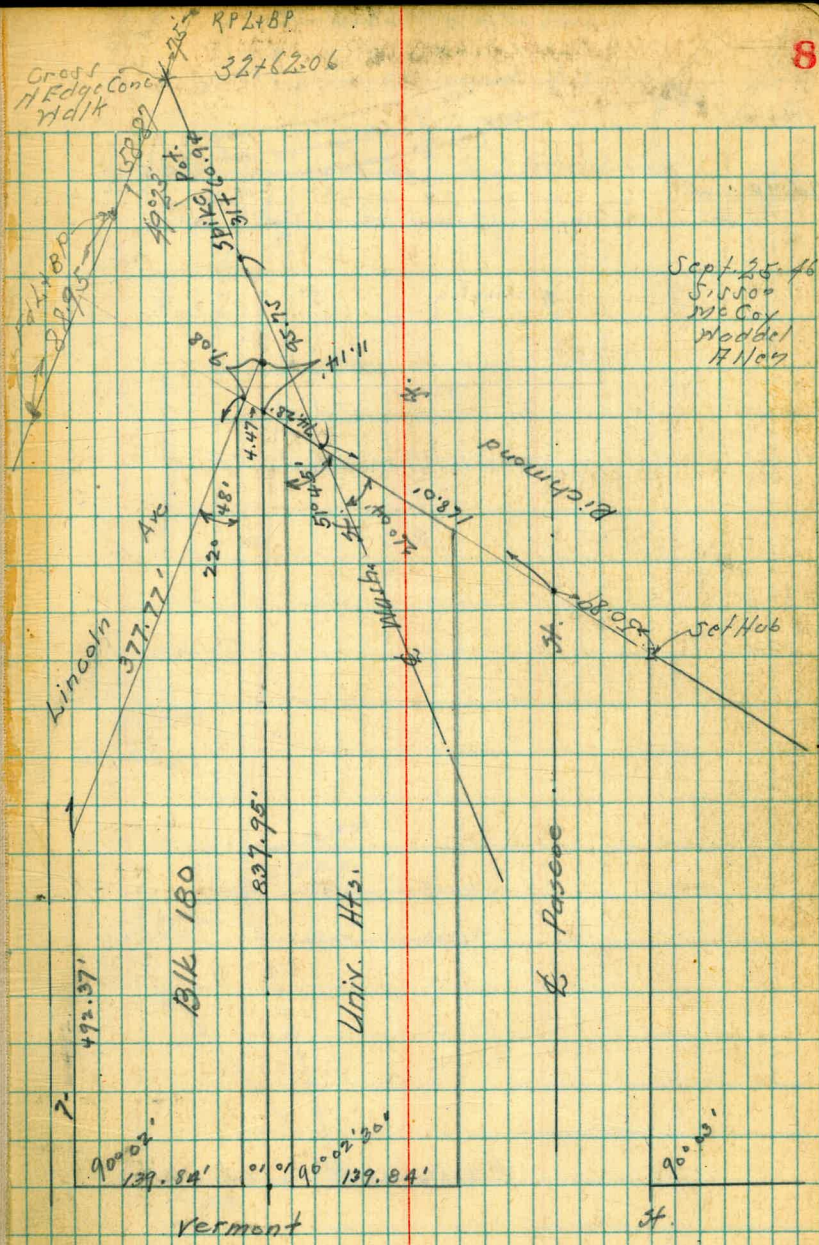
Moore

1-11-39

STATE SET SPIKE IN PAR. P.O.T. 31+60.94

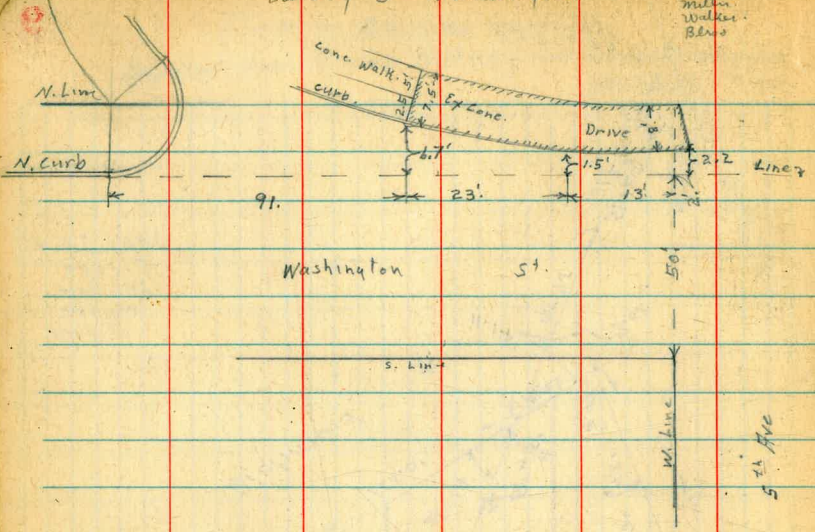


Ties to Blk 180, Univ. Hts.
 Copied Chas. Moore's notes from memorandum
 Mohler

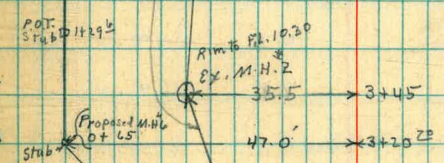
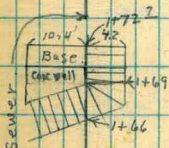
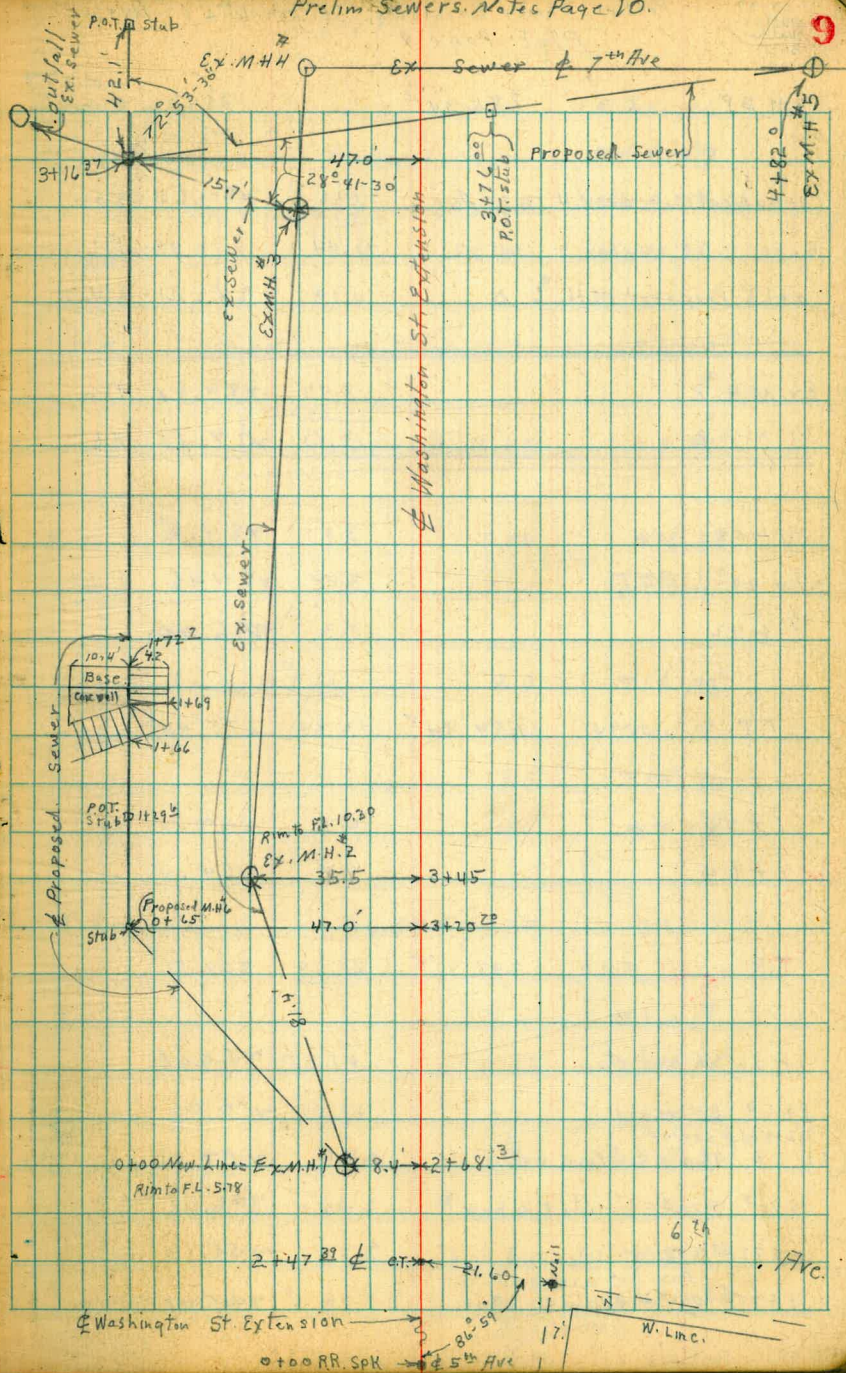


Survey 5th + Washington

3-23-39
Mellin
Walker
Bemis



Prelim Sewers Notes Page 10.



0+00 New Line Ex. M.H. 1
Rim to FL - 5.78

Washington St Extension
0+00 RR. SPK
5th Ave
W. Line

3-23-39
Miller
Walker
Bliss

Prelim. Sewer Washington St. bet. 6th & 7th Aves.
Plat Page 9

B.M. B.P.	2.32	286.34 ✓	284.02	S.W. 5 th & Washington
0+00 New line - Ex. M.H. in 6 th Ave	5.66	280.68	Top	
		5.78 below		
0+00 " " " " " " " "	11.44	274.90	F.L.	
		274.98		
0+65 Proposed M.H. # 6 Δ	4.13	282.21	± Hub	
Ex. M.H. # 2	3.53	287.81	Top	
		10.30 below		
" " " # 2	13.83	277.51	F.L.	
1+00	3.9	287.4		
1+29 ⁶ P.O.T.	3.88	287.46	± slab	
1+42	10.3	276.00		
T.P.	0.94	274.34 ✓	12.94	273.40 ✓
1+55	2.1	277.2		
1+64	9.8	264.5		
T.P.	0.20	248.71 ✓	25.83	248.51 ✓
1+66 w. end step	+1.35	250.06		
1+69 E " "	+1.35	250.06		
0.2 Nat. & sewer				
1+69 Top S. End. Conc. wall	+4.0	257.71		
1+70 ⁵ S. end - W. side conc. base	2.65	246.06		
1+72 ³ S. End E. side conc. Base	2.78	245.93		
1+72 ⁸ Pav. at bottom of steps	3.70	245.01		

248.71

10

1+83 parmt. Not much good	3.75	244.96		
1+96 ⁶ W. Edge Pav	4.62	244.09		
2+19 ⁸ E. Edge 20' conc. strip pav.	5.45	243.76		
2+72	6.0	242.71		
T.P.	0.58 ✓	236.58 ✓	12.71	236.00 ✓
T.P.	1.26	225.16 ✓	12.68	223.90 ✓
Ex. M.H. # 3	8.80	216.36	Top	
	8.40 below			
" " " "	17.20	207.96	F.L.	
		207.99		
3+16 ³⁷ New M.H. # 7 Δ	8.9	216.26		
3+20	10.0	215.16		
3+36	9.5	215.70		
3+46	4.6	220.6		
T.P.	12.68	236.58 ✓	1.26	223.90 ✓
3+69	5.0	231.58		
3+76 ± P.O.T. stub	4.43	237.15		
4+00	4.4	237.70		
4+46	1.3	235.30		
T.P.	10.41	245.42 ✓	1.57	235.01 ✓
4+53	7.0	238.47		
4+82 = Ex. M.H. # 5 ± 7 th Ave	3.00	247.47		
	5.31 below			
	8.31	237.11 = 237.07		

Moore

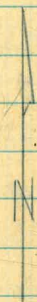
Indexed
C.S.K.

3-27-39. Survey of Lots 49-76

G.H. Bush Add.

+ Location of Bldgs.

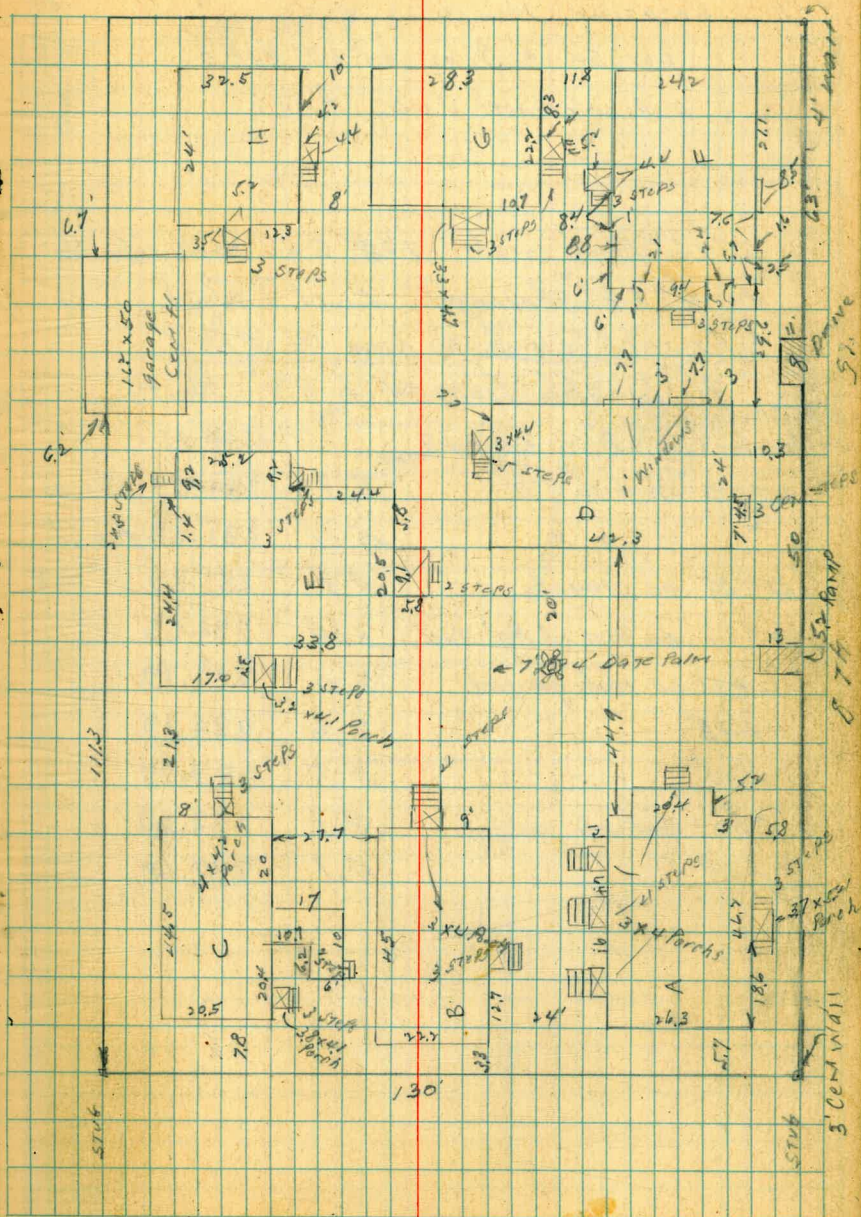
See Con 876 + Washington



WASH.
See 5653-L

ST

11



indexed
c.s.k.

LOCATION House

Lot 44 + 5 1/2 of 65 BK B

J.B. Williams Sub. #855

2" X 6" Floor joists 1'-8" C.C. North + South

1- 4" X 4" Stringer East + West.

LEVELS ON South line Pt. of Way.

Washington From W. cb 8th - West

B.M. at top of

Washington + 8th 2.38 286.79

289.41

0+00 = West cb 8th 5.70 281.09 Paving

" " " " 5.11 281.68 top cb.

0+10 on ground 4.9 281.89 at Wall

0+10 on top of Ret. Wall 1.14 284.65

0+11 on Nat. ground 2.0 284.79

0+45 2.6 284.19

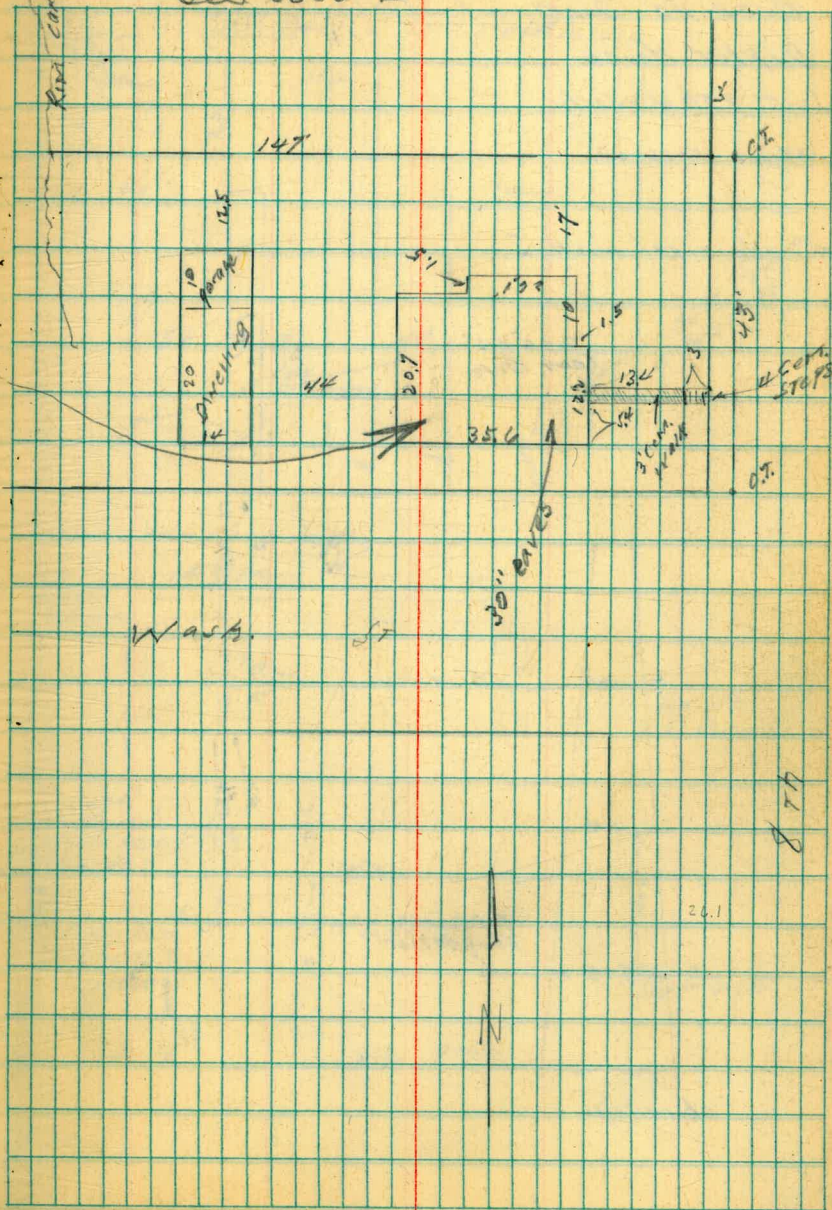
1+00 3.5 283.29

+30 = East side garages 4.1 282.69

1+45 4.1 282.69

12

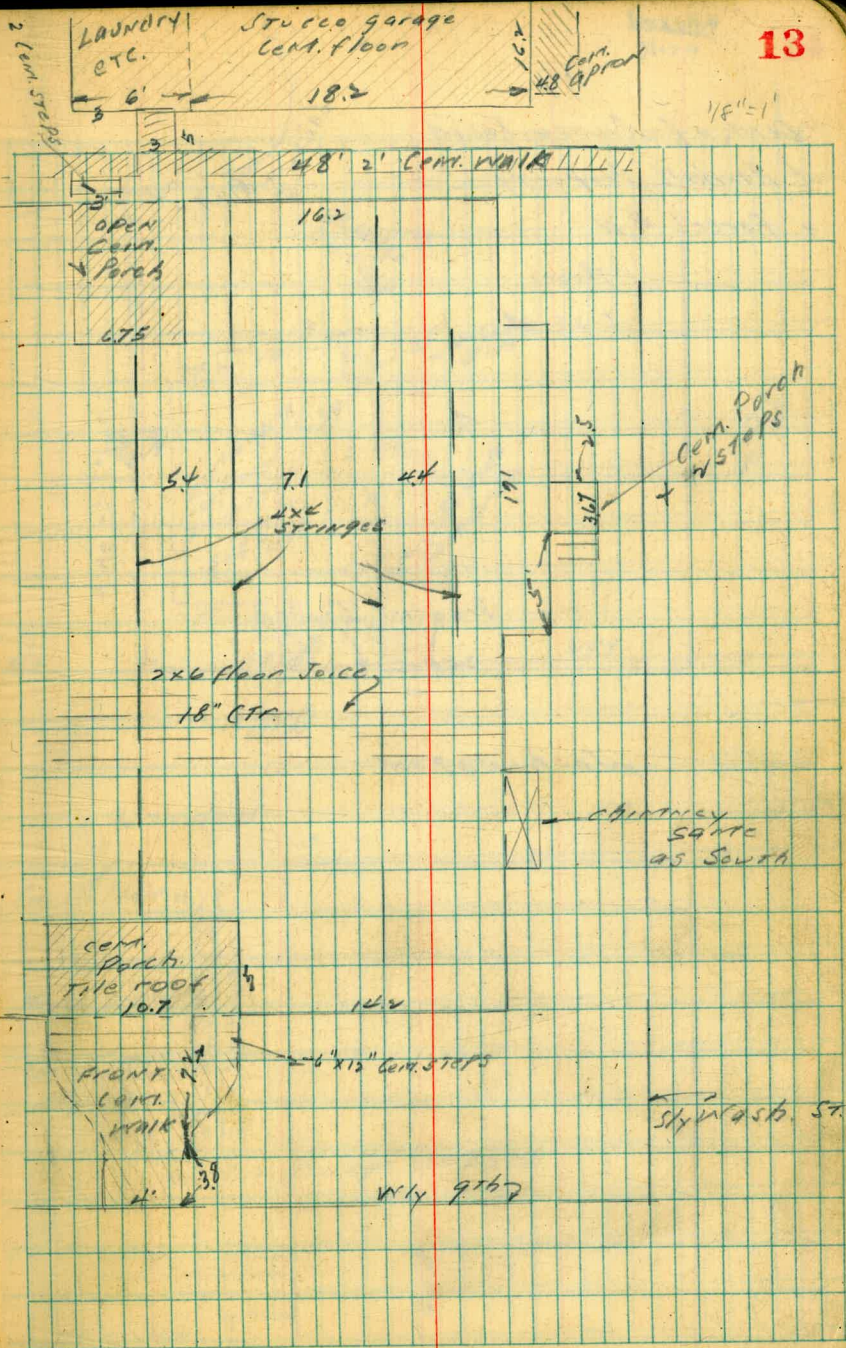
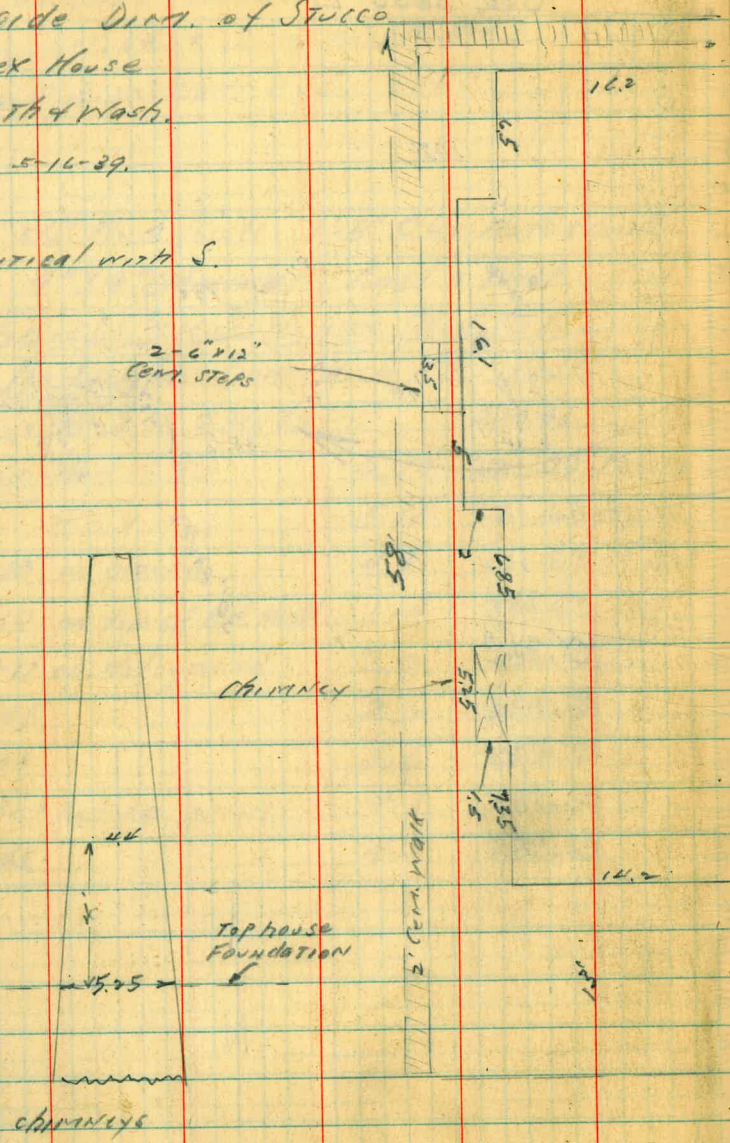
See 5653-L



Indexed
C.S.K.

Outside DIM. of Stucco
Duplex House
Sw. 9th & Wash.
Moore 5-16-29.

N. identical with S.



1/8" = 1'

W 1/4 9th & Wash. St.

Indexed
asite

DIM. of Suzzo Resid.
of Randall Property
Parcel # 11

Moore
5-26-39

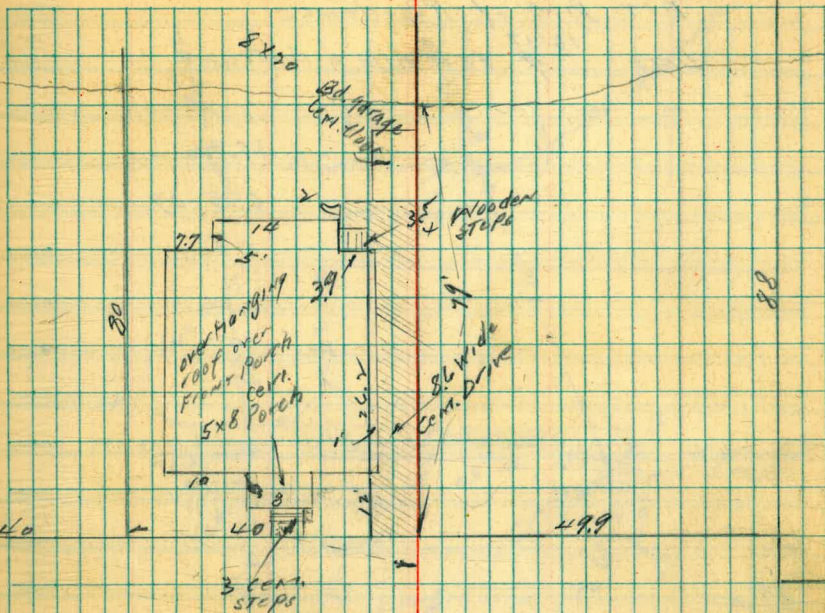
876



90
W. 40' of Lot 43

PRESENT LINE
200

WASHINGTON



to be moved

Con Duplex =	13
	12
	17
	17
	17
House on alley	91.7
	16.3
Laundry under	16.3
Laundry Cont.	16.5
Fire Sta =	0.0
10 /	221.0

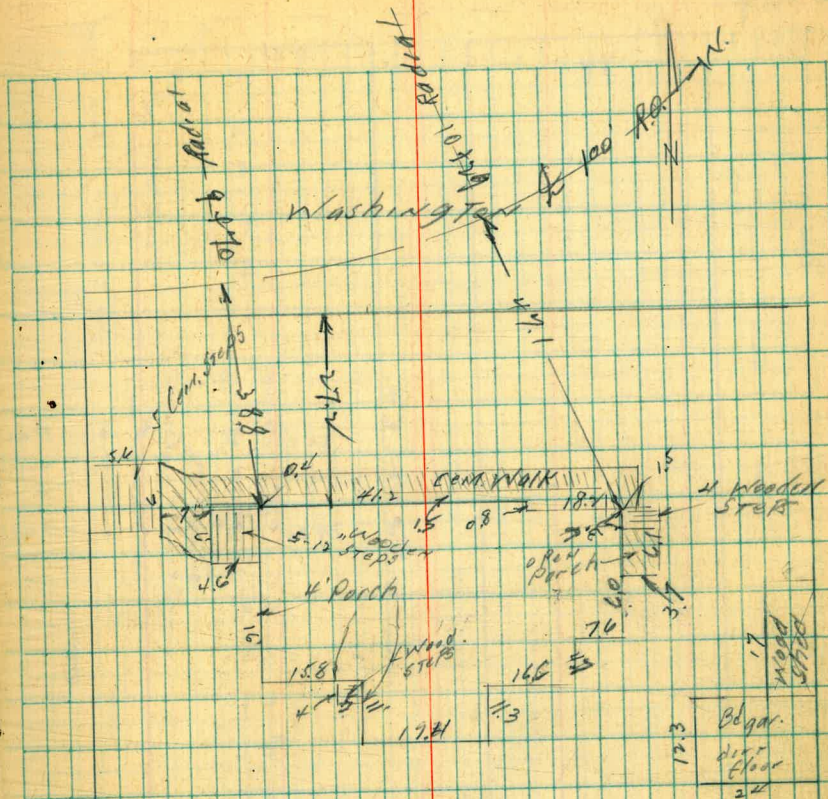
22.1 - Average Set Back

FIRE STA.
on LENCE

92A

EXT. DIM. of Residence
 LOTS 16-17
 9 Estrella & Capron's

Morse
 6-2-29.



2" x 4" underlayment

E + W 2" x 4" Springers 6' Centers

MAIN HOUSE + S 2" x 8" H. joice 3' "

Porch " " 2 x 6 " " 3' "

8 TH

alley

No CONC. FOUNDATION

EXT. Shingled over Vert. Bds. Pine Floors
 House approx 45 years old.

7-11-39
Miller
Walker

Survey Lots 9 & 10 B/M. 164. 2H.
E. side 30th Bet. Lincoln & Polk.

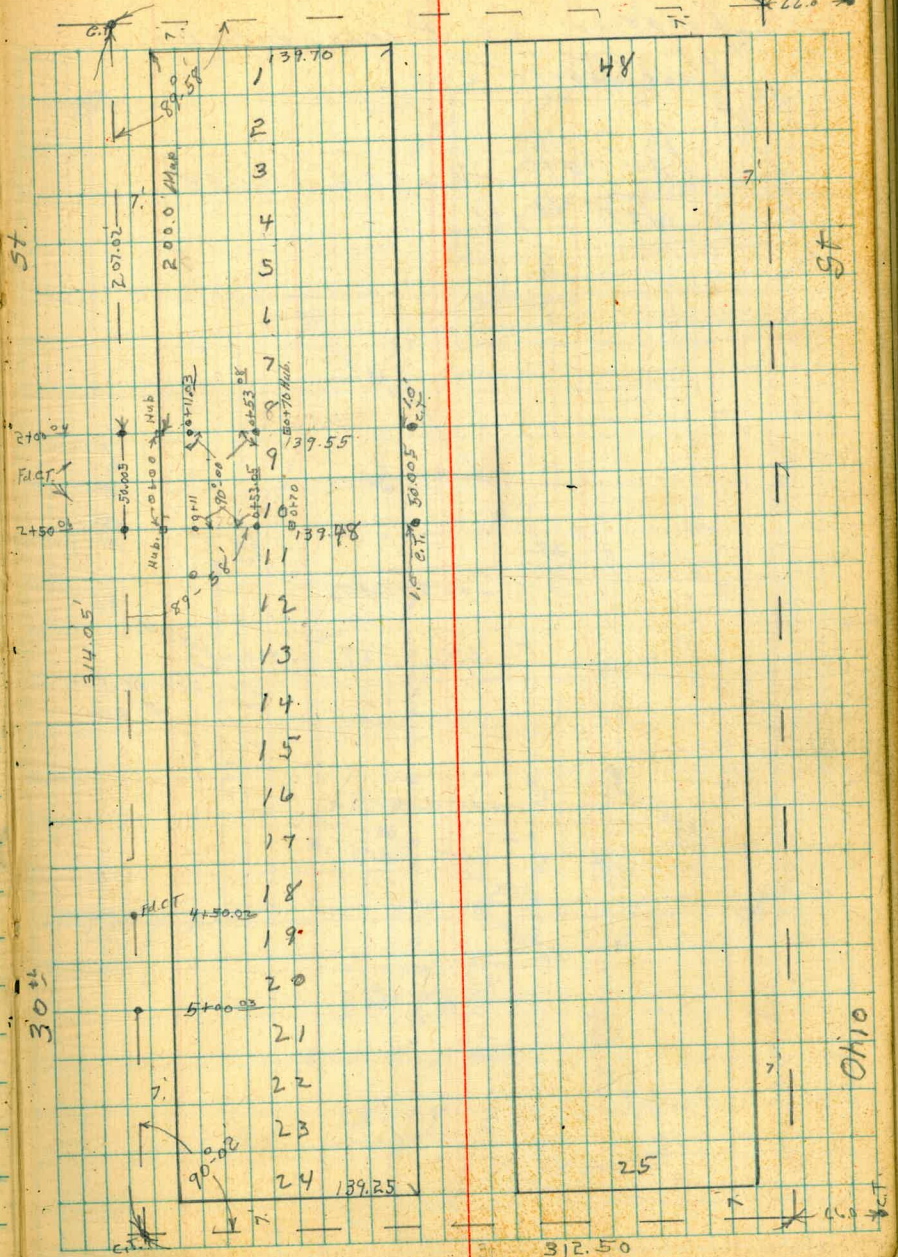
Polk.

Ave

16

313.40

26.0



Lincoln

Ave

Ohio

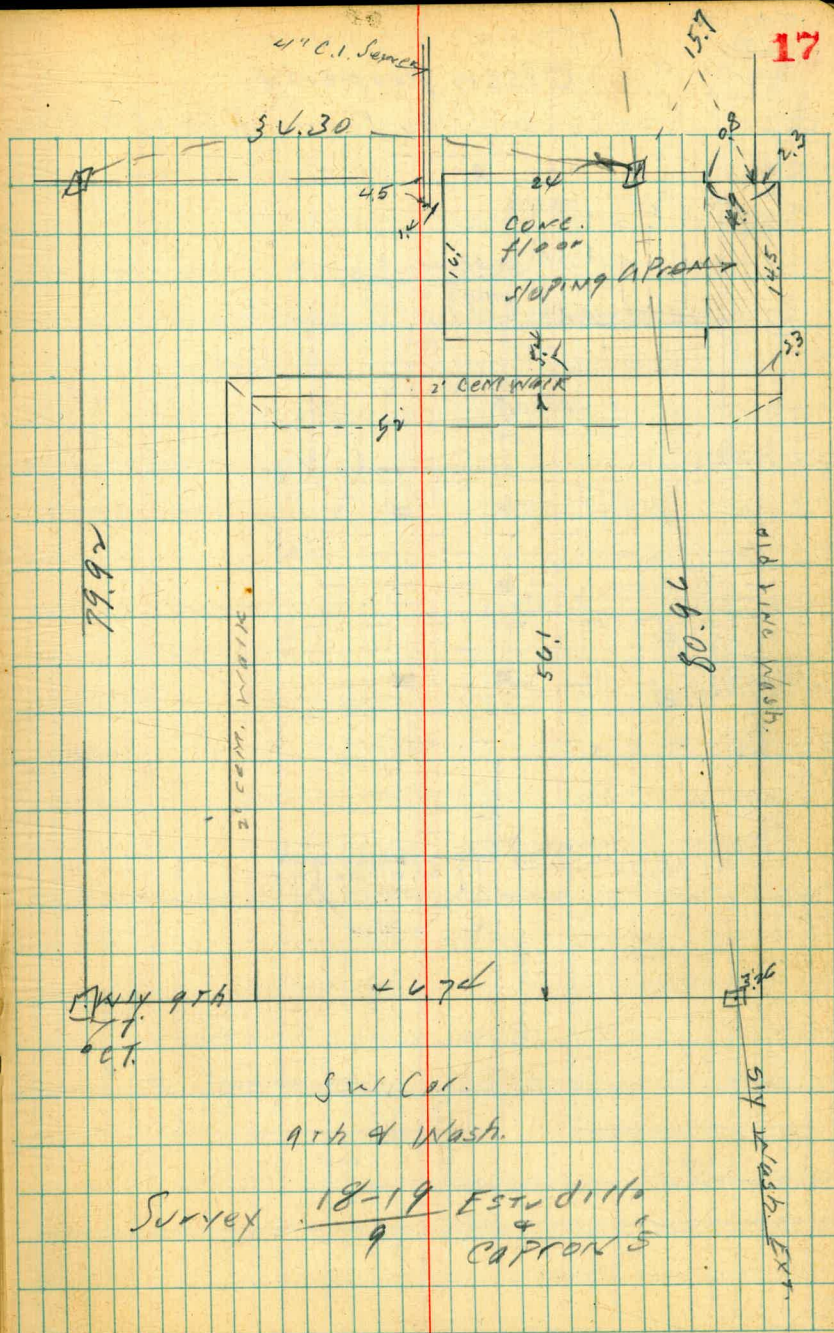
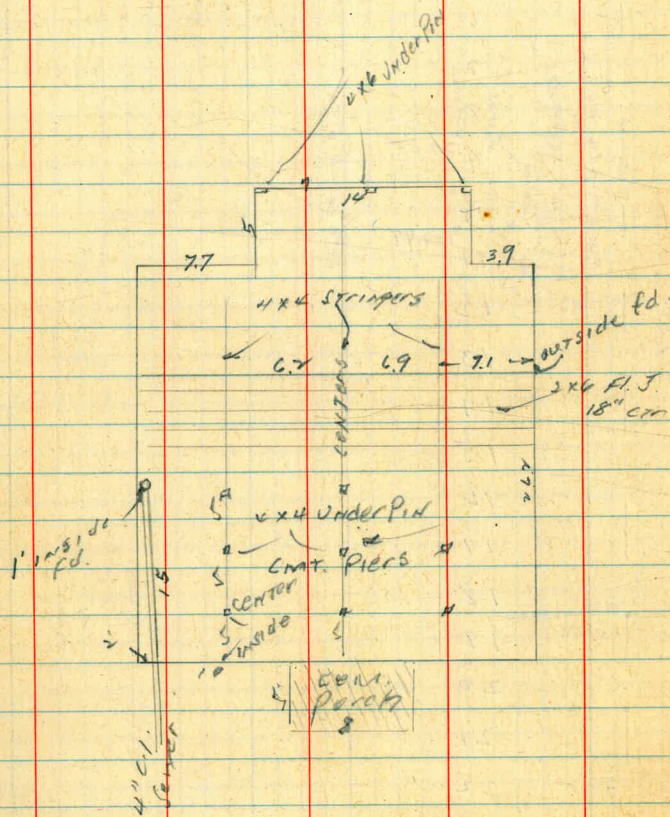
St

St

30th

Location of Piers, under Pin
Floor Joice etc.

Randall Stucco House
See P. 14



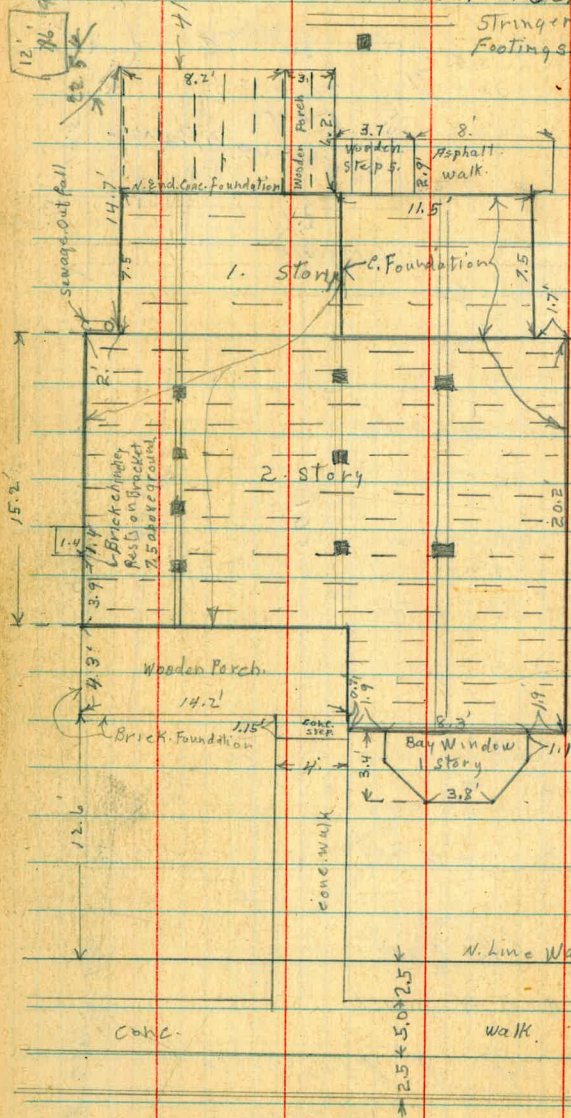
Survey 18-19 Estudillo
9 CAPRON'S

8-30-34
miller
Walker
Bliss

House at 836 Washington St.
Olson Property

Dotted Lines Floor Joists 2x6 - 18" ctrs.

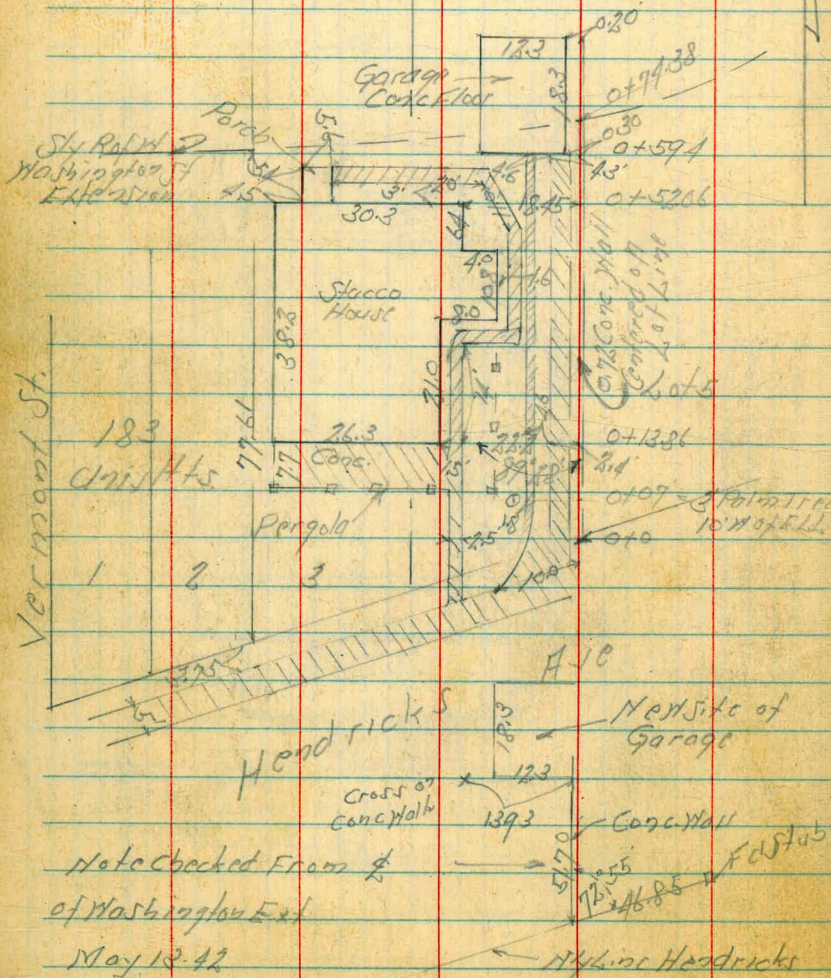
Stringers 4x4
Footings concrete



Location of Improvements
Lots 3-4 Block 183 Units Hts.

Indexed
C.R.K.

Dec. 4-40
Survey
Hortberry
W Moore



Note checked from
of Washington Ext

May 12-42
J. S. 5007
Moore

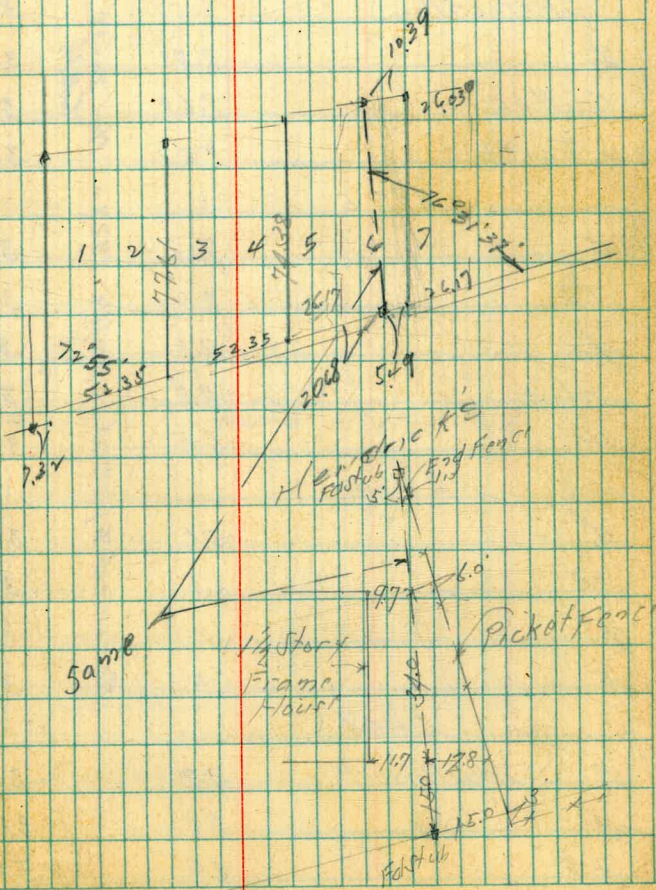
Indexed
C.R.K.

Survey of Lots $\frac{1-7}{183}$ U.H.

10-19-39

for Eddie Brooks

VERMONT ST.



Jan 4-42
Survey
Hortberry
W Moore

same

117
128
150
Folchub

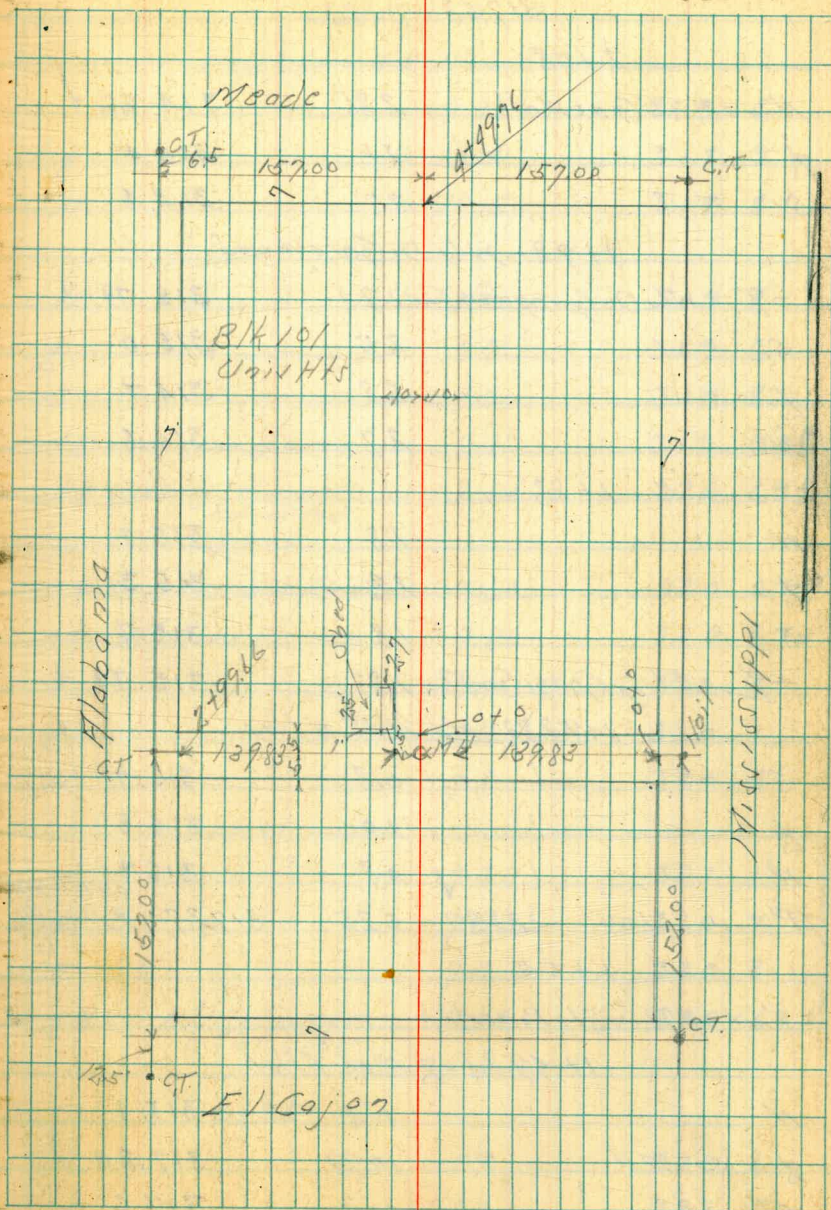
10 Alley Block 101 Unit Hqs
 Between Alabama-Mississippi
 El Cajon - Meade
 Cross Section E + N Alley

BM	10.95	317.52	306.57	NEBP El Cajon Alabama
2+1966 = F Cb Alabama				
S on Pav		9.57	307.95	
N " "		9.40	308.12	↓
2+9966 = E L Alabama				
N Top Cb		8.43	309.09	↓
Gutter on Pav.		8.59	308.93	↓
L " "		8.81	308.71	↓
Gutter " "		8.69	308.83	↓
S Top Cb		8.57	308.95	↓
2+95				
S		7.3	310.2	
+2		8.0	309.5	
L		8.0	309.5	
+3		8.0	309.5	
N		6.5	311.0	
2+75				
N		5.6	311.9	
+2		6.6	310.9	
L				
S		6.5	311.0	
2+48				
S = S Edge Power Pole		4.2	313.3	
L		4.8	312.7	
+2		4.9	312.6	
N		4.3	313.2	

Reduced & plotted in profile 1927 - Nov 20-39
 CBH.

Indexed
 C.S.K.

Nov 18-39
 S.D. 507
 Northburg
 OS Board **21**



31752 ✓

2+08

H	2.5' Conc Walk	2.86	314.66 ✓
S		31	314.4
S		27	314.8

1+98 - Wly Do Garage conc S

-9'	Wly Do Garage Conc Floor	1.73	315.79 ↓
S		2.5	315.0
S		2.8	314.7
H		2.7	314.8

1+82

H		1.8	315.7
S		2.2	315.3
S		1.8	315.7
+9'	Wly Do Garage Conc Floor	1.80	315.72 ↓

1+59.83 = Wly H+S Alley

S		0.8	316.7		
S		1.0	316.5		
H		0.8	316.7		
TP	11.00	322.27	0.25	317.27	0.25 RIMMH 2 H+S Alley

1+55

1' H of SL = Sky Power Pole

1+49.83 = 2 H+S Alley

H		11.2	317.1
S	0.2 MH	10.99	317.28 ✓
S		10.7	317.6

32827 ✓

1+29.83 = EL H+S Alley

S		9.9	318.4
S		10.4	317.9
H		10.5	317.8

1+18

H		8.5	319.8
S		8.7	319.6
S		8.5	319.8

+5' = Wly Conc Apron 8.30 319.97 ✓

+8' = Wly Do Garage Conc Floor 7.58 320.69 ✓

1+10

-8' 02 Garage Floor 7.60 320.67 ✓

-7' Fly Conc Apron 7.80 320.47 ✓

S 7.9 320.4

S 8.2 320.1

H 7.8 320.5

1+01

H 7.2 321.1

S 7.6 320.7

S 7.5 320.8

+8' = Fly Do Garage Conc Floor 7.60 320.67 ✓

0+95

S 5.9 322.4

S 6.9 322.3

H 5.7 322.6

328.27

0+50

N	4.7	323.6
E	4.9	323.4
S	4.9	323.4
0+25		
S	4.3	324.0
E	4.1	324.20+03
N	4.0	324.3 ^{0.2 N of FL} _{5 ft from Pole}

0+0 = W. of Mississippi

N Top Cb	3.27	325.00 ✓
Gutter on Par	3.69	324.83 ✓
E " "	3.90	324.37 ✓
Gutter " "	3.85	324.42 ✓
S Top Cb	3.58	324.69 ✓

0-14 = W. of Mississippi

S 07 Pav	4.22	324.05 ✓
N " "	4.07	324.20 ✓

JP 8.95 328.27

317.27

0+1111 P₁₁₁₁
2 N 1111 P₁₁₁₁

0+25

N	9.0	317.2
E	8.2	318.0
+7	8.2	318.0
F	7.9	318.8

0+51

F	6.8	319.4
E	7.1	319.1

+7.2 = W. of Power Pole

N	7.7	318.5
---	-----	-------

0+98

N	6.0	320.2
E	5.3	320.9
+5	5.3	320.9
F	4.4	321.8

+2 = E. Garage Conc Floor
Exit Entrance
1+12

2.5 E of W. = W. of Power Pole

1+42

-1.2 = E. Garage Dirt Floor	3.7	322.5 ✓
F	4.1	322.1
E	4.3	321.9
N	5.1	321.1
+7 = E. Garage Conc Floor	5.20	321.02

326.22

1+78

-6	= 1/2 Garage Conc Floor	4.22	321.95	✓
-4	= 1/4 Conc Apron	4.26	321.96	✓
H		4.0	322.2	
L		3.2	323.0	
F		2.9	323.3	

2+15

F		2.2	324.0	
L		2.4	323.8	
H		3.0	323.2	

2+30

2.4 F of H.A. - 1/4 Pav. Pk

2+40

H		2.2	324.0	
+2.5	= 1/2 Garage Dirt Floor	2.2	324.0	✓
L		1.8	324.4	
F		1.4	324.8	

2+70

F		0.0	326.2	
+3		0.3	325.9	
L		1.1	325.1	
H		1.6	324.6	
TP	6.29	331.77	0.74	325.48

331.77 ✓

2+94

H		6.3	325.5	
L		6.1	325.7	
F		2.7	329.1	
+2	= 1/2 Garage Wood Floor East End Area	4.56	327.21	✓
	3+06			
-1	= Garage Dirt Floor	5.3	326.5	✓
F		5.7	326.1	
L		6.0	325.8	
H		5.9	325.9	
+0.8	= 1/4 Car Garage Conc. Floor	5.90	325.87	✓
	3+37			
-0.9	= 0.7 Conc Floor of 6 Garage	5.92	325.85	✓
H		5.9	325.9	
L		5.5	326.3	
+8		5.5	326.3	
F		4.8	327.0	
	3+65			
F		4.2	327.6	
+3		5.2	326.6	
L		5.2	326.6	
H		5.9	325.9	
+1.0	= 1/4 Car Garage Conc Floor	5.91	325.86	✓
	3+87			
1.5	F of H.A. - 1/4 Pav. Pk			

331.77 ✓

3177

-10.5 = Sky Dr Garage Conc Floor	5.55	326.22 ✓
H	5.9	325.9
L	5.0	326.8
+5	5.0	326.8
F	4.1	327.7

3193

F	3.5	328.3
+4	4.6	327.2
L	4.7	327.1
H	5.4	326.4
+10.5 = Sky Dr Garage Conc Floor	5.55	326.22 ✓

4104

F - 07 Conc Apron	3.70	328.07 ✓
+1.2 = Sky Garage Conc Floor	3.50	328.27 ✓

4130

H	3.9	327.9
L	3.9	327.9
F	3.7	328.1

414976 = S.L. Meade

F Top Cb	3.65	328.12 ✓
Gutter on Pav	4.07	327.70 ✓
L " "	4.53	327.24 ✓
Gutter " "	4.46	327.31
H Top Cb	4.41	327.36

331.77 ✓

S.C. Meade

H 07 Pav	5.32	326.45
F " "	4.46	327.31 ✓
TP	1.32	328.05
B.M.	9.28	318.77
		5.04
		326.73
		S.F.B.P.
		Meade +
		Alabama
		318.89

Bliss
Isbell
Chapman
12-23-39

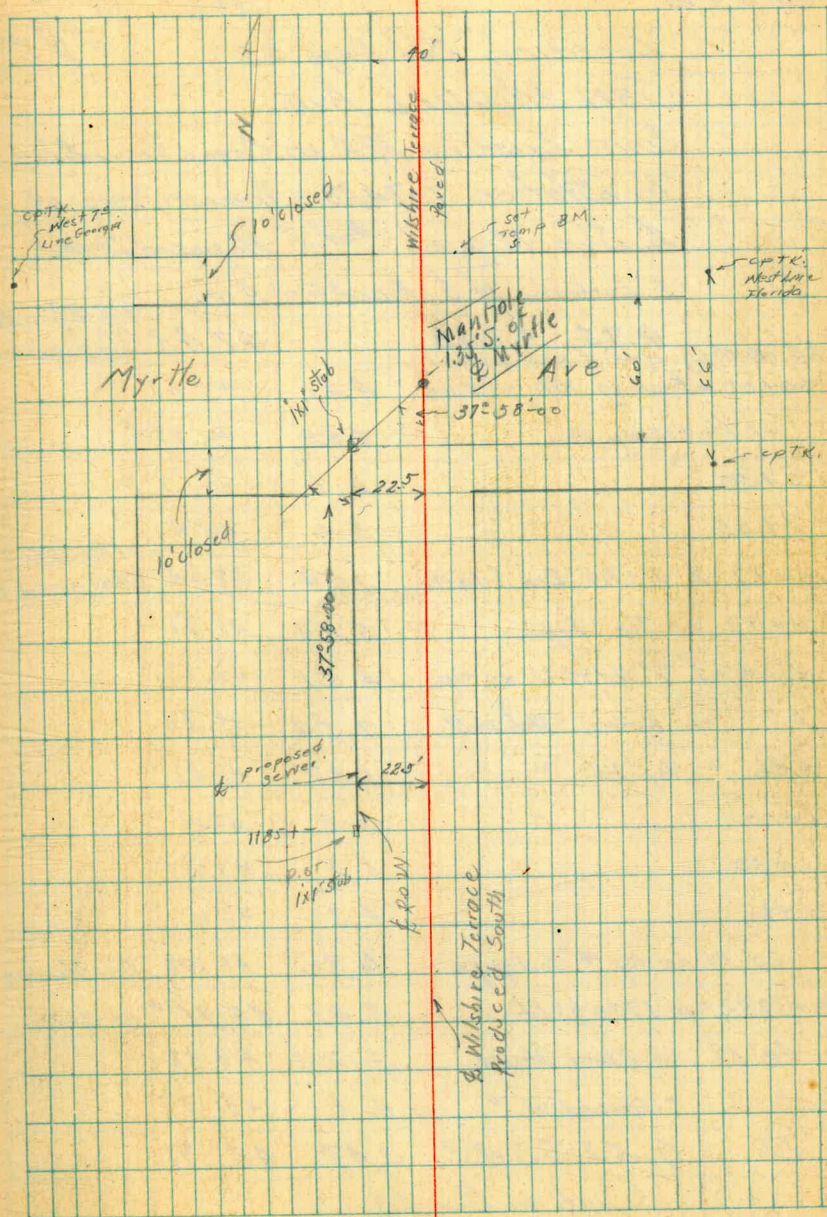
Survey for Sewer Easement and Levels
for Sewer South of Wilshire Terrace

Block 253. Units #15
N.W. B.P.
Upper Alabama

3 M.	118	260.68	259.50	Upper Alabama
TR	0.14	248.39	12.43	248.25
T.P. End Stub <small>on Dead</small>	5.07	242.32	11.14	237.25
0100	Flow Line Sewer	11.27		√31.05
0200	Top Pin	5.83		√36.49
0400	Ground	5.8		√36.5
0706		3.9		√38.4
0723		1.5		240.8
0723	6' East	4.0		238.3
0736 ⁸²	6' East <small>37° 58' 00"</small> Pt. S Line Myrtle	1.24		241.08
0750		2.0		240.3
0750	6' East	2.8		√39.5
1100		4.1		√38.2
1400	6' East	5.3		√37.0
1450		5.3		√37.0
1450	6' East	6.0		√36.3
1796 ⁸²	D. End	5.1		√37.2
1796 ⁸¹	6' East	5.8		√36.5
Top Ch. and East Side of Wilshire Terrace <small>SE in Concluded as B.M. in construction</small>	6.54			235.78

Indexed
C.S.K.

26



Wolker. Preliminary Levels SIERRA VISTA TRACT
Bliss
1st call 3-4-40

— SEWERS —

INDEXED
E.F.B.

Hydro
Relieved
at
100'

Location See Page 28

JAN MIGUEL AVE.

From Existing M.H. in Ocean View Blvd.

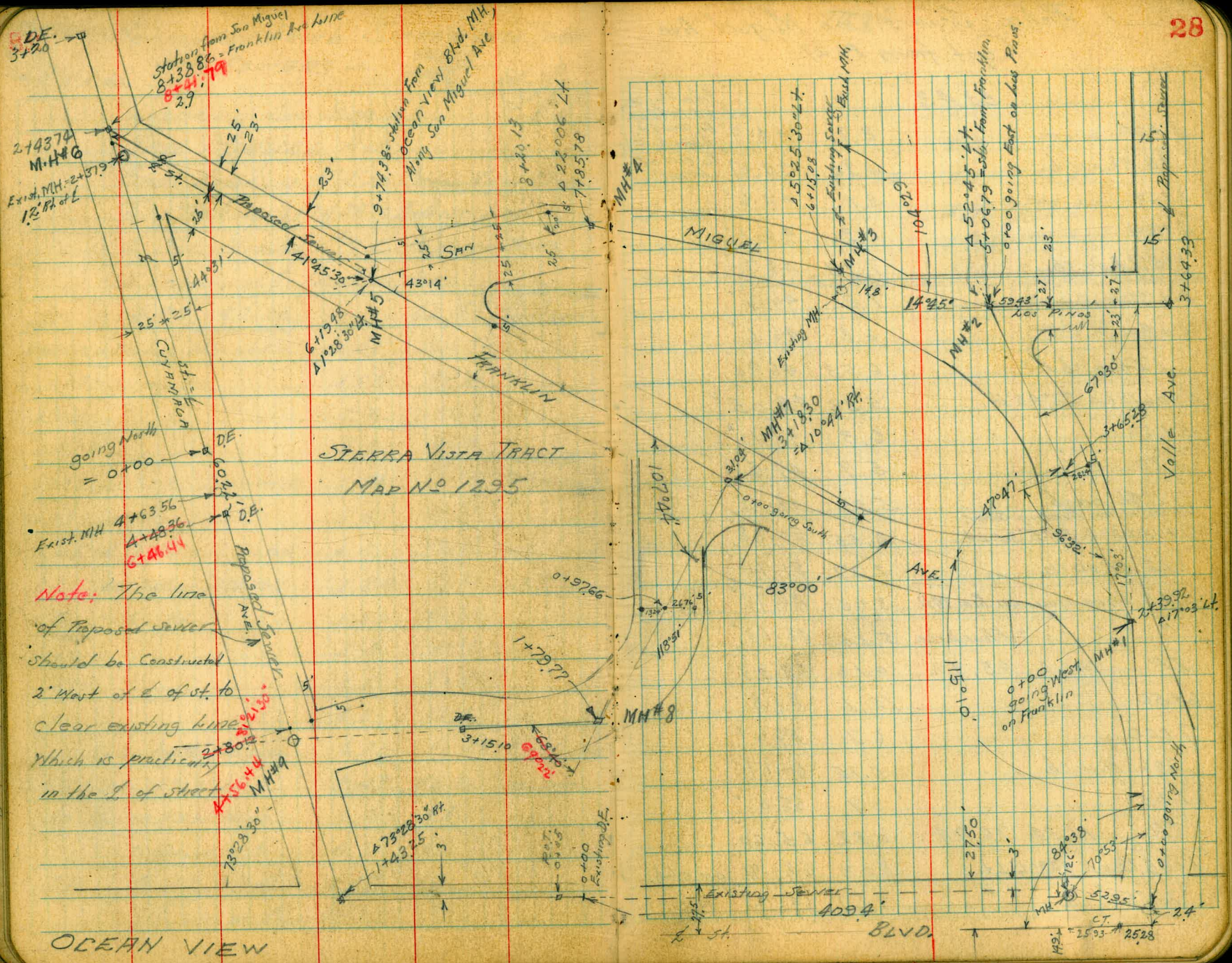
To Station 9+74.38 = Intersection of

E. San Miguel And Proposed Sewer.

2' East of E. Franklin Ave.

	4.95	47.38	42.43	N.E. S.P. in Hd. 120' E San Miguel	Wall (Ocean View)
2.4' on diag. N. of E. Ocean View = 0+00 = Existing M.H. on Rim			4.41	42.97	✓
+07.6 = N. edge Pav.			4.53	42.85	✓
0+50			4.7	42.7	✓
0+85			5.0	42.4	✓
0+97 = 2-20" Iron Culverts			7.54	39.84	1' Rt. of E West end of Pipe
0+97 on Top Pipe			5.87	41.51	✓
1' Lt. = 7' Hd. Wall on top			4.51	42.87	✓
1" on Bottom Hd. Wall			7.54	39.84	✓
1' Rt. " top Hd " "			5.87	41.51	✓
1+10			5.3	42.1	✓
1+50			5.1	42.3	✓
1+90			4.3	43.1	✓
50' Rt. on top 4" Soil pipe			6.30	41.08	Residence
2+39.92 = Δ 17° 03' Lt.			3.47	43.91	on Spite
40' Rt. on Floor House			3.20	44.18	
" " " Ground at "			4.1	43.3	✓
T.P.	9.52	53.43	3.47	43.91	✓

Cont. on Page 29



OCEAN VIEW

Prelim. Sewers San Miguel Ave
Cont. from P-27

	53.43			
3+00		8.7	44.7	From this Sta. all Lots on Rt. and Lt. Above & Et. to end of line
18' Rt. on cb.		8.96	44.47	
3+50		8.8	44.6	
4+00		8.3	45.1	
5' Lt. on cb.		7.73	45.70	
4+50		7.2	46.2	
4+80		6.8	46.6	
1' Rt. on cb. Ret.		6.53	46.90	
5+06.79 = Δ 52°45' Lt.		5.38	48.05	
5+50		6.3	47.1	
+70		5.9	47.5	
1' Rt. on cb.		5.35	48.08	
Intersection Ending Sewer.				
6+15.08 = Δ 5°25'30" Lt.		2.55	50.88	
12' Rt. on cb.		2.27	51.16	
14.8' Lt. on diag. on Rim 144		3.65	49.78	
" " " " " Flow line		5.30	48.13	
T.P. 12.65	65.92	0.16	53.27	
6+50		12.1	53.8	
7+00		6.7	59.2	
206' Rt. on cb.		5.75	60.17	
7+50		0.9	65.0	
T.P. 11.34	76.94	0.32	65.60	
7+85.78 = Δ 22°06' Lt.		8.03	68.91	on stub.
7' Rt. on cb.		7.67	69.27	

76.94 ✓

29

8+00		6.5	70.4	✓
+50		2.0	74.9	✓
T.P. 7.17	83.60	0.51	76.43	✓
9+00		4.7	78.9	✓
15' Rt. on cb.		4.24	79.36	✓
9+74.38 = Intersection Franklin Ave		2.96	80.64	✓ 6+19.48 Franklin Ave
			80.63	→ P-30
			0.01 Error.	

Preliminary Levels For Sewer
IN FRANKLIN AVE.
Bet. San Miguel And Cuyamaca Ave

	10.80	54.71	43.91	Bl. Spike 2+39.92 P27
2+39.92 P27 =0+00			10.80	43.9
0+25 = east edge Conc. Gutter			10.78	43.93
+31.7 = L	"	"	11.71	43.00
+38.4 = W	"	"	10.76	43.95
6+50			10.5	44.2
1+00			7.9	46.8
11' Lt. on cb.			7.88	46.83
1+50			5.4	49.3
3' Rt. on cb.			4.89	49.82
(1+75) 1' Rt. on cb.			2.81	51.90
2+00			1.1	53.6
50' Rt. on Ground at house			4.8	49.9
T.P.	11.54	65.49	0.76	53.95
50' Rt. on Floor of Above House			7.4	58.1
2+50			7.2	58.3
3+18.3 = 70° 44' Rt.			1.63	63.86
21' Rt. on cb.			1.29	64.20
T.P.	12.11	77.03	0.57	64.92
4+00			9.2	67.8
11' Lt. on cb.			9.80	67.2
4+50			6.5	70.5
17' Rt. on cb.			5.66	71.37
5+00			2.8	74.2

77.03 ✓

30

(5+00) 17' Lt. on cb.	2.82	74.21
T.P. 11.88	88.71	0.20
5+50	11.1	77.6
6+19.48 = 1° 28' 30" Lt.	8.08	80.63
17' Lt.	7.23	81.48
6+50	7.3	81.4
7+00	6.3	83.4
13' Rt. on cb.	4.80	83.91
7+50	3.9	84.8
8+00	3.0	85.7
13' Rt. on cb.	2.65	86.06
8+38.86 = E Cuyamaca	3.01	85.70
chk NE. B.P. Cuyamaca - Franklin,	2.56	86.15
		89.70

end of line

Walker
Bliss
Isbell
3-6-40

Preliminary levels for Sewer
IN JANDUL AVE.
From FRANKLIN AVE, South + West.

	8.26	72.12	63.86	El. stub 3+183 P-30
3+183 P-30 = 0+0.0 on stub.	8.26	63.86	✓	
0+30	9.0	63.1	✓	
+50	8.4	63.7	✓	
1' Lt. on cb.	7.64	64.48	✓	
0+97.66	6.9	65.2	✓	
7' Rt. on cb.	6.76	65.36	✓	
1+35	6.6	65.5	✓	
1+79.77 - Δ 68° 40' Lt	5.44	66.68	on stub	
9' Lt. on cb.	4.84	67.28	✓	
2+00	5.4	66.7	✓	
+50	3.8	68.3	✓	
3+15.10 on DE. Stub.	1.51	70.61	chk P-33	
11' Lt. on cb.	0.89	71.23	✓	

Preliminary levels for Sewer

On Lees - PIÑOS AVE.
From San Miguel To Valle Ave
And in Valle Ave From Lees Pinos, North.

	11.69	59.74	48.05	El. stub 5+06.79 P-29
5+06.79 P-29 = 0+0.0	11.69	48.05	✓	
0+50	9.3	50.4	Prop. on Lt. in this block Above Δ El.	
1+00	6.9	52.8	✓	
13' Rt. on cb.	7.13	52.61	✓	
17' Lt. " cb.	5.84	53.90	✓	
1+50	4.8	54.9	✓	
2+00	2.1	57.6	✓	
17' Lt. on cb.	1.19	58.55	Not taken in order.	
(1+50) 50' Rt	9.1	50.6	✓	
(2+00) 50' Rt	6.1	53.6	✓	
(2+70) 40' Rt. on 4" soil line	1.05	58.69	Not taken in order.	
T.P. 13.68	72.28	0.14	59.60	✓
2+50	11.7	60.6	✓	
2+70	10.8	61.5	✓	
3+00	10.3	62.0	✓	
+10	10.3	62.0	✓	
40' Rt. on Ground at House	14.3	58.0	✓	
" " " Basement Floor "	17.3	55.0	✓	
40 " " Main " "	9.5	62.8	✓	
3+64.33 Δ 90° Lt. = Map.	11.09	61.19	on stub	

Cont. P. 32.

Los Piños + Valle Ave Cont. From P. 31

		72.28 ✓		
4+00			8.0	64.3 ✓
+50			1.9	70.4 ✓
T.P.	12.50	84.47	0.31	71.97 ✓
50' RL			14.0	70.5 ✓
5+00			7.2	77.3 ✓
751.33 - Sub. Line - Mag			3.8	80.7 ✓
TP	0.51	72.19	12.79	71.68 ✓
TP	0.22	59.51	12.90	59.29 ✓
Chk. Starting & Mon. sub.			11.45	48.06 ✓
				5+0679
				P-29
			48.08	
			0.02 Error	

Preliminary Levels For Sewer,
 IN Ocean View Blvd.
 And in Cuyamaca Ave.

Location P-28

S.M. in Hd. No. 11 ✓

P-27	10.21	52.64	42.43	
T.P.	13.15	64.94	0.85	51.79 ✓
0+00 in Hedge		4.0	60.9	✓
0+05 on stub.		3.99	60.95	✓
14.5' Lt. on Pav.		4.63	60.31	✓
0+50		2.8	62.1	✓
1+00		1.4	63.5	✓
1+43.25 = Δ 73° 28' 30" Rt.				
T.P.	13.96	78.34	0.56	64.38 ✓
1+43.25 = Δ 73° 28' 30" Rt.		13.93	64.91	✓
14.5' Lt. on Pav.		14.09	64.25	✓
2+00		8.8	69.5	✓
14.5' Lt. on cb.		7.63	70.71	✓
2+50		4.5	73.8	✓
14.5' Lt. on cb.		4.1	74.2	✓
chk. on stub 3+15.10 P-31		7.74	70.60	✓
3+00		2.4	75.9	✓
14.5' Rt. on cb.		2.78	75.56	✓
T.P.	13.24	91.20	0.38	77.96 ✓
3+50		12.0	79.2	✓
14.5' Lt. on cb.		11.39	79.81	✓
4+00		7.7	83.5	✓
14.5' Rt. on cb.		7.10	84.10	✓

91.20 ✓

33

4+48.36 on stub.	4.62	86.58 ✓	
14.5' Lt. on cb.	4.62	86.58 ✓	
4+63.56 on Rim M.H.	3.98	87.22 ✓	Flush Tank Partly on 10' E.M.H.
" " " " Flow "	^{6.35} 10.33	80.87 ✓	
0+00	4.19	87.01 ✓	
+50	4.5	86.7 ✓	
14.5' Rt. on cb.	4.56	86.64 ✓	
1+00	4.5	86.7 ✓	
14.5' Lt. on cb.	4.60	86.60 ✓	
1+50	4.6	86.6 ✓	
14.5' Rt. on cb.	4.72	86.48 ✓	
2+00	5.0	86.2 ✓	
+37.9 = Exist. M.H., 12' Rt.	5.13	86.07 ✓	on River.
2+37.9 = " " Flow here	6.24	84.96 ✓	
2+43.74 on stub P-30	5.53	85.67 ✓	003 = Error. 8+38.86
3+00	7.3	83.9 ✓	
+20	8.15	83.05 ✓	
14.5' Rt. on cb.	7.64	83.56 ✓	

Cross Section Boston Ave.
28th St to 30th St.

Indexed
C.S.K.

BM	584	46.27	40.43	Nix B.P. Boston 225
		0+0 = Elev. 28th		
H.Cb Top	5.81	40.46		
Gutter on Pavement	6.52	39.75		
"	6.66	39.61		
"	6.91	39.36		
"	7.34	38.93	0+50 to	
Gutter " "	7.92	38.35	1+10 walk on	
S.Cb Top	7.29	38.98	South cracked	
		0+50		
S.Cb Top	6.77	39.50	note	
Gutter	7.4	38.9	0+55 to	
"	6.8	39.5	0+58 Cb out on Jo.	
"	6.4	39.9		
"	6.4	39.9		
Gutter	6.2	40.1		
H.Cb Top	5.35	40.92		
		1+0		
H.Cb Top	4.90	41.37		
Gutter	5.9	40.4		
"	6.0	40.3		
"	6.1	40.2		
"	6.5	39.8		
Gutter	6.9	39.4		
S.Cb Top	6.28	39.99		

Red. By Kelley, 7-4-1/1940
Plot By. Hough

80' wide
14 Cb's
13' 1/4

March 30-40
S. S. Co.
Northham
W. Moore

34

	46.27	
	1+50	
S.Cb Top	5.64	40.63
Gutter	6.4	39.9
"	6.0	40.3
"	5.5	40.8
"	5.3	41.0
Gutter	5.3	41.0
H.Cb Top	4.40	41.87
	2+0	
H.Cb in Drive	4.31	42.06
Gutter	4.4	41.9
"	4.8	41.5
"	5.0	41.3
"	5.4	40.9
Gutter	5.9	40.4
S.Cb Top	5.12	41.15
	2+50	
S.Cb Top	4.60	41.67
Gutter	5.2	41.1
"	4.8	41.5
"	4.4	41.9
"	4.3	42.0
Gutter	3.9	42.4
H.Cb Top	3.35	42.92

4627

3+0

Hcb Top		2.70	43.57
Gutter		3.5	42.8
1/4		3.6	42.7
1/2		3.8	42.5
3/4		4.4	41.9
Gutter		4.9	41.6
Scb Top		3.97	42.30

3+50

Scb Top		3.26	43.01	
Gutter		4.2	42.1	
1/4		3.8	42.5	
1/2		3.4	42.9	
3/4		3.3	43.0	
IP	7.49	50.97	2.79	43.48
Gutter			7.6	43.4
Hcb Top			6.93	44.04

4+0

Hcb Top		6.47	44.50
Gutter		7.3	43.7
1/4		7.3	43.7
1/2		7.4	43.6
3/4		7.9	43.1
Gutter		8.2	42.8
Scb Top		7.58	43.39

50.97

4+50

Scb Top		7.04	43.93
Gutter		7.7	43.3
1/4		7.3	43.7
1/2		7.0	44.0
3/4		7.0	44.0
Gutter		6.9	44.1
Hcb Top		5.95	45.02

5+0

Hcb Top		5.43	45.54
Gutter		6.4	44.6
1/4		6.5	44.5
1/2		6.5	44.5
3/4		6.9	44.1
Gutter		7.2	43.8
Scb Top		6.59	44.38

5+50

Scb Top		6.00	44.97
Gutter		6.7	44.3
1/4		6.3	44.7
1/2		5.9	45.1
3/4		5.9	45.1
Gutter		5.8	45.2
Hcb Top		4.94	46.03

5097

6+0 = 116 295 St

Ncb Top	4.44	46.53
Gutter	5.2	45.7
1/4	5.1	45.6
1/2	5.5	45.5
1/4	5.6	45.4
Gutter	5.9	45.1
S cb top	5.48	45.49

N cb 29 1/2 St

29 1/2 St

S Line Top cb	5.44	45.53
S Gutter	6.1	44.9
cb	5.9	45.1
1/4	5.5	45.5
1/2	5.3	45.7
1/4	5.3	45.7
cb	5.3	45.7
N Gutter	5.2	45.8
N Top cb	4.38	46.59

1/2 29 1/2 St

N	4.7	46.3
cb	4.9	46.1
1/4	5.1	45.9
1/2	5.3	45.7
1/4	5.5	45.5
cb	5.7	45.3

5097

ECB 29 1/2 St

S	5.9	45.1
S L Top cb	5.38	45.59
Gutter	6.5	44.5
cb	6.1	44.9
1/4	5.8	45.2
1/2	5.6	45.4
1/4	5.5	45.5
cb	5.4	45.6
N L Gutter	5.3	45.7
N L Top cb	4.45	46.52

N.E. Return
1' of curb
out as
part of road

0+0 - FA 29 1/2 St.

Ncb Top	4.49	46.48
Gutter	5.3	45.7
1/4	5.5	45.5
1/2	5.7	45.3
1/4	5.9	45.1
Gutter	6.3	44.7
S cb Top	5.41	45.56

0+50

S cb Top	5.22	45.75
Gutter	6.0	45.0
1/4	5.6	45.4
1/2	5.3	45.7
1/4	5.3	45.7

50.97

Gutter	5.5	45.5
HcbTop	4.21	46.76
1+0		
HcbTop	4.04	46.93
Gutter	5.1	45.9
1/4	5.1	45.9
1/2	5.1	45.9
1/4	5.4	45.6
Gutter	5.5	45.5
SCbTop	4.95	46.02
1+50		
SCbTop	4.90	46.07
Gutter	5.3	45.7
1/4	5.2	45.8
1/2	4.9	46.1
1/4	4.8	46.2
Gutter	4.8	46.2
HcbTop	3.77	47.20
2+0		
HcbTop	3.61	47.36
Gutter	4.9	46.1
1/4	4.7	46.3
1/2	4.8	46.2
1/4	5.1	45.9
Gutter	5.1	45.9

50.97

SCbTop	4.60	46.37
2+50		
SCbTop	4.40	46.57
Gutter	4.9	46.1
1/4	4.8	46.2
1/2	4.5	46.5
1/4	4.5	46.5
Gutter	4.5	46.5
HcbTop	3.37	47.60
TP	5.81	52.37
3+0		
HcbTop	4.60	47.77
Gutter	5.6	46.8
1/4	5.7	46.7
1/2	5.6	46.8
1/4	6.0	46.4
Gutter	6.2	46.2
SCbTop	5.58	46.79
3+50		
SCbTop	5.33	47.04
Gutter	6.1	46.3
1/4	5.7	46.7
1/2	5.3	47.1
1/4	5.3	47.1
Gutter	5.3	47.1

52.37

HCB		4.40	47.97
	4+10		5+79 to
H		3.5	48.93+86
+4.5-1/4 Conc Walk		3.93	48.45 ^{0.77} 5 1/2' of
Cb Top		4.13	48.24 ^{Walk Broken}
Gutter		4.9	47.5
1/4		5.0	47.4
1/2		5.1	47.3
1/4		5.4	47.0
Gutter		5.8	46.6 4+90 to
Cb Top		5.08	47.29 4+55 on H
+9.5-Sly Conc Walk		4.93	47.44 ^{Walk Cracked}
S		4.8	47.6
	4+50		
S		4.9	47.5
+4.5-Sly Conc Walk		5.01	47.36 4+50 to
Cb Top		5.14	47.23 ^{5+0 on S} curb & walk
Gutter		5.7	46.7 ^{sunken}
1/4		5.4	47.0
1/2		5.0	47.4
1/4		5.0	47.4
Gutter		4.9	47.5
Cb Top		4.06	48.31
+9.5-1/4 Conc Walk		3.93	48.44
H		4.7	47.7

52.37

	4+75		
H		4.3	48.1
+4.5-1/4 Conc Walk		4.00	48.37 4+80 to
Cb Top		4.13	48.24 4+92
Gutter		4.9	47.5 ^{on H curb} out
1/4		5.0	47.4
1/2		5.0	47.4 4+90 to
1/4		5.3	47.1 ^{5+0 on H} Walk Broken
Gutter		5.7	46.7
Cb Top		5.45	46.92
+9.5-Sly Conc Walk		5.02	47.29
S		5.1	47.3
	5+0		
S		4.9	47.5
+4.5-Sly Conc Walk		4.92	47.45
Cb Top		5.01	47.36
Gutter		5.7	46.7
1/4		5.3	47.1
1/2		4.9	47.5
1/4		4.9	47.5
Gutter		4.8	47.6
Cb Top		3.93	48.44
+9.5-1/4 Conc Walk		3.75	48.62
H		4.0	48.4

52.37

51.50

N	3.6	48.8
+ 4.5 = 1/4 Conc Walk	3.44	48.93
Cb Top	3.64	48.73
Gutter	4.6	47.8
1/4	4.5	47.9
1/2	4.6	47.8
1/4	5.0	47.4
Gutter	5.2	47.2
Cb Top	4.58	47.79
+ 9.5 = 1/4 Conc Walk	4.52	47.85
J	4.5	47.9

51.98.5 = WL 30' 9.5'

J	3.6	48.8
+ 4.5 = 1/4 Conc Walk	4.14	48.23
Cb Top	4.38	47.99
Gutter on Parapet	4.82	47.55
1/4 " "	4.33	48.04
1/2 " "	4.01	48.36
1/4 " "	3.96	48.41
Gutter " "	4.05	48.32
Cb Top	3.44	48.93
+ 9.5 = 1/4 Conc Walk	3.19	49.18
H	3.1	49.3
BM	4.33	48.04

SW B.P.
BANK 4.30
48.05

08 Cross Section Dickens St.
Evergreen to Mean High Tide

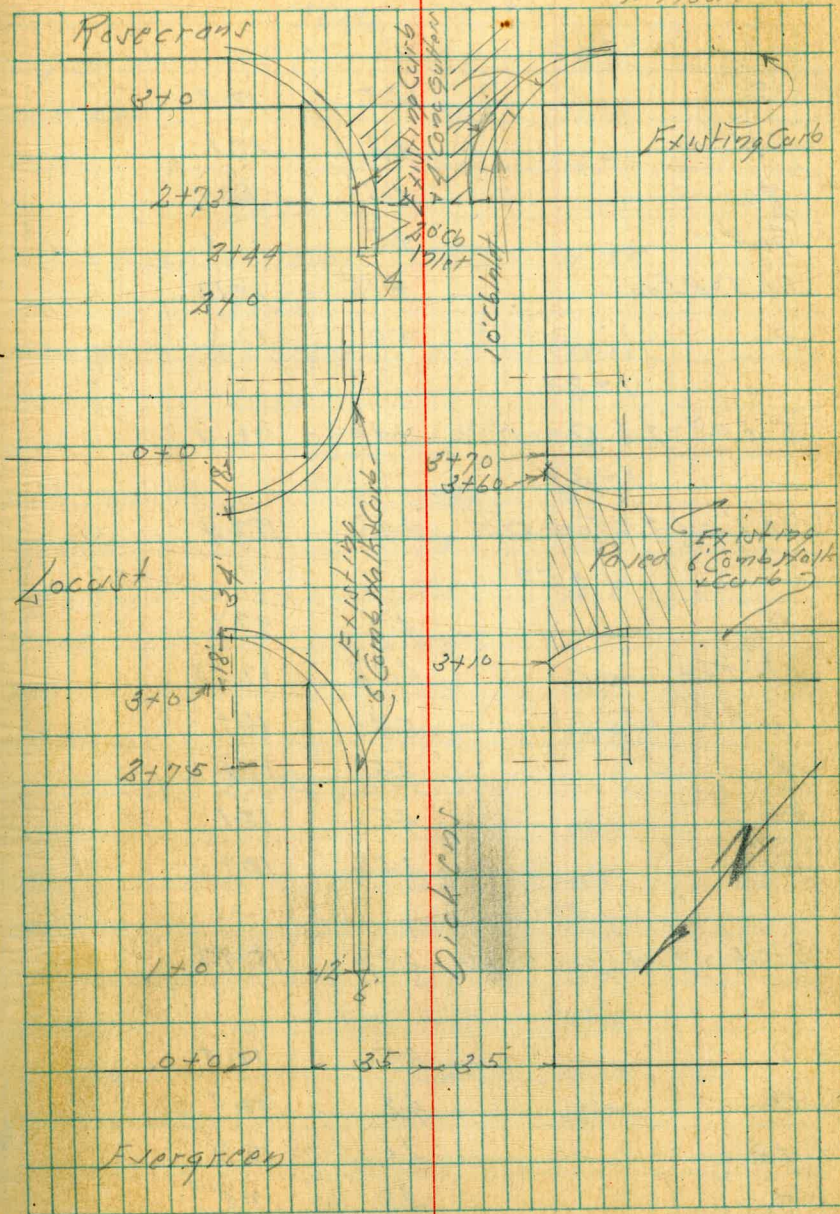
INDEXED
E.P.B.

April 4-40
SIN 03
Northham
18 Moor

40

BM	1240	2232	9.92	Sta. 7 Mon Rosecrans Dickens
0+0 = E.L. Evergreen				
H		2.8	19.5	
cb		2.4	19.9	
+5		2.1	20.2	
+7		3.1	19.2	
z		2.6	19.7	
cb		2.5	19.8	
S		2.2	20.1	
0+25				
S		2.6	19.7	
cb		2.1	19.2	
z		3.5	18.7	
+8		3.7	18.6	
+10		3.0	19.3	
cb		2.1	19.2	
H		2.5	18.8	
0+50				
H		4.5	17.7	
cb		4.0	18.3	
+7		4.1	18.2	
z		3.9	18.4	
cb		3.5	18.8	
S		3.2	19.1	

Notes Red. By J. J. J.
Plot on profile 2589 418-40
C.B. 10/9/40



22.32

1+0

S	3.5	18.8
Cb	4.2	18.1
d	4.3	18.0
Gutter	4.5	17.8
Cb Top End	4.15	18.17
H	5.0	17.3

1+23

S + 0.8 = $\frac{1}{2}$ 3 Conc Walk	3.18	19.14
-------------------------------------	------	-------

1+47

S + 1 = $\frac{1}{2}$ 3.5 Conc Walk	3.48	18.84
-------------------------------------	------	-------

1+50

H	4.7	17.6
Cb Top	4.74	17.58
Gutter	5.4	16.9
d	4.5	17.5
Cb	4.2	18.1
S	3.5	18.9

1+91

S + 0.5 = $\frac{1}{2}$ 10.5 Conc Drive	3.39	18.93
---	------	-------

2+0

S	3.5	18.8
Cb	4.2	18.1
H	4.6	17.7
d	4.8	17.5

41

22.32

Gutter	5.8	16.5
Cb Top	5.32	17.00
H	5.4	16.9

2+20

S = $\frac{1}{2}$ 2.5 Conc Walk	3.52	18.80
---------------------------------	------	-------

2+45

S = $\frac{1}{2}$ 7 Conc Drive	4.17	18.15
--------------------------------	------	-------

2+50

H	5.6	16.7
---	-----	------

Cb Top	5.93	16.39
--------	------	-------

Gutter	6.5	15.8
--------	-----	------

d	5.5	16.8
---	-----	------

+15	5.4	16.9
-----	-----	------

Cb	4.9	17.4
----	-----	------

S	4.4	17.9
---	-----	------

2+75 = Cb BC

S	4.9	17.4
---	-----	------

Cb	5.4	16.9
----	-----	------

+2	6.0	16.3
----	-----	------

d	5.9	16.4
---	-----	------

Gutter	6.8	15.5
--------	-----	------

Cb Top	6.21	16.11
--------	------	-------

H	6.0	16.32
---	-----	-------

22.32

270 = HL Locust

H	6.6	15.7
+10 - Cb Top	6.62	15.70
Gutter	7.0	15.3
cb	7.1	15.2
L	6.4	15.9
cb	6.2	16.1
+5	6.1	16.2
+7	5.3	17.0
S	5.4	16.9

2710

S Cb End	5.72	16.60
Gutter on Paving	6.36	15.96
cb	6.2	16.1
L	6.4	15.9
cb	6.9	15.4
H Gutter	7.4	14.9
H Top Cb	6.82	15.50

2718 = MCb Locust

H	7.6	14.7
cb	6.9	15.4
L	6.5	15.8
cb	6.4	15.9
S on Paving	6.34	15.98

22.32

2735 = L Locust

S on Paving	6.45	15.82
cb	6.8	15.5
L on MH Rim	6.66	15.66
cb	6.9	15.4
H	7.0	15.3

2752 = Cb

H	7.4	14.9
cb	7.2	15.1
L	7.0	15.3
cb	7.0	15.3
S on Paving	6.94	15.35

2760

S Top Cb	6.51	15.81
S on Paving	7.17	15.15
cb	7.4	14.9
L	7.3	15.0
cb	7.4	14.9
H Gutter	7.9	14.4
H Top Cb	7.46	14.86

2770 = FL Locust = 0 + 0

H	7.3	15.0
+10 - Top Cb	7.47	14.85
Gutter	8.0	14.3
cb	7.9	14.6

22.32

2			7.5	14.8	
cb			8.0	14.3	
+4			7.2	15.1	
S			6.8	15.5	
	0 + 25 = cb 25				
S			6.9	15.4	
+5			7.6	14.7	
cb			8.0	14.3	
+6			8.2	14.1	
+10			9.1	13.2	
2			8.3	14.0	
Gutter			8.5	13.8	
cb Top			7.90	14.42	
H			7.9	14.4	
TP	3.06	15.99	9.39	12.93	on state R.P. Guard
	0 + 61				
H on Conc Dr.			2.2	13.7	
cb + Gutter + 2 Dr.			2.88	13.11	
2			2.8	13.2	
+8			2.3	12.7	
+11			2.5	13.5	
cb			2.6	13.4	
S			1.9	14.1	
S	2.25	Conc Walk	0.91	15.08	

15.99

	170				
S			3.0	14.0	
+14			2.3	13.7	
cb			3.2	12.8	
+8			4.3	11.7	
2			3.5	12.5	
Gutter			3.6	12.4	
cb Top			3.09	12.90	
H			3.0	13.0	
	1750				
H			4.0	12.0	
cb Top			4.05	11.94	
Gutter			4.6	11.4	
2			4.7	11.3	
+6			5.0	11.0	
+10			3.7	12.3	
cb			3.2	12.8	
S			2.8	13.2	
	270				
S			4.0	12.0	
cb			4.4	11.6	
+7			4.6	11.4	
+13			5.7	10.3	
2			5.6	10.4	
Gutter			5.5	10.5	

1599

Cb Top End 5.09 10.90

H 5.1 10.9

2+25

H 6.0 10.0

+12 5.4 10.6

Cb 6.0 10.0

S 5.9 10.1

+6 5.8 10.2

+9 4.8 11.2

Cb 4.7 11.3

S 4.3 11.7

2+14

S 4.8 11.2

Cb 4.9 11.1

+5 4.9 11.1

+11 6.0 10.0

S 5.9 10.1

+12 = Sky Cond Gutter 5.97 10.02

Gutter 6.22 9.27

Cb Top End 5.57 10.42

H 5.5 10.5

2+73 = Cb BC

H 6.1 7.9

Cb Top 5.82 10.17

Gutter on Cond Gutter 6.31 9.68

1599

S on Paving 5.91 10.08

Gutter on Cond Gutter 6.00 10.00

Cb Top 5.38 10.61

+5 5.0 11.00

S 5.0 11.0

3+0 = H.L. Paving

S 5.6 10.4

+85 = Cb Top 5.41 10.58

Gutter 6.04 9.95

Cb on Paving 6.01 9.98

S " " 6.12 9.87

Cb " " 6.47 9.52

+95 Gutter 6.72 9.27

+95 Cb Top 6.18 9.81

H 6.4 9.6

TP 1.18 12.03 5.14 10.85

S Top End
Paving
Dickens

See page 75

12.03

0+0 = E.L. Powercrans

S	2.7	9.3
+8.8 = Cb Top	2.86	9.17
Gutter on Conc	3.51	8.52
H Cb + 9 on Conc Gutter	4.31	7.72
H Cb + 9 = Cb Top	3.67	8.36
H	3.4	8.6

0+27 = Cb FC

H	3.3	8.7
+15	2.9	9.1
Cb Top End	4.15	7.88
Gutter on Conc Gutter	4.77	7.26
2	4.1	7.9
Gutter on Conc	4.22	7.81
Cb Top End	3.57	8.46
S	3.0	9.0

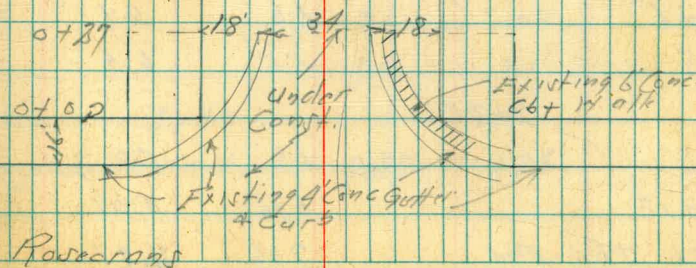
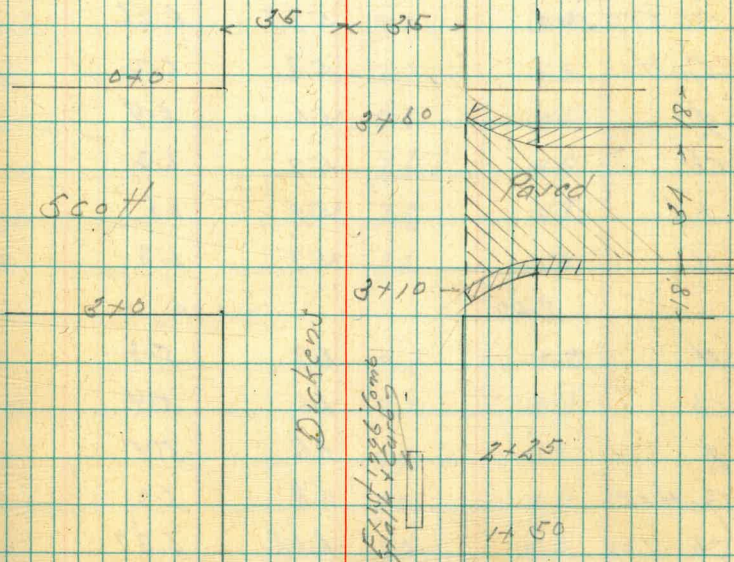
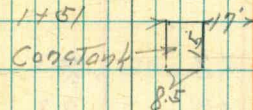
0+50

S on Conc Drive	3.11	8.92
Cb	3.5	8.5
2	3.7	8.3
Cb	3.9	8.1
H	4.6	7.4

1+0

H	4.9	7.1
Cb	4.9	7.1

45



12.03

S	4.7	7.3
Cb	4.7	7.3
+7'	3.8	8.2
S	3.7	8.3

1+50

S	4.7	7.3
411	4.7	7.3
Cb Top End	5.77	6.26
Gutter	5.8	6.2
S	5.6	6.4
Cb	5.7	6.3
+4	5.4	6.6
H	5.7	6.3

2+0

H	6.7	5.3
Cb	6.6	5.4
S	6.6	5.4
Gutter	6.8	5.2
Cb Top	6.64	5.39
+6	6.6	5.4
S	5.5	6.5

2+25

S	6.0	6.0
+12	6.96	5.07
Cb Top-End	7.06	4.97

12.03

Gutter	7.1	4.9
S	7.1	4.9
Cb	7.2	4.8
+2	6.9	5.3
H	6.9	5.1

2+50

H	7.5	4.5
+17	7.0	5.0
Cb	7.7	4.3
S	7.5	4.5
+15	7.6	4.4
Cb	7.2	4.8
S	6.6	5.4

2+75

S	7.2	4.2
+9	7.3	4.2
Cb	7.9	4.1
S	8.0	4.0
Cb	8.0	4.0
+2	7.6	4.4
H	7.9	4.1

2+80

S - 3' Conc'd Halk	7.27	4.76
--------------------	------	------

12.03

370 = H.L. Scott

H	8.2	3.7
716	8.0	4.0
Cb	8.4	3.6
S	8.3	3.7
Cb	8.6	3.4
+5	8.5	3.5
+9	7.6	4.4
S	7.9	4.1

3710

S TopCb	8.29	3.74
S Gutter on Parving	8.86	3.17
Cb	8.6	3.4
S	8.5	3.5
Cb	8.6	3.4
+2	8.2	3.8
H	8.5	3.5

2735 = S Scott

H	9.0	3.0
Cb	9.0	3.0
S M.H. Rim	8.87	3.16
Cb	9.0	3.0
S on Parving	9.00	3.03

12.03

3760

S TopCb	8.95	3.08
S on Parving	9.60	2.43
Cb	9.5	2.5
S	9.5	2.5
Cb	9.8	2.2
H	9.4	2.6

3770 = E.L. Scott = 0 + 6

H	9.8	2.2
+15	9.5	2.5
Cb	10.1	1.9
S	9.8	2.2
Cb	9.8	2.2
+9	10.1	1.9
+11	9.2	2.8
S	9.2	2.8

0 + 2.5

S	9.2	2.2
+9	9.7	2.3
Cb	10.7	1.3
S	10.5	1.5
Cb	10.9	1.1
+2	10.9	1.1
H	10.5	1.5

		12.03		
		0750		
H		11.0	1.0	
Cb		11.3	0.7	
$\frac{1}{2}$		11.2	0.8	
+10		11.3	0.7	
Cb		10.8	1.2	
S		9.8	2.2	
		170		
S		11.8	0.2	
Cb		12.1	-0.1	
$\frac{1}{2}$		12.1	-0.1	
Cb		12.1	-0.1	
H		11.5	+0.4	
		1707		
S = $\frac{1}{2}$	10' Door Wood Floor to Ketterburg Boat Works	11.60	+0.43	
TP	5.38	5.20	12.21	-0.18
		1750		
H		5.6	-0.40	
+18 on High Point Conc Tank		4.95	+0.35	
Cb		5.6	-0.19	
$\frac{1}{2}$		5.5	-0.3	
Cb		5.8	-0.5	
S		5.8	-0.6	
TP	2.55	3.31	5.54	-0.34

		3.21		
		240		
S		4.2	-1.0	
Cb		4.6	-1.4	
$\frac{1}{2}$		4.2	-1.0	
Cb		3.9	-0.7	
H		4.0	-0.8	
		2450		
H		7.1	-3.9	
Cb		6.8	-3.6	
+3		5.9	-2.7	
$\frac{1}{2}$		4.7	-1.5	
Cb		4.2	-1.0	
S		4.0	-0.8	
		2480		
S		6.5	-3.3	
Cb		7.0	-3.8	
$\frac{1}{2}$		7.8	-4.6	
Cb		8.1	-4.9	
H		8.0	-4.2	
TP		0.23	2.98	
+10' to Eucalyptus 17' at Dickers				

CP Cross Section Emerson St.
Rosecrans to Scott

INDEXED

E.F.B.

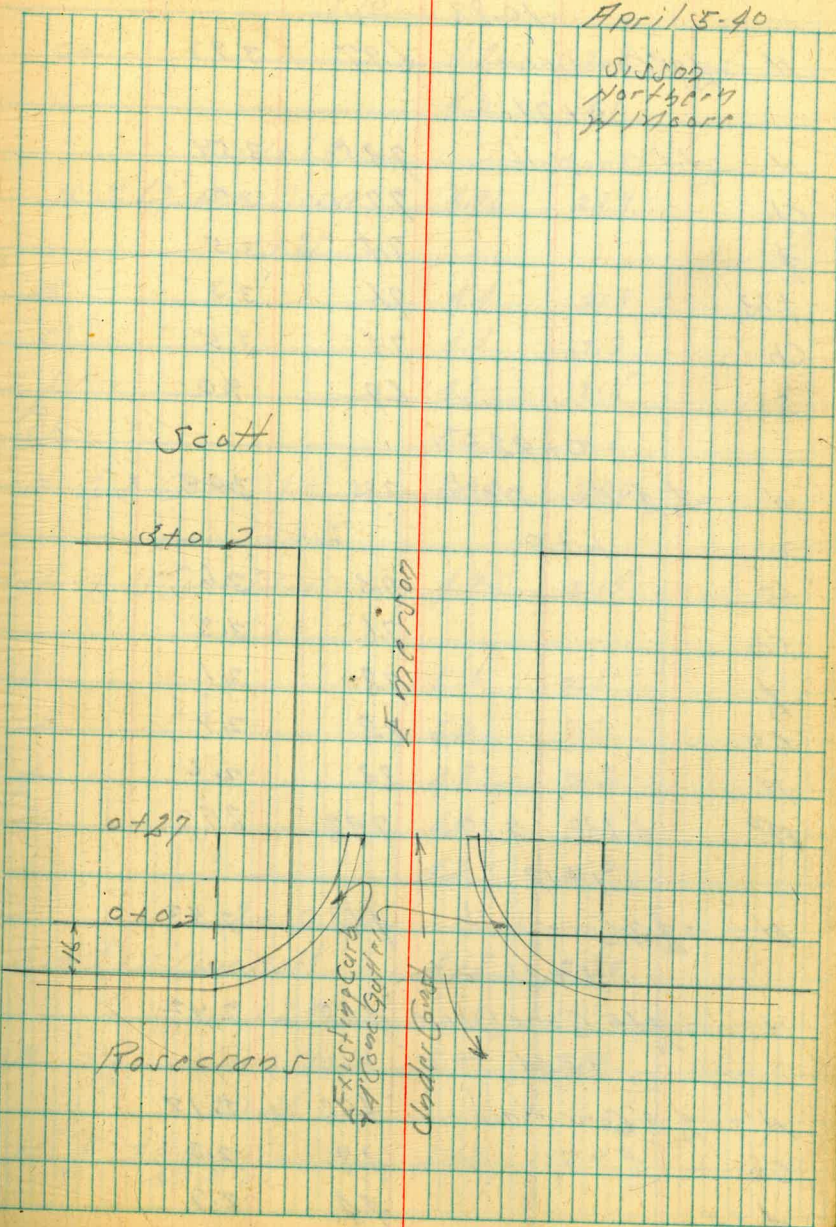
49

B.M.	0.97	10.89	9.92	SIX 7' HIGH ROSECRANS & DIETERS
	0+0 = F.L. ROSECRANS			
S		5.2	5.7	
+8.8 = CB Top		5.42	5.47	
Gutter on Conc.		6.06	4.83	
H CB + 9 on Conc Gutter		6.94	3.95	
H CB + 9 CB Top		6.31	4.58	
H		6.2	4.7	
	0+27 = CB FC			
H		6.9	4.0	
CB Top - End		6.76	4.13	
Gutter on Conc.		7.38	3.51	
H on Subgrade		6.9	4.0	
Gutter on Conc.		6.57	4.32	
CB Top - End		5.97	4.92	
S		5.9	5.0	
	0+45			
S		6.8	4.1	
CB		6.4	4.5	
+4		6.5	4.4	
+6		7.1	3.8	
±		7.2	3.7	
+13		7.5	3.4	
CB		7.0	3.9	
+3'		6.8	4.1	

Red By Brens
Plot on profile # 1128
A-7-40 C.B.H.

April 5-40

SIX 500
North 50' W
W Moore



10-89

H = 2 75' Conc Drive 6.97 3.92

0+71

H = 2 3' Conc Walk 7.25 3.54

Cb 7.7 3.2

S 7.4 3.5

7+13 7.6 3.3

Cb 7.4 3.5

S 6.9 4.0

0+92

H = 2 2' Conc Walk 7.85 3.04

1+0

S 7.3 3.6

Cb 7.6 3.3

S 7.8 3.1

Cb 8.2 2.7

H 8.3 2.6

TP 4.13 7.10 7.92 2.97

1+12

H = 2 3' Conc Walk 4.68 2.42

1+31

H = 2 6.5' Conc Drive 4.68 2.42

1+44

H = 2 3' Conc Walk 4.92 2.18

Cb 4.8 2.3

S 4.4 2.2

7.10

Cb 4.2 2.9

S 4.0 3.1

1+64

H = 2 6.7' Conc Drive 4.96 2.14

1+81

S 4.4 2.7

Cb 4.4 2.7

S 4.6 2.5

Cb 5.0 2.1

H = 2 3' Conc Walk 5.04 2.06

1+95

H = 2 7' Conc Drive 4.95 2.15

2+0

H 5.0 2.1

Cb 5.0 2.1

S 4.8 2.3

Cb 4.6 2.5

S 4.2 2.9

2+17

S = 2 2.5' Conc Walk 4.12 2.98

2+25

H = 2 Conc Walk 5.00 2.10

2+36

H = 2 2 Ribbon Conc Dr 5.08 2.02

5.9 2.1

7.10

2742

S = $\frac{1}{8}$ 10' Conc Drill	4.58	2.42
Cb	4.9	2.3
$\frac{1}{8}$	5.2	1.9
Cb	5.3	1.5
H	5.4	1.7

2769

S = $\frac{1}{8}$ 3' Conc Walk	4.82	2.28
--------------------------------	------	------

2775

H	6.1	1.0
Cb	5.8	1.3
$\frac{1}{8}$	5.7	1.4
Cb	5.4	1.7
S	5.2	1.9

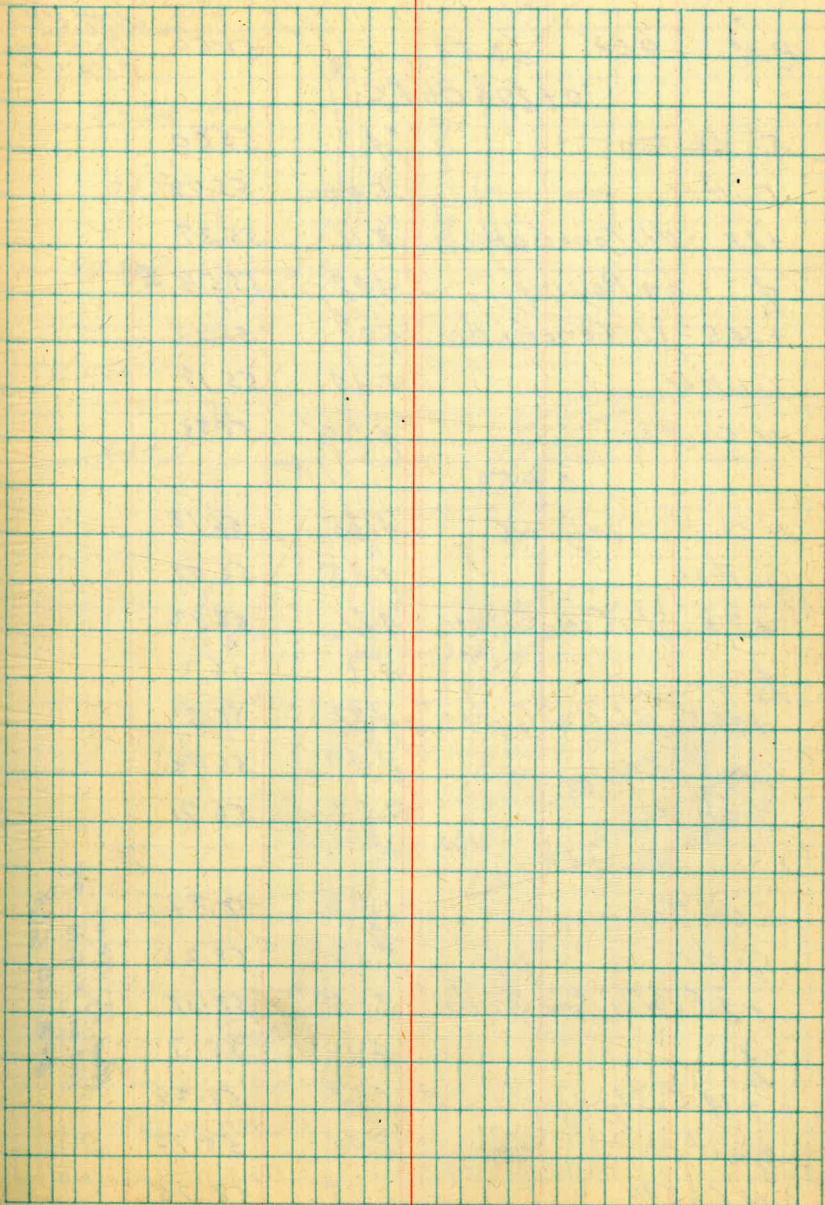
370 = 1/4 L Scott

S	4.5	2.6
Cb	5.8	1.3
$\frac{1}{8}$	6.1	1.0
Cb	6.3	0.8
H	6.4	0.7

Check TP Page 48

4.08	3.02
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Nails in
Euc Type
298



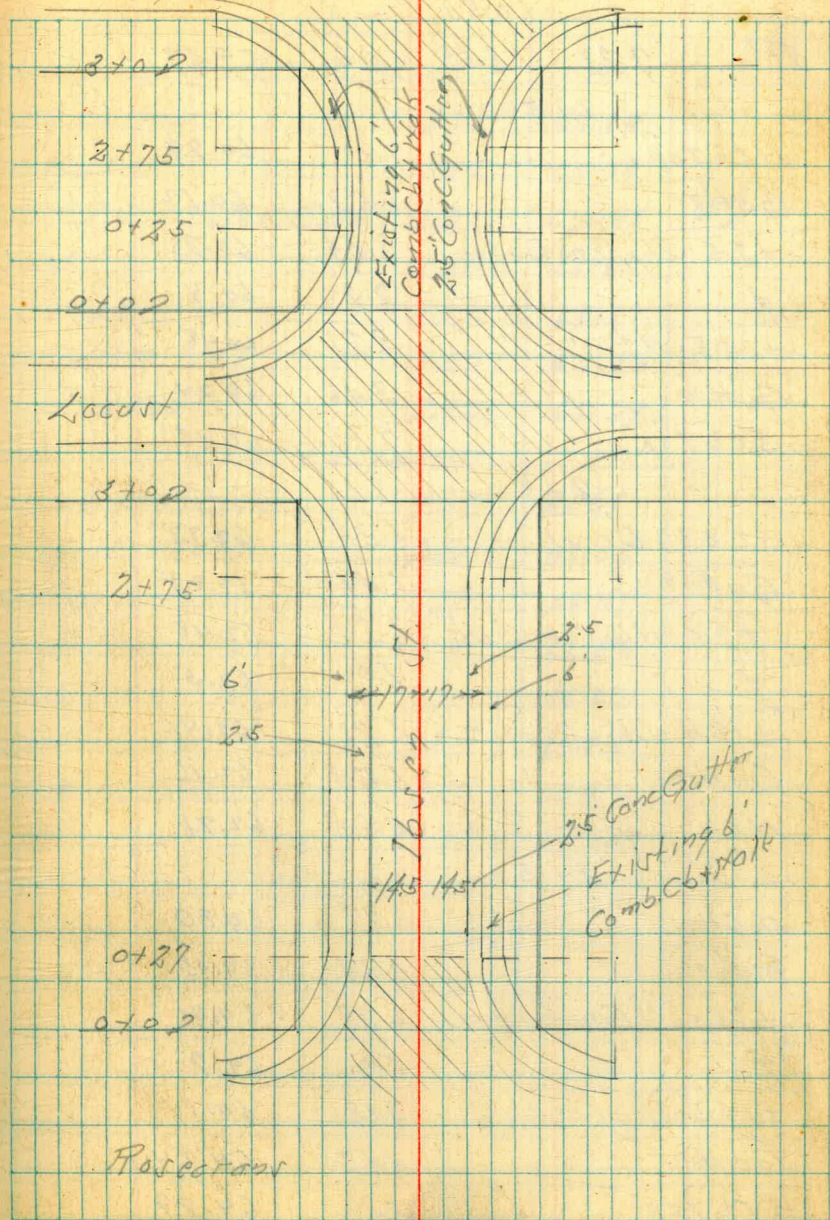
88 Cross Section Ibsen St
Rosecrans to Evergreen

(NOV 1960) April 4-40
S. 11505
North 6th St
at Mount

BM	9.03	60.53	57.50	N.W. Q.P. Rosecrans & Homer
0+27 - C&E.C.				
S C&E Top	4.73	55.80		
Gutter	5.46	55.02		
+2.5 - 1/4 Conc Gutter	5.16	55.37		
± on Paving	4.92	55.54	554	
+14.5 - 1/4 Conc Gutter	5.08	55.48		
Gutter	5.34	55.19		
N C&E Top	4.70	55.83		
0+50				
N C&E 10' D.I.W.I.	4.35	56.18		
Gutter	4.45	56.08		
+2.5 - 1/4 Conc Gutter	4.21	56.32		
±	4.3	56.2		
+14.5 - 1/4 Conc Gutter	4.22	56.31		
Gutter	4.47	56.06		
S C&E Top	3.82	56.21		
1+0				
S C&E Top	1.72	58.81		
Gutter	2.38	58.25		
+2.5 - 1/4 Conc Gutter	2.15	58.38		
±	2.2	58.3		
+14.5 - 1/4 Conc Gutter	2.24	58.29		
Gutter	2.43	58.10		
N C&E Top	1.78	58.75		

Red. by Bemis
Tkt. on Profile 1199
4-8-40 GRH

Evergreen



Rosecrans

		60.53		
TP	9.22	68.69	1.06	59.47
		17.50		
HCB TOP		7.90		60.79
Gutter		8.57		60.12
+2.5-Sly Conc Gutter		8.34		60.35
⌘		8.2		60.5
+14.5-Hly " "		8.21		60.45
Gutter		8.45		60.24
SCb Top		7.81		60.88
		240		
SCb in Drive		6.36		62.33
Gutter		6.44		62.25
+2.5-Hly Conc Gutt		6.21		62.48
⌘		6.2		62.5
+14.5-Sly " "		6.28		62.41
Gutter		6.53		62.16
HCB		5.88		62.81
		2450		
HCB		3.89		64.80
Gutter		4.54		64.15
+2.5-Sly Conc Gutter		4.38		64.41
⌘		4.0		64.7
+14.5-Hly Conc " "		4.18		64.51
Gutter		4.45		64.24
SCb Top		3.80		64.89

		2475 = Cb BC.		
SCb Top		2.95		65.94
Gutter		3.40		65.29
+2.5-Hly Conc Gutter		3.21		64.48 ^{65.48}
⌘		3.01		65.68
+14.5-Sly " "		3.32		65.37
Gutter		3.57		65.12
HCB TOP		2.95		65.74
		340 = F.L. Locust.		
HCB + 100 Cb Top		2.08		66.61
Gutter on Pav		2.62		66.06
Cb " "		2.38		66.41
⌘ " "		2.19		66.50
Cb " "		2.46		66.23
+8 = Gutter		2.84		65.85
+8 Cb Top		2.27		66.42
TP	9.37	75.17	0.89	67.80

75.17

0+0 = 24.6 Locust

H+10 = Cb Top	7.20	67.97
Gutter on Paving	7.68	67.49
Cb " "	7.47	67.20
⌘ " "	7.27	67.90
Cb " "	7.63	67.54
+8 = Gutter	8.15	67.02
+8 = Cb Top	7.50	67.67

0+25 = Cb EC

SCb Top	6.86	68.31
Gutter	7.48	67.69
+2.5 = 1/4 Conc Gutter	7.28	67.89
⌘	7.2	68.0
+14.5 = Sly " "	7.27	67.90
Gutter	7.48	67.69
H Cb Top	6.85	68.32

0+50

H Cb Top Drive	7.07	68.10
Gutter	7.25	67.92
+2.5 = Sly Conc Gutter	7.03	68.14
⌘	7.0	68.2
+14.5 = 1/4 " "	6.98	68.19
Gutter	7.18	67.99
SCb Top	6.53	68.64

75.17

1+0

SCb Top	6.03	69.14
Gutter	6.70	68.47
+2.5 = 1/4 Conc Gutter	6.50	68.67 / +48 to
⌘	6.38	68.79 / +53
+14.5 = Sly " "	6.57	68.60 / Conc Gutter
Gutter	6.74	68.43 / on Spout's
H Cb Top	6.08	69.09 / Out

1+50

H Cb Top	5.62	69.55
Gutter	6.24	68.93
+2.5 = Sly Conc Gutter	6.06	69.11
⌘	5.8	69.4
+14.5 = 1/4 " "	6.08	69.09
Gutter	6.34	68.83
SCb Top	5.64	69.53

2+0

SCb Top	5.09	70.08
Gutter	5.74	69.43
+2.5 = 1/4 Conc Gutter	5.43	69.74
⌘	5.3	69.9
+14.5 = Sly " "	5.58	69.59
Gutter	5.78	69.39
H Cb Top	5.12	70.05

165th St

7517

2+50

HCB Top	4.64	70.53
Gutter	5.33	69.84
+25 = Sky Conc. Gutter	5.05	70.12
$\frac{1}{2}$	4.8	70.4
+14.5 = Sky " "	5.00	70.17
Gutter	5.26	69.91
SCB Top	4.60	70.57

2+75 = C6 BC

SCB Top	4.34	70.83
Gutter	4.98	70.19
+25 = Sky Conc Gutter	4.72	70.45
$\frac{1}{2}$ = M.H. Rim	4.30	70.87
+14.5 Sky " "	4.79	70.38
Gutter	5.05	70.12
HCB Top	4.39	70.78

3+0 = E.L. Fireman

H +10 = Cb Top	4.29	70.88
Gutter	4.94	70.23
Cb on Paving	4.41	70.86
$\frac{1}{2}$ " "	3.97	71.20
Cb " "	4.32	70.85
+8 Gutter	4.73	70.44
+8 Cb Top	4.10	71.07

7517

TP	2.43	65.73	11.87	63.30
TP	1.24	58.77	8.20	57.53
B17			7.28	51.49

NW 8P
Pascoran
+ Hammer
GMSO

RE- Cross Section Berry St
Cass St to James

80' wide
20' curb

BM	11.52	77.92'	16.40	SIX B.P. Last 100'
0-14- E.Cb Cass St				
S on Paving		6.08		71.84
Cb		5.76		72.16
g		5.34		72.58
Cb		5.00		72.92
H		4.57		73.35
0+0- E.Cb Cass St				
H		3.2		74.1
+19.2 = End Cb Top		4.18		73.74
Gutter on Paving		4.77		73.15
g		5.00		72.92
Cb		5.52		72.40
+1 Gutter		5.53		72.39
+1 = End Cb Top		4.98		72.94
S		4.8		73.1
0+6				
S		4.6		73.3
Cb		5.0		72.9
+2		5.3		72.6
g		4.8		73.1
+19		4.5		73.4
Cb		4.1		73.8
+3		3.2		74.7
+13		2.4		75.5
H		2.3		75.6

Red. Guttenrohn
Plat. COH. 5-13-1940

INDEXED
E.F.B.

May 9-40
Sisson
Northberg
H Moore **56**

	77.92	0+40
H	1.4	76.5
+19	2.0	75.9
Cb	2.2	75.7
H	2.8	75.1
g	3.4	74.5
+10	3.8	74.1
+17	4.6	73.3
Cb	4.4	73.5
S on 1/4" Conc Slab	3.84	74.08
1+0		
+8 = 1/4" Garage Conc Floor	2.70	75.22
S = 1/4" Conc Driv	2.93	74.99
Cb	2.8	75.1
+3	3.1	74.8
g	1.9	76.0
Cb	1.4	76.5
+5	0.5	77.4
H = 1/4" 47 Conc Walk	0.04	77.88
TP 10.46 89.46'	0.92	77.00
1+17		
H-3 = 1/4" 1. Ribbon Conc Dr	9.37	78.09
1+22		
S+24 = 1/4" 1/2" Conc Walk	11.83	75.63

87.46			
	1484		
H	= 4' Conc. Walk	9.00	78.46
	1450		
H		8.85	78.61
+16		9.0	78.5
Cb		9.7	77.8
+1		9.9	77.6
♯		10.5	77.0
Cb		11.5	76.0
+5		10.9	77.1
S		11.0	76.5
	1464		
H	= 6.9' Conc. Dr.	8.68	78.78
	1474		
S+13	= 2.25' Conc. Walk	10.20	77.16
	1491		
H+1	= 3' Conc. Walk	8.11	79.35
	2+0		
S		9.6	77.9
+15		9.4	78.1
Cb		9.8	77.7
+2		10.2	77.3
♯		9.5	78.0
+18		9.4	78.1
Cb		9.0	78.5

87.46			
+2		8.7	78.8
H		8.3	79.2
	2+17		
H+1.1	= 2.9' Conc. Drive	7.69	79.77
	2+25		
H+1.3	= 1.4' End 6" Conc. Wall	7.43	80.03
	2+46		
H	= 3' Conc. Walk	7.09	80.37
+1.5	= Sky 3' " "	7.11	80.35
+1.5	Ground	7.4	80.1
+18		8.0	79.5
Cb		8.4	79.1
+1		8.6	78.9
♯		8.5	79.0
+18		9.0	78.5
Cb		8.5	79.0
+15		7.9	79.6
S		8.6	78.9
	2+66		
H+1.7	= 6.6' 2" Ribbon Conc. Drive	6.96	80.50
	Conc. Wall From Part End: 1.4' Conc. Dr.		
	3+0		
S		7.9	79.6
Cb		7.1	80.4
+2		7.9	79.6

87.46

L	7.4	801
+18	7.2	803
C6	6.7	808
+3	6.3	812
H	5.9	816

87.50

H	4.7	828
+18	5.2	823
C6	5.8	817
+2	6.2	813
L	6.4	811
+17	7.1	804
C6	6.6	809
+4	6.5	810
S	7.1	804

91.0

S	6.2	813
C6	5.4	821
+2	6.1	814
L	5.4	821
+15	5.0	825
C6	4.2	833
+3	5.5	840
H	3.6	839

87.46

91.50

H	3.8	847
+18	3.2	84.3
C6	3.5	84.0
+1	4.3	83.2
L	4.6	82.9
+18	5.3	82.2
C6	4.8	82.7
S	5.6	81.9

91.73.5

H+64	= 3' Conc. Walk	1.97	85.49
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91.98 = H.L. DANCER

S	5.2	82.3
C6	4.3	83.2
+1	4.8	82.7
L	4.1	83.4
+18	3.5	84.0
C6	3.8	84.7
+4	2.3	85.2
H	1.7	85.8

TR	0.91	97.91	10.46	97.00
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B.M		11.51	66.40	S.W. BP 65.40
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Cross Section Alley Block 19 Ocean Beach
 From Ebers to Froude Battery
 Del Mar + Coronado

BM 0.63 106.07 ✓ 105.44 ^{N.W. Mon} Coronado
 + EBERS

0-12 - F cb Ebers

H	07 Pav	10.90	9517
L	" "	11.54	9453
S	" "	12.24	9383

0+0 - F L Ebers

S	Top cb	11.39	9468
S	Gutter on Pav	11.43	9464
L	" "	11.41	9466
H	" "	10.63	9544
H	Top cb	10.00	9607

Reduced by Guttensohn + 01
 Plotted by Hough/stimp

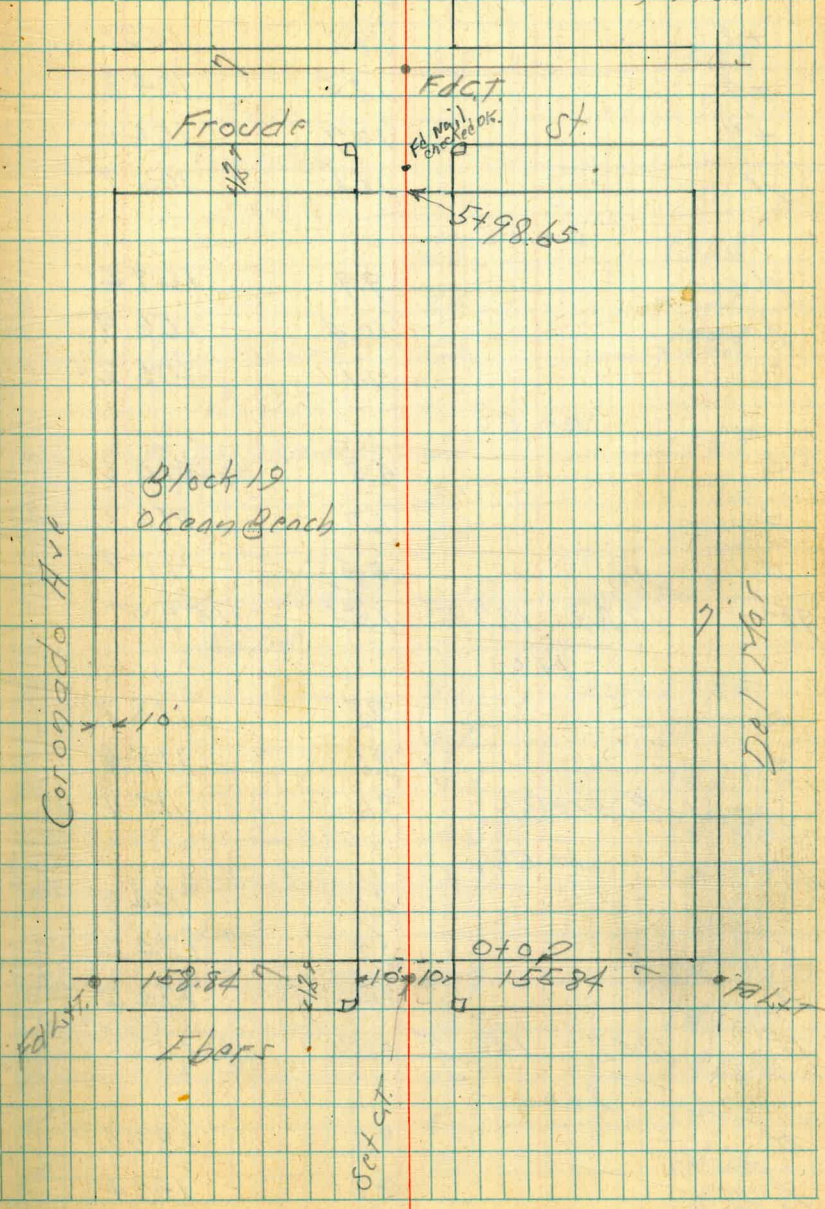
H		0.0	10607
+4		0.2	1059
+5		7.2	989
L		10.7	954
+3		8.8	973
+5		1.9	1042
S		2.2	1039

TP 11.89 117.29 ✓ 0.67 105.40 ✓
 0+10

S		11.6	1057
+5		11.0	1063
+7		14.6	1027
L		15.0	1023

~~INDEXED~~
 EFB

May 9-40 59
 Sisson
 Hartberg
 St Moore



		117.29		
+3		14.2	1031	
+4		12.5	1048	
+7		10.7	1066	
H		10.6	1067	
	0+15			
H		9.9	1074	
L		10.4	1069	
S		11.1	1062	
	0+50			
S		6.5	1108	
L		6.0	1113	
H		5.4	1119	
TP	12.23	127.96	115.73	1.56
	1+0			
H		9.2	1188	
L		9.6	1184	
S - Sky Parter Pole		9.6	1184	
	1+50			
S		4.0	1240	
L		3.8	1242	
H		3.4	1246	
TP	12.52	140.12	127.60	0.36
	2+0			
H		9.7	1304	
L		9.7	1304	

		140.12		
S		9.9	1302	
	2+16			
S + 1/2 Sky Parter Pole				
	2+30			
S		6.3	1338	
L		6.5	1339	
H = 1/2 Door to Shack		6.6	1338	
	2+57			
H + 0.3 = 1/2 Door to Shack		3.2	136.9	
L		2.9	137.2	
S		2.9	137.2	
TP	12.21	152.21	140.00	0.12
	3+04			
S		9.8	1424	
L		9.9	1423	
H		10.1	1421	
+17 = 1/2 Conc Apron		10.27	141.94	
+22 = 1/2 x 3 Car Garage		10.28	141.99	
	3+31			
+22 = 1/2 x 3 Car Garage		10.28	141.93	
+17.5 = 1/2 Conc Apron		10.28	141.93	
H = 1/2 Sky Conc Wall		6.27	145.94	
H Ground		6.4	145.8	
L		6.6	145.6	
S		6.6	145.6	

		152.21		
	3+63			
S		2.7	149.4	
+0.3 = Sky Power Pole				
Z		2.3	149.8	
H		2.3	149.8	
TP	12.42	164.62	0.01	152.20
	4+0			
H		8.3	156.3	
Z		9.2	155.4	
S		9.2	155.4	
	4+50			
S		2.1	162.5	
Z		1.8	162.8	
H		1.3	163.3	
TP	12.36	176.78	0.20	164.42
	4+63			
S+0.4 = Sky Power Pole				
	5+0			
H		5.9	170.9	
Z		6.2	170.6	
+8		6.6	171.2	
S		7.2	169.6	
TP	8.81	185.43	0.16	176.52

		185.43		
	5+50			
-10		10.3	175.1	
S		8.7	176.7	
Z		8.5	177.1	
H		7.6	177.8	
	5+75			
H		4.0	181.1	
Z		4.7	180.7	
S		5.2	180.2	
	5+88			
H = Z Garage Dirt Floor 3.0				
	5+98.65 = H.L. Fraude		182.4	
S Topch		4.35	181.08	
J Gutter on Paving		4.54	180.89	
Z " " "		4.01	181.42	
H " " "		3.24	182.19	
H Topch		2.91	182.52	
	6+10.65 = H.C.B. Fraude			
H on Paving		3.44	181.99	
Z " " "		4.13	181.30	
S " " "		4.95	180.48	
	F.L. Fraude			
H Topch		1.89	182.54	
			182.54	
			For chng See p. 31/1002 8/1/02	
			182.67	

Cross Section Hugo St.
 RE Reservoir to Miller

INDEXED
 EFB

BM	2.10	12.02	9.92	SW 1/4 on Reservoir to Miller
TP	4.64	7.55	9.11	2.91
TP	8.30	12.05	8.80	3.75

0+16 = 14 Cb Reservoir

-25 = Cb Top FC	8.73	3.32	
-25 Gutter on Pav	9.35	2.70	
S	" "	9.19	2.86
Cb	" "	9.13	2.92
±	" "	9.03	3.02
Cb	" "	8.99	3.06
H	" "	9.06	2.99
+25	" "	9.11	2.94
+25 = Cb Top FC	8.50	3.55	

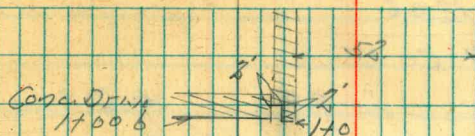
0+0 = 14 Reservoir

H	8.6	3.5	
+8.5 = Cb Top	8.55	3.50	
+8.5 Gutter on Pav	9.35	2.70	
Cb	" "	9.00	3.05
±	" "	9.00	3.05
Cb	" "	9.15	2.95
+9.5	" "	9.31	2.74
+9.5 = Cb Top	8.71	3.34	
S	8.7	3.4	

70' wide
 18' Cb.
 8.5' ±

May 27-40
 Sisson
 Hartgen
 & Moore

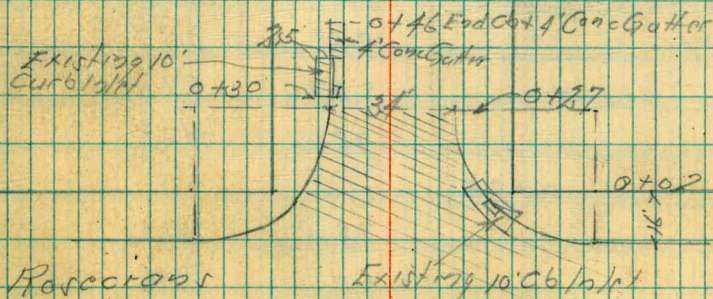
62



Locust

0+02

3+02



12.05

0+27-C6 EC

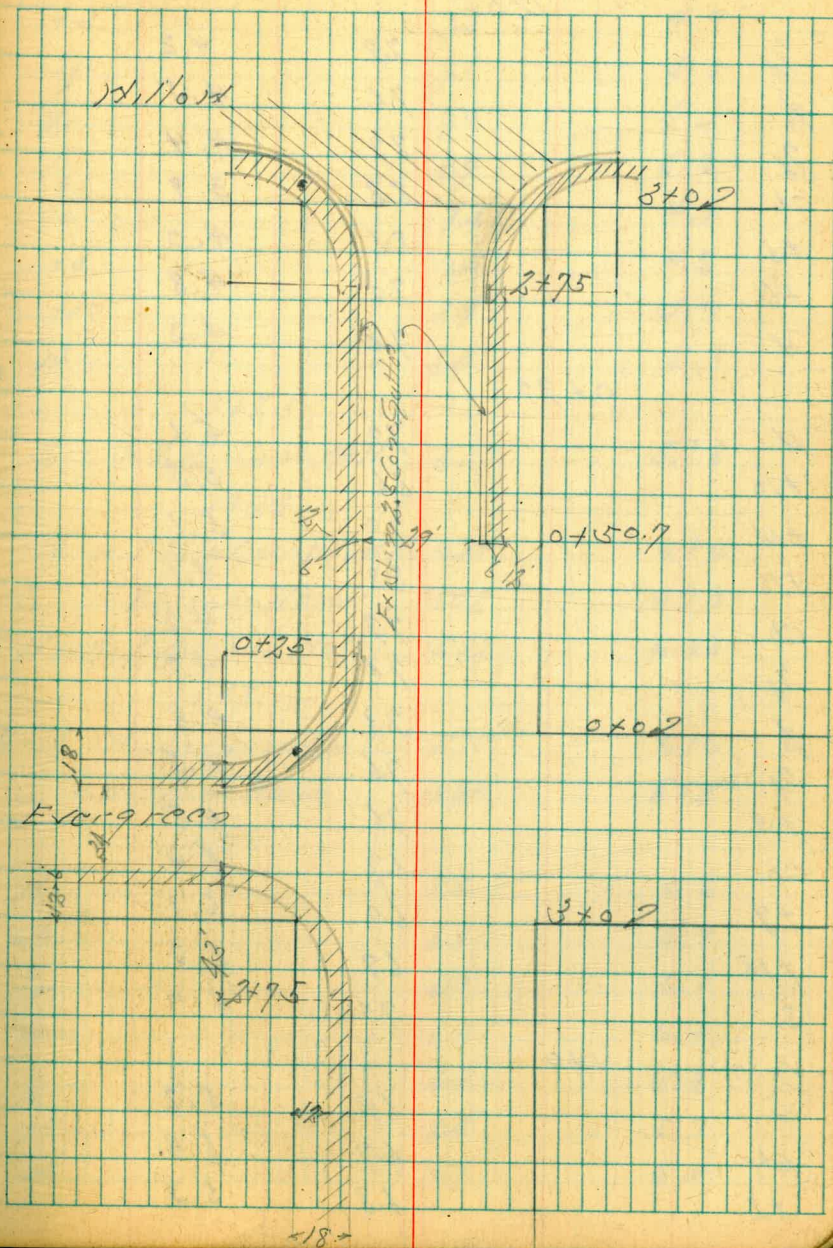
S	7.9	4.2
C6 Top	8.21	3.84
Gutter on Paving	8.84	3.21
1/4 " "	8.68	3.37
1/2 " "	8.64	3.41
1/4 " "	8.73	3.32
Gutter " "	8.88	3.17
C6 Top	8.25	3.80
H	7.5	4.6

0+46

H	8.1	4.0
+1/4	8.0	4.1
C6	8.5	3.6
1/4	8.3	3.8
1/2	8.2	3.9
1/4	8.3	3.8
+1/8 = Edge Cond Gutter	8.4	3.65
Gutter	8.48	3.57
C6 Top = End.	7.87	4.18
S	7.8	4.3

0+75

S	7.8	4.3
C6	7.7	4.4
+1/8	7.9	4.2



12.05

1/4	79	4.2
1/2	76	4.5
1/4	77	4.4
C6	8.2	3.9
+3	8.1	4.0
+6	7.3	4.8
H	7.8	4.3

0+90

H	7.0	5.1
+10	6.6	5.5
+14	7.0	5.1
+16	8.0	4.1
C6	7.9	4.2
1/4	7.4	4.7
1/2	7.3	4.8
1/4	7.6	4.5
+5	7.6	4.5
C6	6.7	5.4
+7	6.0	6.1
+13	6.9	5.2
S	7.4	4.7

1+0

S	6.9	5.2
C6	6.7	5.4
+3	6.8	5.3

12.05

+3	7.2	4.9
1/4	7.1	5.0
1/2	7.0	5.1
1/4	6.9	5.2
C6	7.4	4.7
+4	7.5	4.6
+10	6.4	5.7
H	6.4	5.7

1+23

S	= 1/2 3' Conc Walk	6.27	5.78
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1+33

+18	= Fly Do Garage Conc Floor	5.89	6.16
-----	----------------------------	------	------

S	= Fly Conc Apron	5.92	6.13
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H+57	= 1/2 4.3 Conc Walk	5.82	6.23
------	---------------------	------	------

1+48

S-18	= Fly Do Garage Conc Floor	5.89	6.16
------	----------------------------	------	------

S	= Fly Conc Apron	5.90	6.15
---	------------------	------	------

1+50

H	5.5	6.6
---	-----	-----

C6	6.4	5.7
----	-----	-----

1/4	6.0	6.1
-----	-----	-----

1/2	6.0	6.1
-----	-----	-----

1/4	6.3	5.8
-----	-----	-----

+5	6.4	5.7
----	-----	-----

C6	5.7	6.4
----	-----	-----

12.05		
S		6.3
	2+0	
S		7.7
Cb		7.4
+2		7.1
1/4		7.3
1/2		7.5
1/4		7.4
Cb		7.0
H		8.0
	2+10	
S-02 = 8' Conc Drive	4.14	7.91
	2+35.5	
S	2' Conc Stalk	8.58
	2+50	
H		9.4
+14		9.6
Cb		8.7
+2		8.5
1/4		9.1
1/2		9.1
1/4		9.0
+5		8.5
Cb		9.1
S		8.9

12.05		
	2+75	
S		9.3
Cb		10.0
+2		10.0
+4		9.4
1/4		9.5
1/2		9.8
1/4		9.8
Cb		9.3
+3		10.1
H		10.1
	2+0 = F.A. Locust	
H		10.6
+15		10.5
Cb		10.1
1/4		10.5
1/2		10.5
1/4		10.2
+1		10.0
Cb		10.6
S		10.1
	F.Cb Locust	
S		10.7
Cb		11.1
+1		10.6

12.05

1/4		1.4	10.7
1/2		1.1	11.0
1/4		1.2	10.9
+5		1.6	10.5
cb		0.8	11.3
H		0.6	11.5
	1/2 Locust		
H		0.3	11.8
cb		0.7	11.4
1/4		0.7	11.4
1/2		0.7	11.4
1/4		1.0	11.1
+4		1.1	11.0
cb		0.8	11.3
+3		0.6	11.5
S		0.9	11.2
TP	10.33 22.12	0.26	11.79
	H cb		
S		10.6	11.5
cb		9.8	12.3
+3		10.7	11.4
1/4		10.7	11.4
1/2		10.3	11.8
1/4		10.4	11.7
+4		10.6	11.5

22.12

cb		10.1	12.0
H		9.3	12.8
	1/2 Locust = 0.0		
H		8.3	13.8
cb		8.8	13.3
+2		9.7	12.4
1/4		9.7	12.4
1/2		9.6	12.5
1/4		10.0	12.1
+5		10.1	12.0
cb		9.0	13.1
S		10.0	12.1
	0.25		
S		7.8	14.3
+10		7.3	14.8
cb		7.9	14.2
+2		8.2	13.9
+3		9.2	12.9
1/4		8.8	13.3
1/2		8.5	13.6
1/4		8.6	13.5
+7		8.9	13.2
cb		8.0	14.1
H		7.6	14.5

22-12

0+28		
H = $\frac{1}{2}$ 3' Conc Walk	7.10	15.02
0+50		
H	6.3	15.8
+15	6.7	15.4
Cb	7.1	15.0
$\frac{1}{4}$	7.0	15.1
$\frac{1}{8}$	7.0	15.1
$\frac{1}{4}$	7.1	15.1
Cb	7.9	14.2
+3	7.6	14.5
+5	6.0	16.1
+11	5.8	16.3
S	6.0	16.1
0+69		
H+0.2 = $\frac{1}{2}$ 3' Conc Walk	4.89	17.23
0+91		
H-0.2 = $\frac{1}{2}$ 7' 2 Rib Conc Dr.	4.06	18.06
1+0		
S	4.4	17.7
+15 = $\frac{1}{4}$ Conc Walk	5.7	16.4
Cb 19 Drive Conc.	6.35	15.77
Cb Ground	5.6	16.5
$\frac{1}{4}$	5.1	17.0
$\frac{1}{8}$	4.7	17.4

22-12

$\frac{1}{4}$		5.0	17.1
Cb		5.0	17.1
+2		4.3	17.8
H		4.1	18.0
1+09			
H	= $\frac{1}{2}$ 6.6' 2 Rib Conc Dr.	3.55	18.57
1+26			
H	= $\frac{1}{2}$ 8' Conc Dr. ^{with}	2.85	19.27
1+48			
H-0.3 = $\frac{1}{2}$ 8' Conc Dr. ^{with}		2.18	19.94
1+50			
H		2.2	19.9
+16		2.3	19.8
Cb		3.1	19.0
$\frac{1}{4}$		2.9	19.2
$\frac{1}{8}$		2.8	19.3
$\frac{1}{4}$		3.2	18.9
Gutter		4.0	18.1
S Cb Top		3.78	18.34
TP	11.18	3.56	20.38
2+0			
S Cb Top + Ground		11.20	20.36
$\frac{1}{4}$		10.9	20.7
$\frac{1}{8}$		10.6	21.0
$\frac{1}{4}$		10.6	21.0

37.56

+7	10.6	21.0
Cb	10.3	21.3
+12	9.8	21.8
H	9.5	22.1

2+50

H	7.7	23.9
+15	8.1	23.5
Cb	9.0	22.6
1/4	8.8	22.8
1/2	8.5	23.1
1/4	8.8	22.8
5 Cb Top + Ground	9.01	22.55

2+75

5 Cb Top + Ground	7.95	23.61
1/4	7.7	23.9
1/2	7.4	24.2
1/4	7.8	23.8
Cb	8.1	23.5
+3	7.1	24.5
H	6.7	24.9

SF Return 2

Cb Top BC	7.95	23.61
+10.21	7.46	24.10
+20.43	7.15	24.41
+30.64	6.91	24.65
+40.86	6.63	24.93

37.56

3+0 = Fk. Energy cor

H	5.7	25.9
+15	6.2	25.4
Cb	7.0	24.6
1/4	6.8	24.8
1/2	6.4	25.2
1/4	6.6	25.0
Cb	7.0	24.6
+8 = Gutter at Cb Top	7.0	24.6
5	6.9	24.7

FCb Energy cor

5	6.6	25.0
Cb	6.3	25.3
1/4	5.9	25.7
1/2	5.9	25.7
1/4	6.2	25.4
Cb	6.3	25.3
+3	5.5	26.1
H	5.0	26.6

1/2 Energy cor

H	4.8	26.8
Cb	5.4	26.2
1/4	5.5	26.1
1/2 = M.H.P.M	5.10	26.46
1/4	5.4	26.2

Harpost.

21.56

Cb 5.6 26.0

J 5.7 25.9

W Cb Energ 100

J 5.1 26.5

Cb 5.1 26.5

1/4 4.9 26.7

1/2 4.8 26.8

1/2 5.1 26.5

76 5.1 26.5

Cb 4.7 26.9

H 4.2 27.4

W L Energ 100 20+

H 3.0 28.6

Cb 3.9 27.7

+1 4.7 26.9

1/4 4.4 27.2

1/2 4.3 27.3

1/4 4.4 27.2

Cb 4.7 26.9

+8 Gut 4.9 26.7

+8 Cb Top 4.39 27.17

J 4.3 27.3

S W Pictur 9

BC Top Cb 3.26 28.30

+10.21 Top Cb 3.72 27.84

31.56

+10.21 Gutter 4.54 27.02

+20.43 " 4.98 26.58

+20.43 Cb Top 4.15 27.41

+30.64 " " 4.50 27.06

+30.64 Gutter 5.33 26.23

+40.86 " " 5.56 26.00

+40.86 Cb Top 4.76 26.80

0+2.5 Cb BC

S Cb Top 3.26 28.30

Gutter 4.09 27.47

+2.5 Edge Case Gutter 3.93 27.63

1/4 3.7 27.9

1/2 3.4 28.2

1/4 3.6 28.0

+7 3.8 27.8

Cb 3.9 28.7

1/4 3.2 29.4

H 1.9 29.7

0+1.50

H 1.3 30.3

Cb Top 3.08 29.48

Gutter 2.83 28.73

+2.5 Edge Gut 2.76 28.90

1/4 2.5 29.1

1/2 2.4 29.2

21.56

1/4		26	29.0
+6 = Edge Gutter		2.81	28.75
Gutter		2.97	28.59
SCb Top		2.13	29.43
TP	12.49	43.02	1.03
	17.0		30.53
SCb Top		11.34	31.68
Gutter		12.15	30.87
+2.5 = Edge Gutter		12.01	31.01
1/4		12.0	31.0
1/2		11.8	31.2
1/4		12.0	31.0
+6 = Edge Gutter		12.23	30.79
Gutter		12.28	30.74
HCB Top		11.53	31.49
	17.50		
HCB 17 Drive		10.20	32.82
Gutter		10.35	32.67
+2.5 = Edge Gutter		10.26	32.76
1/4		9.8	33.2
1/2		9.6	33.4
1/4		9.7	33.3
+6 = Edge Gutter		9.76	33.26
Gutter		9.89	33.13
SCb Top		9.06	33.96

43.02

	24.0		
SCb Top		6.87	36.15
Gutter		7.67	35.35
+2.5 = Edge Gut		7.50	35.52
1/4		7.5	35.5
1/2		7.3	35.7
1/4		7.7	35.3
+6 = Edge Gut		8.08	34.94
Gutter		8.18	34.84
HCB Top		7.40	35.60
	27.25		
HCB		6.47	36.55
Gutter		7.27	35.75
+2.5 = Edge Gut		7.18	35.84
1/4		6.7	36.3
1/2		6.3	36.7
1/4		6.3	36.7
+6 = Edge Gut		6.33	36.69
Gutter		6.55	36.47
SCb Top		5.70	37.32
	27.50		
SCb Top		4.32	38.70
Gutter		5.15	37.87
+2.5 = Edge Gut		4.96	38.06
1/4		5.0	38.0

Hugo St.

4302

2	5.0	38.0
1/4	5.4	37.6
+6 = Edgr Gut	5.79	37.23
Gutter	5.87	37.15
+ Cb 10 Drive	5.77	37.25

2+7.5 = Cb BC

+ Cb Top	3.08	39.94
Gutter	3.90	39.12
+2.5 = Edgr Gut	3.76	39.26
1/4	3.4	39.6
2	3.1	39.9
1/4	3.2	39.8
+6 = Edgr Gut	3.21	39.81
Gutter	3.37	39.65
5 Cb Top	2.50	40.52

3+0 = F.L. J. 11/01

5 + 10 = Cb Top	0.28	42.74
Gutter 00 Conc Gut.	1.06	41.96
Cb " Pa 1000	0.97	42.05
1/4 " "	1.11	41.91
2 " "	1.28	41.74
1/4 " "	1.41	41.61
Cb " "	1.58	41.44
+8 = Gutter	1.87	41.15
+8 = Cb Top	1.10	41.92

72

4302

N.E. Return

+10.21 Cb Top	2.36	40.66
Gutter	3.14	39.88
+20.43 Cb Top	1.54	41.48
Gutter	2.36	40.66
+30.64 Cb Top	1.02	42.00
Gutter	1.84	41.18
+40.86 Cb Top	1.02	41.99
Gutter	1.84	41.18

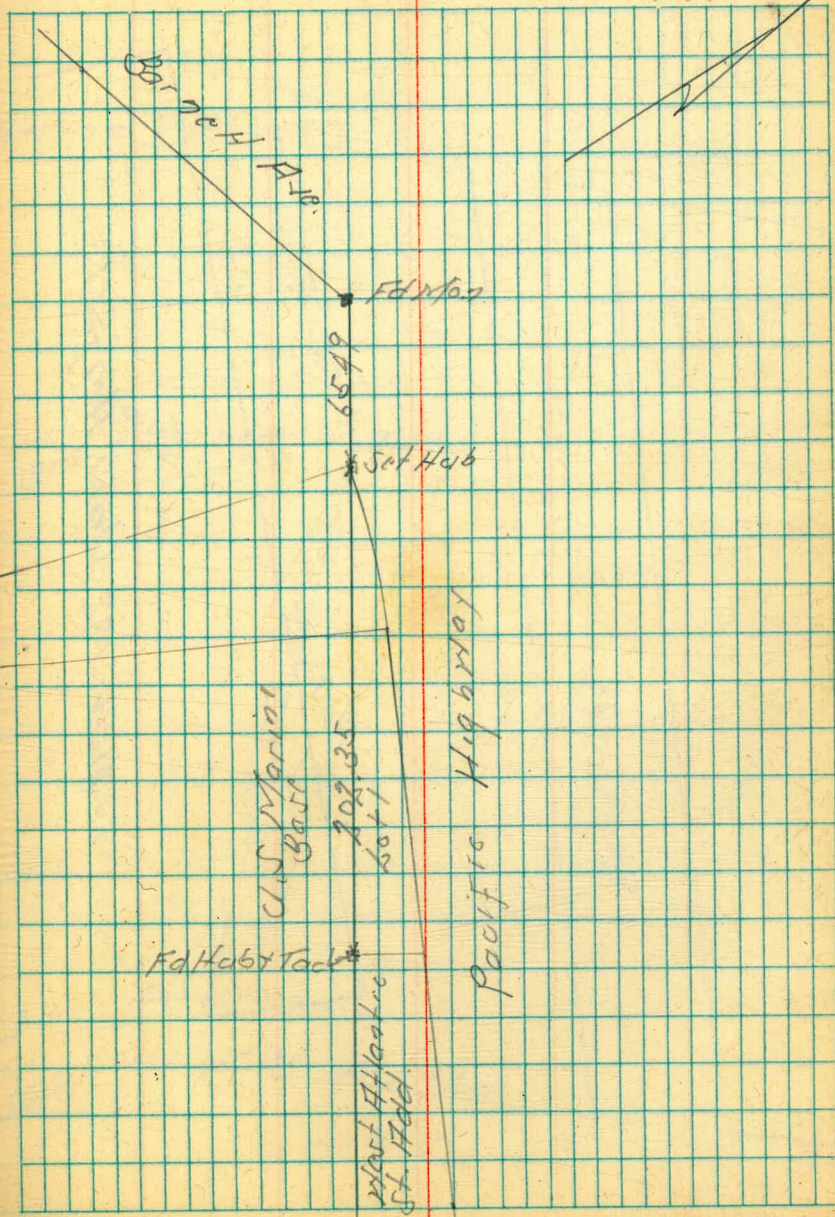
S.F. Return

+10.21 Cb Top	1.59	41.43
Gutter	2.40	40.62
+20.43 Cb Top	0.74	42.28
Gutter	1.52	41.50
+30.64 Cb Top	0.08	42.94
Gutter	0.85	42.17
TP 11.31 52.83	1.50	41.52
+40.86 Cb Top	9.78	43.05
Gutter	10.60	42.23
BM	1.86	51.47

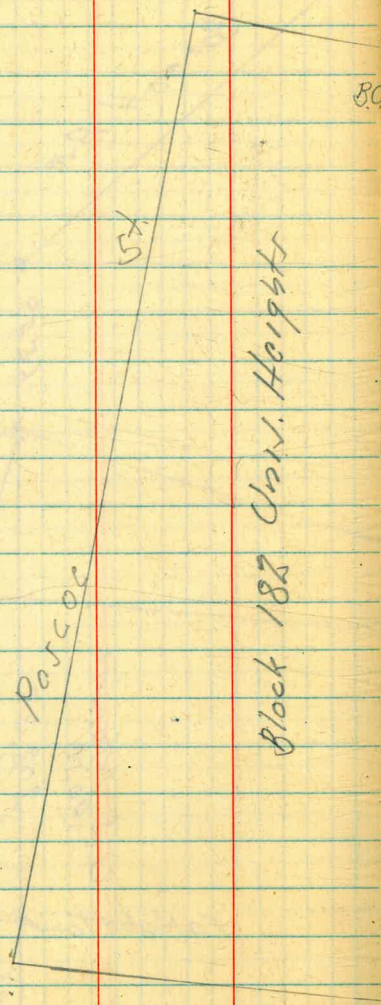
5.48 P
J. 11/01
51.45

Survey Lot 1 West Atlantic Hdd.

May 24^o
SAS 09 72
Harkberg
W Moore



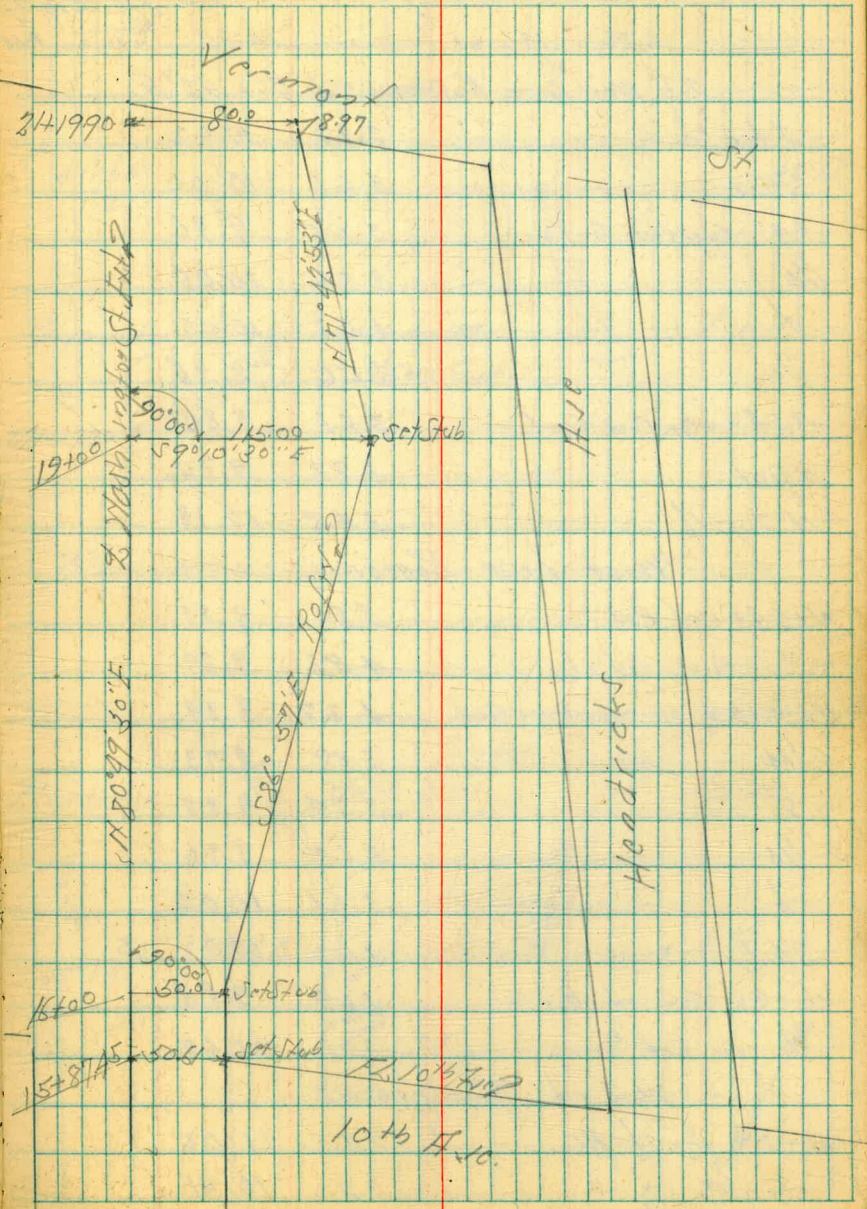
EX Washington Street Extension
 South of 1st Line Block 182 Clav. Hts
 See Sketch Page 4



INDEXED
 EFB

Aug. 30-40
 Sisco
 Northorn
 Osborne

73



Walker
Bliss
Hale
9-7-40

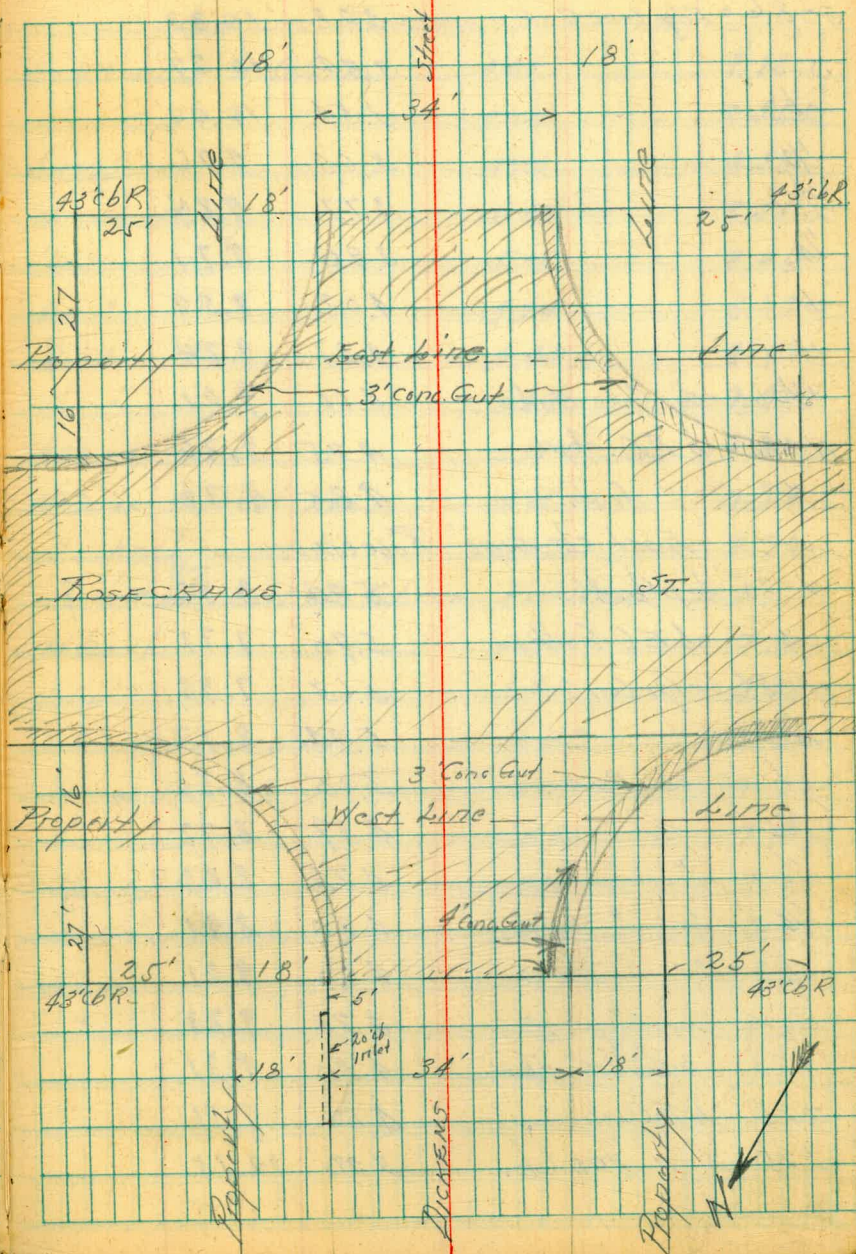
Curb And Paving Levels
on Dickens And Rosecrans Streets

Dickens = 34' Roadway
25' 1/4
S.N. 5th Top H/d
Rosecrans
& Dickens P.H.

2.76	13.61	10.85
27' West Line Rosecrans = cb B.C. 43' R.		
J top cb.	2.99	10.62
" Gut.	3.61	10.00
+ 4' Edge Conc. Gutter	3.65	9.96
1/4	3.56	10.05
2	3.52	10.09
1/4	3.66	9.95
+ 5.5 = edge Conc. Gutt	3.81	9.80
N Gut	3.91	9.70
N top cb.	3.43	10.18
West Line Rosecrans		
N+8.4 = Ncb Ret	3.80	9.81
" Gut. at cb.	4.32	9.29
NL + 12.2 on edge Conc Gutt	4.22	9.39
1/4	3.88	9.73
2	3.74	9.87
1/4	3.65	9.96
cb	3.61	10.00
+ 5.7	3.58	10.03
cb + 9.6 = gut at Ret.	3.63	9.98
cb. on Ret.	3.01	10.60
West cb Rosecrans		
J-25 top cb B.C.	2.55	11.06
Gut. " "	3.20	10.41

INDEXED
E.F.B.

74



1361

Dickens St.

5-8.6 = Edge Conc Gut.	3.28	10.33
5	3.34	10.27
cb	3.54	10.07
1/4	3.65	9.96
2	3.77	9.84
1/4	3.90	9.71
cb	4.02	9.59
H	4.37	9.24
+8.6 on edge Conc. Gut.	4.60	9.01
N+25 = cb F.C. top	4.25	9.36
" " " Gut.	4.85	8.76
East cb line Rosecrans.		
N-25' top cb. Bl.	5.29	8.32
" cb F.C. Gutter.	5.90	7.71
N-8.6 = edge Conc "	5.63	7.98
N line	5.44	8.17
cb " on Pav.	5.05	8.56
1/4 " "	4.89	8.72
2 " "	4.78	8.83
1/4 " "	4.70	8.91
cb " "	4.60	9.01
5 " "	4.38	9.23
+8.6 on ^{edge} Conc. Gutter	4.30	9.31
+25' cb F.C. "	4.10	9.51
+25 " " top cb.	3.50	10.11

1361

Dickens St. 75

East Line Rosecrans

5+8.2 top cb. of Return	4.43	9.18
" Gut " "	5.06	8.55
5+12.2 = edge Conc. Gut.	5.06	8.55
cb on Pav.	5.10	8.51
1/4 " "	5.15	8.46
2 " "	5.24	8.37
1/4 " "	5.44	8.17
cb " "	5.67	7.94
+5.3 edge Conc. Gut.	5.79	7.82
+9.3 Conc. Gut. of Ret.	5.88	7.73
" top cb. " "	5.25	8.36
? → ³⁷ 25' East of Ebene Rosecrans = cb F.C.		
1/4 top cb.	5.71	7.90
" Gut	6.33	7.28
+3' = edge Conc. Gut.	6.23	7.38
1/4 on Pav.	6.04	7.57
2 " "	5.80	7.81
1/4 " "	5.82	7.79
+5.5 = Conc. Gutter	5.74	7.87
5 cb. on "	5.79	7.82
" " top cb.	5.15	8.46

Walker,
Bliss
Hole

from P.N. = 13.61

EMERSON & Rosecrans.
cb + Paving Levels.

9-7-40 25' West of W Line Rosecrans

W top cb	6.59	7.02
" Gut.	7.26	6.35
+ 3' = edge Conc. Gut.	7.26	6.35
1/4 on Paving	7.33	6.38
1/2 " "	7.45	6.16
1/4 " "	7.80	5.81
+ 5.5" Conc.	8.07	5.54
N cb on Gut at Ret.	8.19	5.42
" top cb	7.56	6.05

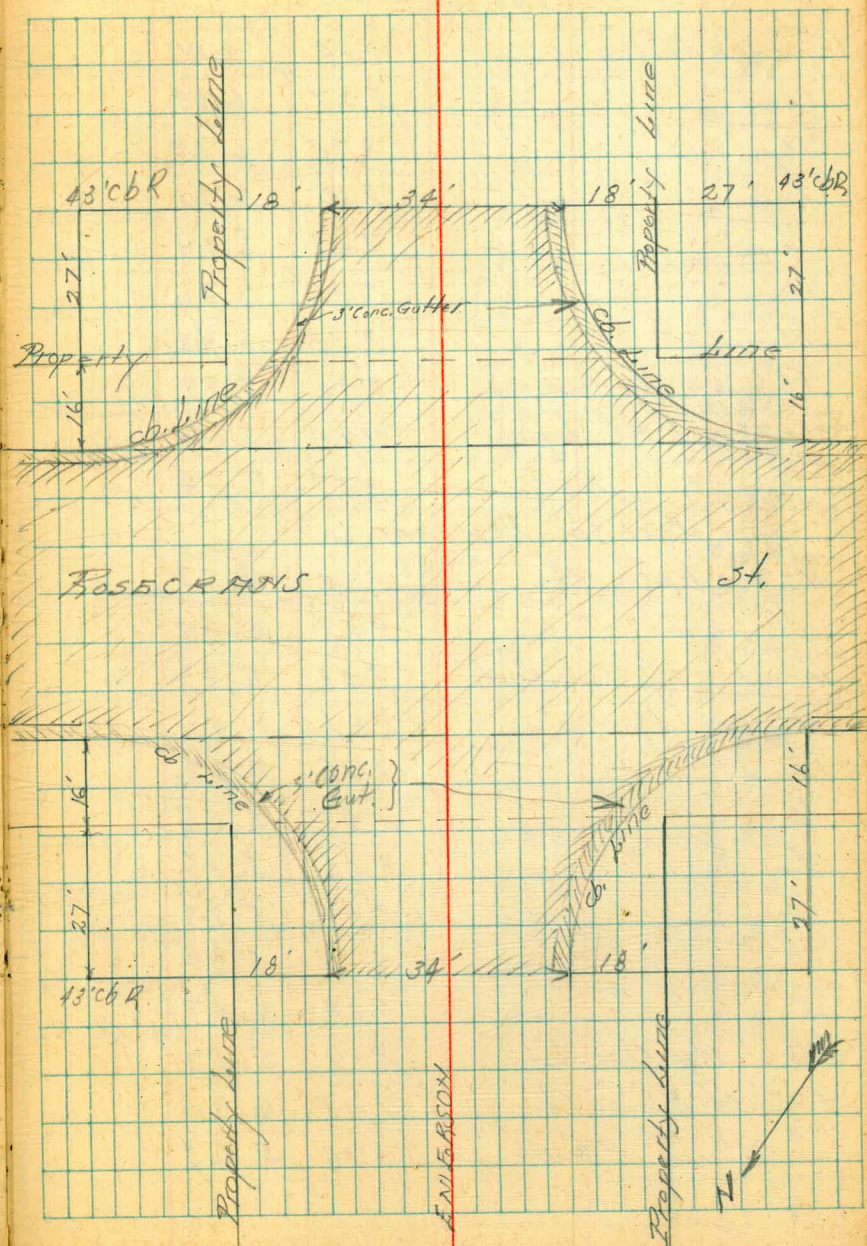
W Line Rosecrans

N+8.5 top cb	7.82	5.79
" Gut at Ret.	8.49	5.12
N+12.2 = edge conc Gut.	8.31	5.30
cb on Pav.	8.10	5.51
1/4 " "	7.81	5.80
1/2 " "	7.56	6.05
1/4 " "	7.42	6.19
cb " "	7.29	6.32
+ 4.7 = edge Conc Gut.	7.26	6.35
+ 9.9 on Gut Iron Grating	7.68	5.93
+ 9.9 " top cb at Return	6.67	6.94

West cb Rosecrans

S-25 top cb EC	6.26	7.35
" Gut " "	6.90	6.71
S-8.6 on edge Gut	7.15	6.46

76



EMERSON ST.

1361

S on Poring	714	6.47
cb " "	727	6.34
1/4 " "	737	6.24
2 " "	750	6.11
1/4 " "	767	5.94
cb " "	785	5.76
N " "	813	5.48
+8.6 on edge Conc. Gult.	832	5.29
N+25 = cb E.C. top cb.	795	5.66
" " " Gult.	857	5.04
East cb. Rosecrans		
N-25 = top cb. B.C.	904	4.57
" Gult " "	967	3.94
N-8.6 = edge Conc. Gult.	938	4.23
N on Poring	921	4.40
cb " "	874	4.87
1/4 " "	857	5.04
2 " "	846	5.15
1/4 " "	830	5.27
cb " "	827	5.34
S " "	814	5.47
+8.6 edge Conc. Gult.	809	5.52
+25 = cb B.C. on cb	727	6.34
" " " " Gult.	798	5.63

EMERSON ST.

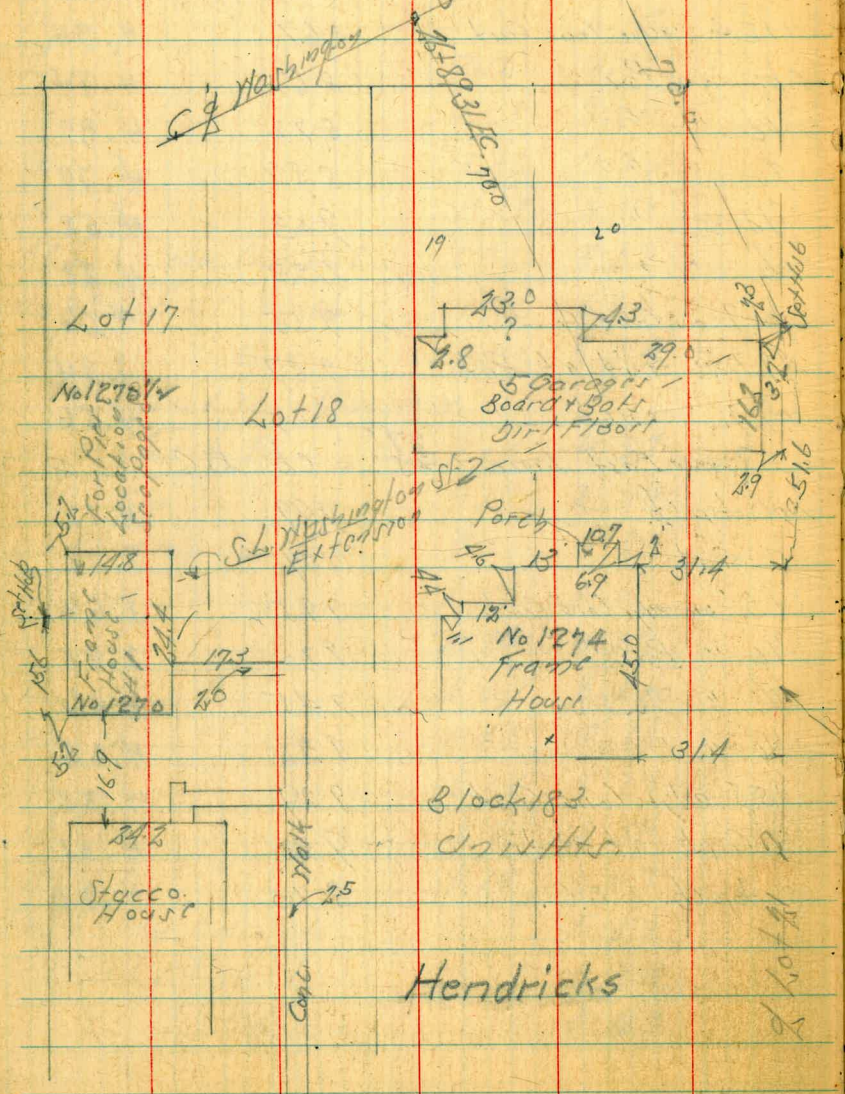
1361

East line Rosecrans.

S+8.5 = top cb. Ret.	810	5.51
" = Gult at "	874	4.87
S+12.4 = edge Conc. Gult.	867	4.94
cb on Por.	867	4.94
1/4 " "	872	4.89
2 " "	882	4.79
1/4 " "	903	4.58
cb " "	933	4.28
+5.7 on Conc. Gult.	955	4.06
+9.7 " Gult at Ret.	967	3.94
+9.7 " on cb "	905	4.56
? → East line + $\frac{27}{25}$ = cb E.C.	930	4.31
N top cb	949	4.12
" Gult	1009	3.52
+3' on edge Conc. Gult.	995	3.66
1/4 " Por.	970	3.91
2 " "	945	4.16
1/4 " "	936	4.25
+5.5 edge Conc. Gult.	939	4.32
S Gult. at Ret.	930	4.31
S top cb. " E.C.	870	4.91

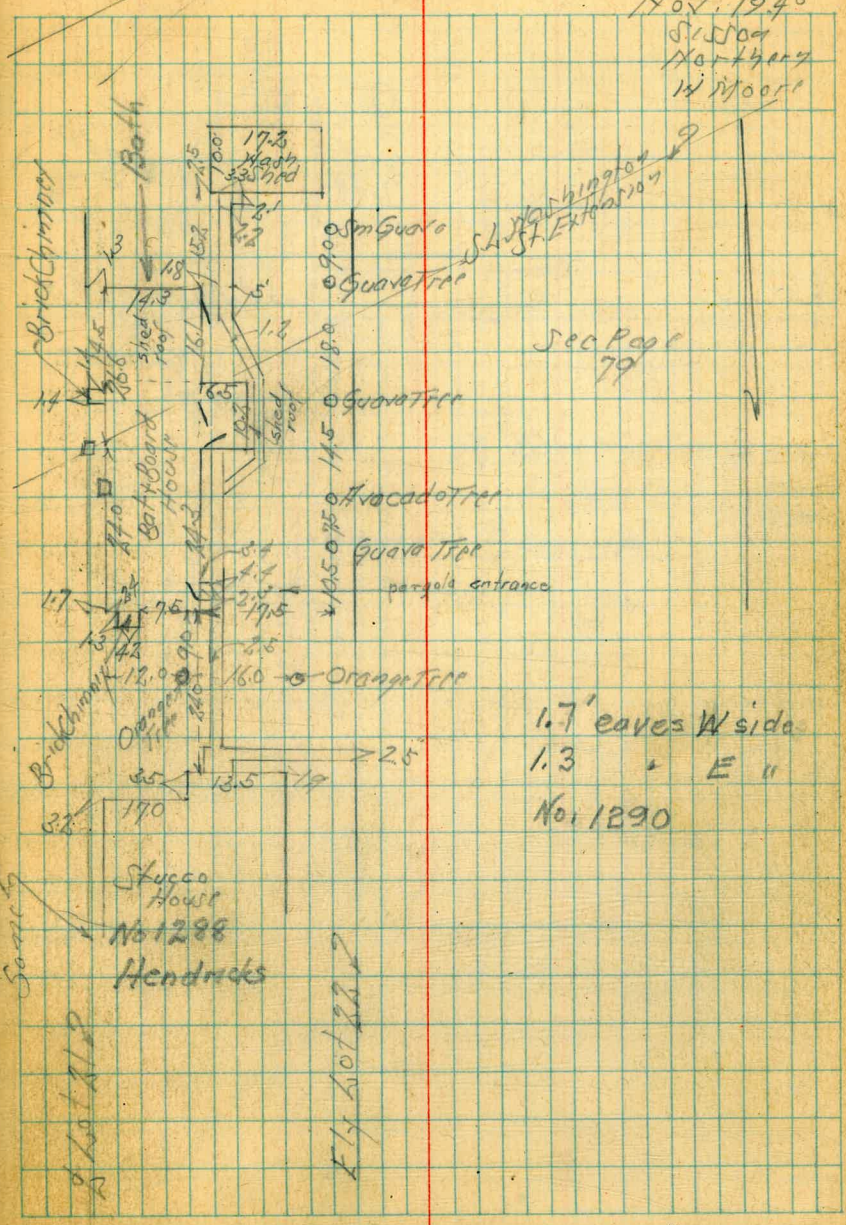
Washington St Extension
 Location of Improvements
 Block 183 Univ. Hts.
 See Pages

Parcoco St.



~~INDEXED~~
 EFB

Nov. 1940
 Stucco
 North
 1st floor



See Page
 79

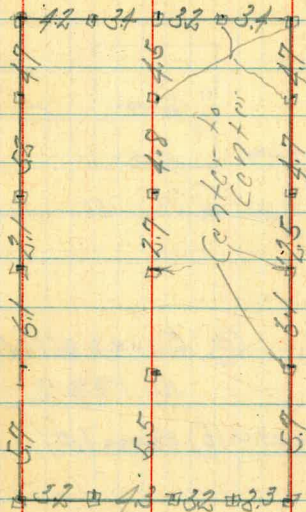
1.7' eaves W side
 1.3 " E "
 No. 1290

Stucco
 House
 No. 1288
 Hendricks

80 Location Concrete Piers
Under House #1 Lot 17 Block 183 Univ. Hts

See Page 78 For House Location

Piers 6" on Top



IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

2°-00'	0.1	21°-00'	12.3	33°-00'	29.7
3°-00'	0.3	21°-30'	13.4	33°-15'	30.1
4°-00'	0.5	22°-00'	14.0	33°-30'	30.5
5°-00'	0.8	22°-30'	14.7	33°-45'	30.9
6°-00'	1.1	23°-00'	15.3	34°-00'	31.3
7°-00'	1.5	23°-30'	15.9	34°-15'	31.7
8°-00'	1.9	24°-00'	16.5	34°-30'	32.1
9°-00'	2.5	24°-30'	17.2	34°-45'	32.5
10°-00'	3.0	25°-00'	17.9	35°-00'	32.9
10°-30'	3.3	25°-30'	18.6	35°-15'	33.3
11°-00'	3.6	26°-00'	19.2	35°-30'	33.7
11°-30'	4.0	26°-30'	19.9	35°-45'	34.1
12°-00'	4.3	27°-00'	20.6	36°-00'	34.6
12°-30'	4.7	27°-30'	21.3	36°-15'	35.0
13°-00'	5.1	28°-00'	22.0	36°-30'	35.4
13°-30'	5.5	28°-30'	22.8	36°-45'	35.8
14°-00'	5.9	29°-00'	23.5	37°-00'	36.2
14°-30'	6.3	29°-30'	24.3	37°-15'	36.6
15°-00'	6.7	30°-00'	25.0	37°-30'	37.1
15°-30'	7.2	30°-15'	25.4	37°-45'	37.5
16°-00'	7.6	30°-30'	25.8	38°-00'	37.9
16°-30'	8.1	30°-45'	26.2	38°-15'	38.3
17°-00'	8.5	31°-00'	26.5	38°-30'	38.7
17°-30'	9.0	31°-15'	26.9	38°-45'	39.1
18°-00'	9.5	31°-30'	27.3	39°-00'	39.6
18°-30'	10.1	31°-45'	27.7	39°-15'	40.0
19°-00'	10.6	32°-00'	28.1	39°-30'	40.5
19°-30'	11.2	32°-15'	28.5		
20°-00'	11.7	32°-30'	28.9		
20°-30'	12.3	32°-45'	29.3		

Chains to Feet

1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains

100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

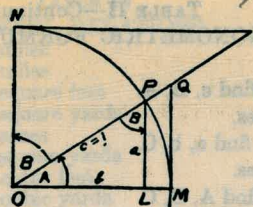


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	9995	31.242	9996	34.368	997	38.189	997	42.964	9998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60'	60'	50'	50'	40'	40'	30'	30'	20'	20'	10'	10'	deg.
cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot

TABLE VII
RODS IN FEET, 10THS AND 100THS OF FEET

Rods	Feet	Rods	Feet	Rods	Feet	Rods	Feet	Rods	Feet
1	16.50	21	346.50	41	676.50	61	1006.50	81	1336.50
2	33.00	22	363.00	42	693.00	62	1023.00	82	1353.00
3	49.50	23	379.50	43	709.50	63	1039.50	83	1369.50
4	66.00	24	396.00	44	726.00	64	1056.00	84	1386.00
5	82.50	25	412.50	45	742.50	65	1072.50	85	1402.50
6	99.00	26	429.00	46	759.00	66	1089.00	86	1419.00
7	115.50	27	445.50	47	775.50	67	1105.50	87	1435.50
8	132.00	28	462.00	48	792.00	68	1122.00	88	1452.00
9	148.50	29	478.50	49	808.50	69	1138.50	89	1468.50
10	165.00	30	495.00	50	825.00	70	1155.00	90	1485.00
11	181.50	31	511.50	51	841.50	71	1171.50	91	1501.50
12	198.00	32	528.00	52	858.00	72	1188.00	92	1518.00
13	214.50	33	544.50	53	874.50	73	1204.50	93	1534.50
14	231.00	34	561.00	54	891.00	74	1221.00	94	1551.00
15	247.50	35	577.50	55	907.50	75	1237.50	95	1567.50
16	264.00	36	594.00	56	924.00	76	1254.00	96	1584.00
17	280.50	37	610.50	57	940.50	77	1270.50	97	1600.50
18	297.00	38	627.00	58	957.00	78	1287.00	98	1617.00
19	313.50	39	643.50	59	973.50	79	1303.50	99	1633.50
20	330.00	40	660.00	60	990.00	80	1320.00	100	1650.00

TABLE VIII
LINKS IN FEET, 10THS AND 100THS OF FEET

Links	Feet	Links	Feet	Links	Feet	Links	Feet	Links	Feet	Links	Feet
1	0.66	18	11.88	35	23.10	52	34.32	69	45.54	86	56.76
2	1.32	19	12.54	36	23.76	53	34.98	70	46.20	87	57.42
3	1.98	20	13.20	37	24.42	54	35.64	71	46.86	88	58.08
4	2.64	21	13.86	38	25.08	55	36.30	72	47.52	89	58.74
5	3.30	22	14.52	39	25.74	56	36.96	73	48.18	90	59.40
6	3.96	23	15.18	40	26.40	57	37.62	74	48.84	91	60.06
7	4.62	24	15.84	41	27.06	58	38.28	75	49.50	92	60.72
8	5.28	25	16.50	42	27.72	59	38.94	76	50.16	93	61.38
9	5.94	26	17.16	43	28.38	60	39.60	77	50.82	94	62.04
10	6.60	27	17.82	44	29.04	61	40.26	78	51.48	95	62.70
11	7.26	28	18.48	45	29.70	62	40.92	79	52.14	96	63.36
12	7.92	29	19.14	46	30.36	63	41.58	80	52.80	97	64.02
13	8.58	30	19.80	47	31.02	64	42.24	81	53.46	98	64.68
14	9.24	31	20.46	48	31.68	65	42.90	82	54.12	99	65.34
15	9.90	32	21.12	49	32.34	66	43.56	83	54.78	100	66.00
16	10.56	33	21.78	50	33.00	67	44.22	84	55.44	101	66.66
17	11.22	34	22.44	51	33.66	68	44.88	85	56.10	102	67.32

125
259
1489

2750
1489
1261

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

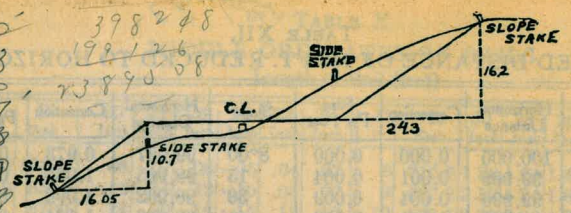
Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	18 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

17003'
115 10'
132 13
129 60
47 47
115 18
162 50
17003'

79562
24
398248
199126
7389008



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

14
122
20.7
5.5
26.2

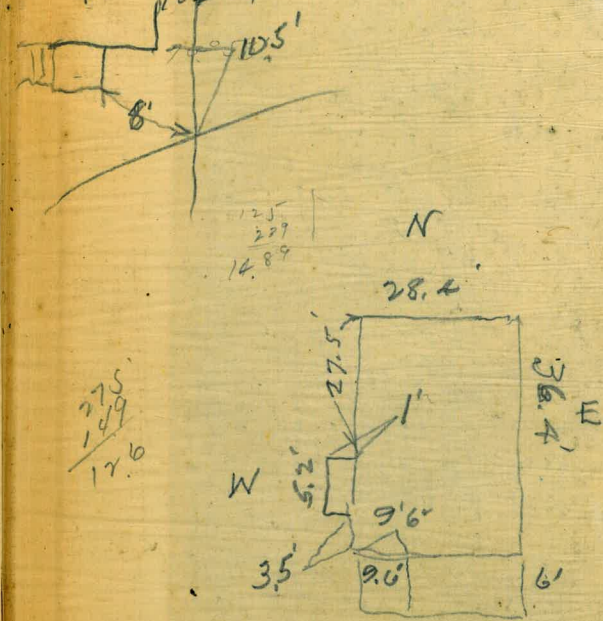
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2218

81.6
2
82.1

24.1
8.0
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34.6

179 60
72 53
107 07
179 60
64 50
115 910'

Vf
House
179 60
75 31
104 29



02853
24
37422
19706
224x8
5143
22
5121
2528
2493
5021
22

14.4 x 16.4 garage

12.5' setback House at 3780
10.0
3798