

1568

POSTS

LEVEL BOOK

No. 331 F

MICROFILMED
DEC 28 1964

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CITY OF SAN DIEGO,
CALIFORNIA.

MADE IN U. S. A.

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ENGINEERING and DRAFTING SUPPLIES

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CHICAGO

73.70

2+84⁺ cor ① $\angle 120^{\circ} 20' Lt$ 2.8 See Page 1

3+00 15.6 E of Cor ① P.O.T. 2.2 71.5

3+85⁻ cor. ② $\Delta 14^{\circ} 52' Lt$ 2.2

4+32⁺ Cor. ③ $\Delta 15^{\circ} 35' Lt$ 2.2

6+19 Cor. ④ $\Delta 12^{\circ} 58' Rt$ 2.2 71.5

7+55.0 Cor. ⑤ $\Delta 55^{\circ} 40' Lt$ 2.2 71.5

8+06 P.O.T. To slope 3.4 70.3

8+11⁻ Cor. 6 $\angle 75^{\circ} 06' Lt$ 2.2 71.5

10+98⁺ Cor. 7 $\angle 91^{\circ} 25' Lt$ 2.2 71.5

11+08 To slope P.O.T. 6.8

11+39⁻ N.E. Cor Shop. 6.8

12+24 $\begin{cases} 50' E. \\ 0+00 \text{ off } + 5 \text{ Page 1} \end{cases}$ 8.6

South Line of Park $S 89^{\circ} 59' E$

5-11-37
Williams
Miller
Walker
Bliss

Additional Topog E. of Machine Shop.

B.M. 0.75 $\pi 72.25$ 71.5 H.W.M.

0+50 E. = E. side Machine Shop 6.8 65.5 ground

1+85 E 2.2 70.0

1+87 E 0.7 71.5

0+80 S

B.M. -0.4 $\pi 71.1$ 71.5 H.W.M. on shop.

0+50 E = E. side Shop 5.7 65.4

1+32 E 5.1 66.0

1+90 E \checkmark 4.1 67.0

2+03 E \checkmark 3.2 68.0

2+09 E \checkmark 2.1 69.0

2+28 E \checkmark 1.1 70.0

2+38 E 4.4 71.5 H.W.M.

0+00 N 45

B.M. 1.5 73.0 71.5 H.W.M. on shop.

1+79 E 7.0 66.0

2+42 E 6.0 67.0

2+50 E 5.0 68.0

2+64 E 4.0 69.0

2+90 3.0 70.0

1.5 71.5

60' N of 00

3

BM.	360	75.1	71.5	H.W.M. on shop
55.E		10.1	65.0	
1+35		9.1	66.0	
1+88 E		8.1	67.0	
2+54 E		7.1	68.0	
2+49 E		6.1	69.0	
3+24 E		5.1	70.0	
E. Line Traverse near Cor 6.		3.6	71.5	

indexed

C.S.K.

Levels for Tide Lines at outlet of
Switzer Conduit Under Mt. S.F. Tracts

4

		This BM. 0.03 High		N.W. 1/4 + National M ¹ M ² Shawton
B.M. BP	3.13	6.93	3.80	
B.M. BP		5.14	1.79 = 1.82	
T.P.	4.73	9.26	2.40	4.53
Nail in Lath			12.59	- 3.33
Nail in Lath			13.89	- 4.63
Top Cap			8.47	0.79 = 0.82

6/24/39

Miller
Walker
BlissLevels W. Entrance Superintendents
Office City Shops. 20th + B.Indexed
c.s.k.

5

B.M. B.P. 2.47 72.70 70.23

S. 2. 20th
+ B. Sts

T.P. 4.32 69.18 7.84 64.86

Top. Landing of steps 0+30.32N }
W. End. Superintendents Office } 3.01 66.17

Top. Step N. End. Landing 3.53 65.65

High water Mark. at steps } 3.09 66.09

0+30.32 N. }

High water Mark. on E. }
Wall City Garage } 3.09 66.09
0+30.32 N. }High water Mark. on E }
Wall City Garage 0+25N } 3.09 66.09New.
B.M. B.P. 7.05 N.W. 19th
+ B.

T.P. 7.34 72.20 4.32 64.86

chk. orig. B.M. 1.97 70.23

Garage
City

Superintendents Office

N+34.35
Top. Landing of stepsN+26.35
3.9N+10.2
S. Wall. 4N. Line
B. 56.7

8-2-39 Columbia St. & See.

Miller
Walker
Blair

Winder to Chalmers.

B.M.B.P

10.26

111.34

101.08

Indexed
c.s.k.

N.W. Winder
& Columbia

6

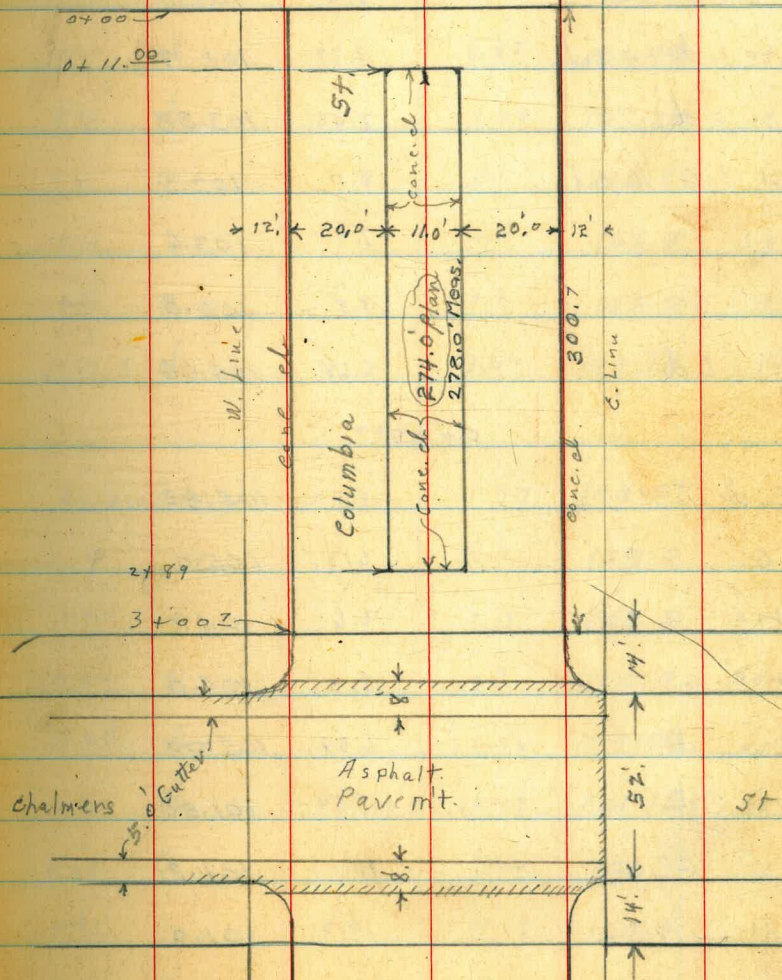
14' N. of sly line Winder St. S dr. Line

Winder St.

W. Line conc'd	10.26	101.08
" " Pav	11.01	100.33
" cl. Line produced	10.56	100.78
+10	9.76	101.58
+20 dr " "	9.17	102.23
+31.9 " "	8.63	102.71
+41	8.35	102.99
+51 = E. dr. Line	8.25	103.09

0+00 = S. Line Winder St.

E. conc. cl	7.45	103.89
Gutter pav S. End.	8.13	103.21
+10 " " "	8.32	103.02
+20 cl. produced	8.60	102.74
+31 " "	9.10	102.24
+41	9.82	101.52
+51 gutter	10.71	100.63
+51 W. dr	10.18	101.16



111.34

0+11

W. cl	10.30	101.04
G	10.6	100.7
+10	10.0	101.3
+20 = G	9.6	101.7
+20 = d N. end	9.17	102.17
+31 = d	7.46	103.88
+31 = G N. end	8.0	103.3
+41	7.7	103.6
+51 = G	7.5	103.8
+51 = E. d	6.68	104.66

0+25

E. cl	5.52	105.82
G	6.3	105.0
+10	6.6	104.7
+20 G	7.3	104.0
+20 d	6.34	105.00
+31 d	8.54	101.80
+31 G	10.1	101.2
+41	10.3	101.0
+51 G	10.8	100.5
+51 W. d	10.42	100.92

111.34

0+50 S.

Columbia St

7

W. cl	10.78	100.56
G	11.1	100.2
+10	10.6	100.7
+20 G	10.3	101.0
+20 d	9.85	101.49
+31 d	7.04	107.30
+31 G	5.1	106.2
+41	4.4	106.9
+51 G	4.3	107.0
+51 E. d	3.60	107.74

0+75

E. conc Drive	2.27	109.07
G	2.3	109.0
+10	2.5	108.8
+20 G	2.9	108.4
+20 d	2.26	109.08
+31 d	10.19	101.15
+31 G	10.6	100.7
+41	10.9	100.4
+51 G	11.2	100.1
+51 W. d	11.05	100.29

111.34

1+00 S

W. cl		11.24	100.06
G		11.5	99.8
+10		11.1	100.2
+20	G	10.9	100.4
+20	cl	10.52	100.82
+31	cl	1.05	110.29
+31	G	1.7	109.6
+41		1.2	110.1
+51	G	1.0	110.3
+51 E. cl.		0.57	110.77

1+25 S.

E. cl		0.25	111.09
G		0.6	110.7
+10		0.7	110.6
+20	G	1.1	110.2
+20	cl	0.73	110.61
+31	cl	10.85	100.49
+31	G	11.2	100.1
+41		11.5	99.8
+51	G	11.8	99.5
+51 W. cl.		11.53	99.81

111.34

1+50

Columbia St

8

W. cl		11.75	99.59
G		12.1	99.2
+10		11.9	99.4
+20	G	11.6	99.7
+20	cl	11.19	100.15
+31	cl	0.78	110.56
+31	G	1.2	110.1
+41		0.8	110.5
+51	G	0.6	110.7
+51 E. cl		0.25	111.09

1+80

E. conc driveway		1.48	109.86
G		1.6	109.7
+10		1.8	109.5
+20	G	2.2	109.1
+20	cl	1.21	110.13
+31	cl	11.58	99.76
+31	G	12.3	99.0
+41		12.4	98.9
+51	G	12.6	98.7
+51 W. cl		12.12	99.22

111.34

1+90

W. d	12.20	99.14
G	12.8	98.5
+10	12.6	98.7
+20 = G	12.5	98.8
+20 = d	11.72	99.62
+31 = d	1.95	109.39
+31 G	2.9	108.4
+41	2.6	108.7
+51 G	2.4	108.9
+51 E d	1.55	109.79

2+00

E. d	2.27	109.07
G	3.3	108.0
+10	3.5	107.8
+20 G	3.8	107.5
+20 d	2.80	108.54
+31 d	11.83	99.51
+31 G	12.8	98.5
+41	12.9	98.4
+51 G	13.1	98.2
+51 W d	12.31	99.03

111.34

Columbia

9

2+10

W. d	12.74	98.60
G	13.5	97.8
+10	13.3	98.0
+20 G	13.1	98.2
+20 d	12.23	99.11
+31 = d	3.98	107.36
+31 G	4.9	106.4
+41	4.6	106.7
+51 G	4.3	107.0
+51 E. d	3.46	107.88

2+25

E. d	5.24	106.10
G	6.1	105.2
+10	6.4	104.9
+20 G	6.8	104.5
+20 d	5.88	105.46
+31 d	12.85	98.49
+31 G	13.6	97.7
<hr/>		
T.P.	4.05	102.46
+41	5.0	97.5
+51 G	5.4	97.1
+51 d	4.63	97.83

102.46

2+50

W. cl	5.87	96.59
G	6.7	95.8
+10	6.2	96.3
+20 G	6.0	96.5
+20 cl	5.05	97.41
+31 cl	0.10	102.36
+31 G	1.4	101.1
+41	0.8	101.7
+51 G	0.6	101.9
+51 = E cl	+0.63	103.09

2+75

E. cl	2.38	100.08
G	3.5	99.0
+10	4.0	98.5
+20 G	4.2	98.3
+20 cl	3.31	99.15
+31 cl	6.13	96.33
+31 G	7.2	95.3
+41	7.5	95.0
+51 G	7.9	94.6
+51 W. cl	7.11	95.35

102.46

2+89

W. cl	7.77	94.69
G	8.4	94.1
+10	8.1	94.4
+20 G	7.6	94.9
+20 = cl s. end.	6.60	95.86
+31 cl s. end.	4.95	97.51
+31 G	5.7	96.8
+41	5.3	97.2
+51 G	4.8	97.7
+51 cl	4.07	98.39

3+00Z - N. Line Chalmers

E. cl	5.39	97.07
G	5.7	96.8
+10	6.1	96.4
+20	6.8	95.7
+31	7.4	94.7
+41	8.3	94.2
+51 G	8.7	93.8
+51 W. cl	8.42	94.04

Columbia

10

102.46

11' S. of N Line = N. Edge conc. gutter

W. ch. Line - 3' = ch. Ret.	8.49	93.97
conc. gutter	8.95	93.51
W. ch. Line " "	8.87	93.59
+10 " "	8.33	94.13
+20 " "	7.77	94.69
+31 " "	7.12	95.34
+41 " "	6.63	95.83
+51 = E. ch. Line " "	6.09	96.37
+ = C	5.95	96.51
+ 3 = ch. Ret.	5.40	97.06

14' S. of N. = N. ch. Line Chalmers

E. Line ch.	5.40	97.06
E " gutter E. End. pav	6.16	96.30
E. ch	6.38	96.08
+10	6.95	95.51
+20	6.46	96.00
+31	8.08	94.38
+41	8.62	93.84
+51 = W. ch. Line	9.08	93.38
W. Line gutter	9.33	93.13
" " ch	8.38	94.08
+12	10.70	91.76

102.46

19' S. of N. Line = { N. edge Asphalt Pav. / S. edge conc. gutter } Columbia

11

W-12	10.53	91.93
W	9.29	93.17
ch	8.78	93.68
+10	8.29	94.17
+20	7.71	94.75
+31	7.22	95.24
+41	6.63	95.83
+51 = E. ch	6.08	96.38
+54	5.90	96.56
E = E. pav.	5.86	96.60

29.5 S. of N. Line

E = E. pav	5.65	96.81
ch	6.00	96.46
+10	6.44	96.02
+20	6.92	95.54
+31	7.40	95.06
+41	7.86	94.60
+51 = W. ch	8.44	94.02
W. Line	9.20	93.26
+12	10.30	92.16

102.46
40' s. of N. = E. Chalmers.

W-12 _i	10.27	92.19
W. Line	9.22	93.24
w. cl	8.39	94.07
+10	7.85	94.61
+20	7.29	95.17
+31	6.79	95.67
+41	6.31	96.15
+51 = E. cl	5.94	96.52
E. Line = E. pav.	5.60	96.86

50.5' s. of N. Line

E. Line = E. pav	5.72	96.74
E. cl	6.05	96.41
+10	6.45	96.01
+20	6.94	95.52
+31	7.49	94.97
+41	8.01	94.45
+51 = W. cl	8.58	93.88
W.	9.37	93.09
+12	10.45	92.01

102.46 Columbia
61' s. of N = N. edge conc gutter
(S. " Asphalt Pav

12

W-12	10.71	91.75
W-5	9.80	92.66
N	9.53	92.93
+5	9.19	93.27
W. cl	8.94	93.52
+10	8.42	94.04
+20	7.82	94.64
+31	7.23	95.23
+41	6.67	95.79
+51 = E. cl	6.18	96.28
E. Line = E. pav.	5.95	96.51

66' s. of N. = S. cl. Line

E gutter E. end.	6.21	96.25
E. conc. cl.	5.43	97.03
E. cl. Line	6.44	96.02
+10	7.01	95.45
+20	7.54	94.92
+31	8.14	94.32
+41	8.67	93.79
+51 = W. cl. Line	9.24	93.20
+58	9.46	93.00

102.46

S. ch. con

W. Line gutter	7.68	92.78
W. " conc. ch	8.65	93.81
+ 5	9.96	92.50
+ 12' gutter	10.96	91.50

69' S. of N. Line = S. edge conc gutter

3' a.w. of W. ch. Line = ch. return	8.63	93.83
" " " " conc gutter	9.17	93.29
W. ch. Line " "	8.94	93.52
+ 10 " "	8.38	94.08
+ 20 " "	7.82	94.64
+ 31 " "	7.23	95.23
+ 41 " "	6.68	95.78
+ 51 = E. ch. Line " "	6.18	96.28
+ 54 = gutter " "	6.03	96.43
+ 54 = ch. Return	5.49	96.97

80' S. of N. = S. Line Chalmers

E. conc. ch. S. End. + ground.	5.48	96.98
+ 10	5.5	97.0
+ 20	6.2	96.3
+ 31	7.1	95.4
+ 41	7.8	94.7

102.46

Columbia

13

+ 49	8.4	94.1
+ 51 ground.	7.8	94.7
+ 51 conc. ch. S. end	8.63	93.83

at this cor. a piece of concrete slab was laying on curb. uncovered, the ch. was not uncovered.

B.M. BP

5.30 97.16

S.E. Chalmers
+ Columbia

ch. Orig. B.M.

1.37 101.09 = 101.08

8-16-39

Nile St. X Sec.
Thorn to University

80' wide
14' obs.
13' 1/4"

Indexed
C.S.K.

BM. 5.54 309.23 303.69 N.S. Thorn + Nile

14' S. of N. line = N. d. line Thorn.

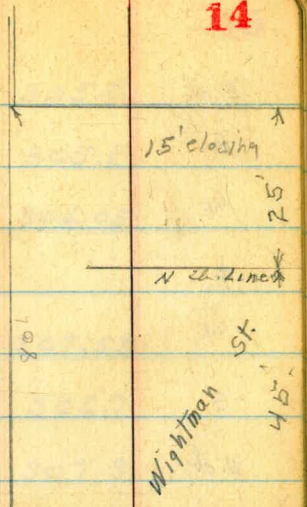
E Line	el.	5.62	303.61
E "	pay	6.23	303.00
el. line	"	6.32	302.91
4	"	6.40	302.83
4	"	6.47	302.76
14	"	6.66	302.57
el. line	"	6.88	302.35
W. Line	G. "	7.20	302.03
"	" d	6.65	302.58
0+00 = N. Line Thorn St			
w. el.		6.16	303.07
G	Pay N. End.	6.68	302.55
14	" "	6.32	302.91
4	" "	6.13	303.10
14	" "	6.15	303.08
G	" "	6.28	302.95
E. d.		5.64	303.59

1 sec - 1930
no book 1208
C.S.K.

S.W.
Rebuilt

6+02.
5+98.
5+76
5+12
5. End gate

6+01 = N. End d.
28' d. ind.
56' el. surr.
83' of walk out.



Y 5+73

BM. S.E. Nile + Nile 314.57

309.23

0+30N.

e. cl	7.86	304.37
G	5.8	303.4
1/4	5.3	303.9
±	5.2	304.0
1/4	5.5	303.7
G	6.2	303.0
w. cl	5.26	303.97

0+65N.

w. cl	4.27	304.96
G	5.2	304.0
1/4	4.5	304.7
±	4.1	305.1
1/4	4.3	304.9
G	4.9	304.3
e. cl	3.79	305.44

1+00

e. cl	2.87	306.36
G	3.6	305.6
1/4	3.3	305.9
±	3.0	306.2

309.23

Nile st.

15

1/4	3.4	305.8
G	4.0	305.2
w. cl	3.18	306.05

1+50

w. cl	1.71	307.52
G	2.5	306.7
1/4	1.9	307.3
±	1.6	307.6
1/4	1.7	307.5
G	2.1	307.1
e. cl	1.44	307.79

2+00

e. cl	10.05	309.28
G	0.5	308.7
1/4	0.4	308.8
±	0.3	308.9
1/4	0.5	308.7
G	0.9	308.3
w. cl	0.22	309.01
T. P.	9.01	318.06
	0.18	309.05

318.06

2+50

w. d	7.61	310.45
G	8.4	309.7
1/4	8.1	310.0
⊕	7.8	310.3
1/4	8.0	310.1
G	8.2	309.9
E. d	7.48	310.58
	2+75	
E. d	6.86	311.20
G	7.6	310.5
1/4	7.4	310.7
⊕	7.4	310.7
1/4	7.6	310.5
G	7.7	310.4
w. d	6.93	311.13
	3+00	
w. d	6.30	311.76
G	7.2	310.9
1/4	7.0	311.1
⊕	6.7	311.4

To page 37 Notes reduced Sept - 1-39
 CBH

318.06

Nile St.

16

1/4	6.9	311.2
G	7.2	310.9
E. d	6.25	311.81
	3+25	
E. d	5.95	312.11
G	6.7	311.4
1/4	6.5	311.6
⊕	6.3	311.8
1/4	6.6	311.5
G	6.8	311.3
w. d	5.95	312.11
	3+50	
w. d	5.59	312.47
G	6.5	311.6
1/4	6.2	311.9
⊕	5.9	312.2
1/4	6.1	312.0
G	6.4	311.7
E. d	5.70	312.36

318.06

4700

E. d	5.24	312.80
G	5.8	312.3
1/4	5.6	312.5
ϕ	5.4	312.7
1/4	5.6	312.5
G	6.0	312.1
w. d	5.08	312.98

4750

w. d	4.55	313.51
G	5.2	312.9
1/4	4.9	313.2
ϕ	4.9	313.2
1/4	5.1	313.0
G	5.6	312.5
E. d	4.82	313.24

5100

E. d	4.39	313.67
G	5.0	313.1
1/4	4.9	313.2
ϕ	4.5	313.6

318.06

Nile St.

17

1/4	4.5	313.6
G	4.7	313.4
w. d	4.10	313.96

5150

w. d	3.60	314.46
G	4.2	313.9
1/4	4.0	314.1
ϕ	4.2	313.9
1/4	4.5	313.6
G	4.6	313.5
E. d	4.02	314.04

5195

E. d	3.64	314.42
G	4.4	313.7
1/4	4.0	314.1
ϕ	3.8	314.3
1/4	3.8	314.3
G	3.9	314.2
w. d	3.23	314.83

318.06

410 S. Line Myrtle St

w. cl		3.05	315.01
G. pav	S. End	3.60	314.46
ly "	" "	3.40	314.66
± "	" "	3.40	314.66
1/4 "	" "	3.62	314.44
G "	" "	4.05	314.01
E. cl		3.50	314.56

10' N of S. = S. cl. Line

E. Line	cl	3.53	314.53
E. "	pav	4.02	314.04
cl. Line	"	3.53	314.53
1/4 "	"	3.50	314.56
± "	"	3.33	314.73
1/4 "	"	3.33	314.73
cl. Line	"	3.53	314.53
w. "	"	3.53	314.53
w. "	cl.	2.96	315.10

10's of N = N cl. line

w. line	cl	2.43	315.63
" "	pav	3.03	315.03

318.06

Nile St

18

cl. line	pav	3.17	314.89
1/4 "	"	3.00	315.06
± "	"	2.96	315.10
1/4 "	"	3.10	314.96
cl. line	"	3.39	314.67
E "	"	3.54	314.52
E "	cl.	2.96	315.10

0+00 = N. Line Myrtle
Dwight. St

E. cl		2.98	315.08
G. pav	N. End	3.38	314.68
1/4 "	" " "	2.97	315.09
± "	" " "	2.82	315.24
1/4 "	" " "	2.84	315.22
G "	" " "	3.06	314.98
w. cl		2.48	315.58

chk B.M.D.P.

3.52

314.54 = 214.57

S.E. Nile
& Myrtle
Sts.

318.06

0+50

W. cl	2.43	315.63
G	3.0	315.1
1/4	2.7	315.4
⊕	2.7	315.4
1/4	2.8	315.3
G	3.4	314.7
E. cl	2.92	315.14

1+00

E. cl	2.83	315.23
G	3.2	314.9
1/4	2.6	315.5
⊕	2.5	315.6
1/4	2.5	315.6
G	2.7	315.4
W. cl	2.18	315.88

1+50

W. cl	2.12	315.94
G	2.15	315.6
1/4	2.3	315.8
⊕	2.2	315.9

318.04

Mile St

19

1/4	2.5	315.6
G	3.1	315.0
E. cl	2.60	315.46

2+00

E. cl	2.44	315.58
G	2.8	315.3
1/4	2.3	315.8
⊕	2.2	315.9
1/4	2.2	315.9
G	2.4	315.7
W. cl	2.03	316.03
T.P.	5.02	320.77

2+50

W. cl	4.69	316.08
G	5.0	315.8
1/4	4.8	316.0
⊕	4.8	316.0
1/4	5.0	315.8
G	5.5	315.3
E. cl	5.17	315.60

320.27

2+82

E. cl 5.01 315.76

+7.8 = wedge walk 4.79 315.98

+12.33 E " " 4.70 316.07

2+82 to 2+84 cl. busted

2+80 to 2+84 walk crushed.

3+00

E cl 12.33 = E. edge walk low 4.73 316.04

4 " -7.1 = W " " " 4.83 315.94

" " " " " 5.02 315.75

G 5.4 315.4

1/4 5.0 315.8

ϕ 4.6 316.2

1/4 4.7 316.1

G 5.0 315.8

W. cl 4.70 316.07

3+11

E. cl 4.90 315.87

+7.8 = W. edge walk 4.65 316.12

+12.33 E " " 4.61 316.16

320.77

3+50

W. cl 4.50 316.27

G 5.0 315.8

1/4 4.6 316.2

ϕ 4.5 316.3

1/4 4.8 316.0

G 5.3 315.5

E. cl 4.77 316.00

+7 = W. walk 4.71 316.06

+12.33 E " " 4.64 316.13

3+75

E. cl -12.33 = E. walk 4.64 316.11

-7 = W. " " 4.77 316.00

E. cl low 4.84 315.89

G 5.1 315.7

1/4 4.7 316.1

ϕ 4.5 316.3

1/4 4.5 316.3

G 4.7 316.1

W. cl 4.35 316.42

Mile St.

20

320.77

4+00

W. cl		4.33	316.44
G		4.6	316.2
1/4		4.5	316.3
ϕ		4.4	316.4
1/4		4.7	316.1
G		5.0	315.8
E. cl	Sunk	4.97	315.80
+7 = W. edge walk	tos.	4.70	316.07
+7 = " " "	" " N Buckled.	4.58	316.19
+12 ³³ 8	" " " "	4.66	316.11
+12 ³³ 2	" " S.	4.60	316.17
Walk. from 3+98 N. To 5+20 on E. N.G.			
	4+25		
E. cl	Low	5.33	315.44
+7.2 = W. edge walk	"	5.21	315.56
+12 ³³ 2 = 2 " "	"	5.43	315.34
	4+50		
E. cl - 7. = W. walk	Low	5.38	315.39
E. cl	"	5.28	315.49
G		5.0	315.8

320.77

Nile St

21

1/4		4.6	316.2
ϕ		4.3	316.5
1/4		4.4	316.4
G		4.7	316.1
W. cl		4.35	316.42
	5+00		
W. cl		4.30	316.47
G		4.7	316.1
1/4		4.5	316.3
ϕ		4.3	316.5
1/4		4.7	316.1
G		5.1	315.7
E. cl	Low	5.00	315.77
+7. = Wedge walk		4.68	316.09
+12 ³³ = 2 " "		4.60	316.17
	5+20		
E. cl - 12 ³³ = E. edge walk	(N.G. to S) or "N"	4.27	316.50
" " - 7 E.W. "	"	4.43	316.34
E. cl	Low	4.94	315.83
G		5.3	315.5

320.77

5+20 (con)

114	4.7	316.1
ϕ	4.3	316.5
114	4.5	316.3
G	4.8	316.0
w. d	4.55	316.22

5+19

w. d + 7. = E. edge walk	4.40	316.37
" " + 12 ³² W " " to S.	4.14	316.59
" " + 12 ³³ " " " " N	4.25	316.52

From 5+07 to Dwight Walk on W Sunk. Not badly cracked

5+07

w - 12 ³³ W side walk	4.09	316.68
w - 7' = E " " to S.	4.24	316.53
w - 7' = E " " to N	4.30	316.47
w. d	4.37	316.40

5+47

w. d - 12 ³³ = w. edge walk	4.33	316.44
" " - 7' = E " "	4.46	316.31
w. d	4.45	316.32
G	4.8	316.0
114	4.4	316.4

320.77

Mile St.

22

ϕ	4.2	316.6
114	4.5	316.3
G	5.1	315.7
E d	4.51	316.26

Sch to S N.E.
" " N O.K.

d. ok. to N.

5+60 Walk. good condition. Low

w. d ok to N	4.15	316.62
+7 = E. edge walk	4.19	316.58
+12 ³³ W " "	4.17	316.60

6+00

w. d - 12 ³³ = W. edge walk	4.02	316.75
--	------	--------

w. d - 7' = E " "	4.00	316.77
-------------------	------	--------

w. d	4.08	316.69
------	------	--------

G	4.8	316.0
---	-----	-------

114	4.3	316.5
-----	-----	-------

ϕ	4.0	316.8
---	-----	-------

114	4.5	316.3
-----	-----	-------

G	5.1	315.7
---	-----	-------

E d	4.26	316.51
-----	------	--------

320.77

6+11⁶⁷ = f. 67' Not S. line Dwight
South Edge full conc. Return.

E. cl	4.22	316.55	
G	5.1	315.7	
1/4	4.4	316.4	
⊕	4.0	316.8	
1/4	4.3	316.5	
G	4.8	316.0	
W. cl	4.11	316.66	
+7 = E edge walk to S.	4.13	316.64	
+7 = " " " N.	4.19	316.58	
+12 ³³ = W. edge walk to S.	4.17	316.60	
+12 ³³ = W " " " N.	4.12	316.65	
+14 = SW. Cor. walk. stub			
6+18 ⁵			
1/2 W. of W. cl. line S. End. cl. inlet.	4.91	315.86	gutter Lip.
6+23			
5' W. of W. cl. line = W. End. cl. inlet	5.03	315.74	gutter Lip.
" " " " " " " "	4.12	316.61	Top. cl
S. W. Return sunk, & Buckled.			Should. Be Replaced
" " cl. inlet seems OK.			

320.77

Nile St.
6+24 = S. cl. Dwight. St. { 14' cl. S
13' 1/4" } 23

W. Line = W. end. cl. Low	4.70	316.07	
gutter	5.1	315.7	
W. cl. line	4.7	316.1	
1/4	4.2	316.6	
⊕	4.1	316.7	
1/4	4.3	316.5	
E. cl	5.1	315.7	
E.	4.8	316.0	
E. E end. cl.	4.29	316.48	
cl. inlet S. E. cor			
Gutter Lip of intake	5.25	315.52	
5. 1/4			
E	4.7	316.1	
cl	4.9	315.9	
1/4	4.3	316.5	
⊕	4.1	316.7	
1/4	4.2	316.6	
cl	4.8	316.0	
W.	4.7	316.1	

320.77

Dwight

W	4.4	316.4
+8	3.8	317.0
cl	4.5	316.3
1/4	4.1	316.7
±	4.0	316.8
1/4	4.2	316.6
cl	4.7	316.1
E	4.5	316.3

N. 1/4

E	4.4	316.4
cl	4.7	316.1
1/4	4.2	316.6
±	3.9	316.9
1/4	4.1	316.7
cl	4.5	316.3
W	4.1	316.7

N. cl.

W. = W. end. cl. Return. N.G.	3.64	317.13
W. ground.	4.0	316.8
cl	4.4	316.4
1/4	4.0	316.8

320.77

Nile St

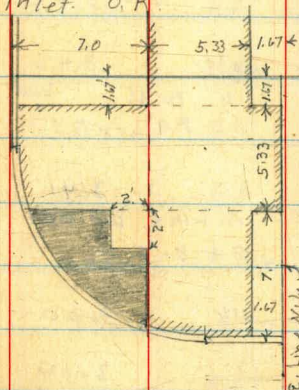
24

±	3.9	316.9
1/4	4.0	316.8
cl	4.6	316.2
E ground	4.1	316.7
E. = E. end. cl. Return	3.75	317.02

N.W. Return sunk & buckled should be replaced.

Shaded Area of N. E. Return to be replaced Nile & Dwight

curb. inlet. O.K.



N. Line Dwight.

N.W. Return

gutter Lip of catch basin 4.13 316.64

N.E. Return

gutter Lip of catch basin 4.58 316.19

		320.77		
1.67 S. of N. line = N. edge solid Return				
E. Line		3.55	317.22	
E. d		3.75	317.02	
G		4.5	316.3	
1/4		3.9	316.9	
±		3.4	317.0	
1/4		4.0	316.8	
G		4.2	316.6	
w. d		3.32	317.45	
1/7 = 0	E. edge walk	3.42	317.35	
+12.33	W " " to N. Low	3.27	317.50	
+12.33	W " " Return to S. "	3.41	317.36	
W. line		3.41	317.36	
	0+00 = N. line Dwight			
	0+8.5 N.			
w. d - 12.33	w. edge walk	3.00	317.77	
" " - 7.2	" " "	3.12	317.65	
" "		3.15	317.62	
T.P., B.P.	6.75	323.80	3.72	317.05 =
	0+50			
w. d		5.81	317.99	
G		6.5	317.3	
1/4		6.5	317.3	

		323.80	Nile St.	
±			4.4	317.4
1/4			6.7	317.1
G			7.1	316.7
E. d			6.30	317.50
	1+00			
E. d			5.84	317.96
G			6.7	317.1
1/4			6.1	317.7
±			5.9	317.9
1/4			6.0	317.8
G			6.0	317.8
w. d			5.26	318.54
	1+50			
w. d			4.77	319.03
G			5.3	318.5
1/4			5.4	318.4
±			5.3	318.5
1/4			5.7	318.1
G			6.1	317.7
E. d			5.33	318.77

323.80
2+00

E. cl	4.78	319.02
G	5.6	318.2
1/4	5.0	318.8
ϕ	4.8	319.0
1/4	4.9	318.9
G	5.0	318.8
W. cl	4.27	319.53

2+50

W. cl	3.71	320.09
G	4.5	319.3
1/4	4.3	319.5
ϕ	4.1	319.7
1/4	4.6	319.2
G	5.1	318.7
E. cl	4.30	319.50

2+78 Bad walk.

E. cl	4.03	319.77
+7' E. = w. edge walk to s.	3.78	320.02
+7' " " " " " N.	3.84	319.96

Replace 1 square each side of Break. 4. Lineal ft.

323.80

Nile St.

+12 ³³ E = E. edge walk to s.	3.66	320.14
" " " " " N.	3.79	320.01
2+98 Bad walk. at joint.		
z. cl	3.80	320.00
+7 = W. edge walk to s.	3.56	320.24
+7 = " " " " N.	3.63	320.17
+12 ³³ E " " " " N+S.	3.49	320.31
Replace 4. Lineal ft. 2. each side.		
3+00		

E. cl 3.80 320.00

G 4.7 319.1

1/4 4.1 319.7

ϕ 3.9 319.9

1/4 3.9 319.9

G 4.1 319.7

w. cl 3.34 320.46

3+10⁵ walk. OK.

E. cl 3.72 320.08

+7 = walk. 3.60 320.20

+12³³ " " 3.46 320.34

35

323.80

3+18 Bad. wall H. cracked at joint.
Replace 4 lineal ft 2. each side.

E. cl		3.61	320.19
+ 7.8 =	walk to S.	3.33	320.47
" =	" " N	3.40	320.40
+ 12 ³³ =	" " S	3.27	320.53
" =	" " N	3.24	320.56

3+50

w. cl		2.74	321.06
G		3.2	320.6
1/4		3.3	320.5
⊕		3.2	320.6
1/4		3.5	320.3
G		4.0	319.8
E. cl		3.32	320.48

4+00

E. cl		2.72	321.08
G		3.5	320.3
1/4		2.9	320.9
⊕		2.6	321.2
1/4		2.8	321.0

323.80

Nile St

27

G		2.4	321.0
w. cl		2.19	321.61
		4.50	
w. cl		1.75	322.02

G		2.3	321.5
1/4		2.3	321.5
⊕		1.9	321.9
1/4		2.2	321.6
G		2.9	320.9
E. cl		2.38	321.42

5+00

E. cl		1.97	321.83
G		2.6	321.2
1/4		2.0	321.8
⊕		1.6	322.2
1/4		1.4	322.0
G		2.1	321.7
w. cl		1.23	322.57

326.09

326.09

Nile St

N. cl.

29

11y 3.4 322.7

w. cl

3.13 322.96

cl 3.3 322.8

W G

3.8 322.3

W 3.0 323.1

cl

4.1 322.0

±

1/4

3.8 322.3

W 2.9 323.2

±

3.8 322.3

cl 3.3 322.8

1/4

4.0 322.1

1/4 3.5 322.6

cl

4.6 321.5

± 3.6 322.5

E G

4.8 321.3

1/4 4.0 322.1

E cl E. end.

4.09 322.00

cl 4.1 322.0

0 + 00 = N. Line Landis

E 4.4 321.7

E. cl

4.17 321.92

1/4

G

4.8 321.3

E 4.6 321.5

1/4

4.2 321.9

cl 4.3 321.8

±

4.0 322.1

1/4 4.0 322.1

1/4

4.0 322.1

± 3.7 322.4

G

4.1 322.0

1/4 3.7 322.4

w. cl

3.22 322.87

cl 3.6 322.5

W 3.6 322.5

0+50

w.d	4.00	322.09
G	4.9	321.2
1/4	4.8	321.3
£	4.7	321.4
1/4	5.2	320.9
G	5.7	320.4
e.d	5.00	321.09
1+00		
e.d	5.85	320.24
G	6.7	319.4
1/4	6.2	319.9
£	5.6	320.5
1/4	5.7	320.4
G	5.5	320.6
w.d	4.81	321.28
1+50		
w.d	5.70	320.39
G	6.5	319.6
1/4	6.4	319.7
£	6.3	319.8

1/4	6.7	319.4
G	7.4	318.7
e.d	6.60	319.49
2+00		
e.d	7.36	318.73
G	8.2	317.9
1/4	7.6	318.5
£	7.2	318.9
1/4	7.2	318.9
G	7.4	318.7
w.d	6.50	319.59
2+50		
w.d	7.46	318.63
G	8.4	317.7
1/4	8.2	317.9
£	8.2	317.9
1/4	8.5	317.6
G	8.9	317.2
e.d	8.30	317.79

326.09

3+00

E.d	9.16	316.93
G	9.6	316.5
1/4	9.2	316.9
£	9.0	317.1
1/4	8.9	317.2
G	9.1	317.0
w.d	8.19	317.99
	3+50	
w.d	9.00	317.09
G	9.6	316.5
1/4	9.8	316.3
£	9.6	316.5
1/4	10.0	316.1
G	10.7	315.4
E.d	9.92	316.17
	4+00	
E.d	10.74	315.35
G	11.5	314.6
1/4	11.0	315.1
£	10.4	315.7

326.09

Nile St

31

1/4	10.5	315.6
G	10.5	315.6
drive way	10.37	315.72
	4+50	
w.d	10.66	315.43
G	11.3	314.8
1/4	11.2	314.7
£	11.3	314.8
1/4	11.8	314.3
G	12.7	313.4
E.d.	11.59	314.50
T.P.	6.48	320.15
	5+17 = N. end. good. walk. on E.	
E.d - 12. ³³	6.61	313.54
E.d - 7.	6.68	313.47
E.d	6.81	313.34
G	7.4	312.7
1/4	7.2	312.9
£	6.7	313.4
1/4	6.8	313.3

G 6.6 313.5

W. eb 5.89 314.26

5+21 N. end good. eb. on 2.

5+47

W. Line 6.6 313.5

W. eb - 2.33 = W. edge walk. 6.44 313.71

" 4 - 7. = E " " 6.47 313.68

" " - 7. = E " " " 6.51 313.64

W. eb 6.54 313.61

G 7.1 313.0

1/4 7.3 312.8

⊕ 7.3 312.8

1/4 7.6 312.5

G 8.2 311.9

d 7.55 312.60

+7 walk 7.53 312.62

+12³³ " 7.58 312.57

E 7.5 312.6

5+56

E 6.72 313.43

+7. = walk 6.75 313.40

Est grade
314.39

Est grade
313.92

+12.33 6.65 313.50

W 7.1 313.0

5+62 = S. End. conc gutter

E eb 7.76 312.39 ✓

conc & S. End. 8.48 311.67

+ 3.75 W = conc & S. End. 8.45 311.70

5+76 = S. End. eb. inlet on 2

E 7.9 312.2

+ 11.5 E. edge conc. eb. inlet. 7.57 312.58

E. d 7.50 312.65 ✓

conc gutter 8.54 311.61

13.75 " " 8.52 311.63

1/4 8.4 311.7

⊕ 7.7 312.4

1/4 7.7 312.4

G 7.9 312.2

W eb. 7.10 313.05

+7. = E. walk 7.00 313.15

+12³³ = W " 6.90 313.25

W. 7.3 312.8

320.15

5+85.5 S. End grating on E.

3.75 W. of E. ch conc. gutter	8.95	311.20
G. ch inlet	9.09	311.06
E. ch	7.81	312.34
+2.5 = E. edge conc. ch inlet	7.84	312.31

5+87⁵ N. end. above grating

3.75 W. of E. ch = conc. gutter	8.99	311.16
G. ch inlet	9.27	310.88
E. ch	7.95	312.20
+2.5 E. edge ch inlet	7.98	312.17

5+95² S. End. ch. inlet. on W.

W. ch		
conc. gutter		
5+98 ¹ W. End. ch. inlet. on E.		
2.5 E. of E. ch. edge conc. ch inlet	8.27	311.88
E. ch	8.22	311.93
conc gutter	9.30	310.85
+3.75 W. = W. edge conc. gutter	9.04	311.11

5+99 = S. Line Wightman Ave

320.15

6+00² = S. End. Solid conc. Return on W.

Nile St

33

W. line ground. to S.	7.7	312.4
W. " Return	7.31	312.84
+1.67 W. edge walk. to S.	7.31	312.84
+7 = E. " " "	7.30	312.85
W. ch	7.30	312.85
Gutter a	8.20	311.95
"	7.8	312.3
E	7.8	312.3
"	8.3	311.8
+9.25 W. edge gutter	9.09	311.06
G.	9.36	310.79
E. ch	8.31	311.84
E. line	7.8	312.3
6+01.4 ¹ N. End. E. ch.		
E. ch. N. End.	8.34	311.81
6+01.3 ² N. End. ch. inlet on W		
W. ch	7.30	312.85
G.	8.20	311.95

14' N 320.15 S. cl. Line

E	7.6	312.5
+12	8.0	312.1
cl	8.7	311.4
1/4	8.1	312.0
±	7.7	312.4
1/4	7.7	312.4
cl	8.0	312.1
W. conc. cl. W. End	7.37	312.78
W ground	6.9	313.2
27' N of S = 5.1/4 on W.		
W	6.7	313.4
cl	7.5	312.6
1/4	7.6	312.5
±	7.5	312.6
1/4	7.8	312.3
cl	8.3	311.8
+1	7.4	312.7
E	6.9	313.2

320.15 N125E

40' N of S = ± on W.		
E	6.6	313.5
+12	7.1	313.0
cl	7.4	312.3
1/4	7.4	312.7
±	7.1	313.0
1/4	7.3	312.8
cl	7.5	312.6
W	6.7	313.4
55' N of S = { 2' N. of N 1/4 on W. N cl. line on E.		
W	6.3	313.8
+7	6.3	313.8
cl	7.2	312.9
1/4	6.9	313.2
±	6.7	313.4
1/4	7.0	313.1
cl	7.5	312.6
+1	6.9	313.2
E ground	6.6	313.5
E conc. cl. E. End	6.24	313.89

320.15
 66' N. of S. = { N. di. on ul
 1' N. of N. Line on E.

e. db	6.13	314.02
G	7.3	312.8
1/4	6.7	313.4
⊕	6.4	313.7
1/4	6.7	313.4
cb	6.8	313.3
+7	5.8	314.3
W ground	5.6	314.5
w. ch. w. end.	5.20	314.95

0+20 = N. Line Wrightman on N.

w. ch.	5.13	315.02
G	6.1	314.0
1/4	6.3	313.8
⊕	6.2	313.9
1/4	6.4	313.7
G	7.0	313.1
E. db	5.92	314.23

320.15

Nitest

35

0+50

E. db	5.10	315.05
G	5.6	314.5
1/4	5.7	314.7
⊕	5.2	314.9
1/4	5.2	314.9
G	5.4	314.7
w. db	4.44	315.71

1+00

w. db	3.74	316.41
G	4.7	315.4
1/4	4.2	315.9
⊕	4.3	315.8
1/4	4.5	315.6
G	5.2	314.9
E. db	4.34	315.77

1+50

E. db	3.46	316.69
G	4.5	315.6
1/4	3.7	316.4
⊕	3.4	316.7

320.15

1.4		3.4	316.7
G		4.0	316.1
W. el		3.01	317.14
	2+00		
W. el		2.25	317.90
G		3.0	317.1
1.4		2.8	317.3
⊕		2.7	317.4
1.4		2.9	317.2
G		3.6	316.5
E. el		2.68	317.47
	250		
E. el		1.89	318.26
G		2.4	317.7
1.4		2.1	318.0
⊕		2.0	318.1
1.4		2.0	318.1
G		2.1	318.0
W. el		1.50	318.65

320.15

Nil. 51

36

3+00

W. el			0.82	319.33
G			1.5	318.6
1.4			1.4	318.7
⊕			1.2	318.9
1.4			1.5	318.6
G			1.6	318.5
E. el			1.18	318.97
	3+50			
E. el			0.32	319.83
G			0.7	319.4
1.4			0.6	319.5
⊕			0.3	319.8
1.4			0.7	319.4
G			0.8	319.3
E. el			0.17	319.98
T.P.	6.38	326.35	0.18	319.97

326.35

4+00

W. d	5.57	320.78
G	6.0	320.3
1/4	5.9	320.4
ϕ	5.8	320.5
1/4	6.1	320.2
G	6.5	319.8
E. d	5.95	320.40

4+50

C. d	5.11	321.24
G	5.8	320.5
1/4	5.4	320.9
ϕ	5.1	321.2
1/4	5.1	321.2
G	5.6	320.7
W. d	4.88	321.47

4+64 = S. End. db. inlet. one

E. d	4.84	321.51
G. hip	5.85	320.50
+ 2. W = S.W. cor. grating	5.60	320.75

326.35

Nile St.

37

4+80 = N. End. above db. inlet. one

E. d	4.69	321.66
G. = hip. of Inlet	5.69	320.66

4+81 = S. Line Univ Ave

W. d	4.38	321.97
G. par. S. End.	4.71	321.64
1/4 " " "	4.67	321.68
ϕ " " "	4.75	321.60
1/4 " " "	5.11	321.24
G " " "	5.36	320.99
E. d	4.70	321.65

N = S. d. Line Univ

E d	4.39	321.96
E. G par	4.80	321.55
db C.B. grating	5.21	321.14
1/4 par	5.18	321.17
ϕ "	5.16	321.19
1/4 "	5.06	321.29
db "	4.90	321.45
W G "	4.65	321.70
W d	4.22	322.13

B.M. B.P. S.W. Nile + Univ Ave

4.23 322.12

322.15

Notes reduced Sept 2 - 39 - C.B.H.

9/5/39
Miller
Walker
BlissX. Sec. Colley c Way S. of El Cajon
Continued from F.B. 1542-72
For Realignment + F.B. 1556-1Indexed
c-s.K.

453.56

B.M. B.P.

0-83

466.10

465.27

N.W. Colley
+ El Cajon

W

1.4

452.2

G.M.K. 2+805 Sec FB 1542-72

3+50

W

10.3 ✓

455.8

W

3.0

450.6

d

10.8 ✓

455.3

d

4.1

449.5

1/4

11.0 ✓

455.1

1/4

3.9

449.7

d

10.9 ✓

455.2

d

4.5

449.1

1/4

11.0 ✓

455.1

+8

4.5

449.1

d

11.1 ✓

455.0

1/4

4.0

449.6

E

10.7 ✓

455.4

d

4.8

448.8

E

4.9

448.7

T.P.

0.21

453.56

12.75

453.35

4+00

-10

8.9

444.7

3+15

E

9.6

444.0

E

1.0

452.6

d

9.8

443.8

d

1.4

452.2

+6

9.4

444.2

1/4

1.6

452.0

1/4

7.7

445.9

+2

2.1

451.5

d

7.4

446.2

d

2.0

451.6

1/4

7.2

446.4

1/4

2.0

451.6

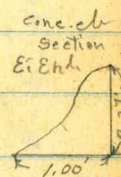
+4

7.4

446.2

cb	6.4	447.2
w.	5.5	448.1
	4+50	
w	7.7	445.9
d	8.5	445.1
+4	8.6	445.0
+5	9.4	444.2
1/4	9.3	444.3
d	9.5	444.1
+7	9.8	443.8
1/4	9.3	444.3
+5	11.7	441.9
d	12.5	441.1
E	13.5	440.1
+10	14.5	439.1
	4+55	
-10	12.6	441.0
E	11.8	441.8
cb	11.0	442.6
1/4	10.1	443.5

d	9.8	443.8
1/4	9.6	444.0
+5	9.6	444.0
+6	8.7	444.9
d	8.6	445.0
w	7.8	445.8
	4+57.5	
	concrete d	Graded.
	Asphalt Pav. N. of Mech. Good	5 ft.
	4+67.5	
	concrete d	Graded.
	4+97.5	
	5+07.5	
	4+57.5	
w	9.0	444.6
d	9.2	444.4
+5	9.8	443.8
1/4	9.8	443.8
d	10.0	443.6
1/4	10.6	443.0
d	11.4	442.2
E	11.7	441.9
+10	12.3	442.3



4+67 E=N. cl. Lin-

-10			12.4	441.2
e			12.2	441.4
el			11.8	441.8
'14			11.2	442.4
±			10.7	443.2
'14			10.2	443.4
cl			10.0	443.6
W	Top. cl	E. End	9.14	444.42
W	gutter pav	" "	9.41	444.15
+50	"		6.38	447.18
+50	Top. cl		6.09	447.47
			4+82 E ST	
-50	Pav p.		6.42	447.14
W.	" E. End.		9.45	444.11
el			10.2	443.4
'14			10.6	443.0
±			11.1	442.5
'14			11.6	442.0
cl			12.0	441.6
e			12.7	440.9
+10			13.3	440.3

4+97 E=S. cl.

-10			13.5	440.1
e			13.1	440.5
cl			12.3	441.3
'14			11.9	441.7
±			11.5	442.1
'14			11.2	442.4
cl			10.6	443.0
W	gutter pav	E. End	9.97	443.59
W	cl.	" "	9.67	443.89
+50	"		6.54	447.02
+50	gutter pav		6.87	446.69
			5+07.5	
W			9.7	443.9
cl			10.4	443.2
'14			10.8	442.8
+5			11.5	442.1
'14			11.8	441.8
±			11.9	441.7
+9			12.2	441.4
'14			11.8	441.8

453.56

441.15

College way

41

cl 12.3 441.3

14 2.5 438.6

e 13.0 440.6

e 2.9 438.2

+10 13.6 440.0

+7 3.0 438.1

5425

14 3.7 437.4

-10 15.5 438.1

+3 5.0 436.1

e 14.3 439.3

cl 5.8 435.3

cl 13.2 440.4

e 7.0 434.1

14 13.2 440.4

+10 8.0 433.1

e 13.4 440.2

5475

14 13.2 440.4

-10 9.1 432.0

+5 13.1 440.5

e 8.2 432.9

cl 11.4 442.2

cl 7.6 433.5

w 10.4 443.2

14 6.6 434.5

5450

+6 6.0 435.1

w 12.4 441.2

e 4.8 436.3

cl 13.4 440.2

14 4.3 436.8

T.P. 0.61 441.15 13.02 440.54

+8 4.1 437.0

cl 2.8 438.3

+4 2.7 438.4

w 2.0 439.1

441.15
6500

w	4.4	436.7
dr	5.4	435.7
+2	6.6	434.5
1/4	6.2	434.9
ϕ	6.6	434.5
1/4	7.6	433.5
dr	8.8	432.3
E	9.9	431.2
+10	10.0	431.1

Drainage from N.E.

6730

-10 ϕ wash	10.5	430.6
G	10.4	430.7
dr	9.9	431.2
1/4	8.6	432.5
ϕ	8.2	432.9
1/4	8.0	433.1
+7	8.1	433.0
+8	6.7	434.4
dr	6.3	434.8
w	4.7	436.4

441.15

College Way

42

6450

w	7.0	434.1
dr	8.1	433.0
+2	9.1	432.0
1/4	9.1	432.0
ϕ	9.0	432.1
1/4	9.3	431.8
dr	10.0	431.1
E ϕ wash	11.1	430.0
+10	10.5	430.6

6490

-10	11.1	430.0
E ϕ wash	11.2	429.9
dr	11.0	430.1
1/4	10.9	431.2
ϕ	10.6	430.5
1/4	10.5	430.6
+8	10.6	430.5
dr	10.0	431.1
w	9.0	432.1

438.78

7+82 (con)

w	10.4	428.4
+10	10.2	428.6
	8+18	
-10	11.3	427.5
w	11.4	427.4
el	11.0	427.8
+3	11.8	427.0
1/4	11.6	427.2
⊕	11.4	427.4
1/4	11.2	427.6
el	10.9	427.9
E	11.0	427.8
+10	10.6	428.2
	8+60	
-10	8.8	430.0
E	9.8	429.0
el	11.0	427.8
1/4	11.0	427.8
⊕	11.1	427.7
1/4	11.3	427.5

low point
in st.

438.78

College way 44

+6	11.6	427.2
el	11.2	427.6
w	Wash spreads out.	11.6
+10		11.7
	9+00	
-10	11.5	427.3
w	11.3	427.5
el	11.1	427.7
+5	11.3	427.5
1/4	10.9	427.9
⊕	10.5	428.3
1/4	10.0	428.8
el	9.8	429.0
E	9.2	429.6
+10	8.0	430.8
	9+57 N. Line	Estelle
-10	6.4	432.4
E	6.8	432.0
el	7.6	431.2
1/4	8.3	430.5

438.78

9+57 con

±	8.8	430.0
14	9.5	429.3
et	10.0	427.8
W	10.6	428.2
110	11.4	427.4

15' s. of N. line

-10	12.2	426.6
W	11.2	427.6
d	10.1	428.7
14	9.5	429.3
±	8.9	429.9
114	8.6	430.2
d	7.9	430.9
E	6.8	432.0

25' s. of N = N. edge asphalt Pav

E	7.51	431.27
±	9.22	429.56
W ₁	10.95	427.83

438.74

10' s. of N. line = S. cl. Estelle

W.	cl	10.60	428.18
W	gutter pav	11.02	427.76
±	" "	9.24	429.50
±	cl	8.88	429.90
E.	"	7.16	431.62
E	gutter pav.	7.57	431.21

13' w. of W line

BM. C.T. (S.T. line Estelle)

0.62 438.16 = 438.15

FB1556-15

College Way
45

Estudillo St Cross Section
Pacific Highway to Moore St.

BM	2.16	8.63	6.47
	0+0 = N.L. Pacific		
E on Walk	4.80	3.83	
+9.3 - Existing C/TOP	4.69	3.94	✓
Gutter	5.63	3.00	✓
Cb on Pav.	5.61	3.02	
+2.5 - 1/4" Box to Oil Sta.	5.53	3.10	
1/4 on Pav	5.26	3.37	
1/4 " "	5.17	3.46	✓
1/4 " "	5.20	3.43	
Cb " "	5.49	3.14	✓
+4.7 - Fly Conc Dr Pav.	5.54	3.09	✓
H	5.06	3.57	
	0+30		
H	4.74	3.89	
Cb = 1/4" Conc. Dr.	5.35	3.28	✓
1/4	5.0	3.6	
1/4	5.0	3.6	
1/4	5.0	3.6	

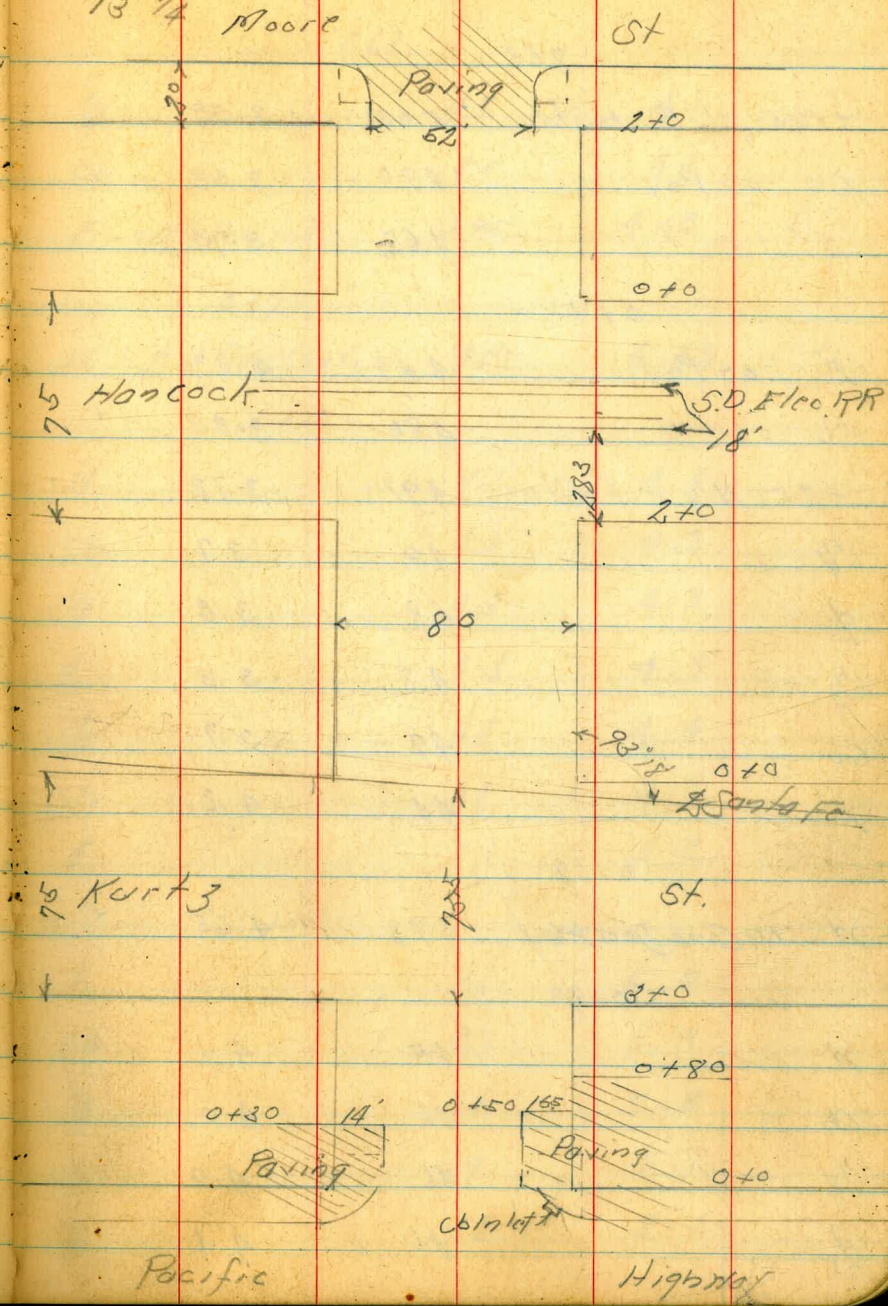
SE Top Hnd
Estudillo x
Pacific

Plotted on new profile Nov-1-37 although #290

80' wide
14' Cb
13' 1/4 Moore

Indexed
C.S.K.

Oct 30-39
Sisson
Hartman 46



8.63

+10.5 - 1/4 Pav to Sto	5.05	3.58	
Cb 07 Pav	4.95	3.68	✓
F " "	4.65	3.98	

0+50

F 07 Pav	4.40	4.23	
Cb " "	4.88	3.83	✓
+2.5 - 1/4 " to Sto	4.91	3.72	
1/4	4.9	3.7	
1/2	4.8	3.8	
1/4	4.8	3.8	
Cb	4.9	3.7	
1/4	4.4	4.2	

0+69

1/4 00 Conc Door Way	3.98	4.65	✓
----------------------	------	------	---

0+80

1/4	4.5	4.1	
Cb	4.6	4.0	
1/4	4.6	4.0	
1/2	4.5	4.1	

8.63

1/4	4.5	4.1	
Cb	4.5	4.1	
F - 1/4 Pav to Sto	3.95	4.68	✓

0+90

1/4 - 1/2 4' Door Conc	4.10	4.53	✓
------------------------	------	------	---

1+10

1/4	4.1	4.5	
Cb	4.3	4.3	
1/4	4.3	4.3	
1/2	4.3	4.3	
1/4	4.2	4.4	
Cb	3.8	4.8	
F	3.3	5.3	

1+50

F	2.6	6.0	
Cb	2.7	5.9	
1/4	2.8	5.8	
1/2	2.9	5.7	
1/4	3.2	5.4	

	8.63			
Cb		3.3	5.3	
N		3.3	5.4	
TP	11.00	17.42	2.21	6.42
	1+82			
N = (Cork Doorway)		11.13	6.29	✓
Cb		11.5	5.9	
1/4		11.0	6.4	
1/2		10.9	6.5	
1/4		10.4	7.0	
Cb		10.0	7.4	
F		10.0	7.4	
	2+25			
F		9.9	7.5	
Cb		9.9	7.5	
1/4		9.3	8.1	
1/2		10.3	7.1	
1/4		10.3	7.1	
Cb		10.5	6.9	
N		10.7	6.7	

	17.42		
	2+60		
N		8.8	8.6
Cb		8.5	8.9
1/4		8.4	9.0
1/2		8.2	9.2
1/4		8.3	9.1
Cb		8.0	9.4
F		7.8	9.6
	3+10 = S.L. Kurtz		
F		6.7	10.7
Cb		6.6	10.8
1/4		6.6	10.8
1/2		6.8	10.6
1/4		7.0	10.4
Cb		7.5	9.9
N		7.5	9.9
	5 Cb Kurtz		
N		7.2	10.2
Cb		7.1	10.3

Kurtz
75 wide
20 Cbs

17.42

1/4	6.8	10.6
1/2	6.5	10.9
1/4	6.5	10.9
Cb	6.6	10.8
F	6.9	10.5

H Kurtz

F	5.4	12.0
Cb	5.1	12.3
1/4	5.3	12.1
1/2	5.4	12.0
1/4	5.5	11.9
Cb	5.5	11.9
H	6.0	11.4

H Cb

H	5.3	12.1
Cb	5.3	12.1
1/4	5.4	12.0
1/2	4.7	12.7
1/4	4.3	13.1
Cb	4.1	13.3

17.42

49

F	3.9	13.5
---	-----	------

Cb + 12.5 = 2 Sink Fe on Center Sk.

F Top Rail	2.81	15.11	✓
1/2	2.51	14.91	✓
H	2.71	14.71	✓

H. Kurtz = 0+0

H	3.2	14.2
Cb	3.1	14.3
1/4	3.1	14.3
1/2	3.0	14.4
1/4	2.9	14.5
Cb	2.8	14.6
F	2.8	14.6

0+10

F	4.0	13.4
Cb	4.1	13.3
1/4	4.2	13.2
1/2	4.6	12.8
1/4	4.5	12.9
Cb	4.5	12.9
H	4.7	12.7

		17.42		
	0+20			
N		3.5	13.9	
Cb		3.2	14.2	
1/4		3.9	14.5	
1/2		2.8	14.6	
1/4		2.8	14.6	
Cb		2.8	14.6	
F		2.8	14.6	
	0+50			
F		1.5	15.9	
Cb		1.7	15.7	
1/4		1.8	15.6	
1/2		2.2	15.2	
1/4		2.2	15.2	
Cb		2.4	15.0	
N		2.7	14.7	
TP	1203	27.83	16.2	15.80
	0+80			
N		11.2	16.6	
Cb		10.6	17.2	

		27.83		
	1/4		11.0	16.8
	1/2		10.2	17.6
	1/4		9.9	17.9
	Cb		10.5	17.3
	F		10.4	17.4
		1+20		
	F		7.5	20.3
	Cb		8.1	19.4
	1/4		7.8	20.0
	1/2		8.0	19.8
	1/4		8.3	19.5
	Cb		8.2	19.6
	N		9.7	18.1
		1+50		
	N		6.3	11.5
	Cb		6.2	21.5
	1/4		6.5	21.3
	1/2		6.2	21.6
	1/4		5.9	21.9
	Cb		5.3	22.5
	F		5.5	22.3

27.83

210 = 84 Hancock

F	3.5	24.3
cb	3.6	24.2
1/4	3.7	24.1
1/2	3.6	24.2
1/4	3.6	24.2
cb	3.4	24.4
H	3.5	24.3

54 + 12

H	3.5	24.3
cb	3.4	24.4
1/4	3.4	24.4
1/2	3.4	24.4
1/4	3.4	24.4
cb	3.4	24.4
F	3.3	24.5

54 + 28.3 = S Rail S.D.Elec R.R

F = Top Rail	2.82	25.01	✓
1/2 " "	2.91	24.92	✓
H " "	3.01	24.82	✓

27.83

54 + 27.5 = 8 Hancock

H	29	24.9	
cb	30	24.8	
1/4	29	24.9	
1/2 02 M.H. Riv	278	25.05	✓
1/4	25	25.3	
cb	27	25.1	
F	28	25.0	

1/2 + 8.8 = N Rail S.D.Elec R.R

F Top Rail	2.72	25.11	✓
1/2 " "	2.78	25.05	✓
H " "	2.84	24.99	✓

1/2 + 25

H	1.9	25.9
cb	1.8	26.0
1/4	2.0	25.8
1/2	1.9	25.9
1/4	2.3	25.5
cb	2.3	25.5
F	2.2	25.6

2783

H.L. Hancock = 0 + 0

F		14	26.4
Cb		1.9	25.9
'4		1.6	26.2
2		1.0	26.8
'4		0.9	26.9
Cb		1.2	26.6
H		1.3	26.5
TP	1227	3986	0.24
		0 + 4	27.59
H		13.0	26.9
Cb		12.9	27.0
'4		12.4	27.5
2		12.5	27.4
'4		11.3	28.6
Cb		11.1	28.8
F		13.0	26.9
		0 + 25	
F		12.5	27.4
15		10.2	29.7

3986

52

Cb		9.9	30.5
'4		9.5	30.4
2		9.9	30.5
'4		9.9	30.5
Cb		9.7	30.2
H		11.7	28.2
		0 + 50	
H		7.1	32.8
Cb		7.0	32.9
'4		7.1	32.8
2		7.4	32.5
'4		7.4	32.5
Cb		7.3	32.6
16		7.9	32.0
F		12.1	27.8
		0 + 75	
F		10.1	29.8
10		4.9	35.0
Cb		4.9	35.0
'4		4.6	35.3

		39.86		
1/2		4.8	35.1	
1/4		4.8	35.1	
cb		5.0	34.9	
N		4.6	35.3	
	1x0			
N		2.2	37.7	
cb		2.2	37.7	
1/4		2.2	37.7	
1/2		1.6	38.3	
1/4		2.1	37.8	
cb		2.7	37.2	
F		3.3	36.6	
TP	11.57	50.20	123	38.63
	1+25			
F		10.2	40.0	
cb		9.2	41.0	
1/4		9.0	41.2	
1/2		8.8	41.4	
1/4		9.5	40.7	
cb		9.5	40.7	

		50.20		
N		10.3	39.9	
	1+50			
N		8.1	42.1	
cb		6.4	43.8	
1/4		6.3	43.9	
1/2		4.9	45.3	
1/4		5.5	44.7	
cb		6.4	43.8	
F		7.1	43.1	
	1+75			
F		5.2	45.0	
cb		3.8	46.4	
1/4		3.1	47.1	
1/2		3.9	46.3	
1/4		3.9	46.3	
cb		4.5	45.7	
N		5.5	44.7	
	2x0 = 52.1000			
N		2.8	47.4	
cb Top		3.06	47.14	v

50.20

Gutter on Pav	3.53	46.67	✓	
" " "	3.39	46.81		
L " "	3.54	46.66	✓	
" " "	3.84	46.36		
Gutter " "	4.38	45.82	✓	
Cb Top	3.94	46.26	✓	
F	4.0	46.2		
20' S.Cb L Moore Plan shows 14' cbs				
F on Pav	4.56	45.64	✓	
L " "	4.03	46.17	✓	
H	3.55	46.65	✓	
TP	12.30	61.80	0.70	49.50
TP	10.98	72.24	0.54	61.26
TP	8.81	80.07	0.98	71.26
B.M.	1.98	78.09		

NE BP
Estudillo
7.20 Falla
78.09

Fdh.T.

Fdh.T.

L-Hon S

Fd Pipe

Fd Fdh

120'

10

0.21
Fd Small
Pipe

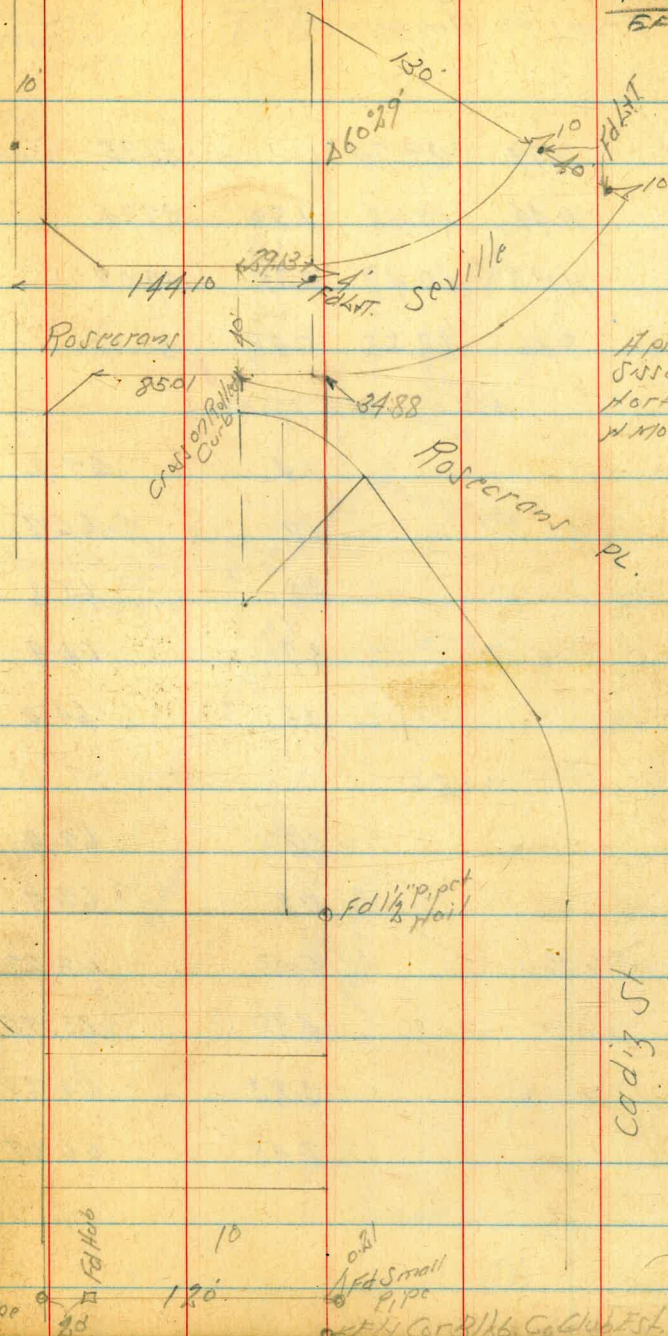
out to Cor 2116 Co. Club Est.

Tic Points Pascerans & Lyon

INDEXED

SFB

54



April 20-4
Sisson
Northway
W Moore

PL.

Cadi 3 St

	68.55		
	0+50		
H 02 Pay	4.80	63.75	
Cb " "	5.76	62.79	
£ " "	6.73	61.82	
+11.5 = Sly "	7.05	61.50	
Cb	7.5	61.1	
S	7.4	61.2	
	0+75		
S	9.5	59.1	
Cb	9.3	59.3	
+8 = Sly Pay	9.21	59.31	
£ 02 "	8.58	59.97	
Cb " "	7.60	60.95	
H " "	6.47	62.08	
	1+0		
H 02 Pay	8.68	59.87	
Cb " "	10.00	58.55	
£ " "	11.00	57.55	
+12 = Sly "	11.42	57.13	

	68.55		
Cb	11.6	57.0	
S	11.8	56.8	
TP	1.81	58.15	12.21
	1+25		
S		3.0	55.2
Cb		3.0	55.2
+5 = Sly Pay		2.76	55.39
£ 02 "		2.49	55.68
Cb " "		1.67	56.48
H " "		0.48	57.67
	1+50		
H 02 Pay		2.17	55.98
Cb " "		3.37	54.78
£ " "		4.11	54.04
+10 = Sly "		4.21	53.94
Cb		1.3	53.8
S		.49	53.3

5815

1+75

-18 = N/4 Pav La Solla	10.30	47.85
J	7.7	50.5
Cb	6.9	51.3
+5 = Pav B.C.	5.70	52.45
J on Pav	5.57	52.58
Cb " "	5.17	52.98
H " "	4.10	54.05

1+85

H on Pav	5.17	52.98
Cb " "	5.82	52.33
J " "	6.20	51.95
+10 " "	6.87	51.28
Cb " "	7.55	50.60
J " "	8.85	49.30
+12 = N/4 Pav La Solla	10.64	47.51

2+0

-6 = N/4 Pav La Solla	11.66	47.09
J on Pav	10.40	47.75

5815

Cb on Pav	9.05	49.10
J " "	8.34	49.81
+10 " "	6.67	51.48
Cb " "	6.62	51.53
H " "	6.49	51.66

2+25

H on Pav	8.34	49.81
Cb " "	8.99	49.16
J " "	10.22	47.93
Cb " "	11.77	46.38
+2 = N/4 Pav La Solla	12.01	46.14
J on Pav	12.13	46.02
TP 260 48.61	12.14	46.01

2+50

J on Pav	3.26	45.35
Cb " "	3.32	45.29
+12 = N/4 Pav La Solla	3.18	45.43
J on Pav	3.00	45.61
Cb " "	1.73	46.98

	48.61			
H on Pav	1.13	47.48		
	2.75			
H on Pav	2.68	45.93		
Cb " "	3.58	45.03		
+5' - Nly Pav La Jolla	4.02	44.59		
f on Pav	4.16	44.45		
	3+0 = E.L. Ampudia			
H = Nly Pav La Jolla Blvd	4.70	43.91		
TP	2.53 46.01 5.13	43.48		
	N.L. Ampudia = 0+0			
S - Sly Edge Walk	3.62	42.39		
+5' - Nly " "	3.73	42.28		
S Cb Top	3.90	42.11		
Gutter	4.50	41.51		
	0+11.4			
S Cb Gutter	4.97	41.04		
S Cb Top	4.43	41.58		
+5' - Nly Edge Walk	4.35	41.66		
S L - Sly " "	4.26	41.75		

	46.01			
	0+50			
S L - Sly Edge Walk	6.27	39.74		
+5' - Nly " "	6.28	39.73		
	0+0 Curb Elev on Sly La Jolla Blvd			
Top Cb	5.06	40.95		
Gutter	5.47	40.54		
	0+50			
Top Cb	5.77	40.24		
Gutter	6.31	39.70		
TP	4.79 39.95 10.85	35.16		
B.M.	8.00	31.95		
				N.Y.B.P. Condor Sandwich 31.95

Curb Levels Withberby + California

INDEXED
E.F.B.

May 20
Sisson
Northgar 59
H. Moore

BM	12.40	82.23		59.83	N.E.B.P. Withberby La Jolla Ave
TP	12.23	93.82	0.64	81.59	
TP	12.19	105.87	0.14	93.68	
TP	11.90	117.58	0.19	105.68	
TP	12.29	129.66	0.21	117.57	
TP	10.93	140.38	0.21	129.45	

E.L. Withberby

S Top Cb		5.46		134.92	
Gutter		5.85		134.53	
N Gutter		4.78		135.60	
N Top Cb		4.33		136.05	
BM		4.29		136.09	N.E.B.P. Sisson Withberby Calif.

Congress St Additional Section

BM	8.50	51.98		43.48	H.E.P. Tech Congress St Hampden 1891-58
				17.75	
S-50	=	La Jolla Blvd		4.15	
S-75	=	S Gutter	" "	5.17	
S-75	=	SCb Top	" "	4.62	
				2+0	
S-62	=	SCb under La Jolla Blvd		5.94	
S-62	=	S Gutter	" "	5.94	
S-36.5	=	La Jolla Blvd		5.00	
				2+25	
S-23	=	La Jolla Blvd		5.87	
S-49	=	S Gutter La Jolla Blvd		6.63	
S-49	=	SCb Top		6.07	
				2+50	
S-36.5	=	SCb Top La Jolla		6.85	
S-36.5	=	Gutter	" "	7.38	
S-9	=	La Jolla Blvd		6.66	

		51.98	
BM	2+75		
TP	$\frac{1}{2} + 20 = \frac{1}{2}$ LaSolla Blvd	7.44	
TP	S	7.51	
TP	+ 241 = S Gutter ^{cb ip 0-} LaSolla Blvd	8.23	
TP	3+0		
TP	- 10.5 = S cb LaSolla Blvd	8.41	43.57
	- 10.5 = S Gutter	8.97	
S	S on Paving	8.52	
	cb " "	8.48	
H	+ 8 = $\frac{1}{2}$ LaSolla Blvd	8.28	
H	$\frac{1}{2}$ on Paving	8.25	
B	cb " "	8.26	
H		8.13	43.85

IMPROVED TABLES
AND
INFORMATION

51.98
2.51
5.47
57.96
5.47
53.49

1364
226

55
105

14
5
17
105
295
400
105
505
810
65
66
14
80

52
10
442
105
300
42.7
257.3

71.5
2
14
50
700
50.13
91.04
115.80
956.97

31007
187
289.7

675
17
925

3077
1020
101.68
111.24
125
0.62
63

Dwight suit
0 + 48 to 1 + 08

lower 2