

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

1565

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.
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Made in U. S. A.

		305.58			
☐	{Temp. Pav pav	S. End N. End			
			3.86	301.72	
W	"	"	3.69	301.59	
W.	ch.	"	3.56	302.02	
0+10 N.					
W-2.			10.2	306.00	
W			1.0	304.6	
+1.0			1.6	304.0	
+2.0	W. Temp. pav		1.2	304.4	
☐			1.2	304.4	
+3	E. Temp. pav		1.2	304.4	
+6			0.9	303.7	
E			+1.2	306.8	yard
T.P.	-12.37	317.67	0.28	305.30	

0+25					
E			10.8	306.9	
+4	E. Temp. pav		11.4	306.3	
☐			11.2	306.5	
5.5	W. Temp. pav		11.2	306.5	
6.5			11.6	306.1	
W					

		317.67			
				(walk ?)	
		0+41.5	S. End. conc.	parch.?	on W. Line 2
W		9.9	307.8	ground	
W		8.81	308.86	Top. parch	
0+50					
W		9.5	308.2		
+2	W. Temp. pav	9.4	308.3		
☐		9.3	308.4		
+3	E. Temp. pav	9.5	308.2		
E		9.3	308.4		
0+64 S. End. 18" conc. gutter on W.					
6.5	w of ☐	8.85	308.82		
		Fence N. End. 0.1 in Alley			
		on W. Line			
0+67 N. End. above conc. walk.					
W	on conc	8.80	308.87		
0+82 ^E garage on W. conc. floor					
W-7.7	floor	8.6	309.7		
W		7.9	309.8		
0.25	E. of W ☐ gutter	8.20	309.47		
+2	W. Temp. pav	7.8	309.9		
☐		7.6	310.1		
+2	E. Temp. pav	7.6	310.1		
E		8.0	309.7		
+5		8.2	309.5		

317.67

0+93 N. End. above conc. gutter

W. line = ϕ gutter 7.83 309.84 Not for yardage

0+97 N. End. Temp. pav

E-5 6.8 310.9

E 6.8 310.9

+5 E. Temp. pav 6.9 310.8

 ϕ 6.7 311.0

+5.5 W Temp. pav 6.9 310.8

W 7.0 310.7

+5 7.2

S. End garage on W conc floor 7.7 Back
1+00 " " " " E " " 5.7 "

-7.7 5.98 311.69

W 6.5 311.2

 ϕ 6.7 311.0

+5 6.7 311.0

+7.4 W. End. conc apron 6.06 311.61

E 6.03 311.64

+2.6 5.35 312.32

+5.7 = floor 5.34 312.33

1+11 = N. End. above garage on W.

W-7.7 = Floor 5.98 311.69

317.67

1+16.5 = N. End above garage on E.

3

E-5.7 = floor 5.30 312.47

E-2.6 W. end conc. apron. 5.33 312.34

E. 5.66 312.01

 ϕ 5.8 311.9

W 5.6 312.1

+3 5.8 311.9

TP, 8.50 324.32 1.85 315.82

1+50

W 9.9 314.4

 ϕ 10.4 313.9

E 10.1 314.2

1+74 = { N. End. N. Entrance garage on E. conc. floor 0.2 Back.
S. " garage on E. conc. floor 8.7 " }

E-8.7 = floor 8.70 315.62

E-0.7 = W. side Door 8.86 315.46

1+87 garage on W. dirt floor 2.3 Back

W-2.3 floor 8.1 316.2

2+00

E 7.9 316.4

 ϕ 7.8 316.5

W Fence on line 7.8 316.5

324.32

2+27 \pm 24' conc. walk on W. Line

W = E. End. walk	6.98	317.44	
2+35 } S. End. garage on w. conc. floor			7.3 Back
" " " " E " "			8.0 "

W-73 = floor 6.47 317.85

W. on conc. apron + ground 6.50 317.82

W+1.0 = E. Edge conc. apron 6.70 317.62

 ϕ 6.5 317.8

E 6.6 317.7

+8. = floor 6.50 317.82

2+46 N. End above garages.

E-8 = floor 6.44 317.88

E 6.4 317.9

 ϕ 6.3 318.0

+ 6.2 = E. edge conc. apron 6.60 317.7

W. ground. " " 6.45 317.87

W+7.3 = floor 6.47 317.85

2+47 S. End. Fence on W. 0.7 in Alley

2+52 " " " " E 0.2 " "

2+67

 ϕ Top. M.H 5.72 318.60

2+76 N. End. above fence on W 1.1 in Alley

324.32

2+87 garage on W dirt floor 8.5 Back 4

W-85 5.5 318.8

2+96 S. End. Fence on W. 0.3 in alley

3+00	{ N. End above fence on E 0.4 in Alley.
	{ S. " cobbles + conc. wall on E. 0.7 in Alley

W 5.1 319.2

+1 4.9 319.4

 ϕ 4.8 319.5

+ 6.8 ground. 4.4 319.9

+ 6.8 Top. wall 2.5 321.8

3+16 Fence on W. 0.6 in Alley

3+19 = N. End. above wall on E. 0.7 in Alley

6.8 E. of ϕ = Top. wall 2.5 321.8

3+25

E 4.2 320.1

 ϕ 4.3 320.6

+ 7.0 = Fence 4.4 319.9

W 4.4 319.9

3+33 7' E. of ϕ = W. side Pepper Tree 14" Diam

3+40 garage on E. dirt floor 3.3 Back

E-3.3 = floor 3.9 320.4

3+49	{ N. End. Fence on W. line
	{ S. " " " " 0.7 in alley

324.32

3+55 N. End. above Fence on W. 6.7' in Alley
 S. End garage on E. 5.3 Back
 3+56 S. End double garage on W. conc. floor 5.3 Back

W-5.3 3.57 320.95

W 3.63 320.69

+ 0.7 = E. Edge conc. apron 3.65 320.67

⊕ 3.8 320.5

E 3.8 320.5

+ 5.3 floor 3.7 320.6

3+78 N. End. above garage on E

W-5.3 = floor 3.52 320.80

0.7 E. of W. = E. edge conc. apron 3.60 320.22

3+80 ⊕ double garage on E. conc. floor 7.2 Back

E-7.2 = floor 3.40 320.92

3+93 Fence on W. line

3+95. " " " 0.8 in Alley

3+99 S. End. Fence on W. 0.5 in Alley.
 conc. curb. on W. 0.3 in Alley

4+00

E 3.2 321.1

⊕ 3.3 321.0

+ 7.2 3.3 321.0

W on Top, etc. 3.0 321.3

T.P. 6.18 327.90 2.60 321.72

327.90

4+39 garage on E conc. floor 10.7 Back ⁵

E-10.7 = floor 5.97 321.93

E-6.7 = W. edge conc. apron. 6.07 321.83

4+49 N. End Fence & conc. db. on W. 0.3' in Alley

W. on Top. conc. Wall 5.92 321.98

+ 0.3 6.0 321.90

⊕ 6.1 321.80

E. 6.0 321.90

4+55 garage on W. dirt floor 5.7 Back

W-5.7 = floor 6.0 321.90

4+76 S. End Board & Bat. House 1.3' in Alley. on W.

4+86 garage on E. conc. floor 1.9' Back.

E-1.9 = floor 5.18 322.72

4+90 ³ N. End. above House on W. 1.3' in Alley.
₅₊₀₀

E 5.0 322.9

⊕ 5.1 322.8

W 5.2 322.7

5+15 garage on W dirt floor 5.3 Back

W-5.3 = floor 5.2 322.7

5+28 S. End. Fence on W. 2.3' in Alley

5+32 " " conc. apron on E. 0.4 Back

E-0.4 = conc apron 4.88 323.02

327.90

5+48 N. End garage on E. conc. floor 5.2 Back.

E-5.2 = floor 4.77 323.13

E-0.4 = w. edge conc. apron 4.85 323.05

5+50

W 5.0 322.9

+2.3 = Fence 5.0 322.9

E 5.1 322.8

+6 5.0 322.9

E 4.8 323.1

5+85

E 4.3 323.6

+1.5 5.0 322.7

E 5.2 322.7

+4 5.1 322.8

+5.2 = Fence 4.2 323.7

W 4.2 323.7

5+97

W 4.5 323.4

+1.7 = fence 4.5 323.4

+4 5.7 322.2

E 5.9 322.0

327.90

+4 5.6 322.3

E 4.6 323.3

5+98.24 = S. Line - Thorn St

E of S. End ch + ground 5.45 322.45

E 6.0 321.9

+7.3 S. End ch + ground 5.89 322.01

5+99.0 = S. End. asphalt pav

7.3 W. of E pav. S. End. 6.00 321.90

E " " " 6.02 321.88

E " " " 5.67 322.23

10' N. of S. Line = S. ch

E. conc ch 5.77 322.13

E. pav. 6.46 321.44

E " " 6.52 321.28

W " " 6.64 321.22

W cov. ch 6.00 321.90

T.P. 3.16 325.24 5.78 322.12

chk B.M. BP 6.10 319.18 = 318.98 + Thorn. N.W. 31st

T.P. 2.54 324.22 3.60 321.68

T.P. 0.15 311.54 12.83 311.39

orig B.M. 9.49 302.05 = 302.06

3-1-39 Re X. Sec. Alley Bk. 20. Univ. Hts.

Miller
Walker
Bliss

Sec F. B. 1442 - P. 67

S. E. Madison
+ Mississippi

B.M.	8.04	348.10	340.06
	0+00 = N. Line Madison		
	0+03		
W		6.0	342.1
+5		6.7	341.4
⊕		6.6	341.5
+5		6.1	342.0
E		4.8	343.3
	0+15		
E		4.6	343.5
⊕		5.0	343.1
+7		5.4	342.2
W		4.7	343.2
	0+50		
W		4.0	344.1
⊕		4.0	344.1
E		3.9	344.2
	0+85 New garage on E. conc. floor 2.2 Back		
E-2.2 = floor		3.00	345.1
	0+92 S. End. Fence on W. 0.4 in alley		

348.10

old.

0+93 garage on E. New conc floor

E-2.2 = floor		2.90	345.2
	1+00		
E		3.0	345.1
⊕		3.2	344.9
W		3.1	345.0
	1+13 N. End above Fence on W. 0.5 in Alley		
	1+29 S. End. Fence on W. 0.3 in Alley		
	1+30 garage on E. gone		
T.P.	8.67	354.37	2.40 345.70
New 1+47 ⊕ double garage on E conc. sill			6.4 Back
E-6.4 = floor		8.07	346.30
	1+50		
W		8.5	345.9
⊕		8.6	345.8
E		8.6	345.8
	1+56 N. End. above Fence on W. 0.3 in Alley		
New 1+60 garage on E. dirt. floor			6.4 Back
E-6.4 = floor		8.2	346.2
New 1+68 S. End. Fence on W. 0.8 in Alley			
	1+87		
E		7.8	346.6
⊕		7.6	346.8
+9.4 = Fence		7.5	346.9

354.37
2+09

W 6.9 347.5

⊕ 7.0 342.4

E 7.3 342.1

New 219 = N. End above Fence on W 0.8' in Alley

2+55

E 6.5 347.9

⊕ 6.4 348.0

W 6.3 348.1

3+03

W 5.46 348.91

+08 5.46 348.91

+2 5.0 349.4

⊕ 5.3 349.1

E 5.4 349.0

3+50

E 5.0 349.4

⊕ 4.6 349.8

W 4.5 349.9

4+00

W 3.9 350.8

⊕ 4.0 350.4

E 4.2 350.2

354.37

4+50

E 3.4 351

⊕ 3.4 351.0

W 3.3 351.1

4+77 S. End. Loose gravel surfacing.

W 2.6 351.8

⊕ on gravel 2.6 351.8

E 2.6 351.8

5+44

E 2.7 351.7

⊕ 2.5 351.9

W 2.8 351.5

5+85

W 2.1 352.3

⊕ 2.4 352.0

E 2.5 351.9

5+95

E 2.6 351.8

⊕ 2.7 351.2

W 2.3 351.1

5+99.5

E. ch. for ch K. 2.64 351.73v

83.82

1/2	Par.	11.10	72.72
c	"	10.81	73.01
1/2	"	10.58	73.24
cb	"	10.39	73.43
+ 16.8	gvt	9.95	73.87
"	" TOP cb	9.18	74.64
0+00 = only Willow			
N		8.5	75.3
+10	TOP END Corb	9.70	74.1
"	gvt	10.39	73.43
cb	Par	10.34	73.48
1/4	"	10.41	73.41
c	"	10.53	73.29
1/4	"	10.92	72.90
cb	"	11.33	72.49
+8	gvt	12.03	71.79
"	TOP cb end	11.24	72.58
S		12.7	71.6
0+04			
-5		13.5	70.3
S		12.8	71.0

83.82

+10		11.1	72.7	10
cb		10.9	72.9	
1/2		10.7	73.1	
c		10.5	73.3	
1/2		7.7	76.1	
cb		5.6	78.2	
N		2.6	81.2	
0+25				
N		2.4	81.4	
cb		5.6	78.2	
1/4		7.6	76.2	
c		9.9	73.9	
1/4		9.4	74.2	
cb		9.9	73.9	
S		14.9	68.9	
+10		15.8	68.0	
0+50				
-10		15.2	68.6	
S		14.6	69.2	
+15		11.3	72.5	
cb		9.9	73.9	
+4		9.4	73.4	
1/4		9.4	73.4	
c		9.6	73.2	

83.82

1/4	6.1	77.7
cb	4.8	79.0
N	1.5	82.3
0+75		
N	1.8	82.0
cb	5.3	78.5
1/4	6.6	77.2
c	8.8	75.0
1/4	8.1	75.7
+4	8.1	75.7
cb	9.7	74.1
S beg. on CONC. WALK	13.42	70.40
0+96		
S end on CONC "	13.12	70.70
1+00		
-10	12.2	71.6
S	12.2	71.6
cb	9.2	74.6
1/4	7.9	75.9
c	8.5	75.3
1/4	6.7	77.1

83.84

cb	5.5	78.3	11
N	3.0	80.8	
1+09. Wedge of CEMENT WALK			
N - 5.5	+ 0.40	84.2	
N - 9.5	+ 0.40	84.2	gar. dirt
1+35			
N	2.2	81.4	
cb	5.3	78.5	
1/4	6.1	77.7	
c	7.8	76.0	
1/4	7.0	76.2	
+4	7.4	76.2	
cb	9.2	74.6	
S	11.0	72.8	
+10	11.2	72.6	
1+85			
- 0.7	8 gar. cent.	8.65	75.17
S		8.65	75.17
+ 7.2	end CONC. APRON	8.70	75.12
cb		8.1	75.7
1/4		7.8	76.5

8387

c		7.1	76.7
1/2		6.8	77.0
cb		6.4	77.6
N		4.7	79.1
+20		0.0	83.8
	2+100		
-20		1.0	82.8
N		4.8	79.0
cb		5.5	78.3
1/2		5.6	78.2
c		4.5	79.3
1/4		5.4	78.4
cb		5.8	78.0
S		5.5	78.3
+10		6.0	77.8
T.P.	12.87 95.58	10.6	82.76
	2+30		
-10		13.1	82.5
S		12.8	82.8

95.58

12

+3		11.0	84.6
cb		10.2	85.4
1/2		9.0	86.6
c		8.3	87.3
1/4		8.4	87.2
cb		9.1	86.5
+5		8.7	86.9
N		14.4	81.2
+20		14.3	81.3
+40		10.4	85.2
	2+50		
-50		8.7	86.9
-25		12.5	83.1
-10		13.5	82.1
N		12.2	83.4
+13		7.7	87.9
cb		7.5	88.1
1/2		6.4	89.2
c		5.6	90.0
1/4		5.8	89.8
cb		5.7	89.9

95.58

+15	7.4	88.0
+16	12.5	83.1
S	12.5	83.1
+10	12.5	83.1
2+50.4		
-10	8.8	86.8
S	8.7	86.9
+0.5	12.5	83.1
+2	12.5	83.1
+3	7.6	88.0

T.P. 12.75 107.83 0.50 95.08

2+95

S cb	10.0	97.8
+9	10.4	97.4
+17	12.9	94.9
S	20.7	87.1
+10	20.7	87.1

3+00 Ely Plum St.

-10	12.5	93.3
-----	------	------

107.83

S	13.5	94.3	13
+3	10.9	96.9	
cb	9.3	98.5	
1/4	9.1	98.7	
C	9.0	98.8	
1/4	8.5	99.3	
cb	8.4	99.4	
+3	8.3	99.5	
+12	12.5	95.3	
N	14.1	93.7	
+29	22.0	85.8	
+55	20.4	85.2	
+70	17.5	90.3	

check to B.M. 15.45 92.38 92.38

Roberts

XSEC Bangor St. 60' wide
 10' cbs
 10' 1/25
 Jennings to Talbot

				Harbor View Marriner
NE. 6d. Hug	12.94	204.13		191.19
T.P.	12.94	216.80	0.27	203.86
T.P.	12.99	229.49	0.30	216.50
T.P.	12.68	241.97	0.20	229.29
T.P.	12.89	254.77	0.09	241.88
T.P. C.T.	12.21	266.92	0.04	254.71
T.P.	9.86	275.73	1.05	265.87

0+100 Pueblo Line

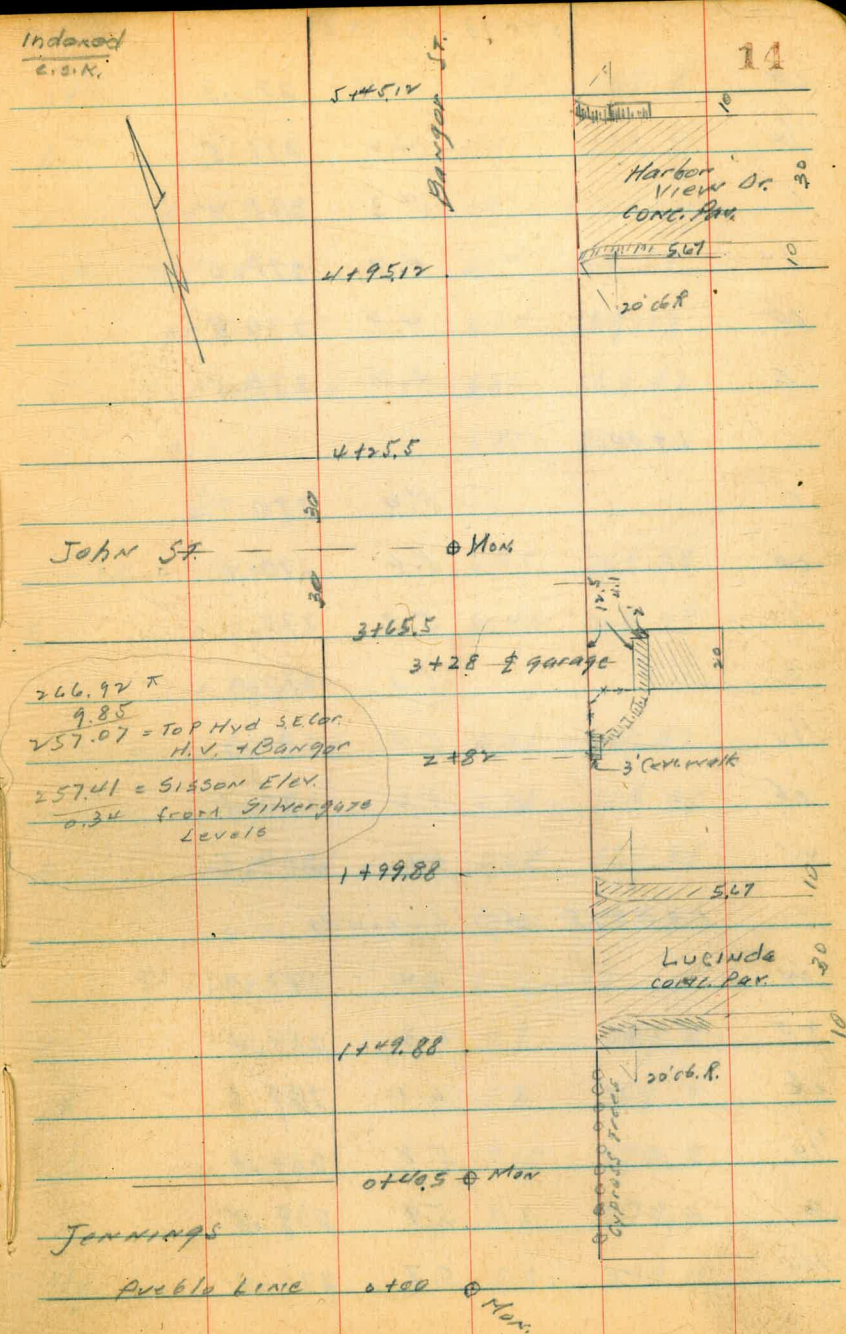
E	4.3	271.4
cb	5.0	270.7
1/4	4.6	271.1
c	4.3	271.4
1/4	3.6	272.1
cb	3.4	272.3
W	3.5	272.2

0+40.50 Nly Jennings to West

W	4.0	271.7
---	-----	-------

Moore
4-5-39

Indoned
C.S.K.



	275.23		
cb		4.4	271.3
1/4		4.2	271.5
c		4.3	271.4
1/4		4.7	271.0
cb		4.9	270.8
E		4.2	271.5
	1+00		
E		5.0	270.7
cb		5.6	270.1
1/4		5.5	270.2
c		5.3	270.4
1/4		5.4	270.3
cb		5.6	270.1
w		6.1	269.6
	1+49.88 Sly Lucinda		
w		4.4	271.3
+5		6.3	269.4
cb		6.1	269.6
1/4		5.8	269.9
c		5.9	269.8
1/4		5.7	270.0

	275.73		15
cb		5.9	269.8
E		5.5	270.2
	1+59.88	5	cb line
E-10	TOP cb	6.4	269.59
"	gut	6.60	269.13
E	TOP cb end	6.31	269.42
"	gut	6.81	268.92
	±		
E-10	Pay	6.35	269.38
E	end "	6.46	269.27
	1+89.88		
E-10	TOP cb	6.31	269.42
"	" gut	6.78	268.95
E	TOP cb end	6.68	269.65
E	gut	7.12	268.61
	1+99.88 Nly Lucinda		
E		5.9	269.8
cb		5.8	269.9
1/4		5.5	270.2
c		5.1	270.6
1/4		5.3	270.4

275.73

cb 6.1 269.6

W 6.3 269.4

2+50

W 6.8 268.9

cb 6.4 269.3

1/4 6.4 269.3

c 5.6 270.1

1/4 5.7 270.0

cb 5.4 270.1

E 5.8 269.9

2+82

E - 0.7 ^{cem.} Wedge walk 6.40 269.33

cb 6.50 269.23

1/4 6.4 269.5

c 6.0 269.7

1/4 6.9 268.8

cb 7.6 268.1

W 7.9 267.8

3+28

W 8.8 266.9

cb 8.7 267.0

275.73

1/4 8.5 267.2 16

c 8.0 267.7

1/4 7.8 267.9

cb 8.1 267.6

E 8.1 267.6

+12.5 E edge ^{cem.} apron 7.67 268.06

+16.6 " 90° corr. 7.53 268.20 floor level

3+65.5 Sly John ST. to West

E 9.7 266.0

cb 9.4 266.1

1/4 9.7 266.0

c 9.8 265.9

1/4 10.1 265.6

cb 10.1 265.6

W 10.1 265.6

+50 10.7 265.0

+100 13.3 262.4

3+95.5 E John ST

W 11.4 264.3

cb 11.7 264.6

1/4 11.1 264.6

275.73

c	11.7	264.5
1/4	11.1	264.6
cb	11.4	264.5
E	10.9	264.8

4+25.50 Nly John St.

E	12.8	262.9
cb	12.8	262.9
1/4	12.4	263.1
c	12.5	263.2
1/4	12.4	263.3
cb	12.6	263.1
W	12.7	263.0
+50	13.3	262.4
+100	15.1	260.6

4+50

W	13.5	262.2
cb	13.0	262.7
1/4	12.9	262.8
c	13.4	262.4
1/4	13.9	261.6
cb	14.0	261.7

275.73

E	13.8	261.9	17
---	------	-------	----

T.P.	0.1	263.42	12.42	263.31
------	-----	--------	-------	--------

4+95.12 Sly Harbor View Dr.

E	4.3	259.1
cb	5.4	258.0
1/4	4.8	258.6
c	4.4	259.0
1/4	3.9	259.5
cb	3.8	259.6
W	3.7	259.7

5+05.12 S cb LIND

c	5.1	258.3
1/4	5.7	257.7
cb	6.9	256.5
E TOP end curb	8.30	255.12
" gut.	8.78	254.64
+10 TOP cb	8.75	254.67
" gut.	9.22	254.20

263.42

E Harbor View

-10	Pav.	9.39	254.03
E	" edge	8.90	254.52
cb		7.6	255.8
1/2		6.5	256.9
c		6.2	257.2

5+35.12 N cb

c		7.4	256.0
1/2		7.9	255.5
cb		8.9	254.5
E	TOP END cb	9.46	253.96
E	QUT	9.93	253.49
+10	cb	9.75	253.67
+10	QUT	10.27	253.15

5+45.72 N 1/4 H. V. Dr.

E		9.3	254.1
cb		9.1	254.3
1/2		8.3	255.1
c		8.2	255.2
+3		7.7	255.7
1/4		5.8	257.6

263.42

cb		8.5	254.9	13
----	--	-----	-------	----

W		8.6	254.8
---	--	-----	-------

5+55

W		10.4	253.0
---	--	------	-------

cb		10.7	252.7
----	--	------	-------

1/2		9.0	254.4
-----	--	-----	-------

+3		7.0	256.4
----	--	-----	-------

c		9.0	254.4
---	--	-----	-------

1/4		9.7	253.7
-----	--	-----	-------

cb		9.6	253.8
----	--	-----	-------

E		10.6	252.8
---	--	------	-------

5+75

-10		15.8	247.6
-----	--	------	-------

E		14.5	248.9
---	--	------	-------

cb		10.2	253.2
----	--	------	-------

1/2		10.6	252.8
-----	--	------	-------

c		9.7	253.7
---	--	-----	-------

+6		10.3	253.1
----	--	------	-------

1/2		12.7	250.7
-----	--	------	-------

+4		15.2	248.2
----	--	------	-------

cb		14.8	248.6
----	--	------	-------

W		14.6	248.8
---	--	------	-------

+10		14.6	248.8
-----	--	------	-------

263.42

5.785

-10	15.9	247.5
W	15.7	247.7
cb	16.2	247.2
1/4	15.6	247.8
c	15.6	247.8
1/4	16.2	247.2
cb	16.2	247.2
E	17.0	246.4
+10	17.1	246.3

T.P. 1.40 252.26 12.56 250.86

6+10

-10	7.5	244.8
E	7.1	245.2
cb	6.8	245.5
1/4	6.6	245.7
c	6.7	245.16
1/4	6.3	246.0
cb	6.3	246.0

252.26

19

W	6.1	246.2
+10	6.0	246.3
	6+40	
-10	7.7	244.6
W	7.9	244.4
cb	7.9	244.4
1/4	8.0	244.3
c	8.2	244.1
1/4	8.3	244.0
cb	8.7	243.6
E	9.3	243.0
+10	9.5	242.8

6+70

-10	10.1	242.2
E	9.7	242.6
cb	9.3	243.0
1/4	9.1	243.2
c	9.2	243.1
1/4	9.2	243.1
cb	9.4	242.9
W	9.3	243.0
+10	10.0	242.3

252.26

7700

-10	13.0	239.3
W	12.2	240.1
cb	12.0	240.3
1/4	11.6	240.7
c	11.1	241.2
1/4	11.7	240.6
cb	12.0	240.3
E	11.7	240.6
+10	11.6	240.7

T.P. 0.04 239.89 12.41 239.85

7+25

-10	3.4	236.5
E	3.0	236.9
cb	2.4	237.5
1/4	2.5	237.4
c	2.7	237.2
1/4	3.0	236.9
cb	4.6	235.3

239.89

20

W	5.7	234.2
+10	6.4	233.5
7+36		
-10	11.2	228.7
W	7.1	232.8
cb	6.2	233.7
1/4	5.1	234.8
c	4.6	235.3
1/4	4.4	235.5
cb	5.1	234.8
E	5.6	234.3
+10	5.9	234.0

7+50

-10	10.1	229.8
E	9.2	230.7
cb	10.0	229.9
1/4	9.4	230.5
c	9.6	230.3
1/4	10.6	229.3
cb	11.3	228.6
W	12.5	227.4
+15	18.0	221.9

		239.89		
T.P.	0.31	227.31	12.89	227.00
	7+75			
-15			20.2	207.1
W			17.5	209.8
06			14.7	212.6
1/4			14.2	213.1
C			14.1	213.2
1/2			14.0	213.3
06			15.0	212.3
E			15.0	212.3
+15			15.5	211.8
T.P.	0.93	215.50	12.74	214.57
T.P.	0.42	203.10	12.82	202.68
8+00 E			7.4	195.7
8+10 E			14.2	188.9
T.P.	0.79	191.19	12.70	190.40
8+21 E			8.5	182.7
T.P.	0.56	179.45	12.30	178.89
T.P.	0.82	167.39	12.88	166.57

21

		167.39		
8+65 E			5.0	162.4
T.P.	0.92	155.45	12.86	154.53
8+80 E			6.5	149.0
9+00 E			5.8	149.7
9+10.4 E Sly Talbot			12.6	142.9
9+23 E			17.8	137.7
9+36.75 Pueblo Cor.			16.3	139.2
T.P.	0.39	143.01	12.83	142.67
T.P.	0.90	130.88	13.03	129.98
T.P.	0.03	118.08	12.83	118.05
T.P.	0.12	105.45	12.75	105.33
T.P.	0.41	92.87	12.99	92.46
T.P.	0.18	80.27	12.76	80.09
T.P.	0.31	67.76	12.82	67.45
T.P.	2.20	57.12	12.84	54.92
check to NWBP	Evergreen Talbot		5.30	51.82
				51.77
				0.05

120.50

1+00

W	3.0	117.5
+27	11.2	109.3
+31	14.5	106.0
+40	14.6	105.9
+62	25.5	95.0
E	27.0	93.5
+15	27.0	93.5
+30	22.1	98.4

1+50

W	0.7	119.8
+26	9.1	111.4
+32	13.5	107.0
+40	13.0	107.5
+61	23.2	97.3
E	24.0	96.5
+6	23.8	96.7
+20	19.1	101.4

T.P.

13.03 131.49 20.4 118.46 2.95b

1+50

131.49

23

2+00

W	7.8	123.7
+26	18.0	113.5
+32	21.7	109.8
+40	22.1	109.4
+59	31.9	99.6
E	32.2	99.3
+20	26.4	105.1

2+50

W	4.4	122.1
+27	16.0	117.5
+33	17.6	113.9
+41	17.8	113.7
E	29.1	102.4
+10	28.1	103.4
+20	23.4	108.1

3+00

W	1.2	130.3
+27	10.0	121.5
+32	13.5	118.0

131.49

+41	13.8	117.7
+41	25.4	106.3
E	26.4	108.1
+8	26.0	105.5
+20	19.8	112.2

T.P. 885 139.60 0.74 130.75 ^{20th} 3+00

3+30

W	5.4	134.0
+26	14.8	124.8
+31	18.8	120.8
+40	19.1	120.5
+65	31.5	108.1
E	31.4	108.0
+5	32.0	107.4
+15	28.3	111.3

3+70.4 90°

W Mon.	3.37	136.23
+10	5.3	134.30

139.60

21

+28	9.9	129.7
+27	13.4	126.4
+40	13.4	126.2
E	28.0	111.6
+12	29.3	110.3
+25	23.8	115.8

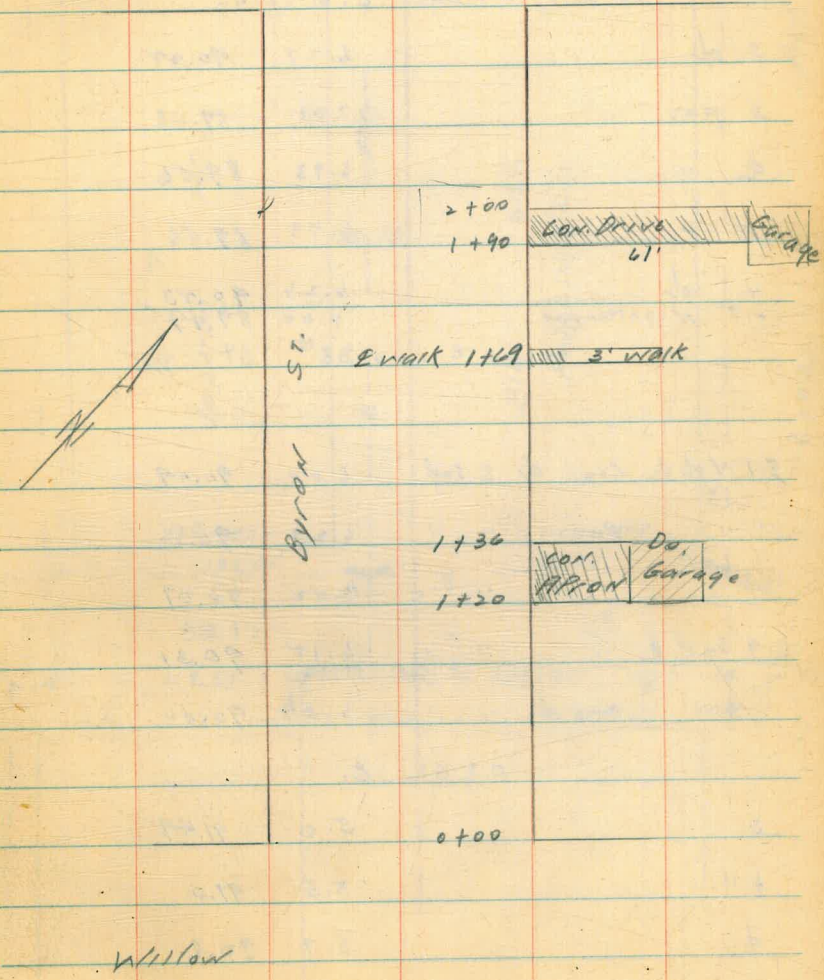
3+70.4 SEIX LINE C/OVE

W Mon.	3.37	136.23
+20	6.1	133.8
+35	8.1	131.5
+38	10.2	129.4
+48	9.8	129.8
+55	12.4	127.2
+65	15.4	124.0
E	21.0	118.6
+5	24.6	115.0
+15	24.2	115.4
+25	20.5	119.1

Garage Levels on Byron St.
betw Willow & Plum

T.P.	689	125.35	118.46	P23
	1+20			
N on apron		8.83	116.49	
+23 garage floor	636	118.96		
	1+26			
N on apron		8.71	116.61	
	1+69			
N E 3' Con. walk	306	122.26		
	1+90			
N on Con Drive	285	122.47		
+20 " " "	130	124.02		
	2+00			
N on Con Drive	273	122.49		
+20 " " "	130	124.02		

Plum



96.49 ✓

	0+35 E		
-5	3.2	93.1	
N	3.2	93.1	
+2	2.6	93.9	
⊕	3.0	93.5	
S	2.6	93.9	
+5	3.0	93.5	

0+54 garage on S. conc. floor 2.4 Back

S - 2.4 = floor	2.77	93.74	
S	2.4	93.7	
+2	2.3	94.2	
⊕	2.3	94.2	
+5	2.5	94.0	
N	3.1	93.4	
+5	3.4	93.1	

0+69 elec Pole s. side 7.02 of ⊕

0+69 w. end. shed on N. 0.1 in Alley

0+85 E " " " 0.2 " "

1+00

N-5	3.3	93.2	
N.	3.1	93.4	
+2	2.3	94.2	

96.49 ✓

⊕		2.5	94.0	27
+6		2.1	94.4	
S		2.6	93.9	
+5		2.8	93.7	
T.P.	5.52	99.96 ✓	2.05	94.44

W. End. Conc. apron
1+15 = w. Edge door to House on S.

5.8 S. of S. w. End conc. apron	5.95	94.01	
8.1 " " " " " "	6.00	93.96	
8.1 " " " floor	5.70	94.26	

1+27 E. End. Single garage on S. used as part of House on W.

5.8 S. of S. E. End. conc. apron	6.08	93.88	
8.1 " " " " " "	6.05	93.91	

W. End. Conc. Drive to Double garage on N 12.7 Back

1+30 " " " " " " " " 57.8 Back

S - 7.8 = floor	5.64	94.34	
S - 5.4 conc. apron	5.86	94.10	
S - 2	5.8	94.2	
S	5.4	94.6	
⊕	5.7	94.3	
+6	5.5	94.5	
N. 2 S. w. cor. Con apron	5.78	94.18	
N+12.7: S. End. Garage	5.70	94.26	

99.96 v

1+39 E. End. garage on S.

S - 7.9 = floor 5.54 94.47

S - 5.4 = conc. apron 5.63 94.33

1+40 W. End. double Garage on S. conc floor 7.88 Back

S - 7.8 = floor 5.30 94.66

S - 5.3. conc. apron 5.58 94.38

1+49 E. End above double garage on N.

N - 12.7 ground E. of garage 5.8 94.2

N - 12.7 = floor 5.54 94.42

N - S.E. Cor conc. apron 5.86 94.10

E. End. above double Garage on S.

1+60 garage on N. dirt floor 8.3 Back

N - 8.3 floor & ground. to E 5.8 94.2

N. 5.7 94.3

+ 1.5 5.2 94.8

± 5.2 94.8

+ 6 5.0 95.0

S 5.4 94.6

+ 5.3 conc. apron 5.41 94.55

+ 7.8 = floor + ground 5.22 94.74

+ 15 ground. E. of garage 5.6 94.4

99.96 v

1+71 W. side House on S.

23

S - 15 5.4 94.6

S - 5. Front of House 5.4 94.6

S - 2. N. edge conc. walk 5.3 94.7

S 5.3 94.7

+ 2 4.9 95.1

± 5.2 94.8

N = fence 4.9 95.1

+ 0.4 N. of Fence 5.6 94.4

+ 15. 5.6 94.4

1+76 E. side door

S - 5. ground. to E. 5.9 94.1

S - 5. floor of House 4.80 95.16

S - 2 conc. stoop. 4.87 95.09

1+95 E. End. Above House on S.

2+00

N - 30 6.4 93.6

N - 0.4 6.1 93.9

N 5.0 95.0

± 5.3 94.7

+ 5 5.1 94.9

S 5.7 94.3

+ 5. 6.1 93.9

+ 15. 6.4 93.6

99.96 ✓

1+83 Guy Wire Deadman 0.2 in Alley

1+99 Elec Co Pole S. side 0.4 out of alley

2+12 garage on S. conc. floor 3.7 Back

S-3.7 = floor 5.79 94.17

2+50

-20 6.6 93.4

S. w. End. Fence 5.8 94.2

+2.5 4.9 95.1

⊕ 4.9 95.1

N. 4.8 95.2

+0.1 = S.W. Por House. 5.2 94.8

+30 5.6 94.4

2+51

N at. House 4.8 95.2

⊕ 4.9 95.1

S. at. fence. 4.9 95.1

2+73 = E. End. above House on N. D. & Back

N. 4.6 95.4

20. N 4.9 95.1

T.P. 4.66 99.89 ✓ 4.73 95.23

2+77 walk to N.

6.5 N of ⊕ S. End. walls 4.85 95.04

99.89 ✓

29

3+00	{	Elec Pole S. Edge 6.9 S. of ⊕		
		S. End. garage on N. dirt. floor	5.5	Back.
		W. " doub " " N conc " "	7.2	Back
		W " " " S. dirt. " "	5.8	Back.

S-5.8 floor 5.6 94.3

S. ground to E 5.3 94.6

S. " " W 4.7 95.2

+2.5 " " 2+W 4.7 95.2

⊕ 4.6 95.3

+7 4.7 95.2

N 5.0 94.9

+4.4 5.08 94.81

+7.2 = door 5.06 94.83

+20. ground W of garage 5.2 94.7

3+18 = E. End. above garage. on N.

N-20 ground. E. of Garage 5.0 94.9

N-8 " " " " 5.0 94.9

N-7.2 floor 5.03 94.86

N-44 conc. Apron 5.04 94.81

99.89 ✓

3+25

N - 7.2 floor of House	3.52	96.37
N - 7.2 wooden porch	3.65	96.74
N - 3.0 concrete walk	5.22	94.67
- 2.5 " wall	5.00	94.9
N	5.0	94.9
+ 1.5	4.7	95.2
⊕	4.8	95.1
+ 5	4.7	95.2
S = Fence.	5.5	94.4
+ 0.5	5.5	94.4
+ 15.	5.8	94.1
3+50	w. End walk. } 0.5 in Alley. on S. E. End. Fence	
S - 15	6.7	93.7
- 2.8 ground.	6.2	93.7
- 2.7 } w. End } S. Edge } conc. walk	5.33	94.56
S, " "	5.33	94.56
+ 0.5 } w. End. } N. side } " "	5.33	94.56
+ 2.5	5.0	94.9
⊕	5.1	94.8
+ 6	5.0	94.9
N	5.2	94.7

99.89 ✓

30

+ 2.5 ground to N.E.	5.5	94.4
+ 2.5 conc. wall to W	5.02	94.87
+ 30. ground.	5.6	94.3

3+77

0.6 N. of S. Line } E. End } N. Edge } conc. walk	5.43	94.46
17' S. of S "	6.2	93.7

3+96 E. Edge garage on S. 0 one floor 17' Back

N - 30.	4.3	95.6
N	4.7	95.2
+ 1	4.4	95.5
⊕	4.6	95.3
+ 5	4.7	95.2
S.	5.6	94.3
+ 17. = floor	6.03	93.86
4+00 W. End. Shed on S. 0.8' in Alley		
0.8' N of S. = W. End. Shed.	4.5	95.4
1.0' " " = S. side Elec. Pole		
⊕	4.5	95.4
N. = W. End. fence	4.1	95.8
+ 1	4.8	95.1
4+07 E. End. above shed on S. 0.8' in Alley		
W " Fence " " 1.2 " "		

99.89 ✓

4+33.

N-O.4 Fence	4.0	95.9
N	4.0	95.9
⊕	4.1	95.8
+6.7 = E. End. Fence	4.1	95.8
S	4.8	95.1
+5.	5.0	94.9
4+37 W. side garage on S. conc. floor 5.8 Back		
S-5.8	4.7	95.2
S	4.8	95.1
+2.5	4.0	95.9
⊕	4.0	95.9
N.	4.4	95.5
4+47 E. side above garage		
N	3.9	96.0
⊕	3.8	96.1
+5	3.7	96.2
S	4.0	95.9
+1	4.6	95.3
+5.8 floor	4.8	95.1
S.	4.6	95.3
4+52		
1.1. N. of S. = W. End. Fence	3.5	96.4

99.89 ✓

31

E	3.9	96.0
N	3.8	96.1
+1. = Fence	3.8	96.1
4+59 = E. End. E. Entrance garage on N.		
-5 ground	4.2	95.7
N-2 = floor	4.1	95.8
N	3.8	96.1
⊕	3.8	96.1
+6.5 = fence	3.7	96.2
S	4.7	95.2
4+79 W. End. w. Entrance garage on N.		
S.	4.7	95.2
1.0' N of S. = fence	4.0	95.9
3.5' " " "	3.6	96.3
⊕	3.7	96.2
N	3.7	96.2
+2 = floor	3.8	96.1
+5 ground.	4.1	95.8
4+90 W. End. garage on S. conc. floor 2.1 Back		
N	4.0	95.9
⊕	3.9	96.0
+4	3.6	96.3
S	4.4	95.5
+0.6 apron	4.6	95.3
+2.1 floor	4.4	95.3
+5. W. of Garage	4.7	95.2

see page 32 for sec. 4+82

99.89 ✓

5+00 E. End. above garage on S.

S-21 floor	4.4	95.3
S-04 apron.	4.4	95.3
S	4.2	95.7
+2.5	4.1	95.8
⊕	4.0	95.9
N.	4.1	95.8
+15.	4.3	95.6
5+01 S. side Elee Pole 6.4 S. of ⊕	6.4	

4+82 see Page 31

N.	3.6	96.3
⊕	3.8	96.1
+3	3.6	96.3
+6.6 Fence.	4.0	95.9
S	4.5	95.4
+5	4.7	95.2

T.P. 3.47 99.47 ✓ 3.89 96.00

5+15

-15	3.9	95.8
-2	4.0	95.5
N	3.7	95.8
⊕	4.0	95.5

99.47 ✓

S 4.0 95.5 32

+3. N. edge conc. walk 3.65 95.84

5+34 W. End. double garage on S. conc. floor 13. Back

S-13. = floor 4.10 95.37

5+50 E. End. above garage on S.

S-13. = floor 4.4 95.1

S 4.9 94.6

⊕ 4.8 94.7

N. 4.6 94.9

5+57	{	Garage on N. dirt floor	5.5	Back
		" " S. " "	3.1	" "

N-5.5 = floor 5.4 94.1

N 5.4 94.1

⊕ 5.3 94.2

S 5.5 94.0

+3. = floor 6.1 93.4

5+65 garage on S. dirt floor 5.5 Back

S-5.5 floor 6.1 93.4

5+77 garage on S. dirt floor 5.5 Back

S-5.5 floor 6.2 93.3

S 6.2 93.3

⊕ 6.2 93.3

N 5.8 93.7

+3.5 S. side House. 5.8 93.7

99.47 ✓

5+85 garage on S. dirt floor 5.4 Back			
S-5.4' floor	6.8	92.7	
T.P.	2.85	95.01 ✓	7.31 92.16
6+00 = W. line 39 th St. = E. End. Garage on S. dirt floor 5.4 Back			
N-100'	0.00	95.01	
N-60	0.8	94.2	
N-20	1.3	93.7	
N	2.5	92.5	
⊕ Alley	2.8	92.2	
S	2.8	92.2	
+5.3 E. End. Garage floor	2.4	92.6	
+5.3 E. of Garage	3.1	91.9	
S+30	3.5	91.5	
S+125 = N. line Logan.	3.7	91.3	
S+139 = N. d. E. End.	3.98	91.03	
10' E = W. d.			
S-125	4.1	90.9	
S-30	4.3	90.7	
⊕ Alley	3.2	91.8	
+20 N	2.3	92.7	

95.01 ✓

33

N+60. N	1.8	93.7	
+100. N	1.4	93.6	
10' E = W. 1/4			
N+100' N	3.7	91.3	
+60' N	3.0	92.0	
+20' N	3.5	91.5	
⊕ Alley	3.7	91.3	
S+30	4.8	90.7	
S+125	5.4	89.6	
10' E = ⊕ 39 th			
S-125	5.6	89.4	
S-30	4.7	90.3	
⊕ Alley	4.1	90.9	
N+20	3.8	91.2	
+60	3.6	91.4	
+100	4.6	90.4	
T.P. C.T.	1.57	91.65 ✓	4.93 90.08
Chk. B.M. B.P.	8.60	83.05 ✓	2 Nat. Ave.

S. 7' line Logan.
3' 0" W. of W.
Line 39thS. W. 39th

8-24-39. X sec. 39th St National to Florence
 Miller (10' cls.)
 Walker (10' 14 5/8)
 Blinn

BM. BP. 8.06 91.11 83.05 S.W. 39th National

14' s of N = N.d. of National

W. db 7.13 83.98

W. g par 7.86 83.25

db " 7.75 83.36

1/4 " 7.77 83.34

± " 7.81 83.30

1/4 " 7.82 83.29

db " 7.81 83.30

E g " 7.78 83.33

E db 7.14 83.9.7

0+00 = N line National

E. N. 2. car Return 7.00 84.11

± db N. end. 7.17 83.96

G par 7.54 83.57

1/4 " " " 7.19 83.92

± " " " 7.20 83.91

1/4 " " " 7.26 83.85

G " " " 7.55 83.56

db " " " 7.19 83.92

W = N. w. car Return 6.92 84.19

Indexed
 C.S.K.

91.11

34

0+50

W 6.1 85.0

+2 6.6 84.5

db 6.6 84.5

1/4 7.0 84.1

± 6.6 84.3

1/4 6.9 84.2

+8 7.1 84.0

db 6.9 84.2

E 6.5 84.7

1+00

E 5.3 85.8

db 5.7 85.4

+2 6.5 84.6

1/4 6.1 85.0

± 5.8 85.3

1/4 5.9 85.2

+5 6.1 85.0

+6 5.1 86.0

db 5.6 85.8

+6 5.7 85.4

W. 5.0 86.1

91.11

1+40

w	4.1	86.4
el	4.6	86.5
+5	5.3	85.5
14	5.1	86.0
⊕	5.1	86.0
14	5.4	85.2
+8	5.9	85.2
dr	4.8	86.3
+6.	4.8	86.3
E	4.2	86.9

1+43 9'.8' W of C. = W. side Tel. Pole
 1+58 9.5' E of W = E " Elec. "

1+60

E	4.1	82.0
+3	4.5	86.6
d.	4.4	86.2
+2	5.4	85.2
14	5.0	86.1
⊕	4.6	86.3
14	4.9	86.2
+4	5.0	86.1

91.11

39th St

35

el	3.1	88.0
+6	3.0	88.1
w	2.4	88.2

1+65-9.8' W of C = W. edge Elec. Guy Pole

1+72

w	2.7	88.4
+5	4.3	86.0
⊕	4.7	86.4
+5	4.5	86.6
+6	5.0	86.1
14	4.8	86.3
⊕	4.7	86.4
14	4.9	86.2
+8	5.3	85.8
d	4.4	86.2
+6	4.3	86.8
E	3.7	82.4

91.11

2+00

E	3.3	82.8
db	4.1	82.0
+2	4.4	86.3
114	4.4	86.2
ϕ	4.3	86.8
114	4.5	86.6
db	4.8	86.3
+5	4.4	86.2
W	3.1	88.0

2+50

W	1.1	90.0
+5	3.0	88.1
db	3.2	82.9
+5	3.2	82.9
+6	4.0	82.1
114	3.7	82.4
ϕ	3.6	82.5
114	3.6	82.5
+8	3.8	82.3
db	3.4	82.2
E	2.4	88.2

91.11

2+75

39th St

36

E	2.3	88.8
db	2.8	88.3
+2	3.4	82.2
44	3.2	82.9
ϕ	3.2	82.9
114	3.3	82.8
+4	3.5	82.6
+5	2.6	88.5
db	2.5	82.6
+5	2.5	82.6
W	1.1	90.0

2+82-10.0E of W. = Elec. Co. Guy wire Dead Man

2+99-10.5E of W = " " " Pole

3+00 s. line Logan Ave { 14' abs.
13' 14.5.

W	0.8	90.3
db	0.9	90.2
+5	1.9	89.2
+6	2.8	88.3
114	2.7	82.4
ϕ	2.7	88.4

91.11

3 + 0 of con)

e. log	2.8	88.3
+ 8	3.1	88.0
el	2.5	88.6
E	2.2	88.9

4.5' N of S = S. Edge walls

W. Line	1.05	90.06
---------	------	-------

9.5' N of S = N edge walk.

W. Line	1.13	89.98
---------	------	-------

11.5' N of S = Tel Pole W. edge 8.5 W of E.

S. el

E	2.6	88.5
el	2.6	88.5
1/4	2.6	88.5
±	2.3	88.8
1/4	2.2	88.9
di	2.2	88.9
W. g.	1.9	89.2
W. el. E. End.	1.19	89.72

91.11

39th st

37

S. 1/4

W	1.6	89.5
d	1.7	89.4
1/4	1.9	89.2
±	2.1	89.0
1/4	2.3	88.8
el	2.5	88.6
E	2.6	88.5

± Logan

E. - 80'	5.5	85.6
E. - 40'	4.0	87.1
E	2.6	88.5
el	2.4	88.7
1/4	2.3	88.8
±	2.1	89.0
1/4	1.8	89.3
el	1.6	89.5
W	1.3	89.8

91.11

N. 114

W	1.2	89.9
cb	1.4	89.2
114	1.6	89.5
⊕	1.8	89.3
114	2.2	88.9
cb	2.3	88.8
E	2.2	88.9

N. cb

E	2.2	88.9
cb	1.9	89.2
114	2.9	89.2
⊕	1.8	89.3
114	1.6	89.5
d	1.2	89.9
W	1.2	89.9
W. cb E. end.	0.15	90.86

+4.5' = S. edge walk

W = E. end. walk 0.07 91.04

+9.5' = N. edge walk

W = E. end. walk +0.07 91.18

91.11

39th St

38

0+00 = N. Line Logan.

W	+0.1	91.2
cb	0.0	91.1
+8	0.7	90.4
+9	1.6	89.5
114	1.6	89.5
⊕	1.7	89.4
114	1.8	89.3
cb	1.9	89.2
E	2.0	89.1
¹¹⁵	2.0	89.1
0+03.5 - 11' E. of W. = E. edge Elec. Pole.		

0+50

E-5	1.3	89.8
E	1.3	89.8
cb	1.3	89.8
114	1.4	89.7
⊕	1.2	89.9
114	1.4	89.7
+1	0.9	90.2
cb	0.2	90.9
W	0.0	91.1

T.P. 6.00 96.57 0.54 90.57

	96.57		
W	4.7	91.9	
dr	5.4	91.2	
114	6.1	90.5	
4	6.0	90.6	
114	6.2	90.4	
+8	6.5	90.0	
dr	5.8	90.8	
E	6.0	90.6	
+5	8.3	88.3	

out of Place

0196 - 9.0' W of E = Tel Pole W edge

1+09 - 9.0' W of E = " 80. Guy wire Dead Man

1+17 - 10.5' E. of W = Elec. Pole

1+18^E = S. Line Alley

E-5.	6.2	90.4
E	5.5	91.1
dr	6.0	90.6
14	5.9	90.7
4	5.7	90.9
114	5.6	91.0
dr	5.2	91.4
W	4.5	92.1

	96.57		39 th St
	1+33 ^E	N. Line Alley	39
W	3.7	92.9	
dr	4.8	91.8	
114	5.3	91.3	
dr	5.5	91.1	
114	5.7	90.9	
+9	5.8	90.8	
dr	5.3	91.3	
+9.4	5.3	91.3	
+9.4	Top. concrete wall S. end.	4.48	92.09
E	ground to N.	4.5	92.1
E	" " S.	5.0	91.6
1+36	8.5' W. of E. = Acacia	6" Diam.	

1+66

E = Top. wall	3.60	92.97
+03 " "	3.60	92.97
+04	5.1	91.5
dr	5.3	91.3
+2	5.7	90.9
114	5.4	91.2
4	5.2	91.4

96.57

1+66 (con)

W 14	5.0	91.6
el	3.8	92.8
+5	3.3	93.3
W.	2.4	94.2

1+84.5

W	2.1	94.5
+5	3.11	93.5
el	3.5	93.1
+5	4.6	92.0
14	4.8	91.8
⊕	5.1	91.5
14	5.4	91.2
+8	5.6	91.0
el	5.2	91.4
E	4.8	91.8

E+0.1 = Top. N. End Wall 3.61 92.96

1+88 - 8.5 W. of E. = Acacia Tree 7" Diam.

96.57

2+25

E	5.2	91.4
el	5.2	91.4
+2	6.4	90.2
14	6.0	90.6
⊕	5.8	90.8
14	5.2	91.4
+3	5.0	91.6
el	3.1	93.5
W.	1.9	94.7

2+53

W	1.4	95.2
+5	2.7	93.9
el	3.2	93.4
+7	6.7	89.9
14	6.7	89.9
⊕	6.9	89.9
14	7.3	89.3
+8	7.7	88.9
el	6.1	90.2
+5	6.4	90.2
E.	5.4	91.2

39th St

40

96.57

2+57

E	5.5	91.1
+5	6.6	90.0
cl	6.8	89.8
fz	7.8	88.8
1/4	7.4	89.2
±	7.1	89.5
1/4	6.9	89.7
+3	6.8	89.8
cl	4.4	91.8
+5	3.6	93.0
w	1.5	95.0

2+58^H = S. Line Florence

w	5.3	91.3
Walk Buried		
+75 E. edge Walk S. End	6.53	90.04
cl S. End.	6.56	90.01
G	6.8	89.8
1/4	7.0	89.6
±	7.2	89.4
1/4	7.5	89.1
G	8.0	88.6

96.57

cl S. End.	7.59	88.98	41
+2.5 W. edge S. End. walk	7.49	89.08	
+7.5 E " S. " "	7.35	89.22	
E	7.2	89.4	
" 10' N = S. cl			
C. cl	7.63	88.94	
E. C	8.4	88.2	
cl	8.2	88.4	
1/4	7.7	88.9	
±	7.4	89.2	
1/4	7.3	89.3	
cl	7.3	89.3	
W. G	7.1	89.5	
W. cl.	6.59	89.98	

chk. E.T. { 3' W. of line 39⁺
5.7' line Logan. 6.52 90.05 = 90.05
Page 33.

9-11-39 X. Sec. 41st + Univ. for Drainage

Miller
Walker
Bliss

B.M.B.P.	6.81	358.74	351.93	N.E. Univ + Central.
				W. ch. Line 41 st
50' N. of N. Line Univ		5.33	353.41	G. pav.
25' " " " "		5.41	353.33	" "
4' " " " "		5.65	353.09	N. End. catch Basin
N. Line Univ gutter		5.80	352.94	{ 5' " "
" " " " ch		4.80	353.94	{ N " Culvert + Headwall Pav. + ch.
14' S. of N. = N. ch. Line Univ.				
W. ch. Line pav.		5.05	353.69	
W " " "		5.38	353.36	
W " " ch		4.88	353.86	
50' W. of N. Line 41 st ch		5.19	353.55	
" " " " " gutter		5.62	353.12	
32 ^{1/4} S. of N. = N. Rail N. Track				
		4.79	353.95	
47 ^{1/2} S. of N. = S. Rail S. Track				
		4.97	353.77	
66' S. of N. = S. ch. Line				
W. ch pav		5.25	353.49	
W. Line "		5.62	353.12	
W. " ch		5.32	353.42	
" " + 30 gutter pav		5.75	352.99	

Indexed
c.s.k.

358.74

42

S. Line Univ.	{ S. End. culvert. N. End. grating	6.24	352.50	G. pav.
" " "				{ ch. pav + Headwall
6' S. of S. Line Univ	= N. End. Driveway to Oil station.	5.11	353.63	
5' S. of S. Line Univ	G. pav	6.16	352.58	
15' " " " "	" " " "	6.04	352.66	
50' " " " "	= S. End. above driveway			
43' S. of S. Line	= N. End. drive	6.38	352.36	G. pav
59' " " " "	= S. End. above driveway to Oil station			

B.M.B.P. N.W. Cor 41st Univ. 4.84 453.90

9-25-39 X Sec. Alley BIK. 175 U.H. Indexed
 Miller c.s.k.
 Walker
 Balbo

B.M.B.P. H.10 289.96 285.86 S.E. Lincoln
 ↓ Mississippi

B.M.B.P.N.W. 5.38 284.58 N.W. Alabama
 & Lincoln

T.P. 4.34 281.54 12.76 277.20

20' s. of original N. Line = N. cl - Lincoln

E. cl 6.40 275.14

C. pav 7.06 274.48

± " 7.75 273.79

W " 8.53 273.01

W cl 8.01 273.53

6' s. of original N. Line

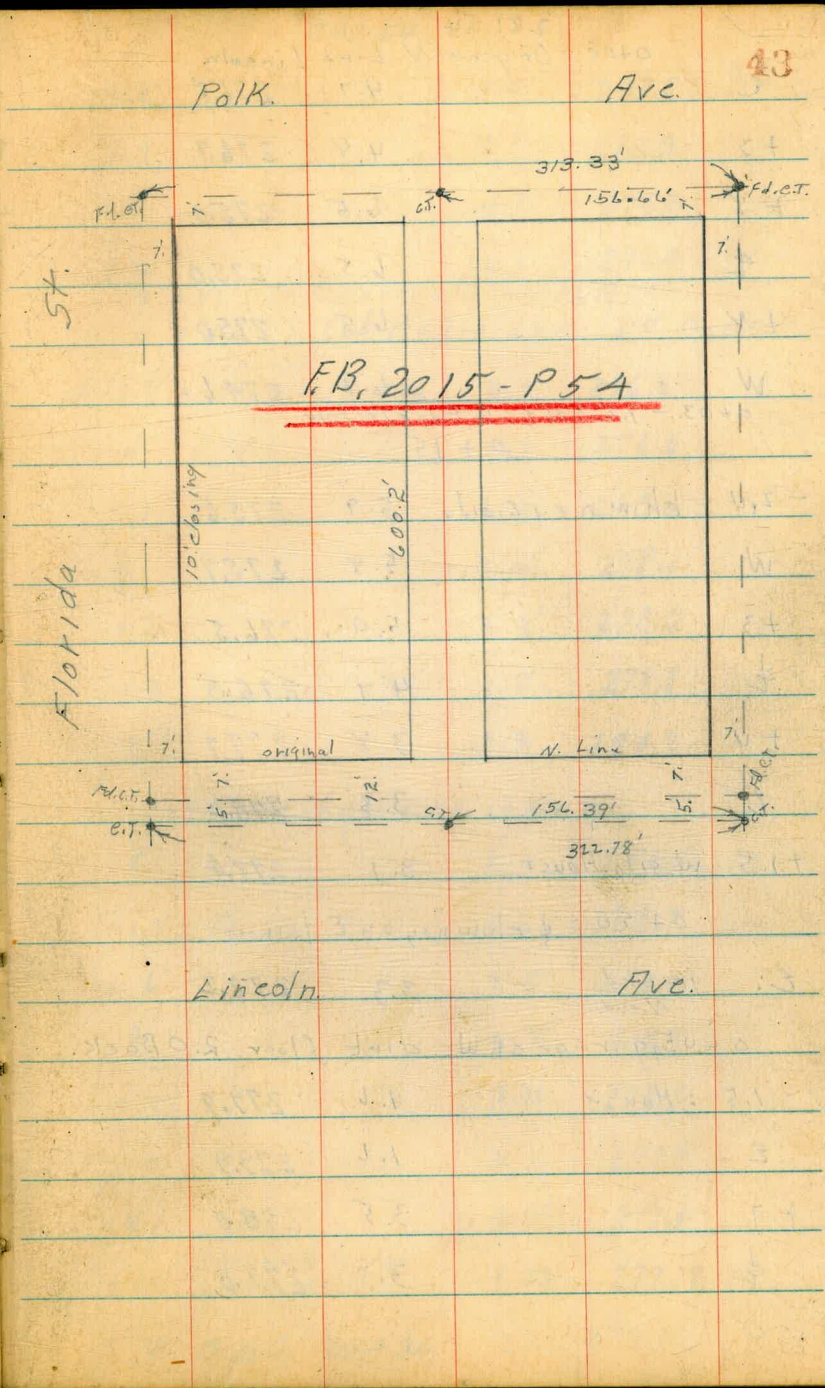
W - 0.24 = cl. N. End. 7.62 273.92

W - 0.24 = pav " " 7.70 273.84

± " " " 7.33 274.21

+9.85 = " " " 6.54 275.00

+9.85 = cl " " 6.34 275.20



	281.54		
E	0+00 = Original N. Line	Lincoln	4.7 276.8
+3			4.4 276.7
+8			6.5 275.0
±			6.5 275.0
+8			6.5 275.0
W	0+03. - 9.2' E of ± = E Edge Tel Pole		6.9 274.6
	0+15		
-2.4	= chimney E. side		5.9 275.6
W			5.8 275.7
+3			5.0 276.5
±			4.7 276.8
+4			3.8 277.7
E			3.3 278.2
+1.5	w. side House		3.1 278.4
	0+20 = ± chimney on E. line		
E.	ground N. end		3.3 278.2
	0+45 garage on W. dirt floor 2.0 Back.		
-1.5	= House		1.6 279.9
E			1.6 279.9
+7			3.5 278.0
±			3.7 277.8

	281.54		
+6			4.0 277.5
+8			4.7 276.8
+W			4.7 276.8
+2			4.7 276.8
	0+51 S. End. Fence on E. 1.2' in Alley		
	0+54 = S. End. House on W. 1.8' Back		
W-1.8	Ground Top. conc. Footing		4.9 276.6
W			4.9 276.6
+1			3.3 278.2
±			3.2 278.3
+3			2.8 278.7
+9			1.8 279.7
E			1.3 280.2
	0+74 = N. End above House on W.		
E			1.0 280.5
+1.5	= Fence		1.6 279.9
+6			2.5 279.0
±			2.4 278.7
+5			3.0 278.5
+9			3.6 277.9
W			4.1 277.4
+1.3	Ground & S. edge 4' conc. walk		4.15 277.59
T.P.	'5.52	284.84	2.22 279.32

284.84

0+93 = E garage on West, 4.0' back conc. Floor.

-4' on Floor above garage 7.14 277.70

0 +97

W 7.0 277.8

+5 6.2 278.6

E 6.0 278.8

+3 6.0 278.8

+8 6.0 278.8

+8.7 at fence 4.9 279.9

E 4.3 280.5

1+00

E 4.3 280.5

+15 = fence 4.3 280.5

+5 5.3 279.5

+7 6.0 278.8

E 6.0 278.8

W = W edge Elec. pole 6.2 278.6

+2 7.6 277.2

+5 7.9 276.9

1+05 end of fence on E 15' in Alley

284.84

1+05 = S. edge garage on E 15' in Alley. St. Entrance
on Floor 3.8 281.0

1+25 = N. edge above garage .35' in Alley.

1+35

-5 7.3 277.5

-2' 7.0 277.8

W 5.9 278.9

E 5.9 278.9

+3 5.7 279.1

+9 at shed 4.9 279.9

E 4.9 279.9

Sta. 1+25 to 1+40 = shed on E 1' in Alley. dirt Floor

1+42 = Tel. pole on E 8.8' E of E = East edge

Sta. 1+40 to 1+76 = Fence on E 1' in Alley.

1+65

E 4.7 280.1

+4 4.9 279.9

+8' 5.8 279.0

E 5.9 278.9

W 6.4 278.4

+2 6.8 278.0

+5 7.3 277.5

284.84

1+68 = 1/2 Garage on W dirt Floor 0.6' Back		
dirt Floor "	6.4	278.4
1+85		
-5	6.5	278.3
W	6.2	278.6
E	5.6	279.2
+2	5.6	279.2
+4	4.7	280.1
E	3.6	281.2
14" in Alley at 1+90 old 0.8' wide.		
5th 1+90 to 2+02 " Conc. Wall on E 14" in Alley		
on top Above Wall	3.54	281.30
2+00		
E	3.5	281.3
+1.7 on top Wall	3.58	281.26
+2	5.0	279.8
+6	5.4	279.4
E	5.8	279.0
W	6.2	278.6
+5	6.4	278.4
2+14 = 1/2 dble. garage on E 1' Back		
dirt Floor =	4.5	280.3

284.84

46

2+25		
W	6.1	278.7
E	5.8	279.0
+3	5.8	279.0
+5	5.1	279.7
E	4.5	280.3
2+32 = 1/2 garage on W 5.2' Back dirt Floor		
dirt Floor	6.2	278.6
2+50		
-5	6.7	278.1
-2	6.4	278.4
W	5.5	279.3
E	5.3	279.5
+3	5.1	279.7
E	3.8	281.0
		3' Back.
2+58 to 2+75 = dble garage on E Conc. Floor		
-3' Sedge Above garage	3.46	281.38 on Conc. Floor
-3' N. " " "	3.44	281.40 " " "
2+64 = Elec. Pole on W. 9.8' W of E-W edge		
2+75		
E	4.4	280.4

28484

L ₂	5.0	279.8
+9	5.0	279.8
W	5.5	279.3
+2	6.1	278.7
+5	6.7	278.1
T _d . 2+76 = Pole on E 92' E of L = E edge		
Sta. 2+77 to 3+27 Fence on E 0.9' in Alley		
3+00		
-5	6.1	278.7
W	5.6	279.2
L	5.2	279.6
+6	5.0	279.8
+7	4.1	280.7
E	3.8	281.0
3+05 = Garage on W Conc. Floor 0.8' Back. on East		
3+27 to 3+37 shed cor. foundation 0.7' in Alley		
3+30		
E + 0.7 on top Foundation above shed	3.7	281.1
+5	4.9	279.9
L	5.2	279.6
W	5.3	279.5
+W	6.3	278.5
+5	6.6	278.2

28484

3+59 = Garage on W. 0.6' Back. dirt Floor		
dirt Floor "	5.4	279.2
3+65		
-5	6.6	278.2
-2	6.0	278.8
W	5.5	279.3
L	5.4	279.4
+7	5.1	279.7
+8	4.7	280.1
E	4.7	280.1
3+37 to 3+74 = ^{chicken} wire fence on E 1' in Alley		
3+90		
E	4.5	280.3
+5	5.1	279.7
L	5.5	279.3
W	5.6	279.2
+2	6.0	278.8
+5	6.0	278.8
4+00 Elec. Pole on W 9.3' W of L = W edge		
3+89 to 4+06 = Fence on E 0.8' in Alley 3+89 0.3' " " 4+06		
4+06 to 4+23 = Sheds on E 0.3' in Alley 4+06 on line 4+23		

28484

W	54	279.4
L	50	279.8
+3	49	279.9
+8	40	280.8
E	39	280.9

4+26 Tel. pole 9'E L = E edge

E	38	281.0
L	51	279.7
W	55	279.3

4+35

-5	72	277.6
W	62	278.6
L	53	279.5
+5	48	280.0
+6	42	280.6
E	37	281.1

4+47 = $\frac{1}{2}$ Garage on W

W. on Conc. Apron.	6.26	278.58
+3.5' = Garage Floor.	6.27	278.57

4+50

E	4.5	280.3
+5	5.5	279.3

28484

L	5.9	278.9	48
W	6.2	278.6	
+5	6.2	278.6	
4+69 to 5+00 = House on West "oz" Back of 5+00 on Conc. Foundation = 6.5			
5+00 to 5+50 = Fence on E. on line ⁵⁺⁵⁰			

W	6.0	278.8
L	6.0	278.8
+8	5.8	279.0
E	5.1	279.7

5+00 Elec pole on W 9.5' W of L = W edge

5+20

E	5.0	279.8
+2	5.0	279.8
+5	5.9	278.9
L	6.2	278.6
+7	6.4	178.4
W	7.0	277.8
+8	7.0	277.8

5+50

-5	7.3	277.5
W	6.3	278.5

284.84

L	5.9	278.9
+5'	5.6	279.2
E	5.0	279.8

5+58 = Tel pole on E 9' E d = E edge pole

5+60

E	4.7	280.1
+2	5.6	279.2
L	6.0	278.8
W	6.2	278.6

5+97 = Cypress Tree on W 1' dia. $\frac{9.3 \text{ in dia.}}{= \text{W face}}$

5+98

W	6.2	278.6
L	6.0	278.8
+9	5.6	279.2
E	4.1	280.7

6+00.2 = South line Polk St.

E top cb.	5.19	279.65
E Gutter on Pav.	5.54	279.30
L on Pav.	6.31	278.53
W on Gutter on Pav.	6.44	278.40
" " cb.	6.36	278.48

284.84

South cb Polk St.

49

W Gutter on Pav.	7.13	277.71		
" top cb.	6.67	278.17		
L on Pav.	6.59	278.35		
E " "	5.92	278.92		
" top cb.	5.18	279.66		
TP	5.64	287.34	3.14	281.70
cb N.W. Alabama & Lincoln	2.75	284.59		
cb S.E. Miss. & Lincoln	1.51	285.83		

Walker
Bliss
Pumpin
9-26-39

Cross Section Alley Blk. 66
Univ. Hts.

Between KANSAS And Utah

From North line Meade to Monroe

5.94 372.72 366.78 S.E. CP Meade + Kansas

North cb. line Meade

-25' on Paving 5.96 366.76

E " " 5.75 366.97

" " cb. 5.32 367.40

E " Pav. 5.74 366.98

W " " 5.72 367.00

" " cb. 5.23 367.49

+25' 5.71 367.01

0+00 = N. line Meade

W. on cb. 5.13 367.59

" " Paving gutter 5.29 367.43

E " " 5.60 367.12 ✓

+10.1 " at cb. 5.51 367.21

" on cb. 5.31 367.41

0+15

E 5.1 367.6

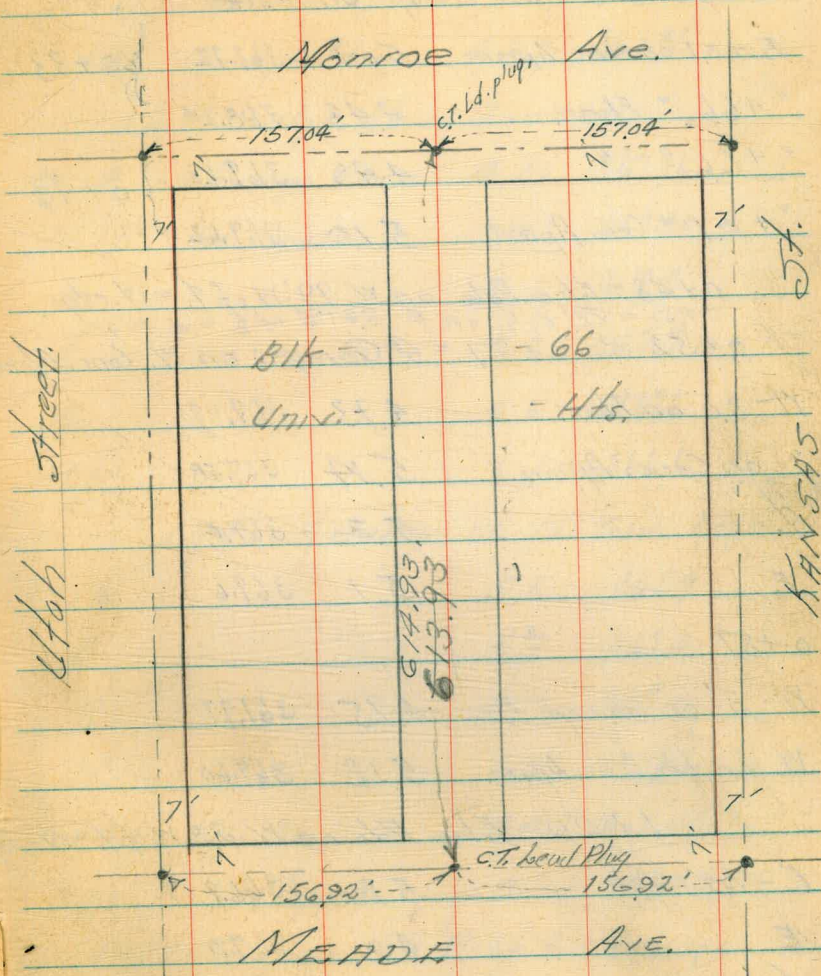
6 5.2 367.5

W 5.4 367.3

Indexed
e.s.k.

New Cross Sections P-76

50



372.72

0+33 to 0+48 = Garage on East.

E + 0.1 on Conc. Apron.	5.00	367.72	} 0+33
" + 6.6 " Floor.	4.48	368.24	
" + 6.6 " "	4.49	368.23	} 0+48
" + 0.1 " Conc. Apron	5.10	367.62	

0+48 = Elec. Pole on W 99' W of E = W edge.

0+50 = Tel. Pole on E 8.4' E of E = E edge

0+52 to 0+87 = 4 Garages on W. Conc. Floor

W - 3.0' on Floor.	4.73	367.99
" on Conc. Apron.	5.14	367.58
W	5.3	367.4
E	5.1	367.6

0+87

W - 3' on Garage Floor 4.75 367.97

W on toe Conc. Apron 5.12 367.60

1+00 = Elec. Pole on W 9.3 W of E = W edge

E - 10'	5.8	366.9
E	5.0	367.7
W	5.1	367.6
W	5.1	367.6

0+96 = W Walk on W 2' wide 3' Back

4.90 367.82

372.72

Alley 66 - Univ. Hts

1+07 = South edge dble Garage on West

W + 1.5 on toe Conc. Apron 5.21 367.51

" + 4.5 " Garage Floor 4.87 367.85

1+25 = N. edge Above Garage

W - 4' on Garage Floor 4.76 367.96

W - 10' " toe Apron 5.32 367.40

W 5.2 367.5

E 5.3 367.4

E 5.6 367.1

+10 6.1 366.6

1+46 = 1/2 Garage on W Conc. Floor

-10 5.8 366.9

E 5.7 367.0

E 5.7 367.0

W 5.5 367.2

+2.5 on Conc. Apron 5.47 367.25

+3.5 " " Floor 5.32 367.40

1+72 = Tel. pole 8.8' E of E = E edge

1+52 to 1+88 = Fence on W 2' in Alley.

1+72

-5 5.4 367.3

W 5.4 367.3

	372.72	Alley 66 Univ Hts.
L	5.4	367.3
E	5.8	366.9
+10	6.1	366.6
1+77		
-10 on Fill	4.6	368.1
E " "	4.9	367.8
+5	5.4	367.3
L	5.4	367.3
W	5.3	367.4
+10	5.3	367.4

2' in Alley 1+88
1+88 to 2+00 = Shed on West. 15' " " 2+00

2+00		
-5	5.7	367.0
W	5.7	367.0
L	5.1	367.6
+3	5.1	367.6
+5	4.6	368.1
E	4.6	368.1
+10	4.6	368.1

2+12 = Elec pole on W 9.3' W of L = W edge
2+20 = Garage on W 0.8' Back dirt Floor
on dirt Floor = 5.8 366.9

	372.72	
T.P.	4.21	372.16
	4.77	367.95
	2+35	
-5'		5.3 366.9
E		4.5 367.7
L		4.3 367.9
+6		4.4 367.8
W		4.8 367.4
+5		5.2 367.0
+30		5.1 367.1
2+75		

-30		5.1 367.1
-2		5.5 366.7
W		5.0 367.2
+2		4.9 367.8
L		4.6 367.6
+5		4.6 367.6
E		5.3 366.9
+10		5.0 367.2

3+00		
-2.5'		5.4 366.8
E-5'		5.7 366.5
E		5.4 366.8

372.16

+4'	46	367.6	
ℓ	49	367.3	
W	49	367.3	
+2	54	366.8	
+5'	46	367.6	
	4.8	367.4	dirt Floor
3+35 = 1/2 dble garage on E 16 Back.			
3+25			
-25	54	366.8	
-10'	53	366.9	
W	50	367.2	
ℓ	49	367.3	
E	49	367.3	
+10	48	367.4	
3+21 = Tel Pole on E 8.6' E of ℓ = E edge			
3+45 = Elec. Pole "W 9.1' W " " = W "			
0.1' in Alley at 3+51			
3+51 to 3+65 = Fence on E 0.5' " " " 3+65			
3+60			
-5	47	367.5	
E	49	367.3	
ℓ	48	367.4	
+6	47	367.5	
W	53	366.9	
+5	45	367.7	

372.16

3+65 to 4+01 = chicken shed on E		0.5' in Alley at 3+45	0.7' " " 53 4+01
4+10			
-5'	42	368.0	
W	48	367.4	
ℓ	48	367.4	
E	49	367.3	
+5'	51	367.1	
+20	52	367.0	
0.2' in Alley at 4+25			
4+25 to 4+75 = Fence on W on line at 4+75			
4+50 = Tel. Pole on E 8.7' E of ℓ = E edge			
-10'	42	368.0	
E	42	368.0	
ℓ	41	368.1	
W	38	368.4	
+5	38	368.4	
4+52 to 5+00 = Fence on E 0.7' in Alley			
4+88 = Elec. Pole on W 8.9' W of ℓ = W edge			
5+00			
-5	38	368.4	
W	33	368.9	
ℓ	32	369.0	
E	34	368.8	
+5	34	368.8	

372.16

5+39 = Garage on W. dirt floor

-5	2.3	369.9
E	2.3	369.9
S	2.4	369.8
W	2.5	369.7
+1.7 on dirt floor	2.3	369.9 at garage
5+00 to 5+51 = Fence on E 0.5' in Alley		
5+51 to 600 = Fence on E 0.2' in Alley		
5+79 = Tel Pole on E 8.7 E of S = E edge.		
5+80		

W	1.6	370.6
S	1.9	370.3
+8	1.8	370.4
E	1.4	370.8

6+01 = South edge existing Paving ^{Monroe} ~~North of~~ South line

E top cb.	0.98	371.18
" Gut. on Paving	0.98	371.18
S " "	1.26	370.90
W " "	1.21	370.95
W top cb.	1.10	371.06

372.16

South cb. Monroe

54

W on cb.	1.53	370.63
" Pav.	1.81	370.35
S " "	1.73	370.43
E " "	1.71	370.45
" " top cb.	1.21	370.95
T.P.	5.19	372.26
chk. B.M.	5.09	367.07
		S.E. Meade
	5.45	366.81 + Kansas
		366.78 = B.M.
		0.03 = Error.

X sec G St
26th to 200 E

80' wide
14' cbs

INDEXED
BRIZENDINE

1700-18
2/3/40

55

sm BT 11.46 183.45 171.99 26TH GST

00-10

N cb 6.49 176.96

N gut pav 7.41 176.04

cb " 7.44 176.01

1/4 " 7.49 175.96

c " 7.55 175.90

1/4 8.07 175.38

cb 8.76 174.69

S gut 9.33 174.12

S cb 8.49 174.96

0+00 E L 26 TH

S 8.0 175.45

cb 8.22 175.23

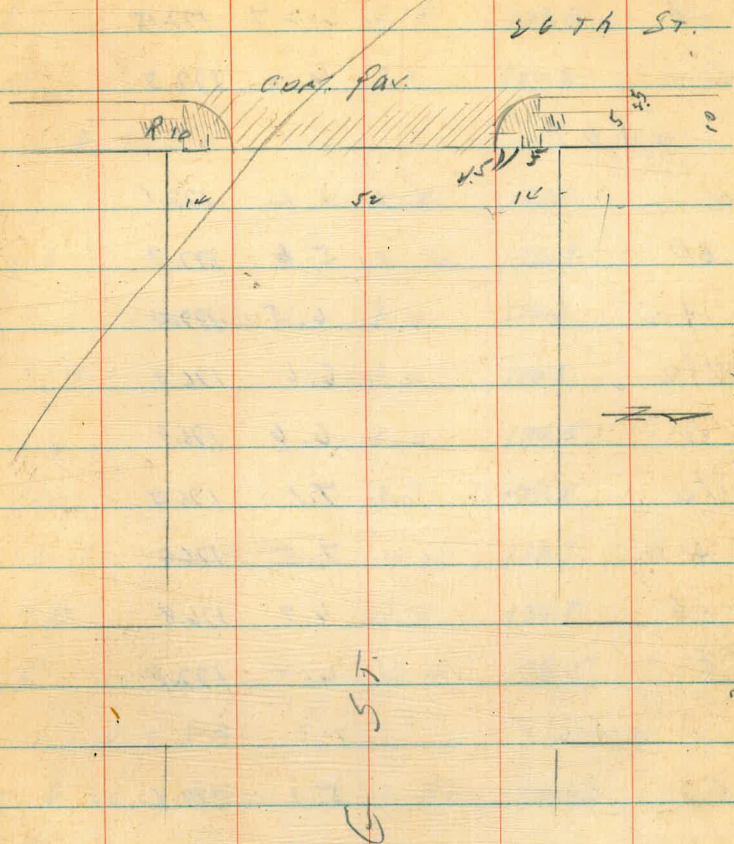
gut pav 8.80 174.65

1/4 " 7.68 175.77

c " 7.10 176.35

1/4 " 6.94 176.51

gut " 7.13 176.32



183.45

N cb	6.27	177.18
N	6.2	177.3
0 + 05		
N	4.4	179.1
cb	5.6	177.9
+2	6.5	177.0
1/2	6.6	176.9
0	6.6	176.9
1/4	7.1	176.4
+11	7.5	176.0
cb	6.7	176.8
S	6.4	177.1
0 + 25		
S	5.1	178.4
cb	4.9	178.6
+2	5.8	177.7
1/2	5.3	178.2
0	4.9	178.6
1/4	4.7	178.8
+11	4.4	178.9

183.45

56

cb	3.8	179.7		
N	3.2	180.3		
0 + 50				
1/2	2.2	181.2		
cb	2.4	180.9		
+3	3.2	180.3		
1/2	2.0	180.5		
0	2.0	180.5		
1/2	3.7	179.8		
+11	4.2	179.3		
cb	3.7	179.8		
S	4.0	179.5		
0 + 59				
- 6 W L APRON	2.80	180.65	Col	
S	3.3	180.2		
0 + 66				
N +1	E W WALK	1.43	182.02	"
0 + 75				
- 6 EL APRON	2.59	180.86		
S	2.9	180.6		

183.45

cb	3.1	180.4	
1/4	4.3	181.2	
c	1.9	181.6	
1/4	2.0	181.5	
+10	2.3	181.2	
cb	1.8	181.7	
N	1.4	182.1	
0+83			
-22 W.L. & car gar.	0.42	182.03	H.C.F.
N	1.3	182.2	
1+00			
N	1.0	182.5	
cb	1.3	182.2	
+3	1.8	181.7	
1/4	1.5	182.0	
c	1.3	182.2	
1/4	2.0	181.5	
cb	2.6	180.9	
+2	2.1	181.4	
S	2.4	181.1	

183.45

57

T.P	5.46	186.84	2.07	181.38	
1+07.1					
-26 W.L. & car gar.	5.55	186.29	CON		
1+10					
-	E.L. & car gar.	3.85	182.99	H.C.F.	
N	4.3	182.5			
1+30					
S		5.8	181.0		
cb		5.7	181.1		
1/4		5.2	181.6		
c		5.2	181.6		
1/4		5.7	181.1		
+10		5.7	181.1		
cb		5.1	181.7		
N		4.7	182.1		
1+37					
S	-26 E.L. & car gar.	5.57	181.27		
S		5.8	181.0		

186.84

1+40

N	5.5	181.3
cb	6.3	180.5
1/2	5.9	180.9
c	5.7	181.1
1/2	5.3	181.5
cb	5.5	181.3
S	5.9	180.9

1+50

S	5.7	181.1
cb	5.1	181.7
1/2	5.1	181.2
c	6.2	180.6
1/2	6.3	180.5
cb	6.5	180.3
N	7.0	179.8

1+60

N -10	10.9	175.9
N	8.4	178.4
cb	7.6	179.2
1/2	7.4	179.2

186.84

58

c	8.4	178.4
7.9	9.9	177.2
1/2	8.3	178.5
+4	6.2	180.6
cb	7.3	179.5
S	7.9	178.9
+5	7.7	179.1

1+61 N+11 14" Tel. P.

1+80

-10	14.0	172.8
S	14.5	172.3
cb	13.1	173.2
1/2	14.7	172.1
c	14.9	171.9
+7	15.2	171.6
1/2	12.9	173.9
cb	14.0	172.8
+10	13.9	172.9
N	15.7	171.1
+10	14.7	170.1

186.84

7400

-10 21.3 165.5

N 21.3 165.5

cb 19.8 167.0

1/4 20.5 166.3

c 20.3 166.5

1/4 19.5 167.4

cb 19.0 167.8

s 18.8 168.0

+10 18.4 168.2

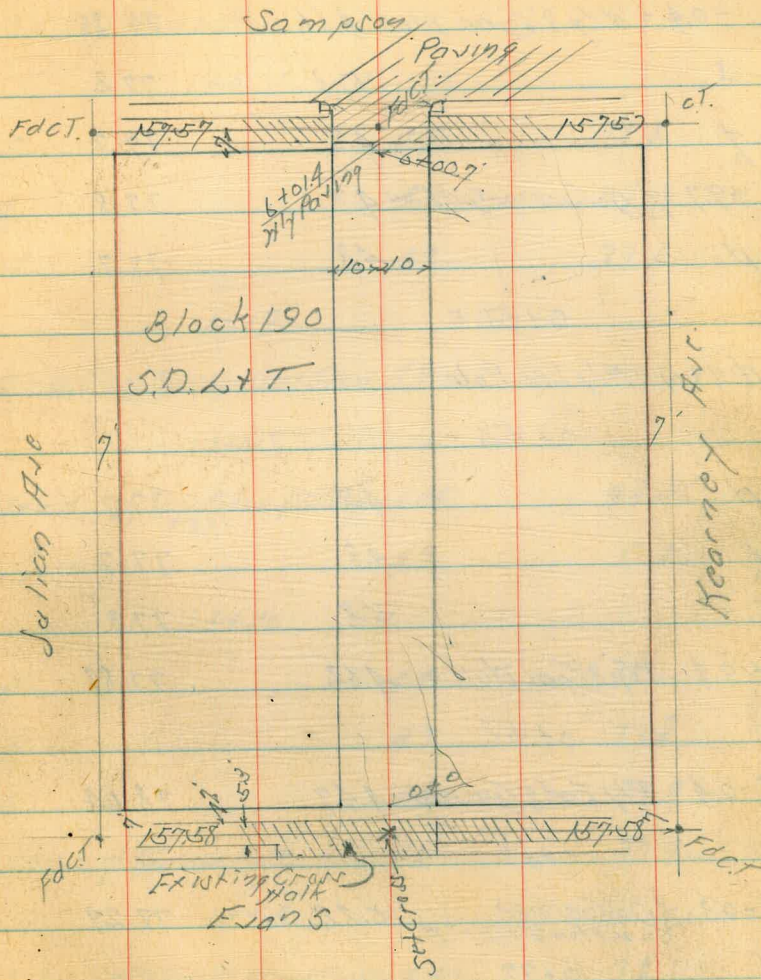
59

Cross Section Alley Block 190
San Diego Land & Tract Co

B.M.	10.51	82.51	72.00	H.H.B.P. Kearney Front
0-10 - F.C.B. Front				
S Topcb		5.18	77.33	
Gutter Dirt		6.0	76.5	
N Topcb		4.60	77.91	
Gutter dirt		5.4	77.1	
0-7.3 - Fly Edge Walk				
N on Conc Cross Walk		4.58	77.93	
S " " "		5.18	77.33	
0-2 - Fly Edge Cross Walk				
S on Conc Walk		5.13	77.38	
N " " "		4.78	77.73	
S " " "		4.42	78.09	
0+0 - F.C. Front				
N		4.4	78.1	
S		4.6	77.9	
S		5.2	77.3	
0+0.7				
S - 0.4 - Fly Edge Conc Walk		4.70	77.81	

Red. x Gorges ch. on Profile 2423
3/14/40 CBH

March 14 40
Sisson
Hortberg
H Moore 60



614.976
T.R.H.

8251

0+36

-0.4 = 1/4 8" Conc. Wall	4.66	77.85
S	5.2	77.2
L	4.8	77.7
+9.7 = 1/2 Do. Garage Dirt Floor	4.7	77.8
H	4.8	77.7

0+50.5

H+0.7 = 1/4 TC/ Pole

0+52

H	4.8	77.7
L	4.8	77.7
S	5.2	77.3
+0.4 = Top 8" Conc. Wall	4.62	77.89

0+52

S-0.4 = Fly End 8" Conc. Wall 4.47 78.04

0+66

S-0.3 = 1/2 Do. Garage
Conc. Floor & Dirt 5.22 77.29

0+77

H = 1/2 Garage Dirt Floor 5.0 77.5

0+85

S-1.3 = 1/2 Garage Dirt Floor 4.9 77.6

8251

61

0+99

S = Fly Pole or Pole

1+0

S	4.7	77.8
L	4.8	77.7
H	4.9	77.6

1+19

S-0.5 = 1/2 Garage Dirt Floor 4.9 77.6

1+30

H+0.4 = 1/2 Conc. Stop 4.5 along Top	4.05	78.46
Ground	4.8	77.7

1+40

H	4.4	78.1
L	4.7	77.8
S	4.6	77.9

+0.4 = 1/2 Garage Dirt 4.6 77.9

1+55

S-0.3 = 1/2 Garage Wood Floor 4.40 78.11

1+67

S = 1/2 Do. Garage Dirt Floor 4.60 77.91

82.51			
Z		4.2	78.3
H		4.0	78.5
1+77			
N+0.5	= 2 Car Garage D.F.	3.8	78.7
1+99			
N+0.7	= Nly Tel. Pole		
2+02			
N+0.3	= Nly 3 Car Garage Dirt Floor	3.3	79.2
Z		3.6	78.9
S		3.6	78.9
2+16.5			
S+0.6	= Sly Porch Pole		
2+36			
S		3.5	79.0
Z		3.3	79.2
+9.7	= Fly 3 Car Garage D.F.	3.3	79.3
2+58			
S	= 2 Garage Dirt Floor	3.7	78.8
TP	1.8°	81.07	3.24
			79.27

81.07			62
2+70			
H		2.0	79.1
Z		2.0	79.1
S		2.3	78.8
2+84			
N	= Nly Garage Conc Floor 7.5 Opening	1.86	79.21
2+96			
N+1.0	= 2.9.5 Conc Apron	1.88	79.19
N	= 2 Garage Conc Floor	1.83	79.24
3+0			
S		2.5	78.6
+0.6 = Sly Porch Pole			
Z		2.5	78.6
H		2.3	78.8
3+10			
N-0.2	= 2 Car Garage Dirt Floor	2.5	78.6
3+26			
N+0.5 = Nly Tel. Pole			
3+32			
-1.5	= 2.26 Conc Walk	2.25	78.82
H		2.6	78.5

	81.07		
L	3.3	77.8	
S	3.3	77.8	
	3+50		
S	4.2	76.9	
L	4.0	77.1	
#6	3.7	77.4	
H	3.0	78.1	
	3+95		
-5 = L Garage Dirt Floor	4.8	76.3	
H	4.8	76.3	
L	4.9	76.2	
S	5.0	76.1	
+1.5 = L Garage Conc. Floor	5.78	75.29	
	4+01		
S+0.2 = 5/4 Power Pole			
	4+03		
S-1.5 = 1/4 ^{Do} Garage Conc Floor	5.17	75.90	
S+1.3 = 1/4 Conc Apron	5.25	75.82	
	4+10		
H-3.2 = L Do Garage Dirt F	4.9	76.2	

	81.07		63
	4+21		
-1.5 = Fly Do Garage Conc Floor	5.08	75.99	
S on Case Apron	5.13	75.94	
+1.3 = 1/4 Conc Apron	5.19	75.88	
L	4.9	76.2	
H	4.9	76.2	
	4+25		
H = L Garage Dirt Floor			
	4+30		
H+0.3 = 1/4 Tel. Pole			
	4+60		
-1 = L Do Garage Dirt Floor	5.1	76.0	
H	5.1	76.0	
L	5.0	76.1	
S	5.3	75.8	
	4+76		
H-1 = L 3 Brick Walk	5.19	75.88	
	5+0		
S	5.0	76.1	
L	4.8	76.3	
H	4.9	76.2	

✓
81.07

5+01		
5+0.6 = Sly Pox Pale		
5+0.6		
5-1 = 1/2 Garage Dirt Floor 4.9	76.2	
5+1.3		
11-0.4 = 1/2 Garage Dirt F 4.3	76.8	
5+2.3		
11	4.2	76.9
1/2	4.4	76.7
S	4.1	76.7
+0.6 = 1/2 Do Garage Dirt Floor 4.4	76.7	
5+3.2		
11+0.6 = 11/4 Top Pale		
5+6.2		
S	3.6	77.5
1/2	3.7	77.4
1/7	3.6	77.5
11	3.3	77.8
11.4 = 1/2 Do Garage Wood Floor 2.95	78.12	

✓
81.07

64

5+8.5

11	3.3	77.8
1/3	3.9	77.2
1/2	4.2	76.9
1/6	4.1	77.0
S	3.9	77.2
6+00.7 = 11/4 Samp 107		
S Top Cb	5.37	75.70
S Ground	5.1	76.0
1/2	5.3	75.8
11	5.0	76.1
11 Top Cb	4.81	76.26
6+01.4 = 11/4 Alley Paving		
11 Top Cb	4.82	76.25
Gutter on Paving	5.10	75.97
1/2 " "	5.42	75.65
Gutter " "	5.40	75.67
S Top Cb	5.41	75.66
6+10.7 = 11 Cb Samp 107		
S on Paving	6.25	74.82

		✓ 81.07		
Z	02 Paving	6.00	75.07	
H	" "	5.74	75.33	
TP	291	79.63	5.35	75.72
BM		8.07	71.56	NHBP Kearney + Sampson 71.53

XSEC OF FLORENCE ST.

37th to 38th 10' 1/2"

SWBP	12.43	59.52		46.89	37th & Natl.
T.P.	11.41	70.59	0.34	59.18	37th & Florence
TR 7' CT.	12.30	81.22	1.67	68.92	

0-10 E. of E. of line 37th

S. h. cb	12.37	68.85
" gut	13.4	67.8
cb	13.2	68.0
1/4	12.7	68.5
c	12.5	68.7
1/4	12.3	68.9
cb	12.2	69.0
N. h. gut	12.4	68.8
" cb	11.75	69.47
0+00 E.L. 37th		
N. cb	11.77	69.45
gut	12.0	69.2
1/4	12.1	69.1
c	12.1	69.1

Red Plot on Profile No. 306 4-18-40 G.B.H.

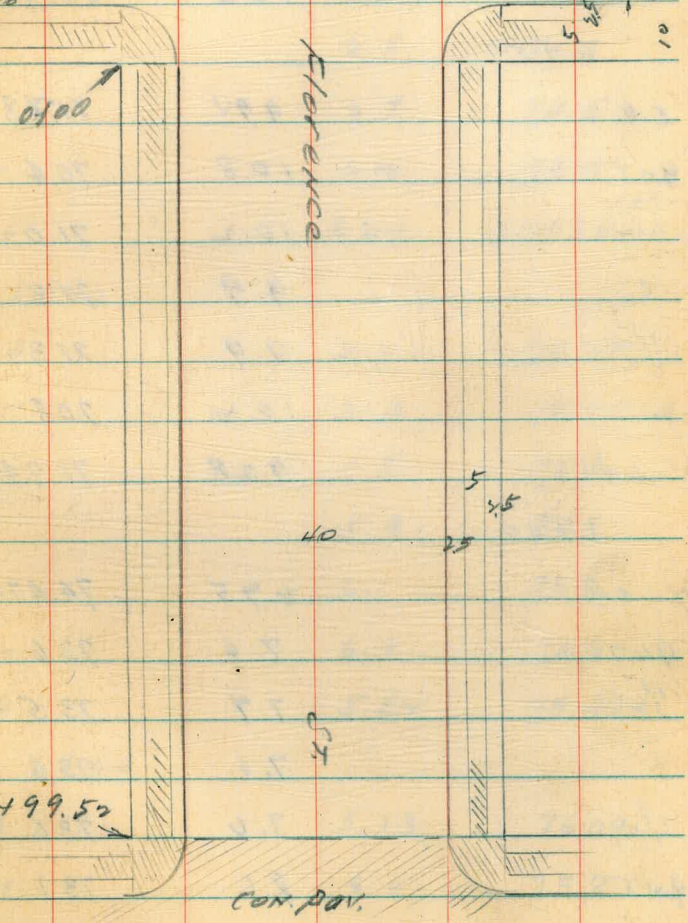
Moore
0509N
Plate
4-17-40

INDEXED
EFB

66

37th
curb

ST. 40



38th

ST.

81.22

1/2	12.4	68.8
gut	12.8	68.4
S cb	12.2x	68.98
0+50		
S cb	9.94	71.88
gut	10.8	70.4
1/4	10.2	71.0
c	9.9	71.3
1/4	9.9	71.3
gut	10.4	70.8
N cb	9.28	71.94
1+00		
N cb	6.75	74.47
gut	7.6	73.6
1/4	7.7	73.5
c	7.6	73.6
1/4	7.6	73.6
gut	8.1	73.1
S cb	7.58	73.64

81.22

67

1420		
900	6.67	74.55
gut	7.5	73.7
1/2	6.8x	74.4
c	6.8	74.4
1/2	6.7	74.5
gut	6.2	75.0
N cb	6.20	75.02 ⁱⁿ drive
1+00		
N cb	5.00	76.22
gut	5.9	75.3
1/4	5.8	75.4
c	5.9	75.3
1/4	6.1	75.1
gut	6.6	74.6
S cb	5.8x	75.40
1+00		
S cb	5.13	76.09
gut	6.0	75.2
1/4	5.4	75.8
c	5.2	76.0

81.22

1/2	5.0	76.2
qut	5.0	76.2
N cb	4.30	76.92
1+80		
N cb	3.70	77.52
qut	4.3	76.9
1/2	4.4	76.8
c	4.6	76.6
1/4	4.9	76.3
qut	5.4	75.8
S cb	4.55	76.67
2+00		
S cb	4.07	77.15
qut	4.9	76.3
1/2	4.2	77.0
c	4.0	77.2
1/4	4.0	77.2
qut	3.8	77.4
N cb	3.24	77.98

81.22

68

2+50

N cb	2.29	78.93
qut	3.0	78.2
1/4	2.8	78.4
c	2.9	78.3
1/4	3.2	78.0
qut	3.9	77.3
S cb	3.07	78.20
3+00		
S cb	2.13	79.09
qut	2.9	78.3
1/2	2.2	79.0
c	2.0	79.2
1/4	2.1	79.1
qut	2.1	79.1
N cb	1.55	79.67
3+50		
N cb	0.56	80.66
qut	1.5	79.7 ✓
1/4	1.2	80.0
c	0.9	80.3

81.22

1/4	1.3	79.9
qut	1.9	79.3
Sob	1.15	80.07

T.P. 805 8805 1.22 80.00

4400

Sob	7.05	81.00
qut	7.9	80.2
1/4	7.2	80.9
c	6.9	81.2
1/4	7.1	81.0
qut	7.4	80.7
Nob	6.53	81.52

4750

Nob	5.68	82.37
qut	6.4	81.7
1/4	6.1	82.0
c	6.0	82.1
1/4	6.5	81.6
qut	6.9	81.2

88.05

69

Sob 4.15 81.90

5400

Sob	5.12	82.93
qut	5.9	82.2
1/4	5.5	82.6
c	5.2	82.9
1/4	5.2	82.9
qut	5.5	82.6
Nob	4.80	83.25

5750

Nob	4.02	84.03
qut	4.6	83.5
1/4	4.4	83.7
c	4.3	83.8
1/4	4.5	83.6
qut	5.2	82.9
Sob	4.15	83.90

5799.50 W.L. 38.5

Sob	3.18	84.87
qut	3.95	84.10

88.05

1/4	Par	3.65	84.40
c	"	3.56	84.49
1/4	"	3.67	84.38
gut	"	3.84	84.21
N cb		3.17	84.88
w. cb. line 3875			
N 4	cb	3.17	84.88
"	gut Par	3.61	84.44
cb	"	3.60	84.45
1/4	"	3.44	84.61
c	"	3.32	84.73
1/4	"	3.40	84.65
cb	"	3.62	84.43
5h	gut	3.64	84.41
5h	cb	3.16	84.89
w. 1/4 on 3876			
5	Par	3.29	84.76
46	"	3.40	84.65
cb	"	3.28	84.77
1/4	"	3.12	84.93

88.05

70

c	Par.	3.08	84.97
1/4	"	3.20	84.85
46	"	3.32	84.73
cb	"	3.23	84.82
N	"	3.05	85.00
T.P. 2.51 90.30 0.26 87.79			
T.P. 2.95 82.96 10.29 80.01			
SEBP. NATL. 43875 6.44 76.52 76.58			

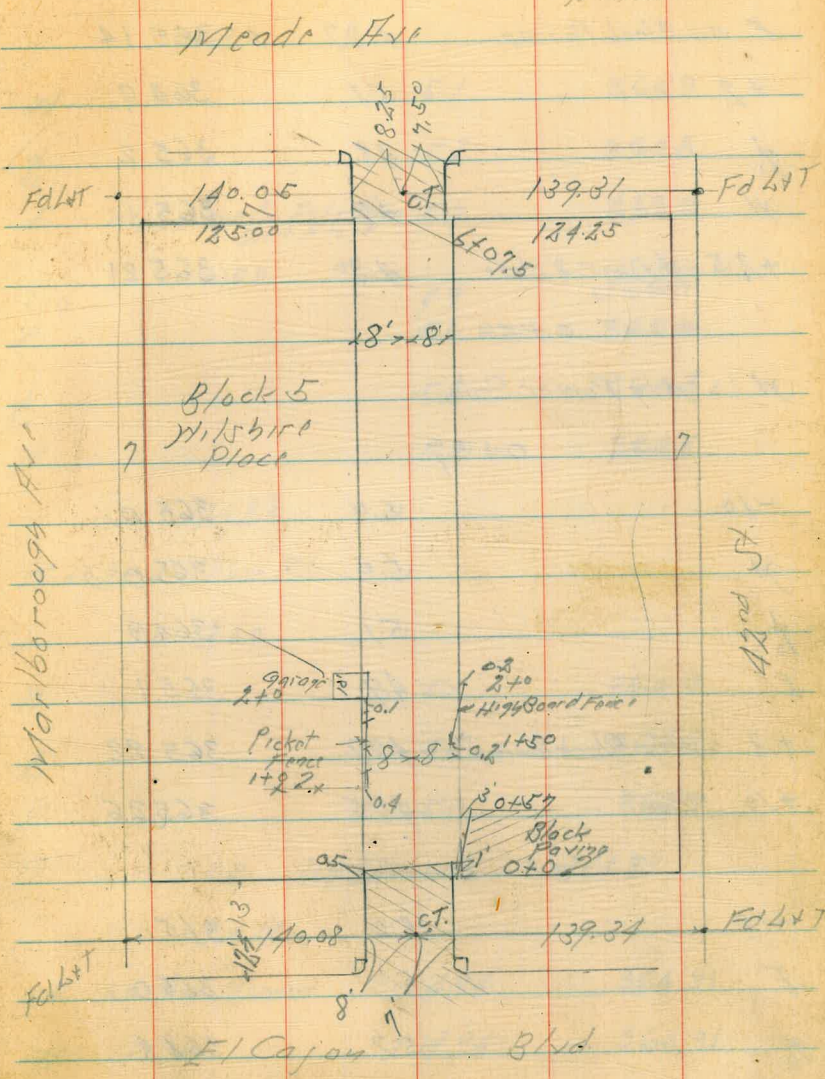
Cross Section Alley Block 5 Wilshire Place
From El Cajon to Meade Between Marlborough & 12th

BM	Station	Elevation	Notes
487	370.01	365.14	S.M.B.P. El Cajon & Marlborough
0-25 = N of El Cajon Blvd			
H	on Paving	5.83	364.18
L	"	5.87	364.14
F	"	5.90	364.11
0-13			
F	+1' - Cb Top	5.10	364.91
	Gutter on Pav.	5.33	364.68
L	"	5.60	364.41
	Gutter	5.05	364.96
H	Cb Top	4.95	365.06
0+0 = N of El Cajon			
H	Cb Top	4.98	365.03
	Gutter on Paving	5.15	364.86
L	"	5.37	364.64
+7	= Gutter "	5.05	364.96
+7	C Top	4.91	365.10
F	"	4.9	365.1
0+17			
-10	"	4.8	365.2

Reduced & Plot on Profile 2565 5-18-40 C.B.H.

INDEXED
EFD

May 17 40
Sisson
Northway
H Moore



370.01		
F on Black Paving	4.87	365.14
+2	5.1	364.9
L	4.8	365.2
H	4.9	365.1
+2.5 - 1/2 Door 8' Wide	4.80	365.21
0+50		
H = 1/4 Ply Porter Pole		
0+57		
-10	5.0	365.0
H	5.0	365.0
L	5.1	364.9
F	4.9	365.1
+3 = 1/4 Black Paving	4.79	365.22
+10 on " "	4.75	365.26
1+0		
-10	5.0	365.0
F	5.0	365.0
L	5.2	364.8
H	5.3	364.7
+10	5.1	364.9

370.01			
1+30			
H		5.1	364.9
L		5.2	364.8
F = 1/4 Garage Slab Entrance		5.0	365.0
1+50			
-10		4.9	365.1
F		5.0	365.0
L		5.2	364.8
H		5.2	364.8
1+88			
H + 0.2 = 1/4 Ply Port Pole			
2+0			
H		5.1	364.9
L		5.2	364.8
F		5.1	364.9
TP	5.02	369.85	5.18 364.83
2+11			
-5 on Conc. Drain		4.94	364.91
H " " "		4.94	364.91
L		5.0	364.9
F		5.0	364.9
+10		4.9	365.0

369.85

2+50

F	4.7	365.2
L	4.8	365.1
H	4.5	365.4
+2.8 Conc Polk	4.44	365.41

3+0

-10	5.0	364.9
H	5.3	364.6
L 07 MH Rim	5.22	364.63
F	4.9	365.0
+10	5.3	364.6

3+26

F	4.7	365.2
L	4.6	365.3
H	4.6	365.3

+0.4 = Wly Pow Polk

3+60

-10	5.3	364.6
H	5.6	364.3
L	5.1	364.8

369.85

73

F	4.8	365.1
+10	5.0	364.9
	4+0	
F	4.9	365.0
L	5.1	364.8
H	5.1	364.8

+0.2 = Wly Pow Polk

TP 5.04 369.75 5.14 364.71

4+50

-10	4.6	365.2
H	5.2	364.6
L	5.0	364.8
F	5.0	364.8
+10	4.7	365.1

4+75

F	4.8	365.0
L	4.6	365.2
H	4.2	365.6

5+0

-10	4.8	365.0
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369.75

H - Wly Parter Pk	4.7	365.1
Z	5.2	364.6
F	5.2	364.6
+10	5.1	364.7

5+25

-10	4.8	365.0
F	5.0	364.8
Z	5.0	364.8
H	4.9	364.9
+10	5.0	364.8

5+50

H	4.6	365.2
Z	4.6	365.2
F	4.6	365.2

5+75

F	4.2	365.6
Z	4.3	365.5
H	4.3	365.5

5+93

-3.3 - Fly Edge Garage	3.78	365.97
No Entrance		
Conc Floor		

369.75

74

H	4.0	365.8
Z	4.1	365.7
F	3.8	366.0

6+07.5 - J.L. Meade

F TopCb	5.98	365.77
Gutter on Pavmg	4.26	365.49
Z " "	4.34	365.41
Gutter 1 " "	4.31	365.44
H TopCb	4.68	365.67

6+21.5 - SCB Meade

H on Pavmg	4.67	365.08		
Z " "	4.71	365.04		
F " "	4.77	364.98		
TP	4.94	371.00	3.69	366.06

BM		5.03	365.97	JW BP Meade Marlborough 366.07
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TP	4.71	370.28	5.43	365.57
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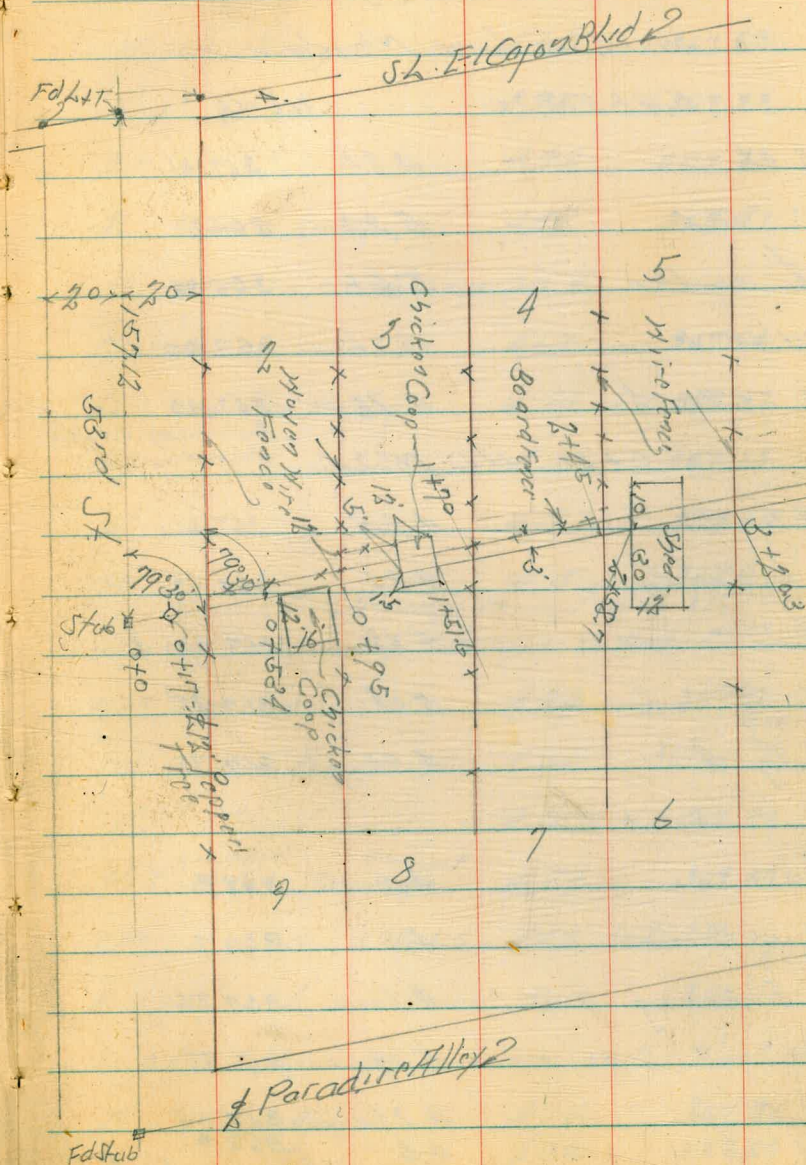
BM		5.13	365.15	JW BP Fico joint Marlborough 365.14
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Levels For Proposed Sewer
Country Paradise

BM	9.57	403.45	393.88	S.W.P. El Cajon 753 rd
0+0	-2	Stub 53 rd St	5.99	397.46 ✓
+12			6.4	397.0 ✓
+15			5.2	398.2 ✓
+50			4.9	398.5 ✓
+95			5.1	398.3 ✓
+10			4.9	398.5 ✓
TP	4.86	403.27	5.04	398.41 ✓
1+35	68' N	1/4 Frame to 454	5.04	398.73 ✓ Floor Elev.
+50			5.1	398.2 ✓
2+0			5.5	397.8 ✓
+50			6.4	396.9 ✓
TP	4.41	401.43	6.25	397.02 ✓
3+54	100' N	1/4 Stucco house 536	6.25	396.07 ✓ Floor Elev.
3+80	75' N	1/4 Frame to 460	6.25	396.83 ✓ Floor Elev.
3+80			5.6	395.8 ✓
3+20.3			7.4	394.0 ✓

~~INDEXED~~
EPB

Aug. 17-40
S.W.P.
El Cajon
North 75th
St. Moore



Walker.		
Bliss		
15bell		
11-20-40		
Re-Cross Section Alley Blk 66		
UNIV. Hts.		
Bet. Kansas And Utah		
from Meade to Monroe		
See Sketch Page 50		
North cb. line Meade		
	5.48	372.26
		366.78
E. cb.	4.85	367.41
" " Gut.	5.27	366.99
L. on Pav.	5.28	366.98
W. " "	5.26	367.00
" " Top cb.	4.78	367.48
		- Beginning crushed Rock Paving
	0+00	- N. line Meade
W Top cb.	4.65	367.61
" Gut on Paving.	4.81	367.45
L. " "	5.18	367.08 ✓
E. " "	5.01	367.25
" Top cb.	4.88	367.38
	0+15	
-10	4.0	368.3
E. on Header	4.6	367.7
" " Paving	4.90	367.36
L. " "	5.09	367.17
W. " "	4.71	367.55
+1	4.3	368.0
+9	4.7	367.6

INDEXED		372.26
EPB		
0+33	= South end of Garage on E. Conc. floor.	26
-5		4.5 367.8
W on Paving		4.63 367.63
L. " "		4.98 367.28
+5 " "		4.93 367.33
E. " Conc. Apron		4.49 367.77
0+49	= North Garage on E	
E. on Conc. Apron		4.67 367.64
L. " on Back Paving		4.89 367.37
+5 " " "		4.83 367.43
W. " " "		4.57 367.69
+5		4.5 367.8
0+52	= E. Conc. Drainage channel on E 2.75' wide	
0+52	= Beginning 4 Garages on West	0+87 = N end.
W-3' on Floor		4.29 367.97
W on Back Paving		4.65 367.61
L. " " "		4.85 367.41
+9.9	= Wedge channel on Conc. Drainage	4.79 367.47
T.P.	4.83 372.60	4.49 367.77
E +2.5'	= on E. Conc. channel	5.00 367.60
0+56.5	= Beginning 11 Garages on E. Conc. Floors.	
E. on Conc. Apron		4.74 367.86
" " " Floor		4.60 368.00

	372.60	Alley Blk. 66 Umn. Hts.		
0+87 = N end 4 Garage	4.61	367.99	on West	
0+94 = Break in Apron to 11 car garage on E.				
E. on Apron	4.80	367.80		
+5.1 on Floor	4.51	368.09		
0+99.3 = Break in Apron to 11 car garage on E				
E. on Apron	4.83	367.77		
+5.1 on Apron	4.77	367.83		
1+00				
E. on Apron	4.82	367.78		
" " Rock Paving	4.93	367.67		
L " " "	5.10	367.50		
W " " "	4.72	367.88		
+3' " " " West edge	4.64	367.96		
+10	4.7	367.9	1.5' back	
1+07 = South edge Dble. Garage on West Conc. Floor				
TP 4.95	372.72	4.83	367.77	
W-45 on Garage Floor	4.85	367.87	Apron Paved over	
			This end of Rock	
1+25 = N. end Above Garage on st			Paving.	
W-46 on Floor Garage	4.63	368.09		
W on Rock paving	4.91	367.81		
L " " "	5.15	367.57		
E on " "	5.07	367.65		
+0.2 on Conc. Apron	5.00	367.72		

	372.72	Alley Blk 66 Umn. Hts		
E +5.3 on Conc. Floor	4.94	367.78	77	
1+46 = E Garage on W				
E-5.4 = on Garage Floor	4.92	367.80		
E-1.4 + Conc. Apron	4.97	367.75		
E	5.1	367.6		
L	5.3	367.4		
W	5.3	367.4		
+3.7 on Conc. Floor	5.32	367.40		
1+72				
-5	5.5	367.2		
W	5.5	367.2		
L	5.3	367.4		
E	5.1	367.6		
+0.8 on Conc. Apron	4.98	367.74		
+5.8 " Floor Garage	4.94	367.78		
on Conc. Apron =	4.95	367.77		
1+75 = N end Conc. Apron to 11 car garage on E				
1+77				
E -10	4.8	367.9		
E	4.9	367.8		
+5	5.3	367.4		
L	5.2	367.5		
W	5.4	367.3		
+10	5.5	367.2		

372.72 Alley Blk 66 Univ. Hts.

1+52 to 1+88 = Fence on W South end 0.5' Back Hard ^{10' Back}

5.82 366.90

1+88 = South end garage on West Conc Floor 1' Back

on Floor = 5.62 367.10

2+01 = N " " " Conc Floor 1.7' Back

2+00

W on Apron 5.60 367.12

E 5.2 367.5

E 4.4 368.3

+10 4.5 368.2

2+07

-10 4.4 368.3

E 4.4 368.3

E 5.1 367.6

W 5.6 367.1

+13 5.7 367.0

2+20 = Garage on W 1' Back ^{Lot goes up from here} 5.6 367.1
dirt floor

2+35

-25 5.6 367.1

-5 5.8 366.9

W 5.3 367.4

+4 5.0 367.7

E 5.0 367.7

E 5.3 367.4

+5 5.4 367.3

372.72 Alley Blk 66 Univ. Hts. ⁷⁵

2+39 = South end Fence on W 1.4' Back

2+76 = N " " " 1.9 "

2+75

-10 6.0 366.7

E 5.7 367.0

+3 5.8 366.9

+6 5.1 367.6

E 5.1 367.6

+8 5.0 367.1

W 5.5 367.2

+2 6.1 366.6

+30 5.7 367.0

3+00

-5 5.3 367.4

W 5.5 367.2

E 5.5 367.2

+5 5.2 367.5

E 6.0 366.7

+25 5.7 367.0

3+25

-10 5.3 367.4

E 5.4 367.3

	372.72	Alley Blk. 66 Univ. Hqs.	
L	5.5	367.2	
W	5.3	367.4	
+10	6.0	366.7	
+25	5.8	366.9	
3+35 = L Old Garage	5.4	367.3	Wood on E 16' Back Floor
3+42			
E	5.2	367.5	
L	5.4	367.3	
W	5.4	367.3	
+5	5.7	367.0	
+20	4.8	367.9	
3+47			
-20	4.8	367.9	
-5'	5.7	367.0	
W	5.4	367.3	
L	5.3	367.4	
+3	5.3	367.4	
+7 on loose dirt	4.2	368.5	
E	5.0	367.7	
3+60			
-5	5.4	367.3	
L	5.1	367.6	

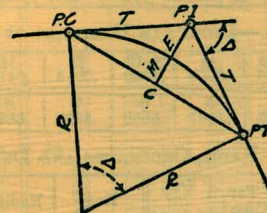
	372.72	Alley Blk. 66 Univ. Hqs. 79	
E+2	4.7	368.0	
+6	5.3	367.4	
L	5.4	367.3	
+6	5.4	367.3	
+8	4.7	368.0	
W	5.2	367.5	
+3	5.5	367.2	
+20	4.7	368.0	
4+00			
-15	3.3	369.4	
W	5.1	367.6	
L	5.1	367.6	
+4	5.3	367.4	
+7	4.5	368.2	
E	5.0	367.7	
+5	5.3	367.4	
4+10			
TP 6.72	374.31	5.13	367.59
-164 = Wcb Kansas		6.5	367.8
-60		7.2	367.1
-20		7.2	367.1
-5		7.2	367.1
E		7.2	367.1
+6		6.7	367.6

L	6.7	367.6
W	6.9	367.4
+15	5.1	369.2
4+27		
-15	6.8	367.5
W	6.9	367.4
+1	6.6	367.7
L	6.7	367.6
+5	6.6	367.7
15	7.1	367.2
+20	7.2	367.1
4+50		
-25	6.3	368.0
E	6.3	368.0
L	6.3	368.0
+6	6.2	368.1
+8	5.9	368.4
W	6.0	368.3
+10	5.8	368.5

Continued P-86

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

$$\text{Radius} = R = \frac{50}{\sin \frac{D}{2}} \quad (1) \quad \text{Degree of Curve} = D \text{ and } \sin \frac{D}{2} = \frac{50}{R} \quad (2)$$

$$\text{Tangent} = T = R \tan \frac{\Delta}{2} \quad (3) \quad \text{Length of Curve} = L = 100 \frac{\Delta}{D} \quad (4)$$

$$\text{Middle ordinate} = M = R(1 - \cos \frac{\Delta}{2}) \quad (5) = R \text{vers} \frac{\Delta}{2} \quad (6)$$

$$\text{External} = E = T \tan \frac{\Delta}{4} \quad (7) = R \div \cos \frac{\Delta}{2} - R \quad (8) = R \text{exsec} \frac{\Delta}{2} \quad (9)$$

$$\text{Long Chord} = C = 2 R \sin \frac{\Delta}{2} \quad (10) \quad \Delta = \text{Central Angle}$$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I. = Sta. 161 + 60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $+8\frac{1}{3} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. - $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^2$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 91.27$ and from Table V correction = .10 or $E = 91.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

TABLE I.—MINUTES IN DECIMALS OF A DEGREE.

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

TABLE II.—INCHES IN DECIMALS OF A FOOT.

1-16	3-32	1/8	3-16	1/4	5-16	3/8	1/2	5/8	3/4	7/8
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III.—RADI, ORDINATES AND DEFLECTIONS.

Deg.	Radius	Mid. Ord.	Tan. Offset	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Offset	Def. for 1 Foot
0° 10'	34377.5	.036	.145	0.05'	7°	819.02	1.528	6.105	2.10'
20	17188.8	.073	.291	0.10	20'	781.84	1.600	6.395	2.20
30	11459.2	.109	.436	0.15	30	764.49	1.637	6.540	2.25
40	8594.42	.145	.582	0.20	40	747.89	1.673	6.685	2.30
50	6875.55	.182	.727	0.25	8	716.78	1.746	6.976	2.40
1	5729.65	.218	.873	0.30	20	688.16	1.819	7.266	2.50
10	4911.15	.255	1.018	0.35	30	674.69	1.855	7.411	2.55
20	4297.28	.291	1.164	0.40	40	661.74	1.892	7.556	2.60
30	3819.83	.327	1.309	0.45	9	637.28	1.965	7.846	2.70
40	3437.87	.364	1.454	0.50	20	614.56	2.037	8.136	2.80
50	3125.36	.400	1.600	0.55	30	603.80	2.074	8.281	2.85
2	2864.93	.436	1.745	0.60	40	593.42	2.110	8.426	2.90
10	2644.58	.473	1.891	0.65	10	573.69	2.183	8.716	3.00
20	2455.70	.509	2.036	0.70	30	546.44	2.292	9.150	3.15
30	2292.01	.545	2.181	0.75	11	521.67	2.402	9.585	3.30
40	2148.79	.582	2.327	0.80	30	499.06	2.511	10.02	3.45
50	2022.41	.618	2.472	0.85	12	478.34	2.620	10.45	3.60
3	1910.08	.655	2.618	0.90	30	459.28	2.730	10.89	3.75
10	1809.57	.691	2.763	0.95	13	441.68	2.839	11.32	3.90
20	1719.12	.727	2.908	1.00	30	425.40	2.949	11.75	4.05
30	1637.28	.764	3.054	1.05	14	410.28	3.058	12.18	4.20
40	1562.88	.800	3.199	1.10	30	396.20	3.168	12.62	4.35
50	1494.95	.836	3.345	1.15	15	383.07	3.277	13.05	4.50
4	1432.69	.873	3.490	1.20	30	370.78	3.387	13.49	4.65
10	1375.40	.909	3.635	1.25	16	359.27	3.496	13.92	4.80
20	1322.53	.945	3.718	1.30	30	348.45	3.606	14.35	4.95
30	1273.57	.982	3.926	1.35	17	338.27	3.716	14.78	5.10
40	1228.11	1.018	4.071	1.40	18	319.62	3.935	15.64	5.40
50	1185.78	1.055	4.217	1.45	19	302.94	4.155	16.51	5.70
5	1146.28	1.091	4.362	1.50	20	287.94	4.374	17.37	6.00
10	1109.33	1.127	4.507	1.55	21	274.37	4.594	18.22	6.30
20	1074.68	1.164	4.653	1.60	22	262.04	4.814	19.08	6.60
30	1042.14	1.200	4.798	1.65	23	250.79	5.035	19.94	6.90
40	1011.51	1.237	4.943	1.70	24	240.49	5.255	20.79	7.20
50	982.64	1.273	5.088	1.75	25	231.01	5.476	21.64	7.50
6	955.37	1.309	5.234	1.80	26	222.27	5.697	22.50	7.80
10	929.57	1.346	5.379	1.85	27	214.18	5.918	23.35	8.10
20	905.13	1.382	5.524	1.90	28	206.68	6.139	24.19	8.40
30	881.95	1.418	5.669	1.95	29	199.70	6.360	25.04	8.70
40	859.92	1.455	5.814	2.00	30	193.18	6.583	25.88	9.00

Notes. Chord Deflection=2 times tangent deflection.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
1°	50.00	.22	11°	551.70	26.50	21°	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
2	100.01	.87	12	602.21	31.56	22	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
3	150.04	1.96	13	652.81	37.07	23	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
4	200.08	3.49	14	703.51	43.03	24	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
5	250.16	5.46	15	754.32	49.44	25	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
6	300.28	7.86	16	805.25	56.31	26	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
7	350.44	10.71	17	856.30	63.63	27	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
8	400.66	13.99	18	907.49	71.42	28	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
9	450.93	17.72	19	958.81	79.67	29	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
10	501.28	21.89	20	1010.3	88.39	30	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
91°	5830.5	2444.9	101°	6950.6	3278.1	111°	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20	5864.6	2469.3	20	6992.0	3310.1	20	8388.9	4429.2
30	5881.7	2481.5	30	7012.7	3326.1	30	8415.1	4450.9
40	5898.8	2493.8	40	7033.6	3342.3	40	8441.5	4472.7
50	5916.0	2506.1	50	7054.5	3358.5	50	8468.0	4494.6
92	5933.2	2518.5	102	7075.5	3374.9	112	8494.6	4516.6
10	5950.5	2531.0	10	7096.6	3391.2	10	8521.3	4538.8
20	5967.9	2543.5	20	7117.8	3407.7	20	8548.1	4561.1
30	5985.3	2556.0	30	7139.0	3424.3	30	8575.0	4583.4
40	6002.7	2568.6	40	7160.3	3440.9	40	8602.1	4606.0
50	6020.2	2581.3	50	7181.7	3457.6	50	8629.3	4628.6
93	6037.8	2594.0	103	7203.2	3474.4	113	8656.6	4651.3
10	6055.4	2606.8	10	7224.7	3491.3	10	8684.0	4674.2
20	6073.1	2619.7	20	7246.3	3508.2	20	8711.5	4697.2
30	6090.8	2632.6	30	7268.0	3525.2	30	8739.2	4720.3
40	6108.6	2645.5	40	7289.8	3542.4	40	8767.0	4743.6
50	6126.4	2658.5	50	7311.7	3559.6	50	8794.9	4766.9
94	6144.3	2671.6	104	7333.6	3576.8	114	8822.9	4790.4
10	6162.6	2684.7	10	7355.6	3594.2	10	8851.0	4814.1
20	6180.2	2697.9	20	7377.8	3611.7	20	8879.3	4837.8
30	6198.3	2711.2	30	7399.9	3629.2	30	8907.7	4861.7
40	6216.4	2724.5	40	7422.2	3646.8	40	8936.3	4885.7
50	6234.6	2737.9	50	7444.6	3664.5	50	8965.0	4909.9
95	6252.8	2751.3	105	7467.0	3682.3	115	8993.8	4934.1
10	6271.1	2764.8	10	7489.6	3700.2	10	9022.7	4958.6
20	6289.4	2778.3	20	7512.2	3718.2	20	9051.7	4983.1
30	6307.9	2792.0	30	7534.9	3736.2	30	9080.9	5007.8
40	6326.3	2805.6	40	7557.7	3754.4	40	9110.3	5032.6
50	6344.8	2819.4	50	7580.5	3772.6	50	9139.8	5057.6
96	6363.4	2833.2	106	7603.5	3791.0	116	9169.4	5082.7
10	6382.1	2847.0	10	7626.6	3809.4	10	9199.1	5107.9
20	6400.8	2861.0	20	7649.7	3827.9	20	9229.0	5133.3
30	6419.5	2875.0	30	7672.9	3846.5	30	9259.0	5158.8
40	6438.4	2889.0	40	7696.3	3865.2	40	9289.2	5184.5
50	6457.3	2903.1	50	7719.7	3884.0	50	9319.5	5210.3
97	6476.2	2917.3	107	7743.2	3902.9	117	9349.9	5236.2
10	6495.2	2931.6	10	7766.8	3921.9	10	9380.5	5262.3
20	6514.3	2945.9	20	7790.5	3940.9	20	9411.3	5288.6
30	6533.4	2960.3	30	7814.3	3960.1	30	9442.2	5315.0
40	6552.6	2974.7	40	7838.1	3979.4	40	9473.2	5341.5
50	6571.9	2989.2	50	7862.1	3998.7	50	9504.4	5368.2
98	6591.2	3003.8	108	7886.2	4018.2	118	9535.7	5395.1
10	6610.6	3018.4	10	7910.4	4037.8	10	9567.2	5422.1
20	6630.1	3033.1	20	7934.6	4057.4	20	9598.9	5449.2
30	6649.6	3047.9	30	7959.0	4077.2	30	9630.7	5476.5
40	6669.2	3062.8	40	7983.5	4097.1	40	9662.6	5504.0
50	6688.8	3077.7	50	8008.0	4117.0	50	9694.7	5531.7
99	6708.6	3092.7	109	8032.7	4137.1	119	9727.0	5559.4
10	6728.4	3107.7	10	8057.4	4157.3	10	9759.4	5587.4
20	6748.2	3122.9	20	8082.3	4177.5	20	9792.0	5615.5
30	6768.1	3138.1	30	8107.3	4197.9	30	9824.8	5643.8
40	6788.1	3153.3	40	8132.3	4218.4	40	9857.7	5672.3
50	6808.2	3168.7	50	8157.5	4239.0	50	9890.8	5700.9
100	6828.3	3184.1	110	8182.8	4259.7	120	9924.0	5729.6
10	6848.5	3199.6	10	8208.2	4280.5	10	9957.5	5758.6
20	6868.8	3215.1	20	8233.7	4301.4	20	9991.0	5787.7
30	6889.2	3230.8	30	8259.3	4322.4	30	10025.0	5817.0
40	6909.6	3246.5	40	8285.0	4343.6	40	10059.0	5846.5
50	6930.1	3262.3	50	8310.8	4364.8	50	10093.0	5876.1

TABLE V.—CORRECTIONS FOR TANGENTS AND EXTERNALS.

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table IV) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.06
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.49
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.52	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.053
20°	.006	.011	.017	.022	.028	.034	.039	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.183
35°	.018	.035	.054	.072	.086	.109	.131	.155	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.429	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.877	.971	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524</										

TABLE VI.—CORRECTIONS FOR SUB-CHORDS AND LONG CHORDS.

FOR SUB-CHORDS ADD										Excess of arc per 100 ft.	LONG CHORDS				
D	10	20	30	40	50	60	70	80	90		D	200	300	400	500
4°	.00	.00	.01	.01	.01	.01	.01	.01	.00	.02	1	199.99	299.97	399.92	499.85
6	.00	.01	.01	.02	.02	.02	.02	.01	.01	.05	2	199.97	299.88	399.70	499.39
8	.01	.02	.02	.03	.03	.03	.03	.02	.01	.08	3	199.93	299.73	399.32	498.63
10	.01	.02	.03	.04	.05	.05	.05	.04	.02	.13	4	199.88	299.51	398.78	497.57
12	.02	.04	.05	.06	.07	.07	.07	.05	.03	.18	5	199.81	299.24	398.10	496.20
14	.02	.05	.07	.08	.09	.10	.09	.07	.04	.25	6	199.73	298.90	397.26	494.53
16	.03	.06	.09	.11	.12	.12	.12	.09	.05	.33	7	199.63	298.51	396.28	492.57
18	.04	.08	.11	.14	.15	.16	.15	.12	.07	.41	8	199.51	298.05	395.14	490.31
20	.05	.10	.14	.17	.19	.20	.18	.15	.09	.51	9	199.38	297.54	393.86	487.75
22	.06	.12	.17	.21	.23	.24	.22	.18	.10	.62	10	199.24	296.99	392.42	484.90
24	.07	.14	.20	.25	.28	.28	.26	.21	.12	.74	12	198.90	295.63	389.12	478.34
26	.09	.17	.24	.29	.32	.33	.31	.25	.15	.86	14	198.51	294.06	385.22	470.65
28	.10	.19	.27	.34	.37	.38	.36	.29	.17	1.00	16	198.05	292.25	380.76	461.86
30	.11	.22	.31	.39	.43	.44	.41	.33	.19	1.15	18	197.54	290.21	375.74	452.02
32	.13	.25	.36	.44	.49	.50	.47	.38	.22	1.31	20	196.90	287.94	370.17	441.15
34	.15	.28	.40	.50	.55	.57	.53	.43	.25	1.48	22	196.32	285.44	364.06	429.30
36	.17	.32	.45	.56	.62	.64	.59	.48	.28	1.66	24	195.63	282.71	357.43	416.53
38	.18	.36	.51	.62	.70	.71	.66	.53	.31	1.86	26	194.87	279.76	350.30	402.89
40	.21	.40	.56	.69	.77	.79	.73	.59	.35	2.06	28	194.06	276.59	342.69	388.42
42	.23	.44	.62	.76	.85	.87	.81	.65	.38	2.28	30	193.18	273.20	334.61	373.20
44	.25	.48	.68	.84	.94	.96	.89	.72	.42	2.50	32	192.25	269.61	326.08	357.28
46	.27	.52	.75	.92	1.02	1.05	.98	.78	.46	2.74	34	191.26	265.81	317.12	340.73
48	.30	.57	.81	1.00	1.12	1.14	1.06	.86	.50	2.99	36	190.21	261.80	307.77	323.61
50	.32	.62	.89	1.09	1.21	1.24	1.15	.93	.55	3.24	38	189.10	257.60	298.03	305.99
52	.35	.67	.96	1.18	1.31	1.35	1.25	1.01	.59	3.52	40	187.94	253.21	287.94	287.94
54	.38	.73	1.04	1.28	1.42	1.46	1.35	1.09	.64	3.80	42	186.72	248.63	277.51	269.54
56	.41	.78	1.12	1.38	1.53	1.57	1.46	1.17	.69	4.09	44	185.44	243.87	266.78	250.85
58	.44	.84	1.20	1.48	1.65	1.69	1.57	1.20	.74	4.40	46	184.10	239.93	255.78	231.95
60	.47	.91	1.29	1.59	1.76	1.81	1.68	1.35	.80	4.72	48	182.71	233.83	244.51	212.92

Note.—When a chord of less than 100 ft. is used the corrections given in the above table should be added to the nominal length of chord to get the length which should be used in order that the 100 ft. points will check with those obtained by using the standard 100 ft. chord. Thus in locating a 14° curve by 25 ft. chords measure 25'.06 for each chord. Long chords are useful in passing obstacles.

TABLE VII.—MIDDLE ORDINATES FOR RAILS IN FEET.

Deg. of Curve	LENGTH OF RAILS.					Deg. of Curve	LENGTH OF RAILS.								
	32	30	28	26	24		22	20	32	30	28	26	24	22	20
1°	.022	.020	.016	.013	.011	.009	.008	16°	.356	.313	.273	.236	.200	.170	.139
2	.045	.038	.034	.029	.025	.021	.017	17	.378	.333	.290	.252	.213	.180	.148
3	.067	.058	.051	.044	.037	.031	.026	18	.400	.351	.306	.265	.225	.190	.156
4	.089	.079	.069	.060	.050	.042	.035	19	.423	.371	.324	.280	.238	.201	.165
5	.112	.099	.086	.074	.063	.053	.044	20	.445	.392	.341	.296	.250	.212	.174
6	.134	.117	.102	.088	.076	.064	.052	21	.466	.410	.357	.309	.262	.222	.182
7	.156	.137	.120	.104	.088	.074	.061	22	.487	.430	.375	.325	.275	.233	.191
8	.179	.158	.137	.119	.100	.085	.070	23	.509	.450	.390	.338	.287	.243	.199
9	.201	.175	.153	.133	.112	.095	.078	24	.531	.469	.408	.354	.299	.253	.208
10	.223	.196	.171	.148	.125	.106	.087	25	.552	.486	.424	.367	.311	.263	.216
11	.245	.216	.188	.163	.139	.117	.096	26	.573	.506	.441	.382	.323	.274	.225
12	.268	.236	.206	.179	.151	.128	.105	27	.594	.524	.457	.396	.335	.284	.233
13	.290	.254	.222	.192	.163	.138	.113	28	.618	.545	.475	.411	.348	.294	.242
14	.312	.275	.239	.207	.175	.148	.122	29	.638	.564	.491	.424	.361	.303	.250
15	.334	.295	.257	.223	.188	.159	.131	30	.660	.583	.508	.438	.374	.313	.259

SLOPE REDUCTIONS.

When distances are measured on a slope they may be reduced to the equivalent horizontal distance by the following approximate rule:—subtract from the slope distance the square of the rise divided by twice the slope distance. Thus for a slope distance of 250.3 ft. and a rise of 15 ft. correction=15²÷2×250.3=.45 (by slide rule) or horizontal distance=250.3-.45=249.85. When vertical angle=V. A. is measured horizontal distance=slope distance—slope distance (1—Cos. V. A.). Thus for slope distance of 248.7 ft. and V. A. of 4° 20' from Table VIII Cos=.99714 and correction=1-.99714=.00286 per foot or total of .286×2½ (near enough)=.57 and horizontal distance=248.7-.57=248.13 ft.

See fig. (a). TRIGONOMETRICAL FORMULAS.

sin. $A = \frac{a}{c}$

cos. $A = \frac{b}{c}$

tan. $A = \frac{a}{b}$

cot. $A = \frac{b}{a}$

sec. $A = \frac{c}{b}$

cosec. $A = \frac{c}{a}$

FORMULA FOR SOLVING TRIANGLES.

Given	Sought.	Right triangles. See fig. (a).
a, c	A, B, b	$\sin. A = \frac{a}{c}, \cos. B = \frac{a}{c}, b = \sqrt{(c+a)(c-a)}$
a, b	A, B, c	$\tan. A = \frac{a}{b}, \cot. B = \frac{a}{b}, c = \sqrt{a^2+b^2}$
A, a	B, b, c	$B=90^\circ-A, b=a \cot. A, c = \frac{a}{\sin. A}$
A, b	B, a, c	$B=90^\circ-A, a=b \tan. A, c = \frac{b}{\cos. A}$
A, c	B, a, b	$B=90^\circ-A, a=c \sin. A, b=c \cos. A$
Given	Sought.	Oblique triangles. See fig. (b).
A, B, a	b	$b = \frac{a \sin. B}{\sin. A}$
A, a, b	B	$\sin. B = \frac{b \sin. A}{a}$
a, b, c	A - B	$\tan. \frac{1}{2}(A-B) = \frac{(a-b) \tan. \frac{1}{2}(A+B)}{a+b}$
a, b, c	A	$\left\{ \begin{aligned} \text{If } s = \frac{1}{2}(a+b+c), \sin. \frac{1}{2}A &= \sqrt{\frac{(s-b)(s-c)}{bc}} \\ \cos. \frac{1}{2}A &= \sqrt{\frac{s(s-a)}{bc}}, \tan. \frac{1}{2}A &= \sqrt{\frac{(s-b)(s-c)}{s(s-a)}} \\ \sin. A &= \frac{2\sqrt{s(s-a)(s-b)(s-c)}}{a^2+b^2+c^2} \end{aligned} \right.$
A, B, C, a	area	$\text{area} = \frac{a^2 \sin. B \sin. C}{2 \sin. A}$
A, b, c	area	$\text{area} = \frac{1}{2}bc \sin. A$
a, b, c	area	$s = \frac{1}{2}(a+b+c), \text{area} = \sqrt{s(s-a)(s-b)(s-c)}$

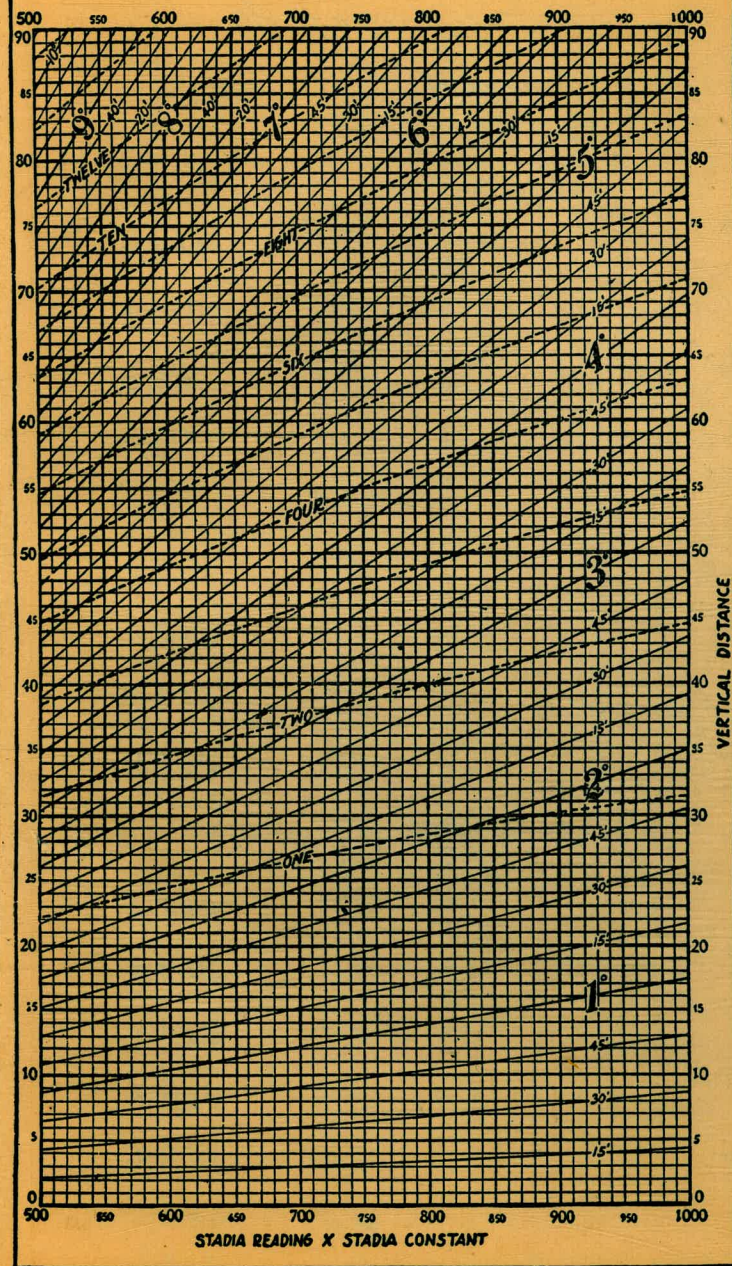
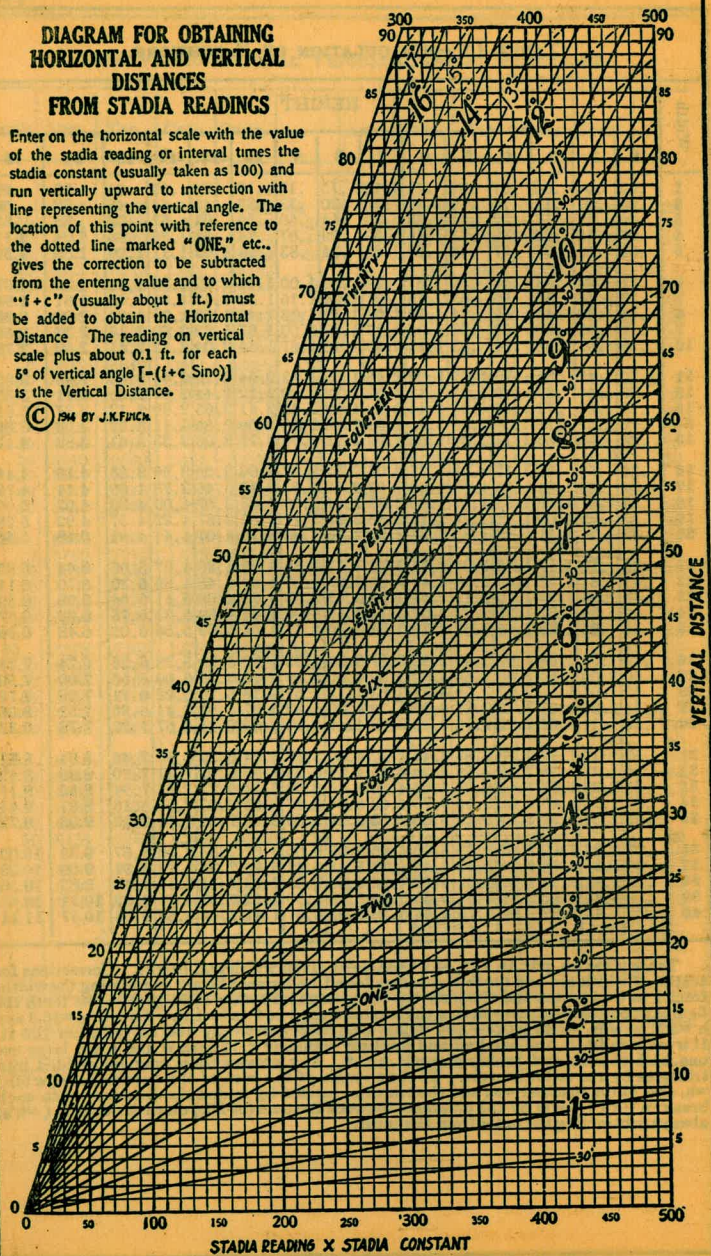
TABLE VIII.—NATURAL TRIGONOMETRICAL FUNCTIONS.

Angle	Sine.	Tan.	Cotg.	Cosin.	Angle	Sine.	Tan.	Cotg.	Cosin.
0°	0	0	∞	1	90°	1	∞	0	0
10	.0029	.0029	343.8	.99998	80	.1392	.1405	7.115	.99027
20	.0058	.0058	171.9	.99996	70	.1421	.1435	6.968	.98986
30	.0087	.0087	114.6	.99993	60	.1449	.1465	6.827	.98944
40	.0116	.0116	85.94	.99989	50	.1478	.1495	6.691	.98902
50	.0145	.0145	63.75	.99985	40	.1507	.1524	6.561	.98858
1	.0175	.0175	57.29	.99981	30	.1536	.1554	6.435	.98814
10	.0204	.0204	49.10	.99979	20	.1564	.1584	6.314	.98769
20	.0233	.0233	42.96	.99977	10	.1593	.1614	6.197	.98723
30	.0262	.0262	38.19	.99976	0	.1622	.1644	6.084	.98676
40	.0291	.0291	34.37	.99975	8	.1650	.1673	5.976	.98629
50	.0320	.0320	31.24	.99974	7	.1679	.1703	5.871	.98580
2	.0349	.0349	28.64	.99973	6	.1708	.1733	5.769	.98531
10	.0378	.0378	26.43	.99972	5	.1736	.1763	5.671	.98481
20	.0407	.0407	24.54	.99971	4	.1765	.1793	5.576	.98430
30	.0436	.0437	22.90	.99970	3	.1794	.1823	5.485	.98378
40	.0465	.0466	21.47	.99969	2	.1822	.1853	5.396	.98325
50	.0494	.0495	20.21	.99968	1	.1851	.1883	5.309	.98272
3	.0523	.0524	19.08	.99967	0	.1880	.1914	5.226	.98218
10	.0552	.0553	18.07	.99966	8	.1908	.1944	5.145	.98163
20	.0581	.0582	17.17	.99965	7	.1937	.1974	5.066	.98107
30	.0610	.0612	16.35	.99964	6	.1965	.2004	4.989	.98050
40	.0640	.0641	15.60	.99963	5	.1994	.2035	4.915	.97992
50	.0669	.0670	14.92	.99962	4	.2022	.2065	4.843	.97934
4	.0698	.0699	14.30	.99961	3	.2051	.2095	4.773	.97875
10	.0727	.0729	13.73	.99960	2	.2079	.2126	4.705	.97815
20	.0756	.0758	13.20	.99959	1	.2108	.2156	4.638	.97754
30	.0785	.0787	12.71	.99958	0	.2136	.2186	4.574	.97692
40	.0814	.0816	12.25	.99957	8	.2164	.2217	4.511	.97630
50	.0843	.0846	11.83	.99956	7	.2193	.2247	4.449	.97566
5	.0872	.0875	11.43	.99955	6	.2221	.2278	4.390	.97502
10	.0901	.0904	11.06	.99954	5	.2250	.2309	4.331	.97437
20	.0929	.0934	10.71	.99953	4	.2278	.2339	4.275	.97371
30	.0958	.0963	10.39	.99952	3	.2306	.2370	4.219	.97304
40	.0987	.0992	10.08	.99951	2	.2334	.2401	4.165	.97237
50	.1016	.1022	9.788	.99950	1	.2363	.2432	4.113	.97169
6	.1045	.1051	9.514	.99949	0	.2391	.2462	4.061	.97100
10	.1074	.1080	9.255	.99948	8	.2419	.2493	4.011	.97030
20	.1103	.1110	9.010	.99947	7	.2447	.2524	3.962	.96959
30	.1132	.1139	8.777	.99946	6	.2476	.2555	3.914	.96887
40	.1161	.1169	8.556	.99945	5	.2504	.2586	3.867	.96815
50	.1190	.1198	8.345	.99944	4	.2532	.2617	3.821	.96742
7	.1219	.1228	8.144	.99943	3	.2560	.2648	3.776	.96667
10	.1248	.1257	7.953	.99942	2	.2588	.2679	3.732	.96593
20	.1276	.1287	7.770	.99941	1	.2616	.2711	3.689	.96517
30	.1305	.1317	7.596	.99940	0	.2644	.2742	3.647	.96440
40	.1334	.1346	7.429	.99939	8	.2672	.2773	3.606	.96363
50	.1363	.1376	7.269	.99938	7	.2700	.2805	3.566	.96285
					6	.2728	.2836	3.526	.96206
					5				
					4				
					3				
					2				
					1				
					0				
					8				
					7				
					6				
					5				
					4				
					3				
					2				
					1				
					0				
					8				
					7				
					6				
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DIAGRAM FOR OBTAINING HORIZONTAL AND VERTICAL DISTANCES FROM STADIA READINGS

Enter on the horizontal scale with the value of the stadia reading or interval times the stadia constant (usually taken as 100) and run vertically upward to intersection with line representing the vertical angle. The location of this point with reference to the dotted line marked "ONE," etc., gives the correction to be subtracted from the entering value and to which "f+c" (usually about 1 ft.) must be added to obtain the Horizontal Distance. The reading on vertical scale plus about 0.1 ft. for each 5° of vertical angle [$-(f+c \sin \alpha)$] is the Vertical Distance.

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Alley Block 66 - Univ. Hts.
Cont. from P-80

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374.31		
5+00		
-10	5.4	368.9
W	5.5	368.8
+3	5.3	369.0
+5	5.6	368.7
E	5.4	368.9
+3	5.6	368.7
+7	5.2	369.1
E	5.4	368.9
+15	5.5	368.8
Dirt Floor		
5+39 = 2 Dble Garages on W 18' Back		
-5	4.7	369.6
F.	4.5	369.8
+6	4.6	369.7
E	4.5	369.8
+5	4.4	369.9
W	4.6	369.7
+1.8 on dirt floor	4.6	369.7

374.31		
5+80		
-1 at Bld.	3.8	370.5
W	3.8	370.5
E	4.0	370.3
+5	4.0	370.3
+9	3.8	370.5
E	3.3	371.0
+3	3.3	371.0
5+95		
S	3.0	371.3
E	3.0	371.3
+1	3.4	370.9
E	3.3	371.0
+7	3.4	370.9
W	3.5	370.8
L1	3.4	370.9
Cont. P-87		

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37431

Alley Bk. 66
Union Hts.

6+01 = South Line Monroe Ave

W top cb.	3.27	371.04
" on paving	3.39	370.92
2" "	3.44	370.87
1" "	3.19	371.12
E top cb.	3.14	371.17

chks
see P. 54

51.77

Hx 2 357.41
cb PC 255.0

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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