

1567



ENGINEERS'
FIELD BOOK
No. 410F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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2.3
4.7
5.3
10.0

1567

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface and is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.

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to b
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30.6

Polk St - Louisiana to Texas	
Beardsley - Logan to Kearney	-5
Alley Blk 6 Wilshire Pl	9
Garrison St. - Rosecrans to Willow	15
Evergreen - Garrison to Hugo	23
Hilltop Dr - W. of 45th	25
E St. - 27th to 28th	28
Topo. - Memorial School	34
Alley Blk 14, Hubbell	46
E St. Sewer - W of 28th	51
Ventura Pl - Mission Blvd. to Ocean Ft. Walk	52
Quimby - Willow to Plum	58

5-9-31 Miller
 2 Miller
 2 Miller
 Polk St. X. Sec. 14 obs. 13. 143
 Louisiana to Texas.
 S.M.B.P. 0.62 325.57 324.95 S.E. Texas
 & Polk

0+00 = W. line + Texas.

S. inside car, solid conc. R12.55	323.02
S ch. conc. dr	2.70 322.87
gutter = W. edge pav.	3.17 322.40
" " " "	2.58 322.99
" " " "	2.43 323.14
" " " "	2.54 323.03
gutter " " "	3.00 322.57
N. conc. dr. w. end	2.64 322.93
N. line = inside solid conc. R12.45	323.12

0+20

N	3.6 322.0
ch	3.5 322.1
+11	4.3 321.3
1/4	4.1 321.5
1/2	3.8 321.8
1/4	3.9 321.7
+12	4.8 320.8
ch	3.8 321.8
S.	3.2 322.4

Indexed
 c.s.K.

0+50 (Bliss. phoned. 6/1/39 J.L.M.)
 325.57

S	6.4 319.2
ch	6.6 319.0
+9	7.2 318.4
1/4	6.7 318.9
1/2	6.6 319.0
1/4	6.4 319.2
+11	7.1 318.5
ch	6.3 319.3
+13	6.3 319.3
N	7.0 318.6

0+83 = garage 0.5 S. of S. line

0.5 S. of S. line = floor 8.60 316.97

1+00

N	10.8 314.8
+12	10.5 314.8
ch	11.4 314.2
1/4	11.0 314.6
1/2	11.0 314.6
1/4	11.1 314.5
ch	11.3 314.3

325.57

ch		10.8	314.8
S		10.3	315.3
T.P.	0.95	313.55	12.97 312.60
1+18 = E. end. double garage - on N. conc. floor 2' back			
+	2.8 S of N Line	0.34	313.21
			S.E. cor conc apron
N. Line	Garage floor	0.30	313.25
			E. end conc apron
+	2.1 = N.E. cor apron	0.28	313.27
1+34			
S		0.6	313.0
712		1.6	312.0
ch		2.2	311.4
1/4		1.5	312.1
±		1.2	312.4
4		1.4	312.2
+11		1.7	311.9
ch		1.3	312.3
+11.2	S.W. cor apron	0.68	312.87
N = W. end. apron		0.45	313.10
+2.1 = N.W. cor. conc. apron		0.24	313.31

313.55

2

1+40 = E. Line Alley

N		1.5	312.1
ch		1.8	311.8
1/4		1.6	312.0
±		1.7	311.9
1/4		1.8	311.8
ch		2.2	311.4
S. ground		2.1	311.5
S. N.E. cor Alley Pav.		2.42	311.13
1+42 = E. Edge Storm Drain Box			
12' N. of ± = S.E. cor		1.88	311.67
17.8 N of ± = N.E. cor		1.93	311.62
147.6 = W. Edge Storm Drain Box			
12' N. of ±		2.13	311.42
17.8 " " "		2.11	311.44
1+50 ± Alley			
S. Line = N. End. Alley Pav.		2.84	310.67
1+60 = W. Line Alley			
S = N. W. Alley Pav		2.73	310.82

313.55
1+62.

S		2.5	311.1
eb		2.7	310.9
+2		3.7	309.9
1/4		3.0	310.6
±		2.1	310.5
1/4		3.1	310.5
eb		3.2	310.4
+4.2	S. edge e. End conc walk	2.97	310.58
+9.6	N. edge e. End "	2.88	310.67
N.	op conc walk	2.18	310.37
N. lawn to e	2+31.9	7.7	305.9
N. S. End. E. edge conc. Drive		8.56	304.99
+4.7	N. Edge W. End. conc walk	7.13	306.42
+10.0	S " " " "	7.20	306.35
eb		7.5	306.1
+2.		7.9	305.7
1/4		7.7	305.9
±		7.9	305.7
1/4		7.9	305.7
+10.		8.2	305.4
eb		7.4	306.2
S		7.4	306.2
+7.5	{N. End. 2' w of Garage Conc. floor}	6.98	306.59

313.55
2+43.

3

S		8.0	305.6
eb		8.5	305.1
+3.		9.1	304.5
1/4		8.6	305.0
±		8.5	305.1
1/4		8.4	305.2
eb		8.5	305.1
N. = W. edge S. End. conc. drive		8.77	304.78
	2+80		
N.		10.9	302.7
+5		10.3	303.3
eb		10.7	302.9
1/4		11.2	302.4
±		11.0	302.6
1/4		11.2	302.4
+9		11.6	302.0
eb		11.1	302.5
S		10.6	303.0

		313.55		
S		300 = 8. Line	Louisiana.	302.1
		11.5		
+5	E. End. S. Line	conc wall	11.82	301.73
+10	E. " N "	" " "	11.92	301.63
cancel	E. End	E. End	11.96	301.59
Gutter	par	E. End.	12.62	300.89
4y	" "	" "	12.24	301.31
Φ	" "	" "	11.96	301.59
4y	" "	" "	11.95	301.60
Gutter	" "	" "	12.41	301.44
N. cone.	ch.	44	11.49	302.06
+ 4	S. side cone.	walk.	11.38	302.17
+ 9	" "	" "	11.35	302.20
N.			11.2	302.4
		3 + 14 = 8	ch. Louisiana	
N	Par.		12.03	301.52
ch	"		12.20	301.35
114	"		11.98	301.57
Φ	"		11.98	301.57
114	"		12.23	301.32
ch	"		12.54	301.01
S	"		12.72	300.83

Plotted

		313.55		
T.P.		12.67	325.27	0.95
orig BM.				0.32
				324.950 ✓

5-7-39
 Beardley
 Logan
 to
 Kearney

Beardley St. X Sec.
 Logan to Kearney

Indexed
 c.s.k.

41.45 N.W. Logan &
 Beardley
 46.04 S.E. Beardley
 & Kearney

BM.			Indexed c.s.k.	
BM. B.P	2.69	48.73	46.04	
	00-14' = S. ch. Line Kearney			
E			3.32	45.41
+ 10 = ch			3.25	45.48
+ 20 = " "			3.06	45.67
+ 30 = E			2.98	45.75
+ 40 = " "			3.02	45.71
+ 50 = vch			3.25	45.48
+ 60 = W Line			3.41	45.32
	0100 = S. Line Kearney			
W ch			2.74	45.99
gutter = s. edge pav			3.34	45.37
" "			3.14	45.59
E			3.06	45.67
" "			3.26	45.47
gutter " "			3.55	45.18
E ch			2.88	45.85
		0+50		
G d			3.50	45.43
G			4.1	44.1

48.73

5

1/4		4.3	44.4
E		4.3	44.4
1/4		4.4	44.3
G		4.4	44.3
W ch		3.52	45.21
	1+00		
W ch		4.29	44.44
E		5.2	43.5
1/4		5.1	43.6
E		4.9	43.8
1/4		5.0	43.7
G		5.1	43.6
E ch		4.29	44.44
	1+402 on e) 1+405 " W side		
	W Line Alley Returns		
E. Line Alley pav.		4.82	43.91
E. ch. E end		4.70	44.03
E ch conc. ch		4.89	43.84
" " ground		5.6	43.1
1/4		5.6	43.1
E		5.6	43.1
1/4		5.7	43.0

w. ch	ground	5.6	43.1
" "	ch.	4.87	43.86
w.	ch. W. End.	4.64	44.09
w.	ground	5.1	43.6
$\left. \begin{array}{l} 1+60 \text{ g on e} \\ 1+60 \text{ 35 on w} \end{array} \right\} = \frac{S}{2} \text{ Line Alley Returns}$			
w.	dirt	5.2	43.5
w	ch. W. End	4.86	43.87
w. ch		5.17	43.56
G.		5.9	42.8
14		6.0	42.7
4		6.0	42.7
14		6.1	42.6
G		5.8	42.9
ch.		5.16	43.57
E	30. End. ch	5.02	43.71
E	35. side pav.	5.10	43.63

1+50 g on east = $\frac{S}{2}$ Alley to E.

E = W. End. pav. 5.22 43.51

Out of order.

E. ch		5.75	42.98
G		6.4	42.3
14		6.5	42.2
4		6.5	42.2
14		6.6	42.1
G		6.6	42.1
w ch		5.73	43.00

2+50

w. ch		6.50	42.23
G		7.3	41.4
14		7.3	41.4
4		7.2	41.5
14		7.1	41.6
G		7.0	41.7
E ch		6.52	42.21

2+75

E. ch		7.28	41.45
E. gutter N. End. open inlet		8.06	40.67
41.9 = " " " "		8.00	40.73
14		7.6	41.1
4		7.4	41.3

w. side

48.73

1/4	7.3	41.4	
W cone gutter in cone Drive	7.73	41.00	
3+01.1 N End open inlet. N. line began			
W cone gutter in drive	7.60	41.13	
G. in open inlet	8.00	40.73	
+1.9 E. " "	7.95	40.78	
+1.9 E. cl. " "	7.64	41.09	
1/4 pav. N Edge	7.33	41.40	
1/4 " " " "	7.35	41.38	
1/4 " " " "	7.37	41.36	
+8 = S. W. Cor Open inlet	7.24	41.49	Top. Wing wall " Head wall " Pav
+8.1 " " " " F.L.	8.50	40.73	
+10 = S. E. " " " F.L.	8.50	40.73	
+10 = E. cl.	7.33	41.40	
3+04.9			
S. cl. + pav.	7.30	41.43	
1/4 " "	7.36	41.37	
1/4 " "	7.31	41.42	
1/4 " "	7.38	41.35	
+7	7.31	41.42	Top. Wing wall Top. Head wall Top. Pav
+8 = S. E. Cor open inlet	7.12	41.61	
+8 F.L. " "	8.01	40.72	
1/4 " "			

48.73

W.G. = F.L. open inlet	8.01	40.74	
W. cl.	7.18	41.55	
14' S of N. Line = N. cl.			
W-15 Gutter	8.25	40.48	
W = F.L. outlet gutter	8.02	40.71	
W. Line Pav & cl.	7.27	41.46	outlet culvert
w cl.	7.45	41.28	cl + pav
1/4	7.43	41.30	
1/4	7.41	41.32	
1/4	7.41	41.32	
cl	7.38	41.35	
E. Pav & dr	7.25	41.48	
G. = F.L. intake	8.57	40.16	
+5 E. End open intake	8.07	40.66	
24' S. of N. Line			
-5	7.68	41.05	
E	7.65	41.08	
cl	7.60	41.13	
1/4	7.58	41.15	
1/4	7.58	41.15	
1/4	7.61	41.12	

ch 7.66 41.07

w 7.73 41.00

+16 8.12 40.61

32.7.5. of N. Line = N. Rail S.D.E. R.R.C.

W. Line 8.10 40.63

e 7.93 40.80

E. Line * 7.84 40.89

8-10-39
Miller
Walker
Bliss

X Sec. Alley Blk. 6 Wilshire Place

indexed
e.s.r.

+ HI - EI
S.W. El Cajon
41st Sts.

B.M. 6.08 370.50 364.42

25' S. of N = N. of Line El Cajon

W. ch 5.42 365.08

W. pav 5.97 364.53

± " 5.96 364.54

E " 5.95 364.55

E. ch 5.32 365.18

15' S. of N. Line

E ch 5.10 365.40

E pav 5.37 365.13

± " 5.68 364.82

W " 5.45 365.05

W ch 5.19 365.31

5' S. of N. Line N. End. good pav.

W. ch 5.01 365.49

W. pav N. End. 5.13 365.37

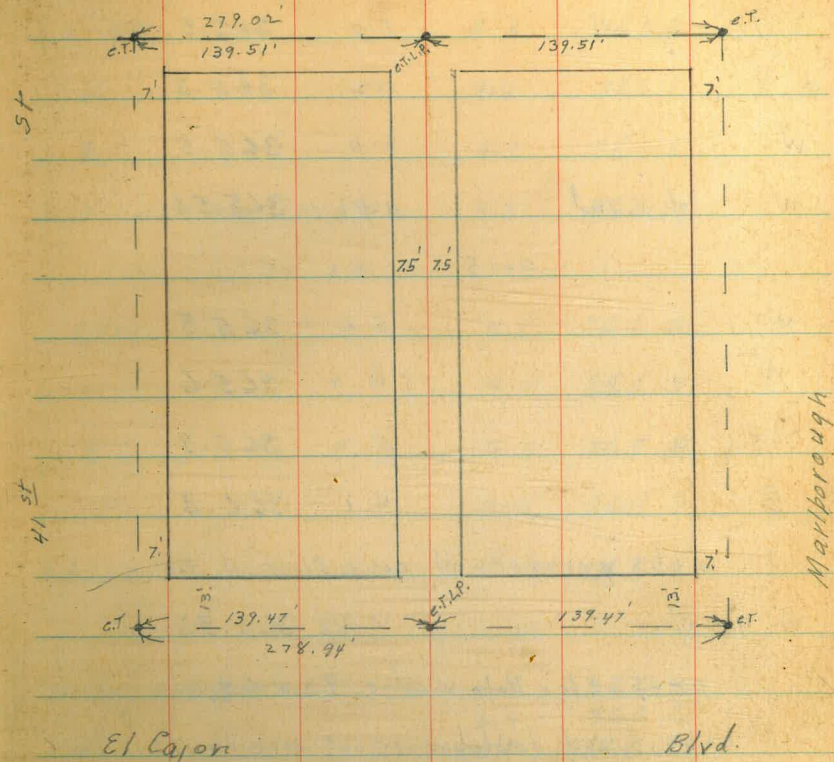
± " " " 5.37 365.13

E " " " 5.07 365.43

E. ch 4.90 365.60

Meade

Ave 9



370.50

0+15' w of E = ch. N. End	4.83	365.67
" " ground	5.0	365.5
±	5.2	365.3
W	5.0	365.5
W ch. N. End.	4.96	365.54
0+15		
W	5.0	365.5
±	4.9	365.6
+5	5.2	365.3
E	4.1	366.4
0+38 garage on W conc. floor 4' Back		
W-4' = floor.	4.67	365.83
0+45 Elec Pole w. edge 9.3 W of ±		
0+49 S. End. double garage one conc. floors 2.3 Back.		
E-2.3 = floor	4.62	365.88
E = w. edge conc. apron	4.67	365.83
±	4.5	366.0
W	4.7	365.8
+10	5.2	365.3
(S. End. Conc. Drive on E. Garage 2.3, 7' Back.		
0+74 N = N. End. above Garage on E.		
E-2.3 floor garage to S.	4.60	365.90
E = w. edge conc. apron	4.65	365.85

370.50

10

0+99 N. End. above cone. Drive on E.		
W-25.	5.3	365.2
W	4.4	366.1
±	4.4	366.1
0.15 E of E = cone Drive N.W. cor.		
4.31	366.19	
1+30		
E-10	4.5	366.0
E	4.5	366.0
±	4.7	365.8
W	4.8	365.7
+20.	5.2	365.3
1+50		
W-20. s. of garage	4.5	366.0
-10	3.9	366.6
W	4.5	366.0
±	4.6	365.9
E	4.7	365.8
+10	4.6	365.9
1+58 garage on W. Conc. floor 10' Back		
W-10' = floor	3.78	366.72
W-6' E conc. apron.	4.08	366.42

370.50

1+63

E-15	4.5	366.0
E	4.5	366.0
±	4.5	366.0
W	4.5	366.0
+10	4.1	366.4
+20 N. of garage	4.3	366.2

1+75

W-20	4.9	365.6
W	4.5	366.0
±	4.3	366.2
E	4.3	366.2
+20	4.5	366.0

1+77 E1-c Pole w. edge 10.2 w. of ±.

1+96

E-20	4.2	366.3
E	4.5	366.0
±	4.4	366.1
W	4.5	366.0
+20	4.8	365.7

370.50

2+00

11

W-20	4.8	365.7
W	4.5	366.0
±	4.4	366.1
+4	4.3	366.2
E	3.4	367.1

(N. edge 30" con. walk. on W.

2+27 } S. End. 3. garages. on w. conc. floors. 10' back.

E	3.5	367.0
+1.5	3.9	366.6
±	4.1	366.4
W	3.8	366.7
+6.0' } N.E. cor. conc. walk.	3.65	366.85
+10.0' } S.E. " " Apron.	3.38	367.12
+10.0' = floor of garage,	3.38	367.12
+20.0' = N. edge walk. S. of garage.	3.8	366.7

2+61 = N. End. above garage on W.

W-20' N of garage	4.4	366.1
W-10' floor.	3.38	367.12
W-6. N.E. cor conc. apron.	3.83	366.67
W	4.0	366.5
±	4.1	366.4
E	4.0	366.5
+20'	3.8	366.7

370.50

2+77

E-10'			3.9	366.6
E			4.0	366.5
±			4.2	366.3
W			4.3	366.2
+10.4	= w. edge Elec. Pole		4.4	366.1
+10'			4.7	.8
+20'			4.4	366.1
		2+98		
-20'			4.4	366.1
-10'			3.5	367.0
W			3.8	366.7
±			4.2	366.3
E			4.0	366.5
+10'			4.0	366.5
		3+00		
-20'			4.0	366.5
W			3.8	366.7
±			4.2	366.3
E			4.0	366.5
+10'			4.0	366.5
T. P.	6.19	372.66	4.03	366.47

372.66

12

3+12 garage on E. 18' Back

E-18'	floor		6.3	366.4
		3+42 garage on W. conc. floor	7.3' back	
W-7.3'	= floor		5.80	366.86
W-3.2'	= E. edge conc. apron.		6.00	366.66
		3+50		
E-10'			6.2	366.5
E			6.0	366.7
±			6.1	366.6
W			6.1	366.6
+20'			6.2	366.5
		3+76		
W-20'			6.0	366.7
W-2.0'	= W. side Elec. Pole			
W			5.9	366.8
±			6.1	366.6
E			6.0	366.7
+10'			6.1	366.6

372.66

-10'	4+00	5.8	367.1
E		5.9	366.8
±		5.9	366.8
W		5.7	367.0
+10'		5.8	366.9
	4+50		
-10'		5.6	367.1
W		5.7	367.0
±		5.8	366.9
E		5.8	366.9
+10'		5.6	367.1
	5+00		
-10		5.2	367.5
E		5.2	367.5
±		5.3	367.4
W		5.3	367.4
+2. = W. edge Elec Pole W. edge		5.3	367.4
+10		5.3	367.4
5+08 garage on W. conc. floor 9.2' Back.			
W-9.2 = floor		4.91	367.75
W-1.5 = conc. apron.		5.15	367.51

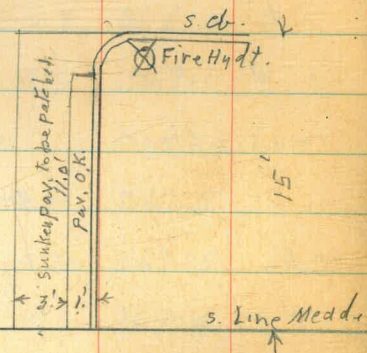
372.66

5+24 garage on E conc. floor	4.1' Back	13
W-10.	4.9	367.8
W	5.0	367.7
±	5.1	367.6
+6	5.0	367.7
E = W. edge conc. apron.	5.23	367.43
+4 = floor	5.21	367.45
5+42 garage on W conc floor 4.5' Back		
E-5'	5.0	367.7
E	4.8	367.9
±	5.0	367.7
W	4.6	368.1
+4.5 = floor	4.51	368.15
	5+60	
-5'	4.9	367.8
W	4.9	367.8
±	5.0	367.7
E	4.6	368.1
+10'	4.8	367.9
	5+95	
E	4.9	367.8
±	5.2	367.5
W	5.0	367.7

372.66

6+07³ = S. Line Meade Ave

W. cone. ch	S. End	5.30	367.96
W. Pav.	" "	5.49	367.27
± " OK.	" "	5.73	366.93
+3.11 OK	" "	5.72	366.94
+4.511 Sunken Ditch	" "		
+6.11 O.K.	" "	5.70	366.96
+7.411 OK	" "	5.67	366.99 ^v
+7.4 ch	" "	5.47	367.29



T.P. 4.89 372.08 5.47 367.19

372.08

15' N. of S. = S. ch. Line Meade 14

E-25.9 pav.	5.50	366.58
E " "	5.39	366.69
E. ch	4.97	367.11
±	5.34	366.74
W G. pav	5.25	366.80
+35. " "	5.05	367.03

chk. BM.

4.06 366.02

N.W. Meade
4 Marlborough
= 366.04

10-2-39
miles
walk
Bliss

Garrison St. X Sec. Rosecrans to Willow.
70' wide, 18' ds. - 2.5' conc. gutters. 7.25 1/4 s.

BM. — 7.89 — 9.04 — 1.15 — S.W. Garrison & Rosecrans.

0+00 = W. Lin. Rosecrans.

8.5. of s. d. = E. End. ch. Ret.	7.94	1.10	conc. d.
" " " "	6.7	2.3	ground
s. ch. line	8.1	0.9	
1/4	7.9	1.1	
1/2	7.7	1.3	
3/4	8.0	1.0	
N. ch.	8.2	0.8	
+8 E. End. conc. d. Ret.	7.77	1.27	
+8 ground.	7.4	1.6	

see New notes
Book 583/66

Reduced Plot
Profile 1169 10-7-39
CSH

0+27 = P.C. 43' d. Rad. Gutter dipped N.E.

N. ch. & ground.	7.21	1.83	
+1 conc. gutter E. End.	8.35	0.69	dipped
+2.5 ground	7.3	1.7	
1/4	7.1	1.9	
1/2	7.0	2.0	
3/4	7.1	1.9	
+7 ground.	7.5	1.5	
+8 conc. gutter E. End	8.56	0.48	dipped
s. conc. d.	7.30	1.74	

Indexed
c.s.K.

9.04

0+31 Gutter O.K.

s. d.	7.19	1.85	15
Gutter	7.95	1.09	
Gutter Lip.	7.84	1.20	
1/4	7.1	1.9	
1/2	6.9	2.1	
3/4	7.0	2.0	
+7. ground	7.24	1.76	
G. Lip.	7.60	1.44	
G.	7.85	1.19	
N. ch.	7.04	2.00	
No walk in this Block on S. 1+00 = E. End. conc. walk on N			
N. ch.	4.99	4.05	
G.	5.85	3.19	
G. Lip.	5.71	3.35	
1/4	5.1	3.9	
1/2	5.0	4.0	
3/4	5.2	3.8	
G.L.	5.66	3.38	
G.	5.80	3.24	
s. d.	4.98	4.06	

9.04

1+50

S. db	3.49	5.55
G.	4.33	4.71
G.L.	4.13	4.91
1/4	3.8	5.2
ϕ	3.8	5.2
1/4	3.9	5.1
G.L.	4.17	4.87
G.	4.31	4.73
N. db	3.49	5.55

2+00 = W. End cone walk on N

H. db	1.98	7.06
G	2.81	6.23
G.L	2.65	6.39
1/4	2.3	6.7
ϕ	2.3	6.7
1/4	2.4	6.6
G.L.	2.64	6.40
G.	2.79	6.25
S. db	1.96	7.08

9.04

2+50

Garrison

16

S. db	0.47	8.57
G.	1.31	7.73
G.L.	1.20	7.84
1/4	1.0	8.0
ϕ	0.9	8.1
1/4	1.0	8.0
G.L	1.25	7.79
G.	1.39	7.65
N. db	0.53	8.51

2+3: gutter regular.

N. db	0.13	8.91
G.	0.94	8.10
G.L.	0.83	8.21
1/4	0.7	8.3
ϕ	0.6	8.4
1/4	0.6	8.4
G.L.	0.76	8.28
G	0.88	8.16
S. db	0.09	8.95

T.P. 12.45 21.07 0.42 8.62

21.07
 2 + 75 } p.c. 43. d Returns.
 E. End. Culvert crossing Locust 10' conc. Pipe

s. cl	11.78	9.29	
± G dipped to F.L. Culvert.	13.05	8.02	
G.L. { Winywall ground.	11.88	9.19	
"	12.2	8.9	
±	12.2	8.9	
"	12.3	8.8	
G	11.86	9.21	
± G. dipped to F.L. Culvert.	13.14	7.93	
N. cl	11.87	9.20	
3+00 = E. Line Locust st.			
N. cl. - 8' = cl. Return + ground	11.13	9.94	
N. cl. Line ground	11.3	9.8	
"	11.5	9.6	
±	11.5	9.6	
"	11.5	9.6	
s. cl Line ground	11.3	9.8	
s. cl + 8' = ground.	10.9	10.2	?
s. cl + 8' = cl. Return	11.15	9.82	
3+10			
18' S of s. cl = S. Line	11.04	10.03	Sly. End. conc. cl.
s. cl Line ground	10.6	10.5	

21.07

Garrison

"	11.7	10.0	17
±	11.1	10.0	
"	11.1	10.0	
N. cl Line	10.8	10.3	
N. line ground.	10.3	10.8	
N " = Nly. End conc. cl.	11.12	9.95	
3+35 = ± Locust			
N	9.7	11.4	
cl	10.2	10.9	
"	10.0	11.1	
±	10.1	11.0	
"	10.0	11.1	
cl	10.0	11.1	
S,	10.0	11.1	
3+60			
S. Line = sly End. conc. cl.	9.0	12.1	↔
" ground.	9.96	11.11	↔
s. cl Line "	9.5	11.6	
"	9.4	11.5	
±	9.6	11.5	
"	9.6	11.5	

21.07

N. cl	3+60 9.8	11.3
N. Line N. by End conc. Return	9.98	11.09
" " ground to S.	9.7	11.4
3+70 = 0+00 = w. line Locust.		
8' N. of N. cl = conc. cl. return	9.68	11.39
" " " " dirt.	9.7	11.4
N. cl. Line	9.6	11.5
"4	9.3	11.8
⊕	9.3	11.8
"4	9.3	11.8
S. cl. Line	9.3	11.8
+ 8. dirt.	8.9	12.2
+ 8. conc. cl. Ret.	9.63	11.44
PI ds. ^{0+26.2} } W. End. Culverts on N + S. gutters 0+25.5		
cl. + Walk. in both sides. Bet. Locust & Evergreen		
S. cl. Headwall basted	8.59	12.48
+ 1 ⊕ G. F.L. 10" Culvert	9.81	11.26
G. L. = Top Headwall	8.58	12.49
"4	8.6	12.5
⊕	8.4	12.7
"4	8.4	12.7

21.07

Garrison

G. L.	8.54	12.51	13
⊕ G. F.L. 10" Culvert	9.80	11.27	
N. cl.	8.60	12.47	
- 0+30 regular gutter			
N. cl.	8.39	12.68	
G	9.22	11.85	
G. L. 1P.	9.06	12.01	
"4	8.2	12.9	
⊕	8.3	12.8	
"4	8.4	12.7	
G. L.	8.99	12.08	
G.	9.14	11.83	
S. cl.	8.36	12.71	
1+00			
S. cl.	4.64	16.43	
G.	5.50	15.57	
G. L. 1P.	5.33	15.74	
"4	5.0	16.1	
⊕	4.8	16.3	
"4	4.9	16.2	
G. L.	5.35	15.92	
G.	5.46	15.61	
N. cl.	4.61	16.46	

	21.07	1+50
N. dr.	1.93	19.04
G.	2.75	18.32
G. Lip.	2.62	18.45
1/4	2.1	19.0
⊕	2.1	19.1
1/4	2.2	18.9
G. Lip.	2.72	18.35
G.	2.82	18.25
S. dr.	2.00	19.07

T.P. — 12.76 — 33.57 — 0.26 — 20.81 —

2+00

S. dr.	11.81	21.76
G.	12.65	20.92
G. L.	12.49	21.08
1/4	12.2	21.4
⊕	12.2	21.4
1/4	12.1	21.5
G. L.	12.43	21.14
G in drive	12.62	20.95

	33.57	Garrison.
N. dr.	2+62 = w. End regular gutter	8.45 25.12 19
G.		9.27 24.30
G. L.		9.17 24.40
1/4		8.9 24.7
⊕		8.8 24.8
1/4		8.8 24.8
G. L.		9.11 24.46
G.		9.24 24.33
S. dr.		8.27 25.30

2+75 = P.C. 43' Curb Radius
E. End 10" conc. Pipe Culverts outlets on S+W Gutter

S. dr.	7.86	25.71
⊕ gutter dipped = Fl. 10" culvert	9.11	24.46 outlet
Head wall busted		
L. G = wing wall	7.90	25.67
1/4	8.1	25.5
⊕	8.1	25.5
1/4	8.2	25.4
G. Lip ground. WW. + H. W. base!	8.4	25.2
⊕ gutter dipped Fl. 10" culvert	9.08	24.49 outlet
N. dr.	7.78	25.79

33.57

3+00 = B. Line Evergreen.

8' N of N. cl. Line = conc. cl.	6.70	26.87
G	7.1	26.5
N. cl. Line	6.8	26.8
"	6.7	26.9
⊕	6.8	26.8
"	6.8	26.8
S. cl. Line	6.8	26.8
8' S = conc. cl. Ret.	6.69	26.88

3+10

S. Line {S. End conc. cl. } Sly Line } cl + ground.	6.39	27.18
S. cl. Line	6.1	27.5
"	6.4	27.2
⊕	6.4	27.2
"	6.3	27.3
N. cl. Line	6.4	27.2
Gutter	7.0	26.6
Nly line Top. cl.	6.39	27.18

3+18

N Line	6.7	26.9
cl	6.1	27.5
"	6.1	27.5

33.57

Garrison.

20

⊕	6.1	27.5
"	6.2	27.4
cl Line	6.1	27.5
Sly line	5.6	28.0
3+35 = ⊕		
Sly line	5.6	28.0
cl	5.6	28.0
"	5.6	28.0
⊕	5.6	28.0
"	5.6	28.0
cl	5.8	27.8
Nly line	6.2	27.4

3+60

Nly line Top cl	5.44	28.13
conc. G.	6.24	27.33
+3.7 G.L.	6.03	27.54
cl. line	5.0	28.6
"	4.9	28.7
⊕	4.8	28.8
"	4.9	28.7
cl. line	4.6	29.0
S " ground.	4.8	28.8
B " Sly. End conc. cl.	5.50	28.07

	33.57	
0+00 = 3+70 = Wly Line Evergreen		
8' sly sly oblique on e. ch Return	4.96	28.61
9 " " " " ground	4.1	29.5
ch line	4.8	28.8
1/4	4.6	29.0
1/4	4.6	29.0
1/4	4.4	29.2
ch Line	4.8	28.8
+4.8 = G, Lip.	5.55	28.02
+8 = G.	5.75	27.82
+8 = cone ch Return	4.97	28.60
0+25 = { F.C. 43' R. ch. Ret. Wly End. 10" cone. Culverts on S. & N. Gutters		
Nly ch	3.49	30.08
+1 = 1/4 gutter, FL inlet	4.70	28.87
+2.5 = G. L. ground, H wall busted	3.6	30.0
1/4	3.4	30.2
1/4	3.2	30.4
1/4	3.3	30.3
G. L. H.W. ok	3.53	30.04
1/4 gutter dipped FL 10" pipe	4.75	28.82
sly ch.	3.54	30.03

Nowalk. on S. bet Evergreen & 0+98.2

	33.57	
0+33.2 = Gutter regular. Garrison		
sly ch	2.90	30.67
G.	3.66	29.81
G.L.	3.60	29.97
1/4	2.9	30.7
1/4	2.9	30.8
1/4	2.9	30.7
G.L.	3.64	29.93
G.	3.75	29.82
Nly ch.	2.91	30.66
chk. BMBP SW. Garrison & Evergreen	3.47	30.10 OK.
T.P. — 12.22 — 45.46 — 0.33 — 33.24 —		
0+75		
Nly ch	11.78	33.68
G	12.59	32.87
G.L.	12.50	32.96
1/4	12.2	33.3
1/4	12.0	33.5
1/4	12.1	33.4
G.L.	12.56	32.90
G	12.63	32.83
sly ch	11.82	33.64

45.46 ✓
1+25

slly cl	8.11	37.35
G.	8.93	36.53
G.L.	8.82	36.64
ly	8.6	36.9
⊕	8.5	37.0
ly	8.6	36.9
G.L.	8.87	36.59
G	8.98	36.48
Nly cl	8.15	37.31

1+75

Nly cl	4.45	41.01
G.	5.32	40.14
G.L.	5.22	40.24
ly	4.9	40.6
⊕	4.7	40.8
ly	4.9	40.6
G.L.	5.73	40.33
G	5.24	40.22
slly cl	4.46	41.00

?
3+00³
3+00³ wly End cone walk on N.

45.46 ✓
2+25

Garrison.
22

slly cl	0.75	44.71
G.	1.58	43.88
G.L.	1.45	44.01
ly	1.3	44.2
⊕	1.1	44.4
ly	1.2	44.3
G.L.	1.66	43.80
G.	1.78	43.68
Nly cl	0.95	44.51

T.P. — 8.68 — 53.85 ✓ — 0.29 — 45.17

2+75 = P.C. 43i R. cl. Ret.

Nly cl	5.57	48.28
G.	6.38	47.47
G.L.	6.24	47.61
ly	6.0	47.8
⊕	6.0	47.9
ly	6.2	47.7
G.L.	6.35	47.50
G	6.53	47.32
slly cl	5.61	48.24

53.85 ✓

Garrison

3+00 = Ely Line

8' S of Sly ch line = ch. Ret.	3.96	49.89
G	4.75	49.10
G.L.	4.70	49.15
Sly ch Line Ely edge pav	4.65	49.17
" " "	4.64	49.21
" " "	4.65	49.20
" " "	4.64	49.21
Nly ch Line " " "	4.77	49.08
+5' G.L.	4.86	48.99
+8' G	4.91	48.94
8' N of N. ch = ch. Ret.	4.09	49.76

Reduced Plot
Profile 1164 - cont

S.W. Garrison
chk. B.M. B.P. & Willow 2.40 51.45 ✓ O.K.

Indexed
C.S.K.

d.w. walk. Both sides 2.5' con. E. on W. None one.

B.M. B.P. 2.88 32.98 ✓ 30.10 S.W. Garrison & Evergreen

0+00 = Nly Line Garrison

8' E of E. ch Line = cone. ch	5.80	27.18
dirt G	6.4	26.6
Ely ch Line	6.0	27.0
" "	5.7	27.3
" "	5.5	27.5
" "	5.5	27.5
Wly ch line	5.5	27.5
G. Lin.	5.56	27.42
G.	5.66	27.32
8' W of Wly ch line = ch. Ret.	4.94	28.14

0+25 = P.C. 43. R. ch. Ret.

Wly ch	5.25	27.73
G	6.05	26.93
+2.5 = G.L.	5.91	27.07
" "	5.9	27.1
" "	5.9	27.1
" - 9.75' W of E. ch	6.2	26.8
2.5' W of E. ch.	6.7	26.3
G	6.9	26.1
Ely ch.	6.23	26.75

32.94
+00

Ely ch	6.94	26.04
G.	7.3	25.7
+2.5	7.1	25.9
"4	6.8	26.2
⊕	6.3	26.7
"4	6.3	26.7
G.L.P.	6.33	26.65
G.	6.47	26.51
Wly ch.	5.68	27.30

1+75 P.C. +3' Rad

Wly ch	6.03	26.95
G	6.88	26.10
G.L.	6.71	26.27
"4	6.8	26.2
⊕	7.1	25.9
"4	7.4	25.6
2.5 W of	7.8	25.2
G. dirt	7.9	25.1
Ely	7.57	25.41

32.98

2+00 = sly. Line - Hugo St.

8' E of E ch. line = ch. Ret	8.04	24.92
G dirt.	8.4	24.6
+2.5	8.1	24.9
E ch. Line	8.0	25.0
"4	7.5	25.5
⊕	7.0	26.0
"4	6.8	26.2
Wly ch Line	6.6	26.4
G.L.	6.82	26.16
G.	7.04	25.94
8' W of Wly ch = ch. Ret.	6.21	26.77

24

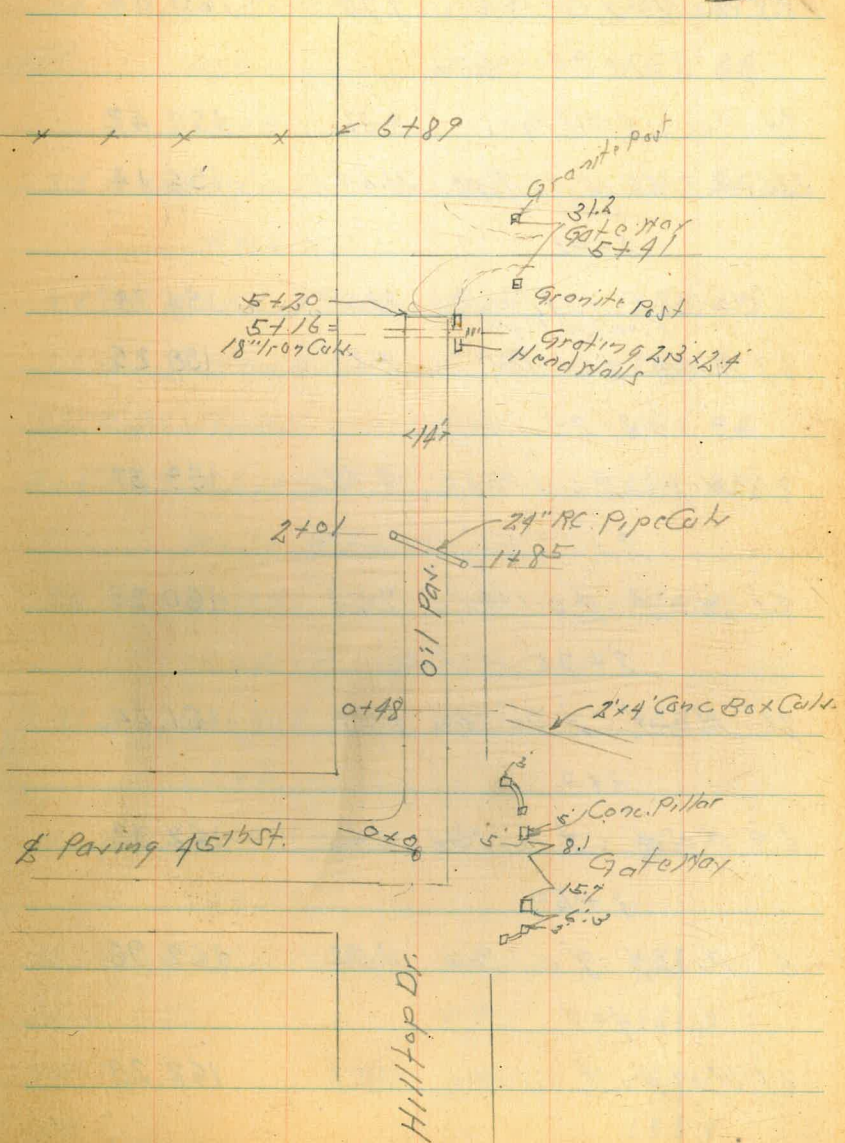
Reduced Plat. Profile 1136
C.B.H. 10-9-39

Hilltop Drive
Levels of Oil Paving West of 45th St

BM	8.33	167.18	158.85	N.M. BP Marked +45th
TP	2.66	166.48	3.26	163.82
TP	2.01	167.78	0.71	165.77
0+10 = E Edge Pav.				
1/2		3.90		163.88
33.5' N of Conc. Base Pillar	4.33			163.45
0+40				
5' N of 1/2 of Oil Pav.	4.38			163.40
0+81				
5' N of 1/2 of Oil Pav.	4.62			163.16
33.5' N of Conc. Base Pillar	4.31			163.47
0+48				
63' N of 1/2 of Oil Pav.	5.56			162.22
22' N of F.L. 2x4 Conc. Box Culvert	7.83			159.95
Top Box Culvert	5.34			162.44
0+75				
6.7' N of 1/2 of Oil Pav.	6.31			161.47
1+0				
7.4' N of 1/2 of Oil Pav.	6.89			160.89

Indexed
C.S.K.

Nov. 15-39
Sisson
Northway 25
Osborne



167.78

1+50

8.8 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 7.74 160.04

1+85

8.4 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 8.36 159.4222.6 H = N.E. 24" RC Pipe
Culvert 11.64 156.14

2+01

8.5 = So. End 24" Org Iron
Flowerbed Pipe 13.00 154.788.7 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 8.53 159.25

2+25

8.8 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 8.41 159.37

2+50

8.1 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 7.53 160.25

2+75

7.6 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 6.34 161.44

3+0

6.9 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 5.46 162.32

3+50

6 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 4.82 162.96

4+0

6.1 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 5.50 162.28

167.78

26

4+50

7.4 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 6.57 161.21

TP 6.20 5.22 162.46

5+0

8.4 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 7.24 160.54

5+16

8.4 S of $\frac{1}{2}$ " = F.L. 18" Iron Culv 9.33 158.458.6 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 6.97 160.8123.5 H of $\frac{1}{2}$ " = Top H.H. 6.94 160.8423.5 H of $\frac{1}{2}$ " = F.L. 18" Culv 8.96 158.82

5+20 = N End Oil Pav

8.6 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Oil Pav 6.97 160.815+41 = $\frac{1}{2}$ " Gate Way on N39 H of $\frac{1}{2}$ " on dirt 5.8 162.0

6+0

11 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Dirt Road 6.1 161.7

6+39

11 H of $\frac{1}{2}$ " = $\frac{1}{2}$ " Dirt Road 4.5 163.3

25.5 " " 5.9 161.9

7.5 " " 7.7 160.1

12.5 " " 8.5 159.3

167.78

6889 = Fence from So.

11' N of z Dirt Road	1.7	166.1
25' S of z	1.3	166.5
75' S	2.7	165.1
125' S	4.4	163.4

27

188.89

1+0

NCb Top	1.01	187.88
Gutter	1.5	187.9
1/4	2.1	186.7
1/2	2.4	186.5
1/4	2.7	186.2
Gutter	2.7	186.2
SCb Top	2.08	186.81

1+20

SCb Top	1.24	187.65
Gutter	2.0	186.9
1/4	2.1	186.8
1/2	1.8	187.1
1/4	1.4	187.5
Gutter	0.9	188.0
NCb Top	0.25	188.62

1+40

NCb Top	+0.09	188.98
Gutter	0.6	188.3
1/4	1.2	187.7
1/2	1.4	187.5

188.89

29

1/4	1.8	187.1
Gutter	1.7	187.2
SCb Top	0.73	188.16
	1+60	
SCb Top	1.27	187.62
Gutter	2.2	186.7
1/4	2.1	186.8
1/2	1.8	187.1
1/4	1.7	187.2
Gutter	1.4	187.5
NCb Top	0.43	188.96
	1+80	
NCb Top	1.73	187.16
Gutter	2.6	186.3
1/4	3.0	185.9
1/2	3.0	185.9
1/4	3.4	185.5
Gutter	3.5	185.9
SCb Top	2.68	186.21

✓
188.89

270

SCb Top	4.57	189.32
Gutter	5.2	183.7
"/4	4.8	189.1
1/2	4.5	189.9
"/4	4.6	189.3
Gutter	4.5	189.9
NCb Top	3.70	185.19

2450

NCb Top	8.76	180.13
Gutter	9.6	179.3
"/4	9.6	179.3
1/2	9.4	179.5
"/4	9.6	179.3
Gutter	10.5	178.9
SCb Top	9.84	179.05
TP	0.41	176.40
	12.90	175.99

370

SCb Top	3.32	179.08
Gutter	3.4	173.0
"/4	2.9	173.5

✓
176.40

30

1/2 0.7 MH Rim	2.22	179.18
"/4	2.7	173.7
Gutter	2.5	173.9
NCb Top	1.44	179.96
	3750	
NCb Top	8.16	168.29
Gutter	8.8	167.6
"/4	9.4	167.0
1/2	9.2	167.2
"/4	9.5	166.9
Gutter	9.9	166.5
SCb Top	9.06	167.39
TP	0.28	163.99
	7.40	12.69
		163.71
SCb Top	3.37	160.62
Gutter	4.2	159.8
"/4	3.9	160.1
1/2	3.7	160.3
"/4	3.9	160.1
Gutter	3.2	160.8
NCb Top	2.40	161.59

16399 ✓

4+50

MCb Top	9.14	159.85
Gutter	9.8	159.2
1/4	10.4	153.6
1/2	10.4	153.6
1/4	10.7	153.3
Gutter	10.8	153.2
SCb Top	10.18	153.81
S.L.	10.4	153.6
TP	6.85	158.52
	12.32	151.67

4+75

-25	18.7	139.8
-15	17.8	141.2
S.L.	8.0	150.5
Cb Top	8.00	150.52
Gutter	8.0	150.5
1/4	7.9	150.6
1/2	7.8	150.7
1/4	7.8	150.7
Gutter	7.7	150.8

15852 ✓

31

Cb Top	7.22	151.30
H	7.4	151.1
+10	12.7	145.8
+15	13.2	145.3
	5+0	
-30	20.0	138.5
-23	20.0	138.5
H.L.	9.3	149.2
Cb Ground	9.5	149.0
Cb Top	10.12	148.40
1/4	9.4	149.1
1/2	9.3	149.2
1/4	9.3	149.2
Cb Ground	9.3	149.2
Cb Top	11.13	147.39
+7	8.9	149.6
5	10.7	147.8
+17	20.5	138.0
+25	22.6	135.9

158.52

5+25

-25	25.0	133.5
-17	22.6	135.9
S.L.	12.7	145.8
+5	9.1	149.9
Cb Ground	9.9	148.6
Cb Top	11.87	146.65
1/4	10.4	148.1
1/2	10.3	148.2
1/4	10.3	148.2
Cb Ground	9.5	149.0
Cb Top	10.88	147.69
H	9.5	149.0
+20	20.3	138.3
+30	21.8	136.7

5+49

-20	24.0	139.5
-20 = FL 30' Drain	21.2	137.2
H.L.	10.2	148.3
+9	9.5	149.0

158.52

32

Cb Top	10.79	147.73
Gutter on Grating	11.61	146.91
1/4	10.9	147.6
1/2	10.7	147.8
1/4	10.9	147.6
+5	11.1	147.9
Gutter on Grating	12.43	146.09
Cb Top	11.61	146.91
+1	10.2	148.3
+8	10.4	148.1
S.L.	11.4	147.1
+20 = FL 30' Drain	27.5	131.0
+30	27.8	130.7

5+75

-20	17.5	141.0
S.L.	9.4	149.1
+8	9.2	149.3
Cb Top	10.06	148.96
Gutter	10.1	148.9
1/4	9.6	148.9
1/2	9.5	149.0

158.52

1/4	9.8	148.7
Gutter	10.1	148.9
Cb Top	9.45	149.07
H	9.3	149.2
+20	20.4	138.1
+30	20.6	137.9
670		
H	6.9	151.6
Cb Top	6.95	151.57
Gutter	7.6	150.9
1/4	7.2	151.3
2	6.9	151.6
1/4	7.0	151.5
Gutter	7.7	150.8
Cb Top	7.38	151.19
+8	7.2	151.3
S	6.4	152.1
6740.7 = 1/2 28 1/2 51		
S	1.4	157.1
Cb Top	1.41	157.11
Gutter	2.5	156.0

158.52

33

1/4	2.2	156.3		
2	2.0	156.5		
1/4	2.5	156.0		
Gutter	2.2	156.3		
Cb Top	0.99	157.53		
H	1.0	157.5		
6750.7 = 1/2 Cb 28 1/2 51				
H	0.9	157.6		
Cb	1.0	157.5		
Gutter	1.8	156.7		
1/4	1.6	156.9		
2 on M.H. Rim	1.24	157.28		
1/4	1.5	157.0		
Gutter	1.8	156.7		
+4	1.1	157.4		
S	1.0	157.5		
TP	12.32	170.32	0.53	157.99
TP	12.81	183.00	0.13	170.19
TP	6.26	188.75	0.51	182.49
BM		8.72	180.03	180.01
S.H. 8P E+37 1/2 51				

Topographical Survey Memorial School
 Grounds. Between Nancy & Ocean View Blvd
 30th and West. See sketch Page 34. This book.

B.M. N.E. 8 p. 29 th and Ocean View Blvd	+	x	-	Elev
	2.06	99.51		97.45
	1.97	88.49	12.99	86.52
Section A: 0+00 SW Prop Cor. 30 th Ocean View				
17' North in Gutter Ocean View			1.1	87.4
14' North Topch Ocean View Blvd			0.5	88.0
14' East Gutter			1.3	87.2
14' East Topch 30 th			0.5	88.0
0+00 Ground			0.3	88.2
0+00 Sidewalk on Ocean View			0.2	88.3
0+00 " " 30 th			0.3	88.2
50' South			2.2	86.3
100 S. Top Ch N Line Hampton Ct.			3.8	84.7
Gutter on Parking			4.5	84.0
125 S Topch on South Line Hampton Ct.			4.9	83.7
Gutter			5.5	83.0
150 S			5.7	82.8
200 S			7.2	81.3
250 S			9.4	79.1
250 S - 40 West			9.1	79.4
" " 45 "			8.1	80.4
300 S			11.0	77.5
300 S - 45 West			10.3	78.2
331.5 S. Top Ch N Line Valle Ct			12.0	76.5
" Gutter			12.5	76.0

1265		T		
		88.99		
345 S		12.5	76.00	
345 S 35 West		11.8	76.7	
345 S 45 "		10.4	78.1	
345 S 50 "		11.0	77.5	
350 S 33 West		12.1	76.4	
352 S 35 "		10.0	78.5	
352 S 20 "		12.5	76.0	
356.3 South Top Ch S Line Valle Ct		12.7	75.8	
" " " Gutter		13.2	75.5	
356.3 " 10' West		12.5	76.0	
360 S		12.4	76.1	
360 S 10 West		10.7	77.8	
360 S 25 "		9.5	79.0	
360 " 50 "		10.0	78.5	
400 " Gutter of 30 th		14.5	74.5	
400 South Top Ch " St		14.0	74.5	
400 " 0' Ground		13.6	76.0	
400 " 2 West		12.5	76.0	
400 " 15 "		11.4	77.1	
400 " 30 "		10.7	77.8	
400 " 50 "		10.2	78.3	
T.P	1.40	80.27	9.62	78.87

T
80.27

470 S.		6.6	73.7
470 "	2' West	5.4	74.9
470 "	9' "	4.1	76.2
470 "	50 "	3.6	76.7
485 "		6.8	73.5
" "	6 West	6.4	73.9
" "	14 "	4.4	75.9
500 S.		6.9	73.4
" "	6 West	5.9	74.4
	20 "	4.6	75.7
550 S.		8.2	72.7
" "	3 West	8.2	72.1
" "	" "	5.9	74.4
" "	25 "	6.2	74.1
" "	50 "	5.3	75.0
563 S Topch	N Line Holly Ct	7.8	72.5
	Gutter	8.4	71.9
563 S.	10 West	8.5	71.8
	25 "	8.0	72.3
	40 "	6.4	73.9
	50 "	6.5	73.8

T
80.27

36

588 South Top Ch	S. Line Holly Ct.	8.2	72.1
	Gutter on Pav 109	8.6	71.7
600 S.	in Gutter of 30 th	9.3	71.6
" "	Top Ch 30 th	8.6	71.7
" "	on Ground	8.4	71.9
600 S.	15' West	8.3	72.0
	50 "	7.2	73.1
650 S.		9.1	71.2
" "	25' West	8.5	71.8
" "	32 "	7.4	72.9
" "	50 "	7.4	72.9
680 S		9.1	71.2
	10 West	7.9	72.4
	50 "	6.6	73.7
700 S.		9.4	70.9
	3' West	7.7	72.6
	30 "	7.0	73.3
	50 "	6.1	74.2
793' South		7.8	72.5
	3' West	5.9	74.4
	50 "	5.5	74.8

7
8027

794.85	TopCb	N Line Martin Ct	79	72.4
" "	in Gutter on Paring		85	71.8
800.S.			85	71.8
	8' West		7.7	72.6
	15 "		6.7	73.6
	50 "		6.1	74.2
816.S.			8.8	71.5
	15'		8.4	71.9
	50'		6.1	74.2
8419.8	TopCb	S Line Martin Ct.	7.6	72.7
" "	Gutter on Paring		8.2	72.1
8422			7.5	72.8
"	2' West		5.6	74.7
	50 "		5.3	75.0
8.40			7.3	73.0
	2' West		5.8	74.5
	25 "		4.5	75.8
	50 "		5.0	75.3
900.S.			6.6	73.7
	4' West		5.0	75.3

7
8027

37

925.S.			6.5	73.8
	2' West		5.2	75.1
	25 "		5.6	74.7
	50		5.6	74.7
935.S.			6.3	74.0
	2' West		5.1	75.2
	21		5.1	75.2
	25		4.3	76.0
1000'S.			5.2	75.1
	2' West		4.6	75.7
	50 "		3.7	76.7
1026.S. TopCb		N Line Greeley Ct.	4.9	75.4
	Gutter		10.4	69.9
1026 Ground			5.0	75.3
	50' West		4.6	75.7
	60 "		5.5	74.8
1051			5.0	75.3
1051.S.	50' West		5.1	75.2
" "	on TopCb	S Line Greeley Ct	4.5	75.8
" "	in Gutter on Paring		5.1	75.2
" "	" "	30 th	5.5	74.8
" "	TopCb on "		4.7	75.6

1055 S			4.5	75.8
	50 West		3.7	76.6
1100 S			4.9	75.4
	50 West		4.9	75.4
1200 S			5.9	74.4
	15 West		5.3	75.0
	50 West		6.3	74.0
1259 ^E S			6.5	73.8
	50 West		6.7	73.6
N Top Cl Marcy St			6.6	73.7
	Gutter on Pavement		7.4	72.6
TD	5.97	81.44	4.80	75.97
Section B 100' West of 30 th				75.77
1259 ^E S = N Line Marcy			8.7	72.7
1200 S			8.0	73.4
1150 S			7.5	73.9
	25 E		6.9	74.5
1125			6.3	75.1
	25 East		6.0	75.4
1100			6.1	75.3
	25 West		7.1	74.3

1060 S			6.4	75.0
1050 S			7.1	74.3
1030 S			7.0	74.4
1025			6.3	75.1
1000			5.6	75.8
935 S			5.4	76.0
930 S			6.3	75.1
920 S			6.5	74.9
910			5.5	75.9
900 S			5.4	76.0
822 S			5.9	75.5
822 S	50 West		5.7	75.7
818 S			6.8	74.6
818 S	50 "		6.8	74.6
800 S			7.0	74.4
800 S	50 "		7.0	74.4
795 S			6.2	75.2
795 S	50 West		6.2	75.2
700 S			6.3	75.1
650 S			6.9	74.5
600 S			7.5	73.9

T
8144

T
90-62

39

550 S		6.4	75.00
550 S	25' West	5.7	75.7
500 S		4.5	76.9
500 S	50' West	4.3	77.1
460 S		2.8	78.6
360 S		3.0	78.4
345 S		2.3	79.1
340 S		3.6	77.0
340 S	25' West	1.3	80.1
"	50 "	2.1	79.3
300 S		2.5	78.9
T.P.	11-56 90-62	2.38	79.06
245 S		10.1	80.5
	10' East	10.3	80.3
	20' West	9.4	81.2
240 S		12.5	78.1
	10' E.	12.0	78.6
	15 W	11.5	79.7
	20 "	8.5	82.1
210 S		11.3	79.3
	36 E	11.4	79.2
	38 "	8.0	82.6

210 S.	10' W.	11.2	79.4
	12. "	6.8	83.8
200' S		9.4	81.2
	36 E	11.1	79.5
	38 "	8.0	82.6
	4' West	9.4	81.2
	6 "	5.8	84.8
180 S		10.4	80.2
	16' West	11.6	79.0
	16 "	6.1	84.5
	25' "	5.5	85.1
	30' "	3.1	87.5
160 S		10.0	80.4
	3' West	7.7	82.9
	30 "	6.3	84.3
	32 "	2.5	88.1
	35 East	10.5	80.1
	40. "	8.8	81.8
150 S.		7.2	83.4
	50' West	6.2	84.4
	25 E.	9.4	81.2
	50 "	8.3	82.3

		T		
		90.62		
100 S			6.5	84.1
	50' East		7.6	83.0
	50 West		5.5	85.1
T.P.	9.46	95.71	4.37	86.25
50'S			9.3	86.4
	60 S Line Ocean View Bld		5.5	90.2
	Top of Ocean View		5.4	90.3
	Gutter		6.1	89.6
Section B, 180' West of 30 th . This section runs only 150 S 0074				
0			3.5	92.2
30'S			4.9	90.8
50'S			6.7	89.0
100'S			9.1	86.6
125'S			9.1	86.6
125 S	5' W		8.3	87.4
125 S	10 W		6.0	89.7
150 S			7.6	88.1
150 S	6' E		9.3	86.4
Sec. C 200' W of 30 th				
0100			2.5	93.2
35			1.4	94.3

		T		
		95.71		40
50 S			3.4	92.3
	8' E		3.4	92.3
100'S			5.3	90.4
	9' E		5.3	90.4
150 S			6.6	89.1
200 S			7.1	88.6
	25' E		7.2	88.5
240			9.9	85.8
	30' East		11.0	84.7
250'S			10.6	85.1
	15' E		10.9	84.8
	25'		12.3	82.4
270			13.3	82.4
	10' West		11.6	84.4
300'S			13.7	82.0
	10' West		11.6	84.4
T.P.	0.72	84.33	12.10	83.61
325 S			3.9	80.4
400 S			4.8	79.5
500 S			6.0	78.3
600 S			7.7	76.6

T
8433

700 S	76	76.7
795 S	75	76.8
800 S	8.7	75.6
820 S	8.7	75.6
825 S	7.5	76.8
900 S	7.9	76.9
910 S	7.9	74.4
920 S	9.5	74.8
930 S	9.5	74.8
935 S	8.2	76.1
1000 S	8.3	76.0
1025 S	9.1	75.2
1035 S	10.5	73.8
1100 S	10.5	73.8
1200 S	11.7	72.6
1259 S ^{N Line Marcy}	12.7	71.6
Section D 300 West 30 th		
1259 S ^{S. N Line Marcy}	13.9	70.4
1200 S	12.2	72.1
1100 S	10.9	73.4
1050	11.3	73.0

T
8433

41

1035 S		11.1	73.2	
1025 S		10.1	74.2	
1000 S		8.9	75.4	
920 S		8.6	75.7	
910 S		7.7	76.6	
900 S		6.8	77.5	
800 S		6.4	77.9	
700 S		5.6	78.7	
600 S		4.8	79.5	
500 S		3.5	80.8	
400 S		3.1	81.2	
340 S		2.2	82.1	
	50 West	0.0	84.3	
TP	12.70	96.31	0.72	83.61
300 S		11.4	84.9	
	50 West	9.5	86.8	
250 S		9.6	86.7	
210 S		8.7	87.6	
200		7.5	88.8	
150 S		7.3	89.0	
100 S		6.2	90.1	
50 S		4.0	92.3	
00		1.5	94.8	

T
96.31

Section E 400

Gutter on Ocean View C-14	1.8	94.5
Top Cb.	1.3	95.0
00	1.1	95.2
10's	1.6	94.7
30's	3.6	92.7
100's	4.7	91.6
200's	6.7	89.6
300's	9.9	86.4
400's	11.7	84.6
T.P. 140	84.84	12.87
500's	2.0	82.8
600's	3.8	81.0
700's	4.5	80.3
800's	5.4	79.4
900's	7.1	77.7
915's	7.8	77.0
925's	9.2	75.6
935's	8.2	76.6
1000's	9.2	75.6

T
84.84

42

1020's	9.9	74.9
1030's	11.7	73.1
1050's	11.3	73.5
1100's	10.7	74.1
1150's	12.5	72.3
1200	11.8	73.0
1259.8 N Line of Marcy	13.7	71.1
Section F 500 West of 30 th		
1259.8 N Line of Marcy	13.3	71.5
1200's	12.1	72.7
1100's	11.5	73.5
1055's	11.1	73.7
1045's	12.1	72.7
1015's	10.1	74.7
1000's	10.1	74.7
900's	8.0	76.8
800's	5.9	78.9
700's	4.5	80.3
600's	3.6	81.2
500's	1.4	83.4

T
84.84

TP	12.62	97.21	0.25	84.59
400s			11.5	85.7
300s			9.7	87.5
200s			6.7	90.5
110s			4.4	92.8
100s			3.7	93.5
60s			2.4	94.8
60s	25 East		3.9	93.3
40s			2.9	94.3
00	S Line Ocean View Blvd		1.2	96.0

Sec. G 600 West of 30th

00		00	97.2
	60 West	0.1	97.1
Gutter	60 West S Line Ocean View	6.6	94.6
100s		2.3	94.9
100s	60 West	3.1	94.1
200s		5.3	91.9
200s	60 West	6.4	90.8
300s		9.1	88.1
"	60 West	9.1	88.1

T
97.21

43

400s			11.9	85.3
400s	60 West		11.6	85.6
400s	100 "		11.4	85.8
400s	200 "		11.3	85.9
400s	300 "		10.5	86.7
460s			12.2	85.0
460s	60 West		12.7	84.5
T.P.	0.53	85.30	12.44	84.77
500's			1.4	83.9
500s	60 West		1.5	83.8
500s	100 "		1.2	84.1
500s	200 "		1.1	84.2
500	300 "		1.0	84.3
600s	300 West		2.5	82.8
600s	200 "	Tennisct:	2.1	83.2
600s	100 "	Tennisct	2.5	82.8
600s	90 "		4.0	81.3
600s	60 "		4.1	81.2
600s			4.5	82.8

T
85.30

700' South on Sec G.	5.3	80.0
700 " " 60' West	5.7	79.6
" " " " 95'	5.1	80.2
" " " " 100 " Tenni Ct	3.6	81.7
700 S. on Sec G 200 West	3.9	81.9
" " " " 285 "	4.6	80.7
300 "	4.8	80.5
715 South on Sec G 300 West	5.3	80.0
" " " " 200 "	5.2	80.1
" " " " 100 "	5.9	79.4
60 "	6.3	79.0
715' South on Sec G	5.8	79.5
800 South on Sec G	6.3	79.0
800 " " 10' W.	8.3	77.0
" " " 60 "	8.0	77.3
" " " 100 "	7.7	77.6
" " " 200	7.3	78.0
" " " 300	7.1	78.2
900 South on Sec G 300 West	8.1	77.2

T
85.30

44

900 S. on Section G 200 West	9.6	75.7
" " " " " 100 "	9.8	75.5
60 "	9.9	75.4
10 "	10.1	75.2
900 South on Sec G	9.0	76.3
1000 South on Sec G 10' East	11.5	73.8
" " " " "	12.7	72.6
T.P. 2.58 75.36	12.52	72.78
1000 South on Sec G 60' West	2.4	73.0
" " " " " 100 "	1.8	73.6
" " " " " 220 " <small>N. End School Bldg. approx.</small>	0.3	75.1
1100 South on Sec G 220' West <small>School Bldg</small>	1.6	73.8
" " " " " 200 "	2.5	72.9
" " " " " 100 "	3.5	71.9
" " " " " 60 "	3.5	71.9
1100 South on Sec G	4.1	71.3
" " " " " 15' East	2.9	72.5

T
75.36

1200 South on Sec G	3' East	3.6	71.8
" " " "		4.6	70.8
" " " " "	60 West	4.4	71.0
" " " " "	100 "	4.2	71.2
" " " " "	220	4.0	71.4
TP		4.67	74.96
1246 ^B South on Sec G. N. Line of Mercy From West		4.3	70.7
1259.8 " " " " " " East		4.3	70.7
1246 ^B South on sec G. 100 West on Paring		5.5	69.9
" " 60 West on Paring		5.4	70.0
" " 60 " 2' North		4.2	71.2
" " 100 West 2' North		4.1	71.3
" " 100 "		5.1	70.3
" " 200 West on Paring		4.5	70.9
" " 200 " 2 North		3.8	71.6
" " 206' " Top cb.		3.4	72.0
" " " " Gutter		4.4	71.0
" " 220 " Top cb		3.7	71.7
" " " " Gutter		4.3	71.1
" " 220 West 65' North of cb S.E. Cor. School Bldg		1.7	

T
74.96

45

Check BM NW 29th Legas

6.53

68.93

68.45 BM NW DP
2023 v. 10904
0.02

Cross Section Alley Bk 14 Hubbell
From 27th to 28th St Between Boston & Newton

BM 10.43 50.86 40.43 N.W. B.P.
Boston x 28th

0-10 = N.C. 28th St

S	07 Paving	6.65	44.21
Z	" "	6.35	44.51
N	" "	6.01	44.85

0+0 = N.L. 28th St

N	Top Cb	5.04	45.82
	Gutter on Paving	5.26	45.60
Z	" "	5.62	45.24
	Gutter " "	5.81	45.05
S	Top Cb	5.78	45.08

0+5"

S		3.0	47.9
+2		3.0	47.9
+5		4.9	46.0
Z		5.0	45.9
+8		5.0	45.9
N		4.2	46.7

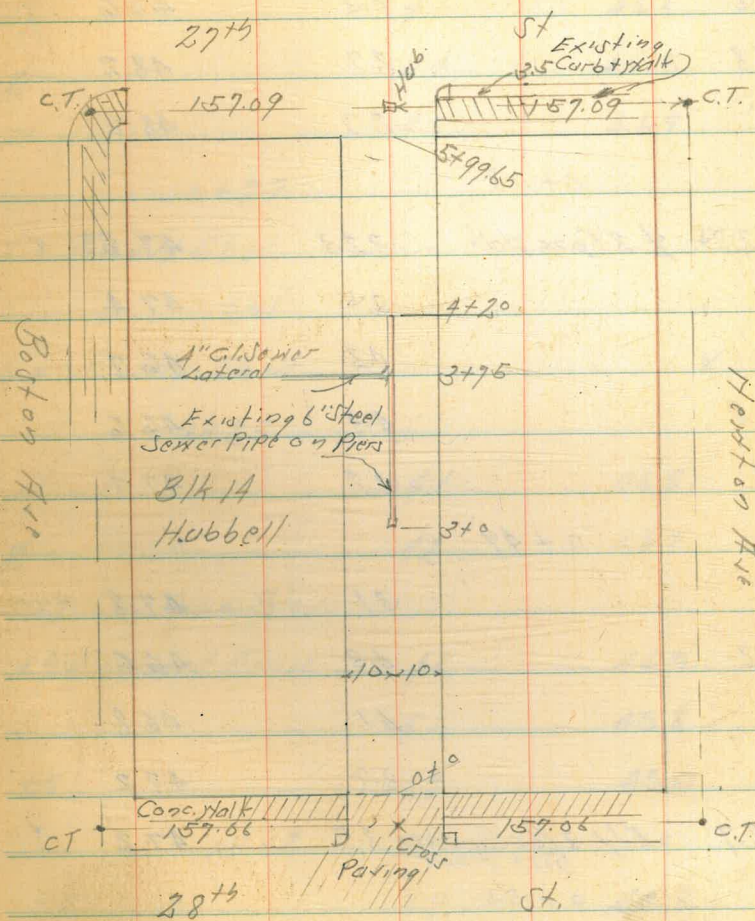
0+15

N		3.2	47.7
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Reduced plotted Feb 1940
on profile. To be checked

INDEXED
EFB

Jan 31 40
Sisson
Northham 46
056077



✓
50.86

+2	4.8	46.1
⊘	4.5	46.4
+5	4.3	46.6
+8	3.7	48.2
S	3.7	48.2

0+38

-2.8 = ⊘ 2' Conc Walk	3.23	47.63 ✓
S	3.5	47.4
⊘	4.2	46.7
+8	4.3	46.6
N	3.2	47.7

0+49

N	3.1	47.8
+2	4.3	46.6
⊘	4.1	46.8
S	3.7	47.2
+2.7 = Fly 3 Car Garage Dirt Floor	3.7	47.2 ✓

0+55

N + 0.2 = Fly Tel Pole

✓
50.86

47

0+74

-2.7 = Fly 3 Car Garage Dirt Floor	4.0	46.9 ✓
S	4.1	46.8
⊘	4.4	46.5
N	4.0	46.9

0+77

S + 1 = Fly Shed ✓

1+01

S + 0.5 = Fly Shed ✓

1+25

N	4.1	46.8
⊘	4.2	46.7

78.9 = Fly Power Pole

+9.5 = Board Fence	4.6	46.3
S	5.1	45.8
+5	5.9	45.0

1+62

-5	6.7	44.2
S	6.3	44.6
+1.5 = Fly Board Fence	4.7	44.2

✓
50.86

♂		4.9	46.0	
♂		4.6	46.3	
	1+64			
S	+0.8 = Fly Shed			✓
	1+76			
S	+0.6 = Fly Shed			✓
H	+0.3 = Fly Tel Pole			
	1+95			
	-0.8 = 1/2 Garage Dirt Floor 4.6		46.3	✓
H		4.6	46.3	
♂		5.1	45.8	
+9		4.9	46.0	
S		5.0	45.9	
+5		5.1	45.8	
TP	243	48.22	5.07	45.79 ✓
	2+17			
H	-0.3 = 1/2 Conc Apron 7 1/2' Wide 1.85		46.37	✓
H	-6.5 = 1/2 Garage Conc Floor 12'5" x 8' Wide 1.53		46.69	✓
	2+25			
S	+0.8 = Fly Sheds			✓

✓
48.22

48

	2+44			
S		3.2	45.0	
♂		3.0	45.2	
H		2.8	45.4	
+7	= 1/2 Garage Dirt Floor 2.4		45.8	✓
	2+51			
S	+0.6 = Fly Sheds			✓
S	+1.3 = Fly Porch Pole			
	2+63			
H		4.2	44.0	
♂	= M.H.P. 1.00	4.60	43.62	✓
S		4.9	43.3	
+5.8	= 1/2 Do Garage Dirt Floor 4.7		43.5	✓
	2+87			
	-1.2 = Floor of Framing 6.62		41.60	✓
S		8.1	40.1	
♂		7.4	40.8	
H		7.0	41.2	
	3+0			
H		9.3	38.9	

✓
4822

40.7 = Nly Tel. Pole
 ⚡ = Top 6" Steel Sewer Pipe 9.40 38.82 ✓
 S 9.5 38.7
 +5 11.0 37.2

3+25

-5 15.5 32.7
 S 14.7 33.5
 ⚡ 13.9 34.3
 ⚡ = Top 6" Steel Sewer Pipe 9.57 38.65 ✓
 H 13.3 34.9
 +5 12.7 35.5

3+48

-10 16.8 31.4
 H 16.8 31.4
 ⚡ 16.6 31.6
 ⚡ = Top Sewer Pipe 9.75 38.47
 +9 = Sly. Power Pole
 S 17.3 30.9
 +10 17.6 30.6

✓
4822

49

3+75

-10 18.2 30.0
 S 16.3 31.9
 ⚡ 16.6 31.6
 ⚡ = Top Sewer Pipe 9.96 38.26
 H 16.6 31.6
 +10 16.5 31.7

4+0

-10 13.3 34.9
 H 13.9 34.3
 ⚡ 14.1 34.1
 ⚡ = Top Sewer Pipe 10.08 38.14 ✓
 S 14.9 33.3
 +10 15.5 32.7

4+20

-5 11.8 36.4
 S 11.5 36.7
 ⚡ = Ground + Top Sewer Pipe 10.17 38.05 ✓
 H 9.1 39.1

48.22 ✓

4+30

H+0.4 = Nly Tel Pole

4+32

H-0.2 = Nly Do Garage
Dirt Floor

4+49

H

Z

+9.5 = Fly 3 Car Garage
Dirt Floor

S

+5

4+75

H+0.6 = Nly 3 Car Garage
Dirt Floor

Z

H

5+05

H+1.1 = Z Garage Dirt Floor

Z

S

5+21

S+1.2 = Sly Pav. Pole

7.5

40.7

✓

6.4

41.8

6.7

41.5

6.5

41.7

✓

6.5

41.7

7.5

40.7

5.5

42.7

✓

5.3

42.9

5.0

43.2

4.6

43.6

✓

5.0

43.2

5.0

43.2

48.22 ✓

50

5+50

S

Z

+9.5 = Nly Tel Pole

H

5+75

H

Z

S

5+99.65 = F.L. 27th St.

S

Z

H Ground

H TopCb

TP

6+09.65 = F.Cb 27th

H.E. Cor 27th Boston TopCb
N End Return

S Ground

Z

H

H TopCb.

BM

5.8

5.6

5.1

6.0

6.2

6.2

8.3

8.4

8.1

7.75

✓

6.79

46.09

8.92

7.2

6.8

6.6

5.77

1.10

42.4

42.6

43.1

42.2

42.0

42.0

39.9

39.8

40.1

40.47

39.30

35.13

38.9

39.3

39.5

40.32

44.93

44.99

Sym Fod Cb
Newport 37

Walker
Bliss
Isbell
52-40

LEVELS on EXISTING SEWER
IN E-street, West of 28th Street

INDEXED
EPB

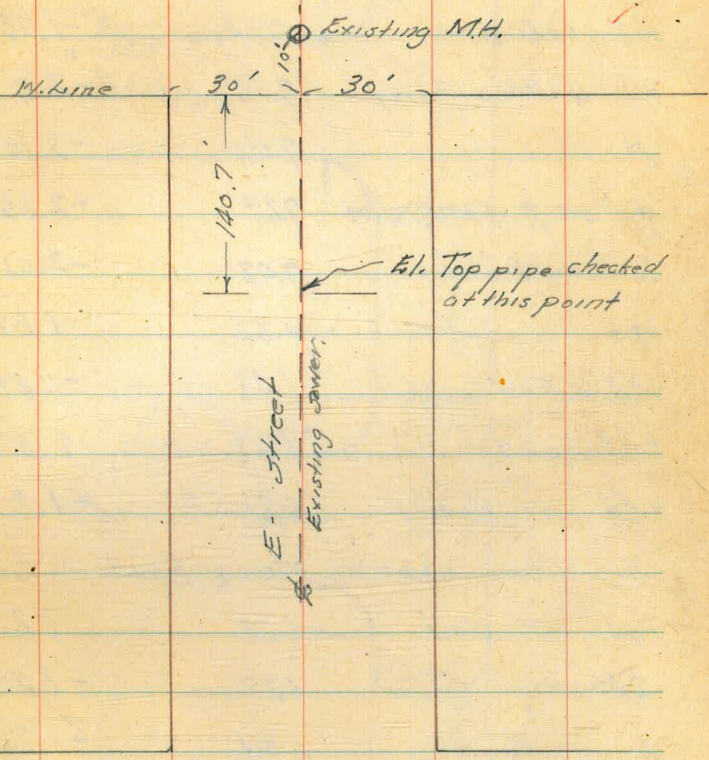
	0.78	158.06	157.28	El. Rim M.H. 6+50.7 P-33 - this book
chh. B.M. NW. Man E-28th	0.80	157.26		This may have been raised 157.40 = B.M. Book.

0.14 = diff in elev.

140.7' West of W.L. 28th	11.45	146.61	on top Sewer Pipe
140.7' " " " "	8.8	149.3	on ground
140.7' " " " "	10.75	147.31	on top South cb.
140.7' " " " "	9.64	148.42	on " North cb.

28th

St.



27th

St.

Cross Section Ventura Place
Mission Blvd. to Ocean Front Walk

INDEXED

EFB

May 10-20
Sisson
North
W. Wall

57.8P
Ventura & 500
Wall

BM	0.38	7.89'	7.51
TP	4.54	5.01'	7.42 0.47'

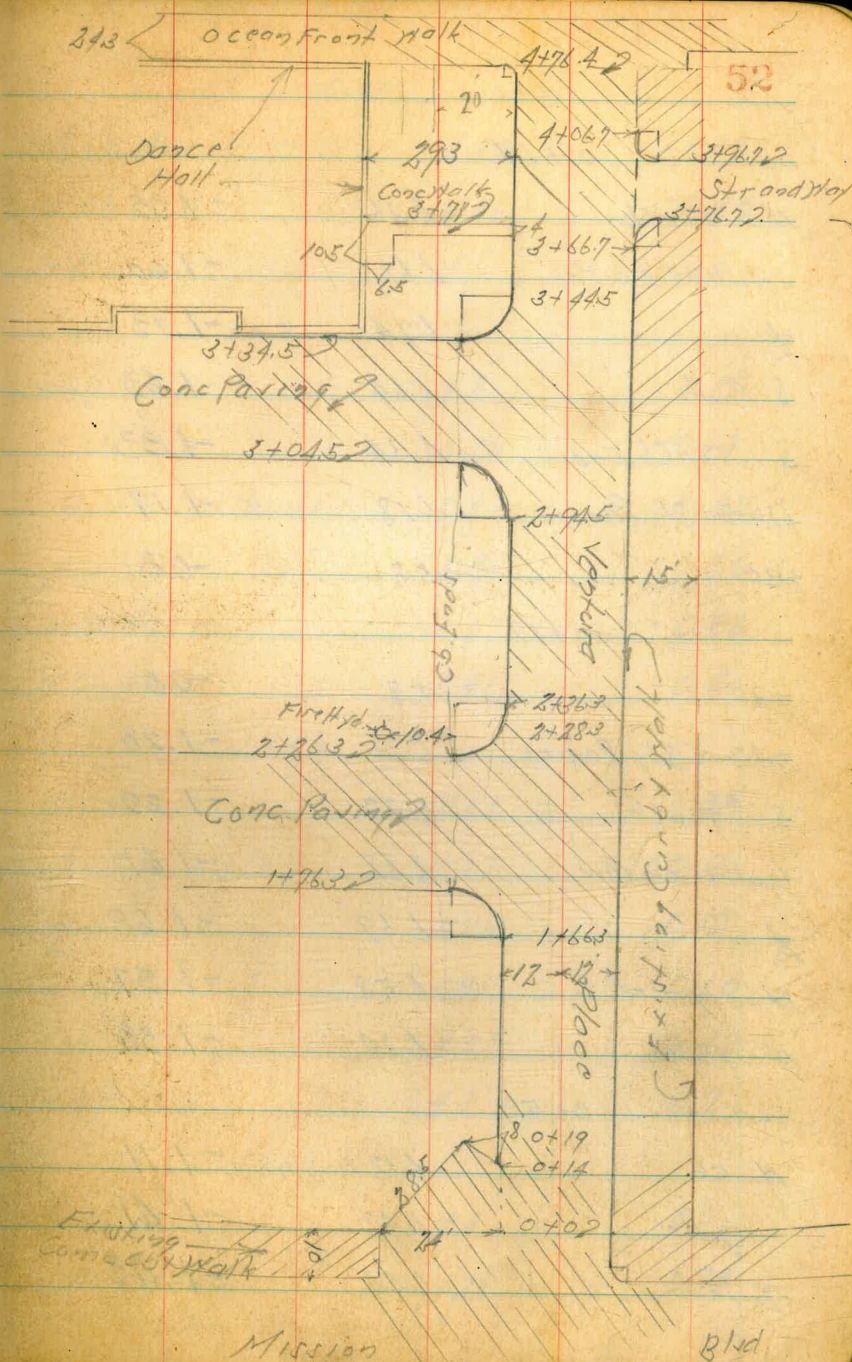
0-10' = 1/2 Cb Mission Blvd

-3 = Cb EC Top Ch	6.74	-1.73
-3 Gutter on Paving	7.12	-2.11
H " "	7.11	-2.10
1/2 on 1/2 3'x2' Grating	7.27	-2.26
S on Paving	7.02	-2.01
+24 " "	6.88	-1.87
+24 = End Cb Walk	6.48	-1.47
+44 on Top Ch	6.38	-1.37
+44 on Paving	6.81	-1.80

0+0 = 1/2 Mission Blvd

-44 = 1/2 Walk	6.22	-1.21
-24 = 1/2 " End	6.27	-1.26
S on Paving	6.73	-1.72
1/2 " "	6.82	-1.81
H " "	6.70	-1.69
H Top Ch	6.48	-1.47

Reduced by
Plotted by - Hough
Guterson



Mission

Blvd

5.01		
0+14		
H TopCb	6.36	-1.35
Gutter on Pav	6.61	-1.60
L " "	6.74	-1.73
S Gutter " "	6.64	-1.63
S TopCb End	6.34	-1.33
+10.5 = Sly Paving	6.18	-1.17
+30	5.8	-0.8
0+19		
-30	5.8	-0.8
-4.7 = Sly Paving	6.21	-1.20
S TopCb	6.30	-1.29
Gutter on Pav	6.62	-1.61
L " "	6.69	-1.68
H Gutter " "	6.58	-1.57
H TopCb	6.34	-1.33
0+50		
H cb	6.12	-1.11
Gutter	6.42	-1.41
L	6.44	-1.43

5.01		
S Gutter	6.28	-1.27
S cb	5.86	-0.85
+30	5.6	-0.6
1+0		
-30	4.8	0.2
S cb Top	5.20	-0.19
Gutter on Paving	5.63	-0.62
L " "	5.86	-0.85
H Gutter " "	5.87	-0.86
H cb Top	5.41	-0.40
1+50		
H cb Top	4.63	38
Gutter on Pav	5.17	-0.16
L " "	5.13	-0.12
S Gutter " "	4.91	0.10
S cb Top	4.52	0.49
+30	4.3	0.7
1+66		
-30	4.3	0.7
S cb Top = BC	4.28	0.73

Ventura Place

5.01

S Gutter on Pav	4.67	0.34
⌘ " "	4.87	0.14
H Gutter " "	4.92	0.09
H Cb Top	4.41	0.60
1+76.3 = E.L. Pav on S		
H Cb Top	4.22	0.79
Gutter on Pav	4.76	0.25
⌘ " "	4.76	0.25
S Cb " "	4.58	0.43
+3 " "	4.52	0.49
+10 = End Cb & Paving	4.54	0.47
+30 on E Edge Pav	4.47	0.54
+50 " Pav	4.43	0.58
2+01.3		
-50 on Paving	4.75	0.26
-30 " "	4.72	0.29
-10 " "	4.73	0.28
S Cb " "	4.76	0.25
⌘ " "	4.63	0.38
H Gutter " "	4.50	0.51
H Cb Top	3.92	1.09

54

5.01

2+26.3 = W/Ly Pav on S		
H Cb Top	3.57	1.44
Gutter on Pav	4.38	0.63
⌘ " "	4.17	0.84
S Cb " "	4.10	0.91
+10 = End Cb & Paving	4.08	0.93
+30 on W/Ly Pav	4.10	0.91
+50 " " "	4.03	0.93
2+36.3		
-30	3.6	1.4
S Cb Top - EC	3.34	1.67
Gutter on Pav	3.77	1.24
⌘ " "	3.93	1.08
H Gutter " "	3.88	1.13
H Cb Top	3.33	1.68
2+50		
H Cb Top	2.95	2.06
Gutter on Paving	3.49	1.52
⌘ " "	3.52	1.49
S Gutter " "	3.27	1.74

	5.01		
SCb Top	2.88	2.13	
+30	3.0	2.0	
TP	6.51	8.45 [✓]	3.07
		1.94 [✓]	
	2+94.5		
-50	5.3	3.2	
-30	5.3	3.2	
SCb Top	4.87	3.58	
Gutter on Pav	5.25	3.20	
⌊ " "	5.66	2.79	
H Gutter " "	5.85	2.60	
Hcb Top = BC	5.31	3.14	
	3+04.5		
Hcb Top	5.03	3.42	
Gutter on Pav	5.62	2.83	
⌊ " "	5.45	3.00	
SCb " "	4.99	3.46	
+10 - End Cb + Paving	5.01	3.44	
+30 on Fly Paving	5.06	3.39	
+50 " " "	5.11	3.34	

	8.45	55
	3+19.5	
-50 on Paving	5.21	3.24
-30 " "	5.14	3.31
-10 " "	5.09	3.36 ³⁰⁴
SCb " "	5.00	3.45
⌊ " "	5.25	3.20
H Gutter " "	5.29	3.16
Hcb Top	4.73	3.72
	3+34.5	
Hcb Top	4.27	4.18
Gutter on Paving	4.74	3.71
⌊ " "	4.92	3.53
SCb " "	4.85	3.60
+10 - End Cb + Paving	4.97	3.48
+30 on Fly " "	5.00	3.45
+50 " " "	5.12	3.32
	3+44.5	
-30	4.6	3.9
SCb Top = BC	4.11	4.34
Gutter	4.58	3.87

Ventura Place

8.45

Z on Paving	4.67	3.78
N Gutter "	4.59	3.86
N cb Top	4.02	4.43

3+66.7

N cb Top - BC	3.50	4.95
Gutter on Pav	4.00	4.45

Z " "	4.14	4.31
-------	------	------

S Gutter "	4.04	4.41
------------	------	------

S cb Top	3.61	4.84
----------	------	------

+22.8 = Nly Conc Slab	3.52	4.93
-----------------------	------	------

+29.3 = Sly " "	3.53	4.92
-----------------	------	------

3+71

-29.3 = Z 4 Conc Walk	3.50	4.95
-----------------------	------	------

S cb + Walk	3.48	4.97
-------------	------	------

3+76.7 = E L Strand Way

-29.3	3.4	5.1
-------	-----	-----

S cb Top	3.40	5.05
----------	------	------

Gutter on Pav	3.79	4.66
---------------	------	------

Z " "	3.87	4.58
-------	------	------

N cb " "	3.71	4.74
----------	------	------

+15 = End cb + Walk	3.41	5.34
---------------------	------	------

8.45

56

3+96.7 = N L Strand Way

-15 = End cb + W	2.88	5.57
------------------	------	------

N cb on Pav	3.60	4.85
-------------	------	------

Z " "	3.65	4.80
-------	------	------

S Gutter "	3.55	4.90
------------	------	------

S cb Top	3.10	5.35
----------	------	------

+29.3	3.2	5.3
-------	-----	-----

4+06.7

-29.3	3.0	5.5
-------	-----	-----

S cb Top	3.01	5.44
----------	------	------

Gutter on Pav	3.50	4.95
---------------	------	------

Z " "	3.61	4.84
-------	------	------

N Gutter " "	3.54	4.91
--------------	------	------

N cb Top	3.11	5.34
----------	------	------

4+50

N cb Top	3.10	5.35
----------	------	------

Gutter on Pav	3.61	4.84
---------------	------	------

Z " "	3.71	4.74
-------	------	------

Gutter	3.53	4.92
--------	------	------

S cb Top	3.05	5.40
----------	------	------

+29.3	3.1	5.4
-------	-----	-----

0.45

4+66.4

-293	34	5.1
S cb Top	3.20	5.25
Gutter on Pav	3.67	4.78
$\frac{1}{2}$ " "	3.73	4.72
N Gutter " "	3.67	4.78
N cb Top	3.24	5.21

4+76.4

N cb Top + Conc. Walk	3.67	4.78
$\frac{1}{2}$ " "	3.68	4.77
S cb Top + Conc. Walk	3.65	4.80
+293 on E. ly Conc. Walk	3.70	4.75
B.M	0.99	7.51

Starting

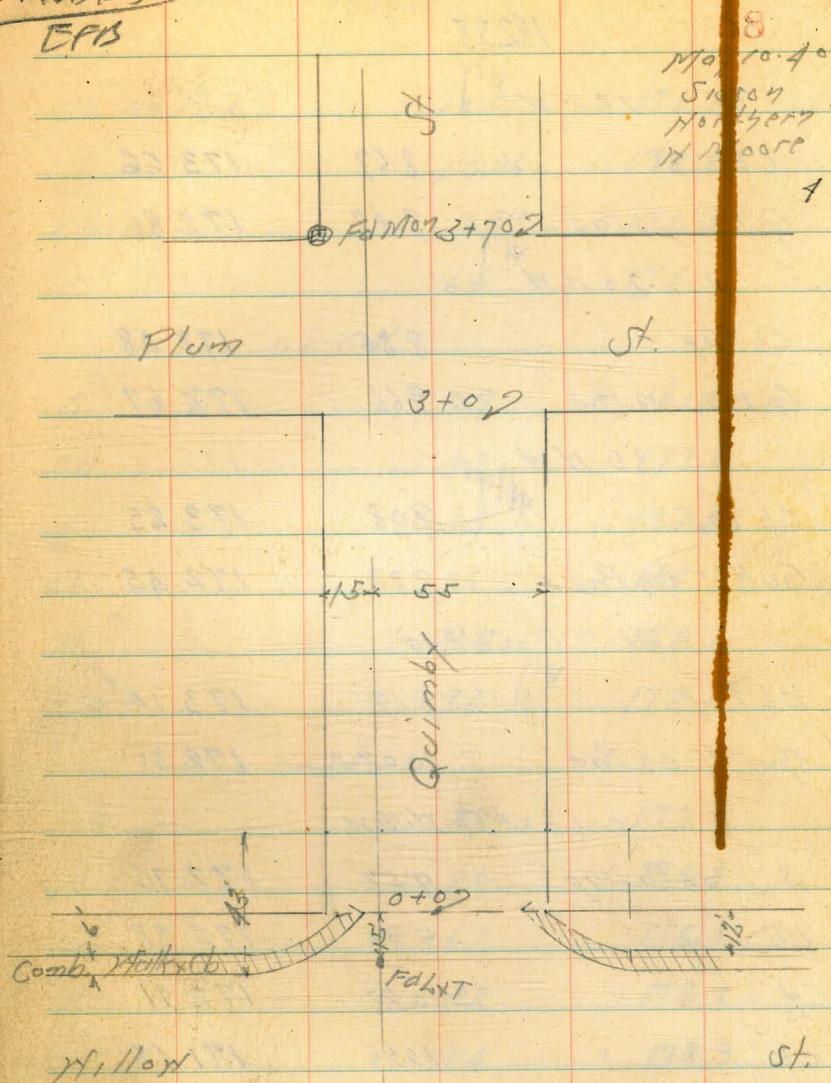
57

Cross Section Quincy St.
Willow to Plum

	HI		S.M.B.P. Rust Hill + Willow
B.M. 12.45	173.78	161.33	
TP 9.96	182.33	1.41	172.37
N.W. Return			
B.C. Cb Top	1160		170.73
Gutter on Pav.	12.38		169.95
10' SW N1/4			
Cb Top	1107		171.26
Gutter on Pav.	11.85		170.48
20' SW N1/4			
Cb Top	10.67		171.66
Gutter on Pav.	11.44		170.89
30' SW N1/4			
Cb Top	10.35		171.98
Gutter on Pav.	11.10		171.23
41' SW = Cb End N1/4			
Cb Top	10.19		172.14
Gutter on Pav.	10.94		171.39
SW Return			
B.C. Cb Top	838		173.95
Gutter on Pav.	919		173.16

Reduced & plotted on profile # 723
5-15-40 CSH

INDEXED
EPB



182.33

10' H W Wly

Cb Top 8.67 173.66

Gutter on Pav 9.47 172.86

20' H W Wly

Cb Top 8.85 173.48

Gutter on Pav 9.66 172.67

30' H W

Cb Top 9.08 173.25

Gutter on Pav 9.88 172.45

41' H W = Cb End

Cb Top 9.19 173.14

Gutter on Pav 10.02 172.31

0-18 = W Cb Willow

S on Paving 9.57 172.76

Cb " " 9.95 172.38

Z " " 10.22 172.11

Cb " " 10.65 171.68

H " " 11.11 171.22

0+0 = H C Willow

H 9.9 172.4

182.33

59

Cb on Pav 10.51 171.82

Z " " 10.06 172.27

Cb " " 9.99 172.34

S 6.4 175.9

0+05'

S 0.9 181.4

Cb 3.2 179.1

Z 5.3 177.0

Cb 7.6 174.7

H 9.5 172.8

+10 9.8 172.5

0+25'

-10 8.7 173.6

H 8.0 174.3

Cb 6.2 176.1

Z 4.2 178.1

+7 3.4 178.9

+10 2.4 179.9

Cb 1.5 180.8

TP 6.09 187.91 0.51 181.82

Quimby St 187.91

5 4.6 183.3

0+50

5 3.2 184.7

cb 5.4 182.5

+7 6.7 181.2

+9 8.3 179.6

5 8.8 179.1

cb 11.0 176.9

H 12.0 175.9

+10 13.6 174.3

0+75

-10 12.5 175.4

H 11.7 176.2

cb 9.6 178.3

5 7.8 180.1

+8 7.7 180.2

+10 6.2 181.7

cb 5.4 182.5

5 3.2 184.7

187.91

60

1+0

5 3.7 184.2

cb 4.4 183.5

+6 5.5 182.4

+9 7.1 180.8

5 7.0 180.9

cb 8.3 179.6

H 10.6 177.3

+10 11.3 176.6

1+25

-10 10.6 177.3

H 10.4 177.5

cb 8.2 179.7

5 6.9 181.5

+9 5.9 182.0

+11 5.2 182.7

cb 5.0 182.9

5 4.8 183.1

1+50

5 6.9 181.0

187.91

cb	6.9	181.0
L	7.3	180.6
cb	8.3	179.6
H	9.6	178.3
+10	9.8	178.1

1+75

-10	9.9	178.0
H	9.4	178.5
cb	8.5	179.4
L	8.4	179.5
cb	8.6	179.3
S	9.7	178.2

2+0

S	11.2	176.7
cb	10.7	177.2
L	10.1	177.8
cb	10.4	177.5
H	9.5	178.4
+10	9.5	178.4

187.91

61

2+25

H	11.5	176.4
cb	11.9	176.0
L	12.7	175.2
TP	1.15	177.18
	11.88	176.03

cb	3.3	173.9
S	4.6	172.6
+10	5.1	172.1

2+50

-15	8.5	168.1
S	7.0	170.2
cb	5.6	171.6
L	4.3	172.9
cb	3.3	173.9
H	1.9	175.3

2+75

H	5.2	172.0
cb	6.7	170.5
L	6.7	170.5
cb	7.3	169.9

177.18

S		9.6	167.6	
+15		10.6	166.6	
	3+0 = EL Plum			
-15		13.2	164.0	
S		12.2	165.0	
cb		11.2	166.0	
S		9.6	167.6	
+10		10.0	167.2	
+12		9.5	167.7	
cb		9.3	167.9	
H		7.8	169.4	
TP	3.52	168.20	12.50	164.68
	3+35 = S Plum			
H		2.0	166.2	
cb		2.8	164.4	
+7		4.2	164.0	
+9		5.0	163.2	
S		5.2	163.0	
cb		6.3	161.9	
S		6.8	161.4	
+15		7.1	161.1	

168.20

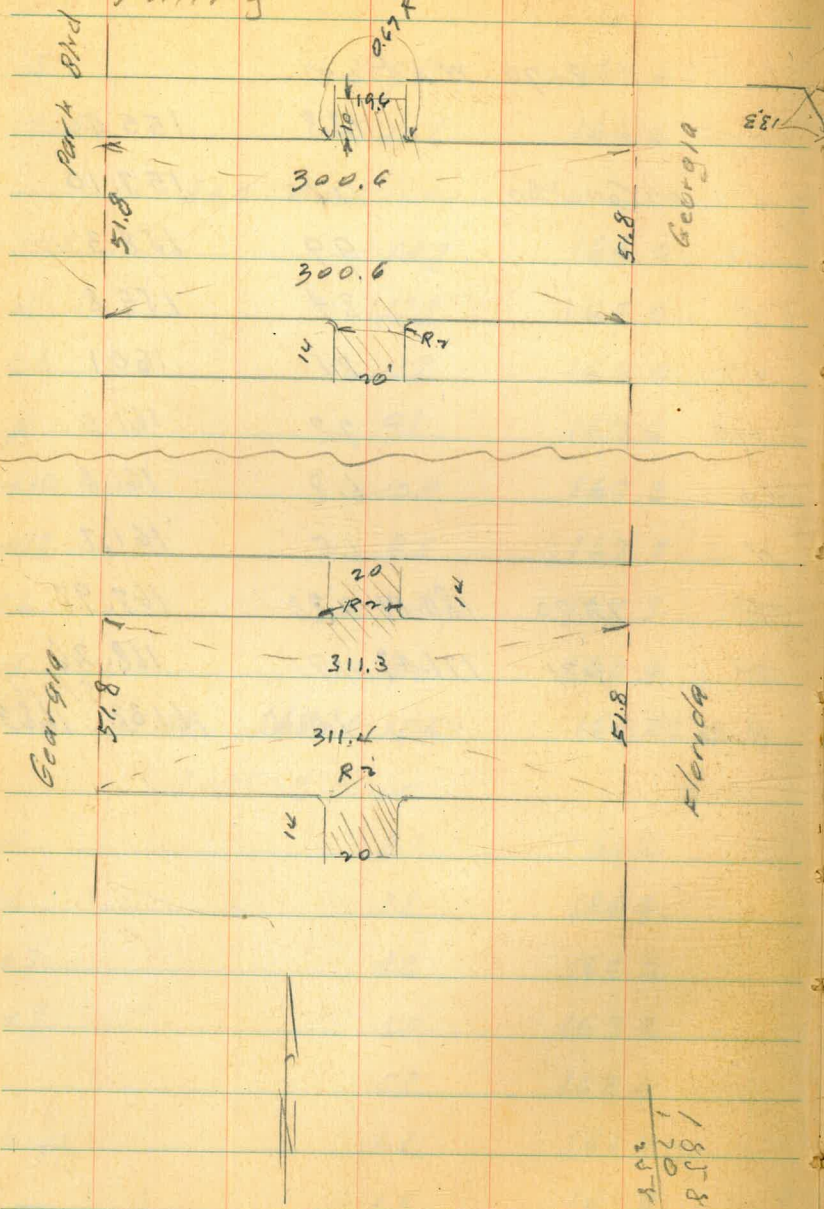
62

	3+70 = WL Plum			
-15		12.8	155.4	
S	on Cond Mo	11.10	157.10	
cb		9.9	158.3	
S		8.4	159.8	
+7		8.1	160.1	
+10		7.2	161.0	
cb		6.8	161.4	
H		6.5	161.7	
TP	12.20	180.17	0.23	167.97
TP	3.21	171.47	11.91	168.26
B M		10.15	161.32	168.33

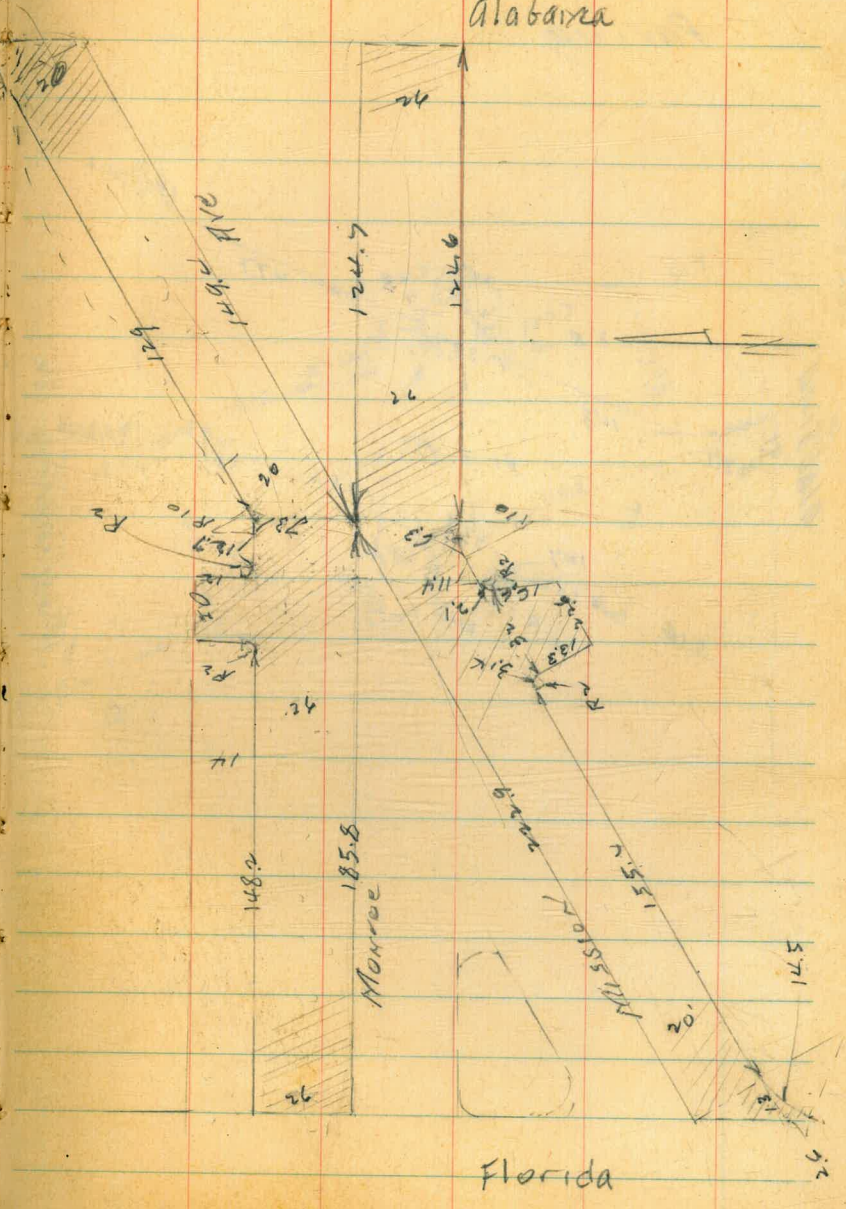
Starting
7.4
9.5
61.1

Slope Meas. Monroe Ave. Moore
 & MISSION AVE. 7-18-40.
 Paving

INDEXED
 EPB



1.52
 1.85
 8.58



Re Cross Section of Arthur Ave.
 Hawley to 35th St
 Original #1542-30

BM 3.82 39893 395.11 NW.B.P.
 Arthur
 Hawley

FCB Hawley

H on Paving	4.55	394.38
CB "	4.30	394.63
1/4 "	4.13	394.80
1/2 "	4.12	394.81
1/4 "	4.23	394.70
CB "	4.54	394.39
J "	4.85	394.08

0+0 = F.C. Hawley

SCB Top	4.33	394.60
Gutter on Paving	4.84	394.09
1/4 "	4.35	394.58
1/2 "	4.17	394.76
1/4 "	4.21	394.72
Gutter "	4.53	394.40
NCB Top	4.18	394.75

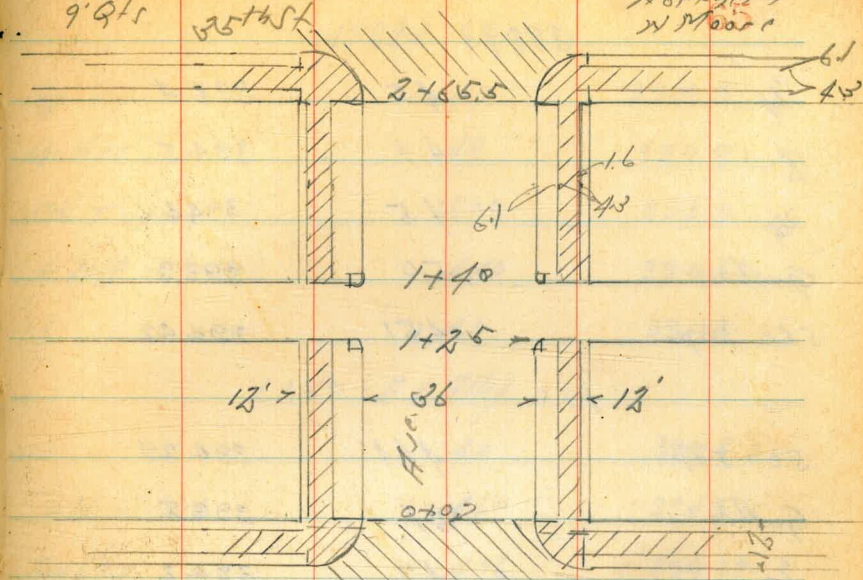
0+15.0

NCB Top	4.19	394.76
Gutter	4.7	394.2

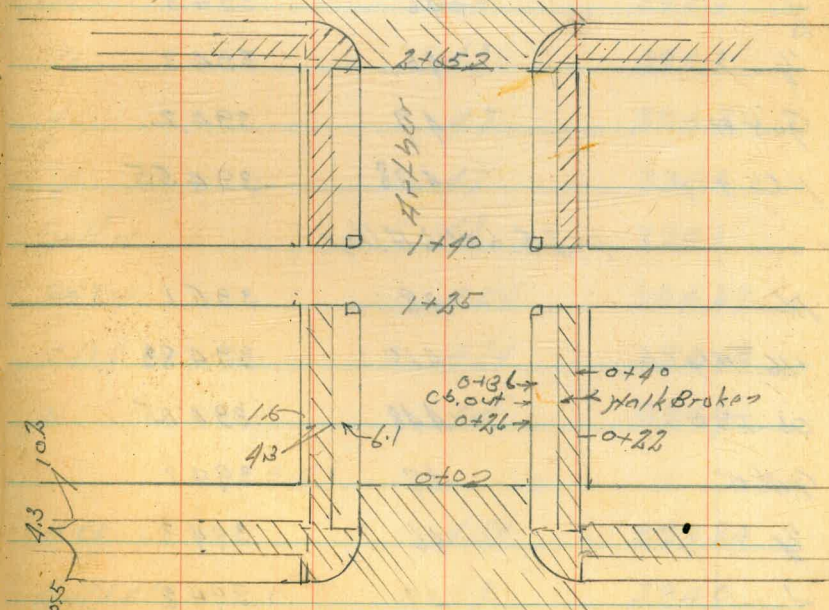
60' Wide
 12' C&G
 9' Q&T

INDEXED
 EFB

July 22-40
 J. Sisson
 Northey's
 W Moore



Mansfield



Hawley

Blvd

39893

1/4	4.5	3944
1/2	4.4	3945
1/4	4.5	3944
Gutter	5.0	3939
SCb Top	4.51	39442

1+0

SCb Top	4.64	39429
Gutter	5.1	3938
1/4	4.7	3942
1/2	4.6	3943
1/4	4.6	3943
Gutter	4.7	3942
HCb Top	4.38	39455

1+25 = N 2 Alley

N	3.8	3951
+1.6 = N 1/2 Cb	4.10	39488
Cb Top	4.48	39445
Gutter	4.7	3942
1/4	4.6	3943
1/2	4.7	3942

39893

68

1/4	4.7	3942
Gutter	4.9	3940
Cb Top	5.00	3939
+ 10.4 = S 1/2 Cb	4.40	394.53
J	4.1	3948

1+40 = E. L. Alley

J	4.1	3948
+1.6 = S 1/2 Cb	4.60	394.33
Cb Top	4.76	39417
Gutter	5.0	3939
1/4	4.8	3941
1/2	4.7	3942
1/4	4.7	3942
Gutter	4.8	3941
Cb Top	4.54	39439
+10.4 = N 1/2 Cb	4.24	39469
N	4.3	3946

1+50

HCb	4.59	39434
Gutter	4.9	3940

398.93

1/4	4.7	394.2
1/2	4.7	394.2
1/4	4.9	394.0
Gutter	5.1	393.8
Scb Top	4.84	394.09

2+0

Scb Top	4.96	393.97
Gutter	5.3	393.6
1/4	5.0	393.9
1/2	5.0	393.9
1/4	5.0	393.9
Gutter	5.1	393.8
H.Cb Top	4.78	394.15

2+50

H.Cb Top	4.98	393.95
Gutter	5.4	393.5
1/4	5.2	393.7
1/2	5.1	393.8
1/4	5.2	393.7
Gutter	5.5	393.4

398.93

67

Scb Top	5.18	393.75
---------	------	--------

2+652 = H.Cb Mansfield

Scb Top	5.20	393.63
Gutter on Paving	5.60	393.33

1/4	5.21	393.72
-----	------	--------

1/2	5.06	393.87
-----	------	--------

1/4	5.11	393.82
-----	------	--------

Gutter	5.40	393.53
--------	------	--------

H.Cb Top	5.03	393.90
----------	------	--------

2+723 = H.Cb Mansfield

H on Paving	5.49	393.44
-------------	------	--------

Cb	5.48	393.45
----	------	--------

1/4	5.28	393.65
-----	------	--------

1/2	5.18	393.75
-----	------	--------

1/4	5.20	393.63
-----	------	--------

Cb	5.61	393.32
----	------	--------

S	5.67	393.26
---	------	--------

0-12 = F.Cb Mansfield

S on Paving	5.89	393.04
-------------	------	--------

Cb	5.87	393.06
----	------	--------

398.93

1/4 on Paving	5.51	393 42
1/2 " "	5.87	393 56
1/4 " "	5.62	393 31
CB " "	6.00	392 93
H " "	6.22	392 71

040 = E.L. Mansfield

H CB Top	5.87	393 06
Gutter on Pav	6.27	392 66
1/4 " "	5.80	393 13
1/2 " "	5.62	393 31
1/4 " "	5.64	393 29
Gutter " "	5.95	392 98
SCB Top	5.55	393 38

0450

SCB Top	5.86	393 07
Gutter	6.5	392 4
1/4	6.3	392 6
1/2	6.2	392 7
1/4	6.3	392 6
Gutter	6.8	392 1

398.93

68

H CB Top	6.18	392 75
140		
H CB Top	6.43	392 50
Gutter	7.0	391 9
1/4	6.6	392 3
1/2	6.3	392 6
1/4	6.4	392 5
Gutter	6.7	392 2
SCB Top	6.12	392 81
TP 4.04	396.49	5.48 392.45

1425 = W.L. Allen

S	3.3	393 2
11.6 = 1/4 CB	3.55	392 94
CB Top	4.03	392 46
Gutter	4.2	392 3
1/4	3.9	392 6
1/2	3.9	392 6
1/4	4.2	392 3
Gutter	4.6	391 9
CB Top	4.01	392 48

396.49

+104. H/Cb 3.75 392.74

H 2.7 393.8

1+40. EL. Allow

H 3.0 393.5

+1.6 = H/Cb 3.80 392.69

Cb Top 4.13 392.36

Gutter 4.8 391.7

1/4 4.3 392.2

1/2 4.0 392.5

1/4 4.0 392.5

Gutter 4.4 392.1

Cb Top 3.84 392.65

+104. S/Cb 3.55 392.94

S 3.3 393.2

1+50

S/Cb Top 3.95 392.54

Gutter 4.5 392.0

1/4 4.1 392.4

1/2 4.1 392.4

1/4 4.3 392.2

69

396.49

Gutter 4.8 391.7

H/Cb Top 4.23 392.26

2+0

H/Cb Top 4.50 391.99

Gutter 5.0 391.5

1/4 4.5 392.0

1/2 4.1 392.4

1/4 4.4 392.1

Gutter 4.8 391.7

S/Cb in Drive 4.67 391.82

2+50

S/Cb Top 4.64 391.85

Gutter 5.1 391.4

1/4 4.9 391.6

1/2 4.7 391.8

1/4 4.9 391.6

Gutter 5.3 391.2

H/Cb Top 4.77 391.72

2+65.5 = H/Cb 35.5

H/Cb Top 4.90 391.59

396.49

Gutter on Porch	5.34	391.15
1/4 " "	5.08	391.41
1/2 " "	4.96	391.53
1/4 " "	5.13	391.36
Gutter " "	5.24	391.25
Scb Top	4.73	391.76

21 77.5 = 21 Cb 3.5 5.5

S on Porch	5.25	391.24
Cb " "	5.23	391.26
1/4 " "	5.21	391.28
1/2 " "	5.26	391.23
1/4 " "	5.34	391.15
Cb " "	5.40	391.09
H " "	5.51	390.98
B-M	4.75	391.74

314.8 P
Arthur
Mt. View
391.73

70

Cross Section Garrison St. (SIDEWALKS)

Rosecrans to Willow

Property line to Curbs only

See Page 154
#583-86

S.M. B.P.
Garrison St.
End of

BM	1.59	31.69	30.10
TP	0.83	20.26	12.26
TP	2.68	11.29	11.65
			8.61

0+0 = N.E. Rosecrans

S		8.5	2.8
+8.2 = Top Existing Cb		8.57	2.72
Ncb +9.8		8.27	3.02
H		8.4	2.9

0+27 = Cb E.C.

H		8.3	3.0
Ncb Top		8.30	2.99
Scb Top		8.57	2.72
S		8.1	3.2

0+31

S		7.9	3.4
Scb Top		8.59	2.70
Ncb "		8.35	2.94
H		8.2	3.1

1+0 = E End Walk on N

H		6.8	4.5
---	--	-----	-----

Reduced & Plotted on X Sec.
7/31/40 G.B.H.

18' Cb

INDEXED
E.P.B.

11.29

July 27, 40
J. W. S. W.
Northway
X Moor

Ncb Top	7.25	4.04
S " "	7.22	4.07
+8	6.8	4.5
S	6.6	4.7

1+50

S	5.5	5.8
Scb Top	5.73	5.56 Broken

2+0 = N End Walk on N

S	4.0	7.3
Scb Top	4.21	7.08
H " "	4.21	7.08
H	3.9	7.3

2+50

H	2.7	8.6
Ncb Top	2.80	8.49
S " "	2.71	8.58
S	2.5	8.8

2+63

S	2.1	9.2
Scb Top	2.32	8.97

11.29

Ncb Top	2.40	8.89
+5	2.1	9.2
H	2.0	9.3
2+75: Cb BC		
H	1.8	9.5
+3	1.7	9.6
+14	1.6	9.7
Hcb	2.08	9.21
S Cb	2.00	9.29
+3	1.6	9.7
+10	1.6	9.7
S	1.8	9.5

3+10 = E. Locust

S	1.2	10.1
+5	0.9	10.4
+10 = Top Existing Cb	1.35	9.94
+10 Ground	1.1	10.2
S Cb "	1.1	10.2
H Cb "	1.2	10.1
+8 "	1.2	10.1

11.29

+8 Top Existing Cb	1.34	9.95
H	0.9	10.4
3+10		
H = Top Cb End	1.33	9.96
H Ground	0.5	10.8
+6 "	0.3	11.0
H Cb "	0.9	10.4
S Cb "	1.2	10.1
+2 "	0.8	10.5
S "	1.1	10.2
S Top Cb End	1.26	10.03

BM	9.87	39.47	30.10	S.M.B.P. Garrison + Elev 91.00
10' E of W.L. F. in ground				
S Top Cb End	11.40		28.07	
S Ground	10.6		28.9	
Scb "	10.7		28.8	
0+0 = W.L. F. in ground				
Scb Ground	10.4		29.1	
+8 "	10.4		29.1	
+8 Cb Top	10.93		28.54	
S	10.2		29.3	
0+25 = Cb FC				
S	8.4		31.1	
+3	9.2		30.3	
+1/6	9.0		30.5	
Scb Top	9.51		29.96	
0+32.3				
Scb Top	8.88		30.59	
+4	8.4		31.1	
+14	8.7		30.8	
S	7.6		31.9	

 Reduced & Plotted on Section
 7/31/40 C.B.H.

	39.47		
0+75			
S	5.2		34.2
+4	5.6		33.9
Scb Top	5.92		33.55
1+0 = E End Conc Walk on S			
Scb Top	4.09		35.38
S	3.4		36.1
TP	11.84	50.68	0.63 38.84
2+00.3 = N End Conc Walk on N			
N Cb Top	7.97		42.71
N	7.8		42.9
2+25			
N	6.0		44.7
N Cb Top	6.22		44.46
2+75 = Cb B.C.			
N Cb Top	2.46		48.22
N	2.4		48.3
3+0 = E.L. Willow			
N	0.7		50.0
+10 = Top Existing Cb	0.95		49.73 ✓

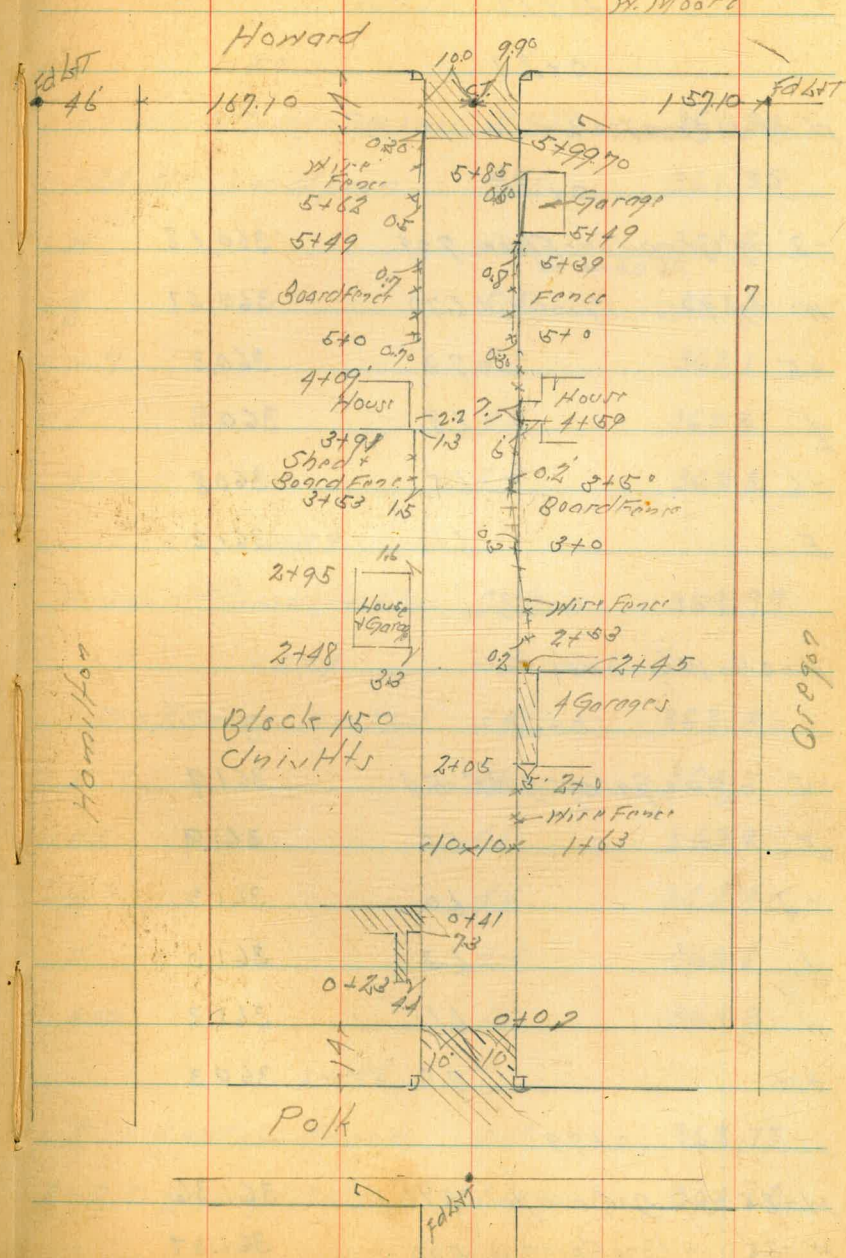
Cross Section Alley Block 150 Ch. W. Hts
 Between Hamilton + Oregon
 From Polk to Howard

BM	1.03	367.05	366.02	S.F. Post Polk
0-14. NCB Polk				
E 02 Paving	8.23		358.82	
S " "	8.58		358.47	
H " "	8.91		358.14	
0+0: NCB Polk				
H Topcb	8.29		358.76	
H 02 Paving	8.37		358.68	
S " "	8.53		358.52	
E " "	8.04		359.01	
E Topcb	7.47		359.58	
TP	8.36	367.27	8.14	358.91
0+5				
F	6.6		360.7	
+5	8.2		359.1	
S	8.4		358.9	
+7	8.2		359.1	
H	7.4		359.9	
0+15				
E + 15: Fly To Polk				

Notes Reddy Plotted
 20th Sept. 10-1940

INDEXED
 EPB

Sept 7-40
 S.W. 200
 Northberg
 W. Moore



367.27

0+23

W-4.4: Conc Walk

0+41

-8' = $\frac{1}{2}$ Garage Conc Floor 7.09 360.18W = $\frac{1}{2}$ 7.3 Conc Apron 6.70 360.57

+5 7.0 360.3

 $\frac{1}{2}$ 6.8 360.5

+6 6.5 360.8

F 6.1 361.2

0+62

W-0.9 = Wly Power Pole

0+68

-5' = $\frac{1}{2}$ Garage Dirt F 5.4 361.9

F 5.4 361.9

+4 6.0 361.3

 $\frac{1}{2}$ 6.3 361.0

W 6.1 361.2

+10 7.0 360.3

0+79

W-8.5: Sly De Garage 5.91 361.36

W-2.5 = " Conc Apron 5.90 361.37

367.27

75

1+0

-8 = Wly De Garage Conc Floor 5.93 361.34

-2.3 = Wly Conc Apron 5.92 361.35

W 5.5 361.8

 $\frac{1}{2}$ 5.5 361.8

+7 5.2 362.1

F 4.8 362.5

+10 4.5 362.8

1+39

W-5.4 = $\frac{1}{2}$ Garage Conc Floor 7.28 359.99

1+44

-2.7 = $\frac{1}{2}$ Garage Conc Floor 3.91 363.86

F 3.6 363.7

+5 4.1 363.2

 $\frac{1}{2}$ 4.4 362.9

W 4.5 362.8

+10 6.1 361.2

1+56

F = $\frac{1}{2}$ 9.4 Conc Apron 2.50 363.77F-2.5 = $\frac{1}{2}$ Garage Conc Floor 3.15 364.12

36727

1+63

F = Sky Wire Fence

1+80

-10 5.3 362.0

-2 4.9 362.4

W 4.1 363.2

+2 3.3 364.0

$\frac{1}{2}$ 3.6 363.7

F = Wire Fence 3.3 364.0

+19 = Wly Front House 3.3 364.0

10+95

W + 0.2 = Wly Power Pole

2+0

F = Wly Wire Fence 2.7 364.6

+5 3.1 364.2

$\frac{1}{2}$ 3.2 364.1

+9 3.0 364.3

W 3.8 363.5

+10 5.2 362.1

TP 7.06 371.31 3.02 364.25

37131

76

2+05

F = Sky Conc Appro 6.05 365.26

-5 = Sky 4 Car Garage 5.57 365.74

2+45

-10 7.1 364.2

W 6.6 364.7

$\frac{1}{2}$ 6.2 365.1

F = Wly Conc Appro 5.70 365.61

+5 = Wly 4 Car Garage Conc F. 5.56 365.75

2+77

F = Wire Fence 5.5 365.8

$\frac{1}{2}$ 5.9 365.4

W 6.2 365.0

+1.3 = Sky Conc Appro 6.31 365.00

+2.5 = Sky 2 Car Garage Conc Floor 6.25 365.06

2+95

W - 1.2 = Wly 2 Car Garage CT 6.18 365.13

W - 0.2 = " Conc Appro 6.14 365.17

2+98

W - 0.2 = Wly Conc Walk 6.16 365.15

371.31

3+0

-10 6.6 364.7

W 5.4 365.9

+0.3 = Wly Por. Pole

⌘ = W H Rim 5.41 365.90

F 5.4 365.9

3+50

-10 4.3 367.0

F 4.4 366.9

+3 4.9 366.4

⌘ 5.0 366.3

+7 5.0 366.3

W 4.5 366.8

+10 5.8 365.5

4+0

-2 = Fly House 3.8 367.5

W 3.8 367.5

⌘ 4.1 367.2

+5 4.1 367.2

F = 8ly Picket Fence 3.6 367.7

+10 3.3 368.0

371.31

4+09

X-1.3 = 5 1/2 x 7 1/2 Conc Wall + Wire 5.69 367.62

4+50

-10 2.5 368.8

F = Fence 2.6 368.7

+5 3.4 367.9

⌘ 3.4 367.9

W 3.5 367.8

+1.3 = Wly 0.75 Conc Wall + Wire Fence 3.50 367.81

+5 4.0 367.3

4+59

X-1.9 = 1/2 Do Garage Dirt F 3.6 367.7

TP 6.55 374.89 2.97 368.34

4+22

F-6.2 = 5 1/2 Do Garage Conc Floor 5.28 369.61

4+99

F-6.2 = 1 1/2 Do Garage Conc Floor 5.33 369.56

5+0

-10 6.5 368.4

W 5.7 369.2

+0.9 = Wly Por. Pole

374.89

Z	5.7	369.2
E	5.8	369.1
+10	5.0	369.9

5449

E - S/G Garage Conc. Ford	5.0	369.9
Z	5.0	369.9
W	5.1	369.8

5457

W-0.8 - 8 Garage Conc. Floor	5.33	369.56
W-0.5 Conc. Lip	5.19	369.70

5485

-5	4.8	370.1
W	5.4	369.5
Z	5.2	369.7
E	5.1	369.8

+0.6 W/G Garage W/Floor	4.43	370.46
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+0.6 Floor Floor	4.43	370.46
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5498

W+0.9 - W/G Pav. Pad		
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374.89

78

5499.70 = S/H Hayward

E TopCb	4.86	370.03
E on Paving	5.18	369.71
Z " "	5.72	369.17
W " "	5.83	369.06
W TopCb	5.75	369.14

643.7 = S/Cb Hayward

W on Paving	6.67	368.22
Z " "	6.21	368.68
E " "	5.63	369.26

TP	0.65	370.04	5.50	369.39
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BM			9.92	360.12
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S/H 7 tack
Hayward
380.10

3-17-55
 M.O. 20006
 REF: See A₂ 29 - Sketch
 Dwg: 5882-L
 X-SECT "E" between 27th + 28th from 180
 100 W. of inlet to 50 E of inlet

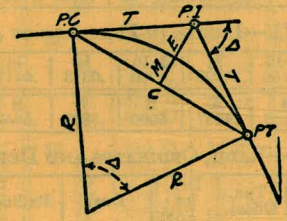
Station	151.59	151.51	150.92	151.50	150.48	150.96	150.93
6+00	23 W	20 CB	20 G		20 G	20 CB	23 W
5+80	149.45	149.41	148.83	149.38	148.51	148.77	148.76
	23 W	20 CB	20 G		20 G	20 CB	23 W
5+60	148.0	147.96	147.35	148.02	146.90	147.27	147.30
	23 W	20 CB	20 G		20 G	20 CB	23 W
5+55 and Broken walk at 5+54.5 End of Clay mark on rt.							
5+49 = Inlet	147.58	146.30	147.48	146.90	146.36	146.89	147.11
	20 CB	20 G		20 G	20 CB	20 CB	23 W (needs orig walk)
5+47 RT. End New CB mark on rt.						146.79	147.09
						20 CB	23 W ok clay
5+40	147.30	146.82	147.20	146.46	146.71	147.21	147.21
	20 CB	20 G		20 G	20 CB	20 CB	23 W ok clay
5+20	147.59	147.10	147.26	146.89	147.51	147.87	147.87
	20 CB	20 G		20 G	20 CB	20 CB	23 W ok clay
5+15 LT. Walk Broken-out							
5+00 Cold-Set Floor with TP CB RT	148.58	148.38	147.90	148.03	147.78	148.58	
	23	20 CB	20 G		20 G	20 CB	
4+87 Beg. Clay 7.5 wide walk meets BKCB on rt.					149.96	149.00	149.18
					20 CB	20 G	23 W ok clay
4+80	150.67	150.58	149.81	149.85	149.79	150.50	149.95
	23	20 CB	20 G		20 G	20 CB	23 W
4+70	151.93	151.85	151.22	151.10	150.87	151.48	151.23
	23	20 CB	20 G		20 G	20 CB	23 W
4+60.5 Beg. New S. CB. 20 RT.							152.35
							20 CB
4+50	153.76	154.81	153.70	153.43	153.19	153.79	153.88
	23 walk	20 CB	20 G		20 G	20 CB	23 W walk

(0+00) = E. Line 27th : E. Inlet = 5+49 (Pg 28)

B.M. Dip. Elev. Rod: 180.01 = S.W. B.P. "E" 42.7 ft.

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

- Radius = $R = \frac{50}{\sin. D/2}$ (1) Degree of Curve = D and $\sin. \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent = $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve = $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate = $M = R(1 - \cos. \frac{\Delta}{2})$ (5) = $R \text{vers} \frac{\Delta}{2}$ (6)
- External = $E = T \tan \frac{\Delta}{4}$ (7) = $R \div \cos. \frac{\Delta}{2} - R$ (8) = $R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord = $C = 2 R \sin. \frac{\Delta}{2}$ (10) Δ = Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I. = Sta. 161 + 60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $+8\frac{1}{2} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. - $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 91.27$ and from Table V correction = .10 or $E = 91.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D? From Table IV $E = 230.9$ and $+42 = 5.5$ or $D = 5^\circ 30'$.

33.57
 3.47
 30.10
 3.2
 4.8

15 - 71 = 1/2 x fence
 85
 156 10/10 to J
 275 15 - 50' More
 125
 26.7
 98.3

Tool Shed 12 = x 24 6 = 5 school BK
 Green 30 x 30 N Edge

89° 56' 30"
 179° 52' 30"
 267° 09'
 135° 45'
 89° 56' 20"

26
 26
 156
 52
 676
 676
 147.52 | 3
 9
 67 | 45
 49

2176
 576
 285
 25
 103 | 352
 309
 1064 | 4300

67
 Green House
 G + 625 4545 - Steve

DISTANCES FROM CENTER OF ROADWAY FOR
 CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.