

1571



EXPLORERS

OF THE WEST

NO. 405

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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ENGINEERING DEPARTMENT
CITY OF SAN DIEGO.
CALIFORNIA.

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface and is sewed with Bing Special Enamel Waterproof Thread.

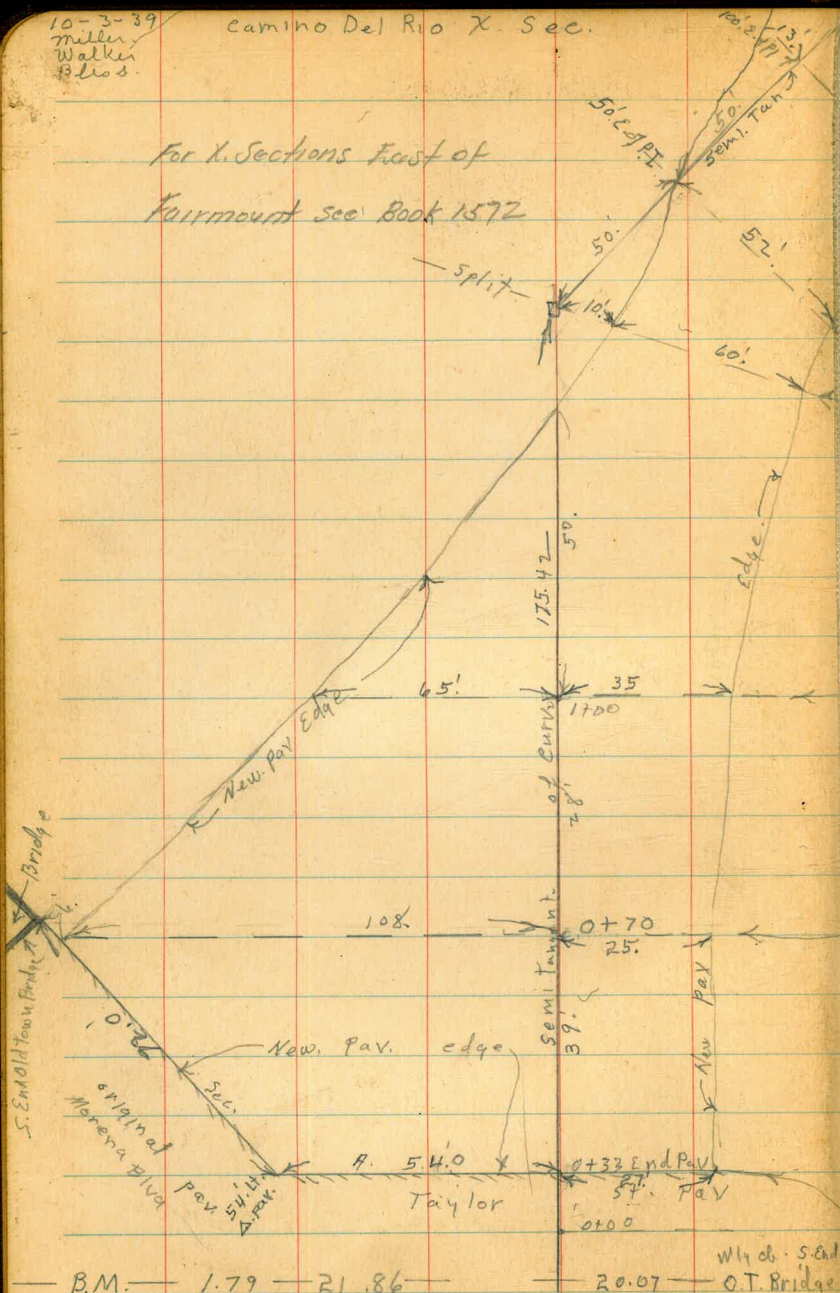
Made in U. S. A.

10-3-39

Miller
Walker
Bliss

camino Del Rio X. Sec.

for X. Sections East of
Fairmount see Book 1572



indexed
C.S.R.

S. Tan

100' E. of P.I.	13.8 8.0 13.3 T.S.	16.6 5.3 8.	16.1 5.8 P.	15.3 6.6 15. P	15.1 6.8 30P	15.1 6.8 40. B.	1
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50' E. of P.I.	13.8 8.1 5.4 7.5.	16.7 5.2 5. Tan B	16.4 5.5 9.0 N. Pav	16.5 6.4 42. S. Pav	15.5 6.4 52. B.
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Curve split. Δ	PI.	14.7	16.7	16.7	16.2	15.8	15.8
	E	7.2	5.2	5.2	5.7	6.1	6.1
	ST.	6.	10.3	20.	40. P	60. P	70. B.
	RT.	RT.	RT.	RT.	RT.	RT.	RT.

1400	18.9 3.0 65.8	18.4 3.5 55. P	17.8 4.1 30. P	17.8 4.6 S. Tan.	16.5 5.4 24. P	16.4 5.5 35. B
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0+70	19.4 2.5 108. P	18.4 3.5 60. P	18.0 3.9 30	17.5 4.4 S. Tan.	17.1 4.8 25. P	17.1 4.8 30. B
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Sec. 7 0+33	19.36 2.50 122. L. Sig Bl. Pav.	18.46 3.38 54.4. Bl. Pav.	17.84 4.02 54.4. D. Pav.	17.61 4.25 27.	17.69 4.27	16.83 5.03 27. Pav	17.16 4.70 30 End. cl.
					21.86		

Actual Stations, \pm Nat. Transit Line
 approx split of Improved Road.
 Pavement \rightarrow asled surface.
 T.S. = Toe of Top. Slope

Lt. Bern Lt. pav

\pm

Rt. pav Rt. Bern

2

7+00

\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow
X 5.8	15.6	15.6	15.4	15.4	15.6	12.3
14.5	4.7	4.7	4.9	4.9	4.7	8.0
30	19.	15.		15.	20.	22.
T.S.						

6+00

\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow
X 1.7	15.9	15.5	14.9	14.7	14.6	14.1
18.6	4.4	4.8	5.4	5.5	5.7	6.2
44.	21.	15.		15	18.	22.
T.S.						T.S.

5+00

\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow
X 1.0	15.4	14.9	14.5	14.5	14.3	14.7
18.5	4.9	5.4	5.8	6.0	6.0	5.6
42.	22.	15.		15.	16.	20.
T.S.						

4+00

\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow
X 7.3	15.5	15.4	14.9	14.7	14.5	13.8
13.0	4.4	4.4	5.4	5.6	5.8	6.5
30	19.	15.		15.	16.	18.
T.S.						

T.P. — 1.21 — 20.31 — 2.76 — 19.10 —

20.31

3+00

\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow
9.6	15.7	15.5	14.8	14.6	14.6	14.1
12.5	6.2	6.4	7.1	7.3	7.3	7.8
T.S.	22.	15.		15.	16.	18.
						T.S.

Sta 1+85³⁵ = E.C. = 175⁵⁵ E. of P.I

21.86

21.86

\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow
X 1.6	16.0	15.7	15.1	14.9	14.9	14.8
10.8	5.9	6.2	6.8	7.0	7.1	7.1
35	18.	15.		6.	20.	30.
T.S.						

T.S. Lt. Perm Lt. Pav. ϕ Rt. Pav. Rt. Barn T.S.

13400

\checkmark $\frac{9.0}{1.5}$ 30. 7.5	\checkmark $\frac{15.5}{5.0}$ 22	\checkmark $\frac{15.6}{4.9}$ 15.	\checkmark $\frac{15.5}{5.0}$	\checkmark $\frac{15}{76.7}$ 4.8 15.	\checkmark $\frac{15.5}{5.0}$ 23.	\checkmark $\frac{10.9}{9.6}$ 29. 7.5
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12400

\checkmark $\frac{8.7}{11.8}$ 31. 7.5	\checkmark $\frac{15.4}{5.1}$ 21	\checkmark $\frac{15.5}{5.0}$ 15.	\checkmark $\frac{15.4}{5.1}$	\checkmark $\frac{15.8}{4.7}$ 15.	\checkmark $\frac{15.8}{4.7}$ 22.	\checkmark $\frac{11.1}{9.4}$ 29. 7.8
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11400

\checkmark $\frac{10.1}{12.4}$ 29. 7.5	\checkmark $\frac{15.8}{4.7}$ 20.	\checkmark $\frac{15.8}{4.7}$ 15.	\checkmark $\frac{15.7}{4.8}$	\checkmark $\frac{15.9}{4.6}$ 15.	\checkmark $\frac{15.7}{4.8}$ 22.	\checkmark $\frac{11.2}{9.3}$ 29. 7.5
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10400

\checkmark $\frac{8.2}{12.3}$ 30. 7.5	\checkmark $\frac{16.1}{4.4}$ 19.	\checkmark $\frac{16.2}{4.3}$ 15.	\checkmark $\frac{16.1}{4.4}$	\checkmark $\frac{16.2}{4.2}$ 15.	\checkmark $\frac{16.2}{4.3}$ 21.	\checkmark $\frac{11.4}{9.1}$ 29. 7.5
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9400

\checkmark $\frac{16.6}{9.9}$ 27. 7.5	\checkmark $\frac{16.2}{4.3}$ 19.	\checkmark $\frac{16.2}{4.3}$ 15.	\checkmark $\frac{16.2}{4.3}$	\checkmark $\frac{16.7}{3.8}$ 15.	\checkmark $\frac{16.6}{3.9}$ 20.	\checkmark $\frac{13.0}{7.5}$ 26. 7.5
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RP — 3.47 — 20.47 — 3.31 — 17.00 —

— 20.47 —

8400

\checkmark $\frac{12.6}{10.7}$ 27. 7.5	\checkmark $\frac{16.2}{4.1}$ 18.	\checkmark $\frac{16.1}{4.2}$ 15.	\checkmark $\frac{15.9}{4.4}$	\checkmark $\frac{16.1}{4.2}$ 15.	\checkmark $\frac{16.0}{4.3}$ 21.	\checkmark $\frac{12.5}{7.8}$ 26. 7.5
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— 20.31 —

— 20.31 —

T.S. Lt. Bern Lt. Pen £ Rt. Pay. Rt. Bern T.S.

<u>11.6</u>	<u>15.7</u>	<u>16.0</u>	<u>16.4</u>	<u>16.3</u>	<u>16.1</u>	<u>10.0</u>
9.1	5.0	4.7	4.3	4.4	4.6	10.7
29.	23.	15.		15.	20.	29.

20.68

<u>10.7</u>	<u>16.5</u>	<u>16.3</u>	<u>16.6</u>	<u>16.5</u>	<u>16.6</u>	<u>10.9</u>
9.8	4.0	4.2	3.9	4.0	3.9	9.6
32.	24.	15.		15.	20.	29.
T.S.						T.S.

<u>10.5</u>	<u>16.1</u>	<u>16.2</u>	<u>16.2</u>	<u>16.0</u>	<u>16.0</u>	<u>9.9</u>
10.0	4.4	4.3	4.3	4.5	4.5	10.6
30.	23.	15.		15.	20.	29.
T.S.						T.S.

<u>10.2</u>	<u>16.1</u>	<u>16.1</u>	<u>15.7</u>	<u>16.0</u>	<u>16.2</u>	<u>9.8</u>
10.3	4.4	4.4	4.6	4.5	4.3	10.7
30.	22.	15.		15.	22.	31.
T.S.						T.S.

<u>10.1</u>	<u>15.6</u>	<u>15.8</u>	<u>15.8</u>	<u>15.9</u>	<u>15.8</u>	<u>8.8</u>
10.4	4.9	4.7	4.7	4.6	4.7	11.7
30.	23.	15.		15.	22.	22.
T.S.						T.S.

<u>9.7</u>	<u>15.5</u>	<u>15.7</u>	<u>15.7</u>	<u>15.7</u>	<u>15.7</u>	<u>9.3</u>
10.8	5.0	4.8	4.8	4.8	4.8	11.2
30.	22.	15.		15.	21.	30.
T.S.						T.S.

20.47

20.47

19700

T.P. 4.14 20.68 3.93 16.54

18400

17400

16400

15400

14400

Reduced 10-10-39
 By CCH 10-10-39. to page 36.

26+00

T.S.	Lt-Berm	Lt-Riv	Σ	Rt-Pay	Rt-Berm	T.S.
<u>13.1</u>	<u>16.2</u>	<u>16.4</u>	<u>16.4</u>	<u>16.4</u>	<u>16.6</u>	<u>12.1</u>
7.6	4.5	4.3	4.3	4.3	4.1	8.6
25.	21.	15.		15.	20.	28.

25+00

<u>10.0</u>	<u>16.6</u>	<u>16.7</u>	<u>16.9</u>	<u>17.0</u>	<u>17.0</u>	<u>11.4</u>
10.7	4.1	4.0	3.8	3.7	3.7	8.3
30.	20.	15.		15.	18.	26.

24+00

<u>10.2</u>	<u>16.3</u>	<u>16.5</u>	<u>16.8</u>	<u>16.8</u>	<u>16.7</u>	<u>10.8</u>
10.5	4.4	4.2	3.9	3.9	4.0	9.9
30.	21.	15.		15.	18.	28.

23+00

<u>10.1</u>	<u>16.5</u>	<u>16.7</u>	<u>16.8</u>	<u>16.9</u>	<u>16.7</u>	<u>10.6</u>
10.6	4.2	4.0	3.9	3.8	4.0	10.1
31.	22.	15.		15.	17.	26.

22+00

<u>9.9</u>	<u>16.2</u>	<u>16.3</u>	<u>16.3</u>	<u>16.3</u>	<u>16.1</u>	<u>10.0</u>
10.8	4.5	4.4	4.4	4.4	4.6	10.7
30.	21.	15.		15.	19.	28.
T.S.						T.S.

21+00

<u>10.7</u>	<u>16.2</u>	<u>16.3</u>	<u>16.2</u>	<u>16.2</u>	<u>16.1</u>	<u>9.9</u>
10.0	4.5	4.4	4.5	4.5	4.6	10.8
30.	21.	15.		15.	20.	29.
T.S.						T.S.

20+00

<u>11.3</u>	<u>16.3</u>	<u>16.1</u>	<u>16.3</u>	<u>16.2</u>	<u>16.4</u>	<u>10.0</u>
9.4	4.4	4.6	4.4	4.5	4.3	11.7
30.	24.	15.		15.	20.	31.
T.S.						T.S.

20.68

20.68

T.P. — 11.72 — 35.78 — 0.19 — 24.06 —

31+00

30+00

29+00

28+00

27+00

T.P. — 8.22 — 24.25 — 4.65 — 16.03 —

chk. B.M. 3 } old. Town Line Mon
 } ♀ Conde. St.

9.20

11.48 ✓

20.68

T.S. Lt. Bern Lt. Pav ♀ Rt. Pav Rt. Bern T.S.

6

<u>20.1</u>	<u>21.8</u>	<u>21.9</u>	<u>22.0</u>	<u>22.1</u>	<u>22.0</u>	<u>30.4</u>
4.2	2.5	2.4	2.3	2.2	2.3	+6.1
26.	21.	15.		15.	21.	27. Top Slope

<u>17.6</u>	<u>19.1</u>	<u>19.3</u>	<u>19.4</u>	<u>19.5</u>	<u>19.3</u>	<u>25.5</u>
6.7	5.2	5.0	4.9	4.8	5.0	+1.2
26.	24.	15.		15.	20.	23. Top S.

<u>15.3</u>	<u>17.1</u>	<u>17.4</u>	<u>17.8</u>	<u>17.8</u>	<u>17.9</u>	<u>14.3</u>
9.0	7.2	6.9	6.5	6.5	6.4	10.0
25.	22.	15.		15.	17.	21.

<u>14.3</u>	<u>16.4</u>	<u>16.7</u>	<u>16.8</u>	<u>17.0</u>	<u>17.0</u>	<u>12.7</u>
10.0	7.9	7.6	7.5	7.3	7.3	11.6
24.	20.	15.		15.	19.	25.

<u>13.8</u>	<u>16.2</u>	<u>16.1</u>	<u>16.3</u>	<u>15.5</u>	<u>16.6</u>	<u>12.2</u>
10.5	8.1	8.2	8.0	8.8	7.7	12.1
25.	21.	15.		15.	19.	25.

24.25

37+00

36+00

T.P. 10.17 45.42 0.53 35.25

35+00

34+00

33+00

32+00

35.78

T.Slope Lt.Berm Lt.pav E Rt.pav Rt.Berm T.Slope

<u>39.7</u>	<u>37.8</u>	<u>37.9</u>	<u>38.1</u>	<u>38.2</u>	<u>38.1</u>	<u>41.7</u>
5.7	7.6	7.5	7.3	7.2	7.3	3.7
22.	20.	15.		15.	18.	21.

<u>37.2</u>	<u>35.7</u>	<u>36.0</u>	<u>36.4</u>	<u>36.5</u>	<u>36.6</u>	<u>40.9</u>
8.2	9.7	9.4	9.0	8.9	8.8	4.5
23.	21.	15.		15.	18.	21.

45.42

<u>34.3</u>	<u>32.9</u>	<u>33.1</u>	<u>33.2</u>	<u>33.6</u>	<u>33.5</u>	<u>37.5</u>
1.5	2.9	2.7	2.6	2.2	2.3	1.7
22.	20.	15.		15.	19.	22.

<u>30.5</u>	<u>30.1</u>	<u>30.3</u>	<u>30.6</u>	<u>31.0</u>	<u>30.9</u>	<u>35.4</u>
5.3	5.7	5.5	5.2	4.8	4.9	0.4
19.	18.	15.		15.	18.	23.

<u>25.7</u>	<u>27.4</u>	<u>27.4</u>	<u>27.7</u>	<u>28.6</u>	<u>29.2</u>	<u>29.6</u>
10.1	8.4	8.4	8.1	7.2	6.6	6.2
22.	21.	15.		15.	20.	23.

<u>23.1</u>	<u>24.4</u>	<u>24.5</u>	<u>24.7</u>	<u>25.1</u>	<u>25.2</u>	<u>27.8</u>
12.7	11.4	11.3	11.1	10.7	10.6	8.0
24.	22.	15.		15.	20.	22.

35.78

44+00

43+00

42+00

41+00

40+00

39+00

38+00

T.Slope Lt.Berm Lt.Pav Σ Rt.Pav Rt.Berm T.Slope

8

<u>38.9</u>	<u>34.4</u>	<u>34.5</u>	<u>34.7</u>	<u>34.9</u>	<u>34.8</u>	<u>39.4</u>
6.5	11.0	10.9	10.7	10.5	10.6	6.0
24.	21.	15.		15.	19.	22.

<u>40.0</u>	<u>36.3</u>	<u>36.4</u>	<u>36.5</u>	<u>36.8</u>	<u>36.7</u>	<u>41.0</u>
5.4	9.1	9.0	8.9	8.6	8.7	4.4
22.	20.	15.		15.	18.	21.

<u>40.5</u>	<u>37.7</u>	<u>37.8</u>	<u>38.0</u>	<u>38.2</u>	<u>38.1</u>	<u>42.1</u>
4.9	7.7	7.6	7.4	7.2	7.3	3.3
22.	20.	15.		15.	19.	22.

<u>41.6</u>	<u>39.3</u>	<u>39.3</u>	<u>39.4</u>	<u>39.7</u>	<u>39.7</u>	<u>42.4</u>
3.8	6.1	6.1	6.0	5.7	5.7	3.0
19.	16.	15.		15.	18.	20.

<u>41.8</u>	<u>39.7</u>	<u>40.0</u>	<u>40.2</u>	<u>40.1</u>	<u>40.1</u>	<u>42.6</u>
3.6	5.7	5.4	5.2	5.3	5.3	2.8
22.	20.	15.		15.	17.	19.

<u>41.6</u>		<u>40.1</u>	<u>40.2</u>	<u>40.5</u>	<u>40.6</u>	<u>42.6</u>
3.8	5.3	5.3	5.2	4.9	4.8	2.8
22.	20.	15.		15.	18.	20.

<u>40.8</u>	<u>39.4</u>	<u>39.5</u>	<u>39.7</u>	<u>40.2</u>	<u>40.2</u>
4.6	6.0	5.9	5.7	5.2	5.2
22.	20.	15.		15.	18.

45.42

T. Slope Lt. Bern Lt. Pav E Rt. Pav. Rt. Bern T. Slope

50+00

<u>24.2</u>	<u>24.0</u>	<u>23.4</u>	<u>23.2</u>	<u>24.2</u>	<u>24.2</u>
10.8	11.0	11.6	11.8	10.8	10.8
20.	15.		15.	18.	20.

49+00

<u>24.6</u>	<u>26.3</u>	<u>25.8</u>	<u>25.3</u>	<u>25.0</u>	<u>24.8</u>	<u>25.7</u>
10.4	8.7	9.2	9.7	10.0	10.2	9.3
21.	18.	15.		15.	19.	20.

48+25

<u>18.3</u>	<u>26.8</u>	<u>26.9</u>	<u>26.8</u>	<u>26.7</u>	<u>26.3</u>	<u>22.0</u>
16.7	8.2	8.1	8.2	8.3	8.7	13.0
31.	19.	15.		15.	21.	29.

46+50

<u>20.6</u>	<u>29.5</u>	<u>29.5</u>	<u>29.4</u>	<u>29.7</u>	<u>29.8</u>	<u>22.0</u>
14.4	5.5	5.5	5.6	5.3	5.2	13.0
31.	19.	15.		15.	19.	28.

45+75

<u>37.3</u>	<u>30.9</u>	<u>31.0</u>	<u>31.0</u>	<u>31.1</u>	<u>31.0</u>	<u>37.0</u>
12.3	4.1	4.0	4.0	3.9	4.0	12.0
24.	21.	15.		15.	20.	23.

45+00

<u>38.2</u>	<u>32.2</u>	<u>32.5</u>	<u>32.7</u>	<u>32.9</u>	<u>32.7</u>	<u>39.2</u>
13.2	2.8	2.5	2.3	2.1	2.3	14.2
27.	23.	15.		15.	22.	25.

± Nail

T.P. — 0.30 — 35.00 — 10.72 — 34.70 — 44+00 — 35.00 —

45.42

55+00

<u>13.8</u>	<u>18.9</u>	<u>18.9</u>	<u>18.9</u>	<u>19.2</u>	<u>19.0</u>	<u>17.4</u>
10.7	5.6	5.6	5.6	5.3	5.5	7.1
2.9	2.1	1.5		1.5	1.9	2.3

54+00

<u>14.5</u>	<u>19.3</u>	<u>19.3</u>	<u>19.2</u>	<u>19.3</u>	<u>19.4</u>	<u>16.8</u>
10.0	5.2	5.2	5.3	5.2	5.1	7.7
2.8	2.1	1.5		1.5	1.9	2.3

53+00

<u>13.6</u>	<u>20.2</u>	<u>20.0</u>	<u>19.8</u>	<u>19.8</u>	<u>19.7</u>	<u>16.7</u>
10.9	4.3	4.5	4.7	4.7	4.4	7.4
3.3	2.2	1.5		1.5	1.8	2.3

52+00

<u>18.7</u>	<u>20.9</u>	<u>20.9</u>	<u>21.0</u>	<u>21.2</u>	<u>21.2</u>	<u>20.5</u>
10.8	3.6	3.6	3.5	3.3	3.3	4.0
3.2	2.2	1.5		1.5	2.0	2.2

51+00

<u>13.6</u>	<u>22.6</u>	<u>22.5</u>	<u>22.2</u>	<u>22.1</u>	<u>22.0</u>	<u>23.3</u>
10.9	1.9	2.0	2.3	2.4	2.5	1.2
3.1	2.0	1.5		1.5	1.7	1.9

50+50

<u>19.7</u>	<u>23.2</u>	<u>22.9</u>	<u>22.7</u>	<u>22.3</u>	<u>22.3</u>	<u>23.8</u>
4.8	1.3	1.6	1.8	2.2	2.2	0.7
2.4	2.1	1.5		1.5	1.7	1.7

T.P. 1.47 24.52 11.95 23.05

35.00

24.52

61+00

60+00

59+00

58+00

T.P.

5.20

24.97

4.75

19.77

57+00

56+00

24.52

T.S. Lt. Pav. Lt. Pav.

±

Rt. Pav. Rt. Berm T.S.

11

14.7 18.9 19.3

20.1

20.9 21.2 19.2

10.7 6.1 5.7
26. 20. 15.

4.9

4.1 3.8 5.8
15. 21. 25.

14.2 18.9 19.0

19.6

20.4 20.9 19.0

10.8 6.1 6.0
29. 22. 15.

5.4

4.6 4.1 6.0
15. 21. 24.

13.9 18.0 18.5

19.1

19.9 20.6 18.4

11.1 7.6 6.5
29. 22. 15.

5.9

5.1 4.4 6.6
15. 21. 24.

14.6 18.3 18.4

18.9

19.7 19.7 16.5

10.4 6.7 6.6
27. 21. 15.

6.1

5.3 5.3 8.5
15. 20. 25.

24.97

12.8 17.7 18.1

18.8

19.6 19.6 16.7

11.7 6.8 6.4
29. 19. 15.

5.7

4.9 4.9 7.8
15. 20. 25.

13.2 18.2 18.6

18.9

19.3 19.4 17.1

11.3 6.1 5.9
28. 21. 15.

5.6

5.2 5.1 7.4
15. 21. 25.

24.52

T.S. Lt. Bern Lt. Ry ϵ Rt. Ry Rt. Bern T.S.

<u>17.1</u>	<u>22.0</u>	<u>21.8</u>	<u>21.9</u>	<u>22.0</u>	<u>22.2</u>	<u>15.9</u>
7.9	3.0	3.2	3.1	3.0	2.8	9.1
2.4	2.1	1.5		1.5	1.9	2.9

<u>16.2</u>	<u>21.6</u>	<u>21.6</u>	<u>21.7</u>	<u>21.9</u>	<u>21.8</u>	<u>17.1</u>
8.8	3.4	3.4	3.3	3.1	3.2	7.9
2.7	2.0	1.5		1.5	1.9	2.6

<u>15.9</u>	<u>21.6</u>	<u>21.3</u>	<u>21.2</u>	<u>21.3</u>	<u>21.2</u>	<u>16.5</u>
9.1	3.4	3.7	3.4	3.7	3.8	8.5
2.8	2.0	1.5		1.5	2.0	2.8

<u>14.2</u>	<u>20.7</u>	<u>20.7</u>	<u>20.8</u>	<u>21.0</u>	<u>21.0</u>	<u>17.5</u>
10.8	4.3	4.3	4.2	4.0	4.0	7.5
3.0	2.0	1.5		1.5	2.0	2.5

<u>15.8</u>	<u>20.6</u>	<u>20.7</u>	<u>20.9</u>	<u>21.1</u>	<u>20.9</u>	<u>19.5</u>
9.2	4.4	4.3	4.1	3.9	4.1	5.5
2.8	1.9	1.5		1.5	1.9	2.3

<u>15.7</u>	<u>20.4</u>	<u>20.6</u>	<u>20.8</u>	<u>20.9</u>	<u>20.9</u>	<u>19.7</u>
9.3	4.4	4.4	4.2	4.1	4.1	5.3
2.4	2.0	1.5		1.5	1.9	2.3

<u>15.3</u>	<u>19.8</u>	<u>20.0</u>	<u>20.4</u>	<u>21.0</u>	<u>21.2</u>	<u>20.1</u>
9.7	5.2	5.0	4.6	4.0	3.8	4.9
2.9	2.1	1.5		1.5	1.9	2.3

24.97

24.97

68+00

67+00

66+00

65+00

64+00

63+00

62+00

T.S. L.B. L.P. \bar{e} R.P. R.B. T.S.

<u>164</u>	<u>207</u>	<u>207</u>	<u>207</u>	<u>207</u>	<u>205</u>	<u>166</u>
9.8	5.5	5.5	5.5	5.5	5.7	9.6
28.	22.	15.		15.	21.	26.

<u>16.7</u>	<u>20.4</u>	<u>20.6</u>	<u>20.7</u>	<u>20.7</u>	<u>20.4</u>	<u>16.4</u>
9.5	5.8	5.6	5.5	5.5	5.8	9.8
28.	22.	15.		15.	20.	26.

<u>17.3</u>	<u>21.0</u>	<u>21.1</u>	<u>21.0</u>	<u>21.0</u>	<u>20.9</u>	<u>16.0</u>
8.9	5.2	5.1	5.2	5.2	5.3	10.2
27.	21.	15.		15.	19.	26.

<u>17.6</u>	<u>21.2</u>	<u>21.2</u>	<u>R1.2</u>	<u>21.1</u>	<u>21.1</u>	<u>16.1</u>
8.6	5.0	5.0	5.0	5.1	5.0	10.1
27.	21.	15.		15.	19.	26.

<u>17.9</u>	<u>21.3</u>	<u>21.4</u>	<u>R1.5</u>	<u>21.4</u>	<u>21.2</u>	<u>16.0</u>
8.3	4.9	4.8	4.7	4.8	5.0	10.2
28.	22.	15.		15.	20.	28.

<u>17.4</u>	<u>21.8</u>	<u>21.8</u>	<u>R1.8</u>	<u>21.9</u>	<u>21.9</u>	<u>15.8</u>
8.8	4.4	4.4	4.4	4.3	4.3	10.4
26.	18.	15.		15.	19.	29.

<u>17.1</u>	<u>22.1</u>	<u>22.1</u>	<u>R2.1</u>	<u>22.2</u>	<u>22.2</u>	<u>17.0</u>
9.1	4.1	4.1	4.1	4.0	4.0	9.2
27.	18.	15.		15.	20.	28.

26.20

75+00

74+00

73+00

72+00

71+00

70+00

69+00

T.P. — 4.03 — 26.20 — 2.80 — 22.17 —
 — 24.97 —

T.S. Lt.B. Lt.P. $\frac{1}{2}$ Rt.P. Rt.B. T.S.

T.P. 6.11 — 27.28 — 4.93 — 21.17

80+00

17.3	21.2	21.1	$\frac{21.0}{21.0}$	20.9	20.9	17.8
8.8	4.9	5.0	5.1	5.2	5.2	8.3
26.	20.	15.		15.	17.	22.

79+00

17.1	21.2	21.2	21.1	20.9	20.9	18.3
9.0	4.9	4.9	5.0	5.2	5.2	7.8
26.	21.	15.		15.	18.	22.

78+00

16.9	20.4	20.5	20.7	20.7	20.8	17.6
9.2	5.7	5.6	5.4	5.4	5.3	8.5
25.	20.	15.		15.	19.	24.

T.P. 5.39 — 26.10 — 5.49 — 20.71

26.10

77+00

18.3	20.5	20.6	20.6	20.8	20.7	17.1
9.7	5.7	5.6	5.6	5.4	5.5	9.1
27.	21.	15.		15.	19.	24.

76+00

16.5	20.5	20.7	20.7	20.6	20.4	17.7
9.7	5.7	5.5	5.5	5.6	5.8	8.5
26.	20.	15.		15.	19.	24.

26.20

26.20

T.S. L.B. L.P. ϕ R.P. B.S. T.S.

87+00

<u>19.2</u>	<u>22.1</u>	<u>22.3</u>	<u>22.3</u>	<u>22.3</u>	<u>22.1</u>	<u>19.3</u>
8.1 27.	5.2 22.	5.0 15.	5.0	5.0 15.	5.2 19.	8.0 25.

86+00

<u>18.5</u>	<u>22.3</u>	<u>22.5</u>	<u>22.4</u>	<u>22.4</u>	<u>22.3</u>	<u>17.7</u>
8.8 28.	5.0 22.	4.8 15.	4.9	4.9 15.	5.0 21.	9.6 28.

85+00

<u>18.1</u>	<u>22.4</u>	<u>22.4</u>	<u>22.3</u>	<u>22.1</u>	<u>21.9</u>	<u>16.9</u>
9.2 27.	4.9 21.	4.9 15.	5.0	5.2 15.	5.4 21.	10.4 27.

84+00

<u>17.7</u>	<u>21.6</u>	<u>21.8</u>	<u>21.9</u>	<u>21.9</u>	<u>21.7</u>	<u>16.8</u>
9.6 26.	5.7 21.	5.5 15.	5.4	5.4 15.	5.6 20.	10.5 27.

83+00

<u>18.1</u>	<u>21.7</u>	<u>21.6</u>	<u>21.6</u>	<u>21.5</u>	<u>21.8</u>	<u>17.0</u>
9.2 27.	5.6 21.	5.7 15.	5.7	5.8 15.	6.0 21.	10.3 27.

82+00

<u>17.3</u>	<u>21.3</u>	<u>21.4</u>	<u>21.3</u>	<u>21.4</u>	<u>21.4</u>	<u>16.7</u>
10.0 25.	6.0 19.	5.9 15.	6.0	5.9 15.	5.9 19.	10.6 25.

81+00

<u>17.3</u>	<u>21.2</u>	<u>21.1</u>	<u>21.1</u>	<u>20.9</u>	<u>20.9</u>	<u>16.8</u>
10.0 25.	6.1 19.	6.2 15.	6.2	6.4 15.	6.4 18.	10.5 24.

27.29

27.28

93+00

<u>205</u>	<u>232</u>	<u>234</u>	<u>241</u>	<u>249</u>	<u>250</u>	<u>216</u>
10.7	8.0	7.8	7.1	6.3	6.2	9.6
26.	21.	15.		15.	24.	31.

92+00

<u>204</u>	<u>226</u>	<u>230</u>	<u>237</u>	<u>244</u>	<u>251</u>	<u>242</u>
10.8	8.6	8.2	7.5	6.8	6.1	7.0
24.	21.	15.		15.	28.	38.

T.P. 4.45 31.17 0.56 26.72

31.17

91+00

<u>202</u>	<u>227</u>	<u>229</u>	<u>236</u>	<u>243</u>	<u>243</u>	<u>208</u>
7.1	4.6	4.4	3.7	3.0	3.0	6.5
25.	21.	15.		15.	25.	32.

90+00

<u>199</u>	<u>222</u>	<u>224</u>	<u>230</u>	<u>235</u>	<u>232</u>	<u>195</u>
7.4	5.1	4.9	4.3	3.8	4.1	7.8
24.	21.	15.		15.	23.	28.

89+00

<u>19.2</u>	<u>223</u>	<u>225</u>	<u>222</u>	<u>22.8</u>	<u>22.5</u>	<u>18.8</u>
8.1	5.0	4.8	4.7	4.5	4.8	8.5
26.	22.	15.		15.	23.	27.

88+00

<u>19.5</u>	<u>22.1</u>	<u>22.3</u>	<u>22.3</u>	<u>22.2</u>	<u>22.1</u>	<u>19.7</u>
7.8	5.2	5.0	5.0	5.1	5.2	7.6
27.	23.	15.		15.	23.	27.

27.28

27.28

T.S. Lt.B. Lt.P. ϕ Rt.P. Rt.B. T.S.

99+60

<u>22.2</u>	<u>27.3</u>	<u>27.1</u>	<u>26.2</u>	<u>25.3</u>	<u>25.1</u>	<u>20.7</u>
9.0	3.9	4.1	5.0	5.9	6.1	10.5
29.	21.	15.		15.	18.	25.

99+00

<u>21.2</u>	<u>26.8</u>	<u>26.8</u>	<u>25.9</u>	<u>24.9</u>	<u>24.8</u>	<u>21.3</u>
10.0	4.4	4.4	5.3	6.3	6.4	9.9
27.	20.	15.		13.	17.	23.

98+00

<u>21.5</u>	<u>26.7</u>	<u>26.3</u>	<u>25.5</u>	<u>24.4</u>	<u>24.2</u>	<u>21.4</u>
9.7	4.5	4.9	5.7	6.8	7.0	9.8
29.	21.	15.		15.	17.	23.

97+00

<u>21.2</u>	<u>26.0</u>	<u>26.0</u>	<u>25.4</u>	<u>24.7</u>	<u>24.6</u>	<u>20.8</u>
10.0	5.2	5.2	5.8	6.5	6.6	10.4
26.	19.	15.		15.	19.	22.

96+00

<u>19.7</u>	<u>25.3</u>	<u>25.2</u>	<u>25.0</u>	<u>24.7</u>	<u>24.7</u>	<u>19.7</u>
11.5	5.9	6.0	6.2	6.5	6.5	11.5
26.	19.	15.		15.	17.	24.

95+00

<u>19.3</u>	<u>24.4</u>	<u>24.4</u>	<u>24.5</u>	<u>24.5</u>	<u>14.5</u>	<u>19.4</u>
11.9	6.8	6.8	6.7	6.7	6.7	11.8
26.	19.	15.		15.	18.	24.

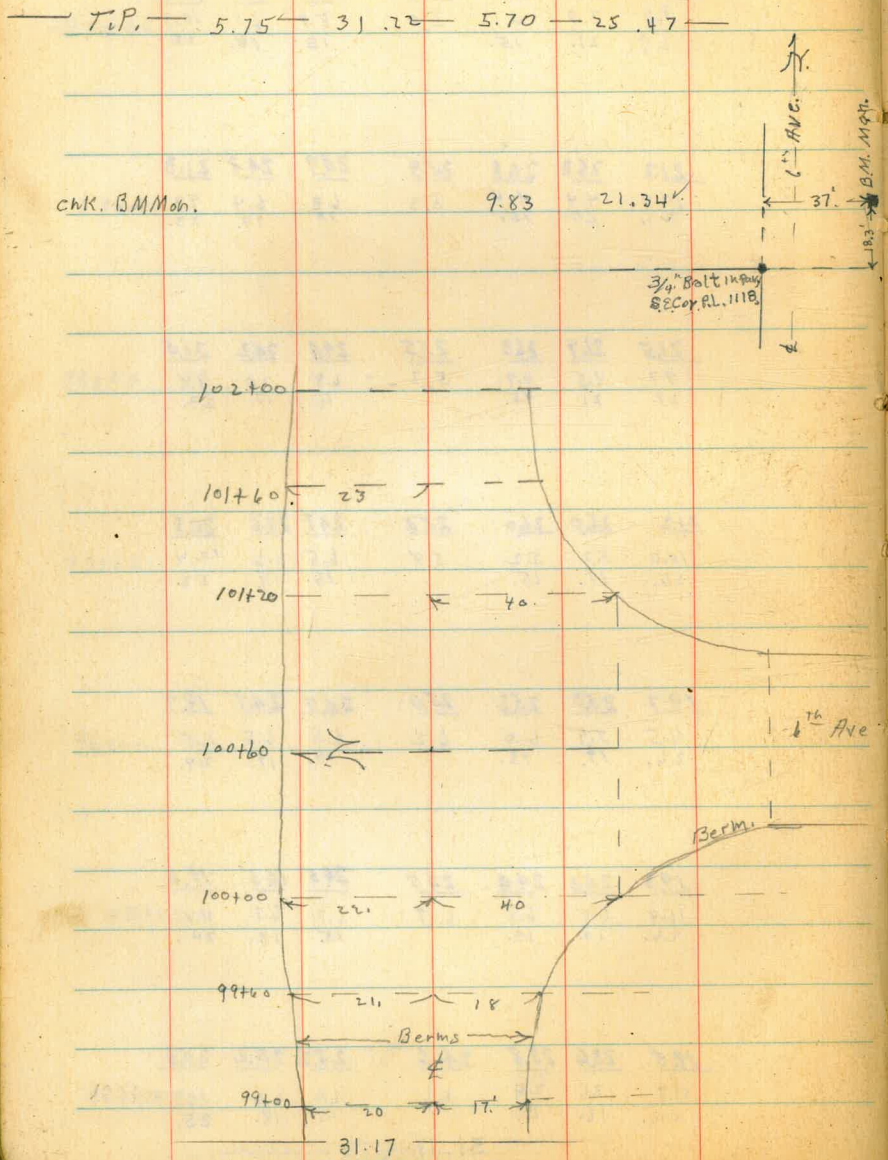
94+00

<u>19.5</u>	<u>23.6</u>	<u>23.8</u>	<u>24.6</u>	<u>25.2</u>	<u>25.2</u>	<u>20.3</u>
11.7	7.6	7.9	6.6	6.0	6.0	10.9
24.	18.	15.		15.	18.	25.

31.17

31.17

103+00



T.S. 4.8 L.P. 4.8 R.P. At. B T.S.

18

<u>226</u>	<u>267</u>	<u>268</u>	<u>266</u>	<u>264</u>	<u>263</u>	<u>231</u>
8.6	4.5	4.4	4.6	4.8	4.9	8.1
28	21	15		15	17	22

31.22

	<u>229</u>	<u>271</u>	<u>270</u>	<u>266</u>	<u>262</u>	<u>258</u>	<u>229</u>
102+00	8.3	4.1	4.2	4.6	5.0	5.4	8.3
	29	22	15		15	17	23

	<u>222</u>	<u>271</u>	<u>270</u>	<u>266</u>	<u>259</u>	<u>250</u>	<u>227</u>
101+60	9.0	4.1	4.2	4.6	5.3	6.2	8.5
	30	23	15		15	24	28

Berm Pav.

	<u>223</u>	<u>272</u>	<u>270</u>	<u>265</u>	<u>259</u>	<u>245</u>	<u>219</u>
101+20	8.9	4.0	4.2	4.7	5.3	6.7	9.3
	30	23	15		15	40	50

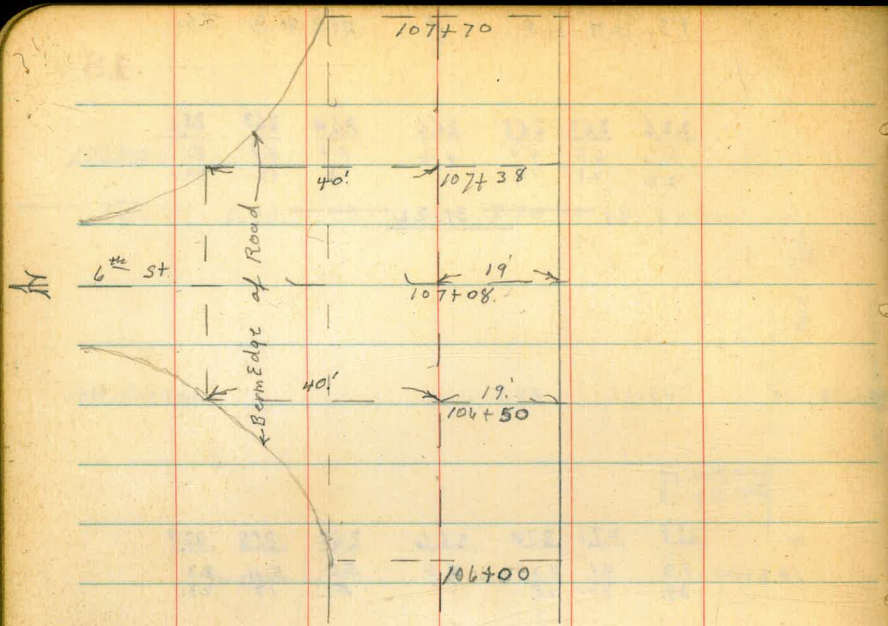
Berm Pav. Toe slope

	<u>214</u>	<u>277</u>	<u>272</u>	<u>264</u>	<u>260</u>	<u>259</u>	<u>259</u>
100+60	9.8	3.5	4.0	4.8	5.2	5.3	5.3
	33	25	15		15	40	50

	<u>214</u>	<u>274</u>	<u>272</u>	<u>263</u>	<u>258</u>	<u>256</u>	<u>214</u>
100+00	9.8	3.8	4.0	4.9	5.4	5.6	9.8
	30	22	15		15	40	50

Berm Pav. Toe slope

31.17



N.W. cor. C.D.R.

T.P. Top Post 5.45 — 32.01 — 4.66 — 26.56 — 46th St. to N.

106+00

105+00

104+00

31.22

T.S. Lt.B. Lt.P. ♀ Rt.P. Rt.B. T.S.

19

	<u>228</u>	<u>27.1</u>	<u>27.3</u>	<u>27.3</u>	<u>27.2</u>	<u>27.2</u>	<u>28.2</u>
107+70	9.2	4.9	4.7	4.7	4.8	4.8	8.8
	28.	21.	15.		15.	19.	26.

	<u>23.2</u>	<u>26.8</u>	<u>27.1</u>	<u>27.1</u>	<u>27.1</u>	<u>27.0</u>	<u>23.8</u>
107+38	8.8	5.2	4.9	4.9	4.9	5.0	8.2
	50.	40. Pav. Berm	15.		15.	19.	25.

	<u>26.9</u>	<u>27.2</u>	<u>26.9</u>	<u>26.7</u>	<u>26.7</u>	<u>23.4</u>
107+08	51	4.8	5.1	5.3	5.3	8.6
	50.	15.		15.	19.	25.

	<u>22.4</u>	<u>26.0</u>	<u>26.9</u>	<u>26.7</u>	<u>26.6</u>	<u>26.5</u>	<u>23.4</u>
106+50	9.6	6.0	5.1	5.3	5.4	5.5	8.6
	48.	40. Pav. Berm	15.		15.	19.	25.

32.01

	<u>22.7</u>	<u>26.5</u>	<u>26.7</u>	<u>26.5</u>	<u>26.5</u>	<u>26.7</u>	<u>23.9</u>
106+00	8.5	4.7	4.5	4.7	4.7	4.5	7.3
	27.	21.	15.		15.	21.	26.

	<u>22.7</u>	<u>26.4</u>	<u>26.5</u>	<u>26.5</u>	<u>26.5</u>	<u>26.3</u>	<u>23.7</u>
	8.5	4.8	4.7	4.7	4.7	4.9	7.5
	26.	21.	15.		15.	19.	24.

	<u>22.9</u>	<u>26.7</u>	<u>26.7</u>	<u>26.6</u>	<u>26.3</u>	<u>26.6</u>	<u>23.5</u>
	8.3	4.5	4.5	4.6	4.9	4.6	7.7
	26.	20.	15.		15.	19.	24.

31.22

114+00

23.5	274	27.4	27.2	272	272	245
8.5	4.6	4.6	4.8	4.8	4.8	7.5
26.	21.	15.		15.	19.	24.

113+00

23.2	270	27.2	270	268	269	241
8.8	5.0	4.8	5.0	5.2	5.1	7.9
26.	21.	15.		15.	20.	24.

112+00

23.5	269	27.1	269	266	266	240
8.5	5.1	4.9	5.1	5.4	5.4	8.0
27.	22.	15.		15.	19.	23.

111+00

23.4	267	26.9	267	264	264	240
8.6	5.3	5.1	5.3	5.6	5.6	8.0
27.	23.	15.		15.	18.	23.

110+00

23.3	271	27.2	269	267	267	23.9
8.7	4.9	4.8	5.1	5.3	5.3	8.1
24.	23.	15.		15.	18.	23.

109+00

23.0	273	27.3	272	268	268	23.9
9.0	4.7	4.7	4.8	5.2	5.2	8.1
27.	21.	15.		15.	19.	24.

108+00

23.6	273	27.5	274	272	27.2	23.3
8.6	4.7	4.5	4.6	4.8	4.8	8.7
27.	20.	15.		15.	19.	26.

32.01

32.01

120+00

119+00

T.P. — 5.82 — 33.73 — 4.10 — 27.91 —

118+00

117+00

116+00

115+00

32.01

T.S. Lt.B. Lt.Pav ϕ Rt.Pav. Rt.D. T.S.

21

<u>24.6</u>	<u>28.2</u>	<u>28.2</u>	<u>28.0</u>	<u>27.9</u>	<u>27.9</u>	<u>25.4</u>
9.1	5.5	5.5	5.7	5.8	5.8	8.3
27.	22.	15.		15.	19.	22.

<u>24.3</u>	<u>27.9</u>	<u>28.0</u>	<u>28.0</u>	<u>27.6</u>	<u>27.6</u>	<u>24.7</u>
9.4	5.8	5.7	5.7	6.1	6.1	9.0
27.	22.	15.		15.	19.	23.

33.73

<u>23.7</u>	<u>27.7</u>	<u>27.8</u>	<u>27.8</u>	<u>27.8</u>	<u>27.6</u>	<u>24.7</u>
8.3	4.3	4.2	4.2	4.2	4.4	7.3
28.	22.	15.		15.	19.	24.

<u>23.9</u>	<u>27.6</u>	<u>27.7</u>	<u>27.7</u>	<u>27.6</u>	<u>27.3</u>	<u>24.1</u>
8.1	4.4	4.3	4.3	4.4	4.7	7.9
27.	22.	15.		15.	19.	25.

<u>23.9</u>	<u>27.6</u>	<u>27.6</u>	<u>27.7</u>	<u>27.4</u>	<u>27.4</u>	<u>24.6</u>
8.1	4.4	4.4	4.3	4.6	4.6	7.4
27.	21.	15.		15.	20.	24.

<u>23.1</u>	<u>27.6</u>	<u>27.6</u>	<u>27.5</u>	<u>27.1</u>	<u>27.1</u>	<u>24.7</u>
8.9	4.4	4.4	4.5	4.9	4.9	7.3
27.	21.	15.		15.	19.	24.

32.01

T.S. Lt.B Lt.P ϕ Rt.P Rt.B T.S.

127+00

<u>26.6</u>	<u>288</u>	<u>290</u>	<u>29.7</u>	<u>30.5</u>	<u>30.5</u>	<u>28.2</u>
7.1	4.9	4.7	4.0	3.2	3.2	5.5
24.	21.	15.		15.	21.	25.

126+00

<u>25.3</u>	<u>293</u>	<u>293</u>	<u>29.8</u>	<u>30.3</u>	<u>30.3</u>	<u>27.3</u>
8.4	4.4	4.4	3.9	3.4	3.4	6.4
26.	21.	15.		15.	19.	24.

125+00

<u>25.0</u>	<u>296</u>	<u>294</u>	<u>29.5</u>	<u>29.5</u>	<u>29.5</u>	<u>26.7</u>
8.7	4.1	4.3	4.2	4.2	4.2	7.0
29.	22.	15.		15.	19.	23.

124+00

<u>24.5</u>	<u>292</u>	<u>292</u>	<u>29.2</u>	<u>29.0</u>	<u>29.0</u>	<u>26.6</u>
9.2	4.5	4.5	4.5	4.7	4.7	7.1
29.	23.	15.		15.	18.	22.

123+00

<u>24.9</u>	<u>28.8</u>	<u>28.8</u>	<u>28.7</u>	<u>28.5</u>	<u>28.5</u>	<u>26.3</u>
8.8	4.9	4.9	5.0	5.2	5.2	7.4
28.	22.	15.		15.	18.	23.

122+00

<u>25.4</u>	<u>28.4</u>	<u>28.6</u>	<u>28.5</u>	<u>28.6</u>	<u>28.6</u>	<u>26.1</u>
8.3	5.3	5.1	5.2	5.1	5.1	7.6
27.	22.	15.		15.	19.	23.

121+00

<u>24.6</u>	<u>28.2</u>	<u>28.4</u>	<u>28.2</u>	<u>28.1</u>	<u>28.1</u>	<u>25.6</u>
9.1	5.5	5.3	5.5	5.6	5.6	8.1
27.	22.	15.		15.	19.	23.

33.73

33.73

134+00

133+00

132+00

131+00

130+00

129+00

T.P.

5.45

35.98

3.20

30.53

128+00

33.73

L.S. Lt.B. Lt.Pav. @ Rt. P. Rt.B. T.S.

23

29.0	31.5	31.2	30.8	30.5	30.6	28.9
7.0	4.5	4.8	5.2	5.5	5.4	7.7
25.	22.	15.		15.	21.	24.

28.5	31.1	31.1	30.3	29.7	29.3	27.9
7.5	4.9	4.9	5.7	6.3	6.7	8.1
26.	22.	15.		15.	21.	24.

28.7	31.9	31.3	30.1	29.1	29.0	27.2
7.3	4.1	4.7	5.9	6.9	7.0	8.8
27.	23.	15.		15.	21.	24.

27.1	31.9	31.4	30.3	29.4	29.0	26.7
8.9	4.1	4.6	5.7	6.6	7.0	9.3
28.	21.	15.		15.	20.	24.

27.2	30.8	30.7	30.0	29.4	29.3	26.2
8.8	5.2	5.3	6.0	6.6	6.7	9.8
25.	20.	15.		15.	21.	25.

27.7	29.0	29.2	29.7	30.4	30.4	26.5
8.3	7.0	6.8	6.3	5.6	5.6	9.5
24.	21.	15.		15.	21.	27.

35.98

27.5	28.7	29.1	29.8	30.7	30.9	26.3
6.2	5.0	4.6	3.9	3.0	2.8	7.4
24.	23.	15.		15.	20.	27.

33.73

T.S. Lt.B Lt.P. ♀ Rt.P. Rt.B. T.S.

140+00

29.3	31.9	32.1	32.0	31.5	31.5	28.2
8.3	5.7	5.5	5.6	6.1	6.1	7.4
26.	22.	15.		15.	18.	25.

139+00

28.9	31.7	31.8	31.8	31.4	31.2	29.0
8.7	5.9	5.8	5.8	6.2	6.4	8.6
27.	22.	15.		15.	18.	22.

T.P. 6.18 — 37.56 — 4.60 — 31.38

37.56

138+00

28.8	31.8	31.8	31.7	31.4	32.1	28.4
7.2	4.2	4.1	4.3	4.6	3.9	7.6
26.	22.	15.		15.	20.	24.

137+00

28.7	31.7	31.7	31.4	31.2	31.1	28.7
7.3	4.3	4.3	4.6	4.8	4.9	7.3
25	21.	15.		15.	19.	24.

136+00

28.5	31.2	31.3	31.0	30.7	31.0	28.7
7.5	4.8	4.7	5.0	5.3	5.0	7.3
24.	20.	15.		15.	19.	23.

135+00

29.3	30.9	31.1	30.8	30.6	30.5	28.7
6.7	5.1	4.9	5.2	5.4	5.5	7.3
25.	22.	15.		15.	18.	23.

35.98

35.98

147+00

146+00

145+00

144+00

143+00

142+00

141+00

37.56

T.S. Lt.B Lt.P. \bar{z} Rt.P. Rt.B T.S.

25

29.9	32.5	32.5	32.5	32.2	32.1	30.9
7.7	5.1	5.1	5.1	5.4	5.5	6.7
25.	21.	15.		15.	20.	23.

29.8	32.6	32.8	32.6	32.9	32.1	30.7
7.8	5.0	4.8	5.0	5.3	5.5	7.0
25.	21.	15.		15.	20.	23.

29.6	32.6	32.9	32.9	32.5	32.4	31.0
8.0	5.0	4.7	4.7	5.1	5.2	6.6
27.	21.	15.		15.	21	24.

29.3	32.6	32.8	32.8	32.5	32.4	30.7
8.3	5.0	4.8	4.8	5.1	5.2	6.9
26.	21.	15.		15.	19.	23

29.5	32.7	33.0	32.9	32.6	32.5	30.9
8.1	4.9	4.6	4.7	5.0	5.1	6.7
26.	22.	15.		15.	19.	22.

29.9	32.8	32.7	32.7	32.4	32.4	30.2
7.7	4.8	4.9	4.9	5.2	5.2	7.4
25.	21.	15.		15.	18.	22.

29.5	32.0	32.4	32.3	32.0	31.9	28.7
8.1	5.6	5.2	5.3	5.6	5.7	8.9
25.	21.	15.		15.	18.	24.

37.56

153+00

33.0	33.7	33.9	33.7	33.6	31.9
5.4	4.7	4.5	4.7	4.8	6.5
24.	15.		15.	20.	24.

152+00

32.5	33.3	33.5	33.6	33.4	33.3	31.9
5.9	5.1	4.9	4.8	5.0	5.1	6.5
24.	21.	15.		15.	20.	24.

151+00

31.4	32.9	33.1	33.3	33.3	33.2	31.7
7.0	5.5	5.3	5.1	5.1	5.2	6.7
24.	21.	15.		15.	21.	24.

150+00

31.8	32.8	32.9	33.1	33.1	32.9	31.2
6.6	5.6	5.5	5.3	5.3	5.5	7.2
24.	21.	15.		15.	19.	23

T.P. — 5.75 — 38.36 — 4.95 — 32.61 —

38.36

149+00

30.3	32.6	32.7	32.8	32.6	32.5	31.5
7.3	5.0	4.9	4.8	5.0	5.1	6.1
25.	22.	15.		15.	20.	23.

148+00

30.0	32.4	32.6	32.5	32.3	32.3	31.7
7.6	5.2	5.0	5.1	5.3	5.3	5.9
25.	22.	15.		15.	21.	23.

37.56

37.56

159+00

T.P. 6.79 42.57 2.58 35.78

158+00

157+00

156+00

155+00

CHK. BM. Mon. 26.5 Lt of 154+22

154+00

38.36

T.S. Lt. B. Lt. P. € Rt. P. Rt. B. T.S.

27

31.8	33.8	33.9	34.9	35.8	36.0	33.4
10.8	8.8	8.7	7.7	6.8	6.6	9.2
27.	25.	15.		15.	22.	26

42.57

31.4	33.4	33.5	34.7	35.9	36.1	33.1
7.0	5.0	4.9	3.7	2.5	2.3	5.3
25.	22.	15.		15.	22.	26

31.6	33.5	33.8	34.8	35.8	36.1	33.7
6.8	4.9	4.6	3.6	2.6	2.3	4.7
26.	23.	15.		15.	21.	25.

32.8	33.5	33.6	34.3	35.0	35.0	32.8
5.6	4.9	4.8	4.1	3.4	3.4	5.6
25.	23	15.		15.	23	26.

31.9	33.0	33.2	33.8	34.4	34.6	31.8
6.5	5.4	5.2	4.6	4.6	3.8	6.6
24.	22.	15.		15.	28.	28.

o.K.
31.1
CHK XSEP.

31.2	32.9	33.3	33.7	33.8	33.7	32.1
7.3	7.2	5.5	5.1	4.7	4.6	6.3
5.0	25.	22.	15.		15	20.
						24.

38.36

T.S. Lt.B Lt.P. £ Rt.P. Rt.B T.S.

166+00

34.8	38.0	38.0	37.6	37.3	37.2
7.8	4.6	4.6	5.0	5.3	5.4
28.	22.	15.		15.	18.

165+00

36.3	38.3	38.3	37.6	37.1	37.1
6.3	4.3	4.3	5.0	5.5	5.5
27.	22.	15.		15.	18.

164+00

34.6	38.1	37.8	36.8	36.1	36.1
8.0	4.5	4.8	5.8	6.5	6.5
27.	21.	15.		15.	18.

163+00

32.4	37.4	37.2	36.2	35.2	35.2
10.2	5.2	5.4	6.4	7.4	7.4
28.	20.	15.		15.	18.

162+00

31.7	36.8	36.6	35.5	34.4	34.7
10.9	5.8	6.0	7.1	8.2	7.9
30.	22.	15.		15.	21.

161+00

32.8	35.8	35.9	35.4	35.1	34.4	34.0
9.8	6.8	6.7	7.2	7.5	8.2	8.6
26.	22.	15.		15.	19.	23.

160+00

31.9	35.2	35.0	35.2	35.2	35.2	33.7
10.7	7.4	7.6	7.4	7.4	7.4	8.9
28.	23.	15.		15.	20.	24.

42.57

42.57

172+00

355	38.9	38.7	38.7	38.5	38.2	36.6
86	5.2	5.4	5.4	5.6	20.	7.5
24.	20.	15.		15.	5.9	24

171+00

35.1	38.2	38.2	38.3	38.1	37.8	35.8
9.0	5.9	5.9	5.8	6.0	6.3	8.3
24.	20.	15.		15.	21.	24.

170+00

34.2	37.5	37.7	37.8	37.7	37.4	35.7
9.9	6.6	6.4	6.3	6.4	6.7	8.4
24.	21.	15.		15.	21.	24.

169+00

34.1	37.1	37.3	37.5	37.2	37.0	35.2
10.0	7.0	6.8	6.6	6.9	7.1	8.7
27	23.	15.		15.	20.	23

T.P. — 6.74 — 44.11 — 5.20 — 37.37 —

44.11

168+00

34.3	37.3	37.4	37.5	37.1	37.0	35.2
8.3	5.3	5.2	5.1	5.5	5.6	7.4
27	22.	15.		15.	19.	23.

167+00

33.6	37.4	37.5	37.3	37.1	37.2	36.1
9.0	5.2	5.1	5.3	5.5	5.4	6.5
26.	21	15.		15.	21.	23

42.57

42.57

T.S. Lt.B. Lt.P. ϕ Rt.P. Rt.B. T.S.

178+00

39.7	46.8	46.7	46.1	45.6	45.6	44.7
14.1	7.0	7.1	7.7	8.2	8.2	9.1
29.	20.	15.		15.	20.	27.

177+00

41.8	45.4	45.5	45.1	44.7	44.4	45.7
12.0	8.4	8.3	8.7	9.1	9.4	9.1
25.	20	15.		15.	20.	25

T.P. 10.71 53.79 1.03 43.08

53.79

176+00

43.2	43.8	43.9	43.6	43.5	43.5	44.1
0.9	0.3	0.2	0.5	0.6	0.6	0.0
22.	22.	15.		15.	21.	22

175+00

40.3	42.0	42.0	42.0	42.2	41.9	44.1
3.8	2.1	2.1	2.1	1.9	2.2	0.0
23.	21.	15.		15.	22.	23.

174+00

37.6	40.8	40.6	40.5	40.3	40.1	39.9
6.5	3.3	3.5	3.6	3.8	4.0	4.2
23.	18	15.		15.	20	23

173+00

36.3	39.7	39.6	39.6	39.5	39.2	37.6
7.8	4.4	4.5	4.5	4.6	4.9	6.5
24.	18.	15.		15.	21.	24.

44.11

44.11

181+00

373	48.4	48.2	47.1	46.4	46.3	44.9
16.5	5.4	5.6	6.7	7.9	7.5	8.9
36.	22.	15		15.	25.	29.

180+50

44.0	48.8	48.5	47.6	47.6	48.0
9.8	5.0	5.3	6.2	6.2	5.8
35.	20.	15.		15.	48.0

Edg + pav. E. edge Texas St. Grad to S.

180+34

49.4	48.9	47.9	47.8	48.7
4.4	4.9	5.9	6.0	5.1
31.8	15.		15	40.

E. edge Texas St. grade to N. Pav Texas St.

180+00

49.0	48.6	49.1	48.1	48.0	48.8
4.8	4.2	4.7	5.7	5.8	5.0
35.	25	15		15	40.

W. side Texas St. grade to N. Pav. Texas St.

179+80

40.8	49.6	49.0	49.0	47.9	47.8	48.8	46.8
13.0	4.2	4.8	4.8	5.9	6.0	5.0	7.0
35.	25.	Lt.P.	&P.	15.	36.	40	44.

W. side Texas St. grade to S.

179+50

40.8	49.3	49.0	47.8	47.0	47.6	45.8
13.0	4.5	4.8	6.0	6.8	6.2	8.0
35.	22.	15.		21.	28	31

Rt.P.

179+00

38.4	48.3	48.1	47.4	46.7	46.8	44.7
15.4	5.5	5.7	6.4	7.1	7.0	9.1
33.	20.	15		15.	27.	30

53.79

53.79

186+00

37.4	41.0	41.9	41.7	42.7	43.0	39.6
10.5	6.9	7.0	6.2	5.2	4.9	8.3
29.	23.	15.		15.	19.	25

185+00

37.1	40.9	41.2	41.8	42.6	43.2	38.8
10.9	7.0	6.7	6.1	5.3	4.7	9.1
25.	19.	15.		15.	20.	27

184+00

37.5	42.6	42.6	42.9	43.4	44.0	39.3
10.4	5.3	5.3	5.0	4.5	3.9	8.6
30.	23.	15.		15.	21.	27.

T.P. — 4.41 — 47.94 — 10.26 — 43.53 —

47.94

183+00

36.7	45.1	44.8	44.3	44.1	44.1	39.1
17.1	8.7	9.0	9.5	9.7	9.7	14.7
35.	23.	15.		15.	21.	27.

182+00

36.2	46.5	46.9	45.7	44.9	44.9	40.2
17.6	7.3	7.1	8.1	8.9	8.9	13.6
36.	22.	15.		15.	17.	26.

Chk. BM 3 Nails Cypress Tree 35 ft } 4.12
Sta 180+50 }

47.67 = 47.69

53.79

53.79

192 + 00

T.P. 6.58 50.70 3.82 44.12

191 + 00

190 + 00

189 + 00

188 + 00

187 + 00

47.94

T.S. Lt.B. Lt.P. ♀ Rt.P. Rt.B. T.S.

33

42.4	43.8	44.2	44.5	44.5	44.5	44.9
8.3	6.9	6.5	6.2	6.2	6.2	5.8
25	22.	15.		15.	17	19

50.70

40.4	43.3	43.5	43.8	44.1	43.9
7.5	4.6	4.4	4.1	3.8	4.0
24.	22.	15.		15.	22.

38.8	43.1	43.0	43.5	43.6	43.4	42.3
9.1	4.8	4.9	4.4	4.3	4.5	5.6
27.	22	15		15.	20	22.

39.4	42.5	42.8	43.2	43.3	43.2	42.1
8.5	5.4	5.1	4.7	4.6	4.7	5.8
27.	22.	15.		15.	21.	23.

39.1	41.3	41.9	42.5	43.1	43.1	41.9
8.8	6.6	6.0	5.4	4.8	4.8	6.0
25.	22.	15		15.	20.	22.

37.3	40.8	41.0	41.9	42.9	42.9	39.6
10.6	7.1	6.9	6.0	5.0	5.0	8.3
26.	23.	15.		15.	18.	23.

47.94

199400

198400

197400

196400

195400

194400

193400

50.70

42.9	48.3	48.5	48.5	48.2	47.7	47.7
7.8	2.4	2.2	2.2	2.5	3.0	3.0
30.	21.	15.		15.	20.	22.

43.2	47.3	47.5	47.9	47.8	47.2	47.6
7.5	3.4	3.2	2.8	2.9	3.5	3.1
27.	20.	15.		15.	20.	21.

44.1	46.6	47.0	47.3	47.0	46.4	47.1
6.6	4.1	3.7	3.4	3.7	4.3	2.6
25.	21.	15.		15.	19.	20.

44.0	45.9	46.4	46.8	46.8	46.2	47.2
6.7	4.8	4.3	3.9	3.9	4.5	3.5
25.	22.	15.		15.	19.	20.

43.8	45.9	46.0	46.3	46.3	45.9	48.6
6.9	4.8	4.7	4.4	4.4	4.8	11.
26.	23.	15.		15.	20.	22.

43.0	45.3	45.5	45.7	45.7	45.2	48.7
7.7	5.4	5.2	5.0	5.0	5.5	2.0
25.	22.	15.		15.	18.	22.

43.2	44.7	44.7	45.0	45.0	45.1	46.9
7.5	6.0	6.0	5.7	5.7	5.6	3.8
25.	22.	15.		15.	18.	20.

50.70

T.S. Lt. B. Lt. P. ♀ Rt. P. Rt. B. T.S.

T.P. — 8.92 — 70.81 — 0.21 — 61.89 —

204+00

62.3	59.2	59.3	59.3	59.1	58.9	65.9
10.2	2.9	2.8	2.8	3.0	3.2	13.8
24.	21.	15.		15.	19.	24.

203+00

57.8	56.2	56.4	56.6	56.7	56.6	62.1
4.3	5.9	5.7	5.5	5.4	5.5	0.0
23.	20.	15.		15.	19.	24.

202+00

53.3	53.6	53.7	54.0	53.9	55.7
8.8	8.5	8.4	8.1	8.2	4.4
25	15.		15.	20.	22.

201+00

46.1	50.7	51.1	51.4	51.3	50.8	50.5	50.5
16.0	11.4	11.0	10.7	10.8	11.3	11.6	11.6
32.	25.	15.		10.	15.	20	22.

T.P. — 12.51 — 62.10 — 1.11 — 49.59 —

— 62.10 —

200+00

44.9	49.0	49.3	49.4	49.2	48.9	47.6
5.8	1.7	1.4	1.3	1.5	1.8	3.1
29.	22.	15.		15.	20.	22.

— 50.70 —

— 50.70 —

T.P. N. End. Catch Basin $\left\{ \begin{array}{l} \text{25 ft of } \pm \\ \text{(20' w of Bdy)} \end{array} \right\}$ 6.15 64.66

206+57 ⁵³ \pm = Old City Boundary See. on Diagonal

206+00

205+00

70.81

64.6	64.7	64.8	64.9	65.0	65.1	67.9
6.2	6.1	6.0	5.9	5.8	5.7	2.9
23.	20.	15.		15.	18	21

65.5	63.9	63.9	63.9	64.1	64.1	69.8
5.3	6.9	6.9	6.9	6.7	6.7	1.0
28	20.	15.		15	19	24

65.7	61.6	61.9	61.9	62.1	62.2	68.7
5.1	7.2	8.9	8.9	4.7	8.6	2.1
25.	21.	15.		15	19	25.

70 81

Reduced & plotted Sec.
10-16-39 C.B. Hough
Pages 4 to 36

Moore
1-5-40

x sec Evergreen

70' wide
18' cbs
8.5 1/4

N L Sterne Sly

SWBP 2.27 196.17

193.90 Willow
Tennyson

T.P. 1.01 184.55 12.43 183.54

T.P. 1.02 173.59 11.98 172.57

N L Sterne = 70' wide
18' cbs
8.5 1/4

E 4.0 169.6

c6 TOP cen c6 3.98 169.61

gut Pav 4.98 168.61

1/4 " 3.93 169.66

c " 3.40 170.19

1/4 " 3.05 170.54

c6 " 2.87 170.72

+7 gut 2.82 170.77

+7 TOP end c6. 2.34 171.23 ✓

+12 2.2 171.4

W + 2.8 176.5

N c6

W + 3.7 177.3

c6 + 0.4 174.0

Indexed
c.s.K.

u3c6R



Core Pav

Evergreen

37

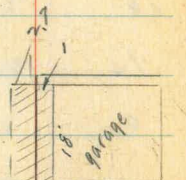
18

0.27 x 6 ob. in lot

Sterne

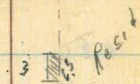
ST

0+01



down

0+048



3

1+04.4

Ret. wall

gar.

1+19

3.7

down

1+45 Cent.
Ret. wall

37.3

12.7

173.59

1/4		0.6	173.0	
+4		4.3	169.3	
0		4.7	168.9	
1/4		4.5	169.1	
cb		4.0	169.6	
E		4.2	169.4	
+10		9.4	164.0	
	N 1/4	Starne		
-10		10.5	163.1	
E		5.4	168.2	
cb		4.4	169.2	✓
1/4		4.9	168.9	
c		5.5	168.1	
+4		5.0	168.6	
1/4		1.3	172.3	
cb		+1.2	174.8	
W		+3.0	176.6	
	E			
W		+3.0	176.6	✓
cb		+0.2	173.8	✓
1/4		1.4	172.2	

173.59

39

+2		1.7	171.9	
+5		5.5	168.1	
c		5.7	167.9	
1/4		5.5	168.1	
cb		4.9	168.7	
+5		5.2	168.4	
E		10.2	163.4	
+10		12.7	159.9	
	S 1/4			
-10		13.0	160.6	
E		11.1	162.5	
+13		4.7	166.9	
cb		6.0	167.6	
1/4		5.9	167.7	
c		6.6	162.0	
+2		6.5	162.1	
+4		1.3	172.3	
1/4		0.8	172.8	
cb		+0.2	173.8	
W		+2.9	176.5	

506

W	+ 2.8	176.4
cb	0.0	173.6
1/2	1.5	172.1
+ 3	2.1	171.5
c	6.8	166.8
1/2	4.7	166.9
cb	7.2	166.4
+ 6	7.9	165.7
E	13.0	160.6
+ 10	15.3	158.3
S.W. STERNE = 0 + 100		
- 10	17.0	156.6
E	14.4	159.2
+ 6	12.0	166.6
cb	9.7	163.9
1/2	8.3	165.3
c	8.5	165.1
+ 3	4.3	169.3
1/2	3.1	170.5
cb	1.0	172.6
W	+ 3.0	176.6

173.59

TP.	1.83	164.18	11.24	162.35	
	0 + 0.1				
E + 2.7	N.L.	apron	4.41	159.77	conn.
E - 1		gar	4.44	159.74	
	0 + 1.9				
W			+ 10.0	174.2	
cb			+ 4.8	171.0	
1/2			+ 4.6	168.8	
+ 6			+ 3.5	167.7	
c			0.7	163.5	
1/2			0.6	163.6	
cb			1.7	162.5	
+ 15.3	SL	apron	4.12	160.06	conn.
E + 1		gar	4.44	159.74	
	0 + 2.5				
E - 1.7	E	conn	5.81	158.37	
	0 + 3.2				
E	LAWN		6.2	158.0	
+ 10	"		4.8	159.4	
cb			1.8	162.4	

164.18

1/2		1.0	162.6
c		2.1	162.1
+4		+1.7	165.9
1/2		+3.7	162.9
cb		+5.4	169.6
w		+8.6	172.8
	o +48		
w		+6.6	170.8
cb		+3.4	167.6
1/2		+2.2	166.4
c		3.4	160.8
1/2		2.9	166.3
cb		2.5	161.7
+7	Lawn	5.5	158.7
E	"	6.3	157.9
+3	2 6.5 cent porch	5.40	158.78
	o +75		
E		7.7	156.5
+11		7.3	156.9
cb		5.7	158.5
1/2		4.3	157.9

164.18

40

c		7.4	156.8
+8		4.2	160.0
1/2		2.4	161.8
cb		0.5	163.7
w		+2.2	166.4
	o +88.4		
E	N end 12' cent Porch	12.71	151.47
	1 +0.4		
w		7.2	157.0
cb		8.8	155.4
1/2		11.2	153.0
c		11.0	153.2
1/2		11.0	153.2
cb		12.0	152.2
+14.4	NW cent apron	18.30	150.88
E +1	" 11' garage	13.28	150.90
T.P.		2.28	153.86
		12.60	151.58
	17.19		
E -1		2.95	150.91
E +8.6	Top cent.	2.95	150.91

153.84

E + 8	2.0	151.3
cb	2.0	151.9
1/2	1.5	152.4
c	1.0	152.9
1/2	0.8	153.1
cb	0.8	153.1
+10	2.0	151.3
W	2.3	151.6

1 + 45

-15	20.0	133.9
W	19.8	134.1
cb	18.3	135.6
1/2	18.0	135.9
+6.4 ground	17.3	136.6
cor. Ret.		
+6.4 Top Cem wall	14.0	139.9
c ground	17.3	136.6
1/2	17.3	136.6
cb	17.0	136.9
E	19.0	134.9
E Top wall	14.0	139.9
+10	19.0	134.9

Plotted RED

41

153.84

TP.	12.02	144.21	2.28	151.58	
check to BM Willow/ Russell			2.84	141.35	141.33

204.88

+12	9.7	195.2
S	12.1	192.8
+10	13.7	191.2
+25	26.3	184.6

0+50

-20	22.3	182.6
-6	17.1	187.8
S	13.3	191.6
+5	11.1	193.8
⊗	8.0	196.9
+15	7.0	197.9
H	5.0	198.9

0+70

H	5.1	199.8
⊗	6.6	197.3
S	10.5	194.4
+15	13.4	191.5

1+0

-15	8.0	196.9
√	6.1	198.8

204.88

⊗	3.4	201.5
H	1.9	203.0
TP	1193	216.59
	0.22	204.66

1+35

H	9.0	202.6
⊗	10.8	205.8
S	12.0	204.6
+10	13.1	203.8

1+70

-10	10.7	205.9
S	9.5	202.1
⊗	7.5	209.1
H	5.8	210.8

2+0

H	3.0	213.6
⊗	5.5	211.1
S	8.4	208.2
+10	10.0	206.4

2+35

-10	7.1	209.5
-----	-----	-------

		216.59		
S			5.5	211.1
L			0.6	216.0
H			+3.6	226.2
TP	12.06	228.39	0.26	216.33
		2+55		
H			6.7	221.6
L			11.2	217.1
S			14.5	213.9
+10			16.8	211.6
		2+75		
-10			13.7	214.7
S			11.8	216.8
L			6.9	221.5
+10			5.6	222.8
H			2.9	228.5
		3+0 = N.L. Witherby		
H			+3.0	231.4
L			2.4	226.0
S			6.0	222.4
+10			7.8	220.6

07. Rock
8'S. 2+35

		228.39		
TP	11.52	239.71	0.20	228.19
		L Witherby		
-10			12.2	227.5
S			9.6	230.1
L			4.6	235.1
H			1.9	237.8
TP	7.00	245.88	0.83	238.88
		L Witherby		
H = W. Stucco House			5.6	240.2
L = " " " "			6.8	239.1
S = " " " "			10.1	235.8
+10			11.2	234.7
		0+0 N.L. Witherby Gay to East		
S			4.8	241.1
Cb			5.3	240.6
L			4.8	241.1
Cb			4.5	241.4
H			4.4	241.5
		0+15 - Ncb Witherby		
H Top Cb			4.34	241.54
N Gutter on Pavng			4.81	241.07

245.88

cb	TopCb	4.55	241.33
	Gutter on Pav.	5.03	240.85
£	TopCb	4.93	240.98
	Gutter on Pav.	5.42	240.46
75	= Cb B.C. TopCb	5.05	240.83
	Gutter on Pav.	5.54	240.37
Cb		5.1	240.8
S		5.2	240.7

0 + 25 = £

S		4.9	241.0
Cb = Cb EC'		5.24	240.64 ✓
	Gutter on Pav.	5.84	240.04
£	on Paving	5.30	240.58
Cb	" "	4.88	241.00
H	" "	4.65	241.23

0 + 35 = FCB

H	TopCb	4.33	241.53
	Gutter on Pav.	4.65	241.23
Cb	" "	4.77	241.11
£	" "	5.18	240.70

45

245.88

Cb	Gutter on Pav.	5.62	240.35
	TopCb	5.22	240.65
S		5.1	240.8

0 + 50 = E.L. Netherby

S		4.8	241.1
Cb	Top	4.86	241.02
	Gutter on Paving	5.37	240.51
£	" "	4.44	241.44
Cb	Gutter " "	4.36	241.52
Cb	Top	3.85	242.03
H		3.63	242.25

TP	0.86	234.58	11.66	234.22
TP	2.54	227.43	9.69	224.89
BM			7.33	220.10

S.W.B.P.
Jan & Jun 11
220.09

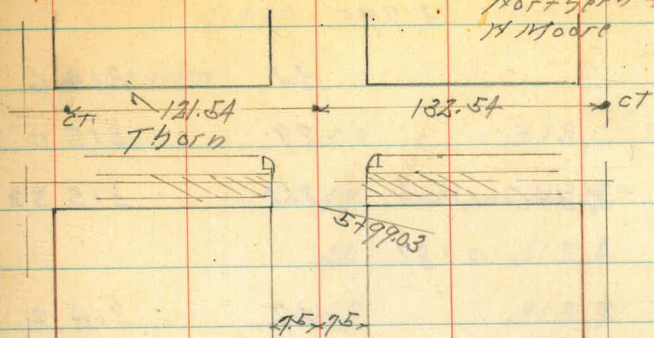
Cross Section Alley Block K Altadena

B.M.	634	317.95	311.61	1st BP Redwood 33rd St
0-10 = H.C.B. Redwood				
H	on Paving	5.13	312.82	
L	"	5.25	312.70	
F	"	5.36	312.59	
0+0 = H.L. Redwood				
F	Top Cb + Gutter	4.65	313.30	
L	on Paving	5.04	312.91	
H	Gutter	4.76	313.19	
H	Top Cb	4.46	313.49	
0+8				
H	= H/L Tile Hall Top	2.75	315.20	2878
H	"	3.2	314.7	
L	"	4.2	313.7	
F	"	3.9	314.0	
0+45				
-8.2	= L Garage Conc Floor	3.21	314.74	
-1.2	= Break Conc Apron	3.18	314.77	
-0.5	= H/L Conc. "	3.42	314.53	
F	"	3.2	314.7	

Red Plot on profile 2878
3-13-40 C.B.H.

Indexed
C.S.K.

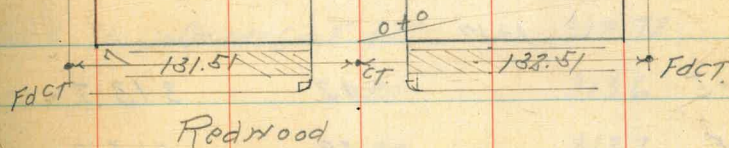
March 9, 40
Sisson
Northern 47
H Moore



Blk K
Altadena

Banerjee

33rd



✓
317.95

Z		33	314.6
H		29	315.0
+0.5 = 2 1/2 Conc Walk		262	315.33
		0+87	
-5		3.7	314.2
H		3.5	314.4
Z		3.5	314.4
F		3.5	314.4
+0.8 = 1 1/2 Conc Walk		3.85	314.10
		0+90	
H +0.5 = 1 1/2 Post Pole			
		1+12	
F +0.6 = 1 1/2 Conc Walk		4.14	313.81
		1+17	
-5		4.2	313.7
F		3.9	314.0
Z		3.8	314.1
+6.3 = 1 1/2 Conc Walk		3.45	314.50
H		3.6	314.3
TP	4.76	318.60	4.11

✓
318.60

48

1+50

-5		5.0	313.6
H		4.9	313.7
Z		4.8	313.8
F		4.7	313.9
+10		5.4	313.2
		1+75	
-10		5.3	313.3
F		4.8	313.8
Z		4.9	313.7
H		4.7	313.9
+5		4.9	313.7
		2+0	
H +0.5 = 1 1/2 Do Garage Conc F		4.88	313.72
Z		5.0	313.6
F		4.9	313.7
+10		5.5	313.1
		2+19	
H +0.5 = 1 1/2 Do Garage Conc Floor		4.89	313.71
		2+22	
H +0.5 = 1 1/2 Post Pole			

✓
318.60

2+24

-5'	5.2	313.4
F	4.9	313.7
£	4.9	313.7
M = £ 2' Conc Walk	4.87	313.73

2+56

M	5.0	313.6
£	5.0	313.6
F	5.0	313.6

+2.5 = Wly Conc Apron 4.99 313.61

+4.2 = ~~£~~ Garage Conc Floor 4.74 313.86

2+75

M - 0.8 = ~~£~~ 2.5' Conc Walk 4.70 313.90

2+0

F 4.9 313.7

£ 4.9 313.7

M 5.0 313.6

2+13

E - 3' = ~~£~~ 3' Door Floor 4.19 314.41

✓
318.60

49

2+18

E - 1' = ~~£~~ 3' Conc Walk 4.52 314.08

2+46

-0.3' = ~~£~~ 2.5' Conc Walk 5.26 313.34

M 5.3 313.3

£ 5.2 313.4

F 5.0 313.6

2+49

M + 0.6 = Wly Pav Pol

2+67

M - 1' = ~~£~~ 2' Conc Walk 5.83 312.77

4+0

-5 5.8 312.8

F 6.0 312.6

£ 6.3 312.3

M 6.0 312.6

+10 6.5 312.1

4+25

-10 7.1 311.5

M 6.3 312.3

✓
318.60

Z			6.5	312.1
F			6.3	312.3
TP	4.22	316.15	6.67	311.93
		4+52		
-4.5	= 1/4 Do. Garage Conc F.	3.43		312.72
F			4.1	312.1
Z			4.2	312.0
H			4.0	312.2
+5			4.8	311.4
		4+69		
F-4.5	= 1/4 Do. Garage Conc F.	3.43		312.72
		4+75		
H+0.7	= 1/4 Porch Pole			
		4+90		
-5			4.4	311.8
H			4.0	312.2
Z			4.0	312.2
F			4.1	312.1
+3.7	= 1/2 Garage Conc Floor	3.62		312.53

✓
316.15

				5+20
-5			3.8	312.4
F			3.8	312.4
Z			4.0	312.2
H			4.1	312.1
+5			4.5	311.7
		5+55		
H			3.8	312.4
Z			3.6	312.6
F			3.6	312.6
+3.8	= 1/2 Garage Conc Floor	3.44		312.71
		5+65		
F-1.2	= 1/2 3.8' Tile Walk	3.51		312.64
F-4'	= 1/2 3.8' Conc. "	3.27		312.88
		5+80		
F			3.5	312.7
Z			4.0	312.2
H			4.0	312.2

✓
316.15

5499.03 = S L Thorn on Paving

W Top Cb	4.29	311 86
Gutter on Paving	4.38	311 77
✓	4.49	311 66
E Gutter	4.04	312 11
E Top Cb	3.81	312 34

6409 = S Cb Thorn

E on Paving	4.60	311 55
✓	4.80	311 35
W	5.05	311 10
BM	1.37	314.78

SMBP
Thorn + 33"
314.8°

Cross Section Alley Block A Altadena

BM 1.10 315.90 314.80
 5th & P
 Thorn St

TP 6.08 310.18 11.80 304.10

0-10 = NCB + Thorn St.

E on Paving 7.41 302.77

1/2 " " 7.54 302.64

1/4 " " 7.58 302.60

0+0 = N. Thorn St.

1/4 TopCb 6.90 303.28

Gutter on Paving 7.05 303.13

1/2 " " 7.16 303.02

Gutter " " 6.88 303.30

E TopCb 6.63 303.55

0+22

-5 6.0 304.2

E 5.8 304.4

1/2 6.0 304.2

1/3 6.1 304.1

+6.3 = 23.5' Walk Conc 6.70 303.48

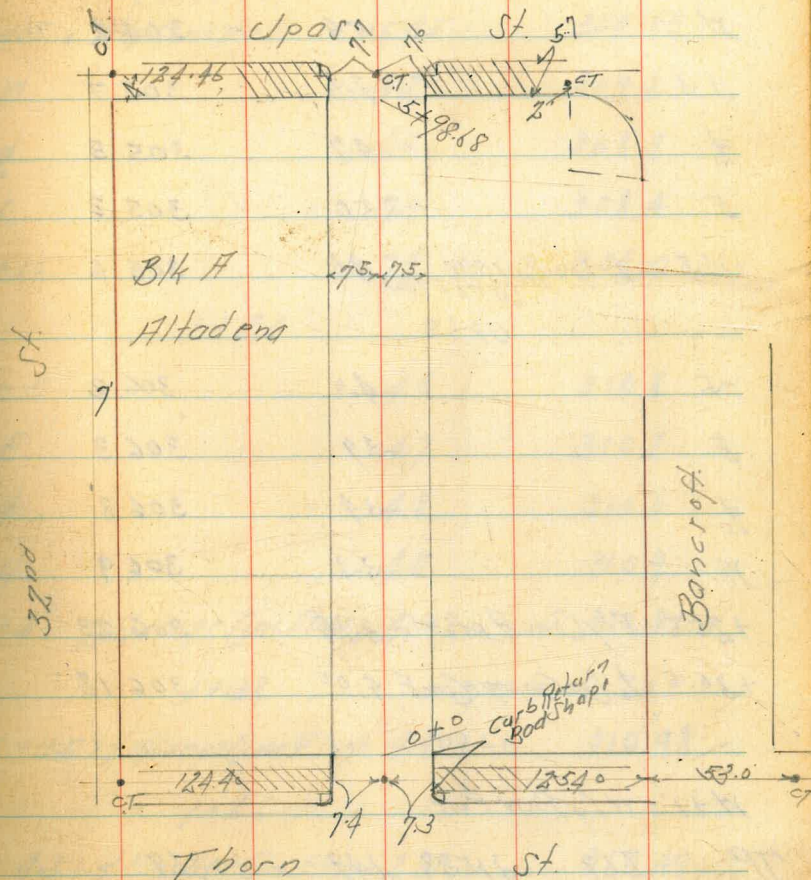
11+22 = Door to Store Conc Floor 6.63 303.55

Red. Plot 3-13-40
 2.594 Profile C.B.H.

Indexed
 c.s.K.

March 7-40
 J. Siron
 Northorn
 H. Moore

52



3/10/18

0+51

-4	5.8	304.4
W	5.4	304.8
+3	4.5	305.7
Z	4.7	305.5
F	5.0	305.2
+14.5 = 1/2 Do Garage Conc Floor	4.6	305.6

0+69

-5	4.0	306.2
F	3.9	306.3
Z	3.4	306.8
W	3.3	306.9
+25.5 = Fly Conc Floor	3.95	306.23
+30.5 = 1/2 Do Garage Conc F.	4.00	306.18

0+80

W+1 = W 1/4 Port. Pole

TP	6.69	315.88	1.49	308.69
----	------	--------	------	--------

0+82

W-4.5 = 1/4 Do Garage Conc Floor	6.22	309.16
----------------------------------	------	--------

3/15/38

0+96

-9.5 = 1/4 Do Garage Conc Floor	6.19	309.19
-1.5 = Fly Conc Walk	5.55	309.83
W	6.2	309.2
Z	6.5	308.9
F	7.0	308.4
+10	7.4	308.0

1+28

-5	4.6	310.8
F	4.7	310.7
Z	4.8	310.6
W	4.5	310.9
+4 = 1/2 Garage Conc Floor	4.57	310.81

1+38

E-11.5 = 1/2 Garage Conc Floor	4.40	310.98
--------------------------------	------	--------

1+66

-4.3 = 1/2 Garage Conc Floor	2.89	312.49
W	2.9	312.5
Z	2.9	312.5
F	2.8	312.6

53

325.28

1+68

E-1.1 = Garage Conc Floor 2.69 312.69

E-0.5 = Fly Conc Apron 2.72 312.66

2+0

-5 1.5 313.9

F 1.3 314.1

L 1.7 313.7

+7 = Fly Pass Pole

H 1.3 314.1

TP 10.47 324.30 1.55 313.83

2+0.5

H-2.5 = Fly Conc Apron 9.51 314.79

H-4.5 = Garage Conc Floor 9.35 314.95

2+40

H 8.5 315.8

L 8.6 315.7

F 8.6 315.7

+5 9.1 315.2

2+57.5

L = M.H. on Road 7.97 316.33

324.30

2+91

-5 6.7 317.6

F 6.2 318.1

L 6.6 317.7

H 6.6 317.7

+6 = Garage Conc Floor 6.43 317.87

3+39

-11.1 = Fly Do Garage Conc F. 4.10 320.20

-7.1 = Fly Conc Apron 4.46 319.84

H 4.7 319.6

L 4.9 319.4

F 4.6 319.7

+5 4.9 319.4

3+56

H-7.3 = Fly Conc Apron 4.32 319.98

H-11.1 = Fly Do Garage Conc F. 4.13 320.17

3+68

-5 4.0 320.3

F 4.0 320.3

L 3.8 320.5

54

✓
324.30

H	35	3208
+10.5 = 2 Garage Conc Floor	3.73	320.57
TP	5.48	326.89
	2.89	321.41
4+0		
-11.5 = Sly Garage C.F.	5.18	321.71
-0.4 = Fly Conc Apron	5.35	321.54
H	5.4	321.5
L	5.6	321.3
F	5.3	321.6
+5	5.6	321.3

4+16

H-0.5 = 1/4 Conc Apron	5.14	321.75
H-11.5 = 1/4 Garage Conc F.	5.15	321.74

4+32

+5	4.9	322.0
F	4.2	322.7
L	4.4	322.5
H = Sly Conc Apron	4.20	322.69
+11 = Sly Garage Conc Floor	3.95	322.94

✓
326.89

4+56		
H+0.2 = Fly Conc Apron	3.93	322.96
H-11 = 1/4 Do. Garage Conc Floor	3.90	322.99
4+78		
H = Fly 2 Conc Walk Extends South to Conc Apron	3.10	323.79
H	3.4	323.5
L	3.7	323.2
F	3.8	323.1

4+80

H+1.4 = 1/4 Pav. Pole

4+87

H-1' = Fly Conc Walk-L	3.37	323.52
7.5' Long		
5+0		

F	2.9	324.0
L	3.0	323.9
H	2.8	324.1
+5	3.3	323.6

5+50

-5	2.4	324.5
H	2.2	324.7

55

✓
326.89

Z	2.3	3246
F	2.2	3247
+5	2.7	3242

5+59

W+0.4 = Wly Pav. Pole

5+61

W-0.5 = Z 5.5 Good Slob	1.56	32533
-------------------------	------	-------

5+70

F	2.2	3247
Z	2.0	3249
W	1.7	3252

5+93

W	1.7	3252
+3	1.9	3250
+5	2.8	3241
Z	2.9	3240
F	2.6	3243

5+97

W+0.8 = Wly Pav. Pole

✓
326.89

56

TP	4.53	328.08	3.34	322.55
----	------	--------	------	--------

5+98.68 = S L Upon

F Top Cb	4.63	323.45
----------	------	--------

Gutter on Paving	4.87	323.21
------------------	------	--------

Z	" "	4.98	323.10
---	-----	------	--------

Gutter .. "	4.63	323.45
-------------	------	--------

W Top Cb	4.41	323.67
----------	------	--------

6+04.38 = S Cb Upon

W on Paving	4.90	323.18
-------------	------	--------

Z .. "	5.00	323.08
--------	------	--------

F .. "	5.10	322.98
--------	------	--------

BM	4.14	323.94	SIX B.P C/par 323.00 323.90
----	------	--------	-----------------------------------

Cross Section Alley Blk 35 City Hts
 (See FB 1828 P. 27 for Re-X sect.)
 N.W. R.P.
 Univ. 35 Hts

BM 4.05 363.59 359.54 Univ. 35 Hts

0+14 = NCS University

M on Pav 5.68 357.91

L " " 5.77 357.82

E " " 5.71 357.88

0+0 = NCS Univ

E Top Cb 5.00 358.590

Gutter on Pav. 5.09 358.50

L " " 5.31 358.28

Gutter " " 5.00 358.59

M Top Cb 4.85 358.74

0+25

-5 4.0 359.6

M 4.0 359.6

L 4.4 359.2

+6 4.2 359.4

E = Wly Stucco Bldg 3.8 359.8

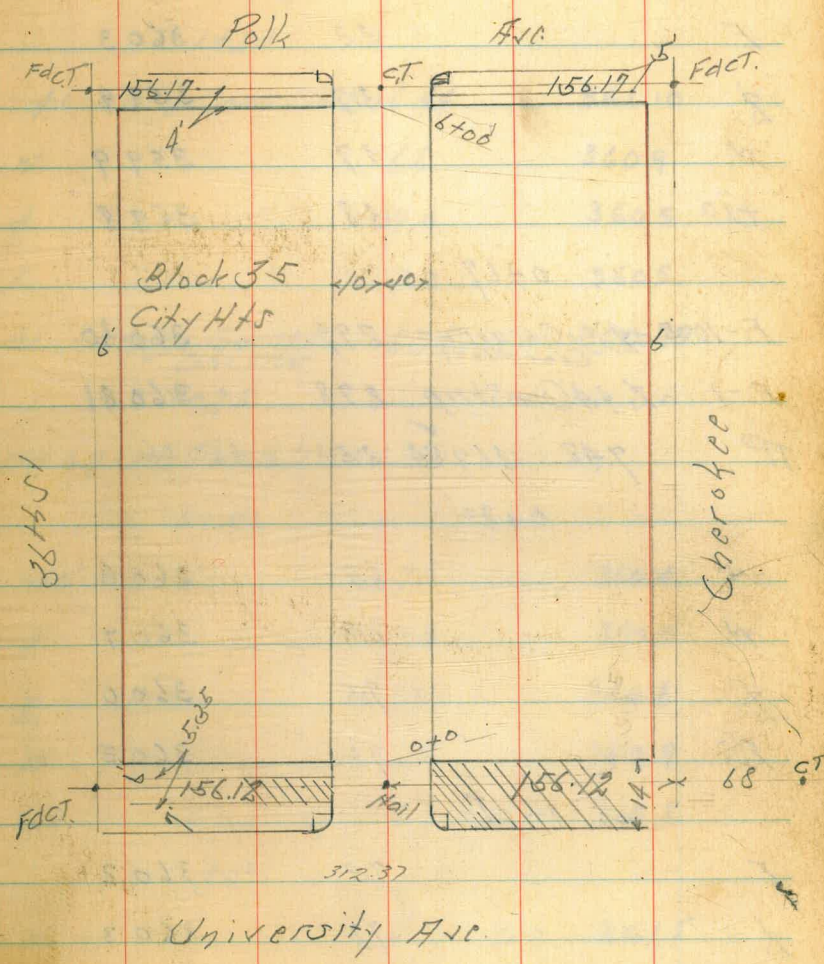
0+49

M -0.2 = Wly Post Pole

Notes Rect. Plot. 3-11-4
 New profile C.B.H.

Indexed
 C.S. K.

March 8-40
 Sisson
 Northey
 Moore
 57



✓
363.59

0+50

-1.3' = 2.2 Conc Walk 3.2 360.4

F 3.3 360.3

2 3.7 359.9

W 3.7 359.9

+1.0 3.8 359.8

0+67

F-10.5' = 2 Do Garage Conc Floor 2.79 360.80

F-1' = 2.44 Conc Strip 2.78 360.81

TP 7.48 367.54 3.53 360.06

0+80

-5 6.9 360.6

W 6.8 360.7

2 7.5 360.0

F 7.0 360.5

1+01

F 7.3 360.2

2 7.2 360.3

W 6.7 360.8

+4.1 = 2.4 Do Garage Conc Floor 6.45 361.09

58

✓
367.54

1+05

F-1' = 2.4 Do Garage Conc F. 6.96 360.58

1+23

-4.1 = 2.4 Do Garage Conc F. 6.44 361.10

W 6.6 360.9

2 7.0 360.5

F 7.0 360.5

+1 = 2.4 Do Garage Conc Floor 6.75 360.79

1+25

W+0.9 = 2.4 Post Pole

1+50

-1.0 7.1 360.4

F 7.0 360.5

2 6.7 360.8

W 6.6 360.9

+1.0 6.7 360.8

2+10

W 6.0 361.5

2 6.3 361.2

F 6.2 361.3

+1.0 6.4 361.1

✓
367.54

2+24.5

W + 0.4 = Wly Power Pole

2+27

-10 5.7 361.8

F 5.7 361.8

L 5.7 361.8

W 5.4 362.1

+0.3 = Sty Conc Apron 5.25 362.19

+5 = Sty 4 Car Garage
Conc Floor 5.15 362.39

2+63

-5 = Wly 4 Car Garage
Conc Floor 5.25 362.29

-0.3 = Wly Conc Apron 5.26 362.28

W 5.3 362.2

L 5.2 362.3

F 5.3 362.2

+5 5.2 362.3

2+73

W = Bottom Open Ditch 5.4 362.1 5.14

W - 50 " " " 5.4 362.1

✓
367.54

59

3+0

F 4.8 362.7

L 4.9 362.6

W 4.9 362.6

3+25

W = Wly Power Pole

3+52

-10 3.9 363.6

W 4.1 363.4

L 4.3 363.2

F 4.2 363.3

+4.7 = L Garage Conc Floor 4.05 363.49

3+93

F - 6.4 = L Garage Conc Floor 3.62 363.92

4+0

F 3.4 364.1

L 3.5 364.0

W 3.3 364.2

+10 3.5 364.0

4+10

F - 6.3 = L Garage Conc Floor 3.30 364.24

367.54

4+26

M+0.2 = Nly Port. Pale

4+32

M-0.7 = Garage Dirt Floor 2.9 364.6

4+50

M 2.9 364.6

L 2.8 364.7

E 2.9 364.6

TP 6.20 371.01 2.73 364.81

4+58

M-5.5 = Sly Do. Garage Conc Floor 5.79 365.22

4+72

M-5.5 = Nly Do Garage C.F. 5.74 365.27

4+78

M-11' = Sly Do. Garage C.F. 5.22 365.79

4+94

M-11' = Nly Do. Garage C.F. 5.32 365.69

5+0

-10 6.3 364.7

F 5.8 365.2

371.01

60

L 5.8 365.2

M 5.8 365.2

5+15

M-5 = Garage Conc Floor 5.32 365.69

5+23.5

M+0.4 = Nly. Porter Pale

5+50

M 5.0 366.0

L 5.2 365.8

E 5.3 365.7

+10 5.7 365.3

5+55

M-0.5 = Garage Conc Floor 4.58 366.43

5+75

-4 = Garage Floor North Entrance 4.9 366.1

E 4.8 366.2

L 4.7 366.3

M 4.4 366.6

✓
371.01

5795

H		4.6	366 4
L		5.0	366 0
F		4.9	366 1

670 S.L. Polk

F	Topcb	5.11	365 90
	Gutter on Paving	5.25	365 76
L	"	5.19	365 82
	Gutter	5.06	365 95
H	Topcb	4.88	366 13

6706.5-506 Polk

H	on Paving	5.46	365 55
L	"	5.63	365 38
F	"	5.72	365 29

TP	1.04	362.57	8.51	362.50
----	------	--------	------	--------

BM		3.99	359.55	NW B.P. Unit X 3674 359.57
----	--	------	--------	----------------------------------

Cross Section Siesta Drive
55th St) West

BM 1.84 ^{435.59} 435.49
 Stations measured on N curb. ^{433.65} ^{SFBP} ^{Alamy +} ^{55th St.}
 $0+0 = \text{N/L } 55\text{th St}$ $\frac{433.45}{2}$ use this for BM. ⁹²⁶

N Cb Top	3.81	431.68
Gutter on Paving	4.23	431.26
L " "	4.29	431.20
S Gutter " "	4.82	430.67
S Cb Top	4.36	430.93

$0+05 = \text{Cb FC}$

S Cb Top	4.54	430.75
Gutter	5.1	430.4
L	4.9	430.6
Gutter	4.7	430.8
N Cb Top	4.01	431.28

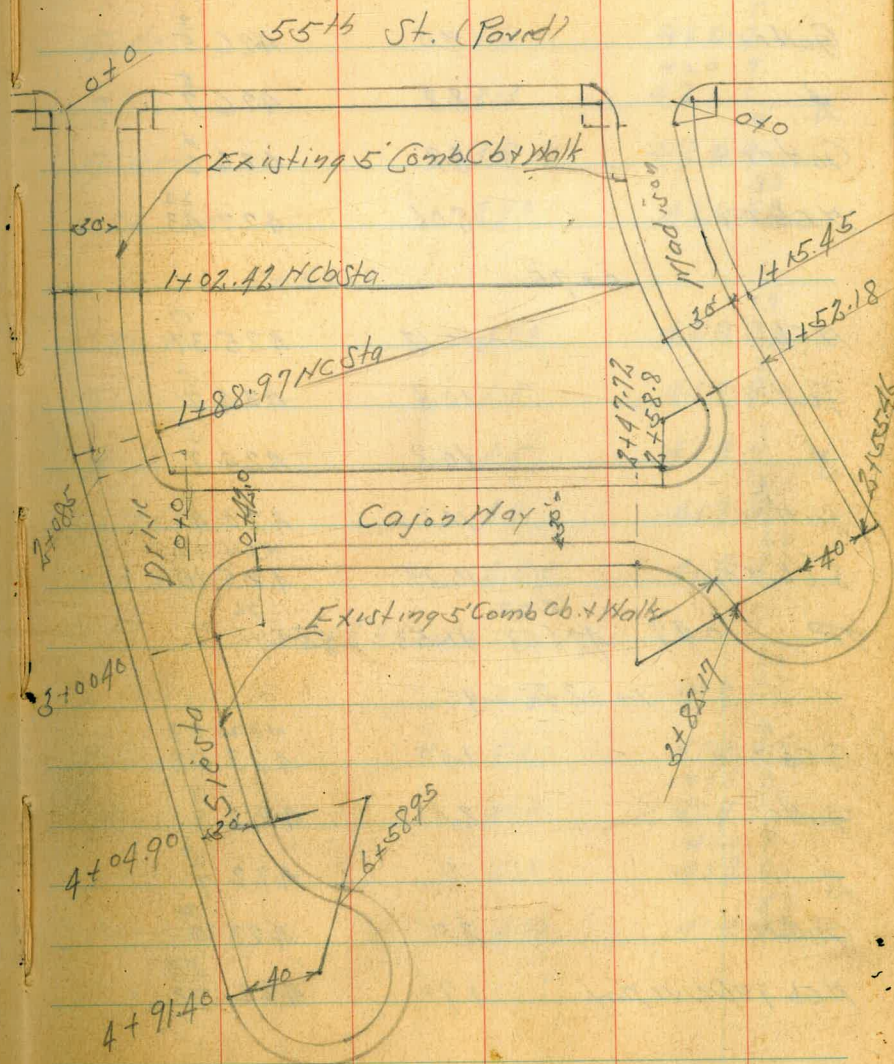
$0+25$

N Cb Top	5.85	429.44
Gutter	6.7	428.6
L	6.6	428.7
Gutter	6.8	428.5
S Cb Top	6.21	429.08

Reduced & Plot on old profile
3/11/40 C.D.H.

Indexed
C.S.K.

62
March 8-40
Sissey
Northey
H. Moore



435.29
435.49

0+50

Scb Top	8.34	426 ⁹⁰ 427 ¹⁵
Gutter	9.0	426 ³ 5
Z	8.8	426 ⁵ 7
Gutter	8.9	426 ⁴ 6
Hcb Top	8.06	427 ²³ 43

0+75

Hcb	10.12	425 ¹⁷ 37
Gutter	10.8	424 ⁵ 7
Z	10.8	424 ⁵ 7
Gutter	11.1	424 ² 4
Scb Top	10.39	424 ⁹⁰ 425 ¹⁰
TP 0.47	424.43 ²³	11.53
		423.96 ⁷⁶

1+02.42 = B.C.

Scb Top	1.40	422 ⁸³ 423 ⁰³
Gutter	2.1	422 ¹ 3
Z	1.7	422 ⁵ 7
Gutter	2.0	422 ² 4
Hcb Top Drive Way	1.70	422 ⁵³ 73

✓ 23
434.43

63

1+31.86

Hcb Top	3.07	421 ¹⁶ 36
Gutter	3.7	420 ⁵ 7
Z	3.3	420 ⁹ 421 ¹
Gutter	3.5	420 ⁷ 9
Scb Top	2.90	421 ³³ 53

1+60.10

Scb Top	4.04	420 ¹⁹ 39
Gutter	4.5	419 ⁷ 9
Z	4.5	419 ⁷
Gutter	4.9	419 ³ 5
Hcb Top	4.54	419 ⁶⁹ 89

1+88.97 = I.C.

Hcb Top	5.18	419 ⁰⁵ 25
Gutter	5.6	418 ⁶ 8
Z	5.3	418 ⁹ 419 ¹
Gutter	5.3	418 ⁹ 419 ¹
Scb Top	4.71	419 ⁵² 72

✓₂₃
124.43

2+085 = CB.C.025

J cb Top	5.15	419.28 ⁰⁸
Gutter	5.8	418.6 ⁴
⌘	5.7	418.7 ⁵
Gutter	6.0	418.4 ²
H cb Top	5.66	418.77 ⁵⁷

2+25

H cb Top	5.96	418.47 ²⁷
Gutter	6.2	418.2 ⁰
⌘	5.9	418.5 ³
Scb Line	6.0	418.4 ²

2+50

Scb Line	6.2	418.2 ⁰
⌘	6.1	418.0 ^{417.8}
Gutter	6.7	417.7 ⁵
H cb Top Drive	6.42	418.01 ^{417.81}

2+75

H cb Top	6.50	417.93 ⁷³
Gutter	6.9	417.5 ³
⌘	6.8	417.6 ⁴
Scb Line	6.7	417.7 ⁵

✓₂₃
124.43

BM

2.42

3+00.4 = BC.025

Scb Top	6.33	417.90
Gutter	7.0	418.10
⌘	7.1	417.4 ²
Gutter	7.3	417.3 ¹
H cb Top Drive	7.18	416.9
		417.1
		417.25 ⁰⁵

3+25

H cb Top	7.12	417.31 ¹¹
Gutter	7.7	416.5 ⁵
⌘	7.4	416.8
Gutter	7.2	417.0
Scb Top	6.66	417.2 ⁰
		417.77 ⁵⁷

3+50

Scb Top	7.02	417.41 ²¹
Gutter	7.6	416.8 ⁶
⌘	7.8	416.6 ⁴
Gutter	8.1	416.3 ¹
H cb Top Drive	7.97	416.46 ²⁶
TP	2.85	418.87
		419.07
	8.21	416.22 ⁰²

64

421.81 SF Top Hxd
422.01 S. Asto +
Co Jumper

418.87
419.07

3+75

Ncb Top	2.46	416.61 ⁴¹
Gutter	3.0	415.9 416.1
Z	2.8	416.3 ¹
Gutter	2.7	416.4 ²
Scb in Drive	262	416.45 ²⁵

4+04.90 = BC 005

Scb Top	2.44	416.63 ⁴³
Gutter	3.2	415.7 ⁷
Z	3.3	415.8 ⁶
Gutter	3.6	415.5 ³
Ncb Top	3.03	415.84 416.04

4+25

Ncb Top	3.62	415.45 ²⁵
Gutter	4.2	414.9 ⁷
15'S = Z	3.6	415.5 ³
33'4S = Gutter	3.6	415.5 ³
33.45 = Scb Top	290	415.97 416.17

418.87
419.07

65

4+50

Ncb Top	4.54	414.53 ³³
Gutter	5.2	413.7 ⁷
15'S = Z	4.5	414.6 ⁴
30'S	4.0	414.9 415.1
50.8'S = Gutter	4.1	414.8 415.0
50.8'S = Scb Top	3.50	415.37 415.57

4+75

Ncb Top	5.46	413.61 ⁴¹
Gutter	6.2	412.7 ⁷
15'S = Z	5.5	413.6 ⁴
30'S	4.8	414.3 ¹
45'S	4.7	414.4 ²

9H.40
4+91.40 = B.C.

Ncb Top	6.03	412.84 413.04
Gutter	6.7	412.4 ²
20'S	6.1	412.8 413.0
40'S = Red. Point	5.4	413.7 ⁵

418.87
419.07

5+19.32

Cb Top	6.90	411.97
Gutter	7.6	412.17
20' E	6.5	411.5
		412.6

5+35.7 = 2 14' Curb Inlet

Cb Top	7.16	411.71
Grating	8.17	410.90

5+47.24

Cb Top	7.14	411.93
Gutter	7.6	411.5
20' E	6.7	412.4

5+75.16

Cb Top	6.55	412.32
Gutter	6.9	412.52
20' E	6.4	412.0
		412.5

6+03.08

Cb Top	5.59	413.28
Gutter	6.0	413.48
20' N	5.8	412.9
		413.1
		413.3

418.87
419.07

6+31.0

Cb Top	4.68	414.19
Gutter	5.2	414.39
20' N	5.2	413.7
		413.9

6+58.95 = P.R.C.

Cb Top	3.80	415.07
Gutter	4.5	415.27
20' N	4.8	414.4
		414.6
		414.3

Cross Section Cajon Way
Siesta Drive to Madison Ave

March 8-40

Indexed
C.S.K.

✓ 35
422.55

67

BM 0.54 ^{422.35}
422.55 ^{421.81}
422.01 ³⁻⁹⁻⁴¹
Siesta
Cajon Way

0+0 = Cb EC. 09 E

		418 92
ECb Top	3.43	419.12
Gutter	4.1	418.5 ³
20" W	4.2	418.4 ²
40" W	4.4	418.2 ⁰

0+42 = EC. 07 W 30" wide

Wcb Top	4.05	418.50 ³⁰
Gutter	4.6	417.8 ^{417.8}
±	4.3	418.3 ¹
Gutter	4.1	418.5 ³
ECb Top	3.65	418.90 ⁷⁰

0+75

ECb Top	3.75	418.80 ⁶⁰
Gutter	4.2	418.4 ²
±	4.5	417.9 ^{417.9}
Gutter	4.9	417.7 ⁵
Wcb in Drive	4.76	417.79 ⁵⁹

Red. Plot on old profile 148
3-12-1940 C.B.H.

Wcb	4.41	417.94
Gutter	5.0	418.14
±	4.6	417.4
Gutter	4.4	417.8
ECb Top	3.90	418.0
		418.2 ⁴⁵
		418.65

1+25

ECb	4.07	418.28
Gutter	4.6	418.48
±	4.8	417.80
Gutter	5.2	418.0
Wcb in Drive	5.12	417.6
		417.8
		417.4 ²
		417.43 ²³

1+50

Wcb Top	4.74	417.61
Gutter	5.5	417.81
±	4.9	416.9
Gutter	4.7	417.1
ECb in Drive	4.78	417.7 ⁵
		417.9 ⁷
		417.77 ⁵⁷

✓35
422.55

1+75

Ecb Top	4.34	418.21 ⁰¹
Gutter	4.9	417.7 ⁵
⌘	5.1	417.5 ³
Gutter	5.6	417.0 ^{416.8}
HCb Top	4.97	417.58 ³⁸

2+0

HCb Top	5.07	417.48 ²⁸
Gutter	5.7	416.9 ⁷
⌘	5.2	417.4 ²
Gutter	5.0	417.6 ⁴
Ecb in DINE	5.02	417.53 ³³

2+25

Ecb Top	4.61	417.94 ⁷⁴
Gutter	5.0	417.6 ⁴
⌘	5.2	417.4 ²
Gutter	5.8	416.8 ⁶
HCb Top	5.15	417.40 ²⁰

2+47.72 = BC on W

HCb Top	5.21	417.34 ¹⁴
Gutter	5.8	416.8 ⁶
⌘	5.3	417.3 ¹
Gutter	5.0	417.6 ⁴
Ecb Top	4.70	417.85 ⁶⁵

2+58.8 = BC on E

Ecb Top	4.75	417.80 ⁶⁰
Gutter	5.2	417.4 ²
15' W = ⌘	5.4	417.2 ⁰
31' W = Gutter	5.8	416.8 ⁶
31' W = Cb Top	5.23	417.32 ¹²
BM	4.66	417.89 ^{417.69}

2+58.8 = BC on East CT

Cross Section Madison Ave
55th St to Cajon Way

Indexed
C.S.K.

Sta on S. cb.

B.M.	8.77	426.46 426.66	417.69 417.89	Ct. 2458.8 Cajon Way
		0+0 H.L. 55th St.		
			50	
N cb Top	0.96	425.70	04	
Gutter on Parking	1.42	425.24	77	
⌘ " "	1.69	424.97	88	
Gutter " "	2.58	424.08	35	
S cb Top	2.11	424.55		
		0+5 = Cb E.C.		
			36	
S cb Top	2.10	424.56	8	
Gutter	2.7	424.0	6	
⌘	1.9	424.8	7	
Gutter	1.8	424.9	31	
H cb Top	1.15	425.51		
		0+23.09		
			39	
H cb Top	2.07	424.59	6	
Gutter	2.9	423.8	6	
⌘	2.9	423.8	9	
Gutter	3.6	423.1		
			73	
S cb Top	2.73	423.93		

Redy Plot on old Profile # 148
3/12/40 C.B.H.

March 9-40

69

V46
426.66

		0+46.18		
S cb Top	3.67	422.79		
Gutter	4.5	422.0		
⌘	3.9	422.6		
Gutter	4.2	422.5		
H cb Top	3.16	423.30		
		0+69.27		
			17	
N cb Top	4.29	422.37	3	
Gutter	5.2	421.5	6	
⌘	4.9	421.8	2	
Gutter	5.3	421.4	28	
S cb to Drive	5.18	421.48		
		0+92.36		
			420.93	
S cb Top	5.53	421.13		
Gutter	6.4	420.3		
⌘	5.9	420.6		
Gutter	6.3	420.4		
H cb Top	5.38	421.08		

✓46
426.66

1+15.45 = FC

Ncb Top	6.99	419.97
Gutter	7.2	420.17
L	7.0	419.5 ³
Gutter	7.3	419.7 ⁵
Scb Top	6.49	419.4 ²
		418.97
		420.17

1+52.18 = BC on N

Scb Top	7.70	418.96 ⁷⁶
Gutter	8.2	418.5 ³
L	8.0	418.7 ⁵
Gutter	8.3	418.4 ²
Ncb Top	7.94	418.72 ⁵²

1+75

Scb in Drive	8.73	417.93 ⁷³
Gutter	8.8	417.9 ⁷
15' N = L	8.3	418.4 ²
30' N	8.7	417.8
		418.0
38.5' N = Gutter	8.9	417.8 ⁶
38.5' N = Topcb	8.45	418.21 ^{.01}

✓46
426.66

70

2+0

Scb Top	8.55	417.91
Gutter	9.1	418.11
15' N = L	8.7	417.6 ⁴
		417.8
30' N	8.7	418.0
		417.8
50' N	9.1	418.0
		417.6 ⁴

2+25

Scb Top	8.83	417.83 ⁶³
Gutter	9.4	417.3 ¹
15' N = L	9.0	417.5 ⁵
		417.7
30' N	8.9	417.6 ⁶
		417.8
50' N	9.0	417.5 ⁵
		417.7
60' N	9.3	417.2 ²
		417.4

2+55.46 = BC. Pt

Scb Top	9.12	417.54 ³⁴
Gutter	9.8	416.9 ⁷
15' N	9.5	417.0 ⁰
		417.2
30' N	9.2	417.3 ³
		417.5 ⁵
40' N = Rad. Point	9.3	417.2 ²
		417.4

✓46
426.66

2+76.58

Scb Top	9.45	417.21 ⁰¹
Gutter	10.0	416.7 ⁵
15' H	9.7	417.0 ^{416 8}
30' H	9.3	417.4 ²

2+97.70

Scb Top	9.78	416.88 ⁶⁸
Gutter	10.4	416.3 ¹
15' H	9.9	416.8 ⁶
30' H	9.5	417.2 ⁰

3+16 = 1/2 14' Carb/plet

Scb Top	9.95	416.71 ⁵¹
Gutter on Grating	10.93	415.73 ⁵³

3+18.82

Scb Top	9.96	416.70 ⁵⁰
Gutter	11.0	415.7 ⁵
15' F	10.1	416.6 ⁴
30' F	9.6	417.1 ^{416 9}

✓46
426.66

71

3+39.94

Wcb Top	9.82	416.83 ⁶³
Gutter	10.6	416.1 ^{415 9}
15' F	10.0	416.7 ⁵
30' F	9.6	417.1 ^{416 9}

3+61.06

Wcb Top	9.79	416.87 ⁶⁷
Gutter	10.4	416.3 ¹
15' F	10.0	416.7 ⁵
30' F	9.7	417.0 ^{416 8}

3+82.17 = P.P.C.

Wcb Top	9.63	417.03 ^{416 83}
Gutter	9.2 ?	417.5 ³
15' SF	9.8	416.7 ⁷
30' SF	9.5	417.2 ⁰

TP	9.95	436.45 ²⁵ 0.16	426.50 ³⁰	SEBP
B.M.		2.76	433.69 ^{4A}	Hdamst 5576 433.63

B.M.	6.63	428.94	422.21	NWBP E/Cajoot 5576JH
------	------	--------	--------	----------------------------

TP	8.05	436.68	0.31	428.63
----	------	--------	------	--------

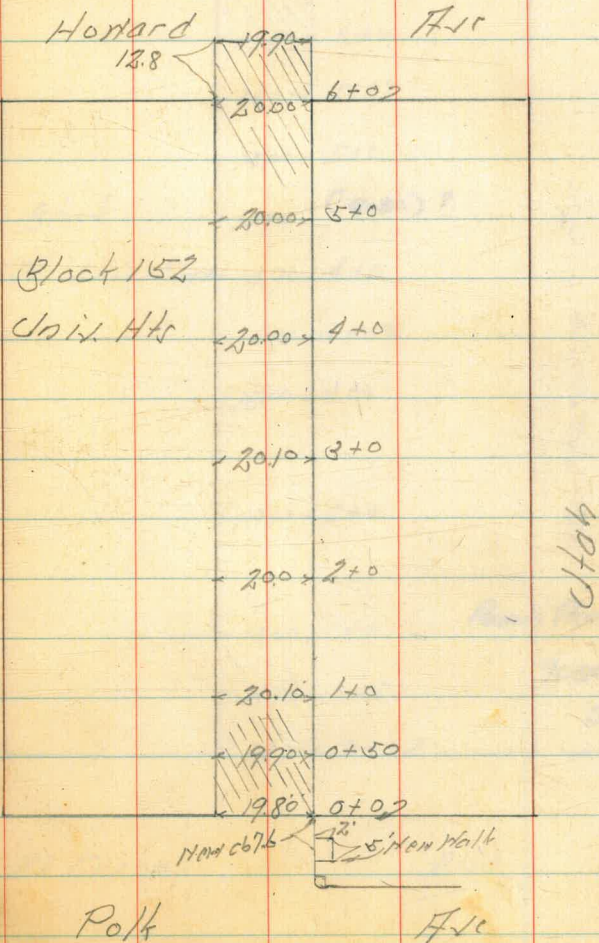
B.M.		2.91	433.77	433.65 SEBP Hdamst 5576
------	--	------	--------	-------------------------------

Final Measurements Paving
Alley Block 152 Univ. Hts.

INDEXED
E.F.B.

Sept 4-40
Sisson
North Spring 72
Walk Moore

Paving Area - 12'252.86
Sqft.



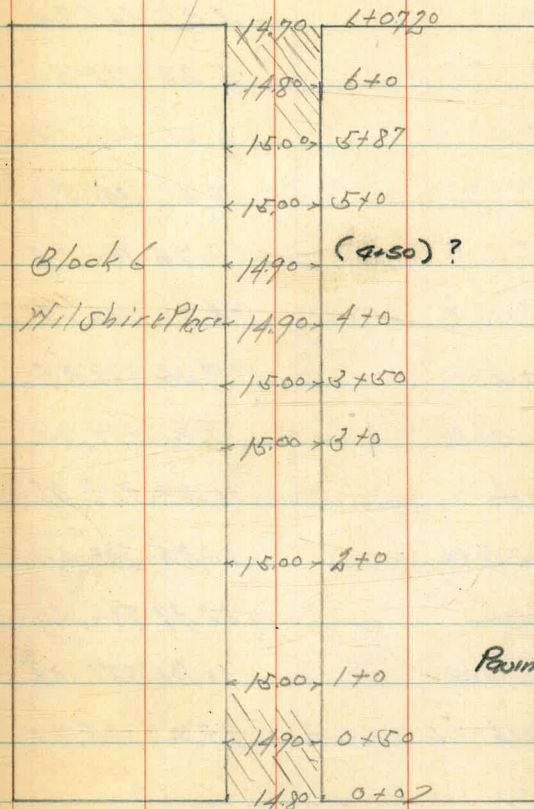
Final Measurements Parking
Alley Block & Wiltshire Place

~~INDEXED~~
FFB

Sept 4-40
S. S. 500
North 73
W. 1/2 part

Meade

Ave.



41 54 54

Marlborough Ave

Paving Area:

9089.90

Sq. Ft.

El Cajon

Blvd

Walker. — Curb levels —
 Bliss. on North cb. Highman St.
 18611 from W.L. Marlborough

11-23-40 To E. line 41st St.

Point	Height	Station	Reading	Reduced Elevation
W.L. Marlborough	1.70		348.79	347.09
-0+00 on cb.			1.81	346.98
+50 " "			3.55	345.24
1+00 " "			5.28	343.51
+40 " "			6.65	342.14
+60 " "			7.46	341.33
+89 " "			7.74	341.05
+79 " "			8.60	340.19
+95 on cb.			9.44	339.35
+95 on stake			8.80	339.99
2+33 on cb.			11.33	337.46
+33 " stake			10.35	338.44
+67 on cb.			12.39	336.40
+67 " stake			11.71	337.08
3+00 on cb. = E. l. 41st St.			13.02	335.77

INDEXED
 EFB

Final Measurement of Paving
Alley Block "A" Altadena

Osborne

SEAN MEYER

4-1-41

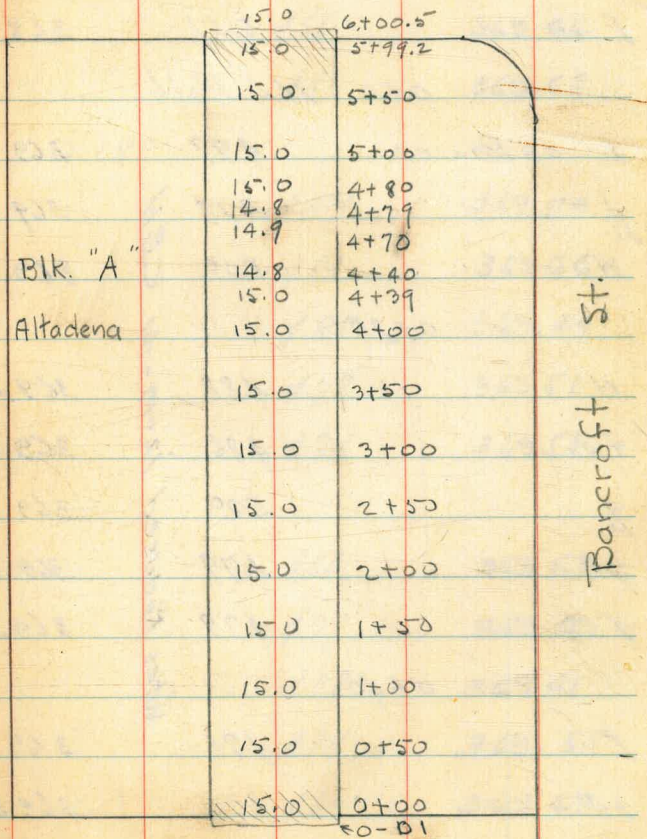
5+99.2 } 4+80.0 }	119.2	15.0 x 15.00	1788.00
4+79 =	1.0	15.0 } 14.8 } x 14.90	14.90
4+70 =	9.0	14.8 } 14.9 } x 14.85	133.65
4+40 =	30.0	14.9 } 14.8 } x 14.85	445.50
4+39 =	1.0	14.8 } 15.0 } x 14.90	14.90
0+00	439.0	15.0 x 15.00	6585.00

Note - This does not include } 8,981.95 ^{sq ft}
Paving in Thorn or Upas }
4-1-1941 CBH

Indexed
cr. sk.

75

UPAS St.



Blk. "A"
Altadena

St.
32nd

Bancroft St.

THORN St.

Cross Section Alley Block 152 University Hts.
From Polk to Howard Between
Idaho & Ctob

BM 4.33 374.29 369.96 S.F.R.P. Polk/Idaho

0-14 = N. Ob. Line Polk

W on Paving 5.35 368.94

± " " 5.45 368.84

F " " 5.51 368.78

0+0 = N.L. Polk

F on Paving 4.99 369.29

± " " 5.18 369.11

W " " 5.00 369.29

0+20

W 4.88 369.41

+4 4.86 369.43

± 5.00 369.29

+6 4.79 369.50

F 4.79 369.50

0+40

F 4.74 369.55

+4 4.74 369.55

± 4.94 369.35

+5 4.83 369.46

W 4.80 369.49

Notes Reduced 12-19-41 C.S.K.

20' wide Indexed
C.S.K.

374.29

0+60

W 4.81 369.48

+3 4.76 369.53

± 4.91 369.38

+6 4.63 369.66

F 4.61 369.68

0+80

F 4.59 369.70

+5 4.63 369.66

± 4.85 369.44

+5 4.78 369.51

W 4.74 369.55

1+0

W 4.66 369.63

+5 4.79 369.50

± 4.88 369.41

+5 4.74 369.55

F 4.60 369.69

1+20

F 4.57 369.72

Dec. 18-41
S. J. S. S. S.
North 369.7
W. Moore 76

37429

+5	4.64	369.65
+	4.82	369.47
+5	4.69	369.60
W	4.58	369.71

1+40

W	4.51	369.78
+5	4.62	369.67
+	4.79	369.50
+5	4.62	369.67
F	4.53	369.76

1+60

F	4.51	369.78
+5	4.56	369.73
+	4.69	369.60
+5	4.61	369.68
W	4.50	369.79

1+80

W	4.47	369.81
+5	4.54	369.75
+	4.65	369.64

37429

177

+5	4.50	369.79
F	4.44	369.85

2+0

F	4.37	369.92
+5	4.48	369.41
+	4.60	369.69
+5	4.50	369.79
W	4.42	369.87

2+20

W	4.26	370.00
+5	4.32	369.97
+	4.48	369.81
+5	4.36	369.93
F	4.30	369.99

2+40

F	4.05	370.24
+5	4.13	370.16
+	4.24	370.05
+5	4.15	370.14
W	4.06	370.23

37429

2460

H	3.89	37040
+5	3.90	37039
2	4.06	37023
+5	3.98	37031
F	3.90	37039

2480

F	3.73	37056
+5	3.87	37042
2	3.98	37031
+5	3.81	37048
H	3.68	37061

240

H	3.45	37084
+5	3.59	37070
2	3.75	37054
+5	3.63	37066
F	3.47	37082

DEEGERS RAILROAD CURVE

COLLECTION TABLES

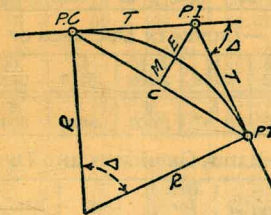


EXPLANATION OF TABLES

Faint, illegible text providing an explanation of the tables, likely containing technical specifications and data descriptions.

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

Radius= $R = \frac{50}{\sin. \frac{D}{2}}$ (1) Degree of Curve= D and $\sin. \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos. \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos. \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin. \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161 + 60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{2} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C.=Sta. P.I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.=Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 638.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 91.27$ and from Table V correction = .10 or $E = 91.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

$\frac{107.08}{2} = 53.54$
 $\frac{107.08}{2} = 53.54$

108.24
 105.86
 22.42
 12.22
 107.08

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.