1575

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

Sea Wall B.M.s

Santa Barbara Pl.	7.03
San Luis Obispo	6.98
El Carmel Pl	7.09
San Juan Pl.	7.07
San Clara Pl.	7.19
San Jose Pl.	7.08
San Rafeal Pl.	7.13
York Court	7.08

X-Sec. Bayside Lane, Ventura Pl. N'ly	1 - 31
X-Sec. Alley 16' wide, Blk. 234. M.B	32 - 33
X-Sec., Alley 16' wide, Blk. 147, M. B.	34 -
X-Sec. Alley 16' " , Blk. 164, M. B.	35 - 36
X-Sec. Alley " " , Blk. 152. M. B.	37 - 38
Location of culverts on Al Bahr Drive at Crespo	39
Alignment proposed extension 49th st., Adams Ave. to 54th St. Ext.	40 - 42
Levels proposed extension 49th - Adams to 54 St. Ext.	43 - 46
X-Sec. of 49th St. Ext.	47 - 60
Ties, 49th St. Ext. to Lot Lines	61 -
Marcella Tract	
X-Sec. Alley Blk. 47, Fairmount Add. - from Trojan to El Cajon, bet. 48th & Estrella	62 - 72
X-Sec. Vine St., Kettner to India	73 - 78
Levels for 54' culvert, change of location	79 -

Xsec of Bayside Lane. 16' wide
Ventura Pl. N/y
Note! Beg. at Ventura Pl.

Moore — Sta. on W.L. Bayside Lane

12-21-39. — gar. aprons & floors are Cem. unless shown dirt.

Seawall Santa Barb.	1.09	8.12 ✓		7.03	BM
T.P.	4.54	3.85 ✓	8.81	-0.69 ✓	
BM: Top Cem. wall			0.46	3.19 ✓	NE Cor. Bayside La Santa Barb
T.P.	4.36	3.38 ✓	4.83	-0.98 ✓	

↓ N.L. Ventura Pl. = 0+00

W	3.6	-0.2
C	3.6	-0.2
E	3.6	-0.2

↓ 0+40

E	3.9	-0.5
C	4.0	-0.6
W	4.2	-0.8

See T.P. Bk. #25 p12

Indexed
C.S.K.

3.38 ✓

0+79 — 1.5 P.P. — E + 0.4

↓ 0+80

W	4.2	-0.8
C	4.2	-0.8
E	4.4	-1.0

↓ 0+94

E	4.6	-1.2
C	4.4	-1.0
W	4.4	-1.0

↓ 1+20

W - 4 S.L. gar	4.45	-1.07	Cem. Ribbon inside garage

↓ 1+33

W	4.8	-1.4
C	4.8	-1.4
E	5.1	-1.7
+ 4.4 S.L. apron	4.87	-1.49
+ 84 " gar	4.71	-1.33

↓ 1+38

W - 4 N.L. gar.	4.58	-1.20	Ribbon

2.38

1+61

E - 4.2 NL apron	4.88	-1.50
E - 8 NC	4.70	-1.32
E	5.2	-1.8
C	5.1	-1.7
W	5.1	-1.7

1+76.23 SL Island

W	4.7	-1.3
C	5.1	-1.7
E	5.2	-1.8

1+80 14" P.P. E -2.0

1+81.23 E Island CT

E Top Walk	5.18	-1.80
W	5.07	-1.69

4.459

1+86.23 NL Island CT = BC SL

W	5.2	-1.8
C	5.2	-1.8
E	5.0	-1.6

T.P. 430.324 4.44 -1.06 Nail pole

3.24

1+40

E	5.2	-2.0
C	5.3	-2.1
W	5.4	-2.2

1+45

E -7.0 SL gar.	4.39	-1.15
E +0.6 " apron	4.49	-1.45

1+67.9

E	4.51	-1.27
E +0.6 apron	4.55	-1.31
C	5.0	-1.8
W	5.0	-1.8

1+75

E -3.3 NL gar.	4.28	-1.04
E +0.6 " apron	4.54	-1.30
E +0.7 10" P.P.		

1+84

W	5.1	-1.9
C	5.1	-1.9
E E Sin. gar.	4.60	-1.36

1+12

E +0.4 SL gar.	4.44	-1.20

3.24 ✓

√ 3+24

E	gar on LINE	4.44	-1.20
E	ground	4.7	-1.5
C		4.7	-1.5
W		4.8	-1.6

√ 3+41

E	+4.0 ℄ 4' walk	4.30	-1.06

√ 3+45

E + 1.8 ℄ 5' shed

√ 3+69.55 ℄ Isthmus Ct.

E		4.56	-1.32
	+2.4 end 4' walk	4.57	-1.33
C		4.7	-1.5
~~W~~		4.7	-1.5
+2	" "	4.60	-1.36

√ 3+64 12" P.P. E + 2.0

√ 4+00

	-2.4 top c.b.	4.34	-1.08
W		4.8	-1.6
C		4.8	-1.6
E		4.8	-1.6

3.24 ✓

√ 4+40

E		4.3	-1.1
C		4.6	-1.4
W		4.7	-1.5

√ 4+50

W-4 ℄ S.N. gar.		4.11	-0.87 N'ly entrance

√ 4+62

E + 1.7 12" P.P. (1.7 in alley)

√ 4+70.62 E.C. 22°05' Lt.

W		4.4	-1.2
C		4.4	-1.2
E		4.4	-1.2

√ 4+98

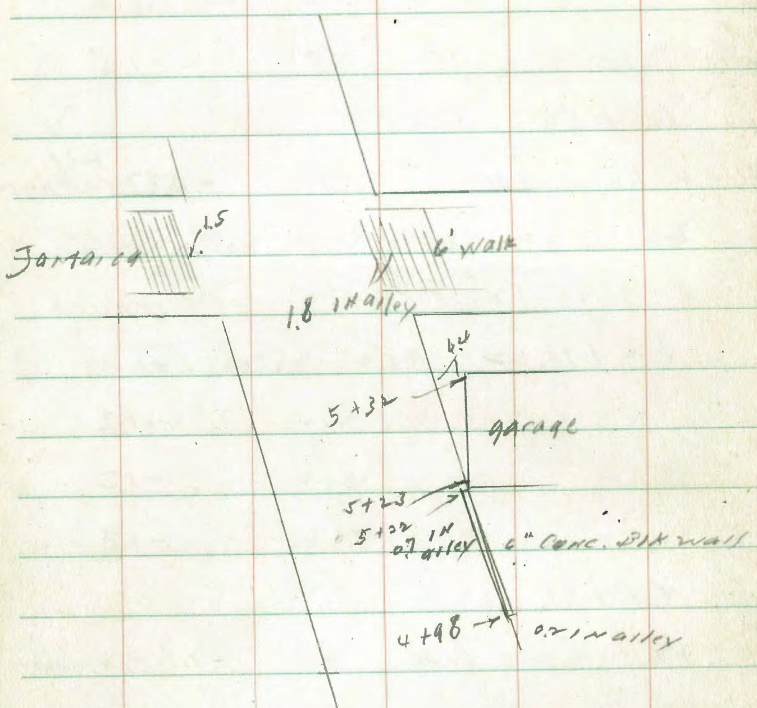
E	+0.7 S. end Conc.	4.3	-1.1 Blk. wall
C		4.3	-1.1
W		4.5	-1.3

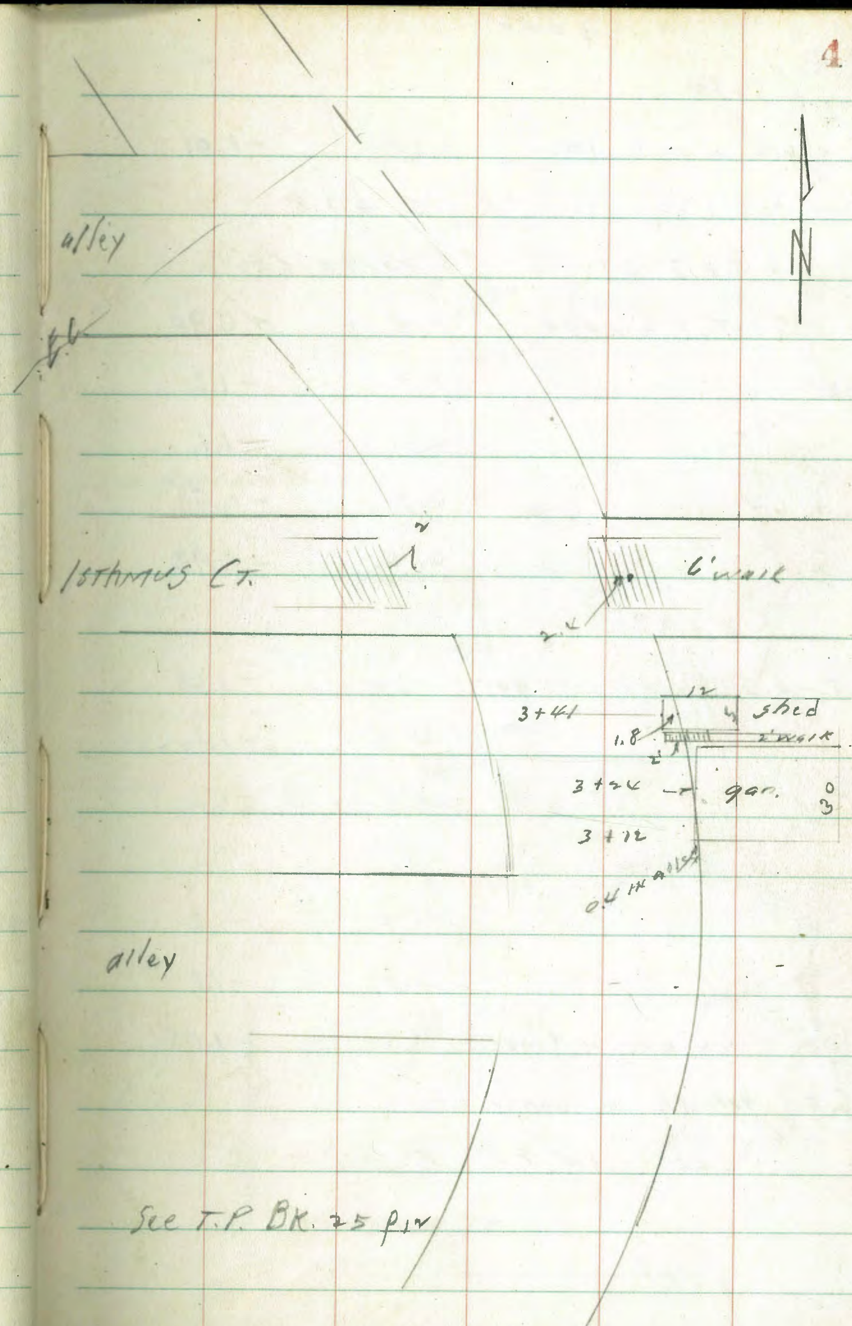
√ 5+22

E + 0.7 N. end Conc. Blk wall

√ 5+23

E	S end gar.	4.25	-1.01


1.5
6' walk
1.8 1N alley
5+32
garage
5+23
5+32
0.7 1N alley
6" Conc. Blk wall
4+98
0.2 1N alley

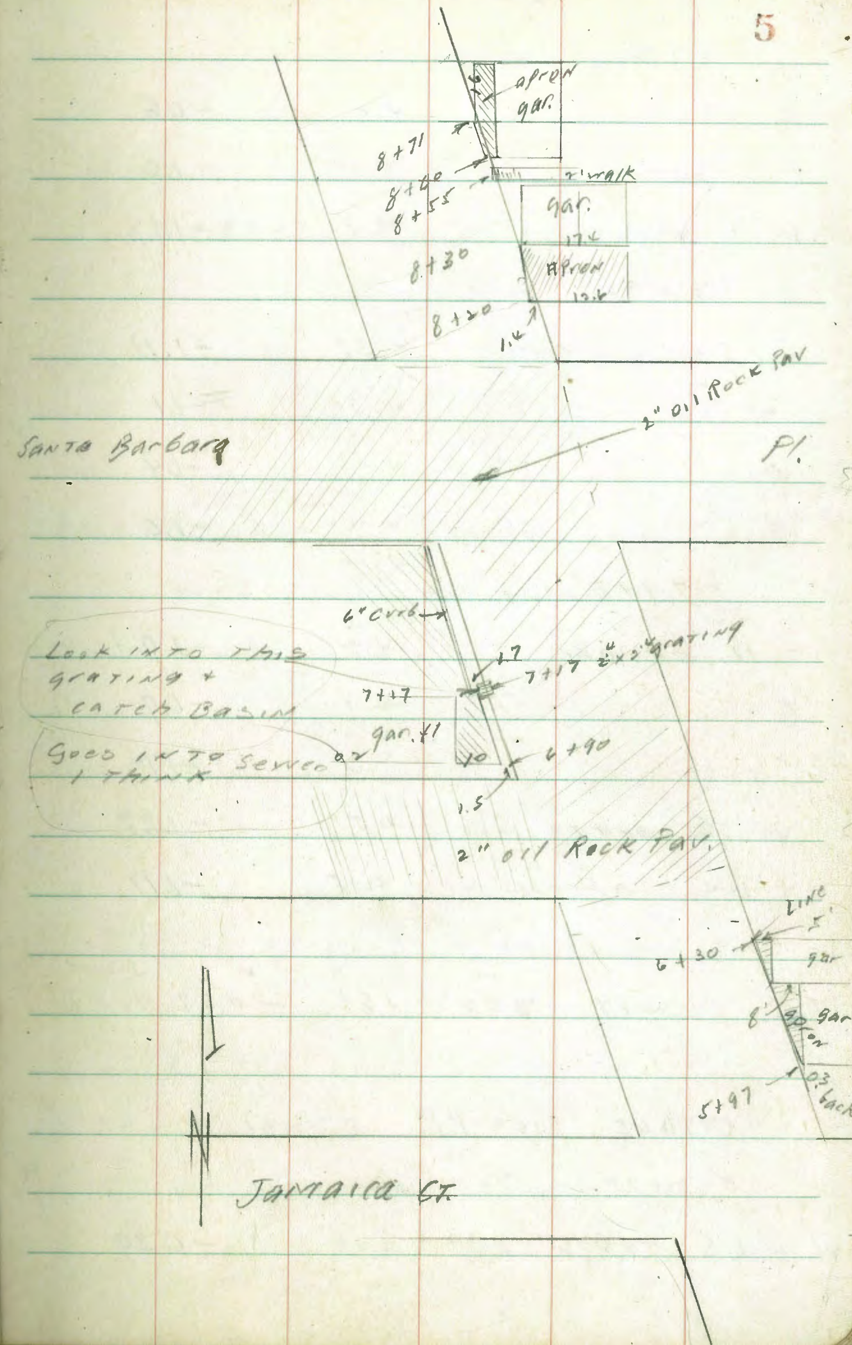

N
alley
Isthmus Ct.
6' walk
2.4
3+41
12
shed
1.8
2' walk
3+26
gar.
3+12
0.4 1N alley
alley

See T.P. Bk. 25 p..

3.24✓

↓ 5+32

E - 6.4	N end gar.	4.25	-1.01
↓ 5+60	12" P.P. E + 1.8		
↓ 5+71.89	℄ Jamaica Ct		
- 1.5	Top 6 walk	4.18	- 0.94
W		4.6	- 1.2
c		4.3	- 1.1
+ 6.2	" "	4.17	- 0.93
E	" "	4.16	- 0.92
↓ 5+97			
E - 0.3	SL apron & gar	4.32	- 1.08
c		4.3	- 1.1
W		4.4	- 1.2
✓ 6+30			
W		4.4	- 1.2
c		4.3	- 1.1
E	NL apron & gar.	4.32	- 1.08
+ 5	gar. fl. 2 higher		
6+61	14" PP E + 1.5		



3.24 ✓

✓ 6+64				
E			3.8	-0.6
C			4.2	-1.0
W			4.3	-1.1
✓ 6+90				
-1.5 S ≮ apron			4.35	-1.11
W			4.3	-1.1
C			4.1	-0.9
E			4.2	-1.0
✓ 7+17				
-11 Sen. gar			4.2	-1.0 dirt
E			4.1	-0.9
C			4.3	-1.1
W E grate			4.51	-1.27
+1.4 apron			4.35	-1.11
T.P.	4.17	3.60 ✓	3.81	-0.57 ✓ S. end Top cb
7+65 12" P.P. E +1.1				
✓ 7+75				
W -1.3 Top 6" cb			4.09	-0.49

3.60 ✓

6

W			4.2	-1.0
C			4.1	-0.9
E			4.2	-0.8
✓ 7+87.97 ℄ Santa Barbara Pl.				
E			4.4	-1.0
C			4.4	-0.8
W			4.3	-0.7
check to NE cor B.M. Top wall		0.39	3.21 ✓	Santa Barbara & Bayside Lane 3.19
Correction of levels				
	0.39	3.58 ✓	3.19	
✓ 8+20				
W			4.6	-1.0
C			4.6	-1.0
+6.4 S.L apron			4.70	-1.12
E " "			4.47	-0.89
✓ 8+30				
E -0.6 SL gar.			4.28	-0.70
E on NE apron			4.55	-0.97

✓ 8+55		
E +0.3 E 2' WALK	4.30	-0.72
✓ 8+60		
E +0.3 St APRON	4.35	-0.77
E -0.8 " GAR.	4.43	-0.65
✓ 8+71		
E +0.3	4.34	-0.76
C	4.6	-1.0
W	4.6	-1.0
✓ 8+85		
E -7.4 N.L APRON	4.36	-0.78
✓ 8+92 10" P.P E +0.4		
✓ 9+50		
W	4.8	-1.2
C	4.7	-1.1
E	4.7	-1.1
✓ 9+90 12" P.P E +0.4		
✓ 10+02.85 E Jersey Ct.		
E Top 6' WALK	4.59	-1.01
+0.4 " "	4.59	-1.01

C	4.8	-1.2
W	4.9	-1.3
W Top 6' WALK	4.46	-0.88
✓ 10+40		
E St APRON	4.46	-1.06
E -1.0 " GAR.	4.17	-0.59
✓ 10+40		
E 0.7 N.L APRON	4.90	-1.32
E -8 N.L GAR	4.17	-0.59
✓ 10+55.85 B.C. RT.		= 0+00
W	5.0	-1.42 (0.6886)
C	4.9	-1.3
E	4.9	-1.3
E +0.7 APRON	4.84	-1.28
T.P. 2.04 3.01	2.59	+0.99 Nail Pole #P3387
✓ 0+35 12" P.P. E +0.2		
✓ 0+50		
E	4.4	-1.4

3.01↵

C	4.2	-1.3
W	4.5	-1.5
1/ + 00		
W	4.6	-1.6
W	4.4	-1.4
C	4.3	-1.3
E		
✓ 1 + 05		
E - 1.5 L. gar.	4.13	-1.12
E - 0.8 " apron	4.46	-1.45
✓ 1 + 28		
E - 0.8 NL "	4.55	-1.54
E - 8.0 " gar	4.14	-1.13
✓ 1 + 41 12" P.P. E - 0.7		
✓ 1 + 52.49 ℄ Kennebec Ct		
W	4.10	-1.09
+ 0.4 E 6' walk	4.10	-1.09
"	4.5	-1.5
	4.4	-1.4
C	4.2	-1.2
E	4.12	-1.11
E + 0.2 " " "		
0 + 88		
E - 0.4 SL apron	4.48	-1.67
E - 1.0 " gar	4.56	-1.55

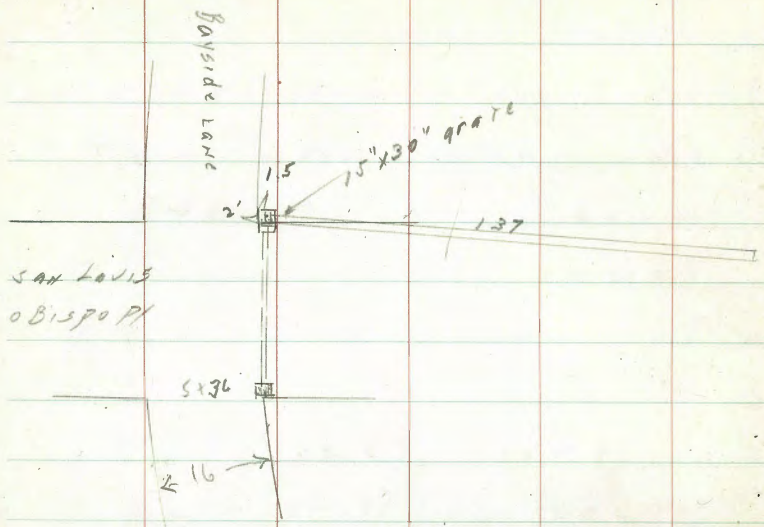
3.01↵

2 + 00		
E	4.5	-1.5
C	4.5	-1.5
W	4.6	-1.6
2 + 07		
E - 0.5 NL apron	4.73	-1.72
E - 7.0 " gar.	4.54	-1.53
2 + 25		
W + 0.5 E 5' walk	4.37	-1.36
2 + 29		
E - 0.5 SL apron	4.47	-1.66
E - 0.8 " gar	4.28	-1.27
2 + 45		
E - 0.5 NL apron	4.74	-1.73
E - 6.2 " gar.	4.25	-1.24
C	4.5	-1.5
+ 7.8 NE Cor gar	4.44	-1.41 N entrance
2 + 47 12" P.P. E - 0.7		
2 + 73		
W	4.8	-1.8
C	4.7	-1.7

		3.01 ✓			
E			4.6	-1.6	✓
+0.5	℄ 8.5'	drive	4.55	-1.54	✓
+32	℄	gar.	3.50	-0.49	✓
	3+00				
E			4.8	-1.8	
C			4.7	-1.7	
W			4.9	-1.9	
	3+42	12" P.P.	E +0.2		
	3+52.43	℄ Kingston Cr.			
W	Top 6'	walk	4.30	-1.29	✓
+0.4	"	" "	4.30	-1.29	✓
+0.5	ground		4.7	-1.7	✓
C		"	4.6	-1.6	✓
E	Top 6'	wk.	4.29	-1.28	✓
	4+00				
E - 3.7	℄ 16'	gar.	4.58	-1.57	✓
E - 0.7	℄ "	apron	4.75	-1.74	✓
E			4.6	-1.6	
C			4.7	-1.7	
W			4.9	-1.9	

		3.01 ✓			
	4+28				
E -1.3	S.L.	gar.	4.75	-1.74	✓
E -0.7	"	apron	4.88	-1.87	✓
	4+46	12" P.P.	E -0.2		
	4+50				
W			4.9	-1.9	
C			4.6	-1.6	
E			4.8	-1.8	
	4+64				
E -8.5	N.L.	gar.	4.68	-1.67	✓
E -0.5	"	apron	4.97	-1.96	✓
	5+00				
E			4.9	-1.9	
C			4.9	-1.9	
W			5.0	-2.0	
T.P.	5.03	3.03 ✓	5.01	-2.00 ✓	
	5+34	12" P.P.	E +0.7		
	5+36				
E	℄ 18"	grating	5.08	-2.05	
	FL 10"	Pipe Cen. out	6.27	-3.24	set by St. Dept.

3.03 ✓



NE Cor.	FL Box + 10" Pipe	6.50	-3.47 ✓
	Top 15"x30" grate	5.25	-2.22 ✓
	FL outlet	7.91	-4.88
T.P.	5.0W	3.02	5.03 -2.00
	5+54.10 ℄ San Luis Obispo Pl.		
W		5.0	-2.0
C		5.0	-2.0
E		5.0	-2.0
	5+75		
E		5.2	-2.2

3.07 ✓

C	5.0	-2.0
W	5.5	-2.5
6+00		
W	5.2	-2.2
C	5.0	-2.0
E	5.2	-2.2
6+18.		
E +03 SL apron	4.76	-1.74 ✓
E -3.8 " gar	4.01	-0.99 ✓
6+50		
E -10 NL gar	4.01	-0.99
E -1.9 " apron	4.76	-1.74 ✓
E	4.8	-1.8
C	4.9	-1.9
W	5.0	-2.0
6+54		
E SL Top conc. wk.	4.28	-1.20 ✓ 12' wide
6+55 1.5 P.P. E +0.5		
6+67		
E SL apron	4.47	-1.45 ✓
E -0.6 SL gar	4.38	-1.36 ✓

3.02

6+80

W-3 E 5.5 WK	4.79	-1.77

6+84

E -4 NL gar.	4.58	-1.36
E " apron	4.63	-1.61

6+91

W-8.7 SL gar.	4.55	-1.53
W-6.7 " apron	4.80	-1.78

7+00

W	4.8	-1.8
C	4.8	-1.8
E	4.9	-1.9

7+09

W-5.4 NL gar	4.42	-1.40
W-3.0 " apron	4.74	-1.72

7+42: 10" PP E+0.4

7+51.21 E Ll d/o CT:

E Top 5' WK	4.46	-1.44
E	4.9	-1.9
C	4.8	-1.8
W	4.9	-1.9
W " " "	4.44	-1.42

3.02

8+00

W	5.0	-2.0
C	4.8	-1.8
E	5.0	-2.0

8+17

W-3.7 SL gar.	4.57	-1.55
W-1.0 " apron	4.69	-1.67

T.P.	4.53	2.73	4.84 -1.80

8+24

E-2 SL gar.	4.19	-1.46

8+37

W-1.0 NL gar.	4.27	-1.49
W+0.7 " apron	4.27	-1.54

8+39

E-3.7 NL gar	4.19	-1.46

8+43 16" P.P. E-0.2

8+50

E	4.7	-2.0
C	4.4	-1.9
W	4.3	-1.6

2.73

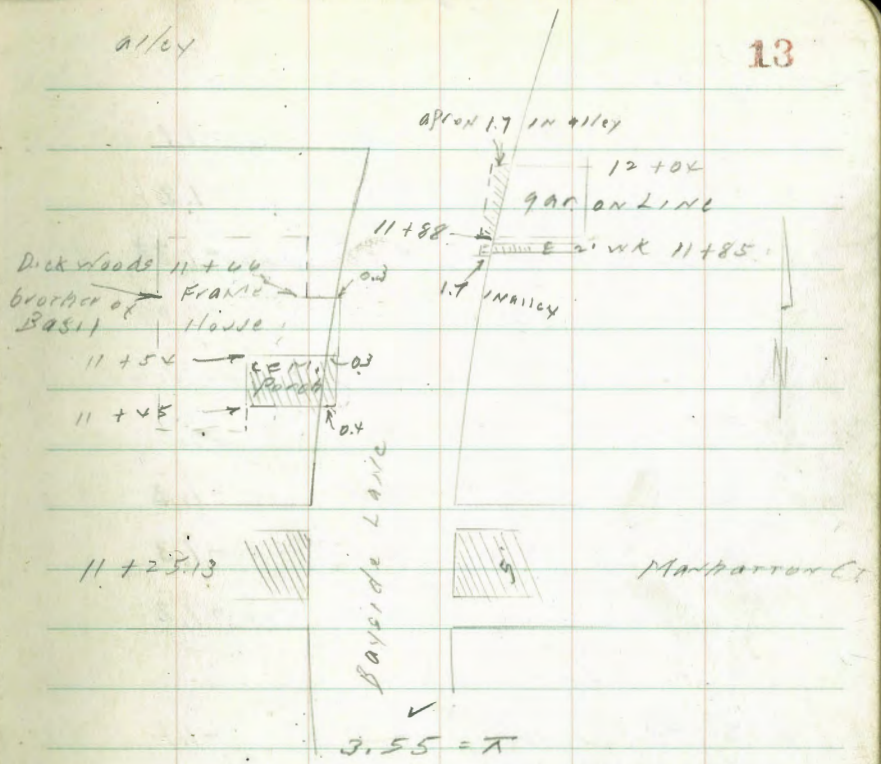
	8+43		
W	E 3' wk.	4.41	-1.68 ✓
	8+80		
W	SL apron	4.55	-1.82 ✓
W-6.5	" gar	4.22	-1.49 ✓
	8+96		
W	NL apron	4.49	-1.76 ✓
W-4.7	" gar	4.19	-1.46 ✓
	9+00		
W		4.4	-1.7
C		4.7	-2.0
E		4.9	-2.2
	9+32 10" PP E -0.2		
	9+38.58 ℄ Liverpool Ct		
E	Top 5' wk.	4.13	-1.40 ✓
E		4.6	-1.9
C		4.6	-1.9
W		4.4	-1.7
W	" "	4.10	-1.37 ✓

2.73

	9+50		
W		4.4	-1.7
C		4.6	-1.9
E		4.8	-2.1
	10+00		
E		4.6	-1.9
C		4.3	-1.6
W		4.2	-1.5
	10+22 14" P.P.		E -3.0
	10+32		
E-5.3	SL gar	3.87	-1.14
E-1.1	" apron	4.12	-1.39
	10+50		
W-3	℄ gar	3.92	-1.19 ✓ 18' wide
W-0.8	℄ apron	4.12	-1.39 ✓ "
W		4.1	-1.4
C		4.1	-1.4
E		4.2	-1.5
+2.2	NL apron	4.10	-1.37 ✓
+6.2	" gar	3.86	-1.13 ✓

2.73

	11+00			
E			4.3	-1.6
C			4.1	-1.4
W			4.1	-1.4
	4+20		12" P.P. E	-1.0
	11+25.13 & Manhatton Ct			
W	& 5' wk		4.06	-1.33
+0.2	"	"	4.06	-1.33
C			4.1	-1.4
E	"	"	4.10	-1.37
T.P.	4.89	3.55	4.07	-1.34
	11+50			
E			5.0	-1.4
C			4.9	-1.3
W			4.9	-1.3
	11+66			
E -4.0	SL gar		4.65	-1.10
E -0.3	"	apron	5.24	-1.69



	11+83		
E -0.5	WL apron	5.24	-1.69
E -4.5	" gar	4.61	-1.06
	11+84		
E	SL 2' work	4.51	-0.96
E+1.7	" apron	4.95	-1.40
	11+88		
E	SL gar	4.50	-0.95
E+1.7	" apron	4.88	-1.33

3.55 ✓

	12+04			
W		4.7	-1.1	
C		4.8	-1.2	
+4.3	NL apron	4.88	-1.33	✓
E	" gar.	4.44	-0.89	✓
	12+18	12" P.P. E on line		
	12+50			
E		5.0	-1.4	
C		4.9	-1.3	
W		4.8	-1.2	
	13+00			
W		4.7	-1.1	
C		4.8	-1.2	
E		4.9	-1.3	
	13+05	10" P.P. E -0.8		
	13+18.05	E El Carmel P/.		
E		5.0	-1.4	
C		4.9	-1.3	
W		4.8	-1.2	
T.P. Rock		5.11	-1.56 ✓	

BMBP	0.95 ✓	8.0 ✓	+7.09	El Carmel
T.P. Rock	check to T.P.		9.64	-1.60 ✓ -1.56
T.P. rock	4.40 ✓	2.80	-1.60 ✓	
	13+50			
W			4.1	-1.3
C			4.3	-1.5
E			4.3	-1.5
	14+00			
E			4.5	-1.7
C			4.4	-1.6
W			4.5	-1.7
+7.5	E do. gar		4.0	-1.2 ✓ wood H.
	14+20	12" P.P.	E -0.4	
	14+36			
W -13	E do. gar		4.3	-1.5 ✓ wood H.
	14+50			
W			4.5	-1.7
C			4.7	-1.9
E			5.0	-2.2

2.80

	15+00		
E		4.7	-1.9
C		4.6	-1.8
W		4.7	-1.9
	15+06	10" P.P. E -0.5	
	15+10.60 ℄ Monterey Ct		
W	Top 5' wall	4.26	-1.46 ✓
W+0.3	" "	4.24	-1.46
E	" "	4.27	-1.47 ✓
	15+50		
W		4.4	-1.6
C		4.7	-1.9
E		5.0	-2.2
	16+00		
E		4.7	-1.9
C		4.5	-1.7
W		4.5	-1.7
	16+06	14 P.P. E -1.2	
	16+50		
W		4.5	-1.7
C		4.5	-1.7
E		4.6	-1.8
+4.7 E Sin. apron		4.43	-1.83 ✓
+4.7 E " gar.		4.38	-1.58 ✓

2.80 ✓

15

	16+98.98 ℄ Nahant Ct		
E	E 5' walk	4.44	-1.66 ✓
C		4.5	-1.7
W		4.6	-1.8
W	" "	4.43	-1.63 ✓
	17+07.32 = E.C. = 0+00		
W		4.7	-1.9
C		4.5	-1.7
E		4.5	-1.7
T.P.	2.00+2.67 ✓	2.13 +0.67 ✓	✓ Nail in T.P. Nahant Bayside

Note.
E.C. = 0+00 change from W.L. Sta to E Sta.

	0+01	12" P.P. E.L.	
	0+50		
E		4.6	-1.9
C		4.6	-1.7
W		4.7	-2.0
	0+81		
E-1.2	E Sin. gar.	4.78	-2.11 ✓
E-0.2	" apron	4.98	-2.31 ✓

2.67 ✓

0+90	12" P.P. E +0.3	
0+88.37	℄ alley	
W	4.8	-2.1
C	4.5	-1.8
E	4.7	-2.0
1+00		
E -4.3 SL gar.	4.74	-2.07 ✓
E -4.4 " apron	4.78	-2.11 ✓
E	4.7	-2.0
C	4.6	-1.9
W	4.8	-2.1
1+18		
E -1.0 N.L gar	4.79	-2.12 ✓
E -0.3 " apron	4.79	-2.12 ✓
1+24		
E -0.7 E 3' walk	4.96	-2.19 ✓ 2.29
1+50		
W	4.9	-2.2
C	4.5	-1.8
E	4.8	-2.1

2.67 ✓

16

1+79	12" P.P. E +0.5	
1+82.37	℄ Nantasket Ct	
W -0.5 E 5' wk.	4.68	-2.01 ✓
E +0.9 " "	4.67	-2.00 ✓
2+00		
E	4.8	-2.1
C	4.6	-1.9
W	4.9	-2.2
2+40 bag 2" of Rock Salt		
W	4.67	-2.00 ✓
C	4.69	-2.02 ✓
E	4.64	-1.99 ✓
2+50		
W -1.0 E 3' wk.	4.43	-1.76 ✓
2+64		
E -3.8 SL gar.	4.44	-1.77 ✓
E -2.6 " apron	4.66	-1.99 ✓
2+78.75 ℄ alley		
E -0.5 N.L gar.	4.47	-1.80 ✓
E " apron	4.60	-1.93 ✓
C	4.5	-1.8
W	4.6	-1.9

2.671

2+82 14" P.P E -1.X

2+86

W -1.2 Ely edge gar. 4.11 -1.44 S. entrance

2+97

E -3.7 S.L. gar. 4.75 -2.08

2+14

E N.L gar. 4.73 -2.06

3+23 end oil Rock Pav

E 4.5 -1.8

C 4.47 -1.80

W 4.41 -1.74.

3+68 1.3 P.P E +0.6

3+80.37 ℄ San Juan Pl

W 4.2 -1.5

C 4.3 -1.6

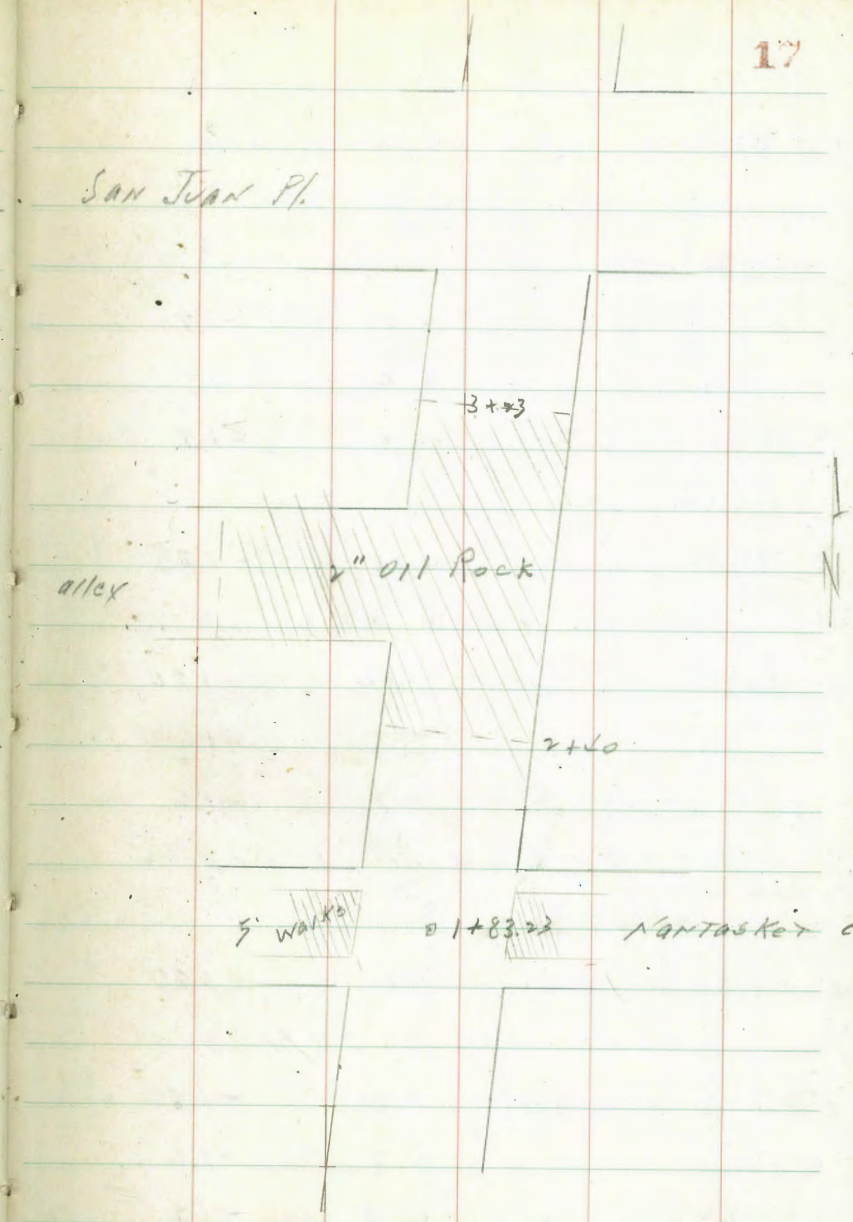
E 4.4 -1.7

4+00

E 4.3 -1.6

C 4.3 -1.6

W 4.4 -1.7



		2.47		
T.P	4.71	3.10	4.28	-1.61
	4+50			
W			4.8	-1.7
C			4.6	-1.5
E			4.6	-1.5
	4+69			
E -2.5	SL gas		4.33	-1.23
	4+82.69		E alley	
E +0.3	NL gas		4.34	-1.26
C			4.7	-1.6
W			4.7	-1.6
	4+84	1.4 P.I.	E +1.0	
	4+87			
E +0.3	SL gas		4.70	-1.60
	5+03			
E	NL gas		4.70	-1.60
C			4.7	-1.6
W			4.9	-1.8

3104

	5+20.			
E	E 2' walk		4.60	-1.50
	5+59			
E -4	E do. gas		4.3	-1.2 Wood Cl.
	5+82	10° P.P.	E	
	5+86.82	E Niantic Ct.		
W	E 5' walk		4.65	-1.55
C			4.6	-1.5
E			4.58	-1.48
	6+13.86	B.C. L.T.	= 0+00	0.6873
E			4.7	-1.6
C			4.6	-1.5
W			4.8	-1.7
T.P.	2.55	3.27	4.38	+0.72 Nail Pole Niantic Ct.
	0+32			
E -0.4	E 2' walk		4.58	-1.31
	0+38			
E	SL gas		4.58	-1.31
C			4.9	-1.6
W			5.1	-1.8

3.27 ✓

0+32		
E NL gar	4.58	-1.31 ✓
0+61 12 FP E		
0+63		
E E 5' wk	4.67	-1.40 ✓
0+75		
W	4.9	-1.6
C	4.8	-1.5
E	4.7	-1.4
+0.4 SL gar.	4.71	-1.44 ✓
0+91		
E -0.4 NL gar	4.7✓	-1.45 ✓
1+00		
E	4.8	-1.5
C	4.7	-1.4
W	4.8	-1.5
1+38		
E -✓ SL arroyo	4.7✓	-1.47 ✓
E -5 " gar	4.5	-0.98 ✓
1+50		
W	4.7	-1.4

3.27 ✓

C	4.7	-1.4
+7.8 NL arroyo	4.65	-1.38 ✓
E +✓.6 NL gar	4.27	-1.00 ✓
5.13 ✓ 3.56 ✓	4.8✓	-1.57 ✓
1+72 10" TW P E +0.✓		
1+77.8 E. ARROYO 4		
W -0.8 E 5' WK	4.95	-1.39 ✓
E -0.✓ " "	5.00	-1.44 ✓
2+00		
E	4.8	-1.2
C	4.9	-1.3
W	5.0	-1.4
2+3✓		
E -1.6 E SIN gar	4.93	-1.37 ✓
2+50		
E -✓.8 SL gar.	4.37	-0.81 ✓
E	4.5	-0.9
C	4.7	-1.1
W	4.8	-1.2

3.54 ✓

2+65

E N.L gar 4.38 -0.82 ✓

2+67 12" PP E+0.7

2+73

E E Sin apron 4.40 -0.84 12' wide level ✓

E-4 " " gar 4.30 -0.74 ✓

3+00

W 4.6 -1.0

C 4.5 -0.9

E 4.4 -1.0

3+32

E-2 SL gar. 4.4 -0.8 dirt

3+50

E N.L. " 4.3 -0.7 "

C 4.5 -0.9

W 4.7 -1.1

3+77 10" Tel. P E+0.3

3+81.5 E OSTEND CT.

E E 5' WK 4.31 -0.75 ✓

W+4 " " 4.44 -0.88 ✓

3.54 ✓

4+00

W 4.8 -1.2

C 4.6 -1.0

E 4.8 -1.2

4+14

E-5 E do. gar 4.7 -1.1 dirt ✓

4+52

E-5 E do. gar 4.7 -1.1 dirt ✓

E 4.7 -1.1

C 4.7 -1.1

W 4.8 -1.2

4+65 14" P.P E-0.5

4+74

E 4 E Sin gar 4.4 -0.7 dirt ✓

5+00

W 4.5 -0.9

C 4.4 -0.8

E 4.6 -1.0

5+22

E-5 E Sin. gar 4.5 -0.9 dirt

3.56 ✓

5+50

E	4.4	-0.8
C	4.3	-0.7
W	4.6	-1.0

5+90 12" PP E +0.4

6+00 approx. ℄ Santa Clara Pl.

W'	4.3	-0.7
C	4.4	-0.8
E	4.4	-0.8

6+15

W	℄ 4' wk	4.30 -0.74

6+50

E	4.4	-1.0
C	4.7	-1.1
W'	4.8	-1.2

6+87 14" P.P. E -2.0

7+00

W	4.7	-1.1
C	4.8	-1.2
E	4.9	-1.3

3.54 ✓

21

Defl. 8°08' Lt.

℄ Sta. angle

7+10.4 P.O.C. = 0+00 beg. line

E	4.9	-1.3
C	4.7	-1.1
W	4.7	-1.1

T.P. 2.37 +1.19 ✓ Top Fence Post

SWBP	3.17	10.36		7.19	Seawall Santa Clara
T.P.	4.09	3.76	10.69	-0.33	
check to above T.P.			2.59	1.17 ✓	0.02

T.P. 2.88 4.05 ✓ +1.17 ✓ Top Post.

0+34

W	5.2	-1.2
C	5.1	-1.0
E	5.5	-1.5
+2.4 ℄ S.M. gar.	5.6	-1.5 dirt ✓

0+55.17 ℄ Portsmouth Ct.

-0.4 ℄ 5' walk	4.6w	-0.57 ✓
E	5.3	-1.2

4.05

C		5.1	-1.0
+7.2		5.1	-1.0
+7.2	℄ 5' walk	4.44	-0.41
	0+58		
W +0.5	beg. 6" cb.	4.47	-0.42 Top
	1+11	12" PP	E +0.2
W	end of 6" cb.	4.69	-0.64 "
	1+18.15 ℄ alley		
W		4.9	-0.9
C		4.7	-0.7
E		5.0	-1.0
	1+81.15 ℄ Pismo Ct.		
E	Top 5' W	4.75	-0.70
C		4.7	-0.7
W	" "	4.72	-0.67
	1+84	12" P.P.	E +0.9
	2+36	16" PP	E +0.4
	2+27		
E -7.2	Sin. gar	5.0	-1.0 Wood F.J.
	2+44.15 ℄ alley		
W		4.9	-0.9

4.05

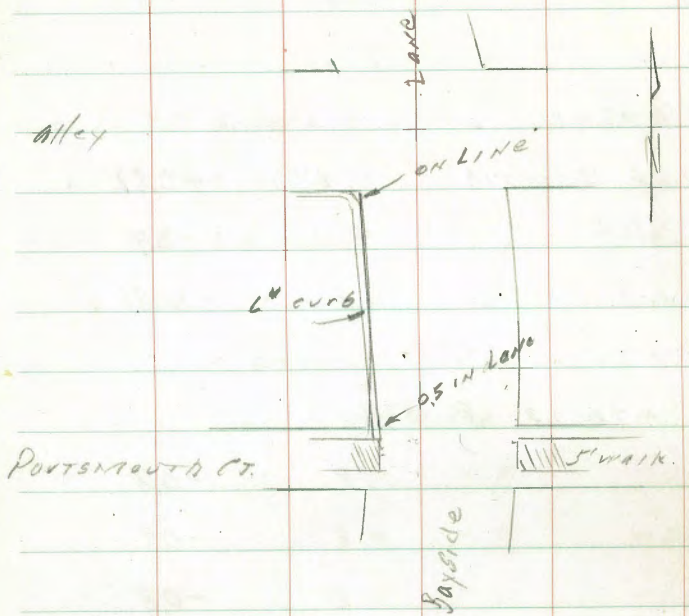
C		4.8	-0.8
E		5.0	-1.0
	3+07.78 ℄ Queenstown Ct.		
E	Top 5' walk	4.87	-0.82
C		4.9	-0.9
W	" " "	4.86	-0.81
	3+57 12" P.P.	E -2.2	
	3+70.68 ℄ alley		
W		4.8	-0.8
C		4.8	-0.8
E		4.8	-0.8

T.P. 4.52 3.82 4.75 -0.70

4+34.22 ℄ Redondo Ct

E	Top 5' walk	4.60	-0.78
C		4.50	-0.68
W	" "	4.48	-0.66

4+89 10" P.P. E -0.7



3.82 ✓

4+97.98 E alley

W	4.8	-1.0
C	4.6	-0.8
E	4.7	-0.9

3.82 ✓

5+15

W - 4.8 E Sin. gar	5.0	-1.2 d. in ✓
5+37		
E - 0.2 SL Conc. slab	4.60	-0.78 to house ✓
5+53		
E - 0.2 SL " "	4.58	-0.76 " " ✓

5+41.77 E Rockaway Ct.

E E 5' walk	4.66	-0.84 ✓
C	4.7	-0.9
+7.6 " "	4.60	-0.78 ✓
6+00		
W	4.8	-1.0
C	4.8	-1.0
E	4.7	-0.9

6+17. 12" P.P. E - 1.4

6+26 alley

E	4.7	-0.9
C	4.7	-0.9
W	4.9	-1.1

T.P.	4.70	3.83 ✓	4.09	-0.87 ✓

3.83

	6+50		
W -2xE Sw. gar.		4.37	-0.54 dirt
W		4.8	-1.0
C		4.8	-1.0
E		4.9	-1.1
	6+97.15 E San Jose Fl.		
E		4.9	-1.1
C		4.8	-1.0
W		4.8	-1.0
T.F.	4.48	4.70	-0.87
	7+14		
E -0.8 SE gar		4.50	-0.89 Conc
	7+27		
E -1.0 NE gar		4.45	-0.84
E		4.6	-1.0
C		4.7	-1.1
W		4.9	-1.3

3.61

	7+58 10 Ft.		E -0.6
	7+78		
W		4.9	-1.3
C		4.8	-1.2
E		4.6	-1.0
+7 E gar		4.9	-1.3 dirt
	8+32.54 E Salem Cr.		
E +0.5 E5' walk		4.29	-0.68
+1		4.8	-1.2
C		4.7	-1.1
W		4.7	-1.1
W E " "		4.23	-0.62
	8+70		
W		4.4	-1.0
C		4.6	-1.0
+7.6 SW Cor gar		4.7	-1.1 dirt
	8+86		
E -2.4 NE "		4.8	-1.2 "

3.61 ✓

8+88 14" P.P. E -1.3

9+00

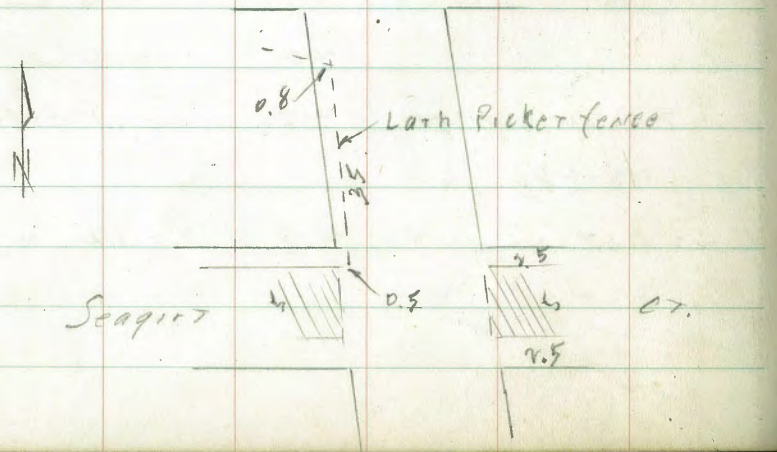
E	4.7	-1.1
C	4.7	-1.1
W	4.7	-1.1

9+23

W -0.5 E 3' wk	4.66	-1.05. ✓

9+60.70 E Seagirt Cr.

W E 5' walk	4.43	-0.82 ✓
C	4.7	-1.1
E	4.9	-1.3
E. " "	4.47	-0.81 ✓



3.61 ✓

9+83

E -1.7 Sin gar	4.7	-1.1 dirt ✓

9+98

E -1.8 Sin. "	4.8	-1.2 dirt ✓

10+13

E 12" P.P. on line	4.7	-1.1
C	4.6	-1.0
W	4.5	-0.9
+9 Sin. gar.	4.5	-0.9 dirt

10+50

W	4.5	-0.9
C	4.7	-1.1
E	4.6	-1.0

10+74

E -1.4 Sin gar	4.8	-1.2 dirt ✓

10+79

W -5.6 Sin. gar	4.6	-1.0 dirt ✓

10+88.84 E Sunset Cr.

W E 5' walk	4.34	-0.71 ✓
E " "	4.34	-0.73 ✓

3.6 ↙

4°08'20"

10 + 93.95 = Δ ↖ Rt. See TP Sk.

E		4.7	-1.1
C		4.7	-1.1
W		4.6	-1.0
T.P.	2.39	3.56 ↙	2.44 4 1.17 ↙	Nail in Pole #385

11 + 42 12" PP E + 4.2

11 + 52.24 = Δ 4°06'30" ↙ Lt.

W		4.4	-1.0
C		4.5	-0.9
E		4.2	-0.6

N + 59

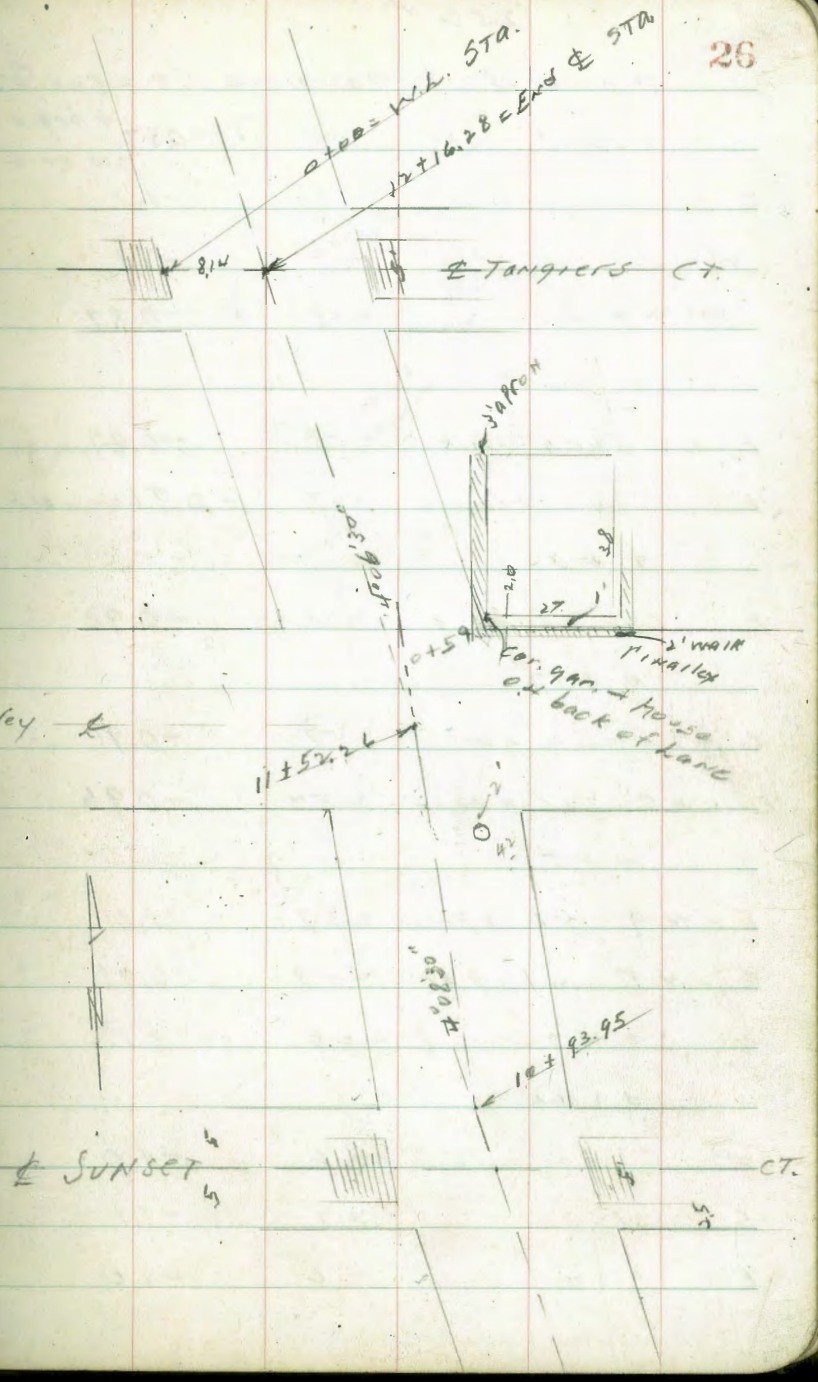
E + 3.1	= Cor apron	4.16	-0.60
E		4.12	-0.56

N + 67

E - 0.2	SW. Cor. gar.	3.92	-0.36

N + 98

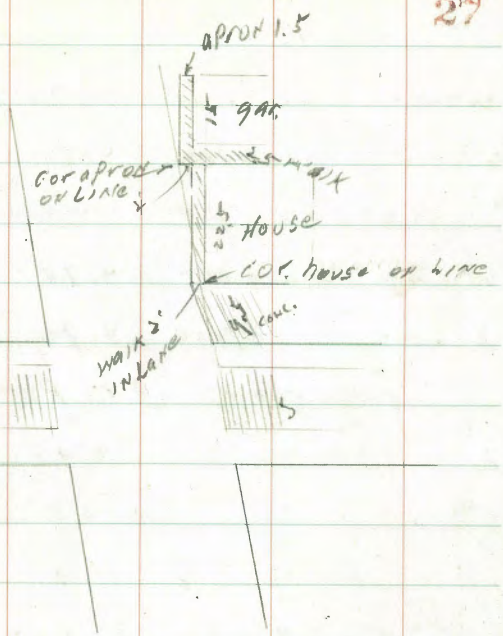
E - 4.2	NE apron	4.21	-0.65
E - 7.2	" gar.	3.91	-0.35



3.5 ✓

12+16.28 & TANGIERS CT = END @ STA.

E	TOP 5 WK	4.43	✓ −0.87 + beg. 0+00 ON W.L
C		4.7	−1.1
W		4.7	−1.1
W	" "	4.43	✓ −0.87
	0 + 1 W		
E	+2 Cor walk	4.53	−0.97
E	" House	4.47	−0.91 on walk
	0 + 3 K		
E	Cor walk	4.48	−0.92
	0 + 37		
E	−2 52 gar	4.47	−0.91 ✓
E	−0.5 " apron	4.5 W	−0.96 ✓
	0 + 5.1		
E	−1.9 WL apron	4.57	−1.01 ✓
E	−4.5 " gar.	4.47	−0.91 ✓
	0 + 5 W	E −0.6	12" P.P.
	0 + 6 W		
W		4.6	−1.0
C		4.7	−1.1
E		4.6	−1.0



3.56

0+74

W – 4.5 S.L. Sin gar	4.70		-1.14
W – 3.1 " apron	4.90		-1.34
0+87			
W – 2.9 N.L. gar	4.70		-1.14
W – 1.5 " apron	4.90		-1.34
1+05.05 B.C. RT.			
E		4.9	-1.3
C		4.8	-1.2
W		4.9	-1.3
1+28.23 E Toulon			
W E 5' walk		4.97	-1.41
C		4.9	-1.3
E " "		4.94	-1.40
1+74			
E E Sin E' gar		4.75	-1.19
E + 1.7 " " " apron		5.21	-1.65
1+80 12" PP E – 1.2			
2+00			
E		5.0	-1.4
C		4.9	-1.3
W		5.0	-1.4

3.56

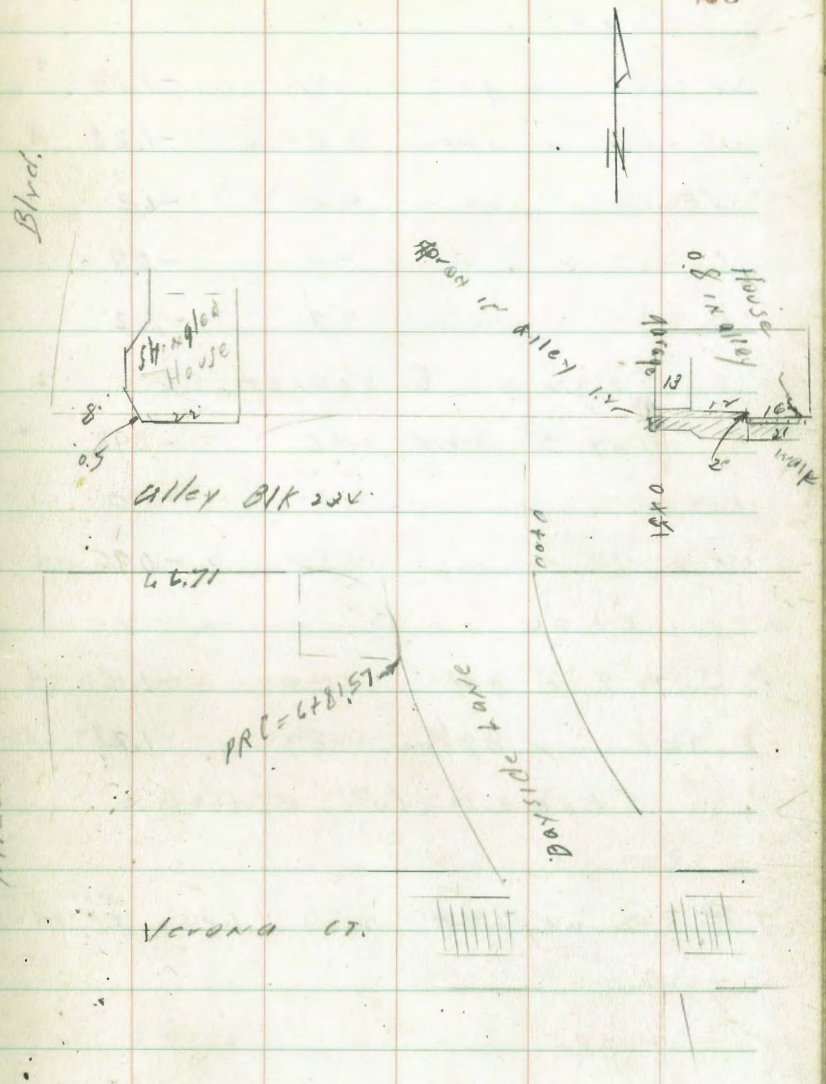
2+04

E – 3 E Sin gar		5.0	-1.4 dirt
2+55.15 E Vanitic Ct.			
W E 5' walk		4.77	-1.21
C		4.8	-1.2
E "		4.81	-1.25
T.P.	4.91	3.54	4.93 – 1.37
3+00			
E		4.7	-1.2
C		4.4	-1.1
W		4.9	-1.4
3+11 12" P.P. E			
3+50			
W		4.7	-1.2
C		4.4	-1.1
E		4.7	-1.2

3.5 ↙

3+88.24 ℄ San Rafeal Pl.

E	4.7	-1.2
C	4.4	-1.1
W	4.0	-1.1
℄ +00		
W	3.7	-1.2
C	4.0	-1.1
E	4.5	-1.0
4+47		
E-0.3 ℄ Sin gar	4.41	-0.87
E+1.5 ∝ apron	4.47	-0.93
4+50		
E	4.4	-0.9
C	4.3	-0.8
W	4.0	-1.1
℄ +50 ∝ 12" P.P. E		
4+67		
W SL apron	4.74	-1.18
W-2.6 ∝ 4 car gar.	4.64	-1.10



3.52 ✓

5+06

W -7.2 NL gar 4.47 -1.13 ✓
W -0.3 " apron 4.82 -1.28 ✓
W 4.8 -1.3
C 4.4 -0.9
E 4.7 -1.2

5+22.11 ℄ Venice Ct.

E Top 5' walk 4.46 -0.92
C 4.5 -1.0
W " " " 4.50 -0.96 ✓

5+44

E -1.7 ℄ 8' gar. 4.70 -1.16 ✓
E +0.8 " " apron 4.82 -1.28 ✓

5+80 12" P.P. E ±0.8

T.P. 2.64 3.97 2.21 +1.33 Nail Pole JP 3919

6+05

E -5.2 ℄ Sin. gar. 4.94 -0.97
E -3.4 " apron 5.25 -1.28 ✓
E 5.2 -1.2

C 5.0 -1.0
W 5.3 -1.3

6+51.03 ℄ Verona Ct.

W. Top ℄ 5' walk 5.06 -1.03 ✓
C 5.0 -1.0
E " " 5.01 -1.04 ✓

6+59 10" Tel. P. E +1.2
" beg. Picket fence E +0.9
6+69 end " " E +0.4

6+72

E -6 SL gar 4.60 -0.63 ✓
E -3.4 " apron 4.64 -0.67 ✓

6+81.57 P.R.C. on W℄.

E 4.9 -0.9
C 4.9 -0.9
W 5.1 -1.1

6+90

E NL gar 4.60 -0.63 on line
E +2.0 " apron 4.65 -0.68

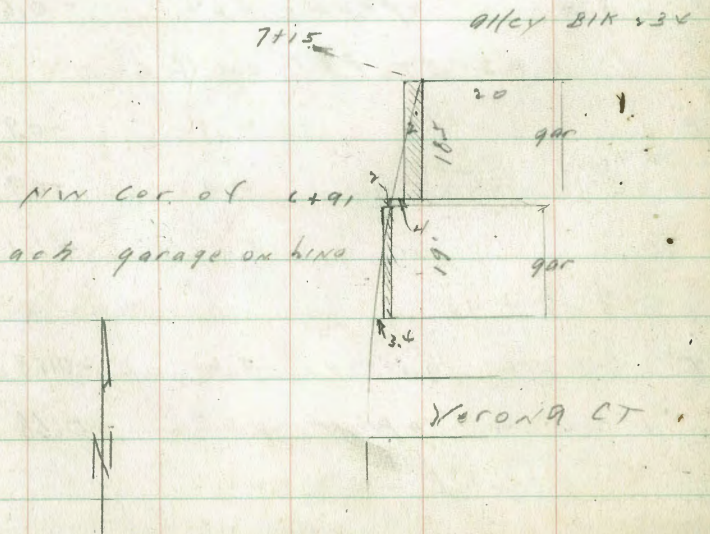
3.97 ✓

6+91

E ~4	S ∠ apron	4.66	-0.69	↓
E - 6	" gar	4.61	-0.64	↓

7+15

W		4.4	-0.6	
c		4.4	-0.6	↓
E 4	N ∠ apron	4.48	-0.67	↓
E	" gar.	4.40	-0.63 S ∠ alley	



Pages 8 to 31 Platon Profiles CBH 1-22-40

Xsec of alley 16' wide
Blk 234 M.B.

S.L. Sta.

3.97 ✓

00 – 10 E. of Mission Blvd

S	on grating	5.24	-1.27
N	"	5.20	-1.23
℄	"	5.30	-1.33

0+00 = ℄ Mission Blvd

N	Top of C	4.70	-0.73
N	Pav	5.33	-1.36
C	"	5.19	-1.22
S	"	5.27	-1.30
S	Top of C	4.58	-0.61

0+07

S-0.5 E 3' walk		4.87	-0.90

0+28

N+0.5 SW gar		4.64	-0.73 dirt

0+33 12" P.P. S-0.3 Back of Shingled House

Indexed C.S.K.

3.97 ✓

0+66.71 P.C.

S		5.0	-1.0
C		4.8	-0.8
N		4.8	-0.8

0+74

N+0.4 ℄ gar		4.8	-0.8 dirt

0+93.41 = P.I.

N		4.8	-0.8
C		4.6	-0.6
S		4.6	-0.6

0+00 = ℄ Bayside Lane

S		4.7	-0.7
C		4.5	-0.5
N		4.7	-0.7

N 12" P.P. on line

0+05

N+0.3 E gar.		4.7	-0.7 dirt

0+20 12" P.P. S+0.4

3.97 ✓

0+21.5			
5 − 0.7 E 3' walk	4.40	−0.43	
0+27			
N +0.3 E "	4.35	−0.38	
0+31			
N +0.3 E gar	4.3	−0.3 dirt	
0+51			
N +1.7 W.L apron	4.26	−0.29	
C	4.2	−0.2	
S	4.3	−0.3	
0+64			
N −1.7 E.L. gar.	4.22	−0.25	
N +1.7 " apron	4.17	−0.25	
0+66.5 Δ of walk			
N +3 S edge 2' walk	4.30	−0.33	
0+85			
S	5.7	−1.2	
C	5.0	−1.0	
+1	4.7	−0.7	
+5 S edge 3' walk	4.74	−0.77	

3.97 ✓

1+20			
N	5.7	−1.2	
S	4.0	−2.0	
1+77 approx line of new alley N & S			10' wide
S	9.1	−5.1	
N	9.1	−5.1	
T.P. 6.17	9.39 ✓	0.70	3.27 ✓
check to BM Seawall & San Rafael Pl. 2.77 ✓		7.15 ✓	7.13

1-2-40

Xsec alley 14' wide

Blk 147 Mission Beach

℄ STA.

T.P. P15	2.60	3.27 ✓		+0.67	Nails Pole Bayside & Nahant
	0+10	E cb Mission Blvd.			
N	Pav		3.17	+0.10	
S	"		3.10	+0.17	
	0+00	E.L. M. Blvd.			
S	cb		2.57	+0.70	
S	Pav.		2.68	+0.59	
C	"		2.66	+0.61	
N	"		2.77	+0.50	
N	cb		2.67	+0.60	
	0+35				
N			3.8	-0.5	
C			3.7	-0.4	
S			3.4	-0.1	
+3.2	℄ S in gar 8' wide		2.93	+0.34	Level floor cem.
	0+49	S+0.5	14" P.P.		

Indexed
E.S.K.

3.27 ✓

	0+57		
N-3	℄ S in gar 8' wide	4.03	-0.76 cem. fl. Level
	0+74		
S		4.6	-1.3
C		4.4	-1.1
N		4.4	-1.1
+0.4	℄ Cem. apron	4.5	-1.2
+4.4	" " gar		8' wide Level
	1+01		
N-5'	W.L. do. gar	4.68	-1.41 cem.
N-1.9	" apron	4.88	-1.61
N		4.9	-1.6
C		4.8	-1.5
S		5.0	-1.7
+4.5	℄ do. gar.	4.8	-1.5 dirt 14' wide
	1+24		
N-5	E.L. do gar. Cem.	4.83	-1.56
N-1.9	" apron	5.07	-1.80
	1+32.7 = W.L. Bayside Lane		
S		4.9	-1.6
C		4.9	-1.6
N		5.0	-1.7

INDEXED
EFB

Moore 2-21-40

Xsec alley Blk 164 M.B. 16' wide

B.M.	2.99	10.06		7.07	San Juan Seawall
T.P.	2.19	7.62	4.63	5.43	

℄ sta.

0+0 E.L. Strandway

S		2.4	5.2	
C		2.4	5.2	
N		2.2	5.3	
	0+20			
S - 6.7	Sin gar dirt	2.7	4.9	
	0+22			
- 1.2	Sin " Cor.	2.91	4.71	8' wide Level
N		3.0	4.6	
C		3.4	4.2	
S		3.0	4.6	
	0+37			
- 7.2	Sin gar dirt	3.0	4.6	
S		3.5	4.1	
C		4.0	3.6	

Plot on profile 2-23-1940 C.B.H.

7.62

N		4.1	3.5	
	0+40			
N - 10.2	℄ do. gar	3.9	3.7	dirt
	0+41			
S - 2	℄ 6' Con walk	4.30	3.3	Level
	0+66			
N		5.2	2.4	
C		5.2	2.4	
S		4.9	2.7	
+5	W.L. do. gar.	4.60	3.02	Con
	0+82			
S - 5	EL " "	4.65	2.97	"
S		5.4	2.2	
C		5.9	1.7	
N		5.9	1.7	
	0+86	S - 0.2	12" PP	
	0+89			
S - 0.1	W.L. do. gar	5.9	1.7	dirt
	1+05			
N		6.7	0.9	
C		6.8	0.8	

762

S			6.1	1.5	
+0.1 wx do. gar					diver
1+22.35 w L Mission Blvd					
S	cb		7.33	0.29	
S	pav		7.41	0.21	
C	"		7.48	0.14	
N	"		7.48	0.14	
N	cb		7.39	0.23	
	w gar Blvd				
N	pav		8.05	-0.43	
C	"		8.12	-0.50	
+3	℄ x-n grate Sump (over)		8.17	-0.55	
S	"		8.12	-0.50	
T.P.	4.15	4.57	7.20	0.42	

2-21-40

X Sec alley Blk 152 M.B 16 wide

INDEXED
EB

E Sta.

4.57

	0 – 10 E gut Blvd.			
N	1½ x 2 grate	5.47	-0.90	
N	Bot. Box	8.50	-3.93	Main drain
C		5.38	-0.81	
S	1½ x 1½ grate	5.44	-0.87	
	0 + 00 EL M. Blvd.			
S	c6	4.93	-0.36	
S	pav	5.46	-0.89	
C	"	5.50	-0.93	
N	"	5.58	-1.01	
N	c6	5.05	-0.48	
	0 + 01.5			
N	-2.8 WL do. gar.	5.05	-0.48	Conc
	0 + 03			
S	+ 0.6 WL Con. apron	4.87	-0.30	
S	-3.8 " " gar	4.68	-0.11	
	0 + 18			
N	-1.5 EL do. gar	5.02	-0.45	
	CEM			

4.57

	0 + 20			
S	+ 0.6 EL Con. apron	4.89	-0.32	
S	-3.6 " " gar.	4.65	-0.08	
	0 + 24			
N	-0.6 & 8' Brick walk	5.11	-0.54	
N		5.4	-0.6	
C		5.4	-0.8	
S		5.3	-0.5	
	0 + 46 S + 0.7 12" P.P.			
	0 + 54			
S	-0.6 WL 3 car gar.	5.72	-1.15	Cem.
S		5.7	-1.1	
C		5.8	-1.2	
N		5.9	-1.3	
	0 + 68			
N	-4 & S, N. gar.	5.95	-1.38	"
N	-2 " apron	6.06	-1.49	"
	0 + 80			
N		6.0	-1.4	
C		6.1	-1.5	
S		6.0	-1.4	
	+ 0.6 EL. 3 car gar.	5.66	-1.09	"

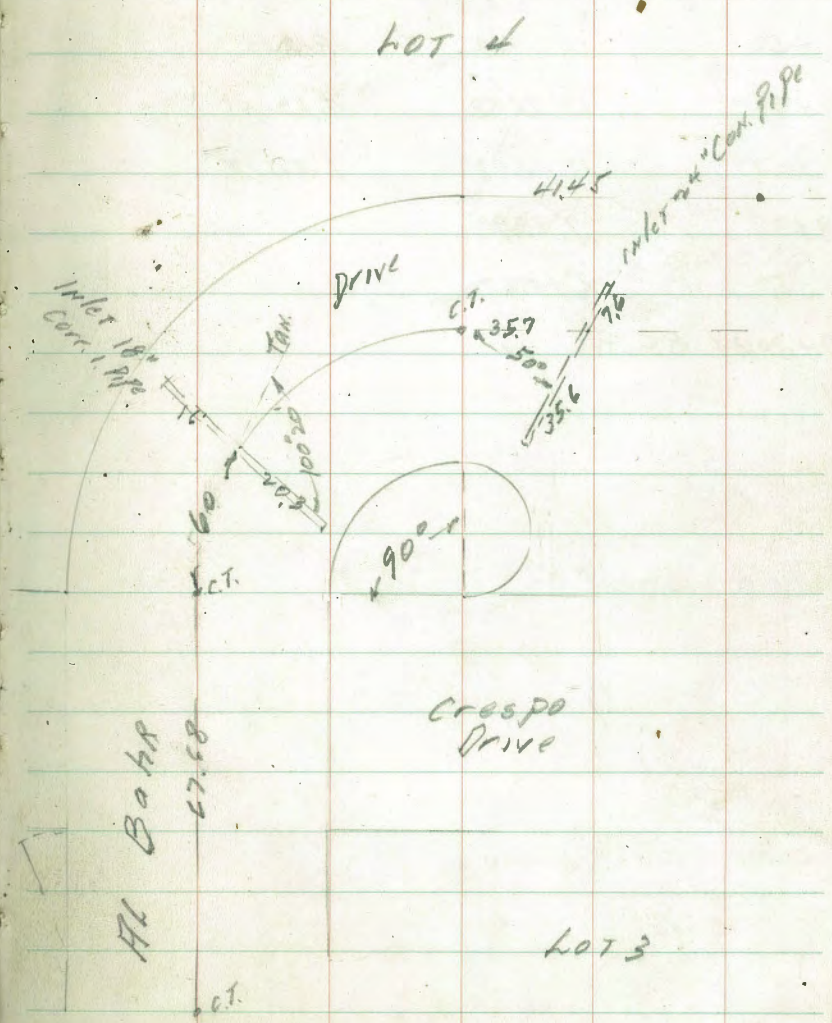
4.57

	0+91			
N	℄ 3' con. wk.		6.2K	-1.67
	1+00			
S			6.2	-1.6
C			6.4	-1.8
N			6.2	-1.6
	1+30			
N			6.3	-1.7
C			6.5	-1.9
S			6.6	-2.0
	1+56.7K	wk Bayside Lane		
S			6.5	-1.9
C			6.5	-1.9
N			6.7	-2.1
T.P.	4.89	3.10	6.36	-1.79
check to T.P. p. 15			2K2	0.68 0.67

INDEXED
EFB

Location of Culverts
on Al Baker Drive
at Crespo

Moore
2-21-40.



Alignment Proposed Extension 49th St.
Adams Ave to 54th St. Extension

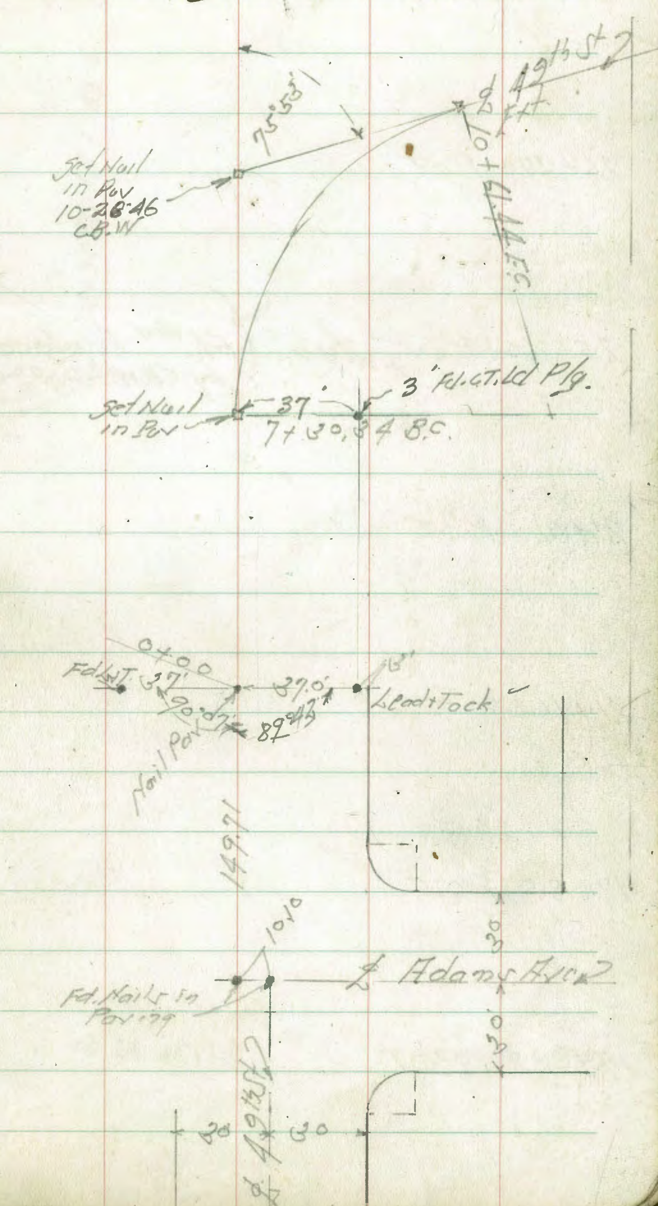
See Page 64 For Land Ties

INDEXED
EFB

	Rt.	
10+61.44 E.C.	37°56.5'	
+50	36°38.0'	
10+0	30°54.18'	Δ 75°53'
+50	25°10.38'	R 250'
9+0	19°26.58'	T 194.91
+50	13°42.78'	L 331.10
8+0	7°58.98'	
+50	2°15.18'	
7+30.34 B.C. Rt.		
0+00		

April 8-40
Sisson
Nortyery
H Moore

This page Plotted on T.P. Sheet 3695
1/17/41 Newcomb
Rec runs off of T.P. sheets made up



30+55.0 P.O.T.

26+87.0 P.O.T.

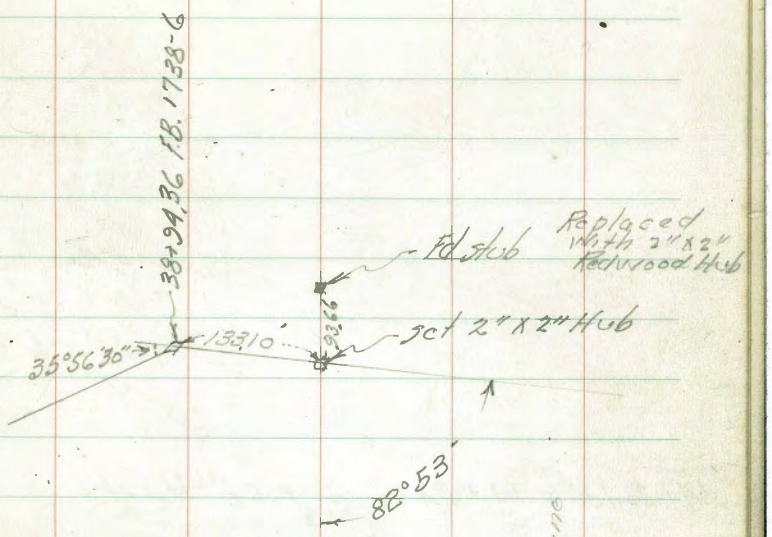
25+36.03 P.O.T. Hub (Fd. Hub Replaced by C.B.W. 10-29-46 With New 2"x2" Redwood)

21+91 P.O.T.

21+16 P.O.T.

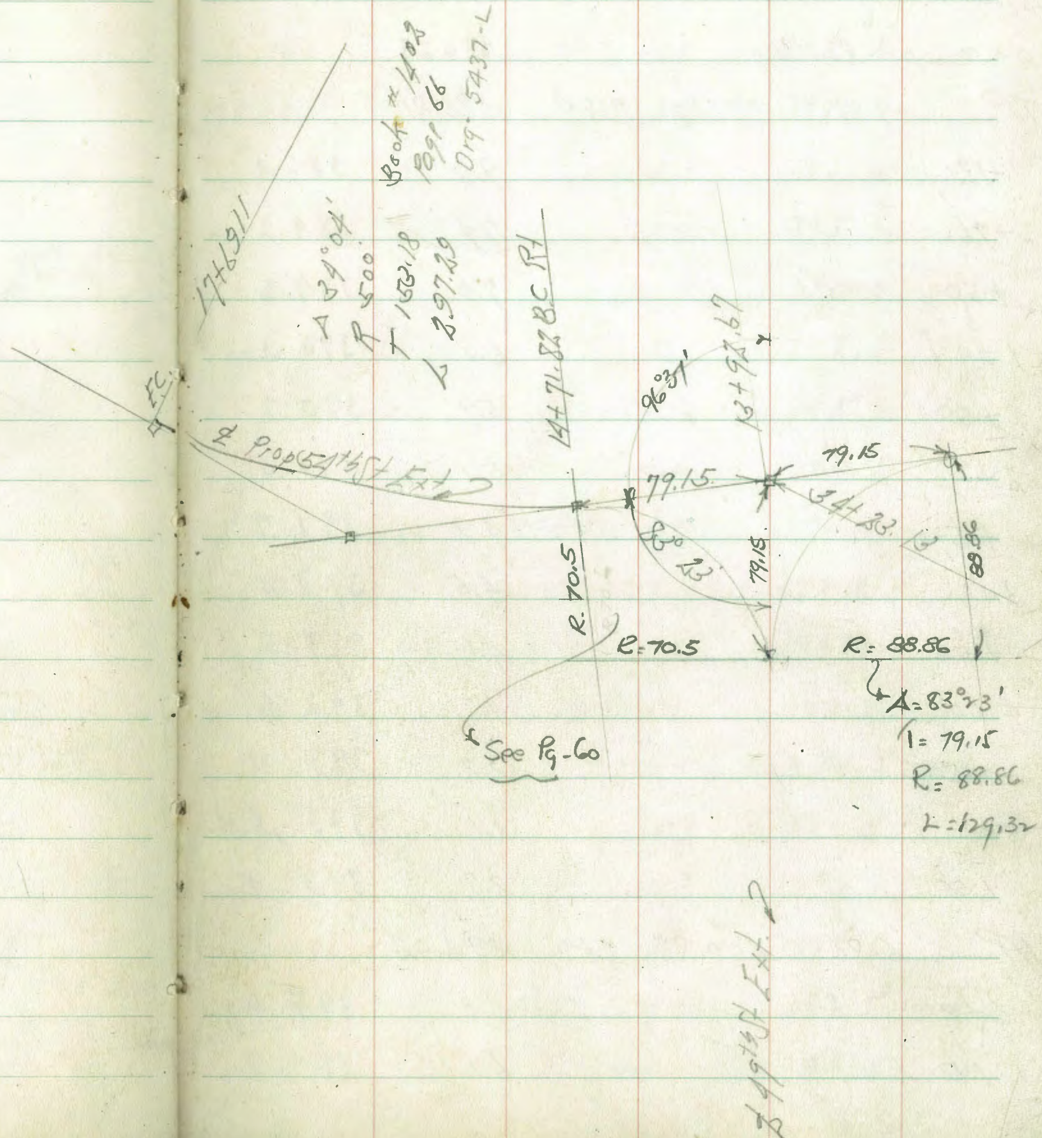
17+85 P.O.T.

17+88.80 POT 17+73.80



Fd Hub 10-29-46 C.B. Walker

34+23.13 = 13+92.67 Prop. 54th St Ext.



32+27.64 P.O.T.

Levels Proposed Extension 49th St.
Adams Ave. to 54th St. Ext.

B.M.	4.82	394.15		389.33	NEBP Adams & Hinono
Adams x 49th St on Paving			10.07	384.08	
0+0 on Paving			7.90	386.25	
TP	9.81	396.62	7.34	386.81	
+12				9.8	386.8
+26				7.4	389.2
+50				7.0	389.6
1+0				6.3	390.3
+50				5.9	390.7
2+0				5.1	391.5
+50				4.9	391.7
3+0				4.5	392.1
+50				4.1	392.5
4+0				4.0	392.6
+50				3.2	393.4
5+0				3.1	393.5
+50				2.7	393.9
TP	6.86	400.88	2.60	394.02	
6+0				6.3	394.6
+50				6.1	394.8

INDEXED
EFB

		400.88			April 10-40 Sisson Northern W. Moore 43
7+0				5.7	395.2
+30.39 B.C. Rl				5.7	395.2
+50				5.8	395.1
8+0				5.8	395.1
+50				5.5	395.4
9+0				5.7	395.2
+50				5.3	395.6
10+0				5.4	395.5
+21.44 E.C.				5.7	395.2
11+0				6.4	394.5
TP	2.01	396.50		6.39	394.49
+50				2.7	393.8
12+0				3.4	393.1
+50				6.1	390.4
+90				12.0	384.5
13+50				5.2	391.3
14+0				4.2	392.3
+50				3.4	393.1
15+0				3.0	393.5
+50				3.0	393.5

		396.50		
16+0			3.4	393.1
+50			3.4	393.1
17+0			4.8	391.7
TP	0.86	390.24	4.12	392.38
+38.80	on Stub		2.81	390.43
+50			5.5	387.7
TP	0.36	381.78	11.82	381.42
+85			2.4	379.4
18+0			9.5	372.3
TP	0.10	369.73	12.15	369.63
+30			12.4	357.3
TP	0.12	358.09	11.76	357.97
TP	0.08	345.74	12.43	345.66
+84			12.7	333.0
TP	3.37	337.00	13.11	333.63
19+0			10.4	326.6
+22 = Bottom Gulch			14.8	312.2
+40			20.3	316.7
+93			12.5	324.5
20+15			6.8	330.2

		337.00		
20+65			0.6	336.4
20+80			1.7	335.3
21+16	P.O.T. on Stub		7.83	329.17
TP	0.56	325.55	12.01	324.99
TP	0.80	314.19	12.16	313.39
21+91			11.9	302.3
TP	0.20	302.02	12.37	301.82
TP	0.12	290.01	12.14	289.88
TP	0.09	277.64	12.46	277.55
22+65			9.7	267.9
23+0			26.0	251.6
+60			35.5	242.1
+48 = Bottom Gulch			37.2	240.4
+54			35.2	242.4
+75			34.8	242.8
24+0			32.3	245.3
+60			14.0	263.6
TP	11.68	289.16	0.16	277.48
25+0			6.0	283.2
TP	11.65	300.72	0.09	289.07

		300.72		
25+36.03	P.O.T. on Stub		1.85	299.37
TP	1.58	303.95	1.85	299.37
+50			2.8	301.1
26+0			2.9	301.0
+37	P.O.T. on Stub		6.20	297.7
+70			10.1	293.8
27+05			16.3	287.6
+22			21.3	282.6
+35			15.1	288.8
+75			6.1	297.8
+90			3.4	300.5
28+0			3.3	300.6
+30			11.1	292.8
+65			11.5	292.4
29+0			7.2	296.7
TP	12.35	311.33	4.98	298.97
+45			7.6	303.7
+70			5.0	306.3
30+0			2.2	309.1
TP	4.60	315.15	0.77	310.55

		315.15		
30+35			2.5	312.6
+55			2.8	312.3
+85			6.0	309.1
31+15			10.5	305.0
+30			12.0	303.1
TP	0.48	303.45	12.18	302.97
+50			6.8	296.6
32+0			12.0	291.4
TP	1.05	292.42	12.08	291.37
32+27.64	P.O.T.		5.11	287.31 on Stub
TP	1.18	281.27	12.33	280.09
+70			9.3	272.0
TP	1.89	271.28	11.88	269.39
33+10			4.0	267.3
+35			3.81	267.47 on Stub
+41			3.4	267.9
+60			8.0	263.3
+80			6.9	264.4
+82	Bottom Gulch		9.2	262.1
34+11			8.5	262.8

271.28

34+16		6.4	264.9	
84+23.18 = 1349267		6.79	264.49	on Stub
14+71.82	B.C. Rt.	4.04	267.24	267.0 M 1402 P69

Moore
Osborn
Hale
6-20-40

X Sec of 49th ST. EXT.

+50

Beg. Hand level
+ + − Rods

1

0+50

0+24

X Sec. at 90° of Radial
unless shown otherwise

0+12

00

0−25

5.17 391.42 386.25 ℄ Par.

INDEXED EPB

LT. ℄ RT.

47

390.3 − 0.4 / 40 = 390.7

391.1 + 0.4 / 40

390.5 − 0.8 / 40 = 390.3

+0.2 / 40 = 390.5

389.5 / 1.9 / 40

389.6

389.8 / 1.6 / 40

388.8 / 2.6 / 40

389.2

390.0 / 1.4 / 40

387.4 / 4.0 / 40

386.8

388.5 / 2.9 / 40

386.3 / 5.1 / 40

386.07 / 5.40 / 26 cc

385.52 / 5.90 / 90T

386.25

386.31 / 5.11 / 90T

386.80 / 4.62 / 26 cc

387.3 / 4.1 / 40

385.54 / 5.88 / 26 cc

385.06 / 6.36 / 90T

385.98 / 5.46 / Par.

385.92 / 5.50 / 90T

386.38 / 5.06 / 26 cc

391.42 −

	LT	℄	RT
5	393.5 0.0 40	393.5	393.6 +0.1 40
+50	392.8 −0.6 40	393.4	393.4 0.0 40
4	392.6 0.0 40	392.6	392.9 +0.3 40
+50	391.9 −0.6 40	392.5	393.0 +0.5 40
3	391.5 −0.6 40	392.1	392.2 +0.1 40
+50	391.3 −0.4 40	391.7	391.4 −0.3 40
2	391.1 −0.4 40	391.5	391.1 −0.4 40

8

+50

+30.3 L B.C. RT.

7

+50

6

+50

LT	℄	RT
394.5 −0.6 40	395.1	395.0 −0.1 40
394.8 −0.3 40	395.1	395.1 0.0 40
394.7 −0.5	395.2	395.2 0.0 40
395.4 +0.7 40	395.2	395.0 −0.7 40
394.8 0.0 40	394.8	394.8 0.0 40
393.6 −1.0 40	394.6	394.5 −0.1 40
393.3 −0.6 40	393.9	394.0 +0.1 40

+50

11

+61.44 EC

10

+50

9

+50

LT		RT
393.8 0.0 40	393.8	393.9 +0.1 40
394.5 0.0 40	394.5	395.2 +0.7 40
395.1 −0.1 40	395.2	394.8 −0.4 40
395.3 −0.2 40	395.5	395.0 −0.5 40
395.6 0.0 40	395.6	395.4 −0.2 40
395.5 +0.3 40	395.2	395.2 0.0 40
395.1 −0.3 40	395.4	395.2 −0.2 40

	LT	℄	RT
15	0.0 / 50	393.5	0.0 / 50
+50	392.6 / −0.5 / 40	393.1	392.9 / −0.2 / 40
14	392.3 / 0.0 / 40	392.3	392.8 / +0.5 / 40
13+50	389.3 / −2.0 / 40	391.3	391.8 / +0.5 / 40
14+90 18" Culv. @ 90° prop.	378.5 / −6.0 / 50	384.5	387.1 / +2.6 / 20 ; 388.1 / +3.6 / 45
	387.8 / −2.4 / 45 ; 389.7 / −0.7 / 20	390.4	390.9 / +0.5 / 40
+50			
14	392.9 / −0.2 / 40	393.1	393.3 / +0.2 / 40

	LT	℄	RT
+85	377.2 −2.2 50	379.4	381.4 +2.0 50
+50	385.7 −2.0 70	387.7	389.2 +1.5 70
+33.8 P.O.T.	389.1 −1.3 70	390.43	390.83 +0.4 70
17	391.4 −0.3 65	391.7	391.9 +0.2 65
+50	392.6 −0.5 60	393.1	392.9 −0.2 60
16	0.0 55	393.1	0.0 55
15+50	0.0 50	393.5	0.0 50

19+22 at 90°

19+22 Prop. 18" C/L. 49°54' LT.

19

+84

+30

18

LT ℄ RT.

332.6 321.9 317.4 317.3 329.3 336.2
+20.4/65 +9.7/35 +7.2/25 −0.9/12 317.7 +16.1/35 +24.0/55

49°54'

294.3 300.6 302.2 306.9 320.6 331.5 339.9
−17.9/125 −11.6/80 −5.0/40 +5.3/20 +8.4/25 +19.3/50 +27.7/75

312.2

CUT INLET 5'

335.2 319.5 323.9 325.2 323.0 333.2
+8.6/50 −7.1/22 −2.7/12 324.6 −1.4/13 −3.6/42 +6.6/60

339.2 323.4 329.0 334.6 337.2
+6.2/50 −9.6/27 −4.0/14 333.0 +1.6/30 +4.2/40

355.6 351.2 362.9
−1.7/55 −6.1/35 357.3 +5.6/55

371.9 372.3
−0.6/50 372.8 +5.1/50

Station			LT			℄		RT
+91			277.6 −24.7 100	284.2 −18.1 75	293.6 −8.7 50	302.3	304.6 +2.3 25	307.7 +5.4 55
21+16			293.5 −35.7 100	304.8 −24.4 75	317.8 −11.4 20	329.17	333.2 +4.0 25	337.7 +8.5 50
+80			293.4 −41.9 100	315.7 −19.6 50	331.1 −4.2 20	335.3	340.7 +5.4 25	347.0 +11.7 50
+65			292.5 −43.9 100	315.3 −21.1 50	331.2 −5.2 20	336.4	343.8 +7.4 25	352.4 +16.0 50
20+15			294.6 −35.6 100	293.1 −37.1 80	309.3 −20.9 40	330.2	336.4 +6.2 15	358.4 28.2 50
+93	Finis deer fly	300.4 −24.1 100	292.9 −31.6 60	308.1 −16.4 30	315.9 −8.6 15	324.5	336.9 +12.4 25	350.5 +26.0 50
19+60			314.3 −2.4 70	311.0 −5.7 32	306.6 −10.1 20	316.7	328.3 +11.6 35	336.2 +19.5 55

+60

24

+75

+71 = Sewer line ← 5 → ← 20 → ← Sewer

+54 Prop. 48" Culv. at 90°

+30

23

22+45

LT	C	RT
263.4	265.2	263.2 / 266.2
0.0 / 90	+1.6 / 45	263.6 −0.4 / 40	+2.6 / 80
247.3	248.0	245.7 / 245.3
+2.0 / 110	+2.7 / 55	245.3 +0.4 / 45	0.0 / 90
241.8	242.3	242.8 / 241.4 / 241.8 / 243.5 / 244.5
−1.0 / 115	−0.5 / 50	242.8 0.0 / 23	−1.4 / 25	−1.0 / 50	+0.7 / 75	+1.7 / 100
237.9	240.0	240.8 / 239.9 / 241.9 / 240.9 / 243.7 / 245.4
Wash −4.5 / 87	Wash −2.4 / 81	−1.6 / 50	Wash −3.8 / 47	−0.5 / 42	242.4 −1.5 / 13	Wash +1.3 / 50	+3.0 / 100
240.4	240.6
−2.0 / 115	−1.8 / 95

F.L. INLET 3' below THIS

238.9	239.9	240.4		247.0	249.1
−4.7 / 115	−3.7 / 85	−1.7 / 35	242.1	+4.9 / 50	7.0 / 100
237.5	239.5	245.2		258.4	259.4
−12.1 / 115	−12.1 / 70	−6.4 / 40	251.6	+7.2 / 50	+7.8 / 100
251.3	259.9		270.9		273.6
−14.6 / 110	−8.0 / 55	267.9	+3.0 / 40		+5.7 / 80

27+05

+70

2

+37

26

+50

+36.03

25+00

LT C PT

267.6	277.3	294.6	302.1
−20.0	−10.3	+7.0	+14.5
80	40	25	50
	287.6		
272.2	284.4	304.0	212.0
−21.6	−9.4	+10.2	+18.2
75	35	25	50
	293.8		
276.5	287.7	305.3	313.1
−21.2	−10.0	+2.6	+15.4
75	35	25	50
	297.7		
278.8	289.4	307.2	312.1
−22.2	−11.6	+6.2	+11.1
75	35	25	50
	301.0		
282.1	296.5	303.1	302.1
−19.0	−4.6	+2.0	+1.0
70	22	15	50
	301.1		
282.3	293.2	299.8	298.3
−17.1	−6.2	+0.4	−1.1
70	35	25	50
	299.37		
278.5	284.4	282.2	280.8
−4.7	+1.2	−1.0	−2.4
80	40	30	65
	283.2		

Station	LT		C		RT.
+65	264.4 −28.0 80	280.7 −11.7 40	292.4	302.1 +9.7 25	313.1 +20.7 45
+30	266.3 −26.5 80	279.8 −13.0 35	292.8	302.6 +9.8 25	315.9 +23.1 45
1					
28	270.0 −30.6 75	283.4 −17.2 35	300.6	310.7 +10.1 25	315.8 +15.2 45
+90	270.0 −30.5 75	284.3 −16.2 35	300.5	309.1 +8.6 25	314.9 +14.4 45
+75	269.9 −27.9 75	285.4 −12.4 35	297.8	307.1 +9.3 25	309.5 +11.7 45
+35	267.6 −21.2 80	276.2 −12.6 40	288.8	294.8 +6.0 25	303.1 +14.3 50
27+22 18" Culv. at 90°	264.6 −18.0 80	272.3 −10.3 40	282.6	288.6 +6.0 25	294.6 +12.0 50

	LT	C	RT
+85	265.0 −44.1 / 85	287.5 −21.6 / 40 309.1	321.2 +12.1 / 25	330.6 +21.5 / 45
+55	268.4 −43.9 / 85	290.1 −27.7 / 40 312.3	328.9 +16.6 / 25	339.0 +26.7 / 45
+35	267.7 −44.9 / 85	289.4 −23.2 / 40 312.6	327.3 +14.7 / 25	338.3 +25.7 / 45
30+00	270.5 −38.6 / 80	289.0 −20.1 / 40 309.1	320.3 +11.2 / 25	330.5 +21.4 / 45
+70	273.4 33.7 / 80	288.5 −17.8 / 40 306.3	317.3 +11.0 / 25	323.5 +17.2 / 45
+45	271.1 −32.6 / 80	288.2 −15.5 / 40 303.7	311.7 +8.0 / 25	318.9 15.2 / 45
29	271.6 −25.1 / 80	284.1 −12.6 / 40 296.7	305.7 +9.0 / 25	318.0 +10.3 / 45

			LT	C	PT			
33+10	260.6 −6.7 115	260.6 −6.7 100	259.7 −7.6 95	259.9 −7.4 80	261.9 −5.4 75	264.0 −3.3 20	262.3	279.2 +11.9 25	292.5 +25.2 60
+70			258.1 −13.9 115		260.1 −11.9 40		272.0	287.5 +15.5 25	303.8 +31.8 50
+27.6			259.6 −27.7 115	260.7 −26.6 60	271.1 −16.2 30		287.31	305.0 +17.7 25	317.1 +29.8 45
32			258.8 −32.6 100	261.8 −29.6 65	275.0 −16.4 35		291.4	306.4 +15.0 25	317.1 +25.7 45
+50			257.5 −39.1 95	260.5 36.1 75	275.6 −21.0 45		296.6	317.2 +20.6 25	326.2 +29.6 45
+30				260.9 −42.2 85	283.9 −19.2		303.1	313.9 +10.8 25	321.9 +18.8 45
31+15				268.0 −42.0 85	283.8 −21.2 40		305.0	315.0 +10.0 25	323.0 +18.0 45

See page 79

34 + 62.86 P.R.C. = 14 + 71.82 54th St. Ext. See Xsec on 54th St. Ext.

+ 33.12 Δ 96°37' LT

R 70.5

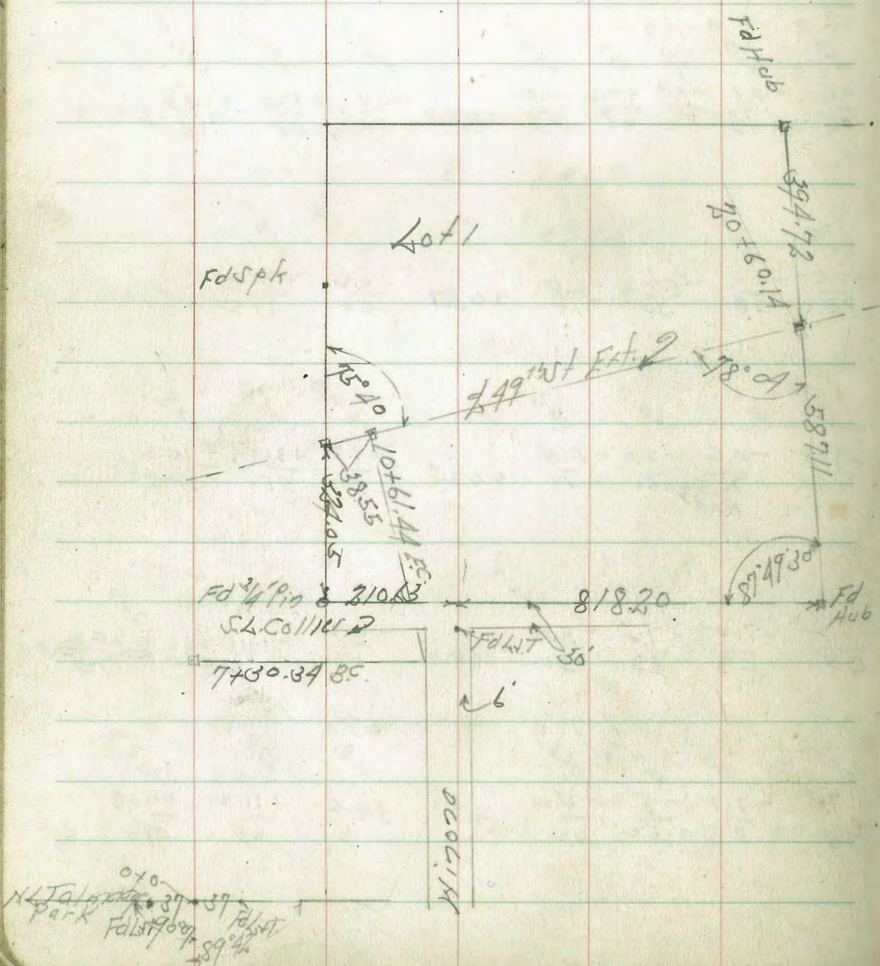
T 79.15

34 + 03.42 L 118.88

Station															
+ 33.12			261.6 1.2 / 115	262.2 −0.6 / 100	260.7 −2.1 / 95	261.0 −1.8 / 73	263.0 +0.2 / 68	262.4 −0.4 / 35	262.8	265.8 +3.0 / 20	274.8 +12.0 / 65	281.4 +18.6 / 115			
34 + 03.42			259.1 −4.6 / 115	261.1 −2.6 / 73	262.7 −1.0 / 68	263.5 −0.2 / 30	263.7 0.0 / 15	263.7	263.9 +0.2 / 50	266.7 +3.0 / 115					
+ 73.70			261.1 −1.7 / 115	261.6 −1.2 / 90	262.2 −0.6 / 70.5 Rad.	260.8 −2.0 / 60	261.3 −1.5 / 7	262.8	264.0 +1.2 / 7	265.8 +3.0 / 55	272.8 ±10.0 / 115				
33 + 43.98 B.C. LT.	264.0 −4.0 / 115		260.9 −7.1 / 91	262.8 −5.2 / 65	260.8 −7.2 / 63	260.8 −7.2 / 33	262.8 −5.2 / 30	268.0	267.8 −0.2 / 10	278.2 +10.2 / 25	288.0 ± 20.0 / 70				
33 + 35	261.5 −6.0 / 115	261.1 −6.4 / 100	261.1 −6.4 / 80	260.1 −7.4 / 75	260.4 −7.1 / 55	262.5 −5.0 / 50	263.5 −4.0 / 20	267.47	268.1 +0.6 / 6	278.7 (94) +11.2 / 25	288.3 +20.8 / 70				

Ties 49th St Extension to Lot Line
Marcellena Tract

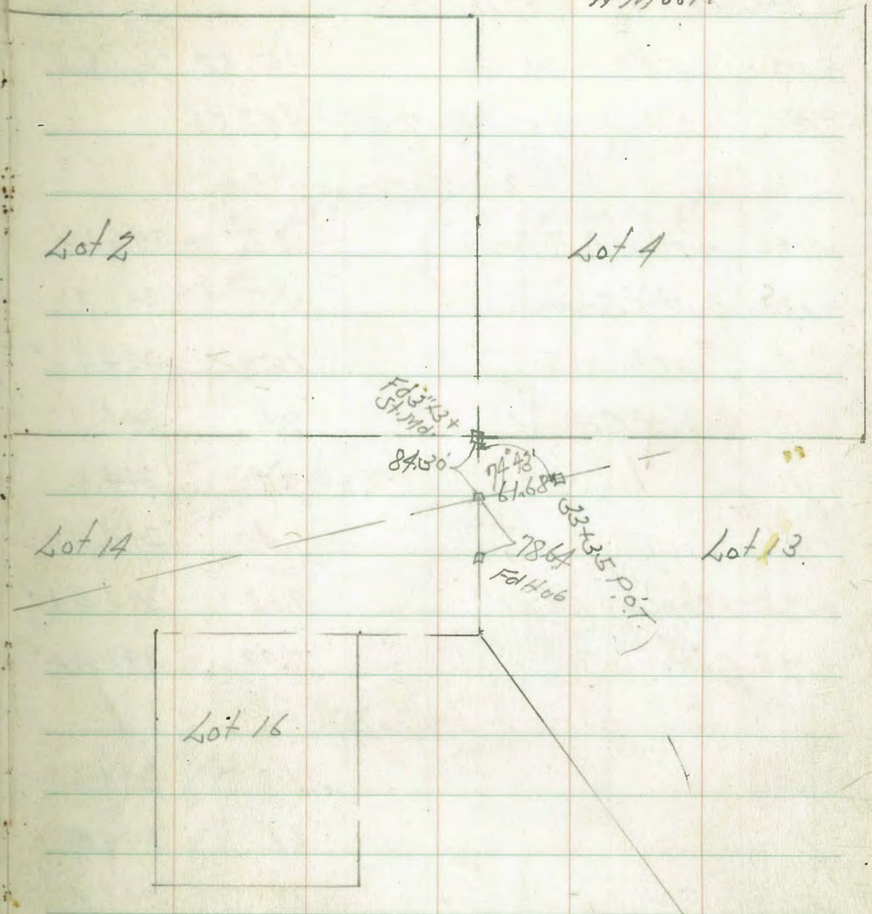
See Page 40 For Alignment



INDEXED
EFB

T.P. sheet not drawn 1/7/41

July 29-40
Northern
W Moore



Cross Section Alley Block 47 Fairmount Add.
From Trojan to El Cajon
Between 48th & Estrella

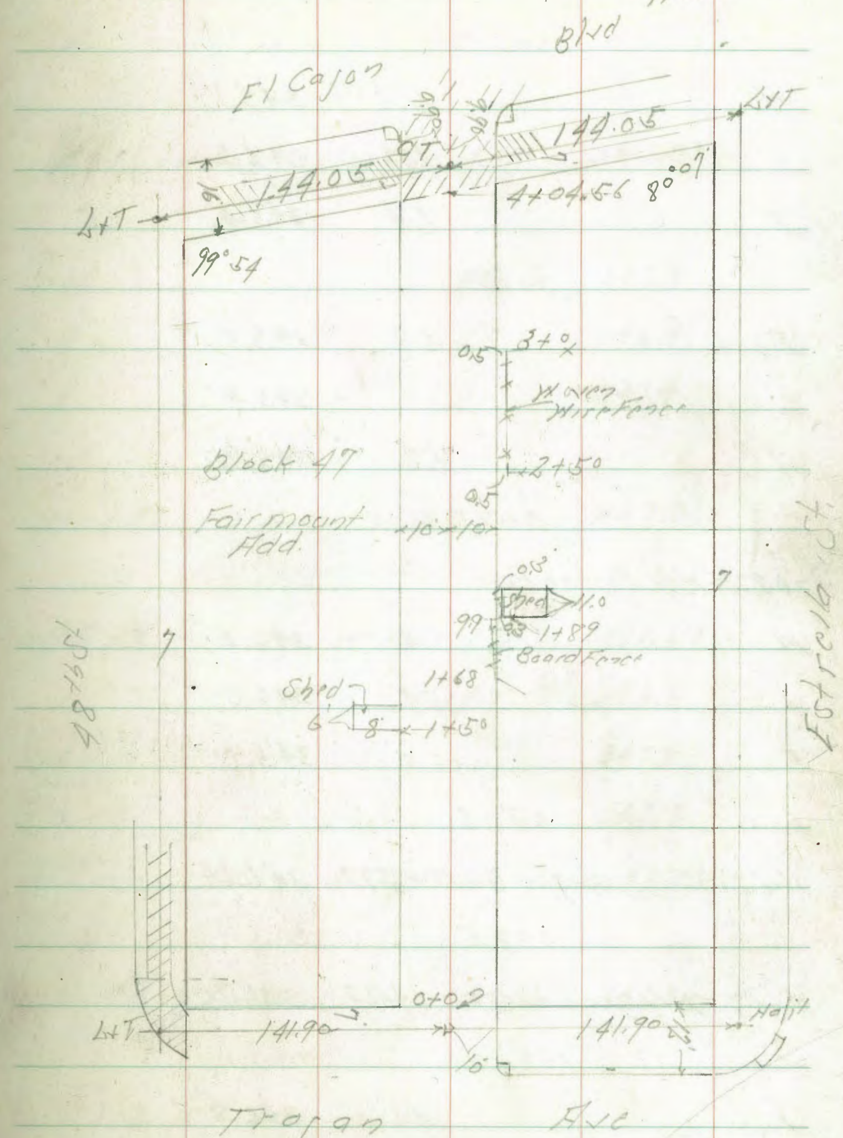
BM	4.84	356.36		351.52	N.W. B.P. El Cajon & Estrella
TP	2.60	351.43	7.53	348.83	
		0-12 N Cb Trojan			
-125	Top Cb W.L. Estrella		4.87	346.56	
-125	Gutter Ground		5.7	345.7	
E	Top Cb		6.50	344.93	
E	Gutter Ground		7.1	344.3	
℄		"	7.2	344.2	
W			7.4	344.0	
+125	Top Cb E L 48th		7.62	343.81	
+125	Gutter on Pav		7.99	343.44	
		0+0 = N.L. Trojan			
W			6.8	344.6	
℄			6.6	344.8	
E			6.6	344.8	
E	Top Cb		6.22	345.21	
		0+1.0			
E			6.1	345.3	
℄			6.4	345.0	
W			6.2	345.2	

Reduced by AJL
Plotted by WMC

INDEXED
EFB

Aug-24-40
Sisson
Hart...
Bliss
W. Moore

20' Wide



	351.43		
	0+25		
W		6.3	345.1
℄		6.2	345.2
E		6.4	345.0
	0+50		
E		5.9	345.5
℄		6.0	345.4
W		6.2	345.2
	0+75		
-0.2 = W ℄ Power Pole			
W		5.3	346.1
℄		5.4	346.0
E		5.5	345.9
	0+78		
W-6.2 = S ℄ Do Garage Conc Floor		4.79	346.64
	0+95		
W-6.2 = W ℄ Do Garage C.F.		4.73	346.70
	1+0		
E		4.6	346.8
℄		4.9	346.5

	351.43		
W		5.0	346.4
	1+17		
W-4.6 = ℄ Garage Conc Floor 8' Opening		4.42	347.01
	1+25		
W		4.6	346.8
℄		4.5	346.9
E		4.0	347.4
	1+41		
W-4.4 = ℄ 8' Garage Conc Floor		4.07	347.36
	1+56		
-10.5 = ℄ 8' Garage Conc Floor		2.86	348.57
E		2.9	348.5
℄		3.6	347.8
W = E ℄ Shed		4.1	347.3
TP	8.37 - 356.29	351	347.92
	1+67		
W-4.4 = ℄ Garage Conc Floor		8.83	347.96
	1+95		
W+0.2 = W ℄ Power Pole			

356.29

1+89

W	8.5	347.8
℄ on M.H. Rim	8.20	348.09
E = Fence	7.8	348.5

2+15

E	8.0	348.3
℄	7.8	348.5
W	8.0	348.3
+10	8.2	348.1

2+31

W-8' = ℄ 75 Garage Conc Floor	7.19	349.10

2+55

-8 = ℄ 75 Garage Conc Floor	7.06	349.23
W	7.1	349.2
℄	6.9	349.4
E	6.8	349.5

2+75

E	6.6	349.7
℄	6.8	349.5
W	6.5	349.8
+10	6.9	349.4

356.29

3+0

-10	6.6	349.7
W	6.5	349.8
+10 = W'ly Power Pole		
℄	6.2	350.1
E	6.2	350.1
+10	6.0	350.3

3+25

E	5.6	350.7
℄	5.4	350.9
W	5.5	350.8
+10	5.9	350.4

3+50

-10	4.8	351.5
W	4.6	351.7
℄	4.7	351.6
+5	4.7	351.6
E	4.4	351.9

3+85

E	2.7	353.6

	356.29		
E		3.5	352.8
W		3.1	353.2
	4+0		
W		3.7	352.6
+B		5.0	351.3
E		5.0	351.3
+B		3.4	352.9
F		2.7	353.6
	4+04.56 - SL El Cajon Blvd		
E Top Cb		5.77	350.52
E on Paving		6.00	350.29
E " "		6.19	350.10
W " "		6.04	350.25
W Top Cb		5.82	350.47
	4+20.8 - S Cb El Cajon		
W on Paving		6.52	349.77
E " "		6.54	349.75
F " "		6.52	349.77
BM		4.77	351.52

NW B.P. El Cajon & Estrella 351.52

Cross Section Alley Block 196 Univ. Hts
From University to Lincoln
Between Florida + Alabama

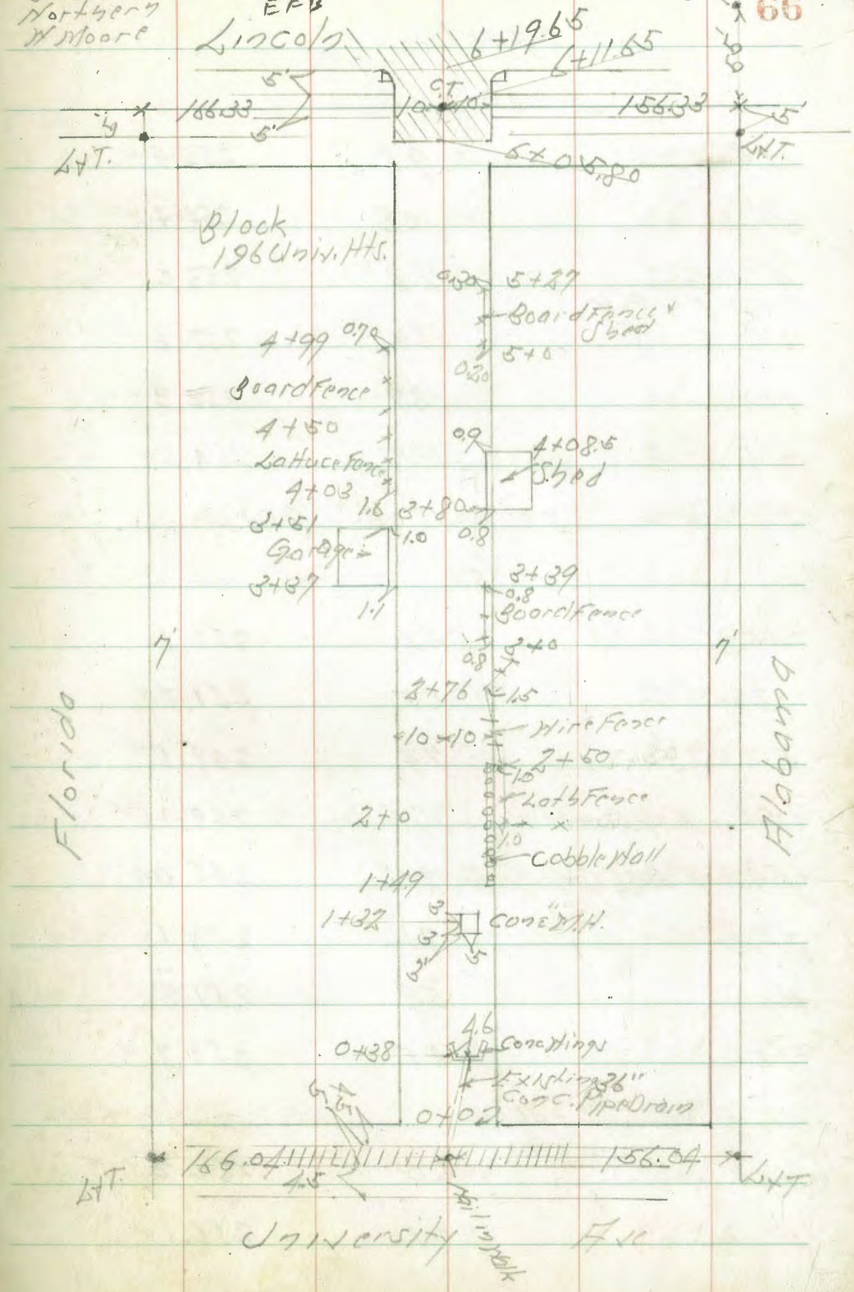
BM	10.20	276.16		265.96	N.W. B.P. University Alabama
		0-14 = N. Cb University			
E Cb Top			2.92	273.24 ✓	
E Gutter			3.63	272.53 ✓	
℄ "			2.91	273.25 ✓	
℄ Cb Top			2.17	273.99 ✓	
W " "			1.50	274.66 ✓	
W Gutter			2.27	273.89 ✓	
		0-4.5: Nly Conc Walk			
W on Walk			1.15	275.01 ✓	
℄ " "			1.83	274.33 ✓	
E " "			2.59	273.57 ✓	
		0+0 - N.L. University			
-10			5.6	270.6 ✓	
E			4.3	271.9 ✓	
℄			3.7	272.5 ✓	
W			2.7	273.5 ✓	
+10			1.2	275.0 ✓	
TP	1.17	265.15	12.18	263.98	

Notes Red. by EBH 4/18/40
Profile By A.J.L.

Sept. 13-40
Sisson
Northern
W Moore

INDEXED
EFB

66



		265.15		
		0+30		
-15			9.8	255.4 ✓
H			10.8	254.4 ✓
℄			12.2	253.0 ✓
+9.5 = Ely Pole				
E			12.6	252.6 ✓
+10			12.9	252.3 ✓
+15			11.1	254.1 ✓
TP	4.06	257.16	12.05	253.10
		0+38		
-15			5.1	252.1 ✓
-12			5.5	251.7 ✓
E			7.4	249.8 ✓
+54	Top Conc H W		7.75	249.41 ✓
+54	FL 36" Conc Drain		12.12	245.04 ✓
℄			7.1	250.1 ✓
H			5.9	251.3 ✓
+15			3.5	353.7 ✓
		0+46		
-15			5.0	252.2 ✓
H			7.1	250.1 ✓

		257.16		
℄			8.4	248.8 ✓
E			9.6	247.6 ✓
+6			5.6	251.6 ✓
+15			5.2	252.0 ✓
		0+60		
-15			5.7	251.5 ✓
-11			5.7	251.5 ✓
E			8.8	248.4 ✓
+6 = Bottom Ditch			9.1	248.1
℄			7.2	250.0 ✓
H			7.2	250.0 ✓
+15			7.4	249.8 ✓
		0+74		
-15			7.2	250.0 ✓
H			7.0	250.2 ✓
+0.6 = Hly Power Pole				
℄			8.1	249.1 ✓
+2 = Bottom Ditch			8.6	248.6
+6			8.6	248.6
E			7.6	249.6 ✓

25716

+4	8.3	248.9 ✓
+10	7.6	249.6 ✓
+15	7.1	2501 ✓
1+00		
-15 = Bot. Ditch	8.0	249.2 ✓
-5	5.8	251.4 ✓
E	6.4	250.8 ✓
℄	8.0	249.2 ✓
+4 = Bot Ditch	8.5	248.7
W	7.4	249.8 ✓
+15	6.3	250.9 ✓
1+33		
-15	4.9	252.3 ✓
-4 = Bot. Ditch	7.7	249.5 ✓
W	5.9	251.3 ✓
+4	4.2	253.0
℄	4.9	252.3 ✓
+3 = Wly Conc MH.	4.90	252.26 ✓
+8 = Ely " " "	4.90	252.26 ✓
E	5.1	252.1 ✓

25716

+5	5.4	251.8 ✓
+15	7.3	249.9 ✓
1+41		
E +0.5 = Ely Tel Pole		
1+49		
-15	7.3	249.9 ✓
-1 = Base Cobble Wall	6.3	250.9 ✓
E Top " "	4.90	252.26 ✓
℄	4.7	2525 ✓
+7	4.7	252.5
W	4.1	253.1 ✓
+3	4.0	253.2 ✓
+10 = Bot Ditch	7.0	250.2 ✓
+12	6.4	250.8 ✓
+15	5.6	251.6 ✓
2+00		
-15	4.1	253.1 ✓
W	4.5	252.7 ✓
+0.5 = Wly Pow Pole		
℄	4.3	253.0 ✓

257.16

E	Top Cobble Wall	4.1	253.1 ✓
+1	= Base " "	6.4	250.8 ✓
+15		6.8	250.4 ✓
	2+25		
-15		4.4	252.8 ✓
E	= Base Cobble Wall	5.2	252.0 ✓
+0.5	Top " "	2.9	254.3 ✓
+3		2.2	255.0
℄		2.5	254.7 ✓
W		2.7	254.5 ✓
+15		3.6	253.6 ✓
	2+50		
-15		2.4	254.8 ✓
W		1.0	256.2 ✓
℄		0.2	257.0 ✓
+7		0.2	257.0
+9.5	= Top Cobble Wall	1.1	256.1 ✓
E	= Base " "	2.3	254.9 ✓
+15		2.2	254.0 ✓
TP	11.62	268.76	0.02 257.14

268.76

	2+52		
-15		9.0	259.8 ✓
-10		10.3	258.5 ✓
E		12.0	256.8 ✓
℄		11.5	257.3 ✓
W		12.4	256.4 ✓
+15		14.0	254.8 ✓
	2+76		
-15		10.0	258.8 ✓
W		8.8	260.0 ✓
℄		8.1	260.7 ✓
+8.5	= Elv Tel. Pole		
+8		7.6	261.2
E		6.8	262.0 ✓
+15		3.9	264.9 ✓
	3+0		
-15		2.0	266.8 ✓
E		2.5	266.3 ✓
+4		4.5	264.3
℄		4.9	263.9 ✓

268.76

W	5.4	263.4 ✓
+1.2 = Sly Wire Fence		
+15	7.4	261.4 ✓
3+35		
-15	4.0	264.8 ✓
W	3.0	265.8 ✓
℄	2.5	266.3 ✓
+8	2.8	266.6
E	1.6	267.2 ✓
3+51		
-5	0.9	267.9 ✓
E	1.1	267.7 ✓
+3	2.0	266.8
℄	2.4	266.4 ✓
+9.7 = Wly Pow Pole		
W	3.8	266.0 ✓
+1.5 = Ely Garage Conc Floor Northe Entrance	3.20	265.56 ✓
3+69		
W -14.5 = ℄ Garage Dirt Floor	4.4	264.4 ✓

268.76

3+80

-10	4.4	264.4 ✓
W	4.2	264.6 ✓
℄	3.4	265.4 ✓
+7	3.1	265.7
E	1.9	266.9 ✓
+10	1.5	267.3 ✓
3+97		
E +1.2 = Ely Tel Pole		
4+0		
E	2.6	266.2 ✓
+3	4.1	264.7
℄	4.1	264.7 ✓
W	4.6	264.2 ✓
+5	5.4	263.4 ✓
+15	6.0	262.8 ✓
TP	11.50 276.21 4.05	264.71
4+50		
-15	14.5	261.7 ✓
-3	13.4	262.8 ✓

276.21

W	11.7	264.5 ✓
℄	11.2	265.0 ✓
E	10.8	265.4 ✓
+15	10.2	266.0 ✓
4+75		
-15	9.3	266.9 ✓
E	10.1	266.1 ✓
℄	10.3	265.9 ✓
W	10.6	265.6 ✓
+2	11.4	264.8 ✓
+5	12.2	264.0 ✓
+15	12.8	263.4 ✓
4+91		
E = ℄ 9.7 Garage Dirt Floor	9.7	266.5 ✓
4+97		
W = W Ly Power-Pole		
5+0		
-15	10.6	265.6 ✓
W	8.7	267.5 ✓
℄	8.5	267.7 ✓

276.21

E	9.0	267.2 ✓
+15	9.0	267.2 ✓
5+05		
W-76 = ℄ 8' Garage Dirt Floor	8.6	267.6 ✓
5+25		
E	5.8	270.4 ✓
℄	6.3	269.9 ✓
W	6.6	269.6 ✓
+15	7.5	268.7 ✓
5+43		
E-4.0 = ℄ 8' Garage Dirt Floor	3.8	272.4 ✓
5+50		
-15	5.6	270.6 ✓
W	4.5	271.7 ✓
℄	4.2	272.0 ✓
+9.4 = Ely Tel Pole		
E	3.4	272.8 ✓
+1	2.8	273.4 ✓
+10	2.6	273.6 ✓

27621

5+57

E-1.6=℄ Garage Conc Floor	2.15	274 06

5+59

W-4.0=℄ Garage Dirt Floor	3.9	272 3

5+65

E-1.7=℄ 8.5 Conc. Walk	1.41	274 80

5+75

-1.7 = W/y House Conc. Foundation	1.1	275 1
E	1.1	275 1
+1	3.0	273 2
℄	3.2	273 0
W	3.3	272 9
+4 = W/y Garage Dirt Floor	3.4	272 8

5+90

-10	3.6	272 6
W	3.1	273 1
℄	3.1	273 1
+9	2.7	273 5
E	0.8	275 4
+1.5 = W/y House	0.6	275 6

27621

6+05.8 = S/y Paving on Lincoln

E Top C6	2.38	273 83
E Gutter on Paving	2.60	273 61
℄ " "	3.41	272 80
W " "	3.82	272 39
W Top C6	3.68	272 53

6+19.65 = SC6 Lincoln

W on Paving			4.50	271 71	
℄ " "			3.74	272 47	
E " "			3.14	273 07	
TP	10.89	285.63	1.47	274.74	N.W. B.P. Lincoln Alabama 285.04
BM	1.13	285.80	0.96	284.67	
TP	1.29	277.22	9.87	275.93	
BM			11.24	265.98	N.W. B.P. Lincoln Alabama 285.96

Cross Section Vine St.
Kettner to India

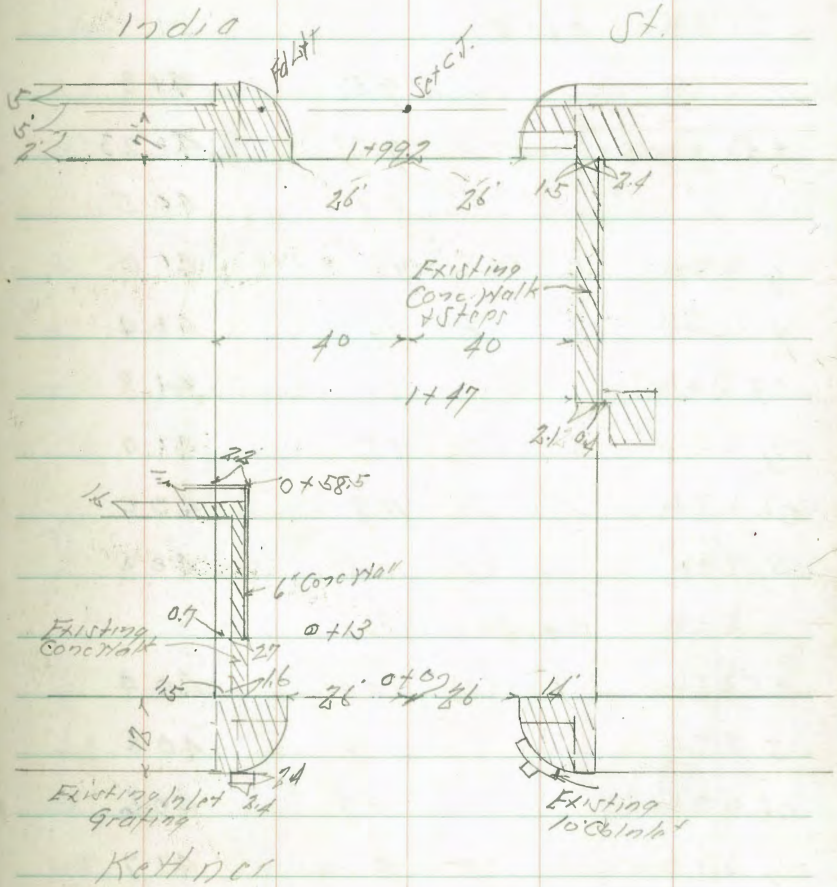
80' wide
14' Cbs
13' Gts

INDEXED
EFB

Oct. 25. 40
Sisson
Northern
M. Moort

BM	11.23	50.81	39.58	SEBP Vine & Kettner
	0+12 : E Cb Kettner			
N Top Cb		11.60	39.81	
N Gutter		11.95	38.86	
+4 = Grating N/s		11.98	38.83	
+6.5 " S/s		11.69	39.12	
Cb		11.62	39.19	
1/4		11.37	39.44	
℄		11.34	39.47	
1/4		11.47	39.34	
Cb		11.67	39.14	
S = Gutter		11.84	38.97	
S = Cb Top		11.26	39.55	
	0+0 = E L Kettner			
S		11.1	39.7	
Cb Top		11.01	39.80	
Gutter on Paving		11.53	39.28	
1/4 "		10.98	39.83	
℄ " "		10.82	39.99	
1/4 " "		10.95	39.86	

Red. by C.B.H.
Plot —
Yard. Ext. 10/28-40



50.81

Gutter on Paving	11.41	39.40
Cb Top	10.59	40.22
N	10.7	40.1
0+05		
N	9.5	41.3
+3 = ℄ Walk	9.58	41.23
Cb	9.3	41.5
¼	9.8	41.0
℄	9.4	41.4
+9	9.0	41.8
¼	9.8	41.0
Cb	10.8	40.0
S	10.5	40.3
0+12		
-5	10.4	40.4
S	10.4	40.4
Cb	10.2	40.6
¼	9.1	41.7
+3	7.7	43.1
℄	8.2	42.6

50.81

¼	8.1	42.7
Cb	8.1	42.7
+11.3	8.9	41.9
+11.3 = Top Conc Wall	7.08	43.73
+1½ of Conc Walk	8.88	41.93
N	9.0	41.8
0+38		
N	8.8	42.0
+3' = Conc Walk	8.71	42.10
+4 = Top Conc Wall	6.10	44.7
Cb	5.3	45.5
¼	5.2	45.6
℄	5.9	44.9
+5	5.5	45.3
¼	3.2	47.6
+8	3.1	47.7
Cb	7.8	43.0
+5	9.2	41.6
S	9.9	40.9
+5	10.0	40.8

50.81

0+58.5

-10		9.3	41.5
5		8.8	42.0
+9		8.4	42.4
Cb		3.4	47.4
+2		0.7	50.1
+6		+0.7	51.5
¼		+1.1	51.9
¢		+1.1	51.9
¼		+0.8	51.6
+6		1.0	49.8
Cb		1.5	49.3
+10		2.2	48.6
+18 = Top Conc Wall		5.3	45.5
+13 = Conc Wall		8.13	42.68
H		8.1	42.7
TP	11.35 61.99	0.17	50.64

0+88

-4 = City Yard		18.1	43.9
H		16.1	45.9

61.99

+3		7.8	54.2
Cb		5.2	56.8
¼		4.4	57.6
¢		4.0	58.0
¼		3.4	58.6
+10		4.9	57.1
Cb		10.0	52.0
+2		15.0	47.0
5		17.1	44.9
+10		17.8	44.2

1+0

-1' = Mid Top Conc Wall		0.0	62.0
5		7.3	54.7
+6		7.5	54.5
Cb		6.8	55.2
+4		1.8	60.2
¼		1.1	60.9
¢		1.8	60.2
¼		1.9	60.1
Cb		2.9	59.1

	61.99			
+9			6.0	56.0
H			13.7	48.3
+4			15.2	46.8
	1+08			
-4			15.1	46.9
H			13.5	48.5
+4			4.8	57.2
Cb			1.8	60.2
1/4			0.2	61.8
℄			0.3	61.7
1/4			0.1	61.9
+10			1.0	61.0
Cb			0.0	62.0
S			+1.2	63.2
TP	11.43	73.12	0.30	61.69
	1+30			
-5			5.0	68.1
S			5.9	67.2
Cb			6.2	66.9
1/4			6.3	66.8

		73.12		
℄			7.0	66.1
+6			5.7	67.4
1/4			6.7	66.4
Cb			8.4	64.7
+2			7.5	65.6
+10			11.3	61.8
H			24.8	48.3
+3 = Sly Pipe Shed			26.8	46.3
	1+47			
-3			24.5	48.6
H			23.1	50.0
+8			14.4	58.7
Cb			4.7	68.4
+4			4.8	68.3
1/4			3.2	69.9
+8			3.8	69.3
℄			2.4	70.7
1/4			2.5	70.6
Cb			2.3	70.8
+10.2 = N 1/2 25 Conc Walk			2.32	70.80
S			2.3	70.8

Vine St.

		73.12		
IP	11.38	84.21	0.29	72.83
		1+65		
S			9.74	74.47
+2 = Edge Conc Walk			9.74	74.47
Cb			9.5	74.7
+7			9.7	74.5
1/4			8.2	76.0
+3			7.7	76.5
+8			9.7	74.5
Δ			9.8	74.4
+9			10.2	74.0
1/4			12.0	72.2
+7			10.6	73.6
Cb			11.4	72.8
+6			11.3	72.9
+12			14.4	69.8
N			33.9	50.3
+10			35.9	48.3
		1+77		
-10			22.5	61.7

		84.21		
N			22.5	61.7
+2			11.5	72.7
+8			8.8	75.4
Cb			8.5	75.7
+5			8.5	75.7
1/4			7.0	77.2
Δ			5.7	78.5
1/4			5.3	78.9
Cb			6.7	77.5
+18 = N/S Conc Walk			6.73	77.48
S			6.7	77.5
		1+93		
S			3.6	80.6
+2 = N/S Conc Walk			3.63	80.58
Cb			4.1	80.1
+6			3.6	80.8
1/4			4.9	79.3
Δ			4.8	79.4
1/4			4.0	80.2
+6			3.5	80.7

84.21

Cb	5.4	78.8
+5	4.8	79.4
H	7.3	76.9
+10	8.2	76.0
1+99.2 = W L India		
-10	5.1	79.1
H	3.9	80.3
Cb Top	4.23	79.98
Gutter on Paving	4.71	79.50
1/4 " "	4.09	80.12
1/2 " "	3.65	80.56
1/4 " "	3.56	80.65
Gutter " "	3.67	80.54
Cb Top	3.19	81.02
+12.5 = Hy Conc Walk	2.94	81.27
S	2.9	81.3
W C b India		
S Cb Top	3.06	81.15
Gutter on Paving	3.41	80.80
Cb " "	3.40	80.81

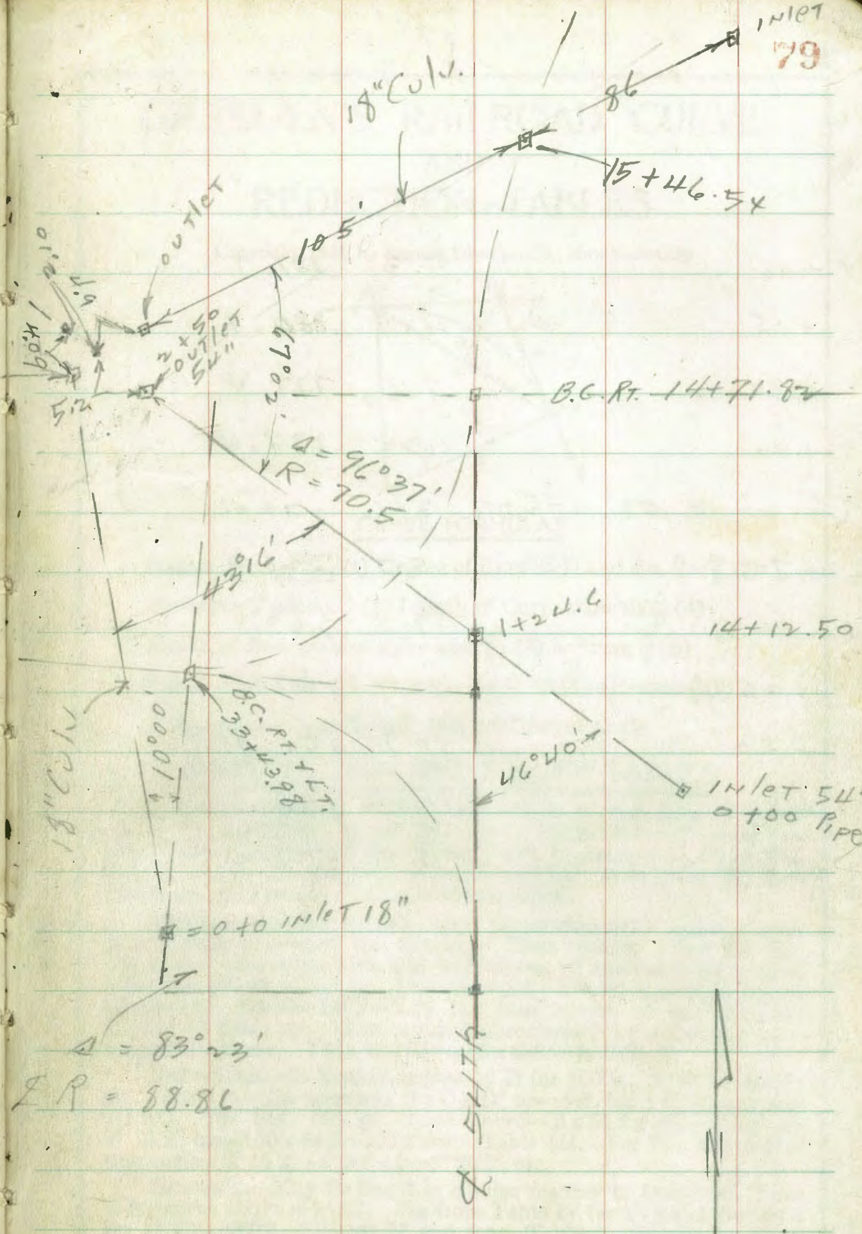
84.21

1/2 on Paving	3.24	80.97
1/4 " "	3.58	80.63
Cb " "	3.17	80.04
H Gut " "	3.37	79.84
H Cb Top	3.03	80.18

Levels for 54" Culv. — Moore 5-10-41

Change of Location — ℄ Int.

	7.80	272.29		264.49	B.M. Hub
0+0 inlet 54" pipe			4.3	268.0	
0+50			6.0	266.3	
0+60			6.0	266.3	1+66 outlet 18" Culv.
0+65			4.5	267.8	
0+92			7.2	264.9	
1			7.5	264.8	
1+22.6 ℄ 54th			8.2	263.9	℄ 49th
1+50			9.1	263.2	
1+60			8.2	264.1	
1+75			9.8	262.5	
2			10.1	262.2	
2+11			10.2	262.1	
2+15			8.8	263.5	
2+27			9.9	262.4	
2+31			12.8	259.5	
2+50 end 54" pipe			13.6	258.7	
T.P.	13.01	285.02	0.28	272.01	

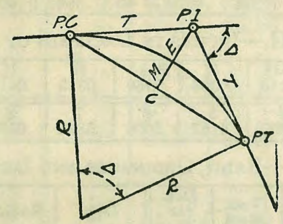


Levels for 18" Culv.
65.5 RT. of ℄ 49th Sta. 33+×398
B.C. RT & LT.

285.02

0+00			3.3	281.7
+15			4.9	280.1
+30			7.6	277.4
+40			10.6	274.4
T.P.	0.58	272.59	13.01	272.01
+70			5.7	266.9
1			9.8	263.8
+25			10.1	262.5
+50			10.9	261.7
+53			12.3	260.0
1+66 outlet			14.1	258.2

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius $=R=\frac{50}{\sin. D/2}$ (1) Degree of Curve $=D$ and $\sin. \frac{D}{2}=\frac{50}{R}$ (2)

Tangent $=T=R\tan\frac{\Delta}{2}$ (3) Length of Curve $=L=100\frac{\Delta}{D}$ (4)

Middle ordinate $=M= R(1-\cos. \frac{\Delta}{2})$ (5) $=R\text{vers}\ \frac{\Delta}{2}$ (6)

External $=E=T\tan\frac{\Delta}{4}$ (7) $=R\div\cos.\frac{\Delta}{2}-R$ (8) $=R\text{exsec}\frac{\Delta}{2}$ (9)

Long Chord $=C=2\ R\ \sin.\frac{\Delta}{2}$ (10) $\Delta=$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta=62°\ 10'$ $D=8°\ 20'$. From Table IV for 1° curve T=3454.1 and ÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157+45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 $(54.50\div100)^2$=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2\div(2\times688.26)$=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=91.27 and from Table V correction=.10 or E=91.37 ft. Or suppose $\Delta=32°$ and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and ÷42=5.5 or D=5° 30′.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

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