1564

FIELD BOOK

No. 385F

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

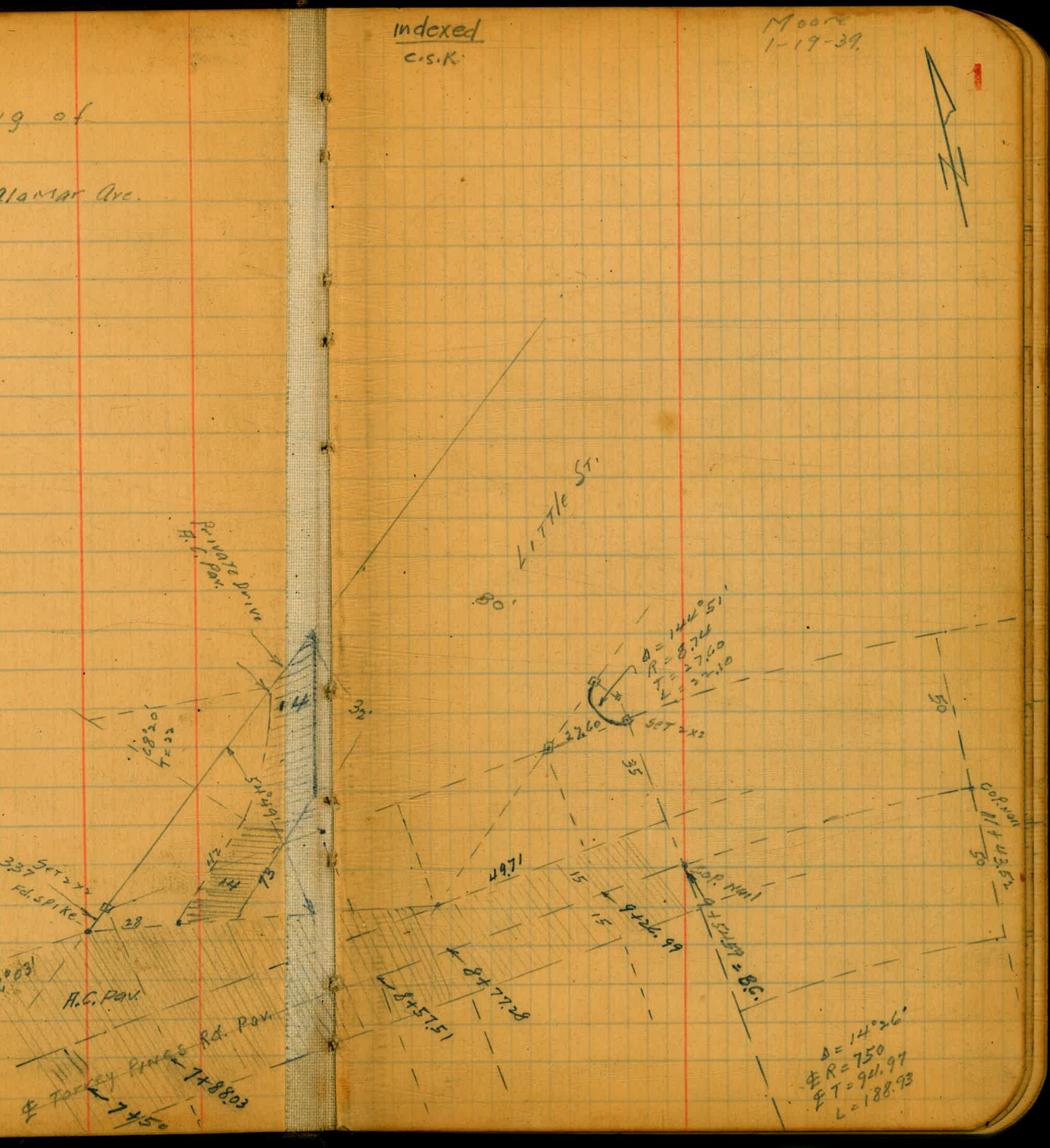
We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

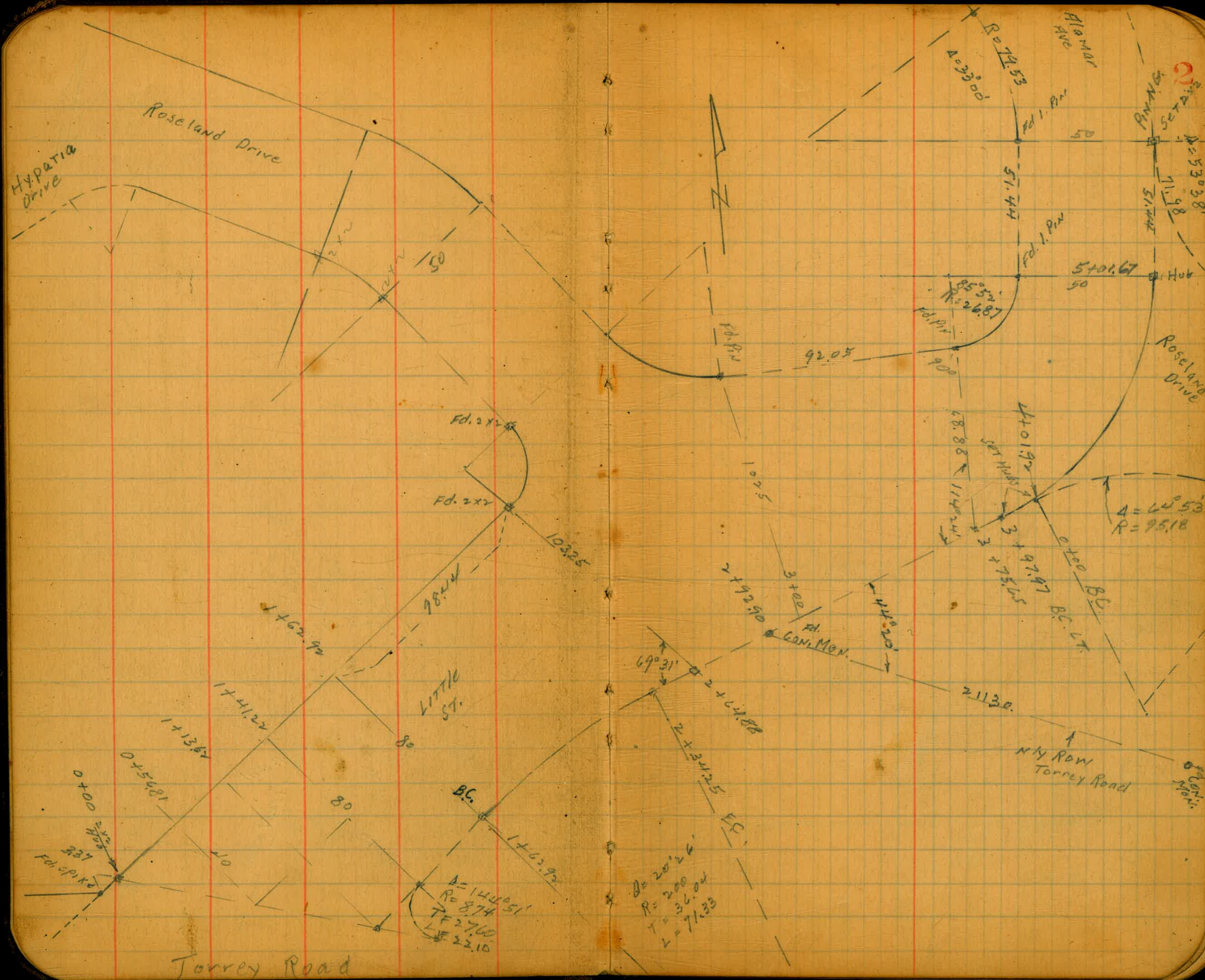
In ordering Fabri-Hide covered books, add the letter *"F"* to catalog number.

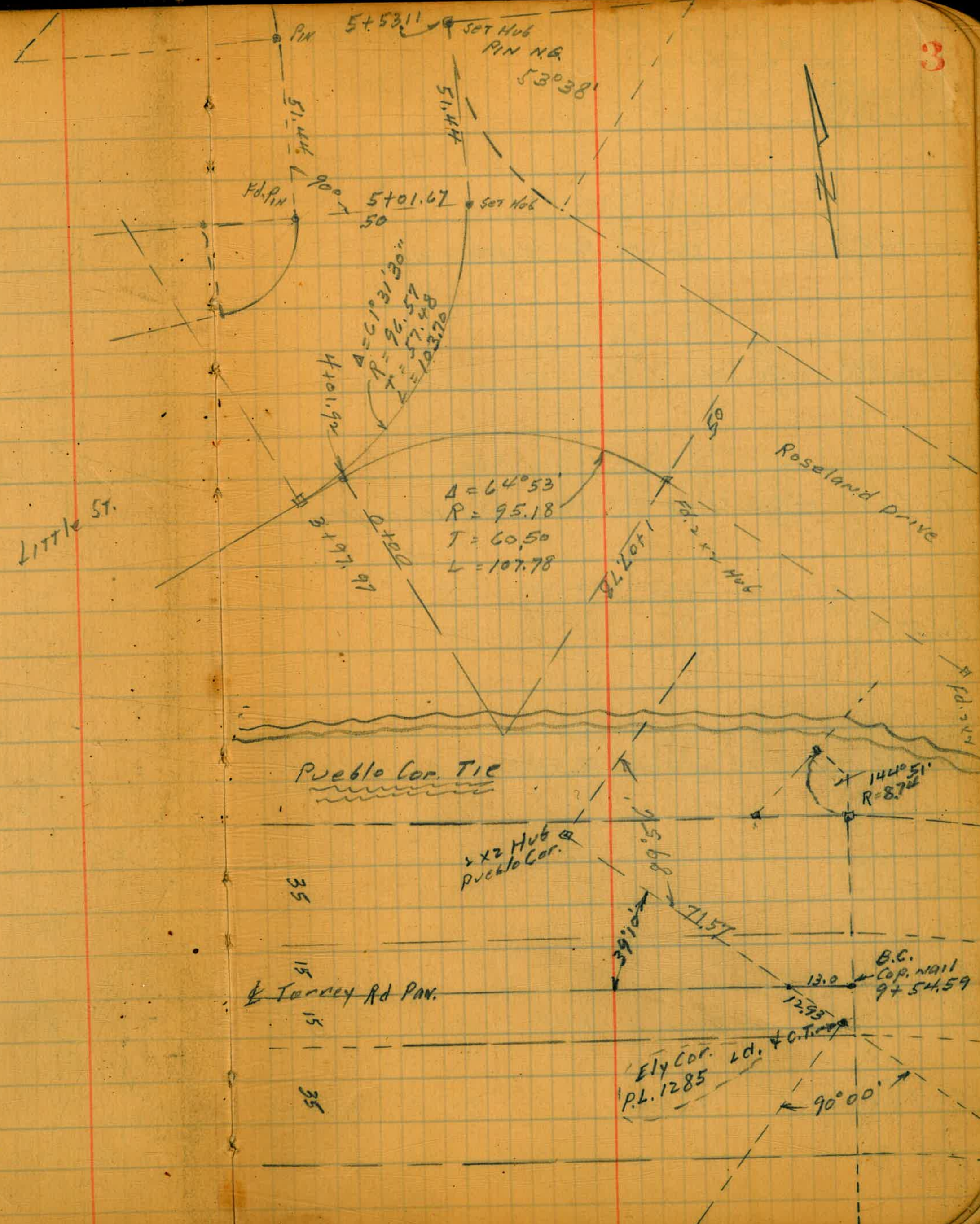
Indexed
C.S.K.

Moore
1-19-39.

Proposed opening of
LITTLE ST.
Torrey Pines Rd. to Alamar Ave.




Roseland Drive
Hypatia Drive
2x2
2x2
50
Fd. 2x2
Fd. 2x2
103.25
98.44
1+62.92
1+41.22
1+13.67
0+56.81
0+00
Fd. spike
Little St.
80
80
10
B.C.
1+63.92
Δ = 144°51'
R = 8.74
T = 27.60
L = 22.10
Torrey Road
Alamar Ave
R = 79.53
Δ = 33°00'
Fd. I. Pin
Fd. I. Pin
Fd. Pin
Fd. Pin
44.15
50
5+01.67
50
Hub
85°52'
R = 26.87
92.05
90°
88.87
4+01.92
Set Hub
Set 2x2
Δ = 53°38'
71.98
44.15
Roseland Drive
Δ = 64°53'
R = 95.18
3+97.97
3+75.65
0+00 B.C.
B.C. LT.
107.5
3+00
2+92.90
Fd. Con. Mon.
44°20'
69°31'
2+64.88
2+34.25
E.C.
211.30
N'ly Row Torrey Road
Con. Mon.
Δ = 20°26'
R = 200
T = 36.04
L = 71.33


Pin
5+53.11
Set Hub
Pin N.G.
53°38'
51.44
51.44
90°
Fd. Pin
5+01.67
50
Set Hub
Δ=61°31'30"
R=96.57
T=57.48
L=103.70
4+01.92
Little St.
3+97.97
4+00
Δ=64°53'
R=95.18
T=60.50
L=107.78
4+07.78
Fd. 2x2 Hub
50
Roseland Drive
Fd. 2x2
Pueblo Cor. Tie
144°51'
R=8.74
2x2 Hub
Pueblo Cor.
35
89.5
71.57
39°10'
15
℄ Torrey Rd Pav.
15
13.0
B.C.
Cop. nail
9+54.59
12.95
Ely Cor.
P.L. 1285
Ld. ℄ C.T.
35
90°00'

Levels on Torrey Pines Rd. & Par.
at Little St

Indexed
C.S.K.

℄ Sta.					
10+04.59	on Curve				
9+54.59	B.C. on Torrey Rd. Copper Nail				
9+26.99	opposite P.I. N.E. Torrey & Little				
8+77.28	opposite ℄ on N'ly edge Par. on Torrey Rd.				
8+57.51					
7+88.03	opposite 0+00 2x2 Hub NW Cor Little St. Torrey Rd.				
7+50					
Set B.M. B.P. in Curb			3.49	90.11	NW Cor. Torrey Rd. Little St.
B.M. N 40' R.P. Hub	8+7	93.60		85.33	9+54.59

℄ Torrey Pines Rd. Par.

86.2 / 7.4 / 50	85.3 / 8.3 / 25	85.0 / 8.60 / 15 E.P.		83.02	10.58 / 15	
79.8 / 13.8 / 50	85.8 / 7.8 / 40	86.4 / 7.2 / 30	85.99 / 7.61 / 15	85.20 / 8.40		84.49 / 9.11 / 15
78.6 / 16.0 / 50	77.6 / 16.8 / 47	86.5 / 7.1 / 35	86.52 / 7.08 / 15 E.P.	86.05 / 7.55		85.43 / 8.17 / 15
77.3 / 16.3 / 50	78.9 / 14.7 / 40	85.4 / 7.7 / 25	82.9 / 5.9 / 20	82.48 / 4.17 / 15 E.P.	87.35 / 6.25	86.95 / 6.65 / 15
83.1 / 10.6 / 50	84.6 / 9.0 / 40	87.4 / 5.7 / 27	87.84 / 5.74 / 20 E.P.	87.95 / 5.65 / 15	87.96 / 5.70	87.59 / 6.01 / 15
89.14 / 4.41 / Hub 50		89.13 / 4.47 / 46 E.P.	89.24 / 5.36 / 15	89.91 / 3.69		89.59 / 4.01 / 15
90.55 / 3.05 / 33 66		90.08 / 3.52 / 33 99	90.59 / 3.01 / 15	90.91 / 2.85		90.48 / 3.12 / 15

93.60

Levels on Little St.   Indexed
e.s.k.

1+41.22	E.C.				Cobblewall
1+13.42					
0+91.5	℄ end drive				
T.P.	0.60	81.32	12.88	80.72	
0+56.81					
0+40					
0+00	2x2 Hub	NW Cor Torrey + Little		P2	
		93.60			

W.L. Little St.   RT.

LT.

74.3 / 7.0 / 1   72.6 / 8.7   71.3 / 10.0 / 10   72.3 / 9.0 / 20   72.9 / 8.6 / 45   70.7 / 10.6 / 50   71.5 / 9.8 / 65   73.2 / 8.1 / 80

77.4 / 3.9 / 3   75.2 / 6.1   73.8 / 7.5 / 13   75.0 / 6.3 / 20   75.4 / 5.9 / 40   75.6 / 5.7 / 48   74.5 / 6.8 / 52   94.7 / 4.6 / 75   7762 / 3.70 / 80 P.I. Hub

78.7 / 2.6 Pav   77.9 / 3.4 / 32 Pav   77.4 / 3.9 / 38   75.4 / 5.9 / 45   76.3 / 5.0 / 60

81.32

84.3 / 9.3   82.4 / 11.2 / 13   82.5 / 11.1 / 20   83.2 / 10.4 / 35 Pav   83.0 / 10.6 / 40

87.8 / 5.8   85.3 / 8.3 / 15   85.1 / 8.5 / 22 Pav   85.6 / 8.0 / 36

89.19 / 4.41 on hub

93.60

T.P.	0.47	56.69	12.68	56.22	
3+00	Taken on angle to Iron Pin P.C.				55.9 / 13.0 / 105 Bank
2+80					
2+64.88	Taken on angle Sec. 69°31'				
2+34.35	E.C.				
T.P.	0.29	68.90	12.71	68.61	
1+98.58	Mid Curve				
1+62.92	B.C. Rt.				
		81.32			

Elly Little

6

Lt. | Rt.

Iron Pin P.C.

53.9/15.0/102.5 53.7/15.2/100 52.7/16.2/95 53.1/15.8/85 54.2/14.7/60 48.8/20.1/49 48.7/20.2/42 50.7/18.2/40 51.4/17.5/25 | 54.9/14.0 | 58.7/10.2/15

55.7/13.4/115 56.1/12.8/100 57.1/11.8/65 58.0/10.9/60 50.3/18.6/50 50.3/18.6/41 54.4/14.5/37 56.7/12.2/20 | 60.8/8.1 | 63.8/5.1/15

66.9/2.0/105 Top Bank 62.8/6.10/103.25 Hub 60.8/8.1/100 60.4/8.5/75 61.3/7.6/55 60.2/8.7/45 58.2/10.7/35 60.4/8.5/25 | 63.1/5.8 | 65.3/3.6/15

62.6/6.3/50 61.7/7.2/46 60.5/8.4/35 61.3/7.6/25 | 67.1/1.8 | 71.1/+2.2/15

68.90

72.6/8.7/88 67.3/14.0/83 66.9/14.4/80 67.1/14.2/60 67.7/13.6/35 65.5/15.8/25 65.5/15.8/15 | 67.5/13.8 | 70.4/10.9/15

73.0/8.3/82 70.5/10.8/80 70.3/11.0/60 70.7/10.6/32 68.9/12.4/26 | 69.1/12.2 | 70.5/10.8/10

81.32

5+53.11	P.C.			
5+01.67	E.C.			
T.P.	3.63	47.49	12.83	43.86
4+49.82	Mid Curve			
3+97.97	B.C. Left			
3+75.45	Taken on angle Line to Iron Pin			
3+30				

56.69

L.T. Ely Little 7

Rt.

W/y Line

Bank 35.5 / 12.0 / 52 · 34.0 / 13.5 / 50 · 34.0 / 13.5 / 25 · 33.7 / 13.8 / 10 · 35.3 / 12.2 / 8 · 35.1 / 12.4 · 34.2 / 13.3 / 10

38.3 / 9.2 / 60 · 38.7 / 8.8 / 50 · 38.5 / 9.0 / 25 · 37.89 / Hub 9.60 · 39.1 / 8.4 / 10

47.49

approx. W/y Line

42.1 / 14.6 / 65 · 40.6 / 16.1 / 55 · 41.5 / 15.2 / 45 · 41.6 / 15.1 / 25 · 41.5 / 15.2

44.2 / 12.5 / 63 · 43.7 / 13.0 / 44 · 44.7 / 12.0 / 30 · 42.5 / 14.2 / 12 · 42.2 / 14.5 · 43.1 / 13.6 / 15

43.6 / 13.1 / 71 · 44.2 / 12.5 / 68.88 · 44.5 / 12.2 / 50 · 45.9 / 10.8 / 30 · 43.9 / 12.8 / 20 · 43.7 / 13.0 · 45.2 / 11.5 / 15

50.7 / 2.0 / 95 · 53.0 / 5.7 / 93 · 53.2 / 5.0 / 85 · 51.2 / 7.5 / 83 · 53.7 / 5.0 / 80 · 53.6 / 5.1 / 50 · 49.9 / 8.8 / 40 · 49.0 / 9.7 / 30 · 49.5 / 9.2 / 15 · 50.6 / 8.1 · 52.9 / 5.8 / 15

56.69

Levels on Roseland Dr.

Set
B.M. >x> RW 3+97.97 P.C. Left 5.15 42.34

1+07.78 E.C.

0+53.89 Mid. Curve

4+01.97 = 0+00 = P.C. Rt.

47.49

5/4 Line
Roseland 8

47.

RT.

47.3	46.7	42.5	45.9	45.9	46.6	46.6
0.7	0.8	2.0	1.2	1.6	0.9	0.9
60	50	40	25	10		15

39.5	40.5	41.5	42.9	43.8
8.0	7.0	6.0	4.6	3.7
60	50	25		15

44.0	44.4	42.5	42.4	46.4
3.5	3.1	5.0	5.1	
50	20	11		

47.49

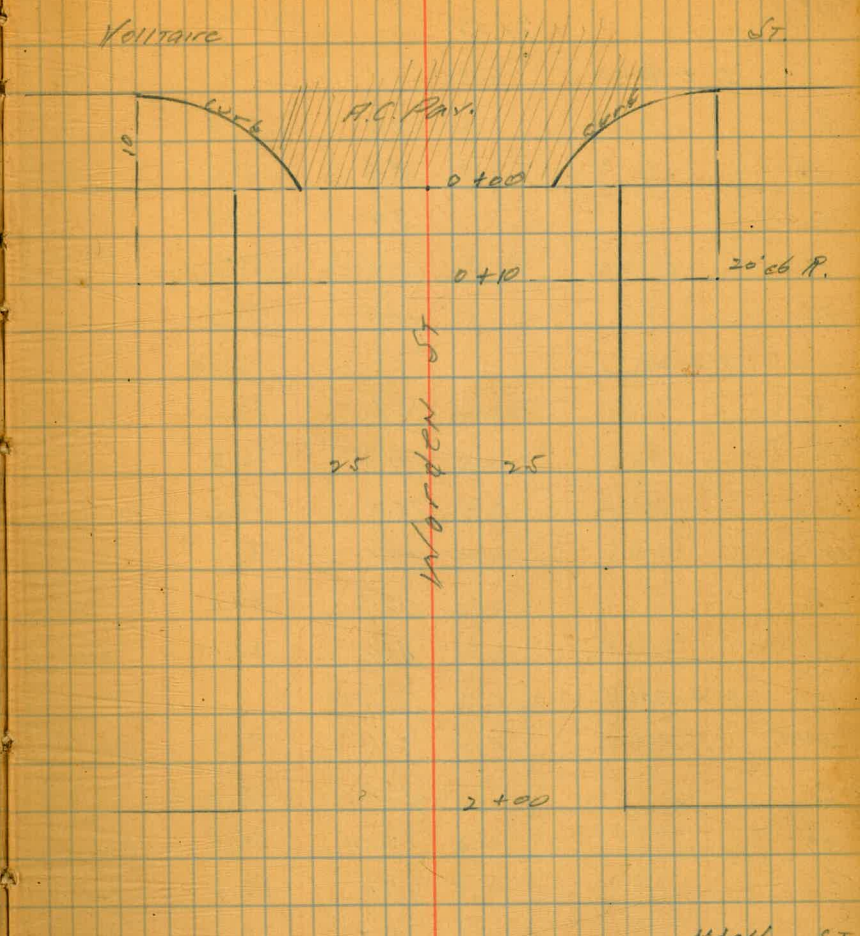
Indexed
C.S.K.

Moore
1-20-39.

9

X Sec. Worden St. 50' wide 10' c6
Voltaire Sly to Udall

S.E.B.P.	0.67	97.07	96.35	Voltaire Villa Dr.
	0-10 S c6 Voltaire			
-10	c6 top PC		7.04	89.96
-10	Pav		7.77	89.30
E	"		8.04	88.98
C	"		8.86	88.16
W	"		10.40	86.62
+10	"		11.05	85.97
+10	c6 top PC.		10.39	86.63
	0+00 S/y V			
W			9.7	87.3
+7.5	top end c6		9.46	87.56
+	out Pav.		9.9	87.10
C	"		8.9	88.10
+17.5			8.56	88.46
+17.5	top end c6		8.13	88.89
E			7.6	89.4



	97.02		
0+10			
E		7.6	89.4
cb		8.6	88.4
c		9.2	87.8
cb		10.4	86.6
W		10.3	86.7
0+20			
W		10.9	86.1
cb		10.5	86.5
c		10.1	86.9
cb		10.1	86.9
+8		10.0	87.0
E		8.0	89.0
0+50			
-2		6.1	90.9
E		11.8	85.2
cb		12.2	84.8
c		11.8	85.2
cb		11.9	85.1
W		12.2	84.8
1+00			
-2		9.3	87.7
W		13.3	83.7
cb		14.1	82.9
c		13.9	83.1

	97.02			
cb			14.6	82.4
E			12.0	85.0
+3			6.0	91.0
T.P.	1.73	85.85	12.90	84.12
1+50				
-2			+08	86.7
E			3.0	82.9
+4			4.8	81.1
cb			5.6	80.3
c			5.0	80.9
cb			5.6	80.3
W			5.3	80.6
+2			2.2	83.7
2+00 N'ly Udall				
-2			6.0	79.9
W			7.2	78.7
cb			7.5	78.4
c			7.5	78.4
cb			7.2	78.7
+8			7.1	78.8
E			6.1	79.8
2			4.9	81.0

85.85

2+20		
E	6.7	79.2
cb	7.7	78.2
c	8.1	77.8
cb	8.0	77.9
W	8.0	77.9
2+29		
−10	14.7	71.2
W	12.8	73.1
cb	11.6	74.3
c	7.8	78.1
cb	7.8	78.1
E	6.8	79.1
2+42		
E	10.6	75.3
cb	11.6	74.3
c	13.6	72.3
cb	15.6	70.3
W	16.1	69.8
+10	17.6	68.3

See Notes by Loudon from here to Tennyson. No change in ground.

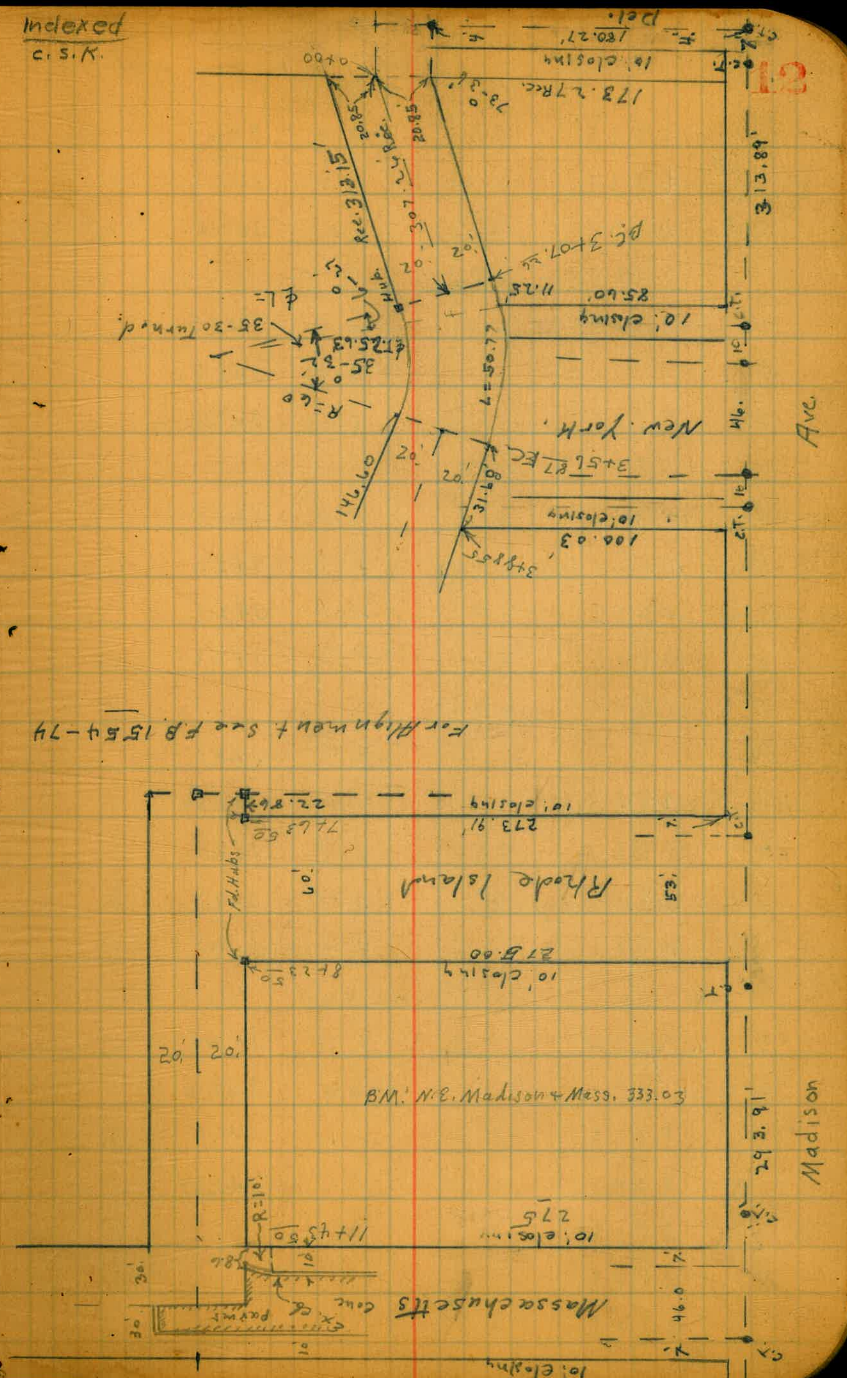
See 2-83-45

4-12-39 Miller Walker Blois

Golden Gate Drive X Sec.
Delaware to Massachusetts

Indexed C.S.K.

BM B.P.	3.30	343.81	.	340.51	S.W. Monroe & New York.
T.P.	6.04	347.52	2.33	341.48	
10' E. of W. ℄ of Delaware =					
= 30' E of 0+00 old. W. Line					
S = 173.27 N of Madison			3.65	343.87	Pav
+20.85 N = ℄			3.88	343.64	"
+32			3.88	343.64	"
+41.70 = N			3.1	343.9	
20' E. of 0+00 = W. ℄ Line					
S+41.70 N = N. Spillway to N			4.68	342.84	
S+32 = pav.			4.24	343.28	
S.+20.85 = ℄ "			4.21	343.31	
S. "			4.10	343.42	
S. = N End Conc. ℄			3.47	344.05	
17.5' E of 0+00 = W. Edge pav					
S.			3.4	344.1	
+7' N Pav w. edge			4.00	343.52	
+20.85 = ℄ " " "			4.16	343.36	
+32 " " "			4.21	343.31	
+41.7			3.8	343.7	
10' E of 00 = W. Line Del to S.					
S+41.7			3.7	343.8	
S+20.85 = ℄			4.0	343.5	
S+7			4.0	343.5	
S = N. End w. Edge 5' Conc. Walk.			3.25	344.27	



347.52

0+00 = original W. Line Del

S	3.3	344.2	
	3.8	343.7	
+ 20.85 = ℄	3.4	343.7	
+ 41.7 = N	4.0	343.5	Top. 1½ to slope

0+50 At ∠ to G. G. Dr.

N	4.0	343.5	
℄	3.9	343.6	
S.	3.8	343.7	

1+00

S on Lawn	4.0	343.5	
+ 12 = N edge Lawn	4.3	343.2	
℄	4.8	342.7	
N	5.3	342.2	

1+53

N	5.4	342.1	
+ 13.5 = M.H. Rim	5.02	342.50	
℄	4.7	342.8	
+ 7 = N edge yard	4.7	342.8	
S in yard	4.7	342.8	

2+00

S. in yard	5.0	342.5	
+ 10 N. edge yard	5.3	342.2	
℄	6.0	341.5	
N	6.2	341.3	

347.52

2+50

N	7.6	339.9	
+ 10	7.9	339.6	
℄	6.9	340.6	
+ 16 N. edge yard.	6.0	341.5	
S	6.0	341.5	

3+07.26 B.C. Rt.

S = N edge yard	7.8	339.7	
℄	8.6	338.9	
N	9.4	338.1	Top. slope

3+32.07 ℄ curve

N	9.5	338.0	Top. slope
℄	8.9	338.6	
S	8.4	339.1	

3+56.87 E.C.

S	9.0	3385	
+ 3	9.8	337.7	
℄	9.5	338.0	
+ 14 Top. slope	10.1	337.4	
T.P. 5.83	343.30	10.05	337.47
N	11.0	332.3	

4+00

N	11.5	331.8	
+ 13 Top. slope	6.4	336.9	
℄	6.1	337.2	
+ 15	6.1	337.2	
S	4.8	338.5	

343.30

4+50

S		5.4	337.9
+10		6.1	337.2
℄		6.5	336.8
+61	Top slope	6.9	336.4

5+03 47 BC. Rt

N		6.6	336.7
+7		5.2	338.1
℄		5.2	338.1
S		5.1	338.2

5+24 4 etr curve

S		4.8	338.5
+12		5.4	337.9
℄		4.8	338.5
N		6.5	336.8

5+45 33 E.C.

N		9.8	333.5
+5	Top. slope	6.3	337.0
℄		5.6	337.7
S		4.5	338.8

6+00

S		5.4	337.9
℄		6.3	337.0
+13		6.7	336.6
N		8.5	334.8

343.30

6+41 14 B.C. Lt

N		8.8	334.5
+10		7.1	336.2
℄		6.3	337.0
S		5.1	338.2

6+90 80 ℄

S		5.4	337.9
+5		6.2	337.1
℄		6.2	337.1
N		6.6	336.7

7+40 64 E.C.

N		6.7	336.6
℄		6.7	336.6
S		5.8	337.5

7+63 50 E. line Rhode Island

S		5.6	337.7
+10		7.0	336.3
℄		6.8	336.5
+10		6.4	336.5
N		8.7	334.6

7+93 50

N		11.0	332.3
+10		7.6	335.7
℄		7.4	335.9
+14		7.1	336.2
S		6.1	337.2

343.30

T.P. Hub	5.50	342.78	6.02	337.28	S.W. R.I. St + G.G. Dr.

8+23.5 = W. Line Rhode Island,

S.		5.5	337.3
℄		7.4	335.4
+8		8.8	334.0
N		12.5	330.3
	8+50		
N		13.0	329.8
+15		8.0	334.8
℄		7.0	335.8
+10		6.7	336.1
S		5.5	337.3
	9+00		
S		5.4	337.4
+10		7.0	335.8
℄		6.7	336.1
+8		7.3	335.5
N		11.3	331.5
	9+50		
N		9.1	333.7
+10		7.5	335.3
℄		7.0	335.8
+7		6.6	336.2
+13		5.3	337.5

342.78

S		5.1	337.7
	10+00		
S		5.3	337.5
℄		5.8	337.0
N		6.4	336.4
	10+50		
N.		6.6	336.2
+8		6.4	336.4
℄		5.3	337.5
S		4.9	337.9
	11+00		
S		5.6	337.2
℄		6.2	336.6
N		6.9	335.9
	11+25		
N		7.2	335.6
℄		6.4	336.4
S		6.2	336.6

11+43.5 = E. Line Mass. St 60. wide 16 els
11+46 = E. Edge conc. walk to S.

S -5.0 = N End & side walk.		7.16	335.62
S.		7.2	335.6
℄		8.0	334.8
N.		7.7	335.1

342.78

11+53 50 = E. ch.

N		8.1	334.7
℄		8.1	334.7
S = N. End. Conc. pav.		8.06	334.72
1.4. E. of above = N. End. Ex. ch. on curve		7.37	335.41
+ 5. Top. ch. at P.C. 10' R. Ret.		7.33	335.45
+ 5 = gutter		8.00	334.78

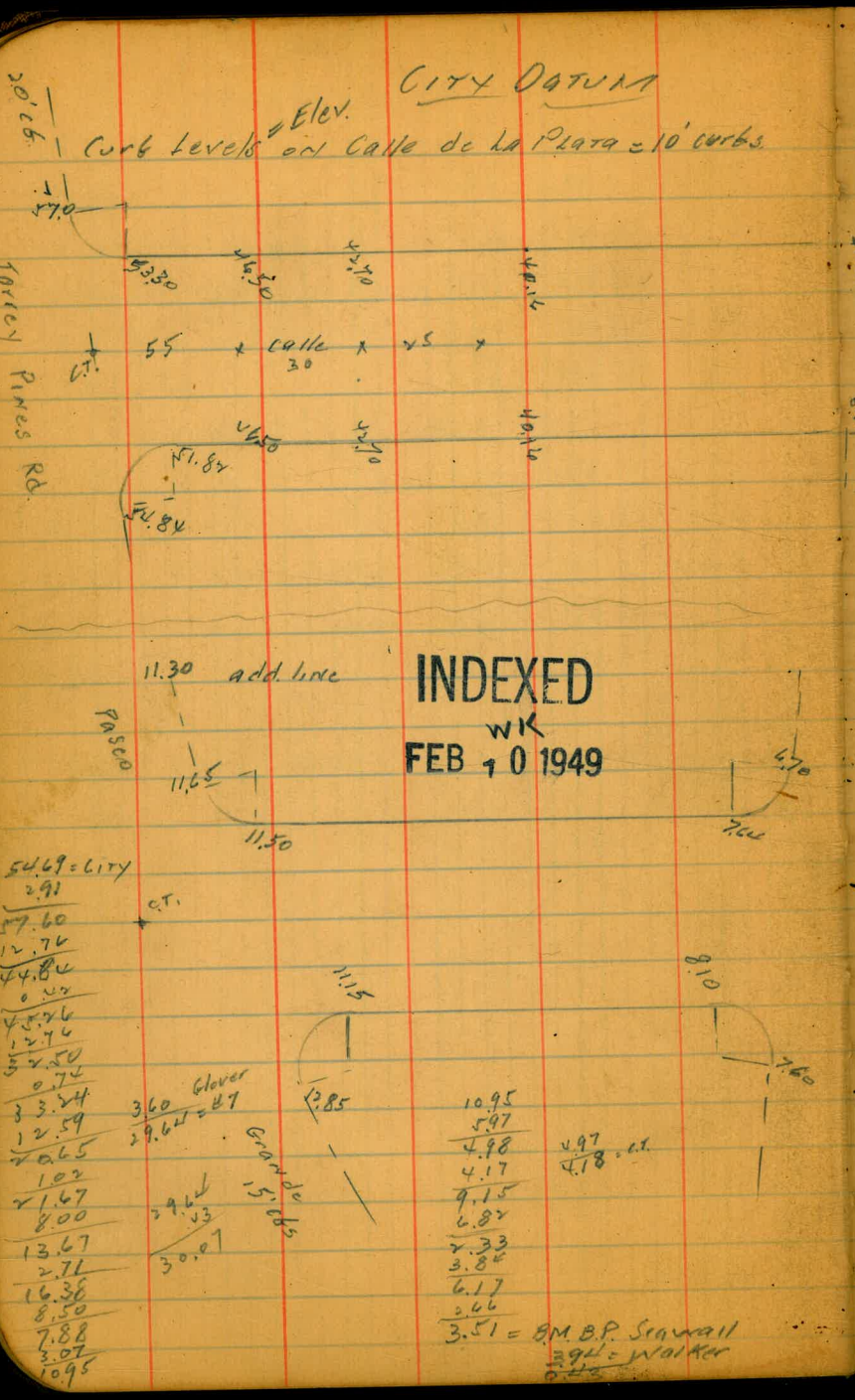
11+73 50 ℄ Mass. St.

S. = Pav. at △		8.00	334.78
℄ = " E. edge		8.51	334.27
+17.5 N. of ℄ = N. End. E. edge Pav.		9.07	333.71
+17.5 N " " = E. End. Ex. conc. ch.		8.58	334.20
N. Line		9.0	333.78
T.P. F. Hydt.	2.54	340.42	4.90	337.88	S.E. Mass. + G.G. Dr. N.E. Mass + Madison
BM. B.P			7.41	333.01 = 333.03	

CITY DATUM

Elev.

Curb Levels on Calle de la Plata = 10' curbs



50.69 = City
2.91
57.60
12.74
44.86
0.27
45.26
1.76
43.50
0.74
33.24
12.59
20.65
1.02
19.67
8.00
13.67
2.71
16.36
8.50
7.88
3.07
10.95

3.60
29.64 = 87

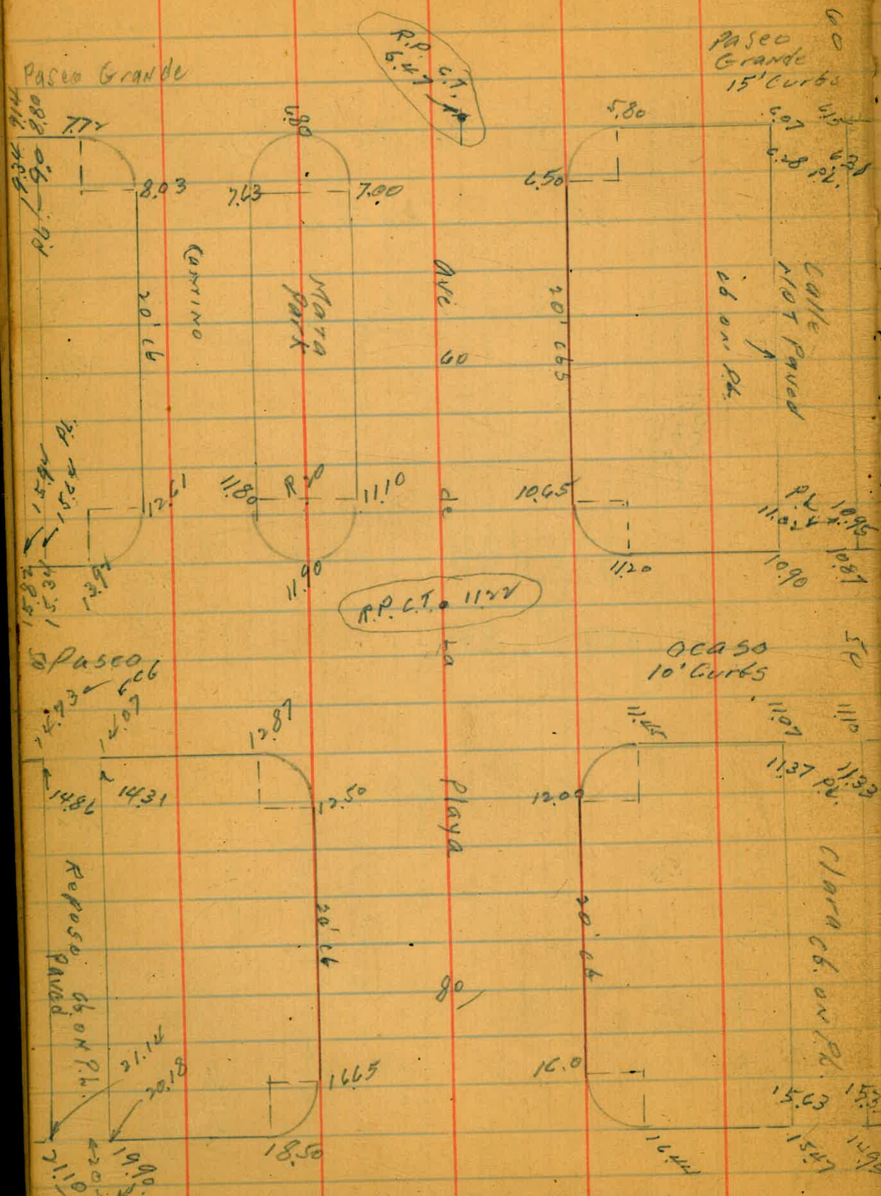
29.64
1.03
30.67

10.95
5.97
4.98
4.17
9.15
6.82
2.33
3.82
6.17
2.66
3.51 = BM B.P. Seawall
3.94 = Walker

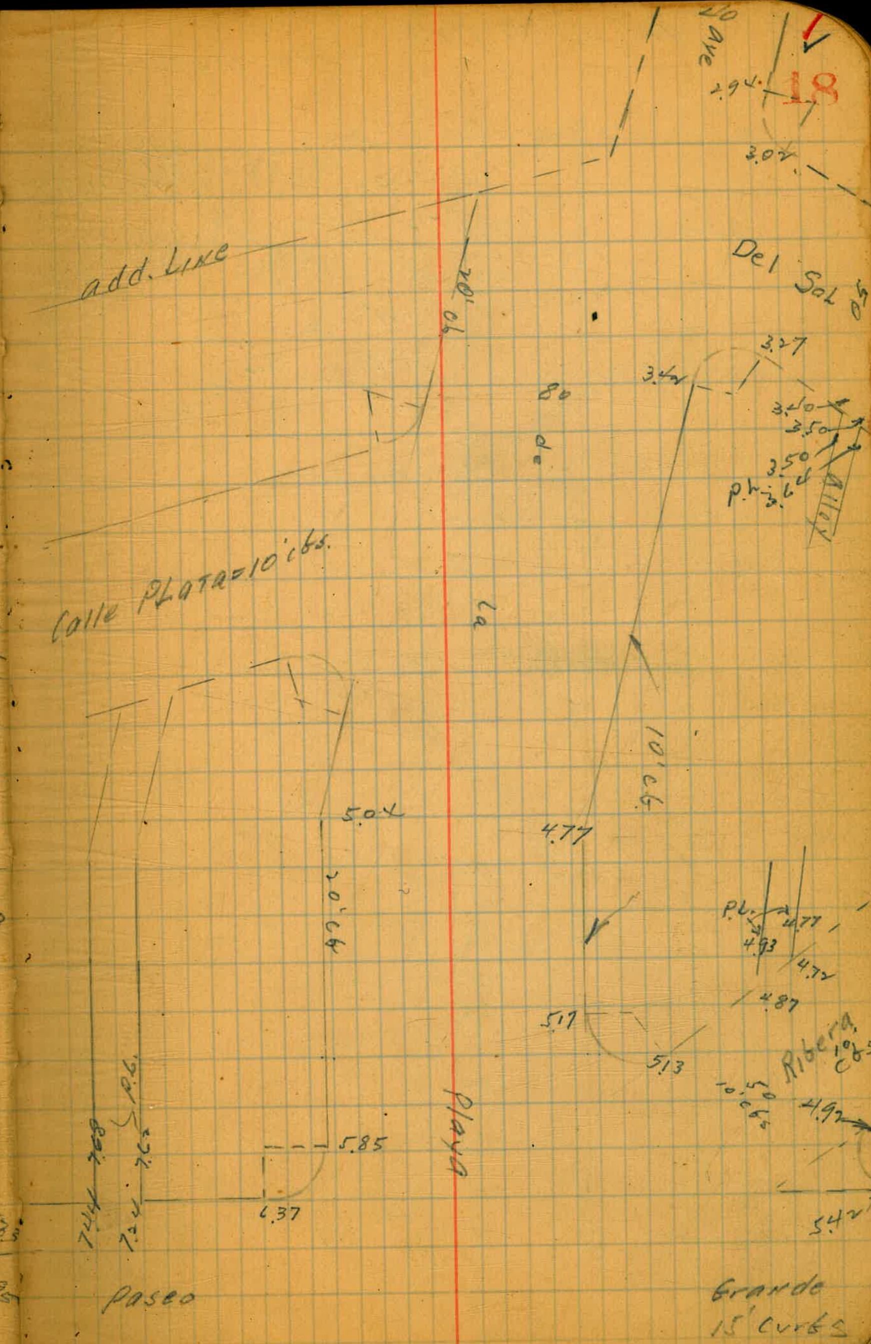
4.97
4.18 C.T.

Ave. de La Playa

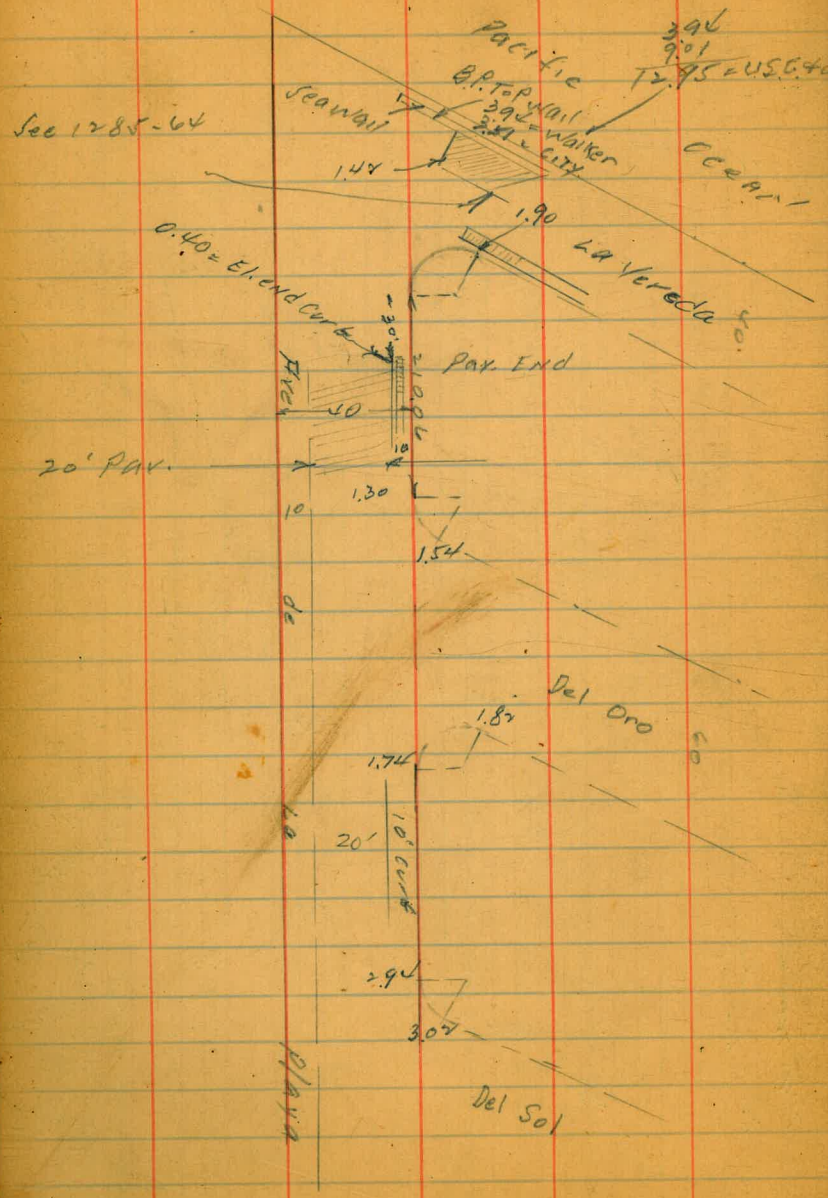
CITY DATUM



La Jolla Shores Drive: 20' curb



Ave. de la Playa. City Datum



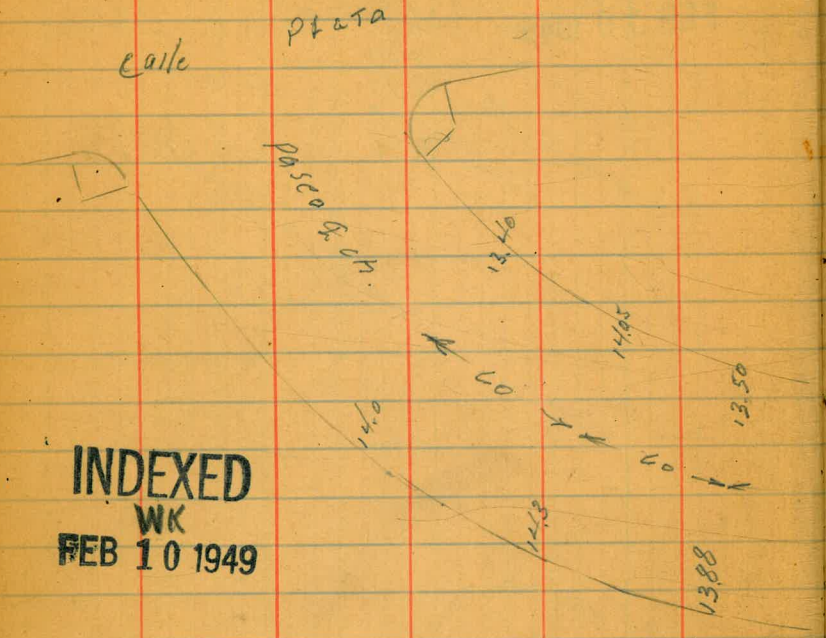
INDEXED
WK
FEB 10 1949

19

3.51	B.M. on Seawall at Playa
3.81	
6.34	
3.77	
2.55	
5.39	
7.94	
2.09	
5.85	= T.P. F.H. Del Sol Ribera

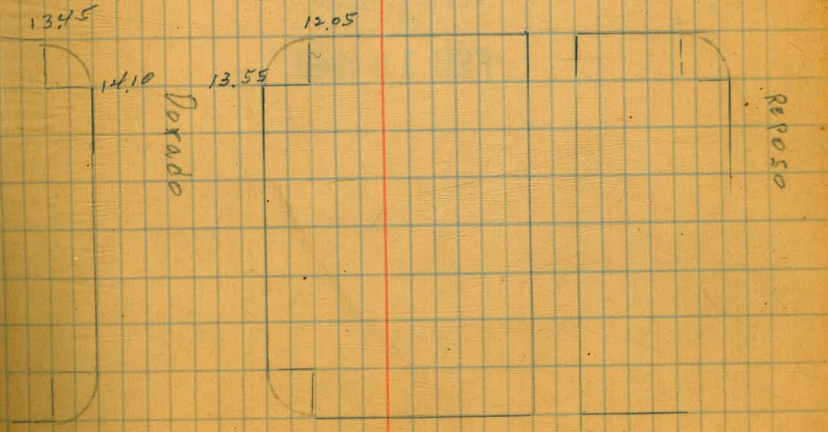
CITY DATUM

El Paseo Grande 15' 6s.



1.685 T

60 — C.T. 60 Grande

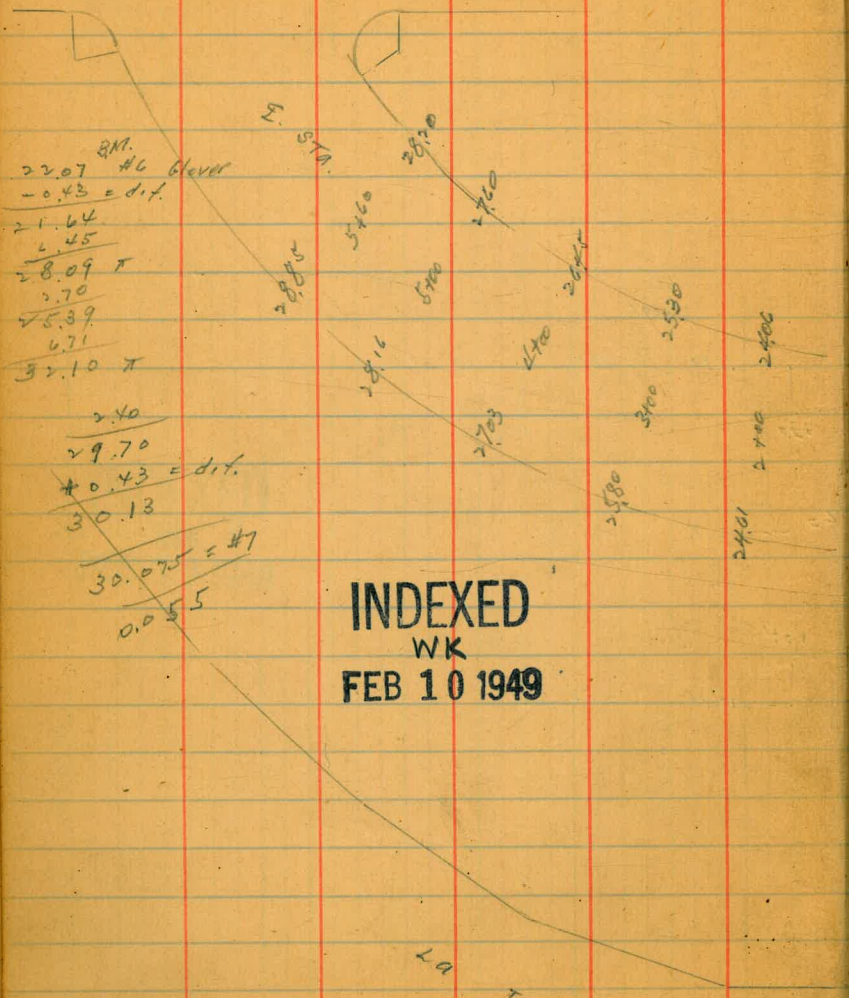


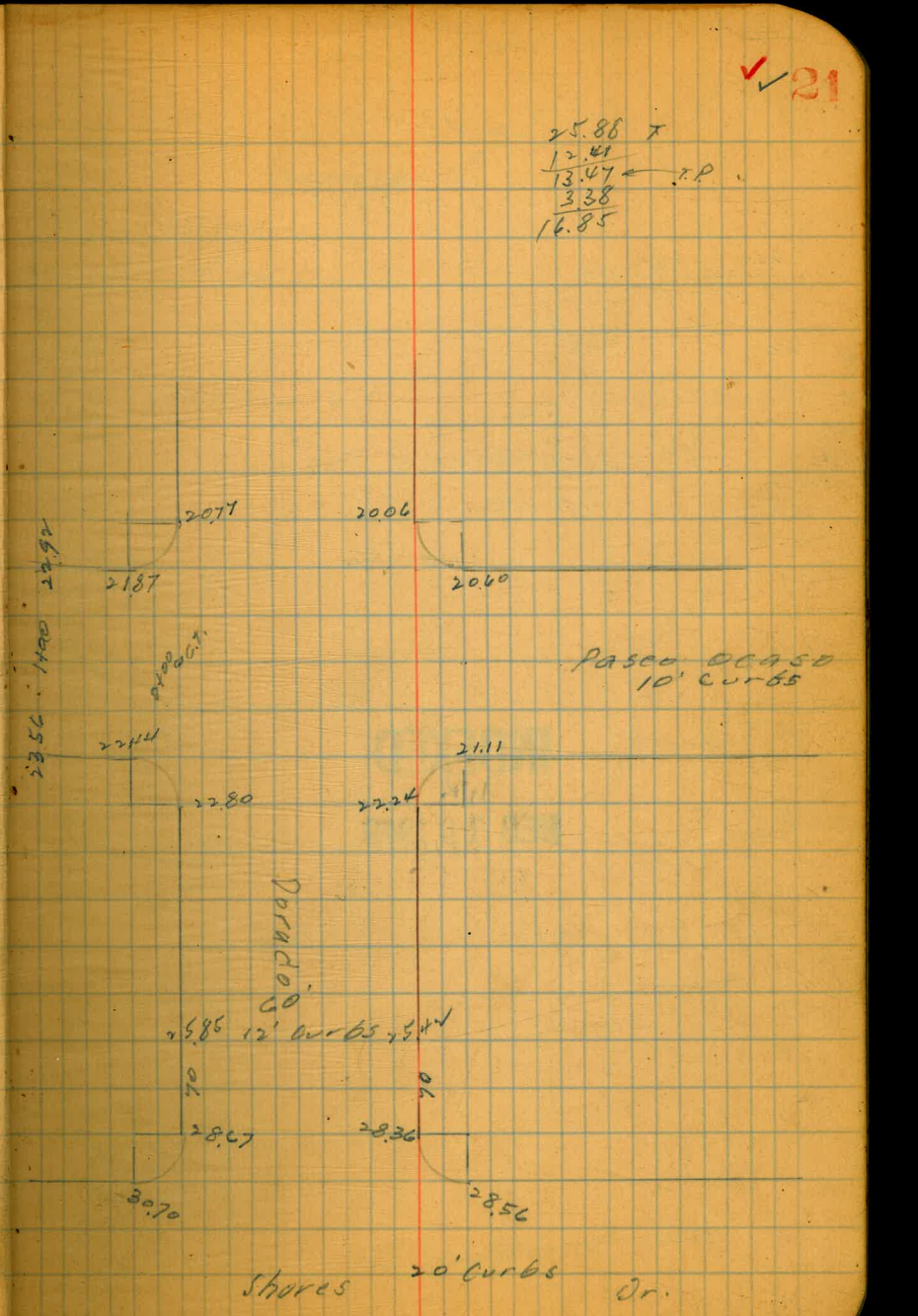
Paseo Ocaso

CITY DATUM

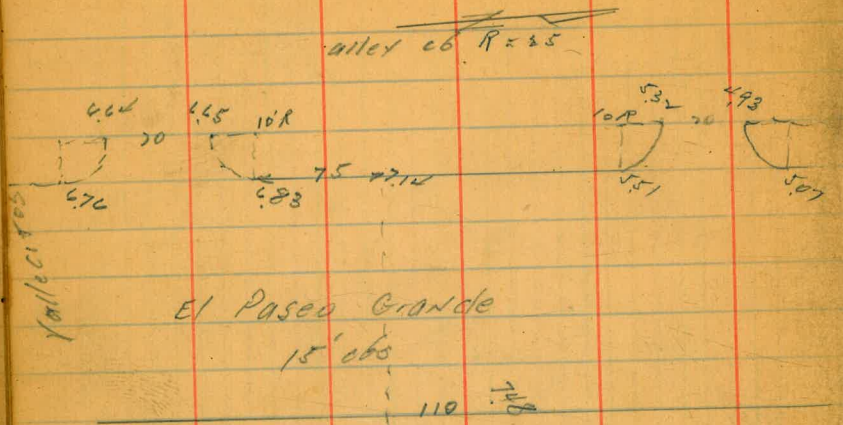
Paseo Ocaso levels

Calle Plata



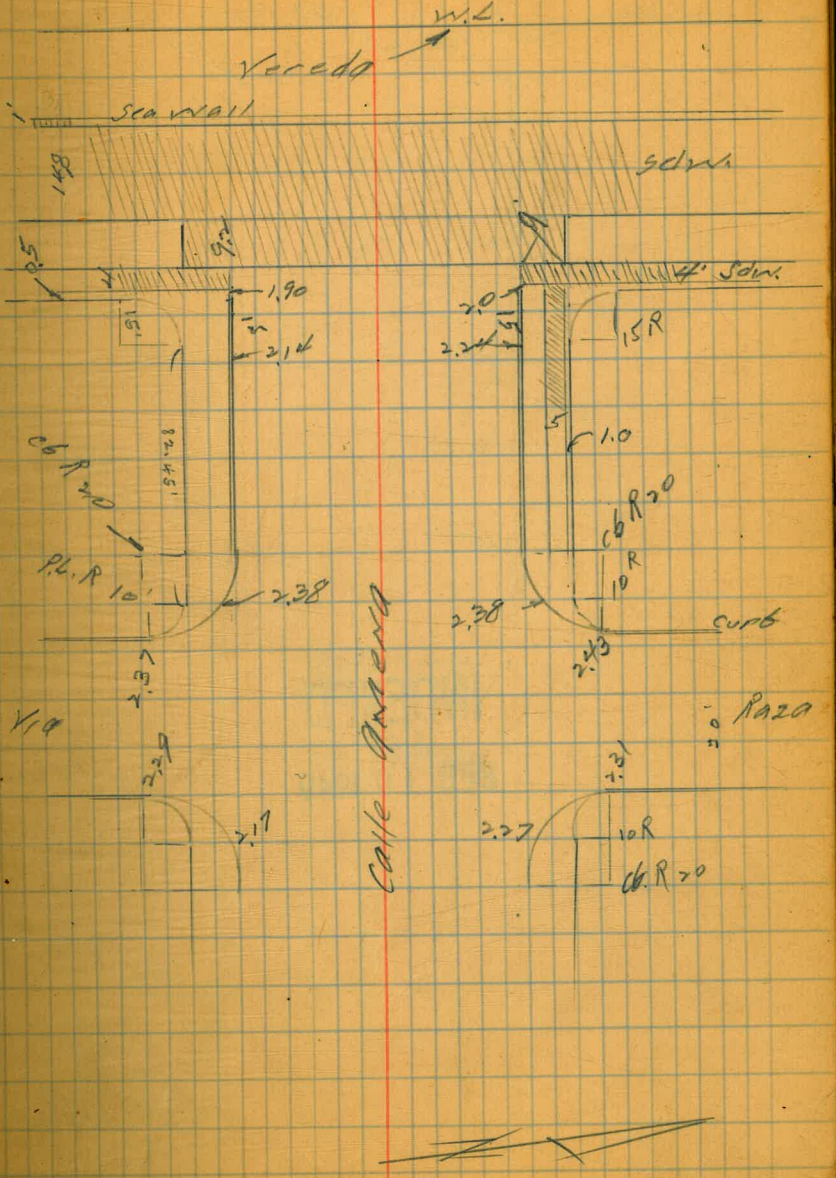


CITY DATUM

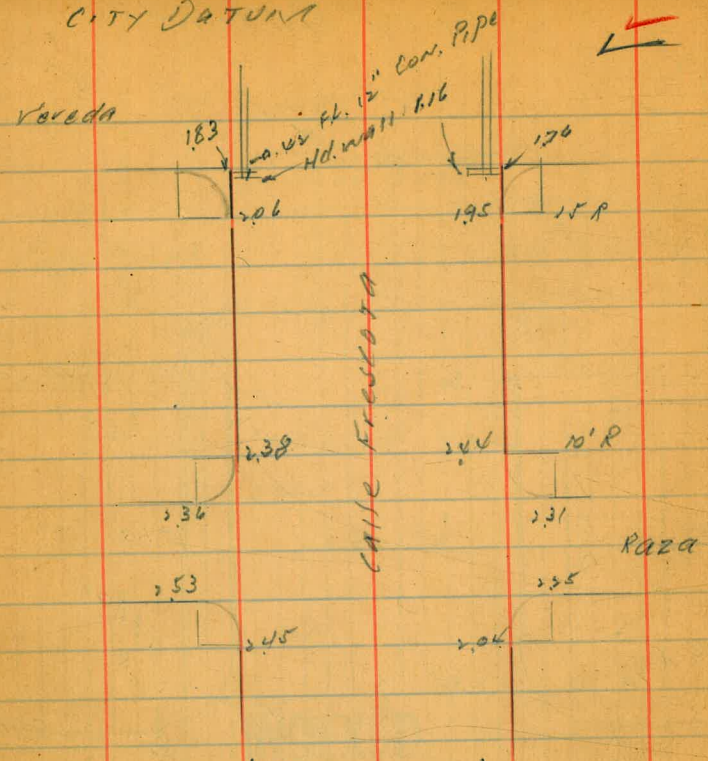


CITY DATUM

22

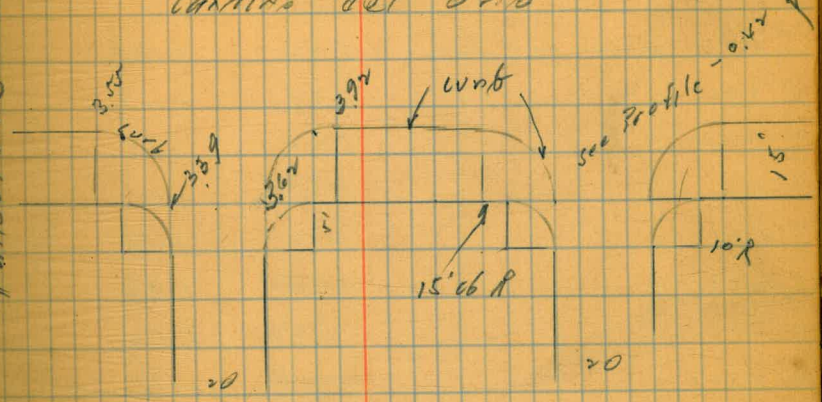


CITY DATUM



CITY DATUM

CANTINA del ORO



Par. E/S Southly edge 20' strip Par.
Ave de la Playa

Δ in S.L. = 0+00 at Cardino Sol

See P 19

			City Datum	So. End Seawall
BM. B.P.	2.28	5.80 ✓	3.5 ±	
5+44 approx. end Par.		5.44	0.36	
5+00		5.3 ±	0.48	
4+50		5.0 ±	0.78	
4+00		4.79	1.01	
3+61		4.6 ±	1.18	
3+33.7C		4.44	1.36	
3+00		4.28	1.5 ±	
2+67		4.09	1.71	
2+50		3.99	1.81	
2+00		3.70	±.10	
1+50		3.42	±.38	
1+00		3.12	±.68	
0+42		2.95	±.85	
0+40		2.78	3.0 ±	
0+00		2.50	3.30	

8" curb face on N/y Side

N/zone
8-9-39

24

Curb Levels
Camino del Oro
" Ocaso Wly to Paseo Grande

				City Datum
BM #5	2.17	27.05		24.88
T.P.	1.50	17.81	10.74	16.31
	Wly Cor. Oro and Ocaso E.C. = 0+00			
N	CL		5.91	11.90
	0+50			
N	S. opposite N		8.89	8.97
S			7.17	10.64
	1+00			
S			9.84	7.97
N			11.40	6.41
	1+16.53 ℄ BVK			
N			11.99	5.84
S			10.00	7.21
T.P.	1.25	7.68	11.38	4.43
	1+56.27			
S			2.57	5.11
N			3.35	4.33
	1+98.54			
N			4.61	3.07
S			4.41	3.27

7.68

T.P.	2.97	4.71	

Cross Section Dalbergia St.
Woden to Division

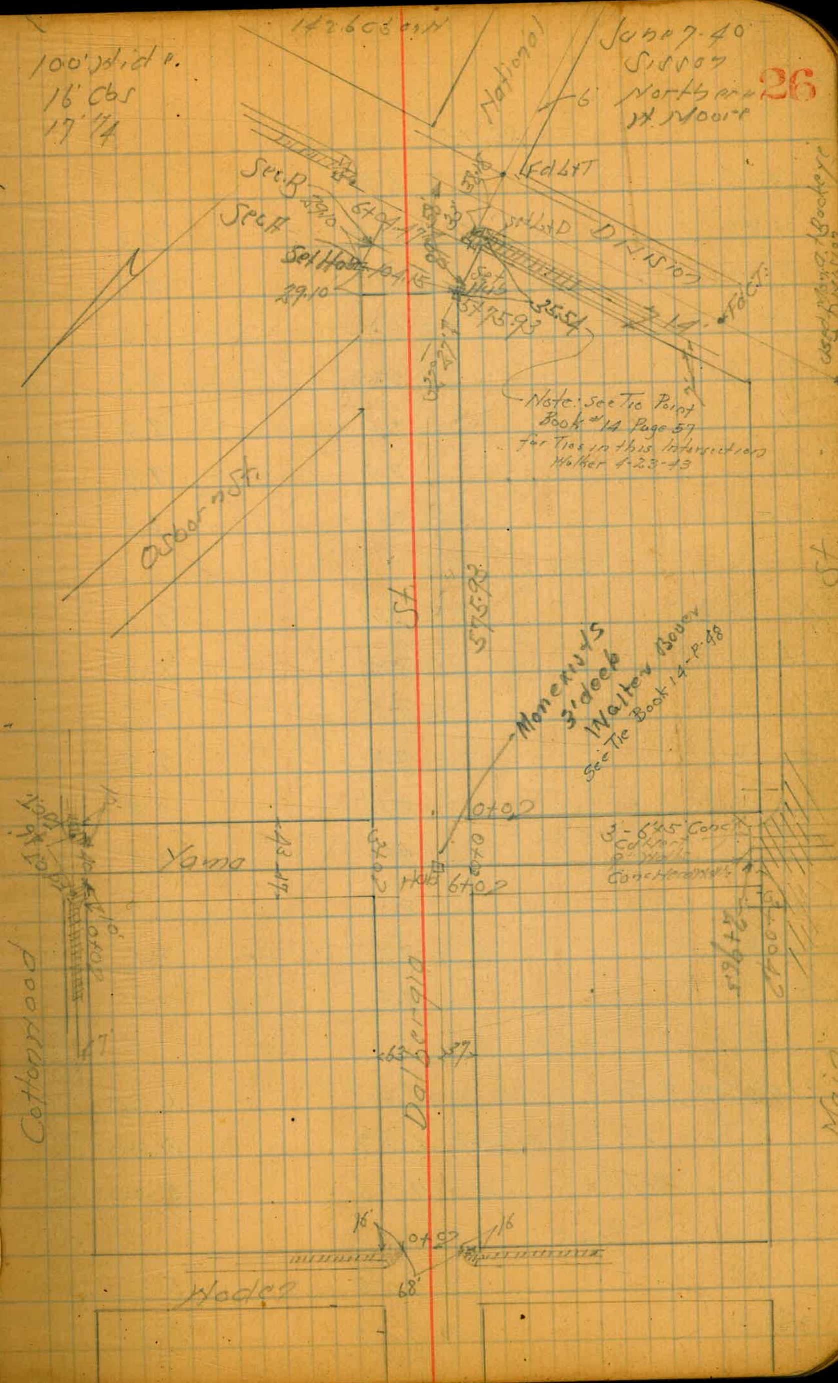
INDEXED
EFB

BM	4.47	19.36		14.89		S.F.B.P Main + Vesta
TP	5.09	15.75	8.70	10.66		
	0+0 = EL		Woden			
S			4.1		11.7	
Cb Top: End			4.27		11.48	
Gutter			4.6		11.2	
+3			4.0		11.8	
1/4			4.0		11.8	
¢			4.0		11.8	
1/4			4.1		11.7	
Gutter			4.2		11.6	
Cb Top End			3.82		11.93	
N			3.8		12.0	
	0+50					
N			6.6		9.2	
Cb			6.0		9.8	
1/4			6.3		9.5	
¢			5.6		10.2	
1/4			5.0		10.8	
+16			5.2		10.6	
Cb			4.6		11.2	
S			4.2		11.6	
	1+0					
S			5.1		10.7	
Cb			5.8		10.0	

Red. + Plot. on Profile 229 · 6-11-40 C.B.H.

100' Wide
16' Cbs
17 1/4

June 7-40
Sisson
Northern
H. Moore



15.75

+1	6.2	9.6
+7	5.5	10.3
¼	6.0	9.8
½	6.8	9.0
¼	7.6	8.2
CL	7.4	8.4
N	7.9	7.9
+10	8.1	7.7
1+50		
N	8.1	7.7
CL	8.3	7.5
¼	8.1	7.7
½	8.3	7.5
¼	8.1	7.7
+12	8.1	7.7
CL	8.8	7.0
+14	8.4	7.4
S	8.5	7.3
1+62½		
-1.0 = ½ 4' Conc Walk	6.97	9.28
N of 1st Step Conc	6.87	8.88
+3 " Bot Step Conc	7.75	8.00
2+0		
S	10.5	5.3
CL	10.2	5.6

15.75

¼	9.5	6.3
+7	8.8	7.0
½	9.1	6.7
¼	8.8	7.0
CL	8.6	7.2
N	8.8	7.0
2+50		
N	8.9	6.9
CL	8.9	6.9
¼	9.2	6.6
½	9.5	6.3
¼	9.7	6.1
+3	10.4	5.4
CL	11.0	4.8
S	10.9	4.9
2+58		
N = ½ 4' Conc Walk	8.74	7.01
3+0		
S	11.1	4.7
CL	11.0	4.8
+1.5	10.8	5.0
¼	10.2	5.6
½	9.7	6.1
¼	9.6	6.2
CL	9.3	6.5

Dalbergia

		15.75			
H			9.1		6.7
	3+50				
H			8.8		7.0
Cb			9.2		6.6
1/4			9.5		6.3
1/2			9.6		6.2
1/4			10.1		5.7
+3			10.7		5.1
Cb			11.0		4.8
S			11.0		4.8
TP	5.83	12.09	9.49	6.26	
	4+0				
S			7.2		4.9
Cb			7.3		4.8
1/4			6.6		5.5
+2			6.3		5.8
1/2			6.2		5.9
1/4			5.8		6.3
Cb			5.8		6.3
H			5.4		6.7
	4+50				
H			5.6		6.5
Cb			5.6		6.5
1/4			5.5		6.6
1/2			5.8		6.3

	12.09		
1/4		6.0	6.1
+3		7.0	5.1
Cb		7.2	4.9
S		7.1	5.0
	5+0		
S		6.7	5.4
Cb		7.0	5.1
+1/4		6.8	5.3
1/4		5.7	6.4
1/2		5.6	6.5
1/4		5.1	7.0
Cb		5.2	6.9
H		5.6	6.5
	5+50		
H		5.4	6.7
Cb		5.1	7.0
1/4		4.8	7.3
1/2		5.3	6.8
1/4		5.7	6.4
+3		6.5	5.6
Cb		6.9	5.2
S		6.6	5.5
	6+0: HL Yoma 60' wide		
S		6.0	6.1
Cb		6.0	6.1

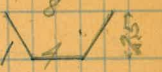
12.09

+13	5.8	6.3
+15	5.2	6.9
¼	5.1	7.0
½	4.9	7.2
¼	4.6	7.5
Cb	5.0	7.1
H	5.2	6.9
	½ Yama	
H	5.0	7.1
Cb	4.9	7.2
¼	5.0	7.1
½	5.2	6.9
¼	5.1	7.0
Cb	5.2	6.9
S	5.2	6.9
	FL Yama = 0+10	
S	5.5	6.6
Cb	5.6	6.5
¼	5.1	7.0
½	4.5	7.6
¼	4.6	7.5
Cb	4.6	7.5
H	5.2	6.9
	0+45	
H	4.9	7.2

12.09

Cb	5.0	7.1
¼	4.7	7.4
½	4.5	7.9
+10	3.8	8.3
¼	4.5	7.9
+6	4.9	7.2
Cb	4.8	7.3
S	4.7	7.4
+15 = ½ Cobble Drain	9.8	2.3
	0+55	
-15	4.9	7.2
S = ½ Bot Cobble Drain	9.7	2.4
+8	7.3	4.8
Cb	5.2	6.9
+7	4.7	7.4
¼	3.9	8.2
+11	3.9	8.2
½	4.3	7.8
¼	4.7	7.4
Cb	5.0	7.1
H	4.9	7.2
	0+66	
H	4.9	7.2
Cb	4.9	7.2
¼	4.6	7.5

Cobble Drain



Dalbergia

12.09

½	4.1	8.0
½ +10	6.5	8.6
¼	3.6	8.5
¼ +6	4.4	7.7
+14	9.8	2.3
Cb	9.8	2.3
+4	9.9	2.2
+7 = ¼ Cobble Drain	9.7	2.4
S	5.0	7.1
+10	4.8	7.3
1+10		
S	5.4	6.7
Cb	5.1	7.0
¼	4.3	7.8
+6	4.7	7.4
½	9.4	2.7
+6 = ½ Wash	10.1	2.0
+11	9.6	2.5
¼	5.1	6.0
Cb	4.9	7.2
N	4.3	7.8
1+24		
-15	4.2	7.9
N	4.2	7.9
+3	8.0	4.1

12.09

+9 = ½ Wash	8.4	3.7
+14	8.0	4.1
Cb	6.6	5.5
+3	4.0	8.1
¼	4.6	7.5
½	4.7	7.4
+5	4.9	7.2
+12	4.0	8.1
¼	4.9	7.2
Cb	5.5	6.6
S	5.7	6.4
1+30		
S	5.5	6.6
Cb	5.6	6.5
¼	4.8	7.3
+4	4.2	7.9
½	5.3	6.8
+10	5.1	6.0
¼	4.4	7.7
Cb	4.1	8.0
+4	3.6	8.5
+9	6.8	5.3
N = ½ Wash	8.0	4.1
+9	8.0	4.1
+10 = Top Wash	4.1	8.0

12.09

1+37

-12 = ½ Wash	8.0	4.1
-7	7.6	4.5
-5 = Top Wash	3.8	8.3
N	4.1	8.0
Cb	4.2	7.9
¼	4.6	7.5
+3	4.2	7.9
+8	5.5	6.6
½	5.3	6.8
+10	5.3	6.8
¼	4.7	7.4
+7	5.5	6.6
Cb	5.7	6.4
S	5.5	6.6

1+50

S	5.7	6.4
Cb	5.8	6.3
¼	5.0	7.1
+5	4.8	7.3
+7	5.5	6.6
½	5.5	6.6
+10	5.3	6.8
¼	4.5	7.6
Cb	4.5	7.6

12.09

N	4.0	8.1
+10	3.8	8.3

2+10

N	4.4	7.7
Cb	4.8	7.3
¼	4.4	7.7
+5	3.7	8.4
+8	5.2	6.9
½	5.3	6.8
+8	5.2	6.9
+15	4.5	7.6
¼	5.1	7.0
+3	5.8	6.3
Cb	6.4	5.7
S	5.9	6.2

2+50

-10	6.6	5.5
S	6.1	6.0
Cb	5.6	6.5
¼	4.6	7.5
+1	3.8	8.3
+6	5.3	6.8
½	5.7	6.4
+11	5.3	6.8
+12	4.8	9.3

Dalberg 10

12.09

			3.0	9.1
¼			3.3	8.8
Cb			3.3	8.8
N			4.0	8.1
+10				
TP	10.63	22.57	0.15	11.94
	2+75			
-10			11.5	11.1
N			11.5	11.1
Cb			11.9	10.7
¼			11.6	11.0
+6			10.8	11.8
+9			12.8	9.8
S			13.5	9.1
D				
+5			12.7	9.9
¼			13.2	9.4
Cb			14.4	8.2
S			15.2	6.3
+15			16.5	6.1
	3+0			
-15			12.3	9.3
S			11.7	10.9
Cb			10.0	12.6
¼			8.3	13.3
+9			5.6	17.0
S			5.1	17.5

22.57

+8	5.6		17.0
¼	7.2		14.4
+14	7.7		14.9
Cb	7.1		15.5
N	6.5		16.1
+10	6.1		16.5
	3+20		
N	+2.0		24.6
Cb	0.9		21.7
+7	2.5		20.1
+10	3.6		19.0
¼	1.3		21.4
+6	4.8		17.8
S	4.4		18.2
D			
+9	5.3		17.3
+13	2.0		20.6
¼	1.4		20.2
Cb	4.1		18.5
S	5.8		16.8
+10	7.6		15.0
TP	10.99	32.60	0.96	21.61
	3+50			
-10	11.8		20.8
S	10.6		22.0
Cb	9.7		22.9

32.60

¼		9.3	23.3
+7		9.3	23.3
+10		14.0	18.6
¼		13.7	18.9
+9		13.6	19.0
¼		6.6	26.0
+5		5.4	27.2
+½		6.2	26.4
Cb		5.8	26.8
N		5.7	26.9
+5		3.7	28.9
	3+85		
N		3.8	28.8
Cb		3.7	28.9
+4		3.1	28.5
+14		3.5	29.1
¼		5.0	27.6
+8		12.5	20.1
¼		12.6	20.0
+10		12.7	19.9
+15		8.6	24.0
¼		8.4	24.2
+6		7.7	24.9
Cb		8.4	24.2
S		9.2	23.4

32.60

+10		10.4	22.2
	4+0		
-10		10.0	22.6
S		9.0	23.6
Cb		7.8	24.8
+13		7.2	25.4
¼		9.3	23.3
+2		10.8	21.8
+8		12.5	20.1
¼		12.7	20.4
+7		12.4	20.2
¼		6.3	26.3
+4		3.0	29.6
+10		3.4	29.2
Cb		3.6	29.0
N		3.4	29.2
TP	2.08 31.84	3.84	29.76
	4+30		
N		2.7	29.1
Cb		3.0	28.8
+6		2.1	29.7
+14		2.7	29.1
¼		3.1	28.7
+2		4.0	27.8
+9		10.3	21.5

Nail Hole 3+85 on N

Dalbergia

31.84

℄	10.3	21.5
+7	10.8	21.0
+12	6.9	24.9
¼	4.6	27.2
+5	4.5	27.3
Cb	5.4	26.4
S	5.8	26.0
+20	7.1	24.7

4+65

-10	2.5	29.3
S	2.8	29.0
Cb	2.8	29.0
¼	2.9	28.9
+5	2.4	29.4
+8	9.0	22.8
℄	9.4	22.4
+6	9.3	22.5
+9	8.0	23.8
¼	7.3	29.5
Cb	3.3	28.5
N	2.9	28.9
+16 Hopea Osbornii	2.9	28.9

540

N	3.8	28.0
Cb	3.3	28.5

31.84

+15	2.9	28.9
¼	4.0	27.8
+7	8.2	23.6
℄	8.2	23.6
+10	8.1	23.7
¼	3.7	28.1
+2	2.0	29.8
Cb	1.8	30.0
S	1.8	30.0

542.5

-3.4 = Base Foundations House Underconst.	2.2	29.6
S	2.3	29.5
Cb	2.7	29.1
+9	2.6	29.2
¼	6.9	24.9
℄	7.5	24.3
+11	7.2	24.6
¼	3.4	28.4
+4	3.6	28.2
Cb	3.9	27.9
+10	3.8	28.0
+11	2.7	29.1
N	3.0	28.8

5+50

N	50	26.8

31.84

+12	3.6	28.2
Cb	4.3	27.5
1/4	4.7	27.1
+9	5.2	26.6
+13	6.7	25.1
1/2	7.1	24.7
1/4	6.7	25.1
+6	6.5	25.3
+13	3.3	28.5
Cb	3.6	28.2
S	3.2	28.6

S+75.93-1 on S

-10	3.6	28.2
S on Stub	4.3	27.5
+12	4.5	27.3
Cb	6.0	25.8
+4	6.3	25.5
1/4	6.6	25.2
1/2	6.1	25.7
+5	5.6	26.2
1/4	5.2	26.6
Cb	4.0	27.8
+4	3.7	28.1
+10	3.5	29.3
1/4	3.4	29.4

31.84

+6	3.2	29.6
+16	6.1	25.7

Soft on Dip 104.15

-10	6.3	25.5
1/4	6.0	25.8
+14	3.4	29.4
Cb	3.2	28.6
+5	4.4	27.4
1/4	5.6	26.2
1/2	5.8	26.0
1/4	6.4	25.4
Cb	6.2	25.6
+5	4.7	27.1
S	4.3	27.5

Scr B - 54 75.93 on S

S	4.3	27.5
+11	4.9	26.9
Cb	6.2	25.6
1/4	6.2	25.6
1/2	6.0	25.8
1/4	6.0	25.8
+13	5.0	26.8
Cb	3.5	28.3
+4	2.7	29.1
+13	6.2	25.6

Dalbergia

	31.84		
N		6.4	25.4
+10		6.3	25.5
6+04.47 = NL Division			
-12.6	Top Cb	5.37	26.47
-12.6	on Paving	5.95	25.89
-21.3	" "	6.19	25.65
N	o " "	6.43	25.41
Cb	" "	6.56	25.28
1/4	" "	6.73	25.11
¢	" "	7.15	24.69
1/4	" "	7.38	24.46
Cb	" "	7.50	24.34
+2	Gutter	7.53	24.31
+2	Cb Top	6.85	24.99
S		6.9	24.9
NCb Division			
S	Gutter	8.08	23.76
S	Cb Top	7.45	24.39
Cb	on Paving	7.82	24.02
1/4	" "	7.52	24.32
¢	" "	7.24	24.60
1/4	" "	7.00	24.84
Cb	" "	6.76	25.08
N	" "	6.61	25.23

	BS	HI	FS	Elev.	
		31.84			
TP	0.38	21.98	10.24	21.60	
BM			13.00	8.98	NW B.P. Marnx Division 8.98
BM	4.40	13.38		8.98	Marnx Division
			4.31	9.07	NE Top Cb Marnx 40 ms
TP	5.11	14.11	4.38	9.00	
TP	9.00	20.88	2.23	11.88	
BM			5.99	14.89	S.E. B.P. Marnx Xesto ~~15.62~~

Cross Section Yamo St
Cottonwood to Main

INDEXED
EFB

60' Wide
10' Cbs
10' QH

37

BM.	8.04	12.11	9.07	N/E Top Cb Main & Yamo
	0+00 S/L Cottonwood			
N		3.8	9.3	
Cb Top		3.43	8.68	
Gutter		3.9	8.2	
¼		3.9	8.2	
½		4.1	8.0	
¼		4.3	7.8	
Gutter		3.8	8.3	
Cb Top		2.99	9.12	
F		3.0	9.1	
	0+50			
F		3.8	8.3	
Cb		3.8	8.3	
+5		4.0	8.1	
+7		4.5	7.6	
¼		4.6	7.5	
½		4.2	7.9	
¼		4.2	7.9	
+5		4.3	7.8	
Cb		3.6	8.5	
N		3.6	8.5	
	0+68			
F +10 = ½	24" Eucalyptus Tree			
	0+92			
F +10.5 = ½	3' Euc	Tree		

Red. & Plot on old profile 6-13-40 C.B.H.

12.11

	1+00	
N	4.2	7.9
Cb	4.2	7.9
+1	4.6	7.5
¼	4.7	7.4
½	4.5	7.6
¼	4.7	7.4
+4	4.7	7.4
+7	4.1	8.0
Cb	4.2	7.9
F	4.0	8.1
	1+15	
F +10 = ½	1.5' Euc Tree	
	1+19	
F = ½	Conc Walk	3.99 8.12
	1+40	
F +10 = ½	1.5' Euc Tree	
	1+50 = ½	Alley
F	4.5	7.6
Cb	4.6	7.5
¼	4.9	7.2
½	4.6	7.5
¼	4.8	7.3
Cb	4.8	7.3
N	4.8	7.3

12.11

1+60

M+9 = Ely Power Pole

1+88

E+0.8 = ± 2' Conc Walk 4.22 7.89

2+0

M	5.0	7.1
Cb	4.8	7.3
+1	5.0	7.1
¼	5.0	7.1
¼	4.8	7.3
¼	5.0	7.1
+2	5.0	7.1
Cb	4.8	7.3
E	4.8	7.3

2+50

E	5.2	6.9
Cb	5.0	7.1
¼	4.9	7.2
¼	5.0	7.1
¼	5.0	7.1
Cb	5.2	6.9
M	5.1	7.0

3+0 = M.L. Dalbergia

M	5.2	6.9
Cb	5.2	6.9
¼		
¼		
¼		
Cb		
E		

12.11

	5.2	6.9
	5.0	7.1
	5.1	7.0
	5.1	7.0
	5.2	6.9

S.L. Dalbergia = 0+0

E	5.5	6.6
Cb	5.6	6.5
¼	5.7	6.4
¼	5.3	6.8
¼	5.8	6.3
Cb	5.8	6.3
M	5.9	6.2

0+50

M	5.6	6.5
Cb	5.5	6.6
¼	5.9	6.2
¼	5.6	6.5
¼	5.2	6.9
Cb	5.4	6.7
E	5.3	6.8
+12 = Top Wash	60	5.1
+19 = Bottom Wash	10.4	1.T.

Yama

12.11

0+70

-25 = E Top Wash	5.4	6.7
-4' = Bot. "	10.6	1.5
E = W Top "	5.5	6.6
Cb	5.3	6.8
¼	5.4	6.7
½	5.8	6.3
¼	6.1	6.0
Cb	5.8	6.3
W	5.7	6.4

1+0

W	5.8	6.3
Cb	5.6	6.5
¼	5.9	6.2
½	5.6	6.5
¼ = Top Wash	5.0	7.1
+3	9.2	2.9
Cb = ½ Wash	10.4	1.7
+4	9.8	2.3
+6 = Top "	5.4	6.7
E	5.1	7.0

NE Top Cl Main Yama

TP	2.43	11.50	3.04	9.07

1+29

E	4.0	7.5
+6	4.3	7.2

11.50

Cb	8.2	3.3
¼	9.6	1.9
+6	9.6	1.9
+8	4.5	7.0
½	4.5	7.0
¼	5.3	6.2
Cb	4.8	6.7
W	6.0	6.5

1+35

W	3.0	8.5
Cb	3.0	8.5
¼	3.3	8.2
+6	3.7	7.8
½	6.3	5.2
+3	9.5	2.0
+7 = ½ Wash	10.0	1.5
¼	9.0	2.5
+8	8.5	3.0
Cb	4.8	6.7
E	3.7	7.8

1+43

E	2.8	7.7
Cb	4.6	6.9
+2	8.5	3.0
¼	9.4	2.1

11+50

+3 = ℄ Wash	10.0	1.5
℄	9.0	2.5
℄ 1/4	8.8	2.7
CL	8.9	2.6
W	8.6	2.9
1+46		
W	4.4	7.1
CL	4.0	7.5
1/4	4.0	7.5
℄	4.6	6.9
+2	4.8	6.7
+4	8.9	2.6
1/4	9.8	1.7
CL	9.0	2.5
+4	4.0	7.5
E	3.7	7.8
1+50		
E	3.9	7.6
+7	4.1	7.4
CL	9.7	1.8
1/4	10.0	1.5
1/4 Top 8" Cast Iron Pipe	80°	3.50
+7	8.8	2.7
℄ : ℄ M.H. or Rim	4.83	6.67
℄ 1/4	5.0	6.5

11+50

CL	5.0	6.5
W	5.3	6.3
1+62		
W 78.5 = E ly Light Pole		
2+0		
W	5.2	6.3
CL	5.1	6.4
1/4	5.1	6.4
℄	5.0	6.5
+2	8.2	3.3
+6	9.7	1.8
1/4	9.9	1.6
CL	9.1	2.4
+4	8.4	3.1
E = Top Wash	4.2	7.3
2+50		
E = Top Wash	4.3	8.2
+6	9.4	2.1
CL	9.7	1.8
1/4	10.1	1.4
℄	8.9	2.6
+5	6.0	5.5
1/4	5.9	5.6
CL	5.7	5.8
W	5.5	6.0

Yama

11.50

2+75

W	5.8	5.7
Cb	5.8	5.7
¼	6.0	6.5
+8	5.8	5.7
½	6.8	4.7
+5	9.9	1.6
¼	10.2	1.3
Cb	9.7	1.8
+4	9.2	2.3
E	4.0	7.5

2+89.5

E	2.7	8.8
F Top Conc. Headwall	4.70	6.80
+1	8.7	2.8
Cb	9.8	1.7
¼	11.0	0.5
½	9.5	2.0
+4	8.8	2.7
+4 Top Conc Headwall	4.80	6.70
¼	5.6	5.9
Cb	5.2	6.3
W	5.3	6.2

11.50

2+96.5 = W ¼ Conc Drain

W	3.6	7.9
Cb	3.8	7.7
¼	4.0	7.5
½	3.5	8.0
+2.5 = W ¼ Top Conc Drain	3.94	7.76
+2.5 Flow Line "	10.52	0.98
¼ Top Drain	3.78	7.72
¼ Flow Line "	10.50	1.00
Cb Top Drain	3.78	7.72
Cb Flow Line	10.46	1.04
+3' = El. Top Drain	3.77	7.73
+3 Flow Line	10.45	1.05
E	2.6	8.9

3+00.4 = W ¼ Main

E	2.3	9.2
+8.4 = Cb Top	2.43	9.07
+8.4 Gutter on Bevins	3.09	8.41
Cb " "	3.08	8.42
¼ " "	2.87	8.63
½ " "	2.83	8.67
¼ " "	2.90	8.60
Cb " "	3.03	8.47
+1.8 " "	3.07	8.43
+1.8 Top Cb	2.48	9.02

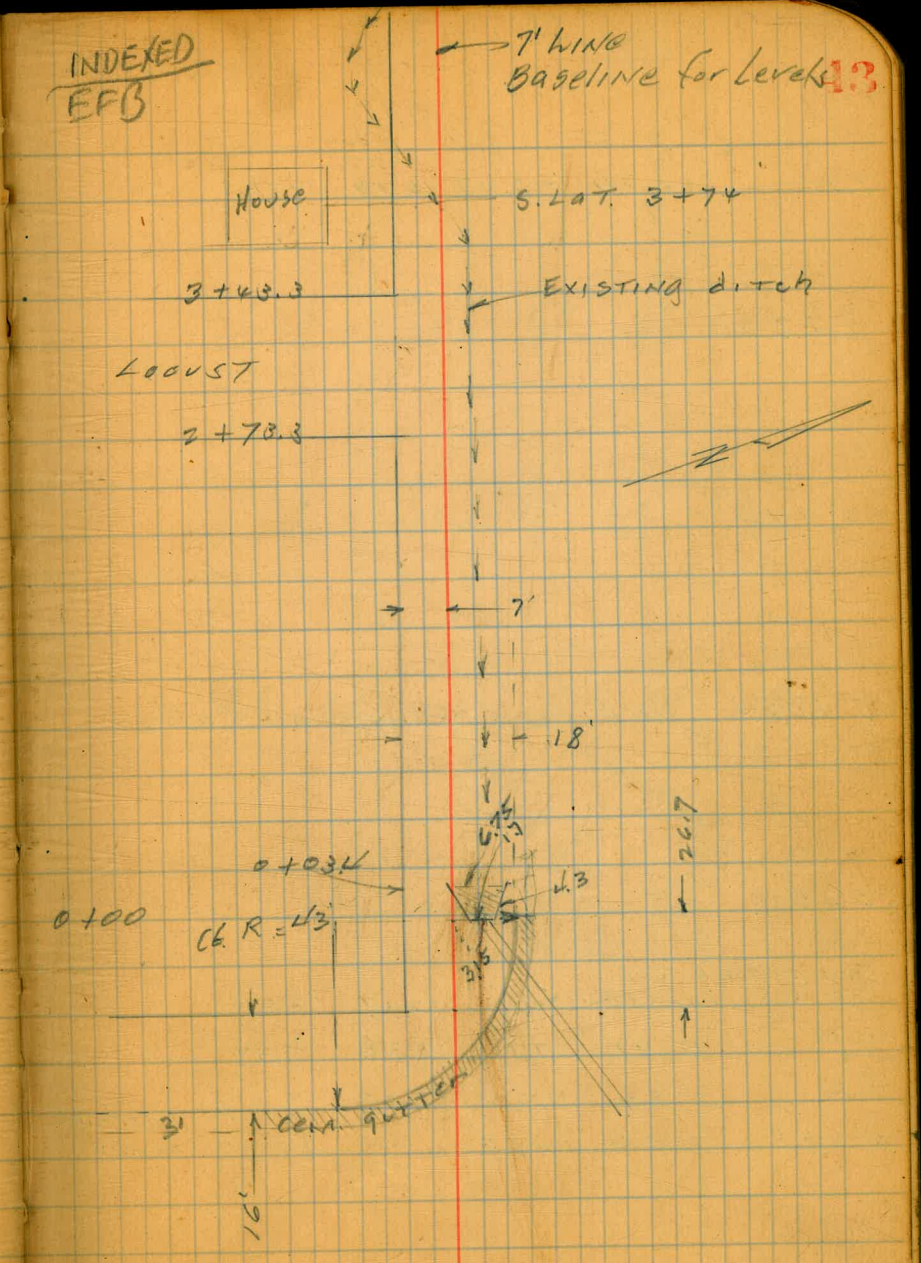
Main St. plan says 12'

		11.50		
W			2.4	9.1
		℄ Cb of Main St		
-10'	Top Cb		2.39	9.11
-10	Gutter on Pav		3.06	8.44
W		" "	3.00	8.50
℄		" "	2.95	8.55
E Cb = ℄	~~2.25~~ Grating		3.14	8.36
E	on Pav		3.05	8.45
+10 =		"	3.18	8.32
+10 =	Cb E.C. Top		2.53	8.97

Levels in drainage ditch on Russell St. Rosecrans to Ly

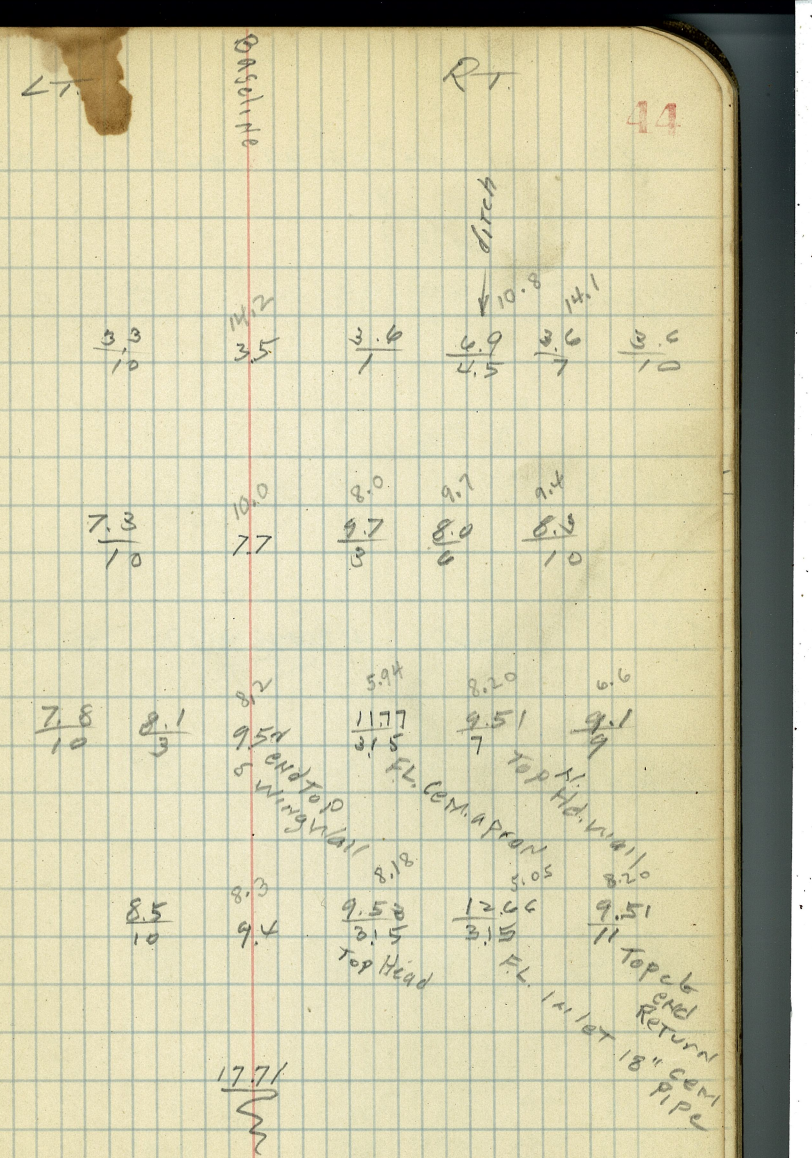
Moore
7-31-40.

INDEXED
EFB



T.P.	17.84	30.47	0.10	17.61
0+50				
0+10				
0+03.4	End Conc. wing wall & apron			
0+00				
Set B.M. B.P. Curb S.W. Rosecrans & Russell			12.17	5.54
T.P.	11.77	17.71	5.38	5.94
T.P.	4.05	11.32	5.18	7.27
N.W.B.F.	4.06	12.45		8.39

Rosecrans Newell



T.P.	1+46	54.99	0.49	42.53
3+00				
2+50				
T.P.	1+68	43.07	0.13	30.34
2+00				
1+50				
1+00				
		30.47		

LT B.L. RT.

ditch

4.1/10 41 6.4/2 6.4/4 4.4/6 4.4/10

4.9/10 9.5 9.7/1 12.2/2.5 12.2/4.5 9.4/6 9.5/10

43.02

ditch

2.4/10 2.7 2.6/1 5.0/3 5.0/5 2.5/7 2.7/10

7.3/10 7.5 7.5/1 10.5/3 10.5/5 7.6/7 7.6/10

12.0/10 12.0 12.0/1.5 15.4/4 15.4/5 12.4/8 11.8/10

ditch

30.47

4+40					8.6 / 30
T.P.	12.44	66.45	0.78	54.21	
4+00					
3+74					
3+40					
3+43.3	W/℄	Locust	St.		
		54.99			

LT. ℄ RT.

10.3/29 10.3/23 (54.4) 8.8/20 (57.9) 9.9/10 9.6 (57.1) 9.8/10

ditch

66.65

3.0/15 5.4/13 (49.6) 5.4/11 (51.2) 3.7/9 4.1 (50.9) 3.8/10

4.4/10 (47.1) 7.9/9 (46.7) 8.3/4 (48.3) 6.7/3 (48.1) 6.9 7.1/10

Top 4" C.I. Sewer Lat. from So.

8.7/10 8.6/5 (43.5) 11.5/2.5 (46.1) 8.9 8.7/10

10.7/10 10.9 (40.5) 14.5/3 (44.1) 10.9/6 11.1/10

54.99

℄

6+30 = BOTTOM WASH

6+10

5+80

T.P.	11.06	89.96 ✓	0.40	78.90 ✓

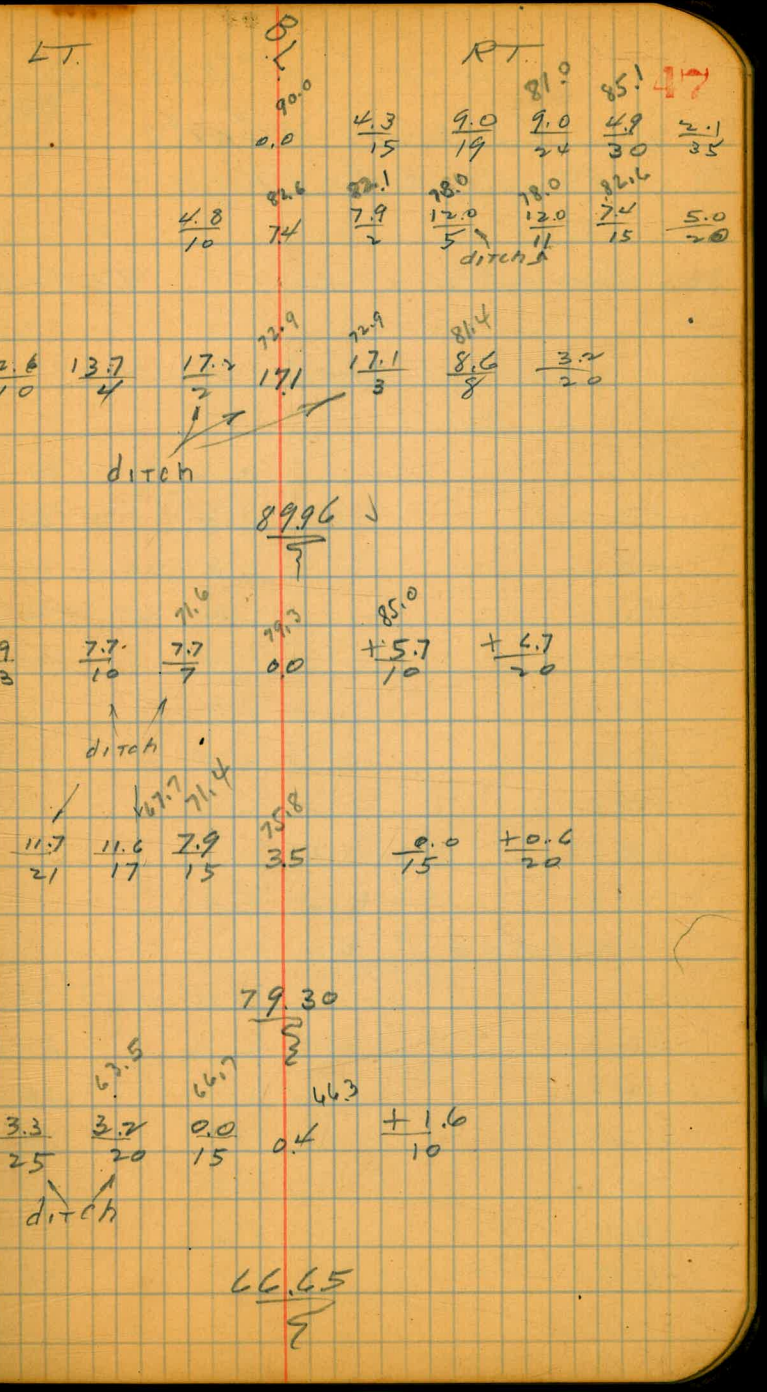
5+65

5+35

T.P.	12.74	79.30 ✓	0.09	66.56 ✓

5+00

66.65



Cont'd. from 1563-77

Xsec of Morell 60' wide 10' curbs

Pacific to Co. Pt. Dr.

			Pacific
SW 7' Mon.	2.83	26.36	23.53 Morell

0+00 S.L. Pacific Beach Dr.

0+50

W	0.6	25.8
c6	1.3	25.1
+7	1.8	24.6
1/4	2.4	24.0
C	1.9	24.5
1/4	2.7	23.7
+4	2.9	23.5
+6	2.5	23.9
c6	2.5	23.9
E	3.1	23.3

1+00

E	3.0	23.4
c6	2.6	23.8
1/4	2.3	24.1
C	1.7	24.7
1/4	1.7	24.7
c6	1.6	24.8
W	1.4	25.0

Notes Read & Plotted
Profile #1268
Aug-2014-40

INDEXED
EFB

26.30

offset to Edge Trees

1+08	2.5	di.	pepper Tree	21'	W of E
1+29	2	"	"	20.4	" "
1+50	1.5	"	"	21	" "
1+69	"	"	"	20.8	" "
1+90	1.4	"	"	20.9	" "

1+19

W	E 4'	Cem Walk	1.49	24.67
+9.9	"	curb	1.81	24.55

1+50

W	2.0	24.4
c6	2.5	23.9
1/4	2.7	23.7
C	2.8	23.6
1/4	3.1	23.3
c6	2.9	23.5
E	3.1	23.3

2+00

E	4.0	22.4
c6	3.4	22.8
1/4	3.7	22.7
C	3.4	23.0
1/4	3.7	22.7
+1	3.5	23.0
c6	2.8	23.6
W	2.3	24.1

	2+25		
E	on c4x11.	4.70	21.66
E-13	Top Bot. Stop c4x11.	4.26	22.10
	2+50		
W		4.0	22.4
c6		4.1	22.3
+7		4.4	22.0
+8		4.9	21.5
1/4		5.0	21.4
C		4.8	21.6
1/4		5.4	21.0
c6		5.3	21.1
E		5.4	21.0
	3+0		
E		6.5	19.9
c6		6.1	20.3
1/4		6.5	19.9
C		6.2	20.2
1/4		6.3	20.1
+2		6.2	20.2
+3		5.8	20.6
c6		5.6	20.8
W		5.4	21.0
	3+50		
W		4.5	19.9
c6		4.7	19.7

26.36

+6	7.2	19.2
+8	8.2	18.4
1/4	8.0	18.4
C	7.7	18.7
1/4	8.0	18.4
c6	8.2	18.2
E	8.7	17.7
+15	9.2	17.2
	4+00	
-15	11.6	14.8
E	11.0	15.4
c6	10.3	16.1
1/4	9.6	16.8
C	9.3	17.1
1/4	9.6	16.8
+1	9.6	16.8
+3	8.9	17.5
c6	8.6	17.8
W	8.3	18.1
	4+50	
W	10.2	16.2
c6	10.6	15.8
+8	10.8	15.6
1/4	11.1	15.3
C	10.5	15.9

26.36

E 1/4		16.1	15 3
c6		12.0	14 4
E		12.2	14 2
+15		12.6	13 8
5+00			
-15		12.9	13 5
E		12.9	13.5
c6		12.6	13 8
1/4		11.7	14.7
C		11.2	15.2
1/4		11.6	14.8
c6		11.4	15 0
W		11.0	15 4
T.P.	6.38	21.60	11.14	15.22

5+16 2' di. pep. Tree 19.3 W of E
5+39 1.2 " " " 19.3 " " "
5+52 1.0 " " " 20.1 " " "

5+40

W		5.7	15.9
W-4.3 E 6' wide cent. walk		5.54	16.06

21.60

5+50

W	5.9	15.7
c6	6.3	15.3
1/4	6.4	15.0
C	6.4	15.2
1/4	6.8	14.8
c6	7.5	14.1
E	7.5	14.1
+15	7.8	13.8
6+00		
-15	6.2	15.4
E	6.5	15.1
c6	6.7	14.9
1/4	6.4	15.2
C	6.0	15.6
1/4	6.2	15.4
+6	6.3	15.3
+7	5.4	16.2
c6	5.2	16.4
W	5.1	16.5

See Fortuna Xsec for 6+12.8
• ML Fortuna

0+0 = SL. Fortuna FB 1563

0+20

W-0.5 E 3' Cent walk	3.73	17.87
W-9.9 Top bot. cent. step	3.14	18.46

21.60

0+20		
W - 11.8 Top. conc. porch	2.06	19.56
0+50		
W	3.6	18.2
+7	3.5	18.1
+8	3.9	17.7
c.b	3.9	17.7
1/4	3.6	18.0
C	3.2	18.4
1/4	3.5	18.1
+1	2.9	18.7
cb	2.8	18.8
E	3.0	18.6
1+00		
E	2.2	19.4
cb	1.8	19.8
+9	2.1	19.5
1/4	2.6	19.0
C	2.4	19.2
1/4	2.7	18.9
cb	2.9	18.7
+1	3.0	18.6
+2	2.4	19.2
W	2.4	19.2
1+09.5		
W	2.3	19.3

21.60

51

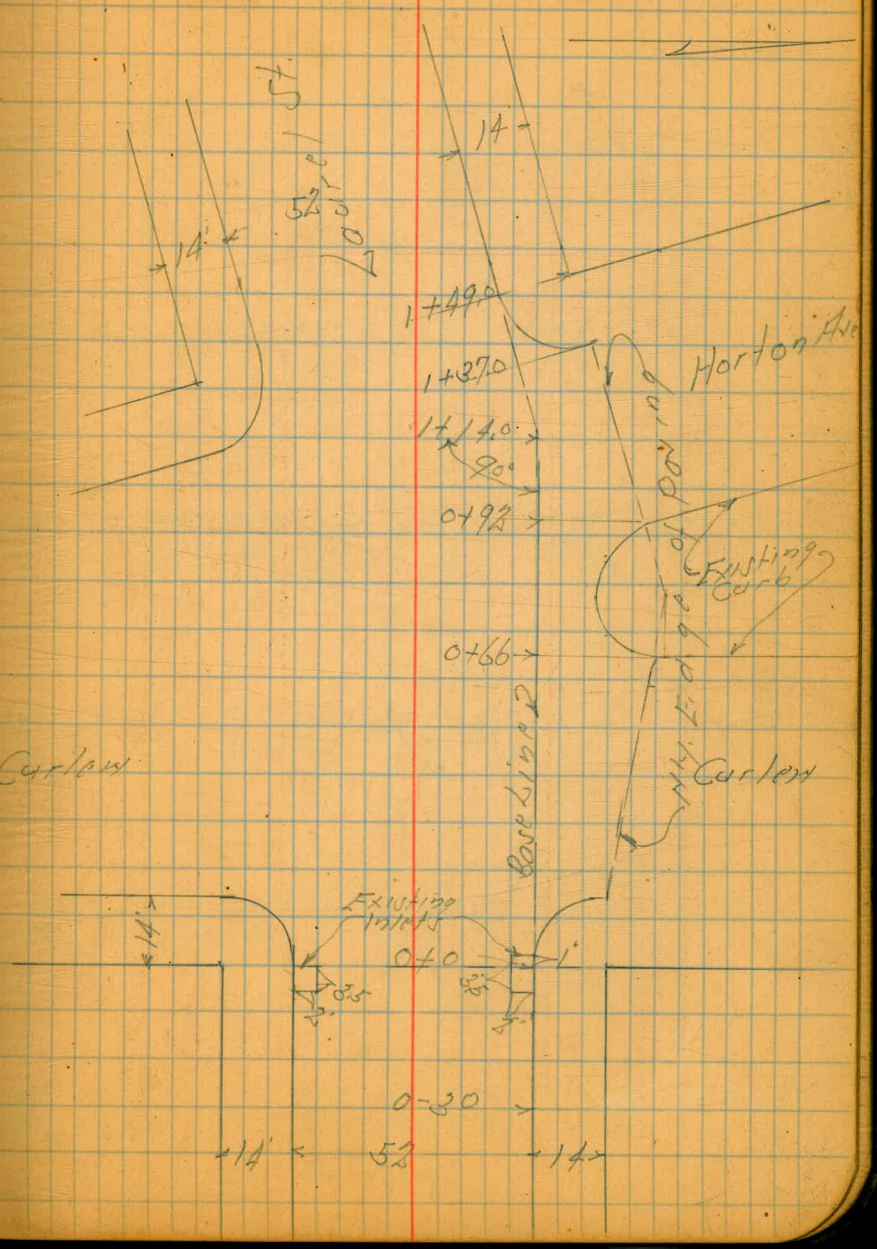
+8	2.4	19.2
+9	3.0	18.6
cb.	3.0	18.6
1/4	2.7	18.9
C	2.3	19.3
1/4	2.6	19.0
+5	2.1	19.5
cb	2.1	19.5
+7	2.3	19.3
E = W & Cr. Pt. Dr.	2.7	18.9
1+32.10		
C	2.4	19.2
W 1/4	2.9	18.7
cb	2.9	18.7
+W	2.9	18.7
+C	2.6	19.0
W	2.6	19.0
1+54.71 W & Cr. Pt. Dr.		
W	2.4	19.2
check to T.P. 1563-55	2.59	19.01 19.00

Paving Levels Laurel St At Carlow

INDEXED
EFB

Oct 29-40
Sisson
Workman
& Moore

52



Paving Levels Laurel St At Carlew St

Station					Lt=S					℄	Rt=N	
0+30					5.85 / 52	5.45 / 40	5.11 / 30	4.84 / 20	4.70 / 10	4.59	4.32 / 15.7=N4 Pav	
0+20					6.09 / 52	5.50 / 40	5.05 / 30	4.78 / 20	4.65 / 10	4.55	4.43 / 14.4=N4 Paving	
0+14			5.90 / 66:Cb	6.76 / 66:Gut	6.23 / 52	5.51 / 40	5.00 / 30	4.77 / 20	4.65 / 10	4.52	4.49 / 13.6=Gut	3.92 / 13.6=Cb
0+0 = E L Carlew				5.93 / 52:Cb	6.39 / 52:Grat	5.57 / 40	4.85 / 30	4.60 / 20	4.55 / 10	4.60 / 0.0:Gut / 0.0:Grat	3.93 / 0.0:Cb	
0-15				5.45 / 52:cb	5.97 / 52:Gut	5.08 / 40	4.40 / 30	4.07 / 20	4.05 / 10	4.17 / 0.0:Gut	3.45 / 0.0:Cb	
0-30				4.92 / 52:cb	5.46 / 52:Gut	4.60 / 40	3.92 / 30	3.61 / 20	3.55 / 10	3.62 / 0.0:Gut	2.95 / 0.0:Cb	
BM	5.88	151.95	146.07	S.E.B.P. Laurel Carlew						151.95		

Laurel at Curlew

Station			Lt					℄	Rt		
1+14.0 = ℄	7.96 / 69:Cb	8.56 / 69:Gut	7.77 / 52	6.47 / 40	6.08 / 30	6.00 / 20	5.93 / 10	5.94	5.44 / 12.9:Hy Pav		
0+92			6.58 / 52	6.00 / 40	5.70 / 30	5.50 / 20	5.52 / 10	5.56	5.57 / 10	5.50 / 20:Gut	4.85 / 20:Cb
0+80			6.29 / 52	5.77 / 40	5.47 / 30	5.25 / 20	5.29 / 10	5.35	5.51 / 9.9:Gut	4.88 / 9.9:Cb	
0+66			5.93 / 52	5.54 / 40	5.27 / 30	5.10 / 20	5.07 / 10	5.11	5.27 / 10	5.31 / 21:Gut	4.83 / 21:Cb
0+50			5.85 / 52	5.53 / 40	5.22 / 30	5.02 / 20	4.95 / 10	4.89	4.56 / 18.6:Hy Pav		
0+40			5.74 / 52	5.47 / 40	5.15 / 30	4.88 / 20	4.79 / 10	4.70	4.32 / 17:Hy Pav		

151.95

151.95

Lt. ℄ Rt.

1+49 = W L Horton 7.97 52-Cb 8.50 52-Gut 7.80 40 7.28 30 6.94 20 6.78 10 6.65 0.0-Gut 5.92 0.0-Cb

1+37 7.95 52 6.97 40 6.55 30 6.37 20 6.26 10 6.41 6.35 14-Gut 5.93 14-Cb

151.95

Cross Section Curlew Place
Washington St to Dove St.

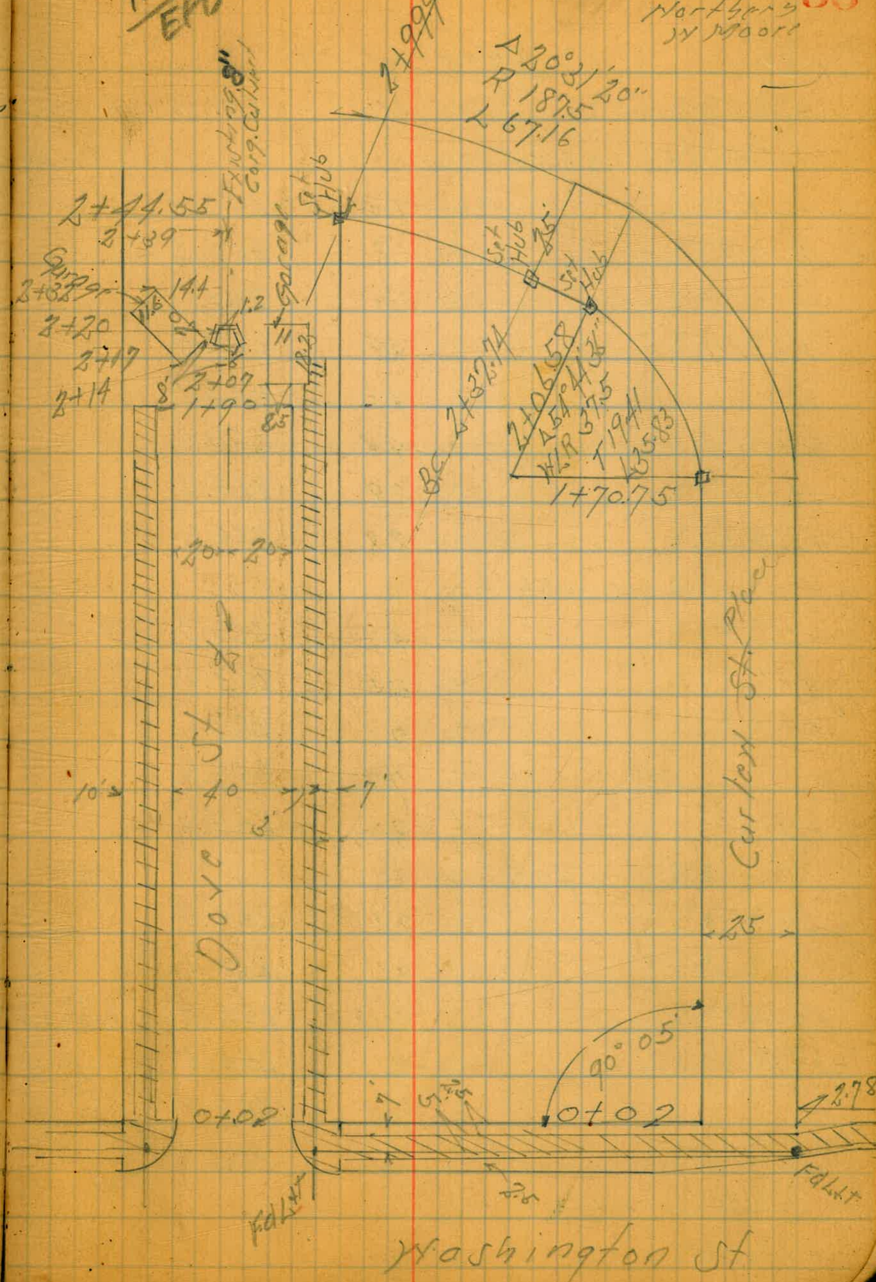
Wat Line Stationing

BM	6.51	269.57		263.06	N.E. BP Washington & Eagle
TP	6.53	267.75	8.35	261.22	
	H Cb Washington				
-18'	= Angle Curb		5.66	262.09	
	Gutter on Pav		6.09	261.66	
W	Cb		6.10	261.65	
	Gutter on Pav		6.53	261.22	
℄	Cb		6.32	261.43	
	Gutter on Pav		6.86	260.89	
E	Cb		6.58	261.17	
	Gutter on Pav		7.16	260.59	
+20	= Angle Curb		6.95	260.80	
	Gutter on Pav		7.29	260.36	
	0+0 = H.L. Washington				
-10			6.7	261.0	
F			6.5	261.2	
℄			6.2	261.5	
W			5.8	261.9	
+10			5.5	262.2	
	0+2				
-10			3.2	264.5	
W			3.2	264.5	
+1			4.7	263.0	
℄			5.5	262.2	
F			6.5	261.2	

Reduced 12-2-40 AL
Plotted 12-4-40 AL

INDEXED EFB

Nov. 28. 40
S. Nov
J.J. Moore



	267.75		
+10		6.7	261.0 ✓
	0+75		
-10		7.3	260.4 ✓
E		6.8	260.9 ✓
℄		6.0	261.7 ✓
+6		4.9	262.8
W		4.6	263.1 ✓
+4		4.4	263.3 ✓
+6		3.9	264.8 ✓
+15		3.8	264.9 ✓
	0+50		
-10		4.7	263.0 ✓
W		5.5	262.2 ✓
℄		7.1	260.6 ✓
E		7.9	259.8 ✓
+10		8.0	259.7 ✓
	0+75		
-10		7.4	260.3 ✓
E		7.6	260.1 ✓
+7		10.8	256.9
℄		9.1	258.6 ✓
W		7.4	260.3 ✓
+10		5.6	262.1 ✓
	1+0		
-10		8.1	259.6 ✓

	267.75		
W		10.3	257.4 ✓
+9		12.5	254.2
℄		11.3	256.4 ✓
+6		8.1	259.6
E		8.6	259.1 ✓
+20		7.7	260.0 ✓
	1+10		
-20		8.2	259.5 ✓
E		8.1	259.6 ✓
℄		14.7	253.8 ✓
+4		16.7	251.0
W		13.4	254.3 ✓
+5		10.0	257.7 ✓
+10		8.8	258.9 ✓
TP	0.20	255.85	12.10 255.65
	1+25		
-10		0.3	255.5 ✓
W		4.8	251.0 ✓
℄	= Toe New Fill	9.0	246.8 ✓
E		7.3	248.5 ✓
+20		9.5	246.3 ✓
	1+45		
-30	on New Fill	24.9	230.9 ✓
E	= Toe " "	21.0	234.8 ✓
℄		15.5	240.3 ✓

		255.85		
W			11.4	244.4 ✓
+10			8.4	247.4 ✓
+20			5.2	250.6 ✓
		1+54		
W -3.5 = W/y 12" Pepper Tree				
		1+70.75 = BC. Lt.		
-20			9.3	258.4 ✓
TP	0.59	244.70	11.74	244.11
-10			2.9	241.8 ✓
W			5.0	239.7 ✓
℄			9.9	234.8 ✓
E			16.6	228.1 ✓
+25			25.8	218.9 ✓
+40 = Top New Fill			32.1	212.6 ✓
		1+90		
-50			42.2	202.5 ✓
-25			34.0	210.7 ✓
E			21.9	222.8 ✓
℄			16.2	229.5 ✓
W			8.7	236.0 ✓
+10			5.1	239.6 ✓
+20			0.8	243.9 ✓
		2+06.58 = E.C.		
-15			2.6	242.1 ✓
W on Stub			7.55	237.15 ✓

		244.70		
℄			12.5	232.2 ✓
E			20.0	224.7 ✓
+20			28.1	216.6 ✓
+50			42.0	202.7 ✓
		2+22.74 BC Lt.		
-35			33.0	211.7 ✓
-20			24.8	219.9 ✓
E			15.8	228.9 ✓
℄			10.0	234.7 ✓
W on Stub			6.44	238.26 ✓
+10			2.1	242.6 ✓
+20			4.4	249.1 ✓
		2+50		
-20			5.0	249.7 ✓
W			2.6	242.1 ✓
℄			8.7	236.0 ✓
L			14.1	230.6 ✓
+15			22.1	222.6 ✓
+35			33.5	211.2 ✓
TP	1.75	253.75	1.70	252.00
		2+75		
-35			33.3	220.4 ✓
-15			25.5	228.2 ✓
E - W			16.8	236.9 ✓
℄			10.0	243.7 ✓

	℄58.75		
W-5		4.2	249.5 ✓
+10	= N½ Frametube =	3.6	250.1 ✓
	℄+99.9 = E.L. Dove St.		
-11.6	= N×E½ Conc. Wall Base	1.0	252.7 ✓
-9		2.6	251.1 ✓
℄		4.1	249.6 ✓
℄		12.5	241.2 ✓
N		20.2	233.5 ✓
+20		26.3	227.4 ✓
+35		32.0	221.7 ✓
B.M.		0.85	℄52.90 on Rock

Cross Section Dove St.
North of Washington

INDEXED
EFB

BM	5.42	268.48	263.06	NE BP Washington & Dove
		0+00 - NL Washington		
ECb Top		5.04	263.44 ✓	
Gutter		5.42	263.06 ✓	
℄		4.47	264.01 ✓	
WGutter		4.68	263.80 ✓	
WCb Top		3.98	264.50 ✓	
		0+50		
WCb Top		4.94	263.54	
Gutter		5.47	263.01	
℄		5.08	263.40	
EGutter		5.88	262.60	
ECb Top		4.49	~~263.99~~ 262.99	
		0+75		
ECb Top		5.75	262.73	
Gutter		6.16	262.32	
℄		5.41	263.04	
Gutter		5.93	262.55	
WCb Top		5.47	263.01	
		1+00		
WCb to Drive		4.53	261.95	
℄		4.06	262.42	
EGutter		4.68	261.80	
ECb Top		4.18	262.30	

Profile No 243
12-8-40
C.S.H.

268.48

	1+25	
ECb Top	7.49	260.99
Gut	7.86	260.62
℄	7.32	261.16
WGut	7.85	260.63
WCb Top	7.50	260.98
	1+50	
WCb	9.00	259.48
Gut.	9.37	259.11
℄	8.80	259.68
EGut	9.39	259.09
ECb Top	8.95	259.53
	1+90	
ECb - End	11.20	257.28
Gut	11.51	257.97
℄	11.00	257.48
WCb to Drive	11.60	256.88
	2+07	
WCb + 8 = Edge Paving	12.06	256.42
℄	11.91	256.57
+ 11 Edge Paving	12.24	256.24
ECb + = Edge Floor Garage	11.45	257.03
TP 209	258.47	12.10 256.38

258.47

2+17

10' E of ℄	1.5	257.0
3' E " " = Top Wing Wall	2.7	256.20
3' E " " Gutter	3.05	255.42
℄ on Conc Apron	3.10	255.32
3' W of ℄ = Gutter	3.01	255.43
3' " " " = Top Cb	2.25	256.22
9' W " ℄ = E/L Garage	2.3	256.2

2+20

℄ = Flow Line on 0.8 Corg Pipe	3.39	255.08
℄ = Top Wing Wall	2.33	256.14

2+30

20' E of ℄	1.8	256.9
10' E " "	2.5	256.0
℄	2.1	256.4
10' W of ℄	3.1	255.4
13' W " " = W/L Garage	8.6	249.9

2+41.55 = SE Curlew Place

30' W of ℄	15.8	242.7
10' W " "	14.5	244.0
℄	14.8	243.7
10' E of ℄	11.0	247.5
20' E " "	10.5	248.0

2+89 = W/L Existing 0.8' Corg. Drain

℄ = Flow Line	9.28	249.89

258.47

2+70

20' E of ℄	26.5	232.0
10' E " "	27.8	231.2
℄	28.7	229.8
10' W of ℄	29.0	229.5
20' " " "	31.1	227.4
B.M.	5.60	252.89

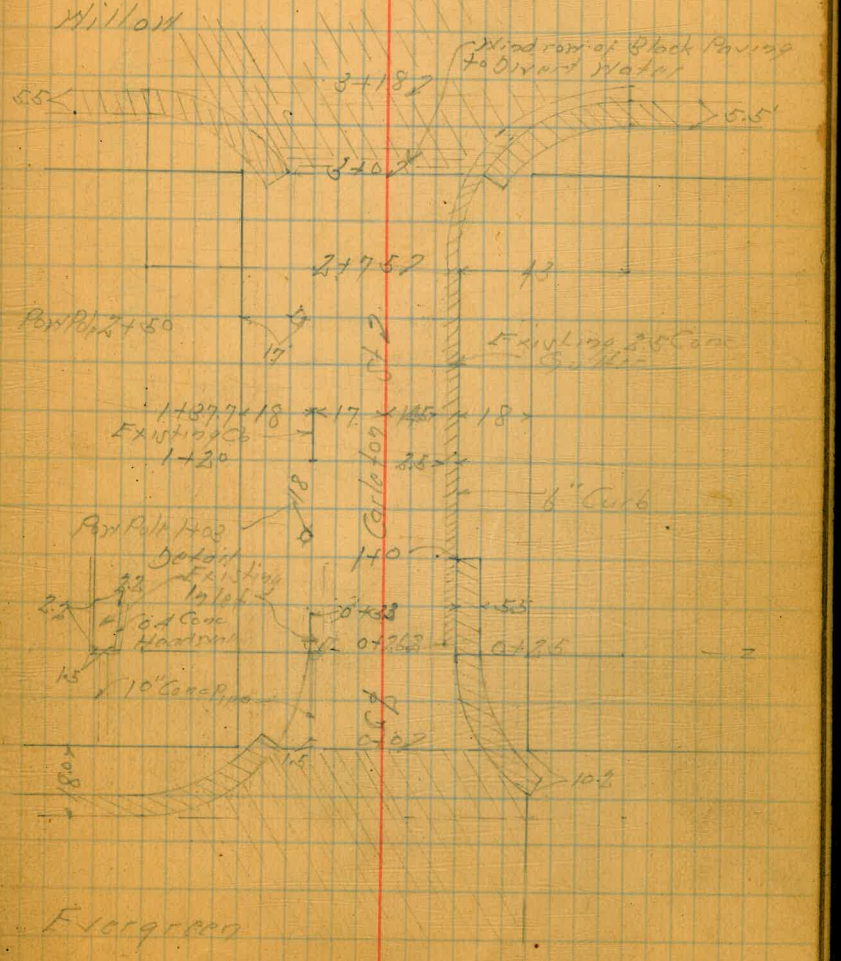
252.90 Page 69

Cross Section Carleton St.
Evergreen to Willow

Indexed
LM.

May 1-1941
Sisson
Norberg
Wilmore

62



Cross Section Carleton St. Evergreen to Willow — 70' Wide — 18 C&S

SECTIONS PLOTTED 1/1/42 WW.O.

NOTES REDUCED BY M.R.Y.

0+26.2					
0+25					
0+10					
0+0 : W.L Evergreen					
0-10.2					
0-18 : W.C.L Evergreen					
TP	5.87	34.33	10.64	28.46	
TP	0.39	39.10	11.81	38.71	
BM	1.01	50.52		49.51	SJWRP Evergreen Carleton Road

St. 5 — Rt. H — 63

29.57 29.38 30.14
4.76 4.95 4.19
19.5-Edge Concrete 17-Gr 17-Cb

31.5 31.1 30.86 29.7 30.9 29.5 29.9 29.6 28.9 29.88
2.8 3.2 3.47 4.6 3.4 4.8 4.4 4.7 5.4 4.45
35 20 17-Cb 17-Fine Gravel 15 8.5 8.5 17 17-Cb

29.6 28.03 27.7 28.0 27.3 27.5 27.1 26.2 26.2 27.25
4.7 6.30 6.6 6.3 7.0 6.8 7.7 8.1 8.1 7.08
35 19.3-Cb 19.3- 17 8.5 8.5 17 19.3-Gr 19.3-Cb

27.6 26.7 26.66 25.98 26.01 25.90 25.47 25.24 25.85
6.7 7.6 7.67 8.35 8.32 8.43 8.86 9.09 8.48
35 30 25-Cb 25-Gr 17 17 25-Gr 25-Cb

26.07 25.39 25.63 25.53 25.25 24.40 24.97
8.26 8.91 8.70 8.80 9.08 9.93 9.36
35-Cb 35-Gr 17 17 35-Gr 35-Cb

26.37 25.77 25.29 25.38 25.31 25.05 24.43
7.96 8.55 9.04 8.95 9.02 9.28 9.90
20-Cb 6-Gr 35 17 17 35-Fine Gr

34.33 ✓

TP	11.82	69.92	0.16	58.10
1+50				
1+377				
1+20				
TP	12.26	58.26	0.04	46.00
1+0				
0+75				
0+50				
TP	11.81	46.04	0.10	34.23
0+32				
		34.33		

55.7 55.0 53.9 54.1 53.9 53.71 53.51 54.26 54.5

52.75

50.0 49.41 48.6 47.7 48.2 48.0 47.89 47.64 48.44 48.5

58.26

45.4 45.4 44.9 43.9 44.3 44.2 44.06 43.82 44.56 44.5

41.0 41.0 40.3 38.7 39.1 39.1 39.10 38.87 39.12

36.0 36.0 35.6 34.9 33.7 34.2 34.2 34.23 34.01 34.78

46.04

32.22 31.8

34.33

2+75 = BC of (C-6)

TP	9.70	88.46	1.30	78.76 ✓
2+50				
2+25				
TP	10.24	80.06	0.10	69.82 ✓
2+02				
1+98				
1+81				
1+78				

69.92

47 X RP

81.1 81.3 80.0 79.2 79.3 79.4 78.9 78.33 78.09 78.84 79.5
7.4 7.2 8.5 9.3 9.4 9.1 9.6 10.13 10.37 9.63 9.0
3.5 2.5 17 15 8.5 8.5 14.5 17 17 3.5

88.46 ✓

75.8 75.2 74.2 74.0 74.4 74.0 73.64 73.40 74.19 74.8
4.3 4.9 5.9 6.1 5.7 6.1 6.43 6.66 5.87 5.3
3.5 17 15 8.5 8.5 14.5 17 17 3.5

70.9 69.9 69.8 69.1 69.2 69.0 68.73 68.57 69.33 69.8
9.3 10.3 10.3 11.0 10.9 11.1 11.33 11.47 10.73 10.3
3.5 17 10 8.5 8.5 14.5 17 17 3.5

80.06 ✓

66.0 66.3 65.3 65.0 64.8
3.9 3.6 4.6 4.9 5.1
3.5 2.5 17 8.5

63.8 64.1 64.1 63.9 63.5 63.42 63.24 64.10 64.3
6.1 5.8 5.8 6.0 6.4 6.50 6.68 5.87 5.6
3.5 17 8.5 14.5 17 17 3.5

63.42 62.92 62.4 61.1 60.4 60.4
6.50 7.00 7.5 8.8 9.5 9.5
3.5 30.9 17 8.5 6

61.55 60.9 60.6 59.7 59.6 59.4 59.29 59.08 59.87 60.1
8.37 9.0 9.3 10.3 10.3 10.5 10.63 10.84 10.05 9.8
3.5 2.5 17 8.5 8.5 14.5 17 17 3.5

69.93 ✓

Lt Contd- Rt

p. 68

BM			11.17	49.49 ✓	SWBP Evergreen & Canby Road 49.51
TP	0.45	60.66	11.46	60.21 ✓	
TP	0.09	71.67	11.56	71.58 ✓	
TP	0.18	83.14	12.20	82.96 ✓	
TP	6.84	95.16	0.14	88.32 ✓	
BM			12.01	76.45	✓ SWBP Willow & Dickens 76.36

Station										
3+18 = ECb Willow	86.21	85.40	85.03	84.81	84.48	84.09	83.42	82.02	82.81	
	2.25	3.06	3.43	3.65	3.98	4.37	5.04	6.44	5.65	
	60-Cb	60-Gut	35	17		17	35	60-Gut	60-Cb	
3+09	85.27	84.53	84.41	84.41	84.28	84.13	83.83	83.10	83.85	
	3.19	3.93	4.05	4.05	4.18	4.33	4.63	5.36	4.61	
	34-Cb	34-Gut	17	8.5		8.5	17	33.5-Gut	33.5-Cb	
3+0 = FL Willow	85.2	84.83	84.9	84.2	84.1	83.9	84.0	83.7	83.91	83.8
	3.3	3.63	3.6	4.3	4.4	4.6	4.5	4.8	4.55	4.7
	35	25.5 [illegible] Cb [illegible]	17	8.5		8.5	17	24.8	24.8	35
2+85		82.8	81.7	81.5	81.3	81.0	80.25	80.10	80.83	81.7
		5.7	6.8	7.0	7.2	7.5	8.21	8.36	7.63	6.8
		35	17	8.5		8.5	15.5 [illegible]	18	18-Cb	35

88.46

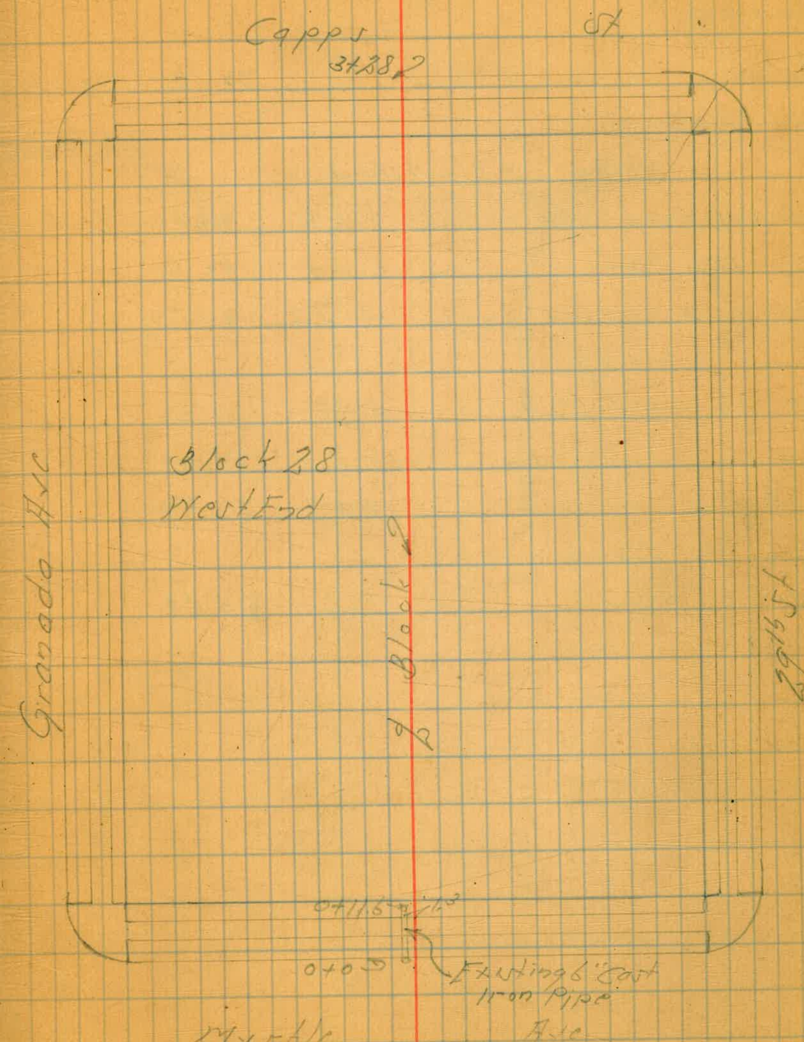
88.46 ✓

Levels Center of Block 28 West End
From Myrtle to Capps

Indexed / LM

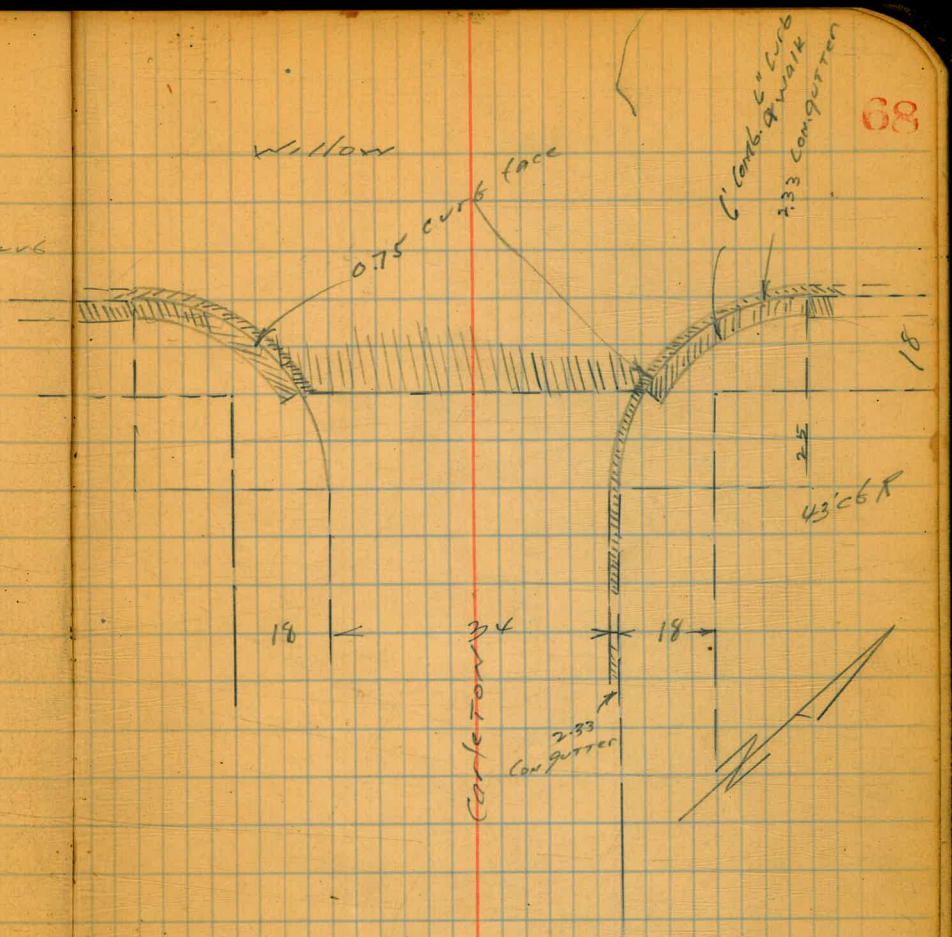
BM	4.01	334.98		330.97	NE BP Myrtle & Granado
0+0 = N Cb Line Top Cb	Myrtle		4.51	330.47	
Flow Line 6" Cast Iron Pipe			5.06	329.92	
0+11.6 = N'ly End 6" Cast Iron Pipe Flow Line			4.95	330.03	
0+30			3.8	331.2	
0+50			3.6	331.4	
TP	4.61	336.12	3.47	331.51 ✓	
0+75			4.8	331.3	
1+0			5.0	331.1	
1+25			4.5	331.6	
1+50			4.6	331.5	
1+65			4.4	331.7	
TP	4.63	335.96	4.79	331.33 ✓	
1+90	℄		4.7	331.3	
1+90	30' W of ℄ Low Spot		4.6	331.4	
2+10			4.6	331.4	
2+25			4.7	331.3	
TP	4.52	336.47	4.01	331.95 ✓	
2+62			4.3	332.2	
TP	2.69	337.93	1.23	335.24 ✓	
3+0			5.7	332.2	
3+28 = S Cb of Capps Cb			5.02	332.91	
Gutter on Paving			5.47	332.46	
BM			4.84	333.09 ✓	NW BP Capps & Granado 333.05

May 1-1941
Sissay
Northing
W Moore



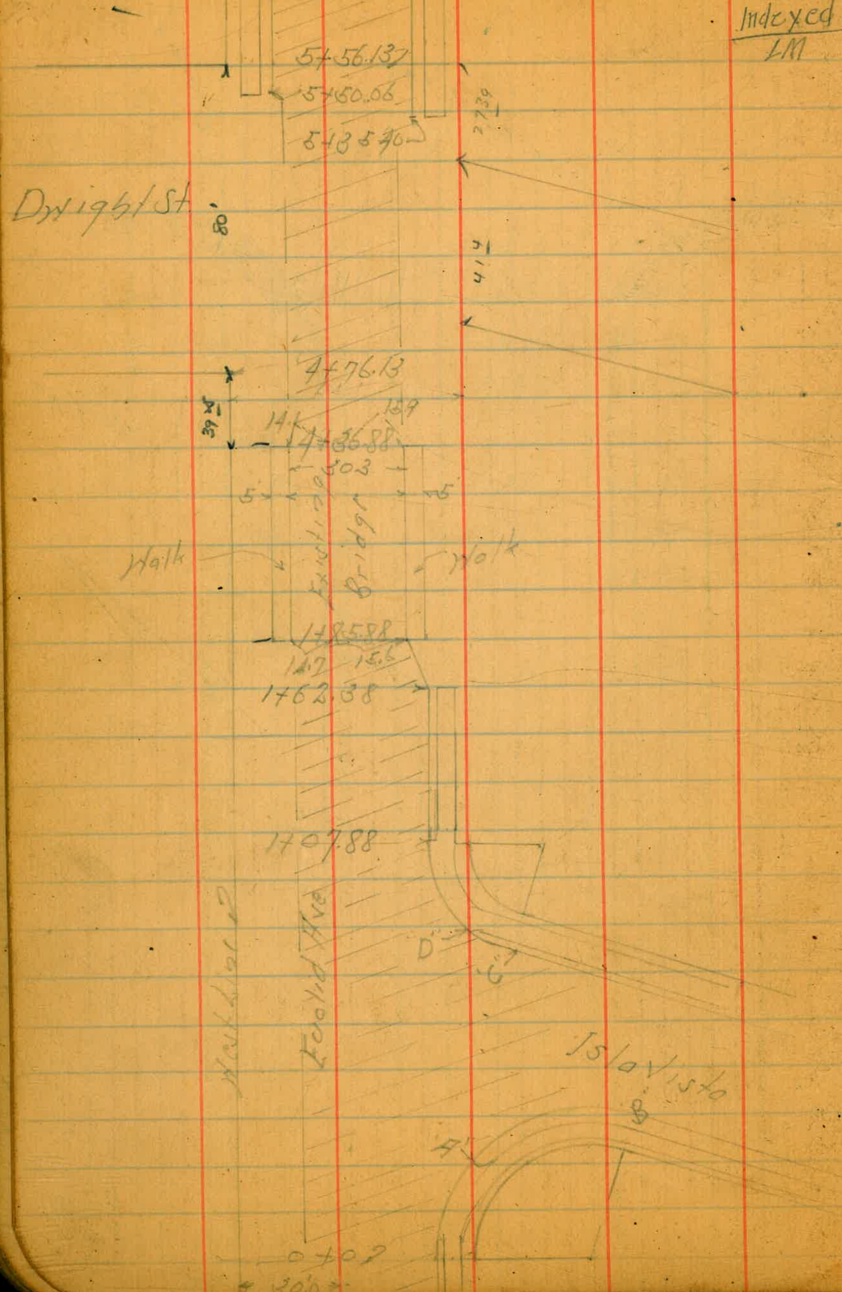
from p. 66

3+18 60' Rt.	6.80	89.61	82.81	Top Curb
	3+00 - El. Willow:			
N	Top curb	5.69	83.92	
C	old Pav	6.00	83.61	
S	Top end Ex curb	4.83	84.78	
	3+09			
S 1/4	old Pav	5.39	84.22	
C	" "	5.52	84.09	
N 1/4	" "	5.67	83.94	
	3+18			
C	Pav.	5.13	84.48	



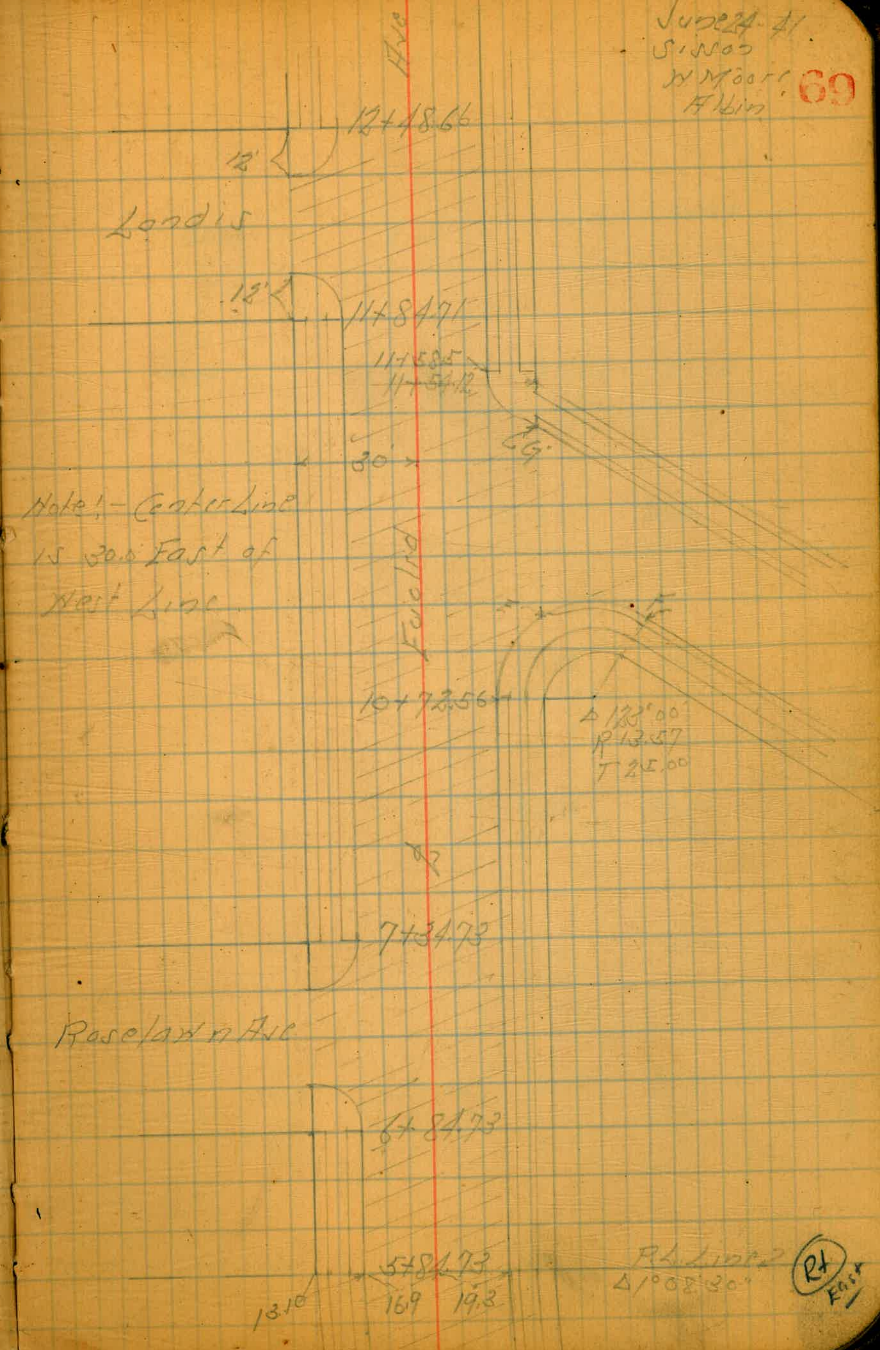
Cross Section Euclid Ave
Isla Vista to Landis

Indexed
LM



June 24-41
Sisson
W Moore
Albin

69



Cross Section Euclid Ave.
Isla Vista to Landis

Station					Remarks	Lt = W	℄	Rt E	
									31.34
1+62.38 = Δ Cb						31.21 5.69 9.4 = Hwy Pav	31.31 5.58	30.45 6.45 18.6	30.39 6.58 18.6
1+07.88 = EC on E						31.89 5.01 9.7 = Hwy Pav	32.01 4.89	31.53 5.37 18.4 Gut	31.93 4.97 18.4 Cb
"D"								31.66 5.24	31.90 5.00
"C" = Prop EC on N								32.46 4.54 Gut	32.86 4.04
"B" = Prop EC on S								32.88 4.02 Gut	33.36 3.54 Cb
"A"								33.18 3.78 Gut	33.40 3.50 Cb
0+0						33.08 3.82 9.8 = Hwy Pav	33.25 3.65	32.91 3.99 18.2 Gut	33.35 3.55 18.2 Cb
BM	1.20	336.90		335.70	S F Top Hyd Isla Vista & Euclid #1566 P13		336.90		

Notes Reduced. 6-27-61

Station		Lt	Lt	℄	Rt	Rt
5+50.6 = S End Cb & Walk on W		32.82 5.73 16.9 = Cb	32.35 6.20 16.9 = Gut.	33.05 5.50	32.55 6.00 19.2 = Gut	33.01 5.54 19.2 = Cb
5+35.40 = S End Cb & Walk on E			32.42 6.13 14 = W¼ Pav	32.81 5.74	32.44 6.11 19.2 = Gut	32.85 5.70 19.2 = Cb
5+16.13 = ℄ Dwight From W			32.37 6.19 14 = W¼ Pav	32.61 5.94	32.38 6.17 16 = E¼ Pav	
4+76.13 = S.L. Dwight From W			32.21 6.34 14 = W¼ Pav	32.37 6.18	32.15 6.40 16 = E¼ Pav	
4+36.88 = N End Bridge		32.70 5.85 14.1	32.30 6.25 14.1 = Deck	32.29 6.26	32.40 6.15 15.9 = Deck	32.69 5.86 15.9
TP	5.72 ✓ 338.55 4.07 332.83 N.W. BP Dwight & Euclid			338.55		
1+85.88 = S End Bridge		31.63 5.27 14.7 = Top Guard	31.33 5.57 14.7 = Deck	31.28 5.62	31.23 5.67 15.6 = Deck	31.61 5.29 15.6 = Cb End
	336.90			336.90		

Euclid Ave.

					Lt		℄	Rt	
BM		268	335.87	N.W. Lot Roselawn & Euclid 335.85					
7+24.73	N Cb Line Roselawn				35.84 2.71 29.8=Cb N/s Return	35.54 3.01 29.8=Gut			
6+94.73	= S Cb Line Roselawn				335.44 3.11 29.3=Cb N/s Return	35.15 3.40 29.3=Gut			
6+84.73	= S L Roselawn				35.36 3.19 17.1	34.94 3.61 17.1	35.24 3.31	34.69 3.86 19	35.11 3.44 19
6+50					34.69 3.86 17	34.28 4.27 17	34.69 3.86	34.18 4.37 19.2	34.60 3.95 19.2
5+84.73	= P L Line				33.49 5.06 16.9	33.08 5.47 16.9	33.63 4.92	33.17 5.38 19.3	33.59 4.96 19.3
5+56.13	= N L Dwight From N				32.87 5.68 16.9=Cb	32.93 6.12 16.9=Gut	33.14 5.41	32.65 5.90 19.3=Gut	33.13 5.42 19.3=Cb

338.55

338.55

Sta.					Lt	Lt	℄	Rt	Rt
10+0					40.30 5.82 17.7	39.86 6.26 17.7	40.42 5.70	39.77 6.35 18.4	40.16 5.96 18.4
9+50					39.51 6.61 17.7	39.19 6.93 17.7	39.52 6.60	38.90 7.22 18.5	39.24 6.88 18.5
9+0						38.29 7.83 17.5 = Driv	38.70 7.42	38.25 7.87 18.6 = Drive	
TP.	8.39	346.12 ✓	0.82	337.73			346.12		
8+50					37.80 0.75 17.4	37.58 0.97 17.4	37.93 0.62	37.39 1.16 18.8	37.79 0.76 18.8
8+0					36.98 1.57 17.3	36.58 1.97 17.3	37.02 1.53	36.55 2.00 18.8	36.92 1.63 18.8
7+34.73 = W.L. Roselawn					36.85 2.70 17.2 = Cb	35.44 3.11 17.2 = Gut	35.98 2.57	35.49 3.06 18.8 = Gutter	35.85 2.70 18.8 = Cb
		338.55					338.55		

Euclid Ave

Station	Lt	Lt	℄	Rt	Rt
G				342.48 3.64 = Gut	42.95 3.17 = Cb
F				42.29 3.83 = Gut	42.78 3.34 = Cb
E				41.14 4.98 = Gut	41.92 4.20 = Cb
10+72.56 - B.C. on Rt	17.8	41.10 5.08 17.8 to Drw	41.64 4.48	40.90 5.22 18.2	41.39 4.73 18.2
10+50	341.14 4.98 17.8 = Cb	40.77 5.35 17.8 = Gutter	41.22 4.90	40.52 5.60 18.3 = Gut	40.88 5.24 18.3 = Cb

346.12

346.12

12+48.66 = N L Landis				
12+36.66 = N Cb L Landis				
TP	4.92	348.28	2.76	348.36
11+96.71 = S Cb Line Landis				
11+84.71 = S L Landis				
11+58.5 = Cb F.C. on Rt				
11+0				
	346.12			

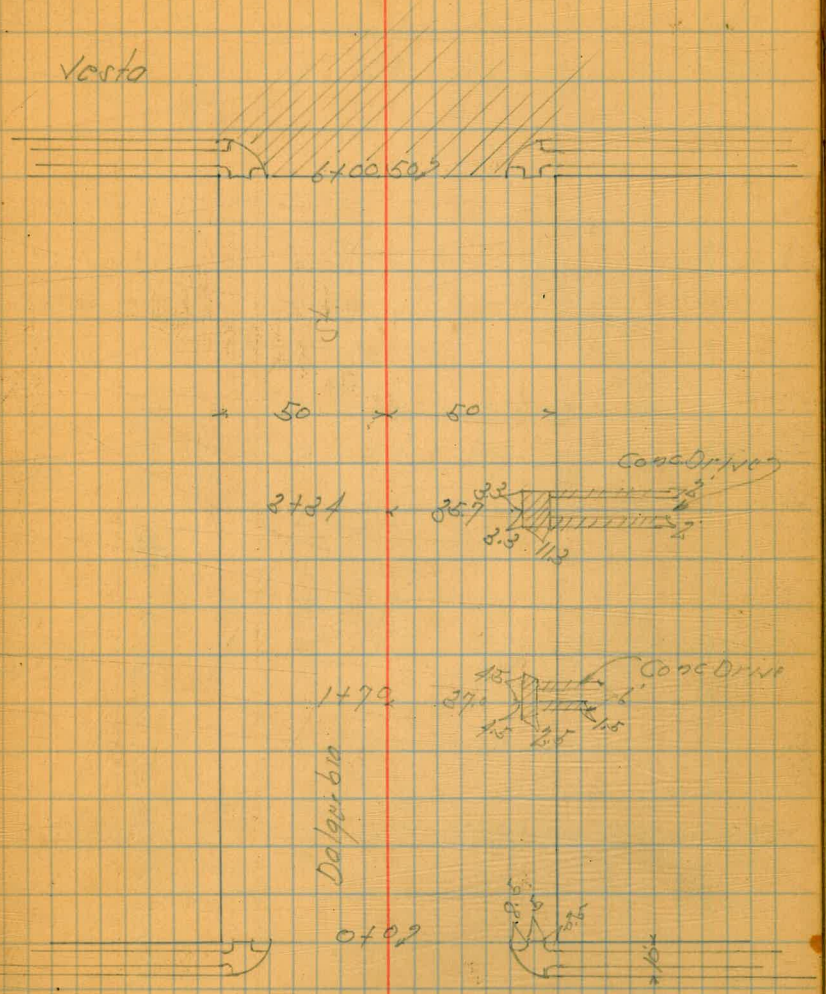
Lt		Z	Rt	
44.22 / 4.06 / 18	43.76 / 4.52 / 18	43.98 / 4.30	43.32 / 4.96 / 18.2	43.82 / 4.46
44.29 / 3.99 / 30=NCb Return	43.98 / 4.30 / 30=Gut	348.28		
43.57 / 2.62 / 30=NCb Return	43.12 / 3.00 / 30=Gut			
43.42 / 2.70 / 18.1	43.01 / 3.11 / 18.1	43.48 / 2.64	42.97 / 3.15 / 18.1	43.31 / 2.81 / 18.1
42.98 / 3.14 / 18.0	42.66 / 3.46 / 18.0	43.05 / 3.07	42.62 / 3.50 / 18.1=Gutt	43.02 / 3.10 / 18.1=Cb
42.08 / 4.04 / 17.8=Cb	41.74 / 4.38 / 17.8=Gut	42.22 / 3.90	41.43 / 4.69 / 18.2=on Parking	

346.12

Cross Section Dalbergia
Dna to Vesta

Nov 22-41
Sisson
Northam
W Moore

76



B.M.			7.43	340.70	N.W. B.P. University of Texas 340.68
TP	4.05	343.13	5.80	339.08	
TP	5.95	344.88	9.85	338.93	
		548.28			

Cross Section Dalbergia St.
Uno St. to Vesta

Indexed
LM

Sketch Page 76

1+0					
0+68					
0+50					
0+05'					
0+0 = F.L. Uno St.					
0-10 = F.Cb. Uno St.					
BM	9.53	22.99	13.46	S.E.B.P. Mono St. + Uno St.	

Notes Reduced. 11.27.41. [illegible]

Lt. = N.E. ℄ Rt. = S.W.

1+0:
20.0 / 3.0 / 50 — 19.7 / 3.3 / 34 — 19.6 / 3.4 / 17 — 19.6 / 3.4 (℄) — 18.9 / 4.1 / 17 — 18.5 / 4.5 / 35 — 18.7 / 4.3 / 40 — 18.8 / 4.2 / 50

0+68:
19.11 / 3.88 / 4.92 = 23.4 / 18.0 / Conc.

0+50:
19.6 / 3.4 / 50 — 19.6 / 3.4 / 34 — 19.3 / 3.7 / 30 — 19.3 / 3.7 / 17 — 19.3 / 3.7 (℄) — 18.8 / 4.2 / 17 — 18.4 / 4.6 / 34 — 18.8 / 4.2 / 40 — 18.8 / 4.2 / 50

0+05':
19.9 / 3.1 / 50 — 19.9 / 3.1 / 36 — 18.8 / 4.2 / 34 — 18.2 / 4.8 / 28 — 18.2 / 4.8 / 17 — 18.2 / 4.8 (℄) — 17.8 / 5.2 / 17 — 17.5 / 5.5 / 32 — 18.2 / 4.8 / 34 — 18.6 / 4.4 / 40 — 18.3 / 4.7 / 50

0+0:
19.4 / 3.6 / 50 — 18.89 / 4.10 / 34 = Cb End — 18.3 / 4.7 / 34 = Gutter — 18.2 / 4.8 / 17 — 18.1 / 4.9 (℄) — 17.8 / 5.2 / 17 — 17.4 / 5.6 / 34 = Gutter — 17.99 / 5.00 / 34 = Cb End — 18.3 / 4.7 / 50

0-10:
18.98 / 4.01 / 50 = Cb — 18.3 / 4.7 / 50 = Gutter — 18.97 / 4.02 / 44 = Cb BC — 18.3 / 4.7 / 34 — 18.2 / 4.8 / 17 — 18.0 / 5.0 (℄) — 17.8 / 5.2 / 17 — 17.4 / 5.6 / 34 — 18.05 / 4.94 / 44 = Cb BC — 17.0 / 6.0 / 50 = Gutter — 18.05 / 4.94 / 50 = Cb

N 22.99 S

Dalbergia

TP	2.48	21.24	4.23	18.76
3+0				
2+50				
2+0				
1+86				
1+70				
1+50				
		22.99		

LH | L | RH

78

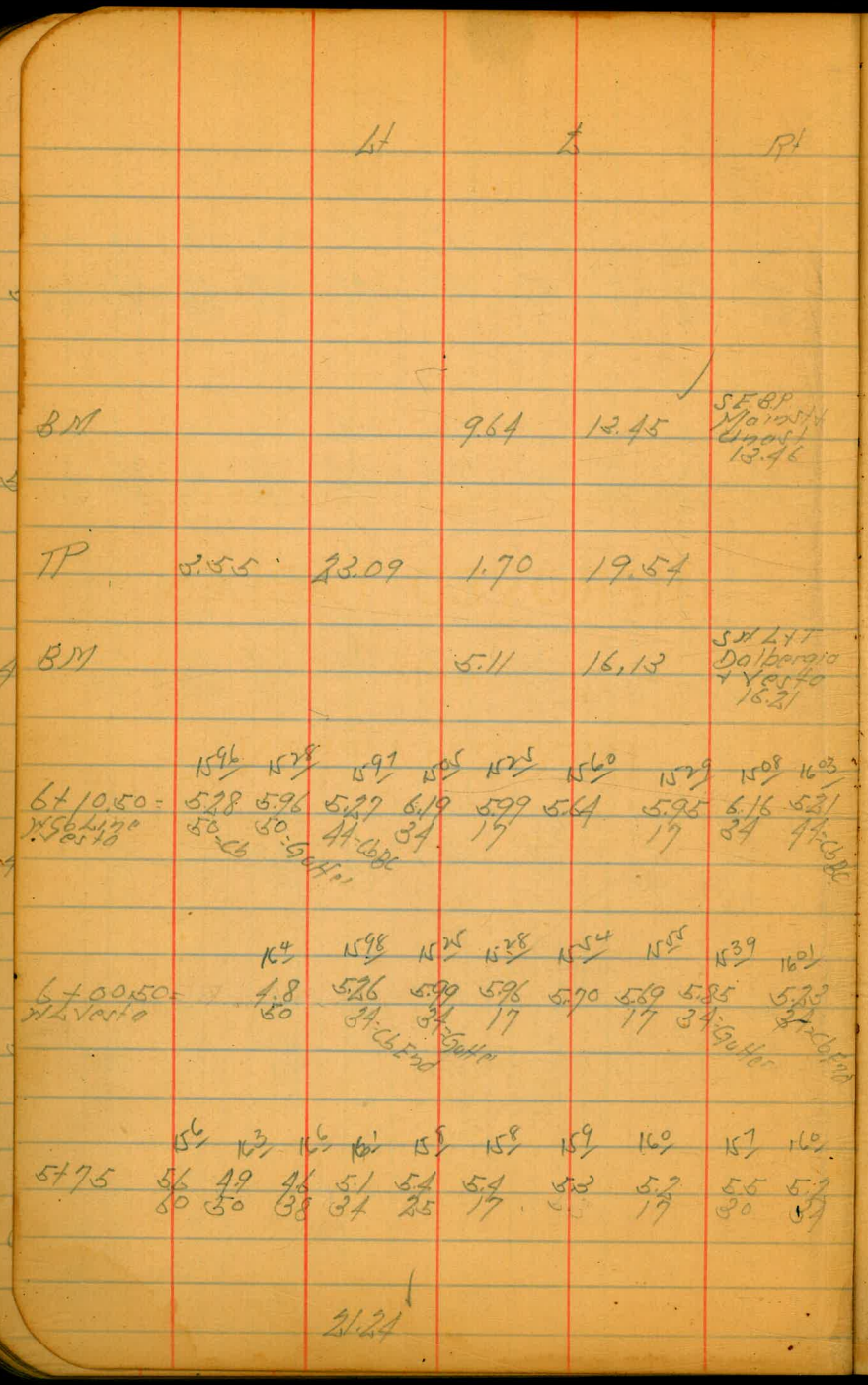
193/ 3.7 50	194/ 3.6 38	188/ 4.2 34	190/ 4.0 17	190/ 4.0	184/ 4.6 17	181/ 4.9 34	185/ 4.5 38	187/ 4.3 50
199 3.1 50	200/ 3.0 40	193/ 3.7 34	193/ 3.7 17	195/ 3.5	189/ 4.1 17	184/ 4.6 34	197/ 3.8 37	191/ 3.9 50
201/ 3.9 50	201/ 3.8 38	195/ 3.6 34	195/ 3.5 17	195/ 3.5	189/ 4.1 17	186/ 4.4 34	190/ 4.0 38	197/ 3.8 50
					1933/ 3.76 37		1977/ 3.76 50	
					1880/ 4.19 37	1904/ 3.93 34		1919/ 3.89 50
203/ 3.7 50	201/ 3.8 38	195/ 3.6 34	196/ 3.4 17	194/ 3.6	189/ 4.1 17	187/ 4.3 34	1890/ 4.09 37	1904/ 3.95 50
				22.99				

Dalbergia

			Lt.				℄		Rt.				
5+50	15^{2} / 6.0 / 60	15^{8} / 5.4 / 50	16^{4} / 4.8 / 45	16^{5} / 4.7 / 38	16^{2} / 5.0 / 34	16^{0} / 5.2 / 26	16^{0} / 5.2 / 17	16^{4} / 4.8	16^{4} / 4.8 / 17	16^{0} / 5.2 / 30	16^{3} / 4.9 / 34	17^{0} / 4.2 / 38	17^{2} / 4.0 / 50
5+0	14^{8} / 6.4 / 60	15^{9} / 5.3 / 50	16^{7} / 4.5 / 45	16^{9} / 4.3 / 37	16^{5} / 4.7 / 34	16^{4} / 4.8 / 27	16^{6} / 4.6 / 17	16^{9} / 4.3	16^{9} / 4.3 / 17	16^{5} / 4.7 / 30	17^{1} / 4.1 / 34	17^{5} / 3.5 / 37	18^{0} / 3.2 / 50
4+50	15^{4} / 5.8 / 60	16^{8} / 4.4 / 50	17^{4} / 3.8 / 45	17^{7} / 3.5 / 37	17^{2} / 4.0 / 34		17^{3} / 3.9 / 17	17^{6} / 3.6	17^{4} / 3.8 / 17		17^{0} / 4.2 / 34	18^{1} / 3.1 / 38	18^{6} / 2.6 / 50
4+0		16^{4} / 4.8 / 60	18^{0} / 3.2 / 50	18^{1} / 3.1 / 40	17^{8} / 3.4 / 34		18^{0} / 3.2 / 17	18^{2} / 3.0	17^{9} / 3.3 / 17		17^{5} / 3.7 / 34	18^{2} / 3.0 / 40	18^{3} / 2.9 / 50
3+50		18^{3} / 2.9 / 60	18^{1} / 3.1 / 50	18^{7} / 2.5 / 48	18^{7} / 2.5 / 38	18^{3} / 2.9 / 34	18^{6} / 2.6 / 17	18^{6} / 2.6	18^{1} / 3.1 / 17		17^{9} / 3.3 / 34	18^{4} / 2.8 / 40	18^{4} / 2.8 / 50
3+34										18^{16} / 2.08 / 35½ ℄ [illegible] Conc Drive	18^{46} / 2.78 / 47 to Drive		18^{50} / 2.74 / 50 to Drive

2124 ✓

21.24



IMPROVED TABLES

AND

INFORMATION